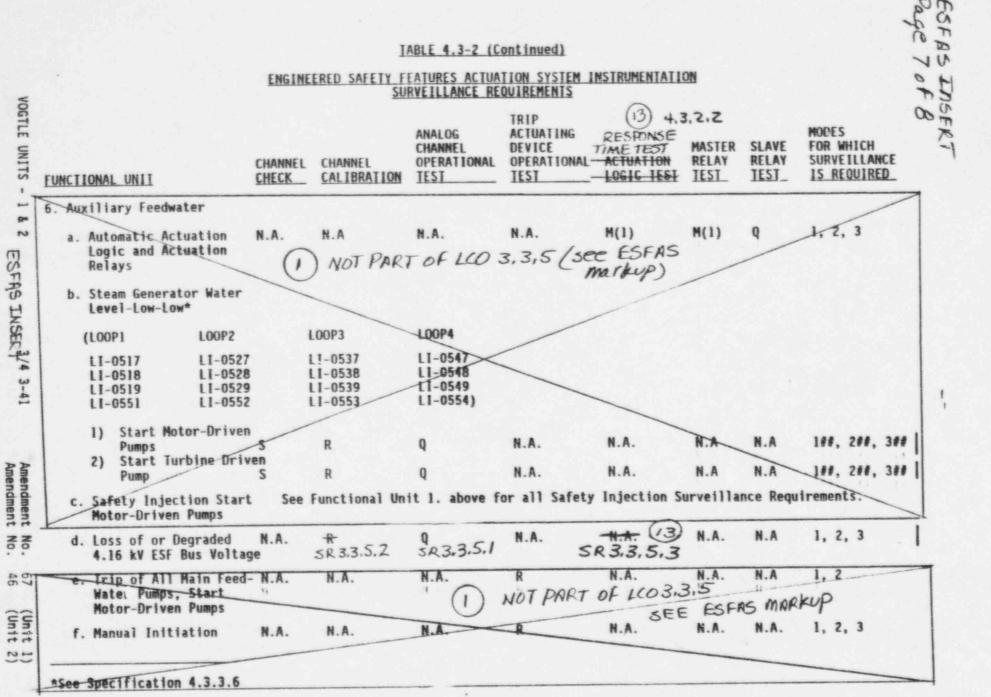
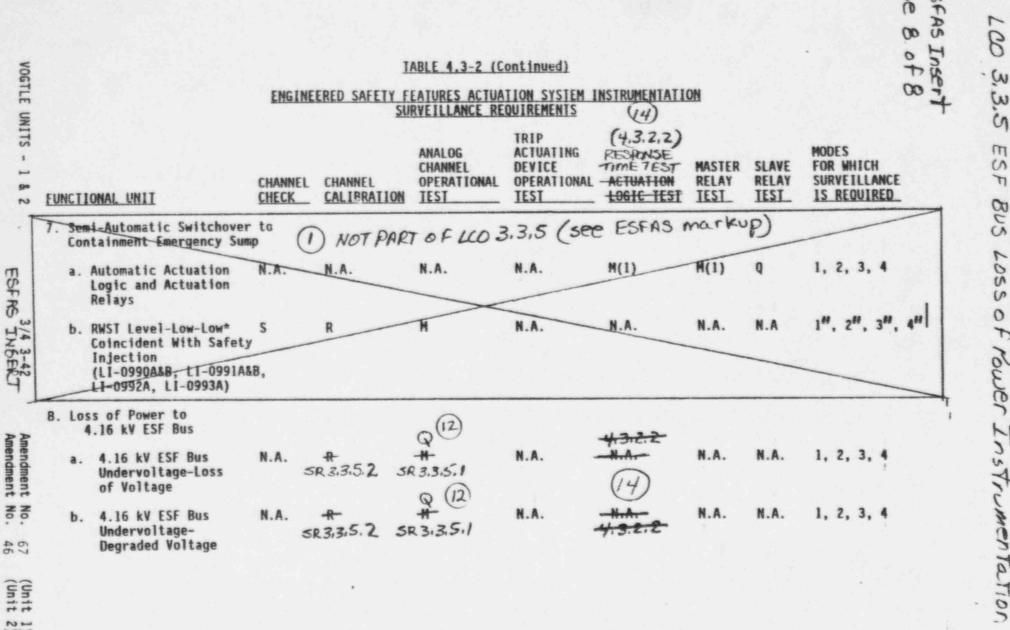
VOGTL	REACTOR TRIP SYS	TABLE 4.3-1 (Continued) (42 10N SURVEILLANC) <u>E REQUIREMENTS</u>		(43)		
VOGTLE UNITS - 1 &	EUNCTIONAL UNIT CHANNEL 13 Steam Generator Water Level	CHANNEL CALIBRATION SR 3. 3.1.10	ANALOG CHANNEL OPERATIONAL IEST SR 3.3,1.7	TRIP ACTUATING DEVICE OPERATIONAL TEST N.A.	ACTUATION LOGIC TEST N.A.	MODES FOR WHICH SURVEILLA <u>IS REQUIR</u> 1', 2'	NCE	(59) RESPONSE TIME TEST SR3.3.1.15
2	13. Steam Generator Water Level5 Low-Low* (LOOP1 LOOP2 LOOP3 LOOP4 L1-0517 L1-0527 L1-0537 L1-0547 L1-0518 L1-0528 L1-0538 L1-0548 L1-0519 L1-0529 L1-0539 L1-0549 L1-0551 L1-0552 L1-0553 L1-0554	BASES (SR 3.3.1.9 (4				
3/4 3-11	 Undervoltage - Reactor Coolant N.A. Pumps Underfrequency - Reactor N.A. Coolant Pumps 	SR 3.3.1.10 A SR 3.3.1.10 A	N.A. N.A.	3R3.3.1.9(4)	N.A.	l" l"	1	SR3.3.1.15 SR3.3.1.15
Amendment Amendment	16. Turbine Trip a. Low Fluid Oil Pressure (PT-6161, PT-6162, PT-6163) b. Turbine Stop Valve Closure N.A.	SR3.3.1.10 SR3.3.1.10 #	SR 3, 3.1.16 *5/8(1, 10) N.A.	SR 3.3.1.14(SR 3.3.1.14(SR 3.3.1.13	↔ N.A.	1 ^{b. r} 1b	I	N/A N/A N/A
nt No. 67 nt No. 46	 17. Safety Injection Input from N.A. ESF 18. Reactor Trip System Interlocks a. Intermediate Range Neutron Flux, P-6 	N.A. 51, 88.3,3.1.11	N.A. 58.3,1.12 R	4	N.A. N.A.	1, 2 2 ^{c. 1}	1	N/A
(Unit 1) (Unit 2)	(19 ← (NI-00358, D&E,) NI-00368, D&G) *See Specification 4.3.3.6 → BA5FS (19)	50	* AFter eac and prior trip set	h mode 3 er to exceeding	try for up	it shut.	town)]
	2511280030 951120 DR ADOCK 05000424 PDR							

