

BYRON SECTIONS 7.2 and 8.0

REVISION 11

JUNE 1984

OFFSITE DOSE CALCULATION MANUAL

COMMONWEALTH EDISON COMPANY

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BYRON

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NUMBER

TITLE

7.2-1

Restricted Area Boundary

TABLE 7.2-1

AQUATIC ENVIRONMENTAL DOSE PARAMETERS

<u>PARAMETER</u>	<u>BYRON</u>	<u>BASIS*</u>
U^W , water usage, liters/hr	0.042	A
U^E , fish consumption, kg/hr	2.4×10^{-3}	B
$1/M^W$, $1/M^E$	1	C
F^W , cfs	5.2×10^4	D
F^E , cfs	4.7×10^3	E
t^E , hr	24	F
t^W , hr	115	G

B_i - Regulatory Guide 1.109, Revision 1, October 1977, Table A-1, Column 2 for freshwater fish. See Table 7.1-12.

F^O , cfs	} Not Applicable. No outdoor tanks without overflow pipes connected to other storage tanks.
F^W_O , cfs	
$1/M^W_O$	
t^W_O , hr	
V^O , gal	
t^O , hr	

*Basis codes:

- A: Reference 6.2, Page 138.
- B: Reference 6.5, Table E-5.
- C: Conservative assumption (implies no additional dilution).
- D: The receiving body of water is taken as the Mississippi River, whose confluence is approximately 115 miles downstream of the plant. F^W is taken as the sum of the following average flow rates:
- | | |
|--|---|
| Rock River at Como, Illinois
(45 miles downstream
of plant) | 5.0×10^3 cfs per Byron Station
Environmental Report, Subsection
2.4.1.2 |
| Mississippi River near DeWitt,
Iowa (approximately 35 miles
upstream of confluence with
Rock River) | 4.7×10^4 cfs per Quad-Cities
Station Units 1 and 2 Safety
Analysis Report, Section 2.4 |
- E: The near-field receiving body of water is the Rock River. F^E is taken as the average flow of the Rock River at the site, 4.7×10^3 cfs per Byron Station Environmental Report, Subsection 2.4.1.2.
- F: Assumption.
- G: There are no potable water intakes on the Rock River downstream of the plant (per Byron Station Environmental Report, Subsection 2.1.3.2.1). For 10 CFR 50 compliance evaluation purposes, t^W is taken as 115 hr, the estimated time of flow to the Mississippi River. The confluence of the Rock River with the Mississippi River is approximately 115 miles downstream of the plant (per Byron Station Environmental Report, Sub-section 2.1.3.2.1). The flow rate is estimated as 1 mph based on the data in Table 2.2-5 of the Byron Station Environmental Report.

TABLE 7.2-2

ANNUAL DESIGN OBJECTIVES SET BY 10 CFR 50,
APPENDIX I, FOR EACH REACTOR

<u>TYPE OF DOSE</u>	<u>ANNUAL DESIGN OBJECTIVES</u>
<u>Airborne Releases</u>	
Gamma Air Dose	10 mrad
Beta Air Dose	20 mrad
Whole Body Dose	5 mrem
Skin Dose	15 mrem
Infant Thyroid Dose	15 mrem
<u>Liquid Releases</u>	
Whole Body Dose	3 mrem
Thyroid Dose	10 mrem
Bone Dose	10 mrem
Skin Dose	10 mrem

TABLE 7.2-3

STATION CHARACTERISTICS

STATION: Byron

LOCATION: 3.7 miles SSW of Byron, Illinois

CHARACTERISTICS OF ELEVATED RELEASE POINT

1) Release Height = _____ m 2) Diameter = _____ m
 3) Exit Speed = _____ ms^{-1} 4) Heat Content = _____ KCal s^{-1}

CHARACTERISTICS OF VENT STACK RELEASE POINTS*

1) Release Height = 60.96 m 2) Effective Diameter = 2.80 m
 3) Exit Speed = 15.34 ms^{-1}

*The station has two adjacent rectangular vent stack release points of the same height and cross section. Their centers are 15.01 m apart.

CHARACTERISTICS OF GROUND LEVEL RELEASE

1) Release Height = 0 m
 2) Building Factor (D) = 60.6 m

METEOROLOGICAL DATA

A 250 ft. Tower is located 1036 m SW of vent stack release point

Tower Data Used in Calculations

Release Point	Wind Speed and Direction	Differential Temperature
<u>Elevated</u>	<u>(NA)</u>	<u>(NA)</u>
<u>Vent</u>	<u>250 ft</u>	<u>250 - 30 ft</u>
<u>Ground</u>	<u>30 ft</u>	<u>250 - 30 ft</u>

TABLE 7.2-4
CRITICAL RANGES

<u>DIRECTION</u>	<u>RESTRICTED AREA BOUNDARY*</u> (m)	<u>NEAREST** RESIDENT</u> (m)	<u>NEAREST DAIRY FARM RANGE**</u> (m)
N	1875	2300	---- †
NNE	1829	2900	---- †
NE	1585	1900	3400
ENE	1234	2100	---- †
E	1227	1900	---- †
ESE	991	2600	5100
SE	1006	2100	5300
SSE	800	1300	---- †
S	945	1100	3200
SSW	975	1000	---- †
SW	1067	1300	---- †
WSW	1212	2700	---- †
W	1189	3100	3100
WNW	1227	3400	5300
NW	1300	1300	5100
NNW	1044	1900	---- †

*Approximate distance from midpoint between gaseous effluent release points. (See FSAR Table 2.1-1a (Amendment 39, September 1982) and ER Table 2.1-1 (Amendment 1, July 1981).)

**Approximate distance from center of plant per 1983 annual survey by Teledyne Isotopes Midwest Laboratories.

†No dairy farm found within 5 miles (8000 m) of station.

TABLE 7.2-5

TERRAIN CORRECTION FACTORS (n_t)* $(h_t = 0$ to Stated Range, Then $h_t =$ Given Value)

<u>DIRECTION</u>	<u>RANGE</u> <u>(miles)</u>	<u>h_t</u> <u>(meters)</u>
N	—	0.0
NNE	—	0.0
NE	—	0.0
ENE	—	0.0
E	9.0	3.0
ESE	—	0.0
SE	5.0	11.0
SSE	4.2	9.0
S	4.4	9.0
SSW	—	0.0
SW	5.0	9.0
WSW	6.5	12.0
W	7.6	14.0
WNW	—	0.0
NW	7.3	9.0
NNW	9.7	6.0

*Within 10 miles

TABLE 7.2-6

X/Q AND D/Q MAXIMA AT OR BEYOND THE UNRESTRICTED AREA BOUNDARY

DOWNWIND DIRECTION	ELEVATED (STACK) RELEASE ^a				MIXED MODE (VENT) RELEASE			GROUND LEVEL RELEASE ^a		
	RADIUS ^b (METERS)	X/Q (SEC/M ³)	RADIUS ^b (METERS)	D/Q (1/M ²)	RADIUS ^b (METERS)	X/Q (SEC/M ³)	D/Q (1/M ²)	RADIUS ^b (METERS)	X/Q (SEC/M ³)	D/Q (1/M ²)
N	1875.	9.557-08	1875.	9.680-10	1875.	2.102-07	1.666-09	1875.	1.007-06	4.937-09
NNE	1829.	1.083-07	1829.	1.048-09	1829.	1.683-07	1.582-09	1829.	8.936-07	4.682-09
NE	1585.	9.628-08	1585.	1.062-09	1585.	1.648-07	1.562-09	1585.	9.067-07	4.912-09
ENE	1609.	9.103-08	1234.	1.305-09	1234.	1.741-07	1.768-09	1234.	1.130-06	6.280-09
E	1400.	1.067-07	1227.	1.787-09	1227.	2.204-07	2.143-09	1227.	1.436-06	7.005-09
ESE	1400.	1.066-07	991.	2.199-09	991.	2.591-07	2.748-09	991.	1.706-06	9.462-09
SE	1500.	9.378-08	1006.	1.846-09	1006.	3.791-07	2.589-09	1006.	2.623-06	1.030-08
SSE	1500.	7.869-08	800.	1.558-09	800.	3.376-07	2.176-09	800.	2.622-06	1.146-08
S	1800.	6.347-08	945.	7.539-10	945.	1.775-07	1.377-09	945.	1.390-06	7.506-09
SSW	1609.	5.441-08	975.	8.453-10	975.	1.310-07	1.191-09	975.	9.962-07	5.632-09
SW	1609.	6.179-08	1067.	9.762-10	1067.	1.257-07	1.467-09	1067.	8.619-07	5.159-09
WSW	1609.	5.528-08	1212.	7.907-10	1212.	1.244-07	1.310-09	1212.	7.873-07	4.685-09
W	1609.	5.338-08	1189.	7.180-10	1189.	1.310-07	1.173-09	1189.	8.107-07	4.424-09
WNW	1400.	5.222-08	1227.	8.600-10	1227.	1.162-07	1.183-09	1227.	7.074-07	3.598-09
NW	1400.	5.652-08	1128.	1.028-09	1128.	1.380-07	1.405-09	1128.	8.763-07	4.804-09
NNW	1400.	8.117-08	1044.	1.591-09	1044.	2.769-07	2.540-09	1044.	1.492-06	8.173-09

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

^aThe elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

^bApproximate distance from midpoint between gaseous effluent release points to location of highest X/Q or D/Q at or beyond the unrestricted area boundary.

TABLE 7.2-6 (Cont'd)

BYRON 1&2

AVERAGE WIND SPEEDS FOR EACH RELEASE MODE

<u>DOWNWIND DIRECTION</u>	<u>AVERAGE WIND SPEED (m/sec)^a</u>		
	<u>ELEVATED^b</u>	<u>MIXED MODE</u>	<u>GROUND LEVEL^b</u>
N	7.6	6.6	4.5
NNE	7.4	6.6	4.7
NE	6.8	6.2	4.6
ENE	6.5	5.8	4.5
E	6.5	5.9	4.5
ESE	6.3	5.7	4.4
SE	6.0	5.4	4.0
SSE	6.0	5.2	3.9
S	5.9	5.2	4.1
SSW	6.0	5.4	4.0
SW	6.6	6.0	4.6
WSW	6.8	6.2	4.8
W	6.7	5.8	4.1
WNW	7.0	6.1	4.2
NW	7.0	6.0	3.9
NNW	7.2	6.2	4.2

^aBased on Byron Site Meteorological Data, January 1974 through December 1976.

^bThe elevated and ground level values are provided for reference purposes only. Routine dose calculations are performed using the mixed mode values.

TABLE 7.2-7

D/Q AT THE NEAREST MILK COW AND MEAT ANIMAL LOCATIONS WITHIN 5 MILES

DOWNWIND DIRECTION	NEAREST MILK COW D/Q(1/M**2)				NEAREST MEAT ANIMAL D/Q(1/M**2)			
	RADIUS (METERS) ^a	ELEVATED RELEASE ^b	MIXED RELEASE	GROUND RELEASE ^b	RADIUS ^c (METERS)	ELEVATED RELEASE ^b	MIXED RELEASE	GROUND RELEASE ^b
N	8000.	1.096-10	1.654-10	3.889-10	1900.	9.553-10	1.637-09	4.827-09
NNE	8000.	1.154-10	1.559-10	3.534-10	2600.	6.727-10	9.430-10	2.536-09
NE	3400.	3.974-10	5.217-10	1.306-09	1800.	9.298-10	1.320-09	3.956-09
ENE	8000.	9.768-11	1.153-10	2.425-10	2400.	6.303-10	7.382-10	2.003-09
E	8000.	1.320-10	1.396-10	2.679-10	1900.	1.142-09	1.234-09	3.325-09
ESE	5100.	2.606-10	2.858-10	5.593-10	2400.	8.078-10	8.659-10	2.079-09
SE	5300.	2.142-10	2.457-10	5.825-10	2600.	6.320-10	7.250-10	2.016-09
SSE	8000.	8.492-11	8.853-11	2.167-10	2400.	5.458-10	5.505-10	1.789-09
S	3200.	2.047-10	2.643-10	9.242-10	1300.	5.683-10	8.863-10	4.357-09
SSW	8000.	5.310-11	5.919-11	1.460-10	2600.	3.063-10	3.337-10	1.048-09
SW	8000.	6.287-11	7.647-11	1.555-10	1400.	7.322-10	1.005-09	3.247-09
WSW	8000.	6.026-11	8.062-11	1.754-10	1400.	6.850-10	1.072-09	3.664-09
W	3100.	2.384-10	3.076-10	8.458-10	3200.	2.269-10	2.929-10	8.006-10
WNW	5300.	1.211-10	1.420-10	2.853-10	2600.	3.586-10	4.207-10	9.875-10
NW	5100.	1.403-10	1.609-10	3.538-10	2300.	4.608-10	5.327-10	1.417-09
NNW	8000.	9.475-11	1.167-10	2.374-10	2400.	6.155-10	7.804-10	1.961-09

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

^aApproximate distance from center of plant as determined by annual census.

^bThe elevated and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode release data.

^cApproximate distance from center of plant per ER Table Q470.2-1 (Amendment 2, September 1981).

