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Robert L. Mittl General Manager Nuclear Assurance and Regulation

November 2, 1984

Director of Nuclear Reactor Regulation U.S. Nuclear Regulatory Commission 7920 Norfolk Avenue Bethesda, MD 20814

Attention: Mr. Albert Schwencer, Chief

Licensing Branch 2 Division of Licensing

Gentlemen:

HOPE CREEK GENERATING STATION DOCKET NO. 50-354 REVISED FSAR QUESTION RESPONSES

Attachment I contains the revised responses to FSAR Ouestion 410.69 and 430.88. In addition, attached to 430.88 is one copy of "Summary of Reduced Standby Diesel Generator Loading to accommodate a standing hurricane after a Loss of Offsite Power." These question responses were revised per discussions held with the auxiliary system and power system branches respectively.

A signed original of the required affidavit is provided to document the submittal of these items.

Should you have any questions or require any additional information on these items, please contact us.

Attachment II contains a copy of revised FSAR question 430.81 originally submitted on October 18, 1984.

Very truly yours,

8411070092 841102 PDR ADDCK 05000354 A PDR

Attachments/Enclosure

C D. H. Wagner USNRC Licensing Project Manager (w/attach.)

W. E. Bateman
USNRC Senior Resident Inspector (w/attach.)
The Energy People

300/

ADD. A. UNGARO, PSB

UNITED STATES OF AMERICA NUCLEAR REGULATORY COMMISSION DOCKET NO. 50-354

#### PUBLIC SERVICE ELECTRIC AND GAS COMPANY

Public Service Electric and Gas Company hereby submits the enclosed responses to FSAR Questions for the Hope Creek Generating Station.

The matters set forth in this submittal are true to the best of my knowledge, information, and belief.

Respectfully submitted,

Public Service Electric and Gas Company

By

Vice President -

Engineering and Construction

Sworn to and subscribed before me, a Notary Public of New Jersey, this 200 day of November 1984.

DAVID K. BURD

NOTARY PUBLIC OF NEW JERSEY

My Comm. Expires 10-23-85

ATTACHMENT I

10/84

# QUESTION 410.69 (SECTION 9.2.1)

Provide a figure(s) in the FSAR which shows the protection of the station service water system from the flood water (including wave effects) of the design basis flood.

### RESPONSE

The general arrangement of the intake structure is provided in Figures 1.2-40 and 1.2-41. Section AA of Figure 1.2-41 is reproduced here as Figure 410.69-1 which identifies the watertight areas and the walls and slabs designed to accommodate flood loads. As described in Sections 2.4.2 and 2.4.5, the south and west exterior walls of the intake structure are subject to a maximum wave run-up elevation of 134.4 feet due to the probable maximum hurricane (PMH). Such waves could overtop the roof of the western portion of the structure at elevation 128 feet. However, a rigorous analysis has been performed to determine the depth of water in the low area (elevation 122.0 feet) after wave impact and to confirm that water does not enter the building through the air intake control dampers (bottom elevation 128.5 feet). Therefore, flood water will not enter into the dry area of the intake structure. On the north side of the intake structure, the maximum water level will be only slightly higher than the still water elevation (113.8 feet) during the PMH. According to Table 2.4.6, the maximum wave elevation for the north side of the intake structure is 26.3 feet MSL (elevation 115.3 feet) due to a postulated multiple dam break. Therefore, flood protection of the north exterior wall to elevation 121.0 feet is adequate.

On the east side of the intake structure, the maximum wave run-up elevation due to the PMH equals 121.97 feet. This elevation is due to a 1% wave traveling in the direction of Fetch "A". Fetch A, which is rotated about 15 degrees from Fetch 1 (as shown in Figures 410.69-2 and 410.69-3), is chosen to maximize the wave run-up elevation. Since this elevation is lower than the bottom of the HVAC exhaust opening, flood water will not enter the intake structure from the east side of the building.

In addition the following assessments have been made to confirm the adequacy of the structure and interior components for the overtopping wave:

- a. The exterior walls are designed to withstand the flood loads including the dynamic wave action effects.
- b. The roof hatches at both elevations 122.0 and 128.0 feet have been sealed (caulking, gaskets, etc.) to prevent any intrusion of water. The hatch covers are

keyed into the openings to prevent any adverse slippage due to wave induced loadings.

c. All Seismic Category I components except for the traveling water screens are located within the dry areas of the structure.

ed. The traveling water-screens, located in the "wet" area between column lines B and C have electric motors which are fully protected against the flood water level.

A condition was postulated where suspended moisture enters the dry areas of the structure through the air intake control dampers. It has been assessed that all of the Seismic Category I components subjected to this environment will continue to function as required.

Section 3.4.1 and Table 3.4-1 have been revised for clarification.

# Insert

d. The foundation for the service water

pumps are designed to accommodate The

wave forces acting on the structure.

Therefore no leakage will occur through

the pump foundations.

Rev. 3

## BCGS PSAR

# OUESTION 430.88 (SECTION 9.9.4)

Provide additional justification to support your statement in Section 9.5.4.3 that sufficient additional fuel can be delivered to the plant site by truck, or barge. In your discussion include sources where diesel quality fuel oil is available and distances travelled from the source to the plant. Also discuss how fuel oil will be delivered onsite under extremely unfavorable environmental conditions. (SRP 9.5.4, Part I)

# ESPURSE

Standby diesel generator fuel oil storage tank fill connections are discussed in Section 9.5.4.2.6. The total capacity of the SDG fuel oil stocage tanks and day tanks is sufficient for seven days of SDG operation at the rated full load indicated in Section 8.3 for a DEA and LOP. Thin this period, additional fuel can be delivered to the plant site by truck or barge. The supply depot is located about 44 miles from the plant in Pensauken h.J. Under extremely unfavorable environmental conditions, deliveries would be made by truck.

(INSERT A')

# INSERT . TO 430.00

Site flooding (i.e. flooding above plant grade elevation) is a highly unlikely event. The highest historical high water was 97.5 feet (PS Datum), recorded November 1950, 4 feet below plant grade. As an estuarine, site flooding is primarily a result of the effects of tide combined with primarily a result of the effects of tide combined with severe storms. The tidal cycle being approximately 12 hours in duration would reasonably be expected to contribute to in duration would reasonably be expected to contribute to site or local flooding for only a few hours. This would afford the opportunity to refuel the fuel oil storage thanks within a few hours of any scheduled refueling.

Severe site flooding to the design flood level is due to the PME as defined in Regulatory Guide 1.59. Precise track position and forward speed (27 knots) as well as other assumptions are necessary to develop the flood levels calculated for the design basis event. A description of the analysis is presented in Section 2.4.5. A forward speed of 27 knots would cause the hurricane to move over 300 miles past the site in 10 hours. The maximum winds are assumed to extend 39 nautical miles. The forward travel speed is a critical parameter in the calculation, as this is what causes the large volume of water to be first forced into the Delaware and then carried up the estuary past the site. Even in the event that the storm should stall, flood water will tend to drain out the bay as the forcing function is no longer available to push water into the bay. There would also be a further reduction of flood waters due to the tidal change. It would be unrealistic as to expect site flooding to persist for more than 24 hours. Open continuous operation of the bisses general for any 2 day periods and fort oll stilment sist be delivered.

