

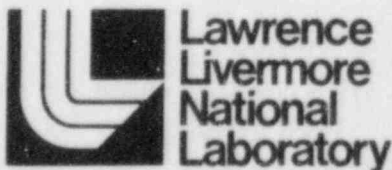
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WIPS—Computer Code for Whip and Impact Analysis of Piping Systems

Part D—Verification Manual

G. H. Powell and F-C. Hu;
University of California, Berkeley, CA

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Prepared by
G. H. Powell and F-C. Hu;
University of California, Berkeley, CA

Lawrence Livermore National Laboratory
7000 East Avenue
Livermore, CA 94550

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WIPS: COMPUTER CODE FOR WHIP and IMPACT ANALYSIS OF PIPING SYSTEMS

PART D VERIFICATION MANUAL

ABSTRACT

This report presents details of a number of examples which have been chosen to verify the WIPS code. The examples have been selected to verify most (but not all) features of WIPS. For each example the following information is provided:

- (1) A description of the example.
- (2) Complete WIPSLOG file listings, detailing the steps followed in setting up the example. These listings will enable a user to reproduce each example.
- (3) DATA file listings.
- (4) Results, including comparisons with previously reported experiments and/or analyses if available.

The conclusions which can be reached from the verification study are as follows.

- (1) WIPS is an effective tool for the analysis of restrained pipes. Nevertheless, it is recommended that additional verification examples be analyzed before WIPS is used for production analysis.
- (2) WIPS is an effective tool for the analysis of unrestrained pipes (with large displacements) up to impact with adjacent objects. Again, however, it is recommended that additional verification examples be analyzed before WIPS is used for production analysis.
- (3) WIPS appears to work well for analyses which make use of the impact analysis option but has not been tested thoroughly. These analyses are extremely complex and very expensive computationally. Considerable additional verification is recommended before production analyses are attempted.

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D1. INTRODUCTION

WIPS (Whip and Impact of Piping Systems) is a special purpose computer code for the analysis of pipe whip following postulated pipe rupture. The scope and purpose of the code have been described in the WIPS Summary Report. User instructions, theoretical data and programmer instructions have been presented in WIPS Reports A, B, and C, respectively. In this report, the results of a number of examples are presented.

The purpose of the examples is to provide verification of the WIPS code, using, where possible, comparisons with previously reported experimental and analytical results. The examples also serve as illustrations on the use of WIPS. Details of the example analyses are presented in Sections D2.1 through D2.7.

D2. EXAMPLES

THE FOLLOWING SECTIONS PRESENT DETAILS OF THE EXAMPLE ANALYSES. EACH EXAMPLE IS PRESENTED AS A SEPARATE CHAPTER TO ALLOW ADDITIONAL EXAMPLES TO BE ADDED IF DESIRED.

D2.1 STATIC BEHAVIOR OF ELBOWS

D2.1.1 PURPOSE

This series of examples tests the curved PIPE element, by comparison with previously reported test results. The influence of large ovaling on the computed behavior is explored. Large displacement effects and strain rate effects are not considered.

D2.1.2 DESCRIPTION

A series of tests on pipe elbows has been reported by Bolt and Greenstreet [2.1.1]. The test configuration is shown in Fig. 2.1.1. All 15 of the test specimens considered in [2.1.1] have been analyzed using WIPS. The properties of the test specimens are summarized in Table 2.1.1.

The pipes were made of ASTM A-106 Grade B carbon steel and ASTM A-312 Type 304L stainless steel. Nominal yield stresses (0.2% offset) were given for the test specimens in [2.1.1]. However, detailed stress-strain curves for the steels were not given, and hence, there is some uncertainty in the specification of the material properties. The trilinear stress-strain curves shown in Tables 2.1.2 through 2.1.5 have been assumed for the WIPS analyses. For the A-312 stainless steel and the A-106 steel with 50 ksi yield, curves similar to those used by Scheller and Mallett [2.1.3] have been assumed. For the weaker A-106 steels, curves similar to the 50 ksi curve have been assumed, but with lower strengths.

There is also uncertainty about the actual dimensions of the elbows. For a supplementary series of tests described in [2.1.2], variations from the nominal dimensions are reported. For the first 15 tests, however, this information was not reported. For the WIPS analyses, nominal dimensions have been assumed as follows:

- 6-in. Schedule 40 Pipe: 6.625 in. O.D. x 0.280 in. wall thickness.
- 6-in. Schedule 80 Pipe: 6.625 in. x 0.432 in.
- Long Radius (LR) Elbow: 9-in. radius to pipe centerline.
- Short Radius (SR) Elbow: 6-in. radius.

D2.1.3 WIPS ANALYSIS MODEL

D2.1.3.1 Geometry and Loading

The WIPS analysis model consisted of three straight PIPE elements and two curved PIPE elements, as shown in Fig. 2.1.2. Loads were applied at node 6 (upwards, downwards, or out-of-plane). The response is static, whereas WIPS performs only dynamic analyses. Static behavior was obtained by specifying negligibly small mass and damping values. In addition, the displacements were controlled by adding a very stiff UBAR (10000 k/in. stiffness) at node 6. A force time history increasing linearly from zero was specified (ramp loading) and the UBAR stiffness, load magnitude, and time step were chosen to extend the UBAR element by 0.05 inches in each time step. Because the UBAR was much stiffer than the PIPE elements, node 6 displaced almost exactly 0.05 inches per step. The displacement increments at node 5 also increased essentially equal amounts in each step. The shear force in PIPE element 5-6 gave the load carried by the pipe specimen.

D2.1.3.2 Ovaling Parameters

The ovaling theory for the PIPE element is only semi-rational and requires that certain ovaling stiffness and strength parameters be specified. An initial ovaling stiffness is determined automatically (the value is consistent with the flexibility factor commonly used in piping analyses), and a nominal ovaling yield strength is also determined automatically. The following parameters must then be specified in order to define a trilinear relationship between ovaling

deformation and a corresponding ovaling "force":

- (1) Owalling strength at first yield, as a multiple of the nominal yield strength. In WIPS, the default value for this multiple is 1.3.
- (2) Owalling stiffness after first yield, as a multiple of the initial ovaling stiffness. The default value is 0.35.
- (3) Owalling stiffness after second yield, as a multiple of the initial ovaling stiffness. The default value is 0.08.

It is not required to specify the ovaling strength at second yield. Second yield is automatically assumed to occur at a deformation of twice the first yield deformation. For the analyses, the default values were used.

In addition, the analyst may specify "small" or "large" ovaling. For small ovaling changes in shape of the pipe cross section are assumed to be small, and cross section properties are computed assuming a circular section. For large ovaling the changes in pipe diameter are assumed to be significant, and cross section properties are progressively recomputed for the ovalled section. All cases were analyzed with large ovaling, one case being re-analyzed with small ovaling for comparison. In addition, one case was analyzed substituting straight elements for the two curved elements. The major effect of this substitution is that ovaling is completely ignored.

D2.1.3.3 Analysis Control Parameters

The analysis control parameters were chosen to ensure a constant time step during the analysis. The Newmark step-by-step option was used, with essentially zero mass and a very small damping factor to eliminate dynamic effects.

D2.1.3.4 WIPS Input

Tables 2.1.6 through 2.1.8 contain WIPSLOG listings up to the WIPS-DATA phase for a typical case (Test PE1). Table 2.1.9 is a listing of the DATA file for the same case. All other DATA files were similar.

D2.1.4 RESULTS

D2.1.4.1 Tests PE1 through PE6

The WIPS and experimental results are compared for Tests PE1 through PE3 in Figs. 2.1.3 through 2.1.5. For Tests PE1 and PE2 (up and down loading, respectively), the agreement is close. For Test PE3 (out-of-plane loading), the computed strength is significantly larger than the measured strength. An analysis of Test PE3 has been reported in [2.1.3] using two other elbow elements, with comparable differences between analysis and experiment.

The computed results for Tests PE1 and PE2 are compared in Fig. 2.1.6. The computed results assuming small ovaling are also shown. The difference in strength for upwards and downwards load is not large and is not likely to have a significant effect for pipe whip analysis. For most applications, therefore, it is recommended that small ovaling be assumed.

Figure 2.1.7 shows the effect of ovaling on strength and stiffness, by comparing analyses of Test PE1 with (a) the elbow modelled with two curved elements (as in Fig. 2.1.2) and (b) the elbow modelled with two straight elements. The main difference in the two analyses is that in the case with straight elements ovaling is ignored. It is clear that ovaling greatly reduces the strength and should not be ignored.

The results for Tests PE4 through PE6 (with internal pressure of 1500 psi) are shown in Figs. 2.1.8 through 2.1.10. For Test PE4 (up loading), the agreement is close. For Test PE5 (down loading), the computed strength is significantly below the measured strength. Note, however, that the test results indicate that specimen PE5 was stiffer than specimen PE4 up to a load of over 8 kips. This is the opposite of what would be expected and suggests significant variability in the test specimens. For the out-of-plane loading (Test PE6), the computed strength again exceeds the measured strength.

D2.1.4.2 Tests PE7 through PE9

The results for Tests PE7 through PE9 (up, down, and out-of-plane loading, respectively, with zero pressure) are shown in Figs. 2.1.11 through 2.1.13. The computed strengths for Tests PE7 and PE8 are significantly below the measured strengths, whereas the results for Test PE9 are in close agreement.

D2.1.4.3 Tests PE10 through PE14

The results for Tests PE10 through PE12 (up, down, and out-of-plane loading, respectively, with zero pressure) are shown in Figs. 2.1.14 through 2.1.16. The tests for these cases were terminated at rather small displacements, and hence, a comparison of strength cannot be obtained. It appears, however, that the computed strengths for the in-plane Tests PE10 and PE11 are below the measured values, whereas the results for Test PE12 could be in close agreement.

The results for Tests PE13 and PE14 (up and out-of-plane loading, respectively, with 1500 psi pressure) are shown in Figs. 2.1.17 and 2.1.18. The computed strength for Test PE13 is far below the measured value. The computed strength for Test PE14 is also low.

D2.1.4.4 Test PE15

The results for Test PE15 (down loading with zero pressure) are shown in Fig. 2.1.19. The agreement is quite close. Close agreement has also been reported in [2.1.3] for a test on a similar elbow (Test PE16).

D2.1.5 CONCLUSION

The computed and measured results agree within about 10% for the in-plane loadings for Tests PE1, PE2, PE4, PE5, and PE15. For these tests the material properties were selected with guidance from [2.1.3], and it appears likely that the assumed properties agree with the actual properties. For the out-of-plane tests PE3 and PE6, the computed strength exceeds the measured strength by about 20%.

For the remaining cases with in-plane loading, the computed strengths are substantially below the measured strengths, whereas for the remaining cases with out-of-plane loading the results agree quite closely. For all of these cases, it is less certain that the material properties have been approximated correctly. More detailed investigation is needed to determine the reasons for the differences.

A detailed study of the differences between the measured and computed strengths would require a major research effort and has not been possible within the present study. Overall, the agreement between analysis and experiment is believed to be sufficiently close for pipe whip applications. It should be noted that pipe elbows are extremely complex structures. The WIPS curved pipe element appears to model the essential features of elbow behavior, while still being reasonably simple theoretically and quite efficient computationally.

D2.1.6 REFERENCES

- 2.1.1 Bolt, S. E. and Greenstreet, W. L., "Experimental Determinations of Plastic Collapse Loads of Elbows," ASME Paper 71-PVP-37, 1971.
- 2.1.2 Greenstreet, W. L., "Experimental Study of Plastic Responses of Pipe Elbows," ORNL/NUREG-24, February 1978.
- 2.1.3 Scheller, J. D. and Mallett, R. H., "Numerical Evaluation of an Inelastic Piping Elbow Element," ASME Paper 79-PVP-41, 1979.

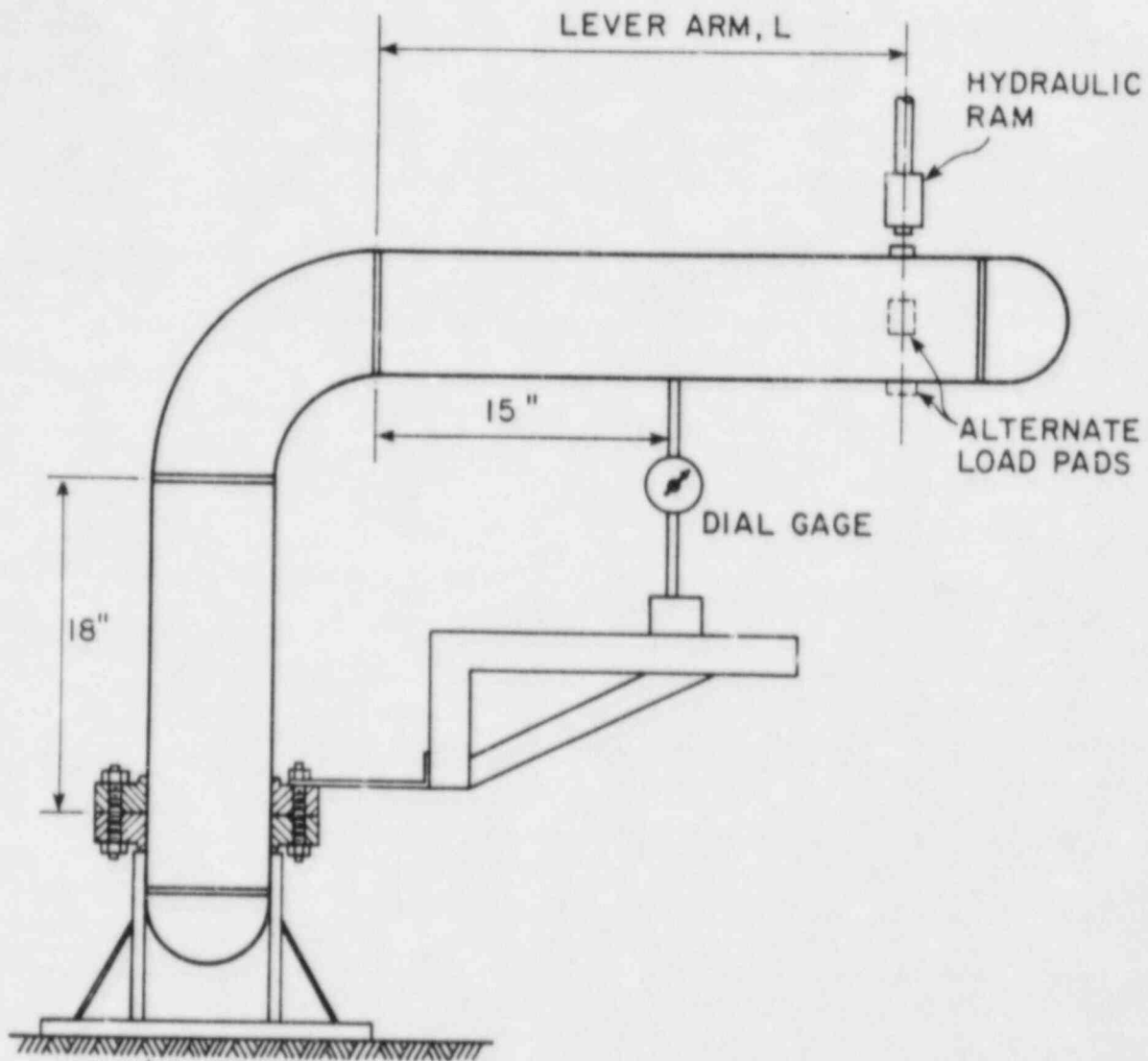


FIG. 2.1.1 TEST CONFIGURATION

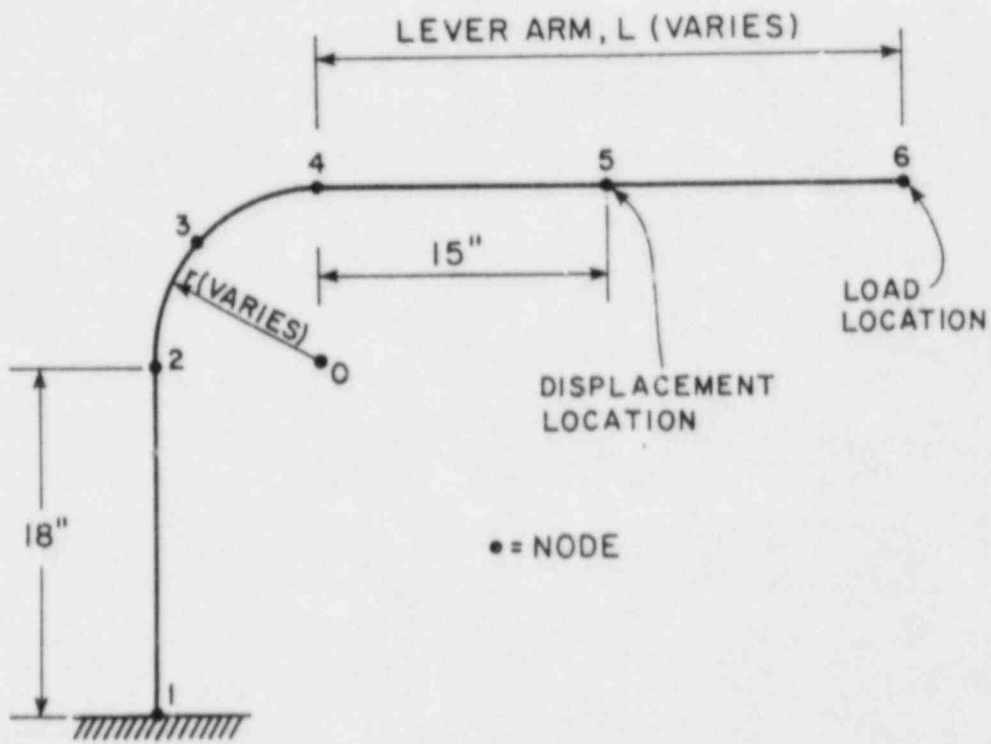


FIG. 2.1.2 ELEMENT SUBDIVISION

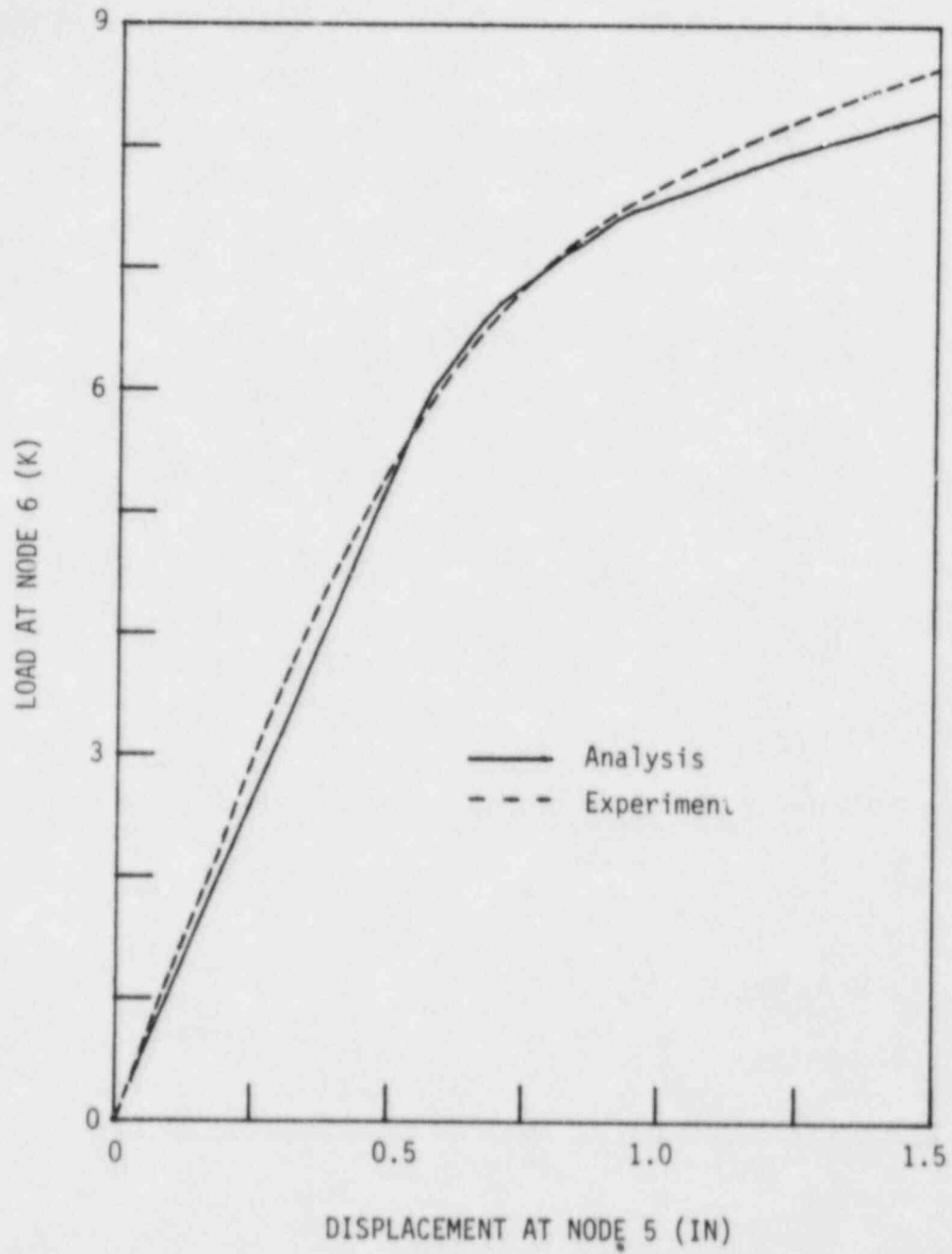


FIG. 2.1.3 TEST PE1.
UPWARDS LOAD, PRESSURE = 0.

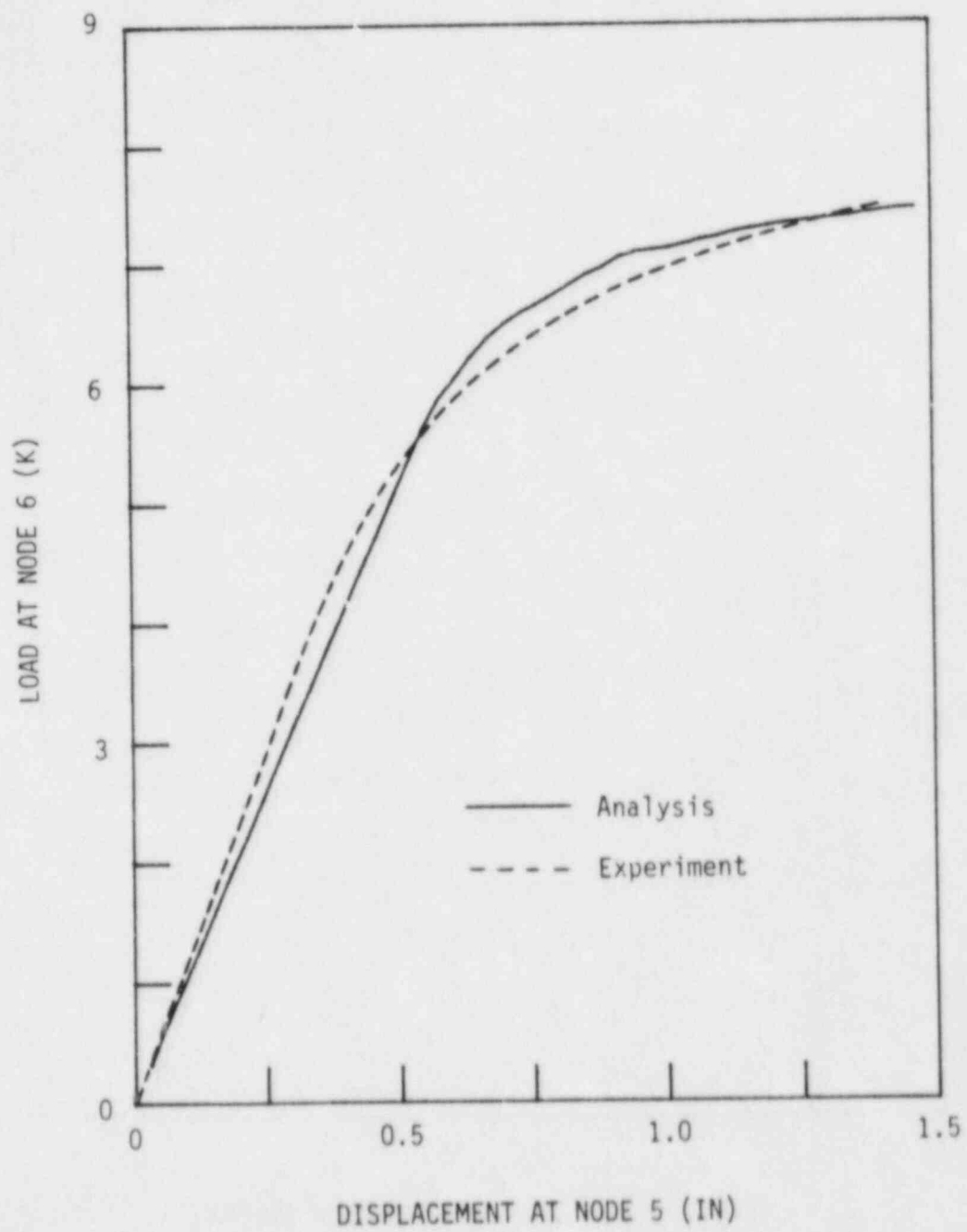


FIG. 2.1.4 TEST PE2.
DOWNWARDS LOAD, PRESSURE = 0.

