

DMB 016

JUL 13 1984

Docket No. 50-302

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Dear Mr. Wilgus:

SUBJECT: CRYSTAL RIVER UNIT 3 - NRC COMMENTS ON THE OFFSITE DOSE  
CALCULATION MANUAL

Amendment No. 69 to the Crystal River Unit 3 operating license was issued on June 27, 1984 to implement the revised radioactive effluent Technical Specifications (RETS). In conjunction with our review of the RETS, we reviewed the proposed Crystal River Unit 3 Offsite Dose Calculation Manual (ODCM) and noted a number of areas in the manual that require revision or clarification. This letter forwards our comments on the ODCM. Florida Power Corporation should resolve the attached comments and revise the ODCM accordingly. In addition, we request that a section be added to the ODCM to provide for total dose calculation, including direct radiation, as required by RETS Section 4.11.3.


Sincerely,

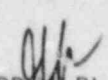
**"ORIGINAL SIGNED BY:"**

George W. Rivenbark, Acting Chief  
Operating Reactors Branch #4  
Division of Licensing

Enclosure:  
As Stated

cc w/enclosure:  
See next page

  
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Crystal River Unit No. 3  
Florida Power Corporation

50-302

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ENCLOSURE

NRC COMMENTS ON THE PROPOSED CRYSTAL RIVER UNIT 3  
OFFSITE DOSE CALCULATION MANUAL (ODCM)

JUNE 1984

CRYSTAL RIVER ODCM REVIEW

Comment

Crystal River ODCM

1. Sections 1.3-1

It is not clear why there are two definitions for  $Q_1$  in Section 1.3-1. Was the second definition meant to be written as

$$Q_1 = (\text{Nuclide Concentration in the Effluent Stream}) \times (\text{Flow})?$$

What is the significance of the "??"?

$Q_1$



\* Effluent Stream Flow Rate Nuclide Concentration  
Flow Rate

- 1) Reactor Building Purge Exhaust Duct = 30,000 cfm =  $2.9 \times 10^7$  cc/sec
- 2) Auxiliary Building and Fuel Handling Area Exhaust Duct = 156,000 cfm =  $7.9 \times 10^7$  cc/sec
- 3) Waste Gas Decay Tank Release Line = 30 cfm max =  $2.9 \times 10^6$  cc/sec

In order for a gaseous release to be within the limits of specification 1.1-1, the following equations must be satisfied:

Eq. 4      Dose Rate  $\div$  300  $\leq$  1

Eq. 5      Dose Rate  $\div$  3000  $\leq$  1

Eq. 6      Dose Rate  $\div$  1500  $\leq$  1  
                  I,T,P

where:

- 300 \* The allowable total body dose rate due to noble gas gamma emissions in mrem/yr.
- 3000 \* The allowable skin dose rate due to noble gas beta emissions in mrem/yr.
- 1500 \* The allowable organ dose rate in mrem/yr.

CRYSTAL RIVER ODCM REVIEW

Comment

Crystal River ODCM

2. Sections 1.3-1 and 1.3-2

The titles for Section 1.3-1 and 1.3-2 should be changed as these sections are not setpoint calculations, but are the pre-release calculations to ascertain 10 CFR Part 20 compliance.

3. Section 1.3-2

The Licensee should state that the activity of all components in the expression were obtained from the most recent analysis. Specifically,  $C_I$ ,  $C_G$ ,  $C_T$ , and  $C_{Fe}$  are obtained on a monthly or quarterly basis.

SETPOINT CALCULATION 1.3-2  
LIQUID RADWASTE RELEASE

I. INTRODUCTION

Prior to initiating a release of liquid radwaste, it must be determined that the concentration of radionuclides to be released and the flow rates at which they are released will not lead to a release concentration greater than the limits of specification 1.1-2 at the point of discharge.

