

QUAD-CITIES NUCLEAR POWER STATION

UNITS 1 AND 2

MONTHLY PERFORMANCE REPORT

SEPTEMBER 1984

COMMONWEALTH EDISON COMPANY

AND

IOWA-ILLINOIS GAS & ELECTRIC COMPANY

NRC DOCKET NOS. 50-254 AND 50-265

LICENSE NOS. DPR-29 AND DPR-30

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I. INTRODUCTION

Quad-Cities Nuclear Power Station is composed of two Boiling Water Reactors, each with a Maximum Dependable Capacity of 769 MWe Net, located in Cordova, Illinois. The Station is jointly owned by Commonwealth Edison Company and Iowa-Illinois Gas & Electric Company. The Nuclear Steam Supply Systems are General Electric Company Boiling Water Reactors. The Architect/Engineer was Sargent & Lundy, Incorporated, and the primary construction contractor was United Engineers & Constructors. The Mississippi River is the condenser cooling water source. The plant is subject to license numbers DPR-29 and DPR-30, issued October 1, 1971, and March 21, 1972, respectively; pursuant to Docket Numbers 50-254 and 50-265. The date of initial Reactor criticalities for Units One and Two, respectively were October 18, 1971, and April 26, 1972. Commercial generation of power began on February 18, 1973 for Unit One and March 10, 1973 for Unit Two.

This report was compiled by Becky Brown and Dave Kimler, telephone number 309-654-2241, extensions 127 and 192.

II. SUMMARY OF OPERATING EXPERIENCE

A. UNIT ONE

September 1-30: Unit One began the month reducing load as requested by the Load Dispatcher. At 0310 hours the unit was holding load at 500 MWe. On September 7, at 0900 hours, the unit began a normal load increase to full power. On September 8, at 0040 hours, load was reduced to 700 MWe for Turbine weekly tests. At 0225 hours the unit began a normal increase to full power. On September 13, at 0100 hours, load was dropped to 700 MWe for a condensate pump changeover. At 0530 hours the unit began a normal load increase to full power. On September 14, at 1610 hours, load was dropped to 300 MWe due to Recombiner fires. At 1805 hours, the unit began a normal load increase to full power. On September 18, at 0040 hours, load was dropped to 650 MWe per the Load Dispatcher. At 0500 hours load was increased to full power. On September 21, at 0930 hours, load was dropped per the Nuclear Engineer for a special control rod maneuver. At 1600 hours the unit began a normal load increase to full power. On September 30, at 0130 hours, load was dropped to 700 MWe for weekly Turbine tests. At 0800 hours the unit began a normal load increase to full power.

B. UNIT TWO

September 1-8: Unit Two began the month at full power. On September 2, at 0045 hours, load was dropped to 700 MWe for weekly Turbine tests. At 0630 hours the unit began a normal load increase to full power. On September 3, at 0100 hours, load was dropped to 700 MWe per the Load Dispatcher. At 1950 hours load was increased to 750 MWe. At 2220 hours, load was dropped to 650 MWe to perform Turbine nightly and MSIV Bi-Weekly tests. On September 4, at 0600 hours, the unit began a normal load increase to full power. On September 6, at 0030 hours, load was dropped to 600 MWe per the Load Dispatcher. At 0210 hours, load was increased to 730 MWe. At 1045 hours tests were performed on the Economic Generation Control System. At 1545 hours the unit began a normal increase to full power. On September 7, at 1110 hours, load was dropped to 730 MWe for EGC testing. At 1620 hours the unit began a normal increase to full power. On September 8, at 2230 hours, load was dropped for weekly Turbine tests.

September 9-30: On September 9, at 0930 hours, the unit began a normal load increase to full power. On September 13, at 1352 hours, load was dropped to 759 MWe to turn off the 2B Circulating Pump. On September 14, at 1400 hours, load was dropped to minimum load, the Generator was turned off, and Turbine Overspeed Tests were performed. At 1909 hours the Generator was synchronized and at 2030 hours, the unit was at 200 MWe. At 0545 hours, on September 17, the unit began a normal load increase to full power. On September 19, at 1205 hours,

B. UNIT TWO

September 9-30: (Continued)

load was dropped 10 MWe for a problem with the HPCI 2J01-4 valve. The problem was resolved and at 1230 hours load was increased to full power. On September 23, at 2330 hours, load was dropped to 700 MWe for Turbine weekly tests. At 0330 hours the unit began a normal load increase to full power. On September 30, at 0130 hours, load was dropped to 700 MWe for weekly Turbine tests. At 0800 hours the unit began a normal load increase to full power.