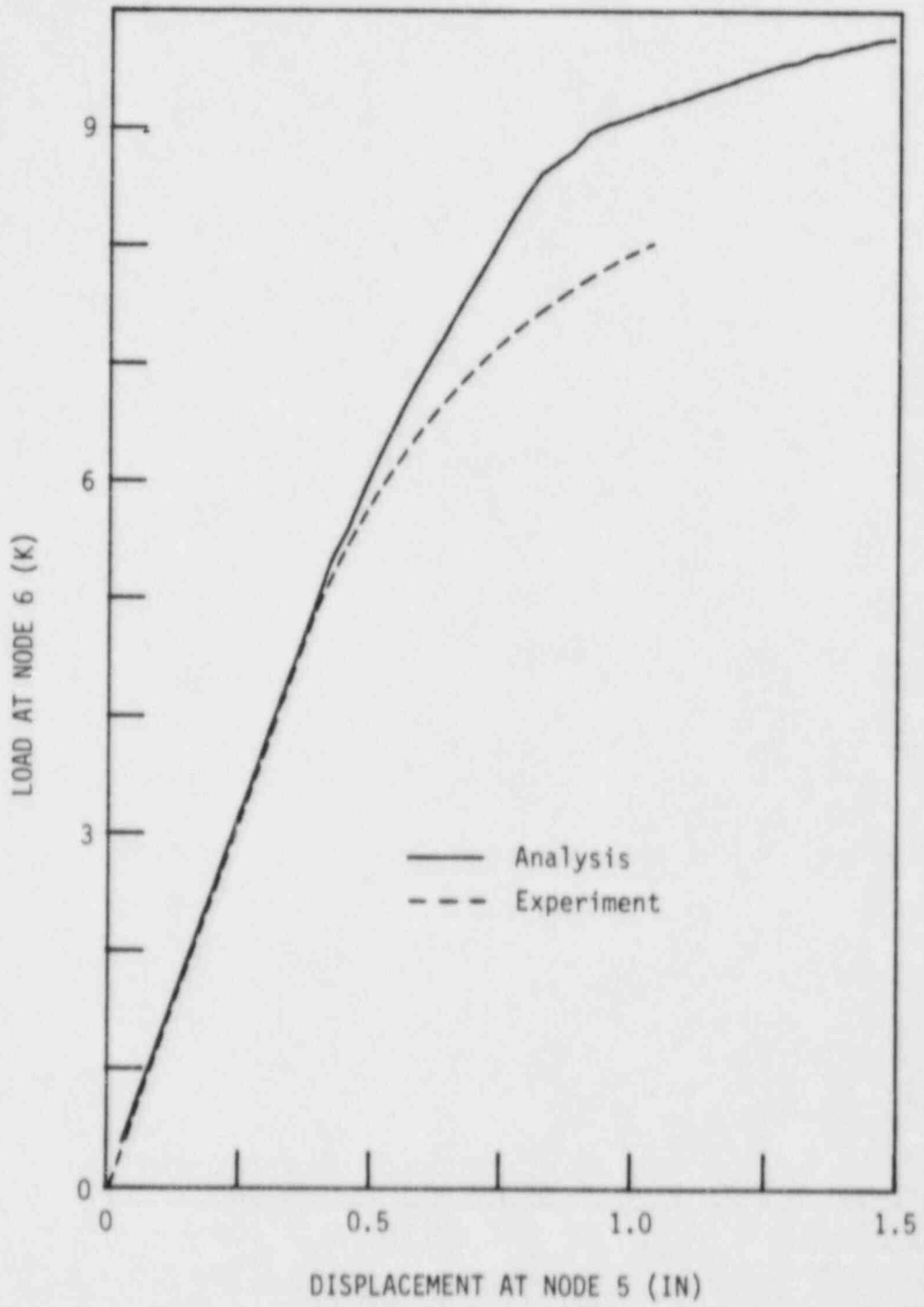


FIG. 2.1.5 TEST PE3.
OUT-OF-PLANE LOAD, PRESSURE = 0.

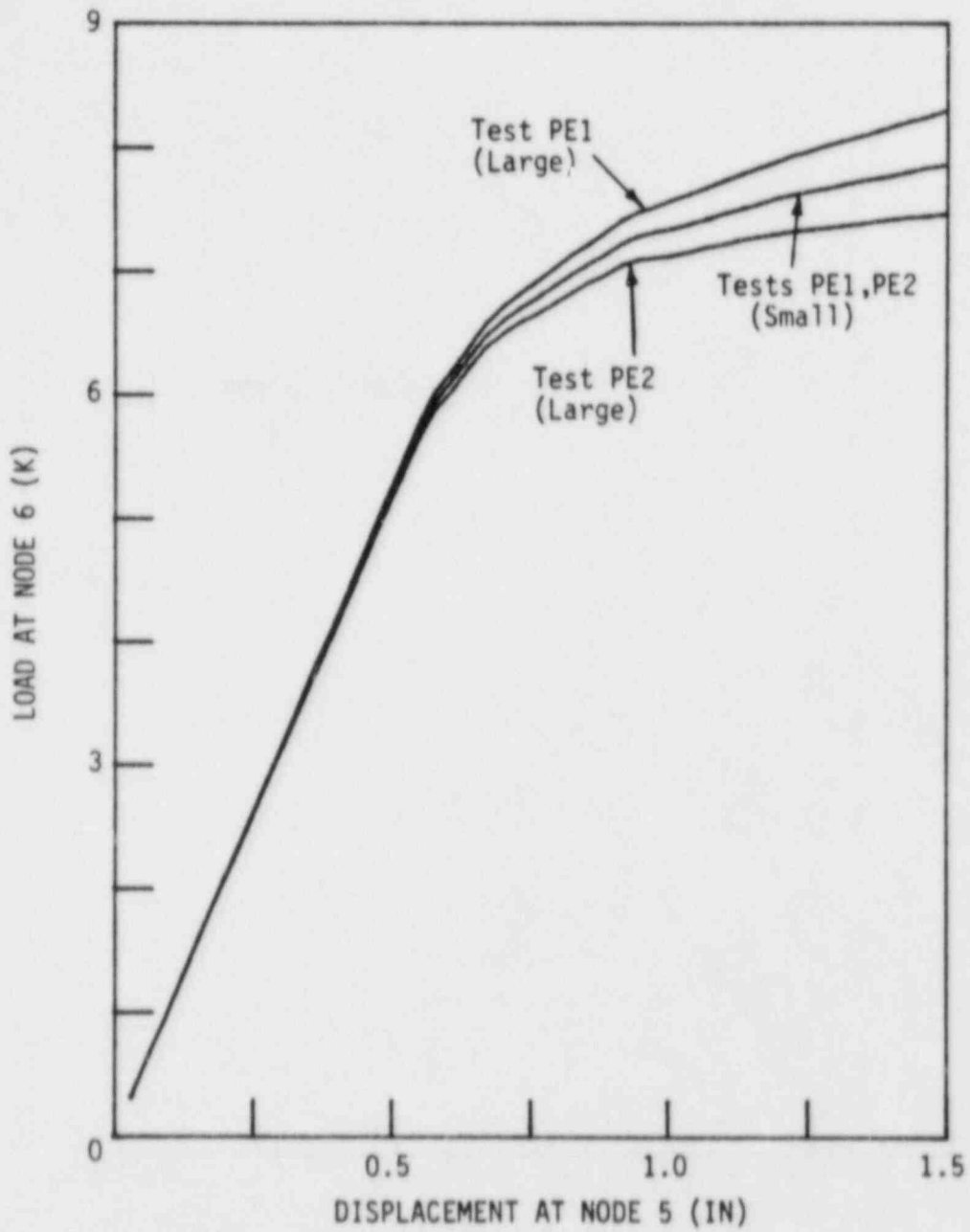


FIG. 2.1.6 COMPARISON OF ANALYSES WITH SMALL AND LARGE OVALING

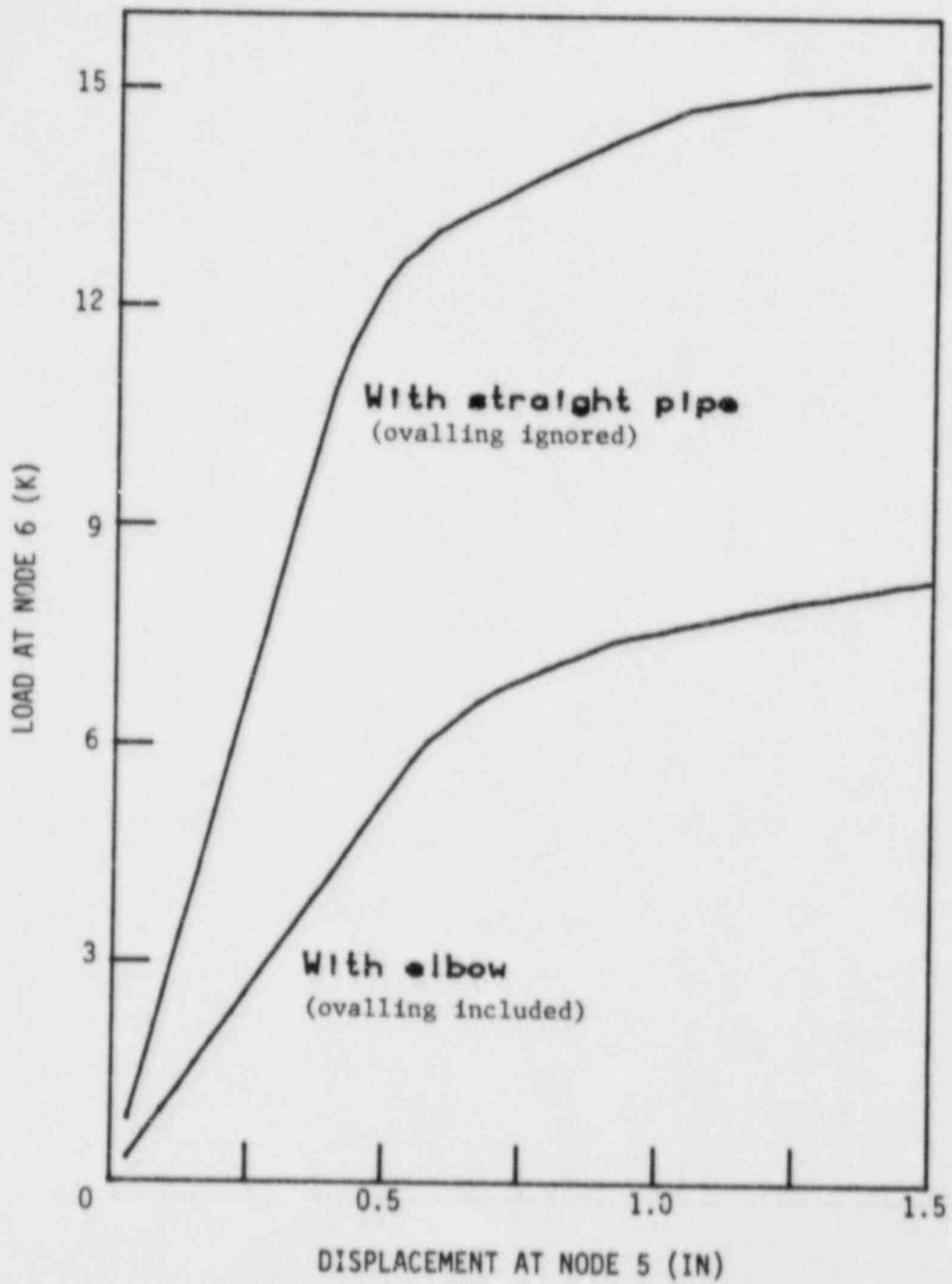


FIG. 2.1.7 EFFECT OF IGNORING OVALING ON ANALYSIS RESULTS (TEST PE1)

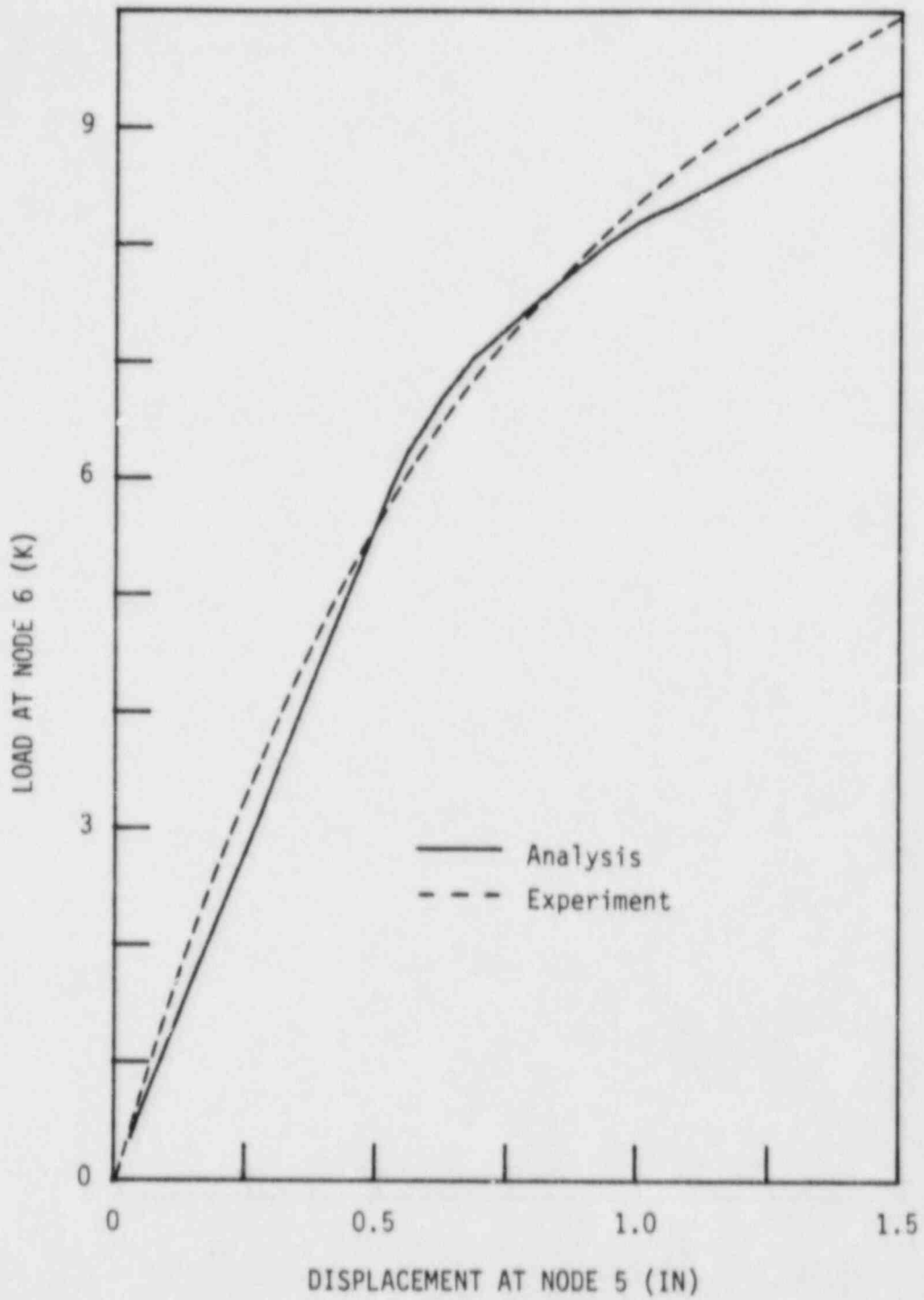


FIG. 2.1.8 TEST PE4.
UPWARDS LOAD, PRESSURE = 1500 PSI.

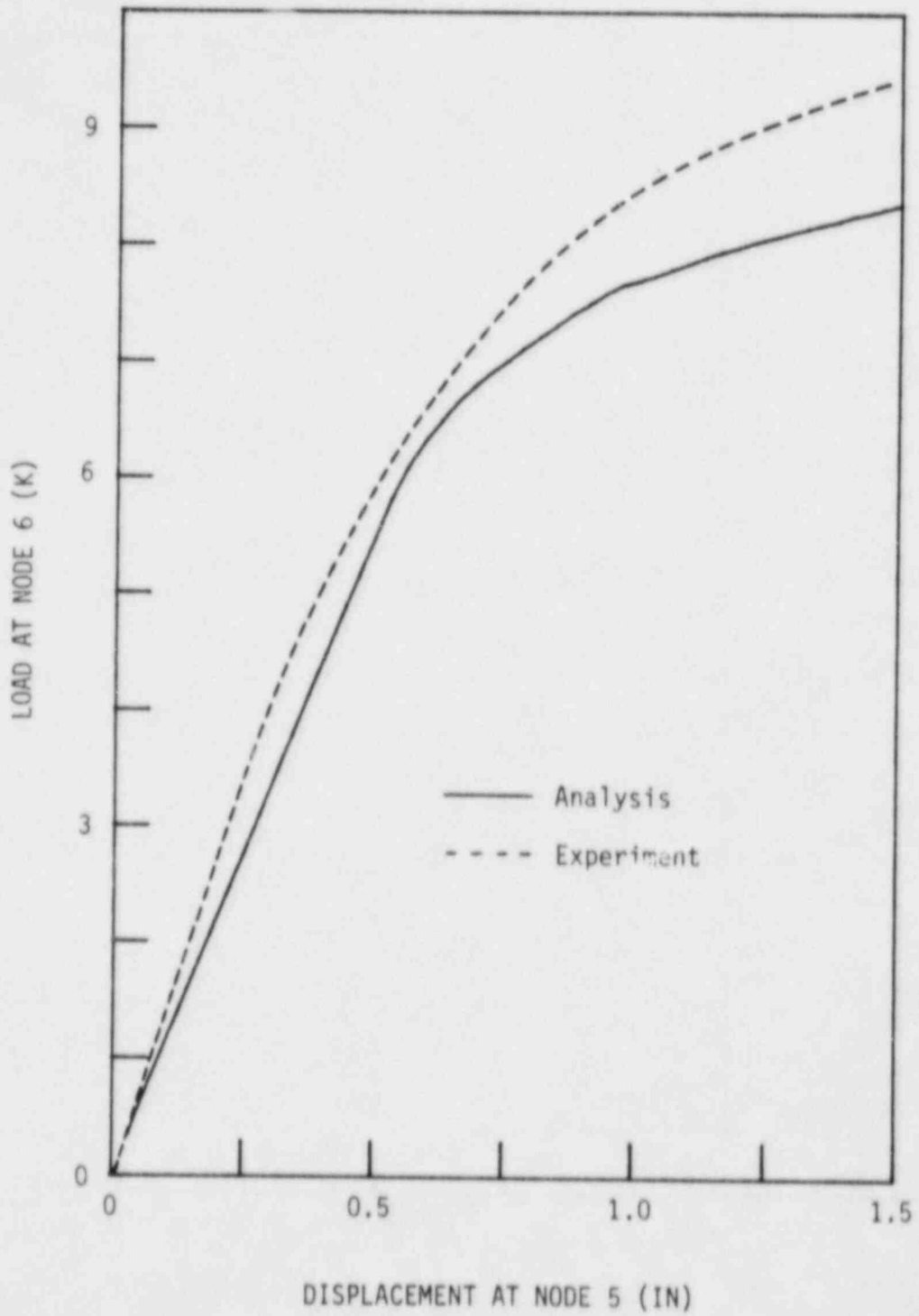


FIG. 2.1.9 TEST PE5.
DOWNWARDS LOAD, PRESSURE = 1500 PSI.

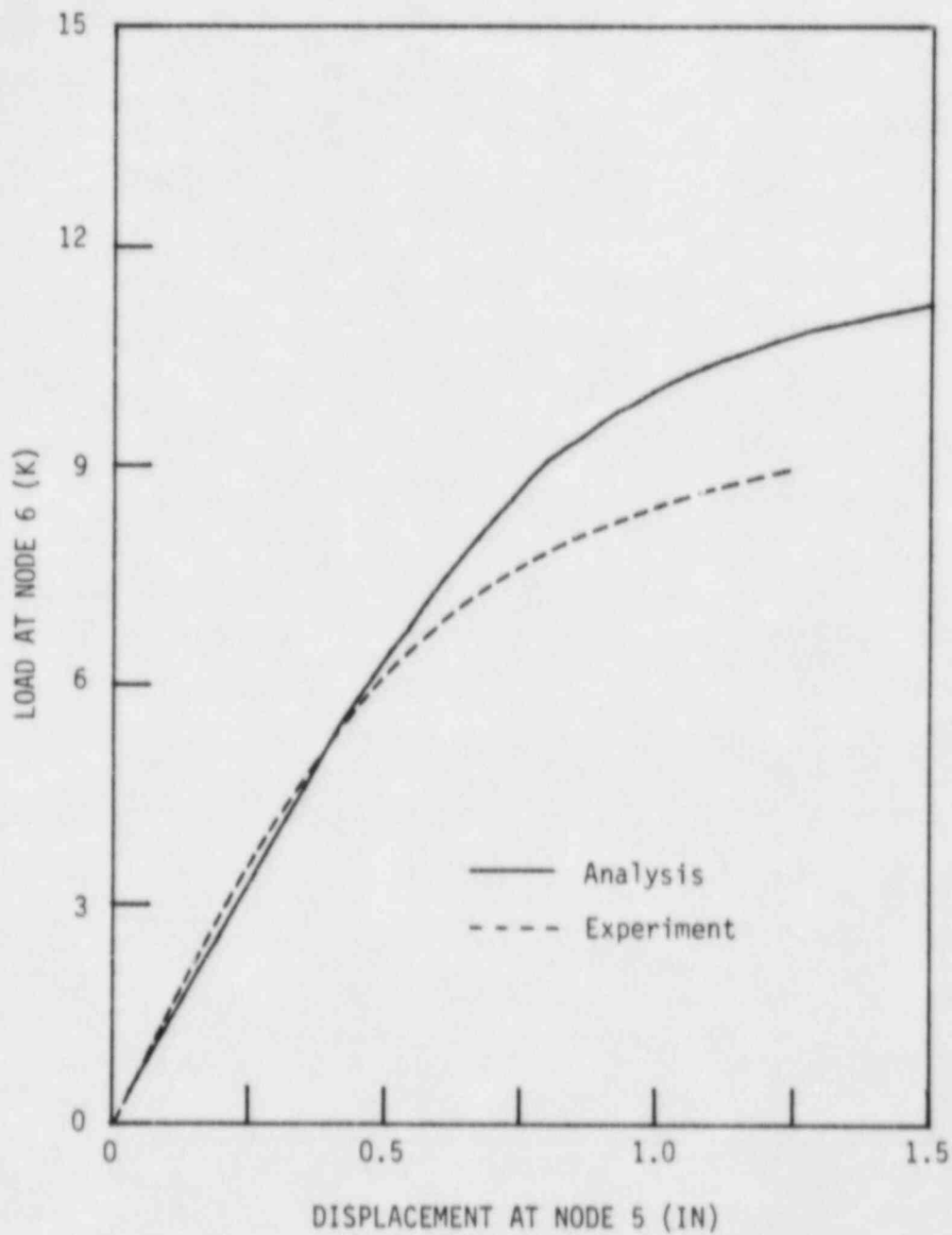


FIG. 2.1.10 TEST PE6.
OUT-OF-PLANE LOAD, PRESSURE = 1500 PSI

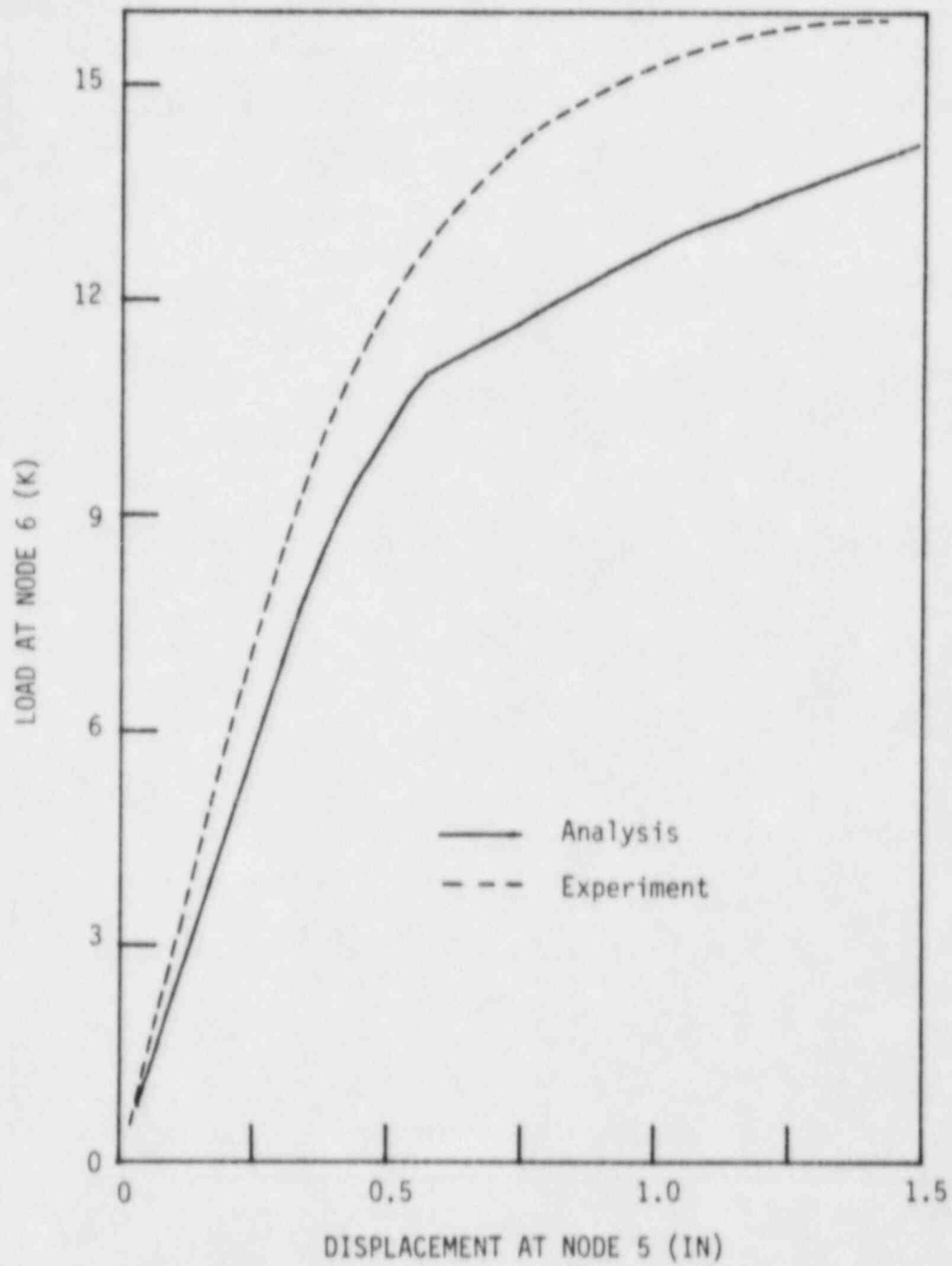


FIG. 2.1.11 TEST PE7.
UPWARDS LOAD, PRESSURE = 0.

