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# GE Nuclear Energy

25A5785 SH NO. 1 REV. 0

EIS IDENT: SBWR PANDA

#### **REVISION STATUS SHEET**

| DOCUMENT TITLE | PANDA | TEST PLAN | - TESTS M2, | M10A, M10B |
|----------------|-------|-----------|-------------|------------|
|----------------|-------|-----------|-------------|------------|

LEGEND OR DESCRIPTION OF GROUPS

TYPE: SPECIFICATION

FMF: SBWR

MPL NO: T10-5010

- DENOTE CHANGE

THIS ITEM IS OR CONTAINS A SAFETY-RELATED ITEM YES NO DE EQUIP CLASS CODE C

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#### 1. SCOPE

This test plan defines the detailed requirements, beyond those already identified in GE Spec 25A5587, for the PANDA transient integral system tests M2, M10A & M10B. This Test Plan specifically covers the test program objectives, the experimental facility configuration, the test facility control, the test instrumentation, the data acquisition, processing and analysis, the test initial and boundary conditions and the test reports for tests M2, M10A & M10B.

This test plan is applicable to the SBWR Design Certification project only.

### 2. APPLICABLE DOCUMENTS

a. PANDA Test Specification, GE Spec 25A5587.

This document provides the general specification of requirements for tests in the PANDA facility to support SBWR Design Certification.

b. PANDA Steady State Tests--

PCC Performance Test Plan & Procedure, PSI Doc. TM-42-94-11/ALPHA 410.

This document provides a general description of the PANDA test facility and the specific plan and procedure for steady state tests of the PCC condenser performance.

c. PANDA PROJECT CONTROL PLAN, GE Doc. PPCP-QA-01.

This document describes the organization, quality related activities, events and procedures necessary to ensure and verify that the PANDA project at PSI is conducted under the provisions of the GE SBWR Quality Assurance Plan as described in NEDG-31831.

d. PANDA Test Plan, GE Spec 25A5764

This test plan defines the detailed requirements, beyond those already identified in GE Spec 25A5587, for the PANDA transient integral system tests M3, M3A, M3B, M4 and M7. This Test Plan specifically covers the test program objectives, the experimental facility configuration, the test facility control, the test instrumentation, the data acquisition, processing and analysis, the test initial and boundary conditions and the test reports for tests M3, M3A, M3B, M4, M7.



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### 3. TEST OBJECTIVES

The objectives of the PANDA integral systems tests are to provide additional data to: (a) provide a sufficient database to confirm the capability of TRACG to predict SBWR containment system performance, including potential systems interaction effects. (Integral Systems Tests) and (b) Demonstrate startup and long-term operation of a passive containment cooling system. (Concept Demonstration).

The specific objectives and approach for the tests covered by this test plan are:

- a) Perform Test M2 with nominal post-LOCA initial conditions with all steam flow directed through the steam line from the RPV to Drywell 2 to create asymmetric distributions of steam and non-condensable gas concentrations and demonstrate the PCCS/containment performance under these conditions. Contingency testing is to be performed at the end of the 20 hour performance of M2 to demonstrate PCC restart in response to increased heat load demand.
- b) Perform Test M10A with nominal post-LOCA initial conditions' with only the two PCC condensers connected to Drywell 2 operational and all steam flow directed through the steam line from the RPV to Drywell 2 to create asymmetric distributions of steam and non-condensable gas concentrations and demonstrate the PCCS/containment performance under these conditions, i.e. long term migration of non-condensible gas (air) from Drywell 1 to Drywell 2.

c) Perform Test M10B with nominal post-LOCA initial conditions' with only the two PCC condensers connected to Drywell 2 operational and all steam flow directed through the steam line from the RPV to Drywell 1 to create asymmetric distributions of steam and non-condensable gas concentrations and demonstrate the PCCS/containment performance under these conditions, i.e. maximum non-condensible gas volume purge rate through each PCC (total volume of DW1 and DW2 through two PCCs).

"Nominal post-LOCA initial conditions" are those used for test M3 which are derived from the SBWR main steam line break LOCA analysis at one hour after LOCA initiation.