TABLE 7.2-8

BYRON 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 83M

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED (STACK) RELEASE*			MIXED MODE (VENT) RELEASE			GROUND LEVEL RELEASE*		
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	SBAR (UCI/SEC)	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	VBAR (UCI/SEC)	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)	GBAR (UCI/SEC)
N	1875.	1875.	1.068-05	9.648-07	1875.	2.360-05	2.131-06	1875.	1.079-04	9.740-06
NNE	1829.	1829.	1.192-05	1.076-06	1829.	1.901-05	1.716-06	1829.	9.390-05	8.479-06
NE	1585.	1585.	1.074-05	9.697-07	1585.	1.846-05	1.667-06	1585.	9.516-05	8.593-06
ENE	1234.	1234.	1.132-05	1.022-06	1234.	2.034-05	1.836-06	1234.	1.229-04	1.110-05
E	1227.	1227.	1.281-05	1.157-06	1227.	2.482-05	2.241-06	1227.	1.536-04	1.387-05
ESE	991.	991.	1.432-05	1.293-06	991.	3.026-05	2.733-06	991.	1.894-04	1.710-05
SE	1006.	1006.	1.251-05	1.130-06	1006.	4.172-05	3.767-06	1006.	2.811-04	2.539-05
SSE	800.	800.	1.120-05	1.011-06	800.	3.735-05	3.372-06	800.	2.846-04	2.570-05
S	945.	945.	8.389-06	7.575-07	945.	2.134-05	1.927-06	945.	1.568-04	1.416-05
SSW	975.	975.	7.085-06	6.397-07	975.	1.572-05	1.420-06	975.	1.124-04	1.015-05
SW	1067.	1067.	8.135-06	7.346-07	1067.	1.503-05	1.357-06	1067.	9.529-05	8.605-06
WSW	1212.	1212.	6.862-06	6.196-07	1212.	1.470-05	1.327-06	1212.	8.648-05	7.809-06
W	1189.	1189.	6.732-06	6.079-07	1189.	1.549-05	1.399-06	1189.	9.002-05	8.129-06
WNW	1227.	1227.	6.640-06	5.996-07	1227.	1.360-05	1.228-06	1227.	7.786-05	7.031-06
NW	1128.	1128.	7.413-06	6.694-07	1128.	1.635-05	1.476-06	1128.	9.772-05	8.824-06
NNW	1044.	1044.	1.074-05	9.694-07	1044.	3.265-05	2.948-06	1044.	1.696-04	1.531-05

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

7.2-9

BYRON

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TABLE 7.2-8 (Cont'd)

BYRON 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 85M

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED(STACK) RELEASE*			MIXED MODE(VENT) RELEASE			GROUND LEVEL RELEASE*		
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	SBAR (UCI/SEC)	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	VBAR (UCI/SEC)	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)	GBAR (UCI/SEC)
N	1875.	1875.	1.731-04	9.137-05	1875.	2.312-04	1.209-04	1875.	6.971-04	3.601-04
NNE	1829.	1829.	1.929-04	1.018-04	1829.	2.179-04	1.143-04	1829.	6.266-04	3.240-04
NE	1585.	1585.	1.809-04	9.554-05	1585.	2.117-04	1.111-04	1585.	6.368-04	3.293-04
ENE	1234.	1234.	2.207-04	1.168-04	1234.	2.398-04	1.259-04	1234.	7.650-04	3.948-04
E	1227.	1227.	2.297-04	1.214-04	1227.	2.644-04	1.385-04	1227.	9.340-04	4.814-04
ESE	991.	991.	2.964-04	1.569-04	991.	3.331-04	1.747-04	991.	1.103-03	5.681-04
SE	1006.	1006.	2.697-04	1.428-04	1006.	3.675-04	1.917-04	1006.	1.569-03	8.060-04
SSE	800.	800.	2.787-04	1.478-04	800.	3.457-04	1.806-04	800.	1.498-03	7.684-04
S	945.	945.	2.116-04	1.122-04	945.	2.348-04	1.232-04	945.	8.918-04	4.589-04
SSW	975.	975.	1.668-04	8.844-05	975.	1.800-04	9.449-05	975.	6.584-04	3.392-04
SW	1067.	1067.	1.795-04	9.508-05	1067.	1.803-04	9.473-05	1067.	5.698-04	2.937-04
WSW	1212.	1212.	1.345-04	7.119-05	1212.	1.579-04	8.276-05	1212.	5.225-04	2.694-04
W	1189.	1189.	1.363-04	7.215-05	1189.	1.653-04	8.663-05	1189.	5.437-04	2.803-04
WNW	1227.	1227.	1.280-04	6.773-05	1227.	1.442-04	7.557-05	1227.	4.705-04	2.426-04
NW	1128.	1128.	1.468-04	7.767-05	1128.	1.693-04	8.868-05	1128.	5.778-04	2.977-04
NNW	1044.	1044.	2.172-04	1.149-04	1044.	2.891-04	1.509-04	1044.	9.390-04	4.827-04

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

7.2-10

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TABLE 7.2-8 (Cont'd)

BYRON 1&2

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 85

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED (STACK) RELEASE*			MIXED MODE (VENT) RELEASE			GROUND LEVEL RELEASE*		
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	SBAR (UCI/SEC)	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	VBAR (UCI/SEC)	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)	GBAR (UCI/SEC)
N	1875.	1875.	2.036-06	1.260-06	1875.	2.723-06	1.686-06	1875.	7.846-06	4.857-06
NNE	1829.	1829.	2.270-06	1.405-06	1829.	2.598-06	1.608-06	1829.	7.093-06	4.390-06
NE	1585.	1585.	2.140-06	1.325-06	1585.	2.532-06	1.568-06	1585.	7.221-06	4.470-06
ENE	1234.	1234.	2.612-06	1.617-06	1234.	2.865-06	1.773-06	1234.	8.564-06	5.301-06
E	1227.	1227.	2.712-06	1.678-06	1227.	3.151-06	1.951-06	1227.	1.050-05	6.502-06
ESE	991.	991.	3.523-06	2.181-06	991.	3.971-06	2.458-06	991.	1.222-05	7.566-06
SE	1006.	1006.	3.204-06	1.983-06	1006.	4.330-06	2.680-06	1006.	1.749-05	1.082-05
SSE	800.	800.	3.322-06	2.057-06	800.	4.080-06	2.526-06	800.	1.654-05	1.024-05
S	945.	945.	2.530-06	1.566-06	945.	2.796-06	1.730-06	945.	9.827-06	6.083-06
SSW	975.	975.	1.989-06	1.231-06	975.	2.145-06	1.328-06	975.	7.266-06	4.498-06
SW	1067.	1067.	2.130-06	1.318-06	1067.	2.148-06	1.329-06	1067.	6.312-06	3.907-06
WSW	1212.	1212.	1.585-06	9.814-07	1212.	1.860-06	1.151-06	1212.	5.812-06	3.597-06
W	1189.	1189.	1.619-06	1.002-06	1189.	1.960-06	1.213-06	1189.	6.043-06	3.741-06
WNW	1227.	1227.	1.513-06	9.366-07	1227.	1.708-06	1.057-06	1227.	5.251-06	3.250-06
NW	1128.	1128.	1.733-06	1.073-06	1128.	1.999-06	1.238-06	1128.	6.410-06	3.968-06
NNW	1044.	1044.	2.568-06	1.590-06	1044.	3.374-06	2.089-06	1044.	1.032-05	6.390-06

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

7.2-11

BYRON

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TABLE 7.2-8 (Cont'd)

BYRON 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 87

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED(STACK) RELEASE*		MIXED MODE(VENT) RELEASE			GROUND LEVEL RELEASE*			
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	SBAR	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	VBAR	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)	GBAR
N	1875.	1875.	5.961-04	4.327-04	1875.	7.713-04	5.596-04	1875.	2.020-03	1.459-03
NNE	1829.	1829.	6.620-04	4.806-04	1829.	7.460-04	5.417-04	1829.	1.807-03	1.305-03
NE	1585.	1585.	6.270-04	4.551-04	1585.	7.268-04	5.278-04	1585.	1.848-03	1.335-03
ENE	1234.	1234.	7.768-04	5.640-04	1234.	8.465-04	6.151-04	1234.	2.256-03	1.629-03
E	1227.	1227.	8.045-04	5.841-04	1227.	9.119-04	6.623-04	1227.	2.713-03	1.958-03
ESE	991.	991.	1.053-03	7.646-04	991.	1.178-03	8.562-04	991.	3.265-03	2.357-03
SE	1006.	1006.	9.613-04	6.980-04	1006.	1.248-03	9.055-04	1006.	4.539-03	3.277-03
SSE	800.	800.	1.005-03	7.299-04	800.	1.214-03	8.819-04	800.	4.446-03	3.209-03
S	945.	945.	7.550-04	5.482-04	945.	8.365-04	6.079-04	945.	2.654-03	1.916-03
SSW	975.	975.	5.964-04	4.330-04	975.	6.421-04	4.666-04	975.	1.964-03	1.418-03
SW	1067.	1067.	6.390-04	4.639-04	1067.	6.471-04	4.703-04	1067.	1.696-03	1.225-03
WSW	1212.	1212.	4.785-04	3.474-04	1212.	5.538-04	4.021-04	1212.	1.555-03	1.123-03
W	1189.	1189.	4.779-04	3.469-04	1189.	5.759-04	4.182-04	1189.	1.620-03	1.170-03
WNW	1227.	1227.	4.526-04	3.286-04	1227.	5.040-04	3.660-04	1227.	1.388-03	1.002-03
NW	1128.	1128.	5.203-04	3.778-04	1128.	5.944-04	4.316-04	1128.	1.723-03	1.244-03
NNW	1044.	1044.	7.732-04	5.614-04	1044.	9.980-04	7.242-04	1044.	2.811-03	2.029-03

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

7.2-12

BYRON

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TABLE 7.2-8 (Cont'd)

BYRON 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 89

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED(STACK) RELEASE*		MIXED MODE(VENT) RELEASE		GROUND LEVEL RELEASE*	
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)
N	1875.	1.463-03	1.122-03	1875.	1.915-03	1875.	5.038-03
NNE	1829.	1.629-03	1.249-03	1829.	1.856-03	1829.	4.538-03
NE	1585.	1.537-03	1.179-03	1585.	1.809-03	1585.	4.623-03
ENE	1234.	1.893-03	1.453-03	1234.	2.091-03	1234.	5.545-03
E	1227.	1.965-03	1.508-03	1227.	2.266-03	1227.	6.740-03
ESE	991.	2.561-03	1.966-03	991.	2.906-03	991.	7.965-03
SE	1006.	2.334-03	1.792-03	1006.	3.087-03	1006.	1.123-02
SSE	800.	2.426-03	1.863-03	800.	2.975-03	800.	1.078-02
S	945.	1.835-03	1.410-03	945.	2.055-03	945.	6.429-03
SSW	975.	1.448-03	1.112-03	975.	1.578-03	975.	4.760-03
SW	1067.	1.500-03	1.190-03	1067.	1.586-03	1067.	4.122-03
WSW	1212.	1.156-03	8.876-04	1212.	1.352-03	1212.	3.787-03
W	1189.	1.170-03	8.978-04	1189.	1.420-03	1189.	3.944-03
WNW	1227.	1.100-03	8.444-04	1227.	1.238-03	1227.	3.404-03
NW	1128.	1.263-03	9.695-04	1128.	1.455-03	1128.	4.196-03
NNW	1044.	1.874-03	1.439-03	1044.	2.432-03	1044.	6.779-03

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

TABLE 7.2-8 (Cont'd)

BYRON 1&2

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 89

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED(STACK) RELEASE*			MIXED MODE(VENT) RELEASE			GROUND LEVEL RELEASE*		
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	SBAR (UCI/SEC)	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	VBAR (UCI/SEC)	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)	GBAR (UCI/SEC)
N	1875.	1875.	4.111-04	3.010-04	1875.	4.062-04	2.974-04	1875.	5.990-04	4.364-04
NNE	1829.	1829.	4.422-04	3.237-04	1829.	4.105-04	3.007-04	1829.	5.406-04	3.939-04
NE	1585.	1585.	4.341-04	3.178-04	1585.	4.221-04	3.093-04	1585.	6.219-04	4.532-04
ENE	1234.	1234.	6.185-04	4.529-04	1234.	5.854-04	4.292-04	1234.	9.721-04	7.080-04
E	1227.	1227.	6.462-04	4.731-04	1227.	5.883-04	4.313-04	1227.	1.008-03	7.343-04
ESE	991.	991.	9.327-04	6.830-04	991.	8.838-04	6.482-04	991.	1.599-03	1.165-03
SE	1006.	1006.	8.489-04	6.216-04	1006.	8.077-04	5.923-04	1006.	1.616-03	1.177-03
SSE	800.	800.	9.994-04	7.319-04	800.	9.545-04	7.001-04	800.	2.238-03	1.630-03
S	945.	945.	6.409-04	4.693-04	945.	6.336-04	4.646-04	945.	1.433-03	1.043-03
SSW	975.	975.	5.305-04	3.885-04	975.	4.979-04	3.622-04	975.	1.049-03	7.640-04
SW	1067.	1067.	5.759-04	4.217-04	1067.	5.305-04	3.889-04	1067.	8.888-04	6.473-04
WSW	1212.	1212.	4.259-04	3.118-04	1212.	4.363-04	3.196-04	1212.	7.908-04	5.759-04
W	1189.	1189.	3.744-04	2.742-04	1189.	3.891-04	2.851-04	1189.	7.491-04	5.455-04
WNW	1227.	1227.	3.884-04	2.844-04	1227.	3.632-04	2.662-04	1227.	5.733-04	4.176-04
NW	1128.	1128.	4.680-04	3.427-04	1128.	4.492-04	3.292-04	1128.	8.016-04	5.839-04
NNW	1044.	1044.	7.275-04	5.327-04	1044.	7.938-04	5.812-04	1044.	1.573-03	1.145-03

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

7.2-14

BYRON

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TABLE 7.2-8 (Cont'd)