BSC: TW

MP84 112 07 1-90

# Question 430.88 con't

While extremely adverse wind, weather and tidal conditions at the Bope Creek Site could interfere with diesel oil delivery for approximately 24-36 hours, it would be a very improbable situation that would preclude delivery by all of the possible evenues truck or balgate that would preclude delivery by all of the possible evenues truck or balgate that would preclude delivery by all of the possible evenues truck or balgate.

There are three key factors which support this conclusion. First, while any storm can remain stationary for an extended period, one in an adverse position (onshore) will lose its energy source and be eroded by surface friction. Secondly, any storm remaining offshore where it can retain all or some of its energy source will be in a position either to cause unusually low tides following the initial surge, or at least to provide shelter from the maximum the initial surge, or at least to provide shelter from the maximum winds because of the long fetch over the lower Jersey peninsula. Winds because of the long fetch over the lower Jersey peninsula. Thirdly, the storm surge capable of seriously flooding the area is Thirdly, the storm surge capable of seriously flooding the area is condition for prolonged periods (24-36 hours) even if the driving force continues.

The following is a brief description of three storm variations:

- A. Burricane stationary in the least favorable position (see

  Figure 430.88-1)

  A hurricane in this position is largely out off from oceanic moisture and it is subject to frictional erosion of its wind speeds. It will decay into a wet, showery situation with modest wind speeds within 12-24 hours.
- B. Hurricane stationary off the coast (see Figure 430.88-2)

  A hurricane anywhere off the coast would continue to receive a substantial portion of its energy and it would not be affected by friction of the land surface. However, its location would preclude the fetch necessary to drive water directly into the preclude the flow over the peninsula would moderate the winds bay, and the flow over the peninsula would moderate the winds at the site. The initial surge should drop within 12 hours and would probably be followed by an abnormally low tide. The clouds and showers associated with the storm might last 24-36 hours.

If the PMH were to stall directly south of the Delaware Bay Inlet, westerly winds could cause high water build-up at the entrance to the bay. It would require a continuous wall of water approximately 12 feet high to maintain flooding conditions water approximately 12 feet high to maintain flooding conditions at the site. A prolonged event (24-36 hours) of this type would be highly improbable.

# Question 430.68 cont'd

# C. Extra-tropical storms

These storms are much larger than hurricanes, and at times they do remain stationary for very long periods. However, much of the above reasoning remains valid for them also. A stationary storm in the unfavorable position needed to generate strong southeasterly winds would be subject to surface friction, and it would lose much of its energy, although in a different way. The sharp contrast between the cold polar air and the tropical maritime air from which such storms are generated would gradually disappear and the air would become homogenous around the circumference of the low pressure area. Such storms weaken slowly over a period of 24-36 hours.

Storms off the coast can maintain their energy source very well, and they may remain vigorous for three or four days. Bowever, if the storm produced a major surge while reaching the vicintity of the sits. it would then generate a period of very low water. Adverse weather could last for several days, in the sense that the winds might be high and precipitation could continue, but transportation of fuel or lube oil should not be a problem.

delete Based upon provious discussions. The probable maximum filod would belete something that the probable maximum filod would belete something the providing for a donsor with the banks after providing for a donsor with the banks.

would be available

baige of truck

The normal method of fuel transport would be by tank truck.

Should any event preclude delivery by truck, the indicate a balgar remaining fuel will provide ample time to arrange an alternate a balgar delivery method.

The refill line extends to the station barge slip. There are sufficient refineries and military installations within a reasonable distance of the station to assure the credibility of there methods of delivery. Among the available privately of these methods of delivery. Among the available privately of 7500 pounds. This arrates to 918 gellons of disselfuel in of 7500 pounds. This arrates to 918 gellons of disselfuel in dieself to operate for approximately 85 minutes. Military dieself to operate for approximately 85 minutes. Military helicopters with greater lifting capacity would also be available.

Similarly, the commitment to refuel with a remaining time day fuel supply/provides ample time to clear roads of any credible snowfall or so extends an elementate delivery method. Getty, Texaco and the Sun Dil Company have refineries within a 75 mile radius of the site. I other debris that May have accumulated as a result of the Storm.

Comprehensive emergency plans are required by federal agencies ie FDMA and NRC. These plans require documentation in the form of letters of agreement and memornadum of understanding between the

# Question 430.88 cont'd

nuclear utility and state and federal governments which provide the use of resources of the various agencies involved. The availability of these resources provides additional assurance that accidents and acts of nature beyond design basis can be addressed.

The SDG fuel oil storage tanks are sized in accordance with the requirements of SRP 9.5.4 and Regulatory Guide 1.137 for a seven day supply of fuel oil to each redundant SDG following a LOCA or LOP.

Each pair of SDG fuel oil storage tanks contains sufficient fuel to operate a diesel engine for approximately seven days, six hours, based on the time dependent generator loading shown in FSAR Table 8.3-3.

During an actual shutdown under these conditions, i.e. LOP and flood, all four diesels would not be required to achieve and maintain cold shutdown. Thus, for a realistic shutdown scenario there in fact would be approximately 14 days fuel oil available for required diesel operation. See attacked glaph and summary table.

A procedure will be implemented which requires PSE&G to order a fuel shipment to top off all the diesel fuel oil tanks once the National Weather Service issues a horricane, tornado, or tropical storm alert for the artifical Island area. Lube oil would also be ordered to bring the ordsite supply to an amount required for sources days operation of the diesels.

PIGURE 430.85-1 MOPE CREEK GENERATING STATION Onshore Burricane - Wind Plows Hope Greek Site

PIGURE 430.88 . 2 MOPE CREEK GENERATING STATION Offshore Burricane - Wind Flows -Hope Creek Site

SUMMARY OF REDUCED STANDBY
DIESEL GENERATOR LOADING TO
ACCOMMODATE A STANDING HURRICANE
AFTER A LOSS OF OFFSITE POWER

On the loss of offsite power, the four standby diesel engines are started. During the period from 13 seconds after the engines start to 10 minutes, the total loading of the engines will be 8006 KW with a total fuel consumption rate of approximately 581 GPH. During the loss of offsite power, the loss of coolant loads are not actuated, such as the RHR pumps, reactor core spray pumps, RB FRVS recirculating fans, heating coils, which are major load contributors.

