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February 28, 1992

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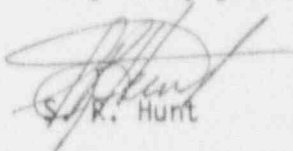
Gentlemen:

Subject: VIRGIL C. SUMMER NUCLEAR STATION
DOCKET NO. 50/395
OPERATING LICENSE NO. NPF-12
SEMI-ANNUAL EFFLUENT AND WASTE
DISPOSAL REPORT (SA 300)

Enclosed is the South Carolina Electric & Gas Company (SCE&G) Semi-Annual Effluent and Waste Disposal Report as required by 10CFR50.36a and Sections 6.9.1.8 and 6.14.2 of the Virgil C. Summer Nuclear Station Technical Specifications.

Should there be any questions, please contact us at your convenience.

Very truly yours,



S. R. Hunt

CJM:SRH:lcd
Enclosure

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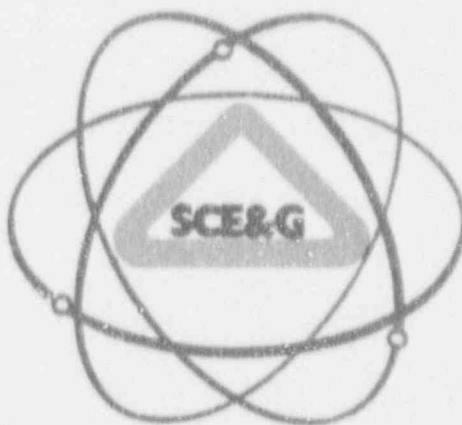
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SEMIANNUAL EFFLUENT AND WASTE DISPOSAL REPORT

FOR THE OPERATING PERIOD
July 1, 1991 - December 31, 1991

February 28, 1992



V. C. SUMMER NUCLEAR STATION
SOUTH CAROLINA ELECTRIC AND GAS COMPANY

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*Virgil C. Summer Nuclear Station
South Carolina Electric & Gas*

This report is being submitted as a summary of quantities of radioactive liquid and gaseous effluents and solid waste released from the Virgil C. Summer Nuclear Station. This report satisfies the requirements in Sections 6.9.1.8 and 6.14.2 of Technical Specifications, Section 1.6.2 of the Offsite Dose Calculation Manual (ODCM), and 10CFR50.36(a). Also included is an assessment of radiation doses from plant releases.

A brief discussion of the Supplemental Information and Tables 2 through 6 is presented in Sections A through D. An evaluation of the radiological impact on man due to operation of the Virgil C. Summer Nuclear Station is presented in Section E and Table 1. A summary of the meteorological data for 1991 is presented in Section F and Tables 7 and 8. Changes made to the Offsite Dose Calculation Manual are noted in Section G.

A. Supplemental Information

Regulatory limits for doses and maximum permissible concentrations presented in Supplemental Information are from the Virgil C. Summer Nuclear Station Technical Specifications and 40 CFR 190. Average energy (\bar{E}) is not applicable to the method for determining release rate limits for fission and activation gaseous effluents; therefore, it has been omitted.

B. Gaseous Effluents

Gaseous effluents released from ground level are summarized in Tables 2 and 3. An elevated release pathway does not exist at Virgil C. Summer Nuclear Station. Cumulative doses are discussed in Section E.

The errors for gaseous effluent totals are given as the square root of the sum of squares of counting errors and flow or volume measurement errors. A systematic error of 15% has been added to estimate total error.

C. Liquid Effluents

Liquid effluents are summarized in Tables 4 and 5. Estimated total errors are expressed as in Section B above.

D. Solid Waste Shipments

Solid waste shipments are summarized in Table 6. Curie content of radioactive waste packages is determined by dose rates and/or analysis of samples by gamma spectroscopy. The total error for each type of Curie content determination is conservatively estimated to be the sum of a 15% systematic error and a 20% photon response error for the detector used.

E. Radiological Impact on Man

Potential doses to the maximum exposed individual in the unrestricted area were calculated using measured plant gaseous effluent and meteorological data in accordance with the Offsite Dose Calculation Manual. The source term involved four (4) waste gas decay tank (WGDT) releases, 19.8 days and 46.3 days

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of Reactor Building purge releases through the 6-inch and 36-inch purge lines, respectively, and a continuous six month main plant vent release. Doses are summarized in Table 1. The total activities released are presented in Tables 2 and 3. Air doses to the maximum exposed individual due to noble gases were $2.51E-2$ and $6.77E-2$ mrad for gamma and beta, respectively. The maximum organ dose attributed to the releases was $3.84E-3$ mrem for the six month period. Cumulative annual doses were $3.03E-2$ mrad, $8.05E-2$ mrad and $7.57E-3$ mrem for gamma, beta and organ dose, respectively.

Measured plant liquid effluent data was used to calculate estimates of doses to individuals in accordance with the Offsite Dose Calculation Manual. The source term consisted of the isotopic contents of 246 Waste Monitor Tank batch releases and continuous Turbine Building Sump and Steam Generator Blowdown† releases. Doses are summarized in Table 1 and total radioactivity released is described in Tables 4 and 5. The total body dose to the maximally exposed individual due to the release of radioactive liquid was $2.98E-2$ mrem. The maximum organ dose was $4.70E-2$ mrem to the thyroid during the six month period. Cumulative annual doses for the hypothetical maximally exposed individual were $7.47E-2$ mrem and $1.05E-1$ mrem for the total body and thyroid (maximum annual organ), respectively.

Radiation doses from nearby uranium fuel cycle sources were not assessed. The ODCM, Sections 1.3.1 and B/1.3 establish a five (5) mile limit beyond which doses from nearby plants are insignificant. There are no uranium fuel cycle plants within a five (5) mile radius of Virgil C. Summer Nuclear Station.

Radiation doses from radioactive effluents to members of the public due to their activities inside the site boundary were assessed in a manner different from that in the Offsite Dose Calculation Manual. Monthly thermoluminescent dosimetry data from eight (8) monitoring locations within the site boundary and ten (10) locations around the site boundary perimeter were analyzed and compared with respective pre-operational background and previous year history. Results showed that 1991 monthly dose rates did not differ significantly from the pre-operational or 1990 dose rates. It was concluded that doses to members of the public inside the site boundary were indistinguishable from normal background dose.

Radiation doses from radioactive effluents to workers at the Fairfield Hydro Station were calculated to be $3.43E-3$ and $9.24E-3$ mrad for gamma and beta, respectively. Annual cumulative doses were $4.14E-3$ and $1.10E-2$ mrad, respectively.

†Note: No releases were made through Steam Generator Blowdown 9/22 - 11/13/91 (outage) and 11/27 - 12/1, 12/6 - 12/16 and 12/17 - 12/31/91 (blowdown recovered through the condenser).

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Table 1
GASEOUS AND LIQUID DOSES

ODCM Section	Gaseous Limits	Third Quarter, 1991		Fourth Quarter, 1991	
		Dose	Percent of Limit	Dose	Percent of Limit
1.2.3.1a,b	5 mrad gamma/qtr. 10 mrad gamma/yr.	2.24E-2 mrad	4.48E-1 2.76E-1*	2.66E-3 mrad	5.31E-2 3.03E-1*
		(July - December total gamma air dose: 2.51E-2 mrad) (January - December total gamma air dose: 3.03E-2 mrad)			
1.2.3.1a,b	10 mrad beta/qtr. 20 mrad beta/yr.	5.97E-2 mrad	5.97E-1 3.62E-1*	8.03E-3 mrad	8.03E-2 4.02E-1*
		(July-December total beta air dose: 6.77E-2 mrad) (January-December total beta air dose: 8.05E-2 mrad)			
1.2.4.1a,b	7.5 mrem organ/qtr. 15 mrem organ/yr.	2.49E-3 mrem	3.33E-2 4.15E-2*	1.35E-3 mrem	1.80E-2 5.05E-2*
		(July-December maximum exposed organ dose: 3.84E-3 mrem) (January-December maximum exposed organ dose: 7.57E-3 mrem)			

Liquid Limits

1.1.3.1a,b	1.5 mrem/qtr. 3.0 mrem/yr.	1.78E-2 mrem	1.19E0 2.09E0*	1.20E-2 mrem	7.98E-1 2.49E0*
		(July-December whole body dose: 2.98E-2 mrem) (January-December whole body dose: 7.47E-2 mrem)			
1.1.3.1a,b	5 mrem organ/qtr. 10 mrem organ/yr.	4.54E-2 mrem	9.09E-1‡ 1.04E0*†	1.55E-2 mrem	3.09E-1‡ 1.05E0*†
		(July-December maximum exposed organ dose: 4.70E-2 mrem)‡ (January-December maximum exposed organ dose: 1.05E-1 mrem)†			

* Includes contribution from previous quarters.

‡ Maximum exposed organ for quarter 3 and the 6 months was the thyroid; for quarter 4, the liver.

† Maximum exposed organs cumulative for quarters 1-3 and 1-4 was the thyroid.

Dose rates and concentrations were below the limits specified in Supplemental Information, Section 2a, b and c during all the effluent releases.

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F. Meteorology

The meteorology data for 1991 is summarized in Table 7 by quarter. The data are shown as joint frequency distributions of wind direction and speed by atmospheric stability class. Table 8 provides the same information for those hours during which batch releases occurred. There were no batch releases during the second quarter.

The wind direction and wind speed data used in the summary were acquired from the 10 meter level of the primary monitoring tower. Stability was determined by the primary differential temperature (61 to 10 meter) when available. In the event primary differential temperatures were unavailable, 40 to 10 meter differential temperatures were substituted.

The combined annual data recovery for wind direction, wind speed, and stability was 97.3%. Data recovery rates for specific parameters were as follows: wind direction (10m) - 97.7%, wind speed (10 m) - 97.7%, and differential temperature (61 - 10m) - 97.9%. The wind direction (61m), wind speed (61m), and differential temperature (40 - 10m) recovery rates were 95.8%, 97.5% and 97.0%, respectively.

G. Offsite Dose Calculation Manual

The Virgil C. Summer Nuclear Station (VCSNS) Offsite Dose Calculation Manual (ODCM) was revised once (Rev. 16) during the affected six month period. A copy of the manual including the revision is included as Attachment I.

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Supplemental Information

1. Regulatory Limits:

a. Fission and Activation Gases:

The air dose to an individual due to noble gases released in gaseous effluents shall be limited to less than or equal to 5 mrad for gamma radiation and 10 mrad for beta radiation during any calendar quarter and 10 mrad for gamma radiation and 20 mrad for beta radiation during any calendar year (ODCM, Section 1.2.3.1).

b. Iodines, Particulates (half-lives > 8 days) and Tritium:

The dose to an individual from radioiodines, tritium and radioactive materials in particulate form with half-lives greater than 8 days in gaseous effluents shall be limited to less than or equal to 7.5 mrem to any organ during any calendar quarter and 15 mrem to any organ during any calendar year (ODCM, Section 1.2.4.1).

c. Liquid Effluents:

The dose or dose commitment to an individual from radioactive materials in liquid effluents released shall be limited to less than or equal to 1.5 mrem to the total body and 5 mrem to any organ during any calendar quarter and 3 mrem to the total body and 10 mrem to any organ during any calendar year (ODCM, Section 1.1 3.1).

d. All Sources:

The annual dose equivalent shall not exceed 25 mrem to the whole body, 75 mrem to the thyroid and 25 mrem to any other organ (40 CFR 190).

2. Maximum Permissible Concentrations:

a. Fission and Activation Gases:

The dose rate in unrestricted areas due to radioactive materials released in gaseous effluents shall be limited to less than or equal to 500 mrem/year to the total body and less than or equal to 3000 mrem/year to the skin (ODCM, Section 1.2.2.1).

b. Iodines, Particulates (half-lives > 8 days) and Tritium:

The dose rate in unrestricted areas due to radioactive materials in effluents shall be limited to less than or equal to 1500 mrem/year to any organ (ODCM, Section 1.2.2.1).

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c. Liquid Effluents:

The concentration of radioactive materials released from the site shall be limited to the concentrations specified in 10 CFR 20, Appendix B, Table II, Column 2 for radionuclides other than dissolved or entrained noble gases. For dissolved or entrained noble gases, the concentration shall be limited to $2E-4$ $\mu\text{Ci/ml}$ total activity (ODCM, Section 1.1.2.1).

3. Average Energy:

Not Applicable

4. Measurements and Approximations of Total Radioactivity:

- a. Fission and activation gases: Gamma spectrometry [Ge(Li) or HPGe]
- b. Iodines: Gamma spectrometry [Ge(Li) or HPGe]
- c. Particulates: Gamma spectrometry [Ge(Li) or HPGe], beta proportional counting, alpha proportional counting
- d. Tritium: Liquid scintillation
- e. Liquid effluents: Gamma spectrometry [Ge(Li) or HPGe], liquid scintillation (H-3), beta proportional counting, alpha proportional counting

5. Batch Releases:

a. Liquid:

- 1. Number of batch releases:
156 for third quarter, 1991
90 for fourth quarter, 1991
- 2. Total time period for batch releases:
1.18E + 4 min. for third quarter, 1991
6.57E + 3 min. for fourth quarter, 1991
- 3. Maximum time period for a batch release:
9.70E + 1 min. for third quarter, 1991
9.10E + 1 min. for fourth quarter, 1991

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4. Average time period for batch releases:
7.59E + 1 min. for third quarter, 1991
7.30E + 1 min. for fourth quarter, 1991
 5. Minimum time period for a batch release:
4.70E + 1 min. for third quarter, 1991
3.60E + 1 min. for fourth quarter, 1991
 6. Average stream flow during periods of release of effluent into a flowing stream:
3.90E + 6 gpm for third quarter, 1991
3.36E + 6 gpm for fourth quarter, 1991
- b. Gaseous:
1. Number of batch releases: 4
 2. Total time period for batch releases: 1.50E + 3 min.
 3. Maximum time period for a batch release: 5.25E + 2 min.
Average time period for a batch release: 3.76E + 2 min.
 5. Minimum time period for a batch release: 2.40E + 2 min.
6. Abnormal Releases:
- a. Gaseous:
1. Number of releases: 0
 2. Total activity released: 0
- b. Liquid:
1. Number of releases: 0
 2. Total activity released: 0

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Table 2

GASEOUS EFFLUENTS-SUMMATION OF ALL RELEASES

		Third Quarter	Fourth Quarter	Est.Total Error, %
A. Fission & activation gases				
1. Total release	Ci	3.23E+2	4.52E+1	3.38E+1
2. Average release rate for period	μCi/sec	4.06E+1	5.69E+0	
3. Percent of ODCM limit	%	*	*	
B. Iodines				
1. Total iodine-131	Ci	1.22E-4	6.56E-5	3.60E+1
2. Average release rate for period	μCi/sec	1.53E-5	8.26E-6	
3. Percent of ODCM limit	%	**	**	
C. Particulates				
1. Particulates with half-lives > 8 days	Ci	0	4.81E-5	3.32E+1
2. Average release rate for period	μCi/sec	0	6.05E-6	
3. Percent of ODCM limit	%	**	**	
4. Gross alpha radioactivity	Ci	0	0	
D. Tritium				
1. Total release	Ci	1.09E-1	0	2.65E+1
2. Average release rate for period	μCi/sec	1.37E-2	0	
3. Percent of ODCM limit	%	**	**	

* Calculated as a percent of dose limits found in Supplemental Information, Section 1a. Third quarter values were 4.48E-1% and 2.76E-1% of the quarterly and cumulative annual gamma dose limits, respectively and 5.97E-1% and 3.62E-1% of the quarterly and cumulative annual beta dose limits, respectively. Fourth quarter values were 5.31E-2% and 3.03E-1% of the quarterly and cumulative annual gamma dose limits, respectively, and 8.03E-2% and 4.02E-1% of the quarterly and cumulative annual beta dose limits, respectively.

** Calculated as a percent of dose limits found in Supplemental Information, Section 1b. The sum of these values for the third quarter was 3.33E-2% and 4.15E-2% of the quarterly and cumulative annual organ dose limits, respectively. The sum of these values for the fourth quarter was 1.80E-2% and 5.05E-2% of the quarterly and cumulative annual organ dose limits, respectively.

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Table 3

GASEOUS EFFLUENTS-GROUND-LEVEL RELEASES

Nuclides Released	Unit	Continuous Mode		Batch Mode	
		Third Quarter	Fourth Quarter	Third Quarter	Fourth Quarter
1. Fission gases					
Krypton-85	Ci	0	0	3.32E-1	3.95E-1
Krypton-85m	Ci	9.12E-2	0	9.10E-5	0
Krypton-87	Ci	2.31E-3	0	0	0
Krypton-88	Ci	7.73E-2	0	0	0
Xenon-133	Ci	3.08E + 2	4.48E + 1	1.60E + 0	3.64E-3
Xenon-135	Ci	1.06E + 1	0	7.54E-3	0
Xenon-135m	Ci	0	0	0	0
Xenon-138	Ci	0	0	0	0
Others: Argon-41	Ci	2.20E-1	0	0	0
Xenon-131m	Ci	1.10E + 0	0	2.89E-2	4.13E-3
Xenon-133m	Ci	8.09E-1	0	1.34E-2	0
Unidentified	Ci	0	0	0	0
Total for period	Ci	3.21E + 2	4.48E + 1	1.98E + 0	4.03E-1
2. Iodines					
Iodine-131	Ci	1.22E-4	6.56E-5	0	0
Iodine-132	Ci	3.17E-5	7.15E-5	0	0
Iodine-133	Ci	2.08E-4	1.78E-6	0	0
Iodine-134	Ci	0	0	0	0
Iodine-135	Ci	0	0	0	0
Total for period	Ci	3.62E-4	1.39E-4	0	0
3. Particulates					
Strontium-89	Ci	0	0	0	0
Strontium-90	Ci	0	0	0	0
Cesium-134	Ci	0	0	0	0
Cesium-137	Ci	0	0	0	0
Barium-Lanth.-140	Ci	0	0	0	0
Others: Cr-51	Ci	0	1.20E-5	0	0
Mn-54	Ci	0	6.68E-7	0	0
Co-58	Ci	0	2.76E-5	0	0
Co-60	Ci	0	6.66E-6	0	0
Nb-95	Ci	0	1.14E-6	0	0
Cs-138	Ci	9.57E-3	0	0	0
Unidentified	Ci	0	0	0	0
Total for period	Ci	9.57E-3	4.81E-5	0	0

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Table 4

LIQUID EFFLUENTS - SUMMATION OF ALL RELEASES

		Third Quarter	Fourth Quarter	Est.Total Error, %
A. Fission & activation products				
1. Total release (not including tritium, gases, alpha)	Ci	2.26E-1	1.05E-1	1.92E + 1
2. Average diluted concentration during period	μCi/ml	3.61E-10	4.39E-10	
3. Percent of applicable limit	%	*	*	
B. Tritium				
1. Total release	Ci	2.29E + 2	6.52E + 1	1.84E + 1
2. Average diluted concentration during period	μCi/ml	3.65E-7	2.74E-7	
3. Percent of applicable limit	%	*	*	
C. Dissolved and entrained gases				
1. Total release	Ci	3.55E-1	3.59E-2	1.86E + 1
2. Average diluted concentration during period	μCi/ml	5.68E-10	1.51E-10	
3. Percent of applicable limit	%	*	*	
D. Gross alpha radioactivity				
1. Total release	Ci	0	0	N/A
E. Volume of waste released (prior to dilution)				
	liters	6.87E + 7	1.94E + 7	3.00E + 0
F. Volume of dilution water used during period				
	liters	6.25E + 11	2.38E + 11	4.30E + 0

* See following page.

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Table 4

LIQUID EFFLUENTS-SUMMATION OF ALL RELEASES

- * Calculated as a percent of dose limits found in Supplemental Information, Section 1c. The sum of these values for the third quarter was 1.19% and 2.09% of the respective quarterly and cumulative annual whole body dose limits and $9.09E-1\%$ and 1.04% of the respective quarterly and cumulative annual organ dose limits. The sum of these values for the fourth quarter was $7.98E-1\%$ and 2.49% of the respective quarterly and cumulative annual whole body dose limits and $3.09E-1\%$ and 1.05% of the respective quarterly and cumulative annual organ dose limits. Dose to the thyroid was the most limiting organ dose for the third quarter and to the liver for the fourth quarter of 1991. Dose to the thyroid was the most limiting for the year.

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 Table 5

LIQUID EFFLUENTS

†Nuclides Released	Unit	Continuous Mode		Batch Mode	
		Third Quarter	Fourth Quarter	Third Quarter	Fourth Quarter
Strontium-89	Ci	0	0	2.47E-4	7.41E-5
Strontium-90	Ci	0	0	4.98E-4	9.36E-5
Cesium-134	Ci	2.07E-3	1.05E-3	2.77E-4	4.02E-4
Cesium-137	Ci	8.75E-4	8.23E-4	2.92E-4	3.16E-4
Iodine-131	Ci	9.61E-3	3.46E-5	2.03E-3	1.64E-3
Cobalt-58	Ci	0	3.47E-4	2.14E-3	4.69E-2
Cobalt-60	Ci	0	2.11E-5	1.72E-2	1.32E-2
Iron-59	Ci	0	0	3.51E-4	9.34E-4
Zinc-65	Ci	0	0	2.66E-5	2.26E-4
Manganese-54	Ci	0	0	1.29E-3	1.90E-3
Chromium-51	Ci	0	0	1.66E-3	1.68E-2
Zirconium-Niobium-95	Ci	0	0	1.30E-4	4.63E-3
Molybdenum-99	Ci	2.17E-4	0	0	0
Technetium-99m	Ci	0	0	3.85E-5	3.57E-6
Barium-Lanth.-140	Ci	3.19E-5	0	8.33E-4	2.51E-4
Cerium-141	Ci	0	0	0	4.65E-5
Other: F-18	Ci	1.93E-2	1.48E-3	9.34E-5	2.41E-4
Na-24	Ci	0	9.18E-4	0	0
*Ni-56	Ci	0	0	0	4.88E-6
Co-57	Ci	0	0	3.01E-5	1.65E-4
Rb-88	Ci	0	0	0	3.61E-5
Ru-103	Ci	0	0	0	2.38E-4
Ru-106	Ci	0	0	2.27E-4	1.56E-4
Ag-110m	Ci	0	0	4.12E-5	1.03E-4
Sn-113	Ci	0	0	0	1.10E-4
*Sb-122	Ci	0	0	2.88E-4	1.71E-5
Sb-124	Ci	0	0	4.39E-4	4.95E-4
Sb-125	Ci	0	0	4.41E-3	7.14E-3
Sb-126	Ci	0	0	7.07E-5	1.59E-5
*Sb-127	Ci	0	0	2.16E-5	0
Te-132	Ci	0	0	9.54E-6	5.32E-5

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 Table 5 (continued)

LIQUID EFFLUENTS

†Nuclides Released	Unit	Continuous Mode		Batch Mode	
		Third Quarter	Fourth Quarter	Third Quarter	Fourth Quarter
I-132	Ci	3.26E-2	3.08E-4	1.18E-5	1.33E-4
I-133	Ci	4.49E-2	4.36E-4	9.50E-5	0
I-134	Ci	2.11E-2	4.63E-4	3.05E-6	0
I-135	Ci	5.63E-2	1.86E-4	3.25E-5	0
Cs-136	Ci	9.26E-5	0	0	3.98E-6
Cs-138	Ci	5.51E-3	1.10E-4	2.41E-5	3.84E-5
Ce-144	Ci	0	0	1.37E-4	1.31E-4
Unidentified	Ci	0	0	0	0
Total for period (above)	Ci	1.93E-1	6.17E-3	3.30E-2	9.85E-2
Xenon-133	Ci	2.48E-4	5.43E-5	3.45E-1	3.48E-2
Xenon-135	Ci	3.18E-3	0	1.66E-4	6.17E-5
Other: Ar-41	Ci	0	0	0	2.57E-6
Kr-85m	Ci	0	0	6.02E-6	4.50E-6
Kr-88	Ci	0	0	3.21E-6	0
Xe-131m	Ci	0	0	4.27E-3	7.87E-4
Xe-133m	Ci	0	0	2.76E-3	1.29E-4
Total entrained gases	Ci	3.43E-3	5.43E-5	3.52E-1	3.58E-2

† Tritium not included. See Table 4 for tritium numbers.

* Dose factors for these trace radionuclides are not included in the ODCM or Regulatory Guide 1.109, consequently the cumulative dose attributed to these isotopes is not reported. The quantity of these isotopes comprised only 1.3E-4% and 3.4E-5% of the total Curies released (including tritium) during the third and fourth quarter, respectively.

SEMIANNUAL EFFLUENT AND WASTE DISPOSAL REPORT

July - December, 1991

Table 6

SOLID WASTE AND IRRADIATED FUEL SHIPMENTS

A. Solid Waste Shipped Offsite for Burial or Disposal (Not irradiated fuel.)

1. Type of waste	Unit	6-month Period	E.T. Total Error, %	1991 Total
a. Spent resins, filter sludges, evaporator bottoms, etc.	m ³	1.97E + 1	3.50E + 1	2.88E + 1
	Ci	1.46E + 1		1.20E + 2
b. Dry compressible waste, contaminated equip., etc.	m ³	3.28E + 1	3.50E + 1	3.94E + 1
	Ci	4.42E + 1		4.45E + 1
c. Irradiated components, control rods, etc.	m ³	0	N/A	0
	Ci	0		0
d. Other (describe)	m ³	0	N/A	0
	Ci	0		0

2. Estimate of major nuclide composition for 6 month period (by type of waste)*

a. Cs-134	%	2.09E + 1
Cs-137	%	1.80E + 1
Ru-106	%	1.55E + 1
Co-58	%	1.11E + 1
Sr-90	%	1.05E + 1
Fe-55	%	6.18E + 0
Ni-63	%	5.64E + 0
Co-60	%	5.50E + 0
Nb-95 + Cr-51 + H-3	%	4.74E + 0
b. Fe-55	%	4.11E + 1
Co-60	%	1.99E + 1
Cs-137	%	1.39E + 1
Cs-134	%	8.32E + 0
Ni-63	%	6.92E + 0
Mn-54 + H-3 + Co-58	%	5.86E + 0
c. None	%	N/A
d. None	%	N/A

* All nuclides with concentrations above 1.0% are listed in descending order by activity level.

3. Solid Waste Disposition (6 month period)

Number of Shipments	Mode of Transportation	Destination
42† (6 mo.) / 59† (12 mo.)	Truck	Barnwell, SC

†Note: 33 (for the 6 month period) and 48 (for 1991 total) are partial shipments of DAW from waste processor to Barnwell, SC.

B. Irradiated Fuel Shipments (Disposition)

Number of Shipments	Mode of Transportation	Destination
None	N/A	N/A

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FIRST QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00

Stability Class: A delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- >24	>24		
N	0	1	0	0	0	0	1	4.39
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	1	0	1	21.29
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	1	0	0	0	0	1	6.56
SW	0	1	3	0	0	0	4	9.84
WSW	0	2	3	0	0	0	5	9.46
W	0	2	2	2	0	0	6	10.81
WNW	0	0	2	2	0	0	4	12.99
NW	0	0	0	1	0	0	1	13.88
NNW	0	2	0	0	0	0	2	4.19
Total	0	9	10	5	1	0	25	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 6
 Hours of No Stability Class : 5
 Total hours of observation : 2160

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FIRST QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00
 Stability Class: B $\Delta T / \Delta z$ 61->10 m ΔT With Substitution
 Wind Sensor Height : 10 meter
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	1	0	0	0	1	4.21
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	1	0	0	1	0	0	2	8.39
SW	0	3	8	0	0	0	11	9.62
WSW	1	1	2	3	0	0	7	11.26
W	0	1	8	4	2	0	15	13.07
WNW	0	7	4	1	0	0	12	8.47
NW	0	1	3	0	0	0	4	8.88
NNW	0	0	0	0	1	1	2	22.19
Total	2	13	26	9	3	1	54	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 6
 Hours of No Stability Class : 5
 Total hours of observation : 2160

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FIRST QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00

Stability Class: C delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	1	0	0	4	0	0	5	12.72
NNE	0	2	1	0	0	0	3	7.50
NE	2	5	2	0	2	0	11	9.12
ENE	0	2	5	0	0	0	7	8.30
E	0	0	1	0	0	0	1	8.19
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	1	0	0	1	13.50
SSE	0	0	0	0	0	0	0	0.00
S	0	0	2	0	0	0	2	10.42
SSW	0	5	2	2	0	0	9	9.23
SW	0	8	9	2	0	0	19	9.15
WSW	0	5	3	1	0	0	9	8.98
W	0	4	8	2	0	0	14	10.44
WNW	0	5	3	1	0	0	9	8.19
NW	0	3	7	1	0	0	11	10.06
NNW	0	0	1	1	2	1	5	18.80
Total	3	39	44	15	4	1	106	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 6
 Hours of No Stability Class : 5
 Total hours of observation : 2160

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FIRST QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00

Stability Class: D delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	9	26	18	21	1	0	75	9.20
NNE	5	21	52	29	5	0	112	11.06
NE	3	19	53	47	1	0	123	11.73
ENE	2	22	27	5	0	0	56	8.70
E	1	16	15	1	0	0	33	8.02
ESE	1	15	9	1	0	0	26	8.15
SE	2	14	8	4	0	0	28	8.25
SSE	4	9	8	2	0	0	23	7.96
S	2	13	17	9	0	0	41	9.65
SSW	5	19	28	6	0	0	58	8.67
SW	10	29	16	7	0	0	62	7.39
WSW	7	19	33	7	0	0	66	9.00
W	18	25	22	11	0	0	76	8.00
WNW	17	30	14	5	0	0	66	6.62
NW	6	28	13	2	0	0	49	6.73
NNW	8	19	20	5	1	0	53	8.48
Total	100	324	353	162	8	0	947	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 1
 Hours of Missing Data for All : 6
 Hours of No Stability Class : 5
 Total hours of observation : 2160

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FIRST QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00

Stability Class: E delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	11	10	4	0	0	0	25	5.30
NNE	12	9	0	1	0	0	22	4.64
NE	2	10	1	0	0	0	13	5.15
ENE	2	8	1	0	1	0	12	7.09
E	5	12	3	0	0	0	20	6.02
ESE	3	6	1	0	0	0	10	4.95
SE	1	24	2	0	0	0	30	5.55
SSE	10	34	15	1	0	0	60	6.47
S	10	44	28	4	0	0	86	7.38
SSW	12	47	13	0	0	0	72	6.23
SW	15	22	9	1	0	0	47	5.85
WSW	12	30	22	1	0	0	65	6.86
W	19	35	9	1	0	0	64	5.69
WNW	20	19	1	0	0	0	40	4.47
NW	7	17	7	0	0	0	31	5.82
NNW	6	16	12	0	0	0	34	6.59
Total	150	343	128	9	1	0	631	

Hours of Calm : 2
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 1
 Hours of Missing Data for All : 6
 Hours of No Stability Class : 5
 Total hours of observation : 2160

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FIRST QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00

Stability Class: F delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	4	0	0	0	0	0	4	2.74
NE	0	2	0	0	0	0	2	5.56
ENE	6	2	0	0	0	0	8	3.88
E	2	1	0	0	0	0	3	3.26
ESE	3	5	0	0	0	0	8	4.59
SE	5	12	1	0	0	0	18	5.32
SSE	1	27	3	0	0	0	31	6.37
S	7	40	0	0	0	0	47	5.67
SSW	6	14	0	0	0	0	20	4.99
SW	13	10	0	0	0	0	23	3.71
WSW	9	11	0	0	0	0	20	4.20
W	5	5	0	0	0	0	10	1.05
WNW	2	4	0	0	0	0	6	4.26
NW	5	4	0	0	0	0	9	3.98
NNW	2	1	0	0	0	0	3	3.13
Total	70	138	4	0	0	0	212	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 6
 Hours of No Stability Class : 5
 Total hours of observation : 2160

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FIRST QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00

Stability Class: G delta T/ delta z bl->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	2	0	0	0	0	0	2	2.43
NNE	2	0	0	0	0	0	2	2.90
NE	3	1	0	0	0	0	4	2.76
ENE	3	0	0	0	0	0	3	2.01
E	1	0	0	0	0	0	1	2.75
ESE	1	0	0	0	0	0	1	2.11
SE	1	3	0	0	0	0	4	4.28
SSE	5	8	0	0	0	0	13	4.35
S	12	6	0	0	0	0	18	3.45
SSW	13	2	0	0	0	0	15	3.06
SW	19	5	0	0	0	0	24	3.24
WSW	21	16	0	0	0	0	37	3.71
W	19	5	0	0	0	0	24	3.65
WNW	12	5	0	0	0	0	17	3.68
NW	5	1	0	0	0	0	6	2.91
NNW	2	1	0	0	0	0	3	2.91
Total	121	53	0	0	0	0	174	

Hours of Calm : 2
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 6
 Hours of No Stability Class : 5
 Total hours of observation : 2160

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FIRST QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00

Stability Class: ALL delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	23	37	23	25	1	0	109	8.30
NNE	23	32	53	30	5	0	143	9.65
NE	10	37	56	47	4	0	154	10.74
ENE	13	34	33	5	1	0	86	7.76
E	9	29	19	1	0	0	58	6.99
ESE	8	26	10	1	0	0	45	6.67
SE	12	53	11	5	0	0	81	6.47
SSE	20	78	26	3	0	0	127	6.50
S	31	103	47	13	0	0	194	7.11
SSW	37	88	43	9	0	0	177	6.80
SW	57	78	45	10	0	0	190	6.40
WSW	50	84	64	12	0	0	210	7.05
W	61	77	49	20	2	0	209	7.21
WNW	51	70	24	9	0	0	154	6.05
NW	23	54	30	4	0	0	111	6.52
NNW	18	39	33	6	4	2	102	8.22
Total	446	919	566	200	17	2	2150	

Hours of Calm : 4
 Hours of Varying Wind Direction : 0
 Hours of Missing Data for All : 6
 Hours of No Stability Class : 5
 Total hours of observation : 2160

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
SECOND QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00

Stability Class: A delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	2	1	0	1	0	0	4	6.96
NNE	4	0	0	0	0	0	4	3.83
NE	3	4	0	0	0	0	7	4.29
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	1	0	0	0	1	9.36
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	2	0	0	0	0	2	7.25
SW	0	4	0	0	0	0	4	5.76
WSW	0	10	1	0	0	0	11	6.02
W	1	6	1	0	0	0	8	6.61
WNW	0	1	2	0	0	0	3	9.25
NW	0	3	1	0	0	0	4	6.91
NNW	5	3	0	0	0	0	8	4.16
Total	15	34	6	1	0	0	56	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 1
 Hours of Missing Data for All : 92
 Hours of No Stability Class : 81
 Total hours of observation : 2184

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
SECOND QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00
 Stability Class: B $\Delta T / \Delta z$ 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	1	2	3	3	1	0	10	11.23
NNE	4	1	0	0	0	0	5	3.42
NE	1	2	2	1	0	0	6	8.05
ENE	1	1	0	1	0	0	3	8.23
E	0	0	0	0	0	0	0	0.00
ESE	0	3	0	0	0	0	3	6.47
SE	0	2	0	0	0	0	2	6.54
SSE	0	0	2	0	0	0	2	9.41
S	1	0	0	0	0	0	1	3.86
SSW	0	8	1	0	0	0	9	7.11
SW	1	6	2	0	0	0	9	6.36
WSW	2	11	2	0	0	0	15	6.27
W	0	3	3	0	0	0	6	7.01
WNW	1	1	4	0	0	0	6	8.15
NW	0	1	0	0	0	0	1	4.13
NNW	4	2	0	1	0	0	7	5.23
Total	16	43	19	6	1	0	85	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 2
 Hours of Missing Data for All : 92
 Hours of No Stability Class : 81
 Total hours of observation : 2184

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
SECOND QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00

Stability Class: C delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (mile./hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	5	3	1	3	0	0	12	7.37
NNE	3	8	2	4	0	0	17	7.51
NE	4	8	5	8	0	0	25	9.46
ENE	0	4	7	0	0	0	11	9.16
E	1	1	7	0	0	0	9	8.83
ESE	0	5	1	0	0	0	6	7.83
SE	0	0	7	0	0	0	7	8.65
SSE	0	1	0	0	0	0	1	7.23
S	0	1	1	0	0	0	2	8.68
SSW	1	9	1	0	0	0	11	5.81
SW	3	12	9	0	0	0	24	6.98
WSW	2	13	3	0	0	0	18	6.47
W	4	1	3	0	0	0	8	5.93
WNW	1	5	0	0	0	0	6	6.19
NW	2	1	0	0	0	0	3	3.53
NNW	3	3	0	0	0	0	6	4.05
Total	29	75	47	15	0	0	166	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 2
 Hours of Missing Data for All : 92
 Hours of No Stability Class : 81
 Total hours of observation : 2184

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
SECOND QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00

Stability Class: D delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	14	27	22	4	0	0	67	7.16
NNE	11	32	14	16	0	0	73	8.20
NE	8	31	80	47	0	0	166	10.54
ENE	2	34	75	15	0	0	126	9.58
E	4	39	28	5	0	0	76	7.99
ESE	1	40	14	1	0	0	56	7.22
SE	3	52	14	0	0	0	69	6.73
SSE	11	41	13	0	0	0	65	6.42
S	11	34	17	1	0	0	63	6.75
SSW	8	28	8	0	0	0	44	5.95
SW	15	38	15	0	0	0	68	5.81
WSW	17	25	5	0	0	0	47	5.12
W	9	14	3	0	0	0	26	4.99
WNW	13	14	2	0	0	0	29	4.69
NW	10	10	0	0	0	0	20	4.34
NNW	14	10	6	1	0	0	31	5.71
Total	151	469	316	90	0	0	1026	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 8
 Hours of Missing Data for All : 92
 Hours of No Stability Class : 81
 Total hours of observation : 2184

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
SECOND QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00

Stability Class: E delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	7	8	0	0	0	0	15	4.10
NNE	3	7	1	0	0	0	11	5.23
NE	7	6	1	0	0	0	14	4.63
ENE	1	11	2	1	0	0	15	7.05
E	1	23	2	0	0	0	26	6.13
ESE	2	16	3	0	0	0	21	6.49
SE	7	31	6	1	0	0	45	6.19
SSE	15	30	3	0	0	0	48	5.23
S	19	39	5	1	0	0	64	5.10
SSW	23	35	2	0	0	0	60	4.40
SW	34	35	2	0	0	0	71	4.52
WSW	12	21	4	1	0	0	38	5.22
W	26	13	0	0	0	0	39	3.70
WNW	22	6	0	0	0	0	28	3.30
NW	12	8	0	0	0	0	20	3.65
NNW	6	6	1	0	0	0	13	4.58
Total	197	295	32	4	0	0	528	

Hours of Calm : 4
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 92
 Hours of No Stability Class : 81
 Total hours of observation : 2184

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
SECOND QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00
 Stability Class: F $\Delta T / \Delta z$ 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	2	1	0	0	0	0	3	3.61
NE	3	2	0	0	0	0	5	3.49
ENE	0	2	0	0	0	0	2	5.88
E	1	5	0	0	0	0	6	5.83
ESE	0	1	0	0	0	0	1	4.03
SE	0	3	0	0	0	0	3	6.56
SSE	4	10	0	0	0	0	14	4.97
S	7	13	1	0	0	0	21	4.85
SSW	12	10	1	0	0	0	23	4.42
SW	12	7	0	0	0	0	19	3.68
WSW	15	7	0	0	0	0	22	3.69
W	10	4	0	0	0	0	14	3.21
WNW	5	2	0	0	0	0	7	3.15
NW	7	2	0	0	0	0	9	3.08
NNW	3	1	2	0	0	0	6	4.87
Total	81	70	4	0	0	0	155	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 92
 Hours of No Stability Class : 81
 Total hours of observation : 2184

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
SECOND QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00

Stability Class: G $\Delta T / \Delta z$ 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	1	1	0	0	0	0	2	4.31
S	7	1	0	0	0	0	8	3.32
SSW	8	0	0	0	0	0	8	2.80
SW	10	3	0	0	0	0	13	3.60
WSW	10	6	0	0	0	0	16	3.75
W	9	4	0	0	0	0	13	3.67
WNW	4	3	0	0	0	0	7	3.69
NW	2	0	0	0	0	0	2	2.22
NNW	0	0	0	0	0	0	0	0.00
Total	51	18	0	0	0	0	69	

Hours of Calm : 1
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 92
 Hours of No Stability Class : 81
 Total hours of observation : 2184

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
SECOND QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00

Stability Class:ALL $\Delta T / \Delta z$ 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	29	41	26	11	1	0	108	7.13
NNE	27	49	17	20	0	0	113	7.32
NE	26	53	88	56	0	0	223	9.63
ENE	4	52	84	17	0	0	157	9.24
E	7	68	37	5	0	0	117	7.53
ESE	3	65	19	1	0	0	88	7.06
SE	10	88	27	1	0	0	126	6.63
SSE	31	83	18	0	0	0	132	5.85
S	45	89	24	2	0	0	160	5.67
SSW	52	92	13	0	0	0	157	5.05
SW	75	105	28	0	0	0	208	5.20
WSW	58	94	15	1	0	0	168	5.13
W	59	45	10	0	0	0	114	4.46
WNW	46	32	8	0	0	0	86	4.54
NW	33	25	1	0	0	0	59	3.97
NNW	35	25	9	2	0	0	71	5.07
Total	540	1006	424	116	1	0	2087	

Hours of Calm : 5
 Hours of Varying Wind Direction : 0
 Hours of Missing Data for All : 92
 Hours of No Stability Class : 81
 Total hours of observation : 2184

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
THIRD QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00

Stability Class: A delta T/ delta z 61->10 m De'ta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	1	0	0	0	0	0	1	2.85
NNE	1	5	0	0	0	0	6	4.66
NE	4	7	1	0	0	0	12	5.06
ENE	0	9	4	0	0	0	13	6.94
E	0	1	1	0	0	0	2	9.12
ESE	0	0	2	0	0	0	2	10.37
SE	1	1	0	0	0	0	2	4.45
SSE	0	5	0	0	0	0	5	5.09
S	0	5	0	0	0	0	5	6.89
SSW	2	9	0	0	0	0	11	6.14
SW	2	24	1	0	0	0	27	5.63
WSW	3	17	2	0	0	0	22	5.54
W	3	7	0	0	0	0	10	5.00
WNW	1	4	0	0	0	0	5	4.63
NW	2	6	1	0	0	0	9	4.97
NNW	4	1	0	0	0	0	5	3.78
Total	24	101	12	0	0	0	137	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 2
 Hours of No Stability Class : 2
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
THIRD QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00

Stability Class: B $\Delta T / \Delta z$ 61->10 m ΔT With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	7	6	0	0	0	0	13	4.18
NNE	7	4	0	0	0	0	11	4.08
NE	1	6	5	2	1	0	15	9.02
ENE	0	4	6	1	0	0	11	9.05
E	0	5	0	0	0	0	5	6.10
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	2	1	0	0	0	3	6.56
S	1	6	3	0	0	0	10	6.64
SSW	2	13	3	0	0	0	18	5.97
SW	2	11	1	0	0	0	14	5.33
WSW	5	16	1	0	0	0	22	5.21
W	3	7	0	0	0	0	10	5.11
WNW	4	7	0	0	0	0	11	4.39
W	0	3	0	0	0	0	3	4.78
NNW	2	1	3	0	0	0	6	7.34
Total	34	91	23	3	1	0	152	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 1
 Hours of Missing Data for All : 2
 Hours of No Stability Class : 2
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
THIRD QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00

Stability Class: C delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	6	6	0	0	0	0	12	4.39
NNE	6	12	2	1	2	0	23	6.98
NE	3	12	18	6	1	0	40	9.74
ENE	0	5	5	1	0	0	11	8.72
E	0	5	2	0	0	0	7	7.07
ESE	0	0	0	0	0	0	0	0.00
SE	1	2	0	0	0	0	3	5.13
SSE	0	4	2	0	0	0	6	7.14
S	1	4	0	0	0	0	5	6.49
SSW	4	7	3	0	0	0	14	5.73
SW	0	14	1	0	0	0	15	5.74
WSW	4	8	2	0	0	0	14	5.22
W	2	9	0	0	0	0	11	5.35
WNW	2	2	0	0	0	0	4	4.21
NW	3	5	0	0	0	0	8	4.96
NNW	4	5	0	0	0	0	9	4.19
Total	36	100	35	8	3	0	182	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 4
 Hours of No Stability Class : 2
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
THIRD QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00

Stability Class: D delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	11	26	13	2	0	0	52	6.50
NNE	13	48	30	8	1	0	100	7.64
NE	8	33	60	23	1	0	125	9.69
ENE	7	45	92	10	0	0	154	9.28
E	7	42	46	1	0	0	96	7.94
ESE	4	28	6	0	0	0	38	6.15
SE	2	32	3	1	0	0	38	6.20
SSE	2	14	3	0	0	0	19	6.30
S	8	11	13	1	0	0	33	7.28
SSW	9	21	7	0	0	0	37	5.77
SW	8	25	1	0	0	0	34	5.23
WSW	11	24	1	0	0	0	36	4.70
W	12	21	0	0	0	0	33	4.16
WNW	11	13	0	0	0	0	24	4.21
NW	14	7	0	0	0	0	21	4.05
NNW	10	14	3	0	0	0	27	4.87
Total	137	404	278	46	2	0	867	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 2
 Hours of No Stability Class : 2
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
THIRD QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00

Stability Class: E delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	3	5	3	0	0	0	11	5.81
NNE	5	4	1	0	0	0	10	4.64
NE	1	3	2	0	0	0	6	6.62
ENE	3	13	2	0	0	0	18	6.51
E	7	19	10	0	0	0	36	6.53
ESE	8	14	0	0	0	0	22	4.55
SE	9	20	1	0	0	0	30	4.87
SSE	17	39	5	0	0	0	61	5.08
S	17	50	4	0	0	0	71	5.02
SSW	36	56	0	0	0	0	92	4.59
SW	35	21	0	0	0	0	56	3.86
WSW	26	33	1	0	0	0	60	4.32
W	26	4	1	0	0	0	31	3.27
WNW	18	1	0	0	0	0	19	3.23
NW	7	5	0	0	0	0	12	4.00
NNW	0	2	1	0	0	0	3	6.22
Total	218	289	31	0	0	0	538	

Hours of Calm : 1
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for A : 2
 Hours of No Stability Class : 2
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
THIRD QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00

Stability Class: F delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0- 75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	2	0	0	0	0	0	2	3.38
NNE	0	1	0	0	0	0	1	4.32
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	1	1	0	0	0	0	2	3.64
ESE	3	1	0	0	0	0	4	3.57
SE	2	6	0	0	0	0	8	4.98
SSE	13	17	0	0	0	0	30	4.38
S	11	12	0	0	0	0	23	4.22
SSW	12	8	1	0	0	0	21	4.02
SW	29	9	0	0	0	0	38	3.44
WSW	20	7	0	0	0	0	27	3.37
W	15	1	0	0	0	0	16	2.82
WNW	10	3	0	0	0	0	13	3.27
NW	6	1	0	0	0	0	7	3.50
NNW	5	1	0	0	0	0	6	3.11
Total	129	68	1	0	0	0	198	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 2
 Hours of No Stability Class : 2
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
THIRD QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00

Stability Class: G $\Delta T / \Delta z$ 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	1	0	1	0	0	0	2	6.21
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	1	0	0	0	0	0	1	2.16
SE	0	0	0	0	0	0	0	0.00
SSE	2	0	0	0	0	0	2	3.24
S	8	2	0	0	0	0	10	3.38
SSW	8	0	0	0	0	0	8	2.39
SW	22	2	0	0	0	0	24	3.10
WSW	40	3	0	0	0	0	43	3.15
W	29	4	0	0	0	0	33	3.44
WNW	3	1	0	0	0	0	4	3.61
NW	3	0	0	0	0	0	3	3.02
NNW	0	0	0	0	0	0	0	0.00
Total	117	12	1	0	0	0	130	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 2
 Hours of No Stability Class : 2
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UN1.1

Table 7
THIRD QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00

Stability Class:ALL delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- 8	8- <13	13- <19	19- 24	>24		
N	30	43	16	2	0	0	91	5.70
NNE	32	75	33	9	3	0	152	6.93
NE	18	61	87	31	3	0	200	9.24
ENE	10	76	109	12	0	0	207	8.85
E	15	73	59	1	0	0	148	7.45
ESE	16	43	8	0	0	0	67	5.54
SE	15	61	4	1	0	0	81	5.50
SSE	34	81	11	0	0	0	126	5.20
S	46	90	20	1	0	0	157	5.48
SSW	73	114	14	0	0	0	201	4.95
SW	98	106	4	0	0	0	208	4.38
WSW	109	108	7	0	0	0	224	4.31
W	90	53	1	0	0	0	144	3.87
WNW	49	31	0	0	0	0	80	3.85
NW	35	27	1	0	0	0	63	4.21
NNW	25	24	7	0	0	0	56	4.81
Total	695	1066	381	57	6	0	2205	

Hours of Calm : 1
 Hours of Varying Wind Direction : 0
 Hours of Missing Data for All : 2
 Hours of No Stability Class : 2
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FOURTH QUARTER 1991

Report Date : 92-02-07

Data Period : 91-10- 1 00:00 to 91-12-31 23:00

Stability Class: A delta T/ delta z 61 >10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	2	1	0	0	0	0	3	3.78
NNE	2	0	0	0	0	0	2	2.65
NE	1	1	0	0	0	0	2	4.43
ENE	0	0	1	0	1	0	2	14.20
E	0	1	1	0	0	0	2	8.01
ESE	0	0	1	0	0	0	1	9.18
SE	0	1	0	0	0	0	1	7.59
SSE	0	3	1	0	0	0	4	7.43
S	0	2	0	0	0	0	2	6.65
SSW	0	0	0	0	0	0	0	0.00
SW	0	4	1	0	0	0	5	7.79
WSW	0	4	5	0	0	0	9	8.26
W	0	4	3	1	0	0	8	8.83
WNW	0	9	3	0	0	0	12	7.18
NW	1	1	3	0	0	0	5	8.00
NNW	1	2	0	0	0	0	3	5.68
Total	7	33	19	1	1	0	61	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 100
 Hours of No Stability Class : 97
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FOURTH QUARTER 1991

Report Date : 92-02-07

Data Period : 91-10-1 00:00 to 91-12-31 23:00

Stability Class: B $\Delta T / \Delta z$ 61--10 m ΔT With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	2	5	0	1	0	0	8	6.03
NNE	4	5	1	0	4	0	14	10.09
NE	1	2	6	4	0	0	13	10.60
ENE	0	2	1	1	0	0	4	8.72
E	1	1	4	0	0	0	6	8.12
ESE	0	0	1	0	0	0	1	8.60
SE	0	2	0	0	0	0	2	6.40
SSE	0	0	0	0	0	0	0	0.00
S	0	2	0	0	0	0	2	5.97
SSW	0	0	0	0	0	0	0	0.00
SW	0	8	4	0	0	0	12	7.11
WSW	0	0	6	2	0	0	8	11.49
W	0	1	2	1	0	0	6	9.61
WNW	1	0	0	0	0	0	6	6.30
NW	0	0	1	0	0	0	5	5.80
NNW	1	0	0	1	0	0	9	5.63
Total	10	46	25	10	4	0	96	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 100
 Hours of No Stability Class : 97
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FOURTH QUARTER 1991

Report Date : 92-02-07

Data Period : 91-10-1 00:00 to 91-12-31 23:00

Stability Class: C delta T/ delta z 61->10 Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	2	9	1	5	0	0	17	8.66
NNE	1	2	3	8	10	0	24	15.80
NE	2	4	5	5	0	0	16	10.22
ENE	0	5	5	1	0	0	11	8.93
E	0	1	2	0	0	0	3	8.73
ESE	0	1	2	0	0	0	3	8.26
SE	0	3	0	0	0	0	3	5.47
SSE	0	4	0	0	0	0	4	6.65
S	0	2	1	1	0	0	4	8.24
SSW	1	3	2	1	0	0	7	8.20
SW	1	6	7	1	0	0	15	7.27
WSW	1	7	1	0	0	0	9	5.99
W	1	0	1	1	0	0	3	8.54
WNW	0	8	0	0	0	0	8	4.91
NW	0	3	1	0	0	0	4	7.49
NNW	1	7	1	0	0	0	9	5.99
Total	10	65	32	23	10	0	140	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 100
 Hours of No Stability Class : 97
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FOURTH QUARTER 1991

Report Date : 92-02-07
 Data Period : 91-10-1 00:00 to 91-12-31 23:00
 Stability Class: D $\Delta T / \Delta z$ 61-10 m ΔT With Substitution
 Wind Sensor Height : 10 meter
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	12	20	15	16	7	1	71	10.52
NNE	11	21	40	26	0	0	98	7.89
NE	4	33	70	39	0	0	146	10.62
ENE	5	29	26	17	1	0	78	9.61
E	2	16	9	1	0	0	28	7.69
ESE	0	5	0	0	0	0	5	4.85
S2	0	6	2	0	0	0	8	6.79
SSE	2	7	14	0	0	0	23	8.53
S	4	19	24	1	0	0	48	8.01
SSW	3	5	12	0	0	0	20	8.41
SW	5	22	20	1	0	0	48	7.34
WSW	8	24	15	0	0	0	47	7.55
W	6	16	8	1	0	0	31	6.62
WNW	6	14	0	0	0	0	20	4.30
NW	2	15	5	0	0	0	22	5.43
NNW	11	11	15	8	0	0	45	8.46
Total	81	263	275	100	8	1	738	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 5
 Hours of Missing Data for All : 100
 Hours of No Stability Class : 97
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. Smith Nuclear Station UNIT 1

Table 7
FOURTH QUARTER 1991

Report Date : 92-02-07

Data Period : 91-10-1 00:00 to 91-12-31 23:00

Stability Class: E $\Delta T / \Delta z$ 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	7	11	5	1	0	0	24	6.00
NNE	7	8	0	0	0	0	15	4.57
NE	4	14	4	0	0	0	22	5.85
ENE	1	18	9	0	0	0	28	7.09
E	7	36	5	0	0	0	48	6.07
ESE	4	24	6	0	0	0	34	6.37
SE	3	24	1	0	0	0	28	5.67
SSE	7	17	7	0	0	0	31	6.31
S	6	22	11	0	0	0	39	6.23
SSW	5	17	11	0	0	0	33	6.48
SW	6	33	7	0	0	0	46	5.57
WSW	8	46	6	0	0	0	60	6.14
W	9	36	6	0	0	0	51	5.32
WNW	9	14	2	0	0	0	25	4.87
NW	1	14	1	0	0	0	16	5.16
NNW	5	4	3	0	0	0	12	5.79
Total	89	338	84	1	0	0	512	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 100
 Hours of No Stability Class : 97
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FOURTH QUARTER 1991

Report Date : 92-02-07
 Data Period : 91-10-1 00:00 to 91-12-31 23:00
 Stability Class: F $\Delta T / \Delta z$ 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	9- <13	13- <19	19- 24	>24		
N	2	2	1	0	0	0	5	5.10
NNE	2	1	0	0	0	0	3	3.67
NE	0	3	0	0	0	0	3	5.79
ENE	1	0	0	0	0	0	1	3.50
E	4	13	1	0	0	0	18	5.43
ESE	2	4	0	0	0	0	6	5.21
SE	5	15	2	0	0	0	22	5.57
SSE	4	25	1	0	0	0	30	5.15
S	7	13	0	0	0	0	21	4.24
SSW	10	7	0	0	0	0	17	3.70
SW	9	22	0	0	0	0	31	4.49
WSW	10	16	0	0	0	0	26	4.15
W	9	16	0	0	0	0	25	4.40
WNW	2	4	0	0	0	0	6	1.00
NW	2	10	0	0	0	0	12	4.43
NNW	0	2	1	0	0	0	3	7.18
Total	70	153	6	0	0	0	229	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 100
 Hours of No Stability Class : 97
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FOURTH QUARTER 1991

Report Date : 92-02-07
 Data Period : 91-10-1 00:00 to 91-12-31 23:00
 Stability Class: G $\Delta T / \Delta z$ 61-10 m ΔT With Substitution
 Wind Sensor Height : 10 meter
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	2	0	0	0	0	0	2	2.81
NE	1	0	0	0	0	0	1	2.05
ENE	2	0	0	0	0	0	2	2.53
E	2	1	0	0	0	0	3	2.88
ESE	4	1	0	0	0	0	5	3.31
SE	6	4	0	0	0	0	10	3.64
SSE	10	12	0	0	0	0	22	4.00
S	27	13	0	0	0	0	40	3.52
SSW	31	14	0	0	0	0	45	3.57
SW	40	20	0	0	0	0	60	3.57
WSW	40	14	0	0	0	0	54	3.48
W	45	9	0	0	0	0	54	3.39
WNW	17	4	0	0	0	0	21	3.12
NW	3	4	0	0	0	0	7	4.21
NNW	2	1	0	0	0	0	3	3.76
Total	232	97	0	0	0	0	329	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 1
 Hours of Missing Data for All : 100
 Hours of No Stability Class : 97
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 7
FOURTH QUARTER 1991

Report Date : 92-02-07
 Data Period : 91-10- 1 00:00 to 91-12-31 23:00
 Stability Class:ALL delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	27	49	22	23	7	1	129	8.75
NNE	29	37	44	34	14	0	158	10.00
NE	13	57	85	48	0	0	203	9.90
ENE	9	54	42	19	2	0	126	8.87
E	16	69	22	1	0	0	108	6.52
ESE	10	35	10	0	0	0	55	6.02
SE	14	55	5	0	0	0	74	5.53
SSE	23	68	23	0	0	0	114	6.06
S	45	73	36	2	0	0	156	5.87
SSW	50	46	25	1	0	0	122	5.43
SW	61	115	39	2	0	0	217	5.51
WSW	67	111	33	2	0	0	213	5.60
W	70	84	20	4	0	0	178	5.19
WNW	35	58	5	0	0	0	98	4.70
NW	9	51	12	0	0	0	72	5.76
NMW	21	34	21	9	0	0	85	7.26
Total	499	996	444	145	23	1	2108	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data for All : 100
 Hours of No Stability Class : 97
 Total hours of observation : 2208

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FIRST QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00
 Stability Class: A delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	1	0	0	0	0	1	4.39
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	1	0	0	0	0	1	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 1
 Hours of No Stability Class : 0
 Total hours of observation : 4

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FIRST QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00
 Stability Class: B $\Delta T / \Delta z$ 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 1
 Hours of No Stability Class : 0
 Total hours of observation : 4

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FIRST QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00

Stability Class: C delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 1
 Hours of No Stability Class : 0
 Total hours of observation : 4

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FIRST QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00

Stability Class: D delta T/ delta z 61->10 m Delta T With Substitutio.