		ENGINE	ERED SAFETY F	EATURES ACTUA	TION SYSTEM I QUIREMENTS	INSTRUMENTATI	ON		7 o F
UNCTIO	NAL UNIT	CHANNEL CHECK	CHANNEL CALIBRATION	ANALOG Channel Operational Test	TRIP ACTUATING DEVICE OPERATIONAL TEST	(4.3.2.2) RESPONSE Time Test ACTUATION LOGIC TEST	33 MASTER RELAY IESI	SLAVE RELAY TEST	MODES FOR WHICH SURVEILLANCE IS REOUIRED
0. C S	ontrol Room Emergency ystem Actuation (Cont	Filtrati	ion LCO 3.	3.7 TABL	E 3.3.7-1				
			tional Unit 1	. above for a	111 Safety Inj	jection Surve	illance	Reguire	ments.
đ	. Intake Radiogas S Monitor (RE-12116, RE-12117	\$ SR3.		# 9 (B)	N.A. (33)	4,3.2.2 4.A. R 3.3.7.6	N.A.	N.A.	Either Unit in 1, 2, 3, 4, \$#, \$#
A	uel Handling Building ccident Ventilation A Common System)	Post ctuation	8 NOT PA	RT OF LCO 3	,3,7 (see)	ESFAS Ma	nkup)		
а	. Manual Initiation	N.A.	N.A.	N.A.	R	N.A.	N.A.	N.A.	(2)
b	. Fuel Handling Building Exhaust Duct Radiation Signal (ARE-2532 A&B ARE-2533 A&B)	\$	R	м	N.A.	N.A.	N.A.	N.A.	(2)
c	 Automatic Actuation Logic and Actuation Relays 	N.A.	N.A. 31	N.A.	N.A.	M(1)	N.A.	N.A.	(2)



1 00 w N S ESF Bus Loss of Ruer Instrumentation



*See Specification 4.3.3.6

10550 Frower Instrumentation

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The following pages replace and supplement the existing pages behind the Enclosure 2 tab for Chapter 3.3, Volume 3.

3/4.3.1 RTS INSTRUMENTATION

CHANGE NUMBER SHE

A

50

DISCUSSION

required Channel Calibration is adequate to ensure the setpoint remains within the required tolerance. This change is considered less restrictive for VEGP but is consistent with NUREG-1431.