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### 4. TEST FACILITY CONFIGURATION

The PANDA test facility is described in detail in Section 3 of PSI report ALPHA 410. For Tests M2, M10A & M10B the PANDA facility will be configured to simulate the SBWR post-LOCA configuration as follows:

1) Table 4.1 identifies the key PANDA facility geometry and effective flow area  $(A/\sqrt{k})$ characteristics. In Table 4.1, the required tolerance for the PANDA as-built value relative to the corresponding SBWR scaled value is tabulated for each of these key characteristics. In addition, the required accuracy for the as-built value for each of the key characteristics is tabulated in Table 4.1. The actual as-built accuracy should be approximately equal to or less than the required accuracy tabulated in Table 4.1. The actual as-built accuracies depend on the source of the as-built value. These sources can be measurements by PSI or Electorwatt (i.e. line losses, line lengths, elevations), manufacturer's specifications or design standards (i.e., PCC/IC tubes), or calculations from as-built dimensions (i.e., vessel volumes, losses for lines without flow tests).

2) The RPV will supply steam to the drywells as follows:

a) For test M2 & M10A the RPV will supply steam only to Drywell 2 through its single connecting steam line.

b) For test M10B the RPV will supply steam only to Drywell 1 through its single connecting steam line.

- 3) RPV heater power will be controlled as a function of time to simulate the scaled decay heat and stored energy release.
- 4) The IC unit will be isolated (i.e., the IC feed, drain and vent will be closed).

5) The PCC units will be lined up as follows:

a) For test M2 all three PCC units will be lined-up to take feedflow from the drywells, to vent noncondensables and steam into the water volume of the suppression pool, and drain condensate to the GDCS volume.

b) For tests M10A & M10B only the two PCC units connected to Drywell 2 will be linedup to take feedflow from the drywell, to vent noncondensables and steam into the water volume of the suppression pool, and drain condensate to the GDCS volume.



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- 6) The PCC pools will be configured as follows:
  - a) the PCC pools will be filled and isolated from each other.
  - b) During the test, no water will be added or drained from the PCC pools.
- 7) The only direct lines of communication between the drywell and wetwell will be through the vacuum breakers (when the wetwell pressure exceeds drywell pressure sufficiently to open the vacuum breaker) and the main vent lines (which will be submerged within the wetwells).
- 8) The GDCS pressure equalization lines to both drywells will be open.
- 9) The GDCS drain line with check valve will be lined up to return PCC condensate to the RPV.
- 10) The Equalizing lines between the RPV and wetwells will be valved out of service.



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Table 4.1: PANDA Transient Integral System Tests

### Key Facility Characteristics

|                         | FOR PANDA              |           |
|-------------------------|------------------------|-----------|
|                         | TO SEWR SCALED VALUE   |           |
|                         | ASBUILT VALUE RELATIVE |           |
| PANDA AS-BUILT ACCURACY | TOLERANCE FOR PANDA    | FARAMETER |

| (sաւութ)         |        |          |
|------------------|--------|----------|
| headers          |        |          |
| permeen          |        |          |
| Distance         | % ⊊ ∓  | umč±     |
| səreiq bra       |        |          |
| -Steel thickness | % ⊊ ∓  | mm č.0 ± |
| uonoas           |        |          |
| cylindrical      |        |          |
| -Steel thickness | % ⊊∓   | mm 8.0±  |
| hgnəd-           | % ⊊ ∓  | um č ±   |
| diameter         |        |          |
| -Outside         | % ⊊ ∓  | um č ±   |
| Headers          |        |          |
| Exchanger        |        |          |
| PCC/IC Heat      |        |          |
| Thickness        | % ⊆I ∓ | mm 2.0 ± |
| Diameter         |        |          |
| -Outside         | % ⊊∓   | mm 8.0 ± |
| -Length          | % ⊊∓   | um č±    |
| SuiqnT           |        |          |
| Exchanger        |        |          |
| PCC/IC Heat      |        |          |
|                  |        |          |



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### Table 4.1: PANDA Transient Integral System Tests

Key Facility Characteristics(continued)

| PARAMETER      | TOLERANCE FOR PANDA AS-<br>BUILT VALUE RELATIVE TO<br>SBWR SCALED VALUE FOR<br>PANDA | PANDA AS-BUILT ACCURACY |
|----------------|--|-------------------------|
| Vessel Volumes |  |                         |
| -RPV           | ± 10 %   | ±2%                     |
| -Drywell 1     | ±10 %  | ±2%                     |
| -Drywell 2     | ± 10 %   | ±2%                     |
| -Wetwell 1     | ±10 %  | ± 2 %                   |
| -Wetwell 2     | ± 10 %   | ± 2 %                   |
| -ĢDCS          | - (1)  | ±2 %                    |
| -IC/PCC pools  | (2)  | ±2%                     |