BYRON 1&2

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 90

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED (STACK) RELEASE*			MIXED MODE (VENT) RELEASE			GROUND LEVEL RELEASE*		
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	SBAR (UCI/SEC)	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	VBAR (UCI/SEC)	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)	GBAR (UCI/SEC)
N	1875.	1875.	1.125-05	7.998-06	1875.	7.471-06	5.312-06	1875.	4.324-06	3.054-06
NNE	1829.	1829.	1.194-05	8.481-06	1829.	8.361-06	5.945-06	1829.	5.383-06	3.802-06
NE	1585.	1585.	1.460-05	1.038-05	1585.	1.163-05	8.268-06	1585.	9.069-06	6.405-06
ENE	1234.	1234.	3.604-05	2.562-05	1234.	2.752-05	1.957-05	1234.	2.745-05	1.938-05
E	1227.	1227.	4.020-05	2.857-05	1227.	3.081-05	2.190-05	1227.	3.305-05	2.334-05
ESE	991.	991.	8.655-05	6.154-05	991.	6.939-05	4.938-05	991.	7.290-05	5.146-05
SE	1006.	1006.	6.896-05	4.903-05	1006.	5.360-05	3.814-05	1006.	6.719-05	4.743-05
SSE	800.	800.	1.246-04	8.864-05	800.	9.173-05	6.532-05	800.	1.368-04	9.654-05
S	945.	945.	5.623-05	3.999-05	945.	4.379-05	3.117-05	945.	6.024-05	4.250-05
SSW	975.	975.	4.486-05	3.190-05	975.	3.367-05	2.396-05	975.	3.851-05	2.717-05
SW	1067.	1067.	4.947-05	3.517-05	1067.	3.940-05	2.800-05	1067.	3.895-05	2.749-05
WSW	1212.	1212.	2.878-05	2.046-05	1212.	2.504-05	1.779-05	1212.	2.607-05	1.840-05
W	1189.	1189.	2.728-05	1.939-05	1189.	2.031-05	1.445-05	1189.	1.678-05	1.184-05
WNW	1227.	1227.	2.812-05	1.999-05	1227.	1.958-05	1.393-05	1227.	1.374-05	9.700-06
NW	1128.	1128.	3.999-05	2.844-05	1128.	2.696-05	1.919-05	1128.	1.820-05	1.285-05
NNW	1044.	1044.	7.876-05	5.601-05	1044.	5.964-05	4.241-05	1044.	4.889-05	3.450-05

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

7.2-15

BYRON

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TABLE 7.2-8 (Cont'd)

BYRON 182

MAXIMUM OFF-SITE FINITE PLUME GAMMA DOSE FACTORS FOR XE131M

DOWNDIR DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED(STACK) RELEASE*		MIXED MODE(VENT) RELEASE		GROUND LEVEL RELEASE*	
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)
N	1875.	1.246-05	2.765-06	1875.	2.486-05	1875.	1.076-04
NNE	1829.	1.390-05	3.085-06	1829.	2.061-05	1829.	9.491-05
NE	1585.	1.266-05	2.858-06	1585.	2.015-05	1585.	9.597-05
ENE	1234.	1.386-05	3.340-06	1234.	2.206-05	1234.	1.200-04
E	1227.	1.529-05	3.554-06	1227.	2.669-05	1227.	1.516-04
ESE	991.	1.790-05	4.420-06	991.	3.223-05	991.	1.817-04
SE	1006.	1.581-05	3.977-06	1006.	4.314-05	1006.	2.728-04
SSE	800.	1.488-05	3.975-06	800.	3.820-05	800.	2.676-04
S	945.	1.130-05	3.026-06	945.	2.253-05	945.	1.485-04
SSW	975.	9.262-06	2.415-06	975.	1.677-05	975.	1.069-04
SW	1067.	1.036-05	2.632-06	1067.	1.612-05	1067.	9.124-05
WSW	1212.	8.352-06	2.022-06	1212.	1.541-05	1212.	8.326-05
W	1189.	8.405-06	2.053-06	1189.	1.626-05	1189.	8.633-05
WNW	1227.	8.095-06	1.941-06	1227.	1.428-05	1227.	7.531-05
NW	1128.	9.101-06	2.208-06	1128.	1.697-05	1128.	9.340-05
NNW	1044.	1.327-05	3.248-06	1044.	3.270-05	1044.	1.590-04

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

TABLE 7.2-8 (Cont'd)

BYRON 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR XE133M

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED(STACK) RELEASE *		MIXED MODE(VENT) RELEASE			GROUND LEVEL RELEASE*			
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	SBAR	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	VBAR	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)	CSAR
N	1875	1875	3.363-05	1.394-05	1875	5.333-05	1.932-05	1875	1.943-04	6.113-05
NNE	1829	1829	3.752-05	1.556-05	1829	4.741-05	1.800-05	1829	1.731-04	5.498-05
NE	1585	1585	3.478-05	1.454-05	1585	4.620-05	1.750-05	1585	1.752-04	5.574-05
ENE	1234	1234	4.075-05	1.757-05	1234	5.142-05	1.967-05	1234	2.145-04	6.680-05
E	1227	1227	4.331-05	1.836-05	1227	5.919-05	2.194-05	1227	2.676-04	8.228-05
ESE	991	991	5.398-05	2.352-05	991	7.295-05	2.740-05	991	3.175-04	9.660-05
SE	1006	1006	4.861-05	2.135-05	1006	8.827-05	3.089-05	1006	4.672-04	1.392-04
SSE	800	800	4.869-05	2.190-05	800	8.037-05	2.871-05	800	4.516-04	1.323-04
S	945	945	3.706-05	1.669-05	945	5.119-05	1.927-05	945	2.580-04	7.798-05
SSW	975	975	2.955-05	1.317-05	975	3.875-05	1.474-05	975	1.877-04	5.737-05
SW	1067	1067	3.218-05	1.419-05	1067	3.809-05	1.469-05	1067	1.613-04	4.964-05
WSW	1212	1212	2.468-05	1.066-05	1212	3.466-05	1.296-05	1212	1.476-04	4.555-05
W	1189	1189	2.505-05	1.085-05	1189	3.649-05	1.362-05	1189	1.532-04	4.735-05
WNW	1227	1227	2.368-05	1.018-05	1227	3.190-05	1.188-05	1227	1.334-04	4.114-05
NW	1128	1128	2.695-05	1.165-05	1128	3.763-05	1.394-05	1128	1.645-04	5.042-05
NNW	1044	1044	3.966-05	1.722-05	1044	6.793-05	2.403-05	1044	2.741-04	8.213-05

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

7.2-17

BYRON

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TABLE 7.2-8 (Cont'd)

BYRON 1&2

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR XE133

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED (STACK) RELEASE *			MIXED MODE (VENT) RELEASE			GROUND LEVEL RELEASE *		
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	SBAR (UCI/SEC)	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	VBAR (UCI/SEC)	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)	GBAR (UCI/SEC)
N	1875.	1875.	3.840-05	1.340-05	1875.	5.939-05	1.898-05	1875.	2.194-04	6.492-05
NNE	1829.	1829.	4.286-05	1.496-05	1829.	5.269-05	1.731-05	1829.	1.959-04	5.833-05
NE	1585.	1585.	3.988-05	1.400-05	1585.	5.143-05	1.689-05	1585.	1.984-04	5.917-05
ENE	1234.	1234.	4.709-05	1.686-05	1234.	5.671-05	1.869-05	1234.	2.420-04	7.119-05
E	1227.	1227.	4.980-05	1.764-05	1227.	6.529-05	2.111-05	1227.	3.006-04	8.769-05
ESE	991.	991.	6.263-05	2.259-05	991.	8.019-05	2.611-05	991.	3.550-04	1.028-04
SE	1006.	1006.	5.653-05	2.049-05	1006.	9.677-05	3.015-05	1006.	5.192-04	1.482-04
SSE	800.	800.	5.700-05	2.099-05	800.	8.759-05	2.759-05	800.	4.987-04	1.406-04
S	945.	945.	4.348-05	1.603-05	945.	5.614-05	1.829-05	945.	2.878-04	8.294-05
SSW	975.	975.	3.458-05	1.266-05	975.	4.257-05	1.397-05	975.	2.102-04	6.104-05
SW	1067.	1067.	3.747-05	1.362-05	1067.	4.193-05	1.389-05	1067.	1.812-04	5.290-05
WSW	1212.	1212.	2.855-05	1.024-05	1212.	3.836-05	1.248-05	1212.	1.660-04	4.857-05
W	1189.	1189.	2.899-05	1.042-05	1189.	4.030-05	1.309-05	1189.	1.724-04	5.046-05
WNW	1227.	1227.	2.729-05	9.752-06	1227.	3.529-05	1.145-05	1227.	1.500-04	4.385-05
NW	1128.	1128.	3.111-05	1.116-05	1128.	4.149-05	1.341-05	1128.	1.843-04	5.362-05
NNW	1044.	1044.	4.589-05	1.650-05	1044.	7.478-05	2.349-05	1044.	3.053-04	8.751-05

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

7.2-18

BYRON

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TABLE 7.2-8 (Cont'd)

BYRON 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR XE135M

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED(STACK) RELEASE *			MIXED MODE(VENT) RELEASE			GROUND LEVEL RELEASE *		
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	SBAR	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	VBAR	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)	GBAR
N	1875	1875	2.796-04	1.722-04	1875	3.384-04	2.079-04	1875	8.143-04	4.977-04
NNE	1829	1829	3.068-04	1.890-04	1829	3.264-04	2.007-04	1829	7.058-04	4.315-04
NE	1585	1585	2.939-04	1.811-04	1585	3.169-04	1.949-04	1585	7.313-04	4.472-04
ENE	1234	1234	3.759-04	2.318-04	1234	3.860-04	2.375-04	1234	9.739-04	5.951-04
E	1227	1227	3.865-04	2.382-04	1227	4.000-04	2.460-04	1227	1.093-03	6.676-04
ESE	991	991	5.161-04	3.183-04	991	5.411-04	3.329-04	991	1.468-03	8.960-04
SE	1006	1006	4.750-04	2.930-04	1006	5.507-04	3.383-04	1006	1.848-03	1.127-03
SSE	800	800	5.132-04	3.167-04	800	5.734-04	3.523-04	800	2.056-03	1.254-03
S	945	945	3.686-04	2.275-04	945	3.920-04	2.411-04	945	1.245-03	7.597-04
SSW	975	975	2.949-04	1.820-04	975	3.006-04	1.849-04	975	9.205-04	5.619-04
SW	1067	1067	3.176-04	1.959-04	1067	3.096-04	1.905-04	1067	7.812-04	4.771-04
WSW	1212	1212	2.419-04	1.492-04	1212	2.676-04	1.645-04	1212	7.102-04	4.338-04
W	1189	1189	2.263-04	1.396-04	1189	2.643-04	1.625-04	1189	7.371-04	4.502-04
WNW	1227	1227	2.227-04	1.373-04	1227	2.357-04	1.449-04	1227	6.060-04	3.700-04
NW	1128	1128	2.585-04	1.594-04	1128	2.829-04	1.739-04	1128	7.847-04	4.791-04
NNW	1044	1044	3.874-04	2.390-04	1044	4.860-04	2.984-04	1044	1.358-03	8.285-04

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

7.2-19

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TABLE 7.2-8 (Cont'd)

BYRON 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR XE135

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED (STACK) RELEASE *		MIXED MODE (VENT) RELEASE			GROUND LEVEL RELEASE *			
		RADIUS ** (METERS)	S (MRAD/YR)/(UCI/SEC)	SBAR (UCI/SEC)	RADIUS ** (METERS)	V (MRAD/YR)/(UCI/SEC)	VBAR (UCI/SEC)	RADIUS ** (METERS)	G (MRAD/YR)/(UCI/SEC)	GBAR (UCI/SEC)
N	1875.	1875.	2.405-04	1.297-04	1875.	3.197-04	1.721-04	1875.	9.558-04	5.129-04
NNE	1829.	1829.	2.681-04	1.446-04	1829.	3.023-04	1.628-04	1829.	8.615-04	4.624-04
NE	1585.	1585.	2.515-04	1.356-04	1585.	2.937-04	1.582-04	1585.	8.750-04	4.697-04
ENE	1234.	1234.	3.067-04	1.655-04	1234.	3.321-04	1.789-04	1234.	1.044-03	5.601-04
E	1227.	1227.	3.190-04	1.721-04	1227.	3.661-04	1.972-04	1227.	1.277-03	6.849-04
ESE	991.	991.	4.121-04	2.224-04	991.	4.604-04	2.480-04	991.	1.499-03	8.037-04
SE	1006.	1006.	3.749-04	2.024-04	1006.	5.064-04	2.724-04	1006.	2.135-03	1.144-03
SSE	800.	800.	3.875-04	2.092-04	800.	4.754-04	2.559-04	800.	2.025-03	1.085-03
S	945.	945.	2.948-04	1.591-04	945.	3.243-04	1.747-04	945.	1.208-03	6.479-04
SSW	975.	975.	2.322-04	1.253-04	975.	2.488-04	1.340-04	975.	8.930-04	4.789-04
SW	1067.	1067.	2.495-04	1.347-04	1067.	2.492-04	1.343-04	1067.	7.741-04	4.152-04
WSW	1212.	1212.	1.866-04	1.007-04	1212.	2.176-04	1.172-04	1212.	7.108-04	3.813-04
W	1189.	1189.	1.898-04	1.024-04	1189.	2.283-04	1.230-04	1189.	7.393-04	3.966-04
WNW	1227.	1227.	1.778-04	9.593-05	1227.	1.991-04	1.072-04	1227.	6.410-04	4.439-04
NW	1123.	1128.	2.038-04	1.100-04	1128.	2.333-04	1.257-04	1128.	7.849-04	4.210-04
NNW	1044.	1044.	3.015-04	1.627-04	1044.	3.966-04	2.134-04	1044.	1.270-03	6.806-04

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

7.2-20

BYRON

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TABLE 7.2-8 (Cont'd)

