

TENNESSEE VALLEY AUTHORITY

CHATTANOOGA, TENNESSEE 37401  
400 Chestnut Street Tower II

August 23, 1984

Director of Nuclear Reactor Regulation  
Attention: Mr. Carl H. Berlinger, Chief  
Core Performance Branch  
Division of Licensing  
U.S. Nuclear Regulatory Commission  
Washington, D.C. 20555

Dear Mr. Berlinger:

In the Matter of the ) Docket No. 50-328  
Tennessee Valley Authority )

Enclosed is the peaking factor limit report for unit 2, cycle 3 operations. This report is being provided in accordance with the requirements of paragraph 6.9.1.14 of the Sequoyah unit 2 technical specifications.

If you have any questions concerning this matter, please get in touch with Jerry Wills at FTS 858-2683.

Very truly yours,

TENNESSEE VALLEY AUTHORITY

*L. M. Mills*  
L. M. Mills, Manager  
Nuclear Licensing

Sworn to and subscribed before me  
this 23<sup>rd</sup> day of Aug. 1984.

*Raylette H. White*  
Notary Public

My Commission Expires 9-5-84  
Enclosure

cc (Enclosure):

U.S. Nuclear Regulatory Commission  
Region II  
Attn: Mr. James P. O'Reilly, Regional Administrator  
101 Marietta Street, NW, Suite 2900  
Atlanta, Georgia 30323

Director of Nuclear Reactor Regulation  
Attn: Ms. E. Adensam, Chief  
Licensing Branch No. 4  
Division of Licensing  
U.S. Nuclear Regulatory Commission  
Washington, D.C. 20555

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ENCLOSURE

PEAKING FACTOR LIMIT REPORT FOR SEQUOYAH UNIT 2 CYCLE 3  
RAOC OPERATION

This peaking Factor Limit Report is provided in accordance with Paragraph 6.9.1.14 of the Sequoyah Unit 2 Technical Specifications.

The Sequoyah Unit 2, Cycle 3 elevation dependent  $W(z)$  values for RAOC operation at beginning, early middle, late middle, and near end-of-life are shown in Figures 1 through 4 respectively. This information is sufficient to determine  $W(z)$  versus core height for Cycle 3 burnups in the range of 0 MWD/MTU to 14500 MWD/MTU through the use of three point interpolation.  $W(z)$  was calculated using the method described in Part B of Reference 1.

The appropriate  $W(z)$  function is used to confirm that the heat flux hot channel factor,  $F_Q(z)$ , will be limited to the Technical Specification values of:

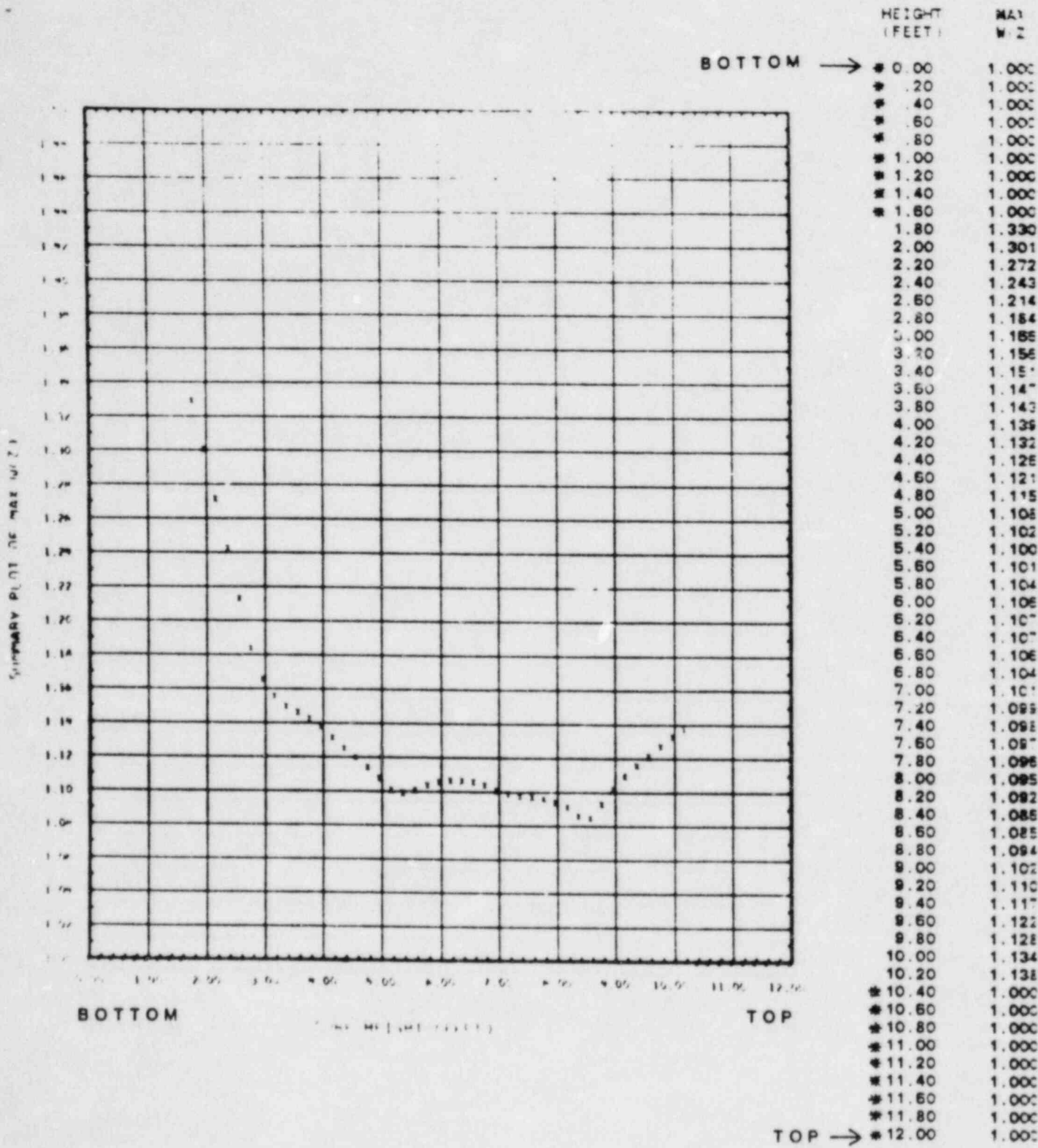
$$F_Q(z) \leq \frac{2.237}{P} [K(z)] \quad \text{for } P > 0.50 \text{ and}$$

$$F_Q(z) \leq 4.474 [K(z)] \quad \text{for } P \leq 0.50$$

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The appropriate elevation dependent  $W(z)$  values, when applied to a power distribution measured under equilibrium conditions, demonstrates that the initial conditions assumed in the LOCA are met, along with the ECCS acceptance criteria of 10CFR50.46.