The Notes affecting the Turbine Trip functions are incorporated into VEGP ITS SRs 3.3.1.14 and 3.3.1.16 and their associated frequencies, consistent with NUREG-1431. In addition, the frequency for the low fluid oil pressure turbine trip function is revised to be consistent with the applicability for this function (above P-9 or 50 % RTP). The TS require that surveillances be performed prior to the Mode of Applicability. The current TS frequency of this surveillance "S/U" (meaning reactor startup) does not clearly state the performance requirement for a function with an applicability of above 50% RTP. Therefore, the frequency of the corresponding VEGP ITS SR 3.3.1.16 is revised to "After each Mode 3 entry for unit shutdown and prior to exceeding the P-9 interlock trip setpoint." This revision is intended as a clarification and is consistent with the intent of the original surveillance frequency and with the Applicability of the instrument function (above P-9). Therefore the revision of this frequency is considered an administrative change.

51 A The VTS Note 4 to exclude neutron detectors from the Channel Calibration is incorporated into the ITS SR 3.3.1.11. This change is considered administrative and is consistent with NUREG-1431.

> A The VTS Note 7 that modifies the frequency of the applicable surveillances, is incorporated into the frequency for ITS SR 3.3.1.4 and SR 3.3.1.5. In addition, since the definition of Staggered Test Basis has been revised the test frequency is now stated as 31 days on a staggered test basis instead of 62 days on a staggered test basis. The actual test frequency for a given channel is not changed. Only the definition of staggered test basis has changed. This change is considered administrative and is consistent with NUREG-1431.

52

3/4.3.1 RTS INSTRUMENTATION

CHANGE NUMBER	<u>SHE</u>	DISCUSSION
53	LG	Note 11 that provides descriptive information regarding the content of the required test is moved into the Bases discussion for the corresponding ITS TADOT SR 3.3.1.4. This change is less restrictive due to the Bases being controlled by the licensee under the Bases Control Program in the Administrative Controls Section of the ITS. This change is consistent with NUREG-1431.
54	LG	Notes 15 and 16 that provide descriptive information regarding the content of the required test are moved to the bases for the applicable ITS SR. This change is less restrictive due to the Bases being controlled by the licensee under the Bases Control Program in the Administrative Controls Section of the ITS. This change is consistent with NUREG-1431.
55	А	A separate line item for the undervoltage and shunt trip mechanisms is provided in the ITS. The separation of these functions facilitates

3/4.3.3 MONITORING INSTRUMENTATION RADIATION MONITORING FOR PLANT OPERATIONS AND APPLICABLE ESFAS PAGES FOR NEW NUREG-1431 LCOS CONTAINMENT VENTILATION ISOLATION AND CONTROL ROOM EMERGENCY FILTRATION

CHANGE NUMBER	SHE		
		with the requirements of the NUREG-1431 LCO that now contains the setpoints.	
32		Not used.	
33	A	A specific SR is identified for Response Time Testing of the Control Room Emergency Filtration Function. This addition of a specific surveillance requirement for Response Time Testing is consistent with NUREG-1431 as the generic surveillance requirement of the current ESFAS TS for Response Time Testing is not used in the NUREG- 1431 format. Each instrument function has the required surveillances identified.	

APPLICABLE ESFAS PAGES FOR THE NEW NUREG-1431 LCO 3.3.5 ESF BUS LOSS OF POWER (LOP) INSTRUMENTATION

CHANGE NUMBER

13

14

SHE

At VEGP the loss of power instrument channels are similar to the protection channels used in the ESFAS and RTS, in that a processed signal from a sensor is used to trip an output bistable that inputs a signal to actuation logic and relays. Similar instrument channels in the ESFAS and RTS currently have quarterly ACOT requirements that have proven adequate, based on operating experience, to ensure operability. Furthermore, the sensors for the loss of power channels are potential transformers (not uv relays) and have no moving parts. The potential transformers are inherently more reliable than the pressure transmitters typically used in RTS and ESFAS instrument channels. The loss of power instrumentation channels at VEGP are at least as reliable as similar channels in the ESFAS and RTS that are tested quarterly. Therefore, a quarterly ACOT on the loss of power instrument channels is adequate to ensure their operability.

A A specific SR is identified for Response Time Testing of the AFW system initiation on the LOP Functions. This addition of a specific surveillance requirement for Response Time Testing is consistent with NUREG-1431 as the generic surveillance requirement of the current ESFAS TS for Response Time Testing is not used in the NUREG-1431 format. Each instrument function has the required surveillances identified.

LS23 The requirement to perform specific response time testing of the Loss of Power (LOP) instrumentation Diesel Generator start is deleted consistent with NUREG-1431 as modified by NRC-22 change package and marked-up on page 3/4 3-42 in Enc 1. The requirement for this testing is redundant to the response time tests performed for the ESF equipment including the Emergency Diesels (in LCO 3.8.1) and Auxiliary Feedwater pumps (SR 3.3.5.3) and the Channel Operational Tests and Channel Calibrations performed on the LOP instrumentation to verify the correct time delays and sensor operation. Note that the ESFAS surveillance requirement (4.3.2.2) for response time testing of the AFW system for LOP initiation is retained as SR 3.3.5.3 as marked

APPLICABLE ESFAS PAGES FOR THE NEW NUREG-1431 LCO 3.3.5 ESF BUS LOSS OF POWER (LOP) INSTRUMENTATION

CHANGE NUMBER SHE

on page 3/4 3-41 in Enc 1. The LOP response time SR for the AFW system initiation is retained consistent with the verification of the VEGP safety analyses assumptions for AFW system initiation with and without offsite power.