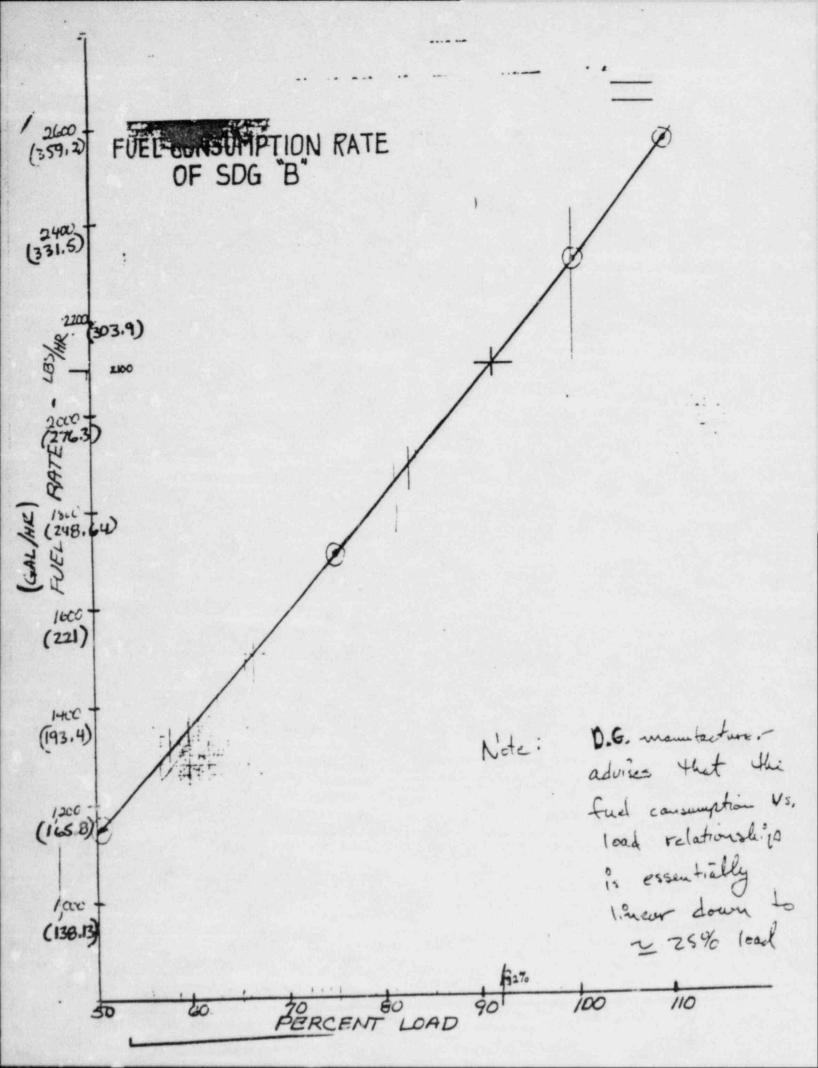
After 10 minutes to one hour, loads are adjusted to 11001 KW with a fuel consumption rate of 773 GPH.

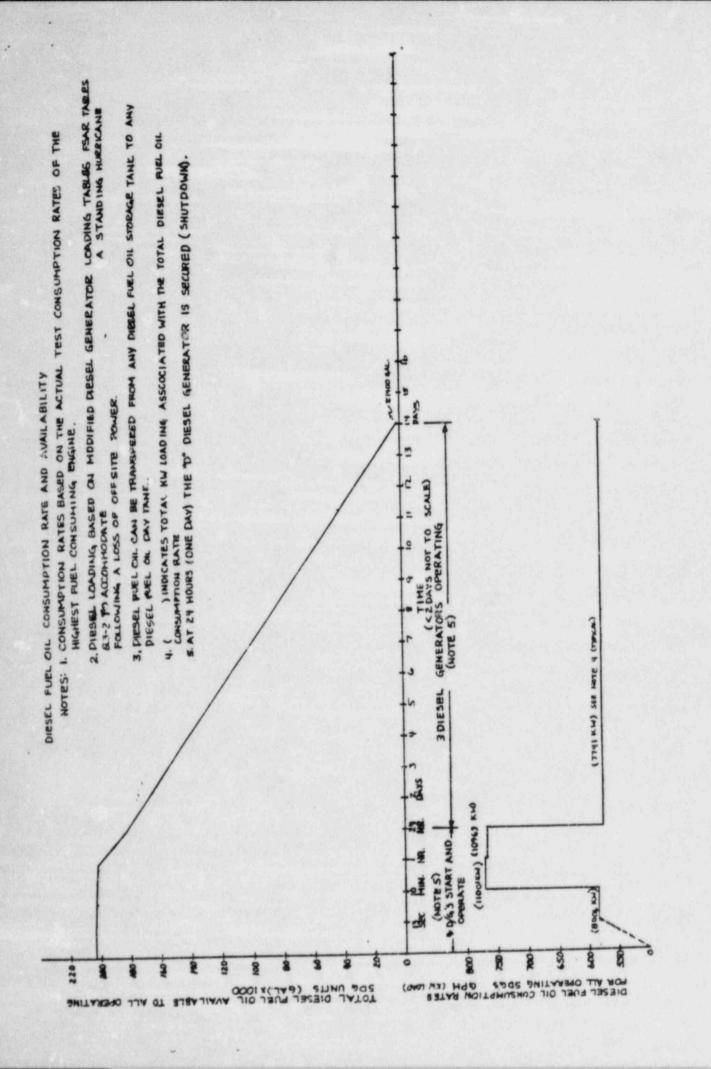
At the end of one hour to 24 hours, the load is adjusted to 10969 KW with a fuel consumption rate of 769 GPH.

After 24 hours, non essential loads will be dropped reducing the load to 7741 KW with a fuel consumption rate of 576 GPH. Additionally after 24 hours, the "D" standby diesel generator will be secured (shutdown) with its share of the load being taken up by the three operating standby diesel generators.

With the loading described above, the standby diesel generators would operate for 14 days without refueling and have a margin of 1400 gallons of fuel left in the storage tanks. This is based on the fuel oil storage tanks being filled to 100% capacity upon receipt of a hurricane, tornado, or tropical storm alert for the Artificial Island area, and the fuel oil consumption rates shown on the attached test data curve of fuel rate versus percent load for standby diesel generator "B".

Attachment





ACCOMMODATE A STANDING HURRICANE FOLLOWING A LOSS OF OFFSITE POWER.

#### TABLE 8.3-2

Page 1of 14 .