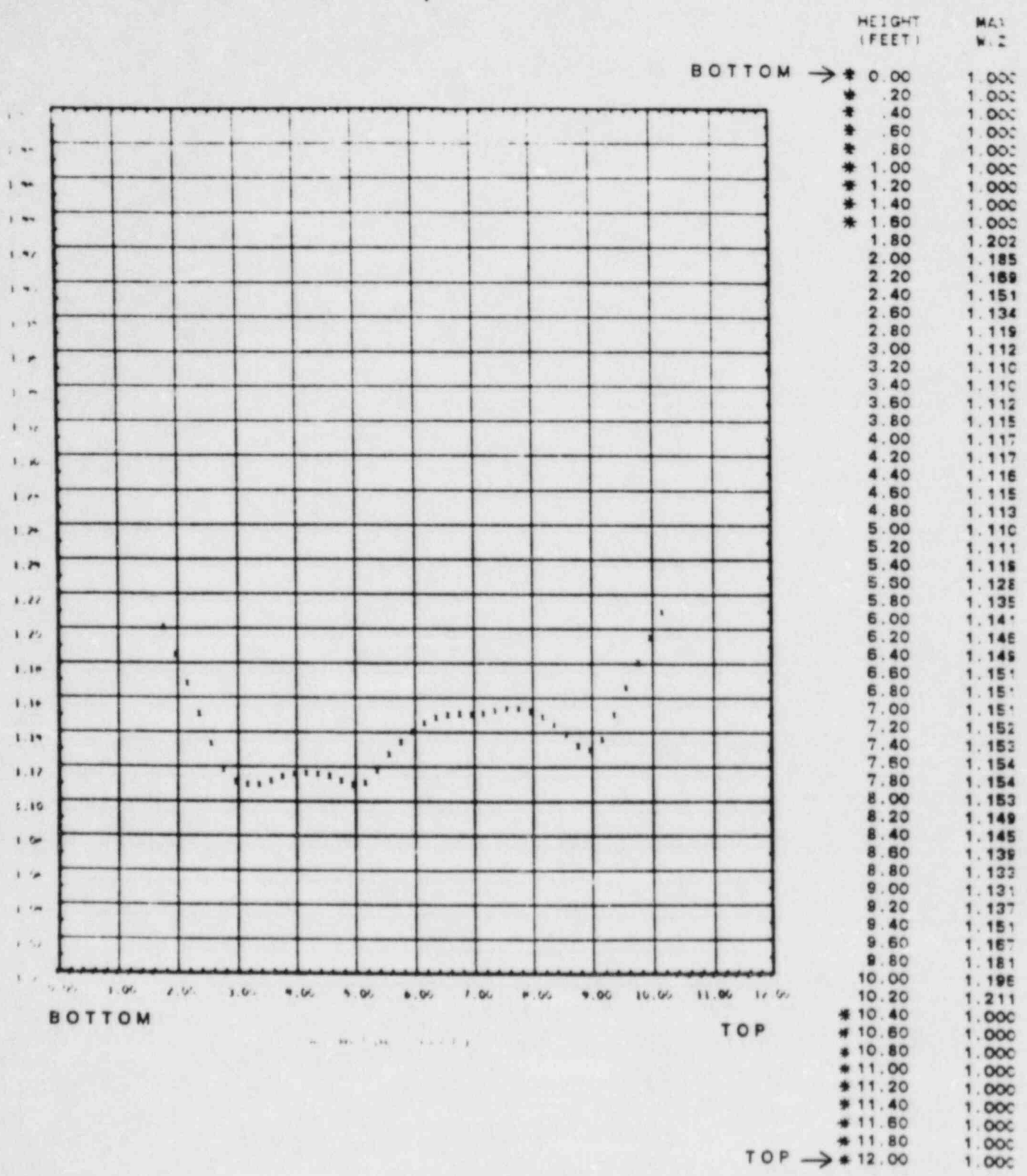
- (1) WCAP-10216-P-A, Relaxation of Constant Axial Offset Control -  $F_Q$   
Surveillance Technical Specification