The following pages replace the corresponding pages behind the Enclosure 3 tab for Chapter 3.3, Volume 3.

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IV. SPECIFIC SIGNIFICANT HAZARDS EVALUATIONS LCO 3.3.5 ESF BUS LOSS OF POWER (LOP) INSTRUMENTATION "LS23"

The requirement to perform specific response time testing of the Loss of Power (LOP) instrumentation Diesel Generator start is deleted consistent with NUREG-1431 as modified by NRC-22 change package and marked-up on page 3/4 3-42 in Enc 1. The requirement for this testing is redundant to the response time tests performed for the ESF equipment including the Emergency Diesels (in LCO 3.8.1) and Auxiliary Feedwater pumps (SR 3.3.5.3) and the Channel Operational Tests and Channel Calibrations performed on the LOP instrumentation to verify the correct time delays and sensor operation. Note that the ESFAS surveillance requirement (4.3.2.2) for response time testing of the AFW system for LOP initiation is retained as SR 3.3.5.3 as marked on page 3/4 3-41 in Enc 1. The LOP response time SR for the AFW system initiation is retained as SR 3.3.5.3 as marked on page 3/4 3-41 in Enc 1. The LOP response time SR for the AFW system initiation is retained with the verification of the VEGP safety analyses assumptions for AFW system initiation with and without offsite power.

1. Does the change involve a significant increase in the probability or consequences of an accident previously evaluated?

The proposed change involves changing the TS surveillance requirements for the ESF Bus Loss of Power Instrumentation to more closely agree with the Westinghouse Standard ITS (NUREG-1431) and does not result in any hardware changes. The Loss of Power Instrumentation is not assumed to be an initiator of any analyzed event. The role of the Loss of Power Instrumentation is to monitor and ensure an adequate voltage is maintained on the ESF Busses as well as providing an anticipatory start of the Auxiliary Feedwater Pumps. The proposed change still ensures the Loss of Power instrumentation remains capable of providing the required monitoring and actuation functions as described in the FSAR and that the results of the analyses in the FSAR remain bounding. Additionally, the proposed change does not impose any new safety analyses limits or alter the plants ability to detect and mitigate events. Therefore, this change does not involve a significant increase in the probability or consequences of an accident previously

2. Does the change create the possibility of a new or different kind of accident from any accident previously evaluated?

The proposed change involves changing the TS requirements for the Loss of Power Inst.umentation to more closely agree with the Westinghouse Standard ITS (NUREG-1431) requirements and does not necessitate a physical alteration of the plant (no new or different type of equipment will be installed) or changes in parameters governing normal plant operation. Thus, this change does not create the possibility of a new or different kind of accident from any accident previously evaluated.

3. Does this change involve a significant reduction in a margin of safety?

The proposed change, which revises the TS requirements for the Loss of Power Instrumentation to be consistent with the Westinghouse Standard ITS (NUREG-1431) requirements does not involve a significant reduction in a margin of safety. The proposed change still requires the Loss of Power Instrumentation to be operable and ensures the monitoring and actuation capability of the instrumentation is available when necessary to assist in the mitigation of accidents. In addition, the proposed change eliminates duplicative testing requirements. As such, any reduction in the margin of safety is insignificant and will likely be offset by the benefit gained through the improved use of utility resources. The following pages replace the corresponding pages behind the Enclosure 4a tab for Chapter 3.3, Volume 3.

SURVEILLANCE REQUIREMENTS (continued) SURVEILLANCE FREQUENCY SR 3.3.1.14 ---NOTE-----15 Verification of setpoint is not required. 18% months Perform TADOT. SR 3.3.1.15 ----NOTE--------NOTE----2. Verification of setpoint is not require. Only required (15) when not performed 27 within previous 31 days Perform TADOT. Prior to reactor startup 15 3.3.1.16 SR ----NOTE-----15 Neutron detectors are excluded from response time testing. Verify RTS RESPONSE TIME is within limits. 0180 months on a STAGGERED TEST BASIS SR 3.3.1.16 1. Only required when not performed within previous 31 days. 29 2. Verification of setpoint is not required. After each MODE 3 entry for unit shutdown and prior to exceeding the P-9 interlock of trip setpoint Perform COT. -W00 STE 3.3-12 Rev. 0, 09/28/92 Vogtle Units land 2