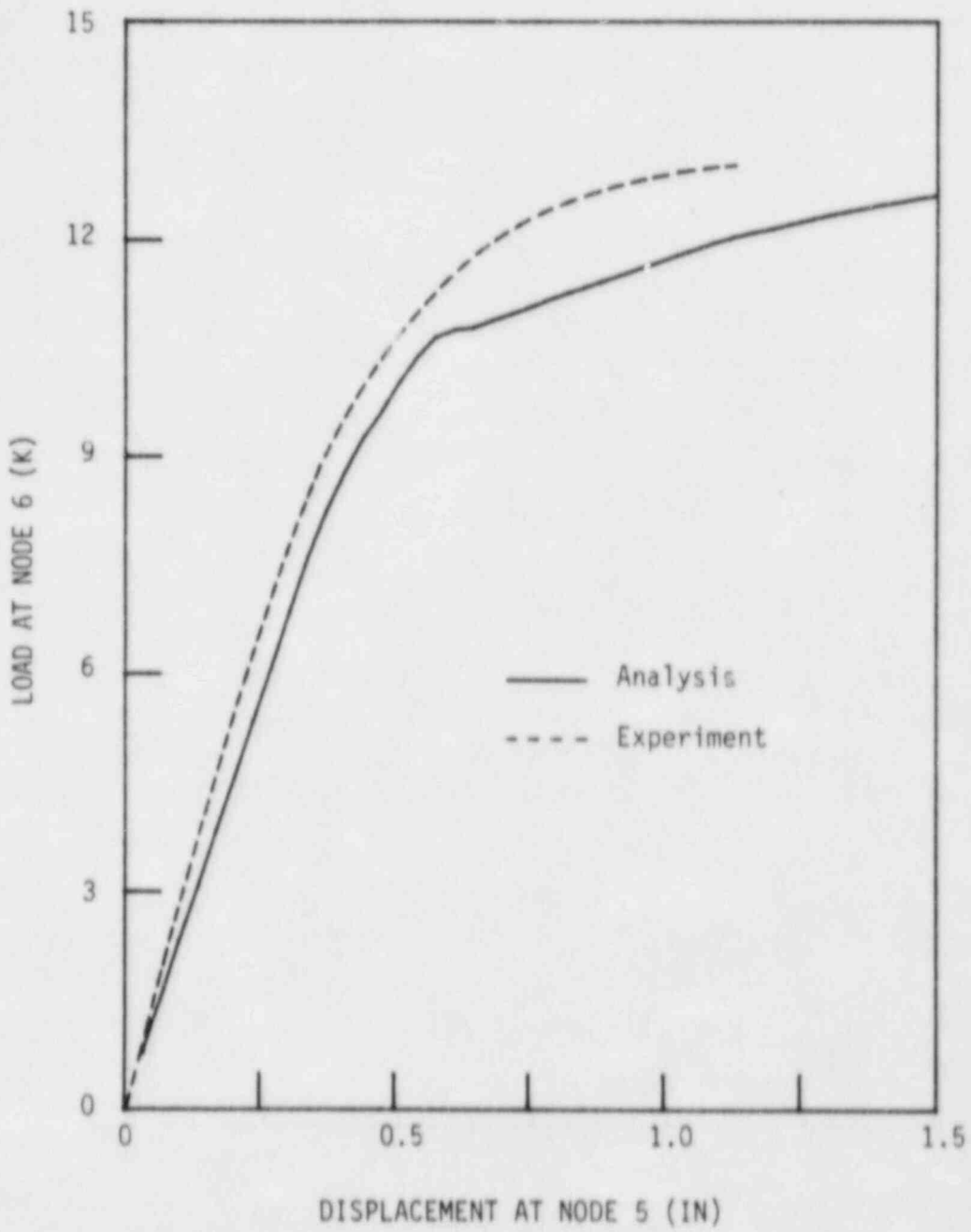


FIG. 2.1.12 TEST PE8.
DOWNWARDS LOAD, PRESSURE = 0.

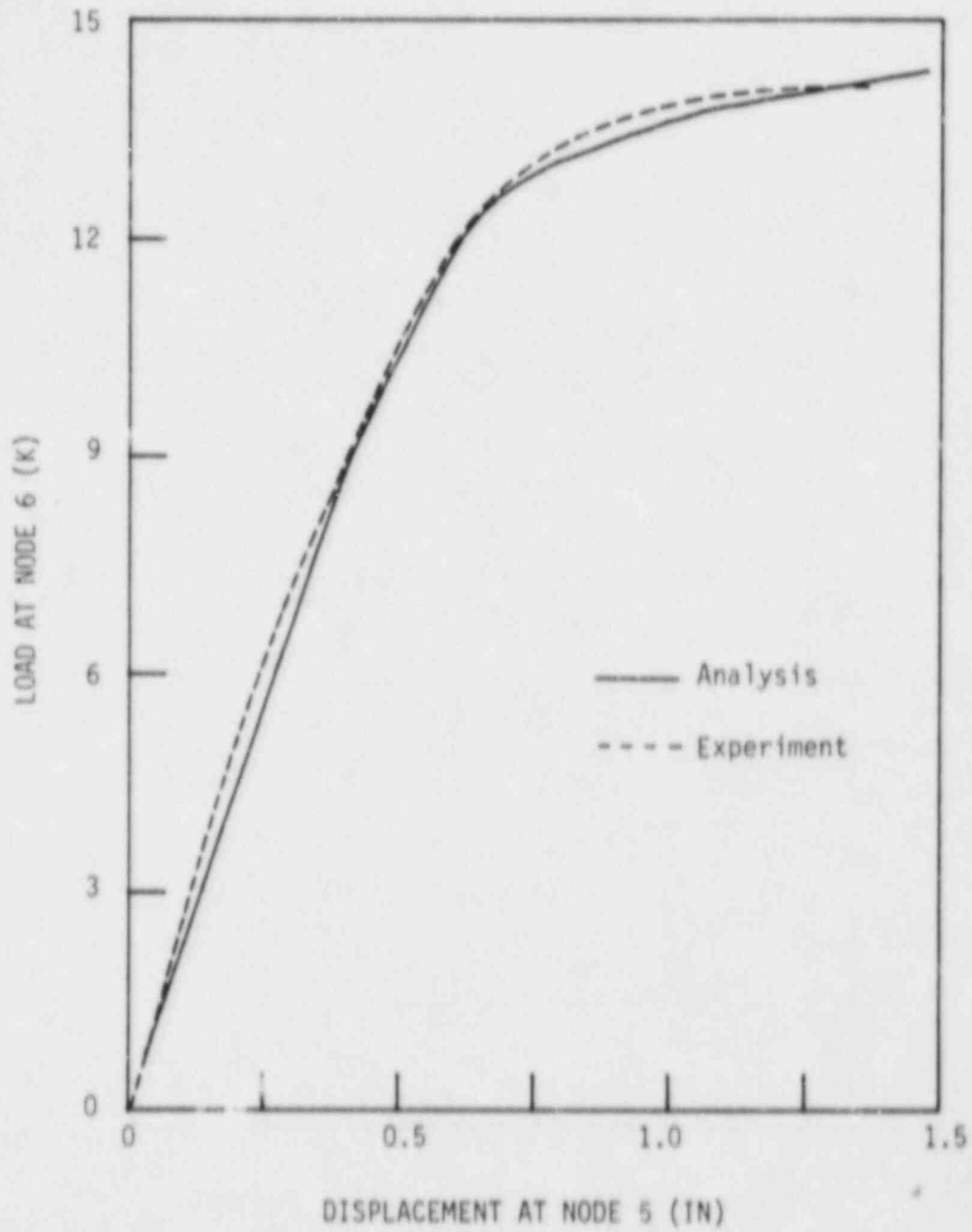


FIG. 2.1.13 TEST PE9.
OUT-OF-PLANE LOAD, PRESSURE = 0.

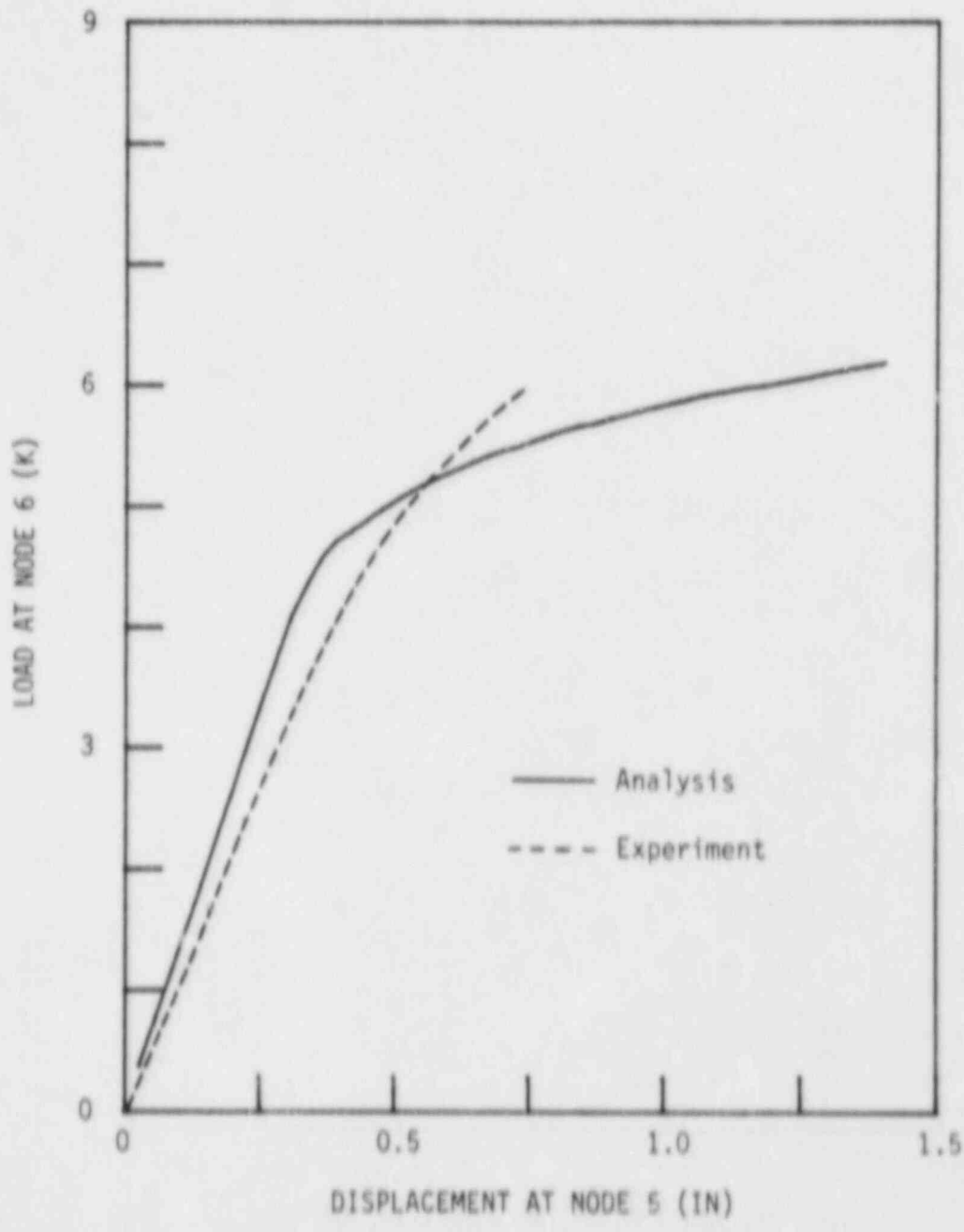


FIG. 2.1.14 TEST PE10.
UPWARDS LOAD, PRESSURE = 0.

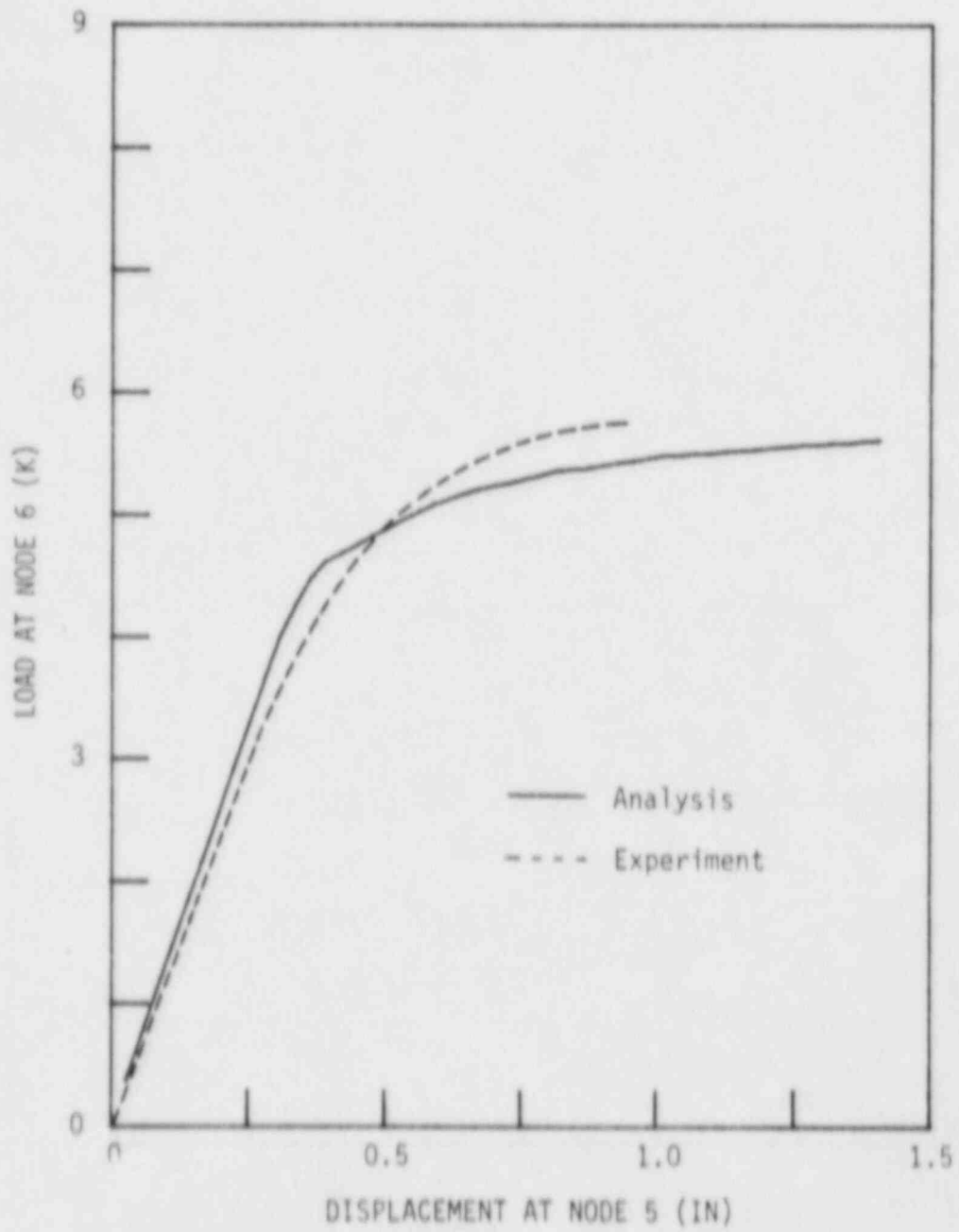


FIG. 2.1.15 TEST PE11.
DOWNWARDS LOAD, PRESSURE = 0.

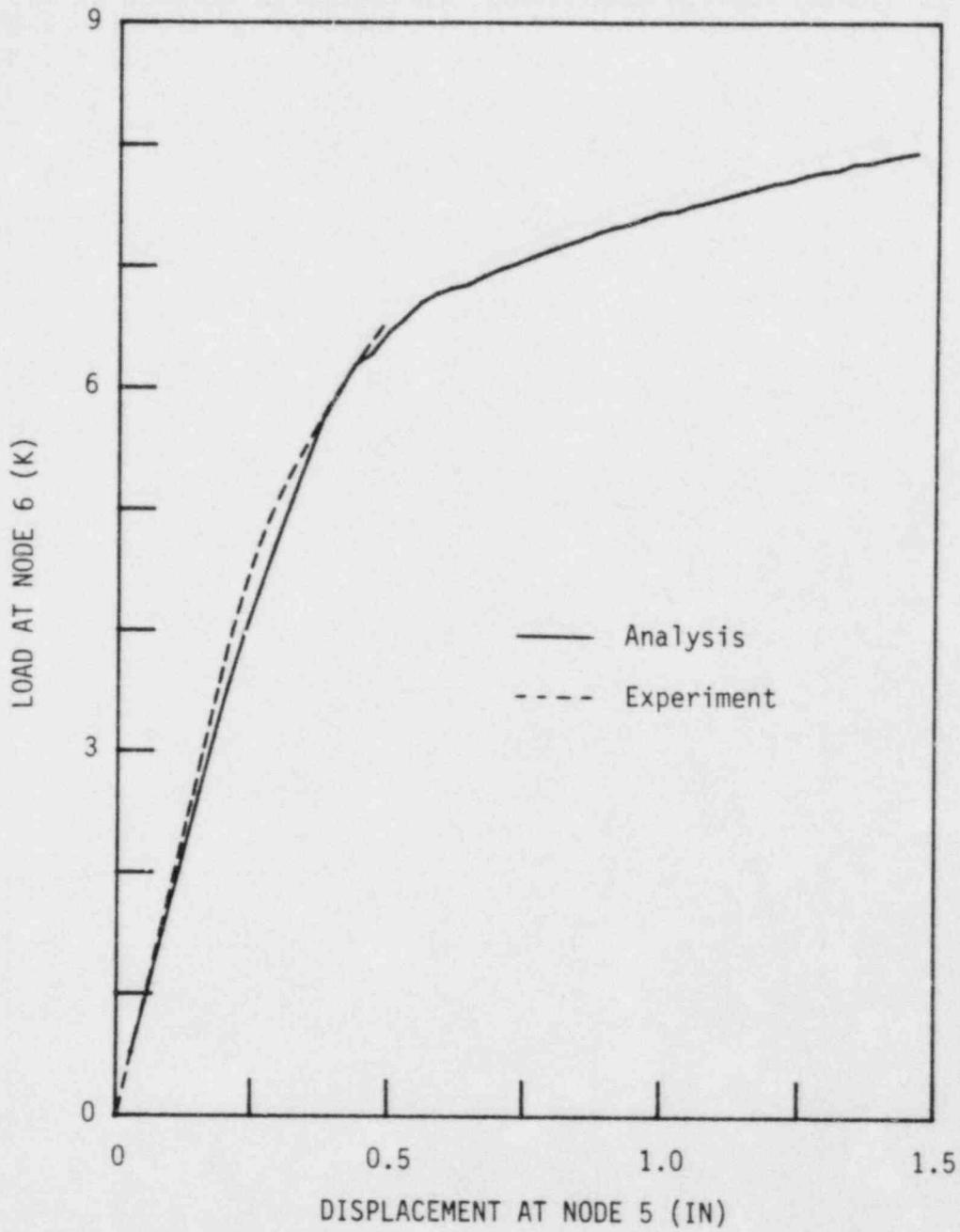


FIG. 2.1.16 TEST PE12.
OUT-OF-PLANE LOAD, PRESSURE = 0.

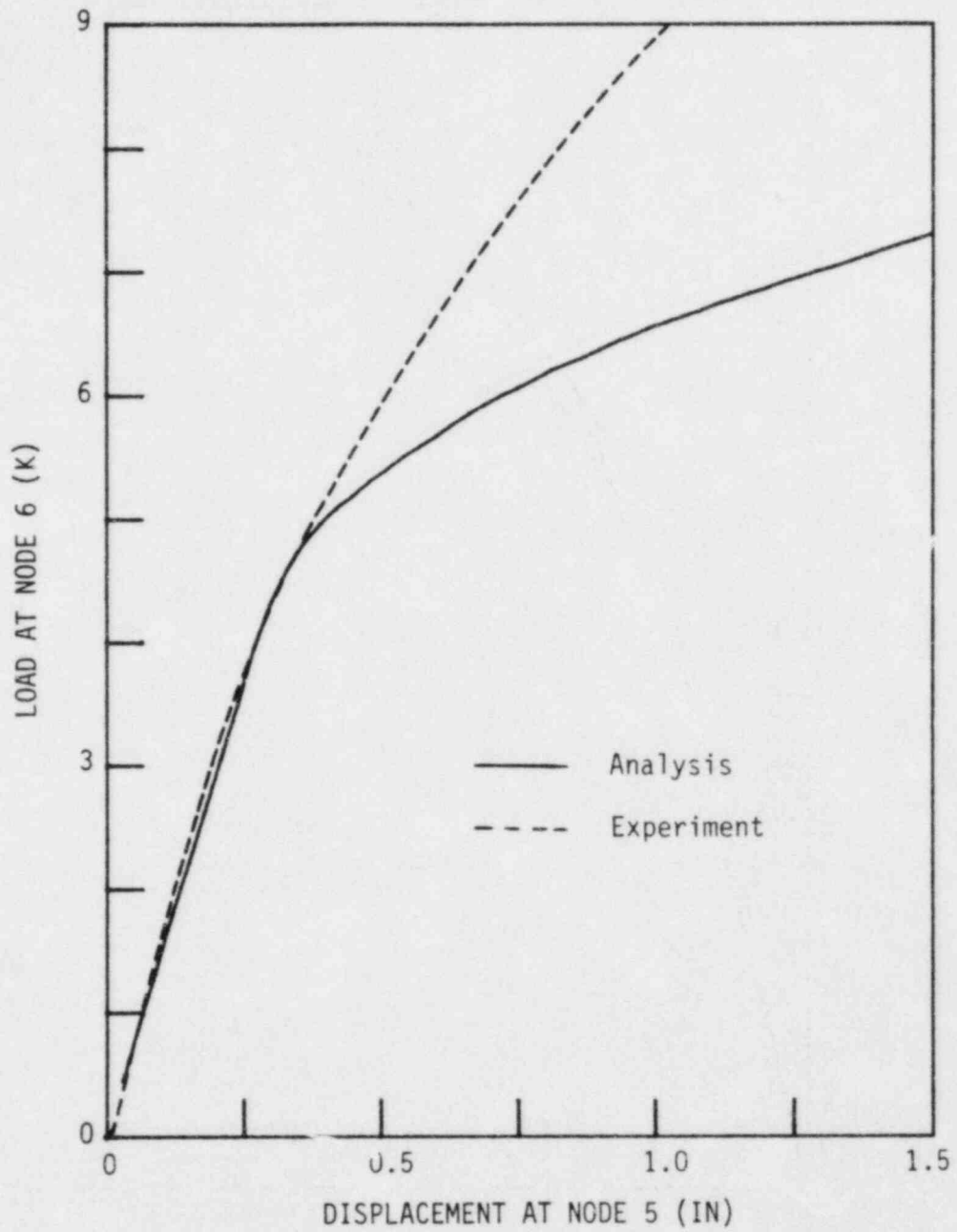


FIG. 2.1.17 TEST PE13.
UPWARDS LOAD, PRESSURE = 1500 PSI.

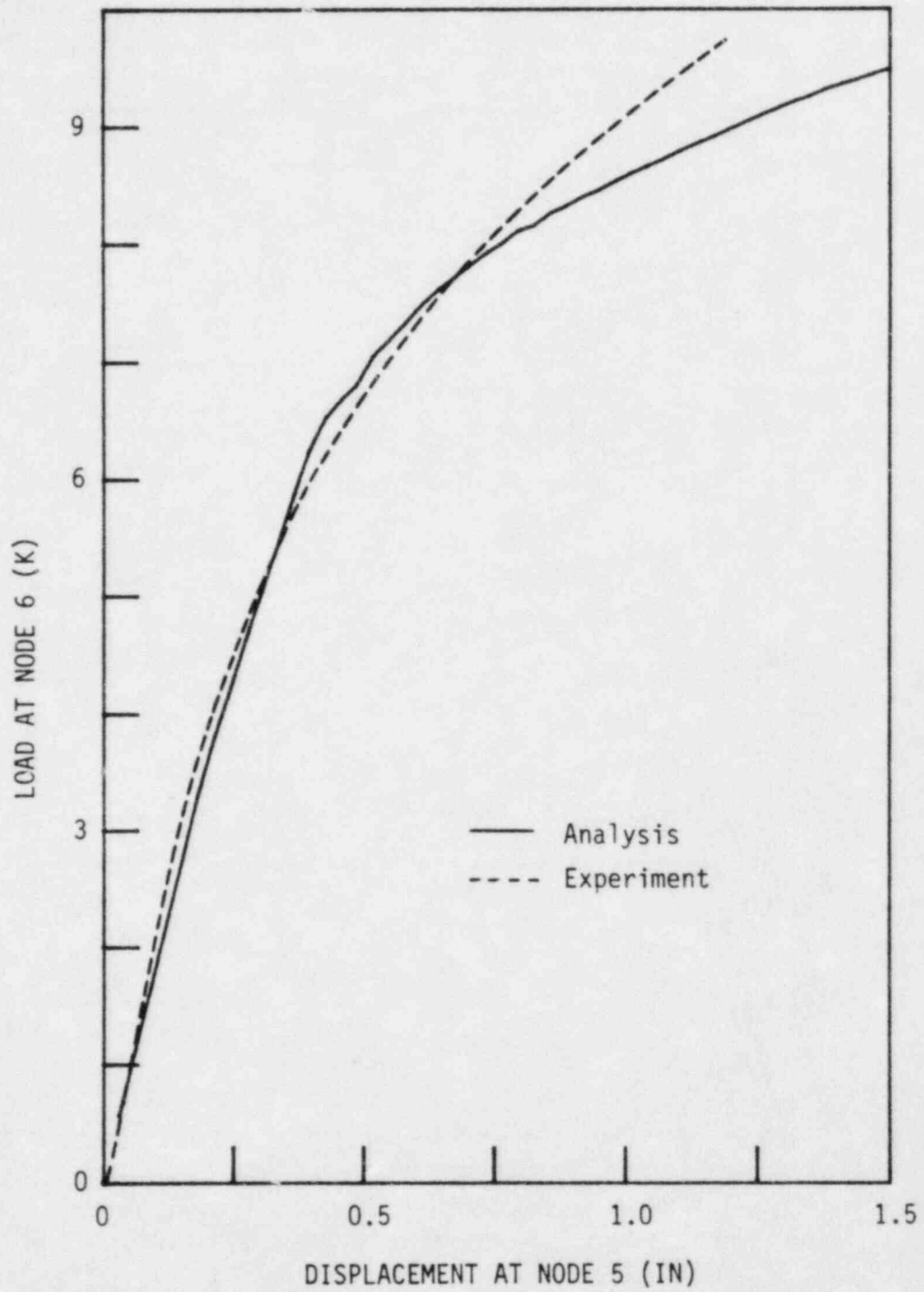


FIG. 2.1.18 TEST PE14.
OUT-OF-PLANE LOAD, PRESSURE = 1500 PSI.