\* Top and bottom 15% excluded as per Technical Specification 4.2.2.2.g

FIGURE 1  
 Sequoyah Unit 2 Cycle 3 RAOC W(z)  
 At 150 MWD/MTU

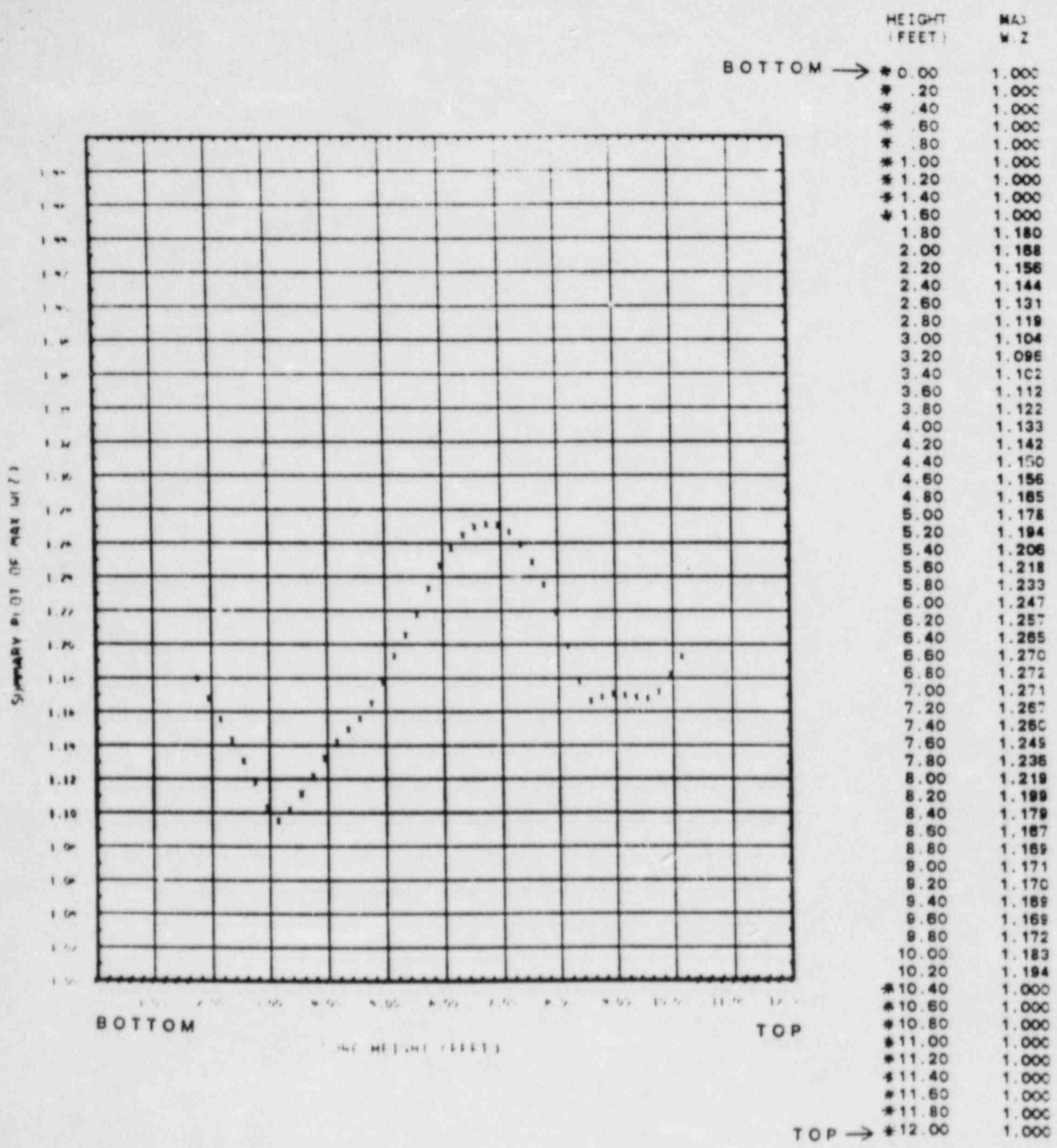
SUMMARY PLOT OF MAX W(z)