	FUNCTION	APPLICABLE MODES OR OTHER SPECIFIED CONDITIONS	REQUIRED	COMDITIONS	SURVETLLANCE REQUIREMENTS	ALLOMABLE	TRIP SETPOINT
03	Continuent Sump Continuent Sump (continued)		anan ber di seta - diasa ana				>
٤.	RUST Level -Law Low	1,2,3,6	•	ĸ	SR 3.3.2.1 SR 3.3.2.5 SR 3.3.2.5 SR 3.3.2.10	A 11512	a (18)%
	Coincident with Sefety Injection	Refer to Fue functions en	ection 1 (Sa	Her Injectio	n) for ell initi	ation	
	end						
3	Coincident with Containment Sump Interni -High	1,2,3,4	4	ĸ	SR 3.3.2.1 SR 3.3.2.5 SR 3.3.2.9 SR 3.3.2.10	2 1500 in. above el. (703) ft	2 () in. above el. []ft
. ESF	FAS Interlocks		dilangin likerang saar				
*.	Reactor Trip, P-6	1,2,3	1 per train, 2 trains	r.M	SR 3.3.2.719		-
b.	Pressurizer Pressure, P-11	1,2,3	3	29	H 3.3.2.4.4 H 3.3.2.4.4	20/0 \$ (1996)- p\$10	2000 5 444 paig
¢.	Tere -LOW LOW, Pot2-	4,8,3	(1) per toop	L	SR 3.3.2.1 SR 3.3.2.5 SR 3.3.2.9	E (550.6)*F	2 (553) °F
d.	SG Water	1.2	(3) per	N	SR 3.3.2.1		5 (82.4)2

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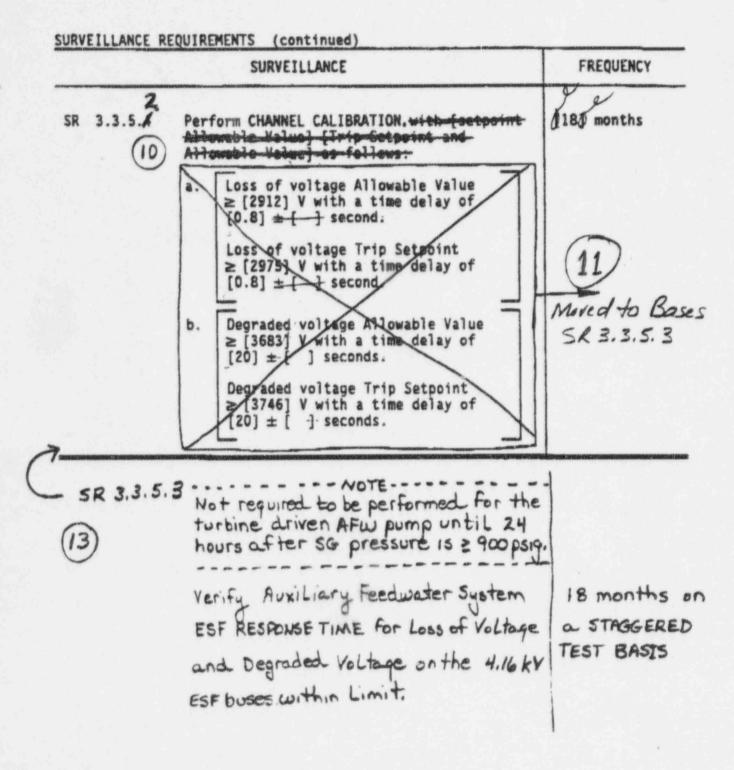
Rev. 0, 09/28/92

ESFAS Instrumentation

3.3.2

LOP DG-Start Instrumentation 3.3.5

TO



Rev. 0, 09/28/92

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CREFS Actuation Instrumentation 3.3.7

and the same of th	SURVEILLANCE	FREQUENCY
SR 3.3.7.3	Perform ACTUATION LOGIC TEST.	31 days on a STAGGERED TEST BASIS
5R 3.3.7.4 1 ^{/B} veg?		21 days on a STAGGERED TEST BASIS
67 3.5.7.9	N/A VEGP	- { 82} days -
4 SR 3.3.7.∮	VERIFICATION OF DEPROINTIS NOT REGUINED.	2188 months
SR 3.3.7.X	Perform CHANNEL CALIBRATION.	a 180 months
SR 3.3.7.6	Verify ESF RESPONSE TIME for radio- gas monitors within Limit.	18 months on a staggered test basis.
	(7)	

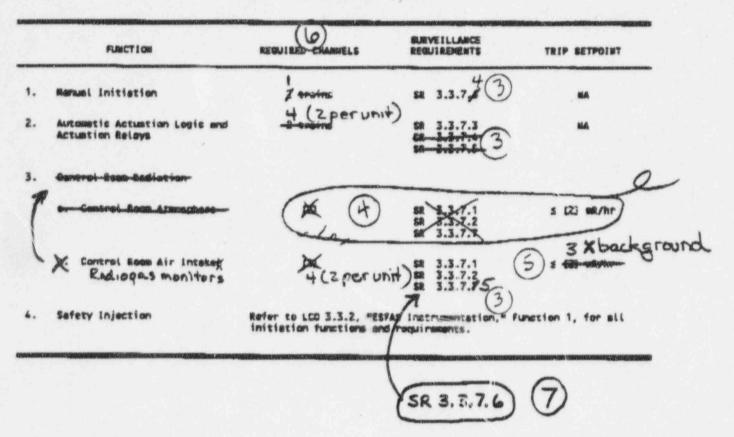
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CREFS Actuation Instrumentation 3.3.7