- (1) GDCS pool volume is not scaled to SBWR
- (2) IC/PCC pool volumes are not scaled to SBWR



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# Table 4.1: PANDA Transient Integral System Tests

Key Facility Characteristics (continued)

| PARAMETER   | TOLERANCE FOR PANDA<br>AS-BUILT VALUE RELATIVE<br>TO SBWR SCALED VALUE<br>FOR PANDA | PANDA AS-BUILT<br>ACCURACY |
|---|---|----------------------------|
| <u>Elevation Differences</u><br>P1V-P2V-P3V<br>discharges                   | ± 2 cm  | ± 1 cm                     |
| P1C inlet to outlet   | ± 10 cm   | $\pm 1 \text{ cm}$         |
| P2C inlet to outlet   | ± 10 cm   | ± 1 cm                     |
| P3C inlet to outlet   | ± 10 cm   | ± 1 cm                     |
| P1V, P2V, P3V<br>discharges relative to<br>normal suppression<br>pool level | ± 5 cm  | ±1 cm                      |
| MVI and MV2<br>discharges relative to<br>normal suppression<br>pool level   | ± 5 cm  | ± 1 cm                     |
| P1V, P2V, P3V<br>discharges relative to<br>MV1 and MV2<br>discharges        | ± 5 cm  | ± 1 cm                     |
| P1F, P2F, P3F inlet<br>relative to MS1 and<br>MS2 discharge                 | + 200 cm∕ − 0   | ± 1 cm                     |



#### PANDA Transient Integral System Tests Table 4.1:

Key Facility Characteristics (continued)

PARAMETER

Elevations

TOLERANCE FOR PANDA AS- PANDA AS-BUILT BUILT VALUE RELATIVE TO ACCURACY SBWR SCALED VALUE FOR PANDA

| (relative to<br>TAF/Heaters) |               |         |
|------------------------------|---------------|---------|
| P1F, P2F, P3F<br>inlet       | + 200 cm/ - 0 | ±5 mm   |
| P1C,P2C,P3C<br>inlet         | ± 5 cm        | ± 5 mm  |
| P1V,P2V,P3V<br>discharge     | ± 5 cm        | ± 5 mm  |
| GRT inlet                    | ± 5 cm        | ± 5 mm  |
| GRT outlet                   | ± 5 cm        | ±5 mm   |
| MV1 outlet                   | ± 5 cm        | ± 5 mm  |
| MV2 outlet                   | ± 5 cm        | ± 5 mm  |
| MSL l outlet                 | ± 5 cm        | ± 5 mm  |
| MSL 2 outlet                 | ± 5 cm        | ± 5 mm  |
| Top of RPV<br>chimney        | ± 25 cm       | ± 50 mm |



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#### Table 4.1: PANDA Transient Integral System Tests

Key Facility Characteristics (continued)

TOLERANCE FOR PANDA AS-BUILT PANDA AS-BUILT PARAMETER VALUE RELATIVE TO SBWR ACCURACY SCALED VALUE FOR PANDA Connecting Line Flow Resistances RPV to DW1  $\pm 20\%$ ±10% RPV to DW 2  $\pm 20\%$  $\pm 10\%$ DW 1 to PCC1 ±20%  $\pm 10\%$ DW 2 to PCC2 + 20%  $\pm 10\%$ DW 2 to PCC3 ±20%  $\pm 10\%$ DW 1 to WW 1 (3) ±10% (LOCA vent) DW 2 to WW 2 (3)± 10% (LOCA vent) PCC1 to GDCS ±20%  $\pm 10\%$ PCC2 to GDCS ± 20%  $\pm 10\%$ PCC3 to GDCS ±20%  $\pm 10\%$ PCC1 to WW 1 ±20%  $\pm 10\%$ PCC2 to WW 2 ±20%  $\pm 10\%$ PCC3 to WW 2  $\pm 20\%$ ± 10% GDCS to RPV ±20% ±10% WW 1 to DW 1 ±20%  $\pm 10\%$ (bypass/vac. brkr)

(3) LOCA vents are not scaled to SBWR



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### 5. CONTROL SYSTEM DESCRIPTION

In order to perform the transient integral system tests, several control systems are to be used to establish initial and boundary conditions for each test. These control systems will be used to manage and regulate the key test parameters prior to the test. Following test initiation, only the RPV heater power and the vacuum breaker controllers will be used. A main control system, which includes the electronic controllers, will be used to perform the operations.