STANDBY DIESEL GENERATOR LOADING
4 STANDBY DIESEL-GENERATORS IN SERVICE
DESIGN BASIS ACCIDENT

			Standby	Diesel Ger Demand kW	nerator A		DYX.		Standby	Dissel Ger Desard kw	nerator B		RS TO
Les	Description	No. Con- nected	13 8	13 s - 10 min	10 min- 60 min	60 min	4HR	o. Con-	13 9	13 8 - 10 min	10 min 60 min	60 min	75
	Class IE Loads										-630-	430	_
1.	Reactor core spray pumps	1	10	-530-				•		-330	991	991	
2.	RRR pumps	,	-001	-001	991	991	991	1		-00+			
	Safety aux cooling system pumps	1	-	476	476	476	476	'		476	+76-	476	
	Core apray pump room unit	2	-	-12-			-	2		-12-	-12-	-12-	
	Motor-operated valves	,			-		-	1					-
5-				20	20	20	20	1		20	20	20	20
•-	Swgr rm unit cooler fans		-	32	32	32	12	1		32	32	32	22
7.	Intake structure supply fans	•					1.6						_
8.	Intake structure traveling screens area fans	•		1.6	1.6	1.6	1.0						
	RHR pump rm unit coolers fans	2		16	16	16	16	2		16	16-	16-	-
9.				100		-		2			•	•	
10.	RCIC pump rm unit coolers			12	42-	42							_
11.	MPCI pump rm unit coolers	2					62	2	62	62	62	62	62
12.	125-V dc battery chargers	2	62	62	62	62	96	•					
13.	Diesel area battery room	1	1	'	'	'		'	'				4
14.	Diesel fuel oil transfer pump	e 2		-			4	2					
15.	Station service water pumps	•	-	634	634	634	634	1		634			-
16.		2		-240-	430-	-130-	-	2		-240-	-110-	420	
17.	Control rm supply fans	-	-		E Car			-	-				

MODIFIED LOADING TABLE TO ACCOMHODATE A STANDING HURRICANE FOLLOWING A LOSS OF OFFSITE POWER.

Description

tation power supply

circulating pumps

heating coils

systems fans

gas compressor

exhaust fans

heating coils

booster pumps

return fans

fans

coolers

dist panels

208Y/120-V ac XPHRS to power

120-V ac Glass 12 instrumen-

Intake structure exhaust fans

Control room chilled water

Control room supply unit

Control room water chillers

Diesel generator room recirc

Primary containment instrument

Battery chargers, 250-V dc Control area battery room

RB PRVS recirculation unit

Traveling screen spray water

Control room supply system

Fuel pool cooling pumps

RB FRVS went unit hesting coil

Control room emergency filter

Safety aux cooling system unit

Item

No.

2

Con-

Page 20f 14 TABLE 6. 3-2 (cont) 0 Standby Diesel Generator B Standby Diesel Generator A Demand kw Demand kW No. 40 min 63 13 8 -10 min 13 8 -10 min-Arnected 60 min Sevend 34 H 10 min 13 8 nected 10 min 60 min 13 9 60 60 60 60 60 41 1 .1 81 41 41 . 1 .1 32 32 32 32 32 32 32 100 100 100 100 100 100 15 15 15 15 15 16 16

MODIFIED LOADING TABLE TO ACCOMHODATE A STANDING HURRICANE FOLLOWING A LOSS OF OFFSITE POWER.

Description

RB FRVS went mys fans

Containment hydrogen recom-

39. Control equip room supply unit

Service water self-cleaning

Standby liquid control gumps

Public address system 120-V

Security system 120-V ac power

NSSS computer 120-V ac power

NOP computer 120-V ac power

480-9 power supply to class 1E

Motor-driven diesel generator fuel oil standby pumps 50. Standby liquid control pump room dust heaters

supply fan

biner system

heating coils

ac power supply

chiller panels Traveling acreens gccs jockey pamp

strainers

eupply

supply

supply

35. Control room emergency filter unit electric heating coils Control equipment room air

Item \_

No.

Con-

Page 3of 14 TABLE 8.3-2 (cont) Standby Diesel Generator B Standby Diesel Generator A Demand kW Demand kW 60 min & Con-60 min 10 min 10 min-13 8 -60 min annected 10 min 60 min 10 min nected 13 8 24 HK. 20.5 20.5 20.5 20.5 20.5 20.5 1.5 1.5 1.5 1.5 1.5 1.5

# MODIFIED LOADING TABLE TO ACCOMMODATE A STANDING HURRICANE FOLLOWING A LOSS OF OFFSITE POWER.

heaters

heater

chillers

heaters

water pumps

Battery room exhaust fan Battery room duct heater

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TABLE 8.3-2 (cont) Page 4of 14 Standby Diesel Generator A Standby Diesel Generator B Demand kw Demand kw 60 min 5 Con-No. 13 8 -10 min-Con-10 min 60 min Description nected 13 8 10 min 13 8 10 min 60 min ZN HE 51. 480-V power supply to hydrogen and oxygen analyzer panels 250-V do battery toom duct 125-V dc diesel area battery room duct heaters 50. HPCI pump room duct heater RCIC pump room duct heaters 250-V dc battery room duct 198 57. Class 1E panel room water 198 198 58. Class 18 panel room chilled 32 32 32 32 59. Class 1E panel room supply 5 40 60 60 return air fans 60. Class 1E panel room electric

MODIFIED LOADING TABLE TO ACCOMMODATE A STANDING HURRICANE FOLLOWING A LOSS

TABLE 8.3-2 (cont)

Page 5of 16

OF	ERICANE FOLLOWING A LO OFFSITE POWER.		standby	Diesel Ger Demand kw	nerator A		8 % 5		Standby	Diesel Ger Demand kw	merator B		AVS TO
<u>Itea</u>	Description	No- Con- nected	13_s	13 s - 10 min	10 min- 60 min	60 min 8	A PA	on-	13 0	13 s - 10 min	10 min 60 min	Sevend Sevend	24 HR
	Non-Class 1E Loads										32	32	12
71.	Turbine-generator turning gear oil pump						7	•					
72.	Standby liquid control solution operating heater	1		•	-10-	-10-		1					-
73.	Drywell cooling unit fans	8	3-2	32	32	22	32	8	32	80	31	3-2. 80	32
74.	Radwaste exhaust fans	1	•	- 1	80	80	80	1			76	76	76
75.	Essential plant lighting	1			61	61	61	1					_
76.	CRD water pumps	1- 3	•				-						_
17.	Turbine building battery room exhaust fans	'			3.4	3.4	-	'					
78.	Turbine generator aux Bearing lift pump Total 9 - 5 hp each Turning gear - 60 hp					-	-	1			•	*	84
79.	Emergency instrument air compressor	1	•				-						
80.	Radwaste supply fans	-	-	-			-	1					
81.	Reactor building supply air handling units	,			150	12.0	120					160	160
82.	Reactor building exhaust fans	1		-	160	160	160	1		160	160	100	100
83.	Radwaste tank went filter fan	. 1		-	6	6	6	1					
84.	Turbine building battery room supply fans	1			3.3	-312-		'					
85.	Radwaste tank went filter heating coils	1				3.6-	_	'					
86.		1				12	17	2 1	-				-