Table 3.3.7-1 (page 1 of 1) CREFS Actuation Instrumentation

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Rev. 0, 09/28/92

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The following pages replace and supplement the existing pages behind the Enclosure 4b tab for Chapter 3.3, Volume 3.

14

INSERT FOR PAGE B 3.3-58 (RTS)

SR 3.3.1.16

SR 3.3.1.16 is the performance of a COT for the low fluid oil pressure portion of the Turbine Trip Functions as described in SR 3.3.1.7 except that the Frequency is after each entry into MODE 3 for a unit shutdown and prior to exceeding the P-9 interlock trip setpoint. The surveillance is modified by two Notes. Note 1 states that the surveillance may be satisfied if performed within the previous 31 days. Note 2 states that verification of the setpoint is not required. The Frequency ensures that the turbine trip on low fluid oil pressure channels is OPERABLE after each unit shutdown and prior to entering the Mode of Applicability (above the P-9 power range neutron flux interlock) for this instrument function.

SURVEILLANCE	SR 3.3.1. (continued)	
REQUIREMENTS	verification that the trip occurs within the requindelay, as the in formation of the second s	red time
	A CHANNEL CALIBRATION is performed every 0180 month approximately at every refueling. CHANNEL CALIBRAT complete check of the instrument loop, including th The test verifies that the channel responds to a me parameter within the necessary range and accuracy.	TION is a ne sensor
	The Frequency of (180) months is based on operating experience and consistency with the typical industry refueling cycle and is justified by the assumption (180) month calibration interval in the determination magnitude of equipment drift in the setpoint analys	of an on of the
REFERENCES	1. FSAR, Section 8.38. 2. FSAR, Chapter 0150.	scussion
PSC	3. Unit Specific RTS/ESFAS Setpoint Methodology 5 4. Technical Requirements Manual, Section 15, "Ro Times." 3. FSAR, Chapter 16.	
The setopio:	ts are as follows:)
		1
≥29	of voltage Allowable Value 12 V with a time delay of 5 0.8 second	
229;	of voltage Trip Setpoint 15 V with a time delay of \$ 0.8 second	G
b. Deg.	rocled bltage Allowable Value	(75
23	683 V with a time delay of 5 20 seconds	

INSERT SR 3.3.5.3 RESPONSE TIME TEST BASES DISCUSSION ON PAGE B 3.3-150 OF ESF LOSS OF POWER TS BASES

SR 3.3.5.3

This SR ensures the individual channel ESF RESPONSE TIMES with and without offsite power for the AFW System are less than or equal to the maximum values assumed in the accident analysis. Response Time testing acceptance criteria are included in the FSAR, Chapter 16 (Ref. 3). Individual component response times are not modeled in the analyses. The analyses model the overall or total elapsed time, from the point at which the parameter exceeds the Trip Setpoint value at the sensor, to the point at which the equipment in both trains reaches the required functional state (e.g., pumps at rated discharge pressure, values in full open or closed position).

For channels that include dynamic transfer functions (e.g., lag, lead/lag, rate/lag, etc.), the response time test may be performed with the transfer functions set to one with the resulting measured response time compared to the appropriate FSAR response time. Alternately, the response time test can be performed with the time constants set to their nominal value provided the required response time is analytically calculated assuming the time constants are set at their nominal values. The response time may be measured by a series of overlapping tests such that the entire response time is measured.

ESF RESPONSE TIME tests are conducted on an 18 month STAGGERED TEST BASIS. Testing of the final actuation devices, which make up the bulk of the response time, is included in the testing of each channel. The final actuation device in one train is tested with each channel. Therefore, staggered testing results in response time verification of these devices every 18 months. The 18 month Frequency is consistent with the typical refueling cycle and is based on unit operating experience, which shows that random failures of instrumentation components causing serious response time degradation, but not channel failure, are infrequent occurrences.

This SR is modified by a Note that clarifies that the turbine driven AFW pump is tested within 24 hours after reaching 900 psig in the SGs.