Wind Sensor Height : 10 meter +++ Batch Release Times Only +++

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	1	0	0	0	0	1	5.25
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	1	0	0	0	0	1	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 1
 Hours of No Stability Class : 0
 Total hours of observation : 4

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FIRST QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00
 Stability Class: E delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	1	0	0	0	0	1	5.59
Total	0	1	0	0	0	0	1	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 1
 Hours of Missing Data for All : 1
 Hours of No Stability Class : 0
 Total hours of observation : 4

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FIRST QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00
 Stability Class: F delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 1
 Hours of No Stability Class : 0
 Total hours of observation : 4

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FIRST QUARTER 1991

Repr/ Date : 92-02-07
 Date Period : 91- 1- 1 00:00 to 91- 3-31 23:00
 Sta' lity Class: G delta T/ delta z 61--10 = Delta T With Substitution
 Wir Sensor Height : 10 meter +++ Ratch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 1
 Hours of No Stability Class : 0
 Total hours of observation : 4

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FIRST QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 1- 1 00:00 to 91- 3-31 23:00
 Stability Class:ALL delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	2	0	0	0	0	2	4.82
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	3.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	1	0	0	0	0	1	5.50
Total	0	3	0	0	0	0	3	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data for All : 1
 Hours of No Stability Class : 0
 Total hours of observation : 4

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
SECOND QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00
 Stability Class: A delta T/ delta z 61- >10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 0

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
SECOND QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00

Stability Class: B delta T/ delta z 61-->10 m Delta T With Substitution

Wind Sensor Height : 10 meter +++ Batch Release Times Only +++

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	1	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 0

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
SECOND QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00
 Stability Class: C $\Delta T / \Delta z$: 61-10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direct. n	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 0

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
SECOND QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00
 Stability Class: D delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 0

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
SECOND QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00
 Stability Class: E delta T/ delta z 61-10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 0

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
SECOND QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00
 Stability Class: F delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 0

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
SECOND QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 4- 1 00:00 to 91- 6-30 23:00
 Stability Class: G $\Delta T / \Delta z$ 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 0

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
SECOND QUARTER 1991

Report Date : 91-02-07

Data Period : 91- 4- 1 00: J to 91- 6-30 23:00

Stability Class:ALL delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter +++ Batch Release Times Only +++

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 0

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
THIRD QUARTER 1991

Report Date : 92-02-07

Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00

Stability Class: A delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter +++ Batch Release Times Only +++

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 16

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
THIRD QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00
 Stability Class: B delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 16

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
THIRD QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00
 Stability Class: C delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 16

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
THIRD QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00
 Stability Class: D $\Delta T / \Delta z$ 61-10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 16

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
THIRD QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 7- 1 10:00 to 91- 9-30 23:00
 Stability Class: E delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	1	0	0	0	0	1	6.56
SSE	0	1	1	0	0	0	2	6.42
S	1	2	0	0	0	0	3	5.39
SSW	0	0	0	0	0	0	0	0.00
SW	1	0	0	0	0	0	1	3.59
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	2	4	1	0	0	0	7	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 16

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
THIRD QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00
 Stability Class: F delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction by Speed

Wind Direction	Wind Speed (miles/hour)						Tot	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	3	0	0	0	0	3	6.13
S	0	0	0	0	0	0	0	0.00
SSW	0	1	0	0	0	0	1	5.06
SW	0	3	0	0	0	0	3	4.23
WSW	1	1	0	0	0	0	2	4.12
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	1	8	0	0	0	0	9	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 16

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
THIRD QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00
 Stability Class: G delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <11	11- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 16

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
THIRD QUARTER 1991

Report Date : 92-02-07
 Data Period : 91- 7- 1 00:00 to 91- 9-30 23:00
 Stability Class:ALL delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75	< 8	8- <13	13- <19	19- 24	>24		
N		0	0	0	0	0	0	0.00
NNn		0	0	0	0	0	0	0.00
NE		0	0	0	0	0	0	0.00
ENE		0	0	0	0	0	0	0.00
E		0	0	0	0	0	0	0.00
ESE	v	0	0	0	0	0	0	0.00
SE	0	1	0	0	0	0	1	6.56
SSE	0	4	1	0	0	0	5	6.24
S	1	2	0	0	0	0	3	5.39
SSW	0	1	0	0	0	0	1	5.06
SW	1	3	0	0	0	0	4	4.07
WSW	1	1	0	0	0	0	2	4.12
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	3	12	1	0	0	0	16	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 16

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FOURTH QUARTER 1991

Report Date : 92-02-07
 Data Period : 91-10- 1 00:00 to 91-12-31 23:00
 Stability Class: A delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	1	0	0	0	1	12.78
W	0	0	2	1	0	0	3	11.92
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	3	1	0	0	4	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 13

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FOURTH QUARTER 1991

Report Date : 92-02-07
 Data Period : 91-10-1 00:00 to 91-12-31 23:00
 Stability Class: B $\Delta T / \Delta z$ 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	1	0	0	1	14.13
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	1	0	0	1	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 13

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FOURTH QUARTER 1991

Report Date : 92-02-07

Data Period : 91-10-1 00:00 to 91-12-31 23:00

Stability Class: C $\Delta T / \Delta z$ 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter +++ Batch Release Times Only +++

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	1	0	0	1	13.16
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	1	0	0	1	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 13

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FOURTH QUARTER 1991

Report Date : 92-02-07
 Data Period : 91-10-1 00:00 to 91-12-31 23:00
 Stability Class: D $\Delta T / \Delta z$ 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	1	1	0	0	2	12.81
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	1	1	0	0	2	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 13

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FOURTH QUARTER 1991

Report Date : 92-02-07
 Data Period : 91-10- 1 00:00 to 91-12-31 23:00
 Stability Class: E delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 13

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FOURTH QUARTER 1991

Report Date : 92-02-07
 Data Period : 91-10- 1 00:00 to 91-12-31 23:00
 Stability Class: F delta T/ delta z 6l->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	1	0	0	0	0	1	5.95
W	0	4	0	0	0	0	4	5.73
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	5	0	0	0	0	5	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 13

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FOURTH QUARTER 1991

Report Date : 92-02-07
 Data Period : 91-10-1 00:00 to 91-12-31 23:00
 Stability Class: G delta T/ delta z 61->10 m Delta T With Substitution
 Wind Sensor Height : 10 meter +++ Batch Release Times Only +++
 Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	0	0	0	0	0	0	0.00
W	0	0	0	0	0	0	0	0.00
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	0	0	0	0	0	0	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 13

JOINT WIND FREQUENCY DISTRIBUTION BY STABILITY CLASS

SITE: V. C. SUMMER Nuclear Station UNIT 1

Table 8
FOURTH QUARTER 1991

Report Date : 92-02-07

Data Period : 91-10- 1 00:00 to 91-12-31 23:00

Stability Class:ALL delta T/ delta z 61->10 m Delta T With Substitution

Wind Sensor Height : 10 meter +++ Batch Release Times Only +++

Hours at Each Wind Direction and Speed

Wind Direction	Wind Speed (miles/hour)						Total'	Mean Speed
	0.75- <4	4- <8	8- <13	13- <19	19- 24	>24		
N	0	0	0	0	0	0	0	0.00
NNE	0	0	0	0	0	0	0	0.00
NE	0	0	0	0	0	0	0	0.00
ENE	0	0	0	0	0	0	0	0.00
E	0	0	0	0	0	0	0	0.00
ESE	0	0	0	0	0	0	0	0.00
SE	0	0	0	0	0	0	0	0.00
SSE	0	0	0	0	0	0	0	0.00
S	0	0	0	0	0	0	0	0.00
SSW	0	0	0	0	0	0	0	0.00
SW	0	0	0	0	0	0	0	0.00
WSW	0	1	1	0	0	0	2	9.37
W	0	4	3	4	0	0	11	10.14
WNW	0	0	0	0	0	0	0	0.00
NW	0	0	0	0	0	0	0	0.00
NNW	0	0	0	0	0	0	0	0.00
Total	0	5	4	4	0	0	13	

Hours of Calm : 0
 Hours of Varying Wind Direction : 0
 Hours of Missing Data for All : 0
 Hours of No Stability Class : 0
 Total hours of observation : 13

ATTACHMENT I

V. C. SUMMER NUCLEAR STATION

Offsite Dose Calculation Manual
Revision 16

Control Copy No. _____

OFFSITE DOSE CALCULATION MANUAL
FOR
SOUTH CAROLINA ELECTRIC AND GAS COMPANY
VIRGIL C. SUMMER NUCLEAR STATION

PSRC Approval J. R. Morel for G6 SWRT 9/20/91
Date

Revision 16

September 1991

Reviewed by: [Signature] 9/20/91
Date

Approved by: [Signature] 9-20-91
Date

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INTRODUCTION

The OFFSITE DOSE CALCULATION MANUAL (ODCM) is an implementing and supporting document of the RADIOLOGICAL EFFLUENT TECHNICAL SPECIFICATIONS (RETS). In accordance with USNRC Generic Letter 89-01, entitled "Implementation of Programmatic Controls for Radiological Effluent Technical Specifications in the Administrative Controls Section of the Technical Specifications and the Relocation of Procedural Details of RETS to the Offsite Dose Calculation Manual or to the Process Control Program", the procedural details for implementing the Radiological Limiting Conditions for Operation have been incorporated into the ODCM. The ODCM describes the methodology and parameters to be used in the calculation of offsite doses due to radioactive liquid and gaseous effluents and in the calculation of liquid and gaseous effluent monitoring instrumentation alarm/trip setpoints. The ODCM contains a list and graphical description of the specific sample locations for the radiological environmental monitoring program. Configurations of the liquid and gaseous radwaste treatment systems are also included.

The ODCM will be maintained at the Station as the reference which details the Radiological Effluent Limiting Conditions for Operation of the V. C. Summer Nuclear Station. Additionally the ODCM will be maintained as the guide for accepted calculational methodologies. Changes in calculation methods or parameters will be incorporated into the ODCM in order to ensure that the ODCM represents the current methodology in all applicable areas. Computer software to perform described calculations will be maintained current with this ODCM.

RESPONSIBILITIES

The ODCM contains the radiological effluent limiting conditions for operation, their applicability, remedial actions, surveillance requirements, and their bases. Plant procedures implement responsibilities for compliance with the ODCM that include:

The Operations group is responsible for:

- Declaring radioactive liquid and gaseous effluent monitor channels operable or inoperable.
- Ensuring the minimum number of operable channels for radioactive liquid and gaseous effluent monitors.
- Notifying the responsible group to implement appropriate action if less than the minimum number of radioactive liquid and gaseous effluent monitor channels are operable.
- Initiating an Off Normal Occurrence Report in accordance with SAP-132, when less than the minimum number of channels operable condition prevails for more than 30 days.
- Restoring to within limits, the concentration of liquid radioactive material exceeding ODCM limits released from the site.
- Ensuring radioactive liquid and gaseous effluent monitor setpoints are set as prescribed in the effluent release permit.
- Suspending release if radioactive liquid and gaseous effluent monitor setpoints are less conservative than ODCM requirements.
- Declaring liquid and gaseous radwaste treatment systems operable or inoperable.
- Ensuring operability of gaseous and liquid radwaste treatment systems and ventilation exhaust treatment system.
- Ensuring appropriate portions of the gaseous and liquid radwaste treatment systems are used to reduce the radioactive materials in liquid and gaseous waste prior to their discharge when the projected doses exceed limits specified by the ODCM.
- Initiating an Off Normal Occurrence Report in accordance with SAP-132, when liquid or gaseous radwaste system is inoperable for more than 31 days.
- Performing channel check and source check at the frequencies shown in Tables 1.1-2 and 1.2-2 for each radioactive liquid and gaseous effluent monitoring instrumentation channel.

Instrumentation and Controls group is responsible for:

- Performing channel calibration and analog channel operational test at the frequencies shown in Tables 1.1-2 and 1.2-2 for each radioactive liquid and gaseous effluent monitoring instrumentation channel.
- Informing the Operations group of surveillance test results.

The Health Physics group is responsible for:

- Establishing setpoints for radioactive liquid and gaseous effluent monitors, consistent with ODCM methodology, and providing setpoint information to Operations.
- Implementing remedial actions as requested by Operations. These actions include grab sampling and analysis and providing the results to Operations.
- Performing periodic radioactive effluent monitor checks to determine backgrounds, normal indications and verifying monitor correlation graphs, and providing this information as necessary to Operations.
- Implementing radioactive gaseous and liquid waste sampling and analysis program in accordance with ODCM Tables 1.1-4 and 1.2-3.
- Informing Operations when at least one Circulating Water Pump or the Circulating Water Jockey Pump is required to provide dilution to the discharge structure.
- Calculating cumulative dose contributions and performing dose projections from liquid and gaseous effluents in accordance with the ODCM and providing the information to Operations.
- Initiating an Off Normal Occurrence Report in accordance with SAP-132, when calculated dose from the discharge of radioactive materials in liquid or gaseous effluents are in excess of the limits specified by ODCM sections 1.1.3.1 or 1.2.3.1.
- Initiating an Off Normal Occurrence Report in accordance with SAP-132, when liquid or gaseous waste is discharged without treatment and is in excess of the limits specified by ODCM sections 1.1.4.1 or 1.2.3.1.
- Initiating an Off Normal Occurrence Report in accordance with SAP-132, when the dose or dose commitment to any member of the public due to releases of radioactivity and radiation is in excess of 25 mrem to the total body or any organ (except the thyroid, which shall be limited to less than or equal to 75 mrem) over 12 consecutive months.

The Corporate Health Physics and Environmental Programs group is responsible for:

- Implementing the Radiological Environmental Monitoring Program as specified in Section 1.4 of the ODCM.
- Initiating an Off Normal Occurrence Report in accordance with SAP-132, when the Radiological Environmental Monitoring Program limiting conditions for operation are exceeded.

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1.0 SPECIFICATION OF LIMITING CONDITIONS FOR OPERATION

1.1 LIQUID EFFLUENTS

1.1.1 Radioactive Liquid Effluent Monitoring Instrumentation

LIMITING CONDITION FOR OPERATION

1.1.1.1 The radioactive liquid effluent monitoring instrumentation channels shown in Table 1.1-1 shall be OPERABLE with their alarm/trip setpoints set to ensure that the limits of ODCM Specification 1.1.2.1 are not exceeded. The alarm/trip setpoints of these channels shall be determined in accordance with ODCM, Section 2.1.

APPLICABLE: At all Times.

ACTION:

- a. With a radioactive liquid effluent monitoring instrumentation channel alarm/ trip setpoint less conservative than required by the above specification, immediately suspend the release of radioactive liquid effluents monitored by the affected channel or declare the channel inoperable.
- b. With less than the minimum number of radioactive liquid effluent monitoring instrumentation channels OPERABLE, take the ACTION shown in Table 1.1-1. Additionally if this condition prevails for more than 30 days, in the next semiannual effluent report explain why this condition was not corrected in a timely manner.
- c. The provisions of Technical Specifications 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

1.1.1.2 Each radioactive liquid effluent monitoring instrumentation channel shall be demonstrated OPERABLE by performance of the CHANNEL CHECK, SOURCE CHECK, CHANNEL CALIBRATION and ANALOG CHANNEL OPERATIONAL TEST operations at the frequencies shown in Table 1.1-2.

TABLE 1.1-1

RADIOACTIVE LIQUID EFFLUENT MONITORING INSTRUMENTATION

	<u>INSTRUMENT</u>	<u>MINIMUM CHANNELS OPERABLE</u>	<u>ACTION</u>
1.	GROSS RADIOACTIVITY MONITORS PROVIDING ALARM AND AUTOMATIC TERMINATION OF RELEASE		
a.	Liquid Radwaste Effluent Line - RM-L5 or RM-L9	1	1
b.	Nuclear (Processed Steam Generator) Blowdown Effluent Line RM-L7 or RM-L9	1	1
c.	Steam Generator Blowdown Effluent Line		
1.	Unprocessed during Power Operation - RM-L10 or RM-L3	1	2
2.	Unprocessed during Startup - RM-L3	1	2
d.	Turbine Building Sump Effluent Line - RM-L8	1	3
e.	Condensate Demineralizer Backwash Effluent Line RM-L11	1	6
2.	FLOW RATE MEASUREMENT DEVICES*		
a.	Liquid Radwaste Effluent Line - Tanks 1 and 2	1/tank	4
b.	Penstock Minimum Flow Interlock**	1	4
c.	Nuclear Blowdown Effluent Line	1	4
d.	Steam Generator (Unprocessed) Blowdown Effluent Line	1	4
3.	TANK LEVEL INDICATING DEVICES		
a.	Condensate Storage Tank	1	5

* In the event that simultaneous releases from both WMT and NBMT are required (which normally will be prevented by procedure) the flow rate for monitor RM-L9 will be determined by adding flow rates for monitors RM-L5 and RM-L7.

** Minimum dilution flow is assured by an interlock that terminates liquid waste releases if the minimum dilution flow is not available.

TABLE 1.1-1 (Continued)

TABLE NOTATION

ACTION 1 With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases may continue for up to 14 days provided that prior to initiating a release:

- a. At least two independent samples are analyzed in accordance with ODCM Specification 1.1.2.4 and
- b. At least two technically qualified members of the Facility Staff independently verify the release rate calculations and discharge line valving;

Otherwise, suspend release of radioactive effluents via this pathway.

ACTION 2 With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue for up to 30 days provided grab samples are analyzed for gross radioactivity (beta and gamma) at a limit of detection of at least $1E-7$ microcuries/gram:

- a. At least once per 8 hours when the specific activity of the secondary coolant is greater than 0.01 microcuries/gram DOSE EQUIVALENT I-131.
- b. At least once per 24 hours when the specific activity of the secondary coolant is less than or equal to 0.01 microcuries/gram DOSE EQUIVALENT I-131.

TABLE 1.1-1 (Continued)

TABLE NOTATION

- ACTION 3 With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue for up to 30 days provided that, at least once per 8 hours, grab samples are collected and analyzed for gross radioactivity (beta and gamma) at a limit of detection of at least $1E-7$ microcuries/gram.
- ACTION 4 With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue for up to 30 days provided the flow rate is estimated at least once per 4 hours during actual releases. Pump curves may be used to estimate flow.
- ACTION 5 With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, liquid additions to this tank may continue for up to 30 days provided the tank liquid level is estimated during all liquid additions to the tank to prevent overflow.
- ACTION 6 With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases may continue for up to 30 days provided that samples are analyzed in accordance with ODCM Specification 1.1.2.2 and Technical Specification 4.11.1.5.

TABLE 1.1-2
 RADIOACTIVE LIQUID EFFLUENT MONITORING INSTRUMENTATION
 SURVEILLANCE REQUIREMENTS

	<u>INSTRUMENT</u>	<u>CHANNEL CHECK</u>	<u>SOURCE CHECK</u>	<u>CHANNEL CALIBRATION</u>	<u>ANALOG CHANNEL OPERATIONAL TEST</u>
1.	GROSS RADIOACTIVITY MONITORS PROVIDING ALARM AND AUTOMATIC TERMINATION OF RELEASE				
a.	Liquid Radwaste Effluent Line - RM-L5 or RM-L9	D	P	R(2)	Q(1)
b.	Nuclear Blowdown Effluent Line RM-L7	D	P	R(2)	Q(1)
c.	Steam Generator Blowdown Effluent Line - RM-L3, RM-L10	D	M	R(2)	Q(1)
d.	Turbine Building Sump Effluent Line - RM-L8	D	M	R(2)	Q(1)
e.	Condensate Demineralizer Backwash Effluent Line RM-L11	D	M	R(2)	Q(4)
2.	FLOW RATE MEASUREMENT DEVICES				
a.	Liquid Radwaste Effluent Line	D(3)	N.A.	R	Q
b.	Penstocks Minimum Flow Interlock	D(3)	N.A.	R	Q
c.	Nuclear Blowdown Effluent Line	D(3)	N.A.	R	Q
d.	Steam Generator Blowdown Effluent Line	D(3)	N.A.	R	Q
3.	TANK LEVEL INDICATING DEVICES				
a.	Condensate Storage Tank	D	N.A.	R	Q

See Table 1.1-3 for explanation of frequency notation.

TABLE 1.1-2 (Continued)

TABLE NOTATION

- (1) The ANALOG CHANNEL OPERATIONAL TEST shall also demonstrate that automatic isolation of this pathway and control room alarm annunciation occurs if any of the following conditions exists:
 1. Instrument indicates measured levels above the alarm/trip setpoint.
 2. Loss of Power (alarm only).
 3. Low flow (alarm only).
 4. Instrument indicates a downscale failure (alarm only).
 5. Normal/Bypass switch set in Bypass (alarm only).
 6. Other instrument controls not set in operate mode.

- (2) The initial CHANNEL CALIBRATION shall be performed using one or more of the reference standards certified by the National Institute of Standards and Technology (NIST) or using standards that have been obtained from suppliers that participate in measurement assurance activities with NIST. These standards shall permit calibrating the system over its intended range of energy and measurement range. For subsequent CHANNEL CALIBRATION, sources that have been related to the initial calibration shall be used.

- (3) CHANNEL CHECK shall consist of verifying indication of flow during periods of release. CHANNEL CHECK shall be made at least once per 24 hours on days on which continuous, periodic, or batch releases are made.

- (4) The ANALOG CHANNEL OPERATIONAL TEST shall also demonstrate that automatic isolation of this pathway and local panel alarm annunciation occurs if any of the following conditions exists:
 1. Instrument indicates measured levels above the alarm/trip setpoint.
 2. Loss of Power (alarm only)
 3. Low flow (alarm only).
 4. Instrument indicates a downscale failure (alarm only).
 5. Normal/Bypass switch set in Bypass (alarm only).
 6. Other instrument controls not set in operate mode.

TABLE 1.1-3

FREQUENCY NOTATION

<u>NOTATION</u>	<u>FREQUENCY</u>
D	At least once per 24 hours.
W	At least once per 7 days.
M	At least once per 31 days.
Q	At least once per 92 days.
SA	At least once per 184 days.
R	At least once per 18 months.
P	Completed prior to each release.
N.A.	Not applicable.

1.1.2 Liquid Effluents: Concentration

LIMITING CONDITION FOR OPERATION

1.1.2.1 The concentration of radioactive material released from the site (see Technical Specification Figure 5.1-4) shall be limited to the concentrations specified in 10 CFR Part 20, Appendix B, Table II, Column 2 for radionuclides other than dissolved or entrained noble gases. For dissolved or entrained noble gases, the concentration shall be limited to $2E-4$ microcuries/ml total activity.

APPLICABLE: At all Times.

ACTION:

With the concentration of radioactive material released from the site exceeding the above limits, immediately restore the concentration to within the above limits.

SURVEILLANCE REQUIREMENTS

1.1.2.2 The radioactivity content of each batch of radioactive liquid waste shall be determined prior to release by sampling and analysis in accordance with Table 1.1-4. The results or pre-release analyses shall be used with the calculational methods in ODCM Section 2.1 to assure that the concentration at the point of release is maintained within the limits of ODCM Specification 1.1.2.1.

1.1.2.3 Post-release analyses of samples composited from batch releases shall be performed in accordance with Table 1.1-4. The results of the previous post-release analyses shall be used with the calculational methods in ODCM Section 2.1 to assure that the concentrations at the point of release were maintained within the limits of ODCM Specification 1.1.2.1.

1.1.2.4 The radioactivity concentration of liquids discharged from continuous release points shall be determined by collection and analysis of samples in

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accordance with Table 1.1-4. The results of the analyses shall be used with the calculational methods in ODCM Section 2.1 to assure that the concentrations at the point of release are maintained within the limits of ODCM Specification 1.1.2.1.

1.1.2.5 At least one Circulating Water Pump or the Circulating Water Jockey Pump shall be determined to be in operation and providing dilution to the discharge structure at least once per 4 hours whenever dilution is required to meet the site radioactive effluent concentration limits of ODCM Specification 1.1.2.1.

TABLE 1.1-4
RADIOACTIVE LIQUID WASTE SAMPLING AND ANALYSIS PROGRAM

Liquid Release Type	Sampling Frequency	Minimum Analysis Frequency	Type of Activity Analysis	Lower Limit of Detection (LLD) ($\mu\text{Ci/mL}$) ^a
A. Batch Waste Release ^d Tanks	P Each Batch	P Each Batch	Principal Gamma Emitters ^f	5×10^{-7}
1. Waste Monitor Tanks			I-131	1×10^{-6}
2. Condensate Demineralizer Backwash Receiving Tank	P One Batch/M	M	Dissolved and Entrained Gases (Gamma emitters)	1×10^{-5}
3. Nuclear Blowdown Monitor Tank	P Each Batch	M Composite ^b	H-3	1×10^{-5}
			Gross Alpha	1×10^{-7}
	P Each Batch	Q Composite ^b	Sr-89, Sr-90	5×10^{-8}
			Fe-55	1×10^{-6}
B. Continuous Release ^e	D Grab Sample	W Composite ^c	Principal Gamma Emitters ^f	5×10^{-7}
1. Steam Generator Blowdown			I-131	1×10^{-6}
2. Turbine Building Sump	M Grab Sample	M	Dissolved and Entrained Gases (Gamma emitters)	1×10^{-5}
3. Service Water Effluent Tank	D Grab Sample	M Composite ^c	H-3	1×10^{-5}
			Gross Alpha	1×10^{-7}
	D Grab Sample	Q Composite ^c	Sr-89, Sr-90	5×10^{-8}
			Fe-55	1×10^{-6}

See Table 1.1-3 for explanation of frequency notation.

TABLE 1-4 (Continued)

TABLE NOTATION

- a. The Lower Limit of Detection (LLD) is the smallest concentration of radioactive material in a sample that will yield a net count above background that will be detected with a 95% probability. LLD also yields a 5% probability of falsely concluding that a blank observation represents a "real" signal.

For a particular measurement system (which may include radiochemical separation):

$$LLD = \frac{4.66 s_b}{(E)(V)(2.22)(Y)(\exp(-\lambda \Delta t))}$$

Where:

LLD is the "a priori" lower limit of detection as defined above (as pCi per unit mass or volume). Current literature defines the LLD as the detection capability for the instrumentation only and the MDC, the minimum detectable concentration, as the detection capability for a given instrument procedure and type of sample.

4.66 is a factor which corrects for the smallest activity that has a probability, p, of being detected, and a probability, 1-p, of falsely concluding its presence.

$$4.66 = 2k \sqrt{1 + (t_b/t_s)}$$

k = a constant whose value depends on the chosen confidence level (NRC recommends a confidence level of 95%)

= 1.6545 at 95% confidence level

t_b = background time

t_s = sample time

s_b is the standard deviation of the background counting rate or the counting rate of blank sample as appropriate (as counts per minute),

E is the counting efficiency (as counts per transformation),

TABLE 1.1-4 (Continued)

TABLE NOTATION

V is the sample size (in units of mass or volume),

2.22 is the number of transformations per minute per picocurie,

Y is the fractional radiochemical yield (when applicable),

λ is the radioactive decay constant for the particular radionuclide,

and

Δt is the elapsed time between midpoint of sample collection and time of counting (for plant effluents, not environmental samples).

The value of s_b used in the calculation of the LLD for a detection system shall be used on the actual observed variance of the background counting rate or of the counting rate of the blank samples (as appropriate) rather than on an unverified theoretically predicted variance. In calculating the LLD for a radionuclide determined by gamma-ray spectrometry the background should include the typical contributions of other radionuclides normally present in the samples. Typical values of E , V , Y , and Δt shall be used in the calculation.

It should be recognized that the LLD is defined as an a priori (before the fact) limit representing the capability of a measurement system and not as a a posteriori (after the fact) limit for particular measurement.*

*For a more complete discussion of the LLD, and other detection limits, see the following:

- (1) HASL Procedures Manual, HASL-300 (revised annually).
- (2) Currie, L. A., "Limits for Qualitative Detection and Quantitative Determination - Application to Radiochemistry" Anal. Chem. 40, 586-93 (1968).
- (3) Hartwell, J. K., "Detection Limits for Radioisotopic Counting Techniques," Atlantic Richfield Handford Company Report ARH-2537 (June 22, 1972).

TABLE 1.1-4 (Continued)

TABLE NOTATION

- b. A composite sample is one in which the quantity of liquid sampled is proportional to the quantity of liquid waste discharged and in which the method of sampling employed results in a specimen which is representative of the liquids released.
- c. To be representative of the quantities and concentrations of radioactive materials in liquid effluents, samples shall be composited in proportion to the rate of flow of the effluent stream. Prior to analyses, all samples taken for the composite shall be thoroughly mixed in order for the composite sample to be representative of the effluent release.
- d. A batch release is the discharge of liquid wastes of a discrete volume. Prior to sampling for analyses, each batch shall be isolated, and then thoroughly mixed, by a method described in ODCM Section 2.0, to assure representative sampling.
- e. A continuous release is the discharge of liquid wastes of a nondiscrete volume; e.g., from a volume of system that has an input flow during the continuous release.
- f. The principal gamma emitters for which the LLD specification applies exclusively are the following radionuclides: Mn-54, Fe-59, Co-58, Co-60, Zn-65, Mo-99, Cs-134, Cs-137, Ce-141, and Ce-144. This list does not mean that only these nuclides are to be detected and reported. Other peaks which are measurable and identifiable, together with the above nuclides, shall also be identified and reported.

1.1.3 Liquid Effluents: Dose

LIMITING CONDITION FOR OPERATION

1.1.3.1 The dose or dose commitment to an individual from radioactive materials in liquid effluents released from the site (see Technical Specification Figure 5.1-4) shall be limited:

- a. During any calendar quarter to less than or equal to 1.5 mrem to the total body and to less than or equal to 5 mrem to any organ, and
- b. During any calendar year to less than or equal to 3 mrem to the total body and to less than or equal to 10 mrem to any organ.

APPLICABLE: At all Times.

ACTION:

- a. With the calculated dose from the release of radioactive materials in liquid effluents exceeding any of the above limits, in lieu of any other report required by ODCM Section 1.6, prepare and submit to the Commission within 30 days, pursuant to Technical Specification 6.9.2, a Special Report which identifies the cause (s) for exceeding the limit (s) and defines the corrective actions to be taken to the releases and the proposed actions to be taken to assure that subsequent releases will be in compliance with ODCM Specification 1.1.3.1.
- b. The provisions of Technical Specifications 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

1.1.3.2 Dose Calculations. Cumulative dose contributions from liquid effluents shall be determined in accordance with ODCM Section 2.2 at least once per 31 days.

ODCM, V.C. Summer, SCE&G Revision 13 (June 1990)

1.1.4 Liquid Waste Treatment

LIMITING CONDITION FOR OPERATION

1.1.4.1 The liquid radwaste treatment system shall be OPERABLE. The appropriate portions of the system shall be used to reduce the radioactive materials in liquid wastes prior to their discharge when the projected doses due to the liquid effluent from the site (See Technical Specification Figure 5.1-4) when averaged over 31 days, would exceed 0.06 mrem to the total body or 0.2 mrem to any organ.

APPLICABLE: At all Times.

ACTION:

- a. With the liquid radwaste treatment system inoperable for more than 31 days or with radioactive liquid waste being discharged without treatment and in excess of the above limits, in lieu of any other report required by ODCM, Section 1.6, prepare and submit to the Commission within 30 days, pursuant to Technical Specification 6.9.2, a Special Report which includes the following information:
 1. Identification of the inoperable equipment or subsystems and the reason for inoperability,
 2. Action(s) taken to restore the inoperable equipment to OPERABLE status, and
 3. Summary description of action(s) taken to prevent a recurrence.
- b. The provisions of Technical Specifications 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

1.1.4.2 Doses due to liquid releases shall be projected at least once per 31 days, in accordance with ODCM Section 2.2.

1.1.4.3 The liquid radwaste treatment system shall be demonstrated OPERABLE by operating the liquid radwaste treatment system equipment for at least 30 minutes at least once per 92 days unless the liquid radwaste system has been utilized to process radioactive liquid effluents during the previous 92 days.

1.2 GASEOUS EFFLUENTS

1.2.1 Radioactive Gaseous Effluent Monitoring Instrumentation

LIMITING CONDITION FOR OPERATION

1.2.1.1 The radioactive gaseous effluent monitoring instrumentation channels shown in Table 1.2-1 shall be OPERABLE with their alarm/trip setpoints set to ensure that the limits of ODCM Specification 1.2.2.1 are not exceeded. The alarm/trip setpoints of these channels shall be determined in accordance with ODCM Section 3.1.

APPLICABLE: As shown in Table 1.2-1

ACTION:

- a. With a radioactive gaseous effluent monitoring instrumentation channel alarm/trip setpoint less conservative than required by the above ODCM Specification, immediately suspend the release of radioactive gaseous effluents monitored by the affected channel or declare the channel inoperable.
- b. With less than the minimum number of radioactive gaseous effluent monitoring instrumentation channels OPERABLE, take the ACTION shown in Table 1.2-1. Additionally if this condition prevails for more than 30 days, in the next semiannual effluent report, explain why this condition was not corrected in a timely manner.
- b. The provisions of Technical Specifications 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

1.2.1.2 Each radioactive gaseous effluent monitoring instrumentation channel shall be demonstrated OPERABLE by performance of the CHANNEL CHECK, SOURCE CHECK, CHANNEL CALIBRATION and and ANALOG CHANNEL OPERATIONAL TEST operations at the frequencies shown in Table 1.2-2.

TABLE 1.2-1

RADIOACTIVE GASEOUS EFFLUENT MONITORING INSTRUMENTATION		MINIMUM CHANNELS OPERABLE	APPLICA- BILITY	ACTION
	<u>INSTRUMENT</u>			
1.	WASTE GAS HOLDUP SYSTEM			
a.	Noble Gas Activity Monitor - Providing Alarm and Automatic Termination of Release (RM-A10 or RM-A3)	1	*	7
2.	MAIN PLANT VENT EXHAUST SYSTEM			
a.	Noble Gas Activity Monitor - Providing Alarm and Automatic Termination of Release from Waste Gas Holdup System (RM- A3)	1	*	9
b.	Iodine Sampler	1	*	11
c.	Particulate Sample	1	*	11
d.	Flow Rate Measuring Device	1	*	8
e.	Sampler Flow Rate Measuring Device	1	*	8
3.	REACTOR BUILDING PURGE SYSTEM			
a.	Noble Gas Activity Monitor Providing Alarm and Automatic Termination of Release (RM-A4)	1	*	10
b.	Iodine Sampler	1	*	11
c.	Particulate Sample	1	*	11
d.	Flow Rate Measuring Device	1	*	8
e.	Sampler Flow Rate Measuring Device	1	*	8

TABLE 1.2-1 (Continued)

TABLE NOTATION

* At all times during releases via this pathway.

ACTION 7 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, the contents of the tank(s) may be released to the environment for up to 14 days provided that prior to initiating the release:

- a. At least two independent samples of the tank's contents are analyzed, and
- b. At least two technically qualified members of the Facility Staff independently verify the release rate calculations and discharge valve lineup;

Otherwise, suspend release of radioactive effluents via this pathway.

ACTION 8 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue for up to 30 days provided the flow rate is estimated at least once per 4 hours.

ACTION 9 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue for up to 30 days provided grab samples are taken at least once per 8 hours and these samples are analyzed for gross activity within 24 hours.

TABLE 1.2-1 (Continued)

TABLE NOTATION

- ACTION 10 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, immediately suspend PURGING of radioactive effluents via this pathway.
- ACTION 11 - With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via the affected pathway may continue for up to 30 days provided samples are continuously collected with auxiliary sampling equipment as required in Table 1.2-3.

TABLE 1.2-2

RADIOACTIVE GASEOUS EFFLUENT
MONITORING INSTRUMENTATION SURVEILLANCE REQUIREMENTS

	INSTRUMENT	CHANNEL CHECK	SOURCE CHECK	CHANNEL CALIBRATION	ANALOG CHANNEL OPERATIONAL TEST	MODES IN WHICH SURVEILLANCE REQUIRED
1.	WASTE GAS HOLDUP SYSTEM					
a.	Noble Gas Activity Monitor - RM-A10 or RM-A3	P	P	R(3)	Q(1)	*
2.	MAIN PLANT VENT EXHAUST SYSTEM					
a.	Noble Gas Activity Monitor - RM-A3	D	M	R(3)	Q(2)	*
b.	Iodine Sampler	W	N.A.	N.A.	N.A.	*
c.	Particulate Sampler	W	N.A.	N.A.	N.A.	*
d.	Flow Rate Measuring Device	D	N.A.	R	Q	*
e.	Sampler Flow Rate Monitor	D	N.A.	R	Q	*
3.	REACTOR BUILDING PURGE SYSTEM					
a.	Noble Gas Activity Monitor - RM-A4	D	P,M	R(3)	Q(1)	*
b.	Iodine Sampler	W	N.A.	N.A.	N.A.	*
c.	Particulate Sampler	W	N.A.	N.A.	N.A.	*
d.	Flow Rate Measuring Device	D	N.A.	R	Q	*
e.	Sampler Flow Rate Monitor	D	N.A.	R	Q	*

See Table 1.1-3 for explanation of frequency notation.

TABLE 1.2-2 (Continued)

TABLE NOTATION

* At all times.

- (1) The ANALOG CHANNEL OPERATIONAL TEST shall also demonstrate that automatic isolation of this pathway and control room alarm annunciation occurs if any of the following conditions exists:
 1. Instrument indicates measured levels above the alarm/trip setpoint.
 2. Loss of Power (alarm only).
 3. Low flow (alarm only).
 4. Instrument indicates a downscale failure (alarm only).
 5. Normal/Bypass switch set in Bypass (alarm only).
 6. Other instrument controls not set in operate mode.

- (2) The ANALOG CHANNEL OPERATIONAL TEST shall also demonstrate that control room alarm annunciation occurs if any of the following conditions exists:
 1. Instrument indicates measured levels above the alarm setpoint.
 2. Loss of Power.
 3. Low flow.
 4. Instrument indicates a downscale failure.
 5. Instrument controls not set in operate mode.

- (3) The initial CHANNEL CALIBRATION shall be performed using one or more of the reference standards certified by the National Institute of Standards and Technology (NIST) or using standards that have been obtained from suppliers that participate in measurement assurance activities with NIST. These standards shall permit calibrating the system over its intended range of energy and measurement range. For subsequent CHANNEL CALIBRATION, sources that have been related to the initial calibration shall be used.

1.2.2 Gaseous Effluents: Dose Rate

LIMITING CONDITION FOR OPERATION

1.2.2.1 The dose rate in unrestricted areas due to radioactive materials released in gaseous effluents from the site (see Technical Specification Figure 5.1-3) shall be limited to the following:

- a. For noble gases: Less than or equal to 500 mrem/yr to the total body and less than or equal to 3000 mrem/yr to the skin, and
- b. For all radioiodines and for all radioactive materials in particulate form and tritium with half lives greater than 8 days: Less than or equal to 1500 mrem/yr to any organ.

APPLICABLE: At all Times.

ACTION:

With the dose rate(s) exceeding the above limits, immediately decrease the release rate to within the above limit(s).

SURVEILLANCE REQUIREMENTS

1.2.2.2 The dose rate due to noble gases in gaseous effluents shall be determined to be within the above limits in accordance with the methods and procedures of the ODCM.

1.2.2.3 The dose rate due to radioiodines, tritium and radioactive materials in particulate form with half lives greater than 8 days in gaseous effluents shall be determined to be within the above limits in accordance with the methods and procedures of ODCM Section 3.2.2 by obtaining representative samples and performing analyses in accordance with the sampling and analysis program specified in Table 1.2-3.

TABLE 1.2-3

RADIOACTIVE GASEOUS WASTE SAMPLING AND ANALYSIS PROGRAM

Gaseous Release Type	Sampling Frequency	Minimum Analysis Frequency	Type of Activity Analysis	Lower Limit of Detection (LLD) ($\mu\text{Ci/ml}$) ^a
A. Waste Gas Storage Tank	P Each Tank Grab Sample	P Each Tank	Principal Gamma Emitters ⁹	1X10 ⁻⁴
B1 Reactor Building -36" Purge Line	P Each Purge ^{b,c}	P Each Purge ^b	Principal Gamma Emitters ⁹	1X10 ⁻⁴
-6" Purge Line			H-3	1X10 ⁻⁶
B2 Reactor Building -6" Purge Line (if continuous)	M ^b Grab Sample	M ^b	Principal Gamma Emitters ⁹	1X10 ⁻⁴
			H-3	1X10 ⁻⁶
C. Main Plant Vent	M ^{b,e} Grab Sample	M ^b	Principal Gamma Emitters ⁹	1X10 ⁻⁴
			H-3	1X10 ⁻⁶
D1. Reactor Building Purge	Continuous Sampler ^f	W ^d Charcoal Sample	I-131 I-133	1X10 ⁻¹² 1X10 ⁻¹⁰
2. Main Plant Vent	Continuous Sampler ^f	W ^d Particulate Sample	Principal Gamma Emitters ⁹ I-131, others	1X10 ⁻¹¹
	Continuous Sampler ^f	M Composite Particulate Sample	Gross Alpha	1X10 ⁻¹¹
	Continuous Sampler ^f	Q Composite Particulate Sample	Sr-89, Sr-90	1X10 ⁻¹¹
	Continuous Monitor	Noble Gas Monitor	Noble Gases Gross Beta	2X10 ⁻⁶

See Table 1.1-3 for explanation of frequency notation.

TABLE 1.2-3 (Continued)

TABLE NOTATION

- a. See Table 1.1-4 notation (a) for definition of LLD.
- b. Analyses shall be also be performed within 24 hours following shutdown, startup, or a THERMAL POWER change exceeding 15 percent of the RATED THERMAL POWER within a one hour period.
- c. Tritium grab samples shall be taken at least once per 24 hours when the refueling canal is flooded.
- d. Samples shall be changed at least once per 7 days and analyses shall be completed within 48 hours after changing (or after removal from sampler). Sampling shall also be performed at least once per 24 hours for a least 7 days following each shutdown, startup or THERMAL POWER change exceeding 15 percent of RATED THERMAL POWER in one hour and analyses shall be completed within 48 hours of changing. When samples collected for 24 hours are analyzed, the corresponding LLD's may be increased by a factor of 10.
- e. Tritium grab samples shall be taken at least once per 7 days from the ventilation exhaust from the spent fuel pool area, whenever spent fuel is in the spent fuel pool.
- f. The ratio of the sample flow rate to the sampled stream flow rate shall be known for the time period covered by each dose or dose rate calculation made in accordance with ODCM Specifications 1.2.2.1, 1.2.3.1 and 1.2.4.1.
- g. The principal gamma emitters for which the LLD specification applies exclusively are the following radionuclides: Kr-87, Kr-88, Xe-133, Xe-133m, Xe-135, and Xe-138 for gaseous emissions and Mn-54, Fe-59, Co-58, Co-60, Zn-65, Mo-99, Cs-134, Cs-137, Ce-141 and Ce-144 for particulate emissions. This list does not mean that only these nuclides are to be detected and reported. Other peaks which are measurable and identifiable, together with the above nuclides, shall also be identified and reported.

1.2.3 Gaseous Effluents: Dose - Noble Gas

LIMITING CONDITION FOR OPERATION

1.2.3.1 The air dose due to noble gases released in gaseous effluents from the site (see Technical Specification Figure 5.1-3) shall be limited to the following:

- a. During any calendar quarter: Less than or equal to 5 mrad for gamma radiation and less than or equal to 10 mrad for beta radiation and,
- b. During any calendar year: Less than or equal to 10 mrad for gamma radiation and less than or equal to 20 mrad for beta radiation.

APPLICABLE: At all Times.

ACTION:

- a. With the calculated air dose from radioactive noble gases in gaseous effluents exceeding any of the above limits, in lieu of any other report required by ODCM section 1.6, prepare and submit to the Commission within 30 days, pursuant to Technical Specification 6.9.2, a Special Report which identifies the cause(s) for exceeding the limit(s) and defines the corrective actions to be taken to releases and the proposed corrective actions to be taken to assure that subsequent releases will be in compliance with ODCM Specification 1.2.3.1.
- b. The provisions of Technical Specifications 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

1.2.3.2 Dose Calculations Cumulative dose contributions for the current calendar quarter and current calendar year shall be determined in accordance with ODCM Section 3.2.3 at least once per 31 days.

1.2.4 Gaseous Effluents: Dose - Radioiodines, Tritium, and Radioactive Materials in Particulate Form.

LIMITING CONDITION FOR OPERATION

1.2.4.1 The dose to an individual from radioiodines, tritium, and radioactive materials in particulate form, and radionuclides (other than noble gases) with half-lives greater than 8 days in gaseous effluents (see Technical Specification Figure 5.1-3) shall be limited to the following:

- a. During any calendar quarter: Less than or equal to 7.5 mrem to any organ and,
- b. During any calendar year: Less than or equal to 15 mrem to any organ.

APPLICABLE: At all Times.

ACTION:

- a. With the calculated dose from the release of tritium, radioiodines, and radioactive materials in particulate form with half lives greater than 8 days in gaseous effluents exceeding any of the above limits, in lieu of any other report required by ODCM Section 1.6, prepare and submit to the Commission within 30 days, pursuant to Technical Specification 6.9.2, a Special Report which identifies the cause(s) for exceeding the limit and defines the corrective actions to be taken to releases and the proposed actions to be taken to assure that subsequent release will be in compliance with ODCM Specification 1.2.4.1.
- b. The provisions of Technical Specifications 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

1.2.4.2 Dose Calculations Cumulative dose contributions for the current calendar quarter and current calendar year shall be determined in accordance with ODCM Section 3.2.3 at least once per 31 days.