II. INFORMATION REQUIRED

Results of appropriate Nuclide Analysis from Section 1.2

III. CALCULATION

$$\text{Discharge Concentration} = \frac{\left( \frac{\sum_i C_{\gamma i}}{MPC_{\gamma i}} + \frac{C_I}{MPC_I} + \frac{C_G}{MPC_G} + \frac{C_G}{MPC_G} + \frac{C_T}{MPC_T} + \frac{C_G}{MPC_G} + \frac{C_{Fe}}{MPC_{Fe}} \right) R}{(F + R)}$$

where:

- $\sum_i C_{\gamma i}$  = Sum of the concentrations of isotope i, in the gamma spectrum
- $C_I$  = Iodine 131 concentration
- $C_G$  = Dissolved or entrained noble gas concentration
- $C_T$  = Tritium Concentration
- $C_G$  = Gross alpha emitters concentration
- $C_{Sr}$  = Sr-89, 90 concentration
- $C_{Fe}$  = Fe-55 concentration
- $R$  = Effluent Stream Flow Rate (600gpm-RM-L7; 100gpm-RM-L2)
- $F$  = Dilution Stream Flow Rate (10,000gpm; Ref: FSAR Sec. 11.2.1.1)
- $MPC$  = 10CFR20 Appendix B, Table II, Column 2 Maximum Permissible Concentration by isotope.

} from most recent analysis

If the Calculated Discharge Concentration is less than or equal to 1, the discharge may be initiated. If the calculated discharge concentration is greater than 1, action must be taken to reduce the effluent concentration or effluent stream flow rate prior to initiating discharge.

CRYSTAL RIVER ODCM REVIEW

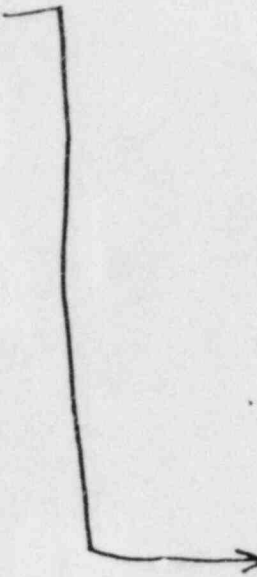
Comment

Crystal River ODCM

4. Section 1.4-5

The term  $\frac{C}{MPC}$  should be written as  $\sum_i \frac{C_i}{MPC_i}$

where  $i$  is the  $i^{th}$  nuclide



Setpoint Adjustment 1.3-3  
Plant Discharge Line Monitor (RM-L2)  
(Batch Type Releases)

INTRODUCTION

Following completion of the analyses required by Section 1.2-4 and determination of release rates and concentration limits in accordance with Section 1.3-2, the monitor setpoint requires adjustment to ensure that alarm and pathway isolation occur if the nuclide concentration or release rate exceeds the limits determined.

METHODOLOGY

Evaporator Condensate Storage Tank or Laundry and Shower Sump Tank contents are circulated through radiation monitor RM-L2 and returned to the auxiliary building sump to obtain the actual count rate at RM-L2 for the concentration contained in the tank for release. The observed count rate is adjusted for release flow, background and statistical counting variations, particular to this release flow path. The resulting value is used as the alarm/trip setpoint and RM-L2 is adjusted to this value prior to initiating the release.

CALCULATION

$$\text{Monitor Setpoint (CPM)} = \left[ \frac{\text{Net CPM} \times \text{Admin. Factor}}{C/MPC} \right] \left[ \frac{FR - FD}{FR} \right] + Bkg + 3.3\sqrt{Bkg}$$

where:

- Net CPM = The observed monitor count rate, in counts per minute.
- Admin. Factor = Administration Factor to account for error in setpoint determination. Admin. Factor = 0.5.
- C/MPC = The ratio of the actual concentration of the tank contents to be released to the Maximum Permissible Concentration (MPC) as listed in 10 CFR 20, Table II, Column 2 for unrestricted areas.
- FR = The release flow rate of waste to be discharged in gallons per minute.
- FD = The dilution flow from the Nuclear Services Sea Water system in gallons per minute.
- BKG = The background count rate at RM-L2 in counts per minute (cpm).
- $3.3\sqrt{Bkg}$  = A statistical spread on the background count rate which represents a 99.93% confidence level on monitor counting. This factor is included to prevent inadvertent high/trip alarms due to random counts on the monitor. Only the positive (+) side of the spread is applied.