BYRON 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR XE137

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED (STACK) RELEASE*			MIXED MODE (VENT) RELEASE			GROUND LEVEL RELEASE*		
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	SBAR (UCI/SEC)	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	VBAR (UCI/SEC)	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)	GBAR (UCI/SEC)
N	1875.	1875.	6.446-05	4.157-05	1875.	6.592-05	4.251-05	1875.	1.103-04	7.093-05
NNE	1829.	1829.	6.951-05	4.483-05	1829.	6.574-05	4.241-05	1829.	9.777-05	6.288-05
NE	1585.	1585.	6.795-05	4.382-05	1585.	6.656-05	4.294-05	1585.	1.097-04	7.055-05
ENE	1234.	1234.	9.459-05	6.101-05	1234.	8.954-05	5.779-05	1234.	1.663-04	1.069-04
E	1227.	1227.	9.821-05	6.335-05	1227.	8.967-05	5.787-05	1227.	1.718-04	1.105-04
ESE	991.	991.	1.392-04	8.980-05	991.	1.318-04	8.509-05	991.	2.672-04	1.718-04
SE	1006.	1006.	1.274-04	8.220-05	1006.	1.270-04	7.874-05	1006.	2.747-04	1.766-04
SSE	800.	800.	1.477-04	9.525-05	800.	1.416-04	9.140-05	800.	3.742-04	2.405-04
S	945.	945.	9.657-05	6.229-05	945.	9.542-05	6.158-05	945.	2.396-04	1.540-04
SSW	975.	975.	7.956-05	5.152-05	975.	7.406-05	4.780-05	975.	1.762-04	1.133-04
SW	1067.	1067.	8.635-05	5.570-05	1067.	7.944-05	5.126-05	1067.	1.488-04	9.566-05
WSW	1212.	1212.	6.460-05	4.167-05	1212.	6.650-05	4.290-05	1212.	1.335-04	8.585-05
W	1189.	1189.	5.686-05	3.667-05	1189.	6.009-05	3.876-05	1189.	1.295-04	8.323-05
WNW	1227.	1227.	5.870-05	3.786-05	1227.	5.565-05	3.591-05	1227.	9.980-05	6.416-05
NW	1128.	1128.	7.014-05	4.524-05	1128.	6.848-05	4.418-05	1128.	1.380-04	8.876-05
NNW	1044.	1044.	1.081-04	6.974-05	1044.	1.210-04	7.804-05	1044.	2.661-04	1.711-04

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

7.2-21

BYRON

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TABLE 7.2-8 (Cont'd)

BYRON 1&2

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR Xe138

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED (STACK) RELEASE *			MIXED MODE (VENT) RELEASE			GROUND LEVEL RELEASE *		
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	SBAR (UCI/SEC)	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	VBAR (UCI/SEC)	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)	GBAR (UCI/SEC)
N	1875.	1875.	6.240-04	4.500-04	1875.	7.439-04	5.360-04	1875.	1.674-03	1.198-03
NNE	1829.	1829.	6.841-04	4.933-04	1829.	7.254-04	5.233-04	1829.	1.453-03	1.040-03
NE	1585.	1585.	6.543-04	4.719-04	1585.	7.055-04	5.091-04	1585.	1.503-03	1.076-03
ENE	1234.	1234.	8.415-04	6.071-04	1234.	8.693-04	6.278-04	1234.	2.004-03	1.434-03
E	1227.	1227.	8.652-04	6.242-04	1227.	8.955-04	6.465-04	1227.	2.238-03	1.601-03
ESE	991.	991.	1.159-03	8.362-04	991.	1.220-03	8.809-04	991.	3.025-03	2.163-03
SE	1006.	1006.	1.067-03	7.703-04	1006.	1.224-03	8.832-04	1006.	3.766-03	2.693-03
SSE	800.	800.	1.155-03	8.336-04	800.	1.288-03	9.298-04	800.	4.217-03	3.014-03
S	945.	945.	8.264-04	5.965-04	945.	8.839-04	6.382-04	945.	2.567-03	1.835-03
SSW	975.	975.	6.624-04	4.782-04	975.	6.789-04	4.903-04	975.	1.901-03	1.359-03
SW	1067.	1067.	7.136-04	5.150-04	1067.	7.000-04	5.055-04	1067.	1.613-03	1.154-03
WSW	1212.	1212.	5.430-04	3.917-04	1212.	5.991-04	4.322-04	1212.	1.466-03	1.048-03
W	1189.	1189.	5.063-04	3.653-04	1189.	5.893-04	4.251-04	1189.	1.520-03	1.087-03
WNW	1227.	1227.	4.997-04	3.605-04	1227.	5.270-04	3.802-04	1227.	1.246-03	8.911-04
NW	1128.	1128.	5.810-04	4.192-04	1128.	6.331-04	4.568-04	1128.	1.622-03	1.160-03
NNW	1044.	1044.	8.715-04	6.290-04	1044.	1.077-03	7.764-04	1044.	2.807-03	2.007-03

BYRON SITE METEOROLOGICAL DATA 1/74 - 12/76

*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

7.2-22

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TABLE 7.2-8 (Cont'd)

BYRON 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR AR 41

DOWNWIND DIRECTION	RESTRICTED AREA BOUND (METERS)	ELEVATED (STACK) RELEASE*		MIXED MODE (VENT) RELEASE			GROUND LEVEL RELEASE*			
		RADIUS** (METERS)	S (MRAD/YR)/(UCI/SEC)	SBAR	RADIUS** (METERS)	V (MRAD/YR)/(UCI/SEC)	VBAR	RADIUS** (METERS)	G (MRAD/YR)/(UCI/SEC)	GBAR
N	1875.	1875.	9.166-04	6.462-04	1875.	1.194-03	8.420-04	1875.	3.209-03	2.262-03
NNF	1829.	1829.	1.019-03	7.187-04	1829.	1.151-03	8.116-04	1829.	2.878-03	2.029-03
NE	1585.	1585.	9.617-04	6.780-04	1585.	1.121-03	7.903-04	1585.	2.936-03	2.070-03
ENE	1234.	1234.	1.186-03	8.362-04	1234.	1.299-03	9.155-04	1234.	3.564-03	2.512-03
E	1227.	1227.	1.232-03	8.687-04	1227.	1.406-03	9.914-04	1227.	4.311-03	3.039-03
ESE	991.	991.	1.602-03	1.130-03	991.	1.808-03	1.274-03	991.	5.133-03	3.619-03
SE	1006.	1006.	1.460-03	1.029-03	1006.	1.929-03	1.360-03	1006.	7.203-03	5.078-03
SSE	800.	800.	1.517-03	1.069-03	800.	1.863-03	1.313-03	800.	6.975-03	4.917-03
S	945.	945.	1.145-03	8.072-04	945.	1.281-03	9.034-04	945.	4.157-03	2.930-03
SSW	975.	975.	9.040-04	6.373-04	975.	9.832-04	6.931-04	975.	3.076-03	2.168-03
SW	1067.	1067.	9.698-04	6.837-04	1067.	9.888-04	6.971-04	1067.	2.663-03	1.877-03
WSW	1212.	1212.	7.269-04	5.125-04	1212.	8.472-04	5.973-04	1212.	2.445-03	1.724-03
W	1189.	1189.	7.302-04	5.148-04	1189.	8.847-04	6.237-04	1189.	2.547-03	1.795-03
WNW	1227.	1227.	6.903-04	4.867-04	1227.	7.726-04	5.447-04	1227.	2.190-03	1.544-03
NW	1128.	1128.	7.918-04	5.582-04	1128.	9.099-04	6.415-04	1128.	2.705-03	1.907-03
NNW	1044.	1044.	1.175-03	8.284-04	1044.	1.530-03	1.078-03	1044.	4.395-03	3.099-03

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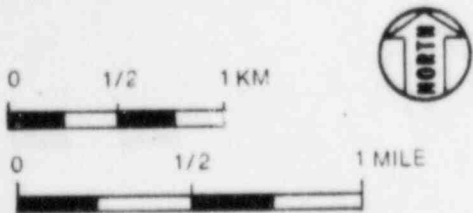
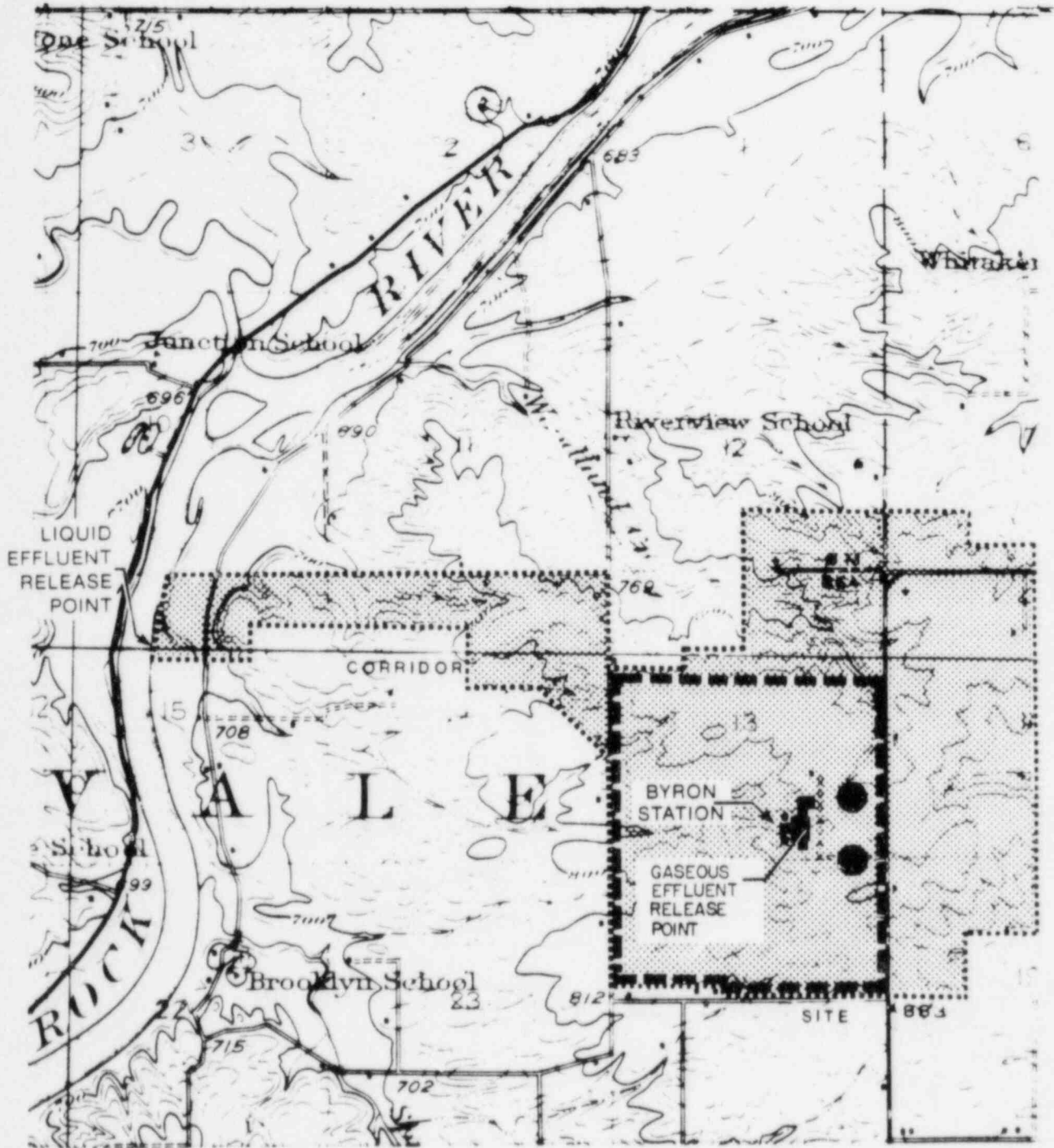
*The elevated (stack) and ground level release data are provided for reference purposes only. Routine dose calculations are performed using mixed mode (vent) release data.

**Approximate distance from midpoint between gaseous effluent release points.

7.2-23

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--- EXCLUSION AREA BOUNDARY
..... RESTRICTED AREA BOUNDARY

BYRON STATION
FIGURE 7.2-1
RESTRICTED AREA BOUNDARY

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8.0 RADIOACTIVE EFFLUENT TREATMENT SYSTEMS,
MODELS FOR SETTING GASEOUS AND LIQUID
EFFLUENT MONITOR ALARM AND TRIP SETPOINTS,
AND ENVIRONMENTAL RADIOLOGICAL MONITORING

8.1 GASEOUS RELEASES

8.1.1 System Design

8.1.1.1 Gaseous Radwaste Treatment System

A gaseous radwaste treatment system shall be any system designed and installed to reduce radioactive gaseous effluents by collecting primary coolant system off-gases from the primary system and providing for delay or holdup for the purpose of reducing the total radioactivity prior to release to the environment. Refer to Figure 8.1-1 for a simplified system flowpath diagram.

8.1.1.2 Ventilation Exhaust Treatment System

A ventilation exhaust treatment system shall be any system designed and installed to reduce gaseous radioiodine or radioactive material in particulate form in effluents by passing ventilation or vent exhaust gases through charcoal adsorbers and/or HEPA filters for the purpose of removing iodines or particulates from the gaseous exhaust stream prior to the release to the environment (such a system is not considered to have any effect on noble gas effluents). Engineered Safety Feature (ESF) atmospheric cleanup systems are not considered to be ventilation exhaust treatment system components.

8.1.2 Alarm and Trip Setpoints

Alarm and trip setpoints of gaseous effluent monitors at the principal points of release of ventilation exhaust air

containing radioactivity are established to ensure that the release limits of 10 CFR 20 are not exceeded. The set-points are found by solving Equations 2.6* and 2.7** for each class of releases.

For this equation, the radioactivity mixture in the exhaust air is assumed to have the composition of gases listed in Table 3.5-7 of the Environmental Report Operating License Stage. According to Subsection 3.5.3.4 of the report, releases of radionuclides in gaseous effluents were calculated using the PWR-GALE computer program and the parameters listed in Table 3.5-5.

Equation 2.6* is rewritten using the fractional composition of each nuclide, f_i , and a total release rate, Q_t , for station vent stack releases (the principal point of release of ventilation exhaust air containing radioactivity):

$$1.11 \sum_i [Q_{tv} (\bar{V}_i \times f_i)] < 500 \text{ mrem/yr} \quad (8.1)$$

f_i Fractional Radionuclide Composition

The release rate of radionuclide i divided by the total release of all radionuclides.