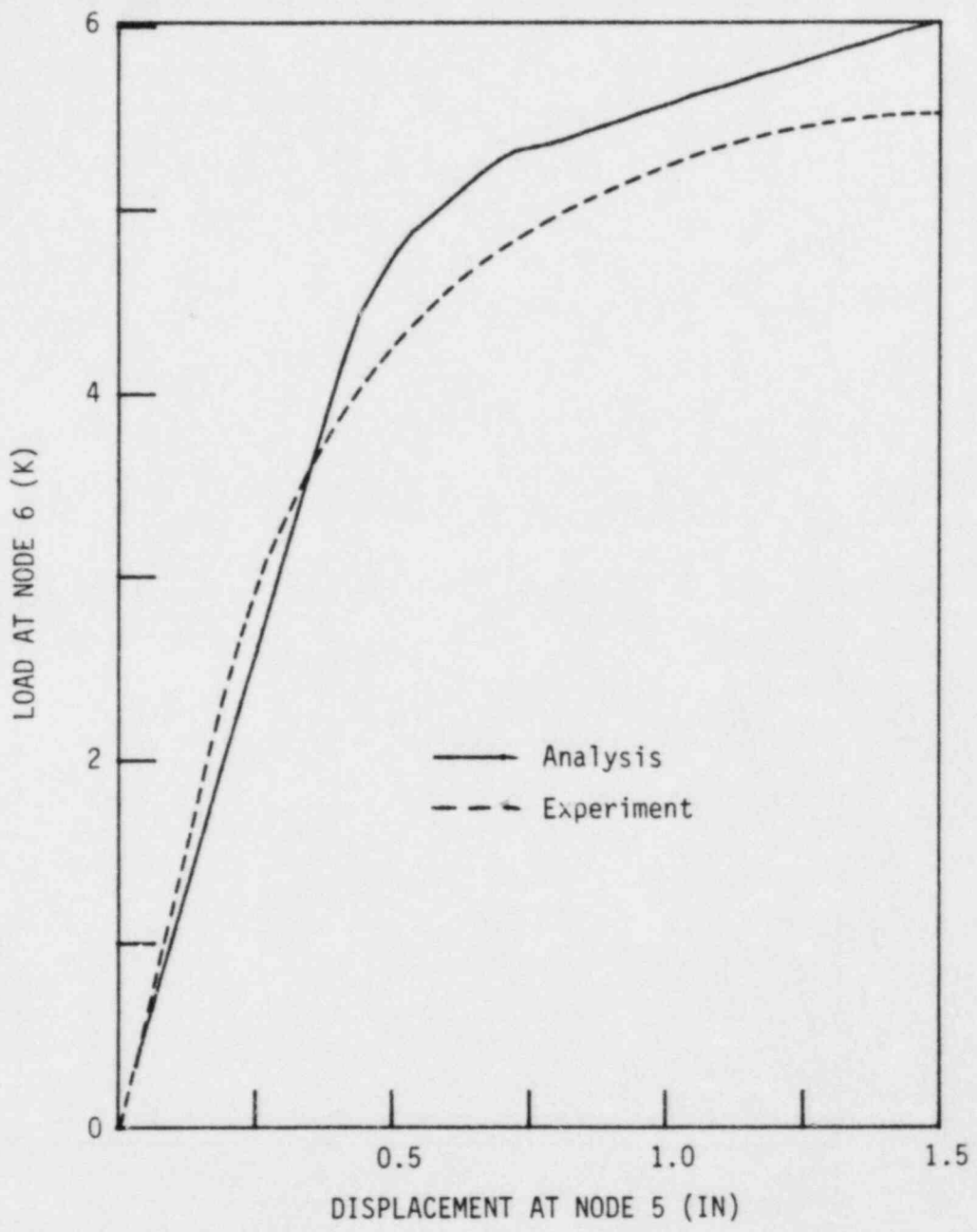


FIG. 2.1.19 TEST PE15.
DOWNWARDS LOAD, PRESSURE = 0.

TABLE 2.1.1 - PROPERTIES OF TEST SPECIMENS

Test No.	Pipe Size	Material	Yield Stress(ksi)	Loading	Lever Arm (in)	Pressure (psi)
PE1	6Sch40LR	A106B	50	Up	28.50	0
PE2				Down	28.25	0
PE3				Side	28.75	0
PE4				Up	27.56	1500
PE5				Down	27.50	1500
PE6				Side	27.75	1500
PE7	6Sch80LR	A106B	37.8	Up	25.00	0
PE8				Down	25.00	0
PE9				Side	25.88	0
PE10	6Sch40SR	A106B	39.6	Up	29.75	0
PE11				Down	30.00	0
PE12				Side	28.00	0
PE13				Up	27.50	1500
PE14				Side	27.00	1500
PE15	6Sch40LR	A312	37.7	Down	26.75	0

TABLE 2.1.2 - TRILINEAR APPROXIMATION - A-106B STEEL, 50 KSI		
Stress (ksi)	Strain	Modulus (ksi)
0	0	30000
45.5	.00152	1700
51.0	.00475	120

TABLE 2.1.3 - TRILINEAR APPROXIMATION - A-106B STEEL, 39.6 KSI		
Stress (ksi)	Strain	Modulus (ksi)
0	0	30000
36	.00120	1415
41.5	.00500	170

TABLE 2.1.4 - TRILINEAR APPROXIMATION - A-106B STEEL, 37.8 KSI		
Stress (ksi)	Strain	Modulus (ksi)
0	0	30000
34	.00113	1500
39.5	.00500	120

TABLE 2.1.5 - TRILINEAR APPROXIMATION - A312-304L STEEL, 37.7 KSI		
Stress (ksi)	Strain	Modulus (ksi)
0	0	29000
33	.00114	1630
45	.00850	210

TABLE 2.1.6 - WIPSLOG LISTING. GEOM PHASE.

```
EXEC - WIPS EXECUTIVE
Creating problem no. 1
Problem description: Bolt-Greenstreet Cases PE1,2,3

NEXT WIPS-EXEC COMMAND : geom

GEOM - SPECIFICATION OF SYSTEM GEOMETRY

Define units
Length (ft,in,m,mm) : in
Force (k,lb,kgf,kN) : k

Specify new GEOM data

START RUN NO. 1
Enter c.p. data in sequence along run

c.p. name and type : 1
coord option : d1
x,y,z :
Any changes? :

c.p. name and type : 2 tn
no. of extra nodes :
coord option :
tn generated automatically
Any changes? :

c.p. name and type : t1 t1
bend radius : 9
coord option :
c.p., dx,dy,dz : 1,,27
Any changes? :

c.p. name and type : 4 tn
no. of extra nodes : 1
coord option :
tn generated automatically
Any changes? :

c.p. name and type : 5
no. of extra nodes :
coord option :
c.p., dx,dy,dz : ,15
offset point defaults to preceding c.p.
Any changes? :

c.p. name and type : 6
no. of extra nodes :
coord option :
c.p., dx,dy,dz : t1 37.5
Any changes? :

c.p. name and type :
last c.p. in this run? : y
display GFDM data for this run? : y
```

Table 2.1.6 (cont'd)

G geom DATA FOR RUN

run no.	c.p. name	c.p. type	bend radius	xtra nods	coord opt	c.p. i	c.p.? j ?	coordinate x,dx,p	coordinate y,dy	data z,dz
1										
1				0	di			0.	0.	0.
2		tn		0	tn			0.	0.	0.
ti	ti		9.000	0	of	1		0.	27.000	0.
4		tn		1	tn			0.	0.	0.
5				0	of	4		15.000	0.	0.
6				0	of	ti		37.500	0.	0.

END OF DATA

STAFF RUN NO. 2

Enter c.p. data in sequence along run

c.p. name and type :

Last run? : y

Display new G geom data? :

Write in session log? :

Modify G geom data? :

Save current G geom data? : y

Comment for file catalog :

G geom DATA SAVED. FILE NAME = G geom0101

Produce COOR data? : y

Display COOR data? : y

COOR DATA

run no.	c.p. name	c.p. type	bend radius	node no.	x coord	y ? ccoord?	z ccoord
1							
1				1	0.	0.	0.
2		tn		2	0.	18.000	0.
ti	ti		9.000 center		0.	27.000	0.
					9.000	18.000	0.
4		tn		3	2.636	24.364	0.
				4	9.000	27.000	0.
5				5	24.000	27.000	0.
6				6	37.500	27.000	0.

END OF DATA

Plot geometry? :

Modify G geom data? :

DATA COMPLETE FOR THIS SESSION

Save final G geom data? : y

Comment for file catalog : Test PE1 (37.5)

G geom DATA SAVED. FILE NAME = G geom0101

Save COOR data? : y

Comment for file catalog : Test PE1 (37.5)

COOR DATA SAVED. FILE NAME = COOR0101

End of this G geom session

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

TABLE 2.1.7 - WIPSLOG LISTING FOR MATL, PIPE, UBAR AND FREC PHASES.

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : matl

MATL - SPECIFICATION OF MATERIAL PROPERTIES

Define units

Length (ft,in,m,mm) : in
Force (k,lb,kgf,kN) : k

Start new MATL file

Specify a new property set? : y

SET NO. = 1

Property set description : ASTM A106B 50ksi Trilinear.

Static moduli (min=2,max=5)
: 30000 1700 120

Yield strengths (no. of moduli minus 1)
: 45.5 51

Strain rate stiffnesses (min=0,max=3)
:

No strain rate effect
Use default tolerances? : y
Poisson ratio (dfit = .3) :
Weight density (dfit=steel) :

Any errors? :

This set added to MATL file

Specify a new property set? :

No. of property sets in MATL file = 1

Display property set descriptions? :
Write in session log? :

Display new property set data? :
Write in session log? :

Display all property set data? : y

MATL PROPERTY DATA

SET NO. 1. ASTM A106B 50ksi Trilinear.

Matl Type	Data Type	Segm No.	Modulus or Coefficient	Stress/Strain Limit
WRC2	static	1	0.3000e+05	0.4550e+02
		2	0.1700e+04	0.5100e+02
		3	0.1200e+03	
	yld.tol.		0.2000e-01	
	stif tol		0.5000e-01	

Table 2.1.7 (cont'd)

```
rate tol          0.5000e-01
poisson           0.3000e+00
density           0.2840e-03
Hit RETURN for next set
END OF DATA

New MATL file created
Comment for file catalog : 1 set

End this MATL session? : y

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : pipe

PIPE - SPECIFICATION OF PIPE PROPERTIES

Define units
  Length (ft,in,m,mm) : in
  Force (k,lb,kgf,kN) : k

No. of MATL property sets available = 1
Display material descriptions? :
Write in session log? :

Start new PIPE file

Specify a new property set? : y

SET NO. = 1
Property set description : 6sch40, A106B 50ksi.
  Outside diameter : 6.625
  Wall thickness : .28
  Weight/unit length (dfit=pipe weight) :
  No. of X-section elements (dfit=12) :
  Material number : 1
  Large ovaling (yes or no)? (dfit=no) : y
  Use default ovaling properties? :
  No. of hardening ratios for ovaling (dfit=2) :
  Hardening ratios for ovaling : .35 .08
  Stiffness modification factor : 1
  Strength modification factor : 1

Any errors? :

This set added to PIPE file

Specify a new property set? : y

SET NO. = 2
Property set description : As for Set 1 but small ovaling.
  Outside diameter : 6.625
  Wall thickness : .28
  Weight/unit length (dfit=pipe weight) :
  No. of X-section elements (dfit=12) :
```


Table 2.1.7 (cont'd)

Material number : 1
 Large ovaling (yes or no)? (dflt=no) :
 Use default ovaling properties? :
 No. of hardening ratios for ovaling (dflt=2) :
 Hardening ratios for ovaling : .35 .08
 Stiffness modification factor : 1
 Strength modification factor : 1

Any errors? :

This set added to PIPE file

Specify a new property set? :

No. of property sets in PIPE file = 2

Display property set descriptions? : y

PIPE PROPERTY DESCRIPTIONS

Set No.	Description
1	6sch40, A106B 50ksi.
2	As for Set 1 but small ovaling.

Display new property set data? :

Write in session log? :

Display all property set data? : y

PIPE PROPERTY DATA

SET NO. 1. 6sch40, A106B 50ksi.

Data Type	Segm No.	Modulus or Data Value	Stress/Strain Limit
Outside diameter		0.6625e+01	
Wall thickness		0.2800e+00	
Unit weight		0.1585e-02	
No. of elements		12	
No. of slices		2	
Stress v strain	1	0.3000e+05	0.4550e+02
	2	0.1700e+04	0.5100e+02
	3	0.1200e+03	
Poisson ratio		0.3000e+00	
Large ovaling		yes	
Ovaling ratios	1	0.3500e+00	
	2	0.0800e-01	

Hit RETURN for next set

SET NO. 2. As for Set 1 but small ovaling.

Data Type	Segm No.	Modulus or Data Value	Stress/Strain Limit
Outside diameter		0.6625e+01	
Wall thickness		0.2800e+00	

Table 2.1.7 (cont'd)

Unit weight		0.1585e-02	
No. of elements		12	
No. of slices		2	
Stress v strain	1	0.3000e+05	0.4550e+02
	2	0.1700e+04	0.5100e+02
	3	0.1200e+03	
Poisson ratio		0.3000e+00	
Large ovaling		no	
Ovaling ratios	1	0.3500e+00	
	2	0.8000e-01	

HIT RETURN for next set
END OF DATA

New PIPE file created
Comment for file catalog : 2 sets

End this PIPE session? : y

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : ubar

UBAR - SPECIFICATION OF U-BAR PROPERTIES

Define units
Length (ft;in;m;mm) : in
Force (k,lb,kgf,kN) : k

Start new UBAR file

Specify a new property set? : y

SET NO. = 1
Property set description : Stiff bar to control displ.
Static stiffnesses (min=2,max=6)
: 2000 200
Static strengths (no. of stiffnesses minus 1)
: 1e6
Extension rate Stiffnesses (min=0,max=3)
:
No extension rate effect
Default gap clearance : .001
Use default tolerances? : y

Any errors? :

This set added to UBAR file

Specify a new property set? :

No. of property sets in UBAR file = 1

Display property set descriptions? :
Write in session log? :

Display new property set data? :

Table 2.1.7 (cont'd)

Write in session log? :

Display all property set data? : y

UBAR PROPERTY DATA

SET NO. 1. Stiff bar to control displs.

Data Type	Segm No.	Stiffness or Coefficient	Force Limit
Static properties	1	0.2000e+04	0.1000e+07
	2	0.2000e+03	
Default gap		0.1000e-02	
Stiffness tol.		0.5000e-01	
Overshoot tol.		0.2000e+00	
Unloading tol.		0.2000e+00	

Hit RETURN for next set
END OF DATA

New UBAR file created
Comment for file catalog : 1 set

End this UBAR session? : y

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : frec

FREC - SPECIFY DYNAMIC FORCE RECORDS

Define units
Length (ft,in,m,mm) : in
Force (k,lb,kgf,kN) : k

Start new FREC file

Specify a new record? : y

RECORD NO. 1

Record name (4 characters) : rec1
Description (max. 40 char.) : Ramp to 10000k in 10 sec.

Enter Time-Force pairs
First pair automatically set to 0,0
Pair no. 2 : 10 10000
Pair no. 3 :
Last pair? : y
Any errors? :

Specify a new record? :

Display any records? :

Write records in session log? :

End this FREC session? : y
New FREC file created
Comment for file catalog : 1 record

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

TABLE 2.1.8 - WIPSLOG LISTING. MODL AND DATA PHASES.

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : mod1

MODL - SPECIFICATION OF ANALYSIS MODEL

Define units
 Length (ft,in,m,mm) : in
 Force (k,lb,kgf,kN) : k

Sequence no. of COOR file : 1

Available element property sets

Type	No. of Sets
pipe	2
ubar	1

Available substructure property sets
 None

DEFINE MODEL IN SEGMENTS

SEGMENT NO. 1

Pipe run no. : 1
 First c.p. of segment : 1
 Full 3D motion? :
 Displacement plane (xy,yz or zx) : xy
 Any substructures in this segment? :
 Boundary condition code for first c.p. : 111111

Specify c.p.name + elem type + optional data

1: 6 pipe pr=1 wf=1e-10
 2: 6 ubar pr=1 dy=-1 gap=.001
 3:

End of segment? : y
 Display commands for this segment? : y

MODL COMMAND TABLE

SEGMENT NO.	1.	Run No.	= 1				
c.p.	elem	optn	data	optn	data	optn	data
1		bcon	111111				
6	pipe	prop	1	ldis	no	this	yes
		loc1	+				
		wfac	0.1000e-09				
6	ubar	prop	1	this	yes		
		ldis	no	gap	0.1000e-02		
		dylj	-1.0000				

Any changes? :

SEGMENT NO. 2

Table 2.1.8 (cont'd)

```
Pipe run no. :
Last segment? : y

Any external substructures? :

Display commands for all segments? :
Write in session log? :

Produce MODL file? : y
Wait while data is processed

Specify initial velocities ? :
Comment for file catalog : PE-1, large ovalling.

MODL file saved. File name = MODL0101
End of this MODL session

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : data

DATA - SET UP WIPS-ANAL INPUT DATA

Sequence no. of MODL file : 1

Problem description (4 lines)
Line 1 : Bolt-Greenstreet Test PE1.
Line 2 :
Line 3 : Large ovalling. ASTM A106B material. To 2.5in displ. at 6.
Line 4 :
GHP 7/82

Set up PAUSE files at end of analysis ? :
Wait while files are processed

Specify data for each loaded point
LOAD NO. 1
Force record name : rec1
Name of loaded c.p. : 6
Force direction (x,y,z or follower) : y
Scale factor (+,- controls direction) : 1
Time delay (sec) (dflt=0) :
LOAD NO. 2
Force record name :
Last load? : y

Time steps : initial + max + min : .05 .051 .049
Max steps + max total time : 50 10
Error tolerances : upper + lower : 1e10 1e-10

Results output intervals
Max. no. of steps : 1
Max. time (secs.) : 1
Integration scheme (newm or hilb)(dflt=newm) :
Damping factor (dflt=0.1) : .0001
Factor for time step increase (dflt=2.0) :
Factor for time step decrease (dflt=0.5) :
Max. unbal. to reduce time step (dflt=no limit) :
Max. unbal. to stop analysis (dflt=no limit) :

DATA file set complete
Comment for file catalog : PE1, Large ovalling.
WIPS-ANAL DATA FILES SET UP. PARENT FILE NAME = DATA0101

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit
```

TABLE 2.1.9 - LISTING OF DATA FILE FOR A TYPICAL CASE (TEST PE1)

```

ECHO0101  SLDG0101  RSLT0101
star,
gbui
new,main,nonl,cart,0
substructure name = main
refn,7
  1  0.          e+00  0.          e+00  0.          e+00
  2  0.          e+00  0.1800000e+02  0.          e+00
  3  0.2f36039e+01  0.2436396e+02  0.          e+00
  4  0.9000000e+01  0.2700000e+02  0.          e+00
  5  0.2400000e+02  0.2700000e+02  0.          e+00
  6  0.3750000e+02  0.2700000e+02  0.          e+00
9999
boun,7
  1  111111
  2  1110
  3  1110
  4  1110
  5  1110
  6  1110
9999
enod,c
matl,3,64
0.200000000e+010.299999982e+000.300000000e+050.170000000e+040.120000000e+03
0.455000000e+020.510000000e+020.999999932e+200.199999996e-010.499999970e-01
0.120000000e+020.200000000e+010.100000000e+010.200000000e+010.100000000e+01
0.100000000e+010.662500000e+010.280000001e+000.158f10788e-020.          e+00
0.349999994e+000.799999982e-010.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.499999970e-01
0.639999986e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.200000000e+010.299999982e+000.300000000e+050.170000000e+040.120000000e+03
0.455000000e+020.510000000e+020.999999932e+200.199999996e-010.499999970e-01
0.120000000e+020.200000000e+010.          e+000.200000000e+010.100000000e+01
0.100000000e+010.662500000e+010.280000001e+000.158f10788e-020.          e+00
0.349999994e+000.799999982e-010.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.499999970e-01
0.639999986e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.200000000e+010.          e+000.100000005e-020.499999970e-010.200000000e+04
0.200000000e+030.100000000e+070.999999932e+200.199999988e+000.199999988e+00
0.199999988e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00

```

Table 2.1.9 (cont'd)

```

0.          e+000.      g+000.          e+000.      e+000.      e+00
0.          e+000.      e+000.          e+000.      e+000.      e+00
0.          e+000.      e+000.          e+000.      e+000.      e+00
0.          e+000.      e+000.          e+000.      e+000.      e+00
0.          e+000.      e+000.          e+000.      e+000.      e+00
0.          e+000.      e+000.          e+000.      e+000.      e+00
elem,2
  2  1  1
  1  0  0  0  6  3  0  1  0  1
0.375000000e+020.260000000e+020.
0.          e+000.100000005e-02
      3  5  1
      1  0  0  0  1  2  1  0  1  1.00  1  0  1
-.100000000e+010.          e+000.          e+000.          e+00
      2  0  0  0  2  3  1  0  1  0  1  1
0.900000095e+010.180000000e+020.          e+000.          e+00
      3  0  0  0  3  4  1  0  1  0  1  1
0.900000095e+010.180000000e+020.          e+000.          e+00
      4  0  0  0  4  5  1  0  1  1  0  1
0.900000000e+010.280000000e+020.          e+000.          e+00
      5  0  0  0  5  6  1  0  1  1  0  1
0.240000000e+020.280000000e+020.          e+000.          e+00

nord,cpto
prof
end
fini
mode
tree,main
fini
mbui
new,main
pmas,7
  1C 0.18575e-14 0.18575e-14 0.18575e-14 0.          e+00 0.          e+00 0.          e+0000
  2C 0.25684e-14 0.25684e-14 0.25684e-14 0.          e+00 0.          e+00 0.          e+0000
  3C 0.14217e-14 0.14217e-14 0.14217e-14 0.          e+00 0.          e+00 0.          e+0000
  4C 0.22588e-14 0.22588e-14 0.22588e-14 0.          e+00 0.          e+00 0.          e+0000
  5C 0.29411e-14 0.29411e-14 0.29411e-14 0.          e+00 0.          e+00 0.          e+0000
  6C 0.13932e-14 0.13932e-14 0.13932e-14 0.          e+00 0.          e+00 0.          e+0000
  6C 0.          e+00 0.          e+00 0.          e+00 0.          e+00 0.          e+0000
end
fini
ptre
new,rec1,pair,2,100
(2elf,7)
  0.          e+00 0.          e+00
  0.1000000e+05 0.1000000e+02
fini
thou,217
      2          65  3  1  0  0
ndyn
mass
dylo,1,1
rec1 2 0.          1.000          1
      6

```


Table 2.1.9 (cont'd)

```

timo,rslt,1,0.1000e+01
auto,defi
inte,newm,0.5000e-01,0.e+00,0.e+00,0.1000e-03
stif
stif,upda
kinr,12
elmr,1,2,6,3
kinr,5
loop,50
zero,ltme
step
unba
auto,init
loop,20
stif
auto,load
load
disp
kinr,10
elmr,9,10
auto,merr,0.1000e-09,0.1000e+11
if,3,3,1,1
entr,1
auto,fact
kinr,1
if,3,2,2,3
entr,2
elmr,1
cont
goto,c
entr,3
auto,step,0.4900e-01,0.5100e-01,0.5000e+00,0.2000e+01
if,4,5,5,4
entr,4
inte,newm,,auto,0.e+00,0.e+00,0.e+00,0.1000e-03
entr,5
if,3,6,6,7
entr,6
kinr,12
elmr,5,2,6
kinr,5
stif,init
goto,f
entr,7
chou
elmr,1,2,4,6,11
kinr,4,9,11
wrou
zero,lrst
unba
summ
elmr,3
kinr,2
stif,upda
auto,exit,0.1000e+02
if,5,f,8,0

entr,f
cont
fini
stop
DATA0101

```


D2.2 PIPE WITH U-BAR RESTRAINT

D2.2.1 PURPOSE

This example tests the PIPE and UBAR elements, by comparison with test results and previously reported analysis results. Analyses are carried out both with and without strain rate effects.

D2.2.2 DESCRIPTION

Analyses and tests of simple pipe whip configurations have been reported by Esswein et al [2.2.1]. An analysis of one of the two configurations has been reported by Hibbitt and Karlsson [2.2.2]. The dimensions are shown in Fig. 2.2.1.

The following static material properties were reported in [2.2.1] for the pipe steel.

$$\sigma = 30000 \epsilon \text{ for } \sigma < 18.6 \quad (2.2.1a)$$

$$\sigma = 61.8 \epsilon^{0.2} \text{ for } \sigma > 18.6 \quad (2.2.1b)$$

where σ = stress (ksi) and ϵ = strain. For the analyses in both [2.2.1] and [2.2.2], the strength was increased by 50% to account for strain rate effects. The equations given in [2.2.1] are inconsistent in this respect. For the analysis in [2.2.2], the following consistent equations were used:

$$\sigma = 30000 \epsilon \text{ for } \sigma < 31.02 \quad (2.2.2a)$$

$$\sigma = (1.5 \times 81.8) \epsilon^{0.2} \text{ for } \sigma > 31.02 \quad (2.2.2b)$$

The following static force-extension relationship was reported in [2.2.1] for the U-bar restraint:

$$F = 681.4 \Delta \text{ for } \Delta < 0.005 \quad (2.2.3a)$$

$$F = 11.79 \Delta^{0.235} \text{ for } \Delta > 0.005 \quad (2.2.3b)$$

where F = restraint force (k) and Δ = extension (in.). For the analyses in [2.2.1] and [2.2.2], the strength was increased by 10% to account for strain rate effects. The following relationships were used:

$$F = 1.1 \times 681.4 \Delta \text{ for } \Delta < 0.005 \quad (2.2.4a)$$

$$F = (1.1 \times 11.79) \Delta^{0.235} \text{ for } \Delta > 0.005 \quad (2.2.4b)$$

For the analyses in [2.2.1] and [2.2.2], the inertia of the vertical leg was lumped at the elbow. This was not done for the WIPS analysis. Note that the rupture disc assembly weighed 210 lbs. This is a large proportion of the total weight and exerts a substantial influence on the response. The element subdivision for the WIPS analysis is shown in Fig. 2.2.2. The blow-down forcing function is shown in Table 2.2.1.

D2.2.3 PROPERTIES FOR WIPS ANALYSIS

The PIPE element with 12 subelements in the cross section was used to model the pipe, and a UBAR element to model the U-bar. Small displacements were assumed. The internal pressure in the pipe was assumed to be zero (i.e. internal pressure effects on pipe strength were ignored).

Analyses with the following material properties were carried out.

Case 1: Multilinear representations of the pipe steel and U-bar properties as shown in Tables 2.2.2 and 2.2.4. These correspond to the properties defined by Eqns. 2.2.1 and 2.2.3, with no allowance for strain rate effects.

- Case 2: Pipe steel and U-bar properties as shown in Tables 2.2.3 and 2.2.5. These correspond to the properties defined by Eqns. 2.2.2 and 2.2.4.
- Case 3: Pipe and U-bar properties as for Case 1, plus trilinear representations of strain rate effects as shown in Table 2.2.6. This strain rate data was used directly for the pipe steel. The data was converted to force-extension data for the U-bar, assuming a bar area of 0.22 in² (0.375 in. dia. bars) and an effective bar length of 9.7 in. The resulting effect is shown in Table 2.2.7. Note that these are assumptions for analysis purposes and do not necessarily represent the true strain rate behavior of the pipe and U-bar materials. The data in Table 2.2.6 is based on data for low carbon steel reported by Manjoine [2.2.3].

D2.2.4 WIPS INPUT DATA

Table 2.2.8 is the WIPSLOG listing for specification of the system geometry. Table 2.2.9 is the WIPSLOG listing for specification of the pipe and U-bar properties and the blowdown force record. Tables 2.2.10 and 2.2.11 are the WIPSLOG listings for the MODL and DATA phases for all three cases. Table 2.2.12 is the DATA file listing for Case 3. The DATA files for Cases 1 and 2 were the same as for Case 3, except for Columns 31-35 of the element cards.

D2.2.5 RESULTS

D2.2.5.1 General

Key results are summarized in Table 2.2.13. Time histories of computed restraint forces are shown in Figs. 2.2.3 through 2.2.5 for each of Cases 1, 2, and 3. The experimental values reported in [2.2.1] are also shown. In Fig. 2.2.4 the analysis results reported in [2.2.2] are shown. The results for all three cases are superimposed in Fig. 2.2.6 for comparison.

The analyses for Figs. 2.2.3 through 2.2.5 were carried out using the Newmark step-by-step option, with $\beta/\Delta t_0 = 0.1$ and $\Delta t_0 = 0.0002$ sec. An analysis was also carried out for Case 2 using the HHT option, with $\alpha = -0.05$. The results are shown in Fig. 2.2.7. These results are very close to those in Fig. 2.2.4.

