



# International Agreement Report

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## Assessment of RELAP5/MOD2 Cycle 36.04 Using LOFT Intermediate Break Experiment L5-1

Prepared by  
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Office of Nuclear Regulatory Research  
U.S. Nuclear Regulatory Commission  
Washington, DC 20555

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Prepared as part of  
The Agreement on Research Participation and Technical Exchange  
under the International Thermal-Hydraulic Code Assessment  
and Application Program (ICAP)

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ICAP

ASSESSMENT OF RELAP5/MOD2, Cycle 36.04

USING LOFT INTERMEDIATE BREAK EXPERIMENT L5-1

### Abstract

The LOFT intermediate break experiment L5-1, which simulates 12 inch diameter FCC line break in a typical PWR, has been analyzed using the reactor thermal/hydraulic analysis code RELAP5/MOD2, Cycle 36.04. The base calculation, which modeled the core with single flow channel and two heat structures without using the options of reflood and gap conductance model, has been successfully completed and compared with experimental data. Sensitivity studies were carried out to investigate the effects of nodalization at reactor vessel and core modeling on major thermal hydraulic parameters, especially on peak cladding temperature(PCT). These sensitivity items are: single flow channel and single heat structure (Case A), two flow channel and two heat structures (Case B), reflood option added (Case C) and both reflood and gap conductance options added (Case D). The code,RELAP5/MOD2 Cycle 36.04 with the base modeling, predicted the key parameters of LOFT IBLOCA Test L5-1 better than Cases A,B,C and D. Thus, it is concluded that the single flow channel modeling for core is better than the two flow channel modeling and two heat structure is also better than single heat structure modeling to predict PCT at the central fuel rods. It is recommended to use the reflood option and not to use gap conductance option for this L5-1 type IBLOCA.

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## Executive Summary

This report describes the assessment calculations using RELAP5/MOD2 Cycle 36.04, a frozen version of the code, to predict the thermal-hydraulic responses of the Loss of Fluid Test (LOFT) L5-1 Intermediate Break Loss of Coolant Accident (IBLOCA). LOFT IBLOCA Test L5-1 simulated 12 inch diameter ECC line break in a typical PWR. The objectives of the present assessment are to provide the applicability and optimum modeling of RELAP5/MOD2 Cycle 36.04 for LOFT IBLOCA Test L5-1. Since ICAP assessment requires sensitivity studies for nodalization and models, the effect of two nodalization and two model option sensitivities on PCT are performed under LOFT L5-1 configuration and sequence. Therefore, the results from this IBLOCA assessment will be helpful to model a similiar transient of a typical PWR IBLOCA. RELAP5/MOD2 Cycle 36.04, used in this assessment, was received in October 1986 from USNRC. Indexing errors were corrected in subroutine RACCUM, IHTCMP and IRFLHT from the frozen code version. There are no changes in physical models and hence the corrected version can also be regarded as RELAP5/MOD2 Cycle 36.04. Results indicated that the base case modeling (single channel and two heat structures) predicted the PCT at the central rods better than Case A and Case B.



However, Case A improved to predict the clad temperature rising time by 10 seconds while Case B improved to predict the PCT in peripheral rods. The code with reflood option underpredicted the PCT than the base case by 7 K. The code, with both reflood and gap conductance model used, also underpredicted the PCT than the base case by 15 K. Conclusively the code, RELAP5/MOD2 Cycle 36.04 with the base modeling, predicted the key parameters of LOFT IBLOCA Test L5-1 better than Cases A, B, C and D. Therefore, it is recommended to use single flow channel and two heat structure modeling; and, to use the reflood option and not to use gap conductance option for this L5-1 type IBLOCA.

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## 1. INTRODUCTION

The International Code Assessment and Applications Program (ICAP) has been conducted by fourteen nations and multinational organizations under the auspices of the USNRC [1][2]. The USNRC selected two Best Estimate (BE) codes: RELAP5/MOD2 [3][4] and TRAC/PF1/MOD1. The goal of the program is to assess the prediction capabilities and models [5] of the current BE thermal hydraulic(T/H) codes utilizing the available facility test and plant data in the world. The USNRC has plans to replace its present 10 CFR 50 Appendix K LOCA/ECCS rule with a best-estimate approach and an evaluation of uncertainty [2]. The USNRC plans to employ the results from code assessment works to provide conclusions relative to code accuracy and uncertainties through ICAP. The present ICAP aims to quantify uncertainties in the codes so that the code may be used for licensing purposes.

Korean contributions to ICAP include the assessments of RELAP5/MOD2 using ten experiments and five actual plant data. Six of the assessments are performed with LOFT Integral Effect Test (IET) data [6] and two with semiscale IET data. Two Separate Effect Test (SET) data for critical flow and condensation are used to assess the code RELAP5/MOD2. The work has been conducted by KAERI (Korea Atomic Energy Research Institute), KEPCO (Korea Electric Power Company) and the overall ICAP work inside Korea has been organized and performed in KNSC (Korea Nuclear Safety Center), which is regulatory body in Korea.

Key thermal and hydraulic phenomena such as blowdown, refill and reflood regarding on LBLOCA and SBLOCA separately are well identified over the past

years. Now, it is necessary to investigate the key phenomena of intermediate break loca (IBLOCA). The LOFT IBLOCA experiment L5-1 [8] simulated 12 inch diameter ECC line break (14 % break of 32 inch main piping) in a typical PWR by utilizing a 0.047 m diameter orifice. As quick look report for Test L5-1 [9] summarized the overalls of the experiment, the objective of experiment L5-1 is to provide data to assess the analytical techniques used to model the principal phenomena of an intermediate size break.

The RELAP5/MOD2/cycle 36.04 [3] was implemented in 1986 on a CDC 170-875 computer of KAERI. The code was corrected regarding to indexing errors in subroutines RACCOM and IHTCMP from the frozen version [11]. There are no changes in physical models and hence the corrected version can also be considered as RELAP5/MOD2 Cycle 36.04. Chen and Modro used RELAP5/MOD1 Cycle 13 for pretest [7] and posttest [12] calculations for LOFT L5-1. E. J. Lee and present authors [10] assessed RELAP5/MOD2 Cycle 36.05 by using LOFT SBLOCA Test data L3-7. The input deck for the LOFT IBLOCA Test L5-1 was basically equivalent to that used for LOFT L3-7 simulation with some modifications, which will be explained in Section 3.2.

The base calculation, which modeled the core with single flow channel and two heat structures without using the options of reflood and gap conductance model, has been successfully completed and compared with experimental data. Two types of nodalization sensitivity studies and two types of model option sensitivity studies were carried out to investigate the following effects on PCTs: single flow channel and single heat structure (Case A), two flow channel and two heat structures (Case B), reflood option added (Case C) and both reflood and gap conductance options added (Case D).

To summarize the objectives, this report aims to provide the applicability and optimum modeling of RELAP5/MOD2 Cycle 35.04 for LOFT IBLOCA Test L5-1. Since ICAP assessment requires sensitivity studies for nodalization and models, the effect of two nodalization and two model option sensitivities on PCT will be quantified under LOFT L5-1 configuration and experiment sequence. Thus, the results from this IBLOCA assessment will be helpful to model a similiar transient of typical PWR.

To address these objectives, the report composed of the following sections. The descriptions of the LOFT system and the experiment L5-1 are provided in Chapter 2. The code and modelling for a base calculation are described in Chapter 3. The results of the base case calculation are discussed in Chapter 4 in terms of thermal and hydraulic behaviors. The scope and results of nodalization and model sensitivity studies are presented in Chapter 6. Final conclusions and recommendations from this assessment are presented in Chapter 7. Appendix A contains the input listing used for base case calculation.

## 2. FACILITY AND TEST

### 2.1 LOFT

The LOFT Integral Effect Test (IET) facility [50 Mwt] has been designed to simulate the major components and system responses of a commercial four-loop PWR [1]. The LOFT facility consists of (1) a reactor vessel with a nuclear core (4 wt% U-235), (2) an intact loop (a steam generator and two primary pumps parallel), (3) a broken loop (simulated pump and steam generator and two quick opening valves), (4) the blowdown suppression system and (5) the emergency core coolant (ECC) system (two LPIS, two HPIS pumps and two accumulators). To relate LOFT into a PWR, the test facility is designed as follows: (1) the same linear heat generation rate of the large reactor is used, (2) LOFT powers are scaled according to component volumes (1:60), (3) flow areas are scaled to provide the identical flow to large reactor values, (4) pipe break areas are set in the ratio of core volume and (5) pressure, temperature and mass flux are identical to large reactor values.

### 2.2 L5-1

The LOFT intermediate break experiment series L5 was designed to identify and evaluate the LOFT system thermal-hydraulic response during an intermediate size break LOCE. Experiment L5-1 was initially operated at thermal power of 45.5 Mwt, vessel temperature difference of 27.0 K, mass flow rate of 308.2 kg/s at 14.93 MPa system pressure. The specific objectives of experiment L5-1 are to (1) obtain sufficient data to characterize the prevalent phenomena caused by an ECCS injection line rupture, (2) generate

applicable data for use as a base line in the future planning of intermediate size break, (3) provide data to assess the analytical techniques used to model the principal phenomena of an intermediate size break. Also, data aquisition system was validated during this experiment L5-1.

### 3. CODE AND MODELING

#### 3.1 RELAP5/MOD2 Cycle 36.04

RELAP5/MOD2 Cycle 36.04, a frozen version of RELAP5/MOD2 used in this assessment, was received at October 1986 from USNRC. The code was corrected regarding to indexing errors in subroutine RACCUM, IHTCMP and IRFLHT. There are no changes in physical models and hence the corrected version can also be regarded as RELAP5/MOD2 Cycle 36.04. These corrections were based on the update work of KWU and STUDEVIK [11].

#### 3.2 Modeling and Nodalization

Break, vessel and system modeling including boundary conditions are described in this section. The break for the IRLOCA was modeled with a motor valve whose rate of change for the normalized valve area was 14.0 unit per sec. The full open area, for instance, of LOFT SBLOCA Test L3-7 was  $1.278E-5$  m<sup>2</sup> while the area of L5-1 break was  $173.49E-5$  m<sup>2</sup> so that the area ratio of two experiments was about 138. For example, L3-7 simulated 1 inch SBLOCA while L5-1 simulated 11.2 inch I.D. accumulator line rupture. The diameter of actual orifice used in L5-1 experiment was 0.047 m [9] while 0.004 m diameter orifice was used for L3-7 and so the diameter ratio of two experiments was 11.7. The option of normal junction, nonhomogeneous, smooth area change and choking modeling applied (0000) were used to model L5-1 break.

The pellet stack length of core was 1.68 m and five sets of 15X15 and



four sets of 12X12 nuclear fuel assemblies existed [8]. Among 1300 fuel rods in the LOFT core, the central 204 fuels were modeled as a central hotter pin and the other 1096 fuels were described as a peripheral heat structure. The core basically was modeled as one flow channel which has six almost equal volume length of 0.221 m. Two heat structures were used to model the central assemblies (12300000) and the peripheral (12310000) assemblies respectively. Thus, a multiplication factor for the 204 central pins was calculated as 57.12 ( $1.68 \times 204 / 6$ ) while the factor for the 1096 peripheral pins was 306.88 ( $1.68 \times 1096 / 6$ ). Both reflood and gap conductance option were not used since the primary pressure was kept higher than 1.0 MPa during the period of interest and a tabular form of temperature vs. gap conductance data was used.

The input deck for LOFT L5-1 was basically from the deck equivalent to that for LOFT L3-7 simulation [10]. Some correction were made from the deck. For instance, core length was corrected to 1.68 from 1.98 m. HPIS was modeled with a time dependent junction connected directly into cold leg. HPIS injection was initiated based on a set pressure, 10.6 MPa of hot leg pressure. Accumulator was modeled with "ACCUM", single volume and a valve. The initial accumulator water level was corrected to be 1.54 m as in experiment and activated when the cold leg pressure was lower than 1.66 MPa. The model "ACCUM" was disconnected in the calculation when accumulator was emptied to overcome an accumulator related error. The flows from accumulator and LPIS were merged into a single volume ECCS header. The values for LPIS capacity were corrected based on the experiment L5-1 and LPIS was activated when the RCS pressure decreased to 1.08 MPa. Primary coolant pump was set to trip at 4.0 seconds. Thermal power was inputted with the combined data from

fission and decay power [8]. Other hydraulic and thermal modelings for primary and secondary loop were conceptually the same as the one used for L3-7 SBLOCA assessment work [10].

The RELAP5/MOD2 nodalization diagram of the base case is shown in Figure 1. The nodalization has 130 volumes, 136 junctions, 143 heat structures and 793 mesh points. Basically the same nodalization concept as L3-7 was applied to L5-1. The nodalization for L3-7 [10] is the reference and few changes were added as described above. Figure 2 shows the comparisons of linear heat generation rate (kW/m) for experiment and calculation along the core height. The history of thermal power from fission and decay was properly described in the input deck.

### 3.3 Initial and Boundary Conditions

The decks L51S12 and L51T12 in Cyber 170-875 were prepared for the purpose of assessment. Convergency was not achieved with the steady deck but the key values for the initial stages (Table 1) were generally within tolerable ranges at 300 second steady calculation. So, the values at 300 seconds were taken as the initial conditions for the following transient calculation. Table 1 shows the initial conditions of both experiment and calculation. The code predicted the primary system mass flow as 308.27 kg/s, hot leg temperature as 581.34 K and cold leg temperature as 553.76 K. Other T/H values for reactor vessel, pressurizer and accumulator were well predicted except the temperatures for the broken loop. The code overpredicted the broken loop hot leg temperature as 561.75 K which was 7.45 K higher than experiment. However, the discrepancy would not affect the

results of later transient because of the small mass flow (about 2.88 kg/s) rate through the broken loop. The major values for the steam generator secondary side were also fairly well predicted. The pressure was 5.00 MPa and steam mass flow rate was 31.5 kg/s initially. Figure 7 shows the initial condition and the transient of primary system inventory. Primary system coolant inventory mass was about 5000 kg and its measurement uncertainty was about 300 kg. The initial offset from the measurement occurred because the mass in the broken loop steam generator and pump was not included in the experiment and analysis [12]. Later, an extra calculation with a revised initial condition might be required to assess its effect on primary system pressure, accumulator and LPSI flow rates, and PCT.

Boundary conditions, composed of initial condition and sequence of event, should be matched with actual experimental conditions to describe the dynamic system boundary properly. Table 2 shows the sequence of events for experiment L5-1 and the base calculation. Within one second, reactor was scrammed and the secondary side inlet/outlet valves were closed and HPIS trip point was reached (10.6 MPa). HPIS injection was initiated with 2.48 seconds delay. Lowest in-core thermal excursion started at 184 and 182 seconds in experiment and base calculation. Accumulator (1.66 MPa) was injected at 185.8 and 189 seconds respectively. Maximum fuel cladding temperature reached 715 K at 198 seconds in experiment and 676 K at 210 seconds in base calculation. So the code underpredicted the PCT by 39 K. Finally LPIS (1.08 MPa) flow was initiated at 201 seconds in calculation and 227 seconds in experiment.

#### 4. RESULTS AND DISCUSSIONS FROM BASE CASE CALCULATION

Table 3 summarizes the list of assessment parameters. It describes the identification of calculated and measured parameter in addition to uncertainties of measurements. The corresponding figure numbers to the assessment parameters are also listed in Table 3. The system phenomena governing the response of L5-1 are classified as hydraulic and thermal behavior for the purpose of further discussions. Hydraulic behavior can be explained primarily with discharge flow rate, depressurization, external ECCS flow, system inventory and core mixture level. Thermal behavior can be categorized with the core thermal power, S/G secondary operation, core void and PCT. Since the break diameter is greater than 9 inch, it experiences a relatively rapid depressurization process compared with a typical SBLOCA. Thus, the transient can be characterized by a blowdown/refill process occurred relatively slower than typical LRLOCA and the safety is mainly affected by accumulator and LPIS flow rather than HPIS flow.

##### 4.1 Hydraulic Behavior

The upper plenum pressure was depressurized very rapidly to 7 MPa in 20 seconds, and then, slowly depressurized at a rate of 1 MPa per 50 seconds until LPIS was initiated (Figure 3). The steam dome pressure was well predicted (Figure 4) besides the mass flow rates of steam generator inlet (Figure 5) and outlet (Figure 6). The primary system inventory was well represented indicating that the discharge and incharge flows from ECCS were properly described (Figure 7). However, Figure 8 shows the density of LLHL overpredicted in 50 sec and 250 sec, probably due to overpredicted system

pressure (Figure 3) and overestimated LPIS flow (Figure 12). Figure 9 and 10 show the density of BLHL and HPIS flow rate matching with the experiment fairly well. Figure 11 shows the liquid level of accumulator and, interestingly a 15 sec stagnant existed in 215 sec because of the repressurized system pressure (Figure 3) due to LPIS flow (Figure 12). Figure 13 shows the flow rate of BLHL and Figure 14 shows the reflooding rate, which influences the PCT most. Figure 14 indicates the negative flow after 37 sec till accumulator injects. The positive mass flow is less than 50 kg/s in reflood phase. The slow depressurization occurred because the energy removed through the break (Figure 15) was less than the energy generated in the reactor core. After the interface between liquid and vapor fell below the break elevation, the rate of energy removal through the break increased. The RCS continued to depressurize after pressurizer was emptied (Figure 16) until accumulator injected.

The calculations showed that a large volume of water supplied from accumulator and LPIS more than compensated for the loss of reactor coolant inventory and repressurized again at 217 seconds (Figure 3, 11 and 12). It was verified again that accumulator and LPIS influenced more on safety than HPIS for this type of larger SBLOCA, i.e. IBLOCA transient (Figure 21). In core wise, the liquid was drained off at 180 seconds and started to be filled up again at 190 seconds due to the accumulator injection at 189 seconds. Significant core uncover occurred but the core quenches again due to the accumulator flow initiation (Figure 18).

Although the primary pressure decreased to 1 MPa in 200 seconds (Figure 3), the accumulator flow was injected at 186 seconds so that the fuel

cladding temperature quickly dropped thereafter (Figure 21). The steam dome pressure was predicted initially properly and overpredicted by 0.2 MPa at 25 seconds but, after 90 seconds, underpredicted up to by 0.8 MPa (Figure 4). The ILHL density at 50 seconds and 250 seconds were overestimated (Figure 8) probably due to overestimated ILHL mass flow rate (Figure 13). The overestimated mass flow rates were caused by overpumping HPIS (Figure 10) and LPIS (Figure 12) flow rates. These overestimated flow rates caused a 17 second stagnant of accumulator water level (Figure 11) at 217 second and it also affected the plateau of core mixture level. The base calculation predicted the key parameters of L5-1 experiment fairly well except two cases: the starting time of cladding temperature rise (dry-out) and earlier heat up in peripheral PCT measured. The base calculation predicted the start time of PCT rise 30 seconds later than the experiment (Figure 21). Figure 15 showed that the integrated break flow was predicted fairly well within maximum range of 200 kg. Figure 7 indicated that the primary system inventory was initially overpredicted by 500 kg and this affected to overpredict the inventory by 400 - 500 kg over the transient. The overestimated water inventory probably caused the heatup to start later. Otherwise the low mass flux CHF correlation from modified Zuber [5] has a deficiency in the operating range because core mass flow was less than order of 20 kg and flow area was 0.17 m<sup>2</sup> and, therefore, the mass flux surely less than 100 kg/m<sup>2</sup>/s. Providing that the discharge flow rate and the inventory were well predicted, Modified Zuber correlation overpredicted Q(CHF) and needs to be examined for this low range mass flux and pressure. Also, fuel cladding temperature measurements in a peripheral assembly 4 at 45 inch (T-4E8-45) indicated an early heat-up, quenching, reheat-up and final quenching (Figure 24). However, the calculation did not catch the early heat-up.

Therefore, nodalization sensitivity study including two-flow channel effect on the peripheral fuel clad temperature is motivated to investigate whether the source of the deficiency comes from the code, modelling or experiment.

#### 4.2 Thermal Behavior

This assessment used a combined thermal power from fission and decay power. History of thermal power from Reference 8 shows that the magnitude of fission power is very small after 10 seconds and thereafter the decay power, ranging from 2 MW to 1 MW, is dominant. A rapid core mixture level drop lead to a core uncovering. As two-phase circulation through the primary loop stops, the mixture levels in the S/G tubes drop steadily on both uphill and downhill side moving into a reflux cooling mode. The vessel mixture level also drops slowly during this S/G tube draining period until the mixture level reaches the bottom of the hot leg. Once the level reaches the bottom of the hot leg, it starts to decrease very rapidly because of the lack of a significant water supplied to the core from S/G. The mixture level affecting the fuel cladding temperature strongly decreases or increases depending upon loop seal clearing or degree of ECCS water supply. In this case, the mixture level increased again due to sufficient ECCS water supply.

Liquid void fraction of 230040000 became zero at 150 sec (Figure 25) and, then, thermal excursion started. At 198 seconds, maximum fuel cladding temperature of 715 K measured while the code predicted the start time of dry-out later by 25 second and the peak as 675 K (Figure 21). At the central and 26 inch (T-5F4-026) location of fuel assemblies, the code still predicted

the start of heatup later with the same heatup rate and underpredicted the peak by 15 K (Figure 20). At the central and 49 inch (T-5E8-49), the code predicted the start time of core heatup 25 seconds later than the one of the experiment and still underpredicted the peak by 40 K (Figure 22). At the peripheral and 26 inch (T-4F9-26), the code overpredicted the peak by 150 K due to highly estimated LHGR at the peripheral locations (Figure 23). The measured peak cladding temperature of 715 K at 198 second was obtained at the central and 37 inch (T-5D8-37) measurement location. The calculation, at central 36.5 inch, with single flow channel and two heat structures underestimated the peak as 675 K at 210 seconds while the experiment produced the PCT as 715 K at 198 seconds.

Consequently, it showed again that compensating effects of discharge flow, decay power and external ECCS water supply decided the mixture level of the core. Considering heat transfer mechanism in core side, the core experienced a slow downward liquid drain off until 180 seconds (blowdown phase) and started to be filled up again from 190 seconds (refill/reflood phase). The first part can be considered as a slow blowdown phase and the second part as a refill or reflood period. Core mixture level increased again due to the flows from accumulator and LPIS. Accumulator and LPIS flow injection finally cooled down the fuel.

The effect of two flow channel and even single heat structure on PCT would be interesting to quantify its effect. The base modeling did not use the options of reflood and gap conductance model. Therefore, the effects of each options on PCT will be demonstrated as alternatives of model sensitivity studies.



## 5. NODALIZATION AND SENSITIVITY STUDIES

From the discussions in the base calculations, two types (Case A and Case B) of nodalization and two types (Case C and Case D) of model option sensitivity studies were proposed to quantify its effect on a key safety parameter, PCT. The central PCT measured at T-5D8-37 was compared with HTTEMP 2300410 and a peripheral PCT measured at T-4E8-45 compared with HTTEMP 2310510. First, a flood option was added to the base modeling and, then, recalculation has been done with gap conductance option added as model sensitivity items.

### 5.1 Nodalization Sensitivity Study

#### 5.1.1 Single Flow Channel and Single Heat Structure (Case A)

Case A, which modeled the core as single flow channel and single heat structure, indicated the start time of clad temperature rise 10 seconds earlier and underpredicted the PCT by 25 K in comparison with the base case. A later peak was calculated due to a stagnation of accumulator flow. Consequently, single pin modeling had advantage of predicting earlier dry-out time but disadvantage of PCT prediction when compared with the base case, which modeled the core as single flow channel and two heat structures (Figure 28).

#### 5.1.2 Two Flow Channel and Two Heat Structures (Case B)

Case B, two flow channel and two heat structures, showed a later heatup

and still lower PCT but better than Case A. However, a second peak was observed and not appeared in the experiment, which was directly due to the stagnant flow from accumulator. Two flow channel and two pin model could improve the central PCT prediction but the peripheral PCT was predicted better. Figure 29 and 30 showed an earlier measurement peak, which was not predicted in calculations. The earlier peak probably was caused by a liquid deentrainment during the experiment and the modeling concept based on one-dimensional could not catch the earlier heatup.

## 5.2 Model Sensitivity Study

### 5.2.1 Reflood Option Added (Case C)

Case C, reflood option only added, predicted the PCT 10 K lower than the base case (Figure 29). The reflood initiation pressure at Volume 230060000 was set as 2.0 MPa because the overall system pressure did not go below 1.0 MPa in experiment and to turn on the reflood option as in the experiment. Case C did not include the accompanying peak during quenching, which was experienced in the base calculation. This straight quenching without the peak behaved more closely to the experiment than the base case. Therefore, using the reflood option is recommended even for the transient process pressure about 2.00 MPa.

### 5.2.2 Reflood and Gap Conductance Option Added (Case D)

Case D, both reflood and gap conductance option used, indicated the start time of clad temperature rise 10 seconds later and even lower PCT by 25

K than the base (Figure 29). The second peak during quenching was observed but the magnitude was negligible. Both models contributed to calculate the PCT lower than the base case. The higher gap conductance values, the lower PCTs were calculated. This study also indicated that the gap conductance data given in the base deck were lower than the data calculated by gap conductance model. Since the heatup rates of the two cases were similar and the PCT was underestimated, it is not recommended to use the gap conductance option for this type IBLOCA; and, instead, tabular form used in the base case is more preferable.

### 5.3 Inventory Sensitivity Study

Primary system inventory mass is the one of key safety parameters for a LOCA. It affects primarily to primary system pressure, ECCS flow rates, core blowdown/flooding rates, and PCT finally. Thus, the effect of the inventory mass was investigated to see its effects on the key T/H parameters for L5-1 type IBLOCA. Figure 31 shows the changes of the primary system inventory, which excluded the mass in the simulated steam generator and pump of the broken loop so that the initial mass and inventory were reduced during the overall transient. Figure 32 shows the effect of the mass inventory on primary system pressure. The reduced one was able to follow the transient of the experiment more closely till blowdown period around 100 seconds. Afterwards, it depressurized more rapidly so that the core started to boil off earlier and, also, the accumulator (Figure 33) and LPIS (Figure 34) were turned on earlier, too. The earlier actuation of the ECCS components resulted in quenching the heater rod to heat up earlier. Therefore, the reduced inventory affected the heater rod to heatup 10 seconds earlier but

the maximum PCT was underestimated due to the earlier ECCS actuation.

## 6. RUN STATISTICS

The input models for the base case of LOFT L5-1 included 130 volumes, 136 junctions and 143 heat structures. Figure 26 compared time step size, DT vs. transient time. Figure 27 compared CPU time vs. transient time. The ratio of CPU vs transient time came out to be about 1537/300, i.e. 5.12 for the base case calculation.

During the transient calculation the following resources were used :

	Base
Computer time CPU (s)	1537
Number of time step DT	6539
Number of Volumes C	130
Transient real time RT(s)	300

The calculated grind time (code efficiency factor) for 300 s is

$$\frac{\text{CPU} * 1600}{\text{C} * \text{DT}} = \frac{(1537) * 1000}{(130) (6539)} = 1.80 \text{ (m sec/vol/step) for Base Case}$$

The computer used was a cyber 170-875

## 7. CONCLUSIONS

RELAP5/MOD2 Cycle 35.04 code was assessed using LOFT L5-1 IBLOCA test data. A base case calculation including single flow channel and two heat structures was carried out without using reflood and gap conductance models as a reference case. Two cases of nodalization studies and two types of model sensitivity studies were conducted to quantify their effects primarily on PCT. Case A modeled the core as single flow channel and single heat structure while Case B modeled the core as two flow channels and two heat structures. Case C used reflood option over the base modeling and Case D added gap conductance option to Case C. Additional calculation with the revised initial inventory showed that it affected to reduce the primary system pressure more rapidly and, therefore, the fuel rod started to heat up 10 seconds earlier so that the accumulator and LPIS were turned on earlier, too. Consequently the revised one improved to predict the core heatup time but the maximum PCT was predicted not more accurately due to the earlier injection flows from accumulator and LPIS. Based on the results from the given scope, the following conclusions can be made.

- 1) Using LOFT IBLOCA test data L5-1, a base case calculation with a base nodalization was successfully executed and matched fairly well with the LOFT IBLOCA L5-1 experimental data.
- 2) The code with base nodalization showed that core clad temperature rise occurred 25 sec later and underpredicted the PCT by 40 K in comparison with the experiment. The modeling with a single flow channel and a single heat structure improved the start of clad temperature rise (heatup) by 10 seconds

but underpredicted the PCT worse by 50 K, compared with the experiment. The model with two-channel and two heat structures predicted the PCT a little better than Case A by 5 K but heatup started later than the base case by 10 seconds. Therefore, the base modeling, a single flow channel and two heat structures, proves to be better than the Case A and the Case B to predict the PCT for LOFT IBLOCA L5-1 transient.

3) The base modeling did not predict the early peak occurred at 125 sec as in temperature measurement at T-4E8-045 (Figure 50) and the limitation of one dimensional modeling caused not to predict the earlier peak observed in the experiment. The model with two channels and two pins improved to predict the PCT in the peripheral assemblies by 20 K compared with the base case; but, still the code overpredicted the reflood PCT at the peripheral assemblies because the modeling assumed higher LHGR.

4) Model sensitivity studies revealed that the case with reflood model option underpredicted the PCT more than the base case by 10 K. The case with both reflood and gap conductance option underpredicted the PCT even worse than the base case by 20 K. Consequently, if both model options were added, then lower PCT was calculated. The higher the gap conductance values, the lower PCTs were calculated. This means that the gap conductance data inputted to the base deck are lower than the values calculated from gap conductance model. So it is recommended to use reflood option and not to use gap conductance option additionally for the IBLOCA application.

5) 25 seconds later dry-out time encountered in calculating the core thermal behavior was not significantly improved through the four proposed sensitivity

studies although Case A improved the start time of dry-out by 10 seconds. Results with the revised initial inventory mass indicated that the reduced inventory improved the core heatup time 10 seconds but the maximum PCT was underestimated due to the earlier injection of accumulator and LPIS. The code should model the depressurization properly to predict the heatup and the CHF modeling at the corresponding pressure and flow rates during the blowdown was the area for further improvements[12,13,14]. So, the originally proposed L5-1 base modelling is the optimum for LOFT IBLOCA Test L5-1 simulation among the tested cases.



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14. H. J. Kim, Letter to R. R. Schultz, Jan 17, 1991

Table 1 INITIAL CONDITIONS FOR EXPERIMENT L5-1

Parameter	Experiment L5-1 Measured Value (EDR [8])	REALP5/MOD2/Cycle 36.04 Calculated Value (L51S12) [I.C. of L51T12]
Primary System		
Mass flow (kg/s)	308.20	308.27
Hot leg pressure (MPa)[a]	14.93	14.87
Cold leg temperature (K)	552.30	553.76
Hot leg temperature (K)	579.10	581.34
Boron concentration (ppm)	669.00	-
Vessel DT (K)	26.80	27.58
Reactor Vessel		
Power level (MW)	45.90	45.77
Max LHGR (kW/m)	46.00	42.50
Pressurizer		
Vapor volume (m3)	0.33	-
Liquid volume (m3)	0.60	-
Liquid temperature (K)	615.00	614.48
Liquid level (m) [a]	1.13	1.10
Broken Loop		
Cold leg temperature (K)	549.20	557.40
Hot leg temperature (K)	554.30	561.75
Steam Generator Secondary Side		
Liquid level (m) [b]	0.27	0.287
Liquid temperature (K)	537.80	533.210
Pressure (MPa)	5.05	5.010
Mass flow (kg/s)	25.30	24.493
Accumulator A		
Liquid level (m) [c]	1.49	1.490
Pressure (MPa)	1.66	1.660
Liquid temperature (K)	308.20	308.200

- [a] Out of specification, but did not impair results  
[b] The liquid level is defined as 0.0 at 2.95 m above the top of the tube sheet  
[c] Liquid level is measured from 0.32 m above the bottom of the accumulator vessel

Table 2 SEQUENCE OF EVENTS FOR EXPERIMENT L5-1

Events	Time after Experiment Initiation (s)		
	Experiment L5-1 [8]	Calculation L5IT12	
Cold leg QOBV opened [a]	0.0	0.0	
Reactor scrammed	0.17	0.06	
Main feed pump tripped and steam control valve started to close	0.17	0.07	
Upper plenum reached saturation	0.20	0.25	
HPIS trip point reached (10.6 MPa)	0.40	0.30	
HPIS injection flow initiated	2.88	2.90	
Primary coolant pump tripped	4.00	4.00	B.C.
Broken loop cold leg reached saturation	10.50	11.00	
Steam generator steam control valve closed	12.10	12.00	
Pressurizer indicated empty	15.50	15.00	
Primary pressure dropped below secondary	53.00	50.00	
Fuel cladding thermal excursion started	108.40	141.00	
Lowest in-core thermal excursion level reached	184.00	181.00	
Accumulator A injection started	185.80	187.25	
Maximum fuel cladding temperature reached (715 K for Experiment L5-1)	198.00	207.00 (675 K at 23004)	
LPIS flow initiated	201.00	195.49	

[a] Experiment initiation is defined to be the time when the broken loop cold leg pressure began to increase.