### 5.1 RPV Heater Power Control

The electrical power to the heaters in the RPV will be controlled automatically following test initiation, to match the decay power and RPV structural heat release specified in Section 9.

### 5.2 Drywell/Wetwell Vacuum Breaker Control

The operation of the vacuum breaker valve will be controlled based on the measured pressure difference between the drywell and wetwell. Drywell pressure is initially established at a value equal to or greater than the wetwell pressure to conform to the post-LOCA condition specified for the beginning of each individual test. During the course of a test if the drywell to wetwell pressure drops below a minimum value the vacuum breaker valve control will automatically open the valve. The wetwell-to-drywell differential pressure at which the vacuum breaker for Drywell 1 opens will be set at 0.47 psi (3.24 kPa), and the differential pressure at which the vacuum breaker for Drywell 1 opens will be set at 0.3 psi (2.06 kPa). The opening and closing differential pressure for the vacuum breaker in Drywell 2 will be set 0.1 psi higher than the corresponding setpoints for the Drywell 1 vacuum breaker, i.e. at 0.57 psi (3.9 kPa) and 0.4 psi (2.8 kPa), respectively.

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#### 6. REQUIRED MEASUREMENTS

'able 6.1 gives the measurements required to meet the objectives for Tests M2, M10A & M10B. With the exception of the temperature indication, no PANDA instrumentation other than that in Table 6.1 is necessary for the performance of Tests M2, M10A & M10B. The sensors identified in Table 6.1 must be operable prior to initiation of these tests. It is acceptable if a sensor is not operable, if the backup identified in the second column is operable.

Temperature measurements in the PCCs and the various connected vessels are desirable, but not all of these temperature measurements are required for the performance of these tests as discussed below. The temperature measurements required for these tests with an accuracy of 1.5°C are as follows:

RPV steam dome (at least one).

PCC tubes; (It is required that 50% of the tube wall and fluid sensors be available. The available sensors must include at least 40% of the probes above and at least 40% of the probes below the horizontal mid-plane of the tube bundle. Within these constraints, the test engineer has responsibility and authority to judge whether or not sufficient PCC temperature sensors are operable to initiate a test).

PCC pools: 30% of the liquid probes including one of the lowest three elevations.

DW: 50% of the fluid probes including either the lowest elevation or one thermocouple from the water-surface probe.

WW: 50% of the gas probes, 50% of the liquid probes and two out of three of the floating probes.

GDCS pool: 50% of the fluid probes and one thermocouple from the floating probe.

Vessel walls: 20% of GDCS, DW, and WW.

System lines: 50% of the gas and liquid temperature probes in each system line used for the test (if number of sensors is odd, round to lower whole number, i.e. 3 sensors total in one line means one is required).

In Table 6.1 a subset of the required instruments are identified as "top priority measurements". Time history plots of these top priority measurements are to be included in the Test File (see Section 7.3) and the Apparent Test Results (ATR) Report (see Section 10). In addition to the top priority measurements identified in Table 6.1, there are other top priority measurements. These are: 1) the total electrical power to the heaters in the RPV which is determined during post-test



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data processing, and 2) some temperature measurements. The top priority temperature measurements are: RPV steam dome temperature measurement, highest and lowest temperature measurement location in each drywell, highest and lowest temperature measurement location in the gas space of each wetwell, highest liquid temperature measurement location in each wetwell, and one temperature measurement in the GDCS drain line and in each of the three PCC vent lines.

As noted in Section 7.4, the operator will perform checks as possible to confirm instrumentation performance. These checks will include comparison of redundant measurements.