D2.2.5.2 Discussion

The computed results for Cases 1, 2, and 3 differ significantly. The restraint force for Case 3 (with strain rate effects) is larger than the experimental value, and the corresponding restraint extension is smaller. This indicates that the assumed relationship between extension rate and strength increase is not correct. The agreement with experiment is closest for Case 2. This is not surprising since the 1.1 factor used in this analysis was probably chosen to match the experimental results.

The time to gap closure is virtually the same for all analyses. This suggests that the motion before gap closure is governed mainly by the inertia of the pipe and that the pipe strength has little effect.

The results for Case 2 using the Newmark and HHT step-by-step schemes were virtually identical. These results were very close to those reported in [2.2.2] up to unloading of the restraint, but the computed rebound behavior was significantly different.

For interest, the number of time steps required for each analysis is shown in Table 2.2.13. The upper midstep error tolerance in all cases was 14% of the initial jet force (7.2 k). The lower tolerance was one-fifth of the upper tolerance.

D2.2.6 CONCLUSION

This example shows that close agreement with experiment can be obtained, provided appropriate assumptions are made for the stiffness and strength properties of the pipe and restraint.

D2.2.7 REFERENCES

- 2.2.1 Esswein, G., Levy, S., Triplett, M., Chan, G., and Varadarajan, N., "Pipe Whip Dynamics," Conference on Dynamic Analysis of Pressure Vessels and Piping, ASME PVP-PB-022, 1978.
- 2.2.2 Hibbitt and Karlsson, "Analysis of Pipe Whip," EPRI NP-1208, Electric Power Research Institute, 1979.
- 2.2.3 Manjoine, M. J., "Influence of Rate of Strain and Temperature on Yield Stresses of Mild Steel," J. Appl. Mech., Vol. II, A-211, 1944.

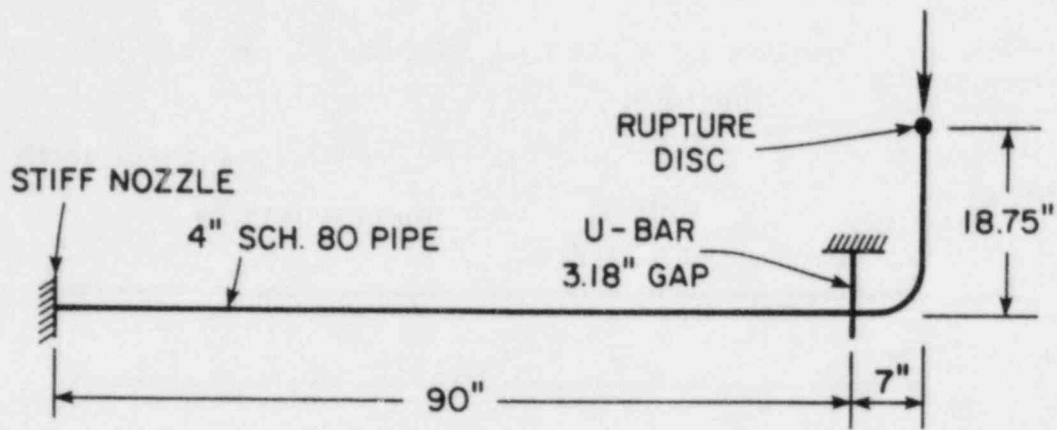


FIG. 2.2.1 SYSTEM DIMENSIONS

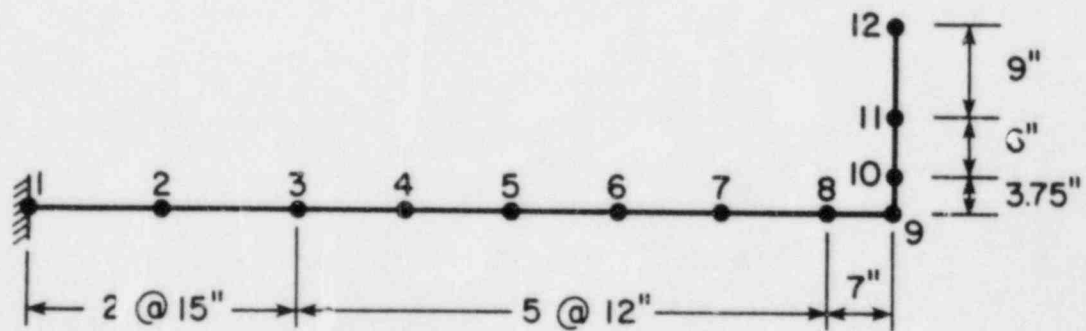


FIG. 2.2.2 ELEMENT SUBDIVISION

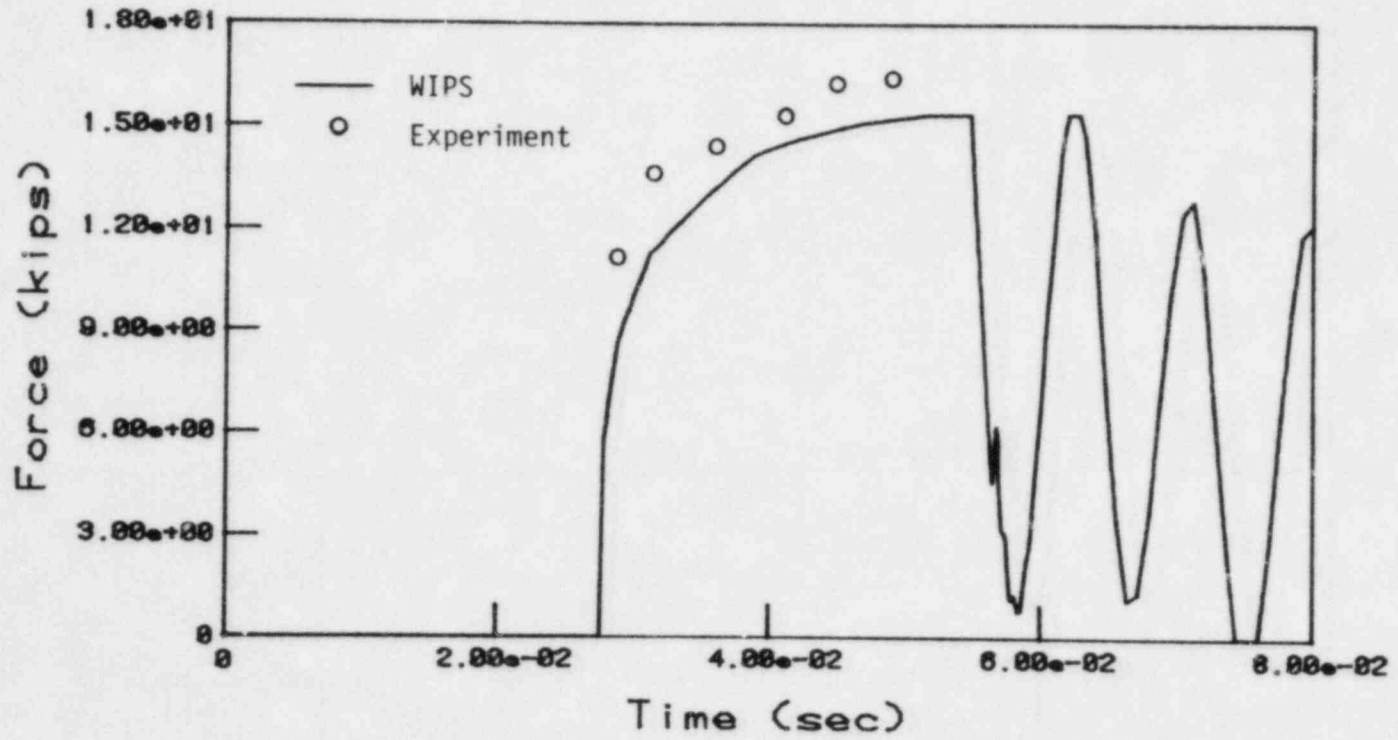


FIG. 2.2.3 RESTRAINT FORCE VS. TIME - CASE 1.

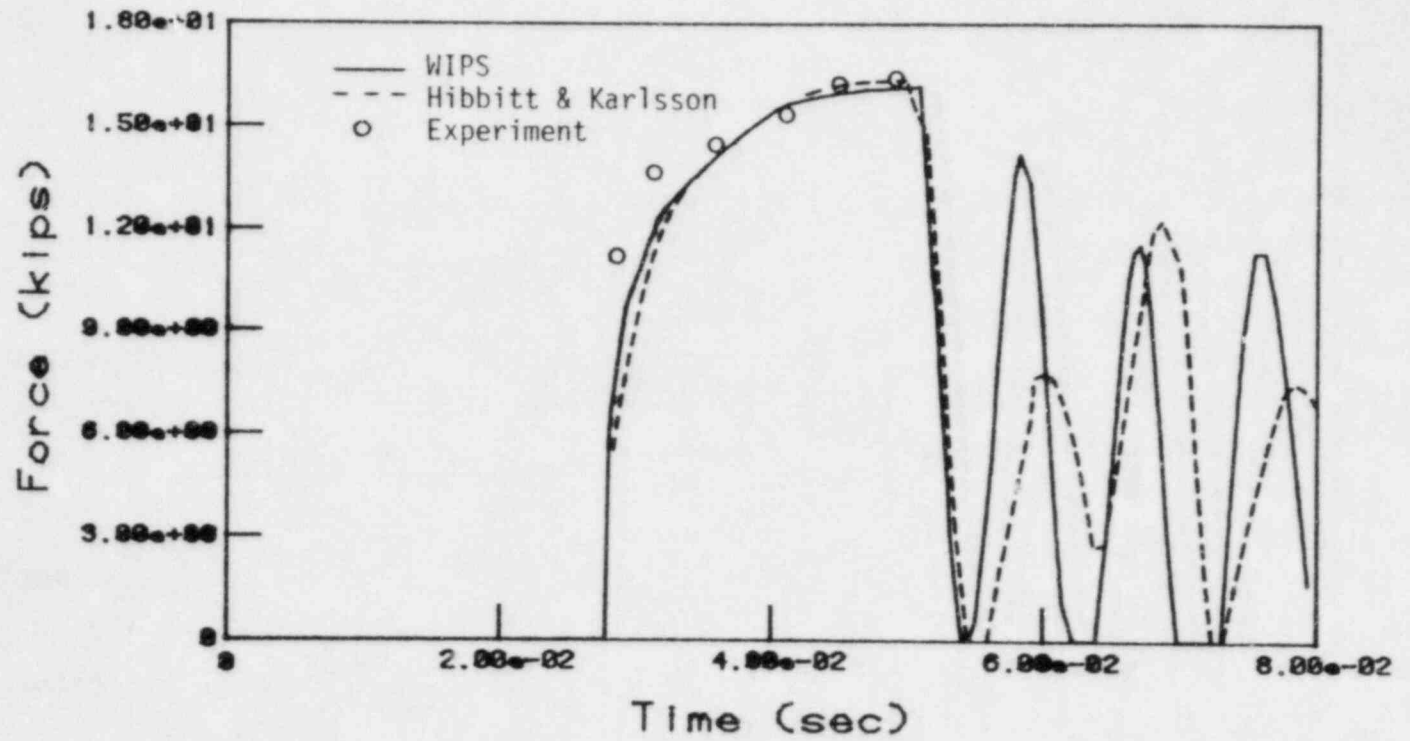


FIG. 2.2.4 RESTRAINT FORCE VS. TIME - CASE 2.

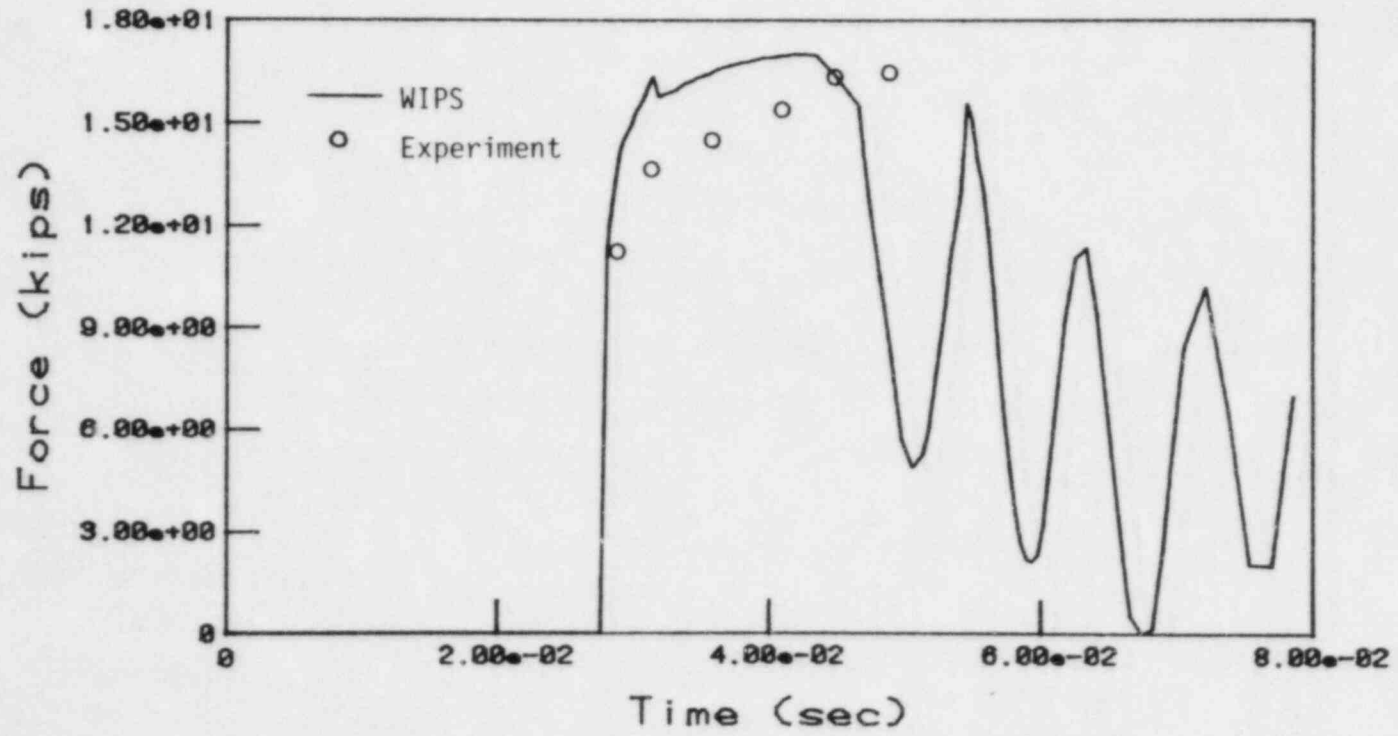


FIG. 2.2.5 RESTRAINT FORCE VS. TIME - CASE 3.

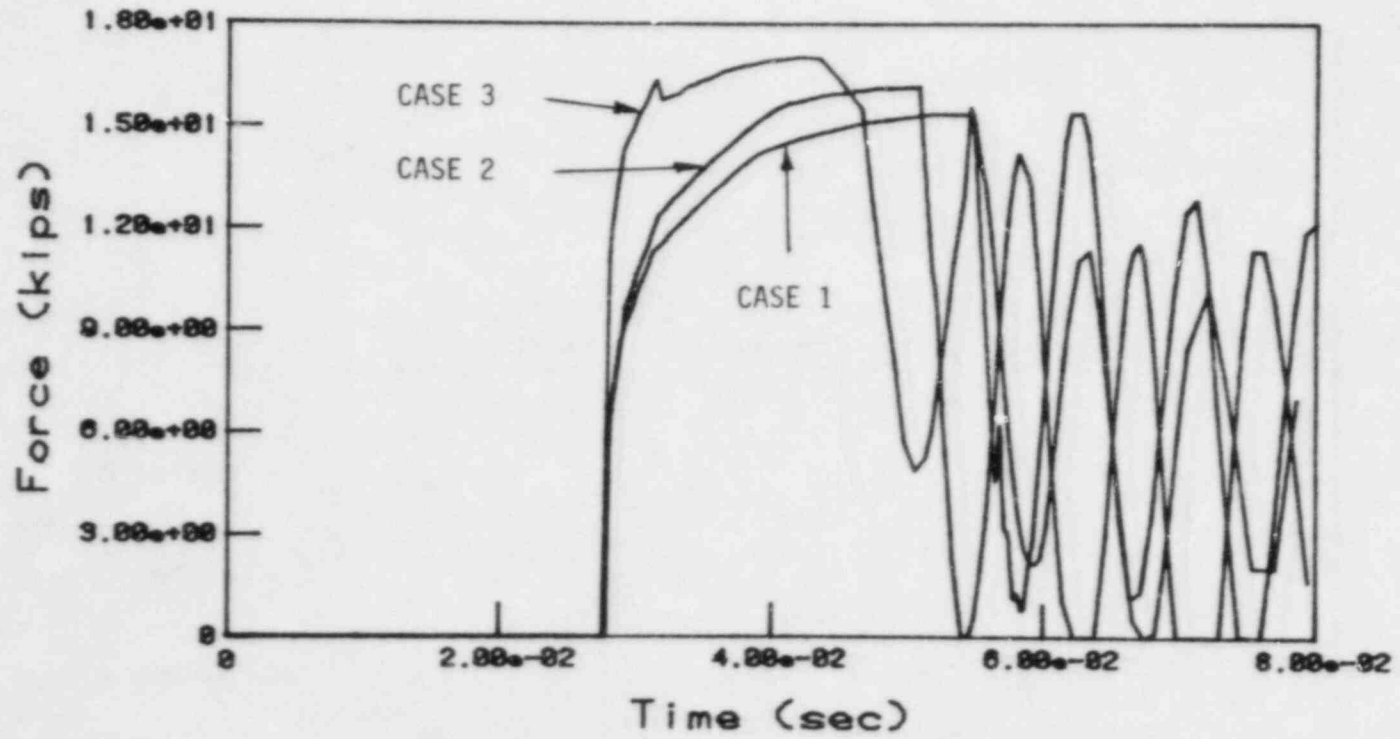


FIG. 2.2.6 RESTRAINT FORCE VS. TIME.
COMPARISON OF CASES 1, 2, AND 3.

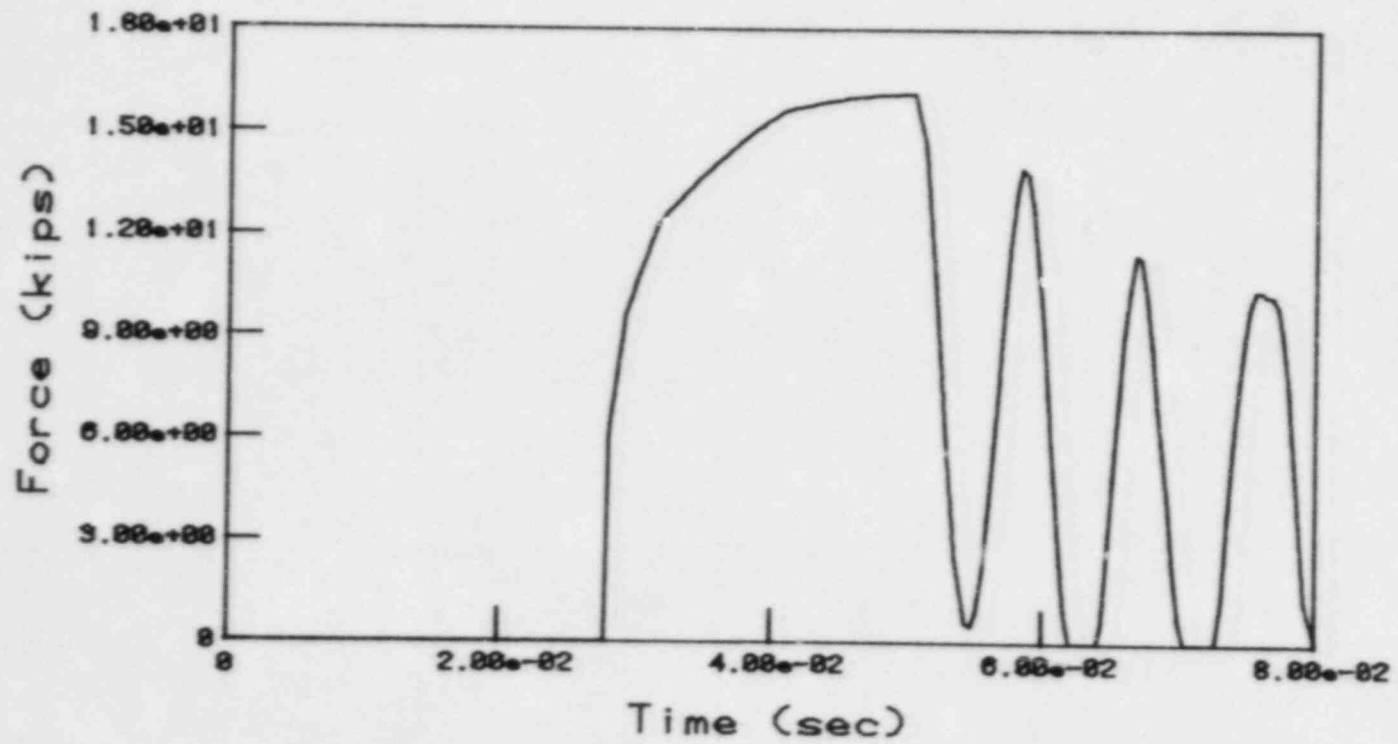


FIG. 2.2.7 RESTRAINT FORCE VS. TIME.
CASE 2 WITH HHT SOLUTION SCHEME.

TABLE 2.2.1 - BLOWDOWN FORCING FUNCTION

Time (sec)	Force (k)
0.00001	7.200
0.00045	7.200
0.00046	7.272
0.02910	7.272
0.02920	7.920
0.10000	7.920

TABLE 2.2.2 - TRILINEAR REPRESENTATION OF PIPE STEEL PROPERTIES FROM EQN. 2.2.1

Stress (ksi)	Strain	Modulus (ksi)
0	0	30000
19.0	.00063	2406
28.0	.00437	421

TABLE 2.2.3 - TRILINEAR REPRESENTATION OF PIPE STEEL PROPERTIES FROM EQN. 2.2.2

Stress (ksi)	Strain	Modulus (ksi)
0	0	30000
31.0	.00103	2607
45.0	.00640	533

TABLE 2.2.4 - MULTILINEAR REPRESENTATION OF U-BAR PROPERTIES FROM EQN. 2.2.3

Force (k)	Extension (in)	Stiffness (k/in)
0	0	681.39
5.50	0.0081	13.43
8.75	0.2500	5.00
11.25	0.7500	2.10
14.20	2.1500	1.00

TABLE 2.2.5 - MULTILINEAR REPRESENTATION OF U-BAR PROPERTIES FROM EQN. 2.2.4

Force (k)	Extension (in)	Stiffness (k/in)
0	0	750.0
6.05	0.0081	14.80
9.63	0.2500	5.50
12.38	0.7500	2.31
15.62	2.1500	1.00

TABLE 2.2.6 - ASSUMED STRAIN RATE EFFECT FOR PIPE STEEL TRILINEAR REPRESENTATION		
Stress Increase (ksi)	Strain Rate (sec ⁻¹)	Stiffness (ksi.sec)
0	0	25.00
9.00	0.36	2.20
18.00	4.44	0.44

TABLE 2.2.7 - ASSUMED STRAIN RATE EFFECT FOR U-BAR TRILINEAR REPRESENTATION		
Force Increase (k)	Extension Rate (in/sec)	Stiffness (k.sec/in)
0	0	0.566
1.98	3.50	0.050
3.96	43.07	0.010

TABLE 2.2.8 - WIPSLOG LISTING. GEOM PHASE.

```
EXEC - WIPS EXECUTIVE
Creating problem no. 1
Problem description: DECC-Esswein

NEXT WIPS-EXEC COMMAND : geom

GEOM - SPECIFICATION OF SYSTEM GEOMETRY

Define units
  Length (ft,in,m,mm) : in
  Force (k,lb,kgf,kN) : k

Specify new GEOM data

START RUN NO. 1
Enter c.p. data in sequence along run

  c.p. name and type : 1
  cocrd option : di
  x,y,z :
  Any changes? :

  c.p. name and type : 3
  no. of extra nodes : 1
  cocrd option :
  c.p., dx,dy,dz : ,30
  offset point defaults to preceding c.p.
  Any changes? :

  c.p. name and type : 8
  no. of extra nodes : 4
  cocrd option :
  c.p., dx,dy,dz : ,60
  offset point defaults to preceding c.p.
  Any changes? :

  c.p. name and type : 9
  no. of extra nodes :
  cocrd option :
  c.p., dx,dy,dz : ,7
  offset point defaults to preceding c.p.
  Any changes? :

  c.p. name and type : 10
  no. of extra nodes :
  cocrd option :
  c.p., dx,dy,dz : ,,3.75
  offset point defaults to preceding c.p.
  Any changes? :

  c.p. name and type : 11
  no. of extra nodes :
  cocrd option :
  c.p., dx,dy,dz : ,,6
  offset point defaults to preceding c.p.
  Any changes? :
```

Table 2.2.8 (cont'd)

c.p. name and type : 12
 no. of extra nodes :
 coord option :
 c.p., dx,dy,dz : ,,9
 offset point defaults to preceding c.p.
 Any changes? :

c.p. name and type :
 Last c.p. in this run? : y
 Display GEOM data for this run? : y

GEOM DATA FOR RUN

run no.	c.p. name	c.p. type	bend radius	xtra nods	coord opt	c.p. i	c.p. j ?	coordinate data		
								x,dx,p	y,dy	z,dz
1	1			0	di			0.	0.	0.
	3			1	of	1		30.000	0.	0.
	8			4	of	3		60.000	0.	0.
	9			0	of	8		7.000	0.	0.
	10			0	of	9		0.	3.750	0.
	11			0	of	10		0.	6.000	0.
	12			0	of	11		0.	9.000	0.

END OF DATA

START RUN NO. 2
 Enter c.p. data in sequence along run

c.p. name and type :
 Last run? : y

Display new GEOM data? :
 Write in session log? :

Modify GEOM data? :

Save current GEOM data? : y
 Comment for file catalog :
 GEOM DATA SAVED. FILE NAME = GEOM0101

Produce COOR data? : y

Display COOR data? : y

COOR DATA

run no.	c.p. name	c.p. type	bend radius	node no.	x coord	y ? coord?	z coord
1	1			1	0.	0.	0.
				2	15.000	0.	0.
	3			3	30.000	0.	0.

Table 2.2.8 (cont'd)

	4	42.000	0.	0.
	5	54.000	0.	0.
	6	66.000	0.	0.
	7	78.000	0.	0.
8	8	90.000	0.	0.
9	9	97.000	0.	0.
10	10	97.000	3.750	0.
Hit RETURN for more				
11	11	97.000	9.750	0.
12	12	97.000	18.750	0.
END OF DATA				

Plot geometry? :

Modify GEOM data? :

DATA COMPLETE FOR THIS SESSION

Save final GEOM data? : y

Comment for file catalog : Esswein discretization,

GEOM DATA SAVED. FILE NAME = GEOM0101

Save COOR data? : y

Comment for file catalog : Esswein discretization.

COOR DATA SAVED. FILE NAME = COOR0101

End of this GEOM session

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

TABLE 2.2.9 - WIPSLOG LISTING. MATL, PIPE, UBAR AND FREC PHASES.