Q_{tv} Total Release Rate, Vent Release ($\mu\text{Ci/sec}$)

The release rate for all radionuclides due to a station vent stack release.

$$Q_{iv} = Q_{tv} f_i \quad (8.2)$$

Equation 8.1 can be solved for Q_{tv} for release limit determinations. Similarly, Equation 2.7** can be rewritten:

$$\sum_i \left[\bar{L}_i \left(\frac{\lambda}{Q} \right)_v Q_{tv} f_i \exp(-\lambda_i R/3600 u_v) + 1.11 \bar{V}_i Q_{tv} f_i \right] < 3000 \text{ mrem/yr} \quad (8.3)$$

* Equation 2.9 of Revision 2.

** Equation 2.10 of Revision 2.

Equation 8.3 can be solved for Q_{tv} and a corresponding release limit can be determined. The most conservative release limit from Equations 8.1 and 8.3 will be used in selecting the appropriate alarm and trip setpoints for a vent release.

The exact settings will be selected to ensure that 10 CFR 20 limits are not exceeded.

Surveillance frequencies for gaseous effluent monitors will be as stated in Table 4.3-9 of the Technical Specifications. Calibration methods will be consistent with the definitions found in Section 1.0 of the Technical Specifications.

8.1.3 Station Vent Stack Monitors

Detectors 1RE-PR028A, B, C, D, and E (particulate, low gas, iodine, high gas, and background subtraction channels, respectively) and 2RE-PR028A, B, C, D, and E monitor station vent stack effluent from the auxiliary building vent stacks.

The particulate detector utilizes a beta scintillator and has a range of 10^{-11} to 10^{-5} $\mu\text{Ci/cc}$. The low and high gas detectors utilize beta scintillators and have ranges of 10^{-6} to 10^{-2} $\mu\text{Ci/cc}$ and 10^{-2} to 10^2 $\mu\text{Ci/cc}$, respectively. The iodine detector utilizes a NaI(Tl) scintillator and has a range of 10^{-11} to 10^{-5} $\mu\text{Ci/cc}$.

Both vent stack effluent monitors feature automatic isokinetic sampling, automatic gaseous composite grab sampling, and tritium sampling.

The monitor skids with associated pumps, detectors, and local controls are located in the auxiliary building on the 477-foot elevation.

Each monitor has a microprocessor (RM-80) which utilizes digital processing techniques to analyze data and control monitor functions. Monitor data, including current radiation levels, high radiation alarms, and monitor operational status, are displayed on a CRT display (RM-11) in the main control room.

A power supply unit furnishes the positive and negative voltages for the circuits, relays, and alarm lights and provides the high voltage for the detectors. The power supply unit is located on the monitor skids. The monitors are powered by local 120-Vac instrumentation buses.

Alarm setpoint determination is addressed in Subsection 8.1.2. The release limits ($\mu\text{Ci}/\text{sec}$) obtained from Equations 8.1 and 8.3 are divided by the normal auxiliary building vent stack flow rates (cc/sec) to obtain the $\mu\text{Ci}/\text{cc}$ alarm setpoint values. Readouts for the vent stack monitors are in $\mu\text{Ci}/\text{cc}$. The cpm to $\mu\text{Ci}/\text{cc}$ conversion is accomplished by use of conversion factors in the radiation monitoring system software.

8.1.4 Containment Purge Effluent Monitors

Detectors 1RE-PR001A, B, and C (particulate, gas, and iodine channels, respectively) and 2RE-PR001A, B, and C monitor containment purge effluent discharge to the auxiliary building vent stacks for Units 1 and 2, respectively.

The particulate detector utilizes a beta scintillator and has a range of 10^{-11} to 10^{-5} $\mu\text{Ci}/\text{cc}$. The gas detector utilizes a beta scintillator and has a range of 10^{-6} to 10^{-2} $\mu\text{Ci}/\text{cc}$. The iodine detector utilizes a NaI(Tl) scintillator and has a range of 10^{-11} to 10^{-5} $\mu\text{Ci}/\text{cc}$.

The monitor skids with associated pumps, detectors, and local controls are located in the auxiliary building on the 475-foot elevation.

Each monitor has a microprocessor (RM-80) which utilizes digital processing techniques to analyze data and control monitor functions. Monitor data, including current radiation levels, high radiation alarms, and monitor operational status, are displayed on a CRT display (RM-11) in the main control room.

A power supply unit furnishes the positive and negative voltages for the circuits, relays, and alarm lights and provides the high voltage for the detectors. The power supply unit is located on the monitor skids. The monitors are powered by local 120-Vac instrumentation buses.

A containment atmosphere sample is obtained and analyzed prior to each containment purge release. The isotopic analysis results of this sample are used to determine the maximum allowed containment purge flow rate and as a basis for determining the containment purge effluent monitor setpoints.

8.1.5 Gas Decay Tank Monitors

Detectors ORE-PR002A and B (low range gas and high range gas, respectively) monitor the radiation level of the gas decay tank discharge to the auxiliary building vent stacks. Detectors ORE-PR002A and B are interlocked with valve 0GWRCV014. Automatically, on a high radiation and/or instrument failure signal from the detectors, vent valve 0GWRCV014 closes to isolate the gas decay tank discharge line.

Both the low range and high range gas detectors utilize beta scintillators and have ranges of 10^{-6} to 10^{-2} $\mu\text{Ci/cc}$ and 10^{-2} to 10^2 $\mu\text{Ci/cc}$, respectively.

The monitor skid with associated pump, detectors, and local controls is located in the auxiliary building on the 346-foot elevation.

The monitor has a microprocessor (RM-80) which utilizes digital processing techniques to analyze data and control monitor functions. Monitor data, including current radiation levels, high radiation alarms, and monitor operational status, are displayed on a CRT display (RM-11) in the main control room.

A power supply unit furnishes the positive and negative voltages for the circuits, relays, and alarm lights and provides the high voltage for the detectors. The power supply unit is located on the monitor skid. The monitor is powered by local 120-Vac instrumentation buses.

A grab sample from the gas decay tank to be released is obtained and analyzed prior to each gas decay tank discharge. The isotopic analysis results of this sample are used to determine the maximum allowed gas decay tank discharge line flow rate and as a basis for determining the gas decay tank monitor interlock and high alarm setpoints.

8.1.6 Allocation of Effluents from Common Release Points

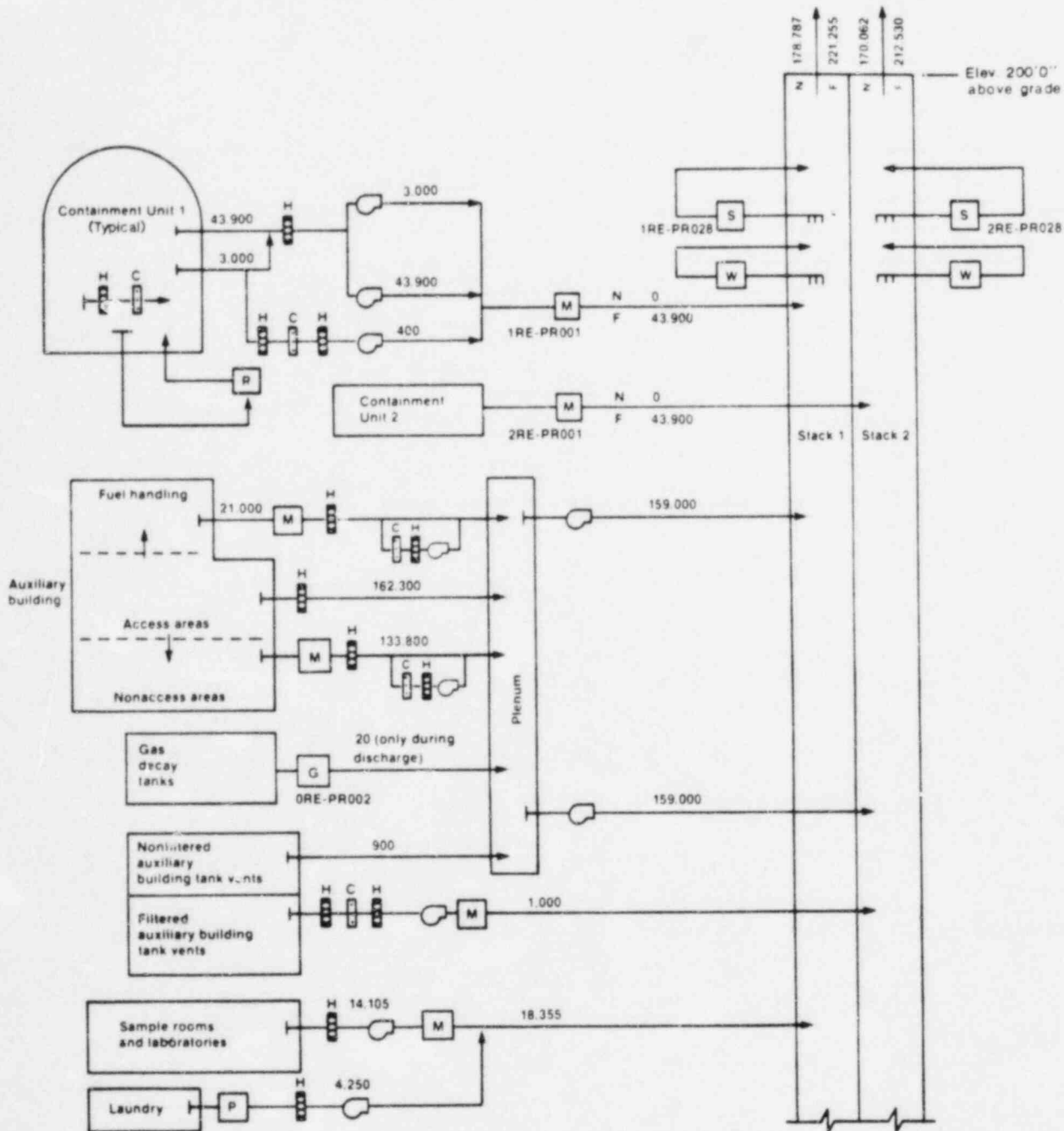
Radioactive gaseous effluents released from the auxiliary building, miscellaneous ventilation system, and the gas decay tanks are comprised of contributions from both units. Under normal operating conditions, it is difficult to apportion the radioactivity between the units. Consequently, allocation will normally be made evenly between units.

8.1.7 Symbols Used in Section 8.1

<u>SYMBOLS</u>	<u>NAME</u>	<u>UNIT</u>
Q_{tv}	Total Release Rate, Vent Release	($\mu\text{Ci}/\text{sec}$)
\bar{V}_i	Gamma Whole Body Dose Constant, Vent Release	(mrad/yr per $\mu\text{Ci}/\text{sec}$)
f_i	Fractional Radionuclide Composition	
\bar{L}_i	Beta Skin Dose Constant	(mrem/yr per $\mu\text{Ci}/\text{m}^3$)
$(X/Q)_v$	Relative Effluent Concentration, Vent Release	(sec/m^3)
λ_i	Radiological Decay Constant	(hr^{-1})
R	Downwind Range	(m)
u_v	Average Wind Speed, Vent Release	(m/sec)
Q_{iv}	Release Rate, Vent Release	($\mu\text{Ci}/\text{sec}$)
V_i	Gamma Dose Constant, Vent Release	(mrad/yr per $\mu\text{Ci}/\text{sec}$)

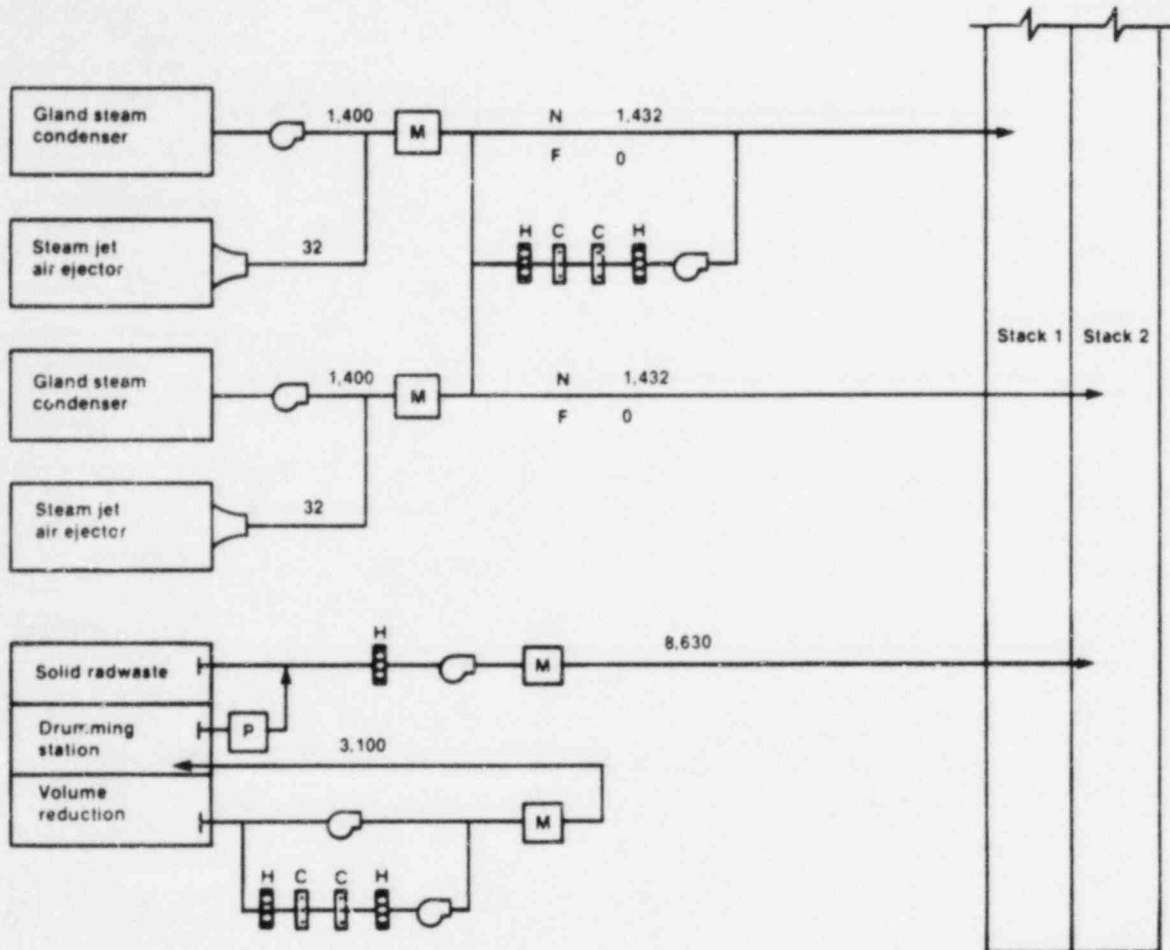
8.1.8 Constants Used in Section 8.1

<u>NUMERICAL VALUE</u>	<u>NAME</u>	<u>UNIT</u>
1.11	Conversion Constant	(mrem/mrad)
3600	Conversion Constant	(sec/hr)