Table 3 List of Assessment Parameters (LOFT L5-1)

Description	Calculation	Measurement	Uncertainty	Figure
Primary System				
Pressure (Pa)	P 25001	PE-1UP-001A	0.140-0.777	3
Steam Dome			EDR [8]	
Pressure (Pa)	P 53001	PE-SGS-001	0.087-0.077	4
Steam Mass				
Flow rate (kg/s)	MFLOWJ 54000	FT-P004-012	0.28	5
Feedwater Mass				
Flow Rate (kg/s)	MFLOWJ 56900	FT-P004-722	2.40	6
Primary System				
Inventory (kg)	CNTRVAR 72	Fig 4 EDR	300.0	7
ILHL				
Density (Mg/m <sup>3</sup> )	RHO 10001	DE-PC-002B	0.13	8
BLCL				
Density (Mg/m <sup>3</sup> )	RHO 34501	DE-BL-002B	0.099	9
HPIS Volume				
Flow Rate (L/s)	MFLOWJ 64000	FT-P128-104	0.014	10
Accumulator				
Level (m)	CNTRVAR 4	LE-ECC-01A	0.007	11
LPIS Volume				
Flow Rate (L/s)	MFLOWJ 63000	FT-P120-085	0.37	12
ILHL Mass				
Flow Rate (kg/s)	MFLOWJ 10001	FT-P139-272	4.6	13
Reflooding Mass				
Flow Rate (kg/s)	MFLOWJ 23001	-	-	14
Integrated Break				
Mass Flow Rate (kg/s)	CNTRVAR 51	QLR [9]	-	15
Pressurizer				
Level (m)	CNTRVAR 2	-	-	16
Steam Generator				
Level (m)	CNTRVAR 1	-	-	17
Reactor Water				
Level (m)	CNTRVAR 0	-	-	18
Cladding Temp (K)	2300110 (7.5 ")	T-5E8-015	4.2 K	
(Central, 15 inch)	2300210 (19.5 ")		at 600 K	19
Cladding Temp (K)	2300310 (27.5 ")	T-5F4-021	"	
(Central, 21 & 26 ")		T-5F4-026	"	20
Cladding Temp (K)	2300410 (36.5 ")	T-5D8-037	"	
(Central, 37 inch)			"	21
Cladding Temp (K)	2300510 (45.5 ")	T-5E8-049	"	
(Central, 49 inch)	2300610 (52.5 ")		"	22
Cladding Temp (K)			"	
(Peripheral, 26 ")	2310310 (27.5 ")	T-4F9-026	"	23
Cladding Temp (K)			"	
(Peripheral, 45 ")	2310510 (45.5 ")	T-4E8-045	"	24
Void Fraction	VOIDF 23001 - 06	-	-	25
Time Step,DT (sec)	CNTRVAR 81	-	-	26
CPU time (sec)	CPUTIME	-	-	27

