



International Agreement Report

Assessment of RELAP5/MOD2 Cycle 36.04 with LOFT Large Break LOCE L2-3

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ICAP

ASSESSMENT OF RELAP5/MOD2 Cycle 36.04

USING LOFT LARGE BREAK LOCE L2-3

Abstract

The LOFT LOCE L2-3 was simulated using the RELAP5/MOD2 Cycle 36.04 code to assess its capability to predict the thermal-hydraulic phenomena in LBLOCA of the PWR. The reactor vessel was simulated with two core channels and split downcomer modelling for a base case calculation using the frozen code. From the results of the base case calculation, deficiencies of the critical flow model and the CHF correlation at high flow rate were identified, and the severeness of the rewetting criteria were also found. Additional calculation using an updated version of RELAP5/MOD2 Cycle 36.04 including modifications of the rewet criteria shows a substantial improvement in the core thermal response.

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Executive Summary

This report documents the assessment calculations using the RELAP5/MOD2 Cycle 36.04 to predict thermal-hydraulic response of Loss of Fluid Test (LOFT) system during the Loss of Coolant Experiment (LOCE) L2-3. LOCE L2-3 simulated a 200 % offset shear at the discharge of the Primary Coolant Pump (PCP) in the four loop commercial PWR.

To simulate LOFT system specific to L2-3 experiment, the reactor core was modelled with two separate flow channels and the reactor vessel downcomer was described by two equally-split channels. Three heat structures were used to describe the LOFT fuel assemblies.

The results of the base case calculation using the frozen code of the RELAP5/MOD2 were compared with the experimental data in terms of loop flows, secondary side pressure, Emergency Core Cooling System (ECCS) performance, reactor vessel behavior and fuel rod thermal response. As result of comparisons, the overall hydraulic behavior was well-predicted, while fuel rod thermal response was poorly predicted.

Major reasons of the discrepancies in the prediction were identified as the code deficiencies in the thermal-hydraulic models : (1) underprediction of cold leg break flow due to the deficiency of critical flow model, (2) poor prediction of the core early heatup during blowdown due to the deficiency of CHF correlation at high flow rate, and (3) poor prediction of rewetting phenomena due to the severeness of the rewet criteria in the frozen code.

To reidentify the deficiencies found in the base case calculation and to determine the effectiveness of the rewet criteria change in the frozen code, a sensitivity calculation was performed using an updated code with the PSI modification. The result of the sensitivity calculation shows that the rewet phenomena was well-predicted by the PSI-modified criteria.

1. Introduction

RELAP5/MOD2(1), a frozen version by US Nuclear Regulatory Commission (USNRC), has been assessed through the International Code Assessment and Application Program (ICAP) for its capability and deficiencies in the prediction of the postulated Large Break Loss of Coolant Accident (LBLOCA) in Pressurized Water Reactor (PWR).

This report is one of the Korean ICAP contributions to support code assessment, code deficiency identification and code improvement. In this study the RELAP5/MOD2 Cycle 36.04 was assessed for the Experiment L2-3 conducted in the Loss of Fluid Test (LOFT) at Idaho National Engineering Laboratory (INEL) [2].

The Experiment L2-3, as one of the Integral Effect Test (IET), was a Large Break Loss of Coolant Experiment (LBLOCE), which represented the postulated LBLOCA in the typical Westinghouse type PWR with four loop. During LOCE L2-3, two Primary Coolant Pumps (PCP) in LOFT system were set to operate without coastdown, this PCP running was found to have significant effect on the reactor core thermal response, i.e., the early core quenching in blowdown phase. This blowdown quenching phenomena was called as 'rewet' which was due to a quick return to the nucleate boiling heat transfer regime from the post dryout regime and was one of the important assessment items in the previous LBLOCA calculations [3, 4].

The objectives of this study are to predict the major hydraulic behavior and thermal response of the LOFT system during the LOCE L2-3 and to identify deficiencies of the frozen RELAP5/MOD2 Cycle 36.04 code in simulating thermal-hydraulic phenomena specific to LBLOCA by comparing the calculation results with the experiment data. From the findings obtained by ICAP activities [5], it was known that the major deficiencies of RELAP5/MOD2 were summarized as the Critical Heat Flux (CHF) correlations, the critical flow model and the

interfacial drag correlations. This study, therefore, is focused to confirm whether the deficiencies as stated above are still found in the Experiment L2-3 simulation. And to investigate the sensitivity of the rewet criteria in the RELAP5/MOD2, an updated version from Cycle 36.04 using the modified rewet criteria by Aksan [6], at Paul Scherer Institute (PSI), Swiss was tested in this study.

The descriptions for LOFT facility and L2-3 experiment are presented in chapter 2, the RELAP5 input modelling in chapter 3 and the results of a base case calculation and their discussions in chapter 4. In chapter 5, a result of sensitivity calculation is described and the conclusions obtained from the present study are summarized in chapter 6.

2. Facility and Test Description

2.1 Facility Description

The LOFT facility is an experimental 50 MWt PWR designed to simulate LOCA's and anticipated transients and to provide data on the thermal-hydraulic phenomena occurring throughout the system [7]. It is a scaled representation of a commercial PWR of Westinghouse type having 4 loops with a volume ratio of 1/60. The LOFT system consists of five major systems: reactor system, primary coolant system, blowdown suppression system, emergency core cooling system and secondary coolant system, and also includes instrumentations. The length of the core and reactor vessel is 1.68 and 7 m, respectively. The overall configuration is shown in Fig.1.

2.2 Test Description

Experiment L2-3 was performed as part of LOFT program Power Ascension Series (L2), which was designed to investigate the response of LOFT nuclear core to the blowdown, refill and reflood transient during LOCE.

Experiment L2-3 represents a postulate 200% double ended offset near of the pump discharge piping in the cold leg of commercial PWR. The specific objectives of L2-3 test were to determine the corewide and spatial variation of fuel rod cladding thermal response, to identify thermal-hydraulic phenomena and their effect on the core of LOFT and to determine the ECCS performance and core reflood characteristics. During L2-3 experiment, primary coolant pumps were set to continue to operate, which results in an early quenching during blowdown, called rewet. The phenomena of rewet is currently known as early return to

nucleate boiling in the core, which has been a common interesting point of code assessment [3, 4].

Prior to Experiment L2-3, LOFT facility was set to be a primary system pressure of 15.06 MPa, primary system cold leg and hot leg temperature of 560.7 K and 592.9 K respectively, and a loop mass flow rate of 199.7 kg/sec. Initial reactor power level was 36.7 MW with a maximum linear heat generation rate (LHGR) of 39.4 kW/m. Table 1 presents a summary of initial conditions of Experiment L2-3.

The experiment was initiated by opening the Quick Opening Blowdown Valves (QOBV) both in hot leg and cold leg. Reactor was scrammed at 0.103 sec after initiation of the experiment by operator signal. Identifiable phenomena in the experiment are listed in Table 2. Injection from accumulator began at 17 sec, approximately when primary system pressure moved down to 4.18 MPa. High Pressure Safety Injection (HPSI) system and Low Pressure Safety Injection (LPSI) system started to inject at 14 sec and 29 sec and LOFT core volume was finally reflooded at approximately 55 sec.

2.3 Measurement Uncertainty

Uncertainties of the experimental data and computed variables were fully discussed in reference [2] for L2-3 test. Uncertainties on the measured values and computed values used for comparisons with calculation in this report are presented in Table 3.

3. Code and Modelling Description

RELAP5/MOD2 Cycle 36.04, frozen version of the code by USNRC, was used in the present calculation with modifications of some indexing schemes. An update procedure is listed in Appendix A, which is exactly the same as that in L2-5 assesment report [8]. Since any RELAP5 input specific to L2-3 experiment was not obtained from INEL, a reference input was developed by the authors based on the input used in the previous L2-5 expericent assessment [8].

3.1 Input Modelling

All components except a reactor core and a reactor vessel downcomer of LCFT for L2-3 experiment were geometrically modelled as the same as those for L2-5 case [8] i.e, equal volumes, junctions and heat structures. A nodalization diagram used in the present calculation is shown in Fig.2. Total number of hydrodynamic volumes, junctions and heat structures are 128, 149 and 27.

The reactor core was modelled by two flow channels; a hot channel and an average channel representing the central fuel assembly (numbered by 5 in the reference [7]) and the other peripheral fuel assemblies, respectively. Each flow channel was divided by six volumes with equal lengths. Two flow channels were linked by six crossflow junctions to allow crossflow in the core with a specified junction loss coefficient of 4.69 for all crossflow junctions. These junction loss coefficients were selected as the same as those in the Best Estimate Prediction for L2-5 experiment [9].

The reactor vessel downcomer was modelled by two split flow channels : an intact side downcomer and a broken side downcomer. Each downcomer has five volumes including a volume representing an upper annulus part above the cold leg nozzles. To describe an azimuthal flow across the downcomer, four

crossflow junctions were used to link four volumes between the intact-side downcomer and the broken-side one with exception of the volumes representing the cold leg nozzles. Loss coefficients at the downcomer crossflow junctions were tuned to match the measured loop flow behavior, according to the reference [9]. The values used in the present calculation ranges from 18.0 to 98.0 with their junction elevations.

Originally LOFT fuel rods had two types of axial power profile : a high power shape for central fuel assembly and a low power shape for peripheral fuel assemblies. Both of them have almost identical shapes but have different magnitudes in LHGR. During L2-3 input preparation, however it is found that an actual summation of rod power integrated over the full length of rod did not match and was lower than the experimental total power level, 36.7 MW. In the present study, three heat structure component were used to model the LOFT fuel rods: 204 hot rods in the central fuel assembly, 572 average rods and 574 intermediate rods in the peripheral fuel assemblies respectively. And the axial power shapes can be determined by the experimental LHGR distributions [2] for the hot rods and average rods. For the intermediate fuel rods heat structure, a mean LHGR distribution of hot and average rods can be used. This modelling scheme of fuel rods can match a given total power. The profiles of LHGR's were shown in Fig.3 and Table 4 presents a summary of reactor vessel modelling.

3.2 Initial Conditions and Boundary conditions

To provide all initial conditions of the whole system prior to transient, a steady state run was carried out with seven steady state controllers : two primary coolant pump speed controllers, a pressurizer heater power controller a pressurizer spray valve area controller, a letdown and charging valve area controller, a main steam control valve (MSCV) area controller and a feedwater

flow rate controller. A steady input deck was provided in Appendix B.

The result obtained from the steady state run was compared with the measured initial conditions in Table 1. The RELAP5 calculated results generally agree with the experimental conditions.

Boundary conditions required to simulate the L2-3 experiment are almost the same as those in L2-5 experiment except PCP running. The PCP speed during the transient was assumed to be constant, which was a simple approximation of the real PCP running behavior showing oscillations around a fixed speed during the transient [2].

Based on the experiment data [2], the reactor power history and containment pressure were described as time dependent tables. Performance curves for HPSI and LPSI flow rate as function of cold leg pressure were provided in the input. Feedwater flow rate was reduced to be zero in 2.5 seconds after LOCE initiation using a time-dependent junction as the same as the L2-5 experiment. And the steam generator secondary side air-cooled condenser was modelled as a time-dependent volume with a constant pressure of 2.069 MPa during the transient. All informations of the boundary conditions were provided in the steady and transient input deck. The transient input deck was listed in Appendix C.

4. Base Case Calculation

The L2-3 LOCE was calculated up to 100 sec using all initial conditions obtained from steady state run. Some additional components such as pressurizer spray, letdown and charging systems used for the steady state calculation are deleted in transient input deck.

The sequence of events during transient calculation are presented in Table 2 as compared with L2-3 experiment chronology. In this chapter, the predicted important thermal-hydraulic parameter such as system pressure, loop mass flow rates and cladding temperatures are compared with the measured data.

4.1 Loop Behavior

Fig.4 shows a comparison of the calculated mass flow rate with the measured one at the broken loop cold leg up to 40 sec. An overall behavior of break flow was well predicted by RELAP5/MOD2 except the underprediction during a short period from 3 sec to 9 sec. This period corresponded to the transition phase from the subcooled break flow to the two-phase break flow. The subcooled break flow was completed at about 3 sec both in calculation and in experiment as shown in Table 2. After that time the break flow was well simulated by the RELAP5 calculation. The underprediction of break flow during the phase transition period can be considered as a deficiency of the RELAP5/MOD2 critical flow model. This led the reactor vessel to contain more coolant inventory than the experiment, which amounts to 400 kg approximately. This overestimated coolant inventory may suppress the core heatup discussed in later chapter.

Fig.5 presents a comparison of mass flow rate in the broken loop hot leg. As expected, the magnitude of break flow was less than that in the cold leg due

to higher flow resistance in the hot leg. The calculated break flow in hot leg was well-agreed with the experimental result.

Mass flow rate in the intact loop cold leg was shown in Fig.6. The predicted mass flow rate was almost similar to the measured one. However, the calculation did not show several jumps which can be found in the experimental behavior with high frequencies after 20 sec. It was regarded as the effect of void oscillation phenomena induced by the highly subcooled ECC injection water during the reflood phase.

Fig.7 indicates a comparison of the net flow into the core, i.e. intact loop cold leg flow minus broken loop cold leg flow. The intact loop cold leg mass flow, driven by the operating pumps, exceeded the broken loop flow from 3 sec to 6 seconds causing an increase in positive core flow, which had reversed after saturation in the lower plenum at about 7 sec. The calculation result was in good agreement with the experimental data.

In general, the predicted loop behaviors agreed well with the experiment data within the range allowed by the instrument uncertainty except the underprediction of cold leg break flow during the transition period.

4.2 Secondary Side Behavior and ECCS Performance

Fig.8 shows a comparison of the steam dome pressure of the steam generator secondary side. The experimental data used in this comparison was not fully qualified one but accurate for initial condition only. The predicted pressure was fairly well-agreed to the measured one up to 40 sec. Difference after 40 sec was considered to have little effect on the primary side behavior since the transient was fast enough to neglect the heat transfer from the secondary side.

Fig.9 presents a comparison of accumulator injection flow rate and Fig.10

a comparison of accumulator liquid level. The calculated injection flow rate was larger before 42 sec and then lower than the experiment, while the accumulator liquid level was well agreed to the experiment. The overprediction of mass flow rate during 20 to 40 sec can be due to a underprediction of the primary system cold leg pressure discussed in later chapter. The overpredicted injection mass amounts to 180 kg approximately. The experiment shows that the injection continued until 60 sec, while the calculation shows that the injection was completed at 42 sec. From the fact that the measured liquid level was almost stationary at 42 sec as shown in Fig.10, it can be stated that the jump and oscillation in the injection mass flow rate is not a real situation but a measurement error.

Figs. 11 and 12 show comparisons of mass flow rates through a HPSI line and LPSI line. During the early period of injection, some overpredictions were found in both injection flow rates, whose total amount was about 65 kg. This overprediction was also due to the primary system pressure. However, the overall injection behaviors were comparatively close to the experiment.

4.3 Vessel Phenomena

Fig.13 shows a comparison of primary system pressure at the upper plenum. The predicted behavior agreed with experiment data very well. A little earlier depressurization was found in calculation than that in the experiment before 10 sec, which was resulted partly from an underprediction of cold leg break flow (Fig.4). The calculation also presented a little lower pressure after 20 sec than the experiment. It resulted in the early high ECC injection behavior as stated in the previous chapter and yielded a underestimation of the liquid coolant temperature in the lower plenum as shown in Fig. 14, which was a saturation temperature at the corresponded pressure.

Fig.15 shows the collapsed liquid levels in the two downcomer channels and in the two core channels of reactor vessel. Since no experiment data for these items were available, the predicted levels are plotted only.

The liquid level behaviors in core were found to be almost identical in both average channel and hot channel. From these level behaviors, it is shown that the LOFT core was almost empty in 5 sec and then filled with liquid up to 2.36 m in 8 sec by the positive net flow into the core as explained in the previous chapter. This substantial liquid filling up for a short period yielded a corewide rewet, and the rewet was completed in 8 sec. A core re-empty was predicted at 14 sec, a lower plenum was fully refilled by ECC water injection at 35 sec, and a core-reflood was completed at 43 sec, approximately. The end of reflood was predicted to be quite earlier than the measured time as shown in Table 1. This earlier end of reflood, i.e., earlier core quenching, than the experiment was due to the overestimated coolant inventory, which was mainly caused by underprediction of cold leg break flow.

The liquid level in the broken side downcomer were predicted to be different from that in the intact side one due to the split nodalization of vessel downcomer. In the early blowdown period up to 3 sec, the broken side liquid level dropped more rapidly than the intact side one due to less flow resistance. Both levels ceased to drop and increased a little slightly at the time of the transition from subcooled break flow to two-phase break flow. The increase of level is caused that the break flow was reduced significantly at the transition time, while the incoming flow was still maintained by the operation of the intact loop pumps. During core rewetting period, downcomer liquid levels decreased again. The slope of the broken side liquid level was slower than that in intact side one, which was due to upward water flow from the lower plenum to the broken side downcomer. At the time of accumulator injection, 16 sec, both levels moved up again with some time delay in the broken side.

4.4 Fuel Thermal Response

Figs. 16, 17, 18, 19, 20 and 21 present comparisons of cladding temperatures of hot fuel rods at 5, 16.5, 27.5, 39, 49.5 and 60 inch elevations from the bottom of core, respectively. From these comparisons, the following features were found.

- 1) For a lower part (5 in and 16.5 in), the predicted DNB (departures from nucleate boiling) times were later than the measured values during blowdown phase. And the calculated cladding temperatures during blowdown heat-up period were appreciably lower and core rewet was completed earlier than the measured data.
- 2) The predicted thermal response during reflood heatup period were also later in timing and smaller in heatup amounts than the experimental data. Consequently, core quenching times were predicted as substantially earlier than the experiment.
- 3) For a middle part (27.5 in and 39 in), the prediction shows earlier DNB's, higher heat up's and earlier core quenches than the experiment, and the absence of blowdown rewets. The peak cladding temperature (PCT) was predicted as 950 K at 27.5 inch elevation in blowdown phase, which was higher than the experiment, 891 K at 24 inch elevations.
- 4) For a higher part (49.5 in and 60 in), core was not heated up both in blowdown and reflood phases.

To find out some reasons of such thermal responses that deviated from the experimental behaviors, the calculated fuel surface heat transfer coefficients were presented as shown in Fig.22 for a volume 2 (16.5 in) and a volume 3 (27.5 in). For a volume 3, heat transfer coefficient rapidly dropped as soon as

the experiment was initiated (transition from the saturated nucleate boiling to the film boiling) and the film boiling heat transfer mode was sustained until 20 sec, while for a volume 2, the saturated nucleate boiling remained for 4 or 5 sec, and then changed to the film boiling during a short period (rewet).

Fig.23 shows liquid fractions at volume 2 and volume 3. Both volumes had experienced an almost similar transient in liquid fraction for the first 2 sec, as shown in this figure, however a DNB was not predicted in volume 2 as shown in Fig.17. As a result of poor prediction of DNB, flow regimes at these two volumes were different during the same period as shown in Fig.24. Therefore, it can be stated that the deficiency of CHF correlation in the frozen RELAP5/MOD2 was also found in the LOCE L2-3 simulation in the condition of high flow rate (the predicted mass flux into the core was about $1000 \text{ kg/m}^2 \text{ sec}$).

The increasing behavior of liquid fraction at volume 3 was almost the same as that in volume 2 during 5 to 8 sec except some time delay, however no rewetting was found at the volume 3. This indicates the severeness of rewet criteria in the frozen RELAP5/MOD2 Cycle 36.04.

Some features found in reflood heat up calculation can be regarded as an over prediction of coolant inventory as mentioned in the previous chapter. Total amount of coolant inventory overestimated by the present calculation was 545 kg, approximately. This amount was not so small when compared to the primary coolant system inventory 5646.8 kg at the steady state condition. This added inventory can be considered to suppress the core heat up during reflood period.

5. Sensitivity Study

From the findings in the base case calculation, the severeness of the rewet criteria in the frozen code was one of the most noticeable problems in the point of the fuel cladding thermal response. In this study, to investigate the sensitivity of rewet criteria, an updated code with PSI modification from the RELAP5/MOD2 Cycle 36.04 was used in the re-calculation with the same input as in the base case calculation. The PSI modification [6] includes three major changes: interfacial friction formula, rewet criteria and heat transfer correlations in reflood phase. A whole list of the updates was presented in the Appendix D. Especially in the rewet, three independent criteria was checked as follows:

- 1) $(T_w + T_{sat}) < 1250 \text{ K}$
- 2) Equilibrium quality less than 0.99
- 3) Mass flux less than -100 kg/sec m^2

Figures 25, 26, 27 and 28 show comparisons of the calculated cladding temperatures by the frozen Cycle 36.04 with those by PSI updated version at 16.5, 27.5, 39 and 49.5 inch elevation, respectively. The predicted thermal responses at 5 and 60 inch elevation were not plotted since almost the same result was obtained as base calculation. Even at 16.5 inch location (Fig.25), a similar thermal response to the base case calculation was obtained except a little higher heat up in blowdown phase. And both calculation still show differences from the experimental cladding temperature.

At the middle elevations, 27.5 inches in Fig.26 and 39 inches in Fig.27, the sensitivity calculation shows the blowdown rewet evidently, which were not predicted in the base case calculation. As the result calculated by the PSI-updated version, the core heatups were a little higher than the base case calculation result. It was due to some modifications of heat transfer coefficients

in the subcooled or saturated transition film boiling regime included in the PSI updates [6].

At 49 inch elevation, the sensitivity calculation result shows a appreciable blowdown heatup and a rewet, which was not found in the base case one. The onset of CHF at this elevation was currently understood as a deficiency of Biasi's CHF correlation in the RELAP5/MOD2. A comparison of void fraction at the 5th volume in hot channel was presented in Fig. 29. In spite that the void fraction predicted by the PSI version was lower than that calculated by cycle 36.04 version until 1.5 sec approximately, as shown in Fig.29, a heatup was found in the calculation by the PSI version.

From these comparisons, it is concluded that the deficiency of the Biasi's CHF correlation was re-identified at high flow rate and that the modification of rewet criteria using PSI updates can predict the rewet phenomena during blowdown phase properly

6. Run Statistics

The main frame computer used in the present calculations was CDC 170-875 Series at KAERI, with NOS Version 2.6.1.

Fig.30 presents the plot of the required CPU time for the transient time in the base case calculation. And the time step size are also plotted in Fig.31. The user-specified maximum time step was 0.05 sec up to 20 second in real time and then reduced to 0.01 sec up to 100 second as recommended in reference[1]. The run statistics is summarized in Table 5 from the major edit and the grind time can be calculated as follows.

Computer time, CPU = 1795.36 - 3.121 = 1792.239 (sec)

Number of time step, DT = 9635 - 76 = 9559

Number of volume, C = 128

Transient real time, RT = 100 (sec)

Grind time = CPU x1000 / (C * DT) = 1.4647 CPU m sec/vol/step

7. Conclusions

RELAP5/MOD2 Cycle 36.04 code was assessed using LOFT L2-3 LBLOCE data. A base case calculation was carried out using the original version of the code. And one sensitivity calculation was conducted with an updated version by the PSI modification. The calculated thermal-hydraulic behaviors were compared with the experimental data to identify code capability. As a result of the present calculations, the following conclusions are obtained :

- 1) Using LOFT LOCE L2-3, a base case calculation and a sensitivity calculation were successfully executed from the point of view of specific objectives and requirements of ICAP assessment activity.
- 2) The loop flow behaviors were fairly well predicted by the frozen RELAP5/MOD2 Cycle 36.04 code. The secondary side behavior and ECCS performance were also well simulated by the base case calculation. Hydraulic behavior such as liquid levels in downcomer and core in the reactor vessel were reasonably predicted. The thermal response of fuel rods was calculated, and the calculated PCT was 950 K, a little higher than the measured PCT of 891 K.
- 3) From the base case calculation using the frozen RELAP5/MOD2, the cold leg break flow was underpredicted due to the deficiency of the critical flow model in the transition phase from subcooled flow to two-phase flow. This led a overprediction of coolant inventory. The early core heatup during the blowdown phase was not well-predicted due to a deficiency of CHF correlation at high flow rate of the frozen code. The rewet phenomena was also poorly predicted due to the severeness of the criteria.
- 4) As a result of the sensitivity calculation using the updated rewet criteria by PSI, blowdown quenching behavior was relatively well-predicted.

References

1. Ransom, V.H. and Wagner, R.J. RELAP5/MOD2 Code Manuals, NUREG/CR-4312, EGG-2396, EG&G Idaho Inc., Dec. 1985.
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3. Carbajo, J.J, "A Study on the Rewetting Temperature," Nuclear Engineering and Design, Vol 84, pp 21-52, 1985.
4. Aksan, S.N., "Investigation on Rapid Cladding Cooling and Quench During the Blowdown Phase of a LBLOCA Using RELAP5/MOD2," Presentation on the Fourth International Topical Meeting on Nuclear Reactor Thermal-Hydraulics(NURETH-4), Karlsruhe, FRG, Oct. 1989
5. Driskell W.E. et al, Summary of ICAP Assessment Results for RELAP5/MOD2, Draft of ICAP Annual Report for 1989, INEL.
6. Aksan, S.N., Analytis, G.Th., and Lubbesmeyer, D., Switzerland's Code Assessment Activities in Support of the ICAP the 16th Water Reactor Safety Meeting, Oct. 1988, Gaithersburg, USA
7. Reeder, P.L., LOFT System and Test Descriptions, NUREG/CR-0247, July 1978
8. Young Seok Bang, et al, Assessment of RELAP5/MOD2 Cycle 36.04 Using LOFT Large Break Experiment L2-5, NUREG/IA (to be published), KAERI, Korea, 1990.
9. Demmie, P.N., et al, Best Estimate Prediction for LOFT Nuclear Experiment L2-3, EGG-LOFT-5869, EG&G, INEL, May 1982.

Table 1 Summary of comparison of the initial conditions
between the measured and the calculated in base case

Parameter	Measured	Calculated
• Primary Coolant System		
Mass flow rate* , kg/s	199.0	199.01
Hot leg pressure* , MPa	15.06	15.07
Cold leg temperature* , K	560.7	560.39
Hot leg temperature , K	592.9	592.75
• Reactor Vessel		
Power level , MW	36.0	36.0
Maximum linear heat generation rate(MLHGR), kW/m	39.4	39.8
• Pressurizer		
Liquid temperature , K	615.3	613.8
Pressure , MPa	15.06	15.066
Liquid level* , m	1.19	1.1723
Water volume, m ³	0.67	0.627
• Steam Generator sec.side		
Saturation temperature , K	482.1	487.88
Pressure , MPa	6.18	6.1
Mass flow rate , kg/s	19.5	19.129
Level* , m	3.11	3.11

Note * : Setpoint in steady state controllers

Table 2 Summary of comparison of the sequence of events between the measured and the calculated in base case

Event	Measured,sec	Calculated,sec
Experiment initiated	0.	0.
End of subcooled blowdown	0.05	**
Reactor scrammed *	0.103	0.103
First indication of DNB	0.96	0.4
End of subcooled break flow (cold leg)	3.0	3.05
Maximum cladding temperature attained	4.95	5.0
Earliest corewide rewet	8.0	7.8
HPSI initiated *	14.0	14.0
Pressureizer emptied	14.0	14.0
Accumulator injection initiated	16.0	15.66
LPSI initiated *	29.0	29.0
Lower plenum refilled	35.0	35.0
Saturated blowdown ended	40.0	**
Accumulator liquid flow ended	45.0	42.0
Core volume reflooded	55.0	43.0

Note * : specified by input , ** : not predicted

Table 3. Uncertainties of Measurements

item	type	range	uncertainty
Primary system pressure	M	0.1 - 20.8 MPa	0.22 MPa
Secondary system pressure	M	0.1 - 8.4 MPa	0.11 MPa
Coolant Temperature	M	311 - 977.4 K	5.1 K
Accumulator liquid level	M	0.0 - 3 m	0.02 m
Accumulator flow rate	M	0.0 - 126.2 l/s	3.5 l/s
HPSI flow rate	M	0.0 - 1.9 l/s	0.02 l/s
LPSI flow rate	M	0.0 - 25.2 l/s	Not available
Mass flow rate at			
broken loop cold leg	C		63.7 kg/s
broken loop hot leg	C		23.7 kg/s
Cladding Temperature	M	422 - 1533 K	6.5 K
Primary Coolant Pump Speed	C	0.0 - 4500 RPM	8.2 RPM
Reactor Power	M	0.0 - 100 %	3.0 %

Note. M : Measured data,

C : Computed variables from the measured data

Table 4. Summary of the important items in nodalization

items	Description
Core	
Number of flow channel	2
Channel area ratio (hot/total)	13.7 %
Number of volume per channel	6
Number of crossflow junction between channels	6
Loss coefficients at crossflow junctions	4.2
Number of heat structure component (hot:average)	1:2
Power ratio (hot/total)	20.5 %
Number of volume per heat structure	6
Gap conductance model	used
Reflood option	Pressure *
Number of mesh point in heat structure	10
Number of maximum fine mesh	8
Number of volume in core bypass component	3
Core Bypass flow ratio	5 %
Downcomer	
Number of flow channel	2
Area ratio (intact side channel/broken side channel)	1/1
Number of volume per flow channel	5
Number of crossflow junctions for downcomer bypass	5
Loss coefficients at crossflow junction	18.0 - 98.0 **

Note * : Pressure at core top less than 0.1 MPa
 ** : Loss coefficients varies with elevation

Table 5 . Run statistics data in base case

Transient time (sec)	CPU time (sec)	Attempted ADV	Repeated ADV	Last DT	Courant DT
0	3.121	0	0	0.35	0
10	122.678	669	12	0.0125	0.01546
20	265.146	1469	12	0.0125	0.01202
25	352.17	1969	12	0.01	0.00958
30	446.903	2469	12	0.01	0.01097
35	542.424	2969	12	0.01	0.00916
40	645.349	3497	12	0.01	0.02857
45	750.017	4020	21	0.01	0.01576
50	845.089	4520	21	0.01	0.02828
55	940.003	5020	21	0.01	0.02852
60	1035.32	5520	21	0.01	0.03126
65	1130.72	6028	25	0.01	0.02552
70	1223.29	6528	25	0.01	0.03884
75	1316.72	7028	25	0.01	0.0450
80	1410.51	7528	25	0.01	0.01604
85	1504.71	8050	35	0.01	0.03274
90	1594.56	8550	35	0.01	0.04819
95	1693.06	9083	50	0.01	0.05249
100	1795.36	9635	76	0.01	0.04379

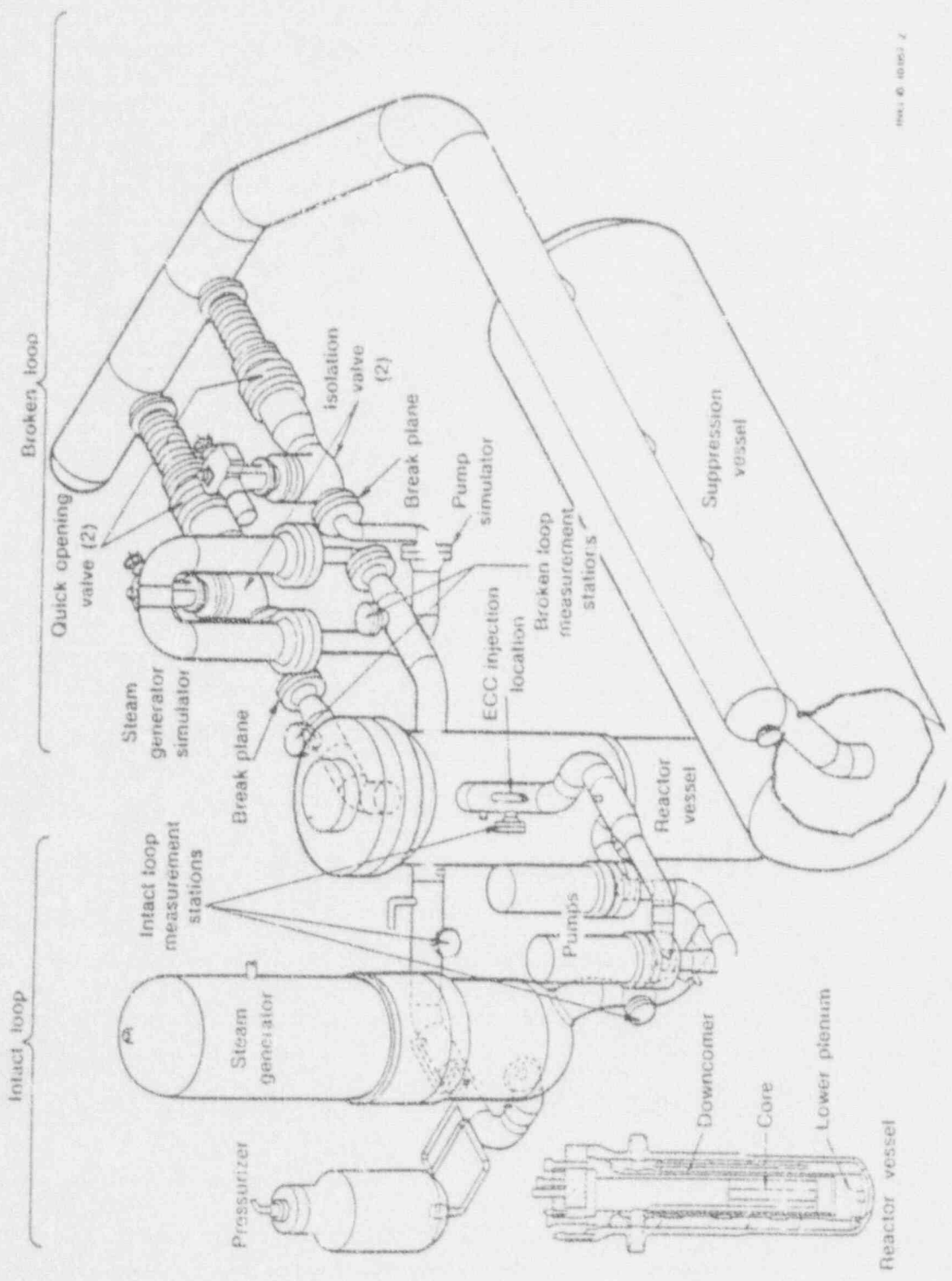


FIG. 10 10103 Z

Fig.1 Axonometric configuration of LOFT L2-3 test

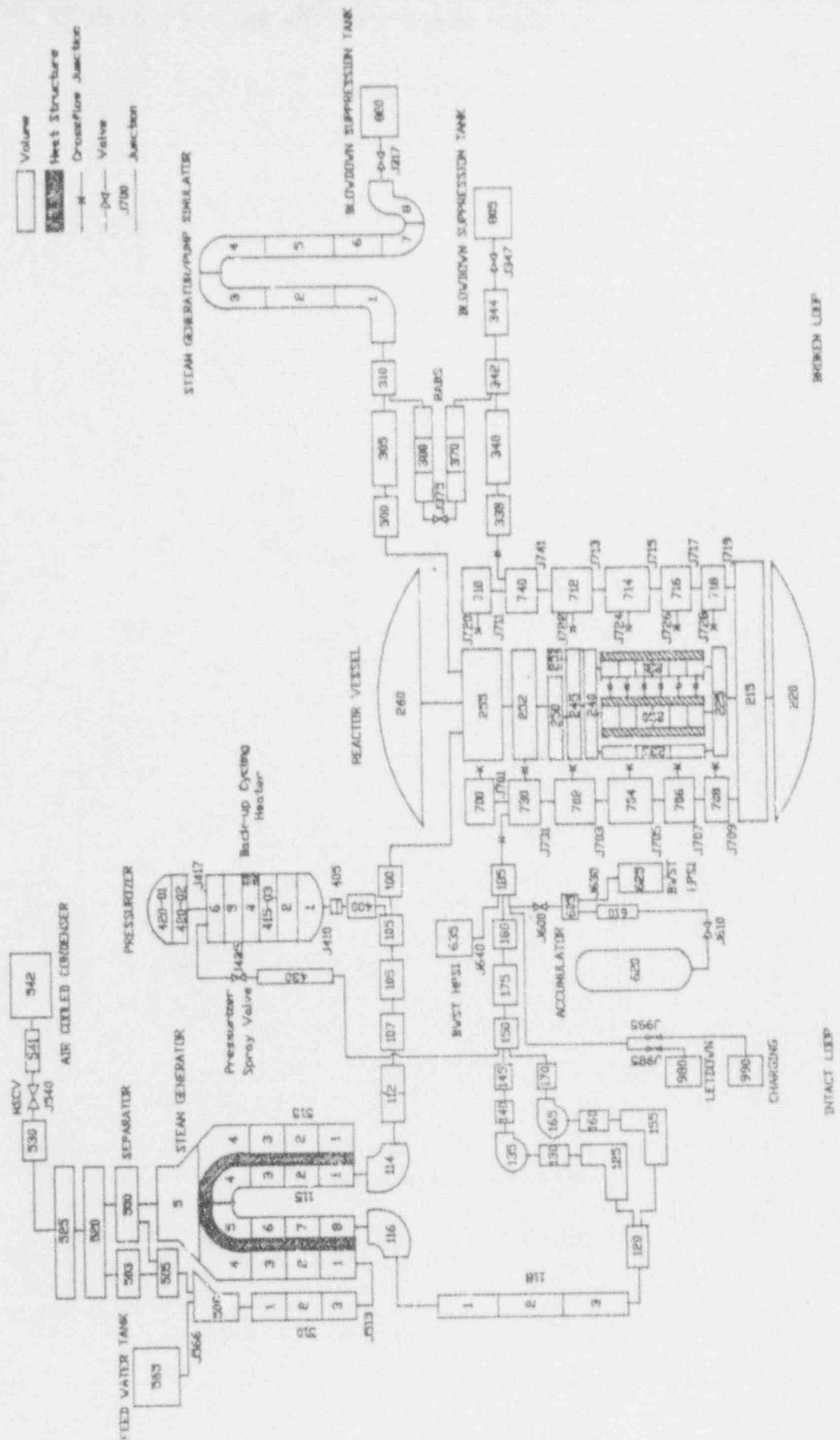


Fig. 2 Nodalization diagram for base case calculation of LGFT L2-3 test

LOFT L2-3 Base Calculation

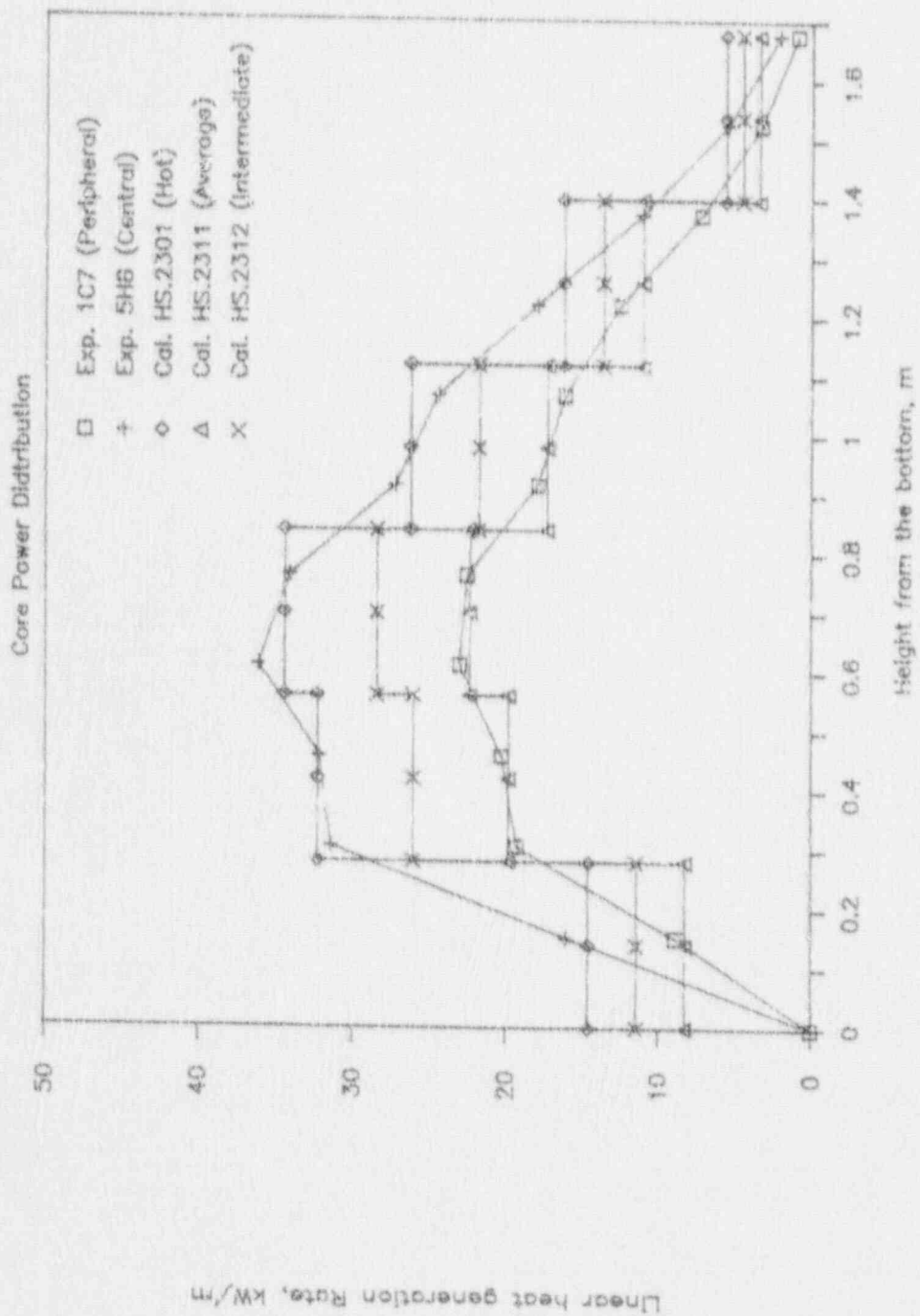


Fig. 3 Axial power distribution in base case calculation of L2-3 test

LOFT L2-3 Base Calculation

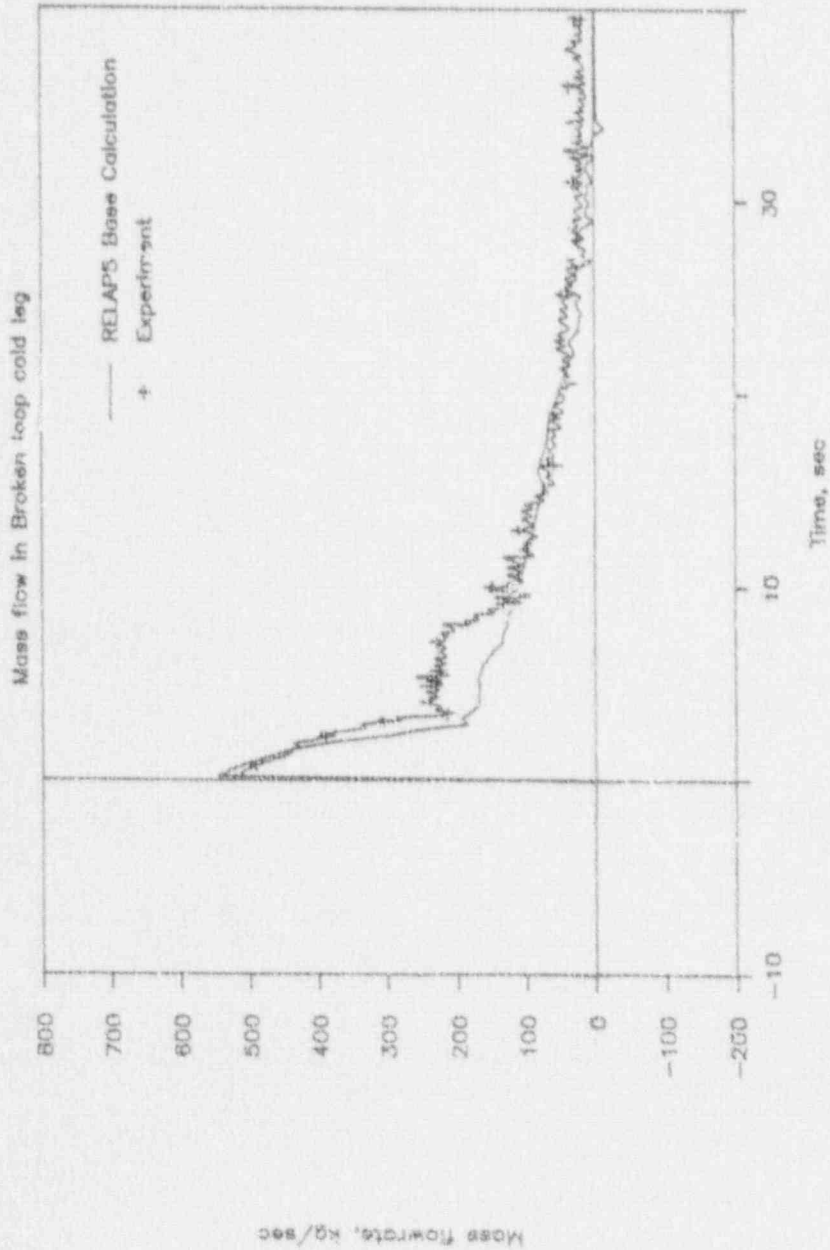


Fig. 4 Comparison of mass flow rate at broken loop cold leg between the base case calculation and the experiment