	WIFIED -	TO		TABLE 8	.3-2 (cont	1)				Page 60	£ 14		•
H	PERICANE FOLLOWING A L	oss	Standby	Diesel Ge	nerator A		6.		Standby	Diesel Ge Demand kw	nerator B		t s
Item	Description	No. Con- nected	13_6	13 s - 10 min	10 min- 60 min	60 min	24 HRS	No. Con- nected	12_8	13 s - 10 min	10 min 60 min	60 min	24 HRS 7 DAYS
67.	Diesel generator starting air compressors	•			-12-	42	-	1			-12-	-11	-
88.	Reactor aux cooling system pumps	1		120	120	120	120	1		120	120	-	_
89.	125-V dc battery chargers	2	1 - Lee	+ 1	102	102	102	2	-		102	102	102
90.	125-V dc battery chargers	1	-	-	31	31	31	1			31	31	31
91.	250-V dc battery chargers			- 1			-	1			51	51	51
92.	Standby liquid control sol mixing heater		-	-	-	-	-	-	-		•	1	-
93.	RPPT auxiliaries Lube oil pump	1	-		21.2	21.2	21.	21		-	21.2	21.2	21.2
	Turning gear motor												
94.	Miscellaneous instrumentation 120-V ac power supply	•			41	41	41	•			41	•1	41
95.	208-V/240-V ac XFMRS to dist panels	2			24	24	24	1		•	12	12	12
96.	Reactor building floor drain sump pumps						-	•	•				-
97.	Drywell equip drain sump pump	a 1				-	_	1					-
98.	Drywell floor drain sump pump	1				•	-	1					
99.	Power supply for unit went radiation monitoring systems	,			3.5	3.5	1.5	•			3.5	3.5	3.5
100	. Power supply for DLD - radiation monitoring systems	-			-		-						
101	. Turbine-generator main seal oil pump						-	1			16	16	16
102	t. Turbine-generator recirc seal oil pump						-	1	15.7		•	•	6

# MODIFIED LOADING TABLE TO ACCOMMODATE A STANDING HURRICANE FOLLOWING A LOSS

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HURRICANE FOLLOWING A	LOSS		TABLE 8.	3-2 (cont	.)	_			Page 7o	£ 14		2.
OF OFFSITE POWER.						ST S		Standby	Diesel Ger Demand kw	nerator B		7 27
Description	No. Con- nected	13 8	13 s - 10 min	10 min- 60 min	60 min	24 HE	No. Con- nected	13_0	13 s - 10 min	10 min 60 min	60 min 1	24 H
Turbine-generator seal oil vacuum pump						-	•			1.5	1.5	1.5
Radwaste ±24-V dc battery room duct heater	1		-		-	-	•	•			-	-
Condensate storage tank heat tracing	1		-	-	-	-	-	•		•	•	-
TSC supply system fan		-	-	-	-	-	-		-	•		-
TSC supply system heating coil		-	-	-	-	-	-		-			-
TSC emergency filter fan	-	-	-		-	-	-					-
TSC emergency filter htg coil		-				-	-	-	-	b •		-
Steam tunnel unit cooler		-	-	-		-	1	-	•	•		-
Turbine building battery room supply fan & htg coil	,	•		-90-	-00-	-	•				( -	-
Turbine building compartment exhaust fan	'					-	1					
Control area 125-V dc battery room duct heater	1			-18	48-	-	•			•	•	-
Remote shutdown panel room supply fan	1					-			•		-	-
Remote shutdown panel room heating coil	•					-					10	-
	1261		4042	.3749	2024			4000-	-3500-	-4737-	-1741-	
	1241				0034	2.0					1/05 3	11.30
		242	19976	3626.3	37023	36	4.5	242	1937	2711.2	2635.12	
	Description  Turbine-generator seal oil vacuum pump  Radwaste 124-V dc battery room duct heater  Condensate storage tank heat tracing  TSC supply system fan  TSC supply system heating coil  TSC emergency filter fan  TSC emergency filter htg coil  Steam tunnel unit cooler  Turbine building battery room supply fan 8 htg coil  Turbine building compartment exhaust fan  Control area 125-V dc battery room duct heater  Remote shutdown panel room supply fan  Remote shutdown panel room	Pescription  Description  No. Connected  Turbine-generator seal oil vacuum pump  Radwaste ±24-V dc battery room 1 duct heater  Condensate storage tank heat 1 tracing  TSC supply system fan  TSC supply system heating coil  TSC emergency filter fan  TSC emergency filter btg coil Steam tunnel unit cooler  Turbine building battery room 1 supply fan & htg coil  Turbine building compartment 1 exhaust fan  Control area 125-V dc battery room duct heater  Remote shutdown panel room 1 supply fan Remote shutdown panel room 1 heating coil	HURRICANE FOLLOWING A LOSS  OF OFFSITE POWER.  Standby D  No. Con- nected 13 s  Turbine-generator seal oil vacuum pump  Radwaste 228-V dc battery room 1 duct heater  Condensate storage tank heat 1	HURRICANE FOLLOWING A LOSS  OF OFFSITE POWER.  Standby Diesel Ger Demand kW  No. Con- nected 13 s 10 min  Turbine-generator seal oil vacuum pump  Radwaste ±28-V dc battery room 1	HUZRICANE FOLLOWING A LOSS  TABLE 8.3-2 (cont of persiste following a loss of persiste following and the persistent of persistent following and the persistent fo	HUERICANE FOLLOWING A LOSS  OF OFFSITE POWER.  Standby Diesel Generator A  No. Con- pected 13 s 10 min 60 m	HUERICANE FOLLOWING A LOSS  TABLE 8.3-2 (cont)  OF OFFSITE POWER.  Standby Diesel Generator A  Demand kW  No.  Con-  Con-  Description  Turbine-generator seal oil  Vacuus pump  Radwaste \$24-V dc battery room 1  duct heater  Condensate storage tank beat 1  TSC supply system fan  TSC supply system heating coil  TSC emergency filter fan  TSC emergency filter btg coil  Steam tunnel unit cooler  Turbine building battery room 1  Turbine building compartment 1  Control area 125-V dc battery 1  Control area 125-V dc battery 1  Remote shutdown panel room 1  1241 - 4042 3748 3834-	HUERICANE FOLLOWING A LOSS  TABLE 8.3-2 (cont)  Description  No.  Con-  pescription  No.  Con- nected 13 s 10 min 60 min 8 wand 7 lonected 13 s 10 min 60 min 6	TABLE 8.3-2 (cont)  OF OFFSITE POWEE.  Standby Diesel Generator A Demand kW  No. Con- nected 13 s 10 min 60 min 50	HURRICANE FOLLOWING A LOSS  Standby Diesel Generator A Demand tw  No. Con- nected 13 s 10 min 60 min	### Page 701 14    Page 701 14	HUERICANE FOLLOWING A LOSS  Standby Diesel Generator A Demand HY  No.  Con- pescription  No.  Con- pescription  Turbine-generator seal oil  Yacuus pump  Radwaste 22e-V dc battery room 1  TSC supply system heating coil  TSC supply fant his cooler  Turbine building battery room 1  Turbine building compartment 1  Turbine building compartment 1  Turbine building compartment 1  Remote shutdown panel room 1