- Not available

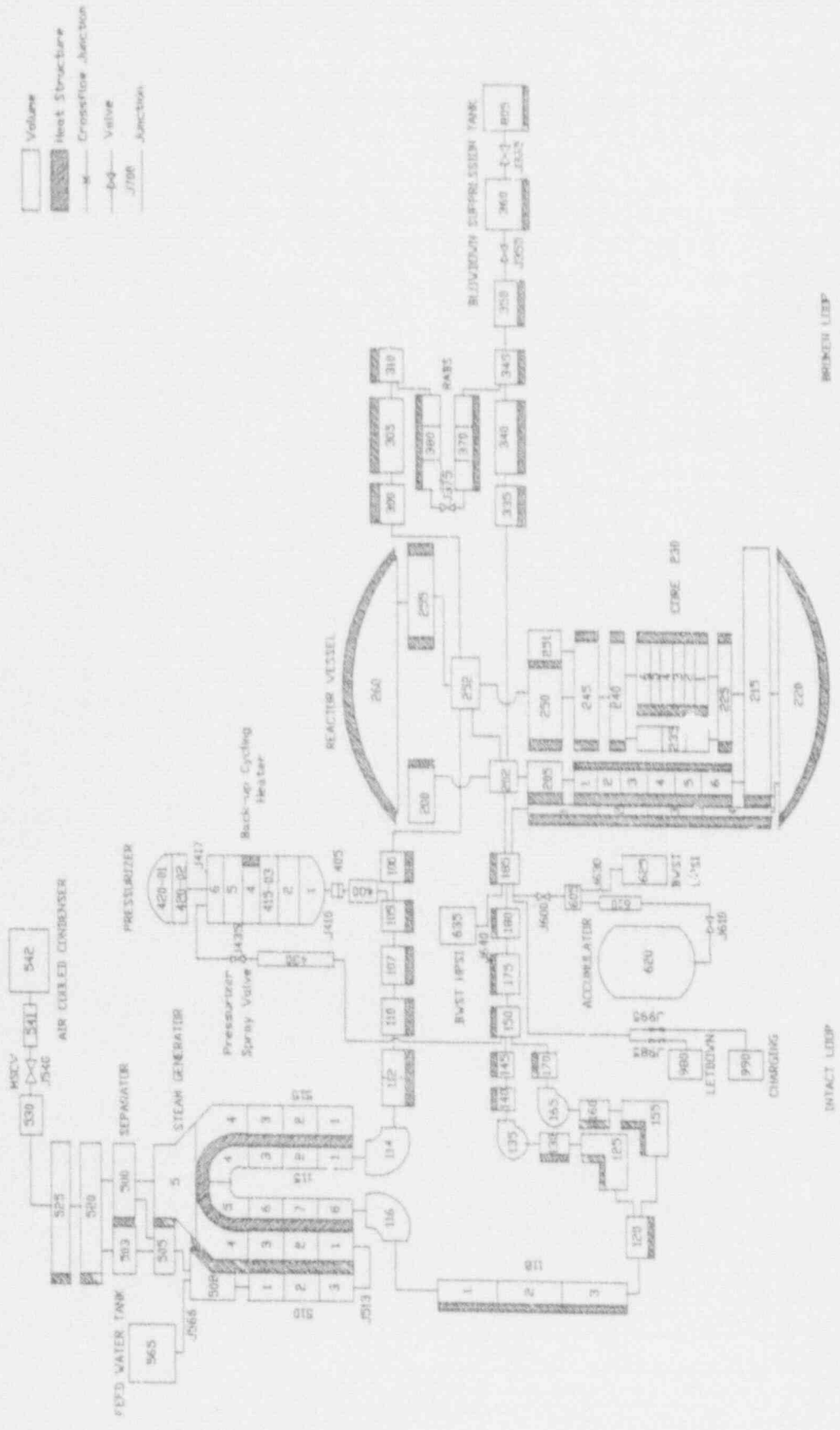


Figure 1. RELAP5 Nodalization for 40FT Test 45-1

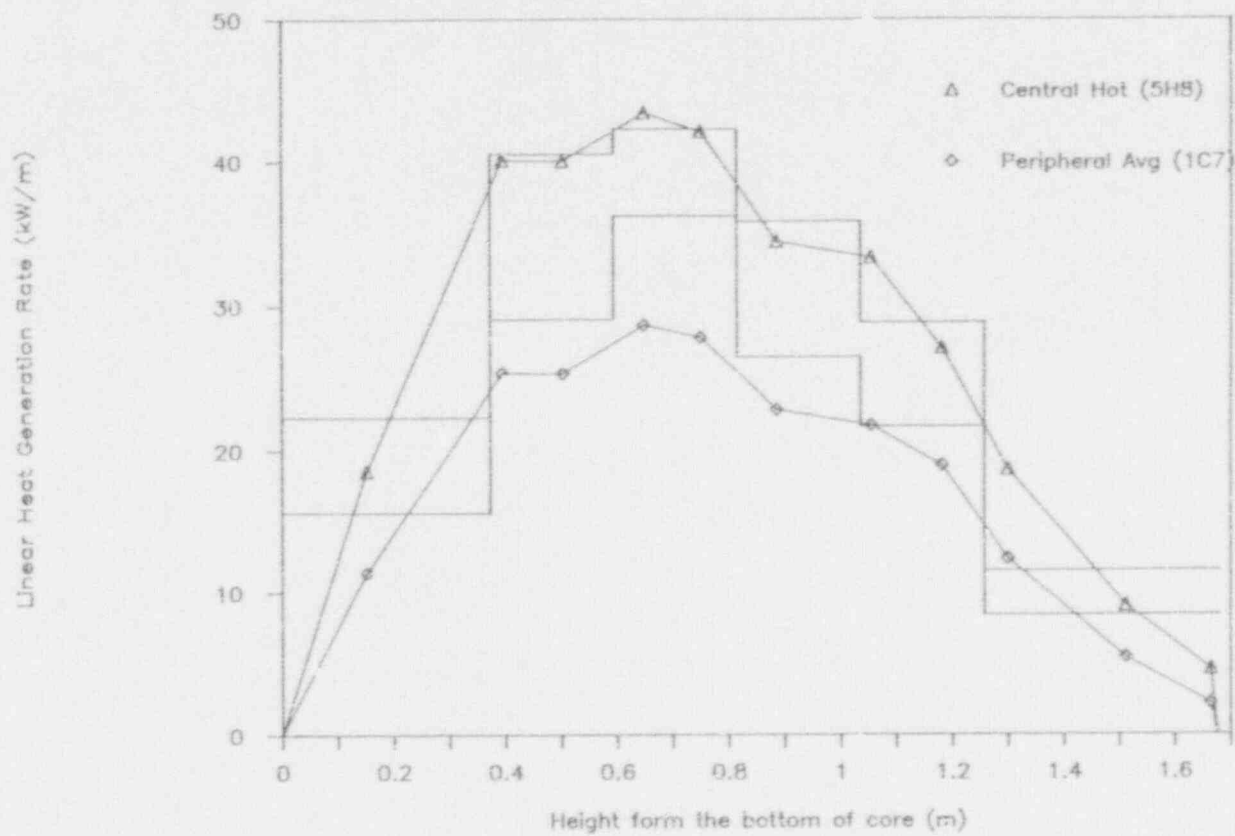


Figure 2. Axial profile of linear heat generation rate for Test L5-1

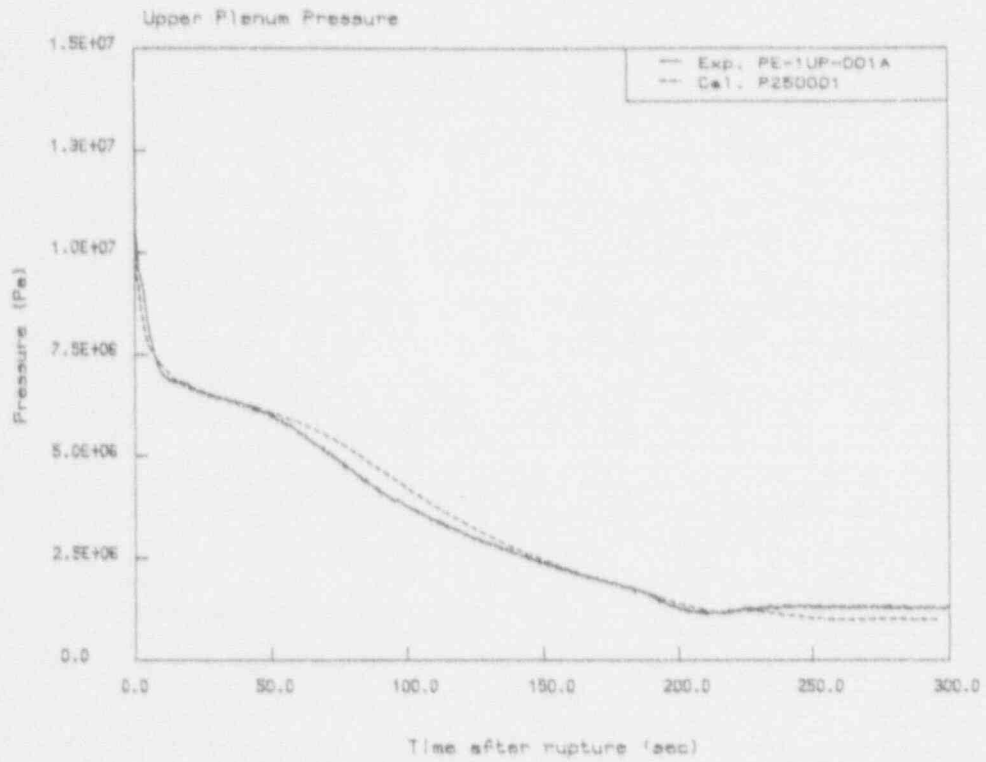


Figure 3. Upper plenum pressure transient

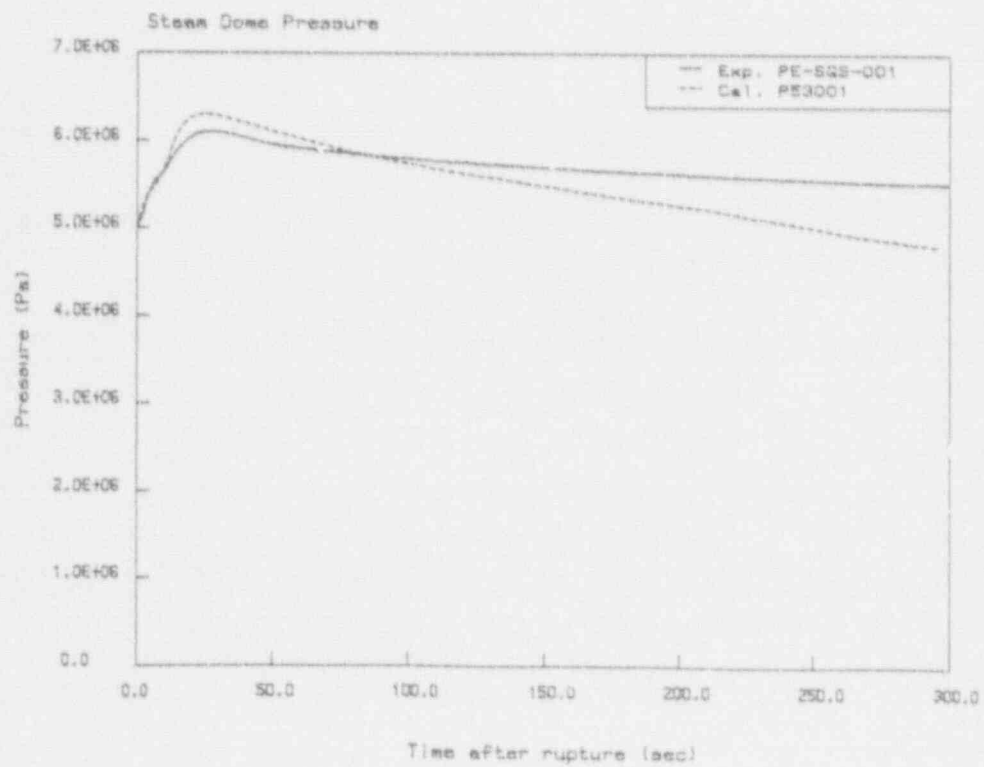


Figure 4. Steam dome pressure transient

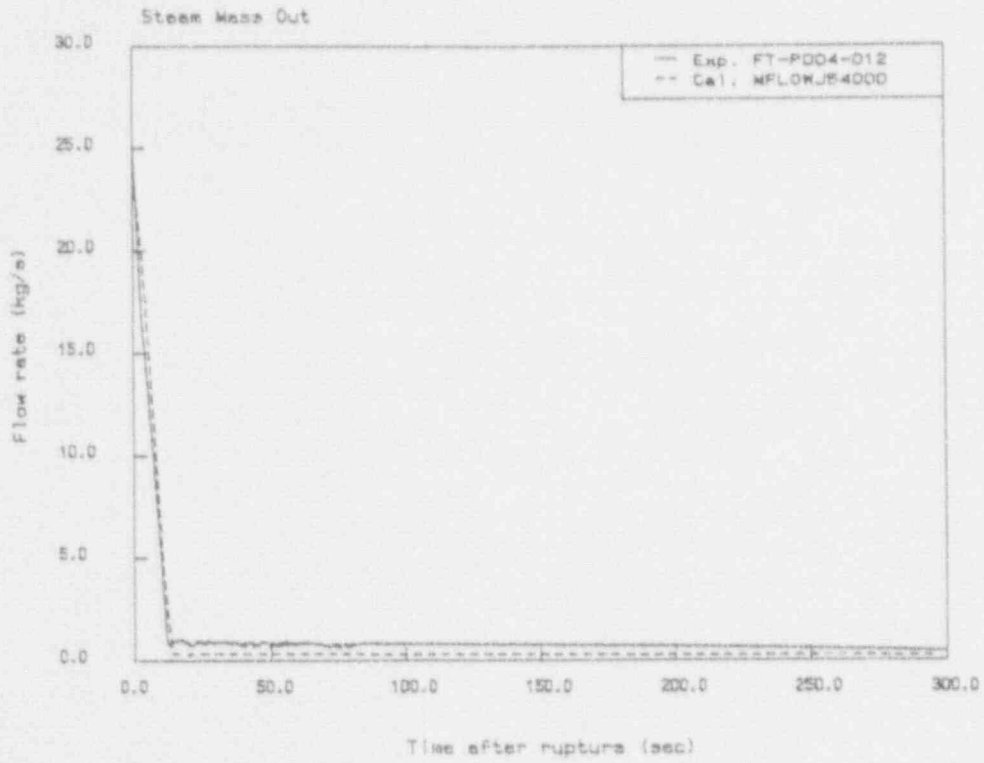


Figure 5. Steam mass flow rate transient

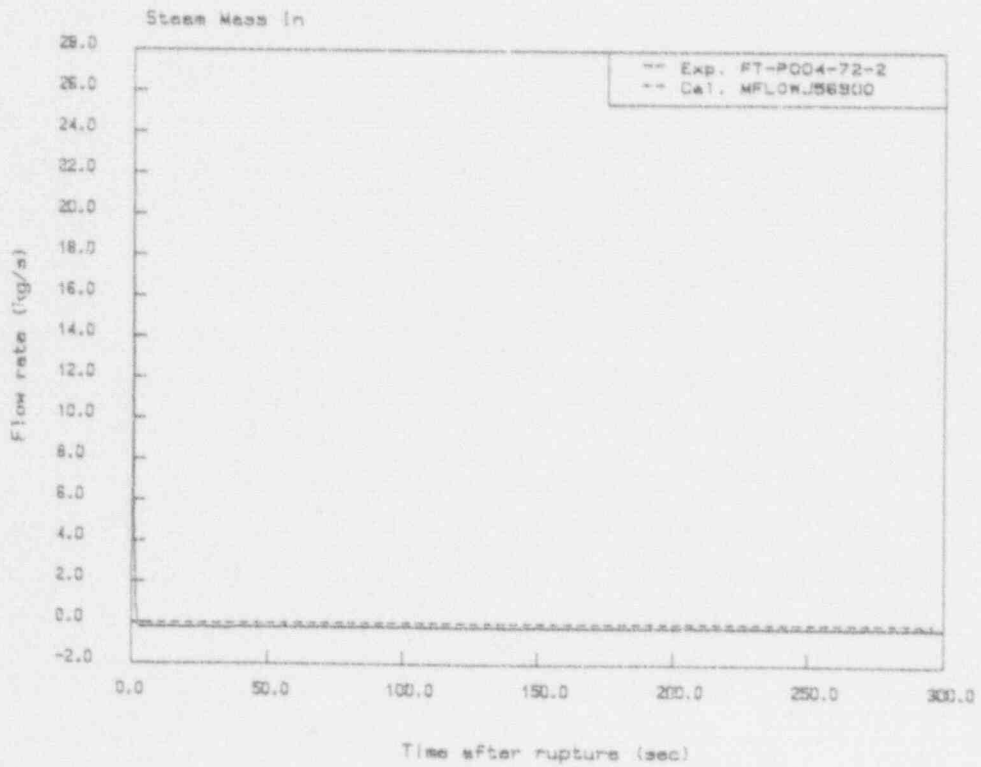


Figure 6. Feedwater mass flow rate transient



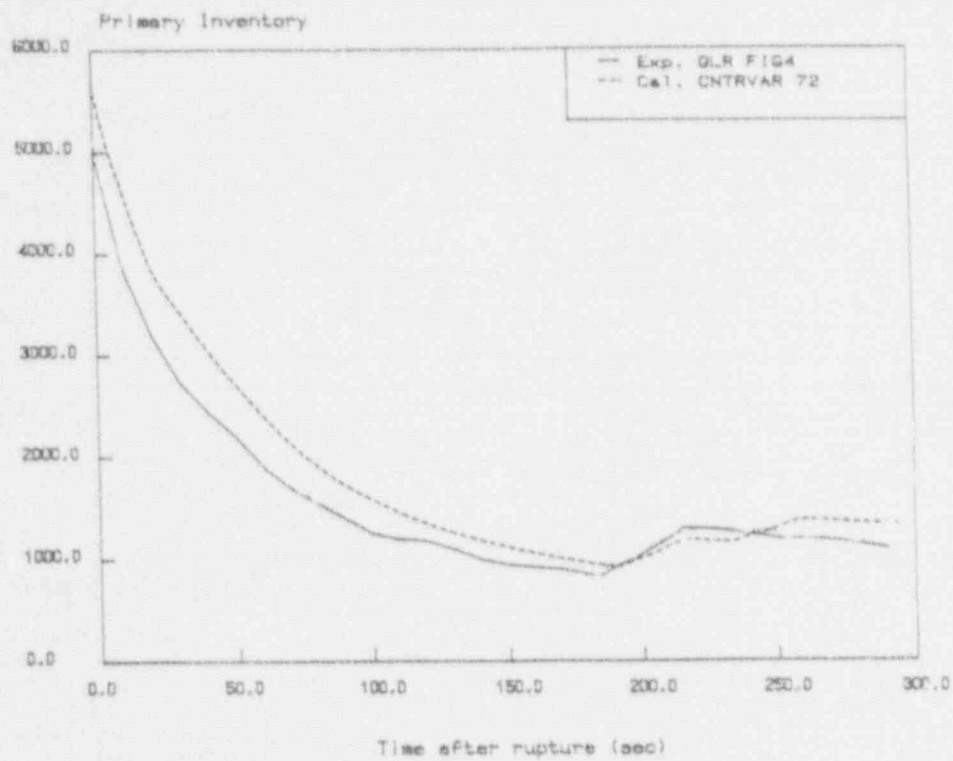


Figure 7. Primary system inventory transient

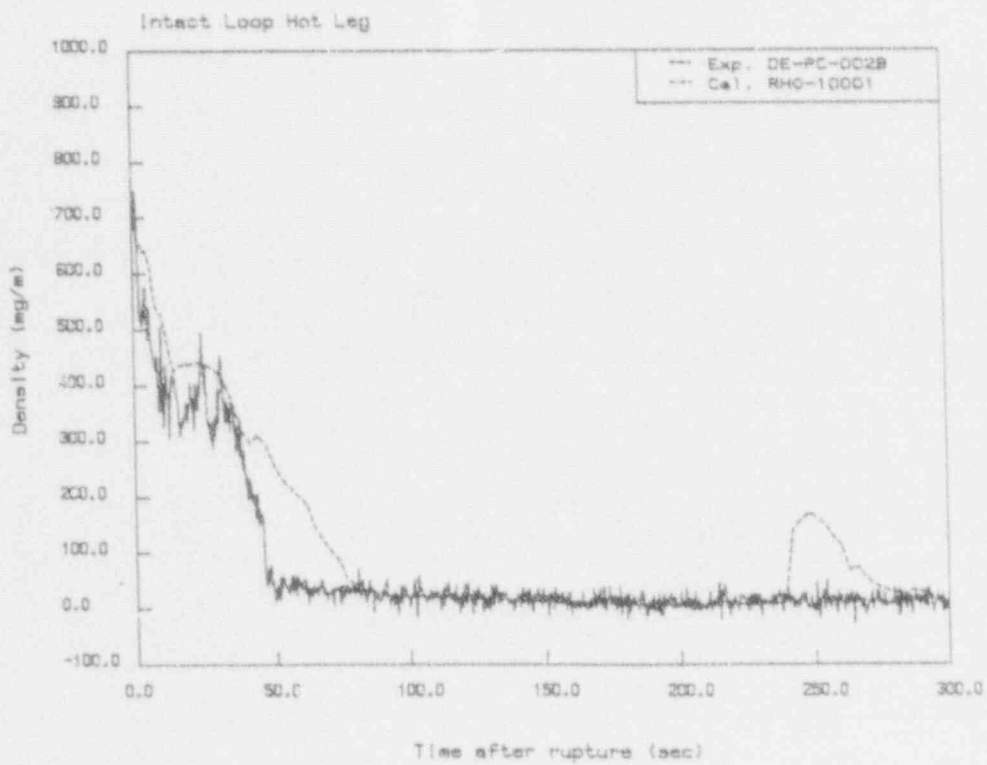


Figure 8. Intact Loop Hot Leg density transient

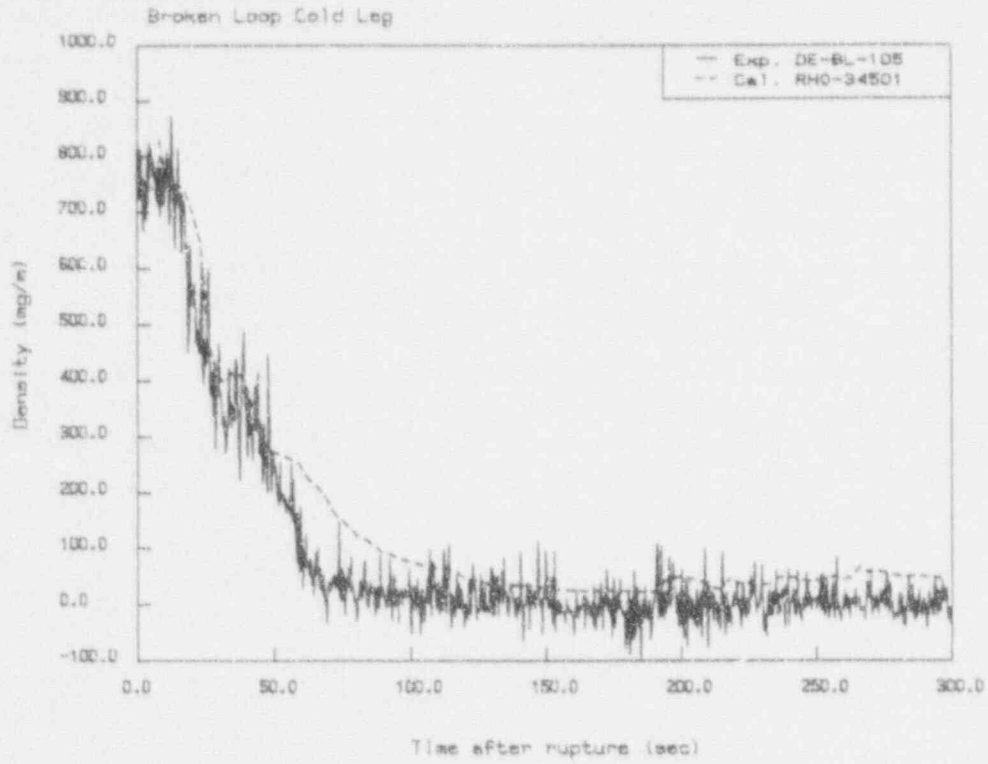


Figure 9. Broken Loop Cold Leg density transient

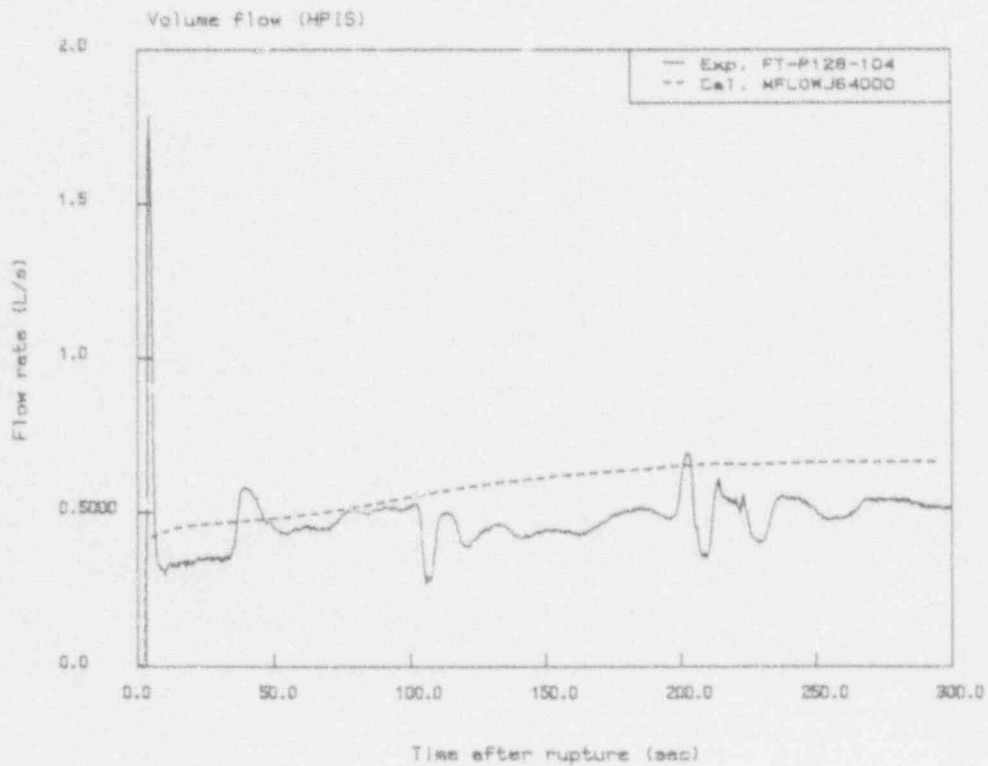


Figure 10. HPIS volume flow rate transient

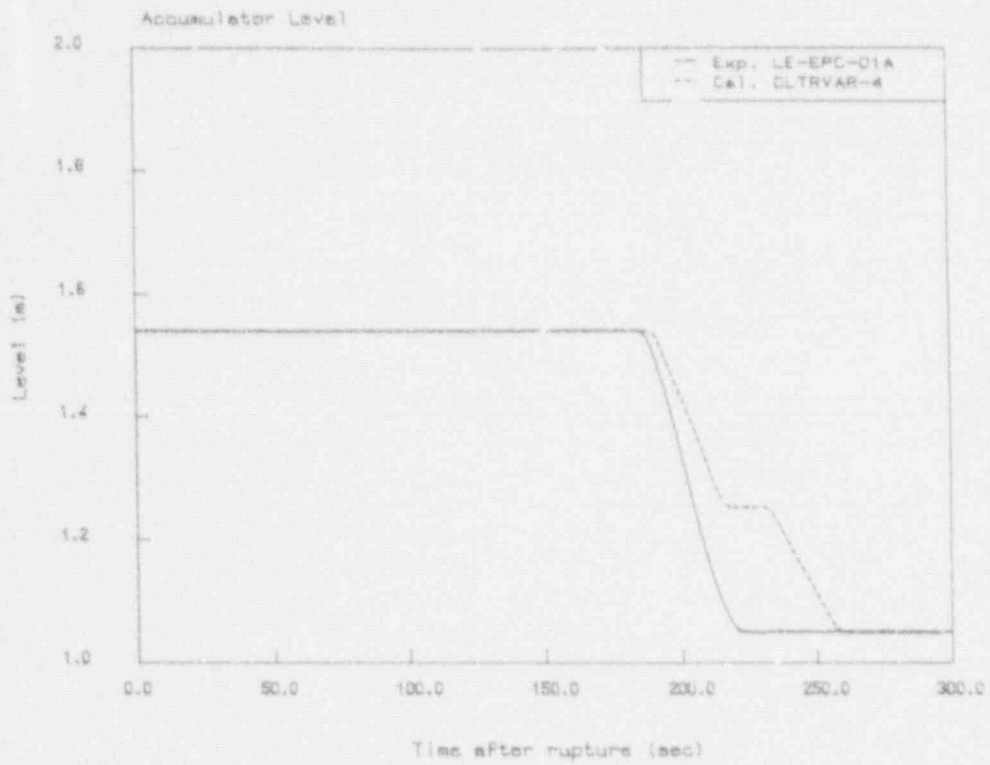


Figure 11. Accumulator level transient

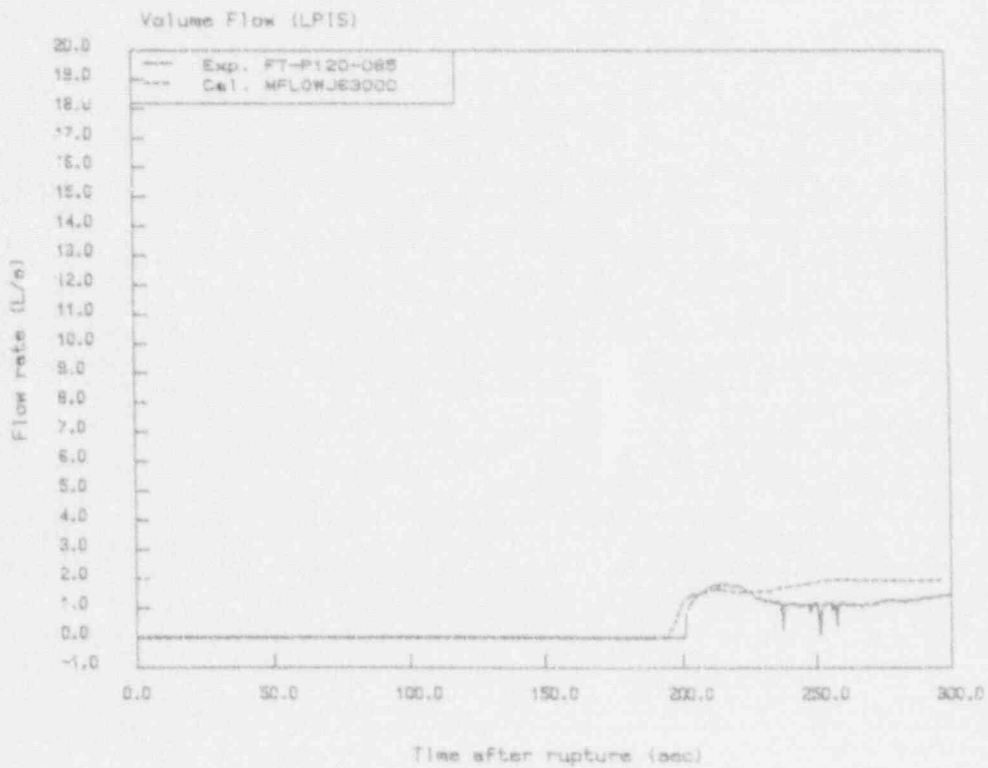


Figure 12. LPIS volume flow rate transient

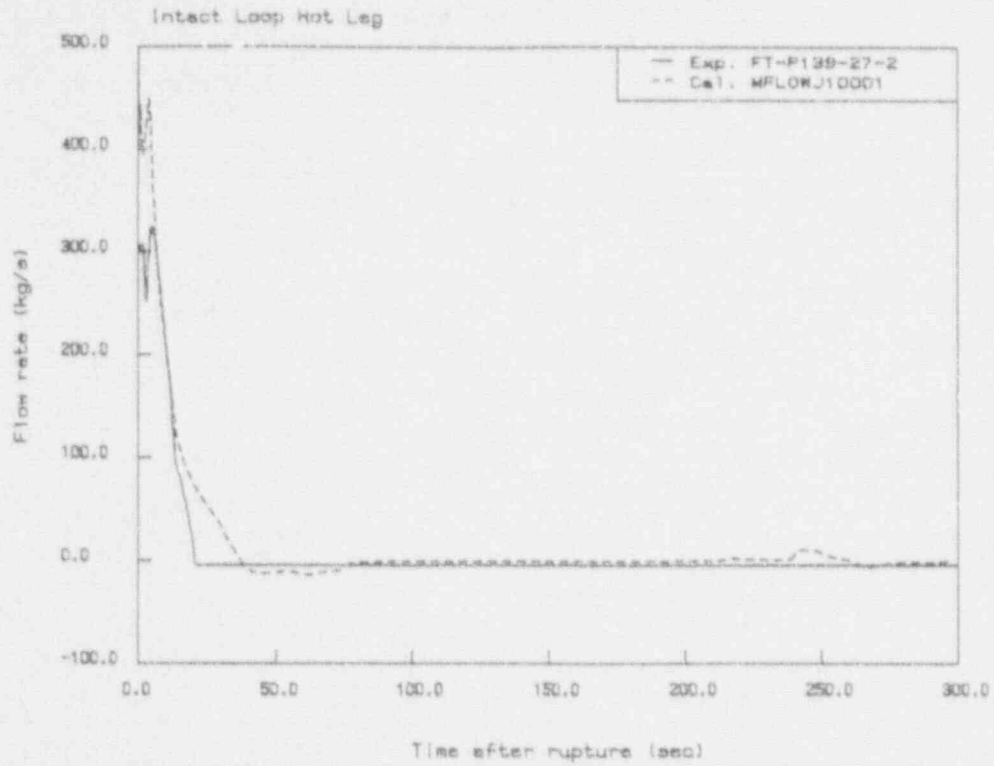


Figure 13. Intact Loop Hot Leg mass flow rate transient

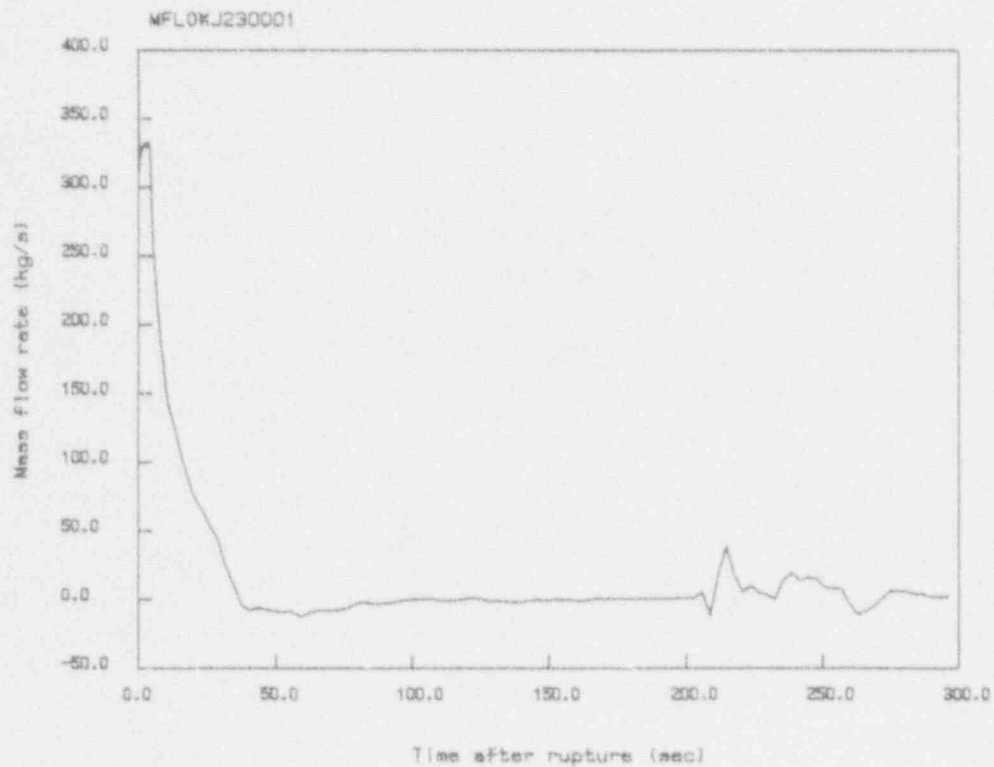


Figure 14. Reflooding mass flow rate transient

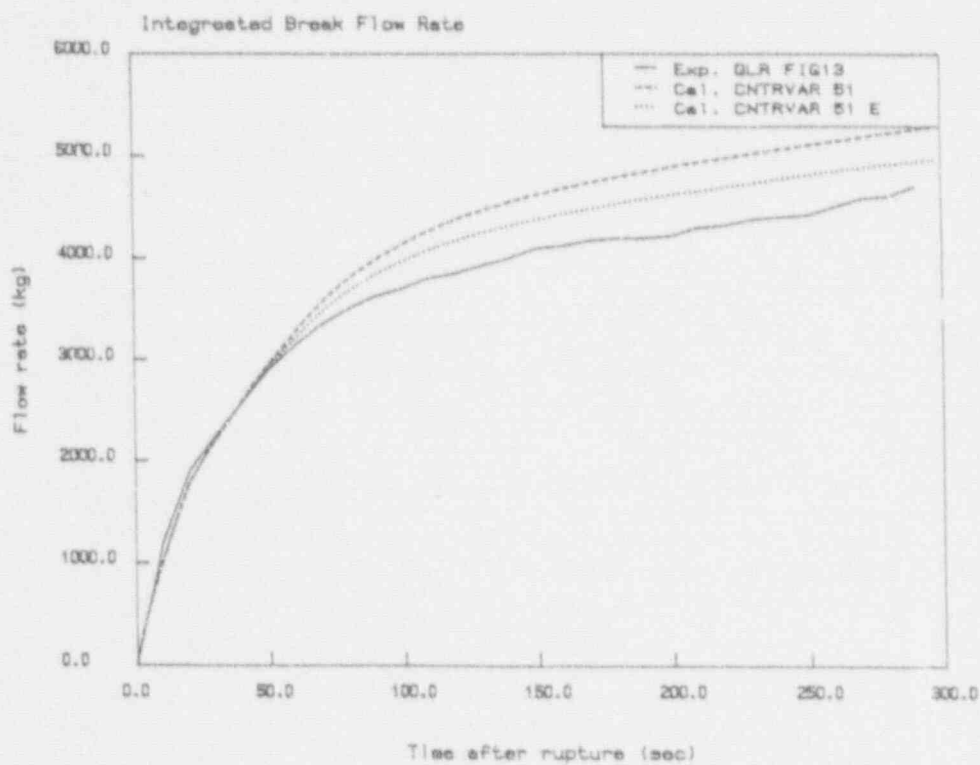


Figure 15. Integrated break mass transient

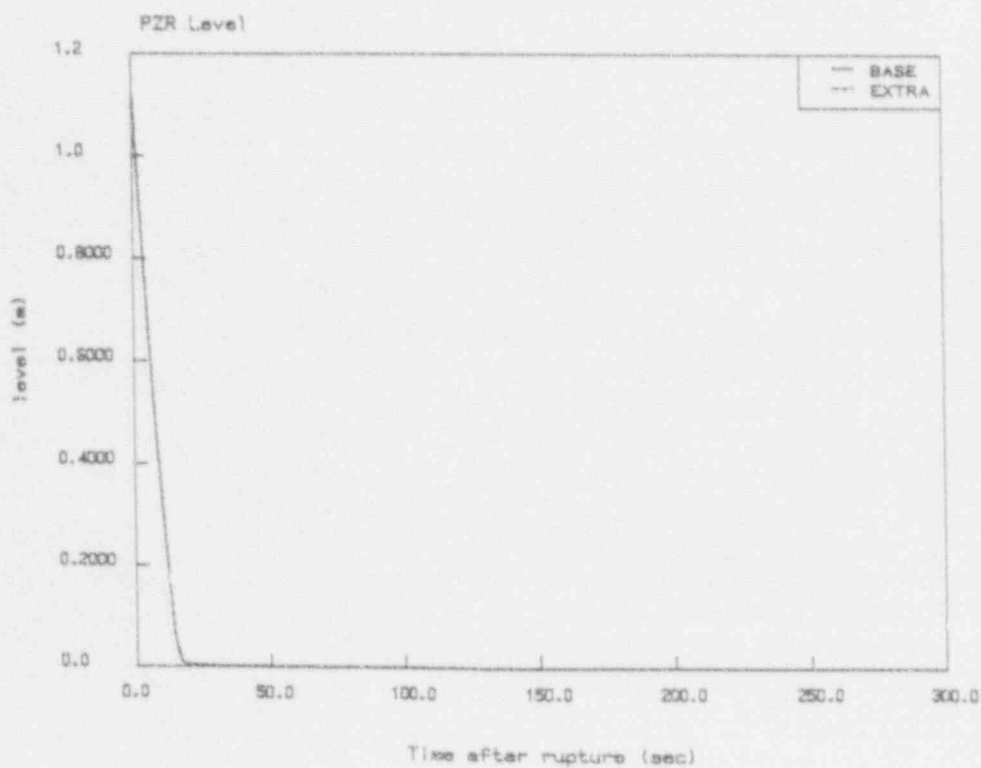


Figure 16. Pressurizer level transient

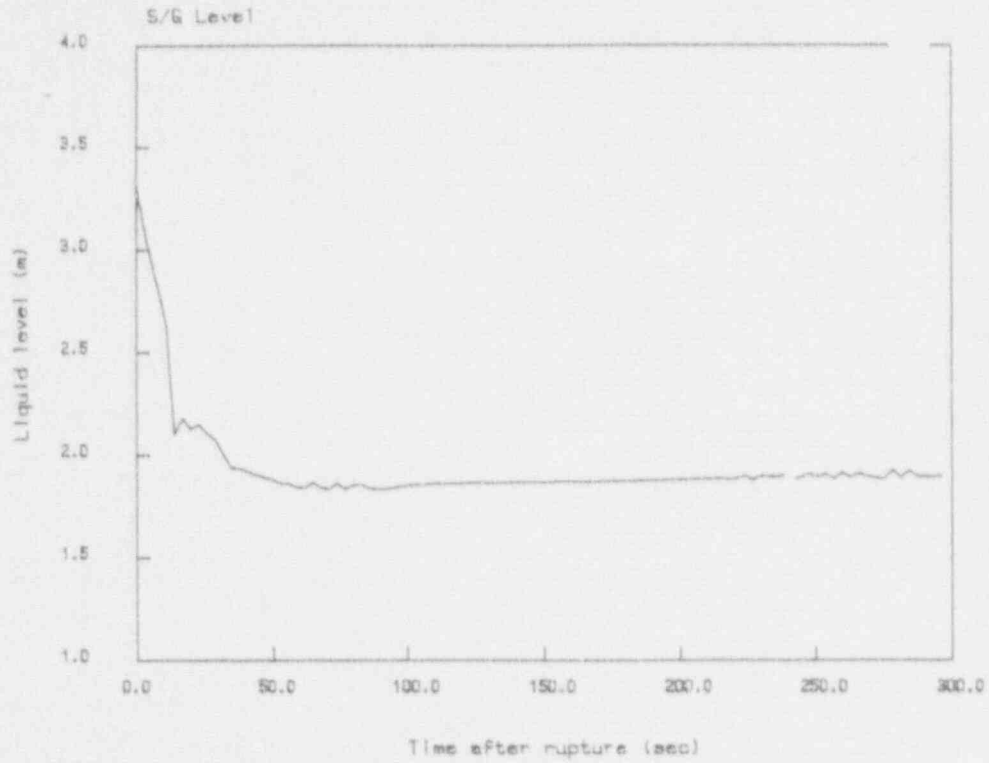


Figure 17. Steam generator level transient

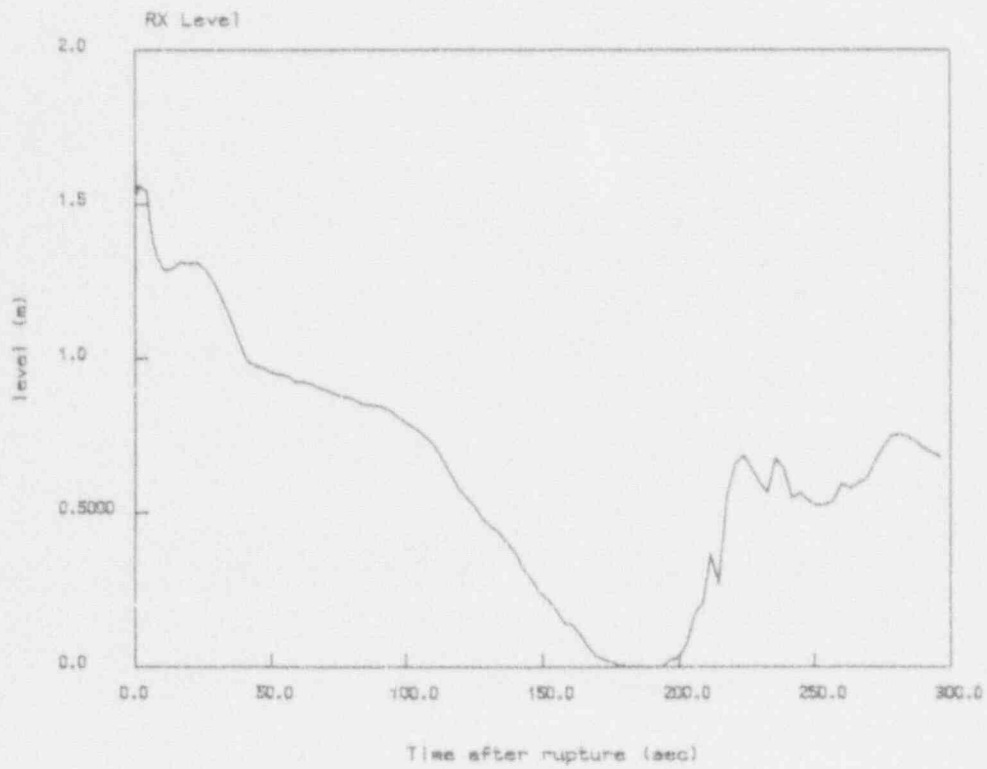


Figure 18. Reactor liquid collapsed level transient

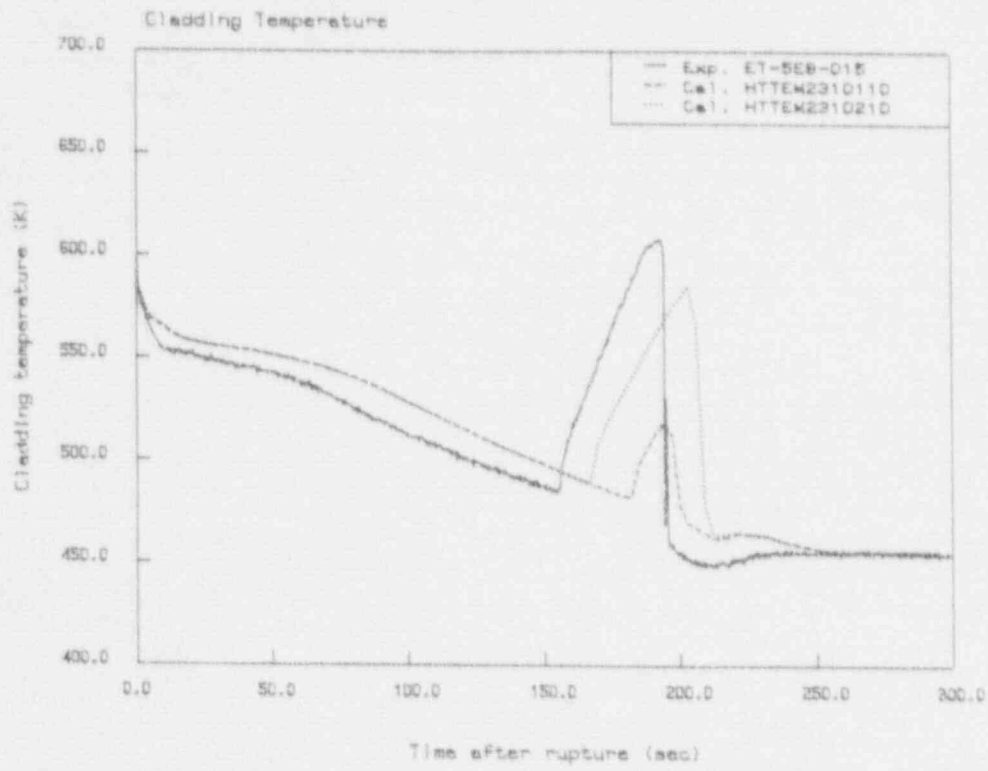


Figure 19. Cladding temperatures at central 15 inch

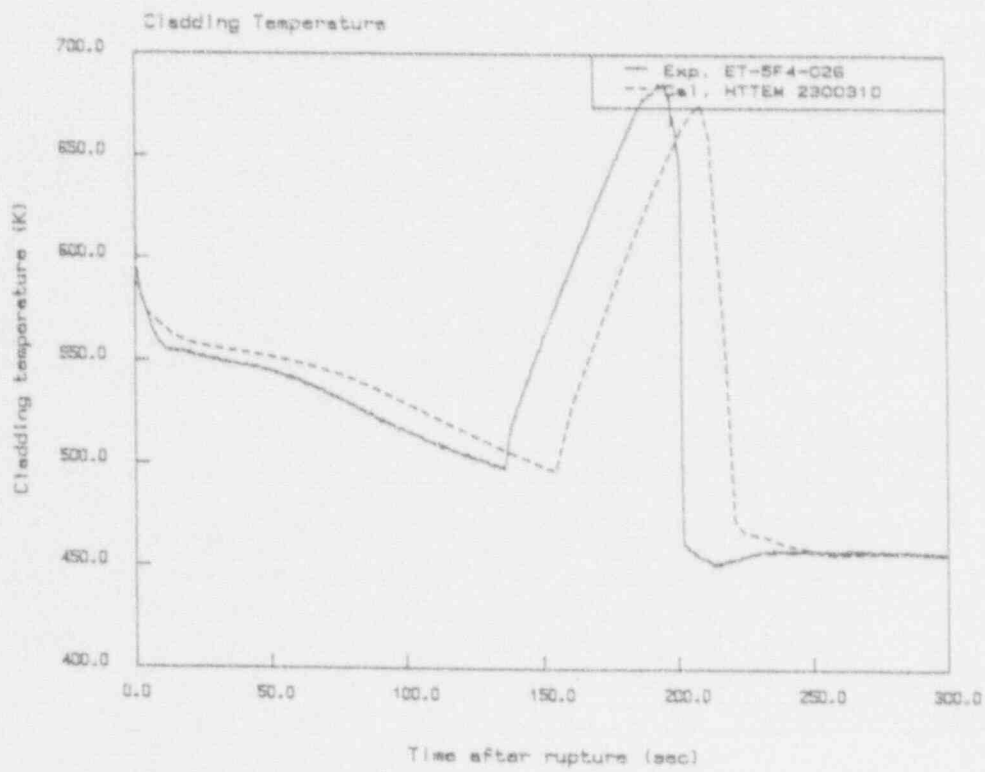


Figure 20. Cladding temperatures at central 21 and 26 inches

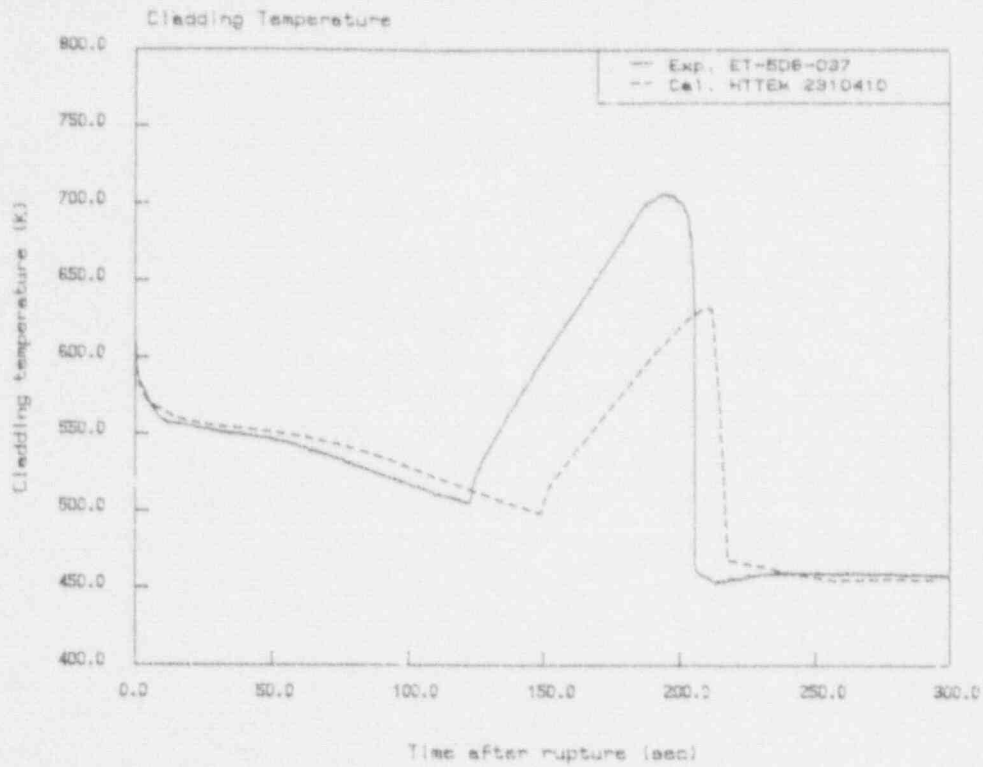


Figure 21. Cladding temperatures at central 37 inch

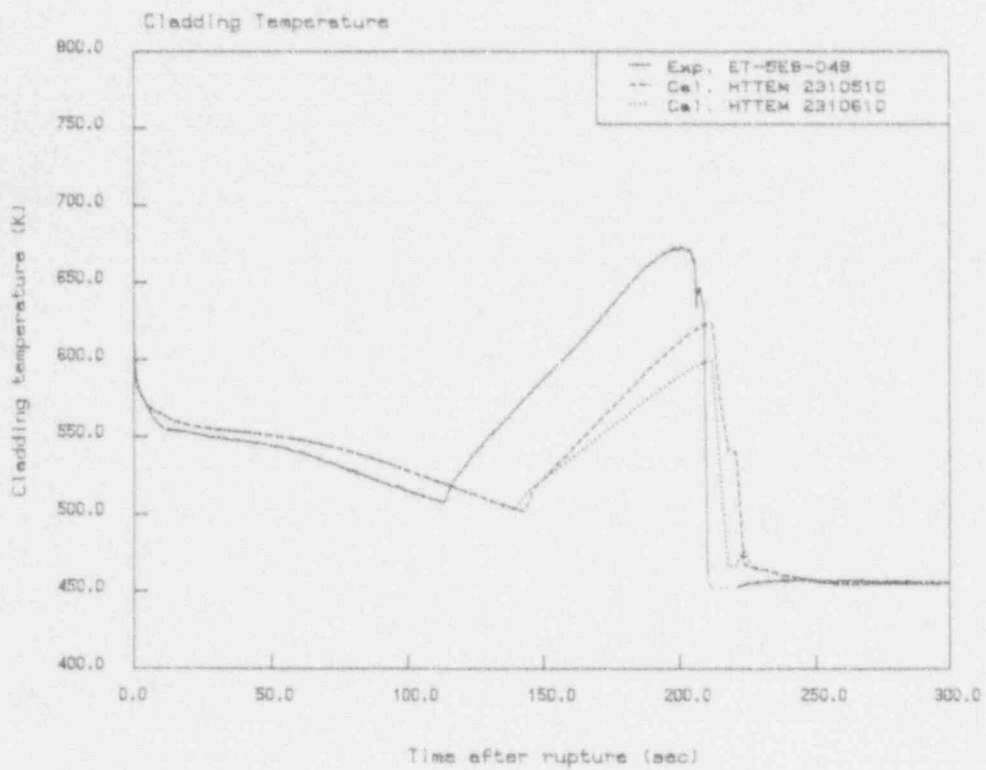


Figure 22. Cladding temperatures at central 49 inch



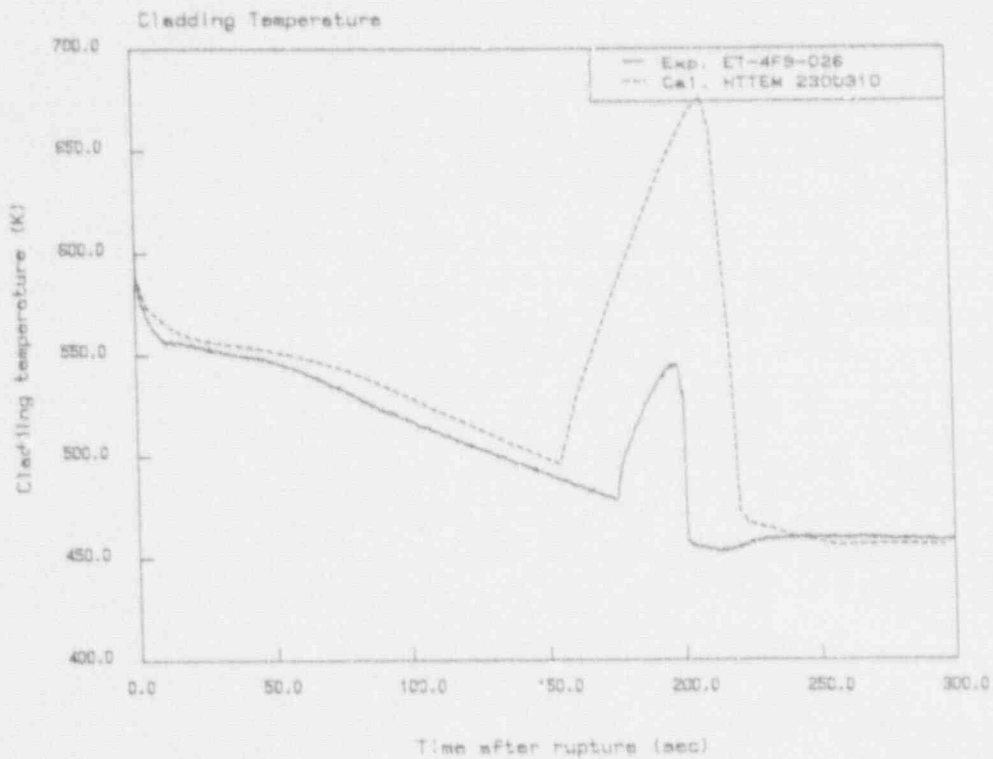


Figure 23. Cladding temperatures at peripheral 26 inch

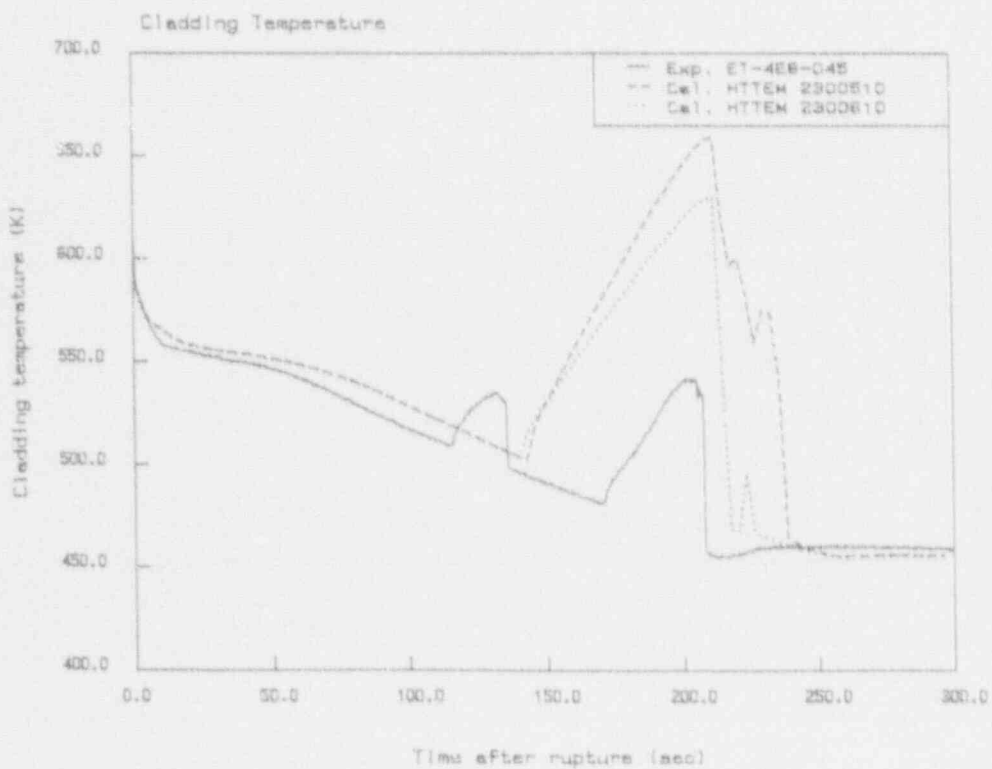


Figure 24. Cladding temperatures at peripheral 45 inch

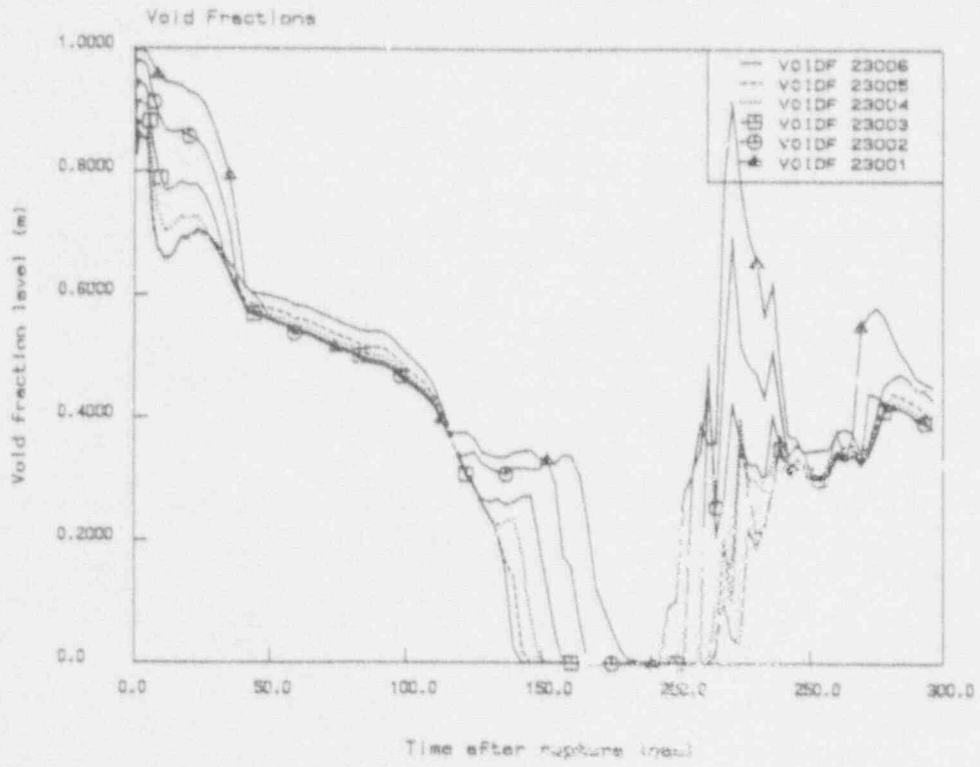


Figure 25. Liquid fractions along the core

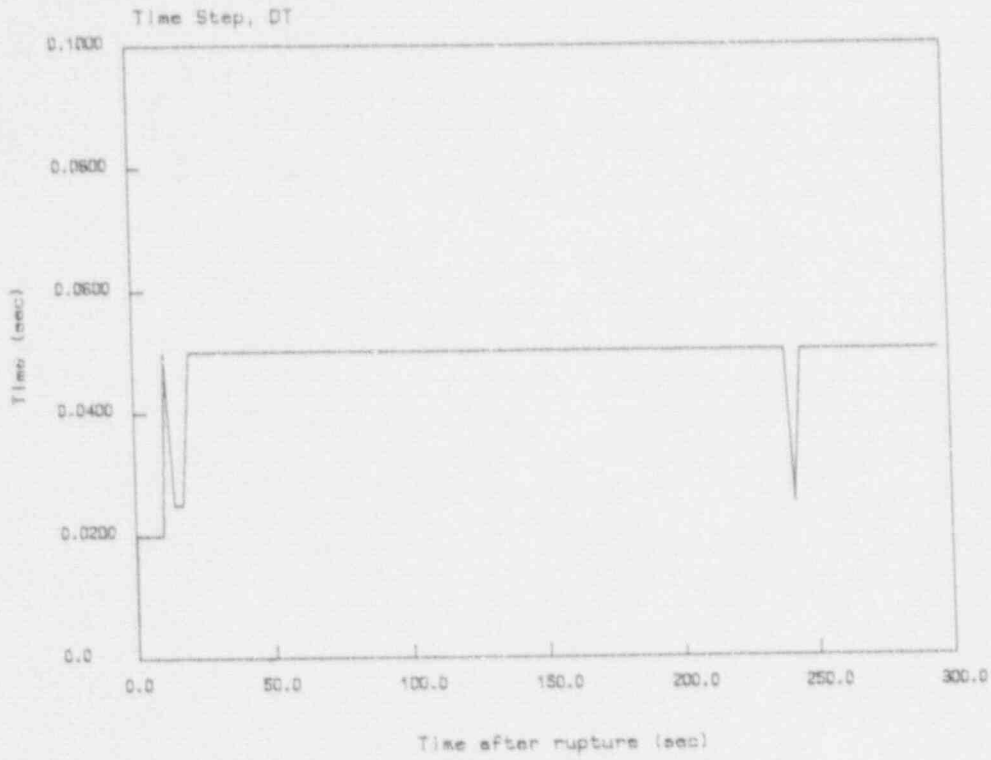


Figure 26. Time step size

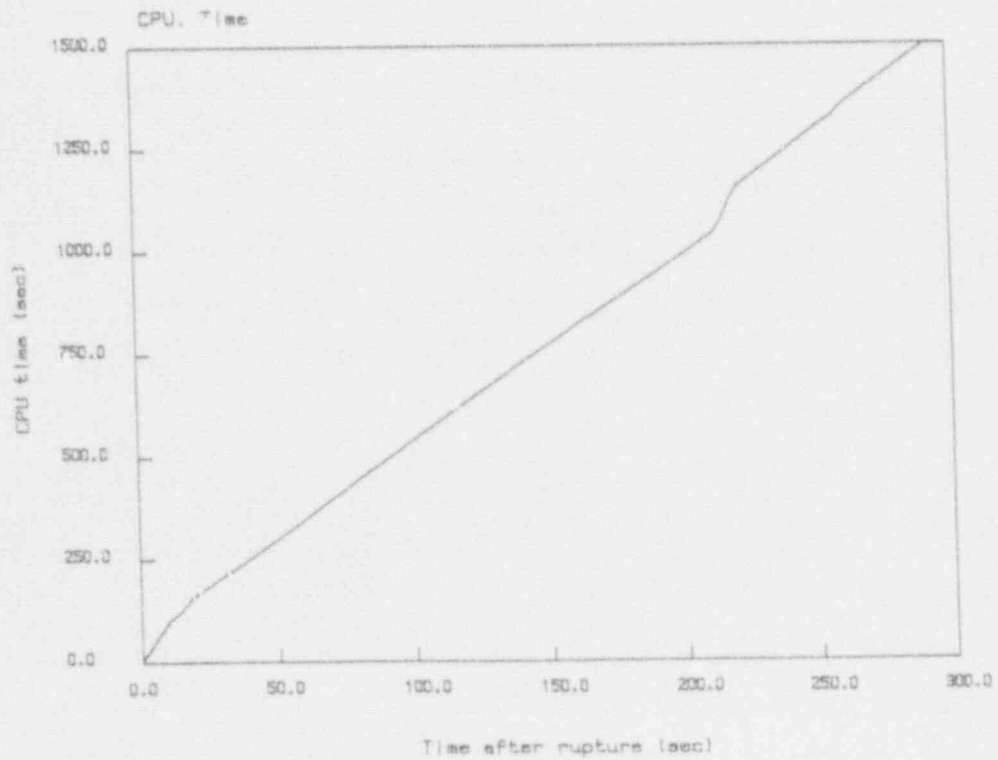


Figure 27. CPU time

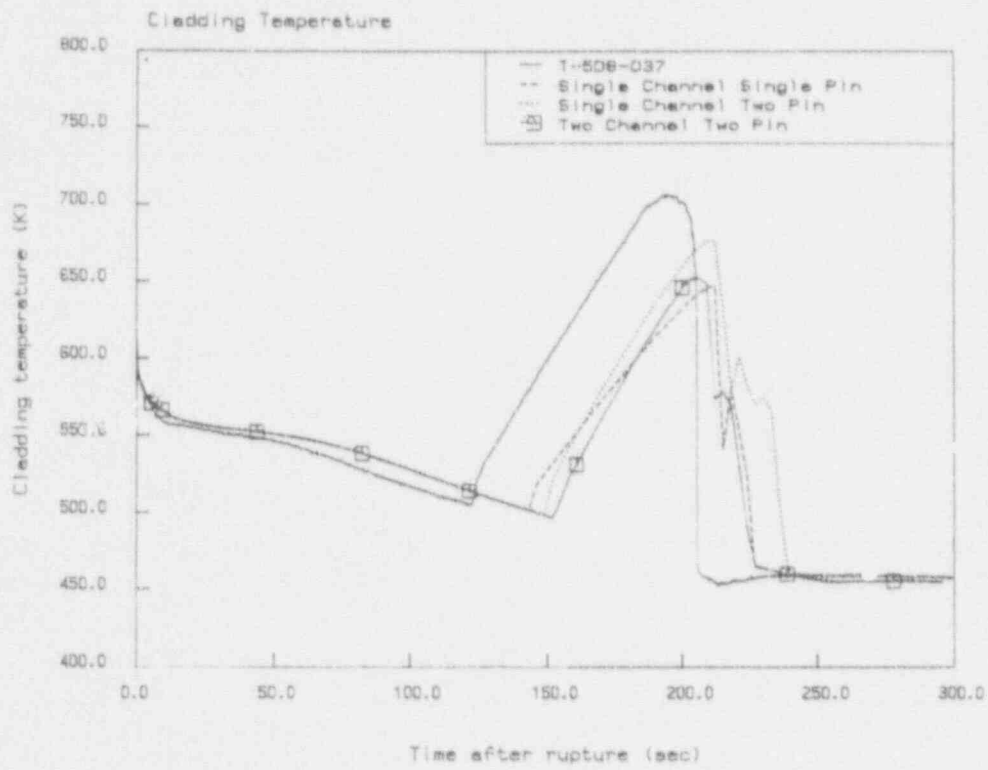


Figure 28. The effect of core nodalization sensitivity on PCT

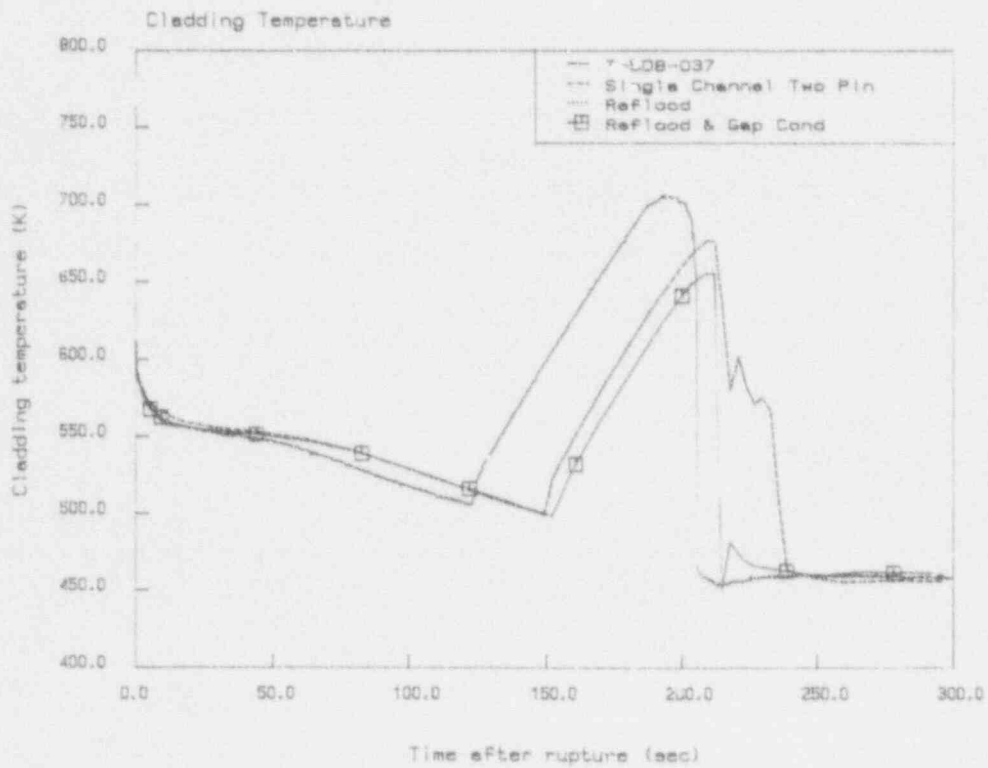


Figure 29. The effect of model option sensitivity on PCT

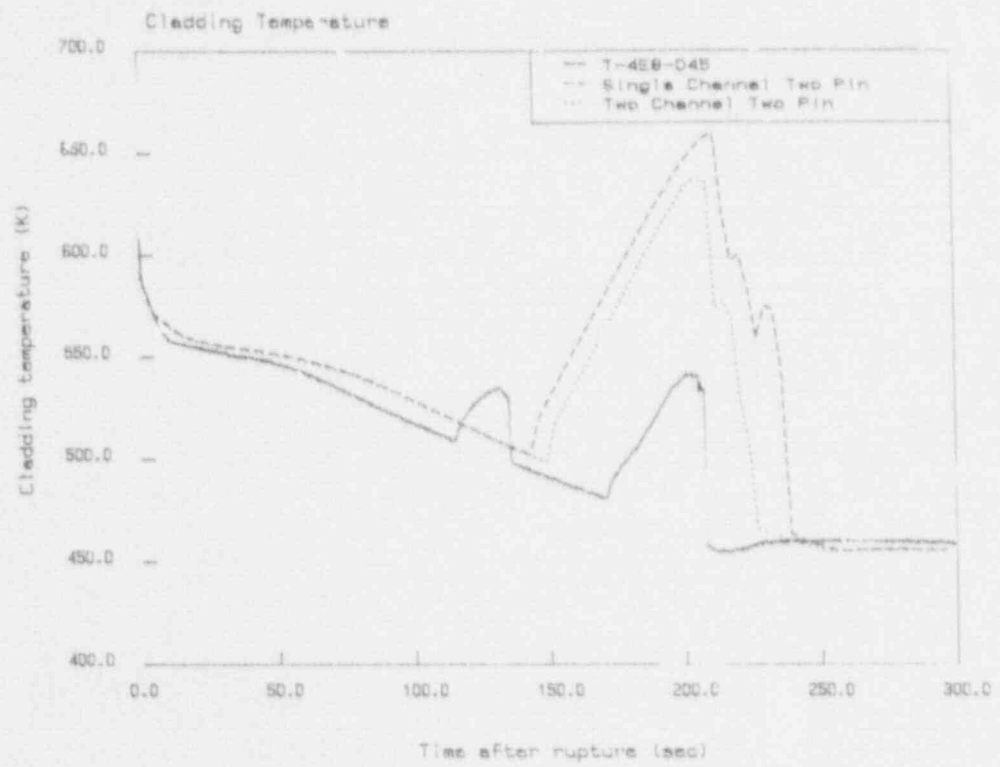


Figure 30. The effect of two flow channels on peripheral clad temperature

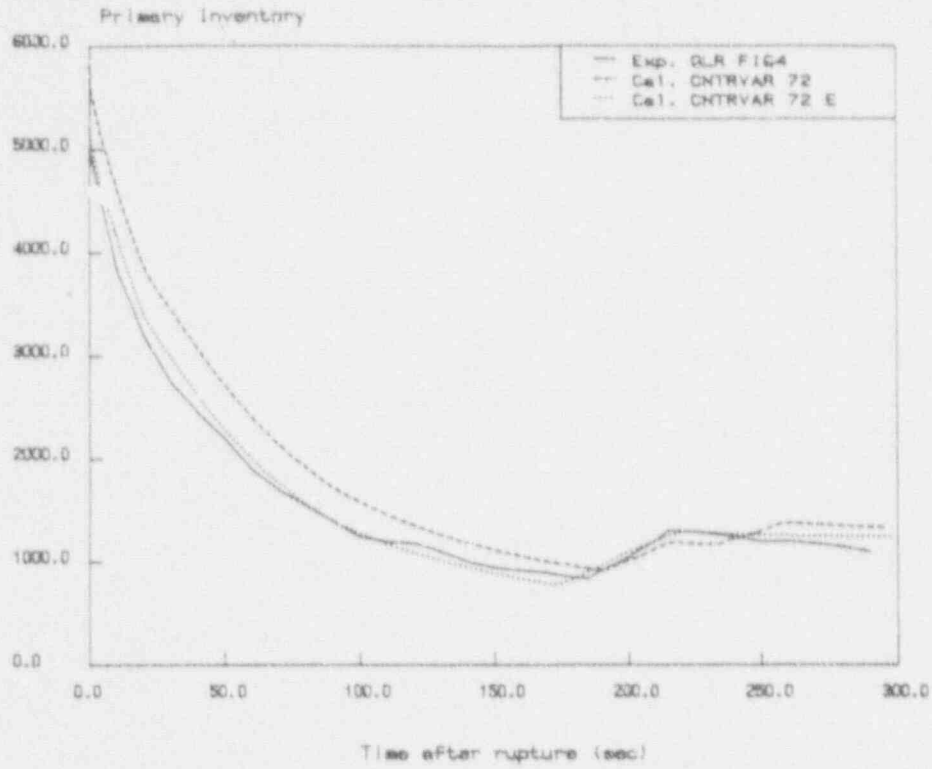


Figure 31. The changes of primary system inventory

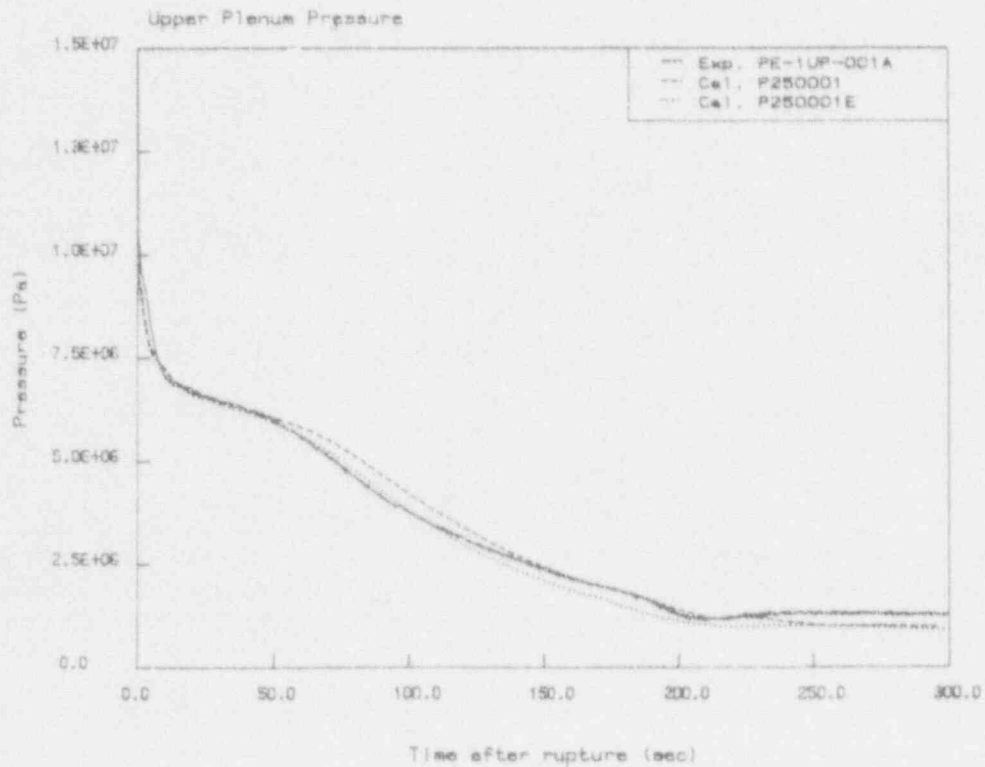


Figure 32. The effect of primary system inventory on primary system pressure

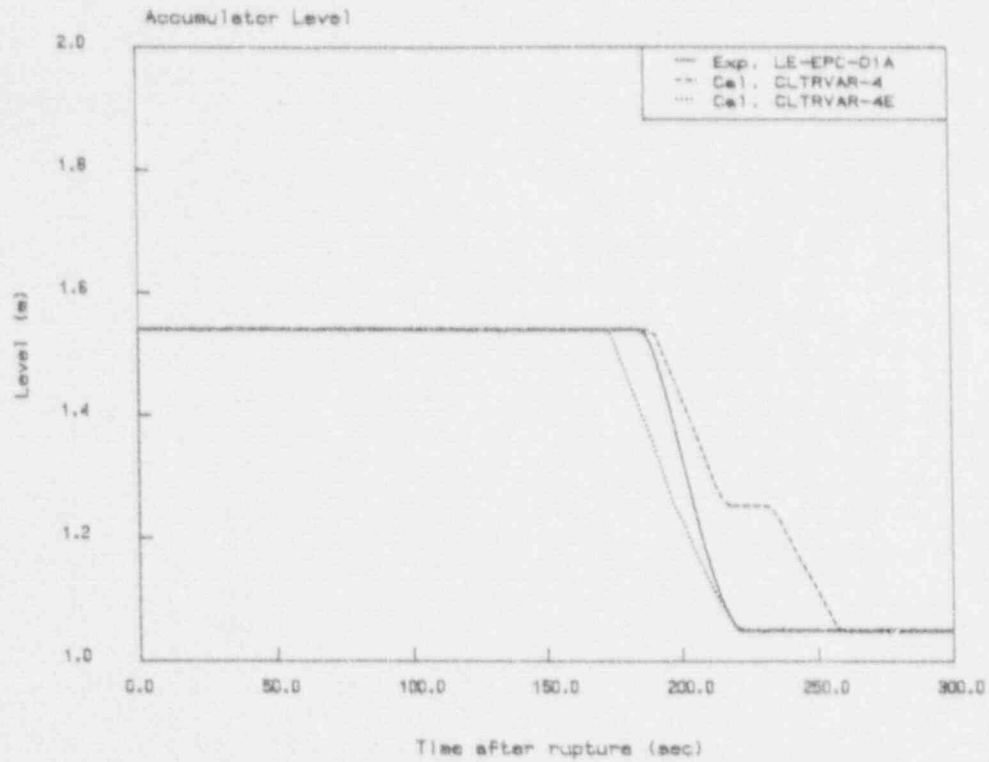


Figure 33. The effect of primary system inventory on accumulator liquid level

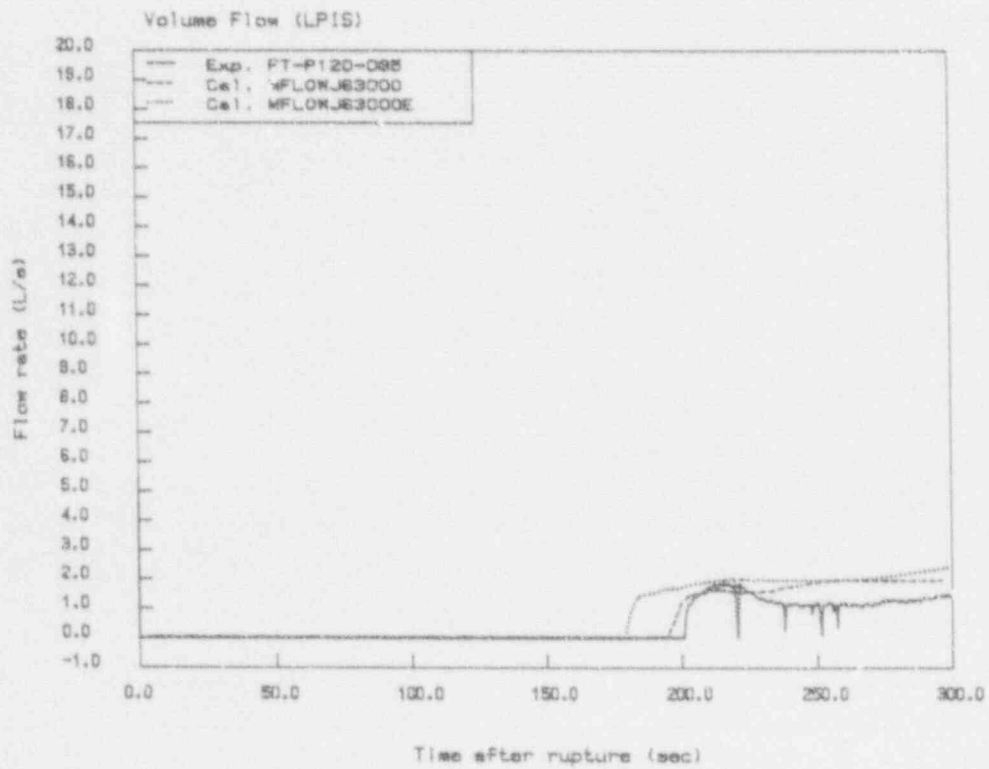


Figure 34. The effect of primary system inventory on LPSI flowrates

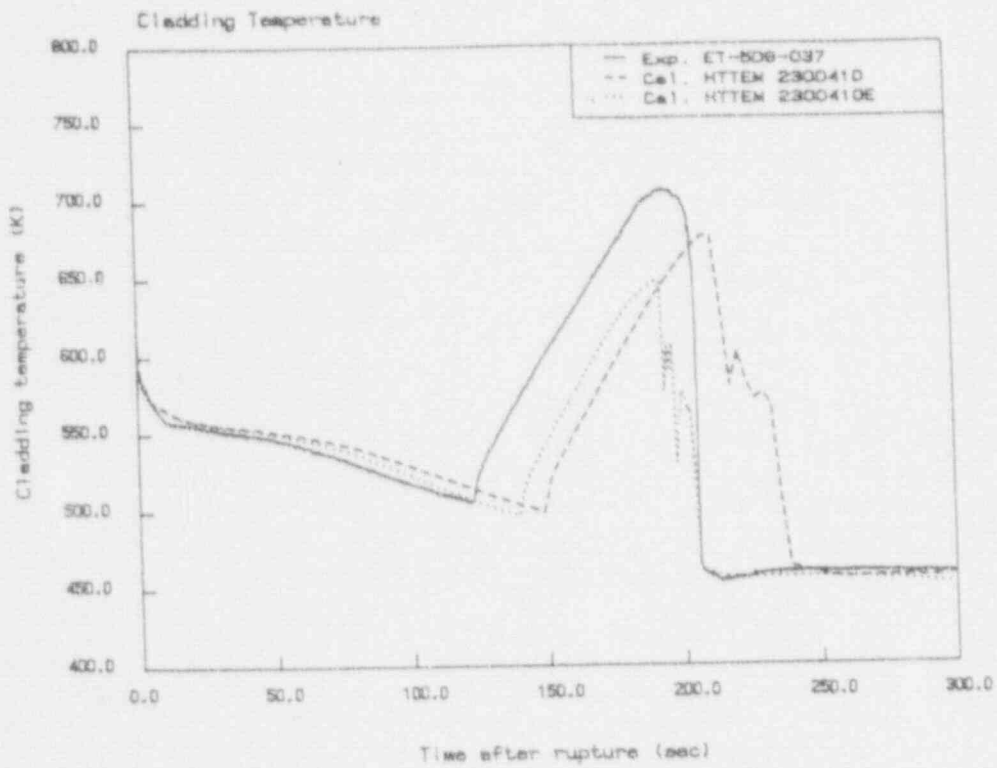


Figure 35. The effect of primary system inventory on PCT



Appendix: Input Listing













1151303	4.2988000	4.2988000	0.0	03			
1151304	4.2777000	4.2777000	0.0	04			
1151305	4.2587000	4.2587000	0.0	05			
1151306	4.2370000	4.2370000	0.0	06			
1151307	4.2166000	4.2166000	0.0	07			
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
* SG OUTLET PLENUM							
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
1160000	"SG OUT PLN"		BRANCH				
1160001	2	0					
1160101	0.0	0.629795	0.33532	0.0	-90.0	-0.512756	
1160102	4.E-5	0.0102	00				
1160200	0	14735800.	1228440.	2465581.	0.0		
1161101	115010000	116000000	0.0	0.0	0.0	0100	
1162101	116010000	118000000	0.0512	0.0	0.0	0100	
1161201	4.1997000	4.1997000	0.0				
1162201	7.7841000	7.7841000	0.0				
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
* PUMP SUCTION PIPING							
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
1180000	"PMP SUC PP"		PIPE				
1180001	3						
1180101	0.0	3					
1180201	0.0	2					
1180301	0.546638	1					
1180302	0.688596	2					
1180303	0.558577	3					
1180401	0.0445625	1					
1180402	0.0445137	2					
1180403	0.0354278	3					
1180501	0.0	3					
1180601	-90.0	3					
1180701	-0.498052	1					
1180702	-0.688596	2					
1180703	-0.355604	3					
1180801	4.E-5	0.0	3				
1180901	0.083	0.083	1				
1180902	0.104	0.104	2				
1181001	00	3					
1181101	0000	2					
1181201	0	14659900.	1228430.	2467190.	0.0	0.0	01
1181202	0	14646900.	1228430.	2467470.	0.0	0.0	02
1181203	0	14644400.	1228430.	2467520.	0.0	0.0	03
1181300	0						
1181301	9.8172000	9.8172000	0.0	01			
1181302	10.006000	10.006000	0.0	02			
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
* PUMP SUCTION TEE							
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----							