LOFT L2-3 Base Calculation

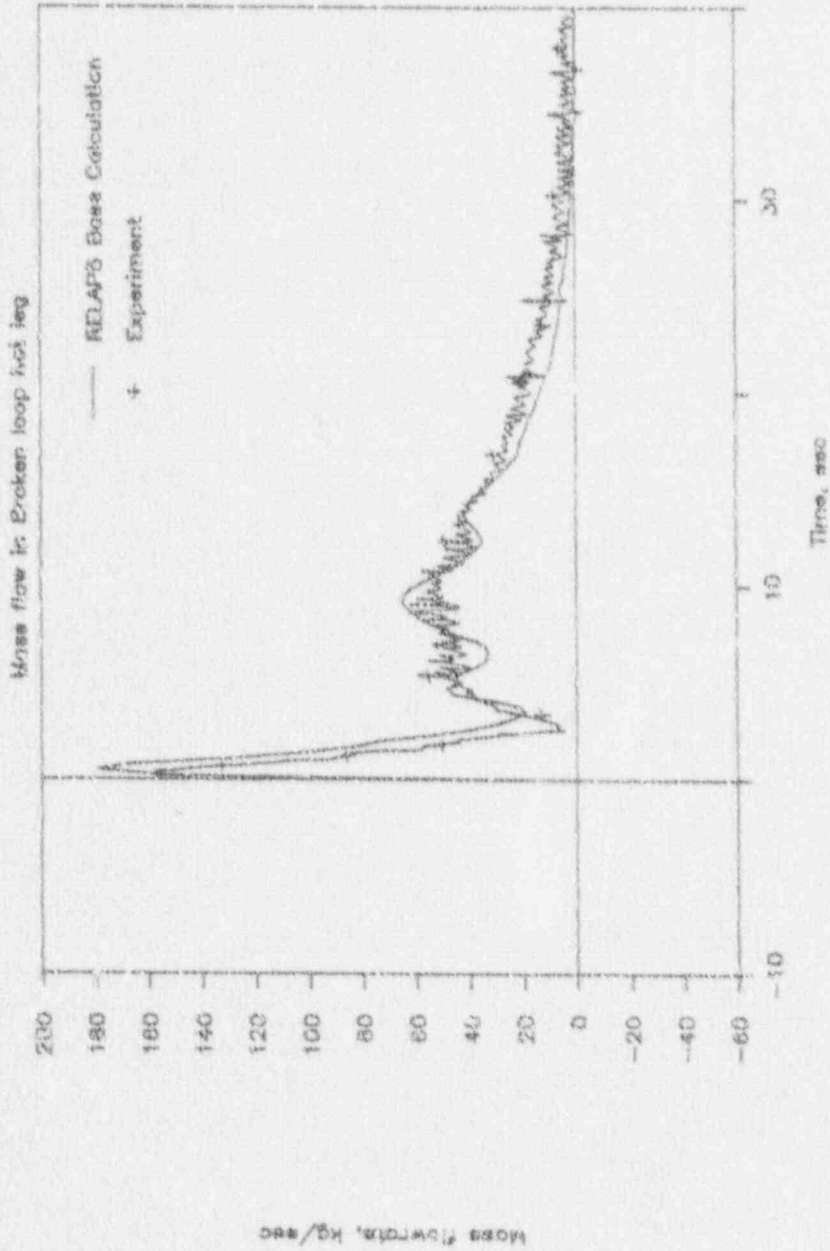


Fig.5 Comparison of mass flow rate at broken loop hot leg between the base case calculation and the experiment

LOFT L2-3 Base Calculation

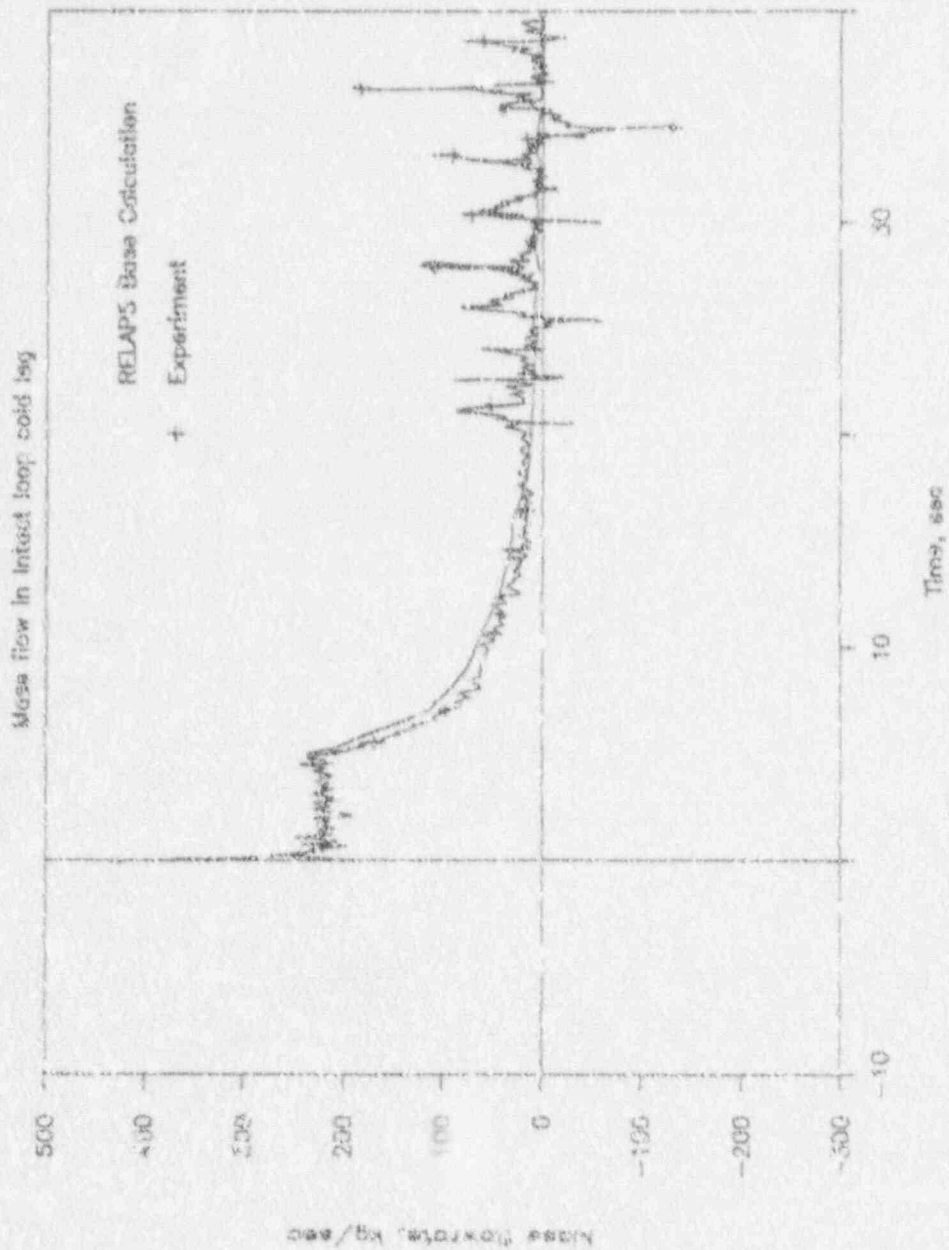


Fig. 6 Comparison of mass flow rate at intact loop cold leg between (1) base case calculation and the experiment

LOFT L2-3 Base Calculation

Net mass flow (NET-BLCL)

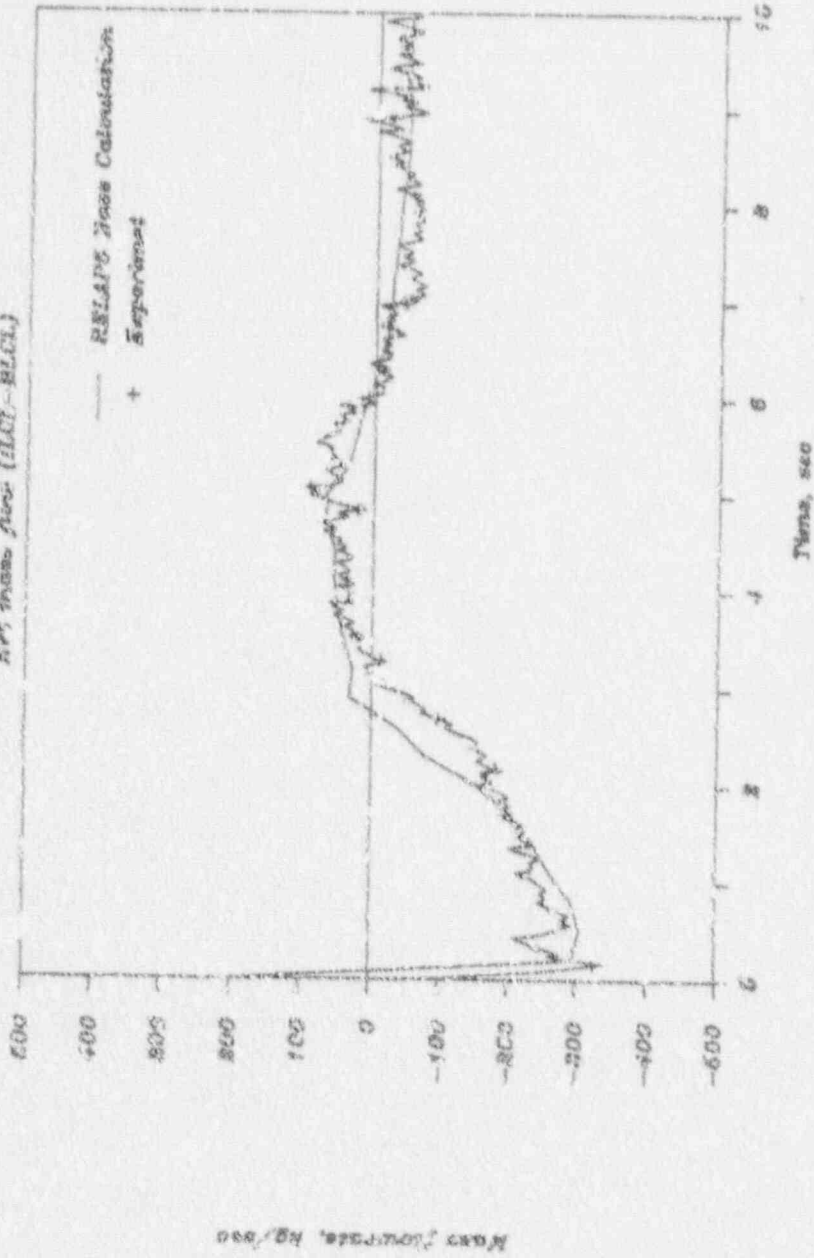


Fig. 7 Comparison of net mass flow rate into the core between the base case calculation and the experiment

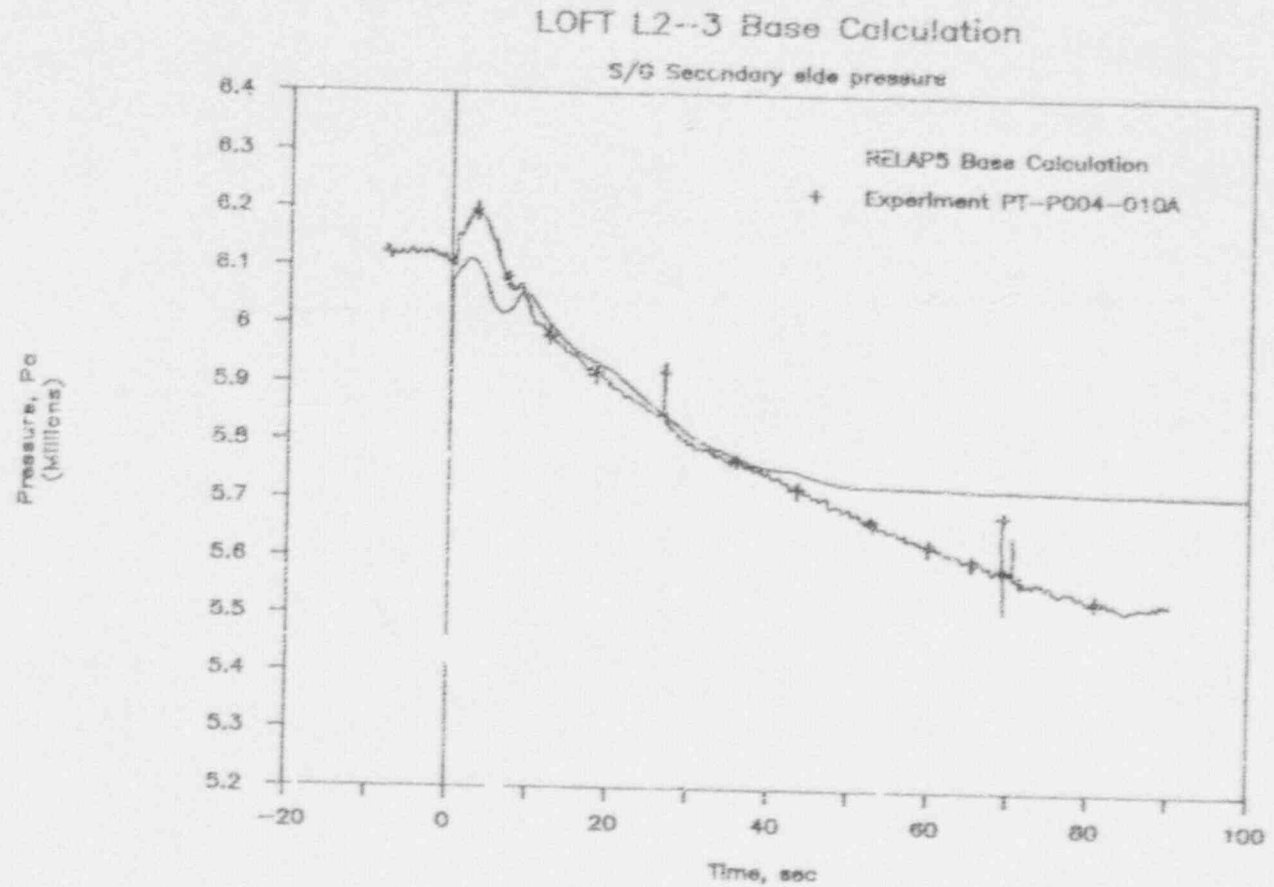
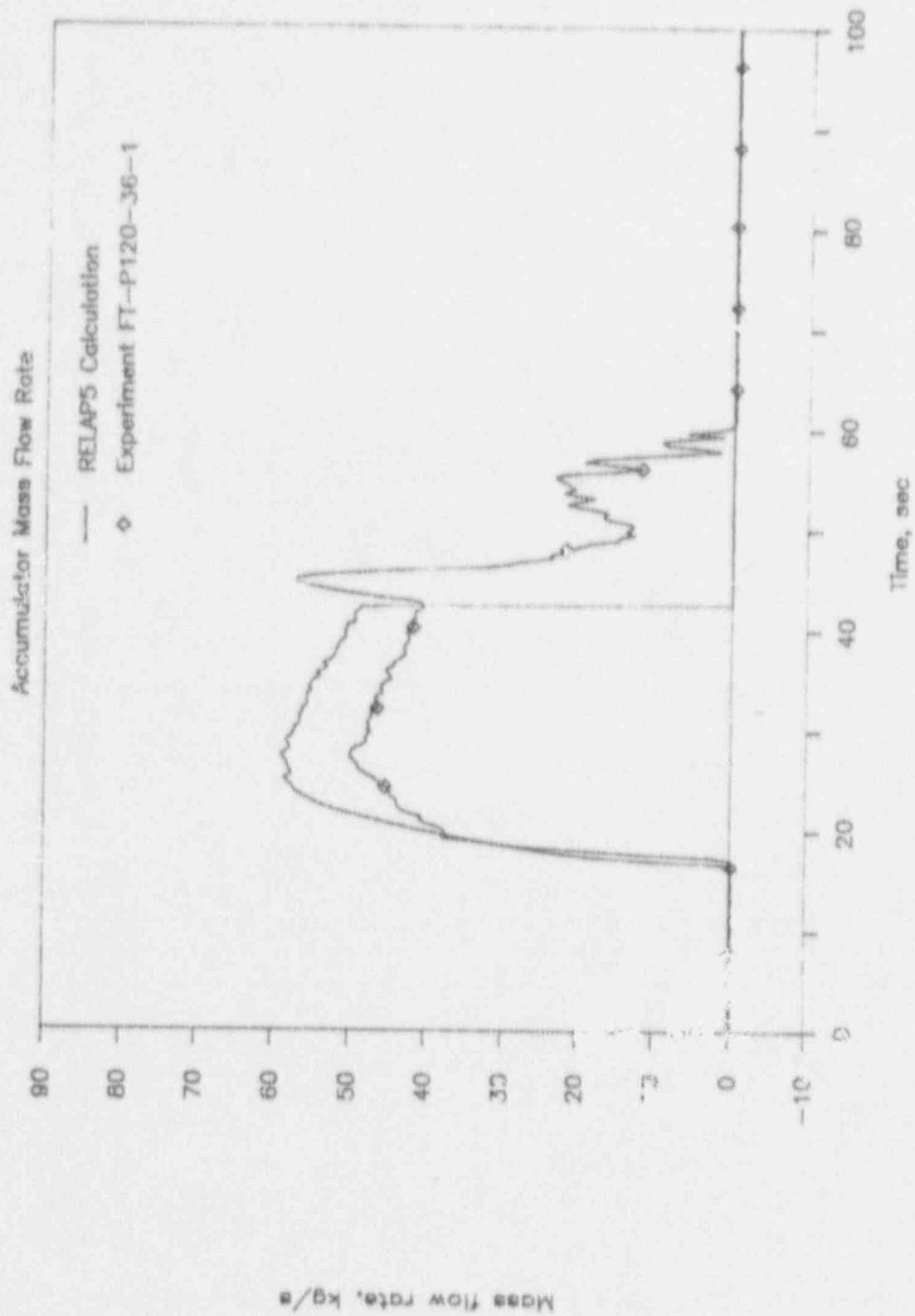


Fig.8 Comparison of steam dome pressure at S/G secondary side between the base case calculation and the experiment

LOFT L2-3 Base Calculation



F. 9 Comparison of accumulator injection flow rate between the base case calculation and the experiment

LOFT L2-3 Base Calculation

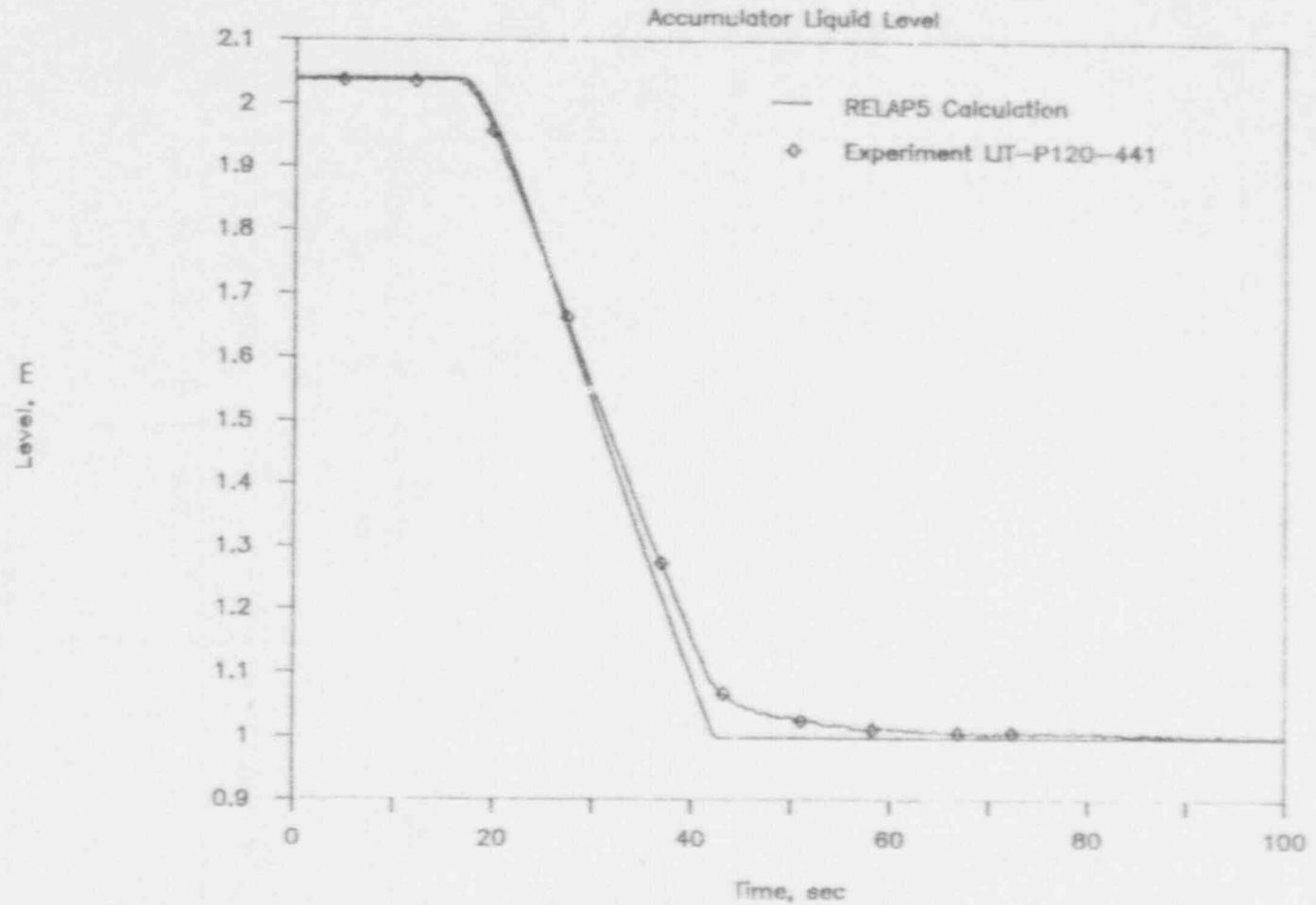


Fig.10 Comparison of accumulator liquid level between the base case calculation and the experiment

L2-3 Base calculation

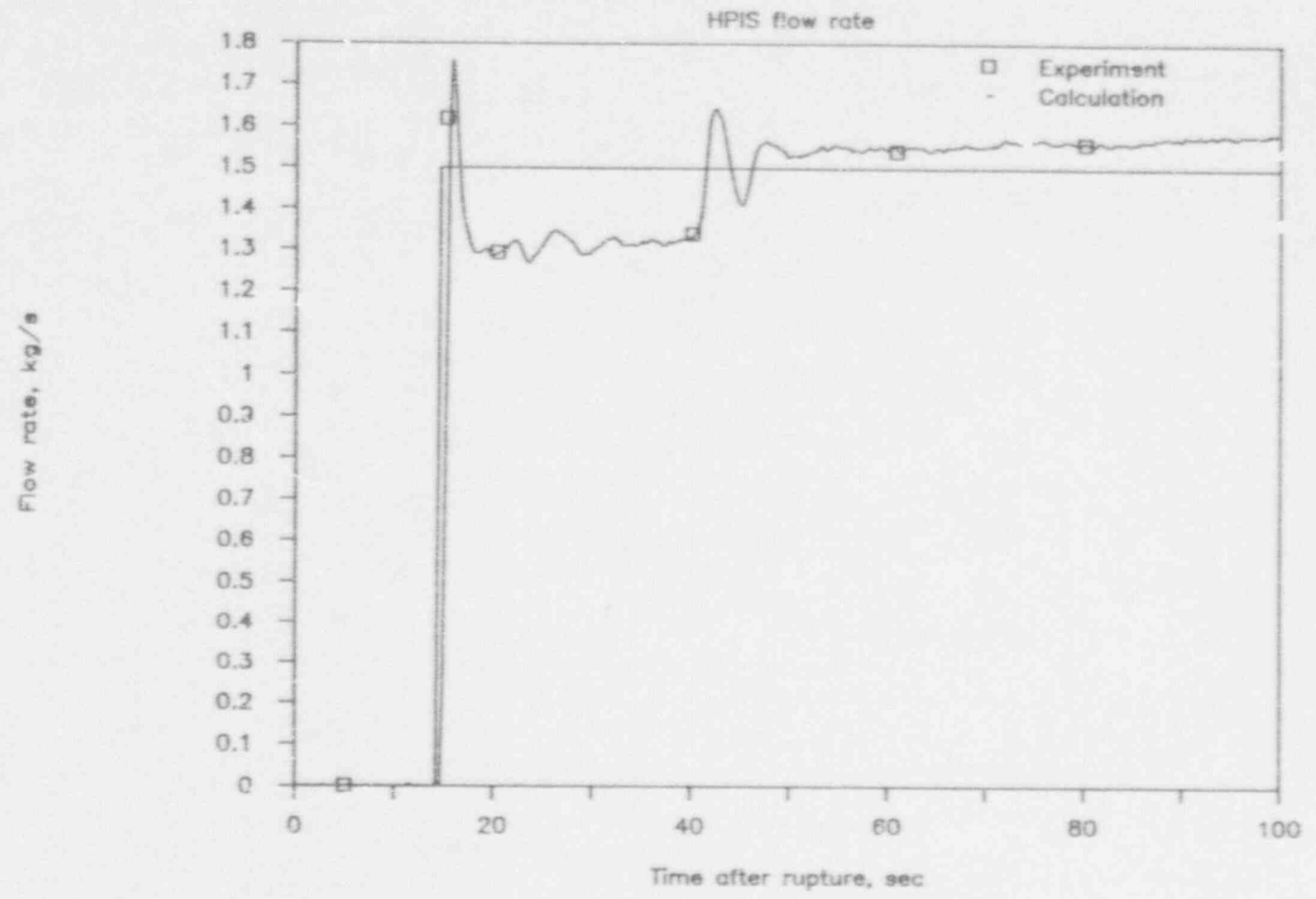


Fig.11 Comparison of HPSI flow rate between the base case calculation and the experiment

L2-3 Base calculation

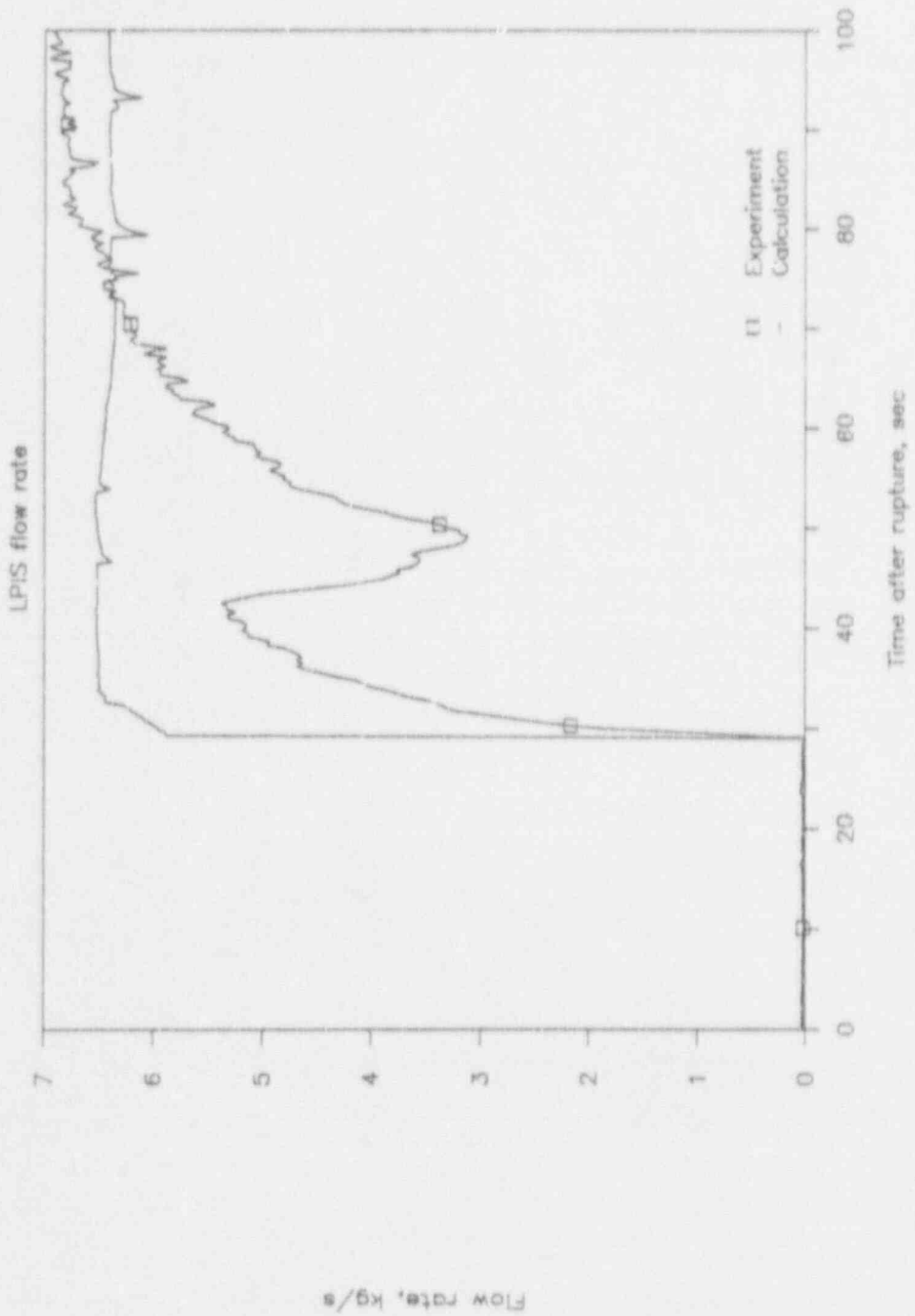


Fig. 12 Comparison of LPSI flow rate between the base case calculation and the experiment

LOFT 1.2-3 Base Calculation

Primary System Pressure

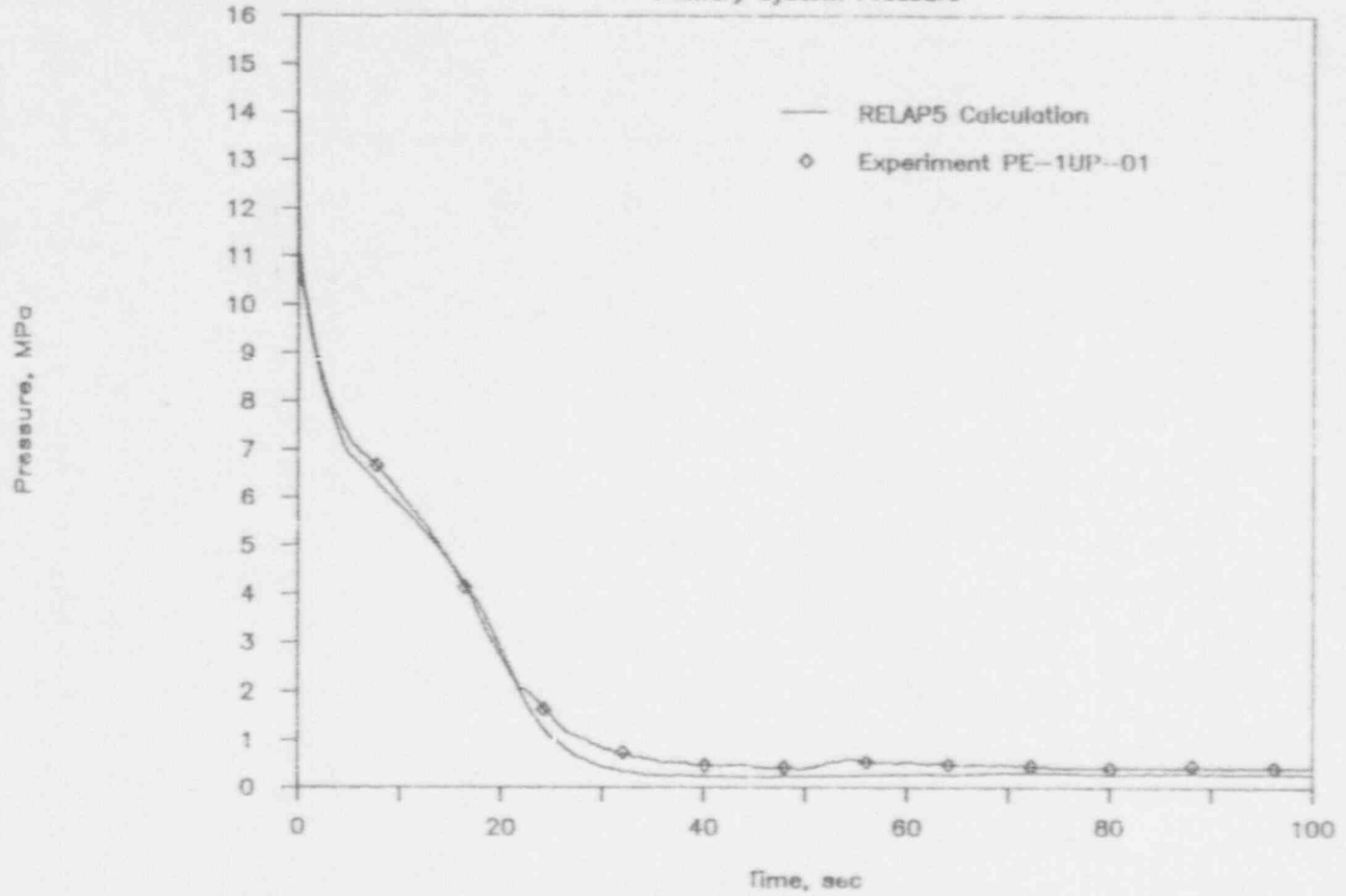


Fig.13 Comparison of primary system pressure between the base case calculation and the experiment