NOU-06-1995 12:21 FROM VOGTLE TECH. SUPPORT SNC ENG/LIC P.09 TO CREFS Actuation Instrumentation 8 3.3.7 BASES SR 3.3.7 SURVEILLANCE REQUIREMENTS A CHANNEL CALIBRATION is performed every \$18\$ months, or (continued) approximately at every refueling. CHANNEL CALIBRATION is a complete check of the instrument loop, including the sensor. The test verifies that the channel responds to a measured parameter within the necessary range and accuracy. The Frequency is based on operating experience and is consistent with the typical industry refueling cycle. WCAP-10271-P A, Supplement 2, Rev 1, June 1990, WOG-25-10 REFERENCES 1. Westinghoose to SCS Letter BBGP-G-0025, dated May 23, 1988. Trensmittal of PMTC FSAR charges. 2. VEGP CALCULATION NO. X6CNA.09.01, Control Room HVAC Technical Specifications, 21 october, 1988. 3. FSAR, Chapter 16 INSERT SR 3.3.7.6 Barer discusion

INSERT SR 3.3.7.6 RESPONSE TIME TEST BASES DISCUSSION ON PAGE B 3.3-168 OF CREFS ACTUATION INSTRUMENTATION TS BASES

SR 3.3.7.6

This SR ensures the individual channel ESF RESPONSE TIME for the CREFS radiogas monitor actuation instrumentation is less than or equal to the maximum values assumed in the accident analysis. Response Time testing acceptance criteria are included in the FSAR, Chapter 16 (Ref. 3). Individual component response times are not modeled in the analyses. The analyses model the overall or total elapsed time, from the point at which the parameter exceeds the Trip Setpoint value at the sensor, to the point at which the equipment in both trains reaches the required functional state (e.g., pumps at rated discharge pressure, values in full open or closed position).

For channels that include dynamic transfer functions (e.g., lag, lead/lag, rate/lag, etc.), the response time test may be performed with the transfer functions set to one with the resulting measured response time compared to the appropriate FSAR response time. Alternately, the response time test can be performed with the time constants set to their nominal value provided the required response time is analytically calculated assuming the time constants are set at their nominal values. The response time may be measured by a series of overlapping tests such that the entire response time is measured.

ESF RESPONSE TIME tests are conducted on an 18 month STAGGERED TEST BASIS. Testing of the final actuation devices, which make up the bulk of the response time, is included in the testing of each channel. The final actuation device in one train is tested with each channel. Therefore, staggered testing results in response time verification of these devices every 18 months. The 18 month Frequency is consistent with the typical refueling cycle and is based on unit operating experience, which shows that random failures of instrumentation components causing serious response time degradation, but not channel failure, are infrequent occurrences. The following pages replace and supplement the existing pages behind the Enclosure 5 tab for Chapter 3.3, Volume 3.

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VEGP ITS Conversion Enclosure 5 - Justifications for Differences from NUREG-1431 Chapter 3.3 -Instrumentation

	LCO 3.3.2 ESFAS
CHANGE NUMBER	JUSTIFICATION
26	The format of the Note modifying Conditions C, D, E, G, H, I, and K was corrected to show that it modifies all the Required Actions.
27	The frequency of SR 3.3.2.9 is revised to 18 months from once per reactor trip breaker cycle consistent with current licensing basis.
28	A Note is added to the Mode of Applicability for Function 7a "Semi- Automatic Switchover to Containment Sump, Automatic Actuation Logic and Actuation Relays". The new Note (h) requires only one train of actuation logic and relays to be operable in Mode 4. This change is consistent with the requirement in LCO 3.5.3 for only one train of RHR to be operable in this Mode. This change provides consistency between the instrument and system LCOs.
29	The NUREG-1431 requirement for a Channel Check of the Pressurizer Pressure P-11 ESFAS function on Table 3.3.2-1 is deleted. This Channel Check is not required by the current VEGP TS for the ESFAS P-11 function. The actual P-11 interlock function is verified operable by the performance of a 92-day COT and an 18-month Channel Calibration. The operation of the pressurizer pressure channels associated with the P-11 interlock are also confirmed operable by the Pressurizer Pressure reactor trip and SI function Channel Checks required by the RTS and ESFAS TS for the same channels. Therefore, the Channel Check of the interlock status lights required by NUREG-1431 has no impact on the reliability or operability of the P-11 interlock at VEGP.

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VEGP ITS Conversion Enclosure 5 - Justifications for Differences from NUREG-1431 Chapter 3.3 -Instrumentation

LCO 3.3.5

LOSS OF POWER (LOP) DIESEL GENERATOR (DG) START INSTRUMENTATION

CHANGE NUMBER

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JUSTIFICATION

VEGP specific Trip Setpoint and Allowable Value. The revised surveillance is consistent with the current VEGP TS requirements.

Due to the complexity of the setpoints and allowable values for loss of and degraded voltage, this information will be moved to the Bases for SR 3.3.5.3.

12

11

The Note modifying Required Action A.1 would be revised to allow either the inoperable channel or the channel to be tested to be bypassed for surveillance testing of the remaining operable channels. The net effect is the same. If the inoperable channel is bypassed, the operable channel must be tested in trip. If the operable channel is tested while it is bypassed, the inoperable channel must remain in trip. Either way, one channel will be bypassed and one channel will be in trip. The existing VEGP TS currently provide for this. Therefore, the proposed change is consistent with current licensing basis.