1200000	"PMP SCT T "		BRANCH				
1200001	3	0					
1200101	0.0	0.759614	0.0487901	0.0	0.0	0.0	
1200102	4.0E-5	0.0	00				
1200200	0	14641700.	1228420.	2467580.	0.0		
1201101	118010000	120000000	0.0	0.1	0.1	0000	
1202101	120010000	125000000	0.0317	0.4	0.4	0100	
1203101	120010000	155000000	0.0317	0.4	0.4	0100	
1201201	10.006000	10.006000	0.0				



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1202201 5.2047000 5.2047000 0.0
1203201 4.7736000 4.7736000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* PUMP1 SUCTION TEE OUTLET
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1250000 "PMP1 SCT T"      BRANCH
1250001 1          0
1250101 0.0        1.00308  0.0640548 0.0        90.0        0.520704
1250102 4.0E-5     0.0        00
1250200 0          14619800. 1228410.  2468040.  0.0
1251101 125010000 130000000 0.0        0.13       0.13       0000
1251201 8.5638000 8.5638000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* PUMP 1 INLET
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1300000 "PMP1 INLET"      SINGLVOL
1300101 0.0        0.457201  0.0177444 0.0        90.0        0.457201
1300102 4.0E-5     0.0        00
1300200 0          14594400. 1228410.  2468590.  0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* PRIMARY COOLANT PUMP 1
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1350000 "PCPUMP1 "      PUMP
1350101 0.0        0.4572    0.0991    0.0        90.0        0.317900
1350102 0
1350108 130010000 0.0        0.017     0.017     0000
1350109 140000000 0.0        0.05      0.05      0000
1350200 0          14870800. 1228670.  2462730.  0.0
1350201 0          8.5640000 8.5640000 0.0
1350202 0          9.0771000 9.0771000 0.0
1350301 0 0 0      -1      -1      695      0
1350302 369.00000 .91178862 .31550000 96.000000 500.60000 1.4310000
1350303 613.6     0.0        207.433   0.0444   19.5987   0.0
1350308 78.53982 0.0        -22.86511 27.16043 5.74589
1350310 0.0       0.0        0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* PUMP 1 OUTLET PUMP SIDE
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1400000 "PMP1 OUT P"      SINGLVOL
1400101 0.0        0.502185  0.0183849 0.0        0.0        0.0
1400102 4.0E-5     0.0        00
1400200 0          15090400. 1228670.  2457720.  0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* PUMP1 OUTLET PIPE TEE SIDE
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1450000 "PMP1 OUT T"      BRANCH
1450001 2          0
1450101 0.0        1.4084    0.0633    0.0        0.0        0.0
1450102 4.0E-5     0.0        00
1450200 0          15099600. 1228660.  2457500.  0.0
1451101 140010000 145000000 0.0        0.0        0.0        0000
1452101 145010000 150000000 0.0        0.1        0.1        0100
1451201 9.0747000 9.0747000 0.0
1452201 7.3917000 7.3917000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* PUMP OUTLET TEE
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
1500000 "PMP OUT T "      BRANCH

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1500001	2	0					
1500101	0.0636463	0.3542995	0.0	0.0	0.0	0.0	
1500102	4.0E-5	0.0	00				
1500200	0	15079600.	1228680.	2457980.	0.0		
1501101	170010000	150000000	0.0183	0.1	0.1	0100	
1502101	150010000	172000000	0.0	0.0	0.0	0000	
1501201	8.0488000	8.0488000	0.0				
1502201	9.9847000	9.9847000	0.0				
*-----	1	1	1	1	1	1	1
* PUMP 2 SUCTION TEE OUTLET							
*-----	1	1	1	1	1	1	1
1550000	"PMP2 SCT T"		BRANCH				
1550001	1	0					
1550101	0.0	1.00308	0.0640548	0.0	90.0	0.520704	
1550102	4.0E-5	0.0	00				
1550200	0	14629600.	1228410.	2467830.	0.0		
1551101	155010000	160000000	0.0	0.13	0.13	0000	
1551201	7.7885000	7.7885000	0.0				
*-----	1	1	1	1	1	1	1
* PUMP 2 INLET PIPE							
*-----	1	1	1	1	1	1	1
1600000	"PMP2 INLET"		SINGLVOL				
1600101	0.0	0.457201	0.0177444	0.0	90.0	0.457201	
1600102	4.0E-5	0.0	00				
1600200	0	14608000.	1228410.	2468300.	0.0		
*-----	1	1	1	1	1	1	1
* PRIMARY COOLANT PUMP 2							
*-----	1	1	1	1	1	1	1
1650000	"PCPUMP2 "		PUMP				
1650101	0.0	0.514	0.0991	0.0	90.0	0.317900	
1650102	0						
1650108	163010000	0.0	0.017	0.017	0000		
1650109	170000000	0.0	0.1	0.1	0000		
1650200	0	14928600.	1228710.	2461510.	0.0		
1650201	0	7.7887000	7.7887000	0.0			
1650202	0	8.0515000	8.0515000	0.0			
1650301	135 135	135	-1	-1	697	0	
1650302	369.00000	.93018970	.31550000	96.000000	500.60000	1.4310000	
1650303	613.6	0.0	207.433	0.0444	19.5987	0.0	
1650308	78.53982	0.0	-22.86511	27.16403	5.74589		
1650310	0.0	0.0	0.0				
*-----	1	1	1	1	1	1	1
* PUMP 2 OUTLET							
*-----	1	1	1	1	1	1	1
1700000	"PMP2 OUT T"		BRANCH				
1700001	0	0					
1700101	0.0	0.514071	0.0192958	0.0	0.0	0.0	
1700102	4.0E-5	0.0	00				
1700200	0	15203100.	1228710.	2454990.	0.0		
*-----	1	1	1	1	1	1	1
* PRESSURIZER SPRAY TEE							
*-----	1	1	1	1	1	1	1
1720000	"PZR SPR T "		BRANCH				
1720001	1	0					
1720101	0.0635359	0.2844229	0.0	0.0	0.0	0.0	
1720102	4.0E-5	0.0	00				
1720200	0	15078900.	1228680.	2458000.	0.0		
1721101	172010000	175000000	0.0	0.0	0.0	0000	