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| Provessio. ** | Backup   | Accuracy        | Location                                     |
|---------------|----------|-----------------|--|
| CB. //B1 •    |          | N/A<br>(On/Off) | Valve position :Vacuum Breaker Line 1        |
| CI2.VB2◆      |          | N/A<br>(On/Off) | Valve position :Vacuum Breaker Line 2        |
| MD.MV1        | MI.MV1   | 0.5 kPa         | pressure diff. meas. Main Vent line DW1->SC1 |
| MD.MV2        | MI.MV2   | 0.5 kPa         | pressure diff. meas. Main Vent line DW2->SC2 |
| MD.P1F#       | MV.P1F   | 0.5 kPa         | pressure diff. meas. PCC1 Feed DW1->PCC1     |
| MD.P1V.2#     | MI.P1V.1 | 0.5 kPa         | pressure diff. meas. PCC1 Vent PCC1->SC1     |
| MD.P2F        | MV.P2F   | 0.5 kPa         | pressure diff. meas. PCC2 Feed DW2->PCC2     |
| MD.P2V.2      | MI.P2V.1 | 0.5 kPa         | pressure diff. meas. PCC2 Vent PCC2->SC2     |
| MD.P3F        | MV.P3F   | 0.5 kPa         | pressure diff. meas. PCC3 Feed DW2->PCC3     |
| MD.P3V.2      | MI.P3V.1 | 0.5 kPa         | pressure diff. meas. PCC3 Vent PCC3->SC2     |
| MD.VB1        | MD.VB2   | 0.5 kPa         | pressure diff. meas. Vacuum Breaker SC1-DW1  |
| MD.VB2        | MD.VB1   | 0.5 kPa         | pressure diff. meas. Vacuum Breaker SC2-DW2  |
| MI.MV1        | MD.MV1   | N/A(on/off)     | phase indicator Main Vent line DW1->SC1      |
| 4I.MV2        | MD.MV2   | N/A(on/off)     | phase indicator Main Vent line DW2->SC2      |
| 4I.P1V.1#     | MD.P1V.2 | N/A(on/off)     | phase indicator PCC1 Vent PCC1->SC1          |
| 41.P2V.1      | MD.P2V.2 | N/A(on/off)     |  |



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| Processid ** | Backup                  | Accuracy       | Location   |
|--------------|-------------------------|----------------|--|
| MI.P3V.1     | MD.P3V.2                | N/A(on/off)    | phase indicator PCC3 Vent PCC3->SC2                            |
| MP.D1+       |                         | 2.5 kPa        | absol. pressure meas. Drywell 1 / DW1                          |
| MP.RP.1 •    |                         | 2.5 kPa        | absol. pressure meas. Reactor Pressure Vessel / RPV            |
| MP.S1 •      |                         | 2.5 kPa        | absol. pressure meas. Suppression Chamber 1 / SC1              |
| ML.U1+#      |                         | 0.0-*          | PCC 1 continued  |
| MIL.01 •#    | and the second          | 0.2 m <b>t</b> | PCC 1 pool level   |
| ML.U2+       |                         | 0.2 m <b>t</b> | PCC 2 pool level   |
| ML.U3+       |                         | 0.2 m <b>t</b> | PCC 3 pool level   |
| ML.RP.1      |                         | 0.2 m          | RPV level  |
| ML.S1        | ML.S2                   | 0.05 m         | Suppression pool level   |
| ML.D1        | ML.D2                   | 0.05 m         | Drywell water level  |
| MPG.D1_1 •   | MPG.D1_2 or<br>MPG.D1_3 | 5.00%          | air partial pres. mea Drywell 1 / DW1 (highest probe in DW1)   |
| MPG.D2_1 •   | MPG.D2_2 or<br>MPG.D2_3 | 5.00%          | air partial pres. meas. Drywell 2 / DW2 (highest probe in DW2) |
| MPG.D1_2     | MPG.D1_1 or<br>MPG.D1_3 | 5.00%          | air partial pres. meas. Drywell 1 / DW1                        |
| MPG.D2_2     | MPG.D2_1 or<br>MPG.D2_3 | 5.00%          | air partial pres. meas. Drywell 2 / DW2                        |