LOFT L2-3 Base Calculation

Lower Plenum Coolant Temperature

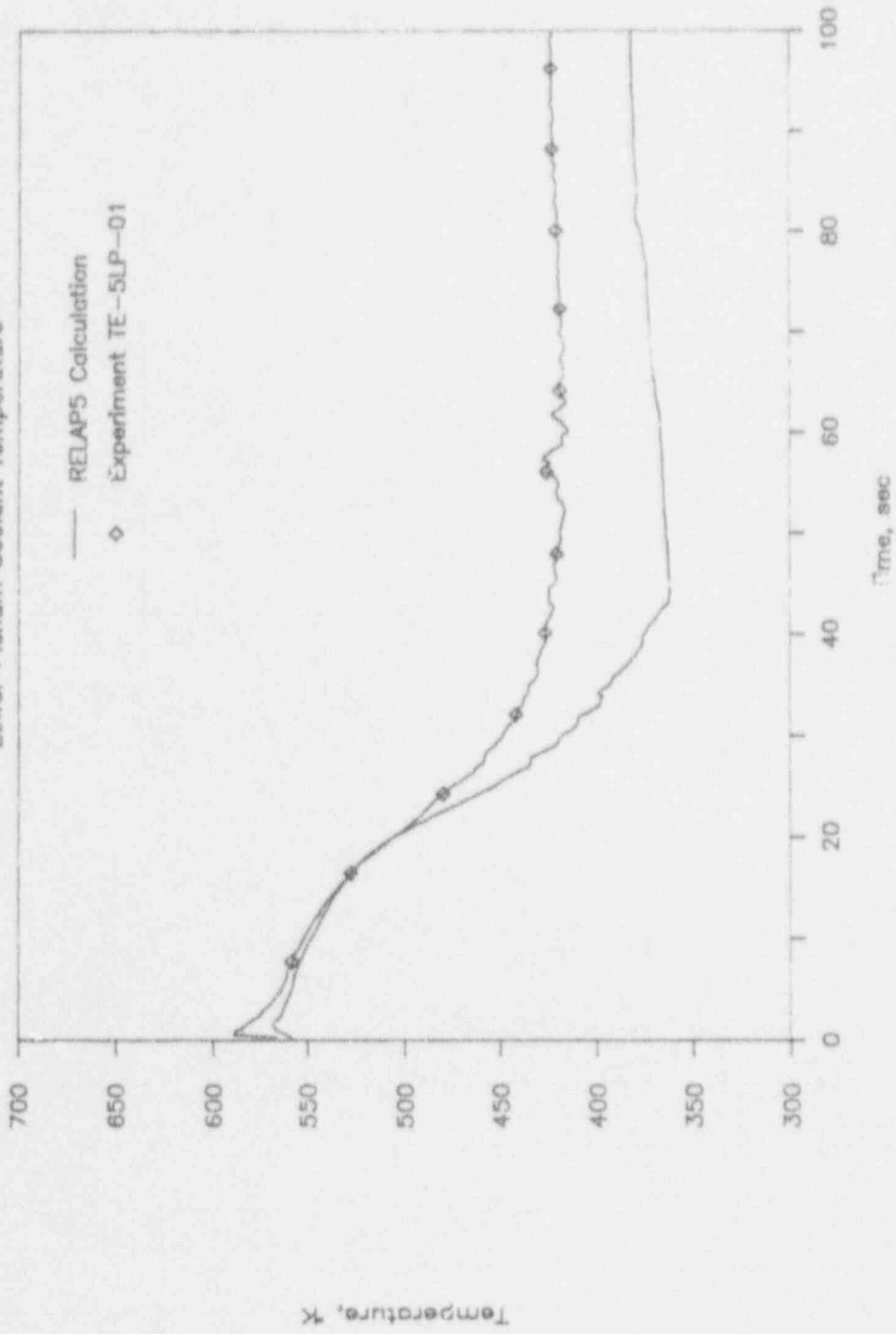


Fig. 14 Comparison of coolant temperature in lower plenum between the base case calculation and the experiment

LOFT L2-3 Base Calculation

Collapsed Water Level in Reactor Vessel

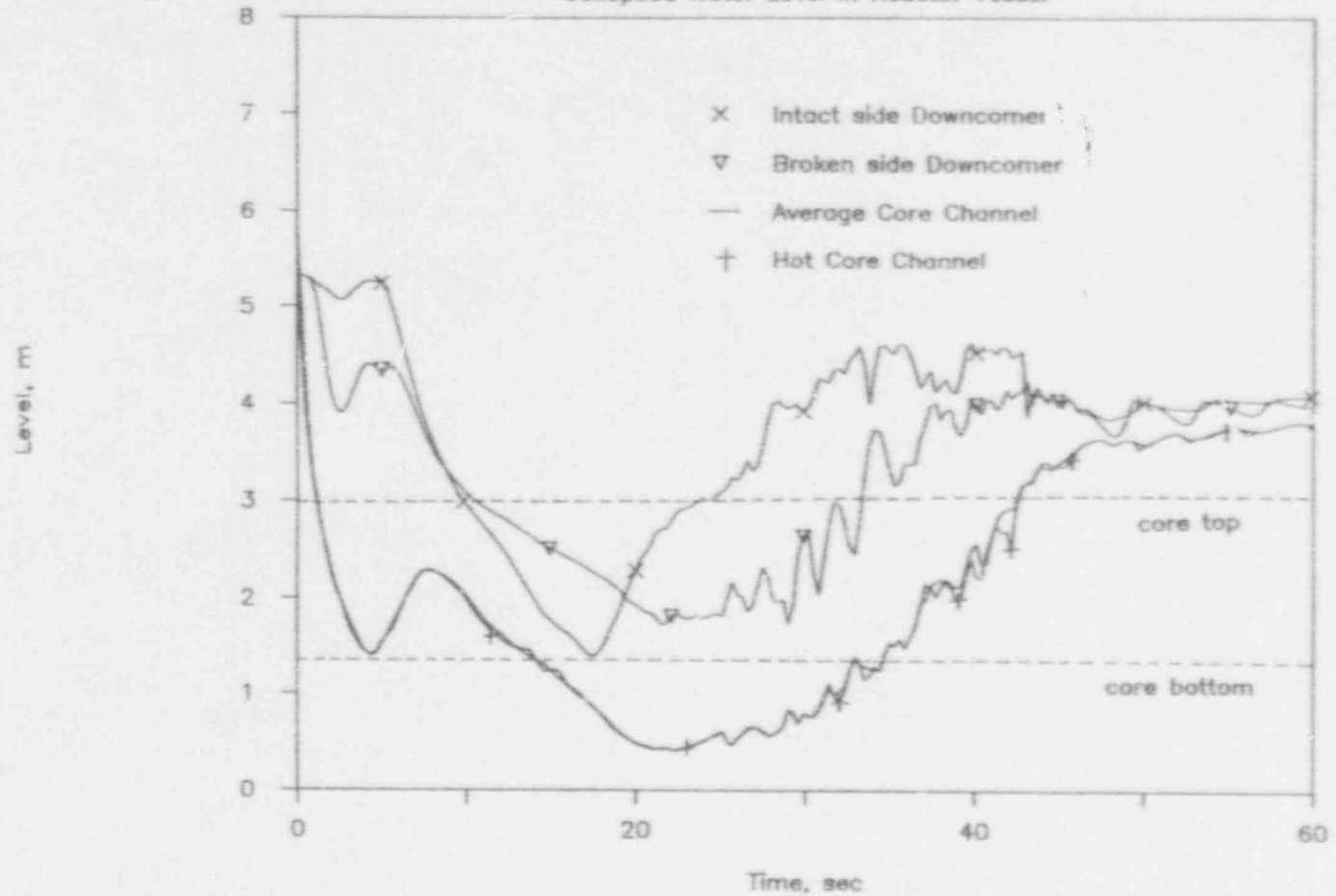


Fig.15 Collapsed liquid levels calculated in the base case calculation for the broken side downcomer, intact side downcomer, hot core channel and average core channel of the reactor vessel

LOFT L2-3 Base Calculation

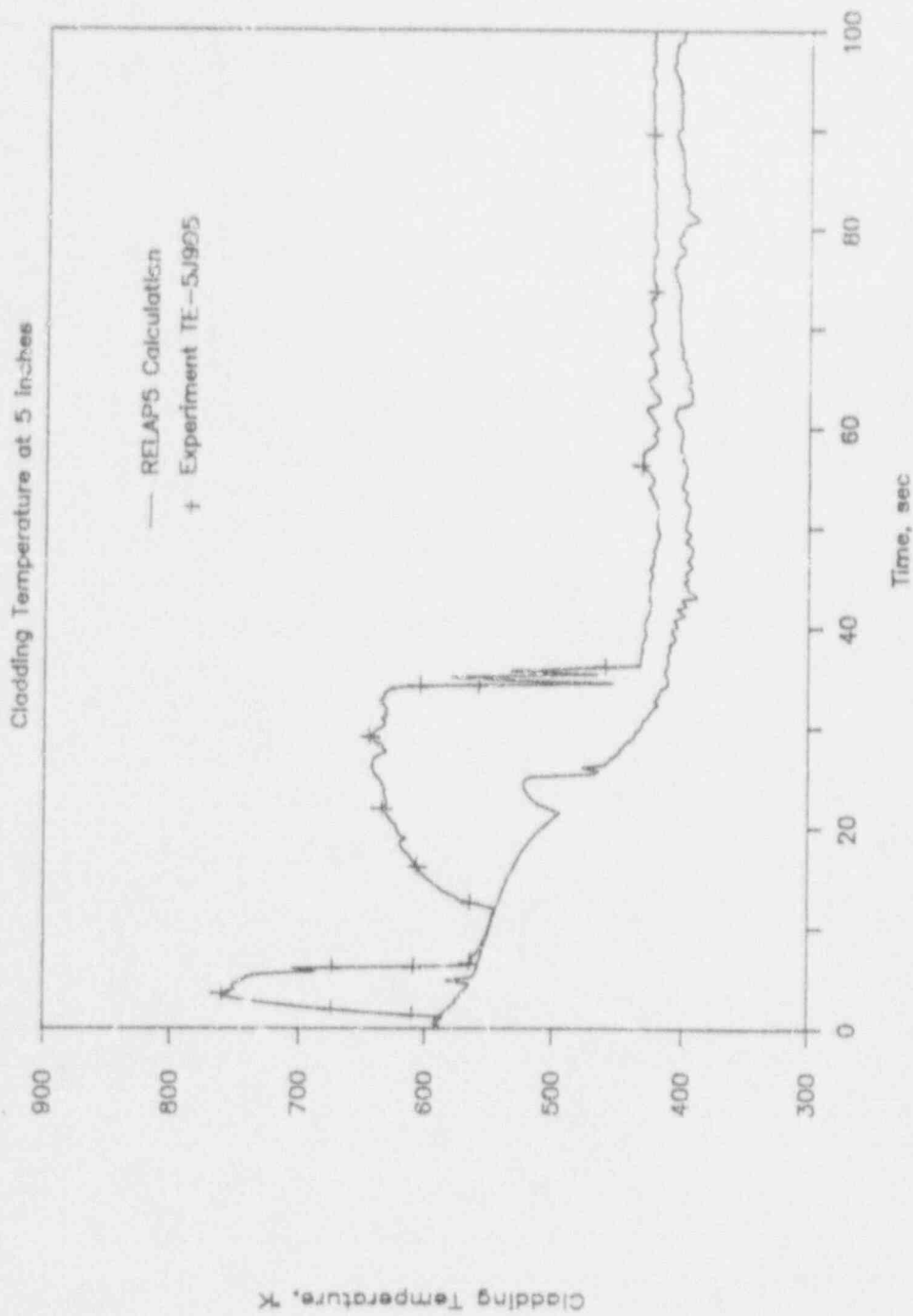


Fig. 16 Comparison of cladding temperature at 5 inches of hot fuel between the base case calculation and the experiment

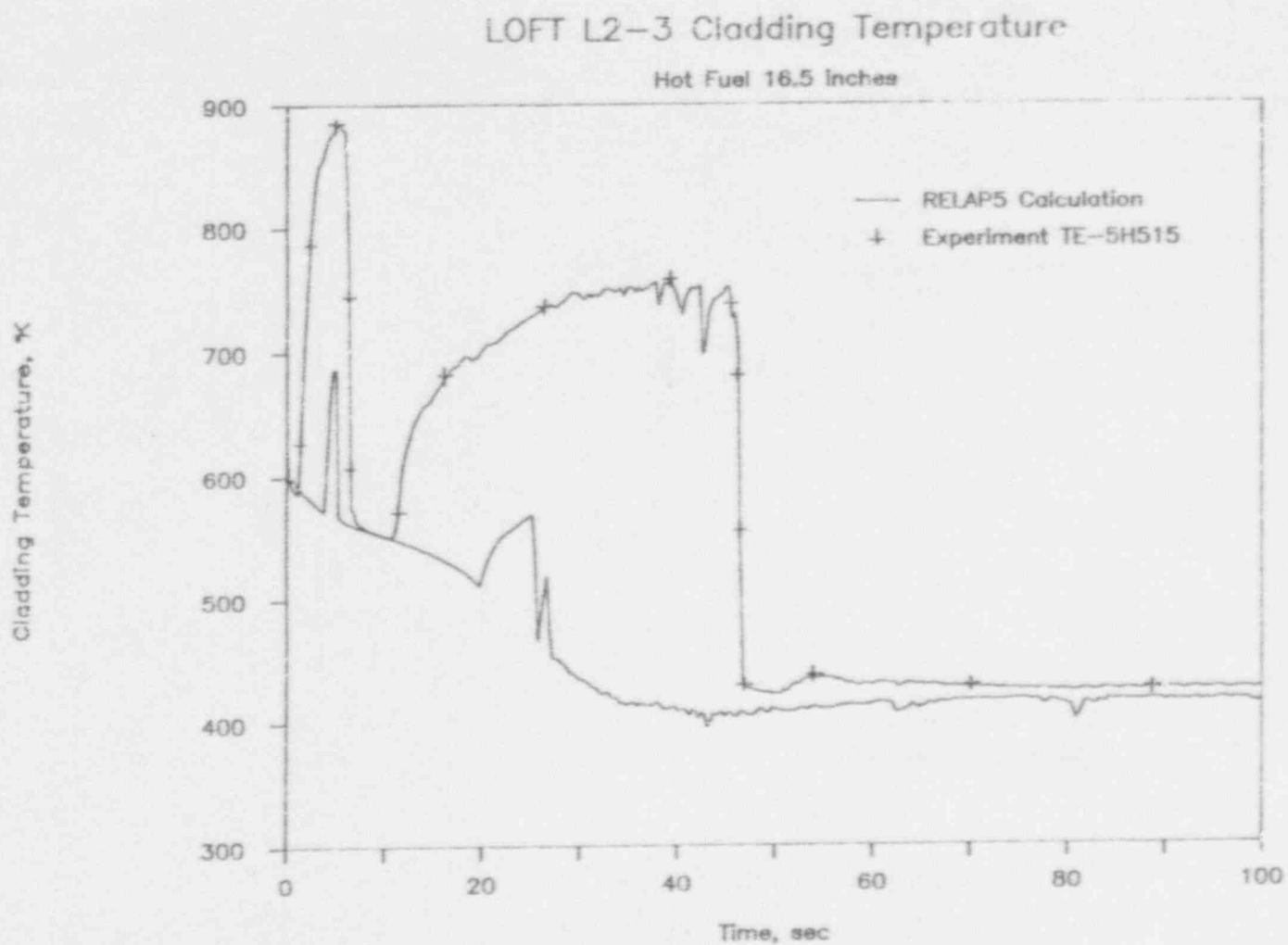


Fig.17 Comparison of cladding temperature at 16.5 inches of hot fuel between the base case calculation and the experiment

LOFT L2-3 Cladding Temperature

Hot Fuel 27.5 inch.

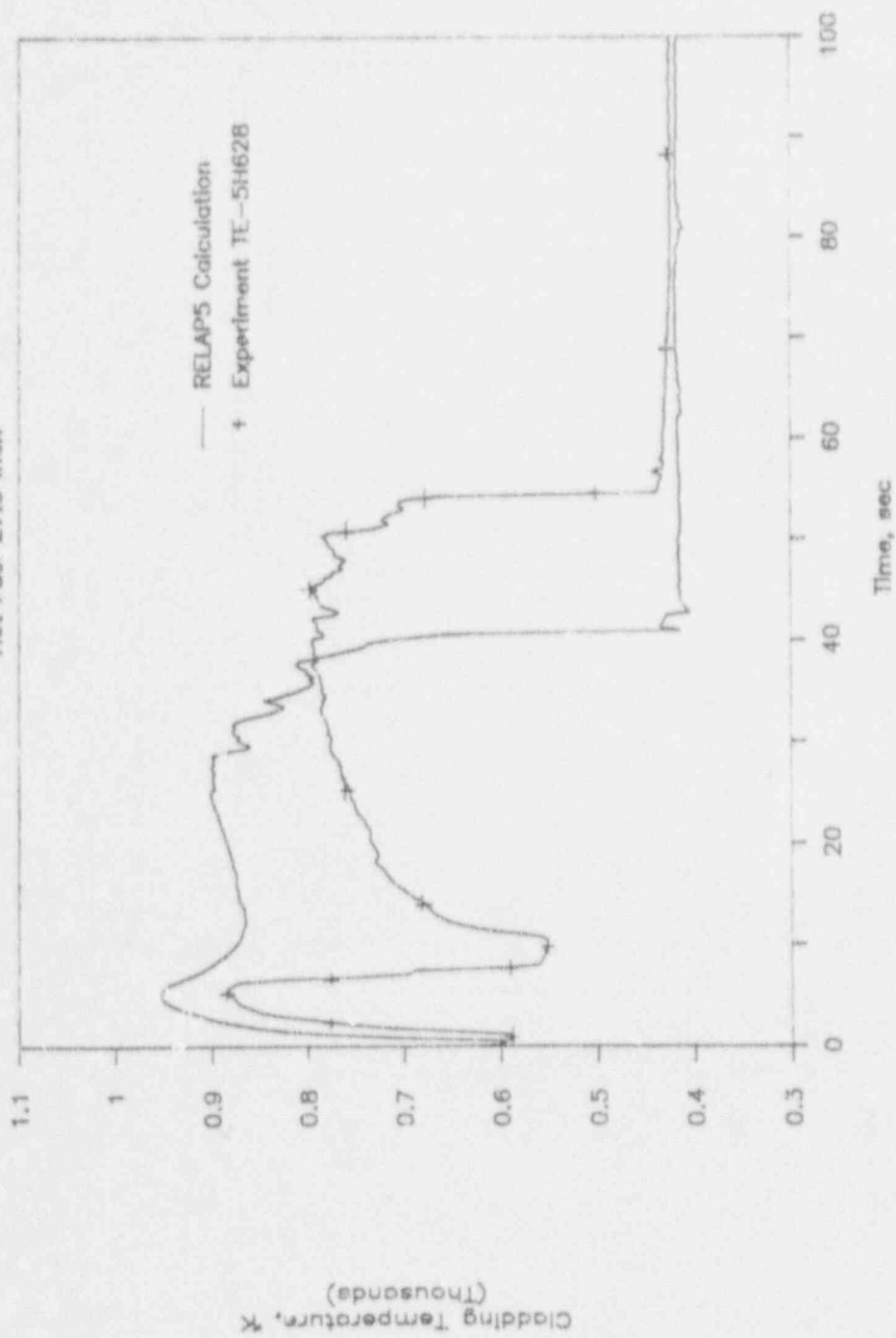


Fig. 18 Comparison of cladding temperature at 27.5 inches of hot fuel between the base case calculation and the experiment

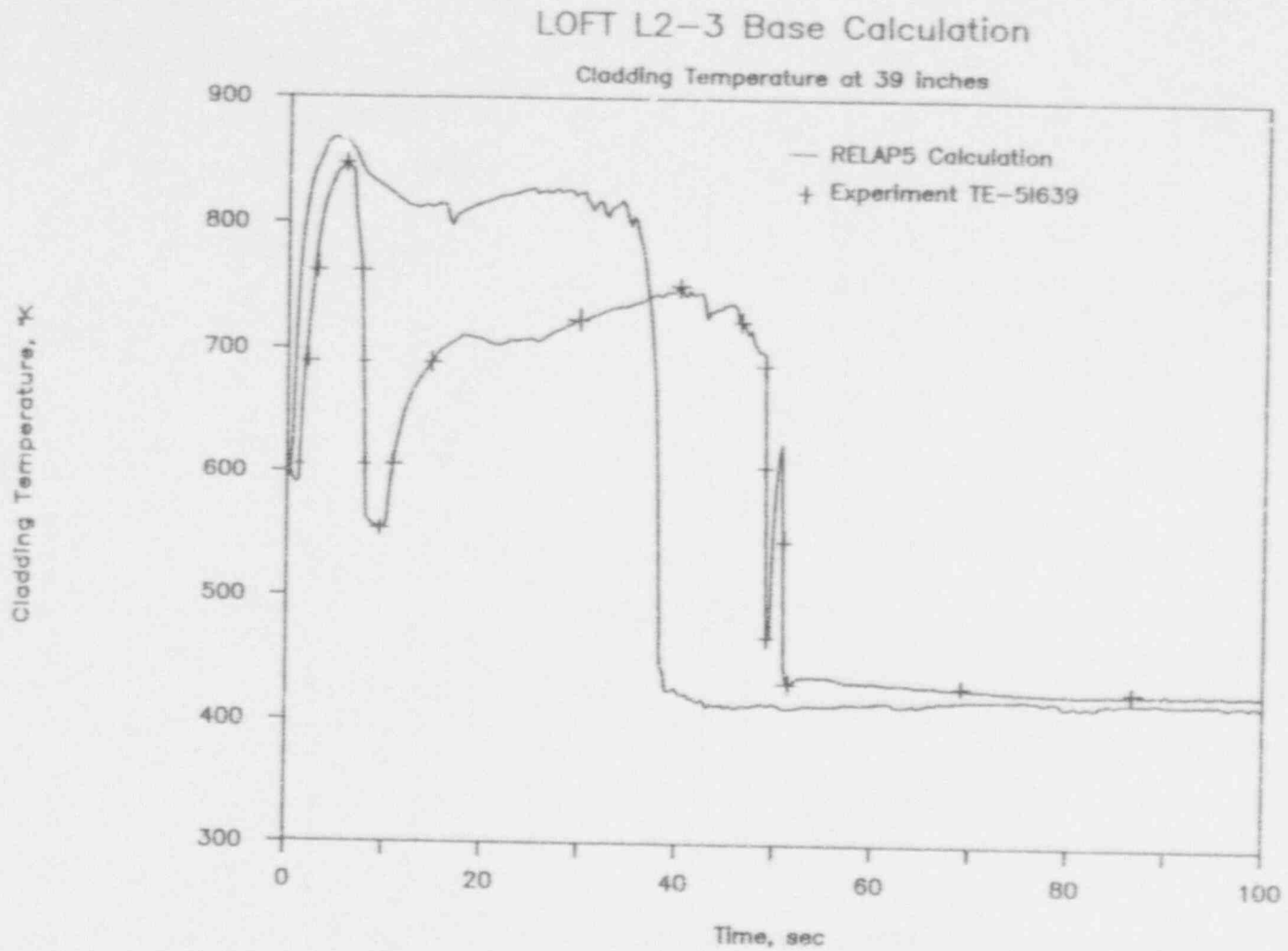


Fig.19 Comparison of cladding temperature at 39 inches of hot fuel between the base case calculation and the experiment

LOFT L2-3 Cladding Temperature

Hot Fuel 49 inches

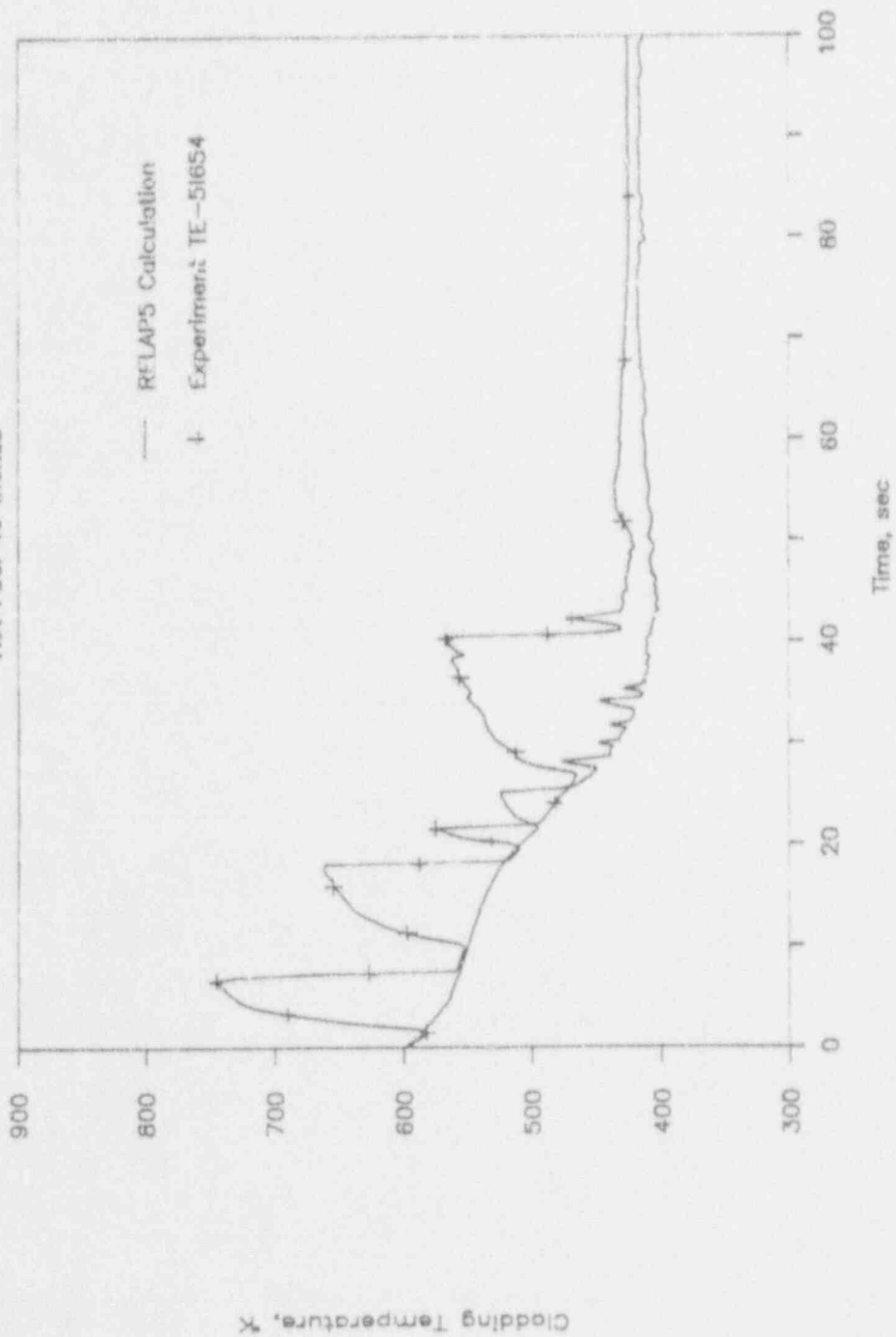


Fig. 20 Comparison of cladding temperature at 49.5 inches of hot fuel between the base case calculation and the experiment

LOFT L2-3 Base Calculation

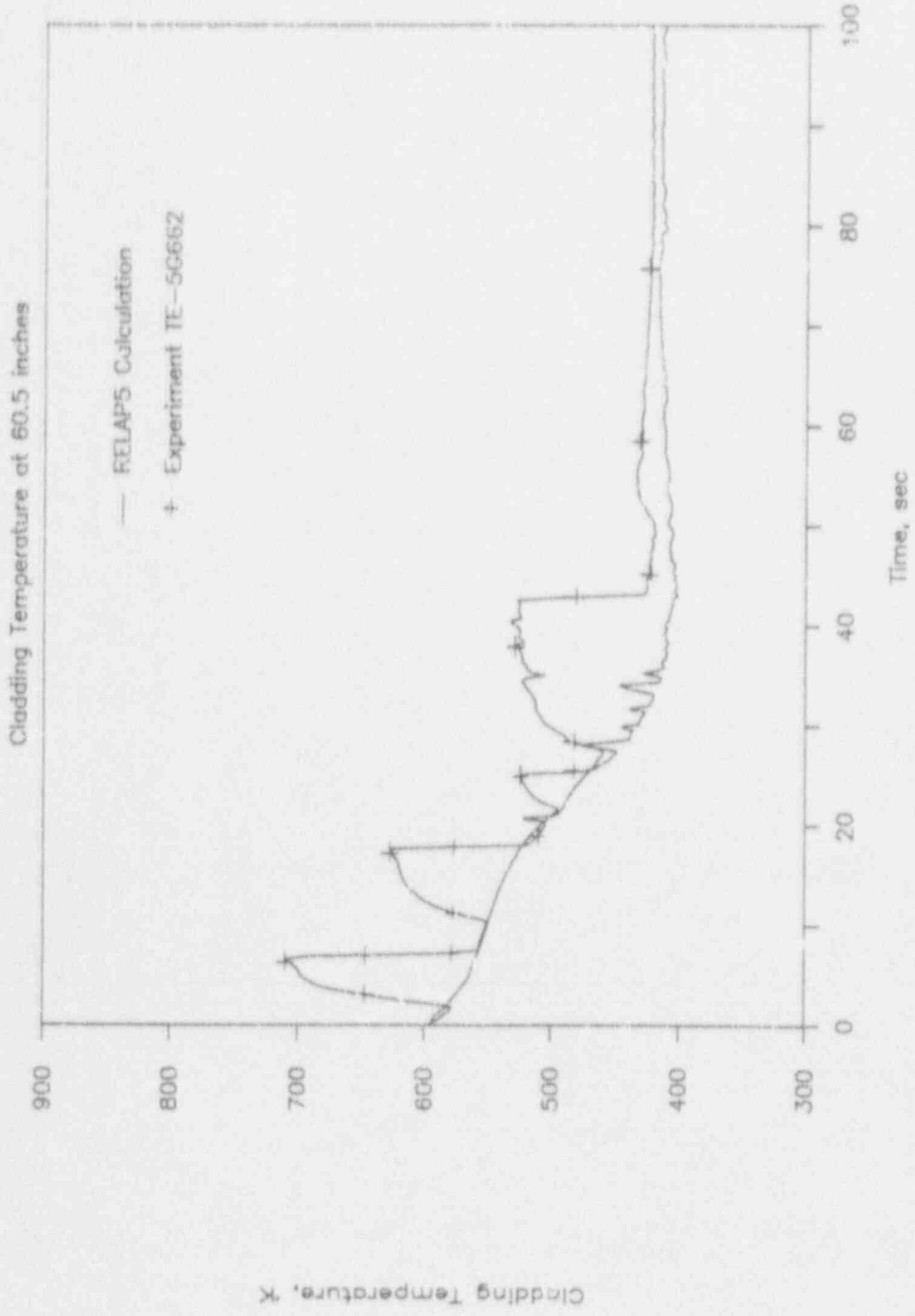


Fig.21 Comparison of cladding temperature at 60 inches of hot fuel between the base case calculation and the experiment

LOFT L2-3 Base Calculation

Hot Fuel Surface Heat Transfer Coef.

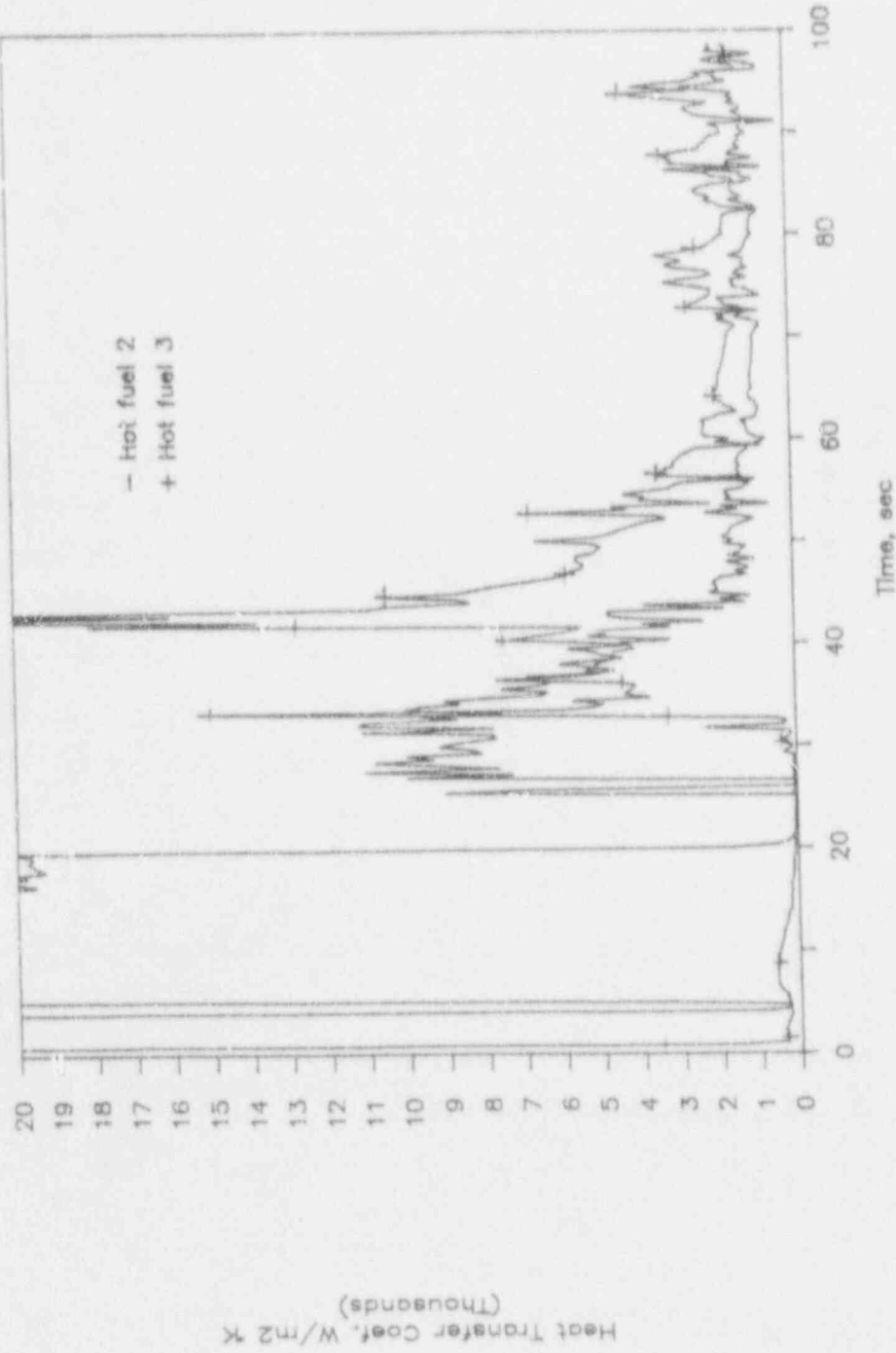


Fig. 22 Wall heat transfer coefficients calculated in the base case calculation at volume 2 and 3 of hot fuel

L2-3 Base Calculation

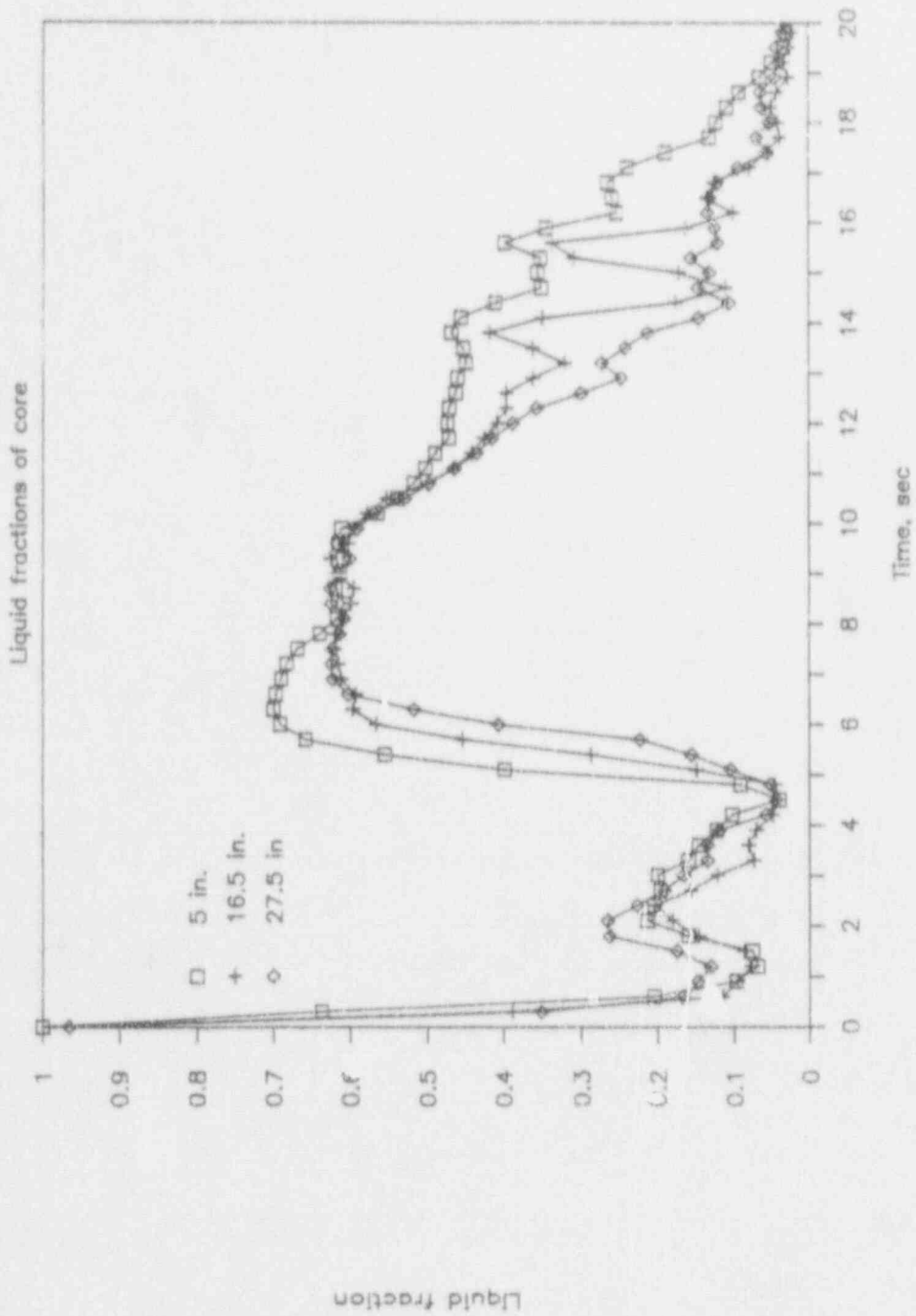


Fig. 23 Liquid fractions calculated in the base case calculation at volume 2 and 3 of hot fuel