13

At VEGP the Loss of Power instrumentation actuates the Auxiliary Feedwater pumps as well as the Diesel Generator. The Loss of Voltage and Degraded Voltage AFW Functions were moved from the ESFAS TS into the proposed ESF Bus Loss of Power TS to consolidate the functions performed by this instrumentation. Generic change NRC-022-C1 deleted the response time testing requirement (NUREG-1431 SR 3.3.5.3) for the Emergency Diesel Generator on loss of voltage and degraded voltage signals. However, the VEGP safety analyses include assumptions for the AFW system response to automatic start signals with and without offsite power available. The VEGP FSAR (Table 16.3-2) contains an explicit line item for the AFW system response to both loss of voltage and degraded voltage on the ESF buses. In addition, the current ESFAS TS contains an SR for response time testing this instrument function. Therefore, a VEGP specific SR 3.3.5.3 to verify the AFW system response time to loss of voltage and degraded voltage on the 4.16 kV ESF buses is

VEGP ITS Conversion Enclosure 5 - Justifications for Differences from NUREG-1431 Chapter 3.3 -Instrumentation

LCO 3.3.5

LOSS OF POWER (LOP) DIESEL GENERATOR (DG) START INSTRUMENTATION

CHANGE NUMBER

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JUSTIFICATION

added to the ESF Bus Loss of Power TS. The proposed SR is the equivalent of the Current TS ESFAS response time test requirement (4.3.2.2) that applies to the current AFW Loss of Voltage and Degraded Voltage Functions in the ESFAS TS. The proposed SR also includes a Note that allows a delay in testing the turbine-driven AFW pump until steam generator pressure reaches an appropriate value for operating the pump. The Note in proposed SR 3.3.5.3 is consistent with the Note in the NUREG-1431 ESFAS TS for other AFW response time testing.

VEGP ITS Conversion Enclosure 5 - Justifications for Differences from NUREG-1431 Chapter 3.3 - Instrumentation

LCO 3.3.7 CONTROL ROOM EMERGENCY FILTRATION SYSTEM (CREFS)

CHANGE NUMBER

JUSTIFICATION

7

A VEGP specific SR for response time testing the radiogas monitor actuation instrumentation has been added to the Improved CREFS TS. The radiogas monitors are required to actuate CREFS for a fuel handling accident in the fuel handling building. The analysis associated with this postulated event assumes a response time which includes the radiogas monitor actuation. The CREFS radiogas monitors are specified in the current VEGP ESFAS TS which has a surveillance requirement for response time testing. The addition of this SR to the Improved CREFS TS is consistent with the surveillance requirement (4.3.2.2) in the current VEGP ESFAS TS. The following page replaces the corresponding page behind the Enclosure 4b tab for Chapter 3.7, Volume 6. NOU-06-1995 12:24 FROM VOGTLE TECH. SUPPORT

TO

AFW System B 3.7.5

BASES (continued)

DSE TURVEILLANCE SR 3.7.5.1 REQUIREMENTS Verifying the correct alignment for manual, power operated. The correct position and automatic valves in the AFW System water and steam is the position of the supply flow paths provides assurance that the proper flow valves necessary paths will exist for AFW operation. This SR does not apply to valves that are locked, sealed, or otherwise secured in to support the position, since they are verified to be in the correct operational needs position prior to locking, sealing, or securing. This SR of the plant at also does not apply to valves that cannot be inadvertently that time, including misaligned, such as check valves. This Surveillance does not require any testing or valve manipulation; rather, it during low power operation and involves verification that those valves capable of being provided that the mispositioned are in the correct position. The 31 day Frequency is based on engineering judgment, is requirements of the consistent with the procedural controls governing valve Technical Specification operation, and ensures correct valve positions. safety analysis are met. 0 SR 3.7.5.2 NRC-13-CI-RI This SR verifies that the AFW pumps develop sufficient discharge pressure to deliver the required flow at the full open pressure of the MSSVs. Because it is undesirable to INSERT -> introduce cold AFW into the steam generators while they are operating, this testing is performed on recirculation flow. Periodically comparing the reference differential pressure developed at this reduced flow detects trends that might be indicative of incipient failure. Performance of inservice testing discussed in the ASME Code, Section XI (Ref. 2) (only required at 3 month intervals) satisfies this requirement. The [31] day Frequency on a STAGGERED TEST BASIS results in testing each pump once every 3 months, as required by Reference 2. This SR is modified by a Note indicating that the SR should

be deferred until suitable test conditions are established. This deferral is required because there is insufficient steam pressure to perform the test.

SR_3.7.5.3

This SR verifies that AFW can be delivered to the appropriate steam generator in the event of any accident or

(continued)

WOG STS

Rev. 0, 09/28/92