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2001201 1.59691-7 1.59691-7 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* INLET ANNULUS
*-----1-----1-----1-----1-----1-----1-----1-----1-----
2020000 "IN AN " BRANCH
2020001 2 0
2020101 0.2617061 0.2851822 0.0 0.0 -90.0 -0.2851822
2020102 3.81-6 0.175 00
2020200 0 15031700. 1228660. 2459150. 0.0
2021101 202010000 205000000 0.0 0.0 0.0 0000
2022101 202000000 252000000 0.0 4.5+4 4.5+4 0003
2021201 2.2804 2.2804 0.0
2022201 6.12444-2 6.12444-2 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* INLET ANNULUS BOTTOM VOLUME
*-----1-----1-----1-----1-----1-----1-----1-----1-----
2050000 "IN AN BOT " BRANCH
2050001 1 0
2050101 0.2296374 0.2525361 0.0 0.0 -90.0 -0.2525361
2050102 3.81-6 0.172 00
2050200 0 15031700. 1228660. 2459150. 0.0
2051101 205010000 210000000 0.0 0.0 0.0 0000
2051201 3.5613000 3.5613000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* DOWNCOMER
*-----1-----1-----1-----1-----1-----1-----1-----1-----
2100000 "DOWNCOMER " ANNULUS
2100001 6
2100101 0.0 6
2100201 0.0 5
2100301 1.0267313 1
2100302 0.4933248 2
2100303 0.7028265 3
2100304 0.5588068 4
2100305 0.6522799 5
2100306 0.4269792 5
2100401 0.1509710 1
2100402 0.0706690 2
2100403 0.1060015 3
2100404 0.0795138 4
2100405 0.0998947 5
2100406 0.06252 6
2100501 0.0 6
2100601 -90.0 6
2100801 3.81-6 0.102 6
2100901 0.0 0.0 5
2101001 00 6
210110? 0000 5
2101201 0 15033300. 1228660. 2459110. 0.0 0.0 01
2101202 0 15038200. 1228660. 2458990. 0.0 0.0 02
2101203 0 15042800. 1228660. 2458880. 0.0 0.0 03
2101204 0 15046500. 1228660. 2458790. 0.0 0.0 04
2101205 0 15051300. 1228660. 2458670. 0.0 0.0 05
2101206 0 15054600. 1228660. 2458590. 0.0 0.0 06
2101300 0
2101301 3.6556000 3.6556000 0.0 01
2101302 3.6555000 3.6555000 0.0 02
2101303 3.6801000 3.6801000 0.0 03

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2101304 3.6801000 3.6801000 0.0 04
2101305 3.5763000 3.5763000 0.0 05
*-----1-----1-----1-----1-----1-----1-----1-----
* LOWER PLENUM TOP VOLUME
*-----1-----1-----1-----1-----1-----1-----1-----
2150000 "LWR PL TOP" BEANCH
2150001 3 0
2150101 0.0 0.3533183 0.24520 0.0 -90.0 -0.3533183
2150102 3.81-6 0.0 00
2150200 0 15052500. 1228660. 2458640. 0.0
2151101 210010000 215000000 0.0 2.00 2.00 0000
2152101 215010000 220000000 0.0 0.005 0.005 0000
2153101 215000000 225000000 0.1499 1.5 1.5 0000
2151201 3.5762000 3.5762000 0.0
2152201 -.1243900 -.1243900 0.0
2153201 4.0692000 4.0692000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* LOWER PLENUM BOTTOM VOLUME
*-----1-----1-----1-----1-----1-----1-----1-----
2200000 "LWR PL BOT" SNGLVOL
2200101 0.0 0.3741720 0.29656 0.0 -90.0 -0.3741720
2200102 4.0E-5 0.0 00
2200200 0 15055200. 1227510. 2458580. 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* JUNCTION FROM COLD LEG TO FILLER GAP
*-----1-----1-----1-----1-----1-----1-----1-----
2220000 "CL-FLLRGAP" SNGLJUN
2220101 185010000 223000000 0.0 15.000 15.000 0100
2220201 0 1.3659000 1.3659000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* REACTOR VESSEL FILLER GAP
*-----1-----1-----1-----1-----1-----1-----1-----
2230000 "FILLER GAP" ANNULUS
2230001 4
2230101 0.0 4
2230201 0.0 3
2230301 1.4218585 1
2230302 1.1961513 2
2230303 1.2110867 3
2230304 0.7802975 4
2230401 0.0899085 1
2230402 0.0722790 2
2230403 0.0334096 3
2230404 0.0309800 4
2230501 0.0 4
2230601 -90.0 4
2230801 3.81-6 0.0 4
2230901 0.0 0.0 3
2231001 00 4
2231101 0000 3
2231201 0 15105600. 1228360. 2457350. 0.0 0.0 01
2231202 0 15115300. 1228100. 2457120. 0.0 0.0 02
2231203 0 15121100. 1227850. 2456970. 0.0 0.0 03
2231204 0 15130300. 1227690. 2456750. 0.0 0.0 04
2231300 0
2231301 1.4291000 1.4291000 0.0 01
2231302 1.3129900 1.3129900 0.0 02
2231303 3.1295000 3.1295000 0.0 03

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*-----1-----1-----1-----1-----1-----1-----1-----1-----
* JUNCTION FROM FILLER GAP TO LOWER PLENUM
*-----1-----1-----1-----1-----1-----1-----1-----1-----
2240000 "FLLRGAP-LP"          SNGLJUN
2240101 223010000 220000000 0.0      15.      15.      0000
2240101 223010000 220000000 0.0      45.      45.      0000
2240201 0          2.1743000 2.1743000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* LOWER CORE SUPPORT STRUCTURE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
2250000 "L CORE SUP"          BRANCH
2250001 2          0
2250101 0.0      0.6561928 0.12094 0.0      90.0      0.6561928
2250102 3.81-6    0.095      00
2250200 0          15038300. 1228490. 2458990. 0.0
2251101 225010000 230000000 0.1134 1.5      1.5      0100
2252101 225010000 235000000 0.0      12.      12.      0100
2251201 3.2020000 3.2020000 0.0
2252201 1.6570000 1.6570000 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* ACTIVE CORE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
2300000 "CORE"          "          PIPE
2300001 6
2300101 0.0      6
2300201 0.1705   1
2300202 0.144    2
2300203 0.1705   3
2300204 0.144    4
2300205 0.1705   5
2300301 0.3728765 1 * 89/11/09 EQUAL LENGTH MODEL
2300302 0.2221000 5
2300303 0.4234231 6
2300401 0.0683340 1
2300402 0.0478582 2
2300403 0.0483329 3
2300404 0.0479138 4
2300405 0.0479052 5
2300406 0.0750459 6
2300501 0.0      6
2300601 90.0     6
2300801 1.27-7   0.012    6
2300901 0.0      0.0      1
2300902 0.66     0.66     2
2300903 0.0      0.0      3
2300904 0.66     0.66     4
2300905 0.0      0.0      5
2301001 00       6
2301101 0000     5
2301201 0          15017600. 1243280. 2459490. 0.0 0.0 01
2301202 0          15012600. 1267710. 2459620. 0.0 0.0 02
2301203 0          15004500. 1294130. 2459810. 0.0 0.0 03
2301204 0          15000500. 1317510. 2459910. 0.0 0.0 04
2301205 0          14992300. 1332930. 2460100. 0.0 0.0 05
2301206 0          14987800. 1337240. 2460200. 0.0 0.0 06
2301300 0
2301301 3.4659000 3.4659000 0.0      01
2301302 4.1523000 4.1523000 0.0      02

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2301303	3.5540000	3.5540000	J.0	03
2301304	4.2594000	4.2594000	0.0	04
2301305	3.6273000	3.6273000	0.0	05

\* CORE BYPASS VOLUME

2350000	"CORE BYPASS"	PIPE					
2350001	3						
2350101	0.0	3					
2350201	0.0	2					
2350301	0.5755754	1					
2350302	0.4824023	2					
2350303	0.6264219	3					
2350401	0.0091280	1					
2350402	0.0072325	2					
2350403	0.0088095	3					
2350501	0.0	3					
2350601	90.0	3					
2350801	3.81-6	0.003	3				
2350901	0.0	0.0	2				
2351001	00	3					
2351101	0000	2					
2351201	0	15001900.	1228490.	2459460.	0.0	0.0	01
2351202	0	15007600.	1228490.	2459740.	0.0	0.0	02
2351203	0	14994900.	1228500.	2460040.	0.0	0.0	03
2351300	0						
2351301	1.7916000	1.7916000	0.0	01			
2351302	1.8500000	1.8500000	0.0	02			

\* UPPER END BOXES AND SUPPORT STRUCTURE

2400000	"UPR END BX"	BRANCH					
2400001	2	0					
2400101	0.0	0.4933248	0.1195494	0.0	90.0	0.4933248	
2400102	3.81-6	0.145	00				
2400200	0	14969100.	1333110.	2460620.	0.0		
2401101	230010000	240000000	0.1118	1.5	1.5	0100	
2402101	235010000	240000000	0.0	12.	12.	0100	
2401201	3.4977000	3.4977000	0.0				
2402201	1.8501000	1.8501000	0.0				

\* UPPER CORE SUPPORT STRUCTURE - CROSS FLOW REGION

2450000	"UPR CR SUP"	BRANCH					
2450001	2	0					
2450101	0.0	0.4933248	0.1280806	0.0	90.0	0.4933248	
2450102	3.81-6	0.145	00				
2450200	0	15420100.	1407960.	2449770.	0.0		
2451101	240010000	245000000	0.0	0.0	0.0	0000	
2452101	245010000	251000000	0.0	0.0	0.0	0100	
2451201	2.1756000	2.1756000	0.0				
2452201	-.24832-4	-.24832-4	0.0				

\* UPPER FLOW SKIRT REGION

2500000	"U FLW SKRT"	BRANCH					
2500001	1	0					
2500101	0.1547532	0.7850547	0.0	0.0	90.0	0.7850547	

2500102	3.81-6	0.131	00				
2500200	0	14955900.	1333110.	2460920.	0.0		
2501101	245010000	250000000	0.0	0.0	0.0		0100
2501201	4.1549000	4.1549000	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* DEAD END OF FUEL MODULES							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
2510000	"DE FL MODS"		SNGLVOL				
2510101	0.0	0.7844123	0.1154214	0.0	90.0		0.7844123
2510102	3.81-6	0.214	00				
2510200	0	14963500.	1329710.	2460750.	0.0		
-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* UPPER HEAD							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
2520000	"UPR HEAD "		BRANCH				
2520001	1	0					
2520101	0.2622585	0.2869580	0.0	0.0	90.0		0.2869580
2520102	3.81-6	0.0	00				
2520200	0	14957200.	1329000.	2460890.	0.0		
2521101	250010000	252000000	0.0	0.006	0.006		0000
2521201	4.1549000	4.1549000	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* UPPER PLENUM BOTTOM VOLUME							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
2550000	"UPR PL BOT"		BRANCH				
2550001	2	0					
2550101	0.2622585	0.6312304	0.0	0.0	90.0		0.6312304
2550102	3.81-6	0.0	00				
2550200	0	14954800.	1328590.	2460950.	0.0		
2551101	252010000	255000000	0.0	0.006	0.006		0000
2552101	255010000	260000000	0.0	0.03	0.03		0000
2551201	3.56869-6	3.56869-6	0.0				
2552201	4.52212-6	4.52212-6	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* UPPER PLENUM TOP VOLUME							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
2600000	"UPR PL TOP"		SNGLVOL				
2600101	0.0	0.7747094	0.1914909	0.0	90.0		0.7747094
2600102	3.81-6	0.0	00				
2600200	0	14949800.	1325010.	2461060.	0.0		
*-----							
* REACTOR VESSEL NOZZLE - BROKEN LOOP HOT LEG							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
3000000	"KVN BLHL "		BRANCH				
3000001	2	0					
3000101	0.0	0.876303	0.0575410	0.0	0.0		0.0
3000102	4.0E-5	0.0	00				
3000200	0	14957200.	1221360.	2460890.	0.0		
3001101	252010000	300000000	0.067014	0.0	0.0		0002
3002101	300010000	305000000	0.063426	0.1	0.1		0000
3001201	-.1240600	-.1240600	0.0				
3002201	-.1311000	-.1311000	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* HOT LEG PIPE TO REFLOOD ASSIST BYPASS TEE							



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*-----1-----1-----1-----1-----1-----1-----1-----
3050000 "HLP-RABS T"      BRANCH
3050001 1          0
3050101 0.0        0.698336 0.0442927 0.0      0.0      0.0
3050102 4.0E-5      0.0          00
3050200 0           14957200. 1221770. 2460890. 0.0
3051101 305010000 310000000 0.0      0.1      0.1      0100
3051201 -.1838800 -.1838800 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* BROKEN LOOP HOT LEG CONTRACTION
*-----1-----1-----1-----1-----1-----1-----1-----
3100000 "BLHL CONTR"      BRANCH
3100001 2          0
3100101 0.0        1.50013 0.0678467 0.0      0.0      0.0
3100102 4.0E-5      0.0          00
3100200 0           14957200. 1222120. 2460890. 0.0
3101101 380010000 310000000 0.0388 0.84 0.84 0100
3102101 310010000 315000000 0.0083647 0.0      0.0      0100
3101201 .21484000 .21484000 0.0
3102201 2.07725-3 2.07725-3 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* STEAM GENERATOR AND PUMP SIMULATOR
*-----1-----1-----1-----1-----1-----1-----1-----
3150000 "SG+PMP SIM"      PIPE
3150001 12
3150101 0.0          12
3150201 0.0083647 2
3150202 0.032603 4
3150203 0.105626 5
3150204 0.032603 7
3150205 0.0083647 9
3150206 0.008364 10
3150207 0.0046398 11
3150301 0.367768 1
3150302 0.552201 2
3150303 0.993978 4
3150304 0.849744 6
3150305 0.993978 8
3150306 1.371350 9
3150307 1.365029 10
3150308 1.674812 11
3150309 0.545209 12
3150401 3.0767-3 1
3150402 4.67621-3 2
3150403 8.60554-2 4
3150404 8.97552-2 6
3150405 8.60554-2 8
3150406 1.82303-2 9
3150407 5.46687-2 10
3150408 1.82489-2 11
3150409 2.83241-2 12
3150601 90.0        5
3150602 -90.0       10
3150603 90.0        11
3150604 0.0          12
3150701 0.127000 1
3150702 0.552201 2
3150703 0.993978 4

```



3350102	4.0E-5	0.0	00				
3350200	0	15031700.	1228270.	2459150.	0.0		
3351101	202000000	335000000	0.064130	1.0	1.0	0002	
3352101	335010000	340000000	0.063426	0.1	0.1	0000	
3351201	.13028000	.13028000	0.0				
3352201	.13170000	.13170000	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* COLD LEG PIPE TO REFLOOD ASSIST BYPASS TEE							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
3400000	"CLP-RABS T"		BRANCH				
3400001	1	0					
3400101	0.0	0.698336	0.0443927	0.0	0.0	0.0	
3400102	4.0E-5	0.0	00				
3400200	0	15031700.	1227890.	2459150.	0.0		
3401101	340010000	345000000	0.0	0.1	0.1	0100	
3401201	.18613000	.18613000	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* BROKEN LOOP COLD LEG CONTRACTION TO BREAK PLANE							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
3450000	"BLCL CONTR"		BRANCH				
3450001	2	0					
3450101	0.0	1.50013	0.0673163	0.0	0.0	0.0	
3450102	4.0E-5	0.0	00				
3450200	0	15424700.	1228050.	2449660.	0.0		
3451101	345000000	370000000	0.0388	0.84	0.84	0100	
3452101	345010000	350000000	0.0046367	0.0	0.0	0100	
3451201	.21516000	.21516000	0.0				
3452201	6.55835-5	6.55835-5	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* SPOOL PIECE AND PIPE TO ISOLATION VALVE							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
3500000	"BRK SP+PPE"		PIPE				
3500001	2						
3500101	0.0	2					
3500201	0.023520	1					
3500301	0.453394	1					
3500302	1.074803	2					
3500401	0.0106640	1					
3500402	0.0407801	2					
3500601	0.0	2					
3500801	4.0E-5	0.0	1				
3500802	4.0E-5	0.0	2				
3500901	0.0	0.0	1				
3501001	00	2					
3501101	0100	1					
3501201	0	15031700.	1218930.	2459150.	0.0	0.0	01
3501202	0	15031700.	1226360.	2459150.	0.0	0.0	02
3501300	0						
3501301	4.59331-5	4.59331-5	0.0	01			
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* COLD LEG ISOLATION VALVE							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
3550000	"CL ISO VLV"		VALVE				
3550101	350010000	360000000	0.0	0.0	0.0	0100	
3550201	0	-6.7943-7	-6.7943-7	0.0			
3550300	TRPVLV						
3550301	678						
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----

\* COLD LEG PIPE BETWEEN ISOLATION VALVE AND QOBV

ID	Description	Material	Length	Weight	Volume	Area	Other
3600000	"CL IS-QOBV"	SNGLVOL					
3600101	0.0	0.569219	0.0297722	0.0	0.0	0.0	
3600102	4.0E-5	0.0	00				
3600200	0	15031700.	1241690.	2459150.	0.0		

\* COLD LEG QUICK OPENING BLOWDOWN VALVE

ID	Description	Material	Length	Weight	Volume	Area	Other
3650000	"CL QOBV "	VALVE					
3650101	360010000	805000000	0.0466	0.0	0.0	0000	
3650201	0	.000000000	.000000000	0.0			
3650300	TRPVLV						
3650301	677						

\* REFLOOD ASSIST BYPASS PIPING - COLD LEG SIDE

ID	Description	Material	Length	Weight	Volume	Area	Other
3700000	"RABS C L "	PIPE					
3700001	3						
3700101	0.0388	2					
3700102	0.0776	3					
3700201	0.0388	2					
3700301	0.0	3					
3700401	0.0279	1					
3700402	0.070	2					
3700403	0.1165	3					
3700601	90.0	1					
3700602	0.0	3					
3700701	0.64	1					
3700702	0.0	3					
3700801	4.0-5	0.0	3				
3700901	0.28	0.28	1				
3700902	0.84	0.84	2				
3701001	00	3					
3701101	0000	2					
3701201	0	15029300.	1226830.	2459210.	0.0	0.0	01
3701202	0	15026900.	1226050.	2459270.	0.0	0.0	02
3701203	0	15026900.	1224760.	2459270.	0.0	0.0	03
3701300	0						
3701301	.21514000	.21514000	0.0	01			
3701302	.21508000	.21508000	0.0	02			

\* REFLOOD ASSIST BYPASS VALVES

ID	Description	Material	Length	Weight	Volume	Area	Other
3750000	"RABS VALVS"	SNGLJUN					
3750101	370010000	380000000	0.0	1.55+4	1.55+4	0000	
3750201	0	.10749000	.10749000	0.0			

\* REFLOOD ASSIST BYPASS PIPING - HOT LEG SIDE

ID	Description	Material	Length	Weight	Volume	Area	Other
3800000	"RABS H L "	PIPE					
3800001	3						
3800101	0.0776	1					
3800102	0.0388	3					
3800201	0.0388	2					
3800301	0.0	3					
3800401	0.0915	1					
3800402	0.048	2					







5080102	4.E-5	0.163697	00					
5080200	0	5228350.0	1094450.	2595690.	0.0			
5081101	508010000	510000000	0.0	0.0	0.0			0100
5081201	.58694	.58694	0.0					
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* STEAM GENERATOR DOWNCOMER								
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
5100000	"DWNCMR	"	ANNULUS					
5100001	3							
5100101	0.232	3						
5100201	0.0	2						
5100301	0.6096	3						
5100401	0.0	3						
5100601	-90.0	3						
5100701	-0.6096	3						
5100801	4.E-5	0.10793	3					
5100901	0.0	0.0	2					
5101001	00	3						
5101101	0000	2						
5101201	0	5233030.0	1094480.	2595670.	0.0			0.0 01
5101202	0	5237770.0	1095280.	2595640.	0.0			0.0 02
5101203	0	5242510.0	1095650.	2595610.	0.0			0.0 03
5101300	0							
5101301	.58704	.58704	0.0	01				
5101302	.58714	.58714	0.0	02				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* JUNCTION FROM DOWNCOMER TO BOILER								
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
5130000	"DNCMR-BLR "	"	SNGLJUN					
5130101	510010000	515000000	0.0	17.5	17.5			0100
5130201	0	.58722	.83849	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* STEAM GENERATOR BOILER								
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
5150000	"BOILER	"	PIPE					
5150001	5							
5150101	0.2776	4						
5150102	3.306294	5						
5150201	0.0	4						
5150301	1.8288	4						
5150302	1.2131	5						
5150401	0.0	5						
5150601	60.0	4						
5150602	90.0	5						
5150701	0.6096	4						
5150702	1.2131	5						
5150801	4.E-5	0.0234	4					
5150802	4.E-5	0.5962	5					
5150901	4.05	4.05	4					
5151001	00	5						
5151101	0100	4						
5151201	0	5241030.0	1154980.	2595580.	.49316			0.0 01
5151202	0	5237440.0	1161810.	2595610.	.71327			0.0 02
5151203	0	5233350.0	1162120.	2595650.	.80605			0.0 03
5151204	0	5232841.0	1161820.	2595680.	.85407			0.0 04
5151205	0	5237361.0	1161540.	2595700.	.87426			0.0 05
5151300	0							
5151301	.94859	1.3289	0.0	01				



5151302	1.5589	2.3557	0.0	02			
5151303	2.1266	3.3332	0.0	03			
5151304	2.6440	4.0529	0.0	94			
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* LOWER PORTION OF STEAM DOME							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
5200000	"LWR STM DM"		BRANCH				
5200001	1	0					
5200101	0.0	0.46956	0.705312	0.0	90.0	0.46956	
5200102	4.E-5	1.383	00				
5200200	0	5219990.0	1161320.	2595680.	1.0		
5201101	520010000	525000000	0.0	0.0	0.0	0100	
5201201	.50120	.64094	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* UPPER PORTION OF STEAM DOME							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
5250000	"UPR STM DM"		BRANCH				
5250001	1	0					
5250101	0.0	0.46956	0.705312	0.0	90.0	0.46956	
5250102	4.E-5	1.383	00				
5250200	0	5219870.0	1161310.	2595700.	1.0		
5251101	525010000	530000000	0.0	0.8	0.8	0100	
5251201	15.687	20.771	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* STEAM PIPE FROM GENERATOR TO CONTROL VALVE							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
5300000	"STEAM PIPE"		SNGLVOL				
5300101	0.04635	25.074	0.0	0.0	0.0	0.0	
5300102	4.E-5	0.0	00				
5300200	0	5203370.0	1160330.	2595740.	.99998		
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* STEAM FLOW CONTROL VALVE							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
5400000	"CV-P4-10 "		VALVE				
5400101	530010000	541000000	0.0047772	0.0	0.0	1100	
5400201	0	16.933	36.097	0.0			
5400300	MTRVLV						
5400301	685	686	0.05	0.645229	540		
20254000	NORMAREA						
20254001	0.0	9.25-4					
20254002	9.25-4	9.25-4					
20254003	1.0	1.0					
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* PIPE DOWNSTREAM OF STEAM CONTROL VALVE							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
5410000	"COND INLET"		BRANCH				
5410001	1	0					
5410101	0.06557	54.44	0.0	0.0	0.0	0.0	
5410102	4.E-5	0.0	00				
5410200	0	2009650.0	907346.	2597920.	.99820		
5411101	541010000	542000000	0.0	0.0	0.0	0100	
5411201	16.933	36.097	0.0				
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
* AIR COOLED CONDENSER							
*-----	1-----	1-----	1-----	1-----	1-----	1-----	1-----
5420000	"CONDENSER "		TMDPVOL				
5420101	0.21677	17.67	0.0	0.0	0.0	0.0	
5420102	4.E-5	0.02	00				

```

5420200 2
5420207 0.0 2.00E6 1.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* STEAM BYPASS VALVE
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
5450000 "STM BYPASS " VALVE
5450101 530010000 546000000 3.2-4 0.0 0.0 0100
5450201 0 .00000000 .00000000 0.0
5450300 TRPVLV
5450301 687
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* AIR COOLED CONDENSER
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
5460000 "CONDENSER " TMDPVOL
5460101 0.21677 17.67 0.0 0.0 0.0 0.0
5460102 4.E-5 0.02 00
5460200 1 516
5460201 0.0 554.8 0.999
5460202 18000. 332.5 0.999
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* FEED STORAGE TANK
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
5650000 "FEED TANK " TMDPVOL
5650101 29.81 3.048 0.0 0.0 0.0 0.0
5650102 4.E-5 0.0 00
5650200 1 689
5650201 -1.0 478.706 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* FEED WATER
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
5660000 "FEED " TMDPJUN
5660101 565000000 508000000 0.05
5660200 1 688
5660201 0.0 25.553 0.0 0.0
5660202 0.7 0.0 0.0 0.0
5660203 59.5 0.0 0.0 0.0
5660204 60.0 0.50364 0.0 0.0
5660205 1860.0 0.50364 0.0 0.0
5660206 1861.0 0.0 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* AUX FEED STORAGE TANK
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
5680000 "AUX FD TNK" TMDPVOL
5680101 29.81 3.048 0.0 0.0 0.0 0.0
5680102 4.E-5 0.0 00
5680200 1
5680201 0.0 305.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
* AUX FEED WATER
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----
5690000 "AUX FEED " TMDPJUN
5690101 568000000 508000000 0.05
5690200 1 690
5690201 -1.0 0.00 0.0 0.0
5690202 0.0 0.50364 0.0 0.0
* * * * *
*
* ECC SYSTEM

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*
*-----1-----1-----1-----1-----1-----1-----1-----
* ECC CHECK VALVE
*-----1-----1-----1-----1-----1-----1-----1-----
6000000 "ECC CHKVLV" VALVE
6000101 605010000 185000000 5.9896-3 0.935 0.935 1120
6000201 0 .00000000 .00000000 0.0
6000300 TRPVLV
6000301 681
*-----1-----1-----1-----1-----1-----1-----1-----
* ECCS HEADER TO PCS
*-----1-----1-----1-----1-----1-----1-----1-----
6050000 "ECCS HEADR" SINGLVOL
6050101 5.9896-3 5.0148 0.0 0.0 90.0 3.3071202
6050102 4.0-5 0.0 01
6050200 0 13595900. 172410. 2489140. 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* ACCUMULATOR VALVE
*-----1-----1-----1-----1-----1-----1-----1-----
6100000 "ACCUM VLV " VALVE
6100101 615010000 605000000 5.9896-3 6.278 6.278 1000
6100201 0 0.0 0.0 0.0
6100300 TRPVLV
6100301 682
*-----1-----1-----1-----1-----1-----1-----1-----
* ACCUMULATOR PIPE
*-----1-----1-----1-----1-----1-----1-----1-----
6150000 "ACC PIPE " SINGLVOL
6150101 0.0 25.997165 0.4074774 0.0 0.0 0.0
6150102 4.0-5 0.0 01
6150200 0 13580200. 112409. 2489450. 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* ACCUMULATOR VESSEL
*-----1-----1-----1-----1-----1-----1-----1-----
*6200000 "ACCUMULATR" ACCUM
*6200101 0.0 1.8103 2.3422 0.0 90.0 1.8103
*6200102 4.0-5 0.0 01
*6200200 4.31+6 306.6
*6200101 615000000 8.2132-3 13.3 13.3 0
*6200200 0.0 1.0662 2.4509 1.6927 0.04445 0 0 0 0
*-----1-----1-----1-----1-----1-----1-----1-----
* BWST LPIS
*-----1-----1-----1-----1-----1-----1-----1-----
6250000 "BWST LPIS " TMDPVOL
6250101 20.44 5.0 0.0 0.0 90.0 5.0
6250102 4.0E-5 0.0 00
6250200 3
6250201 0.0 1.0+5 300.0
*-----1-----1-----1-----1-----1-----1-----1-----
* LOW PRESSURE INJECTION SYSTEM
*-----1-----1-----1-----1-----1-----1-----1-----
6300000 "LPIS " TMDPJUN
6300101 625000000 605000000 5.9896-3
6300200 1 684 P 605010000
6300201 -1.0 0.0 0.0 0.0
6300202 0.0 0.0 0.0 0.0
6300203 8.483+4 7.045 0.0 0.0
6300204 4.297+5 6.091 0.0 0.0

```



12231201	5	4				
12231301	0.0	4				
12231401	551.0	5				
12231501	223010000	0	1	1	1.4218585	1
12231502	223020000	0	1	1	0.7621415	2
12231601	-939	0	3949	1	1.4218585	1
12231602	-939	0	3949	1	0.7621415	2
12231701	0	0.0	0.0	0.0	2	
12231801	0	0.0127	0.1922	1.4218585	1	
12231802	0	0.0127	0.1922	0.7621415	2	
*-----1-----1-----1-----1-----1-----1-----1-----						

\* REACTOR VESSEL WALL BELOW STATION 178 - 3.62 INCHES THICK  
 \* STATION 57.7 TO 178

12232000	4	5	2	1	0.7328	
12232100	0	1				
12232101	4					
12232201	5					
12232301	0.0	4				
12232401	553.0	5				
12232501	223020000	0	1	1	0.4340098	1
12232502	223030000	0	1	1	1.2110867	2
12232503	223040000	0	1	1	0.7802975	3
12232504	220010000	0	1	1	0.3741720	4
12232601	-939	0	3949	1	0.4340098	1
12232602	-939	0	3949	1	1.2110867	2
12232603	-939	0	3949	1	0.7802975	3
12232604	-939	0	3949	1	0.3741720	4
12232701	0	0.0	0.0	0.0	4	
12232801	0	0.0127	0.1922	0.4340098	1	
12232802	0	0.0127	0.1922	1.2110867	2	
12232803	0	0.0127	0.1922	0.7802975	3	
12232804	0	0.0127	0.1922	0.3741720	4	
*-----1-----1-----1-----1-----1-----1-----1-----						

\* REACTOR VESSEL BOTTOM  
 \* STATION 67.7

12200000	1	5	1	1	0.0	
12200100	0	1				
12200101	4	0.092				
12200201	5	4				
12200301	0.0	4				
12200401	551.0	5				
12200501	220010000	0	1	0	1.68	1
12200601	-939	0	3949	0	1.68	1
12200701	0	0.0	0.0	0.0	1	
12200801	0	0.0	0.0	5.00	1	
*-----1-----1-----1-----1-----1-----1-----1-----						

\* REACTOR VESSEL FILLER BLOCKS HEAT STRUCTURES

\* INLET ANNULUS TOP VOLUME  
 \* STATION 264 TO 277

12000000	2	5	2	1	0.508	
12000100	0	1				
12000101	4	0.7264				
12000201		4				
12000301	0.0	4				



12100904	0	0.0127	0.0253	0.5588068	4
12100905	0	0.0127	0.0253	0.6522799	5
12100906	0	0.0127	0.0253	0.4269792	6
12100907	0	0.0127	0.0253	0.3533183	7

\* CORE SUPPORT BARKEL  
 \* STATION 96.44 TO 277

12001000	9	5	2	1	0.381
12001100	0	1			
12001101	4	0.419			
12001201	4	4			
12001301	0.0	4			
12001401	556.0	5			
12001501	0	0	0	1	0.1876129 1
12001502	0	0	0	1	0.2851823 2
12001503	0	0	0	1	0.2525361 3
12001504	0	0	0	1	1.0267313 4
12001505	0	0	0	1	0.4933248 5
12001506	0	0	0	1	0.7028265 6
12001507	0	0	0	1	0.5588068 7
12001508	0	0	0	1	0.6522799 8
12001509	0	0	0	1	0.4269792 9
12001601	200010000	0	1	1	0.1876129 1
12001602	202010000	0	1	1	0.2851823 2
12001603	205010000	0	1	1	0.2525361 3
12001604	210010000	0	1	1	1.0267313 4
12001605	210020000	0	1	1	0.4933248 5
12001606	210030000	0	1	1	0.7028265 6
12001607	210040000	0	1	1	0.5588068 7
12001608	210050000	0	1	1	0.6522799 8
12001609	210060000	0	1	1	0.4269792 9
12001701	0	0.0	0.0	0.0	9
12001901	0	0.1016	0.2155	0.1876129	1
12001902	0	0.1016	0.2155	0.2851823	2
12001903	0	0.1016	0.2155	0.2525361	3
12001904	0	0.1016	0.2155	1.0267313	4
12001905	0	0.1016	0.2155	0.4933248	5
12001906	0	0.1016	0.2155	0.7028265	6
12001907	0	0.1016	0.2155	0.5588068	7
12001908	0	0.1016	0.2155	0.6522799	8
12001909	0	0.1016	0.2155	0.4269792	9

\* FLOW SKIRT - CORE FILLER ASSEMBLY  
 \* STATION 96.44 TO 261.13

12250000	10	5	2	1	0.3
12250100	0	1			
12250101	4	0.38			
12250201	4	4			
12250301	0.0	4			
12250401	575.0	5			
12250501	225010000	0	1	1	0.4269792 1
12250502	230010000	0	1	1	0.372835 2
12250503	230020000	10000	1	1	0.2794034 6
12250504	230060000	0	1	1	0.4234231 7
12250505	240010000	5000000	1	1	0.4933248 9
12250506	250010000	0	1	1	0.7850547 10

12250601	0	0	0	1	0.4269792	1
12250602	0	0	0	1	0.3728765	2
12250603	0	0	0	1	0.2794034	6
12250604	0	0	0	1	0.4234231	7
12250605	0	0	0	1	0.4933248	9
12250606	0	0	0	1	0.7850547	10
12250701	0	0.0	0.0	0.0		10
12250801	0	0.095	0.095	0.4269792	1	
12250802	0	0.0124	0.5713	0.3728765	2	
12250803	0	0.0124	0.5713	0.2794034	6	
12250804	0	0.0124	0.5713	0.4234231	7	
12250805	0	0.145	0.5713	0.4933248	9	
12250806	0	0.131	0.5713	0.7850547	10	

\*-----1-----1-----1-----1-----1-----1-----

\* LOWER CORE SUPPORT STRUCTURE

\* STATION 96.44 TO 116.91

\* INCLUDES CORE SUPPORT BARREL LIP , LOWER CORE SUPPORT

\* STRUCTURE , AND FUEL MODULE LOWER END BOXES

\*-----1-----1-----1-----1-----1-----1-----

12251000	1	5	2	1	0.282	
12251100	0	1				
12251101	4	0.3				
12251201	4	4				
12251301	0.0	4				
12251401	556.0	5				
12251501	225010000	0	1	1	0.4269792	1
12251601	0	0	0	1	0.4269792	1
12251701	0	0.0	0.0	0.0		1
12251801	0	0.095	0.095	0.4269792	1	

\*-----1-----1-----1-----1-----1-----1-----

\* ACTIVE CORE

\* STATION 116.91 TO 182.94

\*-----1-----1-----1-----1-----1-----1-----

12300000	6	10	2	1	0.0	
12300100	0	1				
12300101	5	4.647E-3				
12300102	1	4.742E-3				
12300103	3	5.359E-3				
12300201	1	5				
12300202	-2	6				
12300203	-3	9				
12300301	1.0	5				
12300302	0.0	9				
12300401	575.0	10				
12300501	0	0	0	1	57.000	6 * 1.68X204/6
12300601	230010000	10000	1	1	57.000	6 * 89/11/09
12300701	900	0.03695	0.0	0.0	1	* 100% POWER * 89/11/06
12300702	900	0.03979	0.0	0.0	2	* 100% POWER
12300703	900	0.04153	0.0	0.0	3	* 100% POWER
12300704	900	0.03521	0.0	0.0	4	* 100% POWER
12300705	900	0.02802	0.0	0.0	5	* 100% POWER
12300706	900	0.02161	0.0	0.0	6	* 100% POWER
12300901	0	0.01240	0.01504	1.775	6	

\*  
\* HEAT STRUCTURE MODEL FOR 1096 RODS IN PERIPHERAL

\*-----1-----1-----1-----1-----1-----1-----

\* ACTIVE CORE (PERIPHERAL 1096 RODS)

\* STATION 116.91 TO 182.94