III. PLANT OR PROCEDURE CHANGES, TESTS, EXPERIMENTS, AND SAFETY RELATED MAINTENANCE

A. Amendments to Facility License or Technical Specifications

There were no Amendments to the Facility License or Technical Specifications for the reporting period.

B. Facility or Procedure Changes Requiring NRC Approval

There were no Facility or Procedure changes requiring NRC approval for the reporting period.

C. Tests and Experiments Requiring NRC Approval

There were no Tests or Experiments requiring NRC approval for the reporting period.

D. Corrective Maintenance of Safety Related Equipment

The following represents a tabular summary of the major safety related maintenance performed on Unit One and Unit Two during the reporting period. This summary includes the following headings: Work Request Numbers, LER Numbers, Components, Cause of Malfunctions, Results and Effects on Safe Operation, and Action Taken to Prevent Repetition.

IV. LICENSEE EVENT REPORTS

The following is a tabular summary of all licensee event reports for Quad-Cities Units One and Two occurring during the reporting period, pursuant to the reportable occurrence reporting requirements as set forth in sections 6.6.B.1. and 6.6.B.2. of the Technical Specifications.

UNIT ONE

<u>Licensee Event Report Number</u>	<u>Date</u>	<u>Title of Occurrence</u>
84-18	9-22-84	Standby Gas Treatment
84-18A	9-24-84	Auto-Start

UNIT TWO

There were no Licensee Event Reports for Unit Two for the reporting period.

UNIT ONE MAINTENANCE SUMMARY

W. R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q34506	84-5	Weld Overlay 'J' Jet Pump Riser (02J-S3)	Unknown. Suspect IGSCC induced indications.	Leak would have been detected prior to pipe break.	The cracks were repaired and a weld overlay was performed as designed by Nutech Engineers, Inc.
Q34582	84-5	Weld Overlay 'M' Jet Pump Riser (02M-S3)	Unknown. Suspect IGSCC induced axial indications.	Indications were not 100% through-wall.	The indications were weld overlaid as designed by Nutech Engineers, Inc.
Q34645	84-5	Weld Overlay 'C' Jet Pump Riser (02C-S4)	Unknown. Suspect IGSCC induced indications.	Indications were not 100% through-wall.	The indications were weld overlaid as designed by Nutech Engineers, Inc.
Q34646	84-5	Weld Overlay 'J' Jet Pump Riser (02F-S4)	Unknown. Suspect IGSCC induced axial indications.	Indications were not 100% through-wall.	A weld overlay was performed as designed by Nutech Engineers, Inc.
Q34722	84-5	Weld Overlay 'D' Jet Pump Riser (02D-S4)	Unknown. Suspect IGSCC induced axial indications.	Indications were not 100% through-wall.	A weld overlay was performed as designed by Nutech Engineers, Inc.
Q34723	84-5	Weld Overlay 'G' Jet Pump Riser (02G-S4)	Unknown. Suspect IGSCC induced indications.	Indications were not 100% through-wall.	A weld overlay was performed as designed by Nutech Engineers, Inc.

UNIT ONE MAINTENANCE SUMMARY

W. R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q34889	84-5	Weld Overlay 'E' Jet Pump Riser (02E-S4)	Unknown. Suspect IGSCC induced indications.	Leakage would have been detected and the Unit shutdown prior to pipe break.	A weld overlay was performed as designed by Nutech Engineers, Inc.
Q34910	84-5	Weld Overlay 'B' Jet Pump Riser (02B-S10)	Unknown. Suspect IGSCC induced indications.	Leakage would have been detected and the Unit shutdown prior to pipe break.	A weld overlay was performed as designed by Nutech Engineers, Inc.
Q34947	84-5	Weld Overlay 'G' Jet Pump Riser (02G-S3)	Unknown. Suspect IGSCC induced indications.	Leakage would have been detected and the Unit shutdown prior to pipe break.	A weld overlay was performed as designed by Nutech Engineers, Inc.
Q34948	84-5	Weld Overlay 'J' Jet Pump Riser (02J-S4)	Unknown. Suspect IGSCC induced indications.	Leakage would have been detected and the Unit shutdown prior to pipe break.	A weld overlay was performed as designed by Nutech Engineers, Inc.
Q34949	84-5	Weld Overlay 'J' Jet Pump Riser (02J-F6)	Unknown. Suspect IGSCC induced axial indications.	Leakage would have been detected and the Unit shutdown prior to pipe break.	A weld overlay was performed as designed by Nutech Engineers, Inc.
Q34950	84-5	Weld Overlay 'H' Jet Pump Riser (02H-S3)	Unknown. Suspect IGSCC induced indications.	Leakage would have been detected and the Unit shutdown prior to pipe break.	A weld overlay was performed as designed by Nutech Engineers, Inc.