Comments

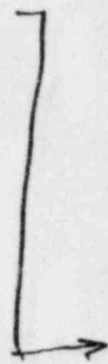
Crystal River ODCM

## 5. Section 2.2-1 and Section 2.2-2

Should the second equation for  $D_p$  be written as

$$D_p = \frac{(D_{L-2}) k_2 + (D_{L-1}) k_1 + (D_L) k}{3}$$

As written "k" has the same value for all three terms.

DOSE PROJECTION METHODOLOGY 2.2-1  
GASEOUS RADWASTE

## I. INTRODUCTION

Crystal River Unit 3 operating practices require use of the waste gas system (Waste Gas Decay Tanks). The normal release paths for gaseous effluents are via ventilation exhaust treatment systems (HEPA and Charcoal Filters). The operability of the ventilation exhaust treatment systems is controlled by the Crystal River Unit 3 Technical Specifications.

As long as these practices and specifications are maintained, the radwaste reduction requirements of Crystal River Unit 3 Technical Specification 3.7.13.3 are met, and there is no need to project doses prior to the release of gaseous radwaste.

## II. CALCULATIONS

Dose projection calculations will be necessary if either system is not available for use. The dose projection will be made using whichever formula below yields the higher projected dose.

$$1) D_p = (D_L) k$$

$$2) D_p = \frac{(D_{L-2}) k + (D_{L-1}) k + (D_L) k}{3}$$

where:

$D_p$  = Projected Dose.

$D_L$  = Dose, calculated in accordance with section 4.3-1 of this manual for the most recently completed (reference) month.

$k$  = A constant to account for the use of the waste gas system during the reference month.

$k = 0$  if the waste gas system was used.

$k = 1$  if the system was not used.

Assumptions:

- 1) Xe-133 and I-131 are major dose contributors.
- 2) I-131 is removed by charcoal filters
- 3) Nominal holdup time is ten days (two Xe-133 half-lives).

References:

- 1) T.S. 3.6.4.2, 3.7.8.1
- 2) FSAR 3.3.1, 3.3.2

CRYSTAL RIVER ODCM REVIEW

Comment

Crystal River ODCM

Calculation of Dose Factors  
in the Ground Plane Pathway ( $R_1^G [D/Q]$ )

$$R_1^G(D/Q) = K' K'' (SF) DFG_1 (1 - e^{-\lambda_1 t}) / \lambda_1$$

units = m<sup>2</sup> · mrem/yr per  $\mu$ Cl/sec

where:

Reference Table, R.G. 1.109

- K' = A constant unit of conversion, 10<sup>6</sup> pCi/ $\mu$ Cl.
- K'' = A constant unit of conversion, 8760 hr/yr
- SF = The shielding factor, (dimensionless, 0.7) E-13
- $\lambda_1$  = The decay constant for the 1th radionuclide, sec<sup>-1</sup>
- t = The exposure period, 3.15 x 10<sup>7</sup> sec (1 year) *15 years*
- DFG<sub>1</sub> = The ground plane dose conversion factor for the 1th radionuclide (mrem/hr per  $\mu$ Cl/m<sup>2</sup>) E-6

6. Calculation of Dose Factors in the Ground Plane Pathway

The t should be for 15 years and not for one year.

The units for DFG<sub>1</sub> should be  $\mu$ Ci, not Ci.

Reference: The equation deriving  $R_1^G(D/Q)$  was taken from NUREG 0133, Section 3.3.1.2.



CRYSTAL RIVER ODCM REVIEW

Comment

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Crystal River ODCM

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7. The total dose calculation including direct radiation was not addressed.

CRYSTAL RIVER ODCM REVIEW

Comment

Crystal River ODCM

3. The following sample locations were omitted:

Sample Location Omitted

Table 5.1-2      C27  
 Table 5.1-1      C14H, C09, C43  
 Figure 5.1        C14H, C43

Note: C09 is identified in Figure 5.1

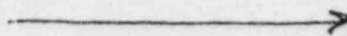


TABLE 5.1-2

RING TLDs  
 (INNER RING)