```

*-----1-----1-----1-----1-----1-----1-----
12310000 6      10      2      1      0.0
12310100 0      1
12310101 5      4.647E-3
12310102 1      4.742E-3
12310103 3      5.359E-3
12310201 1      5
12310202 -2     6
12310203 -3     9
12310301 1.0    5
12310302 0.0    9
12310401 575.0  10
12310501 0      0      0      1      307.00  6 * 1.68X1096/6
12310601 230010000 10000 1      1      307.00  6 * 89/11/09
12310701 900    0.13896 0.0    0.0    1 * 100% POWER
12310702 900    0.15345 0.0    0.0    2 * 100% POWER
12310703 900    0.16486 0.0    0.0    3 * 100% POWER
12310704 900    0.13947 0.0    0.0    4 * 100% POWER
12310705 900    0.11431 0.0    0.0    5 * 100% POWER
12310706 900    0.08461 0.0    0.0    6 * 100% POWER
12310901 0      0.01240 0.01504 1.775 6

```

```

*-----1-----1-----1-----1-----1-----1-----

```

\* UPPER CORE SUPPORT STRUCTURE

\* STATION 190.5 TO 234.5

```

*-----1-----1-----1-----1-----1-----1-----
12400000 2      5      2      1      0.282
12400100 0      1
12400101 4      0.31
12400201 4      4
12400301 0.0    4
12400401 575.0  5
12400501 240010000 5000000 1      1      0.4933248 2
12400601 0      0      0      1      0.4933248 2
12400701 0      0.0    0.0    0.0    2
12400801 0      0.56   0.0    9.9866496 2

```

```

*-----1-----1-----1-----1-----1-----1-----

```

\* FUEL MODULES

\* STATION 187.6 TO 258.4

```

*-----1-----1-----1-----1-----1-----1-----
12510000 1      5      1      1      0.0
12510100 0      1
12510101 4      0.01
12510201 4      4
12510301 0.0    4
12510401 575.0  5
12510501 250010000 0      1      1      1.8      1
12510601 251010000 0      1      1      1.8      1
12510701 0      0.0    0.0    1.8    1
12510801 0      0.0    0.0    1.8    1
12510901 0      0.0    0.0    1.8    1

```