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| Processid **       | Backup                  | Accuracy | Location  |
|--------------------|-------------------------|----------|---|
| MPG.D1_3           | MPG.D1_1 or<br>MPG.D1_2 | 5.00%    | air partial pres. meas. Drywell 1 / DW1             |
| MPG.D2_3           | MPG.D2_1 or<br>MPG.D2_2 | 5.00%    | air partial pres. meas. Drywell 2 / DW2             |
| MPG.S1             | MPG.S2                  | 5.00%    | air partial pres. meas. Wetwell /WW1                |
| MPG.S2             | MPG.S1                  | 5.00%    | air partial pres. meas. Wetwell /WW2                |
| MV.MS1<br>(1)÷     |                         | N/A      | volume flow meas. Main Steam line RPV->DW1          |
| MV.MS2<br>(1)÷     |                         | N/A      | volume flow meas. Main Steam line RPV->DW2          |
| MV.P1F<br>(1)(2) # |                         | 3.00%    | volume flow meas. PCC1 Feed DW1->PCC1               |
| MV.P2F<br>(1)(2)   |                         | 3.00%    | volume flow meas. PCC2 Feed DW2->PCC2               |
| MV.P3F<br>(1)(2)   |                         | 3.00%    | volume flow meas. PCC3 Feed DW2->PCC3               |
| MW.RP.1            |                         | 3.00%    | electrical power meas Reactor Pressure Vessel / RPV |
| W.RP.2             |                         | 3.00%    | electrical power meas Reactor Pressure Vessel / RPV |
| IW.RP.3            |                         | 3.00%    | electrical power meas Reactor Pressure Vessel / RPV |
| fW.RP.4            |                         | 3.00%    | electrical power meas Reactor Pressure Vessel / RPV |
| fW.RP.5            |                         | 3.00%    | electrical power meas Reactor Pressure Vessel / RPV |



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| Table 6.1: INSTRUMENTATION REQUIRED* FOR TEST M2, M10A & M10B |          |   |  |  |  |
|---|----------|---|--|--|--|
| Backup  | Accuracy | Location  |  |  |  |
|   | 3.00%    | electrical power meas Reactor Pressure Vessel / RPV |  |  |  |
|   |          | Backup Accuracy                                     |  |  |  |

- (\*) Top Priority Measurements, additional high priority temperature measurements are defined in the text of this section.
- (\*) It is required that temperature monitoring capability with an accuracy of 1.5°C be available for these tests as described in the text of this section.
- (\*\*) PANDA instrumentation identification system is described in Section 5.2 of ALPHA 410
- (1) Differential accuracy over short time intervals is ±0.02m
- (#) Not required for tests M10A & M10B
- (+) The instruments for the main steam line not being used for test performance are not required.
- For volumetric flow rate measurements, all additional measurements (pressure and temperature) required to convert the volumetric flow rate to a mass flow rate are required.
- (2) 2 out of 3 for M2 and 1 out of 2 for M10A&M10B, respectively, volumetric flowmeters for PCC feed lines are required.
- (3) All instrumentation listed in this table is required to be operable only while the monitored process value is within the instruments operating range as defined in Table 5.3 of ALPHA-410.



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### DATA RECORDING. PROCESSING AND ANALYSIS

#### 7.1 Data Recording

During (approximately) the first two hours of the test (until the first drywell pressure peak is reached) the data for all channels will be recorded at 6 samples per minute. During the rest of the test (after the peak drywell pressure is reached) the data will be recorded at 1 sample per minute. It is necessary that the data sampling rate be sufficient to record opening and closing of the vacuum breakers between the drywells and wetwells.

### 7.2 Data Records

The digitally acquired data will be recorded in real time for the entire duration of the test. Immediately after the test, a copy of the data file will be created in order to have a backup record of the data file. Also to be recorded with this data file are all information required to perform subsequent processing of the data.

#### 7.3 Data Sheets

The following data sheets will be prepared for each test for inclusion in the PANDA Test File (PTF). The unique test number will be printed on each sheet.

- print table containing the list of the measurements with their main characteristics (identification, span, calibration constants, associated error, location on the facility, measurement channel number and sampling frequency)
- 2) graphs of top priority measurements identified in Section 6 as a function of time (time histories). Graphs may show groups of up to 8 test measurements.
- 3) print table showing the position (status) of all on-off valves, just after the beginning and just before the end of the test and periodically throughout the duration of the test.
- 7.4 Data Processing and Analysis

During the preconditioning of the test facility and during the running of the transient tests, the operators will monitor the required instrumentation identified for these tests in Table 6.1. The operators will check whether or not redundant measurements are consistent and perform other congruency checks including zero checks as possible to verify that the instrumentation and data acquisition system are working correctly.



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Following completion of the tests described in Section 9, data reduction will be performed to support preparation of the Apparent Test Results Reports (ATR). This data reduction will include a representative set of time history plots of system flows, differential pressure, vessel pressures, air partial pressure ( $O_2$  sensor readout), and temperatures covering the full test duration for top priority measurements. These results will be reviewed and reported in the ATR (see Section 10).

The Data Transmittal Report (DTR) will transmit all the data for the transient integral system tests (see Section 10).