EXEC - NIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : wat1

MATL - SPECIFICATION OF MATERIAL PROPERTIES

Define units

Length (ft,in,m,mm) : in

Force (k,lb,kgf,kN) : k

Start new MATL file

Specify a new property set? : y

SET NO. = 1

Property set description : Trilinear, no strain rate.

Static moduli (min=2,max=5)

: 30000 2406 421

Yield strengths (no. of moduli minus 1)

: 19 28

Strain rate stiffnesses (min=0,max=3)

:

No strain rate effect

Use default tolerances? : y

Poisson ratio (dfit = .3) :

Weight density (dfit=steel) :

Any errors? :

This set added to MATL file

Specify a new property set? : y

SET NO. = 2

Property set description : Trilinear, with strain rate.

Static moduli (min=2,max=5)

: 30000 2406 421

Yield strengths (no. of moduli minus 1)

: 19 28

Strain rate stiffnesses (min=0,max=3)

: 25 2.2 .44

Strain rate limits (no. of stiffnesses minus 1)

: .36 4.44

Use default tolerances? : y

Poisson ratio (dfit = .3) :

Weight density (dfit=steel) :

Any errors? :

This set added to MATL file

Specify a new property set? : y

SET NO. = 3

Property set description : Trilinear, 50% Increase.

Table 2.2.9 (cont'd)

```

Static moduli (min=2,max=5)
: 30000 2607 533
Yield strengths (no. of moduli minus 1)
: 31 45
Strain rate stiffnesses (min=0,max=3)
:
No strain rate effect
Use default tolerances? : y
Poisson ratio (dflt = .3) :
Weight density (dflt=steel) :
    
```

Any errors? :

This set added to MATL file

Specify a new property set? :

No. of property sets in MATL file = 3

Display property set descriptions? :
Write in session log? :

Display new property set data? :
Write in session log? :

Display all property set data? : y

MATL PROPERTY DATA

SET NO. 1. Trilinear, no strain rate.

Matl Type	Data Type	Segw No.	Modulus or Coefficient	Stress/Strain Limit
mrcz	static	1	0.3000e+05	0.1900e+02
		2	0.2406e+04	0.2800e+02
		3	0.4210e+03	
	yld.tol.		0.2000e-01	
	stif tol		0.5000e-01	
	rate tol		0.5000e-01	
	poisson		0.3000e+00	
	density		0.2840e-03	

Hit RETURN for next set

SET NO. 2. Trilinear, with strain rate.

Matl Type	Data Type	Segw No.	Modulus or Coefficient	Stress/Strain Limit
mrcz	static	1	0.3000e+05	0.1900e+02
		2	0.2406e+04	0.2800e+02
		3	0.4210e+03	
	str.rate	1	0.2500e+02	0.3600e+00
		2	0.2200e+01	0.4440e+01
		3	0.4400e+00	
	yld.tol.		0.2000e-01	

Table 2.2.9 (cont'd)

```

          stif tol      0.5000e-01
          rate tol      0.5000e-01
          poisson       0.3000e+00
          density       0.2840e-03
Hit RETURN for next set

SET NO. 3. Trilinear, 50% increase.

          Matl      Data      Segm      Modulus or      Stress/Strain
          Type      Type      No.      Coefficient      Limit
          MROZ
          static      1      0.3000e+05      0.3100e+02
                              2      0.2607e+04      0.4500e+02
                              3      0.5330e+03
          yld.tol.    0.2000e-01
          stif tol    0.5000e-01
          rate tol    0.5000e-01
          poisson     0.3000e+00
          density     0.2840e-03
Hit RETURN for next set
END OF DATA

New MATL file created
Comment for file catalog : 3 materials

End this MATL session? : y

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : pipe

PIPE - SPECIFICATION OF PIPE PROPERTIES

Define units
Length (ft,in,m,mm) : in
Force (k,lb,kgf,kN) : k

No. of MATL property sets available = 3
Display material descriptions? : y

MATL PROPERTY DESCRIPTIONS
Set No.  Type  Description
  1      MROZ  Trilinear, no strain rate.
  2      MROZ  Trilinear, with strain rate.
  3      MROZ  Trilinear, 50% increase.

Start new PIPE file

Specify a new property set? : y

SET NO. = 1
Property set description : 4sch80, no strain rate.
Outside diameter : 4.5
Wall thickness : .337
Weight/unit length (dflt=pipe weight) :

```

Table 2.2.9 (cont'd)

No. of X-section elements (dflt=12) :
Material number : 1
Large ovaling (yes or no)? (dflt=no) :
Use default ovaling properties? : y

Any errors? :

This set added to PIPE file

Specify a new property set? : y

SET NO. = 2
Property set description : 4sch80, with strain rate
Outside diameter : 4.5
Wall thickness : .337
Weight/unit length (dflt=pipe weight) :
No. of X-section elements (dflt=12) :
Material number : 2
Large ovaling (yes or no)? (dflt=no) :
Use default ovaling properties? : y

Any errors? :

This set added to PIPE file

Specify a new property set? : y

SET NO. = 3
Property set description : 4sch80, 50% strength increase.
Outside diameter : 4.5
Wall thickness : .337
Weight/unit length (dflt=pipe weight) :
No. of X-section elements (dflt=12) :
Material number : 3
Large ovaling (yes or no)? (dflt=no) :
Use default ovaling properties? : y

Any errors? :

This set added to PIPE file

Specify a new property set? :

No. of property sets in PIPE file = 3

Display property set descriptions? : y

PIPE PROPERTY DESCRIPTIONS

Set No.	Description
1	4sch80, no strain rate.
2	4sch80, with strain rate
3	4sch80, 50% strength increase.

Display new property set data? :
Write in session log? :

Table 2.2.9 (cont'd)

Display all property set data? : y

PIPE PROPERTY DATA

SET NO. 1. 4sch80, no strain rate.

Data Type	Segm No.	Modulus or Data Value	Stress/Strain Limit
Outside diameter		0.4500e+01	
Wall thickness		0.3370e+00	
Unit weight		0.1252e-02	
No. of elements		12	
No. of slices		2	
Stress v strain	1	0.3000e+05	0.1900e+02
	2	0.2406e+04	0.2800e+02
	3	0.4210e+03	
Poisson ratio		0.3000e+00	
Large ovaling		no	
Ovaling ratios	1	0.4000e+00	
	2	0.5000e-01	

Hit RETURN for next set

SET NO. 2. 4sch80, with strain rate

Data Type	Segm No.	Modulus or Data Value	Stress/Strain Limit
Outside diameter		0.4500e+01	
Wall thickness		0.3370e+00	
Unit weight		0.1252e-02	
No. of elements		12	
No. of slices		2	
Stress v strain	1	0.3000e+05	0.1900e+02
	2	0.2406e+04	0.2800e+02
	3	0.4210e+03	
Stress v strain rate	1	0.2500e+02	0.3600e+00
	2	0.2200e+01	0.4440e+01
	2	0.2200e+01	
Poisson ratio		0.3000e+00	
Large ovaling		no	
Ovaling ratios	1	0.4000e+00	
	2	0.5000e-01	

Hit RETURN for next set

SET NO. 3. 4sch80, 50% strength increase.

Data Type	Segm No.	Modulus or Data Value	Stress/Strain Limit
Outside diameter		0.4500e+01	
Wall thickness		0.3370e+00	
Unit weight		0.1252e-02	
No. of elements		12	
No. of slices		2	
Stress v strain	1	0.3000e+05	0.3100e+02

Table 2.2.9 (cont'd)

	2	0.2607e+04	0.4500e+02
	3	0.5330e+03	
Poisson ratio		0.3000e+00	
Large ovaling		no	
Ovaling ratios	1	0.4000e+00	
	2	0.5000e-01	

Hit RETURN for next set
END OF DATA

New PIPE file created
Comment for file catalog : 3 sets.

End this PIPE session? : y

EXEC - MIPS EXECUTIVE

NEXT MIPS-EXEC COMMAND : ubar

UBAR - SPECIFICATION OF U-BAR PROPERTIES

Define units
Length (ft;in;mm) : in
Force (k,lb,kgf,kN) : k

Start new UBAR file

Specify a new property set? : y

SET NO. = 1
Property set description : 5 segments, no strain rate.
Static stiffnesses (min=2,max=6)
: 681.39 13.43 5 2.1 1
Static strengths (no. of stiffnesses minus 1)
: 5.5 8.75 11.25 14.2
Extension rate Stiffnesses (min=0,max=3)
:
No extension rate effect
Default gap clearance :
*** error - must be positive
Default gap clearance : 3.18
Use default tolerances? : y

Any errors? :

This set added to UBAR file

Specify a new property set? : y

SET NO. = 2
Property set description : 5 segments, with strain rate.
Static stiffnesses (min=2,max=6)
: 681.39 13.43 5 2.1 1
Static strengths (no. of stiffnesses minus 1)
: 5.5 8.75 11.25 14.2
Extension rate Stiffnesses (min=0,max=3)
: .566 .05 .01

Table 2.2.9 (cont'd)

```

Strength limit (no. of stiffnesses minus 1)
: 1.98 3.96
Default gap clearance : 3.18
Use default tolerances? : y

Any errors? :

This set added to UBAR file

Specify a new property set? : y

SET NO. = 3
Property set description : 5 segments, 10% increase.
Static stiffnesses (min=2,max=6)
: 750 14.8 5.5 2.31 1
Static strengths (no. of stiffnesses minus 1)
: 6.05 9.63 12.38 15.62
Extension rate Stiffnesses (min=0,max=3)
:
No extension rate effect
Default gap clearance : 3.18
Use default tolerances? : y

Any errors? :

This set added to UBAR file

Specify a new property set? :

No. of property sets in UBAR file = 3

Display property set descriptions? : y

UBAR PROPERTY DESCRIPTIONS
Set No.  Description
  1      5 segments, no strain rate.
  2      5 segments, with strain rate.
  3      5 segments, 10% increase.

Display new property set data? :
Write in session log? :

Display all property set data? : y

UBAR PROPERTY DATA

SET NO. 1. 5 segments, no strain rate.

      Data          Segm  Stiffness or   Force
      Type          Mc.   Coefficient   Limit
Static properties  1      0.6814e+03  0.5500e+01
                  2      0.1343e+02  0.8750e+01
                  3      0.5000e+01  0.1125e+02
                  4      0.2100e+01  0.1420e+02
                  5      0.1000e+01

```

Table 2.2.9 (cont'd)

```

      Default gap          0.3180e+01
      Stiffness tol.      0.5000e-01
      Overshoot tol.     0.2000e+00
      Unloading tol.     0.2000e+00
Hit RETURN for next set

```

SET NO. 2. 5 segments, with strain rate.

Data Type	Segm No.	Stiffness or Coefficient	Force Limit
Static properties	1	0.6814e+03	0.5500e+01
	2	0.1343e+02	0.8750e+01
	3	0.5000e+01	0.1125e+02
	4	0.2100e+01	0.1420e+02
	5	0.1000e+01	
Rate effect	1	0.5660e+00	0.1980e+01
	2	0.5000e-01	0.3960e+01
	3	0.1000e-01	
Default gap		0.3180e+01	
Stiffness tol.		0.5000e-01	
Overshoot tol.		0.2000e+00	
Unloading tol.		0.2000e+00	

Hit RETURN for next set

SET NO. 3. 5 segments, 10% increase.

Data Type	Segm No.	Stiffness or Coefficient	Force Limit
Static properties	1	0.7500e+03	0.6050e+01
	2	0.1480e+02	0.9630e+01
	3	0.5500e+01	0.1238e+02
	4	0.2310e+01	0.1562e+02
	5	0.1000e+01	
Default gap		0.3180e+01	
Stiffness tol.		0.5000e-01	
Overshoot tol.		0.2000e+00	
Unloading tol.		0.2000e+00	

Hit RETURN for next set
END OF DATA

New UBAR file created
Comment for file catalog : 3 sets.

End this UBAR session? : y

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : frac

FREC - SPECIFY DYNAMIC FORCE RECORDS

Define units

Length (ft,in,m,mm) : in

Force (k,lb,kgf,kN) : k

Table 2.2.9 (cont'd)

Start new FREC file

Specify a new record ? : y

RECORD NO. 1

Record name (4 characters) : rec1

Description (max. 40 char.) : DECO/Esswein

Enter Time-Force pairs

First pair automatically set to 0,0

Pair no. 2 : .0001 7.2

Pair no. 3 : .00045 7.2

Pair no. 4 : .00046 7.272

Pair no. 5 : .02910 7.272

Pair no. 6 : .02920 7.920

Pair no. 7 : .10000 7.920

Pair no. 8 :

Last pair? : y

Any errors ? :

Specify a new record ? :

Display any records ? :

Write records in session log? :

End this FREC session? : y

New FREC file created

Comment for file catalog : 1 record

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

TABLE 2.2.10 - WIPSLOG LISTING. MODL PHASE.

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : modl

MODL - SPECIFICATION OF ANALYSIS MODEL

Define units

Length (ft,in,m,mm) : in
Force (k,lb,kgf,kN) : k

Sequence no. of COOR file : 1

Available element property sets

Type	No. of Sets
pipe	3
ubar	3

Available substructure property sets
None

DEFINE MODEL IN SEGMENTS

SEGMENT NO. 1

Pipe run no. : 1

First c.p. of segment : 1

Full 3D motion ? :

Displacement plane (xy,yz or zx) : xy

Any substructures in this segment? :

Boundary condition code for first c.p. : 111111

Specify c.p.name + elem type + optional data

1: 8 pipe pr=1 th=no

2: 8 ubar pr=1 dy=1

3: 12 pipe

4: 12,,lumw=.21

5:

End of segment? : y

Display commands for this segment? : y

MODL COMMAND TABLE

SEGMENT NO.	1.	Run No. = 1					
c.p.	eles	optn	data	optn	data	optn	data
1		bcon	111111				
8	pipe	prop	1	ldis	no	this	no
		locl	4				
		wfac	1.0000				
8	ubar	prop	1	this	yes		
		ldis	no				
		dylj	1.0000				
12	pipe	prop	1				

Table 2.2.10 (cont'd)

```

          locl      +      ldis      no      this      yes
          wfac      1.0000
Hit RETURN for more
  12
          tumw      0.2100
Any changes? :

SEGMENT NO.  2

Pipe run no. :
Last segment? : y

Any external substructures? :

Display commands for all segments? :
Write in session log? :

Produce MODL file? : y
Wait while data is processed

Specify initial velocities? :
Comment for file catalog : Case 1. No strain rate.

MODL file saved. File name = MODL0101
End of this MODL session

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : mod1

MODL - SPECIFICATION OF ANALYSIS MODEL

Define units
  Length (ft,in,m,mm) : in
  Force (k,lb,kgf,kN) : k

Sequence no. of COOR file : 1

Available element property sets
  Type      No. of Sets
  pipe      3
  ubar      3
Available substructure property sets
  None

DEFINE MODEL IN SEGMENTS

SEGMENT NO.  1

Pipe run no. : 1
First c.p. of segment : 1
Full 3D motion? :
Displacement plane (xy,yz or zx) : xy
Any substructures in this segment? :
Boundary condition code for first c.p. : 111111

```

Table 2.2.10 (cont'd)

Specify c.p.name + elem type + optional data

- 1: 8 pipe pr=3 th=no
- 2: 8 ubar pr=3
- *** error - direction not defined - use 'jnod' or 'deij'
- 2: 8 ubar pr=3 dy=1
- 3: 12 pipe
- 4: 12, lu=.21
- 5:

End of segment? : y
 Display commands for this segment? : y

MODL COMMAND TABLE

SEGMENT NO.	1.	Run No. = 1					
c.p.	elem	optn	data	optn	data	optn	data
1		bcon	111111				
8	pipe	prop	3				
		locl	+	ldis	no	this	no
		wfac	1.0000				
8	ubar	prop	3				
		ldis	no	this	yes		
		dylj	1.0000				
12	pipe	prop	3				
		locl	+	ldis	no	this	yes
		wfac	1.0000				

Hit RETURN for more
 12
 lumw 0.2100

Any changes? :

SEGMENT NO. 2

Pipe run no. :
 Last segment? : y

Any external substructures? :

Display commands for all segments? :
 Write in session log? :

Produce MODL file? : y
 Wait while data is processed

Specify initial velocities? :
 Comment for file catalog : Case 2. 50%/10% Increases.

MODL file saved. File name = MODL0102
 End of this MODL session

EXEC - WIPS EXECUTIVE

Table 2.2.10 (cont'd)

NEXT WIPS-EXEC COMMAND : wcd1

MODL - SPECIFICATION OF ANALYSIS MODEL

Define units

Length (ft, in, m, mm) : in

Force (k, lb, kgf, kN) : k

Sequence no. of COOR file : 1

Available element property sets

Type No. of Sets

pipe 3

ubar 3

Available substructure property sets

None

DEFINE MODEL IN SEGMENTS

SEGMENT NO. 1

Pipe run no. : 1

First c.p. of segment : 1

Full 3D motion ? :

Displacement plane (xy, yz or zx) : xy

Any substructures in this segment? :

Boundary condition code for first c.p. : 111111

Specify c.p.name + elem type + optional data

1: 8 pipe pr=2 th=no

2: 8 ubar pr=2 dy=1

3: 12 pipe

4: 12, lu=.21

5:

End of segment? : y

Display commands for this segment? : y

MODL COMMAND TABLE

SEGMENT NO.	1.	Run No. = 1						
c.p.	elem	optn	data	optn	data	optn	data	
1		bcon	111111					
8	pipe	prop	2					
		locl	+	ldis	no	this	no	
		wfac	1.0000					
8	ubar	prop	2					
		ldis	no	this	yes			
		dylj	1.0000					
12	pipe	prop	2					
		locl	+	ldis	no	this	yes	
		wfac	1.0000					

Table 2.2.10 (cont'd)

```
Hit RETURN for more
12
          time  0.2100
Any changes? :
SEGMENT NO.  2
Pipe run no. :
Last segment? : y
Any external substructures? :
Display commands for all segments? :
Write in session log? :
Produce MODL file? : y
Wait while data is processed
Specify initial velocities ? :
Comment for file catalog : Case 3. With strain rate.
MODL file saved. File name = MODL0103
End of this MODL session
EXEC = WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : quit
```

TABLE 2.2.11 - WIPSLOG LISTING. DATA PHASE.

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : data

DATA - SET UP WIPS-ANAL INPUT DATA

Sequence no. of MODL file : 1

Problem description (4 lines)

Line 1 : DECO/Esswein Case 1.

GHP 7/82

Line 2 :

Line 3 :

Line 4 :

Set up PAUSE files at end of analysis ? :
Wait while files are processec

Specify data for each loaded point

LOAD NO. 1

Force record name : rec1

Name of loaded c.p. : 12

Force direction (x,y,z or follower) : y

Scale factor (+,- controls direction) : -0.5

Time delay (sec) (dflt=0) :

LOAD NO. 2

Force record name :

Last load? : y

Time steps : initial + max + min : .0002 .004 .00004

Max steps + max total time : 400 .08

Error tolerances : upper + lower : .5 .1

Results output intervals

Max. no. of steps : 1

Max. time (secs.) : 1

Integration scheme (newm or hilb)(dflt=newm) :

Damping factor (dflt=0.1) :

Factor for time step increase (dflt=2.0) :

Factor for time step decrease (dflt=0.5) :

Max. unbal. to reduce time step (dflt=no limit) :

Max. unbal. to stop analysis (dflt=no limit) :

DATA file set complete

Comment for file catalog : Case 1.

WIPS-ANAL DATA FILES SET UP. PARENT FILE NAME = DATA0101

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : data

DATA - SET UP WIPS-ANAL INPUT DATA

Sequence no. of MODL file : 2

Table 2.2.11 (cont'd)

```
Problem description (4 lines)
Line 1 : DECO/Esswein Case 2.
Line 2 :
Line 3 :
Line 4 :
GHP 7/82

Set up PAUSE files at end of analysis ? :
Wait while files are processec

Specify data for each loaded point
LOAD NO. 1
Force record name : rec1
Name of loaded c.p. : 12
Force direction (x,y,z or follower) : y
Scale factor (+,- controls direction) : -.5
Time delay (sec) (dflt=0) :
LOAD NO. 2
Force record name :
Last load? : y

Time steps : initial + max + min : .0002 .004 .00004
Max steps + max total time : 300 .08
Error tolerances : upper + lower : .5 .1

Results output intervals
Max. no. of steps : 1
Max. time (secs.) : 1
Integration scheme (newr or hilb)(dflt=newm) :
Damping factor (dflt=0.1) :
Factor for time step increase (dflt=2.0) :
Factor for time step decrease (dflt=0.5) :
Max. unbal. to reduce time step (dflt=no limit) :
Max. unbal. to stop analysis (dflt=no limit) :

DATA file set complete
Comment for file catalog : Case 2.
WIPS-ANAL DATA FILES SET UP. PARENT FILE NAME = DATA0102

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : data

DATA - SET UP WIPS-ANAL INPUT DATA

Sequence no. of MODL file : 3

Problem description (4 lines)
Line 1 : DECO/Esswein Case 3.
Line 2 :
Line 3 :
Line 4 :
GHP 7/82

Set up PAUSE files at end of analysis ? :
Wait while files are processed
```

Table 2.2.11 (cont'd)

```
Specify data for each loaded point
LOAD NO. 1
  Force record name : rec1
  Name of loaded c.p. : 12
  Force direction (x,y,z or fcllower) : y
  Scale factor (+,- controls direction) : -0.5
  Time delay (sec) (dflt=0) :
LOAD NO. 2
  Force record name :
Last load? : y

Time steps : initial + max + min : .0002 .004 .00004
Max steps + max total time : 300 .08
Error tolerances : upper + lower : .5 .1

Results output intervals
  Max. no. of steps : 1
  Max. time (secs.) : 1
Integration scheme (newm or hilb)(dflt=newm) :
Damping factor (dflt=0.1) :
Factor for time step increase (dflt=2.0) :
Factor for time step decrease (dflt=C.5) :
Max. unbal. to reduce time step (dflt=no limit) :
Max. unbal. to stop analysis (dflt=no limit) :

DATA file set complete
Comment for file catalog : Case 3.
WIPS-ANAL DATA FILES SET UP. PARENT FILE NAME = DATA0103

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

-----
```


TABLE 2.2.12 - LISTING OF DATA FILE FOR CASE 3

```

ECHO103 SLOG103 RSLTC103
star,
gbul
new,main,nonl,cart,0
substructure name = main
refn,13
  1 0.          e+00  0.          e+00  0.          e+00
  2 0.1500000e+02  0.          e+00  0.          e+00
  3 0.3000000e+02  0.          e+00  0.          e+00
  4 0.4200000e+02  0.          e+00  0.          e+00
  5 0.5400000e+02  0.          e+00  0.          e+00
  6 0.6600000e+02  0.          e+00  0.          e+00
  7 0.7800000e+02  0.          e+00  0.          e+00
  8 0.9000000e+02  0.          e+00  0.          e+00
  9 0.9700000e+02  0.          e+00  0.          e+00
 10 0.9700000e+02  0.3750000e+01  0.          e+00
 11 0.9700000e+02  0.9750000e+01  0.          e+00
 12 0.9700000e+02  0.1875000e+02  0.          e+00
9999
boun,13
  1 111111
  2 1110
  3 1110
  4 1110
  5 1110
  6 1110
  7 1110
  8 1110
  9 1110
 10 1110
 11 1110
 12 1110
9999 111111
enod,0
matl,6,64
0.200000000e+010.299999982e+000.300000000e+050.240600000e+040.421000000e+03
0.190000000e+020.280000000e+020.999999932e+200.199999996e-010.499999970e-01
0.120000000e+020.200000000e+010.          e+000.200000000e+010.100000000e+01
0.100000000e+010.450000000e+010.337000012e+000.125171524e-020.          e+00
0.399999976e+000.499999970e-010.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.499999970e-01
0.199999988e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.200000000e+010.299999982e+000.300000000e+050.240600000e+040.421000000e+03
0.190000000e+020.280000000e+020.999999932e+200.199999996e-010.499999970e-01
0.120000000e+020.200000000e+010.          e+000.200000000e+010.100000000e+01
0.100000000e+010.450000000e+010.337000012e+000.125171524e-020.          e+00
0.399999976e+000.499999970e-010.300000000e+010.250000000e+020.220000005e+01
0.439999998e+000.360000014e+000.444000006e+010.999999932e+200.499999970e-01
0.199999988e+000.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+000.          e+00

```


Table 2.2.12 (cont'd)

```

0.          e+000.          e+000.          e+000.          e+00
elen,2
  2  1  1
  1  0  0  0  8  5  0  1  0  1
0.90000000e+020.100000000e+010.          e+000.          e+00
0.          e+000.          e+00
  3  11  1
  1  0  0  0  1  2  2  0  0  1  0  1
0.          e+000.100000000e+010.          e+000.          e+00
  2  0  0  0  2  3  2  0  0  1  0  1
0.150000000e+020.100000000e+010.          e+000.          e+00
  3  0  0  0  3  4  2  0  0  1  0  1
0.300000000e+020.100000000e+010.          e+000.          e+00
  4  0  0  0  4  5  2  0  0  1  0  1
0.420000000e+020.100000000e+010.          e+000.          e+00
  5  0  0  0  5  6  2  0  0  1  0  1
0.540000000e+020.100000000e+010.          e+000.          e+00
  6  0  0  0  6  7  2  0  0  1  0  1
0.660000000e+020.100000000e+010.          e+000.          e+00
  7  0  0  0  7  8  2  0  0  1  0  1
0.780000000e+020.100000000e+010.          e+000.          e+00
  8  0  0  0  8  9  2  0  1  1  0  1
0.900000000e+020.100000000e+010.          e+000.          e+00
  9  0  0  0  9  10  2  0  1  1  0  1
0.960000000e+020.          e+000.          e+00
  10  0  0  0  10  11  2  0  1  1  0  1
0.960000000e+020.375000000e+010.          e+000.          e+00
  11  0  0  0  11  12  2  0  1  1  0  1
0.960000000e+020.975000000e+010.          e+000.          e+00

nord,opto
prof
end
fini
mode
trec,main
fini
mbul
new,main
pmas,14
  10 0.12224e-04 0.12224e-04 0.12224e-04 0.          e+00 0.          e+00 0.          e+0000
  20 0.24448e-04 0.24448e-04 0.24448e-04 0.          e+00 0.          e+00 0.          e+0000
  30 0.22003e-04 0.22003e-04 0.22003e-04 0.          e+00 0.          e+00 0.          e+0000
  40 0.19558e-04 0.19558e-04 0.19558e-04 0.          e+00 0.          e+00 0.          e+0000
  50 0.19559e-04 0.19558e-04 0.19558e-04 0.          e+00 0.          e+00 0.          e+0000
  60 0.19558e-04 0.19558e-04 0.19558e-04 0.          e+00 0.          e+00 0.          e+0000
  70 0.19558e-04 0.19558e-04 0.19558e-04 0.          e+00 0.          e+00 0.          e+0000
  80 0.97790e-05 0.97790e-05 0.97790e-05 0.          e+00 0.          e+00 0.          e+0000
  80 0.57044e-05 0.57044e-05 0.57044e-05 0.          e+00 0.          e+00 0.          e+0000
  90 0.87604e-05 0.87604e-05 0.87604e-05 0.          e+00 0.          e+00 0.          e+0000
  100 0.79455e-05 0.79455e-05 0.79455e-05 0.          e+00 0.          e+00 0.          e+0000
  110 0.12224e-04 0.12224e-04 0.12224e-04 0.          e+00 0.          e+00 0.          e+0000
  120 0.73343e-05 0.73343e-05 0.73343e-05 0.          e+00 0.          e+00 0.          e+0000
  120 0.27344e-03 0.27344e-03 0.27344e-03 0.          e+00 0.          e+00 0.          e+0000
end

```

Table 2.2.12 (cont'd)

```

fini
ptre
newr, recl, pair, 7, 100
(2e15.7)
  0.          e+00  0.          e+00
  0.7200000e+01  0.1000000e-04
  0.7200000e+01  0.4500000e-03
  0.7272000e+01  0.4600000e-03
  0.7272000e+01  0.2910000e-01
  0.7920000e+01  0.2920000e-01
  0.7920000e+01  0.1000000e+00
fini
thou, 241
      2      119      3      1      0      0
ndyn
mass
dylc, 1, 1
recl      2      0.      -0.500      1
      12
time, rsit, 1, 0.1000e+01
auto, defl
inte, newm, 0.2000e-03, 0.e+00, 0.e+00, 0.1000e+00
stif
stif, upda
klnr, 12
elmr, 1, 2, 6, 3
klnr, 5
loop, 300
zero, ltwe
step
unba
auto, init
loop, 20
stif
auto, load
load
disp
klnr, 10
elmr, 9, 10
auto, werr, 0.1000e+00, 0.5000e+00
if, 3, 3, 1, 1
entr, 1
auto, fact
klnr, 1
if, 3, 2, 2, 3
entr, 2
elmr, 1
cont
goto, 0
entr, 3
auto, step, 0.4000e-04, 0.4000e-02, 0.5000e+00, 0.2000e+01
if, 4, 5, 5, 4
entr, 4
inte, newm, , auto, 0.e+00, 0.e+00, 0.e+00, 0.1000e+00
entr, 5
if, 3, 6, 6, 7

```

Table 2.2.12 (cont'd)

```
entr,6  
klnr,12  
elwr,5,2,6  
klnr,5  
stif,init  
goto,8  
entr,7  
chou  
elwr,1,2,4,6,11  
klnr,4,9,11  
wrou  
zero,1rab  
unba  
sume  
elwr,3  
klnr,3  
stif,upda  
auto,exit,0.8000e-01  
lf,5,8,8,0  
entr,8  
cont  
fini  
stop
```

TABLE 2.2.13 - SUMMARY OF RESULTS						
	Expt. [2.2.1]	Case 1	Case 2 (Newmark)	Case 2 (HHT)	Case 2 [2.2.2]	Case 3
(1) Time to Gap Closure (msec)	27	27.7	27.8	27.9	28	27.7
(2) Max. Restraint Extension (in)	2.94	3.34	2.69	2.69	2.7	2.08
(3) Max. Restraint Force (k)	16.3	15.3	16.2	16.2	16.4	17.0
(4) Number of time steps (to 0.08 secs)		126	124	166		111

D2.3 PIPE WHIP ANALYSIS WITH LARGE DISPLACEMENT

D2.3.1 PURPOSE

This example tests the PIPE and GAPF elements, in part by comparison with previously reported analysis results. No test results are available. Large displacements and strain rate effects are considered for the PIPE elements, and the follower force option is exercised. The GAPF element is tested with and without friction. The analysis is only two-dimensional, so that full three-dimensional behavior is not checked.