UNIT ONE MAINTENANCE SUMMARY

W. R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q34951	84-5	Weld Overlay 'H' Jet Pump Riser (02H-S4)	Unknown. Suspect IGSCC induced axial indications.	Leakage would have been detected and the Unit shutdown prior to pipe break.	A weld overlay was performed as designed by Nutech Engineers, Inc.
Q35048	84-5	Weld Overlay 'K' Jet Pump Riser (02K-S3)	Unknown. Suspect IGSCC induced indications.	Leakage would have been detected and the Unit shutdown prior to pipe break.	A weld overlay was performed as designed by Nutech Engineers, Inc.
Q35049	84-5	Weld Overlay 'K' Jet Pump Riser (02K-S4)	Unknown. Suspect IGSCC induced axial indications.	Leakage would have been detected and the Unit shutdown prior to pipe break.	A weld overlay was performed as designed by Nutech Engineers, Inc.
Q35050	84-5	Weld Overlay on 'B' Recircula- tion Header (02B-S7)	Unknown. Suspect IGSCC induced axial indications.	Leakage would have been detected and the Unit shutdown prior to pipe break.	A weld overlay was performed as designed by Nutech Engineers, Inc.
Q36085		IRM-14 Spikes High	Not apparent. Possibly dirty connectors.	Half scrams were received when IRM-14 spikes high. The conservative direction of this system was not compromised.	The chassis and pre- amp connectors were cleaned. Inputs were swapped and cable insulation resistance was checked. No problem was found.
Q36152		2B MSIV Failed to Shut	Failure of one of the pilot valves.	Unit was shutdown and Primary Containment capability was not needed.	Replaced pilot valves.

UNIT ONE MAINTENANCE SUMMARY

W. R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q36679		Repair Welds on Reactor Vessel Bottom Drain (W-1,W-12,W-13)	Slag in old welds.	None. This line has been hydrostatic tested repeatedly with no leakage.	The slag was removed and welds were repaired.
Q36841	84-14	M0 1-1001-29A; Replace Stem	No brakes and no functioning anti- hammer circuitry, so valve hammered shut repeatedly.	None. Unit was shut- down.	Stem was replaced; anti-hammer circuitry was re-wired correctly.
Q36845	84-14	M0 1-1001-29B; Replace Stem	No brakes and no functioning anti- hammer circuitry, so valve hammered shut repeatedly.	None. Unit was shut- down.	Stem was replaced; anti-hammer circuitry was re-wired correctly.
Q36989	84-17	Valves 1-5401A & B Operate Backwards	Improper installa- tion. Reference LER 84-17.	The consequences of this event were minimized by the low power condition of the core, less than 1% and the short time period, 90 minutes, that the vacuum pump could not be isolated.	Re-installed valves correctly.

UNIT TWO MAINTENANCE SUMMARY

W. R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q36153		M0 2-1402-24A Local Station OPEN Indication Light Does Not Work	High ambient temperature.	Due to the large capacity of the batteries, ample time would be available to charge the batteries. If the batteries still are not charged, a half scram would occur, thereby maintaining the conservative direction of the system.	Provided fans for charger and rooms.
Q36997		2B2 24-48 Volt DC Charger Will Not Stay On Equalize	High ambient temperature.	Due to the large capacity of the batteries, ample time would be available to charge the batteries. If the batteries still did not get charged, a half scram would occur, thereby maintaining the conservative direction of the system.	Provided fans for charger and room.