1.2.5 Gaseous Effluents: Gaseous Radwaste Treatment

LIMITING CONDITION FOR OPERATION

1.2.5.1 The GASEOUS RADWASTE TREATMENT SYSTEM and the VENTILATION EXHAUST TREATMENT SYSTEM shall be OPERABLE. The appropriate portions of the GASEOUS RADWASTE TREATMENT SYSTEM shall be used to reduce radioactive materials in gaseous waste prior to their discharge when the projected gaseous effluent air doses due to gaseous effluent releases from the site (See Technical Specification Figure 5.1-3), when averaged over 31 days, would exceed 0.2 mrad for gamma radiation and 0.4 mrad for beta radiation. The appropriate portions of the VENTILATION EXHAUST TREATMENT SYSTEM shall be used to reduce radioactive materials in gaseous waste prior to their discharge when the projected doses due to gaseous effluent releases from the site when averaged over 31 days would exceed 0.3 mrem to any organ.

APPLICABLE: At all Times.

ACTION:

- a. With the GASEOUS RADWASTE TREATMENT SYSTEM and/or the VENTILATION EXHAUST TREATMENT SYSTEM inoperable for more than 31 days or with gaseous waste being discharged without treatment and in excess of the above limits, in lieu of any other report required by ODCM section 1.6, prepare and submit to the Commission within 30 days, pursuant to Technical Specification 6.9.2, a Special Report which includes the following information:
1. Identification of the inoperable equipment or subsystems and the reason for inoperability;
 2. Action(s) taken to restore the inoperable equipment to OPERABLE status, and
 3. Summary description of action(s) taken to prevent a recurrence.

- b. The provisions of Technical Specifications 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

1.2.5.2 Doses due to gaseous releases from the reactor shall be projected at least once per 31 days, in accordance with ODCM Section 3.2.2 for air doses and ODCM Section 3.2.3 for organ doses.

1.2.5.3 The GASEOUS RADWASTE TREATMENT SYSTEM and VENTILATION EXHAUST TREATMENT SYSTEM shall be demonstrated OPERABLE by operating the GASEOUS RADWASTE TREATMENT SYSTEM equipment and VENTILATION EXHAUST TREATMENT SYSTEM equipment for at least 30 minutes, at least once per 92 days unless the appropriate system has been utilized to process radioactive gaseous effluents during the previous 92 days.

1.3 RADIOACTIVE EFFLUENTS: TOTAL DOSE

LIMITING CONDITION FOR OPERATION

1.3.1 The dose or dose commitment to any member of the public, due to releases of radioactivity and radiation, from uranium fuel cycle sources shall be limited to less than or equal to 25 mrem to the total body or any organ (except the thyroid, which shall be limited to less than or equal to 75 mrem) over 12 consecutive months.

APPLICABLE: At all Times.

ACTION:

- a. With the calculated doses from the release of radioactive materials in liquid or gaseous effluents exceeding twice the limits of ODCM Specification 1.1.3.1.a, 1.1.3.1.b, 1.2.3.1.a, 1.2.3.1.b, 1.2.4.1.a, or 1.2.4.1.b, in lieu of any other report required and ODCM Section 1.6, prepare and submit to the Commission, within 30 days, pursuant to Technical Specification 6.9.2, a Special Report which defines the corrective action to be taken to reduce subsequent releases to prevent recurrence of exceeding the limits of ODCM Specification 1.3.1. This Special Report shall include an analysis which estimates the radiation exposure (dose) to a member of the public from uranium fuel cycle sources (including all effluent pathways and direct radiation) for a 12 consecutive month period that includes the release(s) covered by this report. If the estimated dose(s) exceeds the limits of ODCM Specification 1.3.1, and if the release condition resulting in violation of 40 CFR 190 has not already been corrected, the Special Report shall include a request for a variance in accordance with the provisions of 40 CFR 190 and including information of § 190.11 (b). Submittal of the report is considered a timely request, and a variance is granted until staff action on the request is complete. The variance only relates to the limits of 40 CFR 190, and does not apply in any way to the requirements for dose

limitation of 10 CFR Part 20, as addressed in ODCM Specifications 1.1.2 and 1.2.2.

- b. The provisions of Technical Specifications 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

1.3.2 Dose Calculations Cumulative dose contributions from liquid and gaseous effluents shall be determined in accordance with ODCM Specifications 1.1.3.2, 1.2.3.2 and 1.2.4.2.

1.4 RADIOLOGICAL ENVIRONMENTAL MONITORING

1.4.1 Monitoring Program

LIMITING CONDITION FOR OPERATION

1.4.1.1 The radiological environmental monitoring program shall be conducted as specified in Table 1.4-i.

APPLICABILITY: At all times.

ACTION:

- a. With the radiological environmental monitoring program not being conducted as specified in Table 1.4-1 in lieu of any other report required by ODCM Section 1.6, prepare and submit to the Commission, in the Annual Radiological Operating Report, a description of the reasons for not conducting the program as required and the plans for preventing a recurrence.
- b. With the level of radioactivity in an environmental sampling medium exceeding the reporting levels of Table 1.4-2 when averaged over any calendar quarter, in lieu of any other report required by ODCM Section 1.6, prepare and submit to the Commission within 30 days from the end of the affected calendar quarter a Special Report. When more than one of the radionuclides in Table 1.4-2 are detected in the sampling medium, this report shall be submitted if:

$$\frac{\text{concentration (1)}}{\text{limit level (1)}} + \frac{\text{concentration (2)}}{\text{limit level (2)}} + \dots \geq 1.0$$

When radionuclides other than those in Table 1.4-2 are detected and are the result of plant effluents, this report shall be submitted if the potential annual dose to an individual is equal to or greater than the calendar year limits of ODCM Specifications 1.1.3.1, 1.2.3.1

and 1.2.4.1. This report is not required if the measured level of radioactivity was not the result of plant effluents; however, in such an event, the condition shall be reported and described in the Annual Radiological Environmental Operating Report.

- c. With milk or fresh leafy vegetable samples unavailable from one or more of the sample locations required by Table 1.4-1, in lieu of any other report required by ODCM Section 1.6 prepare and submit to the Commission within 30 days, pursuant to Technical Specification 6.9.2, a Special Report which identifies the cause of the unavailability of samples and identifies locations for obtaining replacement samples. The locations from which samples were unavailable may then be deleted from those required by Table 1.4-1, provided the locations from which the replacement samples were obtained are added to the environmental monitoring program as replacement locations.
- d. The provisions of Technical Specifications 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

1.4.1.2 The radiological environmental monitoring samples shall be collected pursuant to Table 1.4-1 and shall be analyzed pursuant to the requirements of Tables 1.4-1 and 1.4-3.

Table 1.4-1 Radiological Environmental Monitoring Program
Virgil C. Summer Nuclear Station

Table 1.4-1 Radiological Environmental Monitoring Program
Virgil C. Summer Nuclear Station

Exposure Pathway and/or Sample	Minimum Number of Sample Locations and Criteria for Selection	Sampling and Collection Frequency	Type & Frequency of Analysis
AIRBORNE: I. Particulates	A) 3 Indicator samples to be taken at locations (in different sectors) beyond but as close to the exclusion boundary as practicable where the highest offsite sectorial ground level concentrations are anticipated. (1)	Continuous sampler operation with weekly collection.	Gross beta following filter change; quarterly composite (by location) for gamma isotopic.
	B) 1 Indicator sample to be taken in the sector beyond but as close to the exclusion boundary as practicable corresponding to the residence having the highest anticipated offsite ground level concentration or dose. (1)	Continuous sampler operation with weekly collection.	Gross beta following filter change; quarterly composite (by location) for gamma isotopic.
	C) 1 Indicator sample to be taken at the location of one of the dairies most likely to be affected. (1) (2)	Continuous sampler operation with weekly collection.	Gross beta following filter change; quarterly composite (by location) for gamma isotopic.
	D) 1 Control sample to be taken at a location at least 10 air miles from the site and not in the most prevalent wind directions. (1)	Continuous sampler operation with weekly collection.	Gross beta following filter change; quarterly composite (by location) for gamma isotopic.
II. Radioiodine	A) 3 Indicator samples to be taken at two locations as given in I.A. above.	Continuous sampler operation with weekly canister collection.	Gamma isotopic for I-131 weekly.
	B) 1 Indicator sample to be taken at the location as given in I.B. above.	Continuous sampler operation with weekly canister collection.	Gamma isotopic for I-131 weekly.
	C) 1 Indicator sample to be taken at the location as given in I.C. above.	Continuous sampler operation with weekly canister collection.	Gamma isotopic for I-131 weekly.
	D) 1 Control sample to be taken at a location as given in I.D. above.	Continuous sampler operation with weekly canister collection.	Gamma isotopic for I-131 weekly.
III. Direct	A) 13 Indicator stations with two or more dosimeters to form an inner ring of stations in the 13 accessible sectors within 1 to 2 miles of the plant.	Monthly or quarterly (3,5)	Gamma dose monthly or quarterly.
	B) 16 Indicator stations with two or more dosimeters to form an outer ring of stations in the 16 accessible sectors within 3 to 5 miles of the plant.	Monthly or quarterly (3,5)	Gamma dose monthly or quarterly.
	C) 8 Stations with two or more dosimeters to be placed in special interest areas such as population centers, nearby residences, schools and in 2 or 3 areas to serve as control stations.	Monthly or quarterly (3,5)	Gamma dose monthly or quarterly.

Table 1.4-1 Radiological Environmental Monitoring Program
Virgil C. Summer Nuclear Station

Exposure Pathway and/or Sample	Minimum Number of Sample Locations and Criteria for Selection	Sampling and Collection Frequency	Type & Frequency of Analysis
WATERBORNE: IV. Surface Water	A) 1 Indicator sample downstream to be taken at a location which allows for mixing and dilution in the ultimate receiving river.	Time composite samples with collection every month (corresponds to USGS continuous sampling site) (3)	Gamma isotopic monthly with quarterly composite (by location) or monthly sample to be analyzed for tritium (5)
	B) 1 Control sample to be taken at a location on the receiving river sufficiently far upstream such that no effects of pumped storage operation are anticipated.	Time composite samples with collection every month (corresponds to USGS continuous sampling site) (3)	Gamma isotopic monthly with quarterly composite (by location) or monthly sample to be analyzed for tritium (5)
	C) 1 Indicator sample from a location immediately upstream of the nearest downstream municipal water supply.	Time composite samples with collection every month (corresponds to USGS continuous sampling site) (3)	Gamma isotopic monthly with quarterly composite (by location) or monthly sample to be analyzed for tritium (5)
	D) 1 Indicator sample to be taken in the upper reservoir of the pumped storage facility in the plant discharge canal.	Time composite samples with collection every month (corresponds to USGS continuous sampling site) (3)	Gamma isotopic monthly with quarterly composite (by location) or monthly sample to be analyzed for tritium (5)
	E) 1 Indicator sample to be taken in the upper reservoir's non-fluctuating recreational area.	Grab sampling monthly (3)	Gamma isotopic monthly with quarterly composite (by location) or monthly sample to be analyzed for tritium (5)
	F) 1 Control sample to be taken at a location on a separate unaffected watershed reservoir.	Grab sampling monthly (3)	Gamma isotopic monthly with quarterly composite (by location) or monthly sample to be analyzed for tritium (5)
V. Ground Water	A) 2 Indicator samples to be taken within the exclusion boundary and in the direction of potentially affected ground water supplies.	Quarterly grab sampling (5)	Gamma isotopic and tritium analyses quarterly (5)
	B) 1 Control sample from unaffected location.	Quarterly grab sampling (5)	Gamma isotopic and tritium analyses quarterly (5)
VI. Drinking Water	A) 1 Indicator sample from a nearby public ground water supply source.	Monthly grab sampling (3)	Monthly (3) gamma isotopic and gross beta analyses and quarterly (5) composite for tritium analyses.
	B) 1 Indicator (finished water) sample from the nearest downstream water supply.	Monthly composite sampling.	Monthly (3) gamma isotopic and gross beta analyses and quarterly (5) composite for tritium analyses.
	C) 1 Control (finished water) sample from the nearest unaffected public water supply.	Monthly composite sampling.	Monthly (3) gamma isotopic and gross beta analyses and quarterly (5) composite for tritium analyses.

Table 1.4-1 Radiological Environmental Monitoring Program
Virgil C. Summer Nuclear Station

Exposure Pathway and/or Sample	Minimum Number of Sample Locations and Criteria for Selection	Sampling and Collection Frequency	Type & Frequency of Analysis
INGESTION: VII. Milk(2)	A) Samples from milking animals in 3 locations within 5 km distance having the highest dose potential. If there are none then 1 sample from milking animals in each of 3 areas between 5 to 8 km distance where doses are calculated to be greater than 1 mrem per year.	Semi-monthly when animals are on pasture, (6) monthly other times (3)	Gamma isotopic and I-131 analysis semi-monthly (6) when animals are on pasture; monthly (3) at other times.
	B) 1 Control sample to be taken at the location of a dairy greater than 20 miles distance and not in the most prevalent wind direction (1)	Semi-monthly when animals are on pasture, (6) monthly other times (3)	Gamma isotopic and I-131 analysis semi-monthly (6) when animals are on pasture; monthly (3) at other times.
	C) 1 indicator grass (forage) sample to be taken at one of the locations beyond but as close to the exclusion boundary as practicable where the highest outside sectorial ground level concentrations are anticipated (1)	Monthly when available (3)	Gamma isotopic.
	D) 1 Indicator grass (forage) sample to be taken at the location of VII(A) above when animals are on pasture.	Monthly when available (3)	Gamma isotopic.
	E) 1 Control grass (forage) sample to be taken at the location of VII(B) above	Monthly when available (3)	Gamma isotopic.
VIII. Food Product	A) 2 samples of broadleaf vegetation grown in the 2 nearest offsite location of highest calculated annual average ground level D/Q if milk sampling is not performed within 3 km or if milk sampling is not performed at a location within 5-10 km where the doses are calculated to be greater than 1 mrem/yr.	Monthly when available (3)	Gamma isotopic on edible portion.
	B) 1 Control sample for the same foods taken at a location at least 10 miles distance and not in the most prevalent wind direction if milk sampling is not performed within 3 km or if milk sampling is not at a location within 5 to 8 km where doses are calculated to be greater than 1 mrem/yr.	Monthly when available (3)	Gamma isotopic on edible portion.
IX. Fish	A) 1 indicator sample to be taken at a location in the upper reservoir.	Semiannual (7) collection of the following species types if available: bass; bream, crappie; catfish, carp; forage fish (shad).	Gamma isotopic on edible portions semiannually.
	B) 1 indicator sample to be taken at a location in the lower reservoir.	Semiannual (7) collection of the following species types if available: bass; bream, crappie; catfish, carp; forage fish (shad).	Gamma isotopic on edible portions semiannually.
	C) 1 indicator sample to be taken at a location in the upper reservoir's non-fluctuating recreational area.	Semiannual (7) collection of the following species types if available: bass; bream, crappie; catfish, carp; forage fish (shad).	Gamma isotopic on edible portions semiannually.

Table 1.4-1 Radiological Environmental Monitoring Program
Virgil C. Summer Nuclear Station

Exposure Pathway and/or Sample	Minimum Number of Sample Locations and Criteria for Selection	Sampling and Collection Frequency	Type & Frequency of Analysis
IX. Fish (continued)	D) 1 Control sample to be taken at a location on the receiving river sufficiently far upstream such that no effects of pumped storage operation are anticipated	Semiannual(7) collection of the following species types if available: bass; bream, crappie; catfish, carp; forage fish (shad).	Gamma isotopic on edible portions semiannually.
AQUATIC: X. Sediment	<p>A) 1 indicator sample to be taken at a location in the upper reservoir.</p> <p>B) 1 indicator sample to be taken at a location in the upper reservoir's non-fluctuating recreation area.</p> <p>C) 1 indicator sample to be taken on the shoreline of the lower reservoir.</p> <p>D) 1 Control sample to be taken at a location on the receiving river sufficiently far upstream such that no effects of pumped storage operation are anticipated.</p>	<p>Semiannual grab sample (7)</p> <p>Semiannual grab sample (7)</p> <p>Semiannual grab sample (7)</p> <p>Semiannual grab sample (7)</p>	<p>Gamma isotopic</p> <p>Gamma isotopic</p> <p>Gamma isotopic</p> <p>Gamma isotopic</p>

NOTES

1. Sample site locations are based on the meteorological analysis for the period of record as presented in Chapters 5 and 6 of the OLER.
2. Milking animal and garden survey results will be analyzed annually. Should the survey indicate new dairying activity, the owners shall be contacted with regard to a contract for supplying sufficient samples. If contractual arrangements can be made, site(s) will be added for additional milk sampling up to a total of 3 Indicator locations.
3. Not to exceed 35 days.
4. Time composite samples are samples which are collected with equipment capable of collecting an aliquot at time intervals which are short (e.g., hourly) relative to the compositing period.
5. At least once per 100 days.
6. At least once per 18 days.
7. At least once per 200 days.

NOTE: Deviations from this sampling schedule may occasionally be necessary if sample media are unobtainable due to hazardous conditions, seasonal unavailability, insufficient sample size, malfunctions of automatic sampling or analysis equipment and other legitimate reasons. If specimens are unobtainable due to sampling equipment malfunction, every effort shall be made to complete corrective action prior to the end of the next sampling period. Deviations from sampling-analysis schedules will be described in the annual report.

TABLE 1.4-2

Reporting Levels for Radioactivity Concentrations in Environmental Samples
Reporting Levels

Analysis	Water (pCi/l)	Airborne Particulate or Gases(pCi/m ³)	Fish (pCi/kg, wet)	Milk (pCi/l)	Food Products (pCi/Kg, wet)
H-3	20,000(a)	N.A.	N.A.	N.A.	N.A.
Mn-54	1,000	N.A.	30,000	N.A.	N.A.
Fe-59	400	N.A.	10,000	N.A.	N.A.
Co-58	1,000	N.A.	30,000	N.A.	N.A.
Co-60	300	N.A.	10,000	N.A.	N.A.
Zn-65	300	N.A.	20,000	N.A.	N.A.
Zr-95	400	N.A.	N.A.	N.A.	N.A.
Nb-95	400	N.A.	N.A.	N.A.	N.A.
I-131	2	0.9	N.A.	3	100
Cs-134	30	10	1,000	60	1,000
Cs-137	50	20	2,000	70	2,000
Ba-140	200	N.A.	N.A.	300	N.A.
La-140	200	N.A.	N.A.	300	N.A.

(a) For drinking water samples. This is the 40 CFR Part 141 value.

TABLE 1.4-3

Maximum Values for the Lower Limits of Detection (LLD)^{a,c}
Reporting Levels

Analysis	Water (pCi/l)	Airborne Particulate or Gases(pCi/m ³)	Fish (pCi/kg, wet)	Milk (pCi/l)	Food Products (pCi/Kg, wet)	Sediment (pCi/Kg, dry)
Gross Beta	4	1 X 10 ⁻²	N.A.	N.A.	N.A.	N.A.
H-3	2000(b)	N.A.	N.A.	N.A.	N.A.	N.A.
Mn-54	15	N.A.	130	N.A.	N.A.	N.A.
Fe-59	30	N.A.	260	N.A.	N.A.	N.A.
Co-58	15	N.A.	130	N.A.	N.A.	N.A.
Co-60	15	N.A.	130	N.A.	N.A.	N.A.
Zn-65	30	N.A.	260	N.A.	N.A.	N.A.
Zr-95	30	N.A.	N.A.	N.A.	N.A.	N.A.
Nb-95	15	N.A.	N.A.	N.A.	N.A.	N.A.
I-131	1b	7 X 10 ⁻²	N.A.	1	60	N.A.
Cs-134	15	5 X 10 ⁻²	130	15	60	150
Cs-137	18	6 X 10 ⁻²	150	18	80	130
Ba-140	60	N.A.	N.A.	60	N.A.	N.A.
La-140	15	N.A.	N.A.	15	N.A.	N.A.

TABLE 1 4-3 (Continued)

TABLE NOTATION

- a. Table 1.4-3 lists detection capabilities for radioactive materials in environmental samples. These detection capabilities are tabulated in terms of the lower limits of detection (LLDs). See Table 1.1-4 notation (a) for definition of LLD.
- b. LLD for drinking water samples.
- c. Other peaks potentially due to reactor operations (fission and activation products) which are measurable and identifiable, together with the radionuclides in Table 1.4-3, shall be identified and reported.

1.4.2 Land Use Census

LIMITING CONDITION FOR OPERATION

1.4.2.1 A land use census shall be conducted and shall identify the location of the nearest milk animal, the nearest residence and the nearest garden* of greater than 500 square feet producing fresh leafy vegetables in each of the 16 meteorological sectors within a distance of five miles.

APPLICABILITY: At all times.

ACTION:

- a. With a land use census identifying a location(s) which yields a calculated dose or dose commitment greater than the values currently being calculated in ODCM Specification 1.2.4.2, in lieu of any other report required by ODCM Section 1.6, prepare and submit to the Commission within 30 days, pursuant to Technical Specification 6.9.2, a Special Report which identifies the new location(s).
- b. With a land use census identifying a location(s) which yields a calculated dose or dose commitment (via the same exposure pathway) 20 percent greater than at a location from which samples are currently being obtained in accordance with ODCM Specification 1.4.1.1, in lieu of any other report required by ODCM Section 1.6, prepare and submit to the Commission within 30 days, pursuant to Technical Specification 6.9.2, a Special Report which identifies the new location. The new location shall be added to the radiological environmental monitoring program within 30 days. The sampling location, excluding the control station location, having the lowest calculated dose or dose commitment (via the same exposure pathway) may be deleted from this monitoring program after October 31 of the year in which this land use census was conducted.

*Broad leaf vegetation sampling may be performed at the site boundary in the direction sector with the highest D/Q in lieu of the garden census.

- c. The provisions of Technical Specifications 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

1.4.2.2 The land use census shall be conducted at least once per 12 months between the dates of June 1 and October 1 using that information which will provide the best results, such as by a door-to-door survey, aerial survey, or by consulting local agriculture authorities.

1.4.3 Interlaboratory Comparison Program

LIMITING CONDITION FOR OPERATION

1.4.3.1 Analyses shall be performed on radioactive materials supplied as part of an Interlaboratory Comparison Program which has been approved by the Commission.

APPLICABILITY: At all times.

ACTION:

- a. With analyses not being performed as required above, report the corrective actions taken to prevent a recurrence to the Commission in the Annual Radiological Environmental Operating Report.
- b. The provisions of Technical Specifications 3.0.3 and 3.0.4 are not applicable.

SURVEILLANCE REQUIREMENTS

1.4.3.2 A summary of the results obtained as part of the above required Interlaboratory Comparison Program shall be included in the Annual Radiological Environmental Operating Report (participants in the EPA crosscheck program shall provide the EPA program code designation for the unit).

1.5 BASES

B/1.1 LIQUID EFFLUENTS

B/1.1.1 Radioactive Liquid Effluent Monitoring Instrumentation

The radioactive liquid effluent instrumentation is provided to monitor and control, as applicable, the releases of radioactive materials in liquid effluents during actual or potential releases of liquid effluents. The alarm/trip setpoints for these instruments shall be calculated in accordance with the procedures in the ODCM to ensure that the alarm/trip will occur prior to exceeding the limits of 10 CFR Part 20. The OPERABILITY and use of this instrumentation is consistent with the requirements of General Design Criteria 60, 63 and 64 of Appendix A to 10CFR Part 50.

B/1.1.2 Concentration

This specification is provided to ensure that concentration of radioactive materials released in liquid waste effluents from the site will be less than the concentration levels specified in 10 CFR Part 20, Appendix B, Table II, Column 2. This limitation provides additional assurance that the levels of radioactive materials in bodies of water outside the site will result in exposures within:

- (1) the Section II.A design objectives of Appendix I, 10 CFR 50, to an individual, and
- (2) the limits of 10 CFR 20.106 (e) to the population.

The concentration limit for dissolved or entrained noble gases is based upon the assumption that Xe-135 the controlling radioisotope and its MPC in air (submersion) was converted to an equivalent concentration in water using the methods described in International Commission on Radiological Protection (ICRP) Publication 2.

B/1.1.3 Dose

This specification is provided to implement the requirements of Sections II.A, III.A and IV.A of Appendix I, 10 CFR Part 50. The Limiting Condition for Operation implements the guides set forth in Section II.A. of Appendix I. The ACTION statements provide the required operating flexibility and at the same time implement the guides set forth in Section IV.A of Appendix I to assure that the releases of radioactive material in liquid effluents will be kept "as low as is reasonably achievable." Also, for fresh water sites with drinking water supplies which can be potentially affected by plant operations, there is reasonable assurance that the operation of the facility will not result in radionuclide concentrations in the finished drinking water that are in excess of the requirements of 40 CFR 141. The dose calculations in the ODCM implement the requirements in Section III.A of Appendix I that conformance with guides of Appendix I be shown by calculational procedures based on models and data, such that the actual exposure of an individual through appropriate pathways is unlikely to be substantially underestimated. The equations specified in the ODCM for calculating the doses due to the actual release rates of radioactive materials in liquid effluents are consistent with the methodology provided in NUREG-0133, "Preparation of Radiological Effluent Technical Specifications for Nuclear Power Plants", section 4.3. NUREG-0133 implements Regulatory Guide 1.109, Revision 1, October 1977 (section C.1 and Appendix A) and Regulatory Guide 1.113, April 1977. Regulatory Guide 1.109, October

1977, is titled "Calculation of Annual Doses to Man from Routine Releases of Reactor Effluents for the Purpose of Evaluating Compliance with 10 CFR Part 50, Appendix I". Regulatory Guide 1.113, April 1977, is titled "Estimating Aquatic Dispersion of Effluents from Accidental and Routine Reactor Releases for the Purpose of Implementing Appendix I".

B/1.1.4 Liquid Waste Treatment

The OPERABILITY of the liquid radwaste treatment system ensures that this system will be available for use whenever liquid effluents require treatment prior to release to the environment. The requirement that the appropriate portions of this system be used when specified provides assurance that the releases of radioactive materials in liquid effluents will be kept "as low as is reasonably achievable." This specification implements the requirements of 10 CFR Part 50.36a, General Design Criterion 60 of Appendix A to 10 CFR Part 50 and the design objective given in Section II.D of Appendix I to 10 CFR Part 50. The specified limits governing the use of appropriate portions of the liquid radwaste treatment system were specified as a suitable fraction of the dose design objectives set forth in Section II.A of Appendix I, 10 CFR Part 50, for liquid effluents.

B/1.2 GASEOUS EFFLUENTS

B/1.2.1 Radioactive Gaseous Effluent Monitoring Instrumentation

The radioactive gaseous effluent instrumentation is provided to monitor and control, as applicable, the releases of radioactive materials in gaseous effluents during actual or potential releases of gaseous effluents. The alarm/trip setpoints for these instruments shall be calculated in accordance with the procedures in the ODCM to ensure that the alarm/trip will occur prior to exceeding the limits of 10 CFR Part 20. The OPERABILITY and use of this instrumentation is consistent with the requirements of General Design Criteria 60, 63 and 64 of Appendix A to 10 CFR Part 50.

B/1.2.2 Dose Rate

This specification is provided to ensure that the dose at any time at the site boundary from gaseous effluents from all units on the site will be within the annual dose limits of 10 CFR Part 20 for unrestricted areas. The annual dose limits are the doses associated with the concentration of 10 CFR Part 20, Appendix B, Table II, Column 1. These limits provide reasonable assurance that radioactive material discharged in gaseous effluents will not result in the exposure of an individual in an unrestricted area, either within or outside the site boundary, to annual average concentrations exceeding the limits specified in Appendix B, Table II of 10 CFR Part 20 (10 CFR Part 20, 106 (b)). For individuals who may at times be within the site boundary, the occupancy of the individual will be sufficiently low to compensate for any increase in the atmospheric diffusion factor above that for the site boundary. The specified release rate limits restrict, at all times, the corresponding gamma and beta dose rates above background to an individual at or beyond the site boundary to less than or equal to 500 mrem/year to the total body or to less than or equal 3000 mrem/year to the skin. These release rate

limits also restrict, at all times, the corresponding thyroid dose rate above background to a child via the inhalation pathway to less than or equal to 1500 mrem/year.

B/1.2.3 Dose - Noble Gases

This specification is provided to implement the requirements of Sections II.B, III.A and IV.A of Appendix I, 10 CFR Part 50. The Limiting Condition for Operation implements the guides set forth in Section II.B of Appendix I. The ACTION statements provide the required operating flexibility and at the same time implement the guides set forth in Section IV.A of Appendix I to assure that the releases of radioactive noble gases in gaseous effluents will be kept "as low as is reasonably achievable". The Surveillance Requirements implement the requirements in Section III.A of Appendix I that conformance with the guides of Appendix I be shown by calculational procedures based on models and data such that the actual exposure of an individual through appropriate pathways is unlikely to be substantially underestimated. The dose calculations established in the ODCM for calculating the doses due to the actual release rates of radioactive noble gases in gaseous effluents are consistent with the methodology provided in NUREG-0133, "Preparation of Radiological Effluent Technical Specifications for Nuclear Power Plants", section 5.3. NUREG-0133 implements Regulatory Guide 1.109, Revision 1, October 1977 and Regulatory Guide 1.111, Revision 1, July 1977. Regulatory Guide 1.109 is entitled "Calculation of Annual Doses to Man from Routine Releases of Reactor Effluents for the Purpose of Evaluating Compliance with 10 CFR Part 50, Appendix I, "Revision 1, October 1977 and Regulatory Guide 1.111 is entitled "Methods for Estimating Atmospheric Transport and Dispersion of Gaseous Effluents in Routine Releases from Light-Water Cooled Reactors, "Revision 1, July 1977. The ODCM equations provided for determining the air doses at the site boundary are based upon the historical average atmospheric conditions.

B/1.2.4 Dose-Radioiodines, Tritium and Radioactive Materials in Particulate Form

This specification is provided to implement the requirements of Sections II.C, III.A and IV.A of Appendix I, 10 CFR Part 50. The Limiting Conditions for Operation are the guides set forth in Section II.C of Appendix I. The ACTION statements provide the required operating flexibility and at the same time implement the guides set forth in Section IV.A Appendix I to assure that the releases of radioactive materials in gaseous effluents will be kept "as low as is reasonably achievable." The ODCM calculational methods specified in the Surveillance Requirements implement the requirements in Section III.A of Appendix I that conformance with the guides of Appendix I be shown by calculational procedures based on models and data, such that the actual exposure of an individual through appropriate pathways is unlikely to be substantially underestimated. The ODCM calculational methods for calculating the doses due to the actual release rates of the subject materials are consistent with the methodology provided in NUREG-0133, "Preparation of Radiological Effluent Technical Specifications for Nuclear Power Plants", section 5.3. NUREG-0133 implements Regulatory Guide 1.109, Revision 1, October 1977 and Regulatory Guide 1.111, Revision 1, July 1977. Regulatory Guide 1.109 is entitled "Calculation of Annual Doses to Man from Routine Releases of Reactor Effluents for the Purpose of Evaluating Compliance with 10 CFR Part 50, Appendix I, "Revision 1, October 1977 and Regulatory Guide 1.111 is entitled

"Methods for Estimating Atmospheric Transport and Dispersion of Gaseous Effluents in Routine Releases from Light-Water-Cooled Reactors," Revision 1, July 1977. These equations also provide for determining the actual doses based upon the historical average atmospheric conditions. The release rate specifications for radioiodines, tritium, and radioactive materials in particulate form are dependent on the existing radionuclide pathways to man, in the unrestricted area. The pathways which were examined in the development of these calculations were: 1) individual inhalation of airborne radionuclides, 2) deposition of radionuclides onto green leafy vegetation with subsequent consumption by man, 3) deposition onto grassy areas where milk animals and meat producing animals graze with consumption of the milk and meat by man, and 4) deposition on the ground with subsequent exposure of man.

B/1.2.5 Gaseous Radwaste Treatment

The OPERABILITY of the GASEOUS RADWASTE TREATMENT SYSTEM and the VENTILATION EXHAUST TREATMENT SYSTEM ensures that the systems will be available for use whenever gaseous effluents require treatment prior to release to the environment. The requirement that the appropriate portions of these systems be used, when specified, provides reasonable assurance that the releases of radioactive materials in gaseous effluents will be kept "as low as is reasonably achievable". This specification implements the requirements of 10 CFR Part 50.36a, General Design Criterion 60 of Appendix A to 10 CFR Part 50, and the design objectives given in Section II.D of Appendix I to 10 CFR Part 50. The specified limits governing the use of appropriate portions of the systems were specified as a suitable fraction of the dose design objectives set forth in Sections II.B and II.C of Appendix I, 10 CFR Part 50, for gaseous effluents.

B/1.3 RADIOACTIVE EFFLUENTS: TOTAL DOSE

The specification is provided to meet the dose limitations of 40 CFR 190. The specification requires the preparation and submittal of a Special Report whenever the calculated doses from plant radioactive effluents exceed twice the design objective doses of Appendix I. For sites containing up to 4 reactors, it is highly unlikely that the resultant dose to a member of the public will exceed the dose limits of 40 CFR 190 if the individual reactors remain within the reporting requirement level. The Special Report will describe a course of action which should result in the limitation of dose to a member of the public for 12 consecutive months to within the 40 CFR 190 limits. For the purposes of the Special Report, it may be assumed that the dose commitment to the member of the public from other uranium fuel cycle sources is negligible, with the exception that dose contributions from other nuclear fuel cycle facilities at the same site or within a radius of 5 miles must be considered. If the dose to any member of the public is estimated to exceed the requirements of 40 CFR 190, the Special Report with a request for a variance (provided the release conditions resulting in violation of 40 CFR 190 have not already been corrected), in accordance with the provisions of 40 CFR 190.11, is considered to be a timely request and fulfills the requirements of 40 CFR 190 until NRC staff action is completed. An individual is not considered a member of the public during any period in which he/she is engaged in carrying out any operation which is part of the nuclear fuel cycle.

B/1.4.1 Monitoring Program

The radiological monitoring program required by this specification provides measurements of radiation of radioactive materials in those exposure pathways and for those radionuclides, which lead to the highest potential radiation exposures of individuals resulting from the station operation. This monitoring program thereby supplements the radiological effluent monitoring program by verifying that the measurable concentrations of radioactive materials and levels of radiation are not higher than expected on the basis of the effluent measurements and modeling of the environmental exposure pathways. The initially specified monitoring program will be effective for at least the first three years of commercial operation. Following this period, program changes may be initiated based on operational experience.

The detection capabilities required by Table 1.4-3 are state-of-the-art for routine environmental measurements in industrial laboratories. It should be recognized that the LLD is defined as an a priori (before the fact) limit representing the capability of a measurement system and not as a posteriori (after the fact) limit for a particular measurement. Analyses shall be performed in such a manner that the stated LLDs will be achieved under routine conditions. Occasionally background fluctuations, unavoidably small sample sizes, the presence of interfering nuclides, or other uncontrollable circumstances may render these LLDs unachievable. In such cases, the contributing factors will be identified and described in the Annual Radiological Environmental Operating Report.

B/1.4.2 Land Use Census

This specification is provided to ensure that changes in the use of unrestricted areas are identified and that modifications to the monitoring program are made if required by the results of this census. The best survey information from the door-to-door, aerial or consulting with local agricultural authorities shall be used. This census satisfies the requirements of Section IV.B.3 of Appendix I to 10 CFR Part 50. Restricting the census to gardens of greater than 500 square feet provides assurance that significant exposure pathways via leafy vegetables will be identified and monitored since a garden of this size is the minimum required to produce the quantity (26 kg/year) of leafy vegetables assumed in Regulatory Guide 1.109 for consumption by a child. To determine this minimum garden size, the following assumptions were used, 1) that 20% of the garden was used for growing broad leaf vegetation (i.e., similar to lettuce and cabbage), and 2) a vegetation yield of 2 kg/square meter.

B/1.4.3 Interlaboratory Comparison Program

The requirement for participation in an Interlaboratory Comparison Program is provided to ensure that independent checks on the precision and accuracy of the measurements of radioactive material in environmental sample matrices are performed as part of the quality assurance program for environmental monitoring in order to demonstrate that the results are reasonably valid.

1.6 REPORTING REQUIREMENTS

1.6.1 Annual Radiological Environmental Operating Report

1.6.1.1 Routine radiological environmental operating reports covering the operation of the unit during the previous calendar year shall be submitted prior to May 1 of each year. The initial report shall be submitted prior to May 1 of the year following initial criticality.

1.6.1.2 The annual radiological environmental operating reports shall include summaries, interpretations, and an analysis of trends of the results of the radiological environmental surveillance activities for the report period, including a comparison with preoperational studies, operational controls (as appropriate), and previous environmental surveillance reports and an assessment of the observed impacts of the plant operation on the environment. The reports shall also include the results of land use censuses required by ODCM Specification 1.4.2.1. If harmful effects or evidence of irreversible damage are detected by the monitoring, the report shall provide an analysis of the problem and a planned course of action to alleviate the problem.

The annual radiological environmental operating reports shall include summarized and tabulated results in the format of Regulatory Guide 4.8, December 1975 of all radiological environmental samples taken during the report period. In the event that some results are not available for inclusion with the report, the report shall be submitted noting and explaining the reasons for missing results. The missing data shall be submitted as soon as possible in a supplementary report.

The report shall also include the following: a summary description of the radiological environmental monitoring program; a map of all sampling locations keyed to a table giving distances and directions from one reactor; and the results of licensee participation in the Interlaboratory Comparison Program, required by ODCM Specification 1.4.3.1.

1.6.2 Semiannual Radioactive Effluent Release Report

1.6.2.1 Routine radioactive effluent release reports covering the operation of the unit during the previous 6 months of operation shall be submitted within 60 days after January 1 and July 1 of each year. The period of the first report shall begin with the date of initial criticality.

1.6.2.2 The radioactive effluent release reports shall include a summary of the quantities of radioactive liquid and gaseous effluents and solid waste released from the unit as outlined in Regulatory Guide 1.21, "Measuring, Evaluating, and Reporting Radioactivity in Solid Wastes and Releases of Radioactive Materials in Liquid and Gaseous Effluents from Light-Water-Cooled Nuclear Power Plants", Revision 1, June 1974, with data summarized on a quarterly basis following the format of Appendix B thereof.

The radioactive effluent release report to be submitted within 60 days after January 1 of each year shall include an annual summary of hourly meteorological data collected over the previous year. This annual summary may be either in the form of an hour-by-hour listing of wind speed, wind direction, and atmospheric stability, and precipitation (if measured) on magnetic tape, or in the form of joint frequency distributions of wind speed, wind direction, and atmospheric stability. This same report shall include an assessment of the radiation doses due to the radioactive liquid and gaseous effluents released from the unit or station during the previous calendar year. This same report shall also include an assessment of the radiation doses from radioactive liquid and gaseous effluents to members of the public due to their activities inside the site boundary (Figures 5.1-3 and 5.1-4 of the VCSNS Technical Specifications) during the year. All assumptions used in making these assessments (i.e., specific activity, exposure time and location) shall be included in these reports. Historical annual average meteorology or meteorological conditions concurrent with the time of release of radioactive materials in gaseous effluents (as determined by sampling frequency and measurement) shall be used for determining the gaseous pathway doses. The assessment of radiation doses shall be performed in accordance with the OFFSITE DOSE CALCULATION MANUAL (ODCM).

The radioactive effluent release report to be submitted within 60 days after January 1 of each year shall also include an assessment of radiation doses to the likely most exposed member of the public from reactor releases and other nearby uranium fuel cycle sources (including doses from primary effluent pathways and direct radiation) for the previous 12 consecutive months to show conformance with 40 CFR 190, Environmental Radiation Protection Standards for Nuclear Power Operation. Acceptable methods for calculating the dose contribution from liquid and gaseous effluents are given in Regulatory Guide 1.109, Rev. 1.

The radioactive effluent release reports shall include unplanned releases from site to unrestricted areas of radioactive materials in gaseous and liquid effluents on a quarterly basis.

1.6.3 Major Changes To Radioactive Waste Treatment Systems (Liquid and Gaseous)

1.6.3.1 Licensee initiated major changes to the radioactive waste systems (liquid and gaseous):

1. Shall be reported to the Commission in the Monthly Operating Report for the period in which the evaluation was reviewed by the Plant Safety Review Committee. The discussion of each change shall contain:
 - a. A summary of the evaluation that led to the determination that the change could be made in accordance with 10 CFR 50.59;
 - b. Sufficient detailed information to totally support the reason for the change without benefit of additional or supplemental information;
 - c. A detailed description of the equipment, components and processes involved and the interfaces with other plant systems;
 - d. An evaluation of the change which shows the predicted releases or radioactive materials in liquid and gaseous effluents that differs from those previously predicted in the license application and amendments thereto;
 - e. An evaluation of the change which shows the expected maximum exposures to individual in the unrestricted area and to the general population that differ from those previously estimated in the license application and amendments thereto;
 - f. A comparison of the predicted releases of radioactive materials, in liquid and gaseous effluents, to the actual releases for the period prior to when the changes are to be made;
 - g. An estimate of the exposure to plant operating personnel as a result of the change; and

- h. Documentation of the fact that the change was reviewed and found acceptable by the PSRC.
2. Shall become effective upon review and acceptance as set forth in Technical Specification 6.5.

1.7 Definitions

ACTION

- 1.7.1 ACTION shall be that part of a specification which prescribes measures required under designated conditions.

ANALOG CHANNEL OPERATIONAL TEST

- 1.7.2 An ANALOG CHANNEL OPERATIONAL TEST shall be the injection of a simulated signal into the channel as close to the sensor as practicable to verify OPERABILITY of alarm, interlock and/or trip functions. The ANALOG CHANNEL OPERATIONAL TEST shall include adjustments, as necessary, of the alarm, interlock and/or trip setpoints such that the setpoints are within the required range and accuracy.

CHANNEL CALIBRATION

- 1.7.3 A CHANNEL CALIBRATION shall be the adjustment, as necessary, of the channel such that it responds within the required range and accuracy to known values of input. The CHANNEL CALIBRATION shall encompass the entire channel including the sensors and alarm, interlock and/or trip functions, and may be performed by any series of sequential, overlapping or total channel steps such that the entire channel is calibrated.

CHANNEL CHECK

- 1.7.4 A CHANNEL CHECKS shall be the qualitative assessment of channel behavior during operation by observation. This determination shall include, where possible, comparison of the channel indication and/or status with other indications and/or status derived from independent instrument channels measuring the same parameter.

GASEOUS RADWASTE TREATMENT SYSTEM

- 1.7.5 A GASEOUS RADWASTE TREATMENT SYSTEM is any system designed and installed to reduce radioactive gaseous effluents by collecting primary coolant system off gases from the primary system and providing for delay or holdup for the purpose of reducing the total radioactivity prior to release to the environment.

OPERABLE - OPERABILITY

- 1.7.6 A system, subsystem, train, component or device shall be OPERABLE or have OPERABILITY when it is capable of performing its specified function(s), and when all necessary attendant instrumentation, controls, electrical power, cooling or seal water, lubrication or other auxiliary equipment that are required for the system, subsystem, train, component or device to perform its function(s) are also capable of performing their related support function(s).

SOURCE CHECK

- 1.7.7 A SOURCE CHECK shall be the qualitative assessment of channel response when the channel sensor is exposed to a radioactive source.

VENTILATION EXHAUST TREATMENT SYSTEM

- 1.7.8 A VENTILATION EXHAUST TREATMENT SYSTEM is any system designed and installed to reduce gaseous radioiodine or radioactive material in particulate form in effluents by passing ventilation or vent exhaust gases through charcoal absorbers and/or HEPA filters for the purpose of removing iodines or particulates from the gaseous exhaust stream prior to the release to the environment (such a system is not considered to have any effect on noble gas effluents). Engineered Safety Feature (ESF) atmospheric cleanup systems are not considered to be VENTILATION EXHAUST TREATMENT SYSTEM components.

2.0 LIQUID EFFLUENT

2.1 Liquid Effluent Monitor Setpoint Calculation

The Virgil C. Summer Nuclear Station is located on the Monticello Reservoir which provides supply and discharge for the plant circulating water. This reservoir also provides supply and discharge capacity for the Fairfield Pumped Storage Facility. The Parr Reservoir located below the pumped storage facility is formed by the Parr Dam.

There are two analyzed release pathways and sources of dilution for liquid effluents: the circulating water discharge canal and the liquid effluent line to the penstocks of the pumped storage facility. All liquid effluent pathways discharge to one of these release points. Generally speaking, very low concentrations of radioactive waste are discharged to the circulating water discharge while higher concentrations of radioactive waste are released to the penstocks of the pumped storage facility during the generation cycle.

The calculated setpoint values will be regarded as upper bounds for the actual setpoint adjustments. That is, setpoint adjustments are not required to be performed if the existing setpoint level corresponds to a lower count rate than the calculated value. Setpoints may be established at values lower than the calculated values, if desired.

Calculated monitor setpoints may be added to the ambient background count rate.

GENERAL NOTE: If no discharge is planned for a specific pathway or if the sum of the effluent concentrations of gamma emitting nuclides equals zero, the monitor setpoint should be established as close to background as practical to prevent spurious alarms and yet alarm should an inadvertent release occur.

2.1.1 Liquid Effluent Monitor Setpoint Calculation Parameters

<u>Term</u>	<u>Definition*</u>	<u>Section of Initial Use</u>
A	= Penstock discharge adjustment factor which will allow the set point to be established in a convenient manner and to prevent spurious alarms. = f_t/f_{dx}	2.1.2
A_{it}	= The site related ingestion dose commitment factor to the total body or organ t , for each identified principal gamma and beta emitter listed in Table 2.2-3 (mrem-ml per hr-uCi). For calculation see section 2.2.2.	2.1.4.4.1
\bar{A}_t	= average A_{it} using maximum organ for each nuclide and weighted by concentration. = $\frac{\sum (A_{it} * C_i)}{\sum C_i}$	2.1.4.4.1
B	= Steam Generator Blowdown adjustment factor which will allow the set point to be established in a convenient manner and to prevent spurious alarms. = f_d/f_{ds}	2.1.4.1
C	= the effluent concentration limit (Specification 1.1.2) implementing 10CFR 20 for the site, in uCi/ml.	2.1.2
C_a	= the effluent concentration of alpha emitting nuclides observed by gross alpha analysis of the monthly composite sample, in uCi/ml.	2.1.2
C_f	= the measured concentration of Fe-55 in liquid waste as determined by analysis of the most recent available quarterly composite sample, in uCi/ml.	2.1.2
C_g	= the effluent concentration of a gamma emitting nuclide, g, observed by gamma-ray spectroscopy of the waste sample, in uCi/ml.	2.1.2
C_i	= the concentration of nuclide i , in uCi/ml, as determined by the analysis of the waste sample.	2.1.2
C_{ir}	= the concentration of radionuclide i , in uCi/ml, in the Monticello Reservoir. Inclusion of this term will correct for possible long-term buildup of radioactivity due to recirculation and for the presence of activity recently released to the Monticello Reservoir by plant activities.	2.1.2
C_s	= the concentration of Sr-89 or Sr-90 in liquid wastes as determined by analysis of the quarterly composite sample, in uCi/ml.	2.1.2
C_t	= the measured concentration of H-3 in liquid waste as determined by analysis of the monthly composite, in uCi/ml.	2.1.2
c	= the setpoint, in uCi/ml, of the radioactivity monitor measuring the radioactivity concentration in the effluent line prior to dilution and subsequent release. This setpoint which is proportional to the volumetric flow to the effluent line and inversely proportional to the volumetric flow of the dilution stream plus the effluent	2.1.2

* All concentrations are in units of uCi/ml unless otherwise noted.

<u>Term</u>	<u>Definition</u>	<u>Section of Initial Use</u>
	stream, represents a value which, if exceeded, would result in concentrations exceeding the limits of 10CFR 20 in the unrestricted area.	
C_B	= the monitor setpoint concentration for RM-L7, the Nuclear Blowdown Monitor Tank discharge line monitor, in $\mu\text{Ci/ml}$	2.1.2.2
C_C	= the monitor setpoint concentration for RM-L9, the combined Liquid Waste Processing System and Nuclear Blowdown System effluent discharge line monitor, in $\mu\text{Ci/ml}$.	2.1.2.3
C_D	= the monitor setpoint concentration for RM-L11, the Condensate Demineralizer Backwash discharge line monitor, in $\mu\text{Ci/ml}$.	2.1.4.2.2
C_M	= the monitor setpoint concentration for RM-L5, the Waste Monitor Tank discharge line monitor, in $\mu\text{Ci/ml}$.	2.1.2.1
C_{Sa}	= the monitor setpoint concentration for RM-L3, the initial Steam Generator Blowdown Effluent line monitor, in $\mu\text{Ci/ml}$.	2.1.4.1.1
C_{Sb}	= the monitor setpoint concentration for RM-L10, the final Steam Generator Blowdown Effluent line monitor, in $\mu\text{Ci/ml}$.	2.1.4.1.1
C_T	= the monitor setpoint concentration for RM-L8, the Turbine Building Sump Effluent line monitor, in $\mu\text{Ci/ml}$.	2.1.4.2.1
CF_D	= the Condensate Demineralize Backwash Effluent Concentration Factor.	2.1.4.2
CF_S	= the Steam Generator Blowdown Effluent Concentration Factor.	2.1.4.3
CF_T	= the Turbine Building Sump Effluent Concentration Factor.	2.1.4.2
DF	= the dilution factor, which is the ratio of the total dilution flow rate to the effluent stream flow rate(s).	2.1.2
D_m	= daily dose projection margin (mrem) for most limiting dose (total body or organ).	2.1.4.4.1
F	= the dilution water flow setpoint as determined prior to the release, in volume per unit time.	2.1.2
F_d	= the flow rate of the Circulating Water System during the time of release of the Turbine Building Sump and/or the Steam Generator Blowdown, in volume per unit time.	2.1.4.1
F_{dc}	= the dilution flow rate of the Circulating Water System used for effluent monitor setpoint calculations, based on 90 percent of expected Circulating Water System flow rate during the time of release and corrected for recirculated Monticello Reservoir activity, in volume per unit time.	2.1.4.1
F_{cp}	= the dilution flow rate through the penstock(s) receiving the radioactive liquid release upon which the effluent monitor setpoint is based, as corrected for any recirculated radioactivity, in volume per unit time.	2.1.2

* (Conservatively this value will be either zero, if no release is to be conducted from this system, or the maximum measured capacity of the discharge pump if a release is to be conducted.)