MODIFIED LOADING TABLE TO Page 8of 14 TABLE 8.3-2 (cont) ACCOMHODATE A STANDING HURRICANE FOLLOWING A LOSS Standby Diesel Generator D Standby Diesel Generator C Demand kw OF OFFSITE POWER. Demand kw No. 60 min & D Con-10 min 60 min & 10 min-13 8 -Con-Poyend-NT Boyond Nrnected 10 min 60 min 13 8 10 min 60 min nected 13 8 Description Item \_ BH PS ZHHR Class IE Loads 570 Reactor core spray pumps RHR pumps 476 476 476 476 476 476 3. Safety aux cooling system -64-2 Core spray pump room unit coolers Motor-operated valves 5. 20 20 20 20 20 Swgr rm unit cooler fans Intake structure supply fans Intake structure traveling screens area fans RHR pump ra unit coolers fans 2 RCIC pump rm unit coolers HPCI pump rm unit coolers 93 93 93 3 93 93 93 93 93 93 125-V dc battery chargers 3 1 1 Diesel area battery room exhaust fans 2 Diesel fuel oil transfer 2 pumps 634 633 634 634 Station service water pumps 634 634 RB PRVS recirculation system fans 32 32 32 32 Control rm supply fans

60

60

208Y/120-V ac XFMRS to power

dist panels

60

60

60

60

60

MODIFIED LOADING TABLE TO ACCOMMODATE A STANDING HUERICANE FOLLOWING A LOSS

## TABLE 8.3-2 (cont)

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O	PERICANE FOLLOWING A L	oss		Diesel Ger Demand kW			٥.			Diesel Ger Demand ky			5 2
<u> Lten</u>	Description	No. Con- nected	13 s	13 s - 10 min	10 min- 60 min	60 min Beyond 24 HRS	Ze HRS	No. Con-	13_8	13 s - 10 sin	10 min 60 min	40 min	24 HES 7 DAYS
19.	120-V ac Class 1E instrumen- tation power supply	•	*1	41	41	41	.41	•	*1	*1	41	41	-
20.	Intake structure exhaust fans	1	-	- 1			-	1		•		•	-
21.	Control room chilled water circulating pumps	1	•	48	48	48	48	•	•		•	•	-
22.	Control room supply unit heating coils	•	- •	90	90	90	90	•			•		-
23.	Control room water chillers	1	-	506	506	506	506	1		•	-		-
24.	Diesel generator room recirc system fans	2		100	100	100	100	2	•	100	100	100	-
25.	Primary containment instrument gas compressor	1	•	•	12	12	12	1	•	•		•	-
26.	Battery chargers, 250-V dc		-	-	-	-	-	-	-	-	•		-
27.	Control area battery room exhaust fans	1		•	•	•	4	1	•				-
28.	RB PRVS recirculation unit	1	-	-100-	-100-	400	-	1	•	400-	-400	-100-	-
29.	Traveling screen spray water booster pumps	1		16	16	16	16	1		16	16	16	-
30.	RB FRVS went unit heating coil	-	-	-		-	_	•	-				-
31.	Control room supply system return fans	•	•	16	16	16	16	1	•	•	•		-
32.	Control room emergency filter fans	1	-	-20-	-24-	-20-	-	1	-		•		-
33.	Safety aux cooling system unit	t 2	-	12	12	12	12	2	-	•			-
34.	Fuel pool cooling pumps	-	-	-			-	-	-	-		•	-
35.	Control room emergency filter unit electric heating coils	1	-	-43-	++	++-	-	•					•"