D2.3.2 DESCRIPTION

Analyses of a cantilevered pipe with large displacements and impact have been reported by Hibbitt and Karlsson [2.3.1]. The dimensions of the pipe are shown in Fig. 2.3.1. The tri-linear stress-strain relationship used for the pipe steel is shown in Table 2.3.1 and the blow-down force record in Table 2.3.2.

Gap-friction (GAPF) elements are located at nodes 16 through 19, with initial gaps specified to represent a flat surface. Each GAPF element is arbitrarily assigned a stiffness of 10^4 k/in, which allows a small amount of flexibility after gap closure. In the analysis reported in [2.3.1], the flat surface was assigned a very large mass, rather than an elastic stiffness. Because impact of an actual pipe would involve substantial local deformation of the pipe, and probably significant deformation of the impacted wall, the assumption of an essentially rigid surface is not realistic, and the computed impact forces are likely to be much larger than those which would occur in actual practice.

The analysis reported in [2.3.1] did not consider strain rate effects. Strain rate effects for the WIPS analysis were assumed to be shown in Table 2.3.3, based on data for low carbon steel reported by Manjoine [2.3.2].

The following WIPS analyses were performed:

- (1) No strain rate effect, zero friction.
- (2) With strain rate effect, friction coefficient = 0.4.

D2.3.3 WIPS ANALYSIS MODEL

D2.3.3.1 Geometry, Loading, and Pipe Properties

The PIPE element subdivision is shown in Fig. 2.3.1. This is similar to the subdivision used in [2.3.1]. It may be noted that only a single element is used in the vertical leg between nodes 19 and 20. This introduces a significant error in the rotational inertia of this leg, and for practical analysis a larger number of nodes is probably desirable. It should also be noted that the initial gap clearance used in the analysis is different from that shown in Fig. 4-12 of Reference 2.3.1. The value used for the current analysis is consistent with that reported in [2.3.3] and is believed to be correct. Motion was permitted in the XY plane only. The default ovaling strengths and stiffnesses were assumed for the curved PIPE elements, with small ovaling assumed. Twelve subelements (the default value) were used in each PIPE element cross section.

The jet force was applied at node 20, directed towards node 19 (i.e. the follower option). To allow for the symmetry, the jet forces shown in Table 2.3.2 were multiplied by 0.5 (because only half of the element strengths and stiffnesses are used in symmetrical segments of the analysis model).

D2.3.3.2 Analysis Control Parameters

The Newmark step-by-step option was used, with the following parameters.

Initial time step = 5×10^{-4} sec.

Minimum time step = 10^{-5} sec.

Maximum time step = 10^{-3} sec.

Initial $\beta/\Delta t$ = 0.1

Lower midstep tolerance = 50 k

Upper midstep tolerance = 250 k

D2.3.3.3 WIPS Input

Tables 2.3.4 through 2.3.8 contain the WIPSLOG listings for the GEOM, MATL, PIPE, GAPF, and FREC phases. Tables 2.3.9 and 2.3.10 contain the WIPSLOG listings for the MODL and DATA phases for Case 1 (no strain rate effect, negligible friction). Table 2.3.11 is a listing of the DATA file for Case 1. The MODL and DATA phases for Case 2 were similar.

D2.3.4 RESULTS

D2.3.4.1 Pipe Motion

The computed pipe locations at four different times are shown in Fig. 2.3.2 for the no-friction case and in Fig. 2.3.3 for the case with friction.

For the no-friction case, the time to initial contact (0.107 sec.) is very close to that reported in [2.3.1], and the deformed shapes are also very similar. For the case with friction, the computed pipe motion after impact is much different, with only a small amount of slip taking place.

The case with friction also included strain rate effects in the PIPE elements. The computed time to impact and the deformed shape at impact were essentially identical to those for the case without strain rate effects. This indicates that the pipe motion up to gap closure is governed mainly by the inertia of the pipe, and (in this example) does not depend greatly on the pipe strength.

D2.3.4.2 Impact Force

For the case with friction, the computed impact force (sum of all gap-friction elements) varied as shown in Fig. 2.3.4. The peak value is 17300 k, reached shortly after initial impact. The analysis then indicated several cycles of separation and new contact, with much lower impact forces. For this analysis, results output was requested every time step, and hence the detailed results shown in Fig. 2.3.4 could be plotted. For the case with no friction, results output was requested only every 20 steps. As a result, no detailed response could be plotted, and the peak impact force was not recorded.

It is important to note that the computed impact forces are strongly dependent on the assumed gap stiffnesses and are not realistic values. In this example each gap element was assumed to have a stiffness of 10^4 k/in., which is much larger than the crush stiffness of an actual elbow. As a result, the computed peak impact force is probably a gross overestimate.

The computed impact force in an analysis of this type may also depend on the method of analysis. In the analysis of [2.3.1], the impacted surface was modelled as a rigid body with very large mass, and a peak impact force of approximately 8500 k was reported.

D2.3.5 CONCLUSION

For the case with no friction, the computed motion of the pipe was very similar to that previously reported in [2.3.1]. This indicates that large displacements behavior of the PIPE elements is computed correctly in two dimensions and that the impacted surface was adequately

represented by stiff GAPF elements.

For the case with friction, the WIPS analysis predicted only a small amount of slip on the impacted surface. No previously reported analysis is available for comparison.

The computed impact force depends on the modelling assumptions and is unlikely to be close to the true impact force. Because the friction force developed in GAPF elements depends on the normal (impact) force, it follows that the computed pipe motion after impact may not be the same as that which would be observed in an actual test.

It can be concluded that the PIPE element can be used to compute the motions of unrestrained pipes up to impact. However, the problem of post-impact behavior is complex, and further study is needed to determine whether impact forces and post-impact motions can be determined with simple models of the type used in this example.

D2.3.6 REFERENCES

- 2.3.1 Hibbitt and Karlsson, "Analysis of Pipe Whip," Report No. EPRI NP-1208, Electric Power Research Institute, 1979.
- 2.3.2 Manjoine, M. J., "Influence of Strain Rate and Temperature on Yield Stresses of Mild Steel," J. Appl. Mech., Vol. II, A-211, 1944.
- 2.3.3 Vijay, D. K. and Kozluk, M. J., "Pipe Whip Analysis of Unrestrained Piping Systems," ASME Paper 80-C27-PVP-149, 1980.

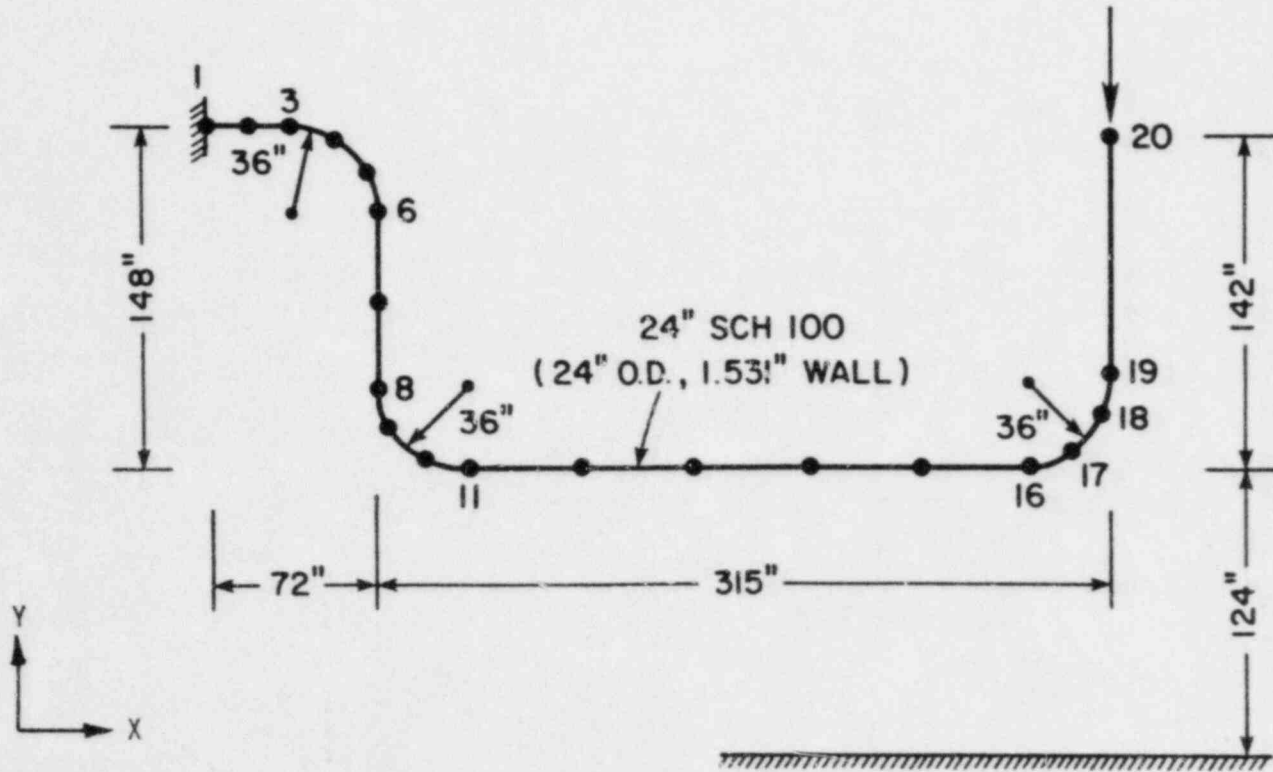


FIG. 2.3.1 PIPE WHIP WITH LARGE DISPLACEMENTS

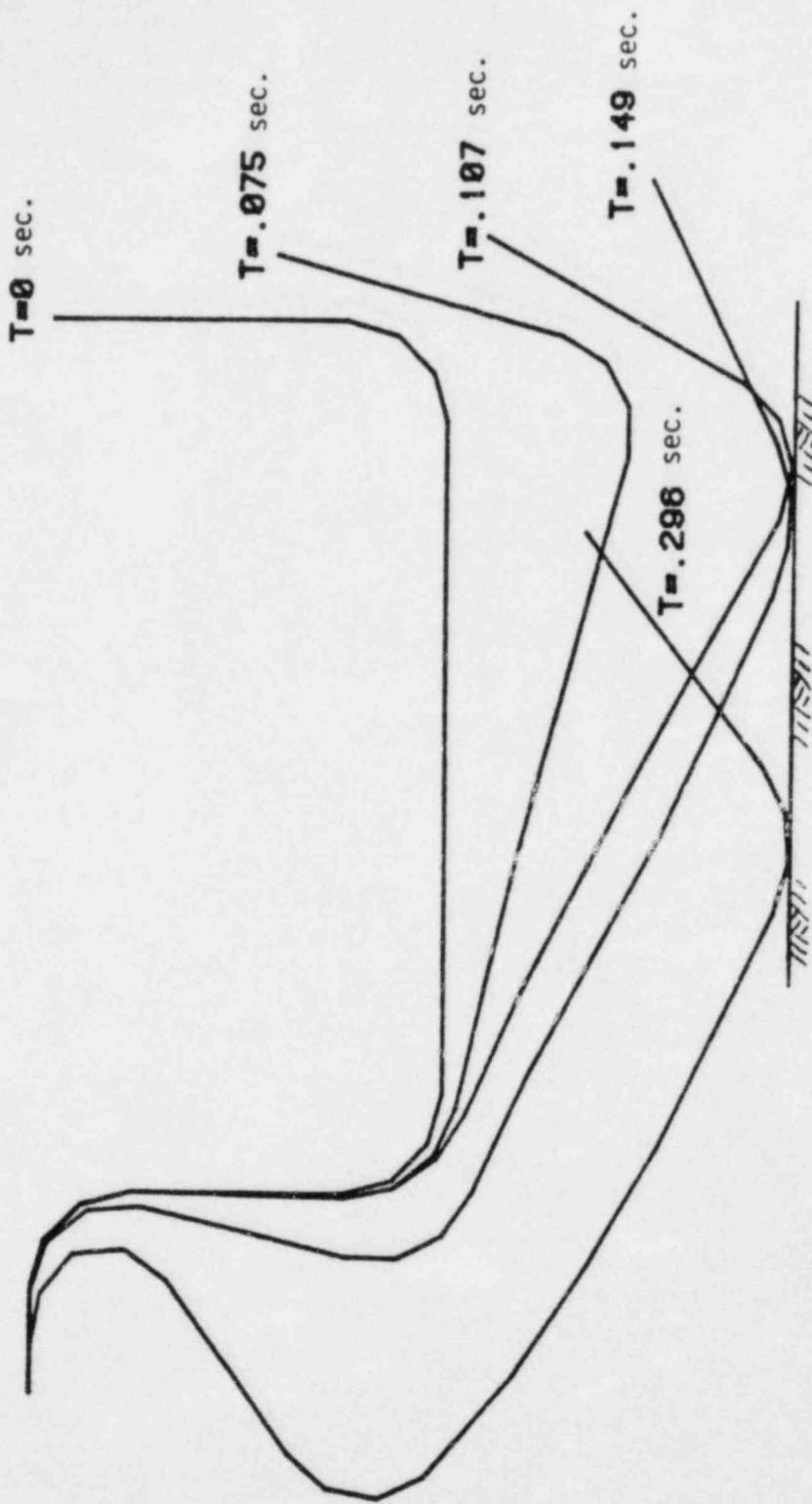


FIG. 2.3.2 DEFORMED SHAPES. CASE WITH NO FRICTION.

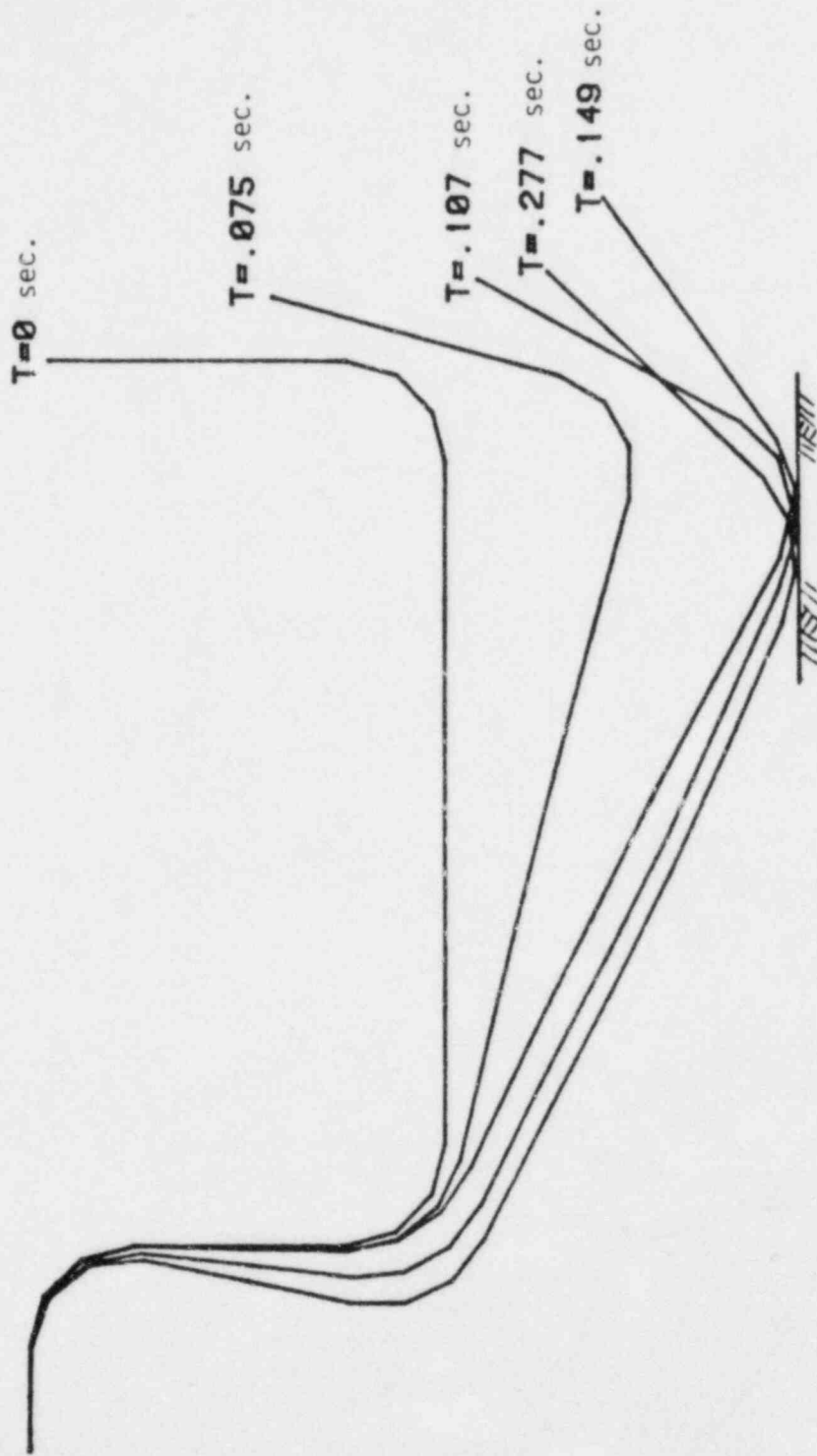


FIG. 2.3.3 DEFORMED SHAPES. CASE WITH FRICTION.

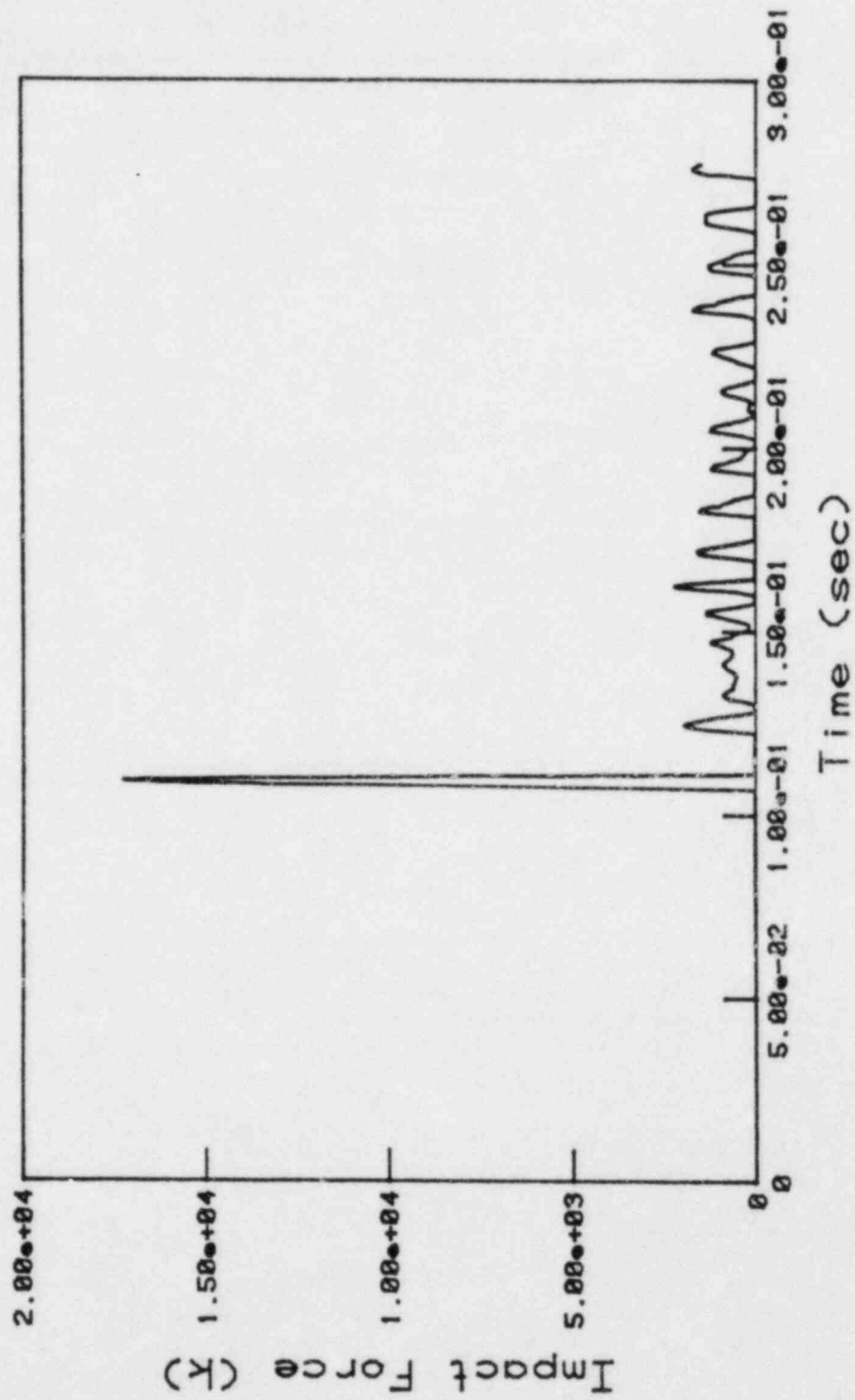


FIG. 2.3.4 COMPUTED IMPACT FORCE. CASE WITH FRICTION.

TABLE 2.3.1 - STATIC STRESS-STRAIN RELATIONSHIP FOR PIPE STEEL		
Stress (ksi)	Strain	Modulus (ksi)
0	0	26700
26.7	0.001	219
44.0	0.080	2

TABLE 2.3.2 - BLOWDOWN FORCE RECORD	
Time (sec)	Force (k)
0	0
0.0001	650
0.0010	880
0.0020	1000
0.0030	880
0.0050	780
0.0200	430
10.0	430

TABLE 2.3.3 - ASSUMED STRAIN RATE EFFECT		
Stress Increase (ksi)	Strain Rate (sec ⁻¹)	Dashpot Stiffness (ksec/in ²)
0	0	25.00
9	0.36	2.20
18	4.44	0.44

TABLE 2.3.4 - WIPSLOG LISTING FOR GEOM PHASE.

```
EXEC - WIPS EXECUTIVE
Creating problem no. 1
Problem description: Hibbitt Fig.4.12 with gapf

NEXT WIPS-EXEC COMMAND : geom

GEOM - SPECIFICATION OF SYSTEM GEOMETRY

Define units
  Length (ft,in,m,mm) : in
  Force (k,lb,kgf,kN) : k

Specify new GEOM data

START RUN NO. 1
Enter c.p. data in sequence along run

  c.p. name and type : 1
  coord option : d!
  x,y,z :
  Any changes? :

  c.p. name and type : 3 tn
  no. of extra nodes : 1
  coord option :
  tn generated automatically
  Any changes? :

  c.p. name and type : t11 t1
  bend radius : 36
  coord option :
  c.p. : dx,dy,dz : 1 72
  Any changes? :

  c.p. name and type : 6 tn
  no. of extra nodes : 2
  coord option :
  tn generated automatically
  Any changes? :

  c.p. name and type : 8 tn
  no. of extra nodes : 1
  coord option :
  tn generated automatically
  Any changes? :

  c.p. name and type : t12 t1
  bend radius : 36
  coord option :
  c.p. : dx,dy,dz : t11 0 -148
  Any changes? :

  c.p. name and type : 11 tn
  no. of extra nodes : 2
  coord option :
  tn generated automatically
```

Table 2.3.4 (cont'd)

Any changes? :

c.p. name and type : 16 tn
 no. of extra nodes : 4
 coord option :
 tn generated automatically
 Any changes? :

c.p. name and type : ti3 ti
 bend radius : 36
 coord option :
 c.p., dx,dy,dz : ti2 315
 Any changes? :

c.p. name and type : 19 tn
 no. of extra nodes : 2
 coord option :
 tn generated automatically
 Any changes? :

c.p. name and type : 20
 no. of extra nodes :
 coord option :
 c.p., dx,dy,dz : ti3 0 142
 Any changes? :

c.p. name and type :
 Last c.p. in this run? : y
 Display GEOM data for this run? : y

GEOM DATA FOR RUN

run no.	c.p. name	c.p. type	bend radius	xtra nodes	coord opt	c.p. I	c.p. J ?	coordinate data x,dx,p	y,dy	z,dz
1				0	di			0.	0.	0.
3	tn			1	tn			0.	0.	0.
ti1	ti		36.000	0	of	1		72.000	0.	0.
6	tn			2	tn			0.	0.	0.
8	tn			1	tn			0.	0.	0.
ti2	ti		36.000	0	of	ti1		0.	-148.000	0.
11	tn			2	tn			0.	0.	0.
16	tn			4	tn			0.	0.	0.
ti3	ti		36.000	0	of	ti2		315.000	0.	0.
19	tn			2	tn			0.	0.	0.
Hit RETURN for more										
20				0	of	ti3		0.	142.000	0.