<u>Term</u>	<u>Definition</u>	<u>Section of Initial Use</u>
F_t	= the flow rate of water through the Fairfield Pumped Storage Station penstock(s) to which radioactive liquids are being discharged during the period of effluent release. This flow rate is dependent upon operational status of Fairfield Pumped Storage Station, in volume per unit time.	2.1.2
f	= the effluent line flow setpoint as determined for the radiation monitor location, in volume per unit time.	2.1.2
f_d	= the maximum permissible discharge flow rate for releases to the Circulating Water, in volume per unit time.	2.1.4.1
f_{db}^*	= the flow rate of the Nuclear Blowdown Monitor Tank discharge, in volume per unit time.	2.1.2
f_{dm}^*	= the flow rate of a Waste Monitor Tank discharge, in volume per unit time.	2.1.2
f_{ds}^*	= the flow rate of the Steam Generator Blowdown discharge, in volume per unit time.	2.1.4.1
f_{dx}	= the flow rate of the tank discharge, either f_{dm} or f_{db} , in volume per unit time.	2.1.2
F_b	= The near field dilution factor for C_i during release from Turbine Building sump.	2.1.4.4.1
f_r	= the recirculation flow rate used to mix the contents of a tank, in volume per unit time.	2.1.2
f_t	= the maximum permissible discharge flow rate for batch releases to the penstocks, in volume per unit time.	2.1.2
MPC_i	= MPC_g , MPC_α , MPC_s , MPC_{Fe} , and MPC_t = the limiting concentrations of the appropriate gamma emitting, alpha emitting, and strontium radionuclides, Fe-55, and tritium, respectively, from 10CFR, Part 20, Appendix B, Table II, Column 2. For gamma emitting noble gas radionuclides, $MPC_i = 2 \times 10^{-4}$ uCi/ml.	2.1.2
SF	= the safety factor, a conservative factor used to compensate for engineering and measurement uncertainties. SF = 0.5, corresponding to a 100 percent variation.	2.1.2
$[C_i]_{LLD}$	= the Lower Limit of Detection (LLD) for radionuclide i in liquid waste in the Waste Monitor Tank, as determined by the analysis required in ODCM Table 1.1-4, in uCi/ml.	2.1.3
$[C_i]_M$	= the concentration of radionuclide i in the waste contained within the Waste Monitor Tank serving as the holding facility for sampling and analysis prior to discharge, in μ Ci/ml.	2.1.3

<u>Term</u>	<u>Definition</u>	<u>Section of Initial Use</u>
$\sum C_g$	= the sum of the concentrations C_g of each measured gamma emitting nuclide observed by gamma-ray spectroscopy of the waste sample, in uCi/ml.	2.1.2
$[\sum C_g]_B$	= the gamma isotopic concentrations of the Nuclear Blowdown Monitor Tank as obtained from the sum of the measured concentrations determined by the analysis required in ODCM Table 1.1-4, in uCi/ml.	2.1.2
$[\sum C_g]_D$	= the gamma isotopic concentrations of the Condensate Demineralizer Backwash effluent (including solids) as obtained from the sum of the measured concentrations determined by the analysis required in ODCM Table 1.1-4, in uCi/ml.	2.1.4.2.2
$[\sum C_g]_M$	= the gamma isotopic concentrations of the Waste Monitor Tank as obtained from the sum of the measured concentrations determined by the analysis required in ODCM Table 1.1-4, in uCi/ml.	2.1.2
$[\sum C_g]_S$	= the gamma isotopic concentrations of the Steam Generator Blowdown as obtained from the sum of the measured concentrations determined by the analysis required in ODCM Table 1.1-4, in uCi/ml.	2.1.4.1.1
$[\sum C_g]_T$	= the gamma isotopic concentrations of the Turbine Building Sump as obtained from the sum of the measured concentrations determined by the analysis required in ODCM Table 1.1-4, in uCi/ml.	2.1.4.2.1
$[\sum (C_i/MPC_i)]_D$	= the sum of the ratios of the measured concentration of nuclide i to its limiting value MPC_i for the Condensate Demineralizer Backwash.	2.1.4.2
$[\sum (C_i/MPC_i)]_S$	= the sum of the ratios of the measured concentration of nuclide i to its limiting value MPC_i for the Steam Generator Blow-down Effluent.	2.1.4.1
$[\sum (C_i/MPC_i)]_T$	= the sum of the ratios of the measured concentration of nuclide i to its limiting value MPC_i for the Turbine Building Sump Effluent.	2.1.4.2
$[\sum (C_i/MPC_i)]_X$	= the sum of the ratios of the measured concentration of nuclide i to its limiting value MPC_i for the tank whose contents are being considered for release. For a WMT, $X = M$. For the NBMT, $X = B$.	2.1.2
t_r	= the minimum time for recirculating the contents of a tank prior to sampling, in minutes.	2.1.2
V	= the volume of liquid in a tank to be sampled, in gallons.	2.1.2
V_j	= release volume for Turbine Building sump release permit in gallons	2.1.4.4.1
Δt_k	= the length of time (in hours) during which concentrations and flow rates are averaged. For purpose of setpoint calculation, $\Delta t_k = 24$ hours.	2.1.4.4.1

2.1.2 Liquid Radwaste Effluent Line Monitors

(RM-L5, RM-L7, RM-L9)

Liquid Radwaste Effluent Line Monitors provide alarm and automatic termination of release functions prior to exceeding the concentration limits specified in 10CFR 20, Appendix B, Table II, Column 2 at the release point to the unrestricted area. To meet this specification, the alarm/trip setpoints for liquid effluent monitors and flow measurement devices are set to assure that the following equation is satisfied:

$$C \geq \frac{cf}{F+f} \quad (1)$$

where:

C = the effluent concentration limit (Specification 1.1.2) implementing 10CFR 20 for the site in uCi/ml.

c = the setpoint, in uCi/ml, of the radioactivity monitor measuring the radioactivity concentration in the effluent line prior to dilution and subsequent release; the setpoint, which is inversely proportional to the volumetric flow of the effluent line and proportional to the volumetric flow of the dilution stream plus the effluent stream, represents a value which, if exceeded, would result in concentrations exceeding the limits of 10CFR 20 in the unrestricted area.

F = the dilution water flow setpoint as determined prior to the release point, in volume per unit time.

f = the effluent line flow setpoint as determined at the radiation monitor location, in volume per unit time.

At the Virgil C. Summer Nuclear Station the Liquid Waste Processing System (LWPS) and the Nuclear Blowdown System (NBS) both discharge to the penstocks of the Fairfield Pumped Storage (FPS) Facility through a

common line. The available dilution water flow (F_{dp}) is assumed to be 90 percent of the flow through the FPS penstock(s) to which liquid effluent is being discharged and is dependent upon operational status of the FPS Facility. The waste tank flow rates (f_{dm} and f_{db}) and the monitor setpoints (c_M , c_B and c_C) are set to meet the condition of equation (1) for a given effluent concentration, C . The three monitor setpoints are determined in accordance with the monitor system configuration for this discharge pathway. The LWPS discharges through RM-L5, which has setpoint c_M for alarm/control functions over releases from either Waste Monitor Tanks 1 or 2. The Nuclear Blowdown discharges through RM-L7, which has setpoint c_B for alarm/control functions over releases from the Nuclear Blowdown Monitor Tank. These two release pathways merge into a common line monitored by RM-L9, which has setpoint c_C for control functions over the common effluent line. Although the piping is arranged so that simultaneous batch releases from the two systems could be practiced, operational releases shall be from only one of the two batch systems at any given time. The method by which their setpoints are determined is as follows:

- 1) The isotopic concentration for a waste tank to be released is obtained from the sum of the measured concentrations as determined by the analysis required in Table 1.1-4:

$$\sum_i C_i = \sum_g C_g + C_a + C_s + C_t + C_f \quad (2)$$

where:

C_i = the concentration of nuclide i , in uCi/ml, as determined by the analysis of the waste sample.

* Values for C_a , C_s , C_t and C_f will be based on most recent available composite sample analyses as required by Table 1.1-4.

- $\sum C_g$ = the sum of the concentrations C_n of each measured gamma emitting nuclide observed by gamma-ray spectroscopy of the waste sample, in uCi/ml.
- C_a^* = the effluent concentration of alpha emitting nuclides observed by gross alpha analysis of the monthly composite sample, in uCi/ml.
- C_s^* = the concentration of Sr-89 and Sr-90 in liquid waste as determined by analysis of the quarterly composite sample, in uCi/ml.
- C_t^* = the measured concentration of H-3 in liquid waste as determined by analysis of the monthly composite sample, in uCi/ml.
- C_i^* = the measured concentration of Fe-55 in liquid waste as determined by analysis of the quarterly composite sample, in uCi/ml.

The C_g term will be included in the analysis of each batch; terms for alpha, strontium, Fe-55, and tritium shall be included as appropriate*. Isotopic concentrations for both the Waste Monitor Tanks (WMT) and the Nuclear Blowdown Monitor Tank (NBMT) may be calculated using equation (2).

Prior to being sampled for analysis, the contents of a tank shall be isolated and recirculated. The minimum recirculation time shall be:

$$t_r = 2V/f_r \quad (3)$$

- t_r = the minimum time for recirculating the contents of a tank prior to sampling.
- V = the volume of liquid in the tank to be sampled.
- f_r = the recirculation flow rate used to mix the contents of a tank.

This is done to ensure that a representative sample will be obtained. Mechanical mixers shall ensure a similar minimum turnover.

- 2) Once isotopic concentrations for either Waste Monitor Tank or the Nuclear Blowdown Monitor Tank have been determined, these values are used to calculate a Dilution Factor, DF, which is the ratio of dilution flow rate to tank flow rate(s) required to assure that the limiting concentration of 10CFR, Part 20, Appendix B, Table II, Column 2 are met at the point of discharge for whichever tank is having its contents discharged.

$$DF = \left[\sum_i \frac{C_i}{MPC_i} \right]_X + SF \quad (4)$$

$$DF = \left[\sum_g \frac{C_g}{MPC_g} + \frac{C_\alpha}{MPC_\alpha} + \frac{C_s}{MPC_s} + \frac{C_{Fe-55}}{MPC_{Fe-55}} + \frac{C_t}{MPC_t} \right]_X + SF \quad (5)$$

where:

$\left[\sum_i \frac{C_i}{MPC_i} \right]_X$ = the sum of the ratios of the measured concentration of nuclide i to its limiting value MPC for the tank whose contents are being considered for release. For a WMT, $X = M$. For the NBMT, $X = B$.

MPC_i = MPC_g , MPC_α , MPC_s , MPC_{Fe-55} , and MPC_t = limiting concentrations of the appropriate gamma emitting, alpha emitting, and strontium radionuclides, Fe-55, and tritium, respectively, given in 10CFR, Part 20, Appendix B, Table II, Column 2. For gamma-emitting noble gas radionuclides MPC_i is to be set equal to 2×10^{-4} μ Ci/ml, according to the Radiological Effluent Technical Specifications.

SF = the safety factor; a conservative factor used to compensate for engineering and measurement uncertainties.

= 0.5, Corresponding to a 100 percent variation.

- 3) The maximum permissible discharge flow rate, f_{di} , may be calculated for the release of either the WMT or NBMT. First the appropriate Dilution Factor is calculated by applying equation (4), using the appropriate concentration ratio term (i.e. M or B).

then,

$$r_i = \frac{F_{dp} + f_{di}}{DF} = \frac{F_{dp}}{DF} \quad \text{for } F_{dp} \gg f_{di} \quad (6)$$

where:

F_{dp} = dilution flow rate to be used in effluent monitor setpoint calculations, based on 90 percent FPS Station expected flow rate, as corrected for any recirculated radioactivity:

$$F_{dp} = (0.9)F_t \left(1 - \sum_i \frac{C_{ir}}{MPC_i} \right) \quad (7)$$

where:

F_t = the flow rate through the Fairfield Pumped Storage Station penstock(s) to which radioactive liquids are being discharged. F_t should normally fall between 2500 and 44800 cfs.

C_{ir} = the concentration of radionuclide i , in uCi/ml, in the intake of Fairfield Pumped Storage Station (that is, in the Monticello Reservoir). Inclusion of this term will correct for possible long-term buildup of radioactivity due to recirculation and for the presence of activity recently released to the Monticello Reservoir by plant activities. For expected discharges of liquid wastes, the summation will be much less than 1.0 and can be ignored (Reference 6).

- f_{dx} = the flow rate of the tank discharge, either f_{dm} or f_{db} .
- f_{db} = flow rate of Nuclear Blowdown Monitor Tank discharge. (Conservatively this value will be either zero, if no release is to be conducted from this system, or the maximum measured capacity of the discharge pump if a release is to be conducted.)
- f_{dm} = flow rate of Waste Monitor Tank discharge. (Conservatively this value will either be zero, if no release is to be conducted from this system, or the maximum measured capacity of the discharge pump if a release is to be conducted.)
- DF = the Dilution Factor from Step 2.

If $f_t \cong f_{dx}$, the release may be made as planned and the flow rate monitor setpoints should be established as in Step 4 (below). Because F_{dp} is normally very large compared to the maximum discharge pump capacities for the Waste Monitor Tank and the Nuclear Blowdown Monitor Tank, it is extremely unlikely that $f_t < f_{dx}$. However, if a situation should arise such that $f_t < f_{dx}$, steps must be taken to assure that equation (1) is satisfied prior to making the release. These steps may include decreasing f_{dx} by decreasing the flow rate of f_{dm} or f_{db} , and/or increasing F_{dp} .

When new candidate flow rates are chosen, the calculations above should be repeated to verify that they combine to form an acceptable release. If they do, the establishment of flow rate monitor setpoints may proceed as follows in Step 4. If they do not, the choice of candidate flow rates must be repeated until an acceptable set is identified.

Note that if $DF \cong 1$, the waste tank concentration for which the calculation is being performed includes safety factors in Step 2 and meets the limits of 10CFR 20 without further dilution. Even though

no dilution would be required, there will be no discharge if minimum dilution flow is not available, since the peristock minimum flow interlock will prevent discharge.

- 4) The dilution flow rate setpoint*, F , is established at 90 percent of the expected available dilution flow rate:

$$F = (0.9) F_e \quad (8)$$

The flow rate monitor setpoint* for the effluent stream shall be set at the selected discharge pump rate (normally the maximum discharge pump rate or zero) f_{dm} or f_{db} chosen in Step 3 above.

- 5) The radiation monitor setpoints may now be determined based on the values of ΣC_i , F , and f which were specified to provide compliance with the limits of 10CFR 20, Appendix B, Table II, Column 2. The monitor response is primarily to gamma radiation, therefore, the actual setpoint is based on ΣC_g .

The setpoint concentration, c , is determined as follows:

$$c \leq \frac{\Sigma C_g}{f} \times A \quad (9)$$

$A =$ Adjustment factor which will allow the setpoint to be established in a practical manner for convenience and to prevent spurious alarms.

$$A = f_i / f_{dx} \quad 10$$

If $A \leq 1$, Calculate c and determine the maximum value for the actual monitor setpoint (cpm) from the monitor calibration graph.

* Set points for flow rates are administrative limits.

If $A < 1$, No release may be made. Reevaluate the alternatives presented in Step 3.

NOTE: If calculated setpoint values are near actual concentrations planned for release, it may be impractical to set the monitor alarm at this value. In this case a new setpoint may be calculated following the remedial methodology presented in Step 3 for the case of $f_t < f_{dx}$.

Within the limits of the conditions stated above, the specific monitor setpoint concentrations for the three liquid radiation monitors RM-L5, RM-L7, and RM-L9 are determined as follows:

2.1.2.1 RM-L5, Waste Monitor Tank Discharge Line Monitor:

$$C_M \leq \left[\sum_g C_g \right]_M (A) \quad (11)$$

C_M is in uCi/ml

*See GENERAL NOTE under 2.1.

2.1.2.2 RM-L7, Nuclear Blowdown Monitor Tank Discharge Line Monitor:

$$C_B \leq \left[\sum_g C_g \right]_B (A) \quad (12)$$

C_B is in uCi/ml

NOTE: In no case should discharge be made directly from the Nuclear Blowdown Holdup Tank to the penstocks.

*See GENERAL NOTE under 2.1.

2.1.2.3 RM-L9, Combined Liquid Waste Processing System and Nuclear Blowdown Waste Effluent Discharge Line Monitor

The monitor setpoint concentration on the common line, c_C , should be the same as the setpoint concentration for the monitor on the active individual discharge line (i.e., c_M or c_B as determined above):

$$C_C \leq \text{MAX}(C_M, C_B) \quad (13)$$

*See GENERAL NOTE under 2.1.

NOTE: In all cases, c_M , c_B , and c_C are the setpoint concentration values in uCi/ml. The actual monitor setpoints (cpm) for RM-L5, RM-L7, and RM-L9 are determined from the calibration graph for the particular monitor. Initially, the calibration curves were determined conservatively from families of response curves supplied by the monitor manufacturers. A sample is shown in Figure 2.1-1. As releases occur, a historical correlation will be prepared and placed in service when sufficient data are accumulated.

2.1.3 Liquid Radwaste Discharge Via Industrial and Sanitary Waste System (RM-L5)

In the Virgil C. Summer Nuclear Station liquid waste effluent system design, there exists a mechanism for discharging liquid wastes via the Industrial Sanitary Waste System. The sample point prior to discharge is one of the Waste Monitor Tanks. The analysis requirements are the requirements listed in Table 1.1-4.

This effluent pathway shall only be used when the following condition is met for all radionuclides, i:

$$\left| C_i \right|_M \leq \left| C_i \right|_{LLD} \quad (14)$$

$\left| C_i \right|_M$ = the concentration of radionuclide i in the waste contained within the Waste Monitor Tank serving as the holding facility for sampling and analysis prior to discharge, in uCi/ml.

$\left| C_i \right|_{LLD}$ = the Lower Limit of Detection, (LLD) for radionuclide i in the liquid waste in the Waste Monitor Tank as determined by the analysis required in Table 1.1-4, in uCi/ml.

When the conditions of equation (14) are met, liquid waste may be released via the Industrial and Sanitary Waste System pathway. The RM-L5 setpoint should be established as close to background as practical to prevent spurious alarms and yet alarm should an inadvertent high concentration release occur.

2.1.4 Steam Generator Blowdown, Turbine Building Sump, and Condensate Demineralizer Backwash Effluent Lines

(RM-L3, RM-L10, RM-L8, RM-L11)

Concentrations of radionuclides in the liquid effluent discharges made via the Turbine Building Sump, Steam Generator Blowdown, and Condensate Demineralizer Backwash are expected to be very low or nondetectable. The first two releases are expected to be continuous in nature and the last a batch release. All will be sampled in an appropriate manner as specified in Table 1.1-4 of the ODCM. The Steam Generator Blowdown Monitors, the Turbine Building Sump Monitor, and the Condensate Demineralizer Backwash Monitor provide alarm and automatic termination of release prior to exceeding the concentration limits specified in 10CFR 20, Appendix B, Table II, Column 2 at the release point to the unrestricted area.

In reality, all of these effluent pathways utilize the circulating water as dilution to the effluent stream, with the circulating water discharge canal being the point of release into an unrestricted area. Steam Generator Blowdown Effluent may be released to the Circulating Water either directly in the Condenser outflow (the normal flow path) or in the first hours following startup via the Industrial and Sanitary Waste System (ISWS) for chemical reasons. The Turbine Building Sump and Condensate Demineralizer Backwash Effluents enter Circulating Water via the sumps and ponds of the Industrial and Sanitary Waste System.

To ensure compliance with ODCM specification 1.1.2.1 (TS 3.11.1.1), normally no dilution is assumed for discharges to the Industrial and Sanitary Waste System. The assumption of no dilution limits discharges to $< .5$ MPC and therefore ODCM specification 1.1.2.1 would not be compromised in the event circulating water dilution is lost. To add operational flexibility for abnormal conditions (radionuclide concentration in Turbine Building sump $> .5$ MPC), discharges from the Turbine Building sump and concentrations in the ISWS may exceed the operational objective, $.5$ MPC, provided circulating water dilution is sufficient to ensure compliance with ODCM specification 1.1.2.1 and liquid effluents are being discharged in compliance with ODCM Specification 1.1.4.1 (TS 3.11.1.3). Two separate setpoint calculations are given for Turbine Building sump discharges (RM-L8). Section 2.1.4.2.1 describes the setpoint calculation normally used, limiting discharges to $.5$ MPC. Section 2.1.4.2.2 provides an alternate setpoint methodology which may be used during abnormal conditions. RM-L8 set-points are considered in compliance with ODCM specification 1.1.1.1 (TS 3.3.3.8) provided the setpoints are adequate to prevent releases in excess of ODCM specification 1.1.2.1 (TS 3.11.1.1).

Two mutually exclusive setpoint calculation processes are outlined below for steam generator blowdown. Section 2.1.4.1 is to be used whenever Steam Generator Blowdown is being released directly to the Circulating Water in the Condenser outflow, which is the normal mode. Section 2.1.4.2 is to be used whenever Steam Generator Blowdown is being released to the Industrial and Sanitary Waste System, or diverted to the Nuclear Blowdown Processing System, both of which are alternate modes.

Normally, water collected by the Nuclear Blowdown Processing System has very low specific activity. This water may be processed to the Turbine Building sump.

NOTE: When Circulating Water is unavailable for effluent dilution, releases containing activity above LLD should be discouraged via pathways

which lead to it. Steam Generator Blowdown should be diverted to the Nuclear Blowdown Processing System. Condensate Demineralizer Backwash may be diverted to the Turbine Building sump or not released. Turbine Building sump effluent should be diverted to the Excess Liquid Waste Processing System. (These steps are to keep the calculated dose to individuals as low as reasonably achievable.) Furthermore, sampling and analysis of the Industrial and Sanitary Waste System is to be initiated and the measured concentrations used in the dose calculations of Section 2.2.

2.1.4.1 Steam Generator Blowdown Effluent Direct to Circulating Water (Normal Mode)

Equation (1) is again used to assure that effluents are in compliance with the aforementioned specification:

$$C \geq \frac{cf}{(F+f)}$$

The available dilution water flow (F_{dc}) is dependent upon the mode of operation of the Circulating Water System. Any change in this value will be accounted for in a recalculation of equation (1). The Steam Generator Blowdown flow rate (f_{ds}) and the Steam Generator Blowdown monitor setpoints (c_{sa} and c_{sb}) are set to meet the condition of equation (1).

RM-L3, the first monitor in the Steam Generator Blowdown discharge pathway, alarms and terminates release of the stream. The discharge is then automatically diverted to the Nuclear Blowdown Processing System. RM-L10, the last monitor in the Steam Generator Blowdown discharge pathway, alarms and terminates the release. Thus, RM-L10 is redundant to RM-L3 and the setpoint (c_{sb}) will be determined in the same manner as RM-L3 (c_{sa}).

The method by which the monitor setpoints are determined is as follows:

- 1) The isotopic concentrations for any release source to be or being released are obtained from the sum of the measured concentrations as determined in Table 1.1-4. Equation (2) is again employed for this calculation:

$$\sum_i C_i = \sum_g C_g + C_a + C_s + C_t + C_f$$

where:

- $\sum_i C_i$ = the sum of the measured concentrations as determined by the analysis of the waste sample, in uCi/ml.
- $\sum_g C_g$ = the sum of the concentrations C_g of each measured gamma emitting nuclide observed by gamma-ray spectroscopy of the waste sample, in uCi/ml.
- C_a = the measured concentration C_a of alpha emitting composite sample, in uCi/ml.
- C_s = the measured concentrations of Sr-89 and Sr-90 in liquid waste as determined by analysis of the most recent available quarterly composite sample, in uCi/ml.
- C_t = the measured concentration of H-3 in liquid waste determined by analysis of the monthly composite sample, in uCi/ml.
- C_f = the measured concentration of Fe-55 in liquid waste as determined by analysis of the most recent available quarterly composite sample, in uCi/ml.

Isotopic concentrations for the Steam Generator Blowdown System effluent, the Turbine Building Sump Effluent, and the Condensate Demineralizer Backwash effluent may be calculated using equation (2).

- 2) Once isotopic concentrations for the Steam Generator Blowdown have been determined, these values are used to calculate a Dilution Factor, DF, which is the ratio of the total dilution flow rate to effluent stream flow rate required to assure that the limiting concentrations of 10CFR, Part 20, Appendix B, Table II, Column 2 are met at the point of discharge.

$$DF = \left[\sum_i \frac{C_i}{MPC_i} \right]_S - SF \quad (15)$$

$$DF = \left[\frac{C_g}{MPC_g} + \frac{C_a}{MPC_a} + \frac{C_s}{MPC_s} + \frac{C_f}{MPC_f} + \frac{C_t}{MPC_t} \right]_S - SF \quad (16)$$

where:

C_i = $C_g, C_a, C_s, C_f,$ and C_t ; measured concentrations as defined in Step 1. Terms $C_a, C_s, C_f,$ and C_t will be included in the calculation as appropriate.

$\left[\sum_i \frac{C_i}{MPC_i} \right]_S$ = the sum of the ratios of the measured concentration of nuclide i to its limiting value MPC_i for the Steam Generator Blowdown effluent.

MPC_i = $MPC_g, MPC_a, MPC_s, MPC_f,$ and MPC_t are limiting concentrations of the appropriate radionuclide from 10CFR, Part 20, Appendix B, Table II, Column 2 limits. For gamma-emitting noble gas radionuclides, MPC_i is to be set equal to 2×10^{-4} uCi/ml.

SF = the same generic term as used in Section 2.1.2, Step 2.

= 0.5

- 3) The maximum permissible effluent discharge flow rate, f_d , may now be calculated for a release from the Steam Generator Blowdown.

$$f_d = \frac{F_{dc} + f_{ds}}{DF} = \frac{F_{dc}}{DF} \text{ for } F_{dc} \gg f_{ds} \quad (17)$$

where:

- F_{dc} = Dilution flow rate for use in effluent monitor setpoint calculations, based on 90 percent of the expected flow rate of the Circulating Water System during the time of release and corrected for any recirculated activity:

$$F_{dc} = (0.9) F_d \left(1 - \sum_i \frac{C_{ir}}{MPC_i} \right) \quad (18)$$

where:

- F_d = the flow rate of the Circulating Water System during the time of the release. F_d should normally fall between 1.78×10^5 and 5.34×10^5 gpm when the plant is operating and should be 5000 gpm when the plant is shutdown and the Circulating Water Jockey pump is operating.

- C_{ir} = the concentration of radionuclide i , in uCi/ml, in the Circulating Water System intake, (that is, in the Monticello Reservoir). Inclusion of this term will correct for possible long-term buildup of radioactivity due to recirculation and for the presence of activity recently released to the Monticello Reservoir by plant activities. For expected discharges of liquid wastes, the summation will be much less than 1.0 and can be ignored (Reference 6).

- f_{ds} = Flow rate of Steam Generator Blowdown discharge. (This value normally will be either zero, if no release is

to be conducted, or the maximum rated capacity of the discharge pump (250 gpm), if a release is to be conducted.)

Note that the equation is valid only for $DF > 1$; for $DF \leq 1$, the effluent concentration meets the limits of 10CFR 20 with no dilution as well as being in compliance with the conservatism imposed by the Safety Factor in Step 2.

If $f_d \geq f_{ds}$, releases may be made as planned. Because F_{dc} is normally very large compared to the maximum discharge pump capacity of the Steam Generator Blowdown System, it is extremely unlikely that $f_d < f_{ds}$. However, if a situation should arise such that $f_d < f_{ds}$, steps must be taken to assure that equation (1) is satisfied prior to making the release. These steps may include diverting Steam Generator Blowdown to the Nuclear Blowdown Processing System or decreasing the effluent flow rate.

When new candidate flow rates are chosen, the calculations above should be repeated to verify that they combine to form an acceptable release. If they do, the establishment of flow rate monitor setpoints should proceed as follows in Step 4. If they do not provide an acceptable release, the choice of candidate flow rates must be repeated until an acceptable set is identified.

- 4) The dilution flow rate setpoint for minimum flow rate, F , is established at 90 percent of the expected available dilution flow rate:

$$F = (0.9) (F_d) \quad (19)$$

Flow rate monitor setpoints for the Steam Generator Blowdown effluent stream shall be set at the selected

discharge pump rate (normally the maximum discharge pump rate) f_{ds} chosen in Step 3 above.

- 5) The Steam Generator Monitor setpoints may be specified based on the values of ΣC_i , F , and f which were specified to provide compliance with the limits of 10CFR 20, Appendix B, Table II, Column 2. The monitor response is primarily to gamma radiation, therefore, the actual setpoint is based on ΣC_g . The monitor setpoint in cpm which corresponds to the calculated value c is taken from the monitor calibration graph. (See NOTE, page 2.0-14.) The setpoint concentration, c , is determined as follows:

$$c \leq \sum_g C_g X B \quad (20)$$

$$B = f_d / f_{ds} \quad (21)$$

If $B \geq 1$, Calculate c and determine the maximum value for the actual monitor setpoint (cpm) from the monitor calibration graph.

If $B < 1$, No release may be made. Reevaluate the alternatives presented in step 3.

NOTE: If the calculated setpoint value is near actual concentrations being released or planned for release, it may be impractical to set the monitor alarm at this value. In this case a new setpoint may be calculated following the remedial methodology presented in steps 3 and 4 for the case $f_d < f_{ds}$.

Within the conditions stated above, the specific monitor setpoint concentrations for the two steam generator blowdown monitors RM-L3 and RM-L10 are calculated as shown below. Since the monitors are sensitive primarily to

gamma radiation, their setpoints will be based on the concentrations of gamma emitting radionuclides.

2.1.4.1.1 For RM-L3, Steam Generator Blowdown Discharge initial monitor, and for RM-L10, Steam Generator Blowdown Discharge final monitor:

$$c_{Sa} \text{ or } c_{Sb} \leq \left[\sum_k C_k \right]_S^{(B)} \quad (22)$$

$\left[\sum_k C_k \right]_S$ = the isotopic concentration of the Steam Generator Blowdown effluent as obtained from the sum of the measured concentrations determined by the analysis required in ODCM Table 1.1-4, in uCi/ml.

*See GENERAL NOTE under 2.1.

2.1.4.2 Turbine Building Sump and Condensate Demineralizer Backwash (Normal Mode)

For conservatism, the Turbine Building Sump and Condensate Demineralizer Backwash monitor setpoints (c_T and c_D) will claim no dilution from the Circulating Water, and will be set at the applicable concentration limit. That is:

$$c \leq C \quad (23)$$

The Turbine Building sump monitor, RM-L8, alarms and terminates release upon exceeding the monitor setpoint (c_T). The discharge can then be manually diverted to the Excess Waste Processing System. RM-L11, the Condensate Demineralizer Backwash monitor, alarms and terminates release upon exceeding the monitor setpoint (c_D). The discharge may then be manually diverted to the Turbine Building sump or simply delayed.

The Turbine Building Sump and Condensate Demineralizer Backwash monitor setpoints are to be established indepen-

dently of each other and without crediting dilution. They are to be based on the measured radionuclide concentrations of the effluent stream and are to ensure compliance with the limits of 10CFR 20, Appendix B, Table II, Column 2 prior to discharge.

For each effluent stream, a concentration factor CF must be calculated, measuring the nearness of approach of the undiluted waste stream to the specified limiting condition of the Maximum Permissible Concentration. That is,

$$CF = \left| \sum_i \frac{C_i}{MPC_i} \right| + SF \quad (24)$$

$$CF_T = \left| \sum_i \frac{C_i}{MPC_i} \right|_T + SF \quad (25)$$

$$CF_D = \left| \sum_i \frac{C_i}{MPC_i} \right|_D + SF \quad (26)$$

where:

$$\left| \sum_i \frac{C_i}{MPC_i} \right|_T = \text{the sum of the ratios of the measured concentration of nuclide } i \text{ to its limiting value } MPC_i \text{ for the Turbine Building sump effluent.}$$

$$\left| \sum_i \frac{C_i}{MPC_i} \right|_D = \text{the sum of the measured concentration of nuclide } i \text{ (in liquid only) to its limiting value } MPC_i \text{ for the Condensate Demineralizer Backwash effluent.}$$

CF_T = the concentration factor for the Turbine Building Sump Effluent.

CF_D = the concentration factor for the Condensate Demineralizer Backwash Effluent.

SF = the generic engineering safety factor used in Section 2.1.2, Step 2.
= 0.5

If $CF \leq 1$, calculate c and determine the actual monitor setpoint (cpm) from the calibration curve.

If $CF > 1$, no release may be made via this path. The release must either be delayed or diverted for additional processing. Because of spurious alarms, these remedial steps may be required if the monitor setpoints are only near the actual concentrations being released.

Within the limits of the conditions stated above, the specific monitor setpoint concentrations for RM-L8 and RM-L11 may now be calculated. Because they are primarily sensitive to gamma radiation, their setpoints will be based on the concentrations of gamma emitting radionuclides as follows:

2.1.4.2.1 For RM-L8, Turbine Building Sump Discharge Monitor:

$$c_T \leq \left| \sum_R C_R \right|_T \div CF_T \quad (27)$$

Where:

- $\left| \sum_R C_R \right|_T$ = The gamma isotopic concentration of the Turbine Building sump effluent as obtained from the sum of the measured concentrations determined by the analysis required in ODCM Table 1.1-4, in uCi/ml.
- CF_T = The Turbine Building sump Effluent Concentration Factor from equation (25).

*See GENERAL NOTE under 2.1.

2.1.4.2.2 For RM-L11, Condensate Demineralizer Backwash Discharge Monitor:

$$c_D \leq \left| \sum_g C_g \right|_D + CF_D \quad (28)$$

where:

$\left| \sum_g C_g \right|_D$ = The gamma isotopic concentration of the Condensate Demineralizer Backwash effluent (including solids) as obtained from the sum of the measured concentrations determined by the analysis required ODCM Table 1.1-4, in uCi/ml.

CF_D = The Condensate Demineralizer Backwash Effluent Concentration Factor from equation (26).

*See GENERAL NOTE under 2.1.

2.1.4.3 Steam Generator Blowdown Effluent Not Directly to Circulating Water (Alternate Mode)

Equation (23) is again used to assure that effluents are in compliance with the aforementioned specification before dilution in the receiving water:

$$c \leq C$$

Because dilution is not considered in the setpoint calculation, it is not necessary to calculate maximum permissible discharge flow rates or anticipated available dilution flow rate.

The functions of the two monitors whose setpoints are to be established are described in Section 2.1.4.1 above. The method for the determination is as follows:

- 1) If a release is found to be permissible, flow rate monitors for the active effluent streams (Steam Generator Blowdown - f_{ct} , Turbine Building sump - f_{dt} , and Condensate Demineralizer - f_{dd}) may have their setpoints established at any operationally convenient value. Since 10CFR 20 is to be

complied with before dilution, the flow rate of discharges is irrelevant.

- 2) The Concentration Factor of equation (24) is again used to ensure the permissibility of the release:

$$CF = \left| \sum_i \frac{C_i}{MPC_i} \right| + SF$$

$$CF_S = \left| \sum_i \frac{C_i}{MPC_i} \right|_S + SF \quad (29)$$

in which all terms are defined in subsection 1.1.3.1 and subscript S refers to the Steam Generator Blowdown Effluent.

If $CF \leq 1$, calculate c and determine the actual monitor setpoint (cpm) from the calibration curve.

If $CF > 1$, no release may be made via this path. The release must either be delayed or diverted for additional processing. Because of spurious alarms, these remedial steps may be required if the monitor setpoints are only near the actual concentrations being released.

Within the above limitations, setpoint concentrations may now be calculated for the two effluent monitors. Because they are primarily sensitive to gamma radiation, their setpoints will be based on the concentrations of gamma emitting radionuclides as follows:

2.1.4.3.1 For RM-L3, Steam Generator Blowdown Discharge initial monitor, and RML-10, Steam Generator Blowdown Discharge final monitor:

$$c_{Sa} \text{ or } c_{Sb} \leq \left| \sum_g C_g \right|_S + CF_S \quad (30)$$

Where:

$\left| \sum_k C_k \right|_S$ = The isotopic concentration of the Steam Generator Blowdown effluent as obtained from the sum of the measured concentrations determined by the analysis required in ODCM Table 1.1-4, in uCi/ml.

CF_s = The Steam Generator Blowdown Effluent Concentration Factor from equation (29).

*See GENERAL NOTE under 2.1.

2.1.4.4 Turbine Building Sump (Abnormal Conditions)

Provided circulating water is available, 1 to 3 circulating water pumps, effluent exceeding .5 MPC may be released from the Turbine Building sump to the industrial and sanitary waste system, using the setpoint in this section, provided the following conditions are met:

- 1) Instantaneous release rate limits of ODCM Specification 1.1.2.1 are not exceeded in the circulating water discharge canal,
- 2) The average radionuclide concentration in the industrial and sanitary waste system (Pond 6B or 008) will not exceed .5 MPC when averaged over one year,
- 3) The radionuclide concentration of the Turbine Building sump effluent does not exceed 15 MPC (ensures radionuclide concentration in discharge canal does not exceed .5 MPC, assuming maximum discharge from Steam Generator Blowdown through RM-L3 and RM-L10 and only one circulating water pump operational),
- 4) The limits of ODCM specification 1.1.4.1 will not be exceeded with the proposed release, and
- 5) Average discharge flow does not exceed values used in setpoint determination.

In addition, the source of radioactivity should be identified and isolated. Radionuclide concentration in Turbine Building sump effluent should be restored to <.5 MPC as soon as possible and normal setpoint reestablished. Radionuclide concentration in Pond 6B and 008 should be restored to < LLD using dilution as necessary. Turbine Building sump samples should be obtained and analyzed every eight hours while the alternate setpoint is

being used to ensure that the setpoint remains conservative with respect to the isotopic mixture.

Alternate setpoint methodology for Turbine Building sump (RM-L8) is available to ensure operational flexibility in the event radioactivity is detected in the Turbine Building sump > .5 MPC and release would result in minimal offsite dose. The alternate setpoint methodology is not intended to be used continuously. To remove restrictions on operation of circulating water, pond concentrations should be restored to < LLD as soon as possible. Acceptability of the release and setpoint determination will be based on the dose limits in specification 1.1.4.1 (TS 3.11.1.3), operation of liquid radwaste treatment system, since this is the most limiting condition for unprocessed effluent. The setpoint methodology follows:

2.1.4.4.1 For RM-L8, Turbine Building Sump (alternate methodology) (57)

$$C_T \leq \left(\frac{D_m}{\bar{A}_i \Delta t_k F_k} \right) \left(\frac{\sum_g C_g}{\sum_i C_i} \right)$$

where:

C_T = setpoint concentration (uCi/ml),

D_m = Daily dose margin (mrem) for most limiting dose (total body or organ).

= .06 mrem/31 day - (total body daily dose for all open permits), or

= .2 mrem/31 day - (organ daily dose using maximum organ for all open permits),

\bar{A}_i = average A_{iL} using maximum organ for each nuclide and weighted by concentration.

(58)

$$= \frac{\sum (A_{iL} \cdot C_i)}{\sum C_i}$$

where:

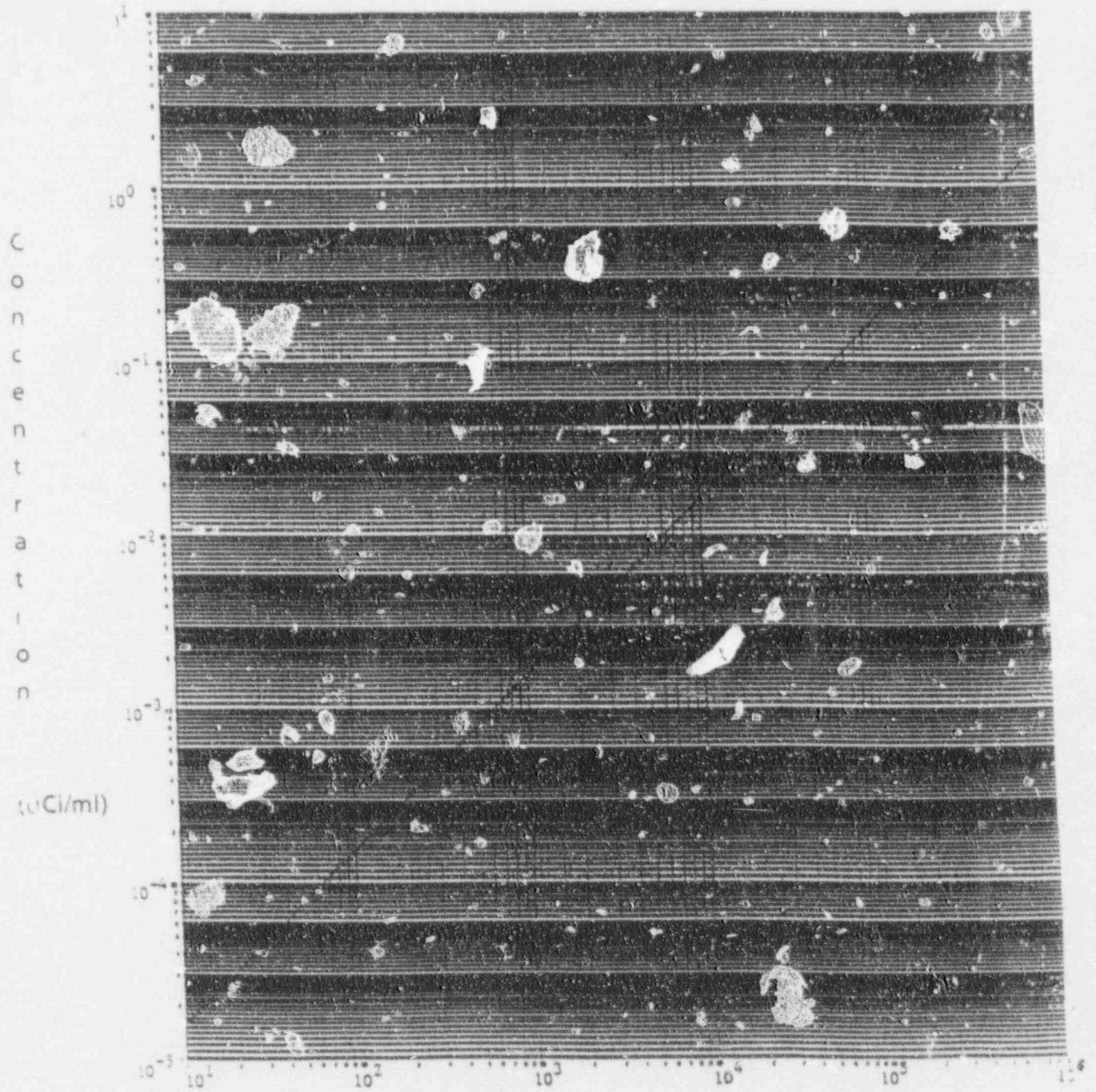
- C_i = Concentration of radionuclide i .
- A_{it} = The site related ingestion dose commitment factor to the total body or organ t , for each identified principal gamma and beta emitter listed in Table 2.2-3 (mrem-ml per hr-uCi). For calculation see section 2.2.2.
- Δt_k = the length of time (in hours) during which concentrations and flow rates are averaged. For purpose of setpoint calculation, $\Delta t_k = 24$ hours.
- F_k = The near field dilution factor for C_i during release from Turbine Building sump.
 $= \frac{\text{(average undiluted waste flow)}}{\text{(average flow from discharge structure)}}$
- $\sum_g C_g$ = The sum of concentrations of each measured gamma emitting radionuclide in the undiluted waste sample.
- $\sum_i C_i$ = The sum of the measured concentrations of all radionuclides in the undiluted waste sample (see equation 2).

For purpose of implementing section 2.1.4.4 release condition 2, the following must be satisfied.

$$\frac{\sum_{j=1}^n \left\{ \left| \sum_{i=1}^k \left(C_i / MPC_i \right) \right|_{T_j} \cdot V_j \right\}}{\sum_{j=1}^n V_j} \leq 5 \quad (59)$$

- where $[\sum(C_i / MPC_i)]_{T_j}$ = the sum of the ratios of the measured concentration of nuclide i to its limiting value MPC_i for the Turbine Building sump effluent for release permit j , including proposed permit,
- V_j = Release volume for Turbine Building sump release permit j (gal), and
- j = index for batch release permits during the previous 12 months including the proposed permit.

Figure 2.1-1
Example Liquid Effluent Monitor
Calibration Curve



2.2 Dose Calculation For Liquid Effluents

The method of this section is to be used in all cases for calculating doses to individuals from routine liquid effluents. Four notes at the end of the section confirm the values which certain parameters are to be assigned in some special cases.

2.2.1 Liquid Effluent Dose Calculation Parameters

<u>Term</u>	<u>Definition</u>	<u>Section of Initial Use</u>
$A_{i\tau}$	= the site related ingestion dose commitment factor to the total body or any organ τ , for each identified principal gamma and beta emitter listed in Table 2.2-3 in mrem-ml per hr- μ Ci.	2.2.2
BF_i	= Bioaccumulation Factor for nuclide i , in fish, pCi/Kg per pCi/l, from Table 2.2-1.	2.2.2
C_{ik}	= the average concentration of radionuclide, i , in undiluted liquid effluent during time period Δt_k from any liquid released, in uCi/ml.	2.2.2
$DF_{i\tau}$	= a dose conversion factor for nuclide, i , for adults in preselected organ, τ , in mrem/pCi found in Table 2.2-2.	2.2.2
D_t	= the cumulative dose commitment to the total body or any organ, τ , from the liquid effluents for the total time period, $\Sigma \Delta t_k$ in mrem (Ref. 1).	2.2.2
D_w	= Dilution Factor from the near field area within one-quarter mile of the release points to the potable water intake for adult water consumption; for V. C. Summer, $D_w = 1$.	2.2.2
F_k	= the near field average dilution factor for C_{ik} during any liquid effluent release.	2.2.2
K_o	= 1.14×10^5 , units conversion factor = $(10^6 \text{ pCi/uCi}) (10^3 \text{ ml/l}) \div 8760 \text{ hr/yr}$	2.2.2

Liquid Effluent Dose Calculation Parameters (continued)

<u>Term</u>	<u>Definition</u>	<u>Section of Initial Use</u>
Δt_k	= the length (in hours) of a time period over which concentrations and flow rates are averaged for dose calculations.	2.2.2
U_f	= 21 kg/yr, fish consumption (adult) (Reference 3).	2.2.2
U_w	= 730 kg/yr, water consumption (adult) (Reference 3)	2.2.2
Z	= applicable near-field dilution factor when no additional dilution is to be considered; Z = 1.	2.2.2

2.2.2 Methodology

The dose contribution from all radionuclides identified in liquid effluents released to unrestricted areas is calculated using the following expression:

$$D_i = \sum_l \left[A_{il} \sum_{k=1} \Delta t_k C_{ik} F_k \right] \quad (31)$$

$$A_{il} = K_o ((U_w/D_w) + U_f B F_i) D F_{il} \quad (32)$$

$$F_k = \frac{(\text{average undiluted liquid waste flow})}{(\text{average flow from the discharge structure}) (Z)} \quad (33)$$

NOTE 1: If radioactivity in the Monticello Reservoir (C_r) becomes > the LLD specified in ODCM, Table 1.1-4, that concentration must be included in the Dose determination. For this part of the dose calculation, $F_k = 1$ and $\Delta t_k =$ the entire time period for which the dose is being calculated.

NOTE 2: During periods when the Circulating Water Pumps are not in operation, the possibility of leakage of activity from the Industrial Water System will be accounted for as follows. Sampling of the liquid in the Sanitary and Industrial Waste

System will be initiated, and the measured concentrations of radionuclides will be used in the dose calculations with $F_k = 1$ and $\Delta t_k =$ the entire time period for which the dose is being calculated.

NOTE 3: During periods when the Circulating Water Pumps are in operation, any releases to the Sanitary and Industrial Waste System are to be credited with dilution in Circulating Water for dose calculation purposes, even though such dilution was not claimed in the setpoint calculation. When taken in union with the note above, this procedure results in some overestimation of dose to the population because discharges made to the Sanitary and Industrial Waste System just before loss of Circulating Water will be counted twice in the dose calculation process.

NOTE 4: If radioactivity in the Service Water becomes $>$ LLD as determined by the analysis required by ODCM, Table 1.1-4, that concentration must be included in the Dose determination. For this part of the dose calculation, $F_k = 1$ and $\Delta t_k =$ the entire time since the last Service Water sample was taken.

TABLE 2.2-1
 BIOACCUMULATION FACTORS*
 (pCi/kg per pCi/liter)

<u>ELEMENT</u>	<u>FRESHWATER FISH</u>
H	9.0E-01
C	4.6E 03
F	1.0E 01
Na	1.0E 02
P	1.0E 05
Cr	2.0E 02
Mn	4.0E 02
Fe	1.0E 02
Co	5.0E 01
Ni	1.0E 02
Cu	5.0E 01
Zn	2.0E 03
Br	4.2E 02
Rb	2.0E 03
Sr	3.0E 01
Y	2.5E 01
Zr	3.3E 00
Nb	3.0E 04
Mo	1.0E 01
Tc	1.5E 01
Ru	1.0E 01
Rh	1.0E 01
Sb	1.0E 00
Te	4.0E 02
I	1.5E 01
Cs	2.0E 03
Ba	4.0E 00
La	2.5E 01
Ce	1.0E 00
Pr	2.5E 01
Nd	2.5E 01
W	1.2E 03
Np	1.0E 01

*Values in Table 2.2-1 are taken from Reference 3, Table A-1

TABLE 2.2-2

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ADULT INGESTION DOSE FACTORS*
(mrem/pCi ingested)

NUCLIDE	BONE	LIVER	T.BODY	THYROID	KIDNEY	LUNG	GI-LLI
H-3	NO DATA	1.05E-07	1.05E-07	1.05E-07	1.05E-07	1.05E-07	1.05E-07
C-14	2.84E-06	5.68E-07	5.68E-07	5.68E-07	5.68E-07	5.68E-07	5.68E-07
F-18	6.24E-07	NO DATA	6.92E-08	NO DATA	NO DATA	NO DATA	1.85E-08
NA-24	1.70E-06	1.70E-06	1.70E-06	1.70E-06	1.70E-06	1.07E-06	1.70E-06
P-32	1.93E-04	1.20E-05	7.46E-06	NO DATA	NO DATA	NO DATA	2.17E-05
CR-51	NO DATA	NO DATA	2.66E-09	1.59E-09	5.86E-10	3.53E-09	6.69E-07
MN-54	NO DATA	4.57E-06	8.72E-07	NO DATA	1.36E-06	NO DATA	1.40E-05
MN-56	NO DATA	1.15E-07	2.04E-08	NO DATA	1.46E-07	NO DATA	3.67E-06
FE-55	2.75E-06	1.90E-06	4.43E-07	NO DATA	NO DATA	1.06E-06	1.09E-06
FE-59	4.34E-06	1.02E-05	3.91E-06	NO DATA	NO DATA	2.85E-06	3.40E-05
†CO-57	NO DATA	1.75E-07	2.91E-07	NO DATA	NO DATA	NO DATA	4.44E-06
CO-58	NO DATA	7.45E-07	1.67E-06	NO DATA	NO DATA	NO DATA	1.51E-05
CO-60	NO DATA	2.14E-06	4.72E-06	NO DATA	NO DATA	NO DATA	4.02E-05
NI-63	1.30E-04	9.01E-06	4.36E-06	NO DATA	NO DATA	NO DATA	1.88E-06
NI-65	5.28E-07	6.86E-08	3.13E-08	NO DATA	NO DATA	NO DATA	1.74E-06
CU-64	NO DATA	8.33E-08	3.91E-08	NO DATA	2.10E-07	NO DATA	7.10E-06
ZN-65	4.84E-06	1.54E-05	6.76E-06	NO DATA	1.03E-05	NO DATA	9.70E-06
ZN-69	1.03E-08	1.97E-08	1.37E-09	NO DATA	1.28E-08	NO DATA	2.96E-09
†BR-82	NO DATA	NO DATA	2.26E-06	NO DATA	NO DATA	NO DATA	1.59E-06
BR-83	NO DATA	NO DATA	4.02E-08	NO DATA	NO DATA	NO DATA	5.79E-08
BR-84	NO DATA	NO DATA	5.21E-08	NO DATA	NO DATA	NO DATA	4.09E-13
BR-85	NO DATA	NO DATA	2.14E-09	NO DATA	NO DATA	NO DATA	LT E-24**
RB-86	NO DATA	2.11E-05	9.83E-06	NO DATA	NO DATA	NO DATA	4.16E-06
RB-88	NO DATA	6.05E-08	3.21E-08	NO DATA	NO DATA	NO DATA	8.36E-19
RB-89	NO DATA	4.01E-08	2.82E-08	NO DATA	NO DATA	NO DATA	2.33E-21
SR-89	3.08E-04	NO DATA	8.84E-06	NO DATA	NO DATA	NO DATA	4.94E-05
SR-90	7.58E-03	NO DATA	1.86E-03	NO DATA	NO DATA	NO DATA	2.19E-04
SR-91	5.67E-06	NO DATA	2.29E-07	NO DATA	NO DATA	NO DATA	2.70E-05
SR-92	2.15E-06	NO DATA	9.30E-08	NO DATA	NO DATA	NO DATA	4.26E-05
Y-90	9.62E-09	NO DATA	2.58E-10	NO DATA	NO DATA	NO DATA	1.02E-04
Y-91M	9.09E-11	NO DATA	3.52E-12	NO DATA	NO DATA	NO DATA	2.67E-10
Y-91	1.41E-07	NO DATA	3.77E-09	NO DATA	NO DATA	NO DATA	7.76E-05
Y-92	8.45E-10	NO DATA	2.47E-11	NO DATA	NO DATA	NO DATA	1.48E-05
Y-93	2.68E-09	NO DATA	7.40E-11	NO DATA	NO DATA	NO DATA	8.50E-05
ZR-95	3.04E-08	9.75E-09	6.60E-09	NO DATA	1.53E-08	NO DATA	3.09E-05
ZR-97	1.68E-09	3.39E-10	1.55E-10	NO DATA	5.12E-10	NO DATA	1.05E-04
NB-95	6.22E-09	3.46E-09	1.86E-09	NO DATA	3.42E-09	NO DATA	2.10E-05
MO-99	NO DATA	4.31E-06	8.20E-07	NO DATA	9.76E-06	NO DATA	9.99E-06

†Values taken from Reference 13, Table 4.