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### 8. SHAKEDOWN TESTS

8.1 Purpose

The purposes of the shakedown tests are to:

- confirm test facility ability to establish a quasi-steady state set of initial conditions
- confirm adequacy of data acquisition system
- confirm ability to achieve a smooth but rapid transition Loween the pre-test initial conditions line-up to the test line-up
- confirm the adequacy of the test procedures.

For tests (M2, M10A & M10B), no shakedown tests are planned.



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9. TEST MATRIX

### 9.1 Test Description

A series of transient integral tests will be conducted using the PANDA facility configured as described in Section 4. The tests will be performed using detailed procedure(s). The following summarizes the approach to be followed by the test procedure(s).

The drywells, wetwells, GDCS tank and PCC pools will be pre-conditioned and brought separately to their required initial conditions (or slightly higher temperatures and/or pressures if heat loss or stabilization is expected to bring conditions within their required range).

Once the initial conditions of the various vessels are confirmed to match the values specified in Table 9.1, the test is initiated as follows:

Start to open all valves which must be open in lines between vessels per the test configuration in Section 4, except the valves in the RPV to drywell steamlines, within a period of approximately 5 minutes.

Then, the following sequence should be performed as quickly as possible:

1) Establish steam flow as follows:

- a) For test M2 & M10A open the valve in the steamline from the RPV to Drywell 2
- b) For test M10B open the valve in the steamline from the RPV to Drywell 1
- 2) Place RPV heater controls in automatic operation to follow the time dependent heater power determined from the specification in Table 9.2.

From this point on for tests M10A & M10B there are no futher operator actions

For tests M10A & M10B after at least 8 hours of test operations and when the indications for both drywells show that non-condensible gas partial pressure is no longer changing, data recording may be terminated, and the test performance declared complete.

(continued on next page for test M2)



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Test M2 will continue for at least 20 hours.

The following describes contingency testing to be done after 20 hours in test M2 as follows:

a. at 20 hr, increase the power to 800 kw.

b. after the system has reached a quasi-steady state condition, close the feedflow line to one of the PCCs. This PCC should be one which is removing the most heat as evidenced by the actual PCC pool level response.

c. after the system has reached a quasi-steady state condition, data recording may be terminated, and the test performance declared complete.



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| INITIAL CONDITIONS FOR PANDA TESTS M2, M10A & M10B |      |         |         |          |           |
|--|------|---------|---------|----------|-----------|
|  | RPV  | Drywell | Wetwell | GDCS     | PCC Pools |
| Total Pressure (kPa)                               | 295  | 294     | 285     | 294      | ≈100      |
| Air Pressure (kPa)                                 | 0    | 13      | 240     | 274      | N/A       |
| Vapor Temperature (K)                              | 406  | 404     | 352     | 333      | N/A       |
| Liquid Temperature (K)                             | 406  | 404     | 352     | 333      | ≈373      |
| Collapsed Water Level (m)<br>(1)                   | 11.2 | (2)     | 3.8     | 10.7 (3) | 23.6      |

Notes:

-(1) Water levels are specified relative to the top of the PANDA heater bundle.

- (2) The nominal DW condition is no water. However, a small amount of spill from the RPV to the DW at the start of the test is acceptable.
- (3) The GDCS level should be positioned in hydrostatic equilibrium with the RPV level (including an appropriate adjustment for temperature difference).



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| TIME FROM SCRAM (sec) | DECAY HEAT (%) | PANDA DECAY HEAT (MW)<br>1.056 |  |  |
|-----------------------|----------------|--------------------------------|--|--|
| 3600 (Test start)     | 0.0132         |                                |  |  |
| 3650                  | 0.0131         | 1.048                          |  |  |
| 4000                  | 0.0127         | 1.016                          |  |  |
| 5000                  | 0.0119         | 0.952                          |  |  |
| 6000                  | 0.0112         | 0.896                          |  |  |
| 7000                  | 0.0107         | 0.856                          |  |  |
| 7200                  | 0.0106         | 0.848                          |  |  |
| 8000                  | 0.0103         | 0.824                          |  |  |
| 9000                  | 0.0100         | 0.800                          |  |  |
| 10000                 | 0.00972        | 6.778                          |  |  |
| 14400                 | 0.00928        | 0.742                          |  |  |
| 18000                 | 0.00881        | 0.705                          |  |  |
| 20000                 | _0.00859       | 0.687                          |  |  |
| 28800                 | 0.00788        | 0.630                          |  |  |
| 30000                 | 0.00781        | 0.625                          |  |  |
| 6000                  | 0.00748        | 0.598                          |  |  |
| 0000                  | 0.00729        | 0.583                          |  |  |
| 0000                  | 0.00689        | 0.551                          |  |  |
| 0000                  | 0.00658        | 0.526                          |  |  |
| 0000                  | 0.00631        | 0.505                          |  |  |
| 0000                  | 0.00609        | 0.487                          |  |  |