LOFT L2-3 Base Calculation

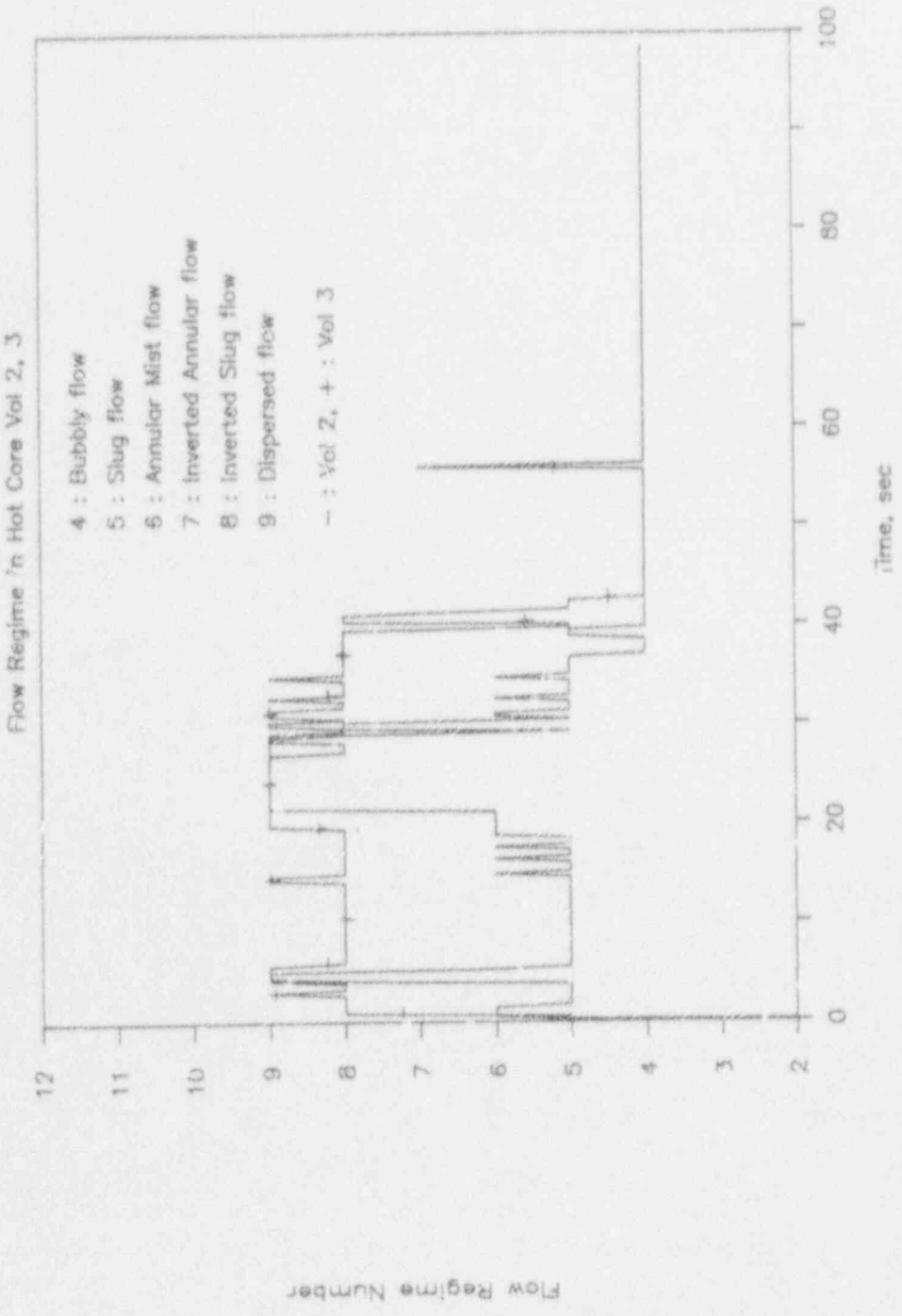


Fig. 24 Flow regimes predicted in the base case calculation at volume 2 and 3 of hot core channel

LOFT L2-3 Cladding Temperature

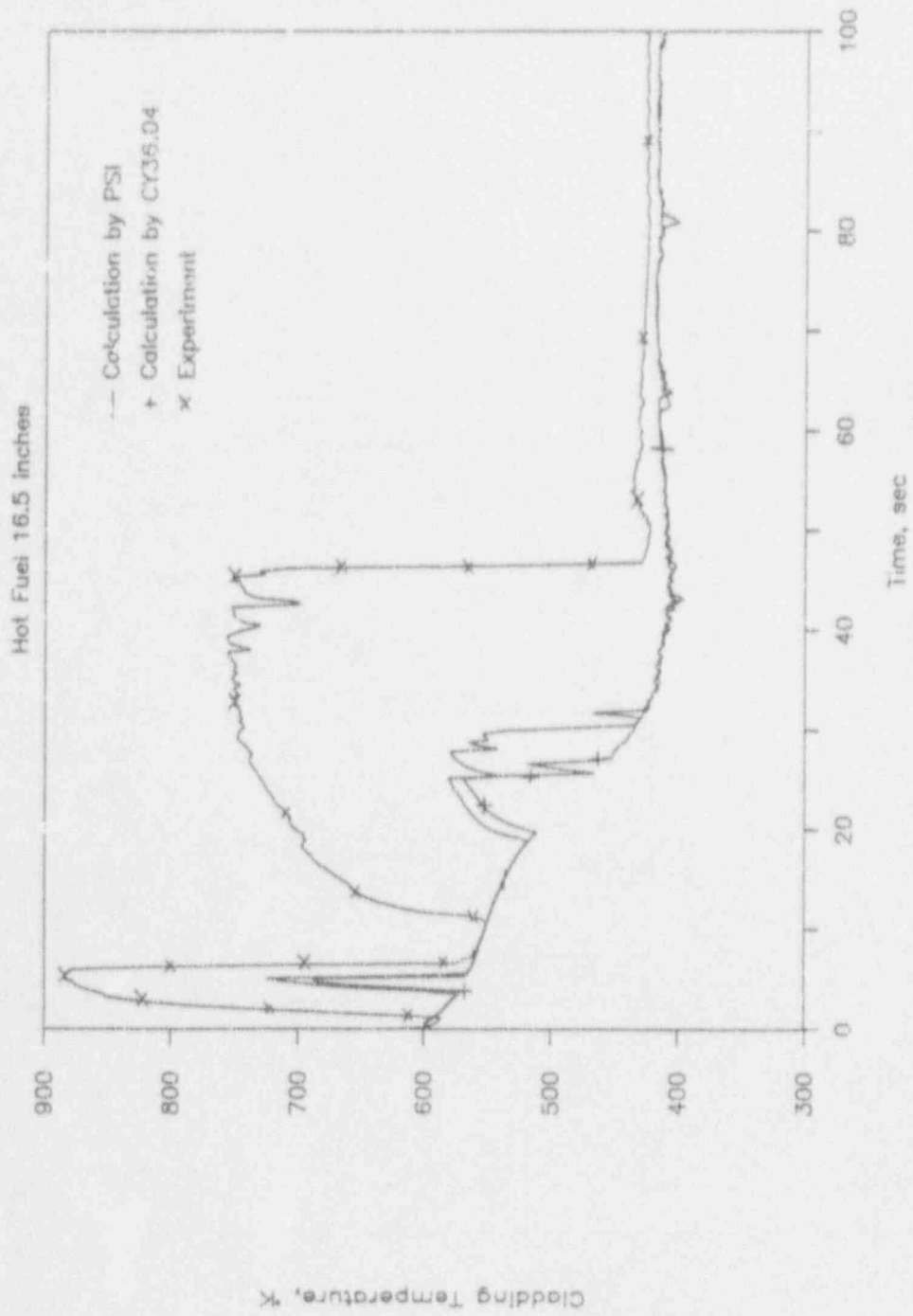


Fig. 25 Comparison of cladding temperature at 16.5 inches of hot fuel between the base case calculation and the sensitivity calculation

LOFT L2-3 Cladding Temperature

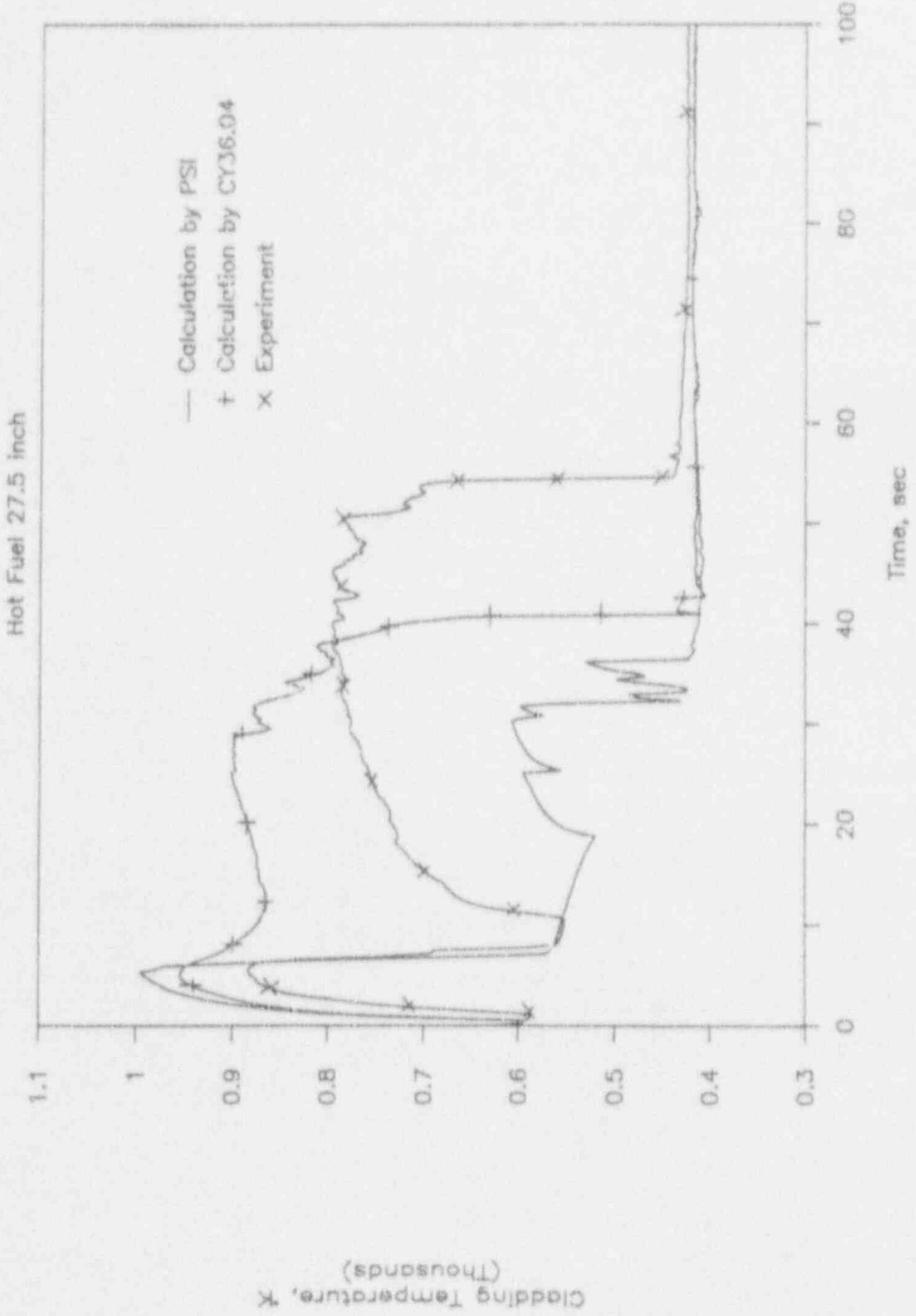


Fig. 26 Comparison of cladding temperature at 27.5 inches of hot fuel between the base case calculation and the sensitivity calculation

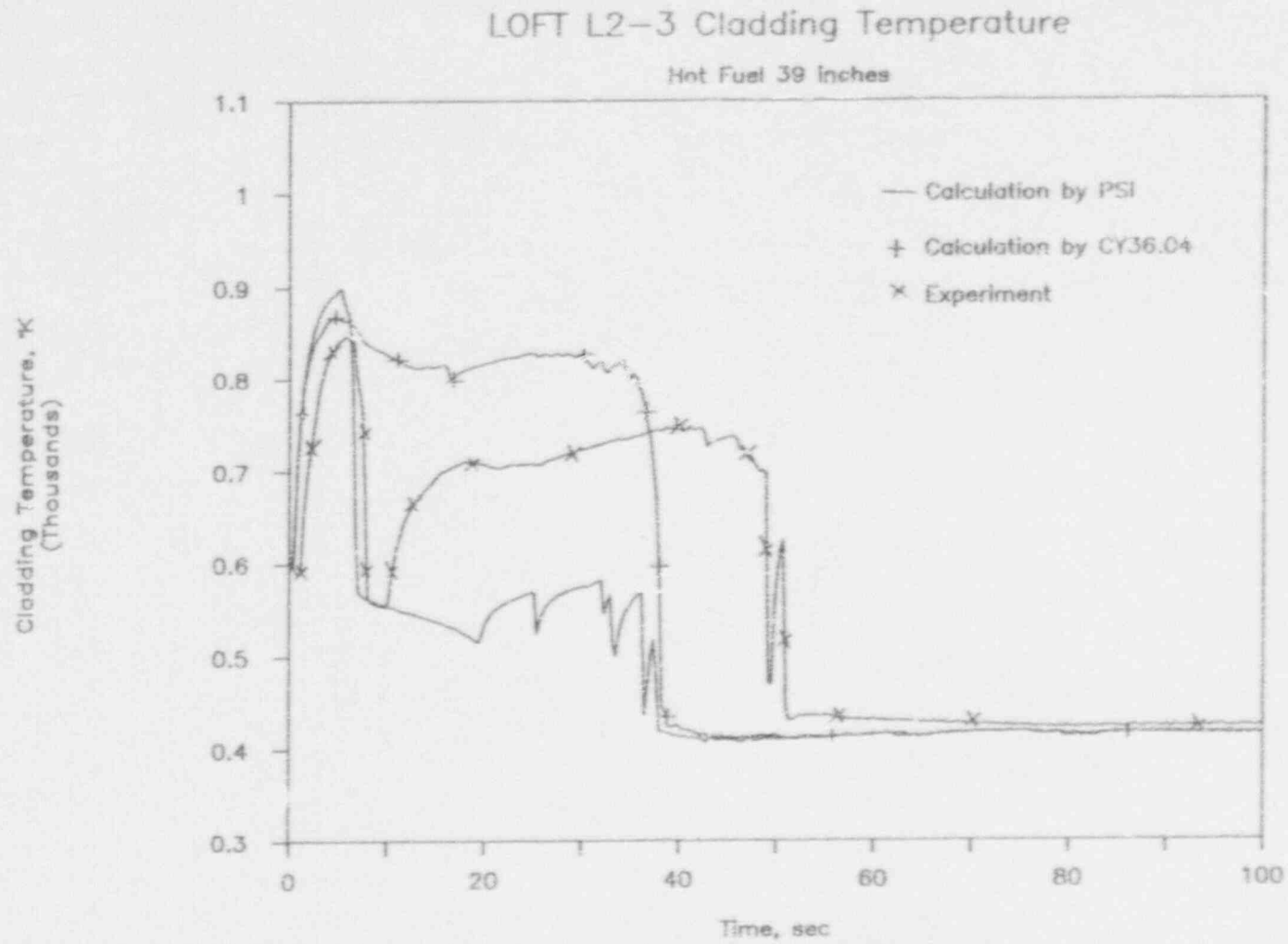


Fig.27 Comparison of cladding temperature at 39 inches of hot fuel between the base case calculation and the sensitivity calculation

LOFT L2-3 Cladding Temperature

Hot Fuel 49 inches

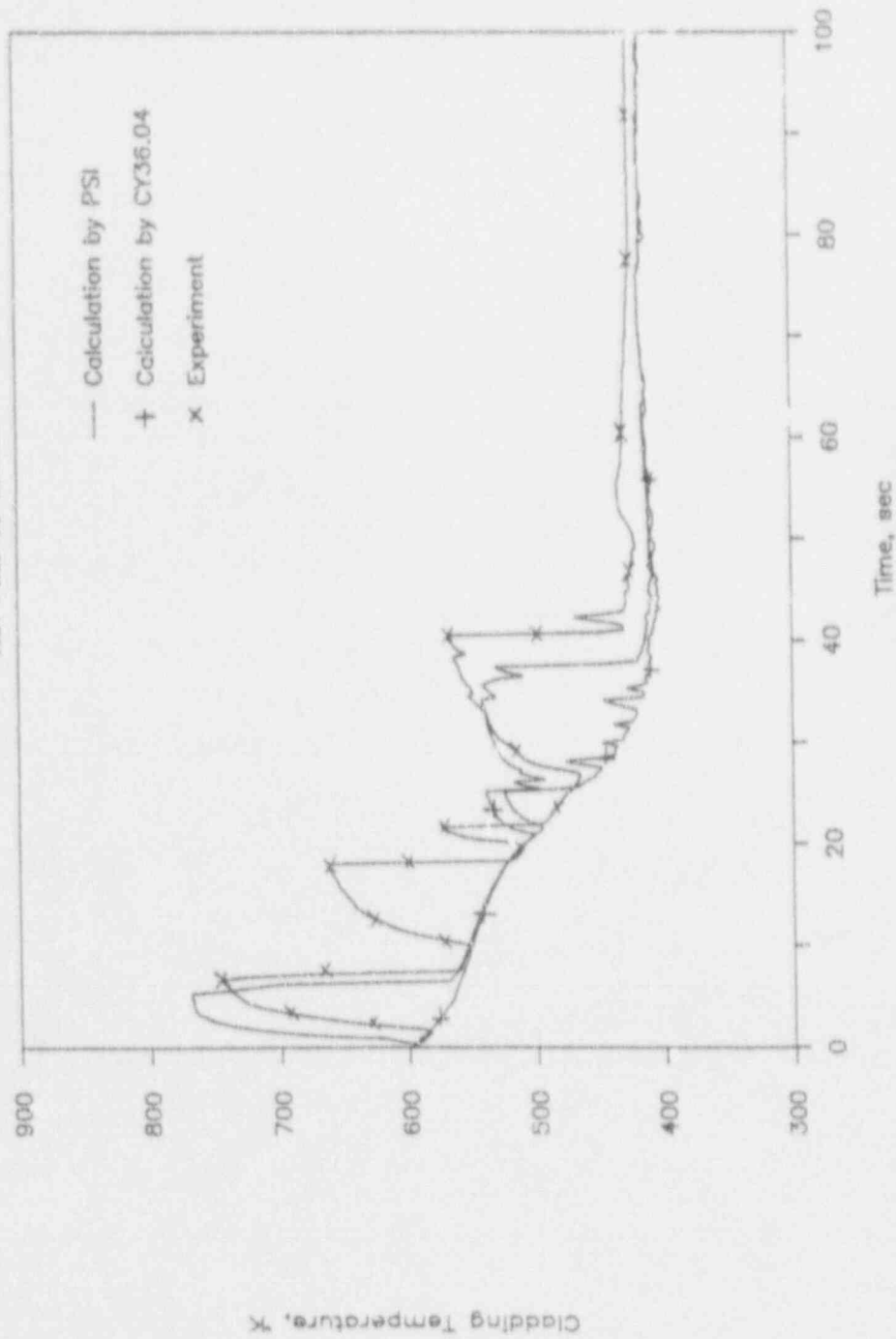


Fig. 28 Comparison of cladding temperature at 49.5 inches of hot fuel between the base case calculation and the sensitivity calculation

LOFT L2-3 Void Fraction Comparison

Void fraction at volume 5

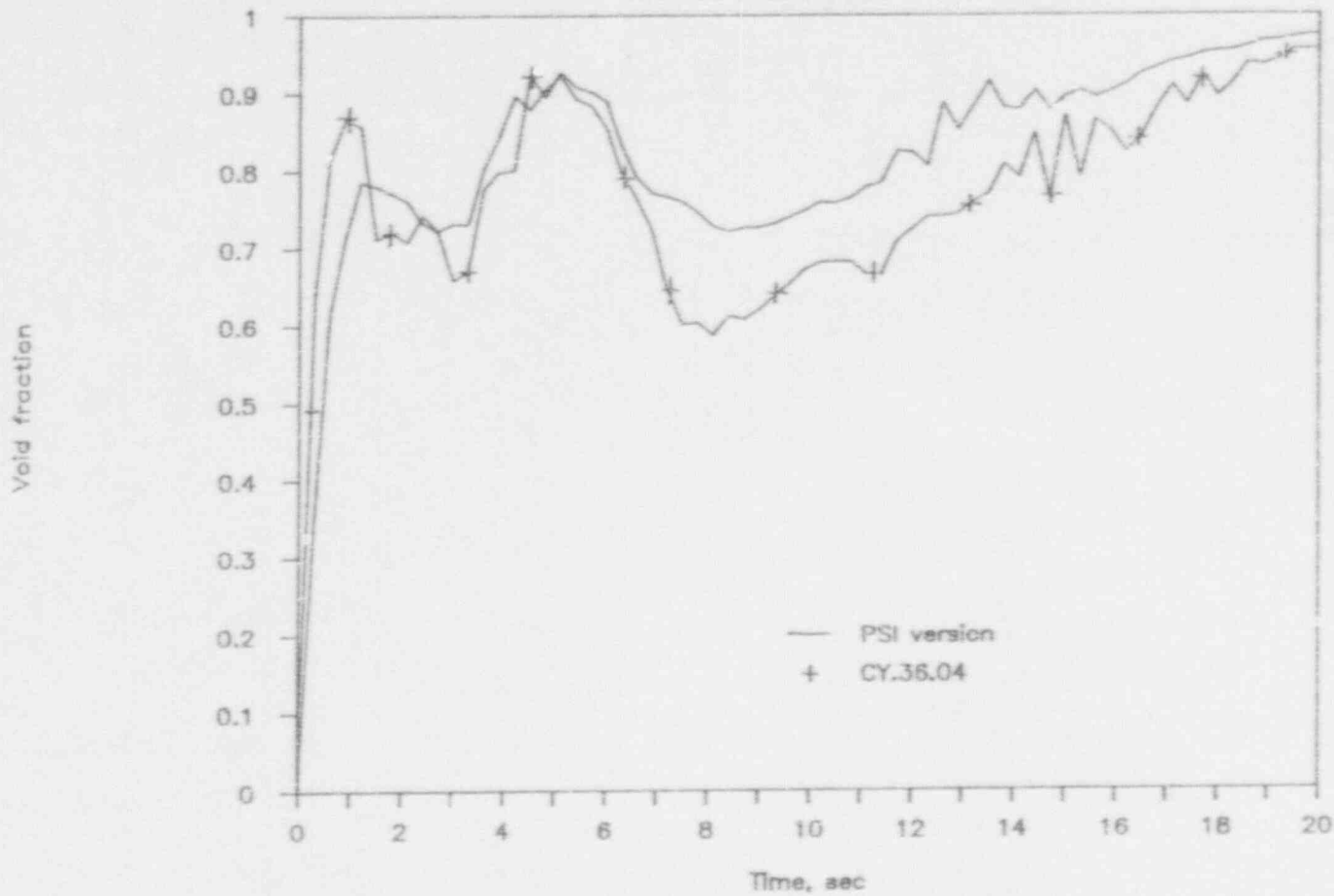


Fig. 29 Comparison of void fraction at volume 5 of hot core channel between the base case calculation and the sensitivity calculation

LOFT L2-3 Base Calculation

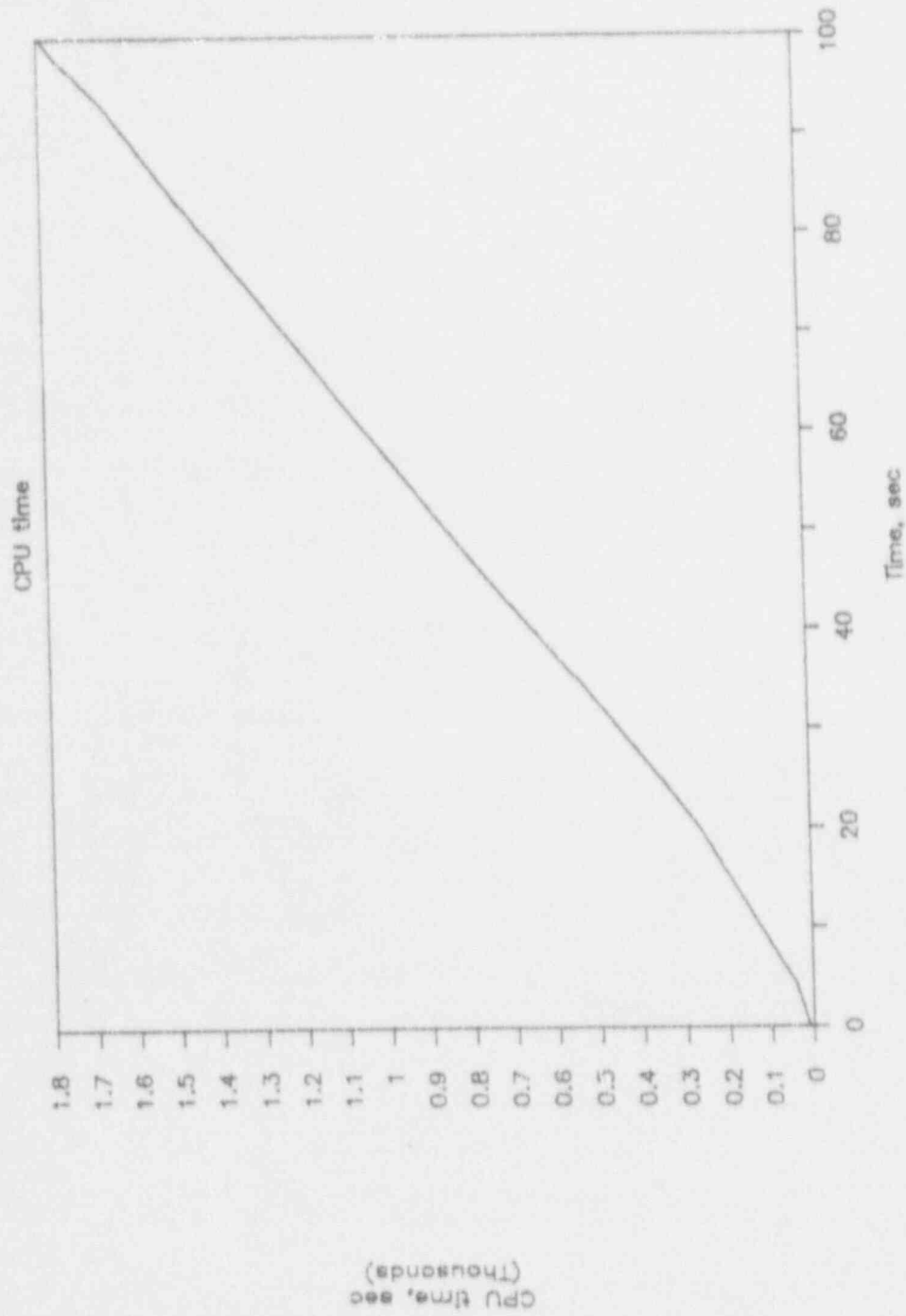


Fig.30 The required CPU time versus the advanced time in the base case calculation

LOFT L2-3 Base Calculation

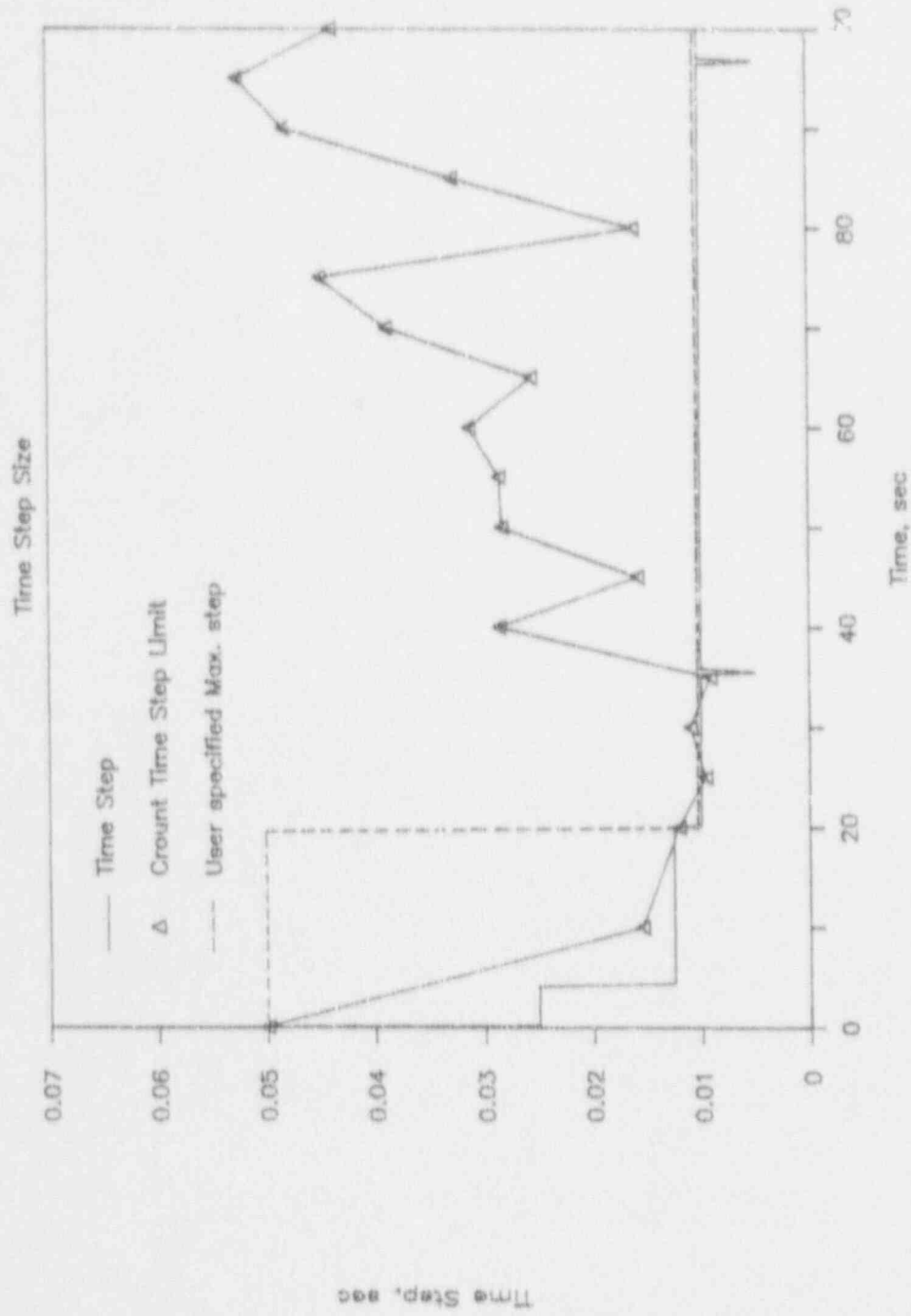


Fig.31 Time step size of base case calculation

Appendix A. Update List for RELAP5/MOD2 Cycle 36.04

APPENDIX A Update list for RELAP5/MODE Cycle 36.04

```

/JOB
RM364B,T300.
/USER
ATTACH,OLDPL=REL364S.
PURGE,RE364BS/NA.
PURGE,RE364BX/NA.
PURGE,RE364BL/NA.
* *****
* IMPORTANT !!
* THE UPDATE DIRECTIVE
* SHOULD HAVE *COMPILE DEFINE
* AS THE FIRST DIRECTIVE
* *****
UPDATE,N=RE364BS.
UPDATE,P=RE364BS,Q,C=R5SEG.
REPLACE,R5SEG.
RETURN,OLDPL.
*DEFINE,RE364BS.
RETURN,RE364BS.
ATTACH,ENVRLX=ENVR41X.
LIBRARY,ENVRLX.
SELECTA,COMPILE,COMP.
LIBRARY.
RETURN,ENVRLX.
REWIND,COMP.
FTN5,I=COMP,DO,ET,STATIC,OPT=2,ROUND,LO=N/A/R/S,L=0.
RETURN,COMP.
REWIND,LGO.
ATTACH,RELAP5I=REL364L.
GTR,RELAP5I,ADD.REL/*
*DEFINE,RELAP5O=RE364BL.
LIBEDIT,P=RELAP5O,I=0,B=ADD,LO=F,U,C.
LIBEDIT,P=RELAP5O,B=LGO,I=0,LO=F,U,C.
RETURN,NULL,LGO,RELAP5I.
RETURN,RLP5F1,RLP5F2.
ATTACH,ENVRL=ENVR41L.
FILE,RSTIN,RT=S,SBF=NO,USE,FO=SQ.
RFL,EC=200.
DEFINE,RE364BX.
SEGLOAD,I=R5SEG,B=RE364BX.
LDSET,LIB=RELAP5O/ENVRL.
LDSET,PRESETA=NGINDEF,ERR=NONE,MAP=SB.
LDSET,STAT=RSTIN.
LIBLOAD,ENVRL,$HDR=*.
LIBLOAD,FTN5LIB,$FERCAP.$,$RPVCAP.$,$FTNRP2.$,$Q2NTRY.$,
NOGO.
PERMIT,RE364BX,KA41202.
RETURN,RELAP5O,ENVRL,COMPILE.
SKIP,KKK.
EXIT.
ENDIF,KKK.
DAYFILE,KMRRDAY.
REPLACE,KMRRDAY.
/EOR
*COMPILE DEFINE
*ID CBD3604
*D DMK3601.484

```

```

*0 PLOTM,24
  ON1 FORMAT ('OF OTFL SCRACH FILE GENERATED.')
*COMPILE DEFINE,SEGBIR
*COMPILE RELAP5
*0 RJW3603,23
  DATA PTITLE,"RELAP5/2/3","6.04-NSC","REACTOR LO","SS OF COOL",
*/
*/   ENDIF
*/   *10 KWU01 ALREADY IMPLEMENTED IN RELAP5OLDPL3604C,
*/       WHICH IS USED AS BASIS
*/   */   CORRECTIONS OF INDEX IN SUBROUTINE RACCUM
*/   *1 RACCUM,618
*/       IELV=1
*/   *8 DMR3602,581
*/       I=IELV
*COMPILE DEFINE,SEGBIR,RACCUM
*10 KWU01
*1 RACCUM,618
  IELV=1
*8 DMR3602,581
  I=IELV
*/   */   END OF KWU-UPDATES TO CYCLE 3604
*COMPILE DEFINE,SEGBIR
*IDENT SK101
*/   THESE UPDATES ARE RECOMMENDED BY SKI TO BE
*/   IMPLEMENTED IN RELAP5/MOD2-36.04
*/   SOURCE:  LETTER FROM STUDEVIK (MR.SANDERVAAG)
*/           TO      KWU      (MR.GRUBER)
*/           1987-06-25
*/
*/   COMPILER RELAP5
*/
*COMPILE IHTCMP
*/
*/   FIX AN INDEXING ERROR IN IHTCMP
*/   ERROR CAUSED ROD PLENUM VOLUME FOR GAP-GAS PRESSURE CALCULATION
*/   TO BE INCORRECT, FOUND AND FIXED BY J.CARABER 70MAY87
*/   FIX ONLY CDC-VERSION CODING
*0 IHTCMP,1041
  L=(.NOT.MASK(43).AND.IHTPTR(1))+FILNDX(8)
*/
*/   UPDATE ROUTINE IREFLT TO ALLOW REFLOOD TO WORK
*/   HEAT STRUCTURE FILE GETS CHANGED ON RESTART (FOR
*/   EXAMPLE BY DELETING OR ALTERING SOME STRUCTURES)
*/   NOTE, HEAT STRS ASSOCIATED WITH REFLOOD CANNOT BE ALTERED
*/   ON RESTART AS IREFLT IS NOW PROGRAMMED
*/
*COMPILE IREFLT
*1 IREFLT,330
C   UPDATE THE GEOMETRY POINTER IN IGLRFL BITS 64-60 IN CASL 1.2
C   HEAT STRUCTURE FILE CHANGED ON RESTART.
  J=(.NOT.MASK(43).AND.IH)+IHT
  J=(.NOT.MASK(43).AND.IHTPTR(J))+IHT
  NCOLS=.NOT.MASK(43).AND.INXGOM(J)
  IGLRFL(I)=(MASK(43).AND.IGLRFL(I)).OR.NCOLS
*/
*/   END OF UPDATES SK101
*/
*/   /EOR
*COMPILE SEGBIR

```

Appendix B. A Base Case Input Deck for a Steady State Calculation


```

/JOB
L23TRAZ,T4000.
/USER
ATTACH,STH2XT,RE364BX.
FILE,RSTPLT,SBF=NO.
DEFINE,RSTPLT=L23RR.
RFL,CM=370000,EC=200.
REDUCE(-)
RE364BX.,*PL=50000.
/END

```

```
* LOFT 12-3 POST LAST ANALYSIS
```

```
-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
```

```
* L2-3 INITIAL CONDITIONS
```

```

*
*          POWER = 36.0 MW
*          PCS FLOW = 199.0 KG/S
*          TCOLD = 560.7 K
*          PCS PRESSURE = 15.06 MPA
*          S/G LEVEL = 1.19 M (45 IN)
*

```

```
-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
```

```
* BASE CASE CALCULATION
```

```

* TWO CORE FLOW CHANNEL MODELLING IMPLEMENTATION
* CORE : HOT CHANNEL(231), AVERAGE CHANNEL(230)
* HOT FUEL RODS(12311), AVERAGE FUEL RODS(12301)
* INTERMEDIATE FUEL RODS(12302)