V. DATA TABULATIONS

The following data tabulations are presented in this report:

- A. Operating Data Report
- B. Average Daily Unit Power Level
- C. Unit Shutdowns and Power Reductions

OPERATING DATA REPORT

DOCKET NO. 50-254

UNIT ONE

DATE October 3

COMPLETED BY DAVE KIMLER

TELEPHONE 309-654-2241X192

OPERATING STATUS

0000 090184

1. Reporting period: 2400 093084 Gross hours in reporting period: 720

2. Currently authorized power level (MWt): 2511 Max. Depend capacity (MWe-Net): 769* Design electrical rating (MWe-Net): 789

3. Power level to which restricted (if any) (MWe-Net): NA

4. Reasons for restriction (if any):

	This Month	Yr. to Date	Cumulative
5. Number of hours reactor was critical	<u>720.0</u>	<u>2612.9</u>	<u>86168.5</u>
6. Reactor reserve shutdown hours	<u>0.0</u>	<u>0.0</u>	<u>3421.9</u>
7. Hours generator on line	<u>720.0</u>	<u>2563.2</u>	<u>82911.1</u>
8. Unit reserve shutdown hours.	<u>0.0</u>	<u>0.0</u>	<u>909.2</u>
9. Gross thermal energy generated (MWH)	<u>1630543</u>	<u>5727126</u>	<u>170833832</u>
10. Gross electrical energy generated (MWH)	<u>536126</u>	<u>1896796</u>	<u>55155412</u>
11. Net electrical energy generated (MWH)	<u>513251</u>	<u>1794423</u>	<u>51400390</u>
12. Reactor service factor	<u>100.0</u>	<u>39.7</u>	<u>79.3</u>
13. Reactor availability factor	<u>100.0</u>	<u>39.7</u>	<u>82.5</u>
14. Unit service factor	<u>100.0</u>	<u>39.0</u>	<u>76.3</u>
15. Unit availability factor	<u>100.0</u>	<u>39.0</u>	<u>77.2</u>
16. Unit capacity factor (Using MDC)	<u>92.7</u>	<u>35.5</u>	<u>61.5</u>
17. Unit capacity factor (Using Des. MWe)	<u>90.3</u>	<u>34.6</u>	<u>60.0</u>
18. Unit forced outage rate	<u>0.0</u>	<u>1.7</u>	<u>6.1</u>

19. Shutdowns scheduled over next 6 months (Type, Date, and Duration of each):

20. If shutdown at end of report period, estimated date of startup NA

*The MDC may be lower than 769 MWe during periods of high ambient temperature due to the thermal performance of the spray canal.

*UNOFFICIAL COMPANY NUMBERS ARE USED IN THIS REPORT

OPERATING DATA REPORT

DOCKET NO. 50-265

UNIT TWO

DATE October 3

COMPLETED BY DAVE KIMLER

TELEPHONE 309-654-2241X192

OPERATING STATUS

0000 090184

1. Reporting period: 2400 093084 Gross hours in reporting period: 720

2. Currently authorized power level (MWt): 2511 Max. Depend capacity (MWe-Net): 769* Design electrical rating (MWe-Net): 769

3. Power level to which restricted (if any) (MWe-Net): NA

4. Reasons for restriction (if any):

	This Month	Yr. to Date	Cumulative
5. Number of hours reactor was critical	<u>720.0</u>	<u>5013.8</u>	<u>82931.3</u>
6. Reactor reserve shutdown hours	<u>0.0</u>	<u>0.0</u>	<u>2985.8</u>
7. Hours generator on line	<u>720.0</u>	<u>4896.9</u>	<u>80106.6</u>
8. Unit reserve shutdown hours.	<u>0.0</u>	<u>0.0</u>	<u>702.9</u>
9. Gross thermal energy generated (MWH)	<u>1681897</u>	<u>11531787</u>	<u>166913875</u>
10. Gross electrical energy generated (MWH)	<u>542770</u>	<u>3716842</u>	<u>53152622</u>
11. Net electrical energy generated (MWH)	<u>520037</u>	<u>3543491</u>	<u>49877551</u>
12. Reactor service factor	<u>100.0</u>	<u>76.3</u>	<u>77.0</u>
13. Reactor availability factor	<u>100.0</u>	<u>76.3</u>	<u>79.8</u>
14. Unit service factor	<u>100.0</u>	<u>74.5</u>	<u>74.4</u>
15. Unit availability factor	<u>100.0</u>	<u>74.5</u>	<u>75.0</u>
16. Unit capacity factor (Using MDC)	<u>93.9</u>	<u>70.1</u>	<u>60.2</u>
17. Unit capacity factor (Using Des. MWe)	<u>91.5</u>	<u>68.3</u>	<u>58.7</u>
18. Unit forced outage rate	<u>0.0</u>	<u>3.2</u>	<u>8.3</u>