ACCOMMODATE A STANDING A LOSS OF OFFSITE ROWEE.  HUERICANE FOLLOWING A LOSS OF OFFSITE ROWEE.  Control equipment room air nected nected as supply fan.  RB FRVS vent sys fans  Containment hydrogen recomment of the band of colls.  Containment hydrogen recomment of the band of the colls.  Containment hydrogen recomment of the band of the	ACCOMMODATE A STANDING, HOLE TO ACCOMMODATE A STANDING, A LOSS Stand OF OFFSITE ROWEE.  No. Cont.  Control equipment room air 1  Supply fan  RB FRVS vent sys fans  Containment hydrogen recom- biner system  Control equip room supply unit 1  Sarvice water self-cleaning 1  Sarvice system 120-V ac power 1  Sarvice computer 120-V ac power 1  Sarvice computer 120-V ac power 1  Sarvice water supply to class 1E 1  Chiller panels  Traveling screens 1  ECS Jockey pump 1  Noter-driven dissel generator 1  Fuel oil standby fumps  Fuel com duct heaters  Fuel com duct heater	ACCOMMODATE A STANDING A LOSS Standby Did OF OFFSITE ROWEL.  Control equipment room air I - nected 13 e control equipment room air I - nected 13 e control equipment room air I - nected 13 e control equip room supply unit I - neatlang colle service water self-cleaning I - neatlang colle strainers system 120-V ac power I 20-5 eupply I duild control pumps neupply Security system 120-V ac power I 20-5 eupply to Class IE I - neupply I - neutply I	ACCOMMODATE A STANDING A LOSS Standby Diversity of Control equipment room air nected 13 e control equipment room air nected 13 e control equipment room air nected 13 e control equipment room aupply unit 1 containment hydrogen racom containment hydrogen racom control equip room supply unit 1 control equipment system 120-V ac power 120-V ac p	ACCOMMODATE A STANDING A LOSS Standby Diesel OF OFFSITE POWEE.  No. Control equipment roos air 1 - 200 supply fan  Control equipment roos air 1 - 200 supply fan  RB FRVS vant sys fans  Control equip roos supply unit 1 - 189  Battainers  Standby liquid control pumps 189  Standby liquid control pumps 189  Standby liquid control pumps 189  Public address system 120-V ac power 1 20.5 20.5 supply  Sacurity system 120-V ac power 189  BOP computer 120-V ac power 189  Supply  BOP computer 120-V ac power 189  Standby liquid control pump 1 - 8  ECS jockey pump 1 - 8  ECS jockey pump 1 - 8  ECS jockey pump 1 - 1 - 1 - 8  ECS jockey pump 1 - 1 - 1 - 8  ECS jockey pump 1 - 1 - 1 - 8  ECS jockey pump 1 - 1 - 1 - 8  ECS jockey pump 1 - 1 - 1 - 8  ECS jockey pump 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	CONTRIBED TO A STANDING A LOSS Standby Dieses Generator C OF OF SITE ROWEE.  HUE RICAME FOLLOWING A LOSS Standby Dieses Generator C Control equipment room air 1 - 200 200 200 200 200 200 200 200 200 2	Control equipment room air nected 13 e 10 min 60 min 20 mi	ACCOMMODATE A STANDING, TABLE 8.3-2 (cont) HUERICANE FOLLOWING A LOSS Standby Disses Generator C  OF OFFSITE FOWLEE.  No.  Control equipment room air supply fan  RB FNUS want mys fans  Control equipment room air supply fan  RB FNUS want mys fans  Control equipment room air supply fan  RB FNUS want mys fans  Control equipment room air supply fan  RB FNUS want mys fans  Control equipment room air supply fan  RB FNUS want mys fans  Control equipment room air supply fan  Strandby liquid control pumps  Control equipment 120-V ac power  ac power supply to class 1E 1 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	Page   Page	Control equipment room sir   Control equipment   Control equipme	ACCOMMODATE A STANDING, TABLE 8.1-2 (cont.)  HUERICANE FOLLOWING, A LOSS Standby Disease Generator C  HUERICANE FOLLOWING, A LOSS Standby Disease Generator C  Control equipment room air 1 - 230 200 200 200 10 1 1 1 1 1 1 1 1 1 1 1 1
Loss Loss	No. No. Standby Standby 13 e	700		TABLE 6. 3-2 (cort)  Jiesel Generator C  Denand kW  13 s - 10 min    200 200  200 200  10 min   60 min    200.5 20.5     10 min   10 min    10 min   10 min	TABLE 8. 3-2 (cont)  Jesel Generator C  Denand KW  13 s - 10 min 60 min 10 min 60 min 741 E41 KGS  200 200 200  200 200 200	TABLE 6. 3-2 (cont)  Jiesel Generator C  Demand kW  13 s - 10 min 60 min 10 min 60 min 241Hg5  290 200 200  200 200  1 1 1  20.5 20.5 20.5  1 1 1  20.5 20.5  20.5 20.5  1 1 1  20.5 20.5  20.5 20.5  1.5 1.5 1.5	TABLE 9.3-2 (cont)  Jessel Generator C  13 a - 10 min 60 min E7 D Con- 10 min 60 min Payend 17 nected  200 200 200 200 100 1  200 200 200 200 200 1  200 200 200 200 200 1  200 2 200 2 200 2 200 2 200 5  200 2 200 2 200 2 200 2 200 5  200 2 200 2 200 2 200 2 200 2  200 2 200 2 200 2 200 2  200 2 200 2 200 2  200 2 200 2 200 2  200 2 200 2 200 2  200 2 2	TABLE 6. 3-2 (cort)  Jessel Generator C  Designed KW  13 s - 10 min 60 min 57 Mo.  14 No.  15 standby plossel  15 standby plossel  16 min 60 min 200 and 57 Mo.  17 T T T T T T T T T T T T T T T T T T T	TABLE 6. 3-2 (cort)  John Jan Go min ETA No.  13 a - 10 min 60 min ETA No.  10 min 60 min ETA No.  200 200 200 200 13 a 19 min  11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TABLE 6. 1-2 (cont)  Johnson Generator C  Johnson Generator C  Johnson Generator C  Johnson Generator D  Johnson G
	Standby 13 e 13 e 1	700		TABLE 6. 3-2 (cort)  Jiesel Generator C  Denand kW  13 s - 10 min    200 200  200 200  10 min   60 min    200.5 20.5     10 min   10 min    10 min   10 min	TABLE 8. 3-2 (cont)  Jesel Generator C  Denand KW  13 s - 10 min 60 min 10 min 60 min 741 E41 KGS  200 200 200  200 200 200	TABLE 6. 3-2 (cont)  Jiesel Generator C  Demand kW  13 s - 10 min 60 min 10 min 60 min 241Hg5  290 200 200  200 200  1 1 1  20.5 20.5 20.5  1 1 1  20.5 20.5  20.5 20.5  1 1 1  20.5 20.5  20.5 20.5  1.5 1.5 1.5	TABLE 9.3-2 (cont)  Jessel Generator C  13 a - 10 min 60 min E7 D Con- 10 min 60 min Payend 17 nected  200 200 200 200 100 1  200 200 200 200 200 1  200 200 200 200 200 1  200 2 200 2 200 2 200 2 200 5  200 2 200 2 200 2 200 2 200 5  200 2 200 2 200 2 200 2 200 2  200 2 200 2 200 2 200 2  200 2 200 2 200 2  200 2 200 2 200 2  200 2 200 2 200 2  200 2 2	TABLE 6. 3-2 (cort)  Jessel Generator C  Designed KW  13 s - 10 min 60 min 57 Mo.  14 No.  15 standby plossel  15 standby plossel  16 min 60 min 200 and 57 Mo.  17 T T T T T T T T T T T T T T T T T T T	TABLE 6. 3-2 (cort)  John Jan Go min ETA No.  13 a - 10 min 60 min ETA No.  10 min 60 min ETA No.  200 200 200 200 13 a 19 min  11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TABLE 6. 1-2 (cont)  Johnson Generator C  Johnson Generator C  Johnson Generator C  Johnson Generator D  Johnson G

MODIFIED LOADING TABLE TO ACCOMMODATE A STANDING HUERICANE FOLLOWING A LOSS

#### TABLE 8.3-2 (cont)

Page 110f 14

	OF OFFSITE POWER.		Standby	Diesel Ge Demand ke	enerator C		0 4		Standby	Diesel Ger Demand kw	nerator D		5 10
Item	Description	No. Con- nected	13_a	13 s - 10 min	10 min- 60 min	60 min	HES	No.	13 .	13 s - 10 min	10 min 60 min	60 min	ZY HES 7 DAYS
52.	250-V dc battery room duct heaters		•				-						
53.	125-V dc diesel area battery room duct heaters	- 1	-24	-31	-31	-31-	-	'	-31	-24-	-21-	31	-
54.	HPCI pump ro m duct heater	-	-	-			-	-					-
55.	RCIC pump room duct heaters				*		-	-		•		•	-
56.	250-V dc battery room duct heater						-	•	-				-
57.	Class 1E panel room water chillers		-		•		-	-					
58.	Class 1E panel room chilled water pumps	-					-						_
59.	Class 1E panel room supply & return air fans	-	-	•			-	•					-
60.	Class 1E panel room electric heaters		-				-		-		, -		-
61.	Battery room exhaust fan		-	-			-	-				•	-
62.	Battery room duct heater	1	-44	44-	-14	-44-	-	1	-44-	-14-	44-	40-	-