<u>LOCATION</u>	<u>DIRECTION</u>	<u>DISTANCE (Ft.)</u>
C60	N	4400
C61	NNE	4400
C62	NE	3300
C63	ENE	4400
C64	E	4400
C65	ESE	1740
C66	SE	1600
C67	SSE	1430
C68	S	1300
C69	SSW	1730
C91	SW	2100
C70	WSW	4400
C71	WNW	3600
C72	NW	3600
C73	NNW	2000

CRYSTAL RIVER ODCM REVIEW

Comment

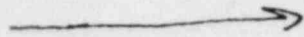
Crystal River ODCM

3. The following sample locations were omitted:

Sample Location Omitted

Table S.1-2  
Table S.1-1  
Figure S.1

C27  
C14H, C09, C43  
C14H, C48



Note: C09 is identified in Figure S.1

Table S.1-1

Environmental Radiological Monitoring  
Stations Locations

STATION	LOCATION	DIRECTION FROM PLANT	DISTANCE FROM PLANT (mi)
C04	State Park Old Dam on River near road intersection	ENE	6.3
C07	Crystal River Public Water Plant	ESE	7.3
C10	Indian Waters Public Water Supply	ESE	3.9
C13	Mouth of Intake Canal	WSW	3.4
C14H	Head of Discharge Canal	NW	0.1
C14G	Discharge Canal at Gulf of Mexico	W	2.4
C18	Yankeetown City Well	N	4.2
C19	NW Corner State Roads 433 & 495	ENE	8.3
C29	Discharge Area	N	2.0
C30	Intake Area	WSW	3.6
C40	Near N.E. Site Boundary near excavated pond & pump station	E	3.3
C41	Onsite meteorological tower	SSW	0.4
C46	North Pump Station	N	0.4
C47	University of Florida, Gainesville	NNE	32
C49	To be determined from annual milk cow census		

CRYSTAL RIVER ODCM REVIEW

Comment

Crystal River ODCM

8. The following sample locations were omitted:

Sample Location Omitted

Table 5.1-2	C27
Table 5.1-1	C14M, C09, C48
Figure 5.1	C14M, C48

Note: C09 is identified in Figure 5.1

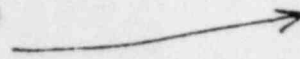
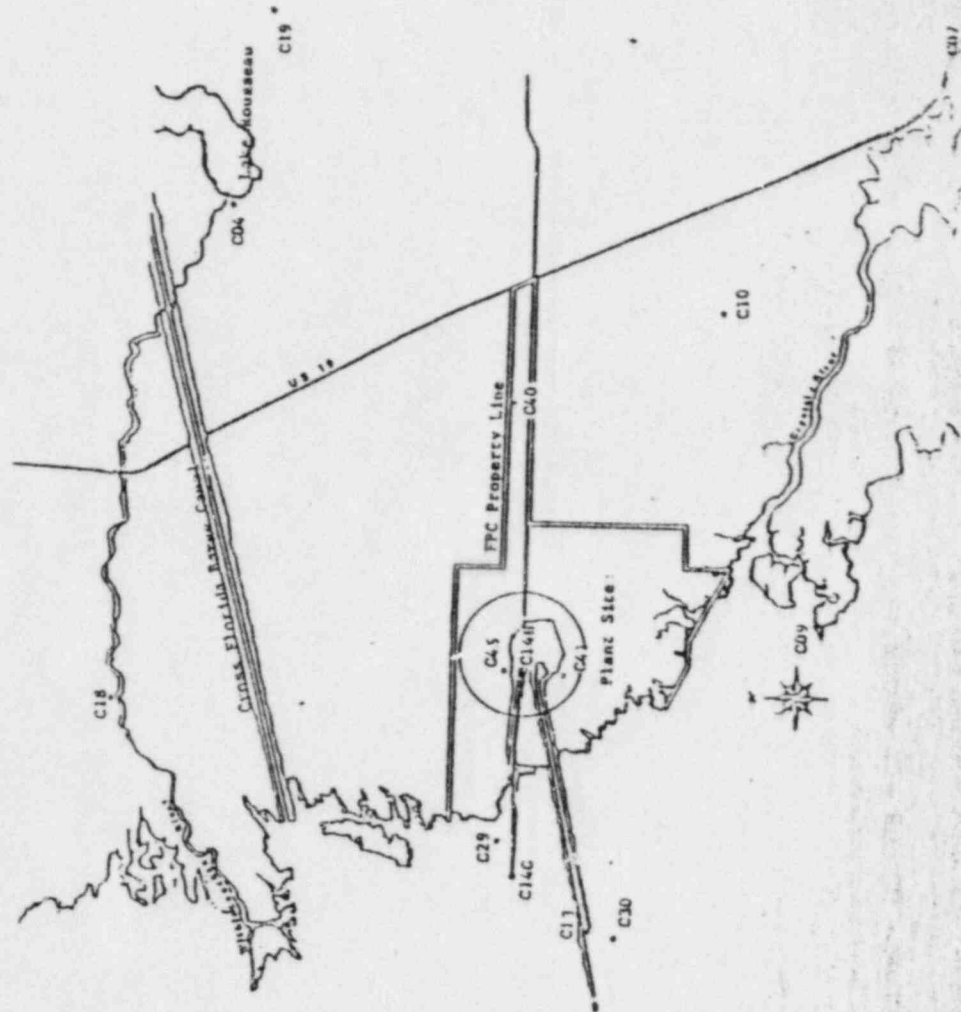