*Values in Table 2.2-2 are taken from Reference 3, Table E-11.

**Less than E-24.

TABLE 2.2-2 (continued)

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NUCLIDE	BONE	LIVER	T.BODY	THYROID	KIDNEY	LUNG	GI-LLI
TC-99M	2.47E-10	6.98E-10	8.89E-09	NO DATA	1.06E-08	3.42E-10	4.13E-07
TC-101	2.54E-10	3.66E-10	3.59E-09	NO DATA	6.59E-09	1.87E-10	1.10E-21
RU-103	1.85E-07	NO DATA	7.97E-08	NO DATA	7.06E-07	NO DATA	2.16E-05
RU-105	1.54E-08	NO DATA	6.08E-07	NO DATA	1.99E-07	NO DATA	9.42E-06
RU-106	2.75E-06	NO DATA	3.48E-07	NO DATA	5.31E-06	NO DATA	1.78E-04
AG-110M	1.60E-07	1.48E-07	8.79E-08	NO DATA	2.91E-07	NO DATA	6.04E-05
†SB-124	2.80E-06	5.29E-08	1.11E-06	6.79E-09	NO DATA	2.18E-06	7.95E-05
†SB-125	1.79E-06	2.00E-08	4.26E-07	1.82E-09	NO DATA	1.38E-06	1.97E-05
†SB-126	1.15E-06	2.34E-08	4.15E-07	7.04E-09	NO DATA	7.05E-07	9.40E-05
TE-125M	2.68E-06	9.71E-07	3.59E-07	8.06E-07	1.09E-05	NO DATA	1.07E-05
TE-127M	6.77E-06	2.42E-06	8.25E-07	1.73E-06	2.75E-05	NO DATA	2.27E-05
TE-127	1.10E-07	3.95E-08	2.38E-08	8.15E-08	4.48E-07	NO DATA	8.68E-06
TE-129M	1.15E-05	4.29E-06	1.82E-06	3.95E-06	4.80E-05	NO DATA	5.79E-05
TE-129	3.14E-08	1.18E-08	7.65E-09	2.41E-08	1.32E-07	NO DATA	2.37E-08
TE-131M	1.73E-06	8.46E-07	7.05E-07	1.34E-06	8.57E-06	NO DATA	8.40E-05
TE-131	1.97E-08	8.23E-09	6.22E-09	1.62E-08	8.63E-08	NO DATA	2.79E-09
TE-132	2.52E-06	1.63E-06	1.53E-06	1.80E-06	1.57E-05	NO DATA	7.71E-05
I-130	7.56E-06	2.23E-06	8.80E-07	1.89E-04	3.48E-06	NO DATA	1.92E-06
I-131	4.16E-06	5.95E-06	3.41E-06	1.95E-03	1.02E-05	NO DATA	1.57E-06
I-132	2.03E-07	5.43E-07	1.90E-07	1.90E-05	8.65E-07	NO DATA	1.02E-07
I-133	1.42E-06	2.47E-06	7.53E-07	3.63E-04	4.31E-06	NO DATA	2.22E-06
I-134	1.06E-07	2.88E-07	1.03E-07	4.99E-06	4.58E-07	NO DATA	2.51E-10
I-135	4.43E-07	1.16E-06	4.28E-07	7.65E-05	1.86E-06	NO DATA	1.31E-06
CS-134	6.22E-05	1.48E-04	1.21E-04	NO DATA	4.79E-05	1.59E-05	2.59E-06
CS-136	6.51E-06	2.57E-05	1.85E-05	NO DATA	1.43E-05	1.96E-06	2.92E-06
CS-137	7.97E-05	1.09E-04	7.14E-05	NO DATA	3.70E-05	1.23E-05	2.11E-06
CS-138	5.52E-08	1.09E-07	5.40E-08	NO DATA	8.01E-08	7.91E-09	4.65E-13
BA-139	9.70E-08	6.91E-11	2.84E-09	NO DATA	6.46E-11	3.92E-11	1.72E-07
BA-140	2.03E-05	2.55E-08	1.33E-06	NO DATA	8.67E-09	1.46E-08	4.18E-05
BA-141	4.71E-08	3.56E-11	1.59E-09	NO DATA	3.31E-11	2.02E-11	2.22E-17
BA-142	2.13E-08	2.19E-11	1.34E-09	NO DATA	1.85E-11	1.24E-11	3.00E-26
LA-140	2.50E-09	1.26E-09	3.33E-10	NO DATA	NO DATA	NO DATA	9.25E-05
LA-142	1.28E-10	5.82E-11	1.45E-11	NO DATA	NO DATA	NO DATA	4.25E-07
CE-141	9.36E-09	6.33E-09	7.18E-10	NO DATA	2.94E-09	NO DATA	2.42E-05
CE-143	1.65E-09	1.22E-06	1.35E-10	NO DATA	5.37E-10	NO DATA	4.56E-05
CE-144	4.88E-07	2.04E-07	2.62E-08	NO DATA	1.21E-07	NO DATA	1.65E-04
PR-143	9.20E-09	3.69E-09	4.56E-10	NO DATA	2.13E-09	NO DATA	4.03E-05
PR-144	3.01E-11	1.25E-11	1.53E-12	NO DATA	7.05E-12	NO DATA	4.33E-18
ND-147	6.29E-09	7.27E-09	4.35E-10	NO DATA	4.25E-09	NO DATA	3.49E-05
W-187	1.03E-07	8.61E-08	3.01E-08	NO DATA	NO DATA	NO DATA	2.82E-05
NP-239	1.19E-09	1.17E-10	6.45E-11	NO DATA	3.65E-10	NO DATA	2.40E-05

ODCM, V.C. Summer, SCE&G: Revision 16 (September 1991)

TABLE 2.2-3
 SITE RELATED INGESTION
 DOSE COMMITMENT FACTOR, A_{it}^*
 (mrem/hr per $\mu\text{Ci/ml}$)
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NUCLIDE	BONE	LIVER	T.BODY	THYROID	KIDNEY	LUNG	GI-LLI
H-3	NO DATA	8.96E + 00	8.96E + 00	8.96E + 00	8.96E + 00	8.96E + 00	8.96E + 00
C-14	3.15E + 04	6.30E + 03	6.30E + 03	6.30E + 03	6.30E + 03	6.30E + 03	6.30E + 03
F-18	6.69E + 01	NO DATA	7.42E + 00	NO DATA	NO DATA	NO DATA	1.98E + 00
NA-24	5.48E + 02	5.48E + 02	5.48E + 02	5.48E + 02	5.48E + 02	5.48E + 02	5.48E + 02
P-32	4.62E + 07	2.87E + 06	1.79E + 06	NO DATA	NO DATA	NO DATA	5.20E + 06
CR-51	NO DATA	NO DATA	1.49E + 00	8.94E-01	3.29E-01	1.98E + 00	3.76E + 02
MN-54	NO DATA	4.76E + 03	9.08E + 02	NO DATA	1.42E + 03	NO DATA	1.46E + 04
MN-56	NO DATA	1.2E + 02	2.12E + 01	NO DATA	1.52E + 02	NO DATA	3.82E + 03
FE-55	1.97E + 02	6.13E + 02	1.43E + 02	NO DATA	NO DATA	3.42E + 02	3.52E + 02
FE-59	1.40E + 03	3.29E + 03	1.26E + 03	NO DATA	NO DATA	9.19E + 02	1.10E + 04
CO-57	NO DATA	3.55E + 01	5.91E + 01	NO DATA	NO DATA	NO DATA	9.01E + 02
CO-58	NO DATA	1.51E + 02	3.39E + 02	NO DATA	NO DATA	NO DATA	3.06E + 03
CO-60	NO DATA	4.34E + 02	9.58E + 02	NO DATA	NO DATA	NO DATA	8.16E + 03
NI-63	4.19E + 04	2.91E + 03	1.41E + 03	NO DATA	NO DATA	NO DATA	5.07E + 02
NI-65	1.70E + 02	2.21E + 01	1.01E + 01	NO DATA	NO DATA	NO DATA	5.61E + 02
CU-64	NO DATA	1.69E + 01	7.93E + 00	NO DATA	4.26E + 01	NO DATA	1.44E + 03
ZN-65	2.36E + 04	7.50E + 04	3.39E + 04	NO DATA	5.02E + 04	NO DATA	4.73E + 04
ZN-69	5.02E + 01	9.60E + 01	6.67E + 00	NO DATA	6.24E + 01	NO DATA	1.44E + 01
BR-82	NO DATA	NO DATA	2.46E + 03	NO DATA	NO DATA	NO DATA	2.82E + 03
BR-83	NO DATA	NO DATA	4.38E + 01	NO DATA	NO DATA	NO DATA	6.30E + 01
BR-84	NO DATA	NO DATA	5.67E + 01	NO DATA	NO DATA	NO DATA	4.45E - 04
BR-85	NO DATA	NO DATA	2.33E + 00	NO DATA	NO DATA	NO DATA	1.09E - 15
RB-86	NO DATA	1.03E + 05	4.79E + 04	NO DATA	NO DATA	NO DATA	2.03E + 04
RB-88	NO DATA	2.95E + 02	1.56E + 02	NO DATA	NO DATA	NO DATA	4.07E - 09
RB-89	NO DATA	1.95E + 02	1.37E + 02	NO DATA	NO DATA	NO DATA	1.13E - 11
SR-89	4.78E + 04	NO DATA	1.37E + 03	NO DATA	NO DATA	NO DATA	7.66E + 03
SR-90	1.18E + 06	NO DATA	2.88E + 05	NO DATA	NO DATA	NO DATA	3.48E + 04
SR-91	8.79E + 02	NO DATA	3.55E + 01	NO DATA	NO DATA	NO DATA	4.19E + 03
SR-92	3.33E + 02	NO DATA	1.44E + 01	NO DATA	NO DATA	NO DATA	6.60E + 03
Y-90	1.38E + 00	NO DATA	3.69E - 02	NO DATA	NO DATA	NO DATA	1.46E + 04
Y-91M	1.30E - 02	NO DATA	5.04E - 04	NO DATA	NO DATA	NO DATA	3.82E - 02
Y-91	2.02E + 01	NO DATA	5.39E - 01	NO DATA	NO DATA	NO DATA	1.11E + 04
Y-92	1.21E - 01	NO DATA	3.53E - 03	NO DATA	NO DATA	NO DATA	2.12E + 03
Y-93	3.83E - 01	NO DATA	1.06E - 02	NO DATA	NO DATA	NO DATA	1.22E + 04
ZR-95	2.77E + 00	8.88E - 01	6.01E - 01	NO DATA	1.39E + 00	NO DATA	2.82E + 03
ZR-97	1.53E - 01	3.09E - 02	1.41E - 02	NO DATA	4.67E - 02	NO DATA	9.57E + 03
NB-95	4.47E + 02	2.49E + 02	1.34E + 02	NO DATA	2.46E + 02	NO DATA	1.51E + 06

*Calculated using equation (32) and Tables 2.2-1 and 2.2-2.

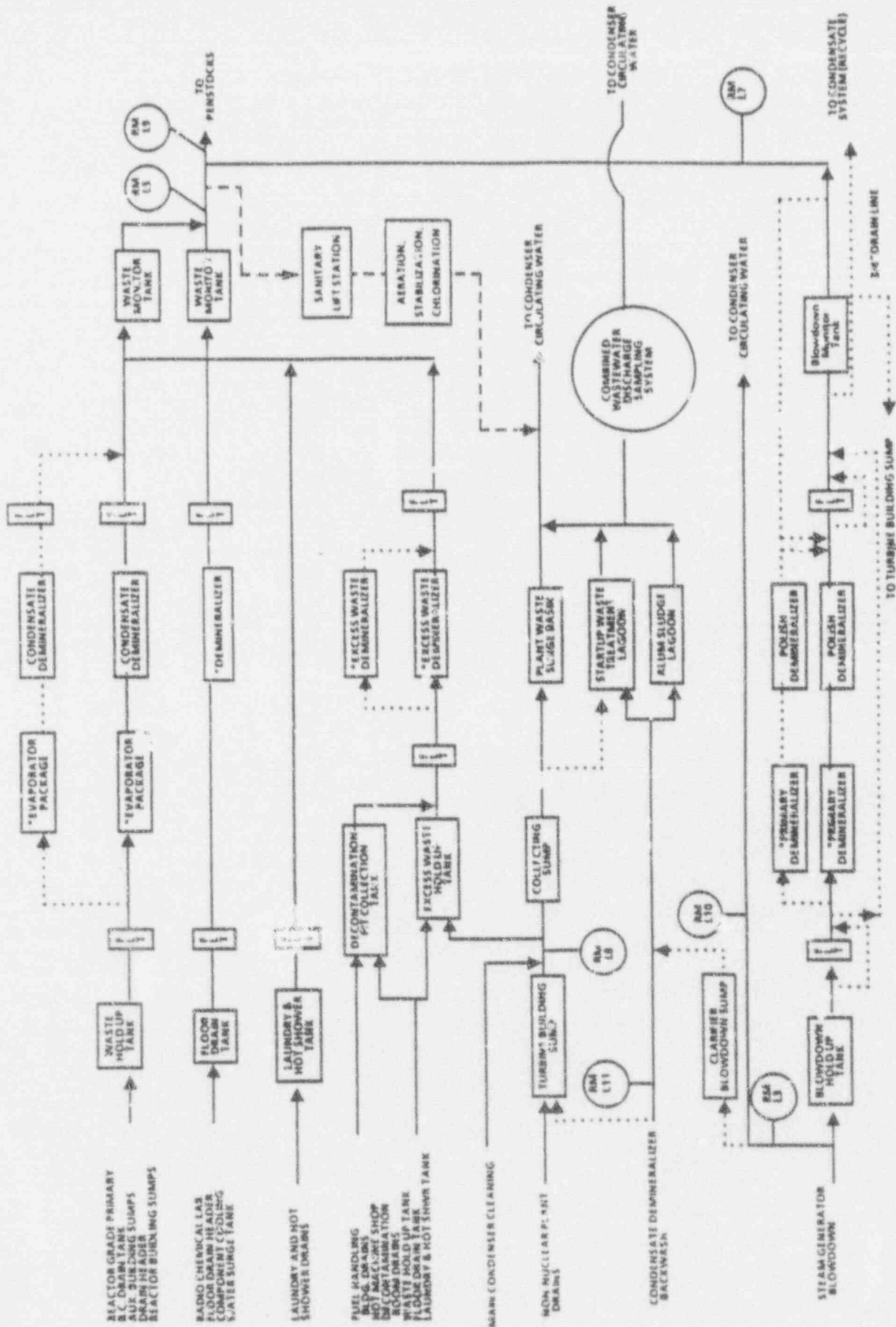
TABLE 2.2-3
 SITE RELATED INGESTION
 DOSE COMMITMENT FACTOR, A_{IC}^*
 (mrem/hr per $\mu\text{Ci/ml}$)

Page 2 of 2

NUCLIDE	BONE	LIVER	T.BODY	THYROID	KIDNEY	LUNG	GI-LLI
MO-99	NO DATA	4.62E + 02	8.79E + 01	NO DATA	1.05E + 03	NO DATA	1.07E + 03
TC-99M	2.94E - 02	8.32E - 02	1.06E + 00	NO DATA	1.26E + 00	4.07E - 02	4.92E + 01
TC-101	3.03E - 02	4.36E - 02	4.28E - 01	NO DATA	7.85E - 01	2.23E - 02	1.31E - 13
RU-103	1.98E + 01	NO DATA	8.54E - 01	NO DATA	7.57E + 01	NO DATA	2.31E + 03
RU-105	1.65E + 00	NO DATA	6.52E - 01	NO DATA	2.13E + 01	NO DATA	1.01E + 03
RU-106	2.95E + 02	NO DATA	3.73E + 01	NO DATA	5.69E + 02	NO DATA	1.91E + 04
AG-110M	1.42E + 01	1.31E + 01	7.80E + 00	NO DATA	2.58E + 01	NO DATA	5.36E + 03
SB-124	2.40E + 02	4.53E + 00	9.50E + 01	5.81E - 01	NO DATA	1.87E + 02	6.81E + 03
SB-125	1.53E + 02	1.71E + 00	3.65E + 01	1.56E - 01	NO DATA	1.18E + 02	1.69E + 03
SB-126	9.85E + 01	2.00E + 00	3.55E + 01	6.03E - 01	NO DATA	6.04E + 01	8.05E + 03
TE-125M	2.79E + 03	1.01E + 03	3.74E + 02	8.39E + 02	1.13E + 04	NO DATA	1.11E + 04
TE-127M	7.05E + 03	2.52E + 03	8.59E + 02	1.80E + 03	2.86E + 04	NO DATA	2.36E + 04
TE-127	1.14E + 02	4.11E + 01	2.48E + 01	8.48E + 01	4.66E + 02	NO DATA	9.03E + 03
TE-129M	1.20E + 04	4.47E + 03	1.89E + 03	4.11E + 03	5.00E + 04	NO DATA	6.03E + 04
TE-129	3.27E + 01	1.23E + 01	7.96E + 00	2.51E + 01	1.37E + 02	NO DATA	2.47E + 01
TE-131M	1.88E + 03	8.81E + 02	7.34E + 02	1.39E + 01	8.92E + 03	NO DATA	8.74E + 04
TE-131	2.05E + 01	8.57E + 00	6.47E + 00	1.69E + 01	8.98E + 01	NO DATA	2.90E + 00
TE-132	2.62E + 03	1.70E + 03	1.59E + 03	1.87E + 03	1.63E + 04	NO DATA	8.02E + 00
I-130	9.01E + 01	2.66E + 02	1.05E + 02	2.25E + 04	4.15E + 02	NO DATA	2.29E + 02
I-131	4.96E + 02	7.09E + 02	4.06E + 02	2.32E + 05	1.22E + 03	NO DATA	1.87E + 02
I-132	2.42E + 01	6.47E + 01	2.26E + 01	2.26E + 03	1.03E + 02	NO DATA	1.22E + 01
I-133	1.69E + 02	2.94E + 02	8.97E + 01	4.32E + 04	5.13E + 02	NO DATA	2.64E + 02
I-134	1.26E + 01	3.43E + 01	1.23E + 01	5.94E + 02	5.46E + 01	NO DATA	2.99E - 02
I-135	5.28E + 01	1.38E + 02	5.10E + 01	9.11E + 03	2.22E + 02	NO DATA	1.56E + 02
CS-134	3.03E + 05	7.21E + 05	5.89E + 05	NO DATA	2.33E + 05	7.75E + 04	1.26E + 04
CS-136	3.17E + 04	1.25E + 05	9.01E + 04	NO DATA	6.97E + 04	9.55E + 03	1.42E + 04
CS-137	3.88E + 05	5.31E + 05	3.48E + 05	NO DATA	1.88E + 05	5.99E + 04	1.03E + 04
CS-138	2.69E + 02	5.31E + 02	2.63E + 02	NO DATA	3.90E + 02	3.85E + 01	2.27E - 03
BA-139	9.00E + 00	6.41E - 03	2.64E - 01	NO DATA	5.99E - 03	3.64E - 03	1.60E + 01
BA-140	1.88E - 03	2.37E + 00	1.23E + 02	NO DATA	8.05E - 01	1.35E + 00	3.88E + 03
BA-141	4.27E + 00	3.30E - 03	1.48E - 01	NO DATA	3.07E - 03	1.87E - 03	2.06E - 09
BA-142	1.98E + 00	2.03E - 03	1.24E - 01	NO DATA	1.72E - 03	1.15E - 03	2.78E - 18
LA-140	3.58E - 01	1.80E - 01	4.76E - 02	NO DATA	NO DATA	NO DATA	1.32E + 04
LA-142	1.83E - 02	8.33E - 03	2.07E - 03	NO DATA	NO DATA	NO DATA	6.08E + 01
CE-141	8.01E - 01	5.42E - 01	6.15E - 02	NO DATA	2.52E - 01	NO DATA	2.07E + 03
CE-143	1.41E - 01	1.04E + 02	1.16E - 02	NO DATA	4.60E - 02	NO DATA	3.90E + 03
CE-144	4.18E + 01	1.77E + 01	2.24E + 00	NO DATA	1.04E + 01	NO DATA	1.41E + 04
PR-143	1.32E + 00	5.28E - 01	6.52E - 02	NO DATA	3.05E - 01	NO DATA	5.77E + 03
PR-144	4.31E - 03	1.79E - 03	2.19E - 04	NO DATA	1.01E - 03	NO DATA	6.19E - 10
ND-147	9.00E - 01	1.04E + 00	6.22E - 02	NO DATA	6.08E - 01	NO DATA	4.99E + 03
W-187	3.04E + 02	2.55E + 02	8.90E + 01	NO DATA	NO DATA	NO DATA	8.34E + 04
NP-239	1.28E - 01	1.25E - 02	6.91E - 03	NO DATA	3.91E - 02	NO DATA	2.57E + 03

LIQUID RADWASTE TREATMENT SYSTEM

FIGURE 2.2-1



3.0 GASEOUS EFFLUENT

3.1 Gaseous Effluent Monitor Setpoints

The calculated setpoint values will be regarded as upper bounds for the actual setpoint adjustments. That is, setpoint adjustments are not required to be performed if the existing setpoint level corresponds to a lower count rate than the calculated value. Setpoints may be established at values lower than the calculated values, if desired.

Calculated monitor setpoints may be added to the ambient background count rate.

3.1.1 Gaseous Effluent Monitor Setpoint Calculation Parameters

<u>Term</u>	<u>Definition</u>	<u>Section of Initial Use</u>
C_v =	count rate of a station vent monitor corresponding to grab sample radionuclide concentrations, X_{iv} , as determined from the monitor's calibration curve, in cpm.	(3.1.2)
C'_v =	the count rate of the monitor on vent v corresponding to X'_v uCi/cc of Xe-133, in cpm.	(3.1.4)
c =	count rate of the gas decay system monitor for measured radionuclide concentrations corrected to discharge pressure, in cpm.	(3.1.3)
c' =	the count rate of the waste gas decay system monitor corresponding to the total noble gas concentration in cpm.	(3.1.4)
D_{SS} =	limiting dose rate to the skin (3000 mrem/year).	(3.1.2)
D_{TB} =	limiting dose rate to the total body (500 mrem/year).	(3.1.2)
F_v =	the flow rate in vent v (cc/sec) (1 cc/sec = 0.002119 cfm).	(3.1.2)
f_s =	the maximum permissible waste gas discharge rate, based on the actual radionuclide mix and skin dose rate (cc/sec).	(3.1.3)

<u>Term</u>	<u>Definition</u>	<u>Section of Initial Use</u>
f_t	= the maximum permissible waste gas discharge rate, based on the actual radionuclide mix and total body dose rate (cc/sec).	(3.1.3)
f_w	= the maximum permissible waste gas discharge rate, the lesser of f_t and f_s (cc/sec).	(3.1.3)
f'_s	= the conservative maximum permissible waste gas discharge rate based on Kr-89 skin dose rate (cc/sec).	(3.1.4)
f'_t	= the conservative maximum permissible waste gas discharge rate based on Kr-89 total body dose rate (cc/sec).	(3.1.4)
K_i	= total body dose factor due to gamma emissions from isotope i (mrem/year per $\mu\text{Ci}/\text{m}^3$) from Table 3.1-1.	(3.1.2)
$K_{\text{Kr-89}}$	= total body dose factor for Kr-89, the most restrictive isotope from Table 3.1-1 (mrem/yr per $\mu\text{Ci}/\text{m}^3$).	(3.1.3)
L_i	= Skin dose factor due to beta emissions from isotope i (mrem/yr per $\mu\text{Ci}/\text{m}^3$) from Table 3.1-1.	(3.1.2)
$L_{\text{Kr-89}}$	= skin dose factor for Kr-89, the most restrictive isotope, from Table 3.1-1 (mrem/yr per $\mu\text{Ci}/\text{m}^3$).	(3.1.3)
M_i	= air dose factor due to gamma emissions from isotope i (mrad/yr per $\mu\text{Ci}/\text{m}^3$) from Table 3.1-1.	(3.1.2)
$M_{\text{Kr-89}}$	= air dose factor for Kr-89, the most restrictive isotope, from Table 3.1-1 (mrad/yr per $\mu\text{Ci}/\text{m}^3$).	(3.1.3)
R_s	= count rate per mrem/yr to the skin.	(3.1.2)
R_t	= count rate per mrem/yr to the total body.	(3.1.2)
R'_s	= conservative count rate per mrem to the skin (Xe-133 detection, Kr-89 dose).	(3.1.4)
R'_t	= conservative count rate per mrem to the total body (Xe-133 detection, Kr-89 dose).	(3.1.4)

<u>Term</u>	<u>Definition</u>	<u>Section of Initial Use</u>
S_d =	count rate of the waste gas decay system noble gas monitor at the alarm setpoint, in cpm.	(3.1.3)
S_v =	count rate of a station vent noble gas monitor at the alarm setpoint, in cpm.	(3.1.2)
S_{vc} =	count rate of the containment purge noble gas monitor at the alarm setpoint, in cpm.	(3.1.2)
S_{vp} =	count rate of the plant vent noble gas monitor at the alarm setpoint, in cpm.	(3.1.2)
X_{id} =	the concentration of noble gas radionuclide i in a waste gas decay tank, as corrected to the pressure of the discharge stream at the point of its flow measurement in uCi/cc.	(3.1.3)
X_v =	the measured concentration of noble gas radionuclide i in the last grab sample analyzed for vent v in uCi/cc.	(3.1.2)
X_d' =	the total noble gas concentration in a waste gas decay tank, as corrected to the pressure of the discharge stream at the point of its flow measurement in uCi/cc.	(3.1.4)
X_v' =	a concentration of Xe-133 chosen to be in the operating range of the monitor on vent v in uCi/cc.	(3.1.4)
$\overline{X/Q}$ =	the highest annual average relative concentration in any sector, at the site boundary in sec/m ³ .	(3.1.2)
1.0 =	mrem skin dose per marad air dose	(3.1.2)
0.25 =	the safety factor applied to each of the two vent noble gas monitors (plant vent and containment purge) to assure that the sum of the releases has a combined safety factor of <u>0.5</u> which allows a 100 percent margin for cumulative uncertainties of measurements.	(3.1.2)

TABLE 3.1-1

DOSE FACTORS FOR EXPOSURE TO A SEMI-INFINITE CLOUD OF NOBLE GASES,*

Nuclide	γ -Body*** (Ki)	β -Skin*** (Li)	γ -Air** (Mi)	β -Air** (Ni)
Kr-85m	1.17E + 03****	1.46E + 03	1.23E + 03	1.97E + 03
Kr-85	1.61E + 01	1.34E + 03	1.72E + 01	1.95E + 03
Kr-87	5.92E + 03	9.73E + 03	6.17E + 03	1.03E + 04
Kr-88	1.47E + 04	2.37E + 03	1.52E + 04	2.93E + 04
Kr-89	1.66E + 04	1.01E + 04	1.73E + 04	1.06E + 04
Kr-90	1.56E + 04	7.29E + 03	1.63E + 04	7.83E + 03
Xe-131m	9.15E + 01	4.76E + 02	1.56E + 02	1.11E + 03
Xe-133m	2.51E + 02	9.94E + 02	3.27E + 02	1.48E + 03
Xe-133	2.94E + 02	3.06E + 02	2.53E + 02	1.05E + 03
Xe-135m	3.12E + 03	7.11E + 02	3.36E + 03	7.39E + 02
Xe-135	1.81E + 03	1.86E + 03	1.92E + 03	2.46E + 03
Xe-137	1.42E + 03	1.22E + 04	1.51E + 03	1.27E + 04
Xe-138	8.83E + 03	4.13E + 03	9.21E + 03	4.75E + 03
Ar-41	8.84E + 03	2.69E + 03	9.30E + 03	1.28E + 03

*Values taken from Reference 3, Table B-1

** $\frac{\text{mrad}\cdot\text{m}^3}{\mu\text{Ci}\cdot\text{yr}}$

*** $\frac{\text{mrem}\cdot\text{m}^3}{\mu\text{Ci}\cdot\text{yr}}$

**** $1.17\text{E} + 03 = 1.17 \times 10^3$

CO1+ 3.1.2 Station Vent Noble Gas Monitors (RM-A3 and RM-A4)

For the purpose of implementation of section 1.2.1 of the ODCM, the alarm setpoint level for the station vent noble gas monitors will be calculated as follows:

S_v = count rate of the plant vent noble gas monitor ($= S_{vp}$ for RM-A3) or the containment purge noble gas monitor ($= S_{vc}$ for RM-A4) at the alarm setpoint level.

$$0.25 \times R_t \times D_{TB} \quad (34)$$

= the lesser of or

$$0.25 \times R_s \times D_{SS} \quad (35)$$

0.25 = the safety factor applied to each of the two vent noble gas monitors (plant vent and containment purge) to assure that the sum of the releases has a combined safety factor of 0.5 which allows a 100 percent margin for cumulative uncertainties of measurements.

D_{TB} = Dose rate limit to the total body of an individual
= 500 mrem/yr

R_t = count rate per mrem/yr to the total body
= $C_v / ((\overline{X/Q}) \times F_v \times \sum_i K_i X_{iv})$ (36)

D_{SS} = Dose rate limit to the skin of the body of an individual in an unrestricted area.
= 3000 mrem/year.

R_s = count rate per mrem/yr to the skin.
= $C_v \div [\overline{X/Q} \times F_v \times \sum_i (L_i + 1.1 M_i) X_{iv}]$ (37)

X_{iv} = the measured concentration of noble gas radionuclide i in the last grab sample analyzed for vent v , $\mu\text{Ci/ml}$. (For the plant vent, grab samples are taken at least

monthly. For the 6" and 36" containment purge lines, the sample is taken just prior to the release and also monthly, if the release is continuous.)

F_v = the flow rate in vent v, cc/sec. (1 cc/sec = 0.002119 cfm)

C_v = count rate, in cpm, of the monitor on station vent v corresponding to grab sample noble gas concentrations, X_{iv} , as determined from the monitor's calibration curve. (Initial calibration curves of the type shown in Figure 2.1-1 have been determined conservatively from families of response curves supplied by the monitor manufacturers. As releases occur, a historical correlation will be prepared and placed in service when sufficient data are accumulated.)

$\overline{X/Q}$ = the highest annual average relative concentration in any sector, at the site boundary

= 5.3×10^{-6} sec/m³ in the SE sector*

K_i = total body dose factor due to gamma emissions from isotope i (mrem/yr per $\mu\text{Ci}/\text{m}^3$) from Table 3.1-1.

L_i = skin dose factor due to beta emissions from isotope i (mrem/yr per $\mu\text{Ci}/\text{m}^3$) from Table 3.1-1.

1.1 = mrem skin dose per mrad air dose

M_i = air dose factor due to gamma emissions from isotope i (mrad/yr per $\mu\text{Ci}/\text{m}^3$) from Table 3.1-1.

* Reference 4, Section 11.3.8 states that this is the annual average relative dispersion at the point on the exclusion boundary where highest concentrations may be expected.

NOTE: At plant startups when no grab sample analysis is available for the continuous releases, the Alternate Methodology of Section 3.1.4 must be used.

3.1.3 Waste Gas Decay System Monitor (RM-A10)

The permissible conditions for discharge through the waste gas decay system monitor (RM-A10) will be calculated in a manner similar to that for the plant vent noble gas monitor. In the case of the waste gas system, however, the discharge flow rate is continuously controllable by valve HCV-014 and permissible release conditions are therefore defined in terms of both flow rate and concentration. Therefore, RM-A10 is used only to insure that a representative sample was obtained.

For operational convenience, (to prevent spurious alarms due to fluctuations in background) the setpoint level will be established at 1.5 times the measured waste concentration.

The maximum permissible flow rate will be set on the same basis but include the engineering safety factor of 0.5. The RM-A10 setpoint level S_d is defined as:

$$S_d \leq 1.5c \quad (38)$$

where:

c = count rate in CPM of the waste gas decay system monitor corresponding to the measured concentration (taken from the monitor calibration curves).

The maximum permissible waste gas flow rate f_w (cc/sec) is calculated from the maximum permissible dose rates at the site boundary according to:

$$f_w \cong \text{the lesser of } f_1 \text{ or } f_2 \quad (39)$$

f_t = the maximum permissible discharge rate based on total body dose rate.

$$= 0.25 \times D_{TB} / [\bar{X}/\bar{Q} \times 1.5 \sum_i X_{id} K_i] \quad (40)$$

f_s = the maximum permissible discharge rate based on skin dose rate.

$$= 0.25 \times D_{SS} / [\bar{X}/\bar{Q} \times 1.5 \sum_i X_{id} (L_i + 1.1M_i)] \quad (41)$$

X_{id} = the concentration of noble gas radionuclide i in the waste gas decay tank whose contents are to be discharged, as corrected to the pressure of the discharge stream at the point of the flow rate measurement. The maximum discharge pressure as governed by the diaphragm valve, 7896, is 30 psia.

NOTE: The factor of 1.5 in the denominators of equations (40) and (41) places f_w on the same basis as S_d .

When a discharge is to be conducted, valve HCV-014 is to be opened until (a) the waste gas discharge flow rate reaches $0.9 \times f_w$ or (b) the count rate of the plant vent noble gas monitor RM-A3 approaches its setpoint, whichever of the above conditions is reached first.

When no discharges are being made from the Waste Gas Decay System, the RM-A10 setpoint should be established as near background as practical to prevent spurious alarms and yet alarm in the event of an inadvertent release.

3.1.4 Alternative Methodology for Establishing Conservative Setpoints

A more conservative setpoint may be calculated to minimize requirements for adjustment of the monitor as follows:

For a plant vent:

R'_t = conservative count rate per mrem/yr to the total body (Xe-133 detection, Kr-89 dose)

$$= C_v' + [\overline{X/Q} \times K_{Kr-89} \times X_v' \times F_v], \quad (42)$$

where:

X_v' = a concentration of Xe-133 chosen to be in the operating range of the monitor on vent v, $\mu\text{Ci/cc}$.

C_v' = the count rate in CPM of the monitor on vent v corresponding to X_v' $\mu\text{Ci/cc}$ of Xe-133.

K_{Kr-89} = total body dose factor for Kr-89, the most restrictive isotope from Table 3.1-1.

R_s' = count rate per mrem/yr to the skin.

$$= C_v' + [\overline{X/Q} \times (L_{Kr-89} + 1.1M_{Kr-89}) \times X_v' \times F_v] \quad (43)$$

where:

L_{Kr-89} = skin dose factor for Kr-89, the most restrictive isotope from Table 3.1-1.

M_{Kr-89} = air dose factor for Kr-89, the most restrictive isotope, from Table 3.1-1.

For the waste gas decay system:

f_t' = the conservative maximum permissible discharge rate based on Kr-89 total body dose rate.

$$= 0.25 \times D_{TB} + [\overline{X/Q} \times 1.5 \times X_d' \times K_{Kr-89}] \quad (44)$$

f_s' = the conservative maximum permissible discharge rate based on Kr-89 skin dose rate.

$$= 0.25 \times D_{SS} + [\overline{X/Q} \times 1.5 \times X_d' \times (L_{Kr-89} + 1.1M_{Kr-89})] \quad (45)$$

X_d' = the total concentration of noble gas radionuclides in the waste gas decay tank whose contents are to be discharged, as corrected to the pressure of the discharge stream at the point of the flow measurement.

c' = count rate in cpm of the waste gas decay system monitor corresponding to X_d' $\mu\text{Ci/cc}$ of Kr-85.

3.1.5 Meteorological Release Criteria for Batch Releases

Planned gaseous batch releases (WGDT) will be made during favorable meteorology. Limiting releases to favorable meteorology provides assurance that release conditions will be conservative with respect to annual average dispersion values ($\overline{X/Q}$, $\overline{X/Q}$). Favorable meteorology is defined in Table 3.1-2.

Table 3.1-2

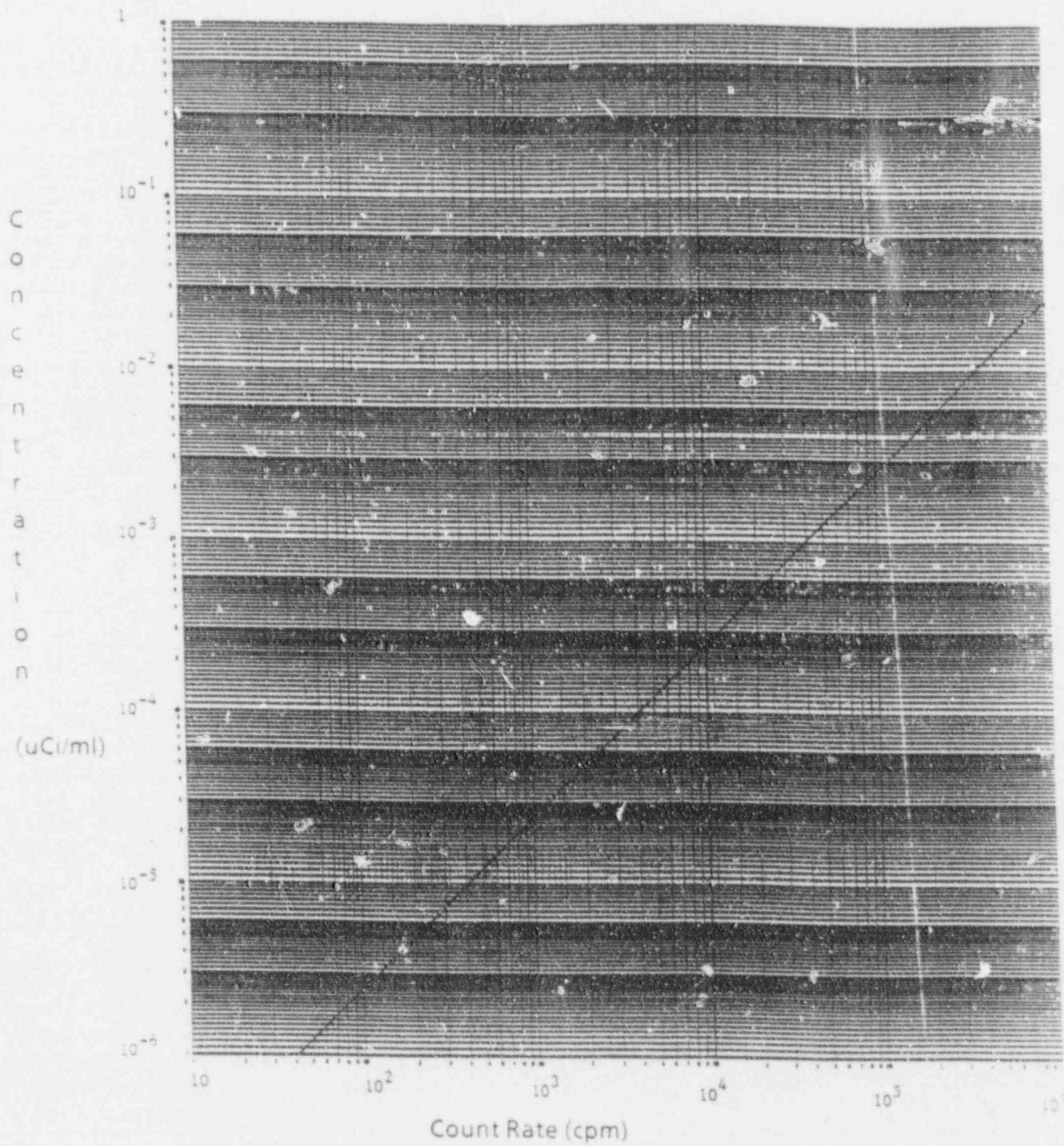
Favorable Meteorology

Differential Temperature (ΔT) ¹ °F		Stability Class	Wind Speed ² (mph)	
61m - 10m	40m - 10m		10m	61m
$\Delta T \leq -1.74$	$\Delta T \leq -1.03$	A	*	*
$-1.74 < \Delta T \leq -1.56$	$-1.03 < \Delta T \leq -0.92$	B	*	*
$-1.55 < \Delta T \leq -1.38$	$-0.92 < \Delta T \leq -0.81$	C	1.3	1.6
$-1.38 < \Delta T \leq -0.46$	$-0.81 < \Delta T \leq -0.27$	D	3.1	4.1
$-0.46 < \Delta T \leq 1.38$	$-0.27 < \Delta T \leq 0.81$	E	3.5	6.6
$1.38 < \Delta T \leq 3.67$	$0.81 < \Delta T \leq 2.16$	F	5.2	14.0
$3.67 < \Delta T$	$2.16 < \Delta T$	G	7.0	18.9

Notes:

- 1 The ΔT values for 61m - 10m are considered as primary indicators for determination of stability class. The 40m - 10m ΔT values are used only when 61m - 10m values are not available. All ΔT values are listed in °F and are based on values in USNRC Regulatory Guide 1.23.
 - 2 The 10m wind speed is considered the primary indication for windspeed. The 61m wind speed indication should only be used if 10m is not available.
- * No wind is required for planned releases.

Figure 3.1-1
Example Noble Gas Monitor
Calibration Curve



3.2 Dose Calculation for Gaseous Effluent

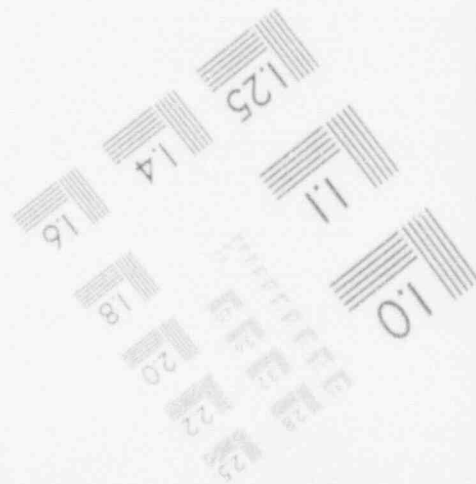
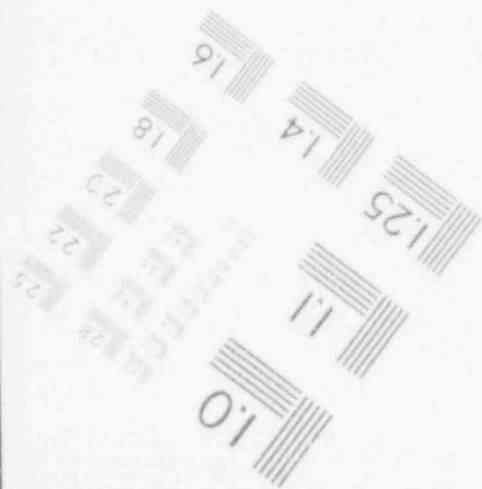
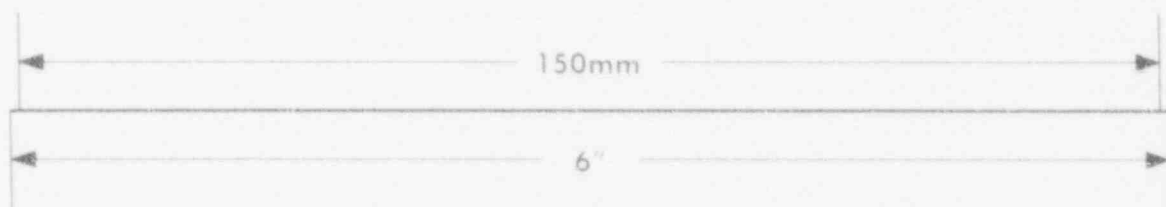
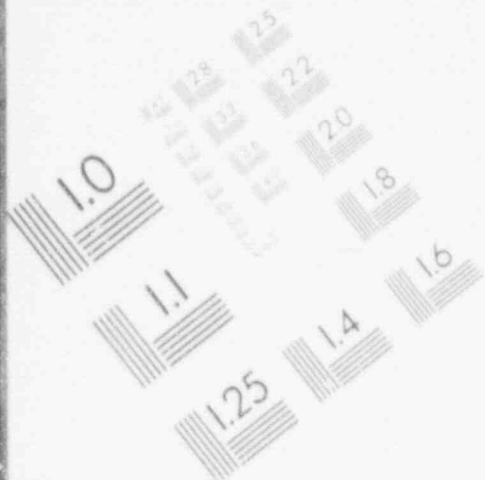
3.2.1 Gaseous Effluent Dose Calculation Parameters

<u>Term</u>	<u>Definition</u>	<u>Section of initial Use</u>
D_o =	average organ dose rate in the current year (mrem/yr).	(3.2.2.2)
D_p =	dose to an individual from radioiodine and radionuclides in particulate form and radionuclides (other than noble gases), with half-lives greater than eight days (mrem).	(3.2.3.2)
D_s =	average skin dose rate in current year (mrem/year).	(3.2.2.1)
D_t =	current total body dose rate (mrem/yr)	(3.2.2.1)
D_β =	air dose due to beta emissions from noble gas radionuclides (mrad).	(3.2.3.1)
D_γ =	air dose due to gamma emissions from noble gas radionuclides (mrad).	(3.2.3.1)
K_i =	total body dose factor due to gamma emissions from isotope i (mrem/year per $\mu\text{Ci}/\text{m}^3$) from Table 3.1-1.	(3.2.2.1)
L_i =	skin dose factor due to beta emissions from noble gas radionuclide i (mrad/yr per $\mu\text{Ci}/\text{m}^3$) from Table 3.1-1.	(3.2.2.1)
M_i =	air dose factor due to gamma emissions from noble gas radionuclide i (mrad/yr per $\mu\text{Ci}/\text{m}^3$) from Table 3.1-1.	(3.2.2.1)
N_i =	air dose factor due to beta emissions from noble gas radionuclide i (mrad per $\mu\text{Ci}/\text{m}^3$) from Table 3.1-1.	(3.2.3.1)
P_i =	dose parameter for radionuclide i, (mrem/yr per $\mu\text{Ci}/\text{m}^3$) for inhalation, from Table 3.2-1.	(3.2.2.2)
\bar{Q}_i =	the release rate of noble gas radionuclide i as determined from the concentrations measured in the analysis of the appropriate sample required by Table 1.2-3 ($\mu\text{Ci}/\text{sec}$).	(3.2.2.1)

<u>Term</u>	<u>Definition</u>	<u>Section of Initial Use</u>
\bar{Q}'_i	= the release rate of non-noble gas radionuclide i as determined from the concentrations measured in the analysis of the appropriate sample required by Table 1.2-3 ($\mu\text{Ci}/\text{sec}$).	(3.2.2.2)
\tilde{Q}_i	= cumulative release of noble gas radionuclide i over the period of interest (μCi).	(3.2.3.1)
\tilde{Q}'_i	= cumulative release of non-noble gas radionuclide i (required by ODCM Specification 1.2.4.1) over the period of interest (μCi).	(3.2.3.2)
R_{ij}	= dose factor for radionuclide i and pathway j, (mrem/yr per $\mu\text{Ci}/\text{m}^3$) or (m^2 -mrem/yr per $\mu\text{Ci}/\text{sec}$) from Tables 3.2-2 through 3.2-6.	(3.2.3.2)
W_{ij}'	= relative dispersion parameter for the maximum exposed individual, as appropriate for his exposure pathway j and radionuclide i.	(3.2.3.2)
	= \bar{X}/\bar{Q}' for inhalation and all tritium pathways	
	= \bar{D}/\bar{Q}' for other pathways and non-tritium radionuclides	
\bar{X}/\bar{Q}	= the highest annual average relative concentration in any sector, at the site boundary in sec/m^3 .	(3.2.2.1)
3.17×10^{-8}	= the fraction of one year per one second	(3.2.3.1)
\bar{X}/\bar{Q}'	= Annual average relative concentration for the location of the maximum exposed individual for the site (sec/m^3).	(3.2.3.2)
\bar{D}/\bar{Q}'	= Annual average relative deposition for the location of the maximum exposed individual for the site (m^{-2}).	(3.2.3.2)

2

IMAGE EVALUATION TEST TARGET (MT-3)



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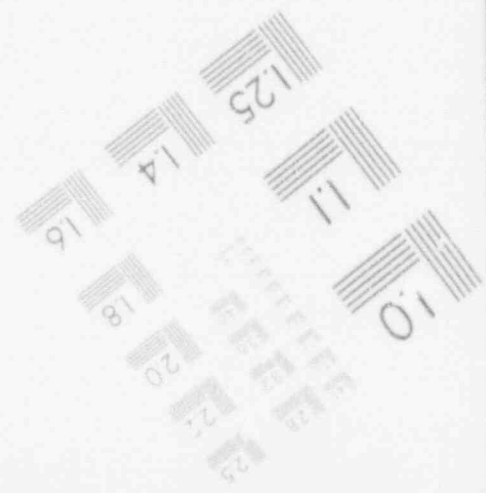
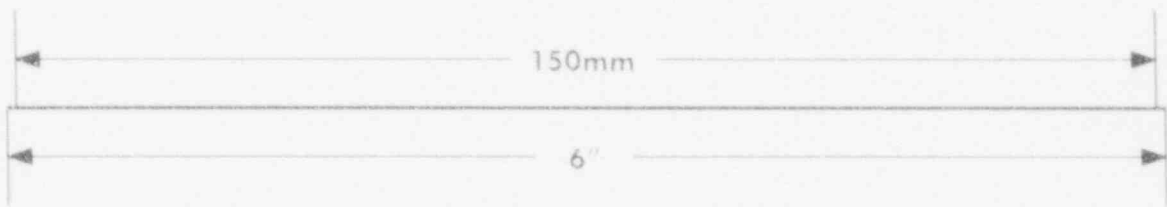
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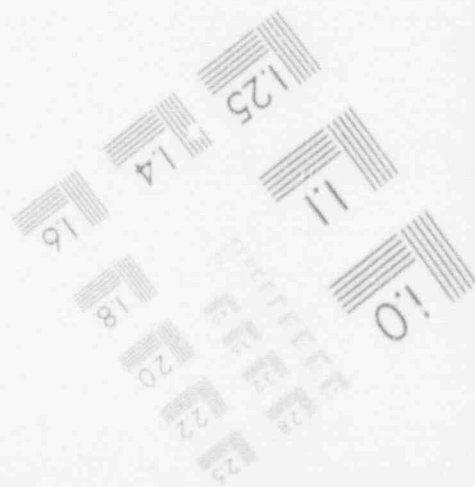
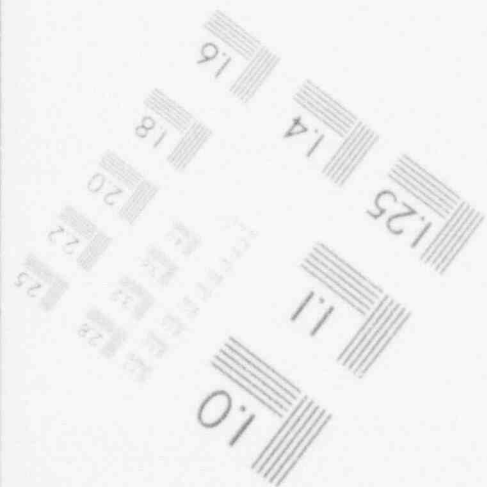
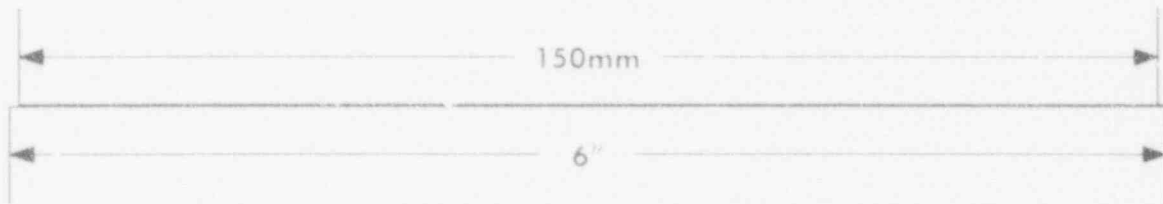
IMAGE EVALUATION TEST TARGET (MT-3)



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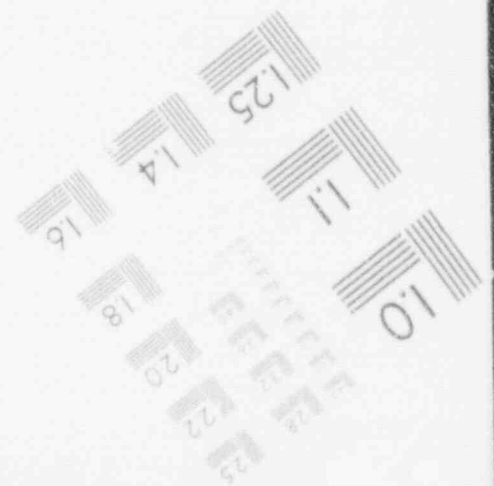
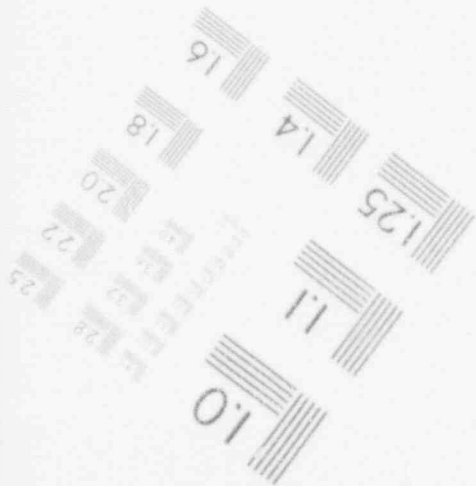
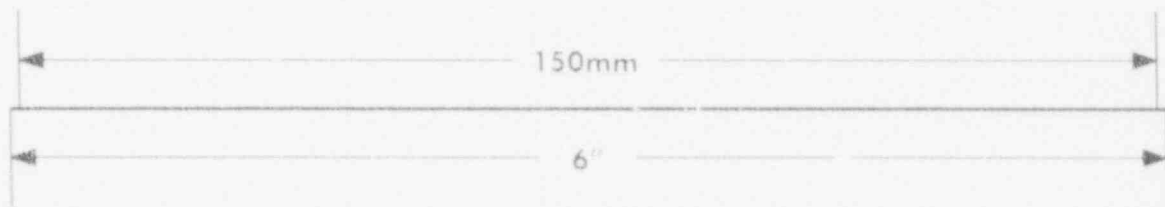
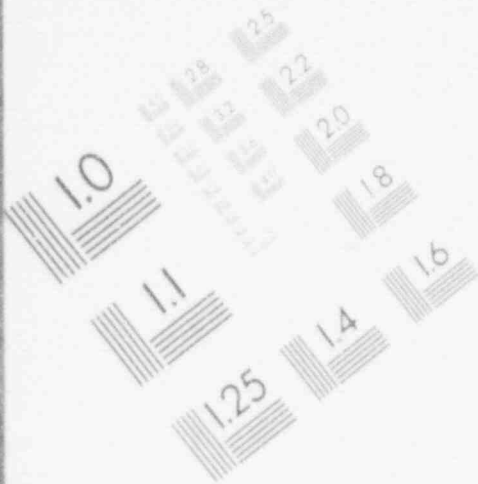
IMAGE EVALUATION TEST TARGET (MT-3)



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IMAGE EVALUATION TEST TARGET (MT-3)



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3.2.2 Unrestricted Area Boundary Dose

3.2.2.1 For the purpose of implementation of section 1.2.2.1a, ($\cong 500$ mrem/year - total body, $\cong 3000$ mrem/year - skin) the dose at the unrestricted area boundary due to noble gases shall be calculated as follows:

$$\begin{aligned} D_t &= \text{current total body dose rate (mrem/yr)} \\ &= \overline{X/Q} \sum_i K_i \overline{Q}_i \end{aligned} \quad (46)$$

$$\begin{aligned} D_s &= \text{current skin dose rate (mrem/yr)} \\ &= \overline{X/Q} \sum_i (L_i + 1.1M_i) \overline{Q}_i \end{aligned} \quad (47)$$

where:

\overline{Q}_i = the release rate of noble gas radionuclide i as determined from the concentration measured in the analysis of the appropriate sample required by Table 1.2-3 ($\mu\text{Ci/sec.}$).