\* Top and bottom 15% excluded as per Technical Specification 4.2.2.2.g

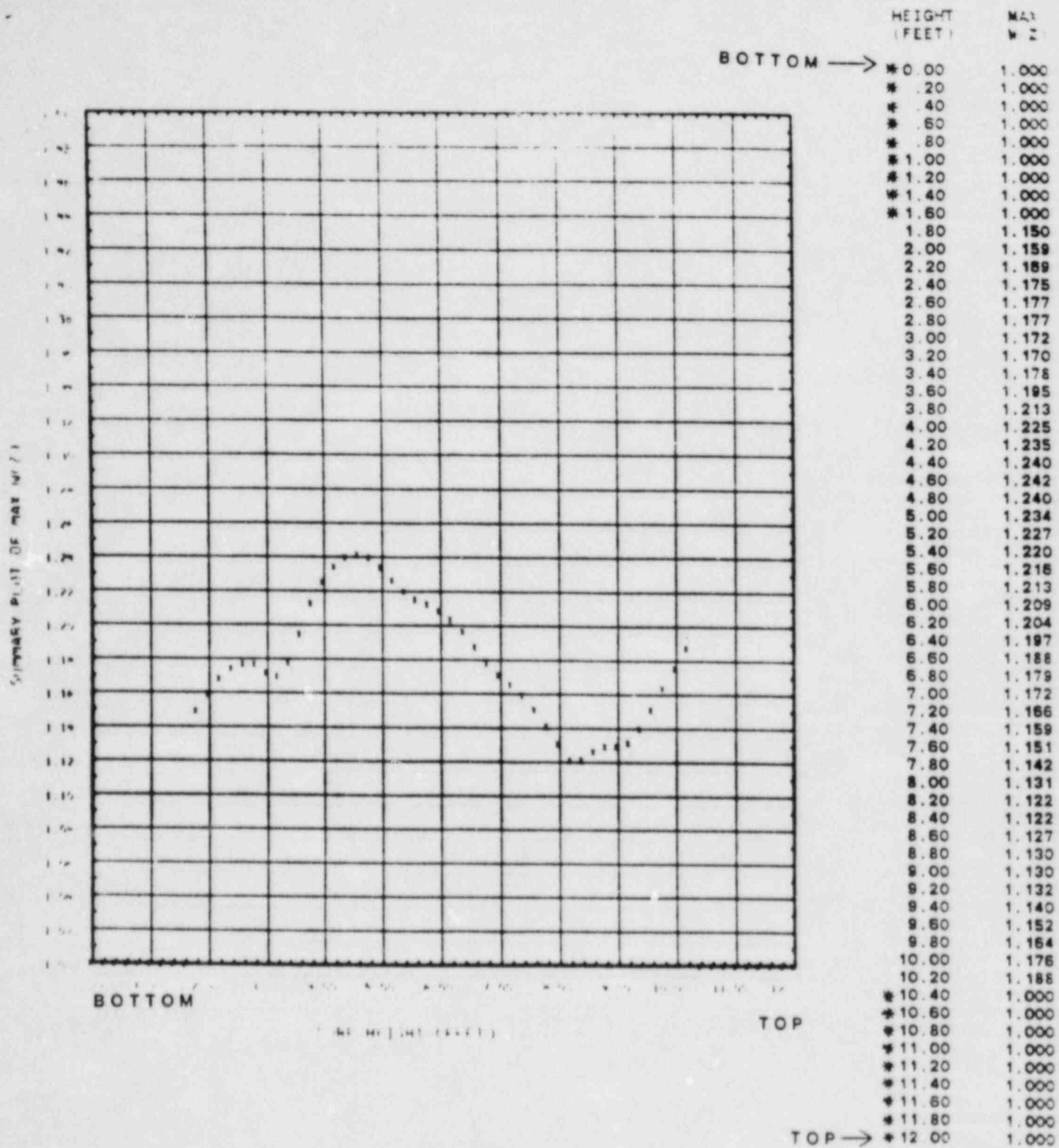
FIGURE 2  
 Sequoyah Unit 2 Cycle 3 RAOC W(z)  
 At 4000 MWD/MTU





\* Top and bottom 15% excluded as per Technical Specification 4.2.2.2.g

FIGURE 3  
 Sequoyah Unit 2 Cycle 3 RAOC W(z)  
 At 8000 MWD/MTU



\* Top and bottom 15% excluded as per Technical Specification 4.2.2.2.g

FIGURE 4  
 Sequoyah Unit 2 Cycle 3 RAOC W(z)  
 At 12000 MWD/MTU