```

```
-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
```

```
0000100 NEW STDY-ST
```

```
0000101 RUN
```

```
0000105 5.0 10.0
```

```
* TIME STEP CONTROL CARDS * REQUIRED
```

```
* END TIME MIN DT MAX DT OPTN MNR MJR RST
```

```
0000201 900.0 1.0-6 1.0 3 1 100 450
```

```
*****
```

```
* MINOR EDIT VARIABLES
```

```
-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
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* STEADY STATE PLOT REQUESTS
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-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
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0000301 P 250010000 * PRIMARY PRESSURE
0000302 P 530010000 * SECONDARY PRESSURE
0000303 TEMPF 250010000 * TE-1UP-001
0000304 TEMPF 185010000 * TE-PC-001
0000305 TEMPF 515010000 * SECONDARY COOLANT TEMPERATURE
0000306 MFLOWJ 540000000 * FT-P004-012 STEM FLOW
0000307 MFLOWJ 985000000 * LETDOWN SINK FLOW
0000308 MFLOWJ 993000000 * CHAGING SOURCE FLOW
0000309 CNTRLVAR 1 * LT-P004-042 S/G LEVEL
0000310 CNTRLVAR 2 * LT-P139-007 PZR LEVEL
0000311 MFLOWJ 566000000 * FT-P004-72-2 FEEDWATER FLOW
0000312 CNTRLVAR 910 * TCONTROL
0000313 MFLOWJ 130010000 * FT-P139-27-1 INT.L.HOT L. FLOW
0000314 P 420010000 * PZR PRESSURE PE-PC-005
0000315 VOIDG 500010000 * SEPARATOR VOID
0000316 TEMPF 100010000 * TE-PC-002 IHHL
0000317 TEMPF 114010000 * TE-SG-001 S/G INLET
0000318 TEMPF 116010000 * TE-SG-002 S/G OUTLET
0000319 TEMPF 300010000 * TE-BL-002 BLHL
0000320 TEMPF 335010000 * TE-BL-001 BLCL

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*-----1-----1-----1-----1-----1-----1-----
* PRESSURIZER CONNECTION TEE STEAM GENERATOR SIDE
*-----1-----1-----1-----1-----1-----1-----
1100000 "PZR T SGS "      BRANCH
1100001 1      0
1100101 0.0606063 0.9207292 0.0      0.0      0.0      0.0
1100102 4.0E-5      0.0      00
1100200 0      15005300. 1410030. 2459800. .00000000
1101101 110010000 112000000 0.0      0.15      0.15      0000
1101201 5.1146000 5.1146000 0.0
*-----1-----1-----1-----1-----1-----1-----
* HOT LEG PIPING
*-----1-----1-----1-----1-----1-----1-----
1120000 "HOT LEG PP"      PIPE
1120001 2
1120101 0.0      2
1120201 0.0      1
1120301 1.38893 1
1120302 0.707637 2
1120401 0.0796973 1
1120402 0.0579614 2
1120501 0.0      2
1120601 0.0      1
1120602 90.0      2
1120701 0.0      1
1120702 0.246447 2
1120801 4.0E-5      0.0      2
1120901 0.20      0.20      1
1121001 00      2
1121101 0000      1
1121201 0      15002900. 1410030. 2459870. .00000000 0.0      01
1121202 0      15005500. 1410030. 2455770. .00000000 0.0      02
1121300 0
1121301 5.1146000 5.1146000 0.0      01
*-----1-----1-----1-----1-----1-----1-----
* SG INLET PLENUM
*-----1-----1-----1-----1-----1-----1-----
1140000 "SG IN PLNM"      BRANCH
1140001 2      0
1140101 0.0      0.629795 0.33532 0.0      90.0      0.512756
1140102 4.E-5      0.0102 00
1140200 0      14987200. 1410020. 2460000. .00000000
1141101 112010000 114000000 0.0512 0.0      0.0      0100
1142101 114010000 115000000 0.0      0.0      0.0      0100
1141201 3.5832000 3.5832000 0.0
1142201 1.9414000 1.9414000 0.0
*-----1-----1-----1-----1-----1-----1-----
* SG U-TUBES
*-----1-----1-----1-----1-----1-----1-----
1150000 "SG TUBES "      PIPE
1150001 8
1150101 0.0      8
1150201 0.151171 7
1150301 0.902      1
1150302 0.6096      3
1150303 0.462908 5
1150304 0.6096      7
1150305 0.902      5
1150401 0.136356 1
1150402 0.0921538 3
1150403 0.0699783 5

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1150404	0.0921538	7						
1150405	0.136356	8						
1150501	0.0	8						
1150601	90.0	4						
1150602	-90.0	8						
1150701	0.902	1						
1150702	0.6096	3						
1150703	0.299572	4						
1150704	-0.299572	5						
1150705	-0.6096	7						
1150706	-0.902	8						
1150801	1.27-7	0.01022	8					
1150901	0.0	0.0	7					
1151001	00	8						
1151101	0000	7						
1151201	0	14979600.	1367230.	2460010.0	.00000000	0.0		01
1151202	0	14972800.	1333400.	2460020.0	.00000000	0.0		02
1151203	0	14967300.	1306120.	2460030.0	.00000000	0.0		03
1151204	0	14962900.	1288520.	2460040.0	.00000000	0.0		04
1151205	0	14962000.	1273520.	2460050.0	.00000000	0.0		05
1151206	0	14964300.	1257470.	2460060.0	.00000000	0.0		06
1151207	0	14967600.	1244800.	2460030.0	.00000000	0.0		07
1151208	0	14971800.	1233820.	2460020.0	.00000000	0.0		08
1151300	0							
1151301	1.8921000	1.8921000	0.0	01				
1151302	1.8565000	1.8565000	0.0	02				
1151303	1.8299000	1.8299000	0.0	03				
1151304	1.8134000	1.8134000	0.0	04				
1151305	1.7997000	1.7997000	0.0	05				
1151306	1.7856000	1.7856000	0.0	06				
1151307	1.7746000	1.7746000	0.0	07				
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
* SG OUTLET PLENUM								
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
1160000	"SG OUT PLN"	BRANCH						
1160001	2	0						
1160101	0.0	0.629795	0.33532	0.0	-90.0	-0.512756		
1160102	4.E-5	0.0102	00					
1160200	0	14976400.	1233810.	2460100.	.00000000			
1161101	115010000	116000000	0.0	0.0	0.0	0100		
1162101	116010000	118000000	0.0512	0.0	0.0	0100		
1161201	1.7656000	1.7656000	0.0					
1162201	3.2740000	3.2740000	0.0					
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
* PUMP SUCTION PIPING								
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
1180000	"PMP SUC PP"	PIPE						
1180001	3							
1180101	0.0	3						
1180201	0.0	2						
1180301	0.546638	1						
1180302	0.688596	2						
1180303	0.558577	3						
1180401	0.0445625	1						
1180402	0.0445137	2						
1180403	0.0354278	3						
1180501	0.0	3						
1180601	-90.0	3						
1180701	-0.498052	1						
1180702	-0.688596	2						
1180703	-0.355604	3						

1180801	4.E-5	0.0	3					
1180901	0.083	0.083	1					
1180902	0.104	0.104	2					
1181001	00	3						
1181101	0000	2						
1181201	0	14965800.	1233810.	2460030.0	.00000000	0.0		01
1181202	0	14967700.	1233810.	2460033.0	.00000000	0.0		02
1181203	0	14970500.	1233810.	2460035.0	.00000000	0.0		03
1181300	0							
1181301	4.1288000	4.1288000	0.0				01	
1181302	4.2081000	4.2081000	0.0				02	
*-----1-----1-----1-----1-----1-----1-----1-----								
* PUMP SUCTION TEE								
*-----1-----1-----1-----1-----1-----1-----1-----								
1200000	"PMP SCT T"		BRANCH					
1200001	3	0						
1200101	0.0	0.759614	0.0487901	0.0	0.0	0.0		
1200102	4.0E-5	0.0	00					
1200200	0	14974000.	1233810.	2460020.	.00000000			
1201101	118010000	120000000	0.063427	0.0	0.0	0000		
1202101	120010000	125000000	0.063427	1.075	1.25	0000		
1203101	120010000	155000000	0.063427	1.075	1.25	0000		
1201201	4.2080000	4.2080000	0.0					
1202201	1.9967000	1.9967000	0.0					
1203201	2.2113000	2.2113000	0.0					
*-----1-----1-----1-----1-----1-----1-----1-----								
* PUMP1 SUCTION TEE OUTLET								
*-----1-----1-----1-----1-----1-----1-----1-----								
1250000	"PMP1 SCT T"		BRANCH					
1250001	1	0						
1250101	0.0	1.00308	0.0640548	0.0	90.0	0.520704		
1250102	4.0E-5	0.0	00					
1250200	0	14974500.	1233810.	2460022.	.00000000			
1251101	125010000	130000000	0.0	0.13	0.13	0000		
1251201	3.2631000	3.2631000	0.0					
*-----1-----1-----1-----1-----1-----1-----1-----								
* PUMP 1 INLET								
*-----1-----1-----1-----1-----1-----1-----1-----								
1300000	"PMP1 INLET"		SNGLVOL					
1300101	0.0	0.457201	0.0177444	0.0	90.0	0.457201		
1300102	4.0E-5	0.0	00					
1300200	0	14968300.	1233810.	2460030.	.00000000			
*-----1-----1-----1-----1-----1-----1-----1-----								
* PRIMARY COOLANT PUMP 1								
*-----1-----1-----1-----1-----1-----1-----1-----								
1350000	"PCPUMP1"		PUMP					
1350101	0.0	0.4572	0.0991	0.0	90.0	0.317900		
1350102	0							
1350108	130010000	0.0	0.017	0.017	0000			
1350109	140000000	0.0	0.05	0.05	0000			
1350200	0	15010900.	1233820.	2459500.	.00000000			
1350201	0	3.2631000	3.2631000	0.0				
1350202	0	3.4591000	3.4591000	0.0				
1350301	0	0	0	-1	-1	0	0	
1350302	369.00000	.35501355	.31550000	96.000000	500.60000	1.4310000		
1350303	613.60000	.00000000	207.43300	.04440000	19.598700	.00000000		
1350310	0.0	0.0	0.0					
*-----1-----1-----1-----1-----1-----1-----1-----								
* PUMP 1 OUTLET PUMP SIDE								
*-----1-----1-----1-----1-----1-----1-----1-----								
1400000	"PMP1 OUT P"		SNGLVOL					

1400101	0.0	0.502185	0.0183849	0.0	0.0	0.0
1400102	4.0E-5	0.0	00			
1400200	0	15046700.	1233820.	2459000.	.00000000	
*-----1-----1-----1-----1-----1-----1-----1-----						
* PUMP1 OUTLET PIPE TEE SIDE						
*-----1-----1-----1-----1-----1-----1-----1-----						
1450000	"PMP1 OUT T"		BRANCH			
1450001	2	0				
1450101	0.0	1.40843	0.0633861	0.0	0.0	0.0
1450102	4.0E-5	0.0	00			
1450200	0	15048400.	1233820.	2458800.	.00000600	
1451101	140010000	145000000	0.0	0.0	0.0	0000
1452101	145010000	150000000	0.0	0.57456	0.050347	0000
1451201	3.4589000	3.4589000	0.0			
1452201	2.8137000	2.8137000	0.0			
*-----1-----1-----1-----1-----1-----1-----1-----						
* PUMP OUTLET TEE						
*-----1-----1-----1-----1-----1-----1-----1-----						
1500000	"PMP OUT T "		BRANCH			
1500001	1	0				
1500101	0.0	0.496511	0.0316011	0.0	0.0	0.0
1500102	4.0E-5	0.0	00			
1500200	0	15042300.	1233820.	2458700.	.00000000	
1501101	150010000	175000000	0.063427	0.0	0.0	0000
1501201	4.2075000	4.2075000	0.0			
*-----1-----1-----1-----1-----1-----1-----1-----						
* PUMP 2 SUCTION TEE OUTLET						
*-----1-----1-----1-----1-----1-----1-----1-----						
1550000	"PMP2 SCT T"		BRANCH			
1550001	1	0				
1550101	0.0	1.00308	0.0640548	0.0	90.0	0.520704
1550102	4.0E-5	0.0	00			
1550200	0	14973600.	1233810.	2460020.	.00000000	
1551101	155010000	160000000	0.0	0.13	0.13	0000
1551201	3.6137000	3.6137000	0.0			
*-----1-----1-----1-----1-----1-----1-----1-----						
* PUMP 2 INLET PIPE						
*-----1-----1-----1-----1-----1-----1-----1-----						
1600000	"PMP2 INLET"		SINGLVOL			
1600101	0.0	0.457201	0.0177444	0.0	90.0	0.457201
1600102	4.0E-5	0.0	00			
1600200	0	14966800.	1233810.	2460030.	.00000000	
*-----1-----1-----1-----1-----1-----1-----1-----						
* PRIMARY COOLANT PUMP 2						
*-----1-----1-----1-----1-----1-----1-----1-----						
1650000	"PCPUMP2 "		PUMP			
1650101	0.0	0.514	0.0991	0.0	90.0	0.317900
1650102	0					
1650108	160010000	0.0	0.017	0.017	0000	
1650109	170000000	0.0	0.1	0.1	0000	
1650200	0	15010900.	1233820.	2459500.	.00000000	
1650201	0	3.6138000	3.6138000	0.0		
1650202	0	3.7364000	3.7364000	0.0		
1650301	135 135 135		-1	-1	0	0
1650302	369.00000	.35501355	.31550000	96.000000	500.60000	1.4310000
1650303	613.60000	.00000000	207.43300	.04440000	19.598700	.00000000
1650310	0.0	0.0	0.0			
*-----1-----1-----1-----1-----1-----1-----1-----						
* PUMP 2 OUTLET						
*-----1-----1-----1-----1-----1-----1-----1-----						
1700000	"PMP2 OUT T"		BRANCH			

7000401	0.0	1						
7000501	0.0	1						
7000601	90.0	1						
7000801	3.81-6	0.172	1					
7001001	00	1						
7001201	0	15028400.	1233830.	2459250.	.00000600	0.0		01
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* JUNCTION - UPPER TO LOWER INLET ANNULUS INTACT SIDE								
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
7010000	"INANMUINT"		SNGLJUN					
7010101	730000000	700000000	0.129467	0.0000	0.0000	0100		
7010201	0	.34062000	.34062000	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* INLET ANNULUS MIDDLE VOLUME INTACT SIDE								
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
7300000	"INANMIDINT"		ANNULUS					
7300001	1							
7300101	0.1308530	1						
7300301	0.2851823	1						
7300401	0.0	1						
7300501	0.0	1						
7300601	-90.0	1						
7300801	3.81-6	0.172	1					
7301001	00	1						
7301201	0	15028400.	1233830.	2459250.	0.0	0.0		01
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* JUNCTION - MIDDLE TO LOWER INLET ANNULUS INTACT SIDE								
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
7310000	"INANMLINT"		SNGLJUN					
7310101	730010000	702000000	0.0709408	0.0	0.0	0100		
7310201	0	1.5959	1.5959	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* INLET ANNULUS LOWER VOLUME INTACT SIDE								
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
7020000	"INANLWINT"		ANNULUS					
7020001	1							
7020101	0.1464354	1						
7020301	0.2525361	1						
7020401	0.0	1						
7020501	0.0	1						
7020601	-90.0	1						
7020801	3.81-6	0.172	1					
7021001	00	1						
7021201	0	15030600.	1233830.	2459300.	.00000000	0.0		01
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* JUNCTION - INLET ANNULUS TO DOWNCOMER INTACT SIDE								
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
7030000	"INAN2DCINT"		SNGLJUN					
7030101	702010000	704000000	0.0709408	0.0000	0.0000	0100		
7030201	0	1.5959000	1.5359000	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* DOWNCOMER UPPER VOLUME INTACT SIDE								
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
7040000	"DNCRUPINT"		ANNULUS					
7040001	1							
7040101	0.0	1						
7040301	1.5200561	1						
7040401	0.1581866	1						
7040501	0.0	1						
7040601	-90.0	1						
7040801	3.81-6	0.102	1					

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7041001 00      1
7041201 0       15036100. 1233810. 2459350. .00000000 0.0      01
*-----1-----1-----1-----1-----1-----1-----
* JUNCTION - UPPER TO MIDDLE DOWNCOMER INTACT SIDE
*-----1-----1-----1-----1-----1-----1-----
7050000 "UPR2MIDINT"     SNGLJUN
7050101 704010000 706000000 0.0709408 0.0000 0.0000 0100
7050201 0       1.5106000 1.5106000 0.0
*-----1-----1-----1-----1-----1-----1-----
* DOWNCOMER MIDDLE VOLUME INTACT SIDE
*-----1-----1-----1-----1-----1-----1-----
7060000 "DNCRMIDINT"     ANNULUS
7060001 1
7060101 0.0      1
7060301 1.2616333 1
7060401 0.1217000 1
7060501 0.0      1
7060601 -90.0     1
7060801 3.81-6   0.102   1
7061001 00      1
7061201 0       15045800. 1233800. 2459500. .00000000 0.0      01
*-----1-----1-----1-----1-----1-----1-----
* JUNCTION - MIDDLE TO LOWER DOWNCOMER INTACT SIDE
*-----1-----1-----1-----1-----1-----1-----
7070000 "MID2LWRINT"     SNGLJUN
7070101 706010000 708000000 0.0709408 0.0000 0.0000 0100
7070201 0       1.4821000 1.4821000 0.0
*-----1-----1-----1-----1-----1-----1-----
* DOWNCOMER LOWER VOLUME INTACT SIDE
*-----1-----1-----1-----1-----1-----1-----
7080000 "DNCRLWRINT"     ANNULUS
7080001 1
7080101 0.0      1
7080301 1.0792591 1
7080401 0.0986806 1
7080501 0.0      1
7080601 -90.0     1
7080801 3.81-6   0.102   1
7081001 00      1
7081201 0       15054000. 1233790. 2458600. .00000000 0.0      01
*-----1-----1-----1-----1-----1-----1-----
* JUNCTION - LOWER DOWNCOMER TO LOWER PLENUM INTACT SIDE
*-----1-----1-----1-----1-----1-----1-----
7090000 "LDC2LPINT"     SNGLJUN
7090101 706010000 215000000 0.0709408 0.0000 0.0000 0100
7090201 0       1.4104000 1.4104000 0.0
*-----1-----1-----1-----1-----1-----1-----
* INLET ANNULUS UPPER VOLUME BROKEN SIDE
*-----1-----1-----1-----1-----1-----1-----
7100000 "JNANUPRBKN"     ANNULUS
7100001 1
7100101 0.1308530 1
7100301 0.1876129 1
7100401 0.0      1
7100501 0.0      1
7100601 90.0     1
7100801 3.81-6   0.172   1
7101001 00      1
7101201 0       15027200. 1233830. 2459250. .00000000 0.0      01
*-----1-----1-----1-----1-----1-----1-----
* JUNCTION - MIDDLE TO UPPER INLET ANNULUS BROKEN SIDE

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*-----1-----1-----1-----1-----1-----1-----1-----1-----							
7110000	"INANMUBKN"		SNGLJUN				
7110101	740000000	710000000	0.129467	0.0000	0.0000	0100	
7110201	0	-.2873200	-.2873200	0.0			
*-----1-----1-----1-----1-----1-----1-----1-----1-----							
* INLET ANNULUS MIDDLE VOLUME BROKEN SIDE							
*-----1-----1-----1-----1-----1-----1-----1-----1-----							
7400000	"INANMIDBKN"		ANNULUS				
7400001	1						
7400101	0.1308530	1					
7400301	0.2851823	1					
7400401	0.0	1					
7400501	0.0	1					
7400601	-90.0	1					
7400801	3.81-6	0.172	1				
7401001	00	1					
7401201	0	15028400.	1233830.	2459250	0.0	0.0	01
*-----1-----1-----1-----1-----1-----1-----1-----1-----							
* JUNCTION - MIDDLE TO LOWER INLET ANNULUS BROKEN SIDE							
*-----1-----1-----1-----1-----1-----1-----1-----1-----							
7410000	"INANMLBKN"		SNGLJUN				
7410101	740010000	712000000	0.0709408	0.0	0.0	0100	
7410201	0	.86411	.86411	0.0			
*-----1-----1-----1-----1-----1-----1-----1-----1-----							
* INLET ANNULUS LOWER VOLUME BROKEN SIDE							
*-----1-----1-----1-----1-----1-----1-----1-----1-----							
7120000	"INANLWBKN"		ANNULUS				
7120001	1						
7120101	0.145454	1					
7120301	0.252351	1					
7120401	0.0	1					
7120501	0.0	1					
7120601	-90.0	1					
7120801	3.81-6	0.172	1				
7121001	00	1					
7121201	0	15029700.	1233820.	2459200.	.00000000	0.0	01
*-----1-----1-----1-----1-----1-----1-----1-----1-----							
* JUNCTION - INLET ANNULUS TO DOWNCOMER BROKEN SIDE							
*-----1-----1-----1-----1-----1-----1-----1-----1-----							
7130000	"INANLWBKN"		SNGLJUN				
7130101	712010000	714000000	0.0709408	0.0000	0.0000	0100	
7130201	0	.86411000	.86411000	0.0			
*-----1-----1-----1-----1-----1-----1-----1-----1-----							
* DOWNCOMER UPPER VOLUME BROKEN SIDE							
*-----1-----1-----1-----1-----1-----1-----1-----1-----							
7140000	"DNCRUPBKN"		ANNULUS				
7140001	1						
7140101	0.0	1					
7140301	1.5300561	1					
7140401	0.1581866	1					
7140501	0.0	1					
7140601	-90.0	1					
7140801	3.81-6	0.102	1				
7141001	00	1					
7141201	0	15036100.	1233800.	2459350.	.00000000	0.0	01
*-----1-----1-----1-----1-----1-----1-----1-----1-----							
* JUNCTION - UPPER TO MIDDLE DOWNCOMER BROKEN SIDE							
*-----1-----1-----1-----1-----1-----1-----1-----1-----							
7150000	"UPR2MIDBKN"		SNGLJUN				
7150101	714010000	716000000	0.0722408	0.0000	0.0000	0100	
7150201	0	1.1432000	1.1432000	0.0			

```

*-----1-----1-----1-----1-----1-----1-----1-----1-----
* DOWNCOMER MIDDLE VOLUME BROKEN SIDE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
7160000 "DNCRMIDBKN" ANNULUS
7160001 1
7160101 0.0 1
7160301 1.2616333 1
7160401 0.1217000 1
7160501 0.0 1
7160601 -90.0 1
7160801 3.81-6 0 ? 1
7161001 00
7161201 0 15045800. 1233780. 2459500. .00000000 0.0 01
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* JUNCTION - MIDDLE TO LOWER DOWNCOMER BROKEN SIDE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
7170000 "MID2LWREBKN" SNGLJUN
7170101 716010000 718000000 0.0709408 0.0000 0.0000 0100
7170201 0 1.3175000 1.3175000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* DOWNCOMER LOWER VOLUME BROKEN SIDE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
7180000 "DNCRLWRBKN" ANNULUS
7180001 1
7180101 0.0 1
7180301 1.0792591 1
7180401 0.0986806 1
7180501 0.0 1
7180601 -90.0 1
7180801 3.81-6 0.102 1
7181001 00 1
7181201 0 15054000. 1233760. 2458600. .00000000 0.0 01
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* JUNCTION - LOWER DOWNCOMER TO LOWER PLENUM BROKEN SIDE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
7190000 "LRDC2LPBKN" SNGLJUN
7190101 718010000 215000000 0.0709408 0.0000 0.0000 0100
7190201 0 1.3892000 1.3892000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* CROSSFLOW JUNCTION - UPPER INLET ANNULUS
*-----1-----1-----1-----1-----1-----1-----1-----1-----
7200000 "UPRINANNXF" SNGLJUN
7200101 700000000 710000000 0.0296780 98.000 18.000 0003
7200201 0 .28732000 .28732000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* CROSSFLOW JUNCTION - LOWER INLET ANNULUS
*-----1-----1-----1-----1-----1-----1-----1-----1-----
7220000 "LWRINANNXF" SNGLJUN
7220101 702000000 712000000 0.0428706 98.000 18.000 0003
7220201 0 .38395000 .38395000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* CROSSFLOW JUNCTION - UPPER DOWNCOMER
*-----1-----1-----1-----1-----1-----1-----1-----1-----
7240000 "UPRDNCMRXF" SNGLJUN
7240101 704000000 714000000 0.03 98.0 18.0 0003
7240201 0 .19557000 .19557000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* CROSSFLOW JUNCTION - MIDDLE DOWNCOMER
*-----1-----1-----1-----1-----1-----1-----1-----1-----
7260000 "MIDDCMRXF" SNGLJUN
7260101 706000000 716000000 0.03 98.0 18.0 0003

```



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7260201 0 .10572000 .10572000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* CROSSFLOW JUNCTION - LOWER DOWNCOMER
*-----1-----1-----1-----1-----1-----1-----1-----
7280000 "LWRDNCMRXF" SNGLJUN
7280101 708000000 718000000 0.03 98.0 18.0 0003
7280201 0 .07171910 .07171910 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* LOWER PLENUM TOP VOLUME
*-----1-----1-----1-----1-----1-----1-----1-----
2150000 "LWR PL TOP" BRANCH
2150001 2 0
2150101 0.0 0.3533183 0.2592277 0.0 -90.0 -0.3533183
2150102 3.81-6 0.0 00
2150200 0 15059400. 1233780. 2458550. .00000000
2151101 215010000 220000000 0.0 0.005 0.005 0000
2152101 215000000 225000000 0.1499 1.5 1.5 0000
2151201 .571898-5 .571894-5 0.0
2152201 1.7076000 1.7076000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* LOWER PLENUM BOTTOM VOLUME
*-----1-----1-----1-----1-----1-----1-----1-----
2200000 "LWR PL BOT" SNGLVOL
2200101 0.0 0.3741720 0.29656 0.0 -90.0 -0.3741720
2200102 4.0E-5 0.0 00
2200200 0 15062100. 1233780. 2458500. .00000000
*-----1-----1-----1-----1-----1-----1-----1-----
* LOWER CORE SUPPORT STRUCTURE
*-----1-----1-----1-----1-----1-----1-----1-----
2250000 "L CORE SUP" BRANCH
*2250001 2 0
2250001 3 0
2250101 0.2832456 0.5709589 0.0 0.0 90.0 0.5709989
2250102 3.81-6 0.095 00
2250200 0 14970400. 1230690. 2460590. 0.0
2251101 225010000 011000000 0.09790318 1.5 1.5 00100
2252101 225010000 021000000 0.01549682 1.5 1.5 00100
2253101 225010000 235000000 0.0 12.0 12.0 00100
2251201 2.0569000 2.0569000 0.0
2252201 2.0569000 2.0569000 0.0
2253201 0.0602599 0.15501 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* PERIPHERAL CORE VOLUME 1
*-----1-----1-----1-----1-----1-----1-----1-----
0110000 "PERI#1" BRANCH
0110001 2 0
0110101 0.1582181 0.279404 0.0 0.0 90.0 0.279404
0110102 1.27-7 0.0 00
0110200 0 14965200. 1241610. 2460710. 0.0
0111101 011010000 012000000 0. 0.0 0.0 00100
0112101 011000000 021000000 0.239275 4.69 4.69 00003
0111201 1.3752 1.3752 0.0
0112201 0.0 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* PERIPHERAL CORE VOLUME 2
*-----1-----1-----1-----1-----1-----1-----1-----
0120000 "PERI#1" BRANCH
0120001 2 0
0120101 0.1462431 0.279404 0.0 0.0 90.0 0.279404
0120102 1.27-7 0.0 00
0120200 0 14965200. 1241610. 2460710. 0.0

```

0121101	012010000	013000000	0.122946	0.66	0.66	00100
0122101	012000000	022000000	0.239275	4.69	4.69	00003
0121201	1.3752	1.3752	0.0			
0122201	0.0	0.0	0.0			

*-----1-----1-----1-----1-----1-----

* PERIPHERAL CORE VOLUME 3

*-----1-----1-----1-----1-----1-----

0130000	"PERI#1"	BRANCH				
0130001	2	0				
0130101	0.1479421	0.279404	0.0	0.0	90.0	0.279404
0130102	1.27-7	0.0	00			
0130200	0	14935200.	1241610.	2460710.	0.0	
0131101	013010000	014000000	0.	0.0	0.0	00100
0132101	013000000	023000000	0.239275	4.69	4.69	00003
0131201	1.3752	1.3752	0.0			
0132201	0.0	0.0	0.0			

*-----1-----1-----1-----1-----1-----

* PERIPHERAL CORE VOLUME 4

*-----1-----1-----1-----1-----1-----

0140000	"PERI#1"	BRANCH				
0140001	2	0				
0140101	0.1452617	0.279404	0.0	0.0	90.0	0.279404
0140102	1.27-7	0.0	00			
0140200	0	14965200.	1241610.	2460710.	0.0	
0141101	014010000	015000000	0.122946	0.66	0.66	00100
0142101	014000000	024000000	0.239275	4.69	4.69	00003
0141201	1.3752	1.3752	0.0			
0142201	0.0	0.0	0.0			

*-----1-----1-----1-----1-----1-----

* PERIPHERAL CORE VOLUME 5

*-----1-----1-----1-----1-----1-----

0150000	"PERI#1"	BRANCH				
0150001	2	0				
0150101	0.1464111	0.279404	0.0	0.0	90.0	0.279404
0150102	1.27-7	0.0	00			
0150200	0	14965200.	1241610.	2460710.	0.0	
0151101	015010000	016000000	0.	0.0	0.0	00100
0152101	015000000	025000000	0.239275	4.69	4.69	00003
0151201	1.3752	1.3752	0.0			
0152201	0.0	0.0	0.0			

*-----1-----1-----1-----1-----1-----

* PERIPHERAL CORE VOLUME 6

*-----1-----1-----1-----1-----1-----

0160000	"PERI#1"	BRANCH				
0160001	1	0				
0160101	0.1510117	0.279404	0.0	0.0	90.0	0.279404
0160102	1.27-7	0.0	00			
0160200	0	14965200.	1241610.	2460710.	0.0	
0161101	016000000	026000000	0.239275	4.69	4.69	00003
0161201	0.0	0.0	0.0			

*-----1-----1-----1-----1-----1-----

* CENTRAL CORE VOLUME 1

*-----1-----1-----1-----1-----1-----

0210000	"CENT#1"	BRANCH				
0210001	1	0				
0210101	0.0250439	0.279404	0.0	0.0	90.0	0.279404
0210102	1.27-7	0.0	00			
0210200	0	14965200.	1241610.	2460710.	0.0	
0211101	021010000	022000000	0.0	0.0	0.0	00100
0211201	1.3752	1.3752	0.0			

*-----1-----1-----1-----1-----1-----

```

* CENTRAL CORE VOLUME 1
*-----1-----1-----1-----1-----1-----1-----
0220000 "CENT#1" BRANCH
0220001 1 0
0220101 0.0250439 0.279404 0.0 0.0 90.0 0.279404
0220102 1.27-7 0.0 00
0220200 0 14965200. 1241610. 2460710. 0.0
0221101 022010000 023000000 0.021054 0.66 0.66 00100
0221201 1.3752 1.3752 0.0
*-----1-----1-----1-----1-----1-----1-----
* CENTRAL CORE VOLUME 3
*-----1-----1-----1-----1-----1-----1-----
0230000 "CENT#1" BRANCH
0230001 1 0
0230101 0.0262243 0.279404 0.0 0.0 90.0 0.279404
0230102 1.27-7 0.0 00
0230200 0 14965200. 1241610. 2460710. 0.0
0231101 023010000 024000000 0.0 0.0 0.0 00100
0231201 1.3752 1.3752 0.0
*-----1-----1-----1-----1-----1-----1-----
* CENTRAL CORE VOLUME 4
*-----1-----1-----1-----1-----1-----1-----
0240000 "CENT#1" BRANCH
0240001 1 0
0240101 0.0250439 0.279404 0.0 0.0 90.0 0.279404
0240102 1.27-7 0.0 00
0240200 0 14965200. 1241610. 2460710. 0.0
0241101 024010000 025000000 0.021054 0.66 0.66 00100
0241201 1.3752 1.3752 0.0
*-----1-----1-----1-----1-----1-----1-----
* CENTRAL CORE VOLUME 5
*-----1-----1-----1-----1-----1-----1-----
0250000 "CENT#1" BRANCH
0250001 1 0
0250101 0.0250439 0.279404 0.0 0.0 90.0 0.279404
0250102 1.27-7 0.0 00
0250200 0 14965200. 1241610. 2460710. 0.0
0251101 025010000 026000000 0.0 0.0 0.0 00100
0251201 1.3752 1.3752 0.0
*-----1-----1-----1-----1-----1-----1-----
* CENTRAL CORE VOLUME 6
*-----1-----1-----1-----1-----1-----1-----
0260000 "CENT#1" BRANCH
0260001 1 0
0260101 0.0262243 0.279404 0.0 0.0 90.0 0.279404
0260102 1.27-7 0.0 00
0260200 0 14965200. 1241610. 2460710. 0.0
0261101 026010000 240000000 0.021054 1.5 1.5 00100
0261201 1.3752 1.3752 0.0
*-----1-----1-----1-----1-----1-----1-----
* CORE BYPASS VOLUME
*-----1-----1-----1-----1-----1-----1-----
2350000 "CORE BYPASS" PIPE
2350001 3
2350101 0.0129428 3
2350201 0.0 2
2350301 0.5588068 3
2350401 0.0 3
2350501 0.0 3
2350601 90.0 3

```

2350801	3.81-6	0.003	3					
2350901	0.0	0.0	2					
2351001	00	3						
2351101	0000	2						
2351201	0	15048000.	1233790.	2459550.0	.00000000	0.0		01
2351202	0	15042400.	1233790.	2459550.0	.00000000	0.0		02
2351203	0	15036500.	1233790.	2459550.0	.00000000	0.0		03
2351300	0							
2351301	.71258000	.71258000	0.0					01
2351302	.73579000	.73579000	0.0					02
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
* UPPER END BOXES AND SUPPORT STRUCTURE								
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
2400000	"UPR END BX"		BRANCH					
2400001	2	0						
2400101	0.2423341	0.5867979	0.0	0.0	90.0	0.5867979		
2400102	3.81-6	0.145	00					
2400200	0	14946300.	1422480.	2461120.	1.37821-3			
2401101	016010000	240000000	0.122945736	1.5	1.5	00100		
2402101	235010000	240000000	0.0	12.	12.	00100		
2401201	.67053000	.87895000	0.0					
2402201	.67053000	.87895000	0.0					
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
* UPPER CORE SUPPORT STRUCTURE - CROSS FLOW REGION								
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
2450000	"UPR CR SUP"		BRANCH					
2450001	2	0						
2450101	0.0	0.4933248	0.1280806	0.0	90.0	0.4933248		
2450102	3.81-6	0.145	00					
2450200	0	15025400.	1417510.	2459600.	.00000000			
2451101	240010000	245000000	0.0	0.0	0.0	0000		
2452101	245010000	251000000	0.0	0.0	0.0	0000		
2451201	1.1669000	1.1669000	0.0					
2452201	.439867-4	.439867-4	0.0					
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
* UPPER FLOW SKIRT REGION								
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
2500000	"U FLW SKRT"		BRANCH					
2500001	1	0						
2500101	0.1547532	0.7850547	0.0	0.0	90.0	0.7850547		
2500102	3.81-6	0.131	00					
2500200	0	15020100.	1410020.	2459600.	.00000000			
2501101	245010000	250000000	0.0	0.0	0.0	0000		
2501201	1.8273000	1.8273000	0.0					
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
* DEAD END OF FUEL MODULES								
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
2510000	"DE FL MODS"		SNGLVOL					
2510101	0.0	0.7844123	0.1154214	0.0	90.0	0.7844123		
2510102	3.81-6	0.214	00					
2510200	0	15021500.	1424270.	2459600.	.00000000			
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
* UPPER HEAD								
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----								
2520000	"UPR HEAD "		BRANCH					
2520001	2	0						
2520101	0.2622585	0.2869580	0.0	0.0	90.0	0.2869580		
2520102	3.81-6	0.0	00					
2520200	0	15019000.	1410020.	2459550.	.00000000			
2521101	250010000	252000000	0.0	0.006	0.006	0000		
2522101	.730000000	252000000	0.0	0.90+4	0.90+4	0003		


```

*-----1-----1-----1-----1-----1-----1-----
3150000 "SG+PMP SIM" PIPE
3150001 8
3150101 0.0 8
3150201 8.3647-3 1
3150202 1.12-2 2
3150203 0.105626 3
3150204 1.12-2 4
3150205 8.3647-3 7
3150301 0.919969 1
3150302 1.987956 2
3150303 0.849744 4
3150304 1.987956 5
3150305 1.371350 6
3150306 1.365029 7
3150307 1.674812 8
3150401 7.75291-3 1
3150402 0.1721108 2
3150403 8.97552-2 4
3150404 0.1721108 5
3150405 1.82303-2 6
3150406 5.46687-2 7
3150407 1.82489-2 8
3150601 90.0 3
3150602 -90.0 7
3150603 90.0 8
3150701 0.679201 1
3150702 1.987956 2
3150703 0.457202 3
3150704 0.457202 4
3150705 -1.987956 5
3150707 -1.371350 6
3150708 -0.520707 7
3150709 1.212851 8
3150801 4.0E-5 0.0 8
3150901 0.93596 0.93596 1
3150902 2.0 2.0 2
3150903 0.5 0.5 3
3150904 2.0 2.0 4
3150905 0.23025 0.23025 5
3150906 2.534 2.534 6
3150907 5.069 5.069 7
3151001 00 8
3151101 0000 7
3151201 0 15015600. 1243880. 2459924. .00000000 0.0 01
3151202 0 15005700. 1237630. 2459924. .00000000 0.0 02
3151203 0 14996600. 1237670. 2459924. .00000000 0.0 03
3151204 0 14996600. 1237680. 2459924. .00000000 0.0 04
3151205 0 15005600. 1237680. 2459924. .00000000 0.0 05
3151206 0 15018100. 1237630. 2459924. .00000000 0.0 06
3151207 0 15025100. 1237680. 2459924. .00000000 0.0 07
3151208 0 15022500. 1237680. 2459924. .00000000 0.0 08
3151300 0
3151301 .910345-3 .910345-3 0.0 01
3151302 .487913-3 .487915-3 0.0 02
3151303 .411825-4 .411825-4 0.0 03
3151304 .289111-3 .289109-3 0.0 04
3151305 .133199-3 .133198-3 0.0 05
3151306 .106449-3 .106449-3 0.0 06
3151307 .266103-4 .266103-4 0.0 07
*-----1-----1-----1-----1-----1-----1-----

```


* HOT LEG BREAK VALVE

```

*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
3170000 "HL BREAK " VALVE
3170101 315010000 800000000 8.3647-3 0.94883 0.94883 0100
3170102 0.93 0.84
3170201 0 .00000000 .00000000 0.0
3170300 TRPVLV
3170301 501
    
```

* REACTOR VESSEL NOZZLE - BROKEN LOOP COLD LEG

```

*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
3350000 "RVN BLCL " BRANCH
3350001 2 0
3350101 0.0 0.749305 0.047970 0.0 0.0 0.0
3350102 4.0E-5 0.0 00
3350200 0 15028400. 1233660. 2459250. .00000000
3351101 740000000 335000000 0.064130 1.455594 0.812933 0002
3352101 335010000 340000000 0.063426 0.1005 0.1005 0000
3351201 .06071680 .06071680 0.0
3352201 .06138070 .06138070 0.0
    
```

* COLD LEG PIPE TO REFLOOD ASSIST BYPASS TEE

```

*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
3400000 "CLP-RABS T" BRANCH
3400001 1 0
3400101 0.0 0.698336 0.0443927 0.0 0.0 0.0
3400102 4.0E-5 0.0 00
3400200 0 15028400. 1233140. 2459250. .00000000
3401101 340010000 342000000 0.063426 0.1005 0.1005 0000
3401201 .06137130 .06137130 0.0
    
```

* BROKEN LOOP COLD LEG RABS TO DTT

```

*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
3420000 "BLCL 2DTT " BRANCH
3420001 1 0
3420101 0.0 0.5715069 0.0362484 0.0 0.0 0.0
3420102 4.0E-5 0.0 00
3420200 0 15028400. 1232540. 2459250. .00000000
3421101 342000000 370000000 0.0388 0.84 0.84 0000
3421201 .10030000 .10030000 0.0
    
```

* BROKEN LOOP COLD LEG DTT TO BREAK PLANE

```

*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
3440000 "BLCL 2BRK " BRANCH
3440001 1 0
3440101 0.0 0.9286231 0.0310679 0.0 0.0 0.0
3440102 4.0E-5 0.0 00
3440200 0 15028400. 1232300. 2459250. .00000000
3441101 342010000 344000000 0.0540157 6.545 14.35 0000
3441201 .759199-5 .759199-5 0.0
    
```

* COLD LEG BREAK VALVE

```

*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
3470000 "CL BREAK " VALVE
3470101 344010000 805000000 8.3647-3 0.415 0.415 0100
3470102 0.93 0.84
3470201 0 .00000000 .00000000 0.0
3470300 TRPVLV
3470301 501
    
```