FIGURE 5.1



Environmental Monitoring  
Sample Station Locations

## CRYSTAL RIVER ODCM REVIEW

Comment

Crystal River ODCM

DOSE CALCULATION 4.3-3  
(LIQUID EFFLUENTS)

The dose or dose commitment to a MEMBER OF THE PUBLIC from radioactive materials in liquid effluents released to UNRESTRICTED AREAS is calculated as follows:

$$D_r = \sum_{i=1}^n \left[ A_{lr} \frac{1}{l^2} \sum_{j=1}^m a_{tj} C_{ij} \right]$$

where:

- $D_r$  = The cumulative dose commitment to the total body or any organ,  $r$ , from the liquid effluents for the total time period  $\sum_{j=1}^m a_{tj}$ , in mrem.
- $a_{tj}$  = The length of the  $l$ th time period over which  $C_{ij}$  is averaged for all liquid releases, in hours.
- $C_{ij}$  = The average concentration of radionuclide,  $i$ , in undiluted liquid effluent during time period  $a_{tj}$  from any liquid release, in  $\mu\text{Ci}/\text{ml}$ .
- $A_{lr}$  = The site related ingestion dose commitment factor to the total body or any organ  $r$  for each identified principal gamma and beta emitter as shown in Table 4.4-17 of this manual, in mrem-ml per hour  $\mu\text{Ci}$ .

## 9. Section 4.3-3

The Licensee should consider use of a near field average dilution factor in the expression for the liquid dose calculation.

## References:

- 1) NUREG 0133, Section 4.3

CRYSTAL RIVER ODCM REVIEW

Comment

Crystal River ODCM

Calculation of Inhalation Pathway Dose Factor ( $P_i$ )

The  $P_i$  should be  $R_i$  in both the title and the expression.

7 yr<sup>0</sup>  $R_i$



CALCULATION OF INHALATION  
PATHWAY DOSE FACTOR ( $P_i$ )

$R_i$  →

$$P_i = K' (BR) DFA_i = \text{mrem/year per } \mu\text{Ci/m}^3 \quad (\text{from section 3.2.1.1 of NUREG 0133})$$

where:

- $K'$  • A constant unit of conversion -  $10^6 \text{ pCi}/\mu\text{Ci}$
- $BR$  • The Breathing Rate of the represented age group:  
(from Table E-3 of Regulatory Guide 1.109).  
1400  $\text{m}^3/\text{yr}$  - infant  
3700  $\text{m}^3/\text{yr}$  - child  
3000  $\text{m}^3/\text{yr}$  - teen  
3000  $\text{m}^3/\text{yr}$  - adult
- $DFA_i$  • The maximum organ inhalation dose factor for the represented age group for the  $i$ th radionuclide, in  $\text{mrem}/\mu\text{Ci}$ .  
The values of  $DFA_i$  are listed in Regulatory Guide 1.109 as follows:  
 $DFA_i$  (infant) - Table E-10  
 $DFA_i$  (child) - Table E-9  
 $DFA_i$  (teen) - Table E-8  
 $DFA_i$  (adult) - Table E-7