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FIGURE 8.1-1
SIMPLIFIED HVAC AND
GASEOUS EFFLUENT
FLOW DIAGRAM
(SHEET 1 OF 2)



- C Charcoal filter
- F Refueling
- G Noble gas radiation monitor (offline)
- H HEPA filter
- M Three-channel radiation monitor for particulate, iodine, and noble gas (offline)
- N Normal operation
- P Particulate monitor (offline)
- R Hydrogen recombiner
- S Normal range stack radiation monitor (particulate, iodine, and noble gas)
- W Wide-range stack noble gas radiation monitor

All flow rates are cubic feet per minute

BYRON STATION

FIGURE 8.1-1
 SIMPLIFIED HVAC AND
 GASEOUS EFFLUENT
 FLOW DIAGRAM
 (SHEET 2 OF 2)

8.2 LIQUID RELEASES8.2.1 System Design

A liquid radwaste treatment system shall be a system designed and installed to reduce radioactive liquid effluents by collecting the liquids, providing for retention or holdup, and providing for treatment by demineralizer or a concentrator for the purpose of reducing the total radioactivity prior to release to the environment. Refer to Figure 8.2-1 for a simplified system flowpath diagram.

8.2.2 Alarm Setpoints

Alarm setpoints of liquid effluent monitors at the principal release points are established to ensure that the limits of 10 CFR 20 are not exceeded in the unrestricted area. Prior to each batch release, a grab sample from the release tank is obtained and analyzed. Equation 8.4 is evaluated for each radionuclide identified in the grab sample isotopic analysis results to determine the maximum allowable flow rate in the liquid radwaste discharge line.

$$F_{\max}^r = \left[\frac{\text{MPC}_i \times F_{\text{act}}^d}{C_i} \right] \div K \quad (8.4)$$

 F_{\max}^r

Maximum Permissible Flow Rate,
Radwaste Discharge

(gpm)

The maximum flow rate permitted in the liquid radwaste discharge line that meets 10 CFR 20 limits.

F_{act}^d	Actual Flow Rate, Initial Dilution Stream (gpm)
	The actual flow rate of the initial dilution stream which carries the radionuclides to the unrestricted area boundary.
MPC_i	Maximum Permissible Concentration of Radionuclide i in the Unrestricted Area (10 CFR 20, Appendix B, Table II, Column 2) ($\mu Ci/ml$)
C_i	Concentration of Radionuclide i in the Release Tank ($\mu Ci/ml$)
K	Conservatism Constant Determined by Station Procedures for Liquid Releases; $K \geq 1.0$. Division by K allows station management to provide a margin of conservatism for liquid batch releases.

After determining F_{max}^r from Equation 8.4, 10 CFR 20 compliance is verified using Equations 8.5 and 8.6.

$$C_i^a = C_i \left[\frac{F_{max}^r}{F_{max}^r + F_{act}^d} \right] \quad (8.5)$$

$C_i^a =$ Concentration of Radionuclide i in the Unrestricted Area. ($\mu Ci/ml$)

$$\sum_i \frac{C_i^a}{MPC_i} \leq 1 \quad (8.6)$$

The alarm setpoints for the liquid radwaste effluent monitor (ORE-PR001) are determined prior to each release and are based on the isotopic analysis results of the release tank grab sample. The alarm setpoints are set so that any deviations from the isotopic analysis results will result in the automatic termination of the release. Readouts for the liquid effluent monitor are in $\mu\text{Ci/ml}$. The cpm to $\mu\text{Ci/ml}$ conversion is accomplished by use of conversion factors in the radiation monitoring system software.

8.2.3 Liquid Radwaste Effluent Monitor

Radiation monitor ORE-PR001 monitors liquid radwaste effluent and is interlocked with release tank discharge valve 0WX353.

On high radiation in the liquid radwaste effluent, the release tank discharge valve is closed automatically.

The release tank (0WX01T) holds 30,000 gallons and is located in the turbine building on the 401-foot elevation.

The monitor utilizes a NaI(Tl) detector with a range for gamma radiation of 10^{-8} $\mu\text{Ci/ml}$ to 10^{-2} $\mu\text{Ci/ml}$. The monitor skid and associated features are located in the turbine building on the 401-foot elevation.

The monitor has a microprocessor (RM-80) which utilizes digital processing techniques to analyze data and control monitor functions. Monitor data, including current radiation levels, high radiation alarms, and monitor operational status, are displayed on a CRT display (RM-11) in the main control room.

A power supply unit furnishes the positive and negative voltages for the circuits, relays, and alarm lights and provides the high voltage for the detector. The power supply is located on the monitor skid. The monitor is powered from local 120-Vac instrumentation buses.

A discussion of alarm setpoints for ORE-PR001 is included in Subsection 8.2.2.

8.2.4 Station Blowdown Monitor

Radiation monitor ORE-PR010 continuously monitors the circulating water blowdown for radioactivity. The monitor utilizes a NaI(Tl) detector with a range for gamma radiation of 10^{-8} $\mu\text{Ci/ml}$ to 10^{-2} $\mu\text{Ci/ml}$. The monitor skid and associated features are located in the turbine building on the 364-foot elevation.

The monitor has a microprocessor (RM-80) which utilizes digital processing techniques to analyze data and control monitor functions. Monitor data, including current radiation levels, high radiation alarms, and monitor operational status, are displayed on a CRT display (RM-11) in the main control room.

A power supply unit furnishes the positive and negative voltages for the circuits, relays, and alarm lights and provides high voltage for the detector. The power supply is located on the monitor skid. The monitor is powered from local 120-Vac instrumentation buses.

The alarm setpoints for the station blowdown monitor are determined prior to each release and are based on the isotopic analysis results of the release tank grab sample and the actual dilution flow rates. The alarm setpoints are set so

that any deviations from the isotopic analysis results or from the specified dilution flow rate will result in an alarm from the monitor. Between batch releases, the station blowdown monitor alarm setpoints are set based upon the I-131 MPC and the average dilution flow rate.

8.2.5 Reactor Containment Fan Cooler (RCFC) and Essential Service Water Outlet Line Monitors

Radiation monitors 1RE-PR002, 2RE-PR002, 1RE-PR003, and 2RE-PR003 monitor the RCFC and essential service water outlet lines for radioactivity. The monitor utilizes a NaI(Tl) detector with a range for gamma radiation of 10^{-8} $\mu\text{Ci/ml}$ to 10^{-2} $\mu\text{Ci/ml}$. The monitor skid and associated features are located in the auxiliary building on the 401-foot elevation.

The monitor has a microprocessor (RM-80) which utilizes digital processing techniques to analyze data and control monitor functions. Monitor data, including current radiation levels, high radiation alarms, and monitor operational status, are displayed on a CRT display (RM-11) in the main control room.

A power supply unit furnishes the positive and negative voltages for the circuits, relays, and alarm lights and provides high voltage for the detector. The power supply is located on the monitor skid. The monitor is powered from local 120-Vac instrumentation buses.

During initial unit startup, alarms are set at twice background.

8.2.6 Administrative and Procedural Controls for Radwaste Discharges

Administrative and procedural controls have been designed to ensure proper control of radioactive liquid radwaste discharge in order to preclude a release in excess of 10 CFR 20 limits. The discharge rate for each batch is calculated by radiation chemistry personnel (Equation 8.4) and then provided to operating staff personnel. All liquid radwaste discharges will be from the release tank 0WX01T. On high radiation in the liquid radwaste effluent, the release tank discharge valve 0WX353 is closed automatically.

The proper valve lineup is performed by the operator prior to each batch discharge, per station procedures. The actual discharge is authorized by the shift engineer.

The system is equipped with a radiation trip point which alarms and initiates automatic valve closure on the radwaste discharge line to prevent the violation of 10 CFR 20 limits.

8.2.7 Determination of Initial Dilution Stream Flow Rates

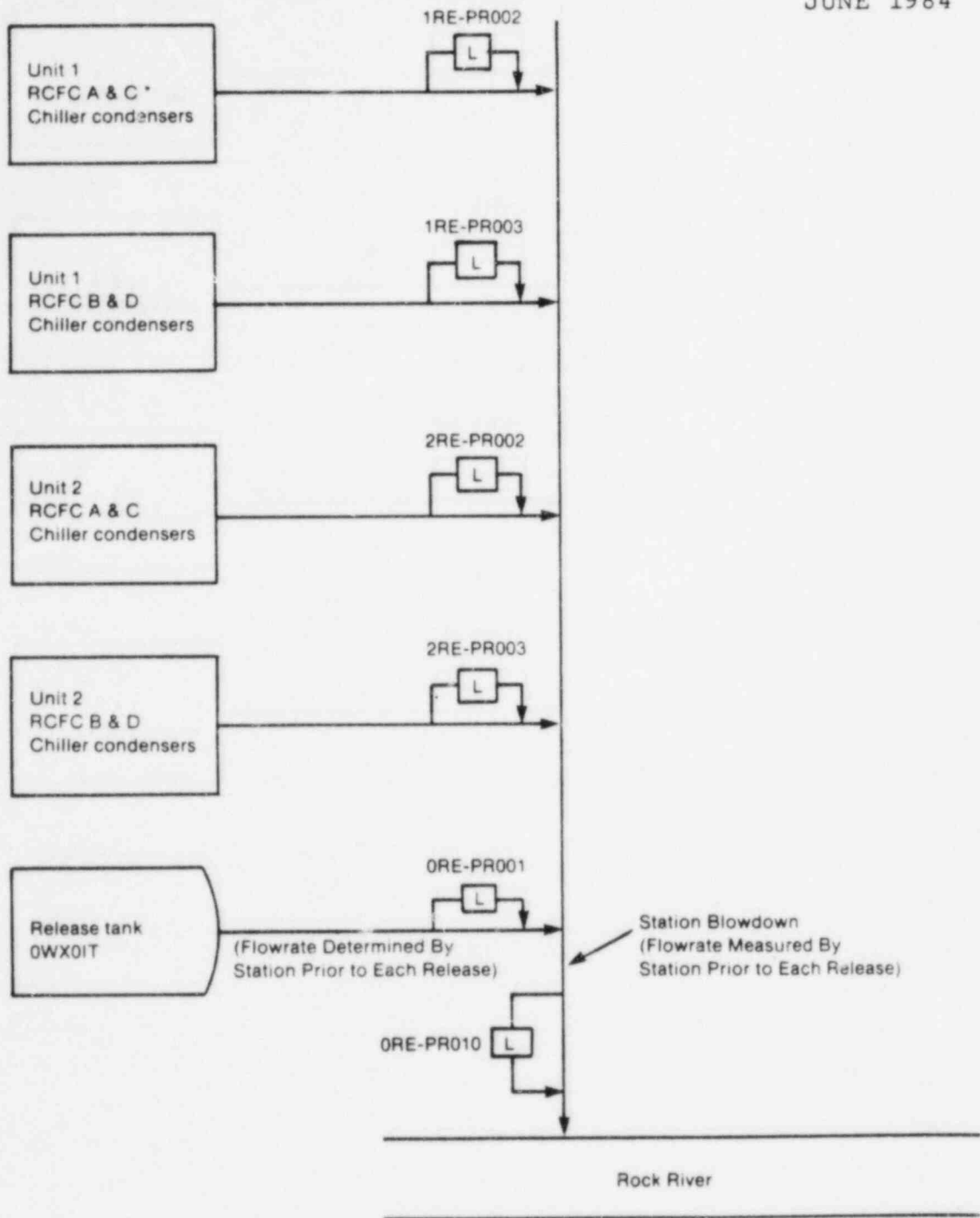
For those release paths which have installed flow monitoring instrumentation, that instrumentation will be used to determine the flow rate of the initial dilution stream. This instrumentation will be operated and maintained as prescribed by the Technical Specifications. For those release paths which do not have installed flow monitoring instrumentation, flow rates will be determined by use of appropriate engineering data such as pump curves, differential pressures, or valve position indication.

8.2.8 Allocation of Effluents from Common Release Points

Radioactive liquid effluents released from the release tank (0WX01T) are comprised of contributions from both units. Under normal operating conditions, it is difficult to apportion the radioactivity between the units. Consequently, allocation will normally be made evenly between units.

8.2.9 Symbols Used In Section 8.2

<u>SYMBOL</u>	<u>NAME</u>	<u>UNIT</u>
C_i^a	Concentration of Radionuclide i in the Unrestricted Area	($\mu\text{Ci/ml}$)
C_i	Concentration of Radionuclide i in the Release Tank	($\mu\text{Ci/ml}$)
MPC_i	Maximum Permissible Concentration of Radionuclide i in the Unrestricted Area	($\mu\text{Ci/ml}$)
F_{max}^r	Maximum Permissible Flow Rate, Radwaste Discharge	(gpm)
F_{act}^d	Actual Flow Rate, Initial Dilution Stream	(gpm)
K	Conservatism Constant Determined by Station Procedures for Liquid Releases; $K \geq 1.0$	



L = Liquid Process Radiation Monitor
RCFC = Reactor Containment Fan Cooler

*In each unit, only the A & C or B & D chiller condensers are operating at one time.