* REFLOOD ASSIST BYPASS PIPING - COLD LEG SIDE

*****1-----1-----1-----1-----1-----1-----1-----*							
3700000 "RABS C L " PIPE							
3700001	3						
3700101	0.0388	2					
3700102	0.0776	3					
3700201	0.0388	2					
3700301	0.0	3					
3700401	0.0279	1					
3700402	0.070	2					
3700403	0.1165	3					
3700601	90.0	1					
3700602	0.0	3					
3700701	0.64	1					
3700702	0.0	3					
3700801	4.0-5	0.0	3				
3700901	0.28	0.28	1				
3700902	0.84	0.84	2				
3701001	00	3					
3701101	0000	2					
3701201	0	15026000.	1232040.	2459300.	.00000000	0.0	01
3701202	0	15023600.	1231420.	2459300.	.00000000	0.0	02
3701203	0	15023600.	1231430.	2459300.	.00000000	0.0	03
3701300	0						
3701301	.10029000	.10029000	0.0	01			
3701302	.10027000	.10027000	0.0	02			
*****1-----1-----1-----1-----1-----1-----1-----*							
* REFLOOD ASSIST BYPASS VALVES							
*****1-----1-----1-----1-----1-----1-----1-----*							
3750000 "RABS VALVS" SNGLJUN							
3750101	370010000	380000000	0.0	0.90+4	0.90+4	0000	
3750201	0	.05011390	.05011390	0.0			
*****1-----1-----1-----1-----1-----1-----1-----*							
* REFLOOD ASSIST BYPASS PIPING - HOT LEG SIDE							
*****1-----1-----1-----1-----1-----1-----1-----*							
3800000 "RABS H L " PIPE							
3800001	3						
3800101	0.0776	1					
3800102	0.0388	3					
3800201	0.0388	2					
3800301	0.0	3					
3800401	0.0915	1					
3800402	0.048	2					
3800403	0.0489	3					
3800601	0.0	1					
3800602	-90.0	2					
3800603	0.0	3					
3800701	0.0	1					
3800702	-0.64	2					
3800703	0.0	3					
3800801	4.0-5	0.0	3				
3800901	0.84	0.84	1				
3800902	0.28	0.28	2				
3801001	00	3					
3801101	0000	2					
3801201	0	15013400.	1231600.	2459400.	.00000000	0.0	01
3801202	0	15015700.	1231730.	2459400.	.00000000	0.0	02
3801203	0	15018100.	1231820.	2459400.	.00000000	0.0	03
3801300	0						
3801301	.10020000	.10020000	0.0	01			
3801302	.10018000	.10018000	0.0	02			

*****1-----1-----1-----1-----1-----1-----1-----*

```

*
* PRESSURIZER
*
*-----1-----1-----1-----1-----1-----1-----
* SURGE LINE PCS SIDE
*-----1-----1-----1-----1-----1-----1-----
4000000 "SRG LN PCS"      BRANCH
4000001 2              0
4000101 1.44561-3 2.30      0.0      0.0      90.0      0.54
4000102 2.3622-5  0.0          00
4000200 0              15012400. 1418060. 2459400. .00000000
4001101 107000000 400000000 1.44561-3 3.9      3.9      0002
4002101 400010000 405000000 1.44561-3 2.85      2.85      1000
4001201 -.0607909 -.0607909 0.0
4002201 -.0608265 -.0608265 0.0
*-----1-----1-----1-----1-----1-----1-----
* PRESSURIZER SURGE LINE
*-----1-----1-----1-----1-----1-----1-----
4050000 "SRG LN PZR"      PIPE
4050001 2
4050101 1.44561-3 2
4050201 1.44561-3 1
4050301 2.30      2
4050401 0.0        2
4050601 90.0       2
4050701 0.30       2
4050801 2.3622-5  0.0        2
4050901 2.85       2.85      1
4051001 00         2
4051101 1000       1
4051201 0          15010800. 1427980. 2459500. .00000000 0.0      01
4051202 6          15010100. 1444040. 2459500. .00000000 0.0      02
4051300 0
4051301 -.0608633 -.0608633 0.0      01
*-----1-----1-----1-----1-----1-----1-----
* PRESSURIZER SURGE LINE
*-----1-----1-----1-----1-----1-----1-----
4100000 "SRG LINE"      SNGLJUN
4100101 405010000 415000000 1.44561-3 0.42      1.00      1000
4100201 0          -.0608789 -.0608789 0.0
*-----1-----1-----1-----1-----1-----1-----
* PRESSURIZER VESSEL
*-----1-----1-----1-----1-----1-----1-----
4150000 "PZR VESSEL"      PIPE
4150001 6
4150101 0.0        2
4150102 0.5653     5
4150103 0.0        6
4150201 0.0        5
4150301 0.1815     1
4150302 0.1524     2
4150303 0.3967     3
4150304 0.5289     4
4150305 0.3967     5
4150306 0.1943     6
4150401 0.0684     1
4150402 0.0838     2
4150403 0.0        5
4150404 0.0732     6
4150501 0.0        6
4150601 90.0       6

```


5030101	0.0	0.4445	0.4384	0.0	90.0	0.4445	
5030102	4.E-5	0.3678	00				
5030200	0	5827350.0	1150000.	2591270.	.99988000		
5031101	505000000	503000000	0.98627	0.0	0.0	0100	
5032101	503010000	520000000	0.98627	0.8	0.0	0100	
5031201	-1.265400	.17607000	0.0				
5032201	-.3871600	.07560020	0.0				
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
* SEPARATOR OUTLET REGION							
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
5050000	"LWR SEPAR "		BRANCH				
5050001	1	0					
5050101	0.0	1.2131	1.4850	0.0	-90.0	-1.2131	
5050102	4.E-5	1.9048	00				
5050200	0	5830080.0	1236530.	2580000.	.02870570		
5051101	505010000	508000000	0.0	0.0	0.0	0100	
5051201	.64364000	-2.022800	0.0				
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
* FEED INLET VOLUME							
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
5080000	"UPR DWNCMR"		BRANCH				
5080001	1	0					
5080101	0.0	0.6096	0.22	0.0	-90.0	-0.6096	
5080102	4.E-5	0.163697	00				
5080200	0	5835210.0	1145280.	2580000.	.00000000		
5081101	508010000	510000000	0.0	0.0	0.0	0100	
5081201	.66587000	.66587000	0.0				
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
* STEAM GENERATOR DOWNCOMER							
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
5100000	"DWNCMR "		ANNULUS				
5100001	3						
5100101	0.232	3					
5100201	0.0	2					
5100301	0.6096	3					
5100401	0.0	3					
5100601	-90.0	3					
5100701	-0.6096	3					
5100801	4.E-5	0.10793	3				
5100901	0.0	0.0	2				
5101001	00	3					
5101101	0000	2					
5101201	0	5839840.0	1145550.	2580000.	.00000000	0.0	01
5101202	0	5844480.0	1145820.	2580000.	.00000000	0.0	02
5101203	0	5849120.0	1146090.	2580000.	.00000000	0.0	03
5101300	0						
5101201	.66594000	.66594000	0.0	01			
5101302	.66602000	.66602000	0.0	02			
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
* JUNCTION - DOWNCOMER TO BOILER							
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
5130000	"DNCMR-BLR "		SNGLJUN				
5130101	510010000	515000000	0.0	17.5	17.5	0100	
5130201	0	.66609000	.88146000	0.0			
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
* STEAM GENERATOR BOILER							
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
5150000	"BOILER "		PIPE				
5150001	5						
5150101	0.2776	4					
5150102	0.306294	5					

5150201	0.0	4					
5150301	1.8288	4					
5150302	1.2131	5					
5150401	0.0	5					
5150601	80.0	4					
5150602	90.0	5					
5150701	0.6096	4					
5150702	1.2131	5					
5150801	4.E-5	0.0234	4				
5150802	4.E-5	0.5962	5				
5150901	4.05	4.05	4				
5151001	00	5					
5151101	0100	4					
5151201	0	5846670.0	1222840.	2580000.	.01975860	0.0	01
5151202	0	5842700.0	1274560.	2580000.	.05552290	0.0	02
5151203	0	5838650.0	1321180.	2580000.	.08907110	0.0	03
5151204	0	5834160.0	1360130.	2580000.	.11715000	0.0	04
5151205	0	5829740.0	1414230.	2580000.	.15606000	0.0	05
5151300	0						
5151301	.83850000	1.1089000	0.0	01			
5151302	1.3147000	1.8082000	0.0	02			
5151303	1.7463000	2.4614000	0.0	03			
5151304	2.1057000	2.9324000	0.0	04			
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
* LOWER PORTION OF STEAM DOME							
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
5200000	"LWR STM DM"	BRANCH					
5200001	1	0					
5200101	0.0	0.46956	0.705312	0.0	90.0	0.46956	
5200102	4.E-5	1.383	00				
5200200	0	5827210.0	1150000.	2591540.	.99979000		
5201101	520010000	525000000	0.0	0.0	0.0	0000	
5201201	-.0806823	.41903000	0.0				
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
* UPPER PORTION OF STEAM DOME							
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
5250000	"UPR STM DM"	BRANCH					
5250001	1	0					
5250101	0.0	0.46956	0.705312	0.0	90.0	0.46956	
5250102	4.E-5	1.383	00				
5250200	0	5827070.0	1150000.	2591710.	.99990000		
5251101	525010000	530000000	0.0	0.8	0.8	0100	
5251201	13.328000	13.578000	0.0				
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
* STEAM PIPE FROM GENERATOR TO CONTROL VALVE							
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
5300000	"STEAM PIPE"	SNGLVOL					
5300101	0.04635	25.074	0.0	0.0	0.0	0.0	
5300102	4.E-5	0.0	00				
5300200	0	5819190.0	1148038.	2591620.	1.0000000		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
* STEAM FLOW CONTROL VALVE							
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
5400000	"CV-P4-10 "	VALVE					
5400101	530010000	541000000	0.0047772	0.0	0.0	1100	
5400201	1	0.0	19.6	0.0			
5400300	MTRVLV						
5400301	685	586	0.05	0.44405	540		
20254000	NORMAREA						
20254001	0.0	0.0					
20254002	9.25-4	9.25-4					


```

20254003 1.0      1.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* PIPE DOWNSTREAM OF STEAM CONTROL VALVE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
5410000 "COND INLET"      BRANCH
5410001 1          0
5410101 0.06557  54.44  0.0  0.0  0.0  0.0
5410102 4.E-5     0.0  00
5410200 0          2072970.0 914598. 2598620. .86686000
5411101 541010000 542000000 0.0  0.0  0.0  0100
5411201 13.013000 25.588000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* AIR COOLED CONDENSER
*-----1-----1-----1-----1-----1-----1-----1-----1-----
5420000 "CONDENSER "      TMDPVOL
5420101 9.21677  17.67  0.0  0.0  0.0  0.0
5420102 4.E-5     0.02  00
5420200 2
5420207 0.0      2.069E6  1.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* SIMPLIFIED FEED SYSTEM
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* FEED STORAGE TANK
*-----1-----1-----1-----1-----1-----1-----1-----1-----
5650000 "FEED TANK "      TMDPVOL
5650101 29.81     3.048  0.0  0.0  0.0  0.0
5650102 4.E-5     0.0  00
5650200 3          502
5650201 0.0      7.58E6  482.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* FEED WATER
*-----1-----1-----1-----1-----1-----1-----1-----1-----
5660000 "FEED "      TMDPJUN
5660101 565000000 508000000 0.05
5660200 1          502
5660201 -100.0    19.150  0.0  0.0  *L2-3
5660202 0.0      19.150  0.0  0.0  *L2-3
5660203 0.5      10.0  0.0  0.0  *L2-5
5660204 1.0      2.50  0.0  0.0  *L2-5
5660205 1.5      1.00  0.0  0.0  *L2-5
5660206 2.0      0.25  0.0  0.0  *L2-5
5660207 2.5      0.00  0.0  0.0  *L2-5
* * * * *
*
* ECC SYSTEM
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* ECC CHECK VALVE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
6000000 "ECC CHKVLV"      VALVE
6000101 605010000 185000000 5.9896-3 0.935  0.935  1120
6000201 0          .00000000 .00000000 0.0
6000300 TRPVLV
6000301 681
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* ECCS HEADER TO PLS
*-----1-----1-----1-----1-----1-----1-----1-----1-----
6050000 "ECCS HEADR"      SVGLVOL
6050101 5.9896-3 5.0148  0.0  0.0  90.0  3.3071200
6050102 4.0-5     0.0  00
6050200 0          4.5E+6  172410. 2459920. .00000000

```

*IC01
*IC01

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*-----1-----1-----1-----1-----1-----1-----1-----
* ACCUMULATOR VALVE
*-----1-----1-----1-----1-----1-----1-----1-----
6100000 "ACCUM VLV " VALVE
6100101 615010000 605000000 5.9896-3 6.278 6.278 1000
6100201 0 -.4902-15 .79206-11 0.0
6100300 TRPVLV
6100301 682
*-----1-----1-----1-----1-----1-----1-----1-----
* ACCUMULATOR PIPE
*-----1-----1-----1-----1-----1-----1-----1-----
6150000 "ACC PIPE " SNGLVOL
6150101 0.0 25.997165 0.4074774 0.0 0.0 0.0
6150102 4.0-5 0.0 00
6150200 0 4.5E+6 112409. 2459920. .00000000
*-----1-----1-----1-----1-----1-----1-----1-----
* ACCUMULATOR VESSEL
*-----1-----1-----1-----1-----1-----1-----1-----
6200000 "ACCUMULATR" ACCUM
6200101 0.0 1.8103 2.3422 0.0 -90.0 -1.8103
6200102 4.0-5 0.0 00
6200200 4.180+6 305.40
6201101 615000000 8.2132-3 40.0 40.0 0
6202200 0.0 1.0662 2.4509 1.6927 0.04445 0 0 0 0
*-----1-----1-----1-----1-----1-----1-----1-----
* BWST LPIS
*-----1-----1-----1-----1-----1-----1-----1-----
6250000 "BWST LPIS " TMDPVOL
6250101 20.44 5.0 0.0 0.0 90.0 5.0
6250102 4.0E-5 0.0 00
6250200 3
6250201 0.0 1.0+5 300.0
*-----1-----1-----1-----1-----1-----1-----1-----
* LOW PRESSURE INJECTION SYSTEM
*-----1-----1-----1-----1-----1-----1-----1-----
6300000 "LPIS " TMDPJUN
6300101 625000000 605000000 5.9896-3
6300200 1 504 P 605010000
6300201 -1.0 0.0 0.0 0.0
6300202 0.0 0.0 0.0 0.0
6300203 8.483+4 7.045 0.0 0.0
6300204 4.297+5 6.091 0.0 0.0
6300205 7.745+5 5.045 0.0 0.0
6300206 0.448+5 4.312 0.0 0.0
6300207 1.119+6 3.454 0.0 0.0
6300208 1.186+6 3.173 0.0 0.0
6300209 1.257+6 2.673 0.0 0.0
6300210 1.236+6 2.159 0.0 0.0
6300211 1.395+6 1.536 0.0 0.0
6300212 1.464+6 0.7182 0.0 0.0
6300213 1.517+6 0.6 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* BWST HPIS
*-----1-----1-----1-----1-----1-----1-----1-----
6350000 "BWST HPIS " TMDPVOL
6350101 20.44 5.0 0.0 0.0 90.0 5.0
6350102 4.0E-5 0.0 00
6350200 3
6350201 0.0 1.0+5 300.0
*-----1-----1-----1-----1-----1-----1-----1-----
* HIGH PRESSURE INJECTION SYSTEM

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```

*-----1-----1-----1-----1-----1-----1-----1-----
6400000 "HPIS " TMDP3LN
6400101 635000000 185000000 5.9896-3
6400200 1 503 P 185010000
6400201 -1.0 0.0 0.0 0.0
6400202 0.0 1.50000000 0.0 0.0
6400203 7.72514+6 1.5 0.0 0.0
6400204 8.3597+6 .31536281 0.0 0.0
6400205 17.2436+6 .31536281 0.0 0.0

```

*-----1-----1-----1-----1-----1-----1-----1-----

* CONTAINMENT

```

*-----1-----1-----1-----1-----1-----1-----1-----
* CONTAINMENT BROKEN LOOP HOT LEG

```

```

*-----1-----1-----1-----1-----1-----1-----1-----
8000000 "CONT BLKL " TMDPVOL
8000101 0.0 1.0 0.1 0.0 0.0 0.0
8000102 0.0 0.0 00
8000200 2 501
8000201 0.0 1.0+5 1.0
8000202 1.0 2.1+5 1.0
8000203 1.2 1.65+5 1.0
8000204 20.0 2.9+5 1.0
8000205 24.0 2.9+5 1.0
8000206 28.0 2.83+5 1.0
8000207 40.0 2.67+5 1.0
8000208 48.0 2.67+5 1.0
8000209 52.0 2.6+5 1.0
8000210 60.0 3.0+5 1.0
8000211 70.0 3.3+5 1.0
8000212 100.0 3.0+5 1.0

```

* CONTAINMENT BROKEN LOOP COLD LEG

```

*-----1-----1-----1-----1-----1-----1-----1-----
8050000 "CONT BLCL " TMDPVOL
8050101 0.0 1.0 0.1 0.0 0.0 0.0
8050102 0.0 0.0 00
8050200 2 501
8050201 0.0 1.0+5 1.0
8050202 1.0 2.1+5 1.0
8050203 1.2 1.65+5 1.0
8050204 20.0 2.9+5 1.0
8050205 24.0 2.9+5 1.0
8050206 28.0 2.83+5 1.0
8050207 40.0 2.67+5 1.0
8050208 48.0 2.67+5 1.0
8050209 52.0 2.6+5 1.0
8050210 60.0 3.0+5 1.0
8050211 70.0 3.3+5 1.0
8050212 100.0 3.0+5 1.0

```

*-----1-----1-----1-----1-----1-----1-----1-----

* REACTOR VESSEL HEAT STRUCTURES

```

*-----1-----1-----1-----1-----1-----1-----1-----
* ACTIVE CORE

```

* STATION 11F.91 TO 182.94

```

*-----1-----1-----1-----1-----1-----1-----1-----
*
* HOT FUEL RODS HEAT STRUCTURE :12311

```

12311000	6	10	2	1	0.0	555	1	8
12311001	7.869+6							
12311011	1.0E-6	2.0E-6	0.0	0.0	6			
12311100	0	1						
12311101	5	4.65564-3						
12311102	1	4.75106-3						
12311103	3	5.36806-3						
12311201	1	5						
12311202	-2	6						
12311203	-3	9						
12311301	1.0	5						
12311302	0.0	9						
12311401	560.0	10						
12311501	0	0	0	1	56.998416	06		
12311601	021010000	1000000	1	1	56.998416	06		
12311701	900	0.02306447	0.	0.	1			
12311702	900	0.051034	0.	0.	2			
12311703	900	0.05449747	0.	0.	3			
12311704	900	0.0414851	0.	0.	4			
12311705	900	0.02567737	0.	0.	5			
12311706	900	0.0090072	0.	0.	6			
12311901	0	0.013833	0.01504	1.6764	06			

AVERAGE FUEL RODS HEAT STRUCTURE :12301

12301000	6	10	2	1	0.0	555	1	8
12301001	7.869+6							
12301011	1.0E-6	2.0E-6	0.0	0.0	6			
12301100	0	1						
12301101	5	4.65564-3						
12301102	1	4.75106-3						
12301103	3	5.36806-3						
12301201	1	5						
12301202	-2	6						
12301203	-3	9						
12301301	1.0	5						
12301302	0.0	9						
12301401	560.0	10						
12301501	0	0	0	1	159.819088	06		
12301601	011010000	1000000	1	1	159.819088	06		
12301701	900	0.036746	0.	0.	1			
12301702	900	0.0879275	0.	0.	2			
12301703	900	0.0990847	0.	0.	3			
12301704	900	0.6768387	0.	0.	4			
12301705	900	0.0491237	0.	0.	5			
12301706	900	0.0153074	0.	0.	6			
12301901	0	0.013633	0.01504	1.6764	6			

INTERMEDIATE FUEL RODS HEAT STRUCTURE :12302

12302000	6	10	2	1	0.0	555	1	8
12302001	7.869+6							
12302011	1.0E-6	2.0E-6	0.0	0.0	6			
12302100	0	1						

20100106	1.03315E3	3.357625
20100107	1.08871E3	3.155129
20100108	1.19982E3	2.983787
20100109	1.28315E3	2.836674
20100110	1.36648E3	2.713792
20100111	1.53315E3	2.521680
20100112	1.61648E3	2.448990
20100113	1.69982E3	2.391875
20100114	1.97759E3	2.289762
20100115	2.25537E3	2.307069
20100116	2.53315E3	2.433413
20100117	2.81093E3	2.561370
20100118	3.08871E3	2.994171
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* UO2 - VOLUMETRIC HEAT CAPACITY		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
20100151	2.73150E2	2.310427E6
20100152	3.23150E2	2.574985E6
20100153	3.73150E2	2.746357E6
20100154	6.7315E2	3.138694E6
20100155	1.37315E3	3.443844E6
20100156	1.77315E3	3.531030E6
20100157	1.97315E3	3.792588E6
20100158	2.17315E3	4.228518E6
20100159	2.37315E3	4.882412E6
20100160	2.67315E3	6.015829E6
20100161	2.77315E3	6.320980E6
20100162	2.87315E3	6.582538E6
20100163	2.97315E3	6.713317E6
20100164	3.11315E3	6.805503E6
20100165	4.60982E3	6.800503E6
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* HELIUM(GAP) - THERMAL CONDUCTIVITY		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
2010201	HELIUM	1.00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* HELIUM(GAP) - VOLUMETRIC HEAT CAPACITY		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
20100251	273.15	5.4
20100252	5000.0	5.4
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* ZIRCALOY-4 - THERMAL CONDUCTIVITY FROM MATPRO		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
20100301	380.4	13.6
20100302	469.3	14.6
20100303	577.6	15.8
20100304	685.9	17.3
20100305	774.8	18.4
20100306	872.0	19.8
20100307	973.2	21.6
20100308	1073.2	23.2
20100309	1123.2	25.4
20100310	1152.3	24.2
20100311	1232.2	25.5
20100312	1331.2	26.6
20100313	1404.2	28.2
20100314	1576.2	33.0
20100315	1625.2	36.7
20100316	1755.2	41.2
20100317	2273.2	55.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		


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*-----1-----1-----1-----1-----1-----1-----1-----
* 001-010 LEVEL CALCULATORS
*-----1-----1-----1-----1-----1-----1-----1-----
* 001 STEAM GENERATOR LEVEL
20500100 SGLVL    SUM    1.0    0.0    1
20500101 0.0      0.4445 VOIDF 503010000
20500102      1.2131 VOIDF 505010000
20500103      0.6096 VOIDF 508010000
20500104      0.6096 VOIDF 510010000
20500105      0.6096 VOIDF 510020000
20500106      0.6096 VOIDF 510030000
* 002 PRESSURIZER LEVEL
20500200 PZRLVL    SUM    1.0    0.0    1
20500201 0.0      0.1815 VOIDF 415010000
20500202      0.1524 VOIDF 415020000
20500203      0.3967 VOIDF 415030000
20500204      0.5289 VOIDF 415040000
20500205      0.3967 VOIDF 415050000
20500206      0.1943 VOIDF 415060000
20500207      0.1029 VOIDF 420010000
20500208      0.1029 VOIDF 420020000
* 003 REACTOR VESSEL LEVEL
20500300 RVLVL    SUM    1.0    0.0    1
20500301 0.0      0.84888 VOIDF 250010000
20500302      0.24333 VOIDF 255010000
20500303      0.9285337 VOIDF 250010000
20500304      0.4933248 VOIDF 245010000
20500305      0.4933248 VOIDF 240010000
20500312      0.4269792 VOIDF 225010000
20500313      0.3533183 VOIDF 215010000
20500314      0.3741720 VOIDF 220010000
* 004 ACCUMULATOR LEVEL
*20500400 ACCMLVL INTEGRAL -6.3480-3 2.0447 0
*20500401 VELFJ 620010000
* 007 REACTOR VESSEL DOWNCOMER LEVEL INTACT SIDE
20500700 RVDCLVLIN SUM    1.0    0.0    1
20500701 0.0      0.3302040 VOIDF 700010000
20500702      0.3951272 VOIDF 702010000
20500703      1.5200561 VOIDF 704010000
20500704      1.2616333 VOIDF 706010000
20500705      1.0792591 VOIDF 708010000
20500706      0.3533183 VOIDF 215010000
20500707      0.3741720 VOIDF 220010000
* 008 REACTOR VESSEL DOWNCOMER LEVEL BROKEN SIDE
20500800 RVDCLVLBK SUM    1.0    0.0    1
20500801 0.0      0.3302040 VOIDF 710010000
20500802      0.3951272 VOIDF 712010000
20500803      1.5200561 VOIDF 714010000
20500804      1.2616333 VOIDF 716010000
20500805      1.0792591 VOIDF 718010000
20500806      0.3533183 VOIDF 215010000
20500807      0.3741720 VOIDF 220010000
*-----1-----1-----1-----1-----1-----1-----1-----
* CORE LEVEL : HOT CHANNEL 009, AVERAGE 010
*-----1-----1-----1-----1-----1-----1-----1-----
* HOT LEVEL
20500900 HOTLVL    SUM    1.0    0.0    1
20500901 0.0      0.279404 VOIDF 021010000
20500902      0.0279404 VOIDF 022010000
20500903      0.0279404 VOIDF 023010000
20500904      0.0279404 VOIDF 024010000

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20500535	0.0279404	VOIDF	025010000
20500906	0.0279404	VOIDF	026010000

*
 * AVERAGE LEVEL

20501000	HOTLVL	SUM	1.0	0.0	1
20501001	0.0	0.0279404	VOIDF	011010000	
20501002		0.0279404	VOIDF	012010000	
20501003		0.0279404	VOIDF	013010000	
20501004		0.0279404	VOIDF	014010000	
20501005		0.0279404	VOIDF	015010000	
20501006		0.0279404	VOIDF	016010000	

-----1-----1-----1-----1-----1-----1-----1-----1-----
 * 061-072 PRIMARY SYSTEM MASS CALCULATOR
 -----1-----1-----1-----1-----1-----1-----1-----1-----

* 061 INTACT LOOP HOT LEG MASS

20506100	ILHLMASS	SUM	1.0	0.0	1
20506101	0.0	0.102752	RHO	100010000	
20506102		7.57291-2	RHO	105010000	
20506103		6.43178-2	RHO	110010000	
20506104		7.96973-2	RHO	112010000	
20506105		5.79614-2	RHO	112010000	

* 062 STEAM GENERATOR PRIMARY MASS

20506200	SGPRIMASS	SUM	1.0	0.0	1
20506201	0.0	0.335320	RHO	114010000	
20506202		0.136356	RHO	115010000	
20506203		9.21538-2	RHO	115020000	
20506204		9.21538-2	RHO	115030000	
20506205		6.99783-2	RHO	115040000	
20506206		6.99783-2	RHO	115050000	
20506207		9.21538-2	RHO	115060000	
20506208		9.21538-2	RHO	115070000	
20506209		0.136356	RHO	115080000	
20506210		0.335320	RHO	116010000	

* 063 PUMP SUCTION PIPING MASS

20506300	PMPSUMASS	SUM	1.0	0.0	1
20506301	0.0	4.45625-2	RHO	118010000	
20506302		4.45137-2	RHO	118020000	
20506303		3.54278-2	RHO	118030000	
20506304		4.87901-2	RHO	120010000	
20506305		6.40548-2	RHO	125010000	
20506306		1.77444-2	RHO	130010000	
20506307		6.40548-2	RHO	155010000	
20506308		1.77444-2	RHO	160010000	

* 064 INTACT LOOP COLD LEG MASS

20506400	ILCLMASS	SUM	1.0	0.0	1
20506401	0.0	9.91000-2	RHO	135010000	
20506402		1.83849-2	RHO	140010000	
20506403		6.33861-2	RHO	145010000	
20506404		3.16011-2	RHO	150010000	
20506405		9.91000-2	RHO	165010000	
20506406		1.92958-2	RHO	170010000	
20506407		3.54280-2	RHO	175010000	
20506408		3.88950-2	RHO	175020000	
20506409		7.30598-2	RHO	180010000	
20506410		6.44920-2	RHO	185010000	

* 065 DOWNCOMER/TOWER PLENUM MASS

20506500	DCLPMASS	SUM	1.0	0.0	1
20506501	0.0	0.0432082	RHO	700010000	
20506502		0.0578606	RHO	702010000	
20506503		0.1581866	RHO	704010000	
20506504		0.1217000	RHO	706010000	

20506505	0.0986806	RHO	708010000		
20506506	0.0432082	RHO	710010000		
20506507	0.0578606	RHO	712010000		
20506508	0.1581866	RHO	714010000		
20506509	0.1217000	RHO	716010000		
20506510	0.0986806	RHO	718010000		
20506511	0.24520	RHO	215010000		
20506512	0.29F	RHO	220010000		
* 067 CORE/UPPER PLENUM MASS					
20506700	CRUPMASS	SUM	1.0	0.0	1
20506701	0.0	0.12094	RHO	225010000	
*20506702		0.0683340	RHO	821010000	
*20506703		0.0478582	RHO	822010000	
*20506704		0.0483329	RHO	823010000	
*20506705		0.0479138	RHO	824010000	
*20506706		0.0479052	RHO	825010000	
*20506707		0.0750459	RHO	826010000	
20506708		0.0091280	RHO	235010000	
20506709		0.0072325	RHO	235020000	
20506710		0.0088095	RHO	235030000	
20506711		0.1195494	RHO	240010000	
20506712		0.1280806	RHO	245010000	
20506713		0.1436936	RHO	250010000	
20506714		0.1154214	RHO	251010000	
20506715		0.083595	RHO	255010000	
20506716		0.310967	RHO	260010000	
* 068 BROKEN LOOP HOT LEG MASS					
20506800	BLHLMASS	SUM	1.0	0.0	1
20506801	0.0	5.75410-2	RHO	300010000	
20506802		4.42927-2	RHO	305010000	
20506803		6.78467-2	RHO	310010000	
20506804		7.75291-3	RHO	315010000	
20506805		1.72111-1	RHO	315020000	
20506806		8.97552-2	RHO	315030000	
20506807		8.97552-2	RHO	315040000	
20506808		1.72111-1	RHO	315050000	
20506809		1.82303-2	RHO	315060000	
20506810		5.46687-2	RHO	315070000	
20506811		1.82489-2	RHO	315080000	
20506812		9.15000-2	RHO	380010000	
20506813		4.80000-2	RHO	380020000	
20506814		4.89000-2	RHO	380030000	
* 069 BROKEN LOOP COLD LEG MASS					
20506900	BLCLMASS	SUM	1.0	0.0	1
20506901	0.0	4.79790-2	RHO	335010000	
20506902		4.43927-2	RHO	340010000	
20506903		3.62484-2	RHO	342010000	
20506904		5.10679-2	RHO	344010000	
20506907		2.79000-2	RHO	370010000	
20506908		7.00000-2	RHO	370020000	
20506909		1.16500-1	RHO	370030000	
* 070 PRESSURIZER MASS					
20507000	PZRMAS	SUM	1.0	0.0	1
20507001	0.0	3.33500-3	RHO	409010000	
20507002		3.33500-3	RHO	405010000	
20507003		3.33500-3	RHO	405020000	
20507004		6.84000-2	RHO	415010000	
20507005		8.38000-2	RHO	415020000	
20507006		2.24255-1	RHO	415030000	
20507007		2.98987-1	RHO	415040000	
20507008		2.24255-1	RHO	415050000	

20507009 7.32000-2 RHO 415060000
 20507010 1.42000-2 RHO 420010000
 20507011 1.42000-2 RHO 420020000
 20507012 2.12609-3 RHO 430010000

* 071 REACTOR VESSEL TOTAL MASS

20507100	RVMASS	SUM	1.0	0.0	1
20507101	0.0	1.0	CNTRLVAR	65	
20507103		1.0	CNTRLVAR	67	

* 072 PCS TOTAL MASS

20507200	PCSMASS	SUM	1.0	0.0	1
20507201	0.0	1.0	CNTRLVAR	61	
20507202		1.0	CNTRLVAR	62	
20507203		1.0	CNTRLVAR	63	
20507204		1.0	CNTRLVAR	64	
20507205		1.0	CNTRLVAR	68	
20507206		1.0	CNTRLVAR	69	
20507207		1.0	CNTRLVAR	70	
20507208		1.0	CNTRLVAR	71	

-----1-----1-----1-----1-----1-----1-----1-----
 * RUN STATISTICS DATA

20507800	OR	SUM	1.	0.	0
20507801	0		CNTRLVAR	79	
20507900	NB	SUM	1.	0.	0
20507901	0		CNTRLVAR	79	
20508100	TSTEP	SUM	1.	0.	0
20508101	0	-1.	CNTRLVAR	78	
20508102		1.	CNTRLVAR	79	

* GENERAL TABLE DATA

-----1-----1-----1-----1-----1-----1-----1-----

TABLE NUMBER	DESCRIPTION
900	REACTOR POWER VS TIME AFTER SCRAM

20290000	POWER	502	1.0	36.0+6
20290001	0	1.0		
20290002	0.0	1.0		
20290003	0.1	0.900689	* FROM L2-3 POSTTEST	
20290004	0.2	0.274300		
20290005	0.3	0.153171		
20290006	0.4	0.110821		
20290007	0.5	0.091625		
20290008	0.6	0.083212		
20290009	0.8	0.073556		
20290010	1.0	0.062500		
20290011	1.5	0.063089		
20290012	2.0	0.059854		
20290013	3.0	0.057265		
20290014	4.0	0.055204		
20290015	6.0	0.052085		
20290016	8.0	0.049776		

1351501	0.000000E+00	2.500000E-01
1351502	2.000000E-01	2.800000E-01
1351503	4.000000E-01	3.400000E-01
1351504	4.118000E-01	2.768000E-01
1351505	5.976300E-01	4.584000E-01
1351506	7.934670E-01	6.992000E-01
1351507	1.000000E+00	1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 6		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1351600	1	6
1351601	0.000000E+00	9.342790E-01
1351602	9.109900E-02	9.229000E-01
1351603	1.865090E-01	8.963000E-01
1351604	2.717620E-01	8.750000E-01
1351605	4.558720E-01	8.433000E-01
1351606	5.744060E-01	8.355000E-01
1351607	7.405760E-01	8.466000E-01
1351608	7.666190E-01	8.469000E-01
1351609	8.714710E-01	8.838000E-01
1351610	1.000000E+00	1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 7		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1351700	1	7
1351701	-1.000000E+00	-1.000000E+00
1351702	-8.000000E-01	-6.300000E-01
1351703	-6.000000E-01	-3.000000E-01
1351704	-4.000000E-01	-5.000000E-02
1351705	-2.000000E-01	1.500000E-01
1351706	0.000000E+00	2.500000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 8		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1351800	1	8
1351801	-1.000000E+00	-1.000000E+00
1351802	-8.000000E-01	-9.700000E-01
1351803	-6.000000E-01	-9.500000E-01
1351804	-4.000000E-01	-8.800000E-01
1351805	-2.000000E-01	-8.000000E-01
1351806	0.000000E+00	-6.700000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* SINGLE PHASE TORQUE DATA		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 1		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1351900	2	1
1351901	0.000000E+00	6.032000E-01
1351902	1.930000E-01	6.325000E-01
1351903	3.930000E-01	7.369000E-01
1351904	5.955200E-01	8.331000E-01
1351905	7.978200E-01	9.229000E-01
1351906	1.000000E+00	1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 2		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1352000	2	2
1352001	0.000000E+00	-6.700000E-01
1352002	4.000000E-01	-2.500000E-01
1352003	5.000000E-01	1.500000E-01
1352004	7.37250E-01	5.265860E-01

1352005	7.680490E-01	6.065940E-01
1352006	8.672300E-01	7.436600E-01
1352007	1.000000E+00	1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 3		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1352100	2	3
1352101	-1.000000E+00	1.984300E+00
1352102	-8.009600E-01	1.394000E+00
1352103	-6.063800E-01	1.097500E+00
1352104	-4.068600E-01	8.220000E-01
1352105	-1.992800E-01	6.648000E-01
1352106	0.000000E+00	6.032000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 4		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1352200	2	4
1352201	-1.000000E+00	1.984300E+00
1352202	-8.223400E-01	1.830800E+00
1352203	-6.337100E-01	1.682400E+00
1352204	-4.585300E-01	1.557000E+00
1352205	-2.670230E-01	1.436200E+00
1352206	-1.761070E-01	1.387900E+00
1352207	-8.931000E-02	1.348100E+00
1352208	0.000000E+00	1.233610E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 5		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1352300	2	5
1352301	0.000000E+00	-4.500000E-01
1352302	4.000000E-01	-2.500000E-01
1352303	5.000000E-01	0.000000E+00
1352304	1.000000E+00	3.569000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 6		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1352400	2	6
1352401	0.000000E+00	1.233610E+00
1352402	9.064300E-02	1.196500E+00
1352403	1.885690E-01	1.109600E+00
1352404	2.734700E-01	1.041600E+00
1352405	4.586690E-01	8.958000E-01
1352406	5.744800E-01	7.807000E-01
1352407	7.381600E-01	6.134000E-01
1352408	7.685200E-01	5.849000E-01
1352409	8.700570E-01	4.877000E-01
1352410	1.000000E+00	3.569000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 7		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1352500	2	7
1352501	-1.000000E+00	-1.000000E+00
1352502	-3.000000E-01	-9.000000E-01
1352503	-1.000000E-01	-5.000000E-01
1352504	0.000000E+00	-4.500000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 8		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1352600	2	8
1352601	-1.000000E+00	-1.000000E+00
1352602	-2.500000E-01	-9.000000E-01

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1352603 -8.000000E-02 -8.000000E-01
1352604 0.000000E+00 -6.700000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* TWO - PHASE MULTIPLIER DATA FROM L3-6 TEST DATA
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1353000 0
1353001 0.000000E+00 0.000000E+00
1353002 1.000000E-01 0.000000E+00
1353003 2.000000E-01 1.000000E-01
1353004 3.000000E-01 2.000000E-01
1353005 3.500000E-01 3.000000E-01
1353006 4.000000E-01 6.000000E-01
1353007 5.000000E-01 6.000000E-01
1353008 6.000000E-01 6.000000E-01
1353009 7.000000E-01 6.000000E-01
1353010 8.000000E-01 5.000000E-01
1353011 9.000000E-01 3.000000E-01
1353012 1.000000E+00 0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1353100 0
1353101 0.000000E+00 0.000000E+00
1353102 1.000000E-01 0.000000E+00
1353103 2.000000E-01 1.000000E-01
1353104 3.000000E-01 3.000000E-01
1353105 3.500000E-01 5.000000E-01
1353106 4.000000E-01 7.500000E-01
1353107 5.000000E-01 7.500000E-01
1353108 6.000000E-01 7.500000E-01
1353109 7.000000E-01 7.500000E-01
1353110 8.000000E-01 7.500000E-01
1353111 9.000000E-01 5.000000E-01
1353112 1.000000E+00 0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* PUMP 2-PHASE DIFFERENCE DATA
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 1
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1354100 1 1
1354101 0.000000E+00 1.000000E+00
1354102 1.000000E+00 1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 2
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1354200 1 2
1354201 0.000000E+00 1.000000E+00
1354202 1.000000E+00 1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 3
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1354300 1 3
1354301 -1.000000E+00 -1.160000E+00
1354302 -9.000000E-01 -1.240000E+00
1354303 -8.000000E-01 -1.770000E+00
1354304 -7.000000E-01 -2.360000E+00
1354305 -6.000000E-01 -2.790000E+00
1354306 -5.000000E-01 -2.910000E+00
1354307 -4.000000E-01 -2.670000E+00

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1354308	-2.500000E-01	-1.690000E+00
1354309	-1.000000E-01	-5.000000E-01
1354310	0.000000E+00	0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 4		
*-----1-----1-----1-----1-----1-----1-----1-----		
1354400	1	4
1354401	-1.000000E+00	-1.160000E+00
1354402	-9.000000E-01	-7.800000E-01
1354403	-8.000000E-01	-5.000000E-01
1354404	-7.000000E-01	-3.100000E-01
1354405	-6.000000E-01	-1.700000E-01
1354406	-5.000000E-01	-8.000000E-02
1354407	-3.500000E-01	0.000000E+00
1354408	-2.000000E-01	5.000000E-02
1354409	-1.000000E-01	8.000000E-02
1354410	0.000000E+00	1.100000E-01
*-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 5		
*-----1-----1-----1-----1-----1-----1-----1-----		
1354500	1	5
1354501	0.000000E+00	0.000000E+00
1354502	2.000000E-01	-3.400000E-01
1354503	4.000000E-01	-6.500000E-01
1354504	6.000000E-01	-9.300000E-01
1354505	8.000000E-01	-1.190000E+00
1354506	1.000000E+00	-1.470000E+00
*-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 6		
*-----1-----1-----1-----1-----1-----1-----1-----		
1354600	1	6
1354601	0.000000E+00	1.100000E-01
1354602	1.000000E-01	1.300000E-01
1354603	2.500000E-01	1.500000E-01
1354604	4.000000E-01	1.300000E-01
1354605	5.000000E-01	7.000000E-02
1354606	6.000000E-01	-4.000000E-02
1354607	7.000000E-01	-2.300000E-01
1354608	8.000000E-01	-5.100000E-01
1354609	9.000000E-01	-9.100000E-01
1354610	1.000000E+00	-1.470000E+00
*-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 7		
*-----1-----1-----1-----1-----1-----1-----1-----		
1354700	1	7
1354701	-1.000000E+00	0.000000E+00
1354702	0.000000E+00	0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 8		
*-----1-----1-----1-----1-----1-----1-----1-----		
1354800	1	8
1354801	-1.000000E+00	0.000000E+00
1354802	0.000000E+00	0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 1		
*-----1-----1-----1-----1-----1-----1-----1-----		
1354900	2	1
1354901	0.000000E+00	1.000000E+00
1354906	1.000000E+00	1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 2		

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*-----1-----1-----1-----1-----1-----1-----1-----1-----
1355000  2          2
1355001  0.000000E+00  1.000000E+00
1355007  1.000000E+00  1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 3
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1355100  2          3
1355101  -1.000000E+00  1.984300E+00
1355102  -8.009600E-01  1.394000E+00
1355103  -6.063800E-01  1.097500E+00
1355104  -4.068600E-01  8.220000E-01
1355105  -1.992800E-01  6.648000E-01
1355106  0.000000E+00  6.032000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 4
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1355200  2          4
1355201  -1.000000E+00  1.984300E+00
1355202  -8.223400E-01  1.830800E+00
1355203  -6.337100E-01  1.682400E+00
1355204  -4.585300E-01  1.557000E+00
1355205  -2.670230E-01  1.436200E+00
1355206  -1.761070E-01  1.387900E+00
1355207  -8.931000E-02  1.348100E+00
1355208  0.000000E+00  1.233610E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 5
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1355300  2          5
1355301  0.000000E+00  -4.500000E-01
1355302  4.000000E-01  -2.500000E-01
1355303  5.000000E-01  0.000000E+00
1355304  1.000000E+00  3.569000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 6
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1355400  2          6
1355401  0.000000E+00  1.233610E+00
1355402  9.064300E-02  1.196500E+00
1355403  1.885690E-01  1.109600E+00
1355404  2.734700E-01  1.041600E+00
1355405  4.586690E-01  8.958000E-01
1355406  5.744800E-01  7.807000E-01
1355407  7.381600E-01  6.134000E-01
1355408  7.685200E-01  5.849000E-01
1355409  8.700570E-01  4.877000E-01
1355410  1.000000E+00  3.569000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 7
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1355500  2          7
1355501  -1.000000E+00  -1.000000E+00
1355502  -3.000000E-01  -9.000000E-01
1355503  -1.000000E-01  -5.000000E-01
1355504  0.000000E+00  -4.500000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 8
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1355600  2          8
1355601  -1.000000E+00  -1.000000E+00

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1355602 -2.500000E-01 -9.000000E-01
1355603 -8.000000E-02 -8.000000E-01
1355604 0.000000E+00 -6.700000E-01
* $$$ REMOVE ALL REMAINING DATA CARDS AFTER ACHIEVING STEADY STATE
* $* $* $* $* $* $* $* $* $* $* $* $* $* $* $* $* $* $* $* $* $*
*
* PUMP DATA
*
* -----1-----1-----1-----1-----1-----1-----1-----1-----
* SINGLE PHASE HEAD CURVES
* -----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 1
* -----1-----1-----1-----1-----1-----1-----1-----1-----
1651100 1 1
1651101 0.000000E+00 1.403300E+00
1651102 1.906100E-01 1.363600E+00
1651103 3.896300E-01 1.318600E+00
1651104 5.939600E-01 1.232800E+00
1651105 7.902000E-01 1.133600E+00
1651106 1.000000E+00 1.000000E+00
* -----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 2
* -----1-----1-----1-----1-----1-----1-----1-----1-----
1651200 1 2
1651201 0.000000E+00 -6.700000E-01
1651202 2.000000E-01 -5.000000E-01
1651203 4.000000E-01 -2.500000E-01
1651204 5.755400E-01 0.000000E+00
1651205 7.443200E-01 2.583000E-01
1651206 7.734800E-01 3.778000E-01
1651207 8.631300E-01 6.326000E-01
1651208 1.000000E+00 1.000000E+00
* -----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 3
* -----1-----1-----1-----1-----1-----1-----1-----1-----
1651300 1 3
1651301 -1.000000E+00 2.472200E+00
1651302 -8.057400E-01 2.047400E+00
1651303 -6.069000E-01 1.831000E+00
1651304 -4.068300E-01 1.624000E+00
1651305 -2.001710E-01 1.470500E+00
1651306 0.000000E+00 1.403600E+00
* -----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 4
* -----1-----1-----1-----1-----1-----1-----1-----1-----
1651400 1 4
1651401 -1.000000E+00 2.472200E+00
1651402 -8.229700E-01 1.996800E+00
1651403 -6.333200E-01 1.589700E+00
1651404 -4.553400E-01 1.327900E+00
1651405 -2.710900E-01 1.194900E+00
1651406 -1.771600E-01 1.060500E+00
1651407 -9.073000E-02 1.015600E+00
1651408 0.000000E+00 9.342790E-01
* -----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 5
* -----1-----1-----1-----1-----1-----1-----1-----1-----
1651500 1 5
1651501 0.000000E+00 2.500000E-01
1651502 2.000000E-01 2.800000E-01
1651503 4.000000E-01 3.400000E-01

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1651504	4.118000E-01	2.768000E-01
1651505	5.976300E-01	4.584000E-01
1651506	7.934670E-01	6.992000E-01
1651507	1.000000E+00	1.000000E+00
* HEAD CURVE NO. 6		
1651600	1	6
1651601	0.000000E+00	9.342790E-01
1651602	9.109900E-02	9.229000E-01
1651603	1.865090E-01	8.963000E-01
1651604	2.717620E-01	8.750000E-01
1651605	4.558720E-01	8.433000E-01
1651606	5.744060E-01	8.355000E-01
1651607	7.405760E-01	8.466000E-01
1651608	7.666190E-01	8.469000E-01
1651609	8.714710E-01	8.838000E-01
1651610	1.000000E+00	1.000000E+00
* HEAD CURVE NO. 7		
1651700	1	7
1651701	-1.000000E+00	-1.000000E+00
1651702	-8.000000E-01	-6.300000E-01
1651703	-6.000000E-01	-3.000000E-01
1651704	-4.000000E-01	-5.000000E-02
1651705	-2.000000E-01	1.500000E-01
1651706	0.000000E+00	2.500000E-01
* HEAD CURVE NO. 8		
1651800	1	8
1651801	-1.000000E+00	-1.000000E+00
1651802	-8.000000E-01	-9.700000E-01
1651803	-6.000000E-01	-9.500000E-01
1651804	-4.000000E-01	-8.800000E-01
1651805	-2.000000E-01	-8.000000E-01
1651806	0.000000E+00	-6.700000E-01
* SINGLE PHASE TORQUE DATA		
* TORQUE CURVE NO. 1		
1651900	2	1
1651901	0.000000E+00	6.032000E-01
1651902	1.930000E-01	6.325000E-01
1651903	3.930000E-01	7.369000E-01
1651904	5.955200E-01	8.331000E-01
1651905	7.978200E-01	9.229000E-01
1651906	1.000000E+00	1.000000E+00
* TORQUE CURVE NO. 2		
1652000	2	2
1652001	0.000000E+00	-6.700000E-01
1652002	4.000000E-01	-2.500000E-01
1652003	5.000000E-01	1.500000E-01
1652004	7.372550E-01	5.265860E-01
1652005	7.680490E-01	6.065940E-01
1652006	8.672300E-01	7.43E500E-01
1652007	1.000000E+00	1.000000E+00

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*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 3
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1652100  2          3
1652101 -1.000000E+00  1.984300E+00
1652102 -8.009600E-01  1.394000E+00
1652103 -6.063800E-01  1.097500E+00
1652104 -4.068600E-01  8.220000E-01
1652105 -1.992800E-01  6.648000E-01
1652106  0.000000E+00  6.032000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 4
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1652200  2          4
1652201 -1.000000E+00  1.984300E+00
1652202 -8.223400E-01  1.830800E+00
1652203 -6.337100E-01  1.682400E+00
1652204 -4.585300E-01  1.557000E+00
1652205 -2.670230E-01  1.436200E+00
1652206 -1.761070E-01  1.387900E+00
1652207 -8.931000E-02  1.348100E+00
1652208  0.000000E+00  1.233610E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 5
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1652300  2          5
1652301  0.000000E+00 -4.500000E-01
1652302  4.000000E-01 -2.500000E-01
1652303  5.000000E-01  0.000000E+00
1652304  1.000000E+00  3.569000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 6
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1652400  2          6
1652401  0.000000E+00  1.733610E+00
1652402  9.064300E-02  1.196500E+00
1652403  1.885690E-01  1.109600E+00
1652404  2.734700E-01  1.041600E+00
1652405  4.586690E-01  8.958000E-01
1652406  5.744800E-01  7.807000E-01
1652407  7.381600E-01  6.134000E-01
1652408  7.685200E-01  5.849000E-01
1652409  8.700570E-01  4.877000E-01
1652410  1.000000E+00  3.569000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 7
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1652500  2          7
1652501 -1.000000E+00 -1.000000E+00
1652502 -3.000000E-01 -9.000000E-01
1652503 -1.000000E-01 -5.000000E-01
1652504  0.000000E+00 -4.500000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 8
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1652600  2          8
1652601 -1.000000E+00 -1.000000E+00
1652602 -2.500000E-01 -9.000000E-01
1652603 -8.000000E-02 -8.000000E-01
1652604  0.000000E+00 -6.700000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----

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* TWO - PHASE MULTIPLIER DATA FROM L3-6 TEST DATA

*-----1-----1-----1-----1-----1-----1-----1-----

* HEAD CURVE

*-----1-----1-----1-----1-----1-----1-----1-----

1653000	0	
1653001	0.000000E+00	0.000000E+00
1653002	1.000000E-01	0.000000E+00
1653003	2.000000E-01	1.000000E-01
1653004	3.000000E-01	2.000000E-01
1653005	3.500000E-01	3.000000E-01
1653006	4.000000E-01	6.000000E-01
1653007	5.000000E-01	6.000000E-01
1653008	6.000000E-01	6.000000E-01
1653009	7.000000E-01	6.000000E-01
1653010	8.000000E-01	5.000000E-01
1653011	9.000000E-01	3.000000E-01
1653012	1.000000E+00	0.000000E+00

*-----1-----1-----1-----1-----1-----1-----1-----

* TORQUE CURVE

*-----1-----1-----1-----1-----1-----1-----1-----

1653100	0	
1653101	0.000000E+00	0.000000E+00
1653102	1.000000E-01	0.000000E+00
1653103	2.000000E-01	1.000000E-01
1653104	3.000000E-01	3.000000E-01
1653105	3.500000E-01	5.000000E-01
1653106	4.000000E-01	7.500000E-01
1653107	5.000000E-01	7.500000E-01
1653108	6.000000E-01	7.500000E-01
1653109	7.000000E-01	7.500000E-01
1653110	8.000000E-01	7.500000E-01
1653111	9.000000E-01	5.000000E-01
1653112	1.000000E+00	0.000000E+00

*-----1-----1-----1-----1-----1-----1-----1-----

* PUMP 2-PHASE DIFFERENCE DATA

*-----1-----1-----1-----1-----1-----1-----1-----

* HEAD CURVE NO. 1

*-----1-----1-----1-----1-----1-----1-----1-----

1654100	1	1
1654101	0.000000E+00	1.000000E+00
1654102	1.000000E+00	1.000000E+00

*-----1-----1-----1-----1-----1-----1-----1-----

* HEAD CURVE NO. 2

*-----1-----1-----1-----1-----1-----1-----1-----

1654200	1	2
1654201	0.000000E+00	1.000000E+00
1654202	1.000000E+00	1.000000E+00

*-----1-----1-----1-----1-----1-----1-----1-----

* HEAD CURVE NO. 3

*-----1-----1-----1-----1-----1-----1-----1-----

1654300	1	3
1654301	-1.000000E+00	-1.160000E+00
1654302	-9.000000E-01	-1.240000E+00
1654303	-8.000000E-01	-1.770000E+00
1654304	-7.000000E-01	-2.360000E+00
1654305	-6.000000E-01	-2.790000E+00
1654306	-5.000000E-01	-2.910000E+00
1654307	-4.000000E-01	-2.670000E+00
1654308	-2.500000E-01	-1.690000E+00
1654309	-1.000000E-01	-5.000000E-01
1654310	0.000000E+00	0.000000E+00

*-----1-----1-----1-----1-----1-----1-----1-----1-----

* HEAD CURVE NO. 4

*-----1-----1-----1-----1-----1-----1-----1-----1-----

1654400	1	4
1654401	-1.000000E+00	-1.160000E+00
1654402	-9.000000E-01	-7.800000E-01
1654403	-8.000000E-01	-5.000000E-01
1654404	-7.000000E-01	-3.100000E-01
1654405	-6.000000E-01	-1.700000E-01
1654406	-5.000000E-01	-8.000000E-02
1654407	-3.500000E-01	0.000000E+00
1654408	-2.000000E-01	5.000000E-02
1654409	-1.000000E-01	8.000000E-02
1654410	0.000000E+00	1.100000E-01

*-----1-----1-----1-----1-----1-----1-----1-----1-----

* HEAD CURVE NO. 5

*-----1-----1-----1-----1-----1-----1-----1-----1-----

1654500	1	5
1654501	0.000000E+00	0.000000E+00
1654502	2.000000E-01	-3.400000E-01
1654503	4.000000E-01	-6.500000E-01
1654504	6.000000E-01	-9.300000E-01
1654505	8.000000E-01	-1.190000E+00
1654506	1.000000E+00	-1.470000E+00

*-----1-----1-----1-----1-----1-----1-----1-----1-----

* HEAD CURVE NO. 6

*-----1-----1-----1-----1-----1-----1-----1-----1-----

1654600	1	6
1654601	0.000000E+00	1.100000E-01
1654602	1.000000E-01	1.300000E-01
1654603	2.500000E-01	1.500000E-01
1654604	4.000000E-01	1.300000E-01
1654605	5.000000E-01	7.000000E-02
1654606	6.000000E-01	-4.000000E-02
1654607	7.000000E-01	-2.300000E-01
1654608	8.000000E-01	-5.100000E-01
1654609	9.000000E-01	-9.100000E-01
1654610	1.000000E+00	-1.470000E+00

*-----1-----1-----1-----1-----1-----1-----1-----1-----

* HEAD CURVE NO. 7

*-----1-----1-----1-----1-----1-----1-----1-----1-----

1654700	1	7
1654701	-1.000000E+00	0.000000E+00
1654702	0.000000E+00	0.000000E+00

*-----1-----1-----1-----1-----1-----1-----1-----1-----

* HEAD CURVE NO. 8

*-----1-----1-----1-----1-----1-----1-----1-----1-----

1654800	1	8
1654801	-1.000000E+00	0.000000E+00
1654802	0.000000E+00	0.000000E+00

*-----1-----1-----1-----1-----1-----1-----1-----1-----

* TORQUE CURVE NO. 1

*-----1-----1-----1-----1-----1-----1-----1-----1-----

1654900	2	1
1654901	0.000000E+00	1.000000E+00
1654906	1.000000E+00	1.000000E+00

*-----1-----1-----1-----1-----1-----1-----1-----1-----

* TORQUE CURVE NO. 2

*-----1-----1-----1-----1-----1-----1-----1-----1-----

1655000	2	2
1655001	0.000000E+00	1.000000E+00

1655007	1.000000E+00	1.000000E+00
* TORQUE CURVE NO. 3		
1655100	2	3
1655101	-1.000000E+00	1.984300E+00
1655102	-8.009600E-01	1.394000E+00
1655103	-6.063800E-01	1.097500E+00
1655104	-4.068600E-01	8.220000E-01
1655105	-1.992800E-01	6.648000E-01
1655106	0.000000E+00	6.032000E-01
* TORQUE CURVE NO. 4		
1655200	2	4
1655201	-1.000000E+00	1.984300E+00
1655202	-8.223400E-01	1.830800E+00
1655203	-6.337100E-01	1.682400E+00
1655204	-4.585300E-01	1.557000E+00
1655205	-2.670230E-01	1.436200E+00
1655206	-1.761070E-01	1.387900E+00
1655207	-8.931000E-02	1.348100E+00
1655208	0.000000E+00	1.233610E+00
* TORQUE CURVE NO. 5		
1655300	2	5
1655301	0.000000E+00	-4.500000E-01
1655302	4.000000E-01	-2.500000E-01
1655303	5.000000E-01	0.000000E+00
1655304	1.000000E+00	3.569000E-01
* TORQUE CURVE NO. 6		
1655400	2	6
1655401	0.000000E+00	1.233610E+00
1655402	9.064300E-02	1.196500E+00
1655403	1.885690E-01	1.109600E+00
1655404	2.734700E-01	1.041600E+00
1655405	4.586690E-01	8.958000E-01
1655406	5.744800E-01	7.807000E-01
1655407	7.381600E-01	6.134000E-01
1655408	7.685200E-01	5.849000E-01
1655409	8.700570E-01	4.877000E-01
1655410	1.000000E+00	3.569000E-01
* TORQUE CURVE NO. 7		
1655500	2	7
1655501	-1.000000E+00	-1.000000E+00
1655502	-3.000000E-01	-9.000000E-01
1655503	-1.000000E-01	-5.000000E-01
1655504	0.000000E+00	-4.500000E-01
* TORQUE CURVE NO. 8		
1655600	2	8
1655601	-1.000000E+00	-1.000000E+00
1655602	-2.500000E-01	-9.000000E-01
1655603	-8.000000E-02	-8.000000E-01
1655604	0.000000E+00	-6.700000E-01

S

* STEADY STATE CONTROL SYSTEM

*-----1-----1-----1-----1-----1-----1-----1-----1-----

* PRIMARY COOLANT PUMP SPEED CONTROLLERS

*-----1-----1-----1-----1-----1-----1-----1-----1-----

* CALCULATE MASS FLOW ERROR

*-----1-----1-----1-----

20590100 MSSERR SUM 1.0 0.0 1
20590101 199.00 -1.0 MFLOWJ 100010000

*-----1-----1-----1-----

* PUMP 1 SPEED

-----1-----1-----1-----

20590200 PCP1SPD INTEGRAL 0.34482 133.000 1
20590201 CNTRLVAR 901

*-----1-----1-----1-----

* PCP1 PUMP VELOCITY TABLE

*-----1-----1-----1-----

1356100 510 CNTRLVAR 902
1356101 0.0 0.0
1356102 369.0 369.0

*-----1-----1-----1-----

* MODIFY PCP1 PUMP DATA

*-----1-----1-----1-----

1350301 0 0 0 -1 0 695 0

*-----1-----1-----1-----

* PUMP 2 SPEED

-----1-----1-----1-----

20590300 PCP2SPD INTEGRAL 0.34482 139.790 1
20590301 CNTRLVAR 901

*-----1-----1-----1-----

* PCP2 PUMP VELOCITY TABLE

*-----1-----1-----1-----

1656100 510 CNTRLVAR 903
1656101 0.0 0.0
1656102 369.0 369.0

*-----1-----1-----1-----

* MODIFY PCP2 PUMP DATA

*-----1-----1-----1-----

1650301 0 0 0 -1 0 697 0

*-----1-----1-----1-----1-----1-----1-----1-----

* PRESSURIZER SPRAY VALVE CONTROLLER

*-----1-----1-----1-----1-----1-----1-----1-----

*-----1-----1-----1-----1-----1-----1-----1-----

* SPRAY LINE

*-----1-----1-----1-----1-----1-----1-----1-----

4300000 "SPRAY " BRANCH
4300001 1 0
4300101 0.0003363 6.322 0.0 0.0 90.0 2.9905
4300102 4.0-5 0.0 00
4300200 0 15037900. 1238620. 2459550. .00000000
4301101 150000000 430000000 0.0 0.0 0.0 0000
4301201 .777018-4 .777018-4 0.0

*-----1-----1-----1-----1-----1-----1-----1-----

* SPRAY VALVE

*-----1-----1-----1-----1-----1-----1-----1-----

4350000 "SPRVLV " VALVE
4350101 430010000 415010000 3.3451E-4 1.5432E01 1.5432E01 0100
4350201 0 .00000000 .00000000 0.0
4350300 SRVVLV