CRYSTAL RIVER ODCM REVIEW

Comment

Calculation of Ingestion Dose Factor Grass-Cow-Meat Pathway

The term  $e^{-\lambda_i t_h}$  should be  $e^{-\lambda_i t_f}$

Crystal River ODCM

Calculation of Ingestion Dose Factor  
Grass-Cow-Meat Pathway (  $R_i^M [D/Q]$  )

*typo*  $t_f$

$$R_i^M [D/Q] = K' \left[ \frac{Q_F (U_{ap})}{\lambda_i + \lambda_w} \right] F_t (r) (DFL_{i,a}) \left[ \frac{f_p f_s}{Y_p} + \frac{(1 - f_p f_s) e^{-\lambda_i t_h}}{Y_s} \right] e^{-\lambda_i t_h}$$

where: Units =  $m^2 \cdot \text{mrem/yr}$  per  $\mu\text{Ci/sec}$

Reference Table, R.G. 1.109

- K' = A constant of unit conversion,  $10^6 \text{ pCi}/\mu\text{Ci}$ .
- QF = The cow's consumption rate, 30 kg/day (wet weight) E-3
- U<sub>ap</sub> = The receptor's meat consumption rate for age (a), in kg/yr E-3
  - Infant - 0
  - Child - 41
  - Teen - 63
  - Adult - 110
- Y<sub>p</sub> = The agricultural productivity by unit area of pasture feed grass 0.7 kg/m<sup>2</sup> E-13
- Y<sub>s</sub> = The agricultural productivity of unit area of stored feed 2.0 kg/m<sup>2</sup> E-13
- F<sub>t</sub> = The stable element transfer coefficients, in days/kg. E-1
- r = Fraction of deposited activity retained on cow's feed grass
  - 1.0 radioiodine E-13
  - 0.2 particulates E-13
- t<sub>f</sub> = Transport time from pasture to receptor, in sec.
  - $1.73 \times 10^6 \text{ sec}$  E-13
  - (20 days)
- t<sub>h</sub> = Transport time from crop field to receptor, in sec.
  - $7.78 \times 10^6 \text{ sec}$  E-13
  - (90 days)
- (DFL)<sub>i,a</sub> = The maximum organ ingestion dose factor for the i<sup>th</sup> radionuclide for the receptor in age group (a), in mrem/pCi E-11 to E-14
- $\lambda_i$  = The decay constant for the i<sup>th</sup> radionuclide, in sec<sup>-1</sup>
- $\lambda_w$  = The decay constant for removal of activity on leaf and plant surfaces by weathering,  $3.73 \times 10^{-7} \text{ sec}^{-1}$  (corresponding to a 14 day half-life).
- f<sub>p</sub> = Fraction of the year that the cow is on pasture (dimensionless) \* 1\*
- f<sub>s</sub> = Fraction of the cow feed that is pasture grass while the cow is on pasture (dimensionless) \* 1\*.

\*Milk cattle are considered to be fed from two potential sources, pasture grass and stored feeds. Following the development in Regulatory Guide 1.109, the values of f<sub>p</sub> and f<sub>s</sub> will be considered unity, in lieu of site specific information provided in the annual land census report by the licensee.

Note: The above equation does not apply to the concentration of tritium in meat. A separate equation is provided in NUREG 0133, section 3.3.1.9 to determine Tritium value.

References: The equation deriving  $R_i^M [D/Q]$  was taken from NUREG 0133, Section 3.3.1.7.

CRYSTAL RIVER ODCM REVIEW

Comment

Crystal River ODCM

Calculation of Ingestion Dose Factor Vegetation Pathway

The term  $\frac{1}{(1+w)}$  should be  $\frac{1}{(\lambda_l + \lambda_w)}$

The definition for  $t_l$  should state it is for leafy vegetation instead of stored vegetation.

The definition for  $\gamma_v$  should use a capital letter  $\gamma$ .