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FIGURE 8.2-1

LIQUID RELEASE FLOWPATH

8.3 SOLIDIFICATION OF WASTE/PROCESS CONTROL PROGRAM

The process control program (PCP) shall contain the sampling, analysis, and formulation determination by which solidification of radioactive wastes from liquid systems is ensured.

8.4 ENVIRONMENTAL RADIOLOGICAL MONITORING

The environmental radiological monitoring program for the environs around Byron Station is given in Table 8.4-1. Reporting levels and lower limits of detection for this program are given in Tables 8.4-2 and 8.4-3, respectively.

Figures 8.4-1, 8.4-2, and 8.4-3 show sampling and monitoring locations.

TABLE 8.4-1

ENVIRONMENTAL RADIOLOGICAL MONITORING PROGRAM^a

EXPOSURE PATHWAY AND/OR SAMPLE	SAMPLING OR MONITORING LOCATIONS	SAMPLING OR COLLECTION FREQUENCY	TYPE AND FREQUENCY OF ANALYSIS
1. <u>Direct Radiation</u>	<u>Indicators</u>	Quarterly	Gamma dose quarterly
	a. <u>Inner Ring</u>		
	101-1, 1.2 mi NNE		
	101-2, 1.2 mi NNE		
	102-1, 1.0 mi NNE		
	102-2, 1.0 mi NNE		
	103-1, 1.7 mi NE		
	103-2, 1.6 mi NE		
	104-1, 1.4 mi ENE		
	104-2, 1.4 mi ENE		
	105-1, 1.3 mi E		
	105-2, 1.3 mi E		
	106-1, 1.4 mi ESE		
	106-2, 1.4 mi ESE		
	107-1, 1.4 mi SE		
	107-2, 1.4 mi SE		
	108-1, 0.6 mi SSE		
	108-2, 0.6 mi SSE		
	109-1, 0.6 mi S		
	109-2, 0.6 mi S		
	110-1, 0.6 mi SSW		
	110-2, 0.6 mi SSW		
	111-1, 0.9 mi SW		
	111-2, 0.8 mi SW		
	112-1, 0.8 mi WSW		
	112-2, 0.7 mi WSW		
	113-1, 0.7 mi W		
	113-2, 0.7 mi W		
	114-1, 0.8 mi WNW		
	114-2, 0.8 mi WNW		
	115-1, 1.0 mi NW		
	115-2, 1.0 mi NW		
	116-1, 1.4 mi NNW		
	116-2, 1.4 mi NNW		
	b. <u>Outer Ring</u>		
	201-1, 4.8 mi N		
	201-2, 5.2 mi N		
	202-1, 4.5 mi NNE		
	202-2, 5.2 mi NNE		
	203-1, 5.1 mi NE		
	203-2, 5.1 mi NE		
	204-1, 4.2 mi ENE		
	204-2, 4.1 mi ENE		
	205-1, 3.9 mi E		
	205-2, 4.1 mi E		

TABLE 8.4-1 (Cont'd)

EXPOSURE PATHWAY AND/OR SAMPLE	SAMPLING OR MONITORING LOCATIONS	SAMPLING OR COLLECTION FREQUENCY	TYPE AND FREQUENCY OF ANALYSIS
1. <u>Direct Radiation</u> (Cont'd)	<u>Indicators</u> (Cont'd)		
	b. <u>Outer Ring</u> (Cont'd)		
	206-1, 4.2 mi ESE		
	206-2, 4.3 mi SE		
	207-1, 4.2 mi SE		
	207-2, 3.7 mi SE		
	208-1, 4.1 mi SSE		
	208-2, 3.8 mi SSE		
	209-1, 3.8 mi S		
	209-2, 3.9 mi SSW		
	210-1, 3.6 mi SSW		
	210-2, 3.6 mi SW		
	211-1, 5.2 mi SW		
	211-2, 4.8 mi WSW		
	212-1, 4.9 mi WSW		
	212-2, 5.1 mi W		
	213-1, 5.0 mi W		
	213-2, 5.2 mi WNW		
	214-1, 4.8 mi WNW		
	214-2, 5.2 mi NW		
	215-1, 5.4 mi NW		
	215-2, 5.2 mi NW		
	216-1, 4.8 mi NNW		
	216-2, 5.1 mi NNW		
	c. <u>Special Interest</u>		
	At each of the airborne pathway indicator locations specified in Part 2 of this table.		
	<u>Controls</u>		
	At each of the airborne pathway control locations specified in Part 2 of this table.		
2. <u>Airborne</u>	<u>Indicators</u>		
<u>Radioiodine and Particulates</u>	a. <u>Near Site Boundary</u>	Continuous sampler operation with sample collection weekly, or more frequently if required by dust loading.	<u>Radioiodine Canister:</u> I-131 analysis biweekly.
	BY-21, North Parking Lot, 0.27 mi N		<u>Particulate Sampler:</u>
	BY-22, CECO Real Estate Office, 0.30 mi E		a. Gross beta radioactivity analysis following filter change. ^b
	BY-23, South of Plant on Deerpath Road, 0.59 mi S		
	BY-24, Met Tower, 0.66 mi SW		
	b. <u>Near Community with Highest Calculated Annual Average Ground Level D/Q</u>		b. Gamma isotopic analysis of composite (by location) quarterly. ^c
	BY-1, Byron, 3.5 mi NNE		

TABLE 8.4-1 (Cont'd)

EXPOSURE PATHWAY AND/OR SAMPLE	SAMPLING OR MONITORING LOCATIONS	SAMPLING OR COLLECTION FREQUENCY	TYPE AND FREQUENCY OF ANALYSIS
2. <u>Airborne</u> (Cont'd)	<p><u>Indicators</u> (Cont'd)</p> <p>c. <u>Other</u></p> <p>BY-2, Stillman Valley, 6.2 mi NE</p> <p>BY-3, Nearsite - East, 3.8 mi E</p> <p>BY-4, Paynes Pt., 4.5 mi SE</p> <p>BY-5, Nearsite - South, 3.6 mi S</p> <p>BY-6, Oregon, 4.6 mi SSW</p> <p><u>Controls</u></p> <p>BY-7, Mt. Morris, 7.8 mi WSW</p> <p>BY-8, Leaf River, 7.0 mi NW</p>		
3. <u>Waterborne</u>	<p><u>Indicators</u></p> <p>BY-9, Woodland Creek, 2.3 mi W</p> <p>BY-11, Byron Discharge Pipe/River, at Station</p> <p>BY-12, Oregon Pool of Rock River, Downstream of Discharge, 4.5 mi SSW</p> <p><u>Controls</u></p> <p>BY-10, Byron Intake Pipe/River, at Station</p> <p>BY-13, Oregon Pool of Rock River, Upstream of Intake, 4.3 mi SSW</p>	Weekly collection composited monthly.	Gamma isotopic analysis ^c monthly. Composite for tritium analysis quarterly.
a. <u>Surface</u>	<p><u>Indicators</u></p> <p>BY-18, Onsite Well, at Station</p> <p><u>Controls</u></p> <p>BY-14, CECO Real Estate Office, 0.3 mi E</p>	Quarterly	Gamma isotopic ^c and tritium analysis quarterly.
b. <u>Ground</u>	<p><u>Indicators</u></p> <p>BY-12, Oregon Pool of Rock River, Downstream of Discharge, 4.5 mi SSW</p> <p><u>Controls</u></p> <p>BY-13, Oregon Pool of Rock River, Upstream of Intake, 4.3 mi SSW</p>	Semiannually	Gamma isotopic analysis ^c semiannually.
c. <u>Sediment from Shoreline</u>	<p><u>Indicators</u></p> <p>BY-15, Groenhagen/Oltmann Farm, 2.0 mi S</p> <p>BY-16, Ashelford Farm, 2.7 mi W</p> <p>BY-20, Meyers Farm, 5.0 mi SE</p> <p><u>Controls</u></p> <p>BY-17, Bosecker/Lingel Farm, 7.0 mi NE</p>	Semimonthly when animals are on pasture, monthly at other times.	Gamma isotopic ^c and I-131 analysis semimonthly when animals are on pasture, monthly at other times.
4. <u>Ingestion</u>			
a. <u>Milk</u>			

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4-1

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TABLE 8.4-1 (Cont'd)

EXPOSURE PATHWAY AND/OR SAMPLE	SAMPLING OR MONITORING LOCATIONS	SAMPLING OR COLLECTION FREQUENCY	TYPE AND FREQUENCY OF ANALYSIS
4. Ingestion (Cont'd)			
b. <u>Fish and Invertebrates</u> Representative samples of commercially and recreationally important species.	<u>Indicators</u> BY-12, Oregon Pool of Rock River, Downstream of Discharge, 4.5 mi SSW <u>Controls</u> BY-13, Oregon Pool of Rock River, Upstream of Intake, 4.3 mi SSW	Three times per year (spring, summer, and fall).	Gamma isotopic analysis ^c on edible portions.
c. <u>Food Products</u> Representative samples of the principal classes of food products.	<u>Indicators</u> From any area within 10 miles of the plant that is irrigated by water in which plant wastes have been discharged.	At time of harvest. ^d	Gamma isotopic analysis ^c on edible portions.
Samples of three different kinds of broadleaf vegetation.	From nearest each of two different offsite locations of highest predicted annual average ground level D/Q (see Table 7.2-6).	Monthly when available and required; <u>required only if milk sampling is not performed.</u>	Gamma isotopic ^c and I-131 analysis.
One sample each of broadleaf vegetation similar to that collected for the above require- ment.	<u>Controls</u> From a location 9.3 to 18.6 miles from the station in direction of lowest predicted annual average ground level D/Q (see Table 7.2-6).	Monthly when available and required; <u>required only if milk sampling is not performed.</u>	Gamma isotopic ^c and I-131 analysis.

^a Deviations are permitted from the required sampling schedule if specimens are unobtainable due to hazardous conditions, seasonal unavailability, malfunction of automatic sampling equipment and other legitimate reasons. If specimens are unobtainable due to sampling equipment malfunction, every effort shall be made to complete corrective action prior to the end of the next sampling period. All deviations from the sampling schedule shall be documented in the Annual Radiological Environmental Operating Report. It is recognized that, at times, it may not be possible or practicable to continue to obtain samples of the media of choice at the most desired location or time. In these instances suitable alternative media and locations may be chosen for the particular pathway in question and appropriate substitutions made within 30 days in the radiological environmental monitoring program. The cause of the unavailability of samples for that pathway and the new location(s) for obtaining replacement samples shall be identified in a Special Report to the Nuclear Regulatory Commission within 30 days. The report shall also include a revised figure(s) and table for the ODCM reflecting the new location(s).

^b Airborne particulate sample filters shall be analyzed for gross beta radioactivity 24 hours or more after sampling to allow for radon and thoron daughter decay. If gross beta activity in air particulate samples is greater than ten times the yearly mean of control samples, gamma isotopic analysis shall be performed on the individual samples.

^c Gamma isotopic analysis means the identification and quantification of gamma-emitting radionuclides that may be attributable to the effluents from the facility.

^d If harvest occurs more than once a year, sampling shall be performed during each discrete harvest. If harvest occurs continuously, sampling shall be monthly. Attention shall be paid to including samples of tuberous and root food products.

TABLE 8.4-2

REPORTING LEVELS FOR RADIOACTIVITY CONCENTRATIONS IN ENVIRONMENTAL SAMPLES

REPORTING LEVELS

<u>ANALYSIS</u>	<u>WATER</u> (pCi/l)	<u>AIRBORNE PARTICULATE</u> <u>OR GASES (pCi/m³)</u>	<u>FISH</u> (pCi/kg, wet)	<u>MILK</u> (pCi/l)	<u>FOOD PRODUCTS</u> (pCi/kg, wet)
H-3	20,000*				
Mn-54	1,000		30,000		
Fe-59	400		10,000		
Co-58	1,000		30,000		
Co-60	300		10,000		
Zn-65	300		20,000		
Zr-Nb-95	400				
I-131	2	0.9		3	100
Cs-134	30	10	1,000	60	1,000
Cs-137	50	20	2,000	70	2,000
Ba-La-140	200			300	

*For drinking water samples. This is 40 CFR Part 141 value. If no drinking water pathway exists, a value of 30,000 pCi/l may be used.

TABLE 8.4-3

DETECTION CAPABILITIES FOR ENVIRONMENTAL SAMPLE ANALYSIS^aLOWER LIMIT OF DETECTION (LLD)^{b,c}

<u>ANALYSIS</u>	<u>WATER (pCi/ℓ)</u>	<u>AIRBORNE PARTICULATE OR GAS (pCi/m³)</u>	<u>FISH (pCi/kg, wet)</u>	<u>MILK (pCi/ℓ)</u>	<u>FOOD PRODUCTS (pCi/kg, wet)</u>	<u>SEDIMENT (pCi/kg, dry)</u>
Gross Beta	4	0.01				
H-3	2000*					
Mn-54	15		130			
Fe-59	30		260			
Co-58,60	15		130			
Zn-65	30		260			
Zr-Nb-95	15					
I-131	1 ^d	0.10		1	60	
Cs-134	15	0.05	130	15	60	150
CS-137	18	0.06	150	18	80	180
Ba-La-140	15			15		

*If no drinking water pathway exists, a value of 3000 pCi/ℓ may be used.

TABLE 8.4-3 (Cont'd)

- a This list does not mean that only these nuclides are to be considered. Other peaks that are identifiable, together with those of the above nuclides, shall also be analyzed and reported in the Annual Radiological Environmental Operating Report.
- b Required detection capabilities for thermoluminescent dosimeters used for environmental measurements are given in Regulatory Guide 4.13.
- c The LLD is defined, for purposes of these specifications, as the smallest concentration of radioactive material in a sample that will yield a net count, above system background, that will be detected with 95 percent probability with only 5 percent probability of falsely concluding that a blank observation represents a "real" signal.