19. Shutdowns scheduled over next 6 months (Type, Date, and Duration of each):

20. If shutdown at end of report period, estimated date of startup NA

*The MDC may be lower than 769 MWe during periods of high ambient temperature due to the thermal performance of the spray canal.

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-254

UNIT ONE

DATE October 3

COMPLETED BY DAVE KIMLER

TELEPHONE 309-654-2241X192

MONTH September 1984

DAY AVERAGE DAILY POWER LEVEL
(MWe-Net)

1.	<u>499.9</u>
2.	<u>478.5</u>
3.	<u>485.4</u>
4.	<u>506.5</u>
5.	<u>559.0</u>
6.	<u>658.1</u>
7.	<u>688.3</u>
8.	<u>726.8</u>
9.	<u>777.1</u>
10.	<u>790.1</u>
11.	<u>784.0</u>
12.	<u>859.6</u>
13.	<u>651.3</u>
14.	<u>714.8</u>
15.	<u>736.6</u>
16.	<u>771.1</u>

DAY AVERAGE DAILY POWER LEVEL
(MWe-Net)

17.	<u>777.9</u>
18.	<u>732.9</u>
19.	<u>786.0</u>
20.	<u>779.1</u>
21.	<u>645.4</u>
22.	<u>720.1</u>
23.	<u>781.3</u>
24.	<u>776.6</u>
25.	<u>781.8</u>
26.	<u>869.8</u>
27.	<u>716.8</u>
28.	<u>788.0</u>
29.	<u>794.6</u>
30.	<u>739.8</u>

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly.

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-265

UNIT TWO

DATE October 3

COMPLETED BY DAVE KIMLER

TELEPHONE 309-654-2241X192

MONTH September 1984

DAY AVERAGE DAILY POWER LEVEL
(MWe-Net)

DAY AVERAGE DAILY POWER LEVEL
(MWe-Net)

1.	<u>774.2</u>
2.	<u>727.7</u>
3.	<u>686.8</u>
4.	<u>713.0</u>
5.	<u>767.8</u>
6.	<u>709.0</u>
7.	<u>737.6</u>
8.	<u>770.0</u>
9.	<u>670.5</u>
10.	<u>772.2</u>
11.	<u>761.5</u>
12.	<u>764.0</u>
13.	<u>733.5</u>
14.	<u>509.0</u>
15.	<u>478.5</u>
16.	<u>524.1</u>

17.	<u>639.6</u>
18.	<u>757.4</u>
19.	<u>773.1</u>
20.	<u>775.1</u>
21.	<u>761.1</u>
22.	<u>769.5</u>
23.	<u>745.3</u>
24.	<u>768.5</u>
25.	<u>766.3</u>
26.	<u>773.0</u>
27.	<u>782.6</u>
28.	<u>773.0</u>
29.	<u>780.3</u>
30.	<u>726.6</u>

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly.

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APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 6
August 1982

DOCKET NO. 050-254UNIT NAME Quad-Cities Unit OneCOMPLETED BY D. KimlerDATE October 4, 1984REPORT MONTH SEPTEMBER 1984TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
84-18	840901	S	0.0	F	5		ZZ	ZZZZZZ	Reduced load to 500 MWe per Load Dispatcher
84-19	840908	S	0.0	B	5		HA	TURBIN	Reduced load to perform weekly Turbine tests
84-20	840913	S	0.0	H	5		HH	PUMPXX	Reduced load for Condensate Pump changeover
84-21	840914	F	0.0	H	5		MB	RECOMB	Reduced load due to Recombiner problems
84-22	840918	S	0.0	F	5		ZZ	ZZZZZZ	Reduced load per Load Dispatcher
84-23	840921	S	0.0	B	5		RB	CONROD	Reduced load for Nuclear Engineer Test and Special Rod Maneuver
84-24	840930	S	0.0	B	5		HA	TURBIN	Reduced load to perform weekly Turbine tests