HUERICAME FOLIOMINICAL LOSS THEIR 8.3-2-2 (Cont.)  OF OFFSITE ROWEE.  Standby Desart Generator C	2 4	MODIFIED LOADING TABLE	52		HCGS	HCGS FSAR								
Cop   Standay Damend   Con-	(I	WERICANE FOLLOWING A L			91							1		
Passification	0	IF OFFSITE POWER.		Standby	mand		1	07					1	01
Standard lighting control and an arrange are an arranged as a standard form of the standard standard and are		Description	No.	13.6	13 s - 10 mis	10 min- 60 min	60 min	ZA HES	No. Con-	1	13 10 min	10 min 60 min	es ain	PAG T
Standay liquid control   Standay   Standay liquid control   Standay   Standay liquid control   Standay liquid   Standa		Non-Class 12 Loads					SAMES							
Standby liquid control         22         21         32         31         32         31         32         31         32         31         32         31         32         31         32         31         32         31         32         31         32         31         32         31         32         31         32         31         32         31         32         31         32         31         32         31         32         31         32         32         31         32<	-	Turbine-generator turning gear oil pump						1				•		ı
Derival Cooling unit fans   11	72.	Standby liquid control	,	•	•			1		•				1
Radwaste axhaust fans Turbine building batenty room ashaust fans Turbine pusics T	-	Drywell cooling unit fans	,	7	31	7.4	32	32		32	35	77	H	1
Cab water pumpe turbling little pumpe substant tighting 1		Radwaste exhaust fans	-			8	&	8		•		•		1
CRD water pumps  Turbine building battery room  ashaust fans  Purbine-generator aux  Basing life pump  Total 9 - 5 h pech  Total 1		Essential plant lighting	-	•	•		•	1	-	4				1
Turbine bailding battery room  swhaust fans  Turbine bailding battery room  Turbine space to aux  Turbing gear - 60 hp  Total 9 - 5 hp each  Turbing gear - 60 hp  Total 9 - 5 hp each  Turbing gear - 60 hp  Tamergency instrument air  Compression  Radusste supply fans  Radusste supply fans  Radusste tank vent filter fans  Turbing bailding tattery room  Turbing colls  Radusste tank vent filter  Radusste tank vent filter  Turbing colls  Radusste fans  Radu	76.	CRD water pumps	-	•		#	-107-	1	-	٠	•			l
Turbine-generator aux  Descring lift pump  Total 9 - 54 hp each  Turning gear - 60 hp  Emergency instrument air  Compressor  Radwasta supply fans  Radwasta tank vent filter fans  Turbine building extery room  Turbine building tattery room  Radwasta tank vent filter	1.	Turbine building battery room exhaust fans	,	•	!	•		1		•				1
Emergency instrument air 80 80 80 1 - 80 80 Bodospressor Raduaste supply fans 1 80 80 80 1 80 Bodospressor Raduaste supply sir 1 - 10 10 10 1 10 10 10 10 10 10 10 10 10 10 10 10 10	±	Turbine-generator aux Bearing lift pump Total 9 - 5 hp each Turning gear - 60 hp		•				1		1	•	٠.	•	1
Reduceste supply fans  Reactor building eurply air  Radwaste tank vent filter fans  Radwaste tank vent filter  Chemical lab exhaust fans  Chemical lab exhaust fans	.62	Emergency instrument air compressor		•			•	1	,	•	•		•	1
Reactor building supply eir 1 - H20		Radwaste supply fans	-	•	•	08	80	80	-	•		8	&	1
Reactor building exhaust fans	:	Reactor building supply air bandling units	-	•	2	PZO	H20	2	-	•				1
Sadwaste tank vent filter fans		Reactor building exhaust fans	,	•				1	-					1
Supply fans Radwaste tank went filter heating coils Chemical lab exhaunt fans			1	,	•			1		•		,	•	1
Radwaste tank went filter	=		1	•	•		•	1						١
	.5			•				1						1
			,					1		•				ı

MODIFIED LOADING TABLE TO ACCOMMODATE A STANDING HUERICANE FOLLOWING A LOSS

TABLE 8.3-2 (cont)

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0	F OFFSITE POWER.		Standby	Diesel Ger Demand kw	merator C		25		Standby	Diesel Ger Demand kw	nerator D		S TO
Iten	Description	No. Con- nected	13.0	13 s - 10 min	10 min- 60 min	60 min	24 HES	No. Con- nected	13.0	13 s - 10 min	10 min 60 min	60 min	24 HES
87.	Diesel generator starting air compressors	1			-12-	-12		'			42	40	
	Reactor aux cooling system						-	•			•		-
89.	125-V dc battery chargers		+ /	1 - 9		-	-					•	-
90.	125-V dc battery chargers	1	-	-	31	31	31	1	-		31	31	_
91.	250-V &c battery chargers			+		-	-						-
92.	Standby liquid control sol mixing heater		-			•	-	'	•		10	-10	
93.	RFPT auxiliaries Lube oil pump	1			21.2	21.2	21.2					•	-
	Turning gear motor												_
94.	Miscellaneous instrumentation 120 V ac power supply	•	-		*1	•1	41	•			*1	*"	
95.	208-V/120-V ac XFMRS to dist panels	. 1	-		12	12	12	'			: 12	12	
96.	Reactor building floor drain sump pumps	2			+	-	_	2			-	+	
97.	Drywell equip drain sump pump		-				-	•					
98.	Drywell floor drain sump pump	-	-			-	-	•	•				-
99.	Power supply for unit went radiation monitoring systems						-		•				
100.	Power supply for DLD - radiation monitoring systems	,			3.5	3.5	3.5	, ,			3.5	3.5	
101	. Turbine-generator mean seal oil pump		-			•	-	-					
102	. Turbine-generator recirc seal oil pump					-	-						-

ACCOMMODATE A STANDING HUERICANE FOLLOWING A LOSS

TABLE 8.3-2 (cont)

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	OF OFFSITE POWER.		Standby D	iesel Gen emand kW	erator C		5		Standby D	iesel Ger	nerator D		25
Item	Description	No. Con- nected	13 8	13 a - 10 min	10 min- 60 min	60 min	24 HR 7 PAYS	No. Con- nected	13.4	13 e - 10 min	16 min	1116	24 H
103.	Turbine-generator seal oil vacuum pump	•					Ī						
104.	Radwaste ±24-V dc battery room duct heater	•											
105.	Condensate storage tank heat tracing	-				•	-	•					
106.	TSC supply system fan	1			20	20	20	-	-				
107.	TSC supply system heating coil	1	-		30	30	30	•	•	•			-
108.	TSC emergency filter fans		-		20	20	20	-		•			-
109.	TSC emergency filter htg coil	1			13	13	13	-					-
110.	Steam tunnel unit cooler	-	-	-	-		-	1		-	•		-
111.	Turbine building battery room supply fan 6 btg coil	. 1			•	-	-	•		•			ī
112.	Turbine building compartment exhaust fan	-					-						-
113.	Control area 125-V dc battery room duct heater						-						
114.	. Remote shutdown panel room supply fan						-	•			•		
115.	Remote shutdown panel room heating coil	-	-				-						
			261	- <del>1335</del> 2540	3199- 1103.7	2907	7 290	77.7	1376 281.5	_1531,5	_ 1700	-3585 1704	

ATTACHMENT II

## QUESTION 430.81 (SECTION 9.5.4)

In Section 9.5.4.2.1 of the FSAR you state that "The interior and exterior surfaces of the [fuel oil storage] tank are corrosion protected by carboline carbo zinc 11 coatings. I&E circular 77-15 discusses the incompatibility between diesel fuel oil and zinc. The reaction results in a substance resembling soap which when heated becomes insoluble and this substance could render diesel generators inoperable due to blocked fuel lines, injectors, etc. This is not acceptable. It is our position that fuel oil storage tanks be provided with internal corrosion protection. Therefore provide the results of tests which show that over the lifetime of the plant that the carboline carbo zinc Il coating used is compatible with the type of diesel fuel oil that will be used at your plant and that the condition described in the circular will not occur or replace the internal coating with a non-zinc base type that is compatible with diesel fuel oil. (SRP 9.5.4, Part II)

### RESPONSE

HCGS will remove the existing inorganic zinc coating from the diesel generator fuel oil tanks. The tanks will be blasted to the white metal interior of SSPC-SP5. Two coats of Americant No. 90 or equivalent will be applied to the tank interior.