$\overline{X/Q}$ = the highest annual average relative concentration in any sector, at the site boundary (for value, see Section 3.1.2).

K_i , L_i , and M_i will be selected for the appropriate radionuclide from Table 3.1-1.

3.2.2.2 For the purpose of implementation of section 1.2.2.1.b ($\cong 1500$ mrem/yr - any organ) organ doses due to radioiodines and all radioactive materials in particulate form and radionuclides (other than noble gases) with half-lives greater than eight days, will be calculated as follows:

$$\begin{aligned} D_o &= \text{current organ dose rate (mrem/yr)} \\ &= \sum_i \overline{X/Q} P_i \overline{Q}_i \end{aligned} \quad (48)$$

where:

$\overline{X/Q}$ = the highest annual average relative concentration in any sector, at the site boundary (for value, see Section 3.1.2)

P_i = dose parameter for radionuclide i , (mrem/yr per $\mu\text{Ci}/\text{m}^3$) for inhalation, from Table 3.2-1.

\overline{Q}_i = the release rate of non-noble gas radionuclide i as determined from the concentrations measured in the analysis of the appropriate sample required by Table 1.2-3 ($\mu\text{Ci}/\text{sec}$).

3.2.3 Unrestricted Area Dose (Air Dose and Dose to Individual)

3.2.3.1 For the purpose of implementation of section 1.2.3.1 (Calendar quarter: $\cong 5$ mrad - γ and $\cong 10$ mrad - β , Calendar year: $\cong 10$ mrad - γ and $\cong 20$ mrad - β) and section 1.2.5.1 (air dose averaged over 31 days: $\cong 0.2$ mrad - γ and $\cong 0.4$ mrad - β), the air dose in unrestricted areas shall be determined as follows:

$$D_\gamma = \text{air dose due to gamma emissions from noble gas radionuclide } i \text{ (mrad)}$$

$$= 3.17 \times 10^{-8} \sum_i M_i \overline{X/Q} \tilde{Q}_i \quad (49)$$

where:

3.17×10^{-8} = the fraction of one year per one second

\tilde{Q}_i = cumulative release of noble gas radionuclide i over the period of interest (μCi).

$$\begin{aligned}
 D_{\beta} &= \text{air dose due to beta emissions from noble gas radio-} \\
 &\quad \text{nuclide } i \text{ (mrad).} \\
 &= 3.17 \times 10^{-8} \sum N_i \overline{X/Q} \overline{Q}_i
 \end{aligned} \tag{50}$$

where, N_i = air dose factor due to beta emission from noble gas radionuclide i (mrad/yr per uCi/m³) from Table 3.1-1.

3.2.3.2 Dose to an individual from radioiodines and radioactive materials in particulate form and radionuclides (other than noble gases), with half-lives greater than eight (8) days (Calendar quarter: ≤ 7.5 mrem any organ, Calendar year: ≤ 15 mrem any organ) will be calculated for the purpose of implementation of section 1.2.4.1 as follows:

$$\begin{aligned}
 D_p &= \text{dose to an individual from radioiodines and radio-} \\
 &\quad \text{nuclides in particulate form, with half-lives greater} \\
 &\quad \text{than eight days (mrem)} \\
 &= 3.17 \times 10^{-8} \sum_{ij} R_{ij} W_{ij}' \overline{Q}'_i
 \end{aligned} \tag{51}$$

where:

W_{ij}' = relative concentration or relative deposition for the maximum exposed individual, as appropriate for exposure pathway j and radionuclide i .

$$\overline{X/Q}' = \begin{cases} \overline{X/Q}' \text{ for inhalation and all tritium pathways} \\ \quad = 2.2 \times 10^{-6} \text{ sec/m}^3 \\ \\ \overline{D/Q}' \text{ for other pathways and non-tritium radionuclides} \\ \quad = 1.2 \times 10^{-6} \text{ m}^{-2} \end{cases}$$

(See the notes to Table 3.2-7 and 3.2-8 for the origin of these factors.)

R_{ij} = dose factor for radionuclide i and pathway j ,
(mrem/yr per $\mu\text{Ci}/\text{m}^3$) or (m^2 - mrem/yr per $\mu\text{Ci}/\text{sec}$)
from Table 3.2-2.

\tilde{Q}_i = Cumulative release of non-noble gas radionuclide
 i (required by ODCM Specification 1.2.4.1) over
the period of interest (μCi).

3.2.4 For the purpose of initial assessments of the impact of unplanned gaseous releases, dose calculations for the critical receptor in each affected sector may be performed using section 3.2.3.1 and section 3.2.3.2 equations as follows:

- (1) For each affected sector, X/Q and D/Q will be calculated for one mile and critical receptor locations using actual meteorological conditions occurring during the unplanned release. Actual X/Q and D/Q values will be compared to annual average dispersion coefficients ($\overline{X/Q}$, $\overline{X/Q'}$, and $\overline{D/Q'}$). The more limiting dispersion coefficients will be used along with methodology in sections 3.2.3.1 and 3.2.3.2 for the initial assessment.
- (2) The location of the critical receptors and the pathways j which should be analyzed are shown in Table 3.2-7. (For very rough calculations, the annual average dispersion coefficients ($\overline{X/Q}$ and $\overline{D/Q}$) for each receptor are shown in Table 3.2-8.)
- (3) The R_{ij} for the appropriate exposure pathways and age groups will be selected from Tables 3.2-3 through 3.2-6.

TABLE 3.2-1
 PATHWAY DOSE FACTORS FOR SECTION 3.2.2.2 (P.)*

Page 1 of 3

AGE GROUP	(CHILD)
ISOTOPE	INHALATION
H-3	1.125E + 03
C-14	3.589E + 04
NA-24	1.610E + 04
P-32	2.605E + 06
CR-51	1.698E + 04
MN-54	1.576E + 06
MN-56	1.232E + 05
FE-55	1.110E + 05
FE-59	1.269E + 06
CO-58	1.106E + 06
CO-60	7.067E + 06
NI-63	8.214E + 05
NI-65	8.399E + 04
CU-64	3.670E + 04
ZN-65	9.953E + 05
ZN-69	1.018E + 04
BR-83	4.736E + 02
BR-84	5.476E + 02
BR-85	2.531E + 01
RB-86	1.983E + 05
RB-88	5.624E + 02
RB-89	3.452E + 02
SR-89	2.157E + 06
SR-90	1.010E + 08
SR-91	1.739E + 05

*See note, page 3-20

Units - mrem/yr per $\mu\text{Ci}/\text{m}^3$

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TABLE 3.2-1

PATHWAY DOSE FACTORS FOR SECTION 3.2.2.2 (P_i)

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AGE GROUP	(CHILD)
ISOTOPE	INHALATION
SR-92	2.424E + 05
Y-90	2.679E + 05
Y-91M	2.812E + 03
Y-91	2.627E + 06
Y-92	2.390E + 05
Y-93	3.885E + 05
ZR-95	2.231E + 06
ZR-97	3.511E + 05
NB-95	6.142E + 05
MO-99	1.354E + 05
TC-99M	4.810E + 03
TC-101	5.846E + 02
RU-103	6.623E + 05
RU-105	9.953E + 04
RU-106	1.476E + 07
AG-110M	5.476E + 06
TE-125M	4.773E + 05
TE-127M	1.480E + 06
TE-127	5.624E + 04
TE-129M	1.761E + 06
TE-129	2.549E + 04
TE-131M	3.078E + 05
TE-131	2.054E + 03
TE-132	3.774E + 05
I-130	1.846E + 06

*See note, page 3.0-20

Units - mrem/yr per $\mu\text{Ci}/\text{m}^3$

ODCM, V.C. Summer, SCE&G Revision 13 (June 1990)

TABLE 3.2-1

PATHWAY DOSE FACTORS FOR SECTION 3.2.2.2 (P.)

Page 3 of 3

AGE GROUP	(CHILD)
ISOTOPE	INHALATION
I-131	1.624E + 07
I-132	1.935E + 05
I-133	3.848E + 06
I-134	5.069E + 04
I-135	7.918E + 05
CS-134	1.014E + 06
CS-136	1.709E + 05
CS-137	9.065E + 05
CS-138	8.399E + 02
BA-139	5.772E + 04
BA-140	1.743E + 06
BA-141	2.919E + 03
BA-142	1.643E + 03
LA-140	2.257E + 05
LA-142	7.585E + 04
CE-141	5.439E + 05
CE-143	1.273E + 05
CE-144	1.195E + 07
PR-143	4.329E + 05
PR-144	1.565E + 03
ND-147	3.282E + 05
W-187	9.102E + 04
NP-239	6.401E + 04

NOTE: The P_i values of Table 3.2-1 were calculated according to the methods of Reference 1, Section 5.2.1, for children. The values used for the various parameters and the origins of those values are given in Table 3.2-9 and its notes.

Units - mrem/yr per $\mu\text{Ci}/\text{m}^3$

ODCM, V.C. Summer, SCE&G: Revision 13 (June 1990)

TABLE 3.2-2

PATHWAY DOSE FACTORS FOR SECTION 3.2.3.2 (R_i)*

Page 1 of 3

AGE GROUP	(CHILD)	(N.A.)	(CHILD)
ISOTOPE	INHALATION	GROUND PLANE	VEGETATION
H-3	1.125E + 03 (Total Body)	0.000E + 00 (Skin)	3.627E + 00 (Total Body)
C-14	3.589E + 04 (Bone)	0.000E + 00 (Skin)	8.894E + 08 (Bone)
NA-24	1.610E + 04 (Total Body)	3.33E + 08 (Skin)	3.729E + 05 (Total Body)
P-32	2.605E + 06 (Bone)	0.000E + 00 (Skin)	3.366E + 09 (Bone)
CR-51	1.698E + 04 (Lung)	5.506E + 06 (Skin)	6.213E + 06 (GI-LLI)
MN-54	1.576E + 06 (Lung)	1.625E + 09 (Skin)	6.648E + 08 (Liver)
MN-56	1.232E + 05 (GI-LLI)	1.068E + 06 (Skin)	2.723E + 03 (GI-LLI)
FE-55	1.110E + 05 (Lung)	0.000E + 00 (Skin)	8.012E + 08 (Bone)
FE-59	1.269E + 06 (Lung)	3.204E + 08 (Skin)	6.693E + 08 (GI-LLI)
CO-58	1.106E + 06 (Lung)	4.464E + 08 (Skin)	3.771E + 08 (GI-LLI)
CO-60	7.067E + 06 (Lung)	2.532E + 10 (Skin)	2.095E + 09 (GI-LLI)
NI-63	8.214E + 05 (Bone)	0.000E + 00 (Skin)	3.949E + 10 (Bone)
NI-65	8.399E + 04 (GI-LLI)	3.451E + 05 (Skin)	1.211E + 03 (GI-LLI)
CU-64	3.670E + 04 (GI-LLI)	6.876E + 05 (Skin)	5.159E + 05 (GI-LLI)
ZN-65	9.953E + 05 (Lung)	8.583E + 08 (Skin)	2.164E + 09 (Liver)
ZN-69	1.018E + 04 (GI-LLI)	0.000E + 00 (Skin)	9.893E-04 (GI-LLI)
BR-83	4.736E + 02 (Total Body)	7.079E + 03 (Skin)	5.369E + 00 (Total Body)
BR-84	5.476E + 02 (Total Body)	2.363E + 05 (Skin)	3.822E - 11 (Total Body)
BR-85	2.531E + 01 (Total Body)	0.000E + 00 (Skin)	0.000E + 00 (Total Body)
RB-86	1.983E + 05 (Liver)	1.035E + 07 (Skin)	4.584E + 08 (Liver)
RB-88	5.624E + 02 (Liver)	3.779E + 04 (Skin)	4.374E - 22 (Liver)
RB-89	3.452E + 02 (Liver)	1.452E + 05 (Skin)	1.642E - 26 (Liver)
SR-89	2.157E + 06 (Lung)	2.509E + 04 (Skin)	3.593E + 10 (Bone)
SR-90	1.010E + 08 (Bone)	0.000E + 00 (Skin)	1.243E + 12 (Bone)
SR-91	1.739E + 05 (GI-LLI)	2.511E + 06 (Skin)	1.157E + 06 (GI-LLI)

* See note, page 3.0-36

** Reference 1, section 5.3.1, page 30, paragraph 1 explains the logic used in selecting these specific pathways.

*** Critical organs for each pathway by nuclide in parentheses.

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$ Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

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TABLE 3.2-2 (continued)

PATHWAY DOSE FACTORS FOR SECTION 3.2.3.2 (R_i)

Page 2 of 3

AGE GROUP	(CHILD)	(N.A.)	(CHILD)
ISOTOPE	INHALATION	GROUND PLANE	VEGETATION
SR - 92	2.424E + 05 (GI-LLI)	8.631E + 05 (Skin)	1.378E + 04 (GI-LLI)
Y - 90	2.679E + 05 (GI-LLI)	5.308E + 03 (Skin)	6.569E + 07 (GI-LLI)
Y - 91M	2.812E + 03 (Lung)	1.161E + 05 (Skin)	1.737E - 05 (GI-LLI)
Y - 91	2.627E + 06 (Lung)	1.207E + 06 (Skin)	2.484E + 09 (GI-LLI)
Y - 92	2.390E + 05 (GI-LLI)	2.142E + 05 (Skin)	4.576E + 04 (GI-LLI)
Y - 93	3.885E + 05 (GI-LLI)	2.534E + 05 (Skin)	4.482E + 06 (GI-LLI)
ZR - 95	2.231E + 06 (Lung)	2.837E + 08 (Skin)	8.843E + 08 (GI-LLI)
ZR - 97	3.511E + 05 (GI-LLI)	3.445E + 06 (Skin)	1.248E + 07 (GI-LLI)
NB - 95	6.142E + 05 (Lung)	1.605E + 08 (Skin)	2.949E + 08 (GI-LLI)
MO - 99	1.354E + 05 (Lung)	4.626E + 06 (Skin)	1.647E + 07 (Kidney)
TC - 99M	4.810E + 03 (GI-LLI)	2.109E + 05 (Skin)	5.255E + 03 (GI-LLI)
TC - 101	5.846E + 02 (Lung)	2.277E + 04 (Skin)	4.123E - 29 (Kidney)
RU - 103	6.623E + 05 (Lung)	1.265E + 08 (Skin)	3.971E + 08 (GI-LLI)
RU - 105	9.953E + 04 (GI-LLI)	7.212E + 05 (Skin)	5.981E + 04 (GI-LLI)
RU - 106	1.476E + 07 (Lung)	5.049E + 08 (Skin)	1.159E + 10 (GI-LLI)
AG - 110M	5.476E + 06 (Lung)	4.019E + 09 (Skin)	2.581E + 09 (GI-LLI)
TE - 125M	4.773E + 05 (Lung)	2.128E + 06 (Skin)	3.506E + 08 (Bone)
TE - 127	1.480E + 06 (Lung)	1.083E + 05 (Skin)	3.769E + 09 (Kidney)
TE - 127	5.624E + 04 (GI-LLI)	3.293E + 03 (Skin)	3.903E + 05 (GI-LLI)
TE - 129M	1.761E + 06 (Lung)	2.312E + 07 (Skin)	2.430E + 09 (GI-LLI)
TE - 129	2.549E + 04 (GI-LLI)	3.076E + 04 (Skin)	7.200E - 02 (GI-LLI)
TE - 131M	3.078E + 05 (GI-LLI)	9.459E + 06 (Skin)	2.163E - 07 (GI-LLI)
TE - 131	2.054E + 03 (Lung)	3.450E + 07 (Skin)	1.349E - 14 (GI-LLI)
TE - 132	3.774E + 05 (Lung)	4.968E + 06 (Skin)	3.111E + 07 (GI-LLI)
I - 130	1.846E + 06 (Thyroid)	6.692E + 06 (Skin)	1.371E + 08 (Thyroid)

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$ Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

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3.0-22

TABLE 3.2-2 (continue)

PATHWAY DOSE FACTORS FOR SECTION 3.2.3.2 (R.)

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AGE GROUP	(CHILD)	(N.A.)	(CHILD)
ISOTOPE	INHALATION	GROUND PLANE	VEGETATION
I-131	1.624E + 07 (Thyroid)	2.089E + 07 (Skin)	4.754E + 10 (Thyroid)
I-132	1.935E + 05 (Thyroid)	1.452E + 06 (Skin)	7.314E + 03 (Thyroid)
I-133	3.848E + 06 (Thyroid)	2.981E + 06 (Skin)	8.113E + 08 (Thyroid)
I-134	5.069E + 04 (Thyroid)	5.305E + 05 (Skin)	6.622E - 03 (Thyroid)
I-135	7.918E + 05 (Thyroid)	2.947E + 06 (Skin)	9.973E + 06 (Thyroid)
CS-134	1.014E + 06 (Liver)	8.007E + 09 (Skin)	2.631E + 10 (Liver)
CS-136	1.709E + 05 (Liver)	1.710E + 08 (Skin)	2.247E + 08 (Liver)
CS-137	9.065E + 05 (Bone)	1.201E + 10 (Skin)	2.392E + 10 (Bone)
CS-138	8.399E + 02 (Liver)	4.102E + 05 (Skin)	9.133E - 11 (Liver)
BA-139	5.772E + 04 (GI-LLI)	1.194E + 05 (Skin)	2.950E + 00 (GI-LLI)
BA-140	1.743E + 06 (Lung)	2.346E + 07 (Skin)	2.767E + 08 (Bone)
BA-141	2.919E + 03 (Lung)	4.734E + 04 (Skin)	1.605E - 21 (Bone)
BA-142	1.643E + 03 (Lung)	5.064E + 04 (Skin)	4.105E - 39 (Bone)
LA-140	2.257E + 05 (GI-LLI)	2.180E + 07 (Skin)	3.166E + 07 (GI-LLI)
LA-142	7.585E + 04 (Lung)	9.117E + 05 (Skin)	2.141E + 01 (GI-LLI)
CE-141	5.439E + 05 (Lung)	1.540E + 07 (Skin)	4.082E + 08 (GI-LLI)
CE-143	1.273E + 05 (GI-LLI)	2.627E + 06 (Skin)	1.364E + 07 (GI-LLI)
CE-144	1.195E + 07 (Lung)	8.042E + 07 (Skin)	1.039E + 10 (GI-LLI)
PR-143	4.329E + 05 (Lung)	0.000E + 00 (Skin)	1.575E + 08 (GI-LLI)
PR-144	1.565E + 03 (Lung)	2.112E + 03 (Skin)	3.829E - 23 (GI-LLI)
ND-147	3.282E + 05 (Lung)	1.009E + 07 (Skin)	9.197E + 07 (GI-LLI)
W-187	9.102E + 04 (GI-LLI)	2.740E + 06 (Skin)	5.380E + 06 (GI-LLI)
NP-239	6.401E + 04 (GI-LLI)	1.976E + 06 (Skin)	1.357E + 07 (GI-LLI)

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$ Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

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TABLE 3.2-3

PATHWAY DOSE FACTORS FOR SECTION 3.2.3.3 (R₁)*

Page 1 of 3

AGE GROUP	(INFANT)	(N.A.)	(INFANT)	(INFANT)	(INFANT)	(INFANT)	(INFANT)	(INFANT)
ISOTOPE	INHALATION	GROUND PLANE	GRS-COW MILK	GRS-COW MEAT	GRS-COW MILK	GRS-GOT MEAT	GRS-GOT MILK	VEGETATION
H-3	6.468E+02	0.000E+00	2.157E+03	0.000E+00	2.157E+03	0.000E+00	4.398E+03	0.000E+00
C-14	2.646E+04	0.000E+00	2.340E+09	0.000E+00	8.189E+08	0.000E+00	2.340E+09	0.000E+00
NA-24	1.056E+04	1.385E+07	1.542E+07	0.000E+00	2.300E-37	0.000E+00	1.851E+06	0.000E+00
P-32	2.030E+06	0.000E+00	1.602E+11	0.000E+00	7.088E+08	0.000E+00	1.924E+11	0.000E+00
CR-51	1.284E+04	5.506E+06	4.700E+06	0.000E+00	1.729E+05	0.000E+00	5.641E+05	0.000E+00
MN-54	9.996E+05	1.625E+09	3.900E+07	0.000E+00	1.118E+07	0.000E+00	4.680E+06	0.000E+00
MN-56	7.168E+04	1.068E+06	2.862E+00	0.000E+00	0.000E+00	0.000E+00	3.436E-01	0.000E+00
FE-55	8.694E+04	0.000E+00	1.351E+08	0.000E+00	4.439E+07	0.000E+00	1.757E+06	0.000E+00
FE-59	1.015E+06	3.204E+08	3.919E+08	0.000E+00	3.384E+07	0.000E+00	5.096E+06	0.000E+00
CO-58	7.770E+05	4.464E+08	6.055E+07	0.000E+00	8.824E+06	0.000E+00	7.251E+06	0.000E+00
CO-60	4.508E+06	2.532E+10	2.098E+08	0.000E+00	7.107E+07	0.000E+00	2.517E+07	0.000E+00
NI-63	3.388E+05	0.000E+00	3.493E+10	0.000E+00	1.221E+10	0.000E+00	4.192E+09	0.000E+00
NI-65	5.012E+04	3.451E+05	3.020E+01	0.000E+00	0.000E+00	0.000E+00	3.635E+00	0.000E+00
CU-64	1.498E+04	6.876E+05	3.807E+06	0.000E+00	7.934E-46	0.000E+00	4.246E+05	0.000E+00
ZN-65	6.468E+05	8.583E+08	1.904E+10	0.000E+00	5.160E+09	0.000E+00	2.285E+09	0.000E+00
ZN-69	1.322E+04	0.000E+00	3.055E-09	0.000E+00	0.000E+00	0.000E+00	3.581E-10	0.000E+00
BR-83	3.808E+02	7.079E+03	9.339E-01	0.000E+00	0.000E+00	0.000E+00	1.124E-01	0.000E+00
BR-84	4.004E+02	2.363E+05	1.256E-22	0.000E+00	0.000E+00	0.000E+00	1.527E-23	0.000E+00
BR-85	2.044E+01	0.000E+00	0.00E+00	0.000E+00	0.000E+00	0.000E+00	0.000E00	0.000E+00
RB-86	1.904E+05	1.035E+07	2.234E+10	0.000E+00	2.827E+08	0.000E+00	2.671E+09	0.000E+00
RB-88	5.572E+02	3.779E+04	1.874E-44	0.000E+00	0.000E+00	0.000E+00	2.304E-45	0.000E+00
RB-89	3.206E+02	1.452E+05	3.414E-52	0.000E+00	0.000E+00	0.000E+00	4.056E-53	0.000E+00
SR-89	2.030E+06	2.509E+04	1.258E+10	0.000E+00	1.280E+09	0.000E+00	2.643E+10	0.000E+00
SR-90	4.088E+07	0.000E+00	1.216E+11	0.000E+00	4.230E+10	0.000E+00	2.553E+11	0.000E+00
SR-91	7.336E+04	2.511E+06	3.215E+05	0.000E+00	0.000E+00	0.000E+00	6.758E+05	0.000E+00
			(PASTURE)	(PASTURE)	(FEED)	(PASTURE)	(PASTURE)	

*See note, page 3.0-36

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$ Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

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TABLE 3 2-3 (continued)

PATHWAY DOSE FACTORS FOR SECTION 3.2.3.3 (R.)

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AGE GROUP	(INFANT)	(INFANT)	(INFANT)	(INFANT)	(INFANT)	(INFANT)	(INFANT)	(INFANT)
ISOTOPE	INHALATION	GROUND PLANE	GRS-COW MILK	GRS-COW MEAT	GRS-COW MILK	GRS-GOT MEAT	GRS-GOT MILK	VEGETATION
SR-92	1.400E+05	8.631E+05	5.005E+01	0.000E+00	0.000E+00	0.000E+00	1.054E+02	0.000E+00
Y-90	2.688E+05	5.308E+03	9.406E+05	0.000E+00	2.335E-05	0.000E+00	1.129E+05	0.000E+00
Y-91M	2.786E+03	1.161E+05	1.876E-15	0.000E+00	0.000E+00	0.000E+00	2.290E-16	0.000E+00
Y-91	2.450E+06	1.207E+06	5.251E+06	0.000E+00	6.324E+05	0.000E+00	6.302E+05	0.000E+00
Y-92	1.266E+05	2.142E+05	1.026E+01	0.000E+00	0.000E+00	0.000E+00	1.234E+00	0.000E+00
Y-93	1.666E+05	2.534E+05	1.776E+04	0.000E+00	2.386E-61	0.000E+00	2.046E+03	0.000E+00
ZR-95	1.750E+06	2.837E+08	8.257E+05	0.000E+00	1.090E+05	0.000E+00	9.910E+04	0.000E+00
ZR-97	1.400E+05	3.445E+06	4.446E+04	0.000E+00	4.980E-35	0.000E+00	5.339E+03	0.000E+00
NB-95	4.788E+05	1.605E+08	2.062E+08	0.000E+00	1.213E+07	0.000E+00	2.475E+07	0.000E+00
MO-99	1.348E+05	4.626E+06	3.108E+08	0.000E+00	1.523E-02	0.000E+00	3.731E+07	0.000E+00
TC-99M	2.030E+03	2.109E+05	1.646E+04	0.000E+00	0.000E+00	0.000E+00	1.978E+03	0.000E+00
TC-101	8.442E+02	2.277E+04	1.423E-56	0.000E+00	0.000E+00	0.000E+00	6.530E-58	0.000E+00
RU-103	5.516E+05	1.265E+08	1.055E+05	0.000E+00	7.573E+03	0.000E+00	1.265E+04	0.000E+00
RU-105	4.844E+04	7.212E+05	3.204E+00	0.000E+00	0.000E+00	0.000E+00	3.851E-01	0.000E+00
RU-106	1.156E+07	5.049E+08	1.445E+06	0.000E+00	4.266E+05	0.000E+00	1.734E+05	0.000E+00
AG-110M	3.668E+06	4.019E+09	1.461E+10	0.000E+00	3.984E+09	0.000E+00	1.752E+03	0.000E+00
TE-125M	4.466E+05	2.128E+06	1.508E+08	0.000E+00	1.799E+07	0.000E+00	1.809E+07	0.000E+00
TE-127M	1.312E+06	1.083E+05	1.037E+09	0.000E+00	2.046E+08	0.000E+00	1.244E+08	0.000E+00
TE-127	2.436E+04	3.293E+03	1.359E+05	0.000E+00	1.267E-65	0.000E+00	1.594E+04	0.000E+00
TE-129M	1.680E+06	2.312E+07	1.392E+09	0.000E+00	7.559E+07	0.000E+00	1.672E+08	0.000E+00
TE-129	2.632E+04	3.076E+04	2.187E-07	0.000E+00	0.000E+00	0.000E+00	2.624E-08	0.000E+00
TE-131M	1.988E+05	9.459E+06	2.288E+07	0.000E+00	1.653E-15	0.000E+00	2.747E+06	0.000E+00
TE-131	8.218E+03	3.450E+07	1.384E-30	0.000E+00	0.000E+00	0.000E+00	1.688E-31	0.000E+00
TE-132	3.402E+05	4.968E+06	6.513E+07	0.000E+00	1.041E-01	0.000E+00	7.842E+06	0.000E+00
I-130	1.596E+06	6.692E+06	8.754E+08	0.000E+00	7.115E-45	0.000E+00	1.051E+09	0.000E+00
			(PASTURE)	(PASTURE)	(FEED)	(PASTURE)	(PASTURE)	

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$ Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

ODCM, V.C. Summer, SCE&G. Revision 13 (June 1990)

3.0-25

TABLE 3.2-3 (continued)

PATHWAY DOSE FACTORS FOR SECTION 3.2.3.3 (R_i)

Page 3 of 3

AGE GROUP	(INFANT)	(N.A.)	(INFANT)	(INFANT)	(INFANT)	(INFANT)	(INFANT)	(INFANT)
ISOTOPE	INHALATION	GROUND PLANE	GRS COW MILK	GRS COW MEAT	GRS COW MILK	GRS GOT MEAT	GRS GOT MILK	VEGETATION
I-131	1.484E+07	2.089E+07	1.053E+12	0.000E+00	1.567E+08	0.000E+00	1.264E+12	0.000E+00
I-132	1.694E+05	1.452E+06	1.188E+02	0.000E+00	0.000E+00	0.000E+00	1.638E+02	0.000E+00
I-133	3.556E+06	2.981E+06	9.601E+09	0.000E+00	1.776E-22	0.000E+00	1.153E+10	0.000E+00
I-134	4.452E+04	5.305E+05	8.402E-10	0.000E+00	0.000E+00	0.000E+00	1.017E-09	0.000E+00
I-135	6.958E+05	2.947E+06	2.002E+07	0.000E+00	0.000E+00	0.000E+00	2.406E+07	0.000E+00
CS-134	7.028E+05	8.007E+09	6.801E+10	0.000E+00	2.191E+10	0.000E+00	2.040E+11	0.000E+00
CS-136	1.345E+05	1.710E+08	5.795E+09	0.000E+00	1.729E+10	0.000E+00	1.744E+10	0.000E+00
CS-137	6.118E+05	1.201E+10	6.024E+10	0.000E+00	2.096E+10	0.000E+00	1.087E+12	0.000E+00
CS-138	8.764E+02	4.102E+05	2.180E-22	0.000E+00	0.000E+00	0.000E+00	6.628E-22	0.000E+00
BA-139	5.096E+04	1.194E+05	2.874E-05	0.000E+00	0.000E+00	0.000E+00	3.265E-06	0.000E+00
BA-140	1.596E+06	2.346E+07	2.410E+08	0.000E+00	6.409E+05	0.000E+00	2.893E+07	0.000E+00
BA-141	4.746E+03	4.734E+04	4.916E-44	0.000E+00	0.000E+00	0.000E+00	5.899E-45	0.000E+00
BA-142	1.554E+03	5.064E+04	1.049E-78	0.000E+00	0.000E+00	0.000E+00	1.259E-79	0.000E+00
LA-140	1.680E+05	2.180E+07	1.880E+05	0.000E+00	4.563E-12	0.000E+00	2.253E+04	0.000E+00
LA-142	5.950E+04	9.117E+05	1.078E-05	0.000E+00	0.000E+00	0.000E+00	1.278E-06	0.000E+00
CE-141	5.166E+05	1.540E+07	1.366E+07	0.000E+00	7.008E+05	0.000E+00	1.640E+06	0.000E+00
CE-143	1.162E+05	2.627E+06	1.536E+06	0.000E+00	1.039E-14	0.000E+00	1.844E+05	0.000E+00
CE-144	9.842E+06	8.042E+07	1.334E+08	0.000E+00	3.749E+07	0.000E+00	1.601E+07	0.000E+00
PR-143	4.326E+05	0.000E+00	7.845E+05	0.000E+00	2.771E+03	0.000E+00	9.407E+04	0.000E+00
PR-144	4.284E+03	2.112E+03	1.171E-48	0.000E+00	0.000E+00	0.000E+00	1.259E-49	0.000E+00
ND-147	3.220E+05	1.009E+07	5.743E+05	0.000E+00	6.902E+02	0.000E+00	6.885E+04	0.000E+00
W-187	3.962E+04	2.740E+06	2.501E+06	0.000E+00	5.275E-22	0.000E+00	2.983E+05	0.000E+00
NP-239	5.950E+04	1.976E+06	9.400E+04	0.000E+00	1.025E-07	0.000E+00	1.132E+04	0.000E+00
			(PASTURE)	(PASTURE)	(FEED)	(PASTURE)	(PASTURE)	

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$ Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

ODCM, V.C. Summer, SCE&G Revision 13 (June 1990)

3.0-26

TABLE 3.2-4

PATHWAY DOSE FACTORS FOR SECTION 3.2.3.3 (R.)*

Page 1 of 3

AGE GROUP	(CHILD)	(N.A.)	(CHILD)	(CHILD)	(CHILD)	(CHILD)	(CHILD)	(CHILD)
ISOTOPE	INHALATION	GROUND PLANE	GRS COW MILK	GRS COW MEAT	GRS COW MILK	GRS GOT MEAT	GRS GOT MILK	VEGETATION
H-3	1.125E+03	0.000E+00	1.421E+03	2.118E+02	1.421E+03	2.543E+01	2.899E+03	3.627E+03
C-14	3.589E+04	0.000E+00	1.195E+09	3.834E+08	4.181E+08	4.601E+07	1.195E+09	8.894E+08
NA-24	1.610E+04	1.385E+07	8.853E+06	1.725E-03	1.321E-37	2.070E-04	1.063E+06	3.729E+05
P-32	2.605E+06	0.000E+00	7.775E+10	7.411E+09	3.440E+08	8.893E+08	9.335E+10	3.366E+09
CF-51	1.698E+04	5.506E+06	5.398E+06	4.661E+05	1.985E+05	5.593E+04	6.478E+05	6.213E+06
MN-54	1.576E+06	1.625E+09	2.097E+07	8.011E+06	6.012E+06	9.613E+05	2.517E+06	6.648E+08
MN-56	1.232E+05	1.068E+06	1.865E+00	2.437E-51	0.000E+00	2.924E-52	2.238E-01	2.723E+03
FE-55	1.110E+05	0.000E+00	1.118E+08	4.571E+08	3.673E+07	5.486E+07	1.453E+06	8.012E+08
FE-59	1.269E+06	3.204E+08	2.025E+08	6.338E+08	1.749E+07	7.605E+07	2.633E+06	6.693E+08
CO-58	1.106E+06	4.464E+08	7.080E+07	9.596E+07	1.032E+07	1.152E+07	8.487E+06	3.771E+08
CO-60	7.067E+06	2.532E+10	2.391E+08	3.838E+08	8.103E+07	4.605E+07	2.870E+07	2.095E+09
Ni-63	8.214E+05	0.000E+00	2.964E+10	2.912E+10	1.036E+10	3.495E+09	3.557E+09	3.949E+10
Ni-65	8.399E+04	3.451E+05	1.909E+01	4.061E-51	0.000E+00	4.873E-52	2.298E+00	1.211E+03
CU-64	3.670E+04	6.876E+05	3.502E+06	1.393E-05	7.299E-46	1.672E-06	3.907E+05	5.159E+05
ZN-65	9.953E+05	8.583E+08	1.101E+10	1.000E+09	2.985E+09	1.200E+08	1.322E+09	2.164E+09
ZN-69	1.018E+04	0.000E+00	1.123E-08	0.000E+00	0.000E+00	0.000E+00	1.043E-10	9.893E-04
BR-83	4.736E+02	7.079E+03	4.399E-01	9.519E-57	0.000E+00	1.142E-57	5.190E-02	5.369E+00
BR-84	5.476E+02	2.363E+05	6.508E-23	0.000E+00	0.000E+00	0.000E+00	7.758E-24	3.822E-11
BR-85	2.531E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB-86	1.983E+05	1.035E+07	8.804E+09	5.816E+08	1.114E+08	6.979E+07	1.053E+09	4.584E+08
RB-88	5.624E+02	3.779E+04	7.150E-45	0.000E+00	0.000E+00	0.000E+00	8.789E-46	4.374E-22
RB-89	3.452E+02	1.452E+05	1.397E-52	0.000E+00	0.000E+00	0.000E+00	1.659E-53	1.642E-26
SR-89	2.157E+06	2.509E+04	6.618E+09	4.815E+08	6.730E+08	5.778E+07	1.390E+10	3.593E+10
SR-90	1.010E+08	0.000E+00	1.117E+11	1.040E+10	3.887E+10	1.248E+09	2.346E+11	1.243E+12
SR-91	1.739E+05	2.511E+06	2.878E+05	55.292E-10	0.000E+00	6.351E-11	6.050E+05	1.157E+06
			(PASTURE)	(PASTURE)	(FEED)	(PASTURE)	(PASTURE)	

*See note, page 3.0-36

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$ Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

ODCM, V.C. Summer, SCE&G Revision 13 (June 1990)

TABLE 3.2-4 (continued)
 PATHWAY DOSE FACTORS FOR SECTION 3.2.3.3 (R_i)

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AGE GROUP	(CHILD)	(W.A.)	(CHILD)	(CHILD)	(CHILD)	(CHILD)	(CHILD)	(CHILD)
ISOTOPE	INHALATION	GROUND PLANE	GRS COW MILK	GRS COW MEAT	GRS COW MILK	GRS GOT MEAT	GRS GOT MILK	VEGETATION
SR-92	2.424E+05	8.631E+05	4.134E+01	3.492E-48	0.000E+00	4.191E-49	8.706E+01	1.378E+4
Y-90	2.679E+05	5.308E+03	9.171E+05	4.879E+05	2.277E-03	5.855E+04	1.101E+05	6.569E+7
Y-91M	2.812E+03	1.161E+05	5.622E-16	0.000E+00	0.000E+00	0.000E+00	6.344E-17	1.737E-5
Y-91	2.627E+06	1.207E+06	5.199E+06	2.400E+08	6.261E+05	2.880E+07	6.240E+05	2.484E+9
Y-92	2.390E+05	2.142E+05	7.210E+00	6.959E-35	0.000E+00	8.350E-36	8.791E-01	4.576E+4
Y-93	3.885E+05	2.534E+05	1.573E+04	1.547E-07	9.134E-61	1.857E-08	1.888E+03	4.482E+6
ZR-95	2.231E+06	2.837E+08	8.786E+05	6.106E+08	1.160E+05	7.328E+07	1.054E+05	8.843E-8
ZR-97	3.511E+05	3.445E+06	4.199E+04	7.015E-01	4.703E-35	8.418E-02	5.042E+03	1.248E+7
NB-95	6.142E+05	1.605E+08	2.287E+08	2.288E+09	1.346E+07	2.673E+08	2.747E+07	2.949E+8
MO-99	1.354E+05	4.626E+06	1.738E+08	2.456E+05	8.512E-03	2.947E+04	2.086E+07	1.647E+7
TC-99M	4.810E+03	2.109E+05	1.874E+04	6.915E-18	0.000E+00	8.298E-19	1.771E+03	5.255E+3
TC-101	5.846E+02	2.277E+04	5.593E-58	0.000E+00	0.000E+00	0.000E+00	2.566E-59	4.123E-29
RU-103	6.623E+05	1.265E+08	1.108E+05	4.009E+09	7.952E+03	4.811E+08	1.329E+04	3.971E+8
RU-105	9.953E+04	7.212E+05	2.493E+00	5.885E-25	0.000E+00	7.061E-26	2.997E-01	5.981E+4
RU-106	1.476E+07	5.049E+08	1.437E+06	6.902E+10	4.243E+05	8.282E+09	1.725E+05	1.153E+10
AG-110M	5.476E+06	4.019E+09	1.678E+10	6.742E+08	4.576E+09	8.090E+07	2.013E+09	2.581E+9
TE-125M	4.773E+05	2.128E+06	7.377E+07	5.690E+08	8.802E+06	6.828E+07	8.853E+06	3.506E+8
TE-127M	1.480E+06	1.083E+05	5.932E+08	5.060E+09	1.171E+08	6.072E+08	7.118E+07	3.769E+9
TE-127	5.624E+04	3.293E+03	1.191E+05	1.607E-08	0.000E+00	1.929-09	1.396E+04	3.903E+5
TE-129M	1.761E+06	2.312E+07	7.961E+08	5.245E+09	4.324E+07	6.294E+08	9.563E+07	2.46E+9
TE-129	2.549E+04	3.076E+04	7.96E-08	0.000E+00	0.000E+00	0.000E+00	9.641E-09	7.204E-2
TE-131M	3.078E+05	9.459E+06	2.244E+07	9.815E+03	1.621E-15	1.178E+03	2.094E+06	2.163E+7
TE-131	2.054E+03	3.450E+07	8.489E-32	0.000E+00	0.000E+00	0.000E+00	1.036E-32	1.349E-14
TE-132	3.774E+05	4.968E+06	4.551E+07	9.325E+06	7.272E-02	1.119E+06	5.480E+06	3.111E+7
I-130	1.846E+06	6.692E+06	3.845E+08	6.758E-04	3.125E-45	8.109E-05	4.617E+08	1.371E+8
			(PASTURE)	(PASTURE)	(FEED)	(PASTURE)	(PASTURE)	

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$

Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

ODCM, V.C. Summer, SCE&G Revision 13 (June 1990)

TABLE 3 2-4 (continue)
 PATHWAY DOSE FACTORS FOR SECTION 3.2.3.3 (R.)

Page 3 of 3

AGE GROUP	(CHILD)	(INFANT)	(CHILD)	(CHILD)	(CHILD)	(CHILD)	(CHILD)	(CHILD)
ISOTOPE	INHALATION	GROUND PLANT	GRS COW MILK	GRS COW MEAT	GRS COW MILK	GRS GOAT MEAT	GRS GOAT MILK	VEGETATION
I-131	1.624E+07	2.089E+07	4.333E+11	5.503E+09	6.448E+07	6.604E+08	5.201E+11	4.754E+10
I-132	1.935E+05	1.452E+06	5.129E+01	2.429E-57	0.000E+00	2.915E-58	7.072E+01	7.314E+03
I-133	3.848E+06	2.981E+06	3.945E+09	1.304E+02	7.299E-23	1.564E+01	4.737E+09	8.113E+08
I-134	5.069E+04	5.305E+05	3.624E-10	0.000E+00	0.000E+00	0.000E+00	4.386E-10	6.622E-03
I-135	7.918E+05	2.947E+06	8.607E+06	1.039E-14	0.000E+00	1.247E-15	1.034E+07	9.973E+06
CS-134	1.014E+06	8.007E+09	3.715E+10	1.513E+09	1.197E+10	1.816E+08	1.115E+11	2.631E+10
CS-136	1.709E+05	1.710E+08	2.773E+09	4.426E+07	8.276E+06	5.311E+06	8.344E+09	2.247E+08
CS-137	9.065E+05	1.201E+10	3.224E+10	1.334E+09	1.122E+10	1.600E+08	9.672E+10	2.392E+10
CS-138	8.399E+02	4.102E+05	5.528E-23	0.000E+00	0.000E+00	0.000E+00	1.681E-22	9.133E-11
BA-139	5.772E+04	1.194E+05	1.231E-05	0.000E+00	0.000E+00	0.000E+00	1.398E-06	2.950E+00
BA-140	1.743E+06	2.346E+07	1.171E+08	4.384E+07	3.114E+05	5.261E+06	1.406E+07	2.767E+08
BA-141	2.919+03	4.734E+04	1.894E-45	0.000E+00	0.000E+00	0.000E+00	2.273E-46	1.605E-21
BA-142	1.643E+03	5.064E+04	1.208E-79	0.000E+00	0.000E+00	0.000E+00	1.450E-80	4.105E-30
LA-140	2.257E+05	2.180E+07	1.894E+05	5.492E+02	4.596E-12	6.590E+01	2.269E+04	3.166E+07
LA-142	7.585E+04	9.117E+05	5.203E-06	0.000E+00	0.000E+00	0.000E+00	6.166E-07	2.141E+01
CE-141	5.439E+05	1.540E+07	1.361E+07	1.382E+07	6.980+05	1.658E+06	1.633E+06	4.082E+08
CE-143	1.273E+05	2.627E+06	1.488E+06	2.516E+02	1.006E-14	3.020E+01	1.787E+05	1.364E+07
CE-144	1.195E+07	8.042E+07	1.326E+08	1.893E+08	3.727E+07	2.271E+07	1.592E+07	1.039E+10
PR-143	4.329E+05	0.000E+00	7.754E+05	3.609E+07	2.738E+03	4.331E+06	9.297E+04	1.575E+08
PR-144	1.565E+03	2.112E-03	2.040E-50	0.000E+00	0.000E+00	0.000E+00	2.353E-51	3.829E-23
ND-147	3.282E+05	1.009E+07	5.712E+05	1.505E+07	6.864E+02	1.805E+06	6.846E+04	9.197E+07
W-187	9.102E+04	2.740E+06	2.420E+06	2.790E+00	5.103E-22	3.348E-01	2.886E+05	5.380E+06
NP-239	6.401E+04	1.976E+06	9.138E+04	2.232E+03	9.336E-08	2.679E+02	1.100E+04	1.357E+07
			(PASTURE)	(PASTURE)	(FEED)	(PASTURE)	(PASTURE)	

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$

Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

ODCM, V.C. Summer, SCE&G Revision 13 (June 1990)

TABLE 3.2-5

PATHWAY DOSE FACTORS FOR SECTION 3.2.3.3 (R₁)*

Page 1 of 3

AGE GROUP	(TEENAGER)	(N.A.)	(TEENAGER)	(TEENAGER)	(TEENAGER)	(TEENAGER)	(TEENAGER)	(TEENAGER)
ISOTOPE	INHALATION	GROUND PLANE	GRS COW MILK	GRS COW MEAT	GRS COW MILK	GRS GOT MEAT	GRS GOT MILK	VEGETATION
H-3	1.272E+03	0.000E+00	8.993E+02	1.754E+02	8.993E+02	2.104E+01	1.835E+03	2.342E+03
C-14	2.600E+04	0.000E+08	4.859E+08	2.040E+08	1.700E+08	2.448E+07	4.859E+08	3.690E+08
NA-24	1.376E+04	1.385E+07	4.255E+06	1.084E-03	6.347E-38	1.301E-04	5.110E+05	2.389E+05
P-32	1.888E+06	0.000E+00	3.931E+10	3.931E+09	1.395E+08	4.717E+08	3.785E+10	1.608E+09
CR-51	2.096E+04	5.506E+06	8.387E+06	9.471E+05	3.085E+05	1.137E+05	1.006E+06	1.037E+07
MN-54	1.984E+06	1.625E+09	2.875E+07	1.436E+07	8.240E+06	1.723E+06	3.450E+06	9.320E+08
MN-56	5.744E+04	1.068E+06	4.856E-01	8.302E-52	0.000E+00	9.932E-53	5.829E-02	9.451E+02
FE-55	1.240E+05	0.000E+00	4.454E+07	2.382E+08	1.463E+07	2.859E+07	5.790E+05	3.259E+08
FE-59	1.528E+06	3.204E+08	2.861E+08	1.171E+09	2.470E+07	1.405E+08	3.720E+06	9.895E+08
CO-58	1.344E+06	4.464E+08	1.095E+08	1.942E+08	1.596E+07	2.330E+07	1.313E+07	6.034E+08
CO-60	8.720E+06	2.532E+10	3.621E+08	7.600E+08	1.227E-08	9.120E+07	4.345E+07	3.238E+09
NI-63	5.800E+05	0.000E+00	1.182E+10	1.519E+10	4.130E+09	1.823E+09	1.419E+09	1.606E+10
NI-65	3.672E+04	3.451E+05	4.692E+00	1.305E-51	0.000E+00	1.566E-52	5.647E-01	3.966E+02
CU-64	6.144E+04	6.876E+05	3.293E+06	1.713E-05	6.863E-46	2.072E-06	3.673E+05	6.465E+05
ZN-65	1.240E+06	8.583E+08	7.315E+09	8.688E+08	1.983E+09	1.043E+08	8.779E+08	1.471E+09
ZN-69	1.584E+03	0.000E+00	1.760E-11	0.000E+00	0.000E+00	0.000E+00	1.635E-12	2.067E-05
BR-83	3.440E+02	7.079E+03	1.790E-01	5.066E-57	0.000E+00	6.079E-58	2.112E-02	2.911E+00
BR-84	4.328E+02	2.363E+05	2.877E-23	0.000E+00	0.000E+00	0.000E+00	3.429E-24	2.251E-11
BR-85	1.832E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB-86	1.904E+05	1.035E+07	4.746E+09	4.101E+08	6.006E+07	4.921E+07	5.675E+08	2.772E+08
RB-88	5.456E+02	3.779E+04	3.886E-45	0.000E+00	0.000E+00	0.000E+00	4.777E-46	3.168E-22
RB-89	3.520E+02	1.452E+05	7.957E-53	0.000E+00	0.000E+00	0.000E+00	9.454E-54	1.247E-26
SR-89	2.416E+06	2.509E+04	2.674E+09	2.545E+08	2.719E+08	3.054E+07	5.617E+09	1.513E+10
SR-90	1.080E+08	0.000E+00	6.612E+10	8.049E+09	2.301E+10	9.659E+08	1.389E+11	7.507E+11
SR-91	2.592E+05	2.511E+06	2.409E+05	5.794E-10	0.000E+00	6.953E-11	5.064E+05	1.291E+06
			(PASTURE)	(PASTURE)	(FEED)	(PASTURE)	(PASTURE)	

*See note, page 3.0-36

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$ Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

ODCM, V.C. Summer, SCE&G Revision 13 (June 1990)

TABLE 3.2-5 (continued)

PATHWAY DOSE FACTORS FOR SECTION 3.2.3.3 (R₁)

Page 2 of 3

AGE GROUP	(TEENAGER)	(N.A.)	(TEENAGER)	(TEENAGER)	(TEENAGER)	(TEENAGER)	(TEENAGER)	(TEENAGER)
ISOTOPE	INHALATION	GROUND PLANE	GRS COW MILK	GRS COW MEAT	GRS COW MILK	GRS GOT MEAT	GRS GOT MILK	VEGETATION
SR-92	1.192E-05	8.631E+05	2.277E+01	2.516E-48	0.000E+00	3.019E-49	4.795E+01	1.012E+04
Y-90	5.592E+05	5.308E+03	1.074E+06	7.470E+05	2.666E-05	8.965E+04	1.289E+05	1.025E+08
Y-91M	3.200E+03	1.161E+05	5.129E-18	0.000E+00	0.000E+00	0.000E+00	6.260E-19	2.285E-07
Y-91	2.936E+06	1.207E+06	6.147E+06	3.910E+08	7.797E+05	4.691E+07	7.780E+05	3.212E+09
Y-92	1.648E+05	2.142E+05	2.828E+00	3.522E-35	0.000E+00	4.226E-36	3.402E-01	2.360E+04
Y-93	5.792E+05	2.534E+05	1.312E+04	1.688E-07	7.620E-61	2.026E-08	1.511E+03	4.983E+06
ZR-95	2.688E+06	2.837E+08	1.201E+06	1.092E+09	1.585E+05	1.310E+08	1.441E+05	1.253E+09
ZR-97	6.304E+05	3.44E+06	4.225E+04	9.231E-01	4.732E-35	1.108E-01	5.073E+03	1.673E+07
NB-95	7.512E+05	1.605E+08	3.338E+08	4.251E+09	1.963E+07	5.101E+08	4.008E+07	4.551E+08
MO-99	2.688E+05	4.626E+06	1.023E+08	1.892E+05	5.013E-03	2.270E+04	1.228E+07	1.293E+07
TC-99M	6.128E+03	2.109E+05	1.055E+04	6.471E-18	0.000E+00	7.766E-19	1.267E+03	5.011E+03
TC-101	6.672E+02	2.277E+04	1.343E-58	0.000E+00	0.000E+00	0.000E+00	1.508E-59	3.229E-29
RU-103	7.832E+05	1.265E+08	1.513E+05	7.162E+09	1.086E+04	8.595E+08	1.815E+04	5.706E+08
RU-105	9.040E+04	7.212E+05	1.263E+00	3.900E-25	0.000E+00	4.680E-26	1.519E-01	4.039E+04
RU-106	1.608E+07	5.049E+08	1.799E+06	1.130E+11	5.312E+05	1.356E+10	2.159E+05	1.484E+10
AG-110M	6.752E+06	4.019E+09	2.559E+10	1.345E+09	6.982E+09	1.614E+08	3.071E+09	4.031E+09
TE-125M	5.360E+05	2.128E+06	8.863E+07	8.941E+08	1.058E+07	1.073E+08	1.064E+07	4.375E+08
TE-127M	1.656E+06	1.083E+05	3.420E+08	3.816E+09	6.753E+07	4.580E+08	4.105E+07	2.236E+09
TE-127	8.080E+04	3.293E+03	9.572E+04	1.689E-08	0.000E+00	2.027E-09	1.122E+04	4.180E+05
TE-129M	1.976E+06	2.312E+07	4.502E+08	3.966E+09	2.500E+07	4.759E+08	5.528E+07	1.514E+09
TE-129	3.296E+03	3.076E+04	2.834E-09	0.000E+00	0.000E+00	0.000E+00	3.433E-10	3.916E-03
TE-131M	6.208E+05	9.459E+06	2.529E+07	1.447E+04	1.827E-15	1.736E+03	3.036E+06	3.248E+07
TE-131	2.336E+03	3.450E+07	2.879E-32	0.000E+00	0.000E+00	0.000E+00	3.515E-33	6.099E-15
TE-132	4.632E+05	4.968E+06	8.581E+07	2.300E+07	1.371E-01	2.760E+06	1.033E+07	7.818E+07
I-130	1.488E+06	6.692E+06	1.742E+08	4.005E-04	1.416E-45	4.806E-05	2.092E+08	8.276E+07
			(PASTURE)	(PASTURE)	(FEED)	(PASTURE)	(PASTURE)	

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$ Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

CDCM, V.C. Summer, SCE&G Revision 13 (June 1990)

3.0-31

TABLE 3.2-5 (continued)

PATHWAY DOSE FACTORS FOR SECTION 3.2.3.3 (R.)