```

4350301 904 999
*-----1-----1-----1-----
* SPRAY VALVE POSITION CALCULATOR
*-----1-----1-----1-----
20590400 SPRAY SUM -1.0 0.0 1 * CONTIN
+ 3 0.0 1.0
20590401 15.06+6 -1.0 P 420010000
*-----1-----1-----1-----
* POSITION VS AREA TABLE
*-----1-----1-----1-----
20299900 NORNAREA
20299901 0.0 0.0
20299902 0.0001 0.0
20299903 1.0 1.0
*-----1-----1-----1-----
* PRESSURIZER HEATERS IN INITIALIZATION
*-----1-----1-----1-----
* PRESSURIZER HEATER TRIPS
*-----1-----1-----1-----
* LT 693 CYLCING HEATERS CARD 2241700
0000585 P 420010000 GT NULL 0 15.06+6 N
0000586 P 420010000 LT NULL 0 15.0599+6 N
0000666 586 OR 693 N
0000667 -585 AND 666 N
0000693 -503 AND 667 N
*-----1-----1-----1-----
* LT 694 BACKUP HEATERS CARD 20241800
0000587 P 420010000 GT NULL 0 15.01+6 N
0000588 P 420010000 LT NULL 0 15.0099+6 N
0000668 588 OR 694 N
0000669 -587 AND 668 N
0000694 -503 AND 669 N
*-----1-----1-----1-----
* PRESSURIZER HEATERS
*-----1-----1-----1-----
14172000 2 9 2 1 0.0
14172100 0 1
14172101 8 8.3820E-3
14172201 4 8
14172301 1.0 8
14172401 615.0 9
14172501 0 0 0 1 5.4864 1
14172502 0 0 0 1 1.8288 2
14172601 415040000 0 1 1 5.4864 1
14172602 415040000 0 1 1 1.8288 2
14172701 417 1.0 0.0 0.0 1 * CYCLING
14172702 418 1.0 0.0 0.0 2 * BACKUP
14172901 0 1.6764E-2 1.6764E-2 5.4864 1
14172902 0 1.6764E-2 1.6764E-2 1.8288 2
*-----1-----1-----1-----
* PRESSURIZER CYCLING HEATERS
*-----1-----1-----1-----
20241700 POWER 693
20241701 0.0 0.0
20241702 1.0 3.6+4
*-----1-----1-----1-----
* PRESSURIZER BACKUP HEATERS
*-----1-----1-----1-----
20241800 POWER 694
20241801 0.0 0.0
20241802 1.0 1.2+4

```

```

*-----1-----1-----1-----1-----1-----1-----1-----1-----
* PRESSURIZER LEVEL CONTROL USING CHARGING AND LETDOWN COMPONENTS
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* MODIFY PZR LEVEL CONTROL VARIABLE
*-----1-----1-----1-----1-----
20500206      0.1249  VOIDF      415050000
205000      0.02477  VOIDF      420010000
205002      0.02477  VOIDF      420020000
*-----1-----1-----1-----1-----
* CHARGING RESERVIOR
*-----1-----1-----1-----1-----
9800000  "CHRG RESRV"      TMDPVOL
9800101  1.0      1.0      0.0      0.0      0.0
9800102  4.0-5      0.0      00
9800200  3
9800201  0.0      2.07+07  559.2
*-----1-----1-----1-----1-----
* CHARGING VALVE
*-----1-----1-----1-----1-----
9850000  "CHRG VALVE"      VALVE
9850101  980000000 185000000 3.8E-05  0.0      0.0      0100
9850201  0      .608458-3 .608458-3 0.0
9850300  SRVVLV
9850301  905      999
*-----1-----1-----1-----1-----
* CHARGING VALVE POSITION CALCULATOR
*-----1-----1-----1-----1-----
20590500  CHARGE  SUM      7.7      0.0      1      *CONTIN
+      3      0.0      1.0
20590501  1.18      -1.0      CNTRLVAR 2
*-----1-----1-----1-----1-----
* LETDOWN SINK
*-----1-----1-----1-----1-----
9900000  "LTDWN SINK"      TMDPVOL
9900101  1.0      1.0      0.0      0.0      0.0
9900102  4.0-5      0.0      00
9900200  3
9900201  0.0      1.4+7      553.2
*-----1-----1-----1-----1-----
* LETDOWN VALVE
*-----1-----1-----1-----1-----
9950000  "LTDWN VLV "      VALVE
9950101  185000000 990000000 2.5-5  0.0      0.0      0100
9950201  0      .00000000 .00000000 0.0
9950300  SRVVLV
9950301  906      999
*-----1-----1-----1-----1-----
* LETDOWN VALVE POSITION CALCULATOR
*-----1-----1-----1-----1-----
20590600  LETDOWN  SUM      -7.7      0.0      1      *CONTIN
+      3      0.0      1.0
20590601  1.1430      -1.0      CNTRLVAR 2
*-----1-----1-----1-----1-----
* STEAM VALVE CONTROLLER
*-----1-----1-----1-----1-----
* CHANGES TO STEAM VALVE
*-----1-----1-----1-----1-----
5400201  0      13.604000 13.604000 0.0
5400300  SRVVLV
5400301  910      540
20254000  NORMAREA

```

```

20254001 0.0      0.0
20254002 0.0001  0.0
20254003 1.0      1.0
*-----1-----1-----1-----
* COMPUTE DELTA T ERROR
*-----1-----1-----1-----
20590700 "DELTA T" SUM      1.0      0.0      1
20590701 560.7     -1.      TEMPF    185010000
*-----1-----1-----1-----
* FILTER DELTA T THRU DEADBAND
*-----1-----1-----1-----
20590800 DEADBAND FUNCTION 1.0      0.0      1
20590801 CNTRLVAR 907      908
20290800 RFAC-T
20290801 -100.     -100.
20290802 -0.1      -0.1
20290803 -0.1      0.0
20290804 0.1      0.0
20290805 0.1      0.1
20290806 100.     100.
*-----1-----1-----1-----
* INTEGRATE DELTA T ERROR
*-----1-----1-----1-----
20590900 "INT D T" INTEGRAL 1.0      0.0      1
20590901 CNTRLVAR 908
*-----1-----1-----1-----
* STEAM VALVE POSITION CALCULATOR
*-----1-----1-----1-----
20591000 TCONTROL SUM      1.0      0.44405  0      *CONTI
*      3      0.40      0.55
20591001 0.44405 -0.0564 CNTRLVAR 908
20591002 -0.0059 CNTRLVAR 909
*-----1-----1-----1-----1-----1-----1-----
* SIMPLIFIED FEED SYSTEM CONTROLLER
*-----1-----1-----1-----1-----1-----1-----
* SIMPLIFIED FEED LOGIC
*-----1-----1-----1-----1-----1-----1-----
20591100 SGLVLERR SUM      1.0      0.0      1
20591101 3.11     -1.0      CNTRLVAR 001
20591200 FEEDFLOW SUM      1.0      0.0      1
20591201 0.0      1.0      MFCWJ    540000000
20591202      48.4      CNTRLVAR 911
*-----1-----1-----1-----1-----1-----1-----
* REPLACE FEED JUNCTION TABLE
*-----1-----1-----1-----1-----1-----1-----
5660200 1      0      CNTRLVAR 912
5660201 -100.0   19.15   0.0      0.0
5660202 -1.0     0.0     0.0     0.0
5660203 0.0     0.0     0.0     0.0
5660204 50.0    50.0    0.0     0.0
5660205
5660206
5660207
*-----1-----1-----1-----1-----1-----1-----
* REPLACE REACTOR POWER TABLE
*-----1-----1-----1-----1-----1-----1-----
. . . . . RELAP5 END CARD

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Appendix C. A Base Case Input Deck for a Transient Calculation

```

L23BTR2,T5000.
/USER
ATTACH,RSTIN=L23R2.
ATTACH,STH2XT,RE364BX.
DEFINE,RSTPLT=L23RSTT.
FILE,RSTIN,SBF=NO.
FILE,RSTPLT,SBF=NO.
*DEFINE.PLOTFL=L23RPL0.
RFL,CM=300000,FC=200.
REDUCE(-)
RE364BX,,*PL=50000.
/EOB
= LOFT L2-3 BASE TRANSIENT TO 100 SEC
0000100 RESTART TRANSNT
0000101 RUN
0000103 5237
0000105 5.0 10.0
*-----1-----1-----1-----1-----1-----1-----1-----
0000201 20.0 1.0-6 0.05 3 2 200 1000
0000202 100.0 1.0-6 0.01 3 10 500 2500
* REMCVE PUMP SPEED CONTROLLERS
*-----1-----1-----1-----1-----1-----1-----1-----
20590100 MSSERR DELETE 0.0 0.0 0.0 0.0 0.0 0.0
20590200 PCP1SPD DELETE 0.0 0.0 0.0 0.0 0.0 0.0
20590300 PCP2SPD DELETE 0.0 0.0 0.0 0.0 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* RENODALIZE PUMP1
*-----1-----1-----1-----1-----1-----1-----1-----
1350000 "PCPUMP1 " PUMP
1350101 0.0 0.4572 0.0991 0.0 90.0 0.317900
1350102 0
1350108 130010000 0.0 0.017 0.017 0000
1350109 140000000 0.0 0.05 0.05 0000
1350200 0 1.49288+7 1.23094+6 2.46151+6 0.
1350201 0 3.0790 3.0790 0.0
1350202 0 3.2641 3.2641 0.0
1350301 0 0 0 -1 -1 0 0
1350302 369.00000 .35501355 .31550000 96.000000 500.60000 1.4310000
1350303 513.60000 .00000000 207.43300 .04440000 19.598700 .00000000
1350310 0.0 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
*
* PUMP DATA
*
*-----1-----1-----1-----1-----1-----1-----1-----
* SINGLE PHASE HEAD CURVES
*-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 1
*-----1-----1-----1-----1-----1-----1-----1-----
1351100 1 1
1351101 0.000000E+00 1.403600E+00
1351102 1.906100E-01 1.363600E+00
1351103 3.896300E-01 1.318600E+00
1351104 5.939600E-01 1.232800E+00
1351105 7.902000E-01 1.133600E+00
1351106 1.000000E+00 1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 2
*-----1-----1-----1-----1-----1-----1-----1-----
1351200 1 2
1351201 0.000000E+00 -6.700000E-01
1351202 2.000000E-01 -5.000000E-01

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1351203	4.000000E-01	-3.500000E-01
1351204	5.755400E-01	0.000000E+00
1351205	7.443200E-01	2.583000E-01
1351206	7.734800E-01	3.778000E-01
1351207	8.631300E-01	4.320000E-01
1351208	1.000000E+00	1.000000E+00

* HEAD CURVE NO. 3

1351300	1	3
1351301	-1.000000E+00	2.472200E-00
1351302	-8.057400E-01	2.047400E+00
1351303	-6.062000E-01	1.831000E+00
1351304	-4.068300E-01	1.624000E+00
1351305	-2.001710E-01	1.470500E+00
1351306	0.000000E+00	1.403500E+00

* HEAD CURVE NO. 4

1351400	1	4
1351401	-1.000000E+00	2.472200E+00
1351402	-8.229700E-01	1.996800E+00
1351403	-6.333200E-01	1.589700E+00
1351404	-4.553400E-01	1.327900E+00
1351405	-2.710900E-01	1.194900E+00
1351406	-1.771600E-01	1.060500E+00
1351407	-9.073000E-02	1.015600E+00
1351408	0.000000E+00	9.342790E-01

* HEAD CURVE NO. 5

1351500	1	5
1351501	0.000000E+00	2.500000E-01
1351502	2.000000E-01	2.800000E-01
1351503	4.000000E-01	3.400000E-01
1351504	4.118000E-01	2.768000E-01
1351505	5.976300E-01	4.584000E-01
1351506	7.934670E-01	6.992000E-01
1351507	1.000000E+00	1.000000E+00

* HEAD CURVE NO. 6

1351600	1	6
1351601	0.000000E+00	9.342790E-01
1351602	9.109900E-02	9.329000E-01
1351603	1.865090E-01	8.963000E-01
1351604	2.717620E-01	8.750000E-01
1351605	4.558720E-01	8.433000E-01
1351606	5.744060E-01	8.355000E-01
1351607	7.405760E-01	8.466000E-01
1351608	7.666190E-01	8.469000E-01
1351609	8.714710E-01	8.838000E-01
1351610	1.000000E+00	1.000000E+00

* HEAD CURVE NO. 7

1351700	1	7
1351701	-1.000000E+00	-1.000000E+00
1351702	-8.000000E-01	-6.000000E-01
1351703	-6.000000E-01	-3.000000E-01
1351704	-4.000000E-01	-5.000000E-02
1351705	-2.000000E-01	1.500000E-01
1351706	0.000000E+00	2.500000E-01


```

*-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 8
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1351800 1 8
1351801 -1.000000E+00 -1.000000E+00
1351802 -8.700000E-01 -9.700000E-01
1351803 -6.000000E-01 -9.500000E-01
1351804 -4.000000E-01 -8.800000E-01
1351805 -2.000000E-01 -8.000000E-01
1351806 0.000000E+00 -6.700000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----
~ SINGLE PHASE TORQUE DATA
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 1
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1351900 2 1
1351901 0.000000E+00 6.032000E-01
1351902 1.930000E-01 6.325000E-01
1351903 3.930000E-01 7.369000E-01
1351904 5.955200E-01 8.331000E-01
1351905 7.978200E-01 9.229000E-01
1351906 1.000000E+00 1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 2
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1352000 2 2
1352001 0.000000E+00 -6.790000E-01
1352002 4.000000E-01 -2.500000E-01
1352003 5.000000E-01 1.500000E-01
1352004 7.372500E-01 5.265800E-01
1352005 7.680490E-01 6.065940E-01
1352006 8.672300E-01 7.436600E-01
1352007 1.000000E+00 1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 3
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1352100 2 3
1352101 -1.900000E+00 1.98430E+00
1352102 -8.009800E-01 1.394000E+00
1352103 -6.063800E-01 1.097500E+00
1352104 -4.068600E-01 8.220000E-01
1352105 -1.992800E-01 6.648000E-01
1352106 0.000000E+00 6.032000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----
~ TORQUE CURVE NO. 4
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1352200 2 4
1352201 -1.000000E+00 1.984300E+00
1352202 -8.223400E-01 1.830870E+00
1352203 -6.337100E-01 1.682400E+00
1352204 -4.585300E-01 1.557070E+00
1352205 -2.670230E-01 1.436270E+00
1352206 -1.761070E-01 1.387900E+00
1352207 -8.931000E-02 1.348100E+00
1352208 0.000000E+00 1.237610E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 5
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1352300 2 5
1352301 0.000000E+00 -4.500000E-01
1352302 4.000000E-01 -2.500000E-01
1352303 5.000000E-01 0.000000E+00
1352304 1.000000E+00 3.569000E-01

```



```

1353112 1.000000E+00 0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* PUMP 2-PHASE DIFFERENCE DATA
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 1
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1354100 1 1
1354101 0.000000E+00 1.000000E+00
1354102 1.000000E+00 1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 2
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1354200 1 2
1354201 0.000000E+00 1.000000E+00
1354202 1.000000E+00 1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 3
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1354300 1 3
1354301 -1.000000E+00 -1.160000E+00
1354302 -9.000000E-01 -1.240000E+00
1354303 -8.000000E-01 -1.770000E+00
1354304 -7.000000E-01 -2.360000E+00
1354305 -6.000000E-01 -2.790000E+00
1354306 -5.000000E-01 -2.910000E+00
1354307 -4.000000E-01 -2.670000E+00
1354308 -2.500000E-01 -1.690000E+00
1354309 -1.000000E-01 -5.000000E-01
1354310 0.000000E+00 0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 4
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1354400 1 4
1354401 -1.000000E+00 -1.160000E+00
1354402 -9.000000E-01 -7.800000E-01
1354403 -8.000000E-01 -5.000000E-01
1354404 -7.000000E-01 -3.100000E-01
1354405 -6.000000E-01 1.700000E-01
1354406 -5.000000E-01 -8.000000E-02
1354407 -3.500000E-01 0.000000E+00
1354408 -2.000000E-01 5.000000E-02
1354409 -1.000000E-01 8.000000E-02
1354410 0.000000E+00 1.100000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 5
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1354500 1 5
1354501 0.000000E+00 0.000000E+00
1354502 2.000000E-01 -3.400000E-01
1354503 4.000000E-01 -6.500000E-01
1354504 6.000000E-01 -9.300000E-01
1354505 8.000000E-01 -1.190000E+00
1354506 1.000000E+00 -1.470000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 6
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1354600 1 6
1354601 0.000000E+00 1.170000E-01
1354602 1.000000E-01 1.300000E-01
1354603 2.500000E-01 1.500000E-01
1354604 4.000000E-01 1.300000E-01
1354605 5.000000E-01 7.000000E-02
1354606 6.000000E-01 -4.000000E-02