```

*-----1-----1-----1-----1-----1-----1-----

```

\* UPPER PLENUM INTERNALS

```

*-----1-----1-----1-----1-----1-----1-----
12551000 3      5      1      1      0.0
12551100 0      1
12551101 4      0.005
12551201 4      4
12551301 0.0    4

```



10060000	6	8	2	1	0.0051054	
10060100	0	1				
10060101	7	0.006348984				
10060201	6	7				
10060301	0.0	7				
10060401	551.0	8				
10060501	115010000	10000	1	1	1124.71	3
10060502	115040000	10000	1	1	849.063	5
10060503	115060000	10000	1	1	1124.71	8
10060601	515010000	10000	1	1	1124.71	3
10060602	515040000	0	1	1	849.063	4
10060603	515040000	0	1	1	849.063	5
10060604	515030000	-10000	1	1	1124.71	8
10060701	0	0	0	0	8	
10060801	0	0	0	0	8	
10060901	0	0	0	0	8	

\* SHROUD - UPPER SECTION

15000000	2	4	2	1	0.3048	
15000100	0	1				
15000101	3	0.3143				
15000201	5	3				
15000301	0.0	3				
15000401	539.0	4				
15000501	500010000	0	1	0	0.85127	1
15000502	515050000	0	1	0	2.51199	2
15000601	503010000	0	1	0	0.87780	1
15000602	505010000	0	1	0	2.59028	2
15000701	0	0.0	0.0	0.0	2	
15000801	0	0.0	0.0	0.0	2	
15000901	0	0.0	0.0	0.0	2	

\* SHROUD - LOWER SECTION

15100000	4	4	2	1	0.6445	
15100100	0	1				
15100101	3	0.6572				
15100201	5	3				
15100301	0.0	3				
15100401	533.0	4				
15100501	515040000	0	1	1	0.646354	1
15100502	515030000	-10000	1	0	2.46858	4
15100601	508010000	0	1	1	0.646354	1
15100602	510010000	10000	1	0	2.51723	4
15100701	0	0.0	0.0	0.0	4	
15100801	0	0.0	0.0	0.0	4	
15100901	0	0.0	0.0	0.0	4	

\* VESSEL WALL

15250000	8	5	2	1	0.7112	
15250100	0	1				
15250101	4	0.76397				
15250201	5	4				
15250301	0.0	4				
15250401	540.0	5				



11001801	0	0	0	1.58878	1
11001802	0	0	0	1.0531192	2
11001803	0	0	0	0.2810215	3
11001804	0	0	0	0.9207292	4
11001805	0	0	0	1.38893	5
11001806	0	0	0	0.688596	6
11001807	0	0	0	0.558577	7
11001808	0	0	0	0.759614	8
11001809	0	0	0	0.3542995	9
11001810	0	0	0	0.2844229	10
11001811	0	0	0	0.4163655	11
11001812	0	0	0	0.613244	12
11001813	0	0	0	1.15189	13
11001814	0	0	0	1.00965	14
*-----1-----1-----1-----1-----1-----1-----1-----					
* STEAM GENERATOR CONNECTIONS					
*-----1-----1-----1-----1-----1-----1-----1-----					
11002000	2	5	2	1	0.1625
11002100	0	1			
11002101	4	0.203			
11002201	4	4			
11002301	0.0	4			
11002401	560.0	5			
11002501	112020000	0	1	1	0.707687 1
11002502	118010000	0	1	1	0.546638 2
11002601	-939	0	3949	1	0.707687 1
11002602	-939	0	3949	1	0.546638 2
11002701	0	0	0	0	2
11002801	0	0	0	0.707687	1
11002802	0	0	0	0.546638	2
*-----1-----1-----1-----1-----1-----1-----1-----					
* .216 METER DIAMETER PIPING					
*-----1-----1-----1-----1-----1-----1-----1-----					
11003000	7	5	2	1	0.108
11003100	0	1			
11003101	4	0.1365			
11003201	4	4			
11003301	0.0	4			
11003401	560.0	5			
11003501	125010000	0	1	1	1.00308 1
11003502	130010000	0	1	1	0.457201 2
11003503	140010000	0	1	1	0.502185 3
11003504	145010000	0	1	1	1.40843 4
11003505	155010000	0	1	1	1.00308 5
11003506	160010000	0	1	1	0.457201 6
11003507	170010000	0	1	1	0.514071 7
11003601	-939	0	3949	1	1.00308 1
11003602	-939	0	3949	1	0.457201 2
11003603	-939	0	3949	1	0.502185 3
11003604	-939	0	3949	1	1.40843 4
11003605	-939	0	3949	1	1.00308 5
11003606	-939	0	3949	1	0.457201 6
11003607	-939	0	3949	1	0.514071 7
11003701	0	0	0	0	7
11003801	0	0	0	1.00308	1
11003802	0	0	0	0.457201	2
11003803	0	0	0	0.502185	3
11003804	0	0	0	1.40843	4

11003805	0	0	0	1.00308	5
11003806	0	0	0	0.457201	5
11003807	0	0	0	0.514071	7
*-----1-----1-----1-----1-----1-----1-----1-----					

\* STEAM GENERATOR PLENA

-----1-----1-----1-----1-----1-----1-----1-----					
11004000	2	5	3	1	0.6858
11004100	0	1			
11004101	4	0.7747			
11004201	5	4			
11004301	0.0	4			
11004401	560.0	5			
11004501	114010000	0	1	1	0.25 1
11004502	116010000	0	1	1	0.25 2
11004601	-939	0	3949	1	0.25 1
11004602	-939	0	3949	1	0.25 2
11004701	0	0	0	0	2
11004801	0	0	0	0.630	1
11004802	0	0	0	0.630	2
11004501	0	0	0	0.630	2
*-----1-----1-----1-----1-----1-----1-----1-----					

\* BROKEN LOOP HOT LEG PIPING

\*-----1-----1-----1-----1-----1-----1-----1-----

\* NOZZLE PIPING

-----1-----1-----1-----1-----1-----1-----1-----					
13000000	3	5	2	1	0.1420
13000100	0	1			
13000101	4	0.1780			
13000201	4	4			
13000301	0.0	4			
13000401	560.0	5			
13000501	300010000	0	1	1	0.876303 1
13000502	305010000	0	1	1	0.698336 2
13000503	310010000	0	1	1	0.974349 3
13000601	-939	0	3949	1	0.876303 1
13000602	-939	0	3949	1	0.698336 2
13000603	-939	0	3949	1	0.974349 3
13000701	0	0	0	0	3
13000801	0	0	0	0.876303	1
13000802	0	0	0	0.698336	2
13000803	0	0	0	0.974349	3
*-----1-----1-----1-----1-----1-----1-----1-----					

\* INLET TO STM GEN SIMULATOR

-----1-----1-----1-----1-----1-----1-----1-----					
13151000	3	5	2	1	0.0515
13151100	0	1			
13151101	4	0.0705			
13151201	4	4			
13151301	0.0	4			
13151401	545.0	5			
13151501	310010000	0	1	1	0.525781 1
13151502	315010000	0	1	1	0.367768 2
13151503	315020000	0	1	1	0.552201 3
13151601	-939	0	3949	1	0.525781 1
13151602	-939	0	3949	1	0.367768 2
13151603	-939	0	3949	1	0.552201 3
13151701	0	0	0	0	3
13151801	0	0	0	0.525781	1

13151802	0	0	0	0.36768	2
13151803	0	0	0	0.552201	3
*-----1-----1-----1-----1-----1-----1-----1-----					
* STEAM GENERATOR SIMULATOR					
*-----1-----1-----1-----1-----1-----1-----1-----					
13152000	6	5	2	1	0.1835
13152100	0	1			
13152101	4	0.2785			
13152201	4	4			
13152301	0.0	4			
13152401	545.0	5			
13152501	315030000	10000	1	1	0.993978 2
13152502	315050000	10000	1	1	0.849744 4
13152503	315070000	10000	1	1	0.993978 6
13152601	-939	0	3949	1	0.993978 2
13152602	-939	0	3949	1	0.849744 4
13152603	-939	0	3949	1	0.993978 6
13152701	0	0	0	0	6
13152801	0	0	0	0.993978	2
13152802	0	0	0	0.849744	4
13152803	0	0	0	0.993978	6
*-----1-----1-----1-----1-----1-----1-----1-----					
* STM GEN SIMULATOR OUTLET					
*-----1-----1-----1-----1-----1-----1-----1-----					
13153000	1	5	2	1	0.0550
13153100	0	1			
13153101	4	0.0705			
13153201	4	4			
13153301	0.0	4			
13153401	545.0	5			
13153501	315090000	0	1	1	1.371350 1
13153601	-939	0	3949	1	1.371350 1
13153701	0	0	0	0	1
13153801	0	0	0	1.371350	1
*-----1-----1-----1-----1-----1-----1-----1-----					
* PUMP SIMULATOR					
*-----1-----1-----1-----1-----1-----1-----1-----					
13154000	1	5	2	1	0.1420
13154100	0	1			
13154101	4	0.1780			
13154201	4	4			
13154301	0.0	4			
13154401	545.0	5			
13154501	315100000	0	1	1	1.365029 1
13154601	-939	0	3949	1	1.365029 1
13154701	0	0	0	0	1
13154801	0	0	0	1.365029	1
*-----1-----1-----1-----1-----1-----1-----1-----					
* PUMP SIMULATOR OUTLET					
*-----1-----1-----1-----1-----1-----1-----1-----					
13155000	1	5	2	1	0.0660
13155100	0	1			
13155101	4	0.0840			
13155201	4	4			
13155301	0.0	4			
13155401	545.0	5			
13155501	315110000	0	1	1	1.674812 1
13155601	-939	0	3949	1	1.674812 1

13155701	0	0	0	0	1	
13155801	0	0	0	1.674812	1	
*-----1-----1-----1-----1-----1-----1-----1-----						
* PIPING BETWEEN BREAK AND ISOLATION VALVE						
*-----1-----1-----1-----1-----1-----1-----1-----						
13156000	1	5	2	1	0.1285	
13156100	0	1				
13156101	4	0.1620				
13156201	4	4				
13156301	0.0	4				
13156401	545.0	5				
13156501	315120000	0	1	1	0.545209	1
13156601	-939	0	3949	1	0.545209	1
13156701	0	0	0	0	1	
13156801	0	0	0	0.545209	1	
*-----1-----1-----1-----1-----1-----1-----1-----						
* BROKEN LOOP COLD LEG PIPING						
*-----1-----1-----1-----1-----1-----1-----1-----						
* NOZZLE PIPING						
*-----1-----1-----1-----1-----1-----1-----1-----						
13350000	5	5	2	1	0.1420	
13350100	0	1				
13350101	4	0.1780				
13350201	4	4				
13350301	0.0	4				
13350401	550.0	5				
13350501	335010000	0	1	1	0.749305	1
13350502	340010000	0	1	1	0.698336	2
13350503	345010000	0	1	1	0.974349	3
13350601	-939	0	3949	1	0.749305	1
13350602	-939	0	3949	1	0.698336	2
13350603	-939	0	3949	1	0.974349	3
13350701	0	0	0	0	3	
13350801	0	0	0	0.749305	1	
13350802	0	0	0	0.598336	2	
13350803	0	0	0	0.974349	3	
*-----1-----1-----1-----1-----1-----1-----1-----						
* SMALL PIPING NEAR BREAK						
*-----1-----1-----1-----1-----1-----1-----1-----						
13501000	1	5	2	1	0.0550	
13501100	0	1				
13501101	4	0.1780				
13501201	4	4				
13501301	0.0	4				
13501401	545.0	5				
13501501	345010000	0	1	1	0.525781	1
13501601	-939	0	3949	1	0.525781	1
13501701	0	0	0	0	1	
13501801	0	0	0	0.525781	1	
*-----1-----1-----1-----1-----1-----1-----1-----						
* PIPING BETWEEN BREAK AND ISOLATION VALVE						
*-----1-----1-----1-----1-----1-----1-----1-----						
13502000	2	5	2	1	0.0865	
13502100	0	1				
13502101	4	0.1095				
13502201	4	4				
13502301	0.0	4				
13502401	545.0	5				







20100102	4.1667E2	6.46
20100103	5.3315E2	5.782385
20100104	6.99817E2	4.633177
20100105	8.66483E2	3.880307
20100106	1.03315E3	3.357625
20100107	1.08871E3	3.155129
20100108	1.19982E3	2.983787
20100109	1.28315E3	2.836674
20100110	1.36648E3	2.713792
20100111	1.53315E3	2.571680
20100112	1.61648E3	2.448990
20100113	1.69982E3	2.391875
20100114	1.97759E3	2.289762
20100115	2.25537E3	2.307069
20100116	2.53315E3	2.433413
20100117	2.81093E3	2.661870
20100118	3.08871E3	2.994171
*-----	1-----	1-----1-----1-----1-----1-----1-----
* UO2 - VOLUMETRIC HEAT CAPACITY		
*-----	1-----	1-----1-----1-----1-----1-----1-----
20100151	2.73150E2	2.310427E6
20100152	3.23150E2	2.571985E6
20100153	3.73150E2	2.746357E6
20100154	6.7315E2	3.138694E6
20100155	1.37315E3	3.443844E6
20100156	1.77315E3	3.531030E6
20100157	1.97315E3	3.792588E6
20100158	2.17315E3	4.228518E6
20100159	2.37315E3	4.882412E6
20100160	2.67315E3	6.015829E6
20100161	2.77315E3	6.320980E6
20100162	2.87315E3	6.582538E6
20100163	2.97315E3	6.713317E6
20100164	3.11315E3	6.800503E6
20100165	4.69982E3	6.800503E6
*-----	1-----	1-----1-----1-----1-----1-----1-----
* GAP - THERMAL CONDUCTIVITY		
*-----	1-----	1-----1-----1-----1-----1-----1-----
20100201	273.15	0.14
20100202	590.0	0.24
20100203	810.0	0.29
20100204	1090.0	0.36
20100205	1370.0	0.42
20100206	3260.0	0.75
*-----	1-----	1-----1-----1-----1-----1-----1-----
* GAP - VOLUMETRIC HEAT CAPACITY		
*-----	1-----	1-----1-----1-----1-----1-----1-----
20100251	273.15	5.4
20100252	3260.0	5.4
*-----	1-----	1-----1-----1-----1-----1-----1-----
* ZIRCALOY-4 - THERMAL CONDUCTIVITY		FROM MATPRO
*-----	1-----	1-----1-----1-----1-----1-----1-----
20100301	380.4	13.6
20100302	469.3	14.6
20100303	577.6	15.8
20100304	685.9	17.3
20100305	774.8	18.4
20100306	872.0	19.8

20100307	973.2	21.8
20100308	1073.2	23.2
20100309	1123.2	25.4
20100310	1152.3	24.2
20100311	1232.2	25.5
20100312	1331.2	26.6
20100313	1404.2	28.2
20100314	1576.2	33.0
20100315	1625.2	36.7
20100316	1755.2	41.2
20100317	2273.2	55.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* ZIRCALOY-4 - VOLUMETRIC HEAT CAPACITY		FROM MATPRO
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
20100351	300.0	1.841E6
20100352	400.0	1.978E6
20100353	640.0	2.168E6
20100354	1090.0	2.456E6
20100355	1093.0	3.288E6
20100356	1113.0	3.865E6
20100357	1133.0	4.028E6
20100358	1153.0	4.709E6
20100359	1173.0	5.345E6
20100360	1193.0	5.044E6
20100361	1213.0	4.054E6
20100362	1233.0	3.072E6
20100363	1243.0	2.332E6
20100364	1477.0	2.332E6
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* S-STEEL - THERMAL CONDUCTIVITY		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
20100401	273.15	12.98
20100402	1199.82	25.1
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* S-STEEL - VOLUMETRIC HEAT CAPACITY		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
20100451	273.15	3.83E6
20100452	366.5	3.83E6
20100453	477.59	4.190E6
20100454	588.59	4.336E6
20100455	699.82	4.504E6
20100456	810.93	4.639E6
20100457	922.04	4.773E6
20100458	1144.26	5.076E6
20100459	1366.5	5.376E6
20100460	1477.59	5.546E6
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* INCONEL-600 - THERMAL CONDUCTIVITY		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
20100601	366.5	13.85
20100602	477.6	15.92
20100603	588.7	18.17
20100604	700.0	20.42
20100605	810.9	22.50
20100606	922.0	24.92
20100607	1033.2	26.83
20100608	1144.3	29.42
20100609	1477.6	36.06

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*-----1-----1-----1-----1-----1-----1-----1-----
* INCONEL-600 - VOLUMETRIC HEAT CAPACITY
*-----1-----1-----1-----1-----1-----1-----1-----
20100651 366.5      3.908+6
20100652 477.6      4.084+6
20100653 588.7      4.260+6
20100654 700.0      4.436+6
20100656 810.9      4.665+6
20100657 922.0      4.929+6
20100658 1033.2     5.105+6
20100659 1477.6     5.727+6
*$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
*
*          CONTROL VARIABLES
*
*-----1-----1-----1-----1-----1-----1-----1-----
* 001-006 LEVEL CALCULATORS
*-----1-----1-----1-----1-----1-----1-----1-----
* 001 STEAM GENERATOR LEVEL
20500100 SGLVL      SUM      1.0      0.0      1
20500101 0.0      0.4445  VOIDF   503010000
20500102      1.2131  VOIDF   505010000
20500103      0.6096  VOIDF   508010000
20500104      0.6096  VOIDF   510010000
20500105      0.6096  VOIDF   510020000
20500106      0.6096  VOIDF   510030000
* 002 PRESSURIZER LEVEL
20500200 PZRLVL     SUM      1.0      0.0      1
20500201 0.0      0.1815  VOIDF   415010000
20500202      0.1524  VOIDF   415020000
20500203      0.3967  VOIDF   415030000
20500204      0.5289  VOIDF   415040000
20500205      0.3967  VOIDF   415050000
20500206      0.1943  VOIDF   415060000
20500207      0.1029  VOIDF   420010000
20500208      0.1029  VOIDF   420020000
* 004 ACCUMULATOR LEVEL
*20500400 ACCMLVL  INTEGRAL -6.3480-3 2.0447  0
*20500401 VELFJ    620010000
*-----1-----1-----1-----1-----1-----1-----1-----
* 061-072 PRIMARY SYSTEM MASS CALCULATOR
*-----1-----1-----1-----1-----1-----1-----1-----
* 061 INTACT LOOP HOT LEG MASS
20506100 ILHLMASS SUM      1.0      0.0      1
20506101 0.0      0.102752 RHO     100010000
20506102      7.57291-2 RHO     105010000
20506103      6.43178-2 RHO     110010000
20506104      7.96973-2 RHO     112010000
20506105      5.79614-2 RHO     112020000
* 062 STEAM GENERATOR PRIMARY MASS
20506200 SGPRIMASS SUM      1.0      0.0      1
20506201 0.0      0.335320 RHO     114010000
20506202      0.136356 RHO     115010000
20506203      9.21538-2 RHO     115020000
20506204      9.21538-2 RHO     115030000
20506205      6.99783-2 RHO     115040000
20506206      6.99783-2 RHO     115050000
20506207      9.21538-2 RHO     115060000

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20506208		9.21538-2	RHO	115070000	
20506209		0.136356	RHO	115080000	
20506210		0.335320	RHO	116010000	
* 063 PUMP SUCTION PIPING MASS					
20506300	PMPSUMASS	SUM	1.0	0.0	1
20506301	0.0	4.45625-2	RHO	118010000	
20506302		4.45137-2	RHO	118020000	
20506303		3.54278-2	RHO	118030000	
20506304		4.87901-2	RHO	120010000	
20506305		6.40548-2	RHO	125010000	
20506306		1.77444-2	RHO	130010000	
20506307		6.40548-2	RHO	155010000	
20506308		1.77444-2	RHO	160010000	
* 064 INTACT LGOP COLD LEG MASS					
20506400	ILCLMASS	SUM	1.0	0.0	1
20506401	0.0	9.91000-2	RHO	135010000	
20506402		1.83849-2	RHO	140010000	
20506403		6.33861-2	RHO	145010000	
20506404		3.16011-2	RHO	150010000	
20506405		9.91000-2	RHO	165010000	
20506406		1.92958-2	RHO	170010000	
20506407		3.54280-2	RHO	175010000	
20506408		3.88950-2	RHO	175020000	
20506409		7.30598-2	RHO	180010000	
20506410		6.44920-2	RHO	185010000	
* 065 DOWNCOMER/LOWER PLENUM MASS					
20506500	DCLPMASS	SUM	1.0	0.0	1
20506501	0.0	0.0864164	RHO	200010000	
20506502		0.0907360	RHO	205010000	
20506503		0.1509710	RHO	210010000	
20506504		0.0706690	RHO	210020000	
20506505		0.1060015	RHO	210030000	
20506506		0.0795138	RHO	210040000	
20506507		0.0998947	RHO	210050000	
20506508		0.06252	RHO	210060000	
20506509		0.24520	RHO	215010000	
20506510		0.29656	RHO	220010000	
* 066 REACTOR VESSEL FILLER GAP MASS					
20506600	FGAPMASS	SUM	1.0	0.0	1
20506601	0.0	0.0899085	RHO	223010000	
20506602		0.0722790	RHO	223020000	
20506603		0.0334096	RHO	223030000	
20506604		0.03098	RHO	223040000	
* 067 CORE/UPPER PLENUM MASS					
20506700	CRUPMASS	SUM	1.0	0.0	1
20506701	0.0	0.12094	RHO	225010000	
20506702		0.0683340	RHO	230010000	
20506703		0.0478587	RHO	230020000	
20506704		0.0483329	RHO	230030000	
20506705		0.0479138	RHO	230040000	
20506706		0.0479052	RHO	230050000	
20506707		0.0750459	RHO	230060000	
20506708		0.0091280	RHO	235010000	
20506709		0.0072325	RHO	235020000	
20506710		0.0088095	RHO	235030000	
20506711		0.1195494	RHO	240010000	
20506712		0.1280806	RHO	245010000	
20506713		0.1436936	RHO	250010000	

20506714		0.1154214	RHO	251010000	
20506715		0.2031741	RHO	255010000	
20506716		0.1914909	RHO	260010000	
* 068 BROKEN LOOP HOT LEG MASS					
20506800	BLHLMASS	SUM	1.0	0.0	1
20506801	0.0	5.75410-2	RHO	300010000	
20506802		4.42927-2	RHO	305010000	
20506803		6.78467-2	RHO	310010000	
20506804		3.07670-3	RHO	315010000	
20506805		4.67621-3	RHO	315020000	
20506806		8.60554-2	RHO	315030000	
20506807		8.60554-2	RHO	315040000	
20506808		8.97552-2	RHO	315050000	
20506809		8.97552-2	RHO	315060000	
20506810		8.60554-2	RHO	315070000	
20506811		8.60554-2	RHO	315080000	
20506812		1.82303-2	RHO	315090000	
20506813		5.46687-2	RHO	315100000	
20506814		1.82489-2	RHO	315110000	
20506815		2.83241-2	RHO	315120000	
20506816		9.15000-2	RHO	380010000	
20506817		4.80000-2	RHO	380020000	
20506818		4.89000-2	RHO	380030000	
* 069 BROKEN LOOP COLD LEG MASS					
20506900	BLCLMASS	SUM	1.0	0.0	1
20506901	0.0	4.79790-2	RHO	335010000	
20506902		4.43927-2	RHO	340010000	
20506903		6.73163-2	RHO	345010000	
20506904		1.06640-2	RHO	350010000	
20506905		4.07801-2	RHO	350020000	
20506906		2.97722-2	RHO	360010000	
20506907		2.79000-2	RHO	370010000	
20506908		7.00000-2	RHO	370020000	
20506909		1.16500-1	RHO	370030000	
* 070 PRESSURIZER MASS					
20507000	PZRMASS	SUM	1.0	0.0	1
20507001	0.0	3.33500-3	RHO	400010000	
20507002		3.33500-3	RHO	405010000	
20507003		3.33500-3	RHO	405020000	
20507004		6.84000-2	RHO	415010000	
20507005		8.38000-2	RHO	415020000	
20507006		2.24255-1	RHO	415030000	
20507007		2.98987-1	RHO	415040000	
20507008		2.24255-1	RHO	415050000	
20507009		7.32000-2	RHO	415060000	
20507010		1.42000-2	RHO	420010000	
20507011		1.42000-2	RHO	420020000	
20507012		2.12609-3	RHO	430010000	
* 071 REACTOR VESSEL TOTAL MASS					
20507100	RVMASS	SUM	1.0	0.0	1
20507101	0.0	1.0	CNTRLVAR	65	
20507102		1.0	CNTRLVAR	66	
20507103		1.0	CNTRLVAR	67	
* 072 PCS TOTAL MASS					
20507200	PCSMASS	SUM	1.0	0.0	1
20507201	0.0	1.0	CNTRLVAR	61	
20507202		1.0	CNTRLVAR	62	
20507203		1.0	CNTRLVAR	63	







1351205	7.443200E-01	2.583000E-01
1351206	7.734800E-01	3.778000E-01
1351207	8.631300E-01	6.326000E-01
1351208	1.000000E+00	1.000000E+00
*-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 3		
*-----1-----1-----1-----1-----1-----1-----		
1351300	1	3
1351301	-1.000000E+00	2.472200E+00
1351302	-8.057400E-01	2.047400E+00
1351303	-6.069000E-01	1.831000E+00
1351304	-4.068300E-01	1.624000E+00
1351305	-2.001710E-01	1.470500E+00
1351306	0.000000E+00	1.403600E+00
*-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 4		
*-----1-----1-----1-----1-----1-----1-----		
1351400	1	4
1351401	-1.000000E+00	2.472200E+00
1351402	-8.229700E-01	1.996800E+00
1351403	-6.323200E-01	1.589700E+00
1351404	-4.553400E-01	1.327900E+00
1351405	-2.710900E-01	1.194900E+00
1351406	-1.771600E-01	1.060500E+00
1351407	-9.073000E-02	1.015600E+00
1351408	0.000000E+00	9.342790E-01
*-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 5		
*-----1-----1-----1-----1-----1-----1-----		
1351500	1	5
1351501	0.000000E+00	2.500000E-01
1351502	2.000000E-01	2.800000E-01
1351503	4.000000E-01	3.400000E-01
1351504	4.118000E-01	2.768000E-01
1351505	5.975300E-01	4.584000E-01
1351506	7.934670E-01	6.992000E-01
1351507	1.000000E+00	1.000000E+00
*-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 6		
*-----1-----1-----1-----1-----1-----1-----		
1351600	1	6
1351601	0.000000E+00	9.342790E-01
1351602	9.109900E-02	9.229000E-01
1351603	1.865090E-01	8.963000E-01
1351604	2.717620E-01	8.750000E-01
1351605	4.558720E-01	8.433000E-01
1351606	5.744060E-01	8.355000E-01
1351607	7.405760E-01	8.466000E-01
1351608	7.666190E-01	8.469000E-01
1351609	8.714710E-01	8.838000E-01
1351610	1.000000E+00	1.000000E+00
*-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 7		
*-----1-----1-----1-----1-----1-----1-----		
1351700	1	7
1351701	-1.000000E+00	-1.000000E+00
1351702	-8.000000E-01	-6.300000E-01
1351703	-6.000000E-01	-3.000000E-01

1351704	-4.000000E-01	-5.000000E-02
1351705	-2.000000E-01	1.500000E-01
1351706	0.000000E+00	2.500000E-01
*-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 8		
*-----1-----1-----1-----1-----1-----1-----1-----		
1351800	1	8
1351801	-1.000000E+00	-1.000000E+00
1351802	-8.000000E-01	-9.700000E-01
1351803	-6.000000E-01	-9.500000E-01
1351804	-4.000000E-01	-8.800000E-01
1351805	-2.000000E-01	-8.000000E-01
1351806	0.000000E+00	-6.700000E-01
*-----1-----1-----1-----1-----1-----1-----1-----		
* SINGLE PHASE TORQUE DATA		
*-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 1		
*-----1-----1-----1-----1-----1-----1-----1-----		
1351900	2	1
1351901	0.000000E+00	6.032000E-01
1351902	1.930000E-01	6.325000E-01
1351903	3.930000E-01	7.369000E-01
1351904	5.955200E-01	8.331000E-01
1351905	7.978200E-01	9.229000E-01
1351906	1.000000E+00	1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 2		
*-----1-----1-----1-----1-----1-----1-----1-----		
1352000	2	2
1352001	0.000000E+00	-6.700000E-01
1352002	4.000000E-01	-2.500000E-01
1352003	5.000000E-01	1.500000E-01
1352004	7.372550E-01	5.265860E-01
1352005	7.680490E-01	6.065940E-01
1352006	8.672300E-01	7.436600E-01
1352007	1.000000E+00	1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 3		
*-----1-----1-----1-----1-----1-----1-----1-----		
1352100	2	3
1352101	-1.000000E+00	1.984300E+00
1352102	-8.009600E-01	1.394000E+00
1352103	-6.063800E-01	1.097500E+00
1352104	-4.068600E-01	8.220000E-01
1352105	-1.992800E-01	6.648000E-01
1352106	0.000000E+00	6.032000E-01
*-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 4		
*-----1-----1-----1-----1-----1-----1-----1-----		
1352200	2	4
1352201	-1.000000E+00	1.984300E+00
1352202	-8.223400E-01	1.830800E+00
1352203	-6.337100E-01	1.682400E+00
1352204	-4.585300E-01	1.557000E+00
1352205	-2.670230E-01	1.436200E+00
1352206	-1.761070E-01	1.387900E+00
1352207	-8.931000E-02	1.348100E+00
1352208	0.000000E+00	1.233610E+00

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*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 5
*-----1-----1-----1-----1-----1-----1-----1-----
1352300 2 5
1352301 0.000000E+00 -4.500000E-01
1352302 4.000000E-01 -2.500000E-01
1352303 5.000000E-01 0.000000E+00
1352304 1.000000E+00 3.569000E-01
*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 6
*-----1-----1-----1-----1-----1-----1-----1-----
1352400 2 6
1352401 0.000000E+00 1.233610E+00
1352402 9.064300E-02 1.196500E+00
1352403 1.885690E-01 1.109600E+00
1352404 2.734700E-01 1.041600E+00
1352405 4.586690E-01 8.958000E-01
1352406 5.744800E-01 7.807000E-01
1352407 7.381600E-01 6.134000E-01
1352408 7.685200E-01 5.849000E-01
1352409 8.700570E-01 4.877000E-01
1352410 1.000000E+00 3.569000E-01
*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 7
*-----1-----1-----1-----1-----1-----1-----1-----
1352500 2 7
1352501 -1.000000E+00 -1.000000E+00
1352502 -3.000000E-01 -9.000000E-01
1352503 -1.000000E-01 -5.000000E-01
1352504 0.000000E+00 -4.500000E-01
*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 8
*-----1-----1-----1-----1-----1-----1-----1-----
1352600 2 8
1352601 -1.000000E+00 -1.000000E+00
1352602 -2.500000E-01 -9.000000E-01
1352603 -8.000000E-02 -8.000000E-01
1352604 0.000000E+00 -6.700000E-01
*-----1-----1-----1-----1-----1-----1-----1-----
* TWO - PHASE MULTIPLIER DATA FROM L5-1 TEST DATA
*-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE
*-----1-----1-----1-----1-----1-----1-----1-----
1353000 0
1353001 0.000000E+00 0.000000E+00
1353002 1.000000E-01 0.000000E+00
1353003 2.000000E-01 1.000000E-01
1353004 3.000000E-01 2.000000E-01
1353005 3.500000E-01 3.000000E-01
1353006 4.000000E-01 6.000000E-01
1353007 5.000000E-01 6.000000E-01
1353008 6.000000E-01 6.000000E-01
1353009 7.000000E-01 6.000000E-01
1353010 8.000000E-01 5.000000E-01
1353011 9.000000E-01 3.000000E-01
1353012 1.000000E+00 0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE

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*-----1-----1-----1-----1-----1-----1-----1-----
1353100 0
1353101 0.000000E+00 0.000000E+00
1353102 1.000000E-01 0.000000E+00
1353103 2.000000E-01 1.000000E-01
1353104 3.000000E-01 3.000000E-01
1353105 3.500000E-01 5.000000E-01
1353106 4.000000E-01 7.500000E-01
1353107 5.000000E-01 7.500000E-01
1353108 6.000000E-01 7.500000E-01
1353109 7.000000E-01 7.500000E-01
1353110 8.000000E-01 7.500000E-01
1353111 9.000000E-01 5.000000E-01
1353112 1.000000E+00 0.000000E+00
*-----1-----1-----1-----1-----1-----1-----
* PUMP 2-PHASE DIFFERENCE DATA
*-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 1
*-----1-----1-----1-----1-----1-----1-----
1354100 1 1
1354101 0.000000E+00 1.000000E+00
1354102 1.000000E+00 1.000000E+00
*-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 2
*-----1-----1-----1-----1-----1-----1-----
1354200 1 2
1354201 0.000000E+00 1.000000E+00
1354202 1.000000E+00 1.000000E+00
*-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 3
*-----1-----1-----1-----1-----1-----1-----
1354300 1 3
1354301 -1.000000E+00 -1.160000E+00
1354302 -9.000000E-01 -1.240000E+00
1354303 -8.000000E-01 -1.770000E+00
1354304 -7.000000E-01 -2.360000E+00
1354305 -6.000000E-01 -2.790000E+00
1354306 -5.000000E-01 -2.910000E+00
1354307 -4.000000E-01 -2.670000E+00
1354308 -2.500000E-01 -1.690000E+00
1354309 -1.000000E-01 -5.000000E-01
1354310 0.000000E+00 0.000000E+00
*-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 4
*-----1-----1-----1-----1-----1-----1-----
1354400 1 4
1354401 -1.000000E+00 -1.160000E+00
1354402 -9.000000E-01 -7.800000E-01
1354403 -8.000000E-01 -5.000000E-01
1354404 -7.000000E-01 -3.100000E-01
1354405 -6.000000E-01 -1.700000E-01
1354406 -5.000000E-01 -8.000000E-02
1354407 -3.500000E-01 0.000000E+00
1354408 -2.000000E-01 5.000000E-02
1354409 -1.000000E-01 8.000000E-02
1354410 0.000000E+00 1.100000E-01
*-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 5

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*-----1-----1-----1-----1-----1-----1-----1-----
1354500  1 5
1354501  0.000000E+00 0.000000E+00
1354502  2.000000E-01 -3.400000E-01
1354503  4.000000E-01 -6.500000E-01
1354504  6.000000E-01 -9.300000E-01
1354505  8.000000E-01 -1.190000E+00
1354506  1.000000E+00 -1.470000E+00
*-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 6
*-----1-----1-----1-----1-----1-----1-----
1354600  1 6
1354601  0.000000E+00 1.100000E-01
1354602  1.000000E-01 1.300000E-01
1354603  2.500000E-01 1.500000E-01
1354604  4.000000E-01 1.300000E-01
1354605  5.000000E-01 7.000000E-02
1354606  6.000000E-01 -4.000000E-02
1354607  7.000000E-01 -2.300000E-01
1354608  8.000000E-01 -5.100000E-01
1354609  9.000000E-01 -9.100000E-01
1354610  1.000000E+00 -1.470000E+00
*-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 7
*-----1-----1-----1-----1-----1-----1-----
1354700  1 7
1354701 -1.000000E+00 0.000000E+00
1354702  0.000000E+00 0.000000E+00
*-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 8
*-----1-----1-----1-----1-----1-----1-----
1354800  1 8
1354801 -1.000000E+00 0.000000E+00
1354802  0.000000E+00 0.000000E+00
*-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 1
*-----1-----1-----1-----1-----1-----1-----
1354900  2 1
1354901  0.000000E+00 1.000000E+00
1354906  1.000000E+00 1.000000E+00
*-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 2
*-----1-----1-----1-----1-----1-----1-----
1355000  2 2
1355001  0.000000E+00 1.000000E+00
1355007  1.000000E+00 1.000000E+00
*-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 3
*-----1-----1-----1-----1-----1-----1-----
1355100  2 3
1355101 -1.000000E+00 1.984300E+00
1355102 -8.009600E-01 1.394000E+00
1355103 -6.063800E-01 1.097500E+00
1355104 -4.068600E-01 8.220000E-01
1355105 -1.992800E-01 6.648000E-01
1355106  0.000000E+00 6.032000E-01
*-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 4

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1652104	-4.068600E-01	8.220000E-01
1652105	-1.992800E-01	6.648000E-01
1652106	0.000000E+00	6.032000E-01
*-----	1-----1-----	1-----1-----1-----1-----
* TORQUE CURVE NO. 4		
*-----	1-----1-----	1-----1-----1-----1-----
1652200	2	4
1652201	-1.000000E+00	1.984300E+00
1652202	-8.223400E-01	1.830800E+00
1652203	-6.737100E-01	1.682400E+00
1652204	-4.585300E-01	1.557000E+00
1652205	-2.677300E-01	1.436200E+00
1652206	-1.761070E-01	1.387900E+00
1652207	-8.931000E-02	1.348100E+00
1652208	0.000000E+00	1.233610E+00
*-----	1-----1-----	1-----1-----1-----1-----
* TORQUE CURVE NO. 5		
*-----	1-----1-----	1-----1-----1-----1-----
1652300	2	5
1652301	0.000000E+00	-4.500000E-01
1652302	4.000000E-01	-2.500000E-01
1652303	5.000000E-01	0.000000E+00
1652304	1.000000E+00	3.569000E-01
*-----	1-----1-----	1-----1-----1-----1-----
* TORQUE CURVE NO. 6		
*-----	1-----1-----	1-----1-----1-----1-----
1652400	2	6
1652401	0.000000E+00	1.233610E+00
1652402	9.064300E-02	1.196500E+00
1652403	1.885690E-01	1.109600E+00
1652404	2.734700E-01	1.041600E+00
1652405	4.586690E-01	8.958000E-01
1652406	5.744800E-01	7.807000E-01
1652407	7.381600E-01	6.134000E-01
1652408	7.685200E-01	5.849000E-01
1652409	8.700570E-01	4.877000E-01
1652410	1.000000E+00	3.569000E-01
*-----	1-----1-----	1-----1-----1-----1-----
* TORQUE CURVE NO. 7		
*-----	1-----1-----	1-----1-----1-----1-----
1652500	2	7
1652501	-1.000000E+00	-1.000000E+00
1652502	0.000000E-01	-9.000000E-01
1652503	0.000000E-01	-5.000000E-01
1652504	0.000000E+00	-4.500000E-01
*-----	1-----1-----	1-----1-----1-----1-----
* TORQUE CURVE NO. 8		
*-----	1-----1-----	1-----1-----1-----1-----
1652600	2	8
1652601	-1.000000E+00	-1.000000E+00
1652602	-2.500000E-01	-9.000000E-01
1652603	-8.000000E-02	-8.000000E-01
1652604	0.000000E+00	-6.700000E-01
*-----	1-----1-----	1-----1-----1-----1-----
* TWO - PHASE MULTIPLIER DATA FROM L5-1 TEST DATA		
*-----	1-----1-----	1-----1-----1-----1-----
* HEAD CURVE		
*-----	1-----1-----	1-----1-----1-----1-----

1653000	0	
1653001	0.000000E+00	0.000000E+00
1653002	1.000000E-01	0.000000E+00
1653003	2.000000E-01	1.000000E-01
1653004	3.000000E-01	2.000000E-01
1653005	4.000000E-01	3.000000E-01
1653006	5.000000E-01	4.000000E-01
1653007	6.000000E-01	5.000000E-01
1653008	7.000000E-01	6.000000E-01
1653009	8.000000E-01	7.000000E-01
1653010	9.000000E-01	8.000000E-01
1653011	1.000000E+00	9.000000E-01
1653012	0.000000E+00	0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1653100	0	
1653101	0.000000E+00	0.000000E+00
1653102	1.000000E-01	0.000000E+00
1653103	2.000000E-01	1.000000E-01
1653104	3.000000E-01	2.000000E-01
1653105	3.500000E-01	3.000000E-01
1653106	4.000000E-01	4.000000E-01
1653107	5.000000E-01	5.000000E-01
1653108	6.000000E-01	6.000000E-01
1653109	7.000000E-01	7.000000E-01
1653110	8.000000E-01	8.000000E-01
1653111	9.000000E-01	9.000000E-01
1653112	1.000000E+00	0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* PUMP 2-PHASE DIFFERENCE DATA		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 1		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1654100	1	1
1654101	0.000000E+00	1.000000E+00
1654102	1.000000E+00	1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 2		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1654200	1	2
1654201	0.000000E+00	1.000000E+00
1654202	1.000000E+00	1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 3		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1654300	1	3
1654301	-1.000000E+00	-1.160000E+00
1654302	-9.000000E-01	-1.240000E+00
1654303	-8.000000E-01	-1.770000E+00
1654304	-7.000000E-01	-2.360000E+00
1654305	-6.000000E-01	-2.790000E+00
1654306	-5.000000E-01	-2.910000E+00
1654307	-4.000000E-01	-2.670000E+00
1654308	-2.500000E-01	-1.690000E+00
1654309	-1.000000E-01	-5.000000E-01
1654310	0.000000E+00	0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		

\* HEAD CURVE NO. 4

	1	4
1654400	1	4
1654401	-1.000000E+00	-1.160000E+00
1654402	-9.000000E-01	-7.800000E-01
1654403	-8.000000E-01	-5.000000E-01
1654404	-7.000000E-01	-3.100000E-01
1654405	-6.000000E-01	-1.700000E-01
1654406	-5.000000E-01	-8.000000E-02
1654407	-3.500000E-01	0.000000E+00
1654408	-2.000000E-01	5.000000E-02
1654409	-1.000000E-01	8.000000E-02
1654410	0.000000E+00	1.100000E-01

\* HEAD CURVE NO. 5

	1	5
1654500	1	5
1654501	0.000000E+00	0.000000E+00
1654502	2.000000E-01	-3.400000E-01
1654503	4.000000E-01	-6.500000E-01
1654504	6.000000E-01	-9.300000E-01
1654505	8.000000E-01	-1.190000E+00
1654506	1.000000E+00	-1.470000E+00

\* HEAD CURVE NO. 6

	1	6
1654600	1	6
1654601	0.000000E+00	1.100000E-01
1654602	1.000000E-01	1.300000E-01
1654603	2.500000E-01	1.500000E-01
1654604	4.000000E-01	1.300000E-01
1654605	5.000000E-01	7.000000E-02
1654606	6.000000E-01	-4.000000E-02
1654607	7.000000E-01	-2.300000E-01
1654608	8.000000E-01	-5.100000E-01
1654609	9.000000E-01	-9.100000E-01
1654610	1.000000E+00	-1.470000E+00

\* HEAD CURVE NO. 7

	1	7
1654700	1	7
1654701	-1.000000E+00	0.000000E+00
1654702	0.000000E+00	0.000000E+00

\* HEAD CURVE NO. 8

	1	8
1654800	1	8
1654801	-1.000000E+00	0.000000E+00
1654802	0.000000E+00	0.000000E+00

\* TORQUE CURVE NO. 1

	2	1
1654900	2	1
1654901	0.000000E+00	1.000000E+00
1654906	1.000000E+00	1.000000E+00

\* TORQUE CURVE NO. 2

	1	1
1654900	1	1

1655000	2	2
1655001	0.000000E+00	1.000000E+00
1655007	1.000000E+00	1.000000E+00
* TORQUE CURVE NO. 3		
1655100	2	3
1655101	-1.000000E+00	1.984300E+00
1655102	-8.009600E-01	1.394000E+00
1655103	-6.063800E-01	1.097500E+00
1655104	-4.068600E-01	8.220000E-01
1655105	-1.992800E-01	6.648000E-01
1655106	0.000000E+00	6.032000E-01
* TORQUE CURVE NO. 4		
1655200	2	4
1655201	-1.000000E+00	1.984300E+00
1655202	-8.223400E-01	1.830800E+00
1655203	-6.337100E-01	1.682400E+00
1655204	-4.585300E-01	1.557000E+00
1655205	-2.670230E-01	1.436200E+00
1655206	-1.761070E-01	1.387900E+00
1655207	-8.931000E-02	1.348100E+00
1655208	0.000000E+00	1.233610E+00
* TORQUE CURVE NO. 5		
1655300	2	5
1655301	0.000000E+00	-4.500000E-01
1655302	4.000000E-01	-2.500000E-01
1655303	5.000000E-01	0.000000E+00
1655304	1.000000E+00	3.569000E-01
* TORQUE CURVE NO. 6		
1655400	2	6
1655401	0.000000E+00	1.233610E+00
1655402	9.064300E-02	1.196500E+00
1655403	1.885690E-01	1.109600E+00
1655404	2.734700E-01	1.041600E+00
1655405	4.586690E-01	8.958000E-01
1655406	5.744800E-01	7.807000E-01
1655407	7.381600E-01	6.134000E-01
1655408	7.685200E-01	5.849000E-01
1655409	8.700570E-01	4.877000E-01
1655410	1.000000E+00	3.569000E-01
* TORQUE CURVE NO. 7		
1655500	2	7
1655501	-1.000000E+00	-1.000000E+00
1655502	-3.000000E-01	-9.000000E-01
1655503	-1.000000E-01	-5.000000E-01
1655504	0.000000E+00	-4.500000E-01
* TORQUE CURVE NO. 8		



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*-----1-----1-----1-----
* SPRAY VALVE POSITION CALCULATOR
*-----1-----1-----1-----
20590400  SPRAY    SUM    -1.0    0.0    1    * CONTIN
+         3        0.0    1.0
20590401  14.90+6  -1.0    P      420010000
* SP      XXXXXXX
* SP - TOP END OF PRESSURE CONTROL BAND ; SPRAY TURNS ON
*-----1-----1-----1-----
* POSITION VS AREA TABLE
*-----1-----1-----1-----
20299900  NORMAREA
20299901  0.0      0.0
20299902  0.0001   0.0
20299903  1.0      1.0
*-----1-----1-----1-----1-----1-----1-----1-----
* PRESSURIZER HEATERS IN INITIALIZATION
*-----1-----1-----1-----1-----1-----1-----1-----
* TRIP SETPOINTS
*-----1-----1-----1-----
* LT 693 CYLCING HEATERS          CARD 20241700
0000585  P      100010000 GT  NULL    0      14.85+6  N
* SP      XXXXXXX
* SP - BOTTOM END OF PRESSURE CONTROL BAND ; HEATERS TURN OFF
0000586  P      100010000 LT  NULL    0      14.8499+6  N
* SP      XXXXXXXXXX
* SP - (BOTTOM END . . .) - DELTA ; HEATERS TURN ON
0000666  586    OR      693    N
0000667  -585   AND     666    N
0000693  -503   AND     667    N
*-----1-----1-----1-----
* LT 694 BACKUP HEATERS          CARD 20241800
0000587  P      420010000 GT  NULL    0      14.85+6  N
* SP      XXXXXXX
* SP - BACKUP HEATERS TURN OFF
0000588  P      420010000 LT  NULL    0      14.84+6  N
* SP      XXXXXXX
* SP - BACKUP HEATERS TURN ON
0000668  588    OR      694    N
0000669  -587   AND     668    N
0000694  -503   AND     669    N
*-----1-----1-----1-----
* PRESSURIZER HEATERS
*-----1-----1-----1-----
14172000  2      9      2      1      0.0
14172100  0      1
14172101  8      8.3820E-3
14172201  4      8
14172301  1.0    8
14172401  615.   9
14172501  0      0      0      1      5.4864  1
14172502  0      0      0      1      1.8288  1
14172601  415040000 0      1      1      5.4864  1
14172602  415040000 0      1      1      1.8288  2
14172701  417    1.0    0.0    0.0    1      * CYCLING
14172702  418    1.0    0.0    0.0    2      * BACKUP
14172901  0      1.6764E-2 1.6764E-2 5.4864  1
14172902  0      1.6764E-2 1.6764E-2 1.8288  2

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*-----1-----1-----1-----
* PRESSURIZER CYCLING HEATERS
*-----1-----1-----1-----
20241700 POWER      693
20241701 -1.0      0.0
20241702 0.0       0.0
20241703 1.0       3.6+4
*-----1-----1-----1-----
* PRESSURIZER BACKUP HEATERS
*-----1-----1-----1-----
20241800 POWER      694
20241801 -1.0      0.0
20241802 0.0       0.0
20241803 1.0       3.6+4
*-----1-----1-----1-----1-----1-----1-----1-----
* PRESS. ZER LEVEL CONTROL USING CHARGING AND LETDOWN COMPONENTS
*-----1-----1-----1-----1-----1-----1-----1-----
* MODIFY PZR LEVEL CONTROL VARIABLE
*-----1-----1-----1-----
20500205                0.1249 VOIDF 415060000
20500207                0.02477 VOIDF 420010000
20500208                0.02447 VOIDF 420020000
*-----1-----1-----1-----
* CHARGING RESERVIOR
*-----1-----1-----1-----
9800000 "CHRG RESRV"      TMDPVOL
9800101 1.0          1.0          0.0          0.0          0.0          0.0
9800102 4.0-5        0.0          00
9800200 3
9800201 0.0          2.07+07 559.2
*-----1-----1-----1-----
* CHARGING VALVE
*-----1-----1-----1-----
9850000 "CHRG VALVE"      VALVE
9850101 98000000 185000000 3.8E-05 0.0          0.0          0100
9850201 0            .00000000 .00000000 0.0
9850300 SRVVLV
9850301 905          999
*-----1-----1-----1-----
* CHARGING VALVE POSITION CALCULATOR
*-----1-----1-----1-----
20590500 CHARGE      SUM      7.7          0.0          1          *CONTIN
+        3          0.0          1.0
20590501 1.09        -1.0        CNTRLVAR 2
* SP      XXXXX
* SP - BOTTOM END OF LEVEL CONTROL BAND ; CHARGING TURNS ON
*-----1-----1-----1-----
* LETDOWN SINK
*-----1-----1-----1-----
9900000 "LTDWN SINK"      TMDPVOL
9900101 1.0          1.0          0.0          0.0          0.0          0.0
9900102 4.0-5        0.0          00
9900200 3
9900201 0.0          1.4+7      559.2
*-----1-----1-----1-----
* LETDOWN VALVE
*-----1-----1-----1-----
9950000 "LTDWN VLV "      VALVE

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9950101 185000000 990000000 2.5-5 0.0 0.0 0100
9950201 0 .00000000 .00000000 0.0
9950300 SRVVLV
9950301 906 999
*-----1-----1-----1-----
* LETDOWN VALVE POSITION CALCULATOR
*-----1-----1-----1-----
20590600 LETDOWN SUM -7.7 0.0 1 *CONTIN
+ 3 0.0 1.0
20590601 1.11 -1.0 CNTRLVAR 2
* SP XXXXX
* SP - TOP END OF LEVEL CONTROL BAND ; LETDOWN TURNS ON
*-----1-----1-----1-----1-----1-----1-----1-----
* STEAM VALVE CONTROLLER
*-----1-----1-----1-----1-----1-----1-----1-----
* CHANGES TO STEAM VALVE
*-----1-----1-----1-----
5400201 0 16.946000 20.832000 0.0
5400300 SRVVLV
5400301 910 540
20254000 NORMAREA
20254001 0.0 0.0
20254002 0.0001 0.0
20254003 1.0 1.0
*-----1-----1-----1-----
* COMPUTE DELTA T ERROR
*-----1-----1-----1-----
20590700 "DELTA T" SUM 1.0 0.0 1
20590701 552.30 -1. IEMP 185010000
* SP XXXXXX
* SP - COLD LEG TEMPERATURE SETPOINT
*-----1-----1-----1-----
* FILTER DELTA T THRU DEADBAND
*-----1-----1-----1-----
20590800 DEADBAND FUNCTION 1.0 0.0 1
20590801 CNTRLVAR 907 908
20290800 REAC-T
20290801 -100. -100.
20290802 -0.25 -0.25
20290803 -0.25 0.0
20290804 0.25 0.0
20290805 0.25 0.25
20290806 100. 100.
*-----1-----1-----1-----
* INTEGRATE DELTA T ERROR
*-----1-----1-----1-----
20590900 "INT D T" INTEGRAL 1.0 0.0 1
20590901 CNTRLVAR 908
*-----1-----1-----1-----
* STEAM VALVE POSITION CALCULATOR
*-----1-----1-----1-----
20591000 TCONTROL SUM 1.0 0.645229 0 *CONTI
+ 3 0.6 0.90
* SP XXXXXXXX
* SP - STEAM VALVE INITIAL POSITION
20591001 0.645229 -0.07126 CNTRLVAR 908
* SP XXXXXXXX
* SP - STEAM VALVE INITIAL POSITION

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20591002          -0.01492 CNTRLVAR 909
*-----1-----1-----1-----1-----1-----1-----1-----
* SIMPLIFIED FEED SYSTEM CONTROLLER
*-----1-----1-----1-----1-----1-----1-----1-----
20591100 SGLVLERR SUM      1.0      0.0      1
20591101 3.20      -1.0      CNTRLVAR 001
* SP          XXXXXX
* SP - STEAM GENERATOR LEVEL SETPOINT
20591200 FEEDFLOW SUM      1.0      0.0      1
20591201 0.0      1.0      MFLOWJ 540000000
20591202          48.4      CNTRLVAR 911
*-----1-----1-----1-----1-----1-----1-----1-----
* REPLACE FEED JUNCTION TABLE
*-----1-----1-----1-----1-----1-----1-----1-----
5660200 1          0          CNTRLVAR 912
5660201 -100.0      25.553      0.0      0.0
* SP          XXXXXX
* SP - INITIAL FEED FLOW RATE
5660202 -1.0      0.0      0.0      0.0
5660203 0.0      0.0      0.0      0.0
5660204 50.0      50.0      0.0      0.0
5660205
5660206
5660207
5660208
5660209
*-----1-----1-----1-----1-----1-----1-----1-----
* CONSTANT REACTOR POWER TABLE
*-----1-----1-----1-----1-----1-----1-----1-----
20290000 POWER
20290001 0.0      45.9+6
20290002 100.      45.9+6
20290003 200.      45.9+6
20290004 1.E+3      45.9+6
20290005
20290006
20290007
20290008
20290009
20290010
20290011
20290012
20290013
20290014
20290015
20290016
20290017
20290018
20290019
20290020
*-----1-----1-----1-----1-----1-----1-----1-----
* REPLACE TRIPS FOR STEADY STATE
*-----1-----1-----1-----1-----1-----1-----1-----
* SCRAM
0000510 TIME      0          GE NULL      0          1.+9      L
* BREAK OPENS
0000511 TIME      0          GE NULL      0          1.+9      L
* HPIS ON

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*-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 1
*-----1-----1-----1-----1-----1-----1-----1-----
1351100  1          1
1351101  0.000000E+00  1.403600E+00
1351102  1.906100E-01  1.363600E+00
1351103  3.896300E-01  1.318600E+00
1351104  5.939600E-01  1.232800E+00
1351105  7.902000E-01  1.133600E+00
1351106  1.000000E+00  1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 2
*-----1-----1-----1-----1-----1-----1-----1-----
1351200  1          2
1351201  0.000000E+00  -5.700000E-01
1351202  2.000000E-01  -5.000000E-01
1351203  4.000000E-01  -2.500000E-01
1351204  5.755400E-01  0.000000E+00
1351205  7.443200E-01  2.583000E-01
1351206  7.734800E-01  3.778000E-01
1351207  8.631300E-01  6.326000E-01
1351208  1.000000E+00  1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 3
*-----1-----1-----1-----1-----1-----1-----1-----
1351300  1          3
1351301  -1.000000E+00  2.472200E+00
1351302  -8.057400E-01  2.047400E+00
1351303  -6.069000E-01  1.831000E+00
1351304  -4.068300E-01  1.624000E+00
1351305  -2.001710E-01  1.470500E+00
1351306  0.000000E+00  1.403600E+00
*-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 4
*-----1-----1-----1-----1-----1-----1-----1-----
1351400  1          4
1351401  -1.000000E+00  2.472200E+00
1351402  -8.229700E-01  1.996800E+00
1351403  -6.333000E-01  1.589700E+00
1351404  -4.553400E-01  1.327900E+00
1351405  -2.710900E-01  1.194900E+00
1351406  -1.771600E-01  1.060500E+00
1351407  -9.673000E-02  1.015600E+00
1351408  0.000000E+00  9.342790E-01
*-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 5
*-----1-----1-----1-----1-----1-----1-----1-----
1351500  1          5
1351501  0.000000E+00  2.500000E-01
1351502  2.000000E-01  2.800000E-01
1351503  4.000000E-01  3.400000E-01
1351504  4.118000E-01  2.768000E-01
1351505  5.976300E-01  4.584000E-01
1351506  7.934670E-01  6.992000E-01
1351507  1.000000E+00  1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 6
*-----1-----1-----1-----1-----1-----1-----1-----

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1352101	-1.000000E+00	7.984300E+00
1352102	-8.009600E-01	1.394000E+00
1352103	-6.063800E-01	1.097500E+00
1352104	-4.068600E-01	8.220000E-01
1352105	-1.992800E-01	6.648000E-01
1352106	0.000600E+00	6.032000E-01
*-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 4		
*-----1-----1-----1-----1-----1-----1-----1-----		
1352200	2	4
1352201	-1.000000E+00	1.984300E+00
1352202	-8.223400E-01	1.830800E+00
1352203	-6.337100E-01	1.682400E+00
1352204	-4.585300E-01	1.557000E+00
1352205	-2.670230E-01	1.436200E+00
1352206	-1.761070E-01	1.387900E+00
1352207	-8.931000E-02	1.348100E+00
1352208	0.000000E+00	1.233610E+00
*-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 5		
*-----1-----1-----1-----1-----1-----1-----1-----		
1352300	2	5
1352301	0.000000E+00	-4.500000E-01
1352302	4.000000E-01	-2.500000E-01
1352303	5.000000E-01	0.000000E+00
1352304	1.000000E+00	3.569000E-01
*-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 6		
*-----1-----1-----1-----1-----1-----1-----1-----		
1352400	2	6
1352401	0.000000E+00	1.233610E+00
1352402	9.064300E-02	1.196500E+00
1352403	1.885690E-01	1.109600E+00
1352404	2.734700E-01	1.041600E+00
1352405	4.586690E-01	8.958000E-01
1352406	5.744800E-01	7.807000E-01
1352407	7.381600E-01	6.134000E-01
1352408	7.685200E-01	5.849000E-01
1352409	8.700570E-01	4.877000E-01
1352410	1.000000E+00	3.569000E-01
*-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 7		
*-----1-----1-----1-----1-----1-----1-----1-----		
1352500	2	7
1352501	-1.000000E+00	-1.000000E+00
1352502	-3.000000E-01	-9.000000E-01
1352503	-1.000000E-01	-5.000000E-01
1352504	0.000000E+00	-4.500000E-01
*-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 8		
*-----1-----1-----1-----1-----1-----1-----1-----		
1352600	2	8
1352601	-1.000000E+00	-1.000000E+00
1352602	-2.500000E-01	-9.000000E-01
1352603	-8.000000E-02	-8.000000E-01
1352604	0.000000E+00	-6.700000E-01
*-----1-----1-----1-----1-----1-----1-----1-----		
* TW - PHASE MULTIPLIER DATA FROM L3-6 TEST DATA		

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*-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1353000  0
1353001  0.000000E+00      0.000000E+00
1353002  1.000000E-01      0.000000E+00
1353003  2.000000E-01      1.000000E-01
1353004  3.000000E-01      2.000000E-01
1353005  3.500000E-01      3.000000E-01
1353006  4.000000E-01      6.000000E-01
1353007  5.000000E-01      6.000000E-01
1353008  6.000000E-01      6.000000E-01
1353009  7.000000E-01      6.000000E-01
1353010  8.000000E-01      5.000000E-01
1353011  9.000000E-01      3.000000E-01
1353012  1.000000E+00      0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1353100  0
1353101  0.000000E+00      0.000000E+00
1353102  1.000000E-01      0.000000E+00
1353103  2.000000E-01      1.000000E-01
1353104  3.000000E-01      3.000000E-01
1353105  3.500000E-01      5.000000E-01
1353106  4.000000E-01      7.500000E-01
1353107  5.000000E-01      7.500000E-01
1353108  6.000000E-01      7.500000E-01
1353109  7.000000E-01      7.500000E-01
1353110  8.000000E-01      7.500000E-01
1353111  9.000000E-01      5.000000E-01
1353112  1.000000E+00      0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* PUMP 2-PHASE DIFFERENCE DATA
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 1
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1354100  1      1
1354101  0.000000E+00      1.000000E+00
1354102  1.000000E+00      1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 2
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1354200  1      2
1354201  0.000000E+00      1.000000E+00
1354202  1.000000E+00      1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* HEAD CURVE NO. 3
*-----1-----1-----1-----1-----1-----1-----1-----1-----
1354300  1      3
1354301  -1.000000E+00      -1.160000E+00
1354302  -9.000000E-01      -1.240000E+00
1354303  -8.000000E-01      -1.770000E+00
1354304  -7.000000E-01      -2.360000E+00
1354305  -6.000000E-01      -2.790000E+00
1354306  -5.000000E-01      -2.910000E+00
1354307  -4.000000E-01      -2.670000E+00
1354308  -2.500000E-01      -1.690000E+00

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1354309	-1.000000E-01	-5.000000E-01
1354310	0.000000E+00	0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 4		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1354400	1	4
1354401	-1.000000E+00	-1.160000E+00
1354402	-9.000000E-01	-7.800000E-01
1354403	-8.000000E-01	-5.000000E-01
1354404	-7.000000E-01	-3.100000E-01
1354405	-6.000000E-01	-1.700000E-01
1354406	-5.000000E-01	-8.000000E-02
1354407	-3.500000E-01	0.000000E+00
1354408	-2.000000E-01	5.000000E-02
1354409	-1.000000E-01	8.000000E-02
1354410	0.000000E+00	1.100000E-01
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 5		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1354500	1	5
1354501	0.000000E+00	0.000000E+00
1354502	2.000000E-01	-3.400000E-01
1354503	4.000000E-01	-6.500000E-01
1354504	6.000000E-01	-9.300000E-01
1354505	8.000000E-01	-1.190000E+00
1354506	1.000000E+00	-1.470000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 6		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1354600	1	6
1354601	0.000000E+00	1.100000E-01
1354602	1.000000E-01	1.300000E-01
1354603	2.500000E-01	1.500000E-01
1354604	4.000000E-01	1.300000E-01
1354605	5.000000E-01	7.000000E-02
1354606	6.000000E-01	-4.000000E-02
1354607	7.000000E-01	-2.300000E-01
1354608	8.000000E-01	-5.100000E-01
1354609	9.000000E-01	-9.100000E-01
1354610	1.000000E+00	-1.470000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 7		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1354700	1	7
1354701	-1.000000E+00	0.000000E+00
1354702	0.000000E+00	0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* HEAD CURVE NO. 8		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1354800	1	8
1354801	-1.000000E+00	0.000000E+00
1354802	0.000000E+00	0.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
* TORQUE CURVE NO. 1		
*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----		
1354900	2	1
1354901	0.000000E+00	1.000000E+00
1354906	1.000000E+00	1.000000E+00

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*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 2
*-----1-----1-----1-----1-----1-----1-----1-----
1355000  2                2
1355001  0.000000E+00      1.000000E+00
1355007  1.000000E+00      1.000000E+00
*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 3
*-----1-----1-----1-----1-----1-----1-----1-----
1355100  2                3
1355101  -1.000000E+00      1.984300E+00
1355102  -8.009600E-01     1.394000E+00
1355103  -6.063800E-01     1.097500E+00
1355104  -4.068600E-01     8.220000E-01
1355105  -1.992800E-01     6.648000E-01
1355106  0.000000E+00      6.032900E-01
*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 4
*-----1-----1-----1-----1-----1-----1-----1-----
1355200  2                4
1355201  -1.000000E+00      1.984300E+00
1355202  -8.223400E-01     1.830800E+00
1355203  -6.337100E-01     1.682400E+00
1355204  -4.585300E-01     1.557000E+00
1355205  -2.670230E-01     1.436200E+00
1355206  -1.761070E-01     1.387900E+00
1355207  -8.931000E-02     1.348100E+00
1355208  0.000000E+00      1.233610E+00
*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 5
*-----1-----1-----1-----1-----1-----1-----1-----
1355300  2                5
1355301  0.000000E+00      -4.500000E-01
1355302  4.000000E-01     -2.500000E-01
1355303  5.000000E-01     0.000000E+00
1355304  1.000000E+00     3.569000E-01
*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 6
*-----1-----1-----1-----1-----1-----1-----1-----
1355400  2                6
1355401  0.000000E+00      1.233610E+00
1355402  9.064300E-02     1.196500E+00
1355403  1.885690E-01     1.109600E+00
1355404  2.734700E-01     1.041600E+00
1355405  4.586690E-01     8.958000E-01
1355406  5.744800E-01     7.807000E-01
1355407  7.381600E-01     6.134000E-01
1355408  7.685200E-01     5.849000E-01
1355409  8.700570E-01     4.877000E-01
1355410  1.000000E+00     3.569000E-01
*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 7
*-----1-----1-----1-----1-----1-----1-----1-----
1355500  2                7
1355501  -1.000000E+00     -1.000000E+00
1355502  -3.000000E-01     -9.000000E-01
1355503  -1.000000E-01     -5.000000E-01
1355504  0.000000E+00     -4.500000E-01

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*-----1-----1-----1-----1-----1-----1-----1-----
* TORQUE CURVE NO. 8
*-----1-----1-----1-----1-----1-----1-----1-----
1355600 2 8
1355601 -1.000000E+00 -1.000000E+00
1355602 -2.500000E-01 -9.000000E-01
1355603 -8.000000E-02 -8.000000E-01
1355604 0.000000E+00 -6.700000E-01
*-----1-----1-----1-----1-----1-----1-----1-----
* RENODALIZE PUMP 2
*-----1-----1-----1-----1-----1-----1-----1-----
1650000 "PCPUMP2 " PUMP
1650101 0.0 0.514 0.0991 0.0 90.0 0.317900
1650102 0
1650108 160010000 0.0 0.017 0.017 0000
1650109 170000000 0.0 0.1 0.1 0000
1650200 0 1.48858+7 1.22768+6 2.46241+6 0.
1650201 0 7.7855 7.7855 0.0
1650202 0 8.0481 8.0481 0.0
1650301 135 135 135 -1 -1 697 0
1650302 369.00000 .92981030 .31550000 96.000000 500.60000 1.4310000
1650303 613.60000 .00000000 207.43300 .04440000 19.598700 .00000000
1650308 0.212845 0.0 -22.86511 27.16043 5.74589
1650310 0.0 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* REMOVE SPRAY VALVE AND CALCULATOR
*-----1-----1-----1-----1-----1-----1-----1-----
4350000 SPRVLV DELETE
20590400 SPRAY DELETE 0.0 0.0 0.0 0.0 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* REMOVE PRESSURIZER TRIPS AND HEATERS
*-----1-----1-----1-----1-----1-----1-----1-----
0000585 DISCARD
0000586 DISCARD
0000666 510 DISCARD
0000667 510 DISCARD
0000693 510 DISCARD
0000587 DISCARD
0000588 DISCARD
0000668 510 DISCARD
0000669 510 DISCARD
0000694 510 DISCARD
14172000 DELETE
20241700 DELETE
20241800 DELETE
*-----1-----1-----1-----1-----1-----1-----1-----
* REMOVE PRESSURIZER LEVEL CONTROLLERS, CHARGING COMPONENT, AND
* LETDOWN COMPONENT
*-----1-----1-----1-----1-----1-----1-----1-----
20500200 PZRLVL SUM 1.0 0.0 1
20500201 0.0 0.1815 VOIDF 415010000
20500202 0.1524 VOIDF 415020000
20500203 0.3967 VOIDF 415030000
20500204 0.5289 VOIDF 415040000
20500205 0.3967 VOIDF 415050000
20500206 0.1943 VOIDF 415060000
20500207 0.1029 VOIDF 420010000
20500208 0.1029 VOIDF 420020000

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9800000 "CHRG R" DELETE
9850000 "CHRG V" DELETE
20590500 CHARGE DELETE 0.0 0.0 0.0 0.0 0.0 0.0
9900000 "LTDWN S" DELETE
9950000 "LTDWN V" DELETE
20590600 LETDOWN DELETE 0.0 0.0 0.0 0.0 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* REMOVE STEAM VALVE CONTROLLS
*-----1-----1-----1-----1-----1-----1-----1-----1-----
5400000 "CV-P4-10 " VALVE
5400101 530010000 541000000 0.0047772 0.0 0.0 1100
5400201 0 16.963 20.945 0.0
5400300 MTRVLV
5400301 685 686 0.05 .649345 540
20254000 NORMAREA
20254001 0.0 7.066-3
20254002 7.066-3 7.066-3
20254003 1.0 1.0
20590700 "DELTA T" DELETE 0.0 0.0 0.0 0.0 0.0 0.0
20590800 DEADBAND DELETE 0.0 0.0 0.0 0.0 0.0 0.0
20590900 "INT D T" DELETE 0.0 0.0 0.0 0.0 0.0 0.0
20591000 TCONTROL DELETE 0.0 0.0 0.0 0.0 0.0 0.0
20290800 DELETE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* REMOVE FEED SYSTEM CONTROLLER
*-----1-----1-----1-----1-----1-----1-----1-----1-----
20591100 SGLVLERR DELETE 0.0 0.0 0.0 0.0 0.0 0.0
20591200 FEEDFLOW DELETE 0.0 0.0 0.0 0.0 0.0 0.0
5660000 "FEED " TMDPJUN
5660101 565000000 508000000 0.05
5660200 1 588
5660201 0.0 25.593 0.0 0.0
5660202 0.7 0.0 0.0 0.0
5660203 59.5 0.0 0.0 0.0
5660204 60.0 0.50364 0.0 0.0
5660205 1860.0 0.50364 0.0 0.0
5660206 1861.0 0.0 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* REPLACE REACTOR POWER TABLE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
20290000 POWER 609 1.0 45.9+6
20290001 0.0 1.0 * FROM F3S-20&F2-2 OF EDR L5-1 89/11/09
20290002 0.50 0.55374
20290003 1.00 0.18625
20290004 1.50 0.10259
20290005 2.00 0.08423
20290006 2.50 0.080020
20290007 3.0 0.07603
20290008 3.5 0.072700
20290009 5.0 0.064940
20290010 10.0 0.055882
20290011 25.0 0.046738
20290012 65. 0.035
20290013 100. 0.031546
20290014 250. 0.025210
20290015 650. 0.0188
20290016 1000. 0.0164
20290017 1500. 0.0140

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20290018 3000, 0.0110
20290019 5000, 0.0092
20290020 1,+5 0.001460 * CHANGED 89/11/06 BASED ON EDR F2-2 F3S-20
*-1- -1- -1- -1- -1- -1- -1-
*-----1-----1-----1-----1-----1-----1-----1-----
* REPLACE TRIPS 510,511,513
*-----1-----1-----1-----1-----1-----1-----
* SCRAM
0000510 P 100010000 LT NULL 0 1.4190+7 L
* BREAK ISOLATION
0000511 TIME 0 LT NULL 0 7302. N
* HPIS ON
0000513 P 100010000 LE NULL 0 10.600+6 L
*-----1-----1-----1-----1-----1-----1-----
*
* RENODALIZE DEAD END OF FUEL MODULES AND BROKEN LOOP
*
*-----1-----1-----1-----1-----1-----1-----
* DEAD END OF FUEL MODULES
*-----1-----1-----1-----1-----1-----1-----
2510000 "DE FL MODS" SINGLVOL
2510101 0.0 0.7844123 0.1154214 0.0 90.0 0.7844123
2510102 3.81-6 0.214 00
2510200 0 1.49207+7 1.33213+6 2.46168+6 0.0
*-----1-----1-----1-----1-----1-----1-----
* REACTOR VESSEL NOZZLE - BROKEN LOOP HOT LEG
*-----1-----1-----1-----1-----1-----1-----
3000000 "RVN BLHL " BRANCH
3000001 2 0
3000101 0.0 0.876303 0.0575410 0.0 0.0 0.0
3000102 4.0E-5 0.0 00
3000200 0 1.49144+7 1.25750+6 2.46181+6 0.0
3001101 252010000 300000000 0.067014 0.0 0.0 0002
3002101 300010000 305000000 0.063426 0.1 0.1 0000
3001201 0.0 0.0 0.0
3002201 0.0 0.0 C.C
*-----1-----1-----1-----1-----1-----1-----
* HOT LEG PIPE TO REFLOOD ASSIST BYPASS TEE
*-----1-----1-----1-----1-----1-----1-----
3050000 "HLP-RABS T" BRANCH
3050001 1 0
3050101 0.0 0.698336 0.0442927 0.0 0.0 0.0
3050102 4.0E-5 0.0 00
3050200 0 1.49144+7 1.25750+6 2.46181+6 0.0
3051101 305010000 310000000 0.0 0.1 0.1 0100
3051201 0.0 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----
* BROKEN LOOP HOT LEG CONTRACTION
*-----1-----1-----1-----1-----1-----1-----
3100000 "BLHL CONTR" BRANCH
3100001 2 0
3100101 0.0 1.50013 0.0678467 0.0 0.0 0.0
3100102 4.0E-5 0.0 00
3100200 0 1.49144+7 1.25750+6 2.46181+6 0.0
3101101 380010000 310000000 0.0388 0.84 0.84 0100
3102101 310010000 315000000 0.0083647 0.0 0.0 0100
3101201 0.0 0.0 0.0
3102201 0.0 0.0 0.0