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### Table 9.2b:

POWER FOR PANDA TESTS M2, M10A & M10B; (Total Power\*) / (Decay Power) vs. Time

| TIME FROM SCRAM (sec) | TOTAL POWER*/DECAY POWER |
|-----------------------|--------------------------|
| 3600 (Test Start)     | 1.070                    |
| 5000                  | 1.058                    |
| 7500                  | 1.038                    |
| 10,000                | 1.025                    |
| 12,500                | 1.019                    |
| 15,000                | 1.016                    |
| 20,000                | 1.010                    |
| 25,000                | 1.008                    |
| 30,000                | 1.007                    |
| 72,000                | 1.000                    |

\* Total power includes contribution from reactor structure stored energy

Note: Tolerance on PANDA power throughout transient is ± 25 kW or 0.025 MW.

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### 9.2 Test Acceptance Criteria

In order to assure the objectives of these tests are met, it is necessary that:

1) the values over the 1 minute period prior to the test for the following initial conditions must be within the specified ranges:

| - Total Pressure (kPa)                  | =         | reference matrix value $\pm 4$ kPa (all vessels except drywell)                  |
|---|-----------|--|
| - Drywell Air Partial Pressure (kl      | Pa)=      | reference matrix value $\pm 2$ kPa   |
| - Mean Vapor Temperature (K)            |           | reference matrix value $\pm 2$ °K(all vessels except GDCS/all tests)             |
| - Mean Vapor Temperature (K)            | 22        | reference matrix value ± 4 °K(GDCS)  |
| - Local Vapor Temperature (K)           | =         | mean value $\pm$ 2 °K(all vessels except GDCS/all tests)                         |
| - Local Vapor Temperature (K)           | =         | mean value ± 4 °K(GDCS)  |
| - Mean Liquid Temperature (K)           | =         | reference matrix value ± 2 °K (except for PCC' pools)                            |
| - Mean Liquid Temperature(K)            |           | Saturation temperature at actual environmental pressure +0/-4 °K (for PCC pools) |
| - Local Liquid Temperature (K)          | =         | mean value ± 2 °K  |
| - Wetwell and GDCS Water Level          | s =       | reference matrix value ± 0.190 m   |
| - RPV Water Level                       | -         | reference matrix value ± 0.200 m   |
| - PCC Pool Level                        | -         | reference matrix value ± 0.200 m   |
| 2) the required instrumentation defined | l in Sect | tion 6 and Table 6.1 be operational  |
|   |           | t, (to be confirmed during post-test data analysis):                             |
| PDV D                                   |           | process saturalitis).  |

RPV Power = reference matrix value ± 25 kW or 0.025 MW



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#### 10. REPORTS

One brief Apparent Test Results (ATR) report will be prepared covering the results for each of the transient integral tests based on the data reduction described in Section 7. The ATR will summarize the apparent results. The format for this report will include: test number, test objective, test date, data recording period, names of data files, list of failed or unavailable instruments considered to be required for the test, list of pressure and differential pressure instruments with zero not in tolerance or over-range during test, deviations from test procedure, problems, table of actual initial conditions based on average and standard deviation over a one minute time period just before the start of the test of all parameters with a specified acceptance criteria in section 9.1 and time history plots of top priority measurements over the test duration. The ATR report is a verified report, approved by the PSI PANDA Project Manager, and will be transmitted to the GE within approximately two weeks of the completion of each transient integral system test.

The Data Transmittal Report (DTR) containing all data for transient integral system tests M2, M10A &10B will be issued approximately two months after the last test is performed. It will provide detailed information on the test facility configuration, test instrumentation, test conditions and the format for the data. In addition, samples of data will be presented in tables and plots. The DTR will be verified before it is issued, approved by the PSI PANDA Project Manager, and then be transmitted to GE.

### 11. TEST HOLD/DECISION POINTS

The Test Procedure(s) must have been reviewed and approved by GE's Project Manager, GE Site QA Representative and PSI's PANDA Project Manager before the transient testing described in Section 9 can be performed.