APPROVED
AUG 16 1982

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APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 6
August 1982

DOCKET NO. 050-265UNIT NAME Quad-Cities Unit TwoCOMPLETED BY D. KimlerDATE October 4, 1984REPORT MONTH SEPTEMBER 1984TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
84-35	840902	S	0.0	B	5		HA	TURBIN	Reduced load to perform weekly Turbine tests
84-36	840903	S	0.0	F	5		ZZ	ZZZZZZ	Reduced load per Load Dispatcher
84-37	840903	S	0.0	B	5		HA	TURBIN	Reduced load to perform Turbine nightly test and MSIV bi-weekly test
84-38	840906	S	0.0	F	5		ZZ	ZZZZZZ	Reduced load per Load Dispatcher and EGC Testing
84-39	840907	S	0.0	B	5		ZZ	ZZZZZZ	Reduced load for Economic Generation Control System test
84-40	840908	S	0.0	B	5		HA	TURBIN	Reduced load to perform weekly Turbine tests
84-41	840913	S	0.0	H	5		HF	PUMPXX	Reduced load to place 2B Circulating Water Pump out of service
84-42	840914	S	1.0	B	9		HA	TURBIN	Reduced load to place Reactor in HOT STANDBY, turn off Generator, and perform Turbine Overspeed Tests APPROVED

AUG 16 1982

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APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 6
August 1982

DOCKET NO. 050-265

UNIT NAME Quad-Cities Unit Two

COMPLETED BY D. Kimler

DATE October 4, 1984

REPORT MONTH SEPTEMBER 1984

TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
84-43	840919	F	0.0	H	5		SF	VALVEX	Reduced load due to problems with HPCI 2301-4 Valve
84-44	840923	S	0.0	B	5		HA	TURBIN	Reduced load to perform weekly Turbine tests
84-45	840930	S	0.0	B	5		HA	TURBIN	Reduced load to perform weekly Turbine tests

APPROVED
AUG 16 1982

VI. UNIQUE REPORTING REQUIREMENTS

The following items are included in this report based on prior commitments to the commission:

A. Main Steam Relief Valve Operations

Relief valve operations during the reporting period are summarized in the following table. The table includes information as to which relief valve was actuated, how it was actuated, and the circumstances resulting in its actuation.

<u>Unit</u>	<u>Date</u>	<u>Valves Actuated</u>	<u>No. & Type Actuations</u>	<u>Plant Conditions</u>	<u>Description of Events</u>
2	9-14-84	2-203-3A	1 Manual	Rx Press	Surveillance
		2-203-3B	1 Manual	920	Technical
		2-203-3C	1 Manual		Specification
		2-203-3D	1 Manual		4.5.D.1.b
		2-203-3E	1 Manual		

B. Control Rod Drive Scram Timing Data For Units One and Two

The basis for reporting this data to the Nuclear Regulatory Commission are specified in the surveillance requirements of Technical Specifications 4.3.C.1 and 4.3.C.2.

The following table is a complete summary of Units One and Two Control Rod Drive Scram Timing for the reporting period. All scram timing was performed with Reactor pressure greater than 800 psig.

RESULTS OF SCRAM TIMING MEASUREMENTS

PERFORMED ON UNIT 1 & 2 CONTROL

ROD DRIVES, FROM 1-1 TO 12-31-84

DATE	NUMBER OF RODS	AVERAGE TIME IN SECONDS AT % INSERTED FROM FULLY WITHDRAWN				Max. Time For 90% Insertion	DESCRIPTION
		5	20	50	90		
		0.375	0.900	2.00	3.5	7 sec.	Technical Specification 3.3.C.1 & 3.3.C.2 (Average Scram Insertion Time)
9-15	88	0.29	0.66	1.42	2.51	2.95 (m-7)	Unit 2 Hot Scram Timing A Sequence

VII. REFUELING INFORMATION

The following information about future reloads at Quad-Cities Station was requested in a January 26, 1978, licensing memorandum (78-24) from D. E. O'Brien to C. Reed, et al., titled "Dresden, Quad-Cities, and Zion Station--NRC Request for Refueling Information", dated January 18, 1978.