Calculation of Ingestion Dose Factor  
Vegetation Pathway (  $R_L^V (D/Q)$  )

$$R_L^V(D/Q) = K' \frac{(r)}{\gamma_v (\lambda_l + \lambda_w)} (DFL)_a \left[ U_a^L t_L e^{-\lambda_l t_L} + U_a^S t_S e^{-\lambda_l t_S} \right]$$

where: Units =  $m^2 \cdot mrem/yr$  per uCi/sec

Reference Table, R.G. 1.103

- $K'$  = A constant of unit conversion, 106 pCi/uCi. E-3
- $U_a^L$  = The consumption rate of fresh leafy vegetation by the receptor in age group (a), in kg/yr.
 

Infant - 0
Child - 26
Teen - 42
Adult - 64
- $U_a^S$  = The consumption rate of stored vegetation by the receptor in age group (a), in kg/yr. E-3
 

Infant - 0
Child - 320
Teen - 630
Adult - 320

$(DFL)_a$  = The maximum organ ingesting dose factor for the  $i$ th radionuclide for the receptor in age group (a), in mrem/pCi. E-11 to E-14

$f_L$  = The fraction of the annual intake of fresh leafy vegetation grown locally. (default 1.0)

$f_S$  = The fraction of the annual intake of stored vegetation grown locally. (default 0.76)

$t_L$  = The average time between harvest of leafy stored vegetation and its consumption,  $3.6 \times 10^4$  seconds, (1 day) *Typo*

$t_S$  = The average time between harvest of stored vegetation and its consumption,  $5.18 \times 10^6$  seconds, (60 days)

$\gamma_v$  = The vegetation areal density, 2.0 kg/m<sup>2</sup> E-13

$r$  = Fraction of deposited activity retained on the vegetation  
1.0 radionuclide  
0.2 particulates E-13

$\lambda_l$  = The decay constant for the  $i$ th radionuclide, in sec<sup>-1</sup>

$\lambda_w$  = The decay constant for removal of activity on leaf and plant surfaces by weathering,  $5.73 \times 10^{-7}$  sec<sup>-1</sup> (corresponding to a 14 day half-life).

Note: The above equation does not apply to the concentrations of tritium in vegetation. A separate equation is provided in NUREG 0133, section 5.3.1.3 to determine tritium values.

Reference: The equation deriving  $R_L^V (D/Q)$  was taken from NUREG 0133, Section 5.3.1.3.



## CRYSTAL RIVER ODCM REVIEW

Comment

Crystal River ODCM

DOSE CALCULATION 4.3-1  
(NOBLE GAS)

The dose to an individual at or beyond the SITE BOUNDARY due to noble gases released in gaseous effluents is calculated as follows:

$$D_{\gamma} = 3.17 \times 10^{-8} \sum_i \left[ M_i (\bar{X}/Q) Q_i \right] \quad \text{gamma radiation}$$

$$D_{\beta} = 3.17 \times 10^{-8} \sum_i \left[ N_i (\bar{X}/Q) Q_i \right] \quad \text{beta radiation}$$

where:

$D_{\gamma}$  = The dose to an individual at or beyond the SITE BOUNDARY due to gamma emissions from noble gases in gaseous effluents in mrad/time period.

$D_{\beta}$  = The dose to an individual at or beyond the SITE BOUNDARY due to beta emissions from noble gases in gaseous effluents in mrad/time period.

$3.17 \times 10^{-8}$  = The number of years in one second.

$M_i$  = The air dose factor due to gamma emissions for each identified noble gas radionuclide, in mrad/year per uCi/m<sup>3</sup>.

$N_i$  = The air dose factor due to beta emissions for each identified noble gas radionuclide, in mrad/year per uCi/m<sup>3</sup>.

$(\bar{X}/Q)$  = The highest calculated annual average relative concentration for areas at or beyond the UNRESTRICTED AREA Boundary,  $2.5 \times 10^{-6}$  sec/m<sup>3</sup>.

$Q_i$  = The average release of noble gas radionuclides in gaseous releases from all vents in uCi. Releases shall be cumulative over the time period of concern.

Section 4.3-1

The units for  $Q_i$  should be  $\mu\text{Ci}$ , not Ci.