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1354608	8.000000E-01	-5.100000E-01
1354609	9.000000E-01	-9.100000E-01
1354610	1.000000E+00	-1.470000E+00
* HEAD CURVE NO. 7		
1354700	1	7
1354701	-1.000000E+00	0.000000E+00
1354702	0.000000E+00	0.000000E+00
* HEAD CURVE NO. 8		
1354800	1	8
1354801	-1.000000E+00	0.000000E+00
1354802	0.000000E+00	0.000000E+00
* TORQUE CURVE NO. 1		
1354900	2	1
1354901	0.000000E+00	1.000000E+00
1354905	1.000000E+00	1.000000E+00
* TORQUE CURVE NO. 2		
1355000	2	2
1355001	0.000000E+00	1.000000E+00
1355007	1.000000E+00	1.000000E+00
* TORQUE CURVE NO. 3		
1355100	2	3
1355101	-1.000000E+00	1.984300E+00
1355102	-8.063600E-01	1.394000E+00
1355103	-6.063800E-01	1.097500E+00
1355104	-4.068600E-01	8.220000E-01
1355105	-1.992800E-01	6.648000E-01
1355106	0.000000E+00	6.032000E-01
* TORQUE CURVE NO. 4		
1355200	2	4
1355201	-1.000000E+00	1.984300E+00
1355202	-8.223400E-01	1.830800E+00
1355203	-6.337100E-01	1.682400E+00
1355204	-4.585300E-01	1.557000E+00
1355205	-2.670230E-01	1.436200E+00
1355206	-1.761070E-01	1.387900E+00
1355207	-8.931000E-02	1.348100E+00
1355208	0.000000E+00	1.233610E+00
* TORQUE CURVE NO. 5		
1355300	2	5
1355301	0.000000E+00	-4.500000E-01
1355302	4.000000E-01	-2.500000E-01
1355303	5.000000E-01	0.000000E+00
1355304	1.000000E+00	3.569000E-01
* TORQUE CURVE NO. 6		
1355400	2	6
1355401	0.000000E+00	1.233610E+00

```

1355402 9.064300E-02      1.196500E+00
1355403 1.885690E-01      1.109600E+00
1355404 2.734700E-01      1.041600E+00
1355405 4.586690E-01      8.958000E-01
1355406 5.744800E-01      7.807000E-01
1355407 7.381600E-01      6.134000E-01
1355408 7.685200E-01      5.849000E-01
1355409 8.700570E-01      4.877000E-01
1355410 1.000000E+00      3.569000E-01
*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 7
*-----1-----1-----1-----1-----1-----1-----1-----
1355500 2 7
1355501 -1.000000E+00      -1.000000E+00
1355502 -3.000000E-01      -9.000000E-01
1355503 -1.000000E-01      -5.000000E-01
1355504 0.000000E+00      -4.500000E-01
*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 8
*-----1-----1-----1-----1-----1-----1-----1-----
1355600 2 8
1355601 -1.000000E+00      -1.000000E+00
1355602 -2.500000E-01      -9.000000E-01
1355603 -8.000000E-02      -8.000000E-01
1355604 0.000000E+00      -6.700000E-01
*-----1-----1-----1-----1-----1-----1-----1-----
* RENODALIZE PUMP 2
*-----1-----1-----1-----1-----1-----1-----1-----
1650000 "PCPUMP2 " PUMP
1650101 0.0 0.514 0.0991 0.0 90.0 0.317900
1650102 0
1650108 160010000 0.0 0.017 0.017 0000
1650109 170000000 0.0 0.1 0.1 0000
1650200 0 1.49287+7 1.23094+6 2.46151+6 0.
1650201 0 3.4623 3.4623 0.0
1650202 0 3.5798 3.5798 0.0
1650301 135 135 135 -1 -1 0 0
1650302 369.00000 36859079 31550000 96.000000 500.60000 1.4310000
1650303 613.60000 300000000 207.43300 304440000 19.598700 300000000
1650310 0.0 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* REMOVE SPRAY LINE, SPRAY VALVE, AND CALCULATOR
*-----1-----1-----1-----1-----1-----1-----1-----
4300000 SPRAY DELETE
4350000 SPRVLV DELETE
20590400 SPRAY DELETE 0.0 0.0 0.0 0.0 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* RENODALIZE PRESSURIZER MASS CALCULATOR
*-----1-----1-----1-----1-----1-----1-----1-----
20507000 FZEMASS SUM 1.0 0.0 1
20507001 0.0 3.33500-3 RHO 400010000
20507002 3.33500-3 RHO 405610000
20507003 3.33500-3 RHO 405020000
20507004 6.84000-2 RHO 415010000
20507005 8.38000-2 RHO 415020000
20507006 2.24255-1 RHO 415030000
20507007 2.98987-1 RHO 415040000
20507008 2.24255-1 RHO 415050000
20507009 7.32000-2 RHO 415060000
20507010 1.42000-2 RHO 420010000
20507011 1.43000-2 RHO 420020000
*-----1-----1-----1-----1-----1-----1-----1-----
* REPLACE PRESSURIZER BACKUP/CYCLING HEATERS POWER TABLE

```


* INSTEAD OF REMOVING PRESSURIZER HEAT STRUCTURE COMPONENTS

```

*-----1-----1-----1-----1-----1-----1-----
20241700 POWER 693
20241701 0.0 0.0
20241702 1.0 0.0
20241800 POWER 694
20241801 0.0 0.0
20241802 1.0 0.0

```

* REMOVE PRESSURIZER LEVEL CONTROLLERS, CHARGING COMPONENT, AND
* LETDOWN COMPONENT

```

*-----1-----1-----1-----1-----1-----1-----
20500200 PZRLVL SUM 1.0 0.0 1
20500201 0.0 0.1815 VOIDF 415010000
20500202 0.1524 VOIDF 415020000
20500203 0.3967 VOIDF 415030000
20500204 0.5289 VOIDF 415040000
20500205 0.3967 VOIDF 415050000
20500206 0.1943 VOIDF 415060000
20500207 0.1029 VOIDF 420010000
20500208 0.1029 VOIDF 420020000
9800000 "CHRG R" DELETE
9850000 "CHRG V" DELETE
20590500 CHARGE DELETE 0.0 0.0 0.0 0.0 0.0 0.0
9900000 "LTDWN S" DELETE
9950000 "LTDWN V" DELETE
20590600 LETDOWN DELETE 0.0 0.0 0.0 0.0 0.0 0.0

```

* REMOVE STEAM VALVE CONTROLLER

```

*-----1-----1-----1-----1-----1-----1-----
5400000 "CV-P4-10 " VALVE
5400101 530010000 541000000 0.0047772 0.0 0.0 0100
5400201 0 14.541 13.536 0.0
5400300 MTRVLV
5400301 685 685 0.05 .416170 540
20254000 NORMAREA
20254001 0.0 0.0
20254002 9.25-4 9.25-4
20254003 1.0 1.0
20590700 "DELTA T" DELETE 0.0 0.0 0.0 0.0 0.0 0.0
20590800 DEADBAND DELETE 0.0 0.0 0.0 0.0 0.0 0.0
20590900 "INT D T" DELETE 0.0 0.0 0.0 0.0 0.0 0.0
20591000 TCONTROL DELETE 0.0 0.0 0.0 0.0 0.0 0.0
20290800 DELETE

```

* REMOVE FEED SYSTEM CONTROLLER

```

*-----1-----1-----1-----1-----1-----1-----
20591100 SGLVLERR DELETE 0.0 0.0 0.0 0.0 0.0 0.0
20591200 FEEDFLOW DELETE 0.0 0.0 0.0 0.0 0.0 0.0
5660000 "FEED " TMDPJUN
5660101 565000000 508000000 0.05
5660200 1 502
5660201 -100.0 19.150 0.0 0.0 *L2-5
5660202 0.0 19.150 0.0 0.0 *L2-5
5660203 0.5 10.0 0.0 0.0 *L2-5
5660204 1.0 2.50 0.0 0.0 *L2-5
5660205 1.5 1.00 0.0 0.0 *L2-5
5660206 2.0 0.25 0.0 0.0 *L2-5
5660207 2.5 0.00 0.0 0.0 *L2-5

```

* REPLACE TRIPS FOR L2-3 TRANSIENT

```

*-----1-----1-----1-----1-----1-----1-----

```


0000501	TIME	0	GE	NULL	0	0.0	L	* BREAK OPEN
0000502	TIME	0	GE	NULL	0	0.103	L	* REACTOR SCRAM
0000503	TIME	0	GE	NULL	0	14.0	N	* HPIS STRAT
0000504	TIME	0	GE	NULL	0	29.0	N	* LPIS START

* MINOR FDIIT VARIABLES

0000301	P	250010000	* PRIMARY PRESSURE PE-1UP-001
0000302	P	530010000	* SECONDARY PRESSURE
0000303	TEMPF	250010000	* UPPER PLENUM TEMP.
0000304	TEMPF	215010000	* LOWER PLENUM TEMP.
0000305	MFLOWJ	340010000	* BLCL MASS FLOW
0000306	MFLOWJ	305010000	* BLHL MASS FLOW
0000307	RHO	100010000	* ILHL DENSITY
0000308	RHO	340010000	* BLCL DENSITY
0000309	RHO	305010000	* BLHL DENSITY
0000310	RHO	185010000	* ILCL DENSITY
0000311	RHO	180010000	* PUMP EXIT DEN.
0000312	MFLOWJ	630000000	* LPSI MASS
0000313	MFLOWJ	640000000	* HPSI
0000314	MFLOWJ	600000000	* ECC MASS
0000315	MFLOWJ	610000000	* ACCUM MASS FLOW
0000316	CNTRLVAR	4	* ACCUMULATOR LEVEL
0000317	PMPVEL	135	* PUMP 1 SPEED
0000318	P	100010000	* ILHL PRESSURE
0000319	VOIDGJ	317000000	* HL BREAK JUNC VOID
0000320	VOIDGJ	347000000	* CL BREAK JUNC VOID
0000321	CNTRLVAR	2	* PZR LEVEL
0000322	CNTRLVAR	1	* S/G LEVEL
0000323	CNTRLVAR	7	* DC LEVEL (INTACT)
0000324	CNTRLVAR	8	* DC LEVEL (BROKEN)
0000325	CNTRLVAR	9	* HOT CORE LEVEL
0000326	CNTRLVAR	10	* AVER CORE LEVEL
0000327	CNTRLVAR	12	* TOTAL COLLAPSED LEVEL
0000328	CNTRLVAR	59	* AVERAGE CORE MASS
0000329	CNTRLVAR	60	* HOT CORE MASS
0000330	CNTRLVAR	71	* CORE MASS
0000331	CNTRLVAR	72	* PCS TOTAL MASS
0000332	CNTRLVAR	75	* TOTAL INJECTED MASS
0000333	CNTRLVAR	77	* TOTAL DISCHARGED MASS
0000334	CNTRLVAR	81	* TIME STEP SIZE
0000335	CPUTIME	0	
0000336	MFLOWJ	180010000	* PUMP DISCHARGE MASS
0000337	MFLOWJ	185010000	* ILCL MASS FLOW
0000338	MFLOWJ	701000000	* DC UPPER ANNULUS MASS
0000339	MFLOWJ	731000000	* DC DOWNWARD MASS
0000340	MFLOWJ	722000000	* CROSS FLOW 1
0000341	MFLOWJ	724000000	* CROSS FLOW 2
0000342	MFLOWJ	726000000	* CROSS FLOW 3
0000343	MFLOWJ	728000000	* CROSS FLOW 4
0000344	MFLOWJ	719000000	* BR. SIDE DC DOWNWARD MASS
0000345	MFLOWJ	225010000	* AVER CORE MASS FLOW
0000346	MFLOWJ	225020000	* HOT CORE MASS FLOW
0000347	MFLOWJ	225030000	* CORE BYPASS FLOW
0000348	VOIDG	021010000	* HOT CH 5 INCH VOID
0000349	VOIDG	023010000	* HOT CH 28 INCH VOID
0000350	VOIDG	025010000	* HOT CH 39 INCH VOID
0000351	VOIDG	013010000	* AVER CH 28 INCH VOID
0000352	VOIDG	015010000	* AVER CH 39 INCH VOID
0000353	VOIDG	225010000	* LOWER PLENUM VOID
0000354	VOIDG	240010000	* UPPER PLENUM VOID

0600355 HTEMP 231100110 * TE-5H5-002
 0000356 HTEMP 231100210 * TE-5J9-005
 0000357 HTEMP 231100310 * TE-5I8-008
 0000359 HTEMP 231100410 * TE-5J7-011
 0000360 HTEMP 231100510 * TE-5H5-015
 0000361 HTEMP 231100610 *

*
 0000362 HTEMP 230100110
 0000363 HTEMP 230100210 * TE-4E8-011
 0000364 HTEMP 230100310 * TE-4F7-015
 0000365 HTEMP 230100410 * TE-4G8-021
 0000366 HTEMP 230100510 * TE-4F8-028
 0000367 HTEMP 230100610 * TE-4F8-032
 0000368 TEMPF 712010000 * TE-1ST-001
 0000369 TEMPF 714010000
 0000370 TEMPF 716010000
 0000371 TEMPF 718010000
 0000372 TEMPF 225010000

*-----1-----1-----1-----1-----1-----1-----1-----1-----
 *-----1-----1-----1-----1-----1-----1-----1-----1-----
 *\$

* ACCUMULATOR, TRIPS, AND CONTROL VARIABLE

*-----1-----1-----1-----1-----1-----1-----1-----1-----
 * ACCUMULATOR VALVE TRIPS

*-----1-----1-----1-----1-----1-----1-----1-----1-----
 0000579 MFLOWJ 610000000 GE NULL 0 0.0 N
 0000580 CNTRLVAR 4 LI NULL 0 1.0 L
 0000582 579 AND -580 N

*-----1-----1-----1-----1-----1-----1-----1-----1-----
 * ACCUMULATOR LEVEL CONTROL VARIABLE

*-----1-----1-----1-----1-----1-----1-----1-----1-----
 20500400 ACCMLVL NTEGRAL -4.776E-3 2.04 0
 20500101 VELFJ 610000000

*-----1-----1-----1-----1-----1-----1-----1-----1-----
 * ECC CHECK VALVE

*-----1-----1-----1-----1-----1-----1-----1-----1-----
 6000000 "ECC CHKVLV" VALVE
 6000101 605010000 185000000 0.0 1.3869 1.3869 0100
 6000201 0 0.0 0.0 0.0
 6000300 TRPVLV
 6000301 681

*-----1-----1-----1-----1-----1-----1-----1-----1-----
 * ECCS HEADER TO PCS

*-----1-----1-----1-----1-----1-----1-----1-----1-----
 6050000 "ECCS HEADR" SINGLVOL
 6050101 5.989E-3 4.8247 0.0 0.0 90.0 2.2061
 6050102 1.0165-5 0.0 10
 6050200 0 4.18E+6 125472. 2600290. 0.0

*-----1-----1-----1-----1-----1-----1-----1-----1-----
 * ACCUMULATOR VALVE

*-----1-----1-----1-----1-----1-----1-----1-----1-----
 6100000 "ACCUM VLV " VALVE
 6100101 615010000 605000000 0.0 8.1009 8.1009 0000
 6100201 0 0.0 0.0 0.0
 6100300 TRPVLV
 6100301 682

*-----1-----1-----1-----1-----1-----1-----1-----1-----
 * ACCUMULATOR PIPE

*-----1-----1-----1-----1-----1-----1-----1-----1-----
 6150000 "ACC PIPE " SINGLVOL

6150101	0.01608	24.5486	0.0	0.0	0.0	0.0
6150102	1.0165-5	0.0	10			
6150200	3	4.18E+6	303.2			
*-----1-----1-----1-----1-----1-----1-----1-----						
* ACCUMULATOR VESSEL						
*-----1-----1-----1-----1-----1-----1-----1-----						
6200000	"ACCUMULATR"		ACCUM			
6200100	1.254	1.8261563	0.0	0.0	-90.0	-1.8261563
6200102	2.286-5	0.0	10			
6200200	4.18E+6	303.2				
6201101	615000000	8.213E-3	40.0000	40.0000	0	
6202200	1.45	0.0	4.0251	0.67056	0.04445	0 0 0 0
*-----1-----1-----1-----1-----1-----1-----1-----						
* ZIRCALOY-4 - THERMAL CONDUCTIVITY FROM MATPRO						
*-----1-----1-----1-----1-----1-----1-----1-----						
20100300	TBL/FCTN	1	1			
20100301	300.0	12.68				
*20100301	380.4	13.6				
20100302	469.3	14.6				
20100303	577.6	15.8				
20100304	685.9	17.3				
20100305	774.8	18.4				
20100306	872.0	19.8				
20100307	973.2	21.8				
20100308	1073.2	23.2				
20100309	1123.2	25.4				
20100310	1152.3	24.2				
20100311	1232.2	25.5				
20100312	1331.2	26.6				
20100313	1404.2	28.2				
20100314	1576.2	33.0				
20100315	1625.2	36.7				
20100316	1755.2	41.2				
20100317	2273.2	55.0				
*-----1-----1-----1-----1-----1-----1-----1-----						
* ZIRCALOY-4 - VOLUMETRIC HEAT CAPACITY FROM MATPRO						
*-----1-----1-----1-----1-----1-----1-----1-----						
20100351	300.0	1.841E6				
20100352	400.0	1.978E6				
20100353	640.0	2.168E6				
20100354	1090.0	2.456E6				
20100355	1093.0	3.288E6				
20100356	1113.0	3.865E6				
20100357	1133.0	4.028E6				
20100358	1153.0	4.709E6				
20100359	1173.0	5.345E6				
20100360	1193.0	5.044E6				
20100361	1213.0	4.054E6				
20100362	1233.0	3.072E6				
20100363	1243.0	2.332E6				
20100364	1477.0	2.332E6				
*-----1-----1-----1-----1-----1-----1-----1-----						
* PLOT EDIT REQUEST						
*-----1-----1-----1-----1-----1-----1-----1-----						
20300100	P	250010000	* PRIMARY PRESSURE PE-1UP-001			
20300200	P	530010000	* SECONDARY PRESSURE			
20300300	TEMPF	250010000	* UPPER PLENUM TEMP.			
20300400	TEMPF	215010000	* LOWER PLENUM TEMP.			
20300500	MFLOWJ	340010000	* BLCL MASS FLOW			
20300600	MFLOWJ	305010000	* BLHL MASS FLOW			
20300700	RHO	100010000	* LLHL DENSITY			
20300800	RHO	340010000	* BLCL DENSITY			
20300900	RHO	305010000	* BLHL DENSITY			

20301000	RHO	180010000	* IBCB DENSITY
20301100	RHO	180010000	* PUMP EXIT DEN.
20301200	MFLOWJ	630000000	* LPSI MASS
20301300	MFLOWJ	640000000	* HPSI
20301400	MFLOWJ	600000000	* ECC MASS
20301500	MFLOWJ	610000000	* ACCUM MASS FLOW
20301600	CNTRLVAR	4	* ACCUMULATOR LEVEL
20301700	PMPVEL	135	* PUMP 1 SPEED
20301800	P	100010000	* ILHL PRESSURE
20301900	VOIDGJ	317000000	* HL BREAK JUNC VOID
20302000	VOIDGJ	347000000	* CL BREAK JUNC VOID
20302100	CNTRLVAF	2	* PZR LEVEL
20302200	CNTRLVAR	1	* S/G LEVEL
20302300	CNTRLVAR	7	* DC LEVEL (INTACT)
20302400	CNTRLVAR	8	* DC LEVEL (BROKEN)
20302500	CNTRLVAR	9	* HOT CORE LEVEL
20302600	CNTRLVAR	10	* AVER CORE LEVEL
20302700	CNTRLVAR	12	* TOTAL COLLAPSED LEVEL
20302800	CNTRLVAR	59	* AVERAGE CORE MASS
20302900	CNTRLVAR	60	* HOT CORE MASS
20303000	CNTRLVAR	71	* CORE MASS
20303100	CNTRLVAR	72	* PCS TOTAL MASS
20303200	CNTRLVAR	75	* TOTAL INJECTED MASS
20303300	CNTRLVAR	77	* TOTAL DISCHARGED MASS
20303400	CNTRLVAR	81	* TIME STEP SIZE
20303500	CPUTIME	0	
20303600	MFLOWJ	180010000	* PUMP DISCHARGE MASS
20303700	MFLOWJ	185010000	* ILCL MASS FLOW
20303800	MFLOWJ	701000000	* DC UPPER ANNULUS MASS
20303900	MFLOWJ	731000000	* DC DOWNWARD MASS
20304000	MFLOWJ	722000000	* CRCS FLOW 1
20304100	MFLOWJ	724000000	* CROSS FLOW 2
20304200	MFLOWJ	726000000	* CROSS FLOW 3
20304300	MFLOWJ	728000000	* CROSS FLOW 4
20304400	MFLOWJ	719000000	* BR. SIDE DC DOWNWARD MASS
20304500	MFLOWJ	225010000	* AVER CORE MASS FLOW
20304600	MFLOWJ	225020000	* HOT CORE MASS FLOW
20304700	MFLOWJ	225030000	* CORE BYPASS FLOW
*			
20304800	VOIDG	021010000	* HOT CH 11 INCH VOID
20304900	VOIDG	023010000	* HOT CH 21 INCH VOID
20305000	VOIDG	025010000	* HOT CH 45 INCH VOID
20305100	VOIDG	013010000	* AVER CH 21 INCH VOID
20305200	VOIDG	015010000	* AVER CH 45 INCH VOID
20305300	VOIDG	225010000	* LOWER PLENUM VOID
20305400	VOIDG	240010000	* UPPER PLENUM VOID
*			
20305500	HTTEMP	231100110	* TE-5H5-002
20305600	HTTEMP	231100210	* TE-5J9-005
20305700	HTTEMP	231100310	* TE-518-008
20305800	HTTEMP	231100410	* TE-5J7-011
20305900	HTTEMP	231100510	* TE-5H5-015
20306000	HTTEMP	231100610	*
*			
20306100	HTTEMP	230100110	
20306200	HTTEMP	230100210	* TE-4E8-011
20306300	HTTEMP	230100310	* TE-4F7-015
20306400	HTTEMP	230100410	* TE-4G8-021
20306500	HTTEMP	230100510	* TE-4F8-028
20306600	HTTEMP	230100610	* TE-4F8-032
20306700	TEMPF	712010000	* TE-1ST-001
20306800	TEMPF	714010000	
20306900	TEMPF	716010000	

20507700 BRMASS INTEGRAL 1.0 0.0 1
20507701 CNTRLVAR 76
20507701 CNTRLVAR 76

*
-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* END OF INPUT
#EOR
#EOR

Appendix D. Updat List for PSI-EIR 83 based on RELAP5/MOD2 Cycle 36.04

APPENDIX D Update list for a updated RELAP5/MOD2 Cycle 36.04

```

/JOB
RM364T.T200.
/USER
ATTACH,OLDPL=REL364S.
PURGE,RE364TS/NA.
PURGE,RE364TX/NA.
PURGE,RE364TL/NA.
* *****
* IMPORTANT !! *
* THE UPDATE DIRECTIVE *
* SHOULD HAVE *COMPILE DEFINE
* AS THE FIRST DIIRECTIVE
*****
UPDATE,N=RE364TS.
UPDATE,P=RE364TS,Q,C=R5SEG.
REPLACE,R5SEG.
RETURN,OLDPL.
*DEFINE,RE364TS.
RETURN,RE364TS.
ATTACH,ENVRLX=ENVR41X.
LIBRARY,ENVRLX.
SELECTA,COMPILE,COMP.
LIBRARY.
RETURN,ENVRLX.
REWIND,COMP.
FTN5,I=COMP,DO,ET,STATIC,OPT=2,ROUND,LO=M/A/R/S.
RETURN,COMP.
REWIND,LGO.
ATTACH,RELAP5I=REL361L.
GTR,RELAP5I,ADD,REL/*
*DEFINE,RELAP50=RE364TL.
LIBEDIT,P=RELAP50,I=0,B=ADD,LO=F,U,C.
LIBEDIT,P=RELAP50,B=LGO,I=0,LO=F,U,C.
RETURN,NULL,LGO,RELAP5I.
RETURN,RLP5F1,RLP5F2.
ATTACH,ENVRL=ENVR41L.
FILE,RSTIN,RT=S,SBF=NO,USE,FO=SQ.
RFL,EC=200.
DEFINE,RE364TX.
SEGLOAD,I=R5SEG,B=RE364TX.
LDSET,LID=RELAP50/ENVRL.
LDSET,PRESETA=NGINDEF,ERR=NONE,MAP=SB.
LDSET,STAT=RSTIN.
LIBLOAD,ENVRL,$HDR=$.
LIBLOAD,FTN5LIB,$FERCAP,$, $RPVCAP,$,$FTNRP2,$,$Q2NTRY,$.
NOGO.
RETURN,RELAP50,ENVRL,COMPILE.
SKIP,KKK.
EXIT.
ENDIF,KKK.
DAYFILE,KMRRDAY.
REPLACE,KMRRDAY.
/EOR
*COMPILE DEFINE
*ID CBD3604
*D DMK3601.484
*D PLOTMD.24

```

```

901 FORMAT ('OPL0TFL SCRACH FILE GENERATED.')
*COMPILE DEFINE,SEGD1R
*COMPILE RELAP5
*D RJW3603.23
  DATA PTITLE/"RELAP5/2/3","6.04-PS1","REACTOR LO","SS OF COOL",
*/
*/   ENDF
*/   *ID KWU01 ALREADY IMPLEMENTED IN RELAP5OLDPL3604C,
*/       WHICH IS USED AS BASIS
*/   */   CORRECTIONS OF INDEX IN SUBROUTINE RACCUM
*/   *I RACCUM.618
*/       IELV=1
*/   *B DMK3602.581
*/       I=IELV
*COMPILE DEFINE,SEGD1R,RACCUM
*ID KWU01
*I RACCUM.618
  IELV=1
*B DMK3602.581
  I=IELV
*/   */   END OF KWU-UPDATES TO CYCLE 3604
*COMPILE DEFINE,SEGD1R
*IDENT SKI01
*/   THESE UPDATES ARE RECOMMENDED BY SKI TO BE
*/   IMPLEMENTED IN RELAP5/MOD2-36.04
*/   SOURCE:   LETTER FROM STUOSV1K (MR.SANDERVAG)
*/           TO      KWU      (MR.GRUBER)
*/           1987-06-25
*/
*/   COMPILE RELAP5
*/
*COMPILE IHTCMP
*/
*/   FIX AN INDEXING ERROR IN IHTCMP
*/   ERROR CAUSED ROD PLENUM VOLUME FOR GAP-GAS PRESSURE CALCULATION
*/   TO BE INCORRECT. FOUND AND FIXED BY D.CARAH8R 20MAY87
*/   FIX ONLY CDC-VERSION CODING
*D IHTCMP.1041
  L=(.NOT.MASK(43).AND.IHTPTR(J))+FILNDX(8)
*/
*/   UPDATE ROUTINE IRLHT TO ALLOW REFLOOD TO WORK
*/   HEAT STRUCTURE FILE GETS CHANGED ON RESTART (FOR
*/   EXAMPLE BY DELETING OR ALTERING SOME STRUCTURES)
*/   NOTE..HEAT STRS ASSOCIATED WITH REFLOOD CANNOT BE ALTERED
*/   ON RESTART AS IRLHT IS NOW PROGRAMMED
*/
*COMPILE IRLHT
*I IRLHT.330
C   UPDATE THE GEOMETRY POINTER IN IGLRFL BITS 44-60 IN CASE THE
C   HEAT STRUCTURE FILE CHANGED ON RESTART.
  J=(.NOT.MASK(43).AND.IH) + IHT
  J=(.NOT.MASK(43).AND.IHTPTR(J)) + IHT
  NCOLS=.NOT.MASK(43).AND.INXGOM(J)
  IGLRFL(I)=(MASK(43).AND.IGLRFL(I)).OR.NCOLS
*/
*/   END OF UPDATES SKI01
*/
*/   START OF PSI UPDATE
*/

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*ID MARTIN
*I PHAINT.9
      COMMON/IFLG2/IFLAG2(1000)
      DIMENSION IFLAG1(1000)
*I PHAINT.151
      IIFL1=(I-IV+IVSKP)/IVSKP
      IFLAG1(IIFL1)=0
*I PHAINT.294
      TGSAT=TGSAT-40.*VOIDF(I)
*I PHAINT.370
      IF(FBUB.GT.0.0.OR.FSLUG.GT.0.0.AND.DIAMV(I).LT.0.018)
        I IFLAG1(IIFL1)=1
*I PHAINT.390
      IF(DIAMV(I).LT.0.018) THEN
        FIC=65.0*VOIDG(I)*VOIDF(I)**3.0*RHO(I)/DIAMV(I)
      ENDIF
*I PHAINT.421
      IF(DIAMV(I).LT.0.018) THEN
        FIC1=65.0*VOIDG(I)*VOIDF(I)**3.0*RHO(I)/DIAMV(I)
      ENDIF
*I PHAINT.424
      IF(DIAMV(I).GE.0.018) THEN
*I PHAINT.425
      ENDIF
*I PHAINT.495
      IF(DIAMV(I).LT.0.018) FIC1=FIC1*0.5
*I PHAINT.633
      IF(DIAMV(I).LT.0.018) THEN
        FIC1=VOID*(FIC1*0.5+1.225*0.4*RHO(I)*SLSLG*VOID**2.)
      ELSE
*I PHAINT.634
      ENDIF
*I PHAINT.505
      IF(DIAMV(I).LT.0.018) FIC=FIC*0.5
*I PHAINT.462
      IF(DIAMV(I).LT.0.018) FIC=FIC*0.5
*I PHAINT.855
      IIFL2=(I-IJ+IJSKP)/IJSKP
      IFLAG2(IIFL2)=0
*I PHAINT.919
      INDK=(K-IV+IVSKP)/IVSKP
      INDL=(L-IV+IVSKP)/IVSKP
      IF(IFLAG1(INDK).EQ.1.OR.IFLAG1(INDL).EQ.1) IFLAG2(IIFL2)=1
*D QFHTRC.156
      HTV2(INDZ)=HCCHFA*EXP(-0.0175*TERM)+GTERM*EXP(-0.012*TERM)
*D QFHTRC.178
      FACBR=(1.+0.025*AMAX1(0.,SATT(IDX)-TEMPF(IDX)))
      HCBR=AMAX1(HTV2(INDZ),(CONVAP*TERM1*TERM2*(SATHG(IDX)-SATHG(IDX)))
*D QFHTRC.179
      L/AMAX1(TMPBDY-SATT(IDX),0.01)+9.68*CSUBPG(IDX))*9.81/(2.*3.14159)
*D QFHTRC.180
      2 *SORT(9.81*TERM1/SIGMA(IDX))/VISC(G(IDX))**0.25*0.62*FACBR)
      VELD=AMAX1(VELG(IDX)-VELF(IDX),0.001)
      DDROP=3.*SIGMA(IDX)/(RHO(G(IDX))*VELD**2)
      IF(DDROP.LT.1.5E-4)DDROP=1.5E-4
      IF(DDROP.GT.3.0E-3)DDROP=3.0E-3
      TERM5=1./(1.+0.35*CSUBPG(IDX)*AMAX1(TMPBDY-SATT(IDX),0.0001)
      1 /AMAX1(SATHG(IDX)-SATHF(IDX),0.01))**3.
      HCFO=0.4*3.14159/4.*(6.*(1.-VOIDG(IDX))/3.14159)**0.6666667

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1   *(9.81*RHOF(IDX)*RHOG(IDX)*AMAX1(SATHG(IDX)-SATHF(IDX),0.01)
2   *TERM5*CONVAP/(AMAX1(TMPBDY-TEMPF(IDX),0.0001)*VISCQ(IDX)
3   *(3.14159/6.)*0.3333333*DDROP)**0.25
   IF(VOIDG(IDX).LE.0.6)THEN
     HCFB=HCBR
   ELSE
     IF(VOIDG(IDX).GE.0.8) THEN
       HCFB=HCFO
     ELSE
       HCFB=(VOIDG(IDX)-0.6)/0.2*HCFG+(0.8-VOIDG(IDX))/0.2
1     *HCBR
   ENDIF
   ENDIF
*D QFHTRC.187,188
   TERM=TERM2+HCFB
*D QFHTRC.209
1   *AMAX1(0.023*(REYN2)**0.4*DIAMV(IDX),TERM4)
*D QFHTRC.221,223
   VELD=AMAX1(VELG(IDX)-VELF(IDX),0.001)
   DDROP=3.*SIGMA(IDX)/(RHOG(IDX)*VELD**2)
   IF(DDROP.LT.1.5E-4) DDROP = 1.5E-4
   IF(DDROP.GT.3.0E-3) DDROP = 3.0E-3
   TERM5=1./(1.+0.35*CSUBPG(IDX)*AMAX1(TMPBDY-SATT(IDX),0.0001)
1   /(SATHG(IDX)-SATHF(IDX))**3.
   HCFO=0.4*3.14159/4.*(6.*(1.-VOIDG(IDX))/3.14159)**0.6666667
1   *(9.81*RHOF(IDX)*RHOG(IDX)*(SATHG(IDX)-SATHF(IDX))
2   *TERM5*CONVAP/(AMAX1(TMPBDY-TEMPF(IDX),0.0001)*VISCQ(IDX)
3   *(3.14159/6.)*0.3333333*DDROP)**0.25
   HCFB=HCFO
*I VEXPLT.9
   COMMON/IFLG2/IFLAG2(1000)
*I VEXPLT.322
   CO=1.0
   C1=1.0
   IIFL2=(1-IJ+IJSKP)/IJSKP
   IF(IFLAG2(IIFL2).EQ.1) THEN
     CO=1.2
     C1=(1.0-CO*VOIDGA)/AMAX1((1.-VOIDGA),1.0E-5)
     IF(C1.LT.0.7) C1=0.7
   ENDIF
*D VEXPLT.323
   FJFG=(FIJ(I)*DX*(ABS(C1*VELGJO(I)-CO*VELFJO(I))+0.01)
*D VEXPLT.507
   DIFF=SCRACH+(FRICFJ+CO*FJFG+VPGNX+HLOSSF)*DT
*D VEXPLT.508
   DIFG=-SCRACH-(FRICGJ+C1*FJFG+VPGNX+HLOSSG)*DT
*I VIMPLT.8
   COMMON/IFLG2/IFLAG2(1000)
*I VIMPLT.435
   CO=1.0
   C1=1.0
   IIFL2=(1-IJ+IJSKP)/IJSKP
   IF(IFLAG2(IIFL2).EQ.1) THEN
     CO=1.2
     C1=(1.0-CO*VOIDGA)/AMAX1((1.-VOIDGA),1.0E-5)
     IF(C1.LT.0.7) C1=0.7
   ENDIF
*D VIMPLT.436
   FJFG=(FIJ(I)*DX*(ABS(C1*VELGJO(I)-CO*VELFJO(I))+0.01)

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*D VIMPLT.591
      COEFV(IDG-1) = (FRICFJ+CO*FJFG+VPGNX+HLCSSF)*DT + SCRACH
*D VIMPLT.592
      COEFV(IDG)  = -(FRICGJ+C1*FJFG+VPGNX+HLOSSG)*DT - SCRACH
*C DEFINE,PHAINI,QFHTRC,VEL,LT,VIMPLT
*/
*/  END OF PSI UPDATE
*/
*/
*COMPILE ACCUM,PHAINI,DTSTEP
*/
*/  PROTECTS SIGMA (SURFACE TENSION) BY 1.0E-7 IN SUBROUTINE PHAINI
*/
*DELETE,PHAINI.200
      DSTAR(I) =DIAMV(I)*SQRT(9.8*RHOFG/AMAX1(SIGMA(I),1.0E-7))
*DELETE,PHAINI.326
      55 VCRIT=2.5*SQRT(SQRT(AMAX1(SIGMA(I),1.0E-7)*RHOFG)/RHOG(I))
*/
*/  CORRECT ERROR IN SUBROUTINE DTSTEP INTRODUCED IN CYCLE 30 SO THAT
*/  STATE PROPERTIES ARE NOT RESET WHEN AT A MINIMUM TIMESTEP DUE TO
*/  MASS ERROR
*/
*DELETE,DTSTEP.161
      IF (NANY .EQ. 0) WRITE (OUTPT,2003)
*/
*/  REWET CRITERIA REDUCTION (89/5/23 AKSAN & ICAP)
*IDENT MARTIN2
*I HTRC1.60
      GGT = RHOF(IV)*VOIDF(IV)*VELF(IV)+
      1   RHOG(IV)*VOIDG(IV)*VELG(IV)
*I HTRC1.111
      IF(GGT.GT.-100.) GO TO 12
*D HTRC1.112
      IF(XE.GT.XEC.OR.TW.GT.(1250.-TSAT)) GO TO 2000
      GO TO 13
      12 IF(XE.GE.XEC) GO TO 2000
      13 CONTINUE
*I HTRC1.82
      IF(GGT.GT.-100.) GO TO 11
*D HTRC1.83
      IF(TW.GT.1250.-TSAT) GO TO 2000
      11 CONTINUE
*I PSTDNB.28
      GGT = RHOF(IV)*VOIDF(IV)*VELF(IV)+
      1   RHOG(IV)*VOIDG(IV)*VELG(IV)
*I PSTDNB.29
      IF(GGT.GT.-100.) GO TO 231
*D PSTDNB.30
      IF(XE.GT.XEC.OR.TW.GT.(1250.-TSAT)) GO TO 235
*I PSTDNB.31
      GO TO 232
      231 IF(XE.GT.XEC) GO TO 235
      232 CONTINUE
*I PSTDNB.124
      IF(GGT.GT.-100.) GO TO 401
*D PSTDNB.126
      1 (1250.-TSAT)) TRANS = .FALSE.
*I PSTDNB.141
      GO TO 499

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401 IF(XE.GE.XEC)TRANS=.FALSE,
    IF(TRANS) THEN
    GO TO 402
    ELSE
    GO TO 403
    ENDIF
402 HTCF=AMAX1(HTBF,HFB)
    HTCG=AMAX1(HTBG,HV)
    QFFO=AMAX1(QTFBF,QFBF)
    QFGO=AMAX1(QTFBG,QFBG)
    GO TO 450
403 HTCF=HFB
    HTCG=HV
    QFFO=QFBF
    QFGO=QFBG
499 CONTINUE
*D PSTDNB.42
    IF(GGT.LT.-100) THEN
    FL=EXP(-5.0*THETA*AMIN1(ABS(TW-TWRTO),SQRT(DTSAT)))
    ELSE
    IF(GGT.GE.-100.AND.GGT.LE.0) THEN
    FL=((EXP(-2.0*THETA*AMIN1(ABS(TW-TWRTO),SQRT(DTSAT)))
1  -EXP(-5.0*THETA*AMIN1(ABS(TW-TWRTO),SQRT(DTSAT))))/100.)*GGT+
2  EXP(-2.0*THETA*AMIN1(ABS(TW-TWRTO),SQRT(DTSAT)))
    ELSE
    FL=EXP(-2.0*THETA*AMIN1(ABS(TW-TWRTO),SQRT(DTSAT)))
    ENDIF
    ENDIF
    FL = FL*AMIN1(1.,(((1.-ALPH)/0.05)**4))
*D PSTDNB.67
    HFB = 0.92163*(SQRT(HFB/SIGMA(IV)))
*I PSTDNB.69
    HCBR = HFB
    VAMA = AMAX1(VELG(IV)-VELF(IV),0.001)
    VFG2 = VAMA**2.
    XA= AMAX1(3.*SIGMA(IV),1.E-10)
    RDIAM =RHOG(IV)*VFG2/XA
    DDROP = 1./RDIAM
    IF(DDROP.LT.1.0E-4) DDROP=1.0E-4
    IF(DDROP.LT.3.0E-3) DDROP=3.0E-3
    TERM5=1./(1.+0.35*CSUBPG(IV)*AMAX1(TW-TSAT,0.001)
1  /AMAX1(SATHG(IV)-SATHF(IV),0.001))*3.
    HCFO=0.2*3.14159/4.*(6.*(1.-VOIDG(IV))/3.14159)**0.6666667
1  *(9.81*RHOF(IV)*RHOG(IV)*AMAX1(SATHG(IV)-SATHF(IV),0.01)
2  *TERM5*THCONS**3/(AMAX1(TW-TEMPF(IV),0.01)*VISCS
3  *(3.14159/6.))*0.3333333*DDROP)**0.25
    HCFO = 0.001*HCFO
    IF(VOIDG(IV).LE.0.60) THEN
    HFB=HCBR
    ELSE
    IF(VOIDG(IV).GE.0.80) THEN
    HFB=HCFO
    ELSE
    HFB=(VOIDG(IV)-0.60)/0.2*HCFO+(0.80-VOIDG(IV))/0.2
1  *HCBR
    ENDIF
    ENDIF
    IF(GGT.LT.0.) THEN
    HHHH=AMAX1(1.E-7,RHOF(IV)-RHOG(IV))

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HFB=1.09680*VOIDF(IV)*SQRT((1./1.)
1  *THCONS**3*RHO(IV)*HHHH*(HFG+0.5*DTSAT*CSUBPG(IV))
2  /(VISCS*DTSAT)**.25
ENDIF
*C HTRC1,PSTDNB,PREDNB
*/
*/ END OF AKSAN UPDATE
*/
/EOB
*COMPILE SEGDIR
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11. ABSTRACT (200 words or less)

The LOFT LOCE L2-3 was simulated using the RELAP5/MOD2 Cycle 36.04 code to assess its capability to predict the thermal-hydraulic phenomena in LBLOCA of the PWR. The reactor vessel was simulated with two core channels and split downcomer modelling for a base case calculation using the frozen code. From the results of the base case calculation, deficiencies of the critical flow model and the CHF correlation at high flow rate were identified, and the severeness of the rewetting criteria were also found. Additional calculation using an updated version of RELAP5/MOD2 Cycle 36.04 including modifications of the rewet criteria shows a substantial improvement in the core thermal response.

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