QUAD-CITIES REFUELING
INFORMATION REQUEST

QTP 300-S32
Revision 1
March 1978

- *
1. Unit: Q1 Reload: 7 Cycle: 8
2. Scheduled date for next refueling shutdown: 11-11-85
3. Scheduled date for restart following refueling: 1-20-86
4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment:
NOT AS YET DETERMINED.
5. Scheduled date(s) for submitting proposed licensing action and supporting information:
SEPTEMBER 13, 1985, IF LICENSING ACTION REQUIRED.
6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:
NONE PLANNED AT PRESENT TIME.
7. The number of fuel assemblies.
a. Number of assemblies in core: 724
b. Number of assemblies in spent fuel pool: 2340
8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:
a. Licensed storage capacity for spent fuel: 3657
b. Planned increase in licensed storage: 0
9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity: 2003

APPROVED

APR 20 1978

Q. C. O. S. R.

QUAD-CITIES REFUELING
INFORMATION REQUEST

QTP 300-S32
Revision 1
March 1978

- *
1. Unit: 2 Reload: 7 Cycle: 8
2. Scheduled date for next refueling shutdown: 4-2-85
3. Scheduled date for restart following refueling: 6-22-85
4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment:
Not as yet determined.
5. Scheduled date(s) for submitting proposed licensing action and supporting information:
January 18, 1985, if licensing action required.
6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:
None planned at present time.
7. The number of fuel assemblies.
a. Number of assemblies in core: 724
b. Number of assemblies in spent fuel pool: 0
8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:
a. Licensed storage capacity for spent fuel: 3897
b. Planned increase in licensed storage: 0
9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity: 2003

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APR 20 1978

Q. C. O. S. R.

VIII. GLOSSARY

The following abbreviations which may have been used in the Monthly Report, are defined below:

ACAD/CAM	-	Atmospheric Containment Atmospheric Dilution/Containment Atmospheric Monitoring
ANSI	-	American National Standards Institute
APRM	-	Average Power Range Monitor
ATWS	-	Anticipated Transient Without Scram
BWR	-	Boiling Water Reactor
CRD	-	Control Rod Drive
EHC	-	Electro-Hydraulic Control System
EOF	-	Emergency Operations Facility
GSEP	-	Generating Stations Emergency Plan
HEPA	-	High-Efficiency Particulate Filter
HPCI	-	High Pressure Coolant Injection System
HRSS	-	High Radiation Sampling System
IPCLRT	-	Integrated Primary Containment Leak Rate Test
IRM	-	Intermediate Range Monitor
ISI	-	Inservice Inspection
LER	-	Licensee Event Report
LLRT	-	Local Leak Rate Test
LPCI	-	Low Pressure Coolant Injection Mode of RHRS
LPRM	-	Local Power Range Monitor
MAPLHGR	-	Maximum Average Planar Linear Heat Generation Rate
MCPR	-	Minimum Critical Power Ratio
MFLCPR	-	Maximum Fraction Limiting Critical Power Ratio
MPC	-	Maximum Permissible Concentration
MSIV	-	Main Steam Isolation Valve
NIOSH	-	National Institute for Occupational Safety and Health
PCI	-	Primary Containment Isolation
PCIOMR	-	Preconditioning Interim Operating Management Recommendations
RBCCW	-	Reactor Building Closed Cooling Water System
RBM	-	Rod Block Monitor
RCIC	-	Reactor Core Isolation Cooling System
RHRS	-	Residual Heat Removal System
RPS	-	Reactor Protection System
RWM	-	Rod Worth Minimizer
SBGTS	-	Standby Gas Treatment System
SBLC	-	Standby Liquid Control
SDC	-	Shutdown Cooling Mode of RHRS
SDV	-	Scram Discharge Volume
SRM	-	Source Range Monitor
TBCCW	-	Turbine Building Closed Cooling Water System
TIP	-	Traversing Incore Probe
TSC	-	Technical Support Center



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NJK-84-298

October 1, 1984

Director, Office of Inspection & Enforcement
United States Nuclear Regulatory Commission
Washington, D. C. 20555
Attention: Document Control Desk

Gentlemen:

Enclosed for your information is the Monthly Performance Report covering the operation of Quad-Cities Nuclear Power Station, Units One and Two, during the month of September 1984.

Very truly yours,

COMMONWEALTH EDISON COMPANY
QUAD-CITIES NUCLEAR POWER STATION

N. J. Kalivianakis
Station Superintendent

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Enclosure

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