Page 3 of 3

AGE GROUP	(TEENAGER)	(IN A.)	(TEENAGER)	(TEENAGER)	(TEENAGER)	(TEENAGER)	(TEENAGER)	(TEENAGER)
ISOTOPE	INHALATION	GROUND PLANE	GRS COW MILK	GRS COW MEAT	GRS COW MILK	GRS GOT MEAT	GRS GOT MILK	VEGETATION
I-131	1.464E+07	2.089E+07	2.195E+11	3.645E+09	3.266E+07	4.375E+08	2.634E+11	3.140E+10
I-132	1.512E+05	1.452E+06	2.242E+01	1.389E-57	0.000E+00	1.667E-58	3.092E+01	4.262E+03
I-133	2.920E+06	2.981E+06	1.674E+09	7.234E+01	3.096E-23	8.680E+00	2.009E+09	4.587E+08
I-134	3.953E+04	5.305E+05	1.583E-10	0.000E+00	0.000E+00	0.000E+00	1.915E-10	7.04E-03
I-135	6.208E+05	2.947E+06	3.777E+06	5.963E-15	0.000E+00	7.156E-16	4.538E+06	5.832E+06
CS-134	1.128E+06	8.007E+09	2.310E+10	1.231E+09	7.443E+09	1.477E+08	6.931E+10	1.671E+10
CS-136	1.936E+05	1.710E+08	1.759E+09	3.671E+07	5.249E+06	4.405E+06	5.292E+09	1.708E+08
CS-137	8.480E+05	1.201E+10	1.781E+10	9.634E+08	6.197E+09	1.156E+08	5.342E+10	1.348E+10
CS-138	8.560E+02	4.102E+05	3.149E-23	0.000E+00	0.000E+00	0.000E+10	9.576E-23	6.935E-11
BA-139	6.464E+03	1.194E+05	7.741E-07	0.000E+00	0.000E+00	0.000E+00	8.794E-08	2.403E-01
BA-140	2.032E+06	2.346E+07	7.483E+07	3.663E+07	1.990E+05	4.396E+06	8.981E+06	2.130E+08
BA-141	3.288E+03	4.734E+04	7.703E-46	0.000E+00	0.000E+00	0.000E+00	9.244E-47	8.699E-22
BA-142	1.912E+03	5.064E+04	5.010E-30	0.000E+00	0.000E+00	0.000E+00	6.012E-81	5.613E-39
LA-140	4.872E+05	2.180E+07	2.291E+05	8.689E+02	5.560E-12	1.043E+02	2.745E+04	5.104E+07
LA-142	1.200E+04	9.117E+05	4.611E-07	0.000E+00	0.000E+00	0.000E+00	5.465E-08	2.529E+00
CE-141	6.136E+05	1.540E+07	1.696E+07	2.252E+07	8.700E+05	2.703E+06	2.036E+06	5.404E+08
CE-143	2.552E+05	2.627E+06	1.671E+06	3.695E+02	1.130E-14	4.434E+01	2.006E+05	2.040E-07
CE-144	1.336E+07	8.042E+07	1.655E+08	3.089E+08	4.650E+07	3.706E+07	1.986E+07	1.326E-10
PR-143	4.832E+05	0.000E+00	9.553E+05	5.817E+07	3.374E+03	6.980E+06	1.146E+05	2.310E+08
PR-144	1.752E+03	2.112E+03	1.238E-53	0.000E+00	0.000E+00	0.000E+00	1.331E-54	3.097E-26
ND-147	3.720E+05	1.009E+07	7.116E+05	2.453E+07	8.552E+02	2.942E+06	8.530E+04	1.424E+08
W-187	1.768E+05	2.740E+06	2.646E+06	3.989E+00	5.579E-22	4.787E-01	3.155E+05	7.839E+06
NP-239	1.320E+05	1.976E+06	1.060E+05	3.387E+03	1.083E-07	4.064E+02	1.276E+04	2.097E+07
			(PASTURE)	(PASTURE)	(FEED)	(PASTURE)	(PASTURE)	

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$ Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

ODCM, V.C. Summer, SCE&G. Revision 13 (June 1990)

3.0-32

TABLE 3.2-6

PATHWAY DOSE FACTORS FOR SECTION 3.2.3.3 (R₁)*

Page 1 of 3

AGE GROUP	(ADULT)	(IN A.)	(ADULT)	(ADULT)	(ADULT)	(ADULT)	(ADULT)	(ADULT)
ISOTOPE	INHALATION	GROUND PLANE	GRS COW MILK	GRS COW MEAT	GRS COW MILK	GRS GOAT MEAT	GRS GOAT MILK	VEGETATION
H-3	1.264E+03	0.000E+00	6.904E+02	2.940E+02	6.904E+02	3.528E+01	1.408E+03	2.845E+03
C-14	1.816E+04	0.000E+00	2.634E+08	2.414E+08	9.219E+07	2.897E+07	2.634E+08	2.276E+08
NA-24	1.024E+04	1.885E+07	2.438E+06	1.356E-03	3.636E-38	1.628E-04	2.926E+05	2.690E+05
P-32	1.320E+06	0.000E+00	1.709E+10	4.651E+09	7.559E+07	5.582E+08	2.052E+10	1.403E+09
CR-51	1.440E+04	5.506E+06	7.187E+06	1.772E+06	2.644E+05	2.127E+05	8.624E+05	1.168E+07
MN-54	1.400E+06	1.625E+06	3.578E+07	2.812E+07	7.389E+06	3.375E+06	3.091E+06	9.585E+08
MN-56	2.024E+04	1.068E+06	1.328E-01	4.958E-52	0.000E+00	5.949E-53	1.594E-02	5.082E+02
FE-55	7.208E+04	0.000E+00	2.511E+07	2.933E+08	8.250E+06	3.519E+07	3.265E+05	2.096E+08
FE-59	1.016E+06	3.204E+08	2.327E+08	2.080E+09	2.009E+07	2.495E+08	3.024E+06	9.875E+08
CO-58	9.280E+05	4.464E+08	9.565E+07	3.703E+08	1.394E+07	4.443E+07	1.147E+07	6.252E+08
CO-60	5.968E+06	2.532E+10	3.082E+08	1.413E+09	1.044E+08	1.695E+08	3.7E+06	3.139E+09
NI-63	4.320E+05	0.000E+00	6.729E+09	1.888E+10	2.351E+09	2.256E+09	8.075E+08	1.040E+10
NI-65	1.232E+04	3.451E+05	1.219E+00	7.405E-52	0.000E+00	8.886E-53	1.464E-01	2.026E+02
CU-64	4.896E+04	6.876E+05	2.031E+06	2.307E-05	4.233E-46	2.769E-06	2.415E+05	7.841E+05
ZN-65	8.640E+05	8.583E+08	3.798E+09	1.132E+09	1.183E+09	1.358E+08	4.588E+08	1.009E+09
ZN-69	9.200E+02	0.000E+00	4.031E-12	0.000E+00	0.000E+00	0.000E+00	4.837E-13	1.202E-05
BR-83	2.408E+02	7.079E+03	1.399E-01	8.648E-57	0.000E+00	1.038E-57	1.698E-02	4.475E+00
BR-84	3.128E+02	2.363E+05	1.69E-23	0.000E+00	0.000E+00	0.000E+00	2.029E-24	2.475E-11
BR-85	1.280E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
RB-86	1.352E+05	1.027E+07	2.595E+09	4.870E+00	3.201E+07	5.845E+07	3.113E+08	2.194E+08
RB-88	3.872E+02	3.779E+04	2.129E-45	0.000E+00	0.000E+00	0.000E+00	2.573E-46	3.428E-22
RB-89	2.560E+02	1.476E+05	4.496E-53	0.000E+00	0.000E+00	0.000E+00	5.396E-54	3.961E-26
SR-89	1.400E+06	2.509E+04	1.451E+09	3.014E+08	1.475E+08	3.617E+07	3.046E+09	9.961E+09
SR-90	9.920E+07	0.000E+00	4.680E+10	1.244E+10	1.628E+10	1.493E+09	9.828E+10	6.846E+11
SR-91	1.912E+05	2.511E+06	1.377E+05	7.233E-10	0.000E+00	8.680E-11	2.872E+05	1.451E+06
			(PASTURE)	(PASTURE)	(FEED)	(PASTURE)	(PASTURE)	

*See note, page 3.0-36

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$ Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

ODCM, V.C. Summer, SCE&G Revision 13 (June 1990)

3.0-33

TABLE 3.2-6 (continued)

PATHWAY DOSE FACTORS FOR SECTION 3.2.3.3 (R₁)

Page 2 of 3

AGE GROUP	(ADULT)	(INFANT)	(ADULT)	(ADULT)	(ADULT)	(ADULT)	(ADULT)	(ADULT)
ISOTOPE	INHALATION	GROUND PLANE	GRS COW MILK	GRS COW MEAT	GRS COW MILK	GRS GOT MEAT	GRS GOT MILK	VEGETATION
SR-92	4.304E+04	8.631E+05	9.675E+00	2.334E-48	0.000E+00	2.801E-49	2.05E+01	8.452E+03
Y-90	5.056E+05	5.308E+03	7.511E+05	1.141E+06	1.865E-05	1.369E+05	9.028E+04	1.410E+08
Y-91M	1.920E+03	1.161E+05	1.883E-19	0.000E+00	0.000E+00	0.000E+00	2.262E-20	1.527E-08
Y-91	1.704E+06	1.207E+06	4.726E+06	6.231E+08	5.691E+05	7.477E+07	5.672E+05	2.814E+09
Y-92	7.352E+04	2.142E+05	9.772E-01	2.657E-35	0.000E+00	3.188E-36	1.17E-01	1.603E+04
Y-93	4.216E+05	2.534E+05	7.091E+03	2.075E-07	4.290E-61	2.490E-08	8.43E+02	5.517E+06
ZR-95	1.768E+06	2.837E+08	9.587E+05	1.903E+09	1.265E+05	2.284E+08	1.151E+05	1.194E+09
ZR-97	5.232E+05	3.445E+06	2.707E+04	1.292E+00	3.032E-35	1.550E-01	3.4E+03	2.108E+07
NB-95	5.048E+05	1.605E+08	2.787E+08	7.748E+09	1.639E+07	9.297+08	3.344E+07	4.798+08
MO-99	2.480E+05	4.626E+06	5.741E+07	2.318E+05	2.813E-03	2.781E+04	6.878E+06	1.426E+07
TC-99M	4.160E+03	2.102E+05	5.553E+03	7.439E-18	0.000E+00	8.927E-19	6.641E+06	5.187E+03
TC-101	3.992E+02	2.277E+04	7.406E-59	0.000E+00	0.000E+00	0.000E+00	8.888E-60	3.502E-29
RU-103	5.048E+05	1.265E+08	1.189E+05	1.229E+10	8.537E+03	1.475E+09	1.426E+04	5.577E+08
RU-105	4.816E+04	7.212E+05	5.240E-01	3.533E-25	0.000E+00	4.239E-26	6.245E-02	3.294E+04
RU-106	9.360E+06	5.049E+08	1.320E+06	1.811E-11	3.898E+05	2.173E+10	1.584E+05	1.247E+10
AG-110M	4.632E+06	4.019E+09	2.198E+10	2.523E+09	5.996E+09	3.028E+08	2.638E+09	3.979E+09
TE-125M	3.136E+05	2.128E+06	6.626E+07	1.460E+09	7.906E+06	1.751E+08	7.955E+06	3.927E+08
TE-127M	9.600E+05	1.083E+05	1.860E+08	4.531E+09	3.671E+07	5.437E+08	2.223E+07	1.418E+09
TE-127	5.736E+04	3.293E+03	5.278E+04	2.034E-08	0.000E+00	2.441E-09	6.172E+03	4.532E+09
TE-129M	1.160E+06	2.312E+07	3.028E+08	5.698E+09	1.645E+07	6.838E+08	3.636E+07	1.261E+09
TE-129	1.936E+03	3.076E+04	1.183E-09	0.000E+00	0.000E+00	0.000E+00	1.42E-10	2.80E-03
TE-131M	5.560E+05	9.459E+06	1.753E+07	2.190E+04	1.266E-15	2.628E+03	2.102E+06	4.428E+07
TE-131	1.392E+03	3.450E+07	1.578E-32	0.000E+00	0.000E+00	0.000E+00	1.927E-33	6.575E-15
TE-132	5.096E+05	4.958E+06	7.356E+07	4.287E+07	1.170E-01	5.144E+06	8.827E+06	1.312E+08
I-130	1.136E+06	6.692E+06	1.050E+08	5.272E-04	8.535E-46	6.326E-05	1.254E+08	9.809+07
			(PASTURE)	(PASTURE)	(FEED)	(PASTURE)	(PASTURE)	

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$ Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

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TABLE 3.2-6 (continued)
 PATHWAY DOSE FACTORS FOR SECTION 3.2.3.3 (R.)

Page 3 of 3

AGE GROUP	(ADULT)	(IN...)	(ADULT)	(ADULT)	(ADULT)	(ADULT)	(ADULT)	(ADULT)
ISOTOPE	INHALATION	GROUND PLANE	GRS COW MILK	GRS COW MEAT	GRS COW MILK	GRS GOT MEAT	GRS GOT MILK	VEGETATION
I-131	1.192E+07	2.089E+07	1.388E+11	5.034E+09	2.065E+07	6.040E+08	1.665E+11	3.785E+10
I-132	1.144E+05	1.452E+06	1.541E+01	1.816E-57	0.000E+00	2.179E-58	1.849E+01	5.016E+03
I-133	2.152E+06	2.981E+06	9.891E+08	9.336E+01	1.830E-23	1.120E+01	1.189E+09	5.331E+08
I-134	2.984E+04	5.305E+05	8.886E-11	0.000E+00	0.000E+00	0.000E+00	1.066E-10	4.563E-03
I-135	4.480E+05	2.947E+06	2.217E+06	7.644E-15	0.000E+00	9.172E-16	2.676E+06	6.731E+06
CS-134	8.480+05	8.007E+09	1.345E+10	1.565E+09	4.333E+09	1.878E+08	4.035E+10	1.110E+10
CS-136	1.464E+05	1.710E+08	1.039E+09	4.724E+07	3.093E+06	5.669E+06	3.117E+09	1.675E+08
CS-137	6.208E+05	1.201E+10	1.010E+10	1.193E+09	3.513E+09	1.431E+08	3.03E+10	8.696E+09
CS-138	6.208E+02	4.102E+05	1.786E-23	0.000E+00	0.000E+00	0.000E+00	5.146E-23	7.730E-11
BA-139	3.760E+03	1.194E+05	7.863E-08	0.000E+00	0.000E+00	0.000E+00	9.435E-09	5.225E-02
BA-140	1.272E+06	2.346E+07	5.535E+07	5.917E+07	1.472E+05	7.100E+06	6.643E+06	2.646E+08
BA-141	1.936E+03	4.734E+04	4.327E-46	0.000E+00	0.000E+00	0.000E+00	5.193E-47	9.463E-22
BA-142	1.192E+03	5.064E+04	2.509E-80	0.000E+00	0.000E+00	0.000E+00	3.011E-81	2.463E-39
LA-140	4.584E+05	2.180E+07	1.672E+05	1.385E+03	4.059E-12	1.662E+02	2.006E+04	7.319E+07
LA-142	6.328E+03	9.117E+05	6.273E-08	0.000E+00	0.000E+00	0.000E+00	7.531E-09	6.768E-01
CE-141	3.616E+05	1.540E+07	1.25E+07	3.632E+07	6.424E+05	4.358E+06	1.503E+06	5.097E+08
CE-143	2.264E+05	2.627E+06	1.15E+06	5.547E+02	7.768E-15	6.656E+01	1.38E+05	2.758E+07
CE-144	7.776E+06	8.042E+07	1.21E+08	4.928E+08	3.398E+07	5.914E+07	1.451E+07	1.112E+10
PR-143	2.008E+05	0.000E+00	6.918E+05	9.204E+07	2.445E+03	1.104E+07	8.297E+04	2.748E+08
PR-144	1.016E+03	2.112E+03	6.716E-54	0.000E+00	0.000E+00	0.000E+00	7.745E-55	3.303E-26
ND-147	2.208E+05	1.009E+07	5.231E+05	3.935E+07	6.286E+02	4.722E+06	6.273E+04	1.853E+08
W-187	1.552E+05	2.740E+06	1.796E+06	5.912E+00	3.787E-22	7.094E-01	2.14E+05	1.046E+07
NP-239	1.192E+05	1.976E+06	7.409E+04	5.152E+03	7.545E-08	6.182E+02	8.876E+03	2.872E+07
			(PASTURE)	(PASTURE)	(FEED)	(PASTURE)	(PASTURE)	

Units -

Inhalation and all tritium - mrem/yr per $\mu\text{Ci}/\text{m}^3$

Other pathways for all other radionuclides - $\text{m}^2 \cdot \text{mrem}/\text{yr}$ per $\mu\text{Ci}/\text{sec}$

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NOTE: The R_i values of Table 3.2-2 through 3.2-6 were calculated in accordance with the methods of Section 5.3.1 of Reference 1. Columns in those tables marked "Pasture" are for freely-grazing animals ($f_p = f_s = 1$). Columns marked "Feed" are for animals fed solely locally-grown stored feed ($f_p = f_s = 0$). The values used for each parameter and the origins of the values are given in Table 3.2-9 and its notes.

Table 3.2-7

CONTROLLING RECEPTORS, LOCATIONS, AND PATHWAYS*

<u>SECTOR</u>	<u>DISTANCE (METERS)</u>	<u>PATHWAY</u>	<u>AGE GROUP</u>	<u>ORIGIN (FOR INFORMATION ONLY)</u>
N**	6,100	Vegetation	Child	-Vegetable Garden
NNE**	5,300	Vegetation	Child	-Vegetable Garden
NE	4,500	Vegetation	Ch.	-Vegetable Garden
	4,500	Grass/Cow/Meat	Child	Grazing Beef Cattle
ENE	2,600	Vegetation	Child	-Vegetable Garden
	2,600	Grass/Cow/Meat	Child	Grazing Beef Cattle
E	1,800	Vegetation	Child	-Vegetable Garden
ESE	1,800	Vegetation	Child	-Vegetable Garden
SE	2,400	Vegetation	Child	-Vegetable Garden
SSE	,300	Vegetation	Child	-Vegetable Garden
S**	6,300	Vegetation	Child	-Vegetable Garden
SSW**	5,500	Vegetation	Child	-Vegetable Garden
SW**	5,300	Vegetation	Child	-Vegetable Garden
WSW	3,100	Grass/Cow/Meat	Child	-Grazing Beef Cattle
W	4,300	Vegetation	Child	-Vegetable Garden
	3,500	Grass/Cow/Meat	Child	Grazing Beef Cattle
WNW**	7,700	Vegetation	Child	-Vegetable Garden
NW**	6,600	Vegetation	Child	-Vegetable Garden
	6,600	Grass/Cow/Meat	Child	Grazing Beef Cattle
NNW	4,800	Vegetation	Child	-Vegetable Garden
	4,800	Grass/Cow/Meat	Child	Grazing Beef Cattle

* See note on the following page for the method used to identify these controlling receptors.

** If a cow were located at 5.0 miles (8,000 meters) in this sector, an infant consuming only its milk would receive a greater total radiation dose than would the real receptor listed. However, such an infant would not be the Maximum Exposed Individual for the site.

NOTE: The controlling receptor in each sector was identified in the following way. Receptor locations and associated pathways were obtained from the August 1991 field survey. A child was assumed at each location, except that where a milk cow was listed, an infant was assumed. $\overline{X/Q}$ for each candidate receptor was obtained by interpolation of values in Table 6.1-10 of Reference 5; $\overline{D/Q}$ for each candidate receptor was obtained by interpolation of values in Table 6.1-13 of Reference 5. Expected annual releases of each nuclide were taken from Table 5.2-2 of Reference 5. The pathway dose factors given above in Tables 3.2-3 and 3.2-4 were then used with the referenced values in the methodology of Section 5.3 of Reference 1 to compute total annual doses at each candidate receptor site for the pathways existing at that site. The controlling receptor for each sector was then chosen as the candidate receptor with the highest total annual dose of any candidate receptor in the given sector. All listed pathways are in addition to inhalation and ground plane exposure.

Table 3.2-8

ATMOSPHERIC DISPERSION PARAMETERS
FOR CONTROLLING RECEPTOR LOCATIONS*

<u>SECTOR</u>	<u>\bar{X}/Q'</u>	<u>\bar{D}/Q'</u>	<u>DISTANCE (MILES/METERS)</u>
N	1.5 E-07	7.0 E-10	3.8 / 6,100
NNE	2.5 E-07	1.1 E-09	3.3 / 5,300
NE	3.7 E-07	1.8 E-09	2.8 / 4,500
ENE	1.1 E-06	5.8 E-09	1.6 / 2,600
E	2.2 E-06	1.2 E-08	1.1 / 1,800
ESE	2.2 E-06	8.4 E-09	1.1 / 1,800
SE	1.6 E-06	5.8 E-09	1.5 / 2,400
SSE	3.0 E-07	1.0 E-09	2.7 / 4,300
S	1.7 E-07	3.7 E-10	3.9 / 6,300
SSW	2.0 E-07	6.4 E-10	3.4 / 5,500
SW	2.6 E-07	1.0 E-09	3.3 / 5,300
WSW	6.4 E-07	3.2 E-09	1.9 / 3,100
W	2.2 E-07	9.2 E-10	2.7 / 4,300
W	3.2 E-07	1.5 E-09	2.2 / 3,500
WNW	5.9 E-08	2.2 E-10	4.8 / 7,700
NW	9.6 E-08	4.1 E-10	4.1 / 6,600
NNW	1.8 E-07	9.8 E-10	3.0 / 4,800

- * Annual average relative dispersion and deposition values for the receptor locations in Table 3.2-7. Values were obtained by interpolation in Tables 6.1-10 and 6.1-13 of Reference 5. Those tables are based on one year (1975) of meteorological readings and the FSAR dispersion model (ground-level release, sector-averaged model, with open terrain recirculation factors, dry depletion by Figure 3.3-1, and using decay with a half-life of 8.0 days). As a result of the analysis described in the note to Table 3.2-7, the location of the maximum exposed individual for the site was identified as being the vegetable garden at 1.1 miles in the E sector. Therefore, the site \bar{X}/Q' and \bar{D}/Q' (Section 3.2.3.2 and following) are those from this table for that location.

Table 3.2-9
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PARAMETERS USED IN DOSE FACTOR CALCULATIONS

Parameter	Value	Origin of Value		
		Table in R.G. 1.109	Section of NUREG- 0133	Site- Specific
For P_i				
DFA _i	Each radionuclide	E-9		Note 2
BR	3700 m ³ /yr	E-5		
For Ri (Vegetation)				
r	Each element type	E-1		
Y _v	2.0 kg/m ²	E-15		
λw	5.83 E-7 sec ⁻¹		5.3.1.3	
DFL _i	Each age group and radio- nuclide	E-11 thru E-14		Note 2
U _a ^c	Each age group	E-5		
f _i	1.0		5.3.1.5	
t _L	8.6 E + 4 seconds	E-15		
U _a ^s	Each age group	E-5		
f _g	0.76		5.3.1.5	
t _h	5.18 E + 6 seconds	E-15		
H	8.84 gm/m ³			Note 1
For Ri (Inhalation)				
BR	Each age group	E-5		
DFA _i	Each age group and nuclide	E-7 thru E-10		Note 2

PARAMETERS USED IN DOSE FACTOR CALCULATIONS

Parameter	Value	Origin of Value		
		Table in R.G. 1 109	Section of NUREG- 0133	Site- Specific
	For R _i (Ground Plane)			
SF	0.7	E-15		
DFG	Each radionuclide	E-6		
t	4.73 E + 8 sec		5.3.1.2	
	For R _i (Grass/Animal/Meat)			
Q _c (Cow)	50 kg/day	E-3		
Q _c (Goat)	6 kg/day	E-3		
U _{ad}	Each age group	E-5		
λ _w	5.73 E-7 sec ⁻¹		5.3.1.3	
F _i (Both)	Each element	E-1		
r	Each element type	E-15		
DFL _i	Each age group and nuclide	E-1 thru E-14		Note 2
f _p	1.0			Note 3
f _s	1.0			Note 3
Y _p	0.7 kg/m ³	E-15		
t _h	7.78 E + 6 sec	E-15		
Y _s	2.0 kg/m ²	E-15		
t _f	1.73 E + 6 sec	E-15		
H	8.84 gm/m ³			Note 1

Table 3.2-9

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PARAMETERS USED IN DOSE FACTOR CALCULATIONS

<u>Parameter</u>	<u>Value</u>	<u>Origin of Value</u>		
		<u>Table in R.G. 1.109</u>	<u>Section of NUREG- 0133</u>	<u>Site- Specific</u>
	For R _i (Grass/Animal/Milk)			Note 4
Q _F (Cow)	50 kg/day	E-3		
Q _F (Goat)	6 kg/day	E-3		
U _{sp}	Each age group	E-5		
λ _w	5.73 E-7 sec ⁻¹		5.3.1.3	
F _m	Each element	E-1 & E-2		
r	Each element type	E-15		
DFL _i	Each age group and nuclide	E-11 thru E-14		Note 2
Y _p	0.7 kg/m ²	E-15		
t _h	7.78 E + 6 sec	E-15		
Y _s	2.0 kg/m ²	E-15		
t _i	1.73 E + 5 sec	E-15		
f _p	1.0			Note 5
f _s	1.0			Note 5
f _p	0.0			Note 5
f _s	0.0			Note 5
H	8.84 gm/m ³			Note 1

Table 3.2-9 (Continued)

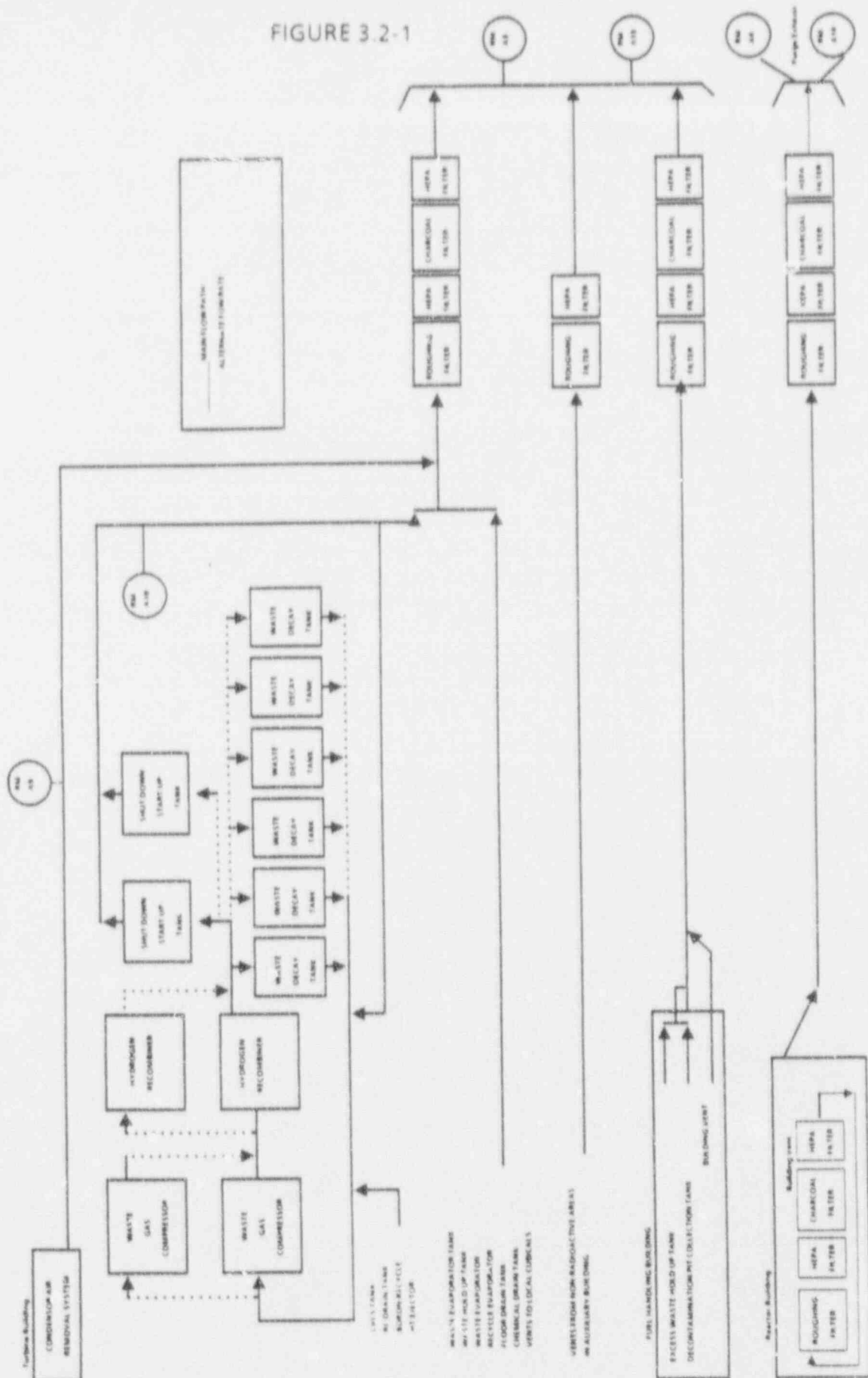
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NOTES

1. Site-specific annual average absolute humidity. For each month, an average absolute humidity was calculated from the 7 years of monthly average temperatures in Table 2.3-49 of Reference 4 and the 5 years of monthly average dew points in Table 2.3-64 of Reference 4. The 12 monthly values were averaged to obtain the annual average of 8.84 gm/m^3 . (Section 5.2.1.3 of Reference 1 gives a default value of 8 gm/m^3 .)
2. Inhalation and ingestion dose factors were taken from the indicated source. For each age group, for each nuclide, the organ dose factor used was the highest dose factor for that nuclide and age group in the referenced table.
3. Typically beef cattle are raised all year on pasture. Annual land surveys have indicated that the small number of goats raised within 5 miles typically are used for grass control and not food or milk. Nevertheless, the goats were treated as full meat and milk sources where present, despite the fact that their numbers cannot sustain the meat consumption rates of Table E-5 of Reference 3.
4. According to the August 1990 land use census, dairy cattle possibly graze at 4.9 miles in the West sector. If dairy cattle graze at this location, the dose to an infant consuming milk from these animals would be less than the dose received by the critical receptor identified for the sector. No other milking activity within five miles of the plant was identified. These values are included for reference only.
5. Two columns of R_i 's were calculated - one for cows kept exclusively on local pasture ($f_p = f_s = 1$), and one for cows kept exclusively on locally grown stored feed ($f_p = f_s = 0$). See the note on page 2.0-37.

GASEOUS RADWASTE TREATMENT SYSTEM

FIGURE 3.2-1



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3.3 Meteorological Model for Dose Calculations

3.3.1 Meteorological Model Parameters

<u>Term</u>	<u>Definition</u>	<u>Section of Initial Use</u>
b =	height of the containment building.	(3.3.2.1)
D_g =	deposition rate for ground-level releases relative to the distance from the containment building (from Figure 3.3-3).	(3.3.2.2)
D/Q =	the sector averaged relative deposition for any distance in a given sector (m^{-2}).	(3.3.2.2)
i =	wind speed class. The wind speed classes are given in Table 4A of Reference 10 as 1-3, 4-7, 8-12, 13-18, 19-24, and > 24 miles per hour.	(3.3.2.1)
N =	total hours of valid meteorological data.	(3.3.2.1)
n_{ij} =	number of hours meteorological conditions are observed to be in a given wind direction, wind speed class i, and atmospheric stability class j.	(3.3.3.1)
n =	number of hours wind is in given direction.	(3.3.2.1)
r =	distance from the containment building to the location of interest for dispersion calculations (m).	(3.3.2.1)
$\Delta T/\Delta Z$ =	temperature differential with vertical separation ($^{\circ}K/100m$).	(3.3.2.1)
T =	terrain recirculation factor, Figure 3.3-4.	(3.3.2.1)
u_i =	wind speed (midpoint of wind speed class i) at ground level (m/sec).	(3.3.2.1)
X/Q =	the sector average relative concentration at any distance in a given sector. (sec/m^3).	(3.3.2.1)
δ =	plume depletion factor at distance r from Figure 3.3-1.	(3.3.3.1)

<u>Term</u>	<u>Definition</u>	<u>Section of Initial Use</u>
σ_z	= vertical standard deviation of the plume (in meters), at distance r for ground level releases under the stability category indicated by $\Delta T / \Delta Z$, from Figure 3.3-2.	(3.3.2.1)
2.032	= $(2/\pi)^{1/2}$ divided by the width in radians of a 22.5° sector (0.3927 radians).	(3.3.2.1)
2.55	= the inverse of the number of radians in a 22.5° sector $\frac{1}{(22.5^\circ)(0.0175 \text{ Radians}^\circ)}$	(3.3.2.2)

3.3.2 Meteorological Model

3.3.2.1 Atmospheric dispersion for routine venting or other routine gaseous effluent releases is calculated using a ground-level, wake-corrected form of the straight line flow model.

$$\begin{aligned}
 X/Q &= \text{the sector-averaged relative concentration at any distance in the given sector (sec/m}^3\text{)} \\
 &= 2.032 \delta T \sum_{ij} \frac{n_{ij}}{N r u_i \sum_{kj} n_{kj}} \quad (52)
 \end{aligned}$$

where:

2.032 = $(2/\pi)^{1/2}$ divided by the width in radians of a 22.5° sector (0.3927 radians).

δ = plume depletion factor at distance r for the appropriate stability class from Figure 3.3-1.

i = wind speed class. The wind speed classes are given in Table 4A of Reference 10 as 1-3, 4-7, 8-12, 13-18, 19-24, and > 24 miles per hour.

n_{ij} = number of hours meteorological conditions are observed to be in a given wind direction, wind speed class i, and atmospheric stability class j.

$$\begin{aligned}
 N &= \text{total hours of valid meteorological data.} \\
 r &= \text{distance from the containment building to location of interest (m)} \\
 u_i &= \text{wind speed (midpoint of wind speed class } i) \text{ at ground level (m/sec).} \\
 \sum_z &= \text{the lesser of } (a_z^2 + b^2/2\pi)^{1/2} \text{ or } (\sqrt{3} \sigma_z) \quad (53)
 \end{aligned}$$

where:

$$\begin{aligned}
 \sigma_z &= \text{vertical standard deviation of the plume (in meters) at distance } r \text{ for ground level releases under the stability category indicated by } \Delta T/\Delta Z, \text{ from Figure 3.3-2.} \\
 T &= \text{terrain recirculation factor, from Figure 3.3-4} \\
 \pi &= 3.1416 \\
 b &= \text{height of the containment building (50.9m)} \\
 \Delta T/\Delta Z &= \text{temperature differential with vertical separation (}^\circ\text{K/100m).}
 \end{aligned}$$

Note: For calculation of X/Q using actual meteorological data for a particular release, u_i = the average wind speed for hour i and n_{ij} = number of hours with wind speed i and stability class j .

3.3.2.2 Relative deposition per unit area for all releases is calculated for a ground-level release.

$$\begin{aligned}
 D/Q &= \text{the sector-averaged relative deposition at any distance in a given sector (m}^{-2}\text{).} \\
 &= \frac{2.55 D_g^n}{r N} \quad (54)
 \end{aligned}$$

where,

$$D_g = \text{deposition rate for ground-level releases relative to distance (} r \text{) from the containment building (from Figure 3.3-3).}$$

2.55 = the inverse of the number of radians in a 22.5° sector

$$\frac{1}{(22.5^\circ)(0.0175 \text{ Radians/}^\circ)}$$

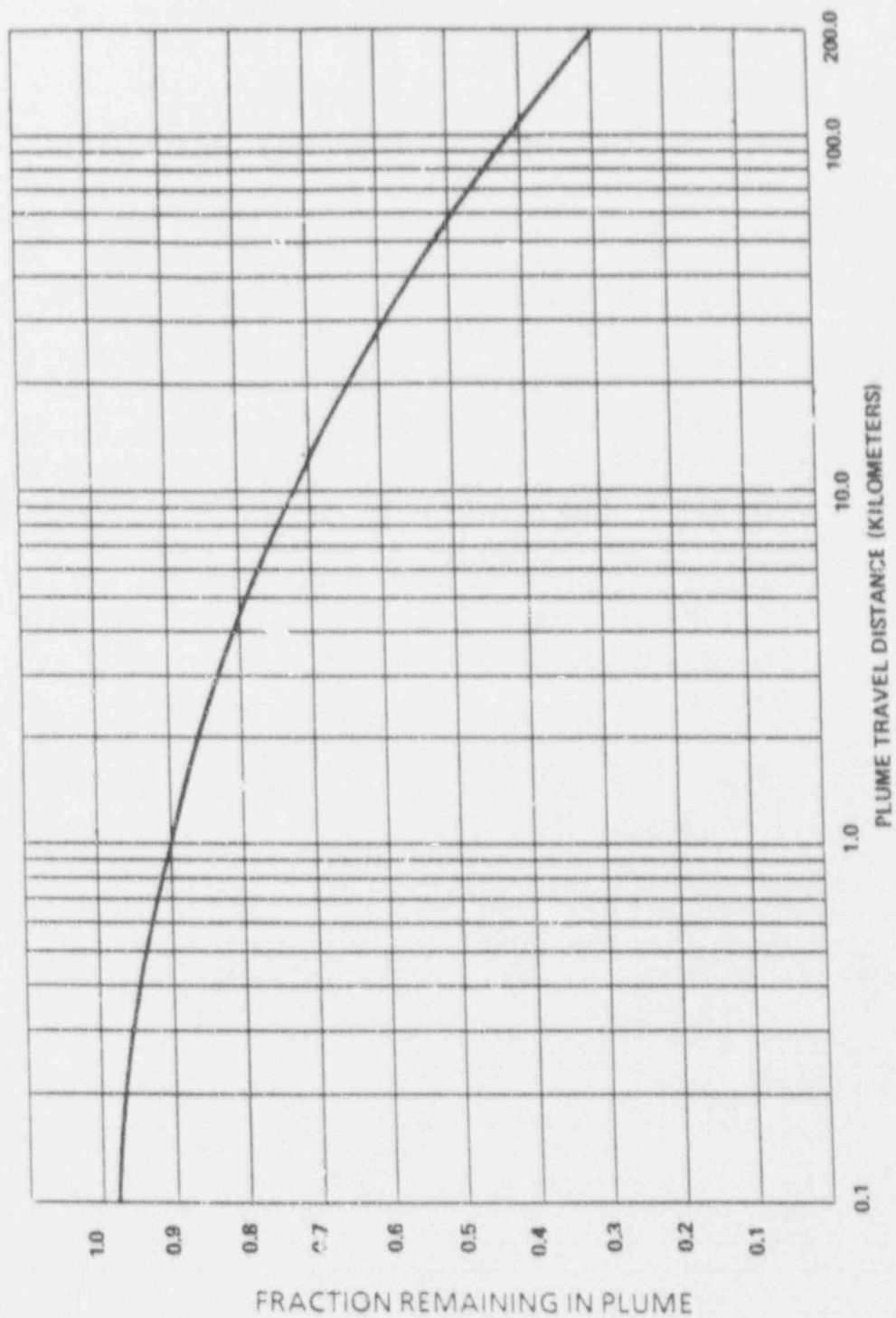
n = number of hours wind is in given direction (sector).

N = total hours of valid meteorological data.

FIGURE 3.3-1

Plume Depletion Effect for Ground Level Releases (8)
(All Atmospheric Stability Classes)

Graph taken from Reference 8, Figure 2

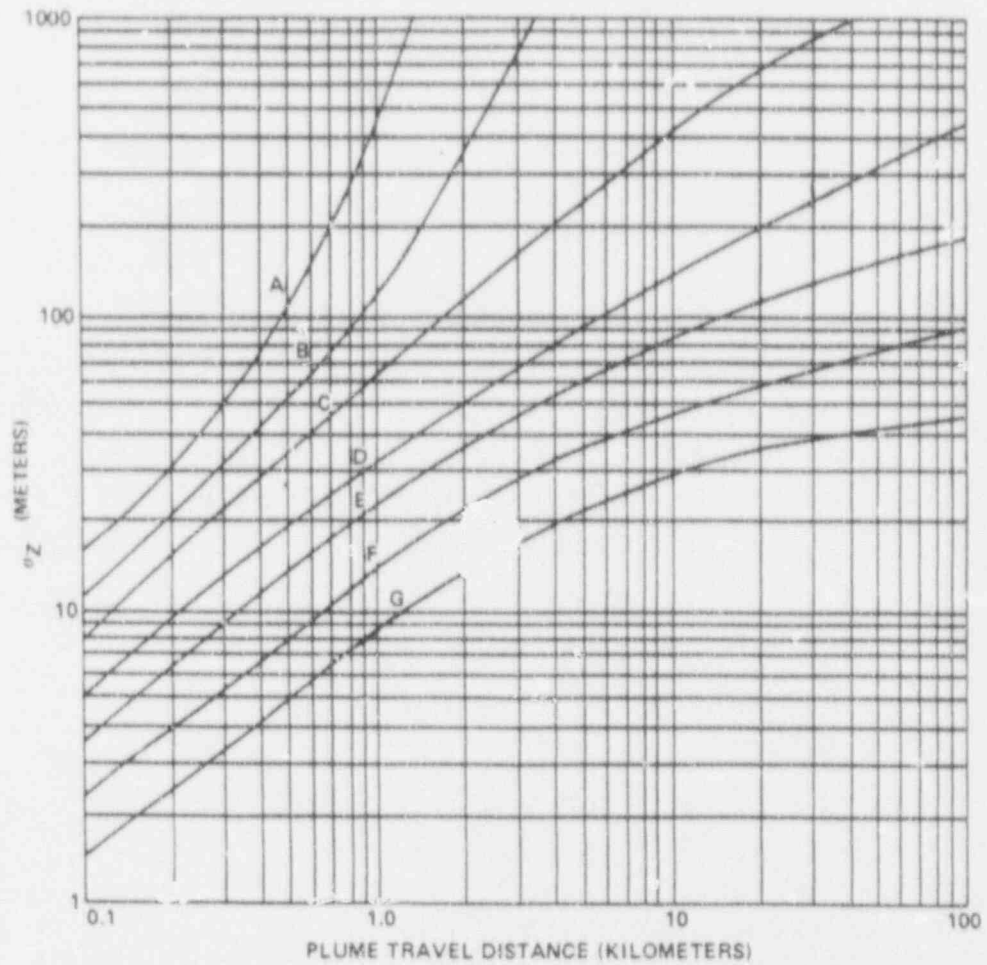


ODCM, V.C. Summer, SCE&G Revision 13 (June 1990)

FIGURE 3.3-2

Vertical Standard Deviation of Material in a Plume (σ_z)
 (Letters denote Pasquill Stability Classes)

Graph taken from Reference 8, Figure 1



Temperature Change
 with Height $\Delta T/\Delta Z$ ($^{\circ}\text{K}/100\text{m}$)

Pasquill
 Categories

Stability
 Classification

< -1.9

A

Extremely Unstable

-1.9 to -1.7

B

Moderately Unstable

-1.7 to -1.5

C

Slightly Unstable

-1.5 to -0.5

D

Neutral

-0.5 to 1.5

E

Slightly Stable

1.5 to 4.0

F

Moderately Stable

> 4.0

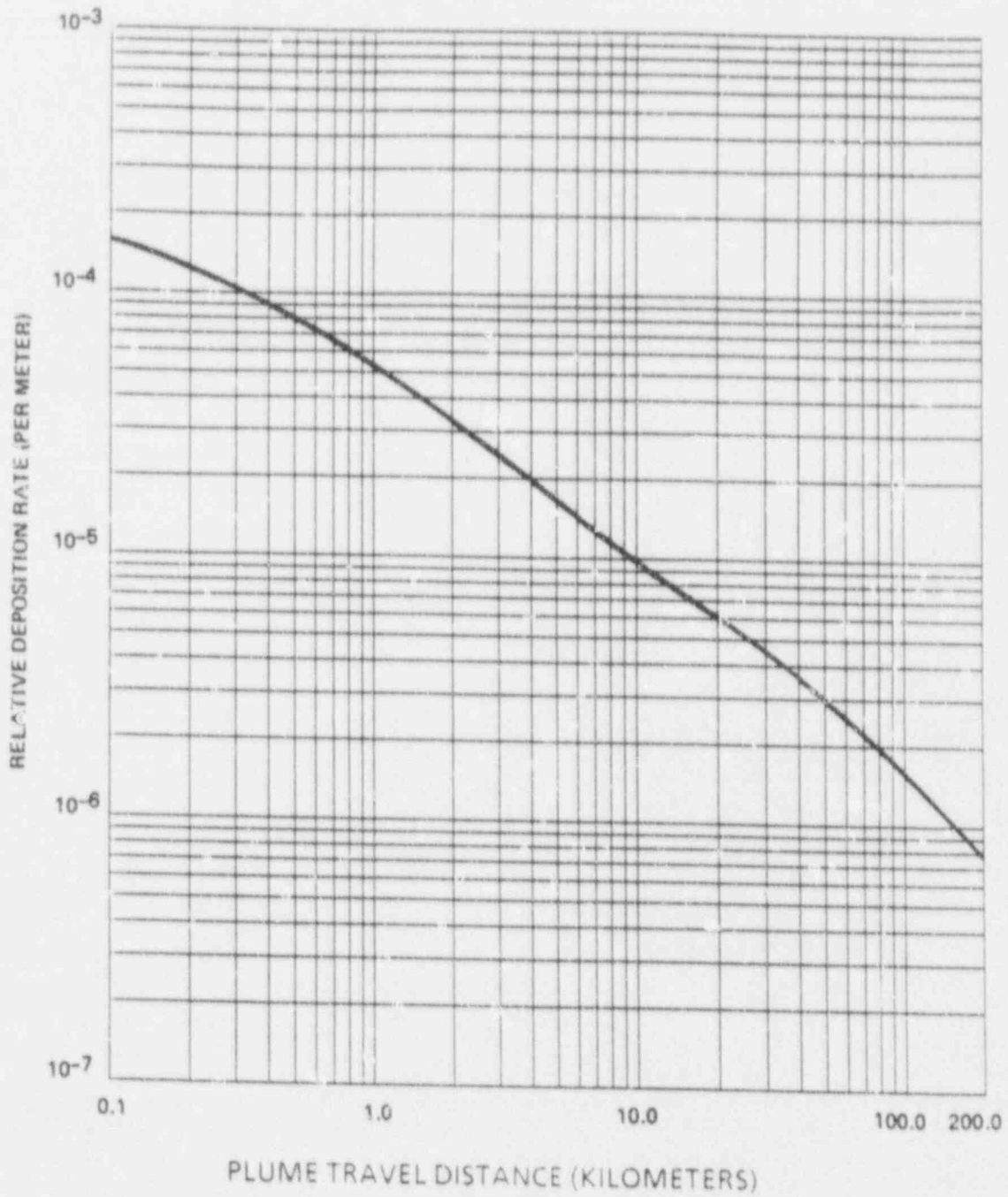
G

Extremely Stable

FIGURE 3.3-3

Relative Deposition for Ground Level Releases (D_g)
(All Atmospheric Stability Classes)

Graph taken from Reference 8, Figure 6

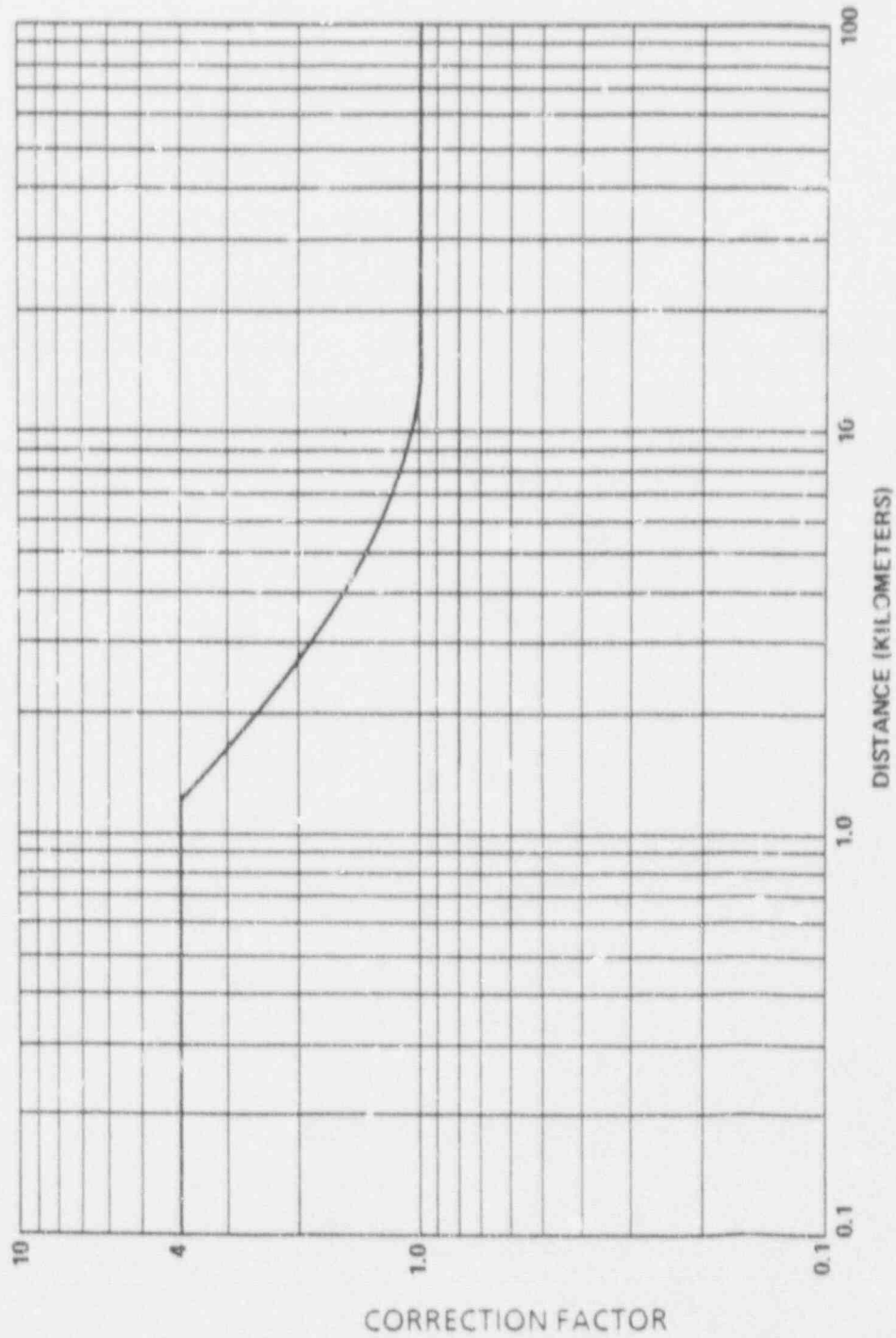


ODCM, V.C. Summer, SCE&G Revision 13 (June 1990)

FIGURE 3.3-4

Open Terrain Recirculation Factor

Graph taken from Reference 7, Figure 2



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4.0 RADIOLOGICAL ENVIRONMENTAL MONITORING

Sampling locations as required in section 1.4.1 of the ODCM Specifications are described in Table 4.0-1 and shown on Figures 4.0-1 and 4.0-2. As indicated by the ditto (") marks in the table, entries in the sampling frequency and analysis frequency columns apply to all samples below the entry until a new entry appears.

RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM
 VIRGIL C. SUMMER NUCLEAR STATION
 TABLE 4.0-1

Exposure Pathway and/or Sample	Criteria for Selection of Sample Number & Location	Sampling and Collection Frequency	Sample ¹ Location	Locations Mi/Dir	Type & Frequency of Analysis
AIRBORNE: I. Particulate	A) 3 Indicator samples to be taken at locations (in different sectors) beyond but as close to the exclusion boundary as practicable where the highest offsite sectorial ground level concentrations are anticipated. ²	Continuous sampler operation with weekly collection.	2 5 10	1.2 SW 0.9 SE 2.5 NNE	Gross beta following filter change; Quarterly Composite (by location) for gamma isotopic.
	B) 1 Indicator sample to be taken in the sector beyond but as close to the exclusion boundary as practicable corresponding to the residence having the highest anticipated offsite ground level concentration or dose. ²	Continuous sampler operation with weekly collection.	6	1.0 ESE	Gross beta following filter change; Quarterly Composite (by location) for gamma isotopic.
	C) 1 Indicator sample to be taken at the location of one of the dairies most likely to be affected. ^{2,4}	Continuous sampler operation with weekly collection.	14 ⁴	6.3 W	Gross beta following filter change; Quarterly Composite (by location) for gamma isotopic.
	D) 1 Control sample to be taken at a location at least 10 air miles from the site and not in the most prevalent wind direction. ²	Continuous sampler operation with weekly collection.	17	24.7 SE	Gross beta following filter change; Quarterly Composite (by location) for gamma isotopic.

RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM
 VIRGIL C. SUMMER NUCLEAR STATION
 TABLE 4.0-1

Exposure Pathway and/or Sample	Criteria for Selection of Sample Number & Location	Sampling and Collection Frequency	Sample ¹ Location	Locations Mi/Dir	Type & Frequency of Analysis
II. Radioiodine	A) 3 Indicator samples to be taken at two locations as given in I(A) above. B) 1 Indicator sample to be taken at the location as given in I(B) above. C) 1 Indicator sample to be taken at the location as given in I(C) above. D) 1 Control sample to be taken at a location similar in nature to I(D) above	Continuous sampler operation with weekly canister collection. Continuous sampler operation with weekly canister collection. Continuous sampler operation with weekly canister collection. Continuous sampler operation with weekly canister collection.	2 5 10 6 14 17	1.2 SW 0.9 SE 2.5 NNE 1.0 ESE 6.3 W 24.7 SE	Gamma isotopic for I-131 weekly Gamma isotopic for I-131 weekly Gamma isotopic for I-131 weekly Gamma isotopic for I-131 weekly
III. Direct	A) 13 Indicator stations to form an inner ring of stations in the 13 accessible sectors within 1 to 2 miles of the plant.	Monthly or quarterly exchange ^{5,7} ; two or more dosimeters at each location	1,2 3,4 5,6 7,8 9,10 29 30 47	1.2 S, 1.2 SW 1.2 W, 1.2 WNW 0.9 S E, 1.0 ESE 1.2 E, 1.5 ENE 2.2 NE, 2.5 NNE 0.9 WSW, 1.0 SSW 1.0 NW	Gamma dose monthly or quarterly

RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM
 VIRGIL C. SUMMER NUCLEAR STATION
 TABLE 4.0-1

Exposure Pathway and/or Sample	Criteria for Selection of Sample Number & Location	Sampling and Collection Frequency	Sample ¹ Location	Locations Mi/Dir	Type & Frequency of Analysis
	B) 16 Indicator stations to form an inner ring of stations in the 16 accessible sectors within 3 to 5 miles of the plant.	Monthly or quarterly exchange ^{5,7} ; two or more dosimeters at each location.	12,14 32,33 34,35 36,37 41,42 43 45 46 49 53,55	4 2 N, 6 3 W 4 5 NNE, 4 2 ENE 4 8 ESE, 4 8 SE 3 1 SSE, 1 9 NW 3 9 S, 1 9 SSW 5 2 SW 5 9 WSW 3 7 WNW 4 0 NNW 3 0 NE, 2 8 E	Gamma dose monthly or quarterly
	C) 8 Stations to be placed in special interest areas such as population centers, nearby residences, schools and in 2 or 3 areas to serve as controls.	Monthly or quarterly exchange ^{5,7} ; two or more dosimeters at each location.	11,13 15,16 17,18 31,54	3 3 N, 2 9 NNW 2 5 SSW, 28 0 W 24 7 SE, 16 5 S 5 8 NNE, 1 7 ENE	Gamma dose monthly or quarterly.
WATERBORNE: IV Surface Water	A) 1 Indicator sample downstream to be taken at a location which allows for mixing and dilution in the ultimate receiving river.	Time composite samples with collection every month. ⁵	21 ^{3,6}	2 7 SSW	Gamma isotopic monthly with quarterly composite (by location) to be analyzed for tritium. ⁷
	B) 1 Control sample to be taken at a location on the receiving river, sufficiently far upstream such that no effects of pumped storage operation are anticipated.	Time composite samples with collection every month. ⁵	22 ³	30 0 NNW	Gamma isotopic monthly with quarterly composite (by location) to be analyzed for tritium. ⁷

RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM
 VIRGIL C. SUMMER NUCLEAR STATION
 TABLE 4.0-1

Exposure Pathway and/or Sample	Criteria for Selection of Sample Number & Location	Sampling and Collection Frequency	Sample ¹ Location	Locations Mi/Dir	Type & Frequency of Analysis
	C) 1 Indicator sample from a location immediately upstream of the nearest downstream municipal water supply.	Time composite samples with collection every month. ⁵	17	24.7 SE	Gamma isotopic monthly with quarterly composite (by location) to be analyzed for tritium. ⁷
	D) 1 Indicator sample to be taken in the upper reservoir of the pumped storage facility at the plant discharge canal.	Time composite samples with collection every month. ⁵	23 ³	0.5 ESE	Gamma isotopic monthly with quarterly composite (by location) to be analyzed for tritium. ⁷
	E) 1 Indicator sample to be taken in the upper reservoir's non-fluctuating recreational area.	Grab sampling monthly. ⁵	24 ³	5.5 N	Gamma isotopic monthly with quarterly composite (by location) to be analyzed for tritium. ⁷
	F) 1 Control sample to be taken at a location on a separated unaffected watershed reservoir.	Grab sampling monthly. ⁵	18 ³	16.5 S	Gamma isotopic monthly with quarterly composite (by location) to be analyzed for tritium. ⁷
	G) 1 Indicator sample to be taken in the upper reservoir at the intake of the pumped storage facility.	Time composite samples with collection every month. ⁵	25 ³	0.8 WNW	Gamma isotopic monthly with quarterly composite (by location) to be analyzed for tritium. ⁷

RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM
 VIRGIL C. SUMMER NUCLEAR STATION
 TABLE 4.0-1

Exposure Pathway and/or Sample	Criteria for Selection of Sample Number & Location	Sampling and Collection Frequency	Sample ¹ Location	Locations Mi/Dir	Type & Frequency of Analysis
V. Ground Water	A) 2 Indicator samples to be taken within the exclusion boundary and in the direction of potentially affected ground water supplies.	Quarterly grab sampling ⁷	26 27	Onsite Onsite	Gamma isotopic and tritium analyses quarterly ⁷
	B) 1 Control sample from an unaffected location	Quarterly grab sampling ⁷	16	20.1 W	Gamma isotopic and tritium analyses quarterly ⁷
VI. Drinking Water	A) 1 Indicator sample from a nearby public ground water supply source.	Monthly grab sampling ⁵	28	2.4 SSE	Monthly ⁵ gamma isotopic and gross beta analyses and quarterly ⁷ composite for tritium analyses.
	B) 1 Indicator (finished water) sample from the nearest downstream water supply	Monthly composite sampling	17	24.7 S	Monthly ⁵ gamma isotopic and gross beta analyses and quarterly ⁷ composite for tritium analyses.
	C) 1 Control (finished water) sample from an unaffected water supply.	Monthly composite sampling	39	14.0 SSE	Monthly ⁵ gamma isotopic and gross beta analyses and quarterly ⁷ composite for tritium analyses.

RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM
 VIRGIL C. SUMMER NUCLEAR STATION
 TABLE 4.0-1

Exposure Pathway and/or Sample	Criteria for Selection of Sample Number & Location	Sampling and Collection Frequency	Sample ¹ Location	Locations Mi/Dir	Type & Frequency of Analysis
INGESTION: VII. Milk ⁴	A) Samples from milking animals in 3 locations within 5 km having the highest dose potential. If there are none then 1 sample from milking animals in each of 3 areas between 5 to 8 km distance where doses are calculated to be greater than 1 mrem per year. ¹⁰	Semimonthly when animals are on pasture ⁸ , monthly other times ⁵	To be supplied when milking animals are found in accordance with internal criteria.		Gamma isotopic and I-131 analysis semimonthly ⁸ when animals are on pasture, monthly other times ⁵
	B) 1 Control sample to be taken at the location of a dairy > 20 miles distance and not in the most prevalent wind direction. ²	Semimonthly when animals are on pasture ⁸ , monthly other times ⁵	16	20 1 W	Gamma isotopic and I-131 analysis semimonthly ⁸ when animals are on pasture, monthly other times ⁵
	C) 1 Indicator grass (forage) sample to be taken at one of the locations beyond but as close to the exclusion boundary as practicable where the highest offsite sectorial ground level concentrations are anticipated. ²	Monthly when available ⁵	6	1.0 ESE	Gamma isotopic
	D) 1 Indicator grass (forage) sample to be taken at the location of VII(A) above when animals are on pasture	Monthly when available ⁵	To be supplied when milking animals are found in accordance with internal criteria.		Gamma isotopic

RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM
 VIRGIL C. SUMMER NUCLEAR STATION
 TABLE 4.0-1

Exposure Pathway and/or Sample	Criteria for Selection of Sample Number & Location	Sampling and Collection Frequency	Sample ¹ Location	Locations Mi/Dir	Type & Frequency of Analysis
	E) 1 Control grass (forage) sample to be taken at the location of VII(3) above	Monthly when available ⁵	16	20 1 W	Gamma isotopic
VIII. Food Products	A) 2 samples of broadleaf vegetation grown in the 2 nearest offsite locations of highest calculated annual average ground level D/Q if milk sampling is not performed within 3 km or if milk sampling is not performed at a location within 5-10 km where the doses are calculated to be greater than 1 mrem/yr. ¹⁰	Monthly when available ⁵	6 8	1 0 ESE 1 5 ENE	Gamma isotopic on edible portion.
	B) 1 Control sample for the same foods taken at a location at least 10 miles distance and not in the most prevalent wind direction if milk sampling is not performed within 3 km or if milk sampling is not performed at a location within 5-8 km where the doses are calculated to be greater than 1 mrem/yr. ¹⁰	Monthly when available ⁵	18	16 5 S	Gamma isotopic on edible portion.
IX. Fish	A) 1 Indicator sample to be taken at a location in the upper reservoir.	Semiannual ⁹ collection of the following specie types if available: bass, bream, crappie, catfish, carp, forage fish (shad).	23 ¹	0 3-5	Gamma isotopic on edible portions semiannually ⁹

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RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM
 VIRGIL C. SUMMER NUCLEAR STATION
 TABLE 4.0-1

Exposure Pathway and/or Sample	Criteria for Selection of Sample Number & Location	Sampling and Collection Frequency	Sample Location	Locations M/Dir	Type & Frequency of Analysis
	B) 1 Indicator sample to be taken at a location in the lower reservoir. C) 1 Indicator sample to be taken at a location in the upper reservoir's non-fluctuating recreational area. D) 1 Control sample to be taken at a location on the receiving river sufficiently far upstream such that no effects of pumped storage operation are anticipated.	Semiannual ⁹ collection of the following species types if available: bass; bream, crappie, catfish, carp; forage fish (shad). Semiannual ⁹ collection of the following species types if available: bass; bream, crappie, catfish, carp; forage fish (shad). Semiannual ⁹ collection of the following species types if available: bass; bream, crappie, catfish, carp; forage fish (shad).	21 ³ 24 ³ 22 ³	1-3 5.5-6.5 30.0 NNW	Gamma isotopic on edible portions semiannually ⁹ Gamma isotopic on edible portions semiannually ⁹ Gamma isotopic on edible portions semiannually ⁹
AQUATIC: X. Sediment	A) 1 Indicator sample to be taken at a location in the upper reservoir. B) 1 Indicator sample to be taken at a location in the upper reservoir's non-fluctuating recreational area.	Semiannual grab sample ⁹ Semiannual grab sample ⁹	23 ³ 24 ³	0.5 ESE 5.5 N	Gamma isotopic Gamma isotopic

RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM
 VIRGIL C. SUMMER NUCLEAR STATION
 TABLE 4.0-1

Exposure Pathway and/or Sample	Criteria for Selection of Sample Number & Location	Sampling and Collection Frequency	Sample ¹ Location	Locations Mi/Dir	Type & Frequency of Analysis
	C) 1 Indicator sample to be taken on the shoreline of the lower reservoir. D) 1 Control sample to be taken at a location on the receiving river sufficiently far upstream such that no effects of pumped storage operation are anticipated.	Semiannual grab sample ⁹ Semiannual grab sample ⁹	21 ¹ 22 ¹	2.7 SSW 30.0 NNW	Gamma isotopic. Gamma isotopic.

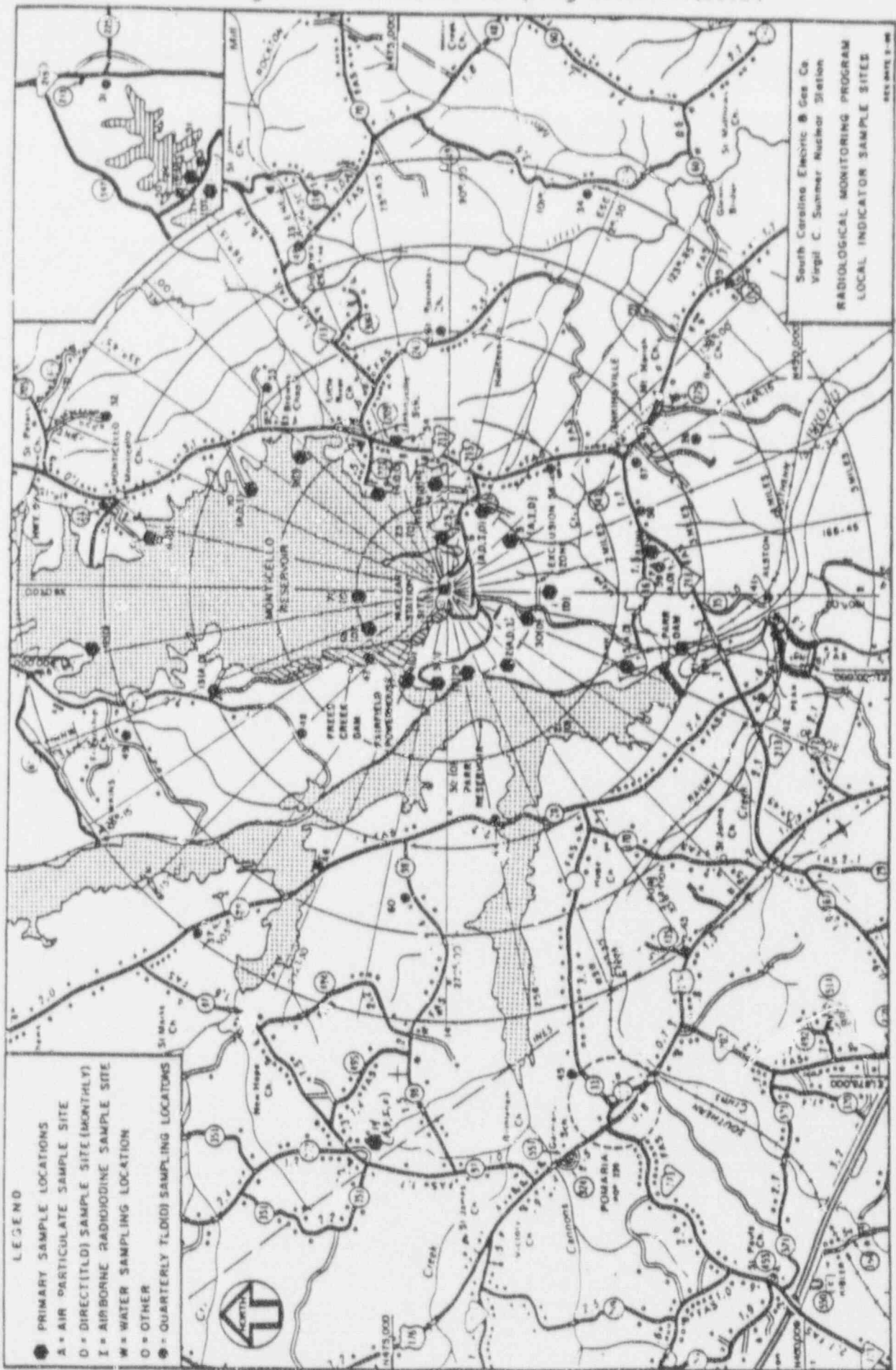
RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM
VIRGIL C. SUMMER NUCLEAR STATION
TABLE 4.0-1

NOTES

- (1) Location numbers refer to Figures 4.0-1 and 4.0-2.
- (2) Sample site locations are based on the meteorological analysis for the period of record as presented in Chapters 5 and 6, V.C. Summer Operating License Environmental Report
- (3) Though generalized areas are noted for simplicity of sample site enumeration, airborne, water and sediment sampling is done at the same location whereas biological sampling sites are generalized areas in order to reasonably assure availability of samples.
- (4) Milking animal and garden survey results will be analyzed annually. Should the survey indicate new dairying activity the owners shall be contacted with regard to a contract for supplying sufficient samples. If contractual arrangements can be made, site(s) will be added for additional milk sampling up to a total of 3 Indicator Locations.
- (5) Not to exceed 35 days.
- (6) Time composite samples are samples which are collected with equipment capable of collecting an aliquot at time intervals which are short (e.g. hourly) relative to the compositing period.
- (7) At least once per 100 days.
- (8) At least once per 18 days.
- (9) At least once per 200 days.
- (10) The dose shall be calculated for the maximum organ and age group, using the guidance/methodology contained in Regulatory Guide 1.109, Rev. 1 and the parameters particular to the Site.

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FIGURE 4.0-1
Radiological Environmental Sampling Locations (Local)



Radiological Environmental Sampling Locations

(Remote)

LEGEND

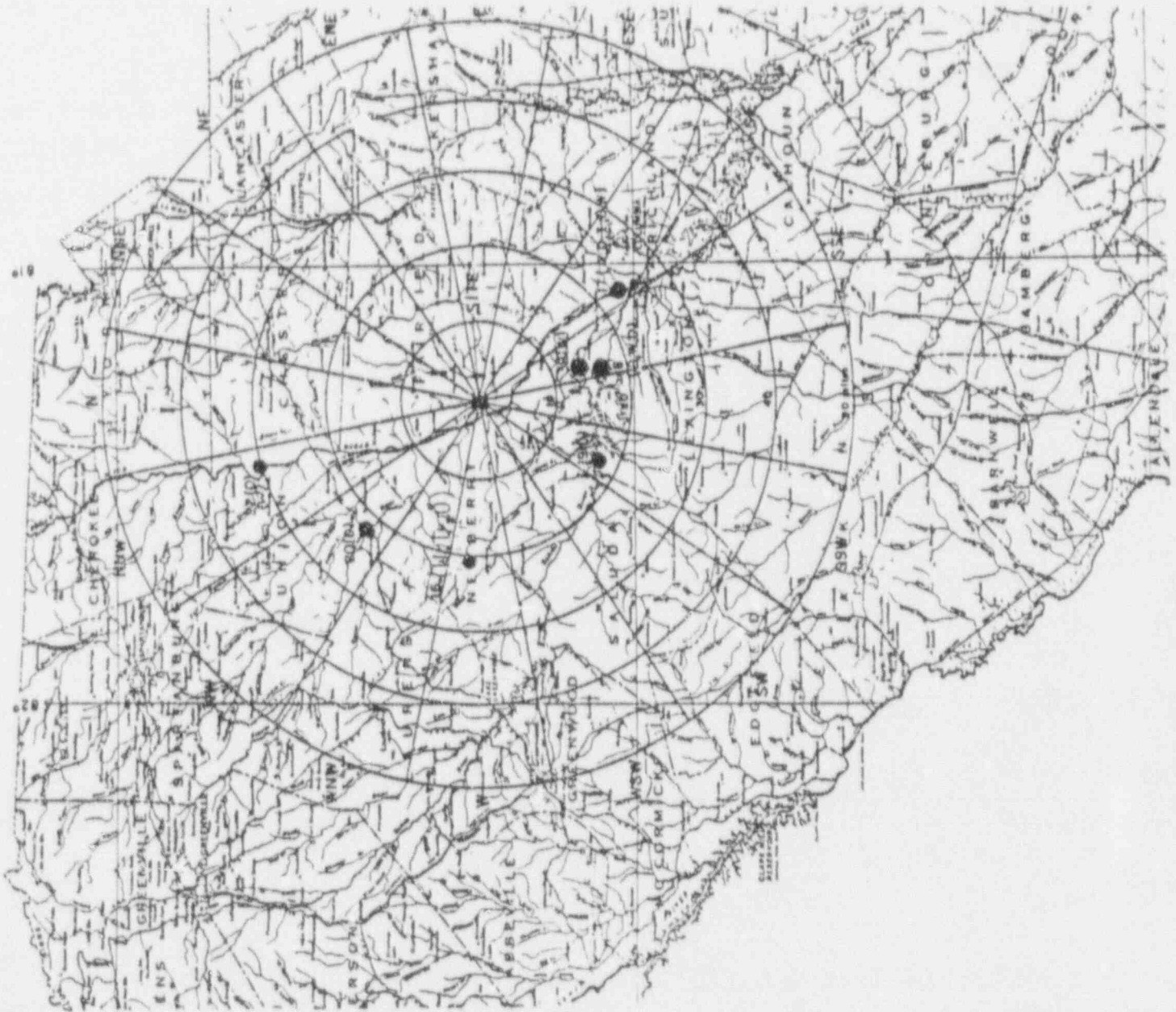
- CONTROL SAMPLE LOCATIONS
- A= AIR PARTICULATE SITE
- D= DIRECT(I/D) SITE
- I= AIRBORNE RADIOIODINE SITE
- W= WATER SITE
- O= OTHER (GARDEN PRODUCTS, FISH, SEDIMENT, GRASS, MILK)

REFERENCE
THE BASE FOR THIS MAP WAS PREPARED FROM A
PORTION OF USGS STATE OF GEORGIA, 1970



South Carolina Electric & Gas Co.
Virgil C. Summer Nuclear Station

Regional Location Map



Appendix A

Worked Examples of Monitor Setpoint Calculations and Dose Calculations

A. RM-L5, RM-L7 and RM-L9

Given:	V	=	5100 gal	Nuclide Concentrations:		
	f_r	=	100 GPM	H-3	=	2.70E-2 uCi/ml
	F_{dp}	=	2.1E6 GPM	Mn-54	=	3.59E-7 uCi/ml*
	f_{dx}	=	60 GPM	Fe-55	=	4.35E-6 uCi/ml
	F_t	=	2.33E6 GPM	Fe-59	=	5.38E-7 uCi/ml*
	C_{ir}/MPC_i	=	8.73E-6	Co-58	=	5.83E-7 uCi/ml*
	Δt_k	=	1.25 hr	Co-60	=	2.76E-6 uCi/ml*
				Sr-89	=	6.50E-8 uCi/ml
				Sr-90	=	1.74E-7 uCi/ml
				Ic-99m	=	2.10E-7 uCi/ml*
				Sb-124	=	5.49E-7 uCi/ml*
				Sb-125	=	3.24E-6 uCi/ml*
				I-131	=	3.83E-5 uCi/ml*
				I-133	=	5.92E-8 uCi/ml*
				Xe-133	=	1.12E-4 uCi/ml*
				Xe-133m	=	8.46E-7 uCi/ml*
				La-140	=	1.77E-7 uCi/ml*

* = make up ΣC_g

1) Monitor Setpoint Calculations

The method outlined in section 2.1.2 by which these monitor setpoints are calculated is as follows (see Section 2.1.1 for definitions of terms):

a) The minimum recirculation time shall be:

$$\begin{aligned}t_r &= 2V/f_r \\ &= 2(5100 \text{ gal}) / 100 \text{ gal/min} \\ &= 102 \text{ min}\end{aligned}$$

- b) The isotopic concentration to be released is obtained from the sum of the measured concentrations.

$$\begin{aligned} \sum_i C_i &= \sum_g C_g + C_a + C_s + C_t + C_f \\ &= 1.60E-4 \text{ uCi/ml} + 0 + 2.39E-7 \text{ uCi/ml} + 2.70E-2 \text{ uCi/ml} + \\ &\quad 4.35E-6 \text{ uCi/ml} \\ &= 2.71E-2 \text{ uCi/ml} \end{aligned}$$

- c) Once isotopic concentrations have been determined, these values are used to calculate a Dilution Factor, DF.

$$\begin{aligned} DF &= \left[\sum_i \frac{C_i}{MPC_i} \right]_x + SF \\ DF &= \left[\sum_g \frac{C_g}{MPC_g} + \frac{C_a}{MPC_a} + \frac{C_s}{MPC_s} + \frac{C_f}{MPC_f} + \frac{C_t}{MPC_t} \right]_x + SF \\ &= \left[\sum \left(\frac{3.59E-7}{1E-4} + \frac{5.38E-7}{6E-5} + \frac{5.38E-7}{1E-4} \right. \right. \\ &\quad + \frac{2.76E-6}{5E-5} + \frac{2.1E-7}{6E-3} + \frac{5.49E-7}{2E-5} \\ &\quad + \frac{3.24E-6}{1E-4} + \frac{3.83E-5}{3E-7} + \frac{5.92E-8}{1E-6} \\ &\quad \left. \left. + \frac{1.12E-4}{2E-4} + \frac{8.46E-7}{2E-4} + \frac{1.77E-7}{2E-4} \right) + 0 \right. \\ &\quad \left. + \left(\frac{6.5E-8}{3E-6} + \frac{1.74E-7}{3E-7} \right) + \frac{4.35E-6}{8E-4} + \frac{2.7E-2}{3E-3} \right] + 0.5 \\ &= 138 / 0.5 = 276 \end{aligned}$$

- d) The maximum permissible discharge flow rate, f_t , is now calculated.

$$f_t = \frac{F_{dp} + f_{dx}}{DF} = \frac{F_{dp}}{DF} \quad \text{for } F_{dp} \gg f_{dx}$$

$$\frac{2.1E6 \text{ gpm} + 60 \text{ gpm}}{276}$$

$$= 7600 \text{ gpm}$$

and,

$$F_{dp} = (0.9) F_t \left(1 - \sum_i \frac{C_{ir}}{MPC_i} \right)$$

$$= (.9) 2.33E6 (1 - 0.00000873)$$

$$= 2.1E6 \text{ gpm}$$

- e) The dilution flow rate setpoint, F , is established at 90 percent of the expected available dilution flow rate:

$$\begin{aligned} F &= (0.9) F_t \\ &= (.9) 2.33E6 \text{ gpm} \\ &= 2.1E6 \text{ gpm} \end{aligned}$$

The flow rate monitor setpoint for the effluent stream shall be set at the selected discharge pump rate (normally the maximum discharge pump rate or zero).

- f) The radiation monitor setpoints is now determined based on the values of $\sum C_i$, F , and f which were specified. The monitor response is primarily to gamma radiation, therefore, the actual setpoint is based on $\sum C_g$.

The setpoint concentration, c , is determined as follows:

$$c \leq \sum_g C_g(A)$$

$$A = f_t / f_{da}$$

$$= \frac{7600 \text{ gpm}}{60 \text{ gpm}}$$

$$= 127$$

If $A < 1$, No release may be made. Reevaluate the alternatives presented in Step d).

If $A \geq 1$, Calculate c and determine the maximum value for the actual monitor setpoint (cpm) from the monitor calibration graph.

$$c \leq \sum_g C_g(A) = (1.60E-4 \text{ uCi/ml})(127)$$

$$= 2.03E-2 \text{ uCi/ml}$$

$c \cong$ cpm equivalent to $2.03E-2 \text{ uCi/ml}$

- Reading from Figure 2.1-1 yields:

$$C \cong 12,000 \text{ cpm}$$

- g) Within the limits of the conditions stated above, the specific monitor setpoints (in uCi/ml) for the three liquid radiation monitors RM-L5, RM-L7, and RM-L9 are determined as follows:

RM-L5. Waste Monitor Tank Discharge Line Monitor:

$$C_M \leq \left| \sum_g C_g \right|_M(A)$$

RM-L7, Nuclear Blowdown Monitor Tank Discharge Line Monitor:

$$C_B \leq \left| \sum_g C_g \right|_B(A)$$

RM-L9, Combined Liquid Waste Processing System and Nuclear Blow-down Waste Effluent Discharge Line Monitor

The monitor setpoint on the common line, c_c , should be the same as the setpoint for the monitor on the active individual discharge line (i.e., c_M , or c_B as determined above):

$$C_C \leq \text{MAX}(C_M, C_B)$$

Liquid Radwaste Discharge Via Industrial and Sanitary Waste System (RM-L5)

The RM-L5 setpoint should be established as close to background as practical to prevent spurious alarms and yet alarm should an inadvertent high concentration release occur.

2) Dose Calculation

The dose contribution from all radionuclides identified in liquid effluents released to unrestricted areas is calculated using the expression*:

$$D_i = \sum_i \left[A_{it} \sum_{k=1} \Delta t_k C_{ik} F_k \right]$$

where:

$$F_k = \frac{f_{dx}}{(F_t)(1)} = \frac{60 \text{ gpm}}{2.33E6 \text{ gpm}} \\ = 2.6E-5$$

$$= \sum_i \left[(8.96)(1.25)(2.7E-2)(2.6E-5) + (908)(1.25)(3.59E-7)(2.6E-5) + (143)(1.25) \right. \\ (4.35E-6)(2.6E-5) + (1260)(1.25)(5.38E-7)(2.6E-5) + (339)(1.25)(5.83E-7)(2.6E-5) \\ + (958)(1.25)(2.76E-6)(2.6E-5) + (1370)(1.25)(6.5E-8)(2.6E-5) + (288,000)(1.25) \\ (1.74E-7)(2.6E-5) + (1.06)(1.25)(2.1E-7)(2.6E-5) + (95)(1.25)(5.49E-7)(2.6E-5) + \\ \left. (36.5)(1.25)(3.24E-6)(2.6E-5) + (486)(1.25)(3.83E-5)(2.6E-5) + (89.7)(1.25) \right]$$

$$(5.92E-8)(2.6E-5) + (0.0476)(1.25)(1.77E-7)(2.6E-5) \\ = 1.025E-5 \text{ mRem (to the Whole Body)}$$

*Dose calculation example was done only for Whole Body. Bone, Liver, Thyroid, Kidney, Lung and GI-LLI also must be done to address all dose receptors.

B. RM-L3, RM-L8, RM-L10 and RM-L11

Normal Mode

Given:

f_r	=	100 GPM	H-3	=	3.71E-2 uCi/ml
F_{dc}	=	3.114E5 GPM	I-131	=	1.04E-5 uCi/ml*
f_{ds}	=	250 GPM	I-133	=	6.14E-7 uCi/ml*
F_d	=	3.46E5 GPM	Cs-134	=	1.47E-6 uCi/ml*
C_{ir}/MPC_i	=	8.54E-6	Cs-137	=	1.73E-6 uCi/ml*
Δt_k	=	2.5 hr			

* = make up ΣC_g

1) Monitor Setpoint Calculations

The method outlined in section 2.1.4.1 by which these monitor setpoints are calculated is as follows:

- a) Total isotopic concentration and the Dilution Factor are calculated as in steps a) and b) of example A.

$$\sum_i C_i = \sum_g C_g + C_a + C_s + C_i + C_f \\ = 1.42E-5 \text{ uCi/ml} + 0 + 0 + 3.71E-2 \text{ uCi/ml} + 0 \\ = 3.71E-2 \text{ uCi/ml}$$

$$DF = \left[\sum_i \frac{C_i}{MPC_i} \right]^{1/x} \div SF \\ = \left[\sum \frac{1.04E-5}{3.0E-7} + \frac{6.14E-7}{1.0E-6} + \frac{1.47E-6}{9.0E-6} + \frac{1.73E-6}{2.0E-5} \right]$$

$$+ 0 + 0 + 0 + \frac{3.71E-2}{3.0E-3} \Big| \div 0.5$$

$$= 48/0.5 = 96$$

- b) The maximum permissible effluent discharge flow rate, f_d , is now calculated.

$$f_d = \frac{F_{dc} + f_{ds}}{DF} = \frac{F_{dc}}{DF} \text{ for } F_{dc} \gg f_{ds}$$

$$= \frac{3.114E5 \text{ GPM} + 250 \text{ GPM}}{96}$$

$$= 3,245 \text{ GPM}$$

and,

$$F_{dc} = (0.9) F_d \left[1 - \sum_i \frac{C_{ir}}{MPC_i} \right]$$

$$= (0.9)(3.46E5 \text{ GPM})(1 - 8.54E-6)$$

$$= 3.11E5 \text{ GPM}$$

If $f_d \geq f_{ds}$ releases may be made as planned.

- c) The dilution flow rate setpoint for minimum flow rate, F , is established at 90 percent of the expected available dilution flow rate:

$$F = (0.9) (F_d)$$

$$= 3.114E5 \text{ GPM}$$

Flow rate monitor setpoints for the Steam Generator Blowdown effluent stream shall be set at the selected discharge pump rate (normally the maximum discharge pump rate) f_{ds} chosen in Step b) above.

- d) The Steam Generator Monitor setpoints are specified based on the values of $\sum C_i$, F , and f which were specified. The monitor response is

primarily to gamma radiation, therefore, the actual setpoint is based

on $\sum C_g$. The monitor setpoint in cpm which corresponds to the calculated value c is taken from the monitor calibration graph. The setpoint concentration, c , is determined as follows:

$$c \leq \sum_g C_g (B)$$

$$B = f_d / f_{os}$$

$$= \frac{3,245 \text{ GPM}}{250 \text{ GPM}}$$

$$= 13$$

If $B \geq 1$, Calculate c and determine the maximum value for the actual monitor setpoint (cpm) from the monitor calibration graph.

If $B < 1$, No release may be made. Reevaluate the alternatives presented in step b).

$$c \leq \sum_g C_g (B) = (1.42E-5 \text{ uCi/ml})(13)$$

$$= 1.85E-4 \text{ uCi/ml}$$

$c \leq$ cpm equivalent to $1.85E-4 \text{ uCi/ml}$

- Reading from Figure 2.1-1 yields:

$$C \leq 105 \text{ cpm}$$

- e) The Turbine Building Sump and Condensate Demineralizer Backwash monitor setpoints are established independently of each other and without crediting dilution. They are based on the measured radionuclide concentrations of the effluent stream and are to ensure compliance with the limits of 10CFR 20, Appendix B, Table II, Column 2 prior to discharge.

For each effluent stream, a concentration factor CF must be calculated, measuring the nearness of approach of the undiluted

waste stream to the specified limiting condition of the Maximum Permissible Concentration. That is,

$$CF = \left[\sum_i \frac{C_i}{MPC_i} \right] + SF$$

If $CF \leq 1$, calculate c and determine the actual monitor setpoint (cpm) from the calibration curve.

If $CF > 1$, no release may be made via this path. The release must either be delayed or diverted for additional processing. Because of spurious alarms, these remedial steps may be required if the monitor setpoints are only near the actual concentrations being released.

- f) Within the limits of the conditions stated above, the specific monitor setpoints (in uCi/ml) for the two Steam Generator Blowdown monitors RM-L3 and RM-L10 and the setpoints for RM-L8 and RM-L11 are now calculated. Because they are primarily sensitive to gamma radiation, their setpoints will be based on the concentrations of gamma emitting radionuclides as follows:

For RM-L3, Steam Generator Blowdown Discharge initial monitor, and for RM-L10, Steam Generator Blowdown Discharge final monitor:

$$c_{Sa} \text{ or } c_{Sb} \leq \left[\sum_g C_g \right]_S (B)$$

For RM-L8, Turbine Building Sump Discharge Monitor:

$$c_T \leq \left[\sum_g C_g \right]_T + CF_T$$

For RM-L11, Condensate Demineralizer Backwash Discharge Monitor:

$$c_D \leq \left[\sum_g C_g \right]_D + CF_D$$

2) Dose Calculation

The dose contribution from all radionuclides identified in liquid effluents released to unrestricted areas is calculated using the expression*:

$$D_i = \sum_i \left[A_{it} \sum_{k=1} \Delta t_k C_{ik} F_k \right]$$

where:

$$F_k = \frac{f_{ds}}{(F_d)(1)} = \frac{2500 \text{ gpm}}{3.46E5 \text{ gpm}} = 7.2E-4$$

$$= \sum_i \left[(8.96)(2.5)(3.7E-2)(7.2E-4) + (486)(2.5)(1.04E-5)(7.2E-4) + (89.7)(2.5)(6.14E-7)(7.2E-4) + (589,000)(2.5)(1.47E-6)(7.2E-4) + (348,000)(2.5)(1.73E-6)(7.2E-4) \right]$$

$$= 3.25E-4 \text{ mRem (to the Whole Body)}$$

*Dose calculation example was done only for Whole Body, Bone, Liver, Thyroid, Kidney, Lung and GI-LLI also must be done to address all dose receptors.

C. RM-A3 and RM-A4

Given:

$$\begin{aligned} X/Q &= 5.3E-6 \text{ sec/m}^3 \\ F_v &= 481 \text{ cc/sec} \\ \Delta t_k &= 0.6 \text{ hr} \end{aligned}$$

Nuclide Concentrations:

$$\begin{aligned} \text{Kr-85m} &= 1.1E-6 \text{ uCi/ml} \\ \text{Kr-88} &= 3.5E-7 \text{ uCi/ml} \\ \text{Xe-131m} &= 3.9E-6 \text{ uCi/ml} \\ \text{Xe-133} &= 8.5E-4 \text{ uCi/ml} \\ \text{Xe-133m} &= 1.2E-5 \text{ uCi/ml} \\ \text{Xe-135} &= 5.1E-5 \text{ uCi/ml} \\ \text{I-131} &= 6.73E-8 \text{ uCi/ml} \end{aligned}$$

$$(0.6 \text{ hr})(3600 \text{ sec/hr})(481 \text{ cc/sec}) = 1.04E6 \text{ cc}$$

$$C_v = 3.5E4 \text{ cpm (summed Noble Gas concentrations, used Example Noble Gas Calibration Curve, Figure 3.1-1).}$$

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1) Monitor Setpoint Calculations

The method outlined in section 3.1.2 by which the Station Vent Noble Gas Monitor setpoints are calculated is as follows:

- a) Determine the count rate per mrem/yr to the total body (R_t)

$$\begin{aligned}
 R_t &= C_v / \left[(X/Q) (F_v) \left(\sum_i K_i X_{iw} \right) \right] \\
 &= 3.5E4 \text{ cpm} / \left[(5.3E-6 \frac{\text{sec}}{\text{m}^3})(481 \frac{\text{cc}}{\text{sec}}) \{ (1.17E3)(1.1E-6) + (1.47E4)(3.5E-7) \right. \\
 &\quad \left. + (9.15E1)(3.9E-6) + (2.94E2)(8.5E-4) + (2.51E2)(1.2E-5) + (1.81E3)(5.1E-5) \} \right] \\
 &= 3.5E4 / (5.3E-6)(481)(0.352) \\
 &= 3.9E7 \text{ cpm} / \text{mRem/yr}
 \end{aligned}$$

- b) Determine the count rate per mrem/yr to the skin (R_s)

$$\begin{aligned}
 R_s &= C_v / \left[(X/Q) (F_v) \left(\sum_i (L_i + 1.1 M_i) X_{iw} \right) \right] \\
 &= 3.5E4 / \left[(5.3E-6)(481) \{ (2.8E3)(1.1E-6) + (1.9E4)(3.5E-7) + (648) \right. \\
 &\quad \left. (3.9E-6) + (3.9E2)(8.5E-4) + (1.4E3)(1.2E-5) + (4E3)(5.1E-5) \} \right] \\
 &= 3.5E4 / (5.3E-6)(481)(0.566) \\
 &= 2.4E7 \text{ cpm} / \text{mRem/yr}
 \end{aligned}$$

- c) Determine the count rate at the alarm setpoint level. This will be less than or equal to the lesser of:

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$(0.25)(R_t)(500 \text{ mrem/yr})$, or

$(0.25)(R_s)(3000 \text{ mrem/yr})$

$(0.25)(3.9E7)(500) = 4.9E9 \text{ cpm}$

$(0.25)(2.4E7)(3000) = 1.8E10 \text{ cpm}$

so use $4.9E9 \text{ cpm}$

d) If two simultaneous releases out of the main plant vent should occur, calculate the setpoint for each type of release and use highest setpoint obtained.

2) Dose Calculation

a) Unrestricted Area Boundary Dose Rate (Section 3.2.2)

$$D_t = X/Q \sum_i K_i Q_i \text{ (mrem/yr)}$$

$$= 5.3E-6 \sum_i (1.2E3)(481)(1.1E-6) + (1.5E4)(481)(3.5E-7)$$

$$+ (9.2E1)(481)(3.9E-6) + (2.9E2)(481)(8.5E-4) + (2.5E2)(481)$$

$$(1.2E-5) + (1.8E3)(481)(5.1E-5)$$

= $9E-4 \text{ mRem/yr}$ to total body.

$$D_s = X/Q \sum_i (L_i + 1.1 M_i)(Q)D_t = X/Q \sum_i K_i Q_i \text{ (mrem/yr)}$$

$$= 5.3E-6 \sum_i [1460 + (1.1)(1.2E3)](481)(1.1E-6) + [2370 + (1.1)(1.5E4)]$$

$$(481)(3.5E-7) + [476 + (1.1)(1.5E2)](481)(3.9E-6) + [306 + (1.1)$$

$$(3.5E2)](481)(8.5E-4) + [994 + (1.1)(3.3E2)](481)(1.2E-5) +$$

$$[1860 + (1.1)(1.9E3)](481)(5.1E-5)$$

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= 2.1E-3 mRem/yr to skin.

$$D_o = \sum_i X/Q P_i Q_i$$

$$= (5.3E-6) (1.624E+7) (6.73E-8) (481)$$

$$= 2.8E-3 \text{ mrem/yr (Organ Dose Rate)}$$

b) Unrestricted Area Dose to Individual (Section 3.2.3)

$$D_\gamma = 3.17E-8 \sum_i M_i X/Q Q_i$$

$$= 3.17E-8 \sum_i [(1.2E3)(5.3E-6)(1.1E-6)(1.04E6) + (1.5E4)(5.3E-6)(3.5E-7)$$

$$(1.04E6) + (1.5E2)(5.3E-6)(3.9E-6)(1.04E6) + (353)(5.3E-6)(8.5E-4)(1.04E6)$$

$$+ (327)(5.3E-6)(1.2E-5)(1.04E6) + (1.9E3)(5.3E-6)(5.1E-5)(1.04E6)]$$

$$= 5.6E-8 \text{ mrad } \gamma \text{ air dose.}$$

$$D_\beta = 3.17E-8 \sum_i N_i X/Q Q_i$$

$$= 3.17E-8 \sum_i [(2.0E3)(5.3E-6)(1.1E-6)(1.04E6) + (2.9E3)(5.3E-6)(3.5E-7)$$

$$(1.04E6) + (1.1E3)(5.3E-6)(3.9E-6)(1.04E6) + (1.1E3)(5.3E-6)(8.5E-4)(1.04E6)$$

$$+ (1.5E3)(5.3E-6)(1.2E-5)(1.04E6) + (2.5E3)(5.3E-6)(5.1E-5)(1.04E6)]$$

$$= 1.82E-7 \text{ mrad } \beta \text{ air dose.}$$

$$D_p = 3.17E-8 \sum_i R_{ij} W_{ij} Q_i$$

$$= 3.17E-8 \sum_j [(1.624E7)(2.2E-6)(6.73E-8)(1.04E6) + (2.089E7)(1.2E-8)$$

$$(6.73E-8)(1.04E6) + (4.754E10)(1.2E-8)(6.73E-8)(1.04E6)$$

= 1.35E-6 mrem individual dose due to radioiodines and radionuclides in particulate form with $t_{1/2} > 8$ days.

D. RM-A10

Given: $X/Q = 5.3E-6 \text{ sec/m}^3$
 $\text{Kr-89} = 1E-5 \text{ uCi/ml}$

1) Monitor Setpoint Calculation

Permissible release conditions for the Waste Gas System are defined in terms of both radionuclide concentration and waste gas flow rate (using previous nuclide concentrations).

a) The maximum permissible flow rate is set on the same basis but include the engineering safety factor of 0.5. The RM-A10 setpoint level S_d is defined as:

$$S_d \leq 1.5c$$

b) The maximum permissible waste gas flow rate f_w (cc/sec) is calculated from the maximum permissible dose rates at the site boundary according to:

$$f_w \leq \text{the lesser of } f_t \text{ or } f_s$$

f_t = the maximum permissible discharge rate based on total body dose rate.

$$\begin{aligned} &= \frac{0.25 \times 500 \text{ mrem/yr}}{(X/Q)(1.5) \sum_i (X_{id})(K_i)} \\ &= (0.25)(500) / 5.3E-6(1.5((1E-5)(1.66E4)) \\ &= 9.47E7 \text{ cc/sec} \end{aligned}$$

f_s = the maximum permissible discharge rate based on skin dose rate.

$$= \frac{0.25 \times 3000 \text{ mrem/yr}}{(X/Q)(1.5) \sum_i X_{id} (L_i + 1.1 M_i)}$$

$$= (.25)(3000) / [(5.3E-6) (1.5) ((1E-5) (1.01E4 + 1.1 (1.73E4)))]$$

$$= 3.24E8 \text{ cc/sec}$$

so $f_w \leq 9.47E7 \text{ cc/sec}$

- c) When a discharge is to be conducted, valve HCV-014 is to be opened until:
- (a) the waste gas discharge flow rate reaches $(0.9) (f_w)$ or
 - (b) the count rate of the plant vent noble gas monitor RM-A3 approaches its setpoint, whichever is reached first.

E. Alternative Methodology for Establishing Conservative Setpoints (using previous nuclide concentrations)

A more conservative setpoint is calculated to minimize requirements for adjustment of the monitor as follows:

1. For a plant vent:

R'_t = conservative count rate per mrem/yr to the total body (Xe-133 detection, Kr-89 dose).

$$= C'_v \div [(X/Q) (K_{Kr-89}) (X'_v) (F_v)],$$

Note: C'_v is based on the given Kr-89 concentration being applied to the Example Noble Gas Monitor Calibration Curve, Figure 3.1-1.

$$= 3.3E4 \text{ cpm} / [(5.3E-6)(16,600)(8.5E-4)(481)]$$

$$= 9.2E5 \text{ cpm}$$

R'_s = count rate per mrem/yr to the skin.

$$\begin{aligned}
&= C_v' \div [(X/Q) ((L_{Kr-89} + 1.1M_{Kr-89})) (X_v') (F_v)] \\
&= 3.3E4 \text{ cpm} / [(5.3E-6)(29,130)(8.5E-4)(481)] \\
&= 5.2E5 \text{ cpm}
\end{aligned}$$

2. For the waste gas decay system:

$$\begin{aligned}
f_t' &= \text{the conservative maximum permissible discharge rate} \\
&\quad \text{based on Kr-89 total body dose rate.} \\
&= (0.25) (D_{TB}) \div [(X/Q) (1.5) (X_d') (K_{Kr-89})] \\
&= (0.25)(500) / (5.3E-6)(1.5)(9.18E-4)(1.7E4) \\
&= 1.01E6 \text{ cc/sec}
\end{aligned}$$

$$\begin{aligned}
f_s' &= \text{the conservative maximum permissible discharge rate} \\
&\quad \text{based on Kr-89 skin dose rate.} \\
&= (0.25) (D_{SS}) \div [(X/Q) (1.5) (X_d') (L_{Kr-89} + 1.1M_{Kr-89})] \\
&= (0.25)(3000) / (5.3E-6)(1.5)(9.18E-4)(2.9E4) \\
&= 3.54E6 \text{ cc/sec}
\end{aligned}$$