7 yps

CRYSTAL RIVER ODCM REVIEW

Comment

Crystal River ODCM

SETPOINT CALCULATION 1.3-1  
GASEOUS RADWASTE RELEASE

I. INTRODUCTION

Prior to initiating a release of gaseous radwaste, it must be determined that the concentration of radionuclides to be released, and the flow rates at which they are released will not exceed the dose rate limitations of Specification 1.1-1.

II. INFORMATION REQUIRED

Results of appropriate Nuclide Analysis from Section 1.2

III. CALCULATIONS

A. Noble Gas Gamma Emissions

Eq. 1 Dose Rate<sub>g</sub> =  $\sum_i [K_i ((\bar{X}/Q) Q_i)]$  mrem/yr.

B. Noble Gas Beta Emissions

Eq. 2 Dose Rate<sub>β</sub> =  $\sum_i [(L_i + 1.1M_i) ((\bar{X}/Q) Q_i)]$  mrem/yr.

C. Iodine 131, Tritium, Radioactive Particulates

Eq. 3 Dose Rate I,T,P =  $\sum_i P_i ((\bar{X}/Q) Q_i)$  mrem/yr.

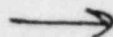
where:

- K<sub>i</sub> = The total body dose factor due to gamma emissions for each identified noble gas radionuclide, in mrem/yr per μCi/m<sup>3</sup>. (See Table 1.3-1).
- L<sub>i</sub> = The skin dose factor due to beta emissions for each identified noble gas radionuclide, in mrem/yr per μCi/m<sup>3</sup>. (See Table 1.3-1).
- M<sub>i</sub> = The air dose factor due to gamma emissions for each identified noble gas radionuclide, in mrad/yr per μCi/m<sup>3</sup> (unit conversion constant of 1.1 mrem/mrad converts air dose to skin dose). (See Table 1.3-1).
- P<sub>i</sub> = The dose parameter for radionuclides other than noble gases for the inhalation pathway, in mrem/yr per μCi/m<sup>3</sup>. (See Table 1.3-2).
- Q<sub>i</sub> = The release rate of radionuclides, i, in gaseous effluent from individual release sources, in μCi/sec (per unit, unless otherwise specified).

( $\bar{X}/Q$ ) = 2.5x10<sup>-6</sup> sec/m<sup>3</sup>. (F) all vent releases. The highest calculated annual average relative concentration for any area at or beyond the unrestricted area boundary.

Section 1.3-1

The word "For" is spelled as "Fbr" in the  $\frac{\bar{X}}{Q}$  definition.



Handwritten note:  $\frac{\bar{X}}{Q}$  is  $\frac{1}{4} P_0$

## CRYSTAL RIVER ODCM REVIEW

Comment

Crystal River ODCM

Section 1.3-3

- a. Shouldn't the value  $3.26 \times 10^8$  cc be  $1.36 \times 10^7$  cc? The  $3.26 \times 10^8$  value is not used in the calculation.
- b. The "u" is missing from most of the units, e.g.,  $2.08 \mu\text{Ci}$  and  $6.62 \times 10^{-1} \mu\text{Ci}$ .

In order to determine the total quantity of Iodine 131 collected on the filter, the values of  $C_v$  above are multiplied by the volume assumed to have passed through the filter, ( $3.26 \times 10^8$  cc).

$$Q_I = C_v \times f_v \times k$$

where:

$Q_I$  = The total quantity of Iodine 131 collected on the filter in  $\mu\text{Ci}$ .

$C_v$  = The concentration of Iodine 131 in the vent in  $\mu\text{Ci}/\text{cc}$ .

$f_v$  = The assumed total volume of vent atmosphere that has passed through the filter,  $1.36 \times 10^7$  cc (1 CFM for 3 hours).

$k$  = The Iodine removal efficiency of the filters: 96%

Solving for  $Q_I$  for the Reactor Building vent yields:

$$Q_{I(RB)} = 2.08 \mu\text{Ci} \quad 2.08 \mu\text{Ci}$$

Solving for  $Q_I$  for the Auxillary Building and Fuel Handling Area vent yields:

$$Q_{I(AB)} = 6.62 \times 10^{-1} \mu\text{Ci}$$

These values are translated to counts per minute for the Iodine monitoring channels through use of the appropriate calibration curves.