```

* STEAM GENERATOR AND PUMP SIMULATOR			
ID	DESCRIPTION	PIPE	
3150000	"SG+PMP SIM"	PIPE	
3150001	12		
3150101	0.0	12	
3150201	0.0083647	2	
3150202	0.032603	4	
3150203	0.105626	5	
3150204	0.032603	7	
3150205	0.0083647	9	
3150206	0.008364	10	
3150207	0.0046398	11	
3150301	0.367768	1	
3150302	0.552201	2	
3150303	0.993978	4	
3150304	0.849744	6	
3150305	0.993978	8	
3150306	1.371350	9	
3150307	1.365029	10	
3150308	1.674812	11	
3150309	0.545209	12	
3150401	3.0767-3	1	
3150402	4.67621-3	2	
3150403	8.60554-2	4	
3150404	8.97552-2	6	
3150405	8.60554-2	8	
3150406	1.82303-2	9	
3150407	5.46687-2	10	
3150408	1.82489-2	11	
3150409	2.83241-2	12	
3150601	90.0	5	
3150602	-90.0	10	
3150603	90.0	11	
3150604	0.0	12	
3150701	0.127000	1	
3150702	0.552201	2	
3150703	0.993978	4	
3150704	0.457202	5	
3150705	-0.457202	6	
3150706	-0.993978	8	
3150707	-1.37135	9	
3150708	-0.520701	10	
3150709	1.212851	11	
3150710	0.0	12	
3150801	4.0E-5	0.0	3
3150802	4.0E-5	0.124	4
3150803	4.0E-5	0.0	6
3150804	4.0E-5	0.124	7
3150805	4.0E-5	0.0	12
3150901	0.2	0.2	1
3150902	0.0	0.0	2
3150903	93.9	93.9	4
3150904	0.4	0.4	5
3150905	93.9	93.9	7
3150906	0.0	0.0	8
3150907	0.2	0.2	9
3150908	4.1	4.1	10

3150909	0.4	0.4	11				
3151001	00	12					
3151101	0000	1					
3151102	0100	2					
3151103	0000	7					
3151104	0100	8					
3151105	0000	10					
3151106	0100	11					
3151201	0	14914000.	1257500.	2461820.	0.0	0.0	01
3151202	0	14911400.	1257500.	2461870.	0.0	0.0	02
3151203	0	14905500.	1257500.	2461990.	0.0	0.0	03
3151204	0	14998100.	1257500.	2462150.	0.0	0.0	04
3151205	0	14992600.	1257500.	2462270.	0.0	0.0	05
3151206	0	14992600.	1257500.	2462270.	0.0	0.0	06
3151207	0	14998100.	1257500.	2462150.	0.0	0.0	07
3151208	0	14905500.	1257500.	2461990.	0.0	0.0	08
3151209	0	14914500.	1257500.	2461810.	0.0	0.0	09
3151210	0	14921600.	1257500.	2461660.	0.0	0.0	10
3151211	0	14919000.	1257500.	2461710.	0.0	0.0	11
3151212	0	14914300.	1257500.	2461810.	0.0	0.0	12
3151300	0						
3151301	0.0	0.0	0.0	11			

\*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----

\* REACTOR VESSEL NOZZLE - BROKEN LOOP COLD LEG

\*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----

3350000 "RVN BLCL " BRANCH

3350001	2	0				
3350101	0.0	0.749305	0.047979	0.0	0.0	0.0
3350102	4.0E-5	0.0	00			
3350200	0	1.49889+7	1.23500+6	2.46018+6	0.0	
3351101	202000000	335000000	0.064130	1.0	1.0	0002
3352101	335010000	340000000	0.0	0.1	0.1	0000
3351201	0.0	0.0	0.0			
3352201	0.0	0.0	0.0			

\*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----

\* COLD LEG PIPE TO REFLOOD ASSIST BYPASS TEE

\*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----

3400000 "CLP-RABS T" BRANCH

3400001	1	0				
3400101	0.0	0.698336	0.0443927	0.0	0.0	0.0
3400102	4.0E-5	0.0	00			
3400200	0	1.49889+7	1.23500+6	2.46018+6	0.0	
3401101	340010000	345000000	0.0	0.1	0.1	0100
3401201	0.0	0.0	0.0			

\*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----

\* BROKEN LOOP COLD LEG CONTRACTION TO BREAK PLANE

\*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----

3450000 "BLCL CONTR" BRANCH

3450001	2	0				
3450101	0.0634	0.974	0.0	0.0	0.0	0.0
3450102	4.0E-5	0.0	00			
3450200	0	1.49889+7	1.23500+6	2.46018+6	0.0	
3451101	345000000	370000000	0.0388	0.84	0.84	0100
3452101	345010000	350000000	0.0	0.0	0.0	0100
3451201	0.0	0.0	0.0			
3452201	0.0	0.0	0.0			

\*-----1-----1-----1-----1-----1-----1-----1-----1-----1-----

\* SPOOL PIECE AND PIPE TO ISOLATION VALVE

```

*-----1-----1-----1-----1-----1-----1-----1-----1-----
3500000 "BRK SP+PPE"          SNGLVOL
3500101 0.0525 0.823 0.0 0.0 0.0 0.0
3500102 4.0E-5 0.0 00
3500200 0 1.49889+7 1.23500+6 2.46018+6 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* REMOVE COLD LEG ISOLA. VALVE AND COLD LEG PIPE BETWEEN
* ISOLATION VALVE AND QOB.
*-----1-----1-----1-----1-----1-----1-----1-----1-----
3550000 "CL ISO VLV"          DELETE
3600000 "CL IS-QOBV"          DELETE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* COLD LEG QUICK OPENING BLOWDOWN VALVE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
3650000 "CO QOBV "          VALVE
3650101 350010000 805000000 1.729E-3 0.0 0.0 0100 1.0 1.0
3650201 0 0.0 0.0 0.0 0.0
3650300 MTRVLV
3650301 677 502 14.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* REFLOOD ASSIST BYPASS PIPING - COLD LEG SIDE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
3700000 "RABS C L "          PIPE
3700001 3
3700101 0.0388 2
3700102 0.0776 3
3700201 0.0388 2
3700301 0.0 3
3700401 0.0279 1
3700402 0.070 2
3700403 0.1165 3
3700601 90.0 1
3700602 0.0 3
3700701 0.64 1
3700702 0.0 3
3700801 4.0-5 0.0 3
3700901 0.28 0.28 1
3700902 0.84 0.84 2
3701001 00 3
3701101 0000 2
3701201 0 1.49865+7 1.23500+6 2.46023+6 0.0 0.0 01
3701202 0 1.49841+7 1.23500+6 2.46028+6 0.0 0.0 02
3701203 0 1.49841+7 1.23500+6 2.46028+6 0.0 0.0 03
3701300 0
3701301 0.0 0.0 0.0 01
3701302 0.0 0.0 0.0 02
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* REFLOOD ASSIST BYPASS VALVES
*-----1-----1-----1-----1-----1-----1-----1-----1-----
3750000 "RABS VALVS"          SNGLJUN
3750101 370010000 380000000 0.0 1.55+2 1.55+2 0000
3750201 0 0.0 0.0 0.0
*-----1-----1-----1-----1-----1-----1-----1-----1-----
* REFLOOD ASSIST BYPASS PIPING - HOT LEG SIDE
*-----1-----1-----1-----1-----1-----1-----1-----1-----
3800000 "RABS H L "          PIPE
3800001 3
3800101 0.0776 1

```





0000329	SATTEMP	415030000	* TE-139-20
0000330	SATTEMP	205010000	* TE-1ST-1 / TE-2ST-1
0000331	SATTEMP	210010000	* TE-1ST-2 / TE-2ST-2
0000332	SATTEMP	210050000	* TE-1ST-6 / TE-2ST-6
0000333	SATTEMP	210060000	* TE-1ST-7 / TE-2ST-7
0000334	SATTEMP	215010000	* TE-1ST-10 / TE-2ST-10
0000335	SATTEMP	220010000	* TE-1ST-13 / TE-2ST-13
0000336	SATTEMP	250010000	* TE-1UP-6
0000337	SATTEMP	251010000	* TE-2UP-4
0000338	SATTEMP	255010000	* TE-1UP-3

\*-----1-----1-----1-----1-----1-----1-----1-----1-----

\* DENSITIES

\*-----1-----1-----1-----1-----1-----1-----1-----1-----

0000341	RHO	345010000	* DE-BL-1
0000342	RHO	310010000	* DE-BL-2
0000343	RHO	180010000	* DE-PC-1
0000344	RHO	100010000	* DE-PC-2
0000345	RHO	118020000	* DE-PC-3

\*-----1-----1-----1-----1-----1-----1-----1-----1-----

\* VELOCITIES

\*-----1-----1-----1-----1-----1-----1-----1-----1-----

0000351	VELF	345010000	* FE-BL-1
0000352	MFLOWJ	630000000	* LPISL-2
0000353	VELF	180010000	* FE-PC-1
0000354	VELF	100010000	* FE-PC-2
0000355	VELG	345010000	* FE-BL-1
0000356	VELG	310010000	* FE-BL-2
0000357	VELG	180010000	* FE-PC-1
0000358	VELG	100010000	* FE-PC-2

\*-----1-----1-----1-----1-----1-----1-----1-----1-----

\* MASS FLOW RATES

\*-----1-----1-----1-----1-----1-----1-----1-----1-----

0000361	MFLOWJ	345020000	* BREAK PLANE BLCL
0000362	MFLOWJ	315110000	* BREAK PLANE BLHL
0000363	MFLOWJ	345020000	* DTT-RAKE BLCL
0000364	MFLOWJ	310020000	* DTT-RAKE BLHL
0000365	MFLOWJ	180010000	* DTT-RAKE ILCL
0000366	MFLOWJ	100020000	* DTT-RAKE ILHL
0000367	MFLOWJ	400010000	* PRES. SURGE LINE FLOW
0000369	MFLOWJ	541010000	* FE-P4-12
0000370	MFLOWJ	566000000	* FE-P4-72-1
0000371	MFLOWJ	230010000	* REFLOODING FLOW
0000372	CNTRLVAR	51	* INT BRK FLOW
0000373	HTTEMP	231000110	
0000374	HTTEMP	231000210	
0000375	HTTEMP	231000310	
0000376	HTTEMP	231000410	
0000377	HTTEMP	231000510	
0000378	HTTEMP	231000610	

\*-----1-----1-----1-----1-----1-----1-----1-----1-----

\* CLADDING TEMPERATURES CONTROL MODULE

\*-----1-----1-----1-----1-----1-----1-----1-----1-----

0000381	HTTEMP	230000110	*
0000382	HTTEMP	230000210	*
0000383	HTTEMP	230000310	*
0000384	HTTEMP	230000410	*
0000385	HTTEMP	230000510	*
0000386	HTTEMP	230000610	*



\* REACTOR VESSEL LIQUID LEVEL CONTROL VARIABLE

\*  
20501000 RVLVL SUM 0.2794034 0.0 1  
20501001 0.0 1.0 VOIDF 230010000  
20501002 1.0 VOIDF 230020000  
20501003 1.0 VOIDF 230030000  
20501004 1.0 VOIDF 230040000  
20501005 1.0 VOIDF 230050000  
20501006 1.0 VOIDF 230060000

\* REPLACE HPIS 89.2.13

\* DELAYED HPIS INJECTION

0000583 TIME,0 GE TIMEOF,513 2.48 L -1.0 \* 89/11/08  
0000683 583 AND 583 L  
6400000 "HPIS" TMDPJUN  
6400101 625000000 185000000 5.9896-3  
6400200 1 683 P 185010000 \* 89/11/08  
6400201 0.0 0.0 0.0 0.0  
6400202 0.0 0.700 0.0 0.0  
6400203 3.5+6 0.575 0.0 0.0  
6400204 6.6+6 0.460 0.0 0.0  
6400205 17.0+6 0.100 0.0 0.0

\* LPIS CAPACITY CORRECTED BASED ON EXPERIMENT DATA TAPE

\* "LPIS " TMDPJUN

6300101 625000000 605000000 5.9896-3  
6300200 1 684 P 605010000  
6300201 0.0 5.5 0.0 0.0  
6300202 0.2+6 5.0 0.0 0.0  
6300203 0.6+6 4.0 0.0 0.0  
6300204 0.8+6 3.0 0.0 0.0  
6300205 1.0+6 2.0 0.0 0.0  
6300206 1.2+6 1.6 0.0 0.0  
6300207 1.3+6 1.5 0.0 0.0  
6300208 1.4+6 1.4 0.0 0.0  
6300209 1.5+6 0.0 0.0 0.0

\* IMPROVE ACCUMULATOR (E J LEE 89.2.28)

\*-----1-----1-----1-----1-----1-----1-----1-----

\* ACCUMULATOR VALVE TRIPS

\*-----1-----1-----1-----1-----1-----1-----1-----

579 MFLOW 610000000 GE NULL 0 0.0 N  
0000580 CNTRLVAR 4 LT NULL 0 1.050 L \* E.JL 89/10/03

\* MODIFIED THE LIMIT OF ACCUM EMPTY CASE INTO 1.52 FROM 0.939 (P160 EDR, 89.5.15) E.JL

0000682 579 AND -580 N  
\*-----1-----1-----1-----1-----1-----1-----1-----

\* ACCUMULATOR LEVEL CONTROL VARIABLE

\*-----1-----1-----1-----1-----1-----1-----1-----

20500400 ACCMLVL INTEGRAL -6.549E-3 1.54 0

20500401 VELFJ 620010000

\*-----1-----1-----1-----1-----1-----1-----1-----

\* ECC CHECK VALVE

```

*-----1-----1-----1-----1-----1-----1-----1-----
6000000 "ECC CHKVLV" VALVE
6000101 605010000 185000000 0.0 1.3869 1.3869 0100
6000201 0 0.0 0.0 0.0
6000300 TRPVLV
6000301 681
*-----1-----1-----1-----1-----1-----1-----1-----
* ECCS HEADER TO PCS
*-----1-----1-----1-----1-----1-----1-----1-----
6050000 "ECCS HFAER" SNGLVOL
6050101 5.989E-3 4.8247 0.0 0.0 0.0 2.2061
6050102 1.0165-5 0.0 10
6050200 0 1.66E+6 125472. 2600290. 0.0
*-----1-----1-----1-----1-----1-----1-----1-----
* ACCUMULATOR VALVE
*-----1-----1-----1-----1-----1-----1-----1-----
6100000 "ACCUM VLV " VALVE
6100101 615010000 605000000 0.0 8.1009 8.1009 0000
6100201 0 0.0 0.0 0.0
6100300 TRPVLV
6100301 682
*-----1-----1-----1-----1-----1-----1-----1-----
* ACCUMULATOR PIPE
*-----1-----1-----1-----1-----1-----1-----1-----
6150000 "ACC PIPE " SNGLVOL
6150101 0.01608 24.5486 0.0 0.0 0.0 0.0
6150102 1.0165-5 0.0 10
6150200 3 1.66E+6 308.2
*-----1-----1-----1-----1-----1-----1-----1-----
* ACCUMULATOR VESSEL
*-----1-----1-----1-----1-----1-----1-----1-----
*
* MOVE TO S/S COMPONENT BY B. D. CHUNG
*
*
6200000 "ACCUMULATR" ACCUM
6200101 1.254 1.8261563 0.0 0.0 -90.0 -1.8261563
6200102 2.286-5 0.0 10
6200200 1.66E+6 308.2
6201101 615000000 8.13E-3 6.7532 8.3202 0
6202200 1.10 0.0 4.0251 0.67056 0.04445 0 0 0 0
*-----1-----1-----1-----1-----1-----1-----1-----
*****
*** TRIP CHANGE FOR L5-1
0000518 TIME 0 GE NULL 0 4.0 N
0000695 518 AND 518 N
0000697 518 AND 518 N
*
* LPIS
0000520 P 100010000 LT NULL 0 1.08+6 N
*
* RUN STATISTICS
*
20507800 OLDTIME SUM 1. 0. 0
20507801 0. 1. CNTRLVAR 79
*
20507900 NEWTIME SUM 1. 0. 0
20507901 0. 1. TIME 0.

```

```

*
20508100 TSTEP SUM 1. 0. 0
20508101 0. -1. CNTRLVAR 78
20508102 1. CNTRLVAR 79

```

\*

\*

\*00 PLOT REQUEST VARIABLES \*

\*

```

20300100 P 250010000 * UPPLENUM PRESSURE(PE-1UP-1A1)
20300200 P 530010000 * STEAMDOME PRESSURE(PE-SGS-1)
20300300 HTTEMP 230000110
20300400 HTTEMP 230000210
20300500 HTTEMP 230000310
20300600 HTTEMP 230000410
20300700 HTTEMP 230000510
20300800 HTTEMP 230000610
20300900 HTTEMP 231000110 * PERIPHERAL 89/11/10
20301000 HTTEMP 231000210
20301100 HTTEMP 231000310
20301200 HTTEMP 231000410
20301300 HTTEMP 231000510
20301400 HTTEMP 231000610
20301600 VELFJ 112010000 * IL HL LIQUID VEL
20301700 VELGJ 112010000 * IL HL VAPOR VEL
20301800 RHO 100010000 * IL HL DENSITY(DE-PC-2)
20301900 RHO 345010000 * BL CL DENSITY(DE-BL-1)
20302000 MFLOWJ 365000000 *BREAK FLOW(FR-BL-111)
20302100 MFLOWJ 640000000 *HPIS FLOW
20302200 MFLOWJ 230010000 * REFLOODING RATE
20302300 CPUTIME 0 *CPU TIME
*20302400 ACVLIQ 620000000 *ACCUUM VOL
20302500 MFLOWJ 545000000 * STEAM MASS OUT
20302600 MFLOWJ 540000000 * STAEM MASS OUT
20302700 MFLOWJ 569000000 * STEAM MASS IN
20302800 MFLOWJ 566000000 * STAEM MASS IN (AUX)
20302900 VOIDF 515010000 * SG2
20303000 VOIDF 515020000 *
20303100 VOIDF 515030000
20303200 VOIDF 515040000
20303300 VOIDF 515050000
20303400 VOIDG 250010000 * UPPER PLENUM
20303500 VOIDF 250010000
20303600 VOIDF 245010000
20303700 VOIDF 240010000
20303800 VOIDF 230060000
20303900 VOIDF 230050000
20304000 VOIDF 230040000
20304100 VOIDF 230030000
20304200 VOIDF 230020000
20304300 VOIDF 230010000
20304400 VOIDF 225010000
20304500 VOIDF 215010000
20304600 MFLOWJ 610000000
20304700 MFLOWJ 630000000 *LPIS
20304800 RHO 345010000 *DENSITY BEFORE BREAK
20304900 VOIDG 345010000
20305000 VELFJ 180010000 * LIQ VELOCITY AT ILCL (FE-PC-001B)
20305100 CNTRLVAR 1

```

203 15200 CNTRLVAR 2  
203 15300 CNTRLVAR 4  
20305400 CNTRLVAR 10  
20305500 CNTRLVAR 71  
20305600 CNTRLVAR 81 \* TIME STEP DT FROM CV 81  
20305700 MFLOWJ 100010000  
20305800 CNTRLVAR 72  
20305900 CNTRLVAR 51 \* INT BRK FLOW

\*  
. \* END OF INPUT DATA

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(See instructions on the reverse)

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10. SUPPLEMENTARY NOTES

11. ABSTRACT (200 words or less)

The LOFT intermediate break experiment L5-1, which simulates 12 inch diameter ECC line break in a typical PWR, has been analyzed using the reactor thermal/hydraulic analysis code RELAP/MOD2, Cycle 36.05. The base calculation, which modeled the core with single flow channel and two heat structures without using the options of reflood and gap conductance model has been successfully completed and compared with experimental data. Sensitivity studies were carried out to investigate the effects of nodalization at reactor vessel and core modeling on major thermal hydraulic parameters, especially on peak cladding temperature (PCT). These sensitivity items are: single flow channel and single heat structure (Case A), two flow channel and two heat structures (Case B), reflood options added (Case C) and both reflood and gap conductance options added (Case D). The code, RELAP/MOD2 Cycle 36.04 with the base modeling, predicted the key parameters of LOFT IBLOCA Test L5-1 better than Cases A, B, C and D. Thus, it is concluded that the single flow channel modeling for core is better than the two flow channel modeling and two heat structure is also better than a single heat structure modeling to predict PCT at the central fuel rods. It is recommended to use the reflood option and not to use gap conductance option for this L5-1 type IBLOCA.

12. KEY WORDS/DESCRIPTORS (List words or phrases that will assist researchers in locating the report.)

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Experiment L5-1

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