For a particular measurement system, which may include radiochemical separation:

$$LLD = \frac{4.66 s_b}{E \cdot V \cdot 2.22 \cdot Y \cdot \exp(-\lambda \Delta t)}$$

where:

- LLD = the "a priori" lower limit of detection (picoCuries per unit mass or volume),
- s_b = the standard deviation of the background counting rate or of the counting rate of a blank sample as appropriate (counts per minute),
- E = the counting efficiency (counts per disintegration),
- V = the sample size (units of mass or volume),
- 2.22 = the number of disintegrations per minute per picoCurie,
- Y = the fractional radiochemical yield, when applicable,
- λ = the radioactive decay constant for the particular radionuclide, (sec^{-1}), and
- Δt = the elapsed time between sample collection, or end of the sample collection period, and time of counting (sec).

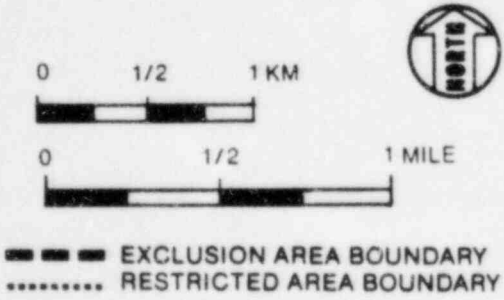
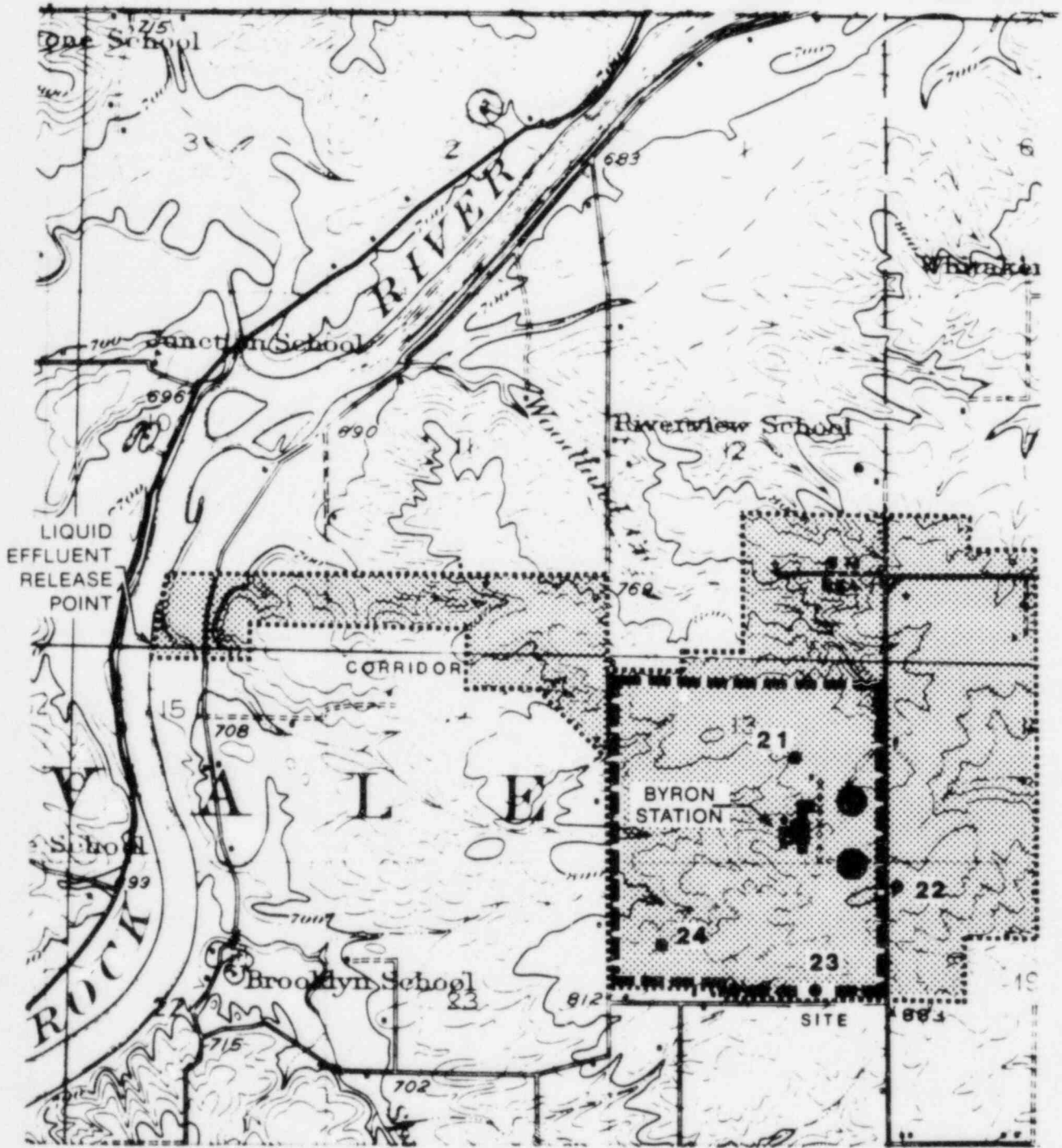
Typical values of E, V, Y, and Δt should be used in the calculation.

It should be recognized that the LLD is defined as an a priori (before the fact) limit representing the capability of a measurement system and not as an a posteriori (after the fact) limit for a particular measurement. Analyses shall be performed in such a manner that the stated LLDs will be achieved under routine conditions. Occasionally

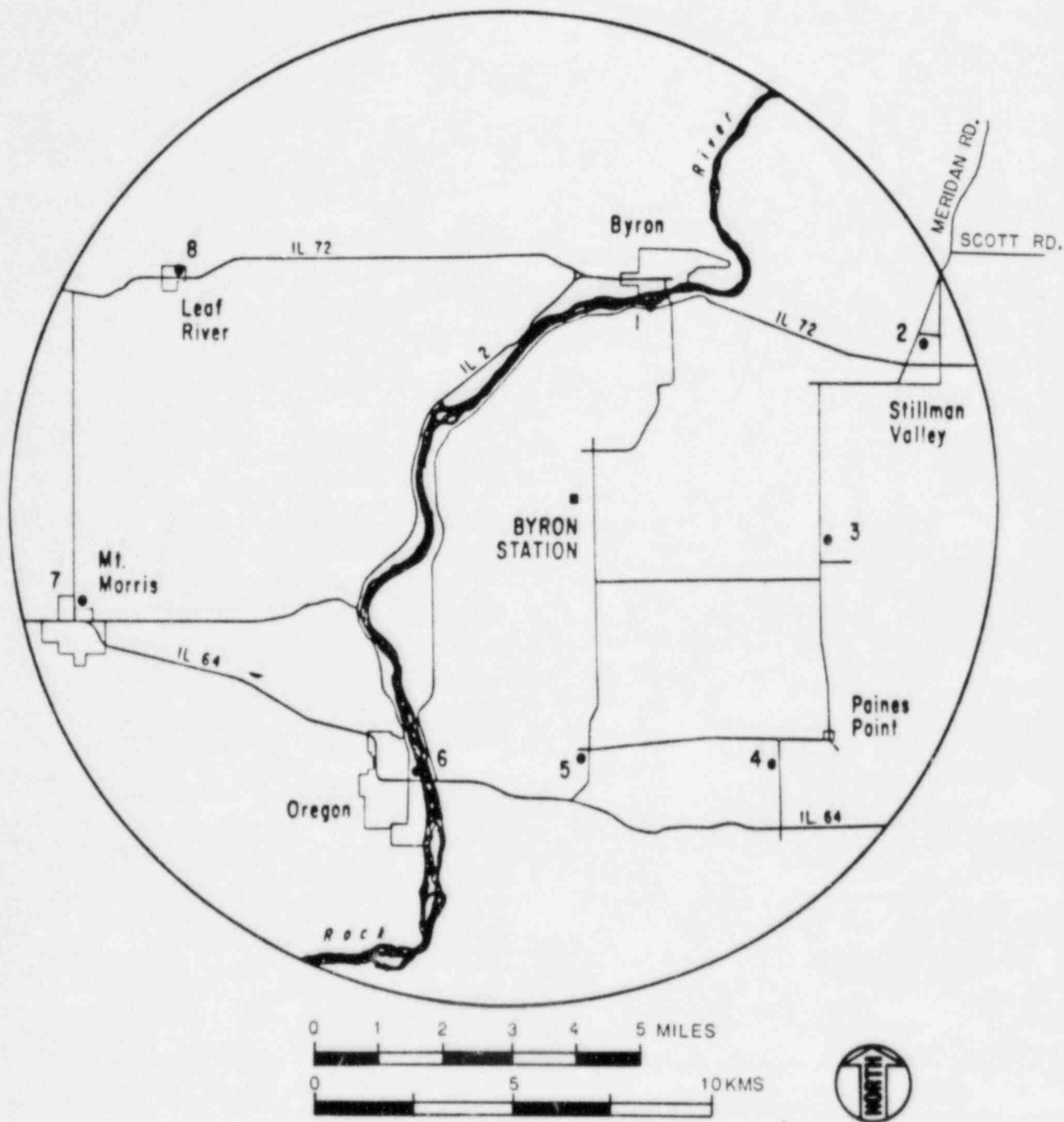
TABLE 8.4-3 (Cont'd)

background fluctuations, unavoidable small sample sizes, the presence of interfering nuclides, or other uncontrollable circumstances may render these LLDs unachievable. In such cases, the contributing factors shall be identified and described in the Annual Radiological Environmental Operating Report.

- ^d LLD for drinking water samples. If no drinking water pathway exists, an LLD of 60 pCi/l may be used.



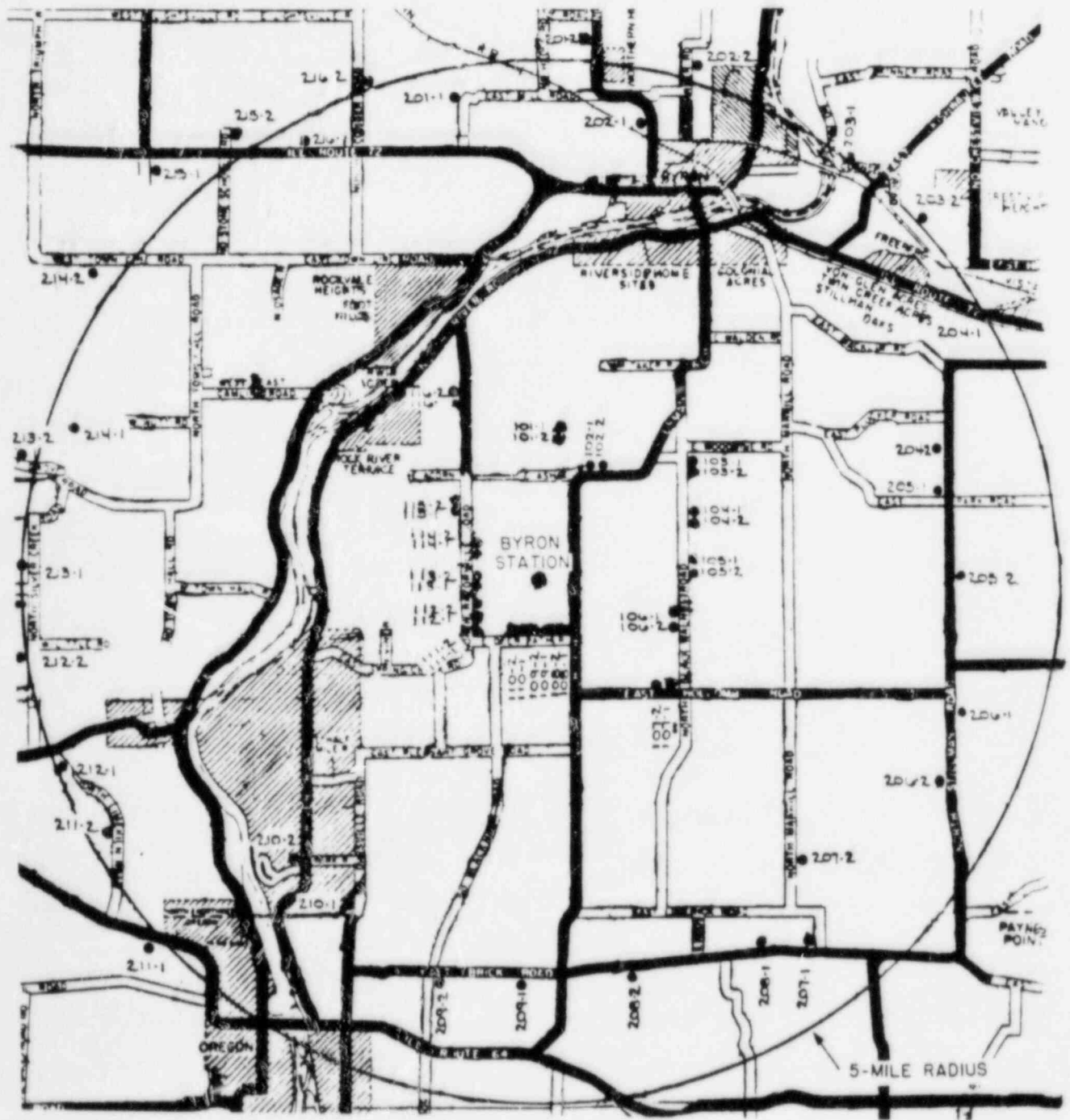
BYRON STATION
FIGURE 8.4-1
ONSITE AIR SAMPLING LOCATIONS



BYRON STATION

FIGURE 8.4-2

OFFSITE AIR SAMPLING LOCATIONS



●-TLD



BYRON STATION
FIGURE 8.4-3
INNER RING AND OUTER RING TLD LOCATIONS