END OF DATA

START RUN NO. 2
 Enter c.p. data in sequence along run

c.p. name and type :
 Last run? : y

Table 2.3.4 (cont'd)

Display new GEOM data? :
 Write in session log? :
 Modify GEOM data? :
 Save current GEOM data? : y
 Comment for file catalog :
 GEOM DATA SAVED. FILE NAME = GEUM0101
 Produce COOR data? : y
 Display COOR data? : y

COORD DATA

run no.	c.p. name	c.p. type	bend radius	node no.	x coord	y ? coord?	x coord
1				1	0.	0.	0.
				2	18.000	0.	0.
	3	tn		3	36.000	0.	0.
	ti1	ti	36.000 center		72.000	0.	0.
					36.000	-36.000	0.
				4	54.000	-4.823	0.
				5	67.177	-18.000	0.
	6	tn		6	72.000	-36.000	0.
				7	72.000	-72.000	0.
	8	tn		8	72.000	-112.000	0.
	Hit RETURN for more						
	ti2	ti	36.000 center		72.000	-148.000	0.
					108.000	-112.000	0.
				9	76.823	-130.000	0.
				10	90.000	-143.177	0.
	11	tn		11	108.000	-148.000	0.
				12	156.600	-148.000	0.
				13	205.200	-148.000	0.
				14	253.800	-148.000	0.
				15	302.400	-148.000	0.
	16	tn		16	351.000	-148.000	0.
	Hit RETURN for more						
	ti3	ti	36.000 center		387.000	-148.000	0.
					351.000	-112.000	0.
				17	369.000	-143.177	0.
				18	382.177	-130.000	0.
	19	tn		19	387.000	-112.000	0.
	20			20	387.000	-6.000	0.
	END OF DATA						

Plot geometry? :
 Modify GEOM data? :
 DATA COMPLETE FOR THIS SESSION
 Save final GEOM data? : y

Table 2.3.4 (cont'd)

Comment for file catalog : Hibbitt Fig.4.12 Example
GEOM DATA SAVED. FILE NAME = GEOM0101
Save COOR data? : y
Comment for file catalog : Hibbitt Fig.4.12. From GEOM0101
COOR DATA SAVED. FILE NAME = COOR0101

End of this GEOM session

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : geom

GEOM - SPECIFICATION OF SYSTEM GEOMETRY

Define units
Length (ft,in,m,mm) : in
Force (k,lb,kgf,kN) : k

Modify existing GEOM file? : y
Sequence no. : 1

Display existing GEOM data? :
Write in session log? :

Modify GEOM data? : y
Specify modifications
Change data for a c.p.? : y
c.p. name : 19
enter revised data
c.p. type : tn
no. of extra nodes :
coord option :
tn generated automatically
Any changes? :

More changes? : y
Change data for a c.p.? :
Insert new c.p.'s? : y
name of preceding c.p. : 16
enter data for new c.p.'s

c.p. name and type : 17
no. of extra nodes :
coord option : cu
c.p.i, c.p.j, proportion : 16 19 .33333
Any changes? :

c.p. name and type : 18
no. of extra nodes :
coord option : cu

Table 2.3.4 (cont'd)

c.p.i, c.p.j, proportion : 16 19 .6667
 Any changes? :

c.p. name and type :

More changes? :

Display modified GEOM data? :

Write in session log? : y

MODIFIED GEOM DATA

run no.	c.p. name	c.p. type	bend radius	xtra nods	coord opt	c.p. i	c.p. j ?	coordinate data		
								x,dx,p	y,dy	z,dz
1										
	1			0	dl			0.	0.	0.
	3	tn		1	tn			0.	0.	0.
	t11	tl	36.000	0	of	1		72.000	0.	0.
	6	tn		2	tn			0.	0.	0.
	8	tn		1	tn			0.	0.	0.
	t12	tl	36.000	0	of	t11		0.	-148.000	0.
	11	tn		2	tn			0.	0.	0.
	16	tn		4	tn			0.	0.	0.
	17			0	cu	16	19	0.333	0.	0.
	18			0	cu	16	19	0.667	0.	0.
	t13	tl	36.000	0	of	t12		315.000	0.	0.
	19	tn		0	tn			0.	0.	0.
	20			0	of	t13		0.	142.000	0.

Save current GEOM data? : y

Comment for file catalog :

GEOM DATA SAVED. FILE NAME = GEOM0102

Produce COOR data? : y

Display COOR data? : y

COOR DATA

run no.	c.p. name	c.p. type	bend radius	node no.	x coord	y ? coord?	z coord
1							
	1			1	0.	0.	0.
	3	tn		2	18.000	0.	0.
	t11	tl	36.000	3	36.000	0.	0.
			center		72.000	0.	0.
				4	36.000	-36.000	0.
				5	54.000	-4.823	0.
				6	67.177	-18.000	0.
	6	tn		7	72.000	-36.000	0.
				8	72.000	-74.000	0.
	8	tn		8	72.000	-112.000	0.

HIT RETURN for more

Table 2.3.4 (cont'd)

c12	tl	36.000		72.000	-148.000	0.
		center		108.000	-112.000	0.
			9	76.823	-130.000	0.
			10	90.000	-143.177	0.
11	tn		11	108.000	-148.000	0.
			12	156.600	-148.000	0.
			13	205.200	-148.000	0.
			14	253.800	-148.000	0.
			15	302.400	-148.000	0.
			16	351.000	-148.000	0.
16	tn					
Hit RETURN for more						
17			17	369.000	-143.177	0.
18			18	382.177	-130.000	0.
t13	tl	36.000		387.000	-148.000	0.
		center		351.000	-112.000	0.
19	tn		19	387.000	-112.000	0.
20			20	387.000	-6.000	0.

END OF DATA

Plot geometry? :

Modify GEOM data? :

DATA COMPLETE FOR THIS SESSION

Save final GEOM data? : y

Comment for file catalog : Hibbitt Fig.4.12, 17,18 added.

GEOM DATA SAVED. FILE NAME = GEOM0102

Save COOR data? : y

Comment for file catalog : Hibbitt Fig.4.12, 17,18 added.

COOR DATA SAVED. FILE NAME = COOR0102

End of this GEOM session

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

TABLE 2.3.5 - WIPSLOG LISTING FOR MATL PHASE.

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : mat1

MATL - SPECIFICATION OF MATERIAL PROPERTIES

Define units

Length (ft,in,m,mm) : in

Force (k,lb,kgf,kN) : k

Start new MATL file

Specify a new property set? : y

SET NO. = 1

Property set description : Hibbitt material, no strain rate.

Static moduli (min=2,max=5)

: 26700 219 2

Yield strengths (no. of moduli minus 1)

: 26.7 44

Strain rate stiffnesses (min=0,max=3)

:

No strain rate effect

Use default tolerances? : y

Poisson ratio (dfit = .3) :

Weight density (dfit=steel) :

Any errors? :

This set added to MATL file

Specify a new property set? : y

SET NO. = 2

Property set description : Hibbitt material, with strain rate.

Static moduli (min=2,max=5)

: 26700 219 2

Yield strengths (no. of moduli minus 1)

: 26.7 44

Strain rate stiffnesses (min=0,max=3)

: 25 2.2 .44

Strain rate limits (no. of stiffnesses minus 1)

: .36 4.44

Use default tolerances? : y

Poisson ratio (dfit = .3) :

Weight density (dfit=steel) :

Any errors? :

This set added to MATL file

Specify a new property set? :

No. of property sets in MATL file = 2

Table 2.3.5 (cont'd)

Display property set descriptions? : y

MATL PROPERTY DESCRIPTIONS

Set No. Type Description
 1 mroz Hibbitt material, no strain rate.
 2 mroz Hibbitt material, with strain rate.

Display new property set data? : y

MATL PROPERTY DATA

SET NO. 1. Hibbitt material, no strain rate.

Matl Type	Data Type	Segm No.	Modulus or Coefficient	Stress/Strain Limit
mroz	static	1	0.2670e+05	0.2670e+02
		2	0.2190e+03	0.4400e+02
		3	0.2000e+01	
		yld.tol.		0.2000e-01
		stif tol		0.5000e-01
		rate tol		0.5000e-01
		poisson		0.3000e+00
		density		0.2840e-03

Hit RETURN for next set

SET NO. 2. Hibbitt material, with strain rate.

Matl Type	Data Type	Segm No.	Modulus or Coefficient	Stress/Strain Limit	
mroz	static	1	0.2670e+05	0.2670e+02	
		2	0.2190e+03	0.4400e+02	
		3	0.2000e+01		
		str.rate	1	0.2500e+02	0.3600e+00
			2	0.2200e+01	0.4440e+01
			3	0.4400e+00	
		yld.tol.		0.2000e-01	
		stif tol		0.5000e-01	
		rate tol		0.5000e-01	
		poisson		0.3000e+00	
	density		0.2840e-03		

Hit RETURN for next set

END OF DATA

Display all property set data? :
 Write in session log? :

New MATL file created
 Comment for file catalog :

End this MATL session? : y

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

TABLE 2.3.6 - WIPSLOG LISTING FOR PIPE PHASE.

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : pipe

PIPE - SPECIFICATION OF PIPE PROPERTIES

Define units

Length (ft,in,m,mm) : in

Force (k,lb,kgf,kN) : k

No. of MATL property sets available = 2

Display material descriptions? :

Write in session log? :

Start new PIPE file

Specify a new property set? : y

SET NO. = 1

Property set description : 24sch100, no strain rate, small oval.

Outside diameter : 24

Wall thickness : 1.531

Weight/unit length (dflt=pipe weight) :

No. of X-section elements (dflt=12) :

Material number : 1

Large ovaling (yes or no)? (dflt=no) :

Use default ovaling properties? : y

Any errors? :

This set added to PIPE file

Specify a new property set? : y

SET NO. = 2

Property set description : 24sch100, with strain rate, small oval.

Outside diameter : 24

Wall thickness : 1.531

Weight/unit length (dflt=pipe weight) :

No. of X-section elements (dflt=12) :

Material number : 2

Large ovaling (yes or no)? (dflt=no) :

Use default ovaling properties? : y

Any errors? :

This set added to PIPE file

Specify a new property set? :

No. of property sets in PIPE file = 2

Display property set descriptions? : y

PIPE PROPERTY DESCRIPTIONS

Table 2.3.6 (cont'd)

```
Set No.  Description
  1      24sch100, no strain rate, small oval.
  2      24sch100, with strain rate, small oval.
```

Display new property set data? : y

PIPE PROPERTY DATA

SET NO. 1. 24sch100, no strain rate, small oval.

Data Type	Segm No.	Modulus or Data Value	Stress/Strain Limit
Outside diameter		0.2400e+02	
Wall thickness		0.1531e+01	
Unit weight		0.3069e-01	
No. of elements		12	
No. of slices		2	
Stress v strain	1	0.2670e+05	0.2670e+02
	2	0.2190e+03	0.4400e+02
	3	0.2000e+01	
Poisson ratio		0.3000e+00	
Large ovaling		no	
Ovaling ratios	1	0.3500e+00	
	2	0.8000e-01	

Hit RETURN for next set

SET NO. 2. 24sch100, with strain rate, small oval.

Data Type	Segm No.	Modulus or Data Value	Stress/Strain Limit
Outside diameter		0.2400e+02	
Wall thickness		0.1531e+01	
Unit weight		0.3069e-01	
No. of elements		12	
No. of slices		2	
Stress v strain	1	0.2670e+05	0.2670e+02
	2	0.2190e+03	0.4400e+02
	3	0.2000e+01	
Stress v strain rate	1	0.7500e+02	0.2000e+00
	2	0.5250e+01	0.1353e+02
	2	0.5250e+01	
Poisson ratio		0.3000e+00	
Large ovaling		no	
Ovaling ratios	1	0.3500e+00	
	2	0.8000e-01	

Hit RETURN for next set

END OF DATA

Display all property set data? :
Write in session log? :

New PIPE file created
Comment for file catalog :

End this PIPE session? : y

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

TABLE 2.3.7 - WIPSLOG LISTING FOR GAPF PHASE.

```

EXEC - WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : gapf
GAPF - SPECIFICATION OF GAP FRICTION PROPERTIES

Define units
  Length (ft;in;mm) : in
  Force (k,lb,kgf,kN) : k

Start new GAPF file

Specify a new property set? : y

SET NO. 1
Property set description : 10000k/in, fric. coeff.=1.e-6
Normal stiffness : 10000
Tangent stiffness : 10000
Friction coefficient : 1e-6
Use default tolerances?
Stiffness tolerance (dflt=.05) :
Overshoot tolerance (dflt=200lb) :
Any errors? :

This set added to GAPF file

Specify a new property set? : y

SET NO. 2
Property set description : 10000k/in, fric. coeff.=0.4
Normal stiffness : 10000
Tangent stiffness : 10000
Friction coefficient : .4
Use default tolerances? y
Any errors? :

This set added to GAPF file

Specify a new property set? :

No. of property sets in GAPF file = 2

Display property set descriptions? : y

GAPF PROPERTY DESCRIPTIONS
  Set No.  Description
    1      10000k/in, fric. coeff.=1.e-6
    2      10000k/in, fric. coeff.=0.4

Display new property set data? : y

GAPF PROPERTY DATA

Set No.  Data Type          Data Value
  1

```

Table 2.3.7 (cont'd)

Normal stiffness	0.1000e+05
Tangent stiffness	0.1000e+05
Friction coefficient	0.1000e-05
Stiffness tolerance	0.5000e-01
Overshoot tolerance	0.2000e+00

HIT RETURN for next set

2

Normal stiffness	0.1000e+05
Tangent stiffness	0.1000e+05
Friction coefficient	0.4000e+00
Stiffness tolerance	0.5000e-01
Overshoot tolerance	0.2000e+00

HIT RETURN for next set
END OF DATA

Display all property set data? :
Write in session log? :

New GAPF file created
Comment for file catalog :

End this GAPF session? : y

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

TABLE 2.3.8 - WIPSLOG LISTING FOR FREC PHASE.

```
EXEC - WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : frec
FREC - SPECIFY DYNAMIC FORCE RECORDS

Define units
  Length (ft,in,m,mm) : in
  Force (k,lb,kgf,kN) : k

Start new FREC file

Specify a new record ? : y

RECORD NO. 1

Record name (4 characters) : rec1
Description (max. 40 char.) : Hibbitt record, max. 1000k.

Enter Time-Force pairs
First pair automatically set to 0,0
  Pair no. 2 : .0001 650
  Pair no. 3 : .001 880
  Pair no. 4 : .002 1000
  Pair no. 5 : .003 880
  Pair no. 6 : .005 780
  Pair no. 7 : .02 430
  Pair no. 8 : 10 430
  Pair no. 9 :
Last pair? : y
Any errors ? :

Specify a new record ? :

Display any records ? : y
Record number (dflt=all) :

RECORD NO. 1. Name = rec1
      Time      Force
      0.         0.         e+00
      0.00010    0.6500e+03
      0.00100    0.8800e+03
      0.00200    0.1000e+04
      0.00300    0.8800e+03
      0.00500    0.7800e+03
      0.02000    0.4300e+03
      10.00000   0.4300e+03
END OF RECORD

Write records in session log? :

End this FREC session? : y
New FREC file created
Comment for file catalog :

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit
```

TABLE 2.3.9 - WIPSLOG LISTING FOR MODL PHASE, CASE 1.

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : mod1

MODL - SPECIFICATION OF ANALYSIS MODEL

Define units

Length (ft,in,m,mm) : in

Force (k,lb,kgf,kN) : k

Sequence no. of COOR file : 2

Available element property sets

Type No. of Sets

pipe 2

gapf 2

Available substructure property sets

None

DEFINE MODEL IN SEGMENTS

SEGMENT NO. 1

Pipe run no. : 1

First c.p. of segment : 1

Full 3D motion? :

Displacement plane (xy-yz or zx) : xy

Any substructures in this segment? :

Boundary condition code for first c.p. : 111111

Specify c.p.name + elem type + optional data

1: 16 pipe pr=1 ldy

2: 16 gapf pr=1 dy=-1 gap=124

3: 17 pipe

4: 17 gapf gap=128.82

5: 18 pipe

6: 18 gapf gap=142

7: 19 pipe

8: 19 gapf gap=160

9: 20 pipe

10:

End of segment? : y

Display commands for this segment? : y

MODL COMMAND TABLE

SEGMENT NO.	1.	Run No. = 1						
c.p.	elem	optn	data	optn	data	optn	data	
1								
16	pipe	bcon	111111					
		prop	1					
		locl	+	ldis	yes	this	yes	
		wfac	1.0000					
16	gapf							

Table 2.3.9 (cont'd)

		prop	1				
		this	yes				
17	pipe	dyij	-1.0000	gap	124.0		
		prop	1				
		locl	+	ldis	yes	this	yes
		wfac	1.0000				
Hit RETURN for more							
17	gapf						
		prop	1				
		this	yes				
18	pipe	dyij	-1.0000	gap	128.8		
		prop	1				
		locl	+	ldis	yes	this	yes
		wfac	1.0000				
18	gapf						
		prop	1				
		this	yes				
		dyij	-1.0000	gap	142.0		
Hit RETURN for more							
19	pipe						
		prop	1				
		locl	+	ldis	yes	this	yes
		wfac	1.0000				
19	gapf						
		prop	1				
		this	yes				
		dyij	-1.0000	gap	160.0		
20	pipe						
		prop	1				
		locl	+	ldis	yes	this	yes
		wfac	1.0000				

Hit RETURN for more
Any changes? :

SEGMENT NO. 2

Pipe run no. :
Last segment? : y

Any external substructures? :

Display commands for all segments? :
Write in session log? :

Produce MODL file? : y
Wait while data is processed

Specify initial velocities? :
Comment for file catalog : No friction, no strain rate.

MODL file saved. File name = MODL0101
End of this MODL session

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

TABLE 2.3.10 - WIPSLOG LISTING FOR DATA PHASE, CASE 1.

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : data

DATA - SET UP WIPS-ANAL INPUT DATA

Define units

Length (ft,in,m,mm) : in
Force (k,lb,kgf,kN) : k

Sequence no. of MODL file : 1

Problem description (4 lines)

Line 1 : Example as in Fig.4.12 of Hibbitt-Karlisson Report.
Line 2 :
Line 3 : PIPE with no strain rate. GAPF with negligible friction.
Line 4 :

Set up PAUSE files at end of analysis ? :
Wait while files are processed

Specify data for each loaded point

LOAD NO. 1

Force record name : rec1
Name of loaded c.p. : 20
Force direction (x,y,z or follower) : foll
Follower c.p. name : 19
Scale factor (+,- controls direction) : .5
Time delay (sec) (dflt=0) :

LOAD NO. 2

Force record name :
Last load? : y

Time steps : initial + max + min : .0005 .001 .00001
Max steps + max total time : 1500 .3
Error tolerances : upper + lower : 50 10

Results output intervals

Max. no. of steps : 20
Max. time (secs.) : .02
Integration scheme (newm or hilb)(dflt=newm) :
Damping factor (dflt=0.1) :
Factor for time step increase (dflt=2.0) :
Factor for time step decrease (dflt=0.5) :
Max. unbal. to reduce time step (dflt=no limit) :
Max. unbal. to stop analysis (dflt=no limit) :

DATA file set complete

Comment for file catalog : No s.r., no friction.
WIPS-ANAL DATA FILES SET UP. PARENT FILE NAME = DATA0101

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

TABLE 2.3.11 - DATA FILE LISTING. CASE 1.

```

ECH00102  SLOG0102  RSLT0102
star,
gbui
new,main,nonl,cart,0
substructure name = main
refn,21
  1  0.          e+00  0.          s+00  0.          e+00
  2  0.1800000e+02  0.          s+00  0.          e+00
  3  0.3600000e+02  0.          s+00  0.          e+00
  4  0.5400000e+02 -0.4823090e+01  0.          e+00
  5  0.6717691e+02 -0.1800000e+02  0.          e+00
  6  0.7200000e+02 -0.3600000e+02  0.          e+00
  7  0.7200000e+02 -0.7400000e+02  0.          e+00
  8  0.7200000e+02 -0.1120000e+03  0.          e+00
  9  0.7682310e+02 -0.1300000e+03  0.          e+00
 10  0.9000001e+02 -0.1431769e+03  0.          e+00
 11  0.1080000e+03 -0.1480000e+03  0.          e+00
 12  0.1566000e+03 -0.1480000e+03  0.          e+00
 13  0.2052000e+03 -0.1480000e+03  0.          e+00
 14  0.2538000e+03 -0.1480000e+03  0.          e+00
 15  0.3024000e+03 -0.1480000e+03  0.          e+00
 16  0.3510000e+03 -0.1480000e+03  0.          e+00
 17  0.3689998e+03 -0.1431770e+03  0.          e+00
 18  0.3821770e+03 -0.1299998e+03  0.          e+00
 19  0.3870000e+03 -0.1120000e+03  0.          e+00
 20  0.3870000e+03 -0.6000000e+01  0.          e+00
9999
boun,21
  1  111111
  2  1110
  3  1110
  4  1110
  5  1110
  6  1110
  7  1110
  8  1110
  9  1110
 10  1110
 11  1110
 12  1110
 13  1110
 14  1110
 15  1110
 16  1110
 17  1110
 18  1110
 19  1110
 20  1110
9999 111111
enod,0
matl,4,64
0.20000000e+010.299999982e+000.267000000e+050.219000000e+030.200000000e+01
0.267000008e+020.440000000e+020.999999932e+200.199999996e-010.499999970e-01
0.120000000e+020.200000000e+010.          s+000.200000000e+010.100000000e+01
0.100000000e+010.240000000e+020.153100002e+010.306922067e-010.          s+00
0.349999976e+000.799999970e-010.          s+000.          s+000.          s+00

```


Table 2.3.11 (cont'd)

0.359999962e+02-	.360000038e+020.		e+000.		e+00
5	0 0 0 5 6	1	1 1 0	1	1
0.359999962e+02-	.360000038e+020.		e+000.		e+00
6	0 0 0 6 7	1	1 1 1	0	1
0.730000000e+02-	.360000000e+020.		e+000.		e+00
7	0 0 0 7 8	1	1 1 1	0	1
0.730000000e+02-	.740000000e+020.		e+000.		e+00
8	0 0 0 8 9	1	1 1 0	1	1
0.108000008e+03-	.112000000e+030.		e+000.		e+00
9	0 0 0 9 10	1	1 1 0	1	1
0.108000008e+03-	.112000000e+030.		e+000.		e+00
10	0 0 0 10 11	1	1 1 0	1	1
0.108000008e+03-	.112000000e+030.		e+000.		e+00
11	0 0 0 11 12	1	1 1 1	0	1
0.108000000e+03-	.147000000e+030.		e+000.		e+00
12	0 0 0 12 13	1	1 1 1	0	1
0.156600006e+03-	.147000000e+030.		e+000.		e+00
13	0 0 0 13 14	1	1 1 1	0	1
0.205200012e+03-	.147000000e+030.		e+000.		e+00
14	0 0 0 14 15	1	1 1 1	0	1
0.253800003e+03-	.147000000e+030.		e+000.		e+00
15	0 0 0 15 16	1	1 1 1	0	1
0.302400024e+03-	.147000000e+030.		e+000.		e+00
16	0 0 0 16 17	1	1 1 0	1	1
0.351000000e+03-	.112000000e+030.		e+000.		e+00
17	0 0 0 17 18	1	1 1 0	1	1
0.351000000e+03-	.112000000e+030.		e+000.		e+00
18	0 0 0 18 19	1	1 1 0	1	1
0.351000000e+03-	.112000000e+030.		e+000.		e+00
19	0 0 0 19 20	1	1 1 1	0	1
0.386000000e+03-	.112000000e+030.		e+000.		e+00
4	4 1		0.		
1	0 0 0 16 0	3	1 1		
0.	e+000.100000000e+010.		e+000.100000000e+010.		e+00
0.	e+000.124000000e+03				
2	0 0 0 17 0	3	1 1		
0.	e+000.100000000e+010.		e+000.100000000e+010.		e+00
0.	e+000.128820007e+03				
3	0 0 0 18 0	3	1 1		
0.	e+000.100000000e+010.		e+000.100000000e+010.		e+00
0.	e+000.142000000e+03				
4	0 0 0 19 0	3	1 1		
0.	e+000.100000000e+010.		e+000.100000000e+010.		e+00
0.	e+000.160000000e+03				

```

nord,opto
prof
end
fini
mode
tree,main
fini
mbui
new,main
pwas,24

```

Table 2.3.11 (cont'd)

```

10 0.35967e-03 0.35967e-03 0.35967e-03 0. e+00 0. e+00 0. e+0000
20 0.71935e-03 0.71935e-03 0.71935e-03 0. e+00 0. e+00 0. e+0000
30 0.73204e-03 0.73204e-03 0.73204e-03 0. e+00 0. e+00 0. e+0000
40 0.74472e-03 0.74472e-03 0.74472e-03 0. e+00 0. e+00 0. e+0000
50 0.74472e-03 0.74472e-03 0.74472e-03 0. e+00 0. e+00 0. e+0000
60 0.11317e-02 0.11317e-02 0.11317e-02 0. e+00 0. e+00 0. e+0000
70 0.15186e-02 0.15186e-02 0.15186e-02 0. e+00 0. e+00 0. e+0000
80 0.11317e-02 0.11317e-02 0.11317e-02 0. e+00 0. e+00 0. e+0000
90 0.74472e-03 0.74472e-03 0.74472e-03 0. e+00 0. e+00 0. e+0000
100 0.74472e-03 0.74472e-03 0.74472e-03 0. e+00 0. e+00 0. e+0000
110 0.13435e-02 0.13435e-02 0.13435e-02 0. e+00 0. e+00 0. e+0000
120 0.19422e-02 0.19422e-02 0.19422e-02 0. e+00 0. e+00 0. e+0000
130 0.19422e-02 0.19422e-02 0.19422e-02 0. e+00 0. e+00 0. e+0000
140 0.19422e-02 0.19422e-02 0.19422e-02 0. e+00 0. e+00 0. e+0000
150 0.19422e-02 0.19422e-02 0.19422e-02 0. e+00 0. e+00 0. e+0000
160 0.97112e-03 0.97112e-03 0.97112e-03 0. e+00 0. e+00 0. e+0000
160 0.37236e-03 0.37236e-03 0.37236e-03 0. e+00 0. e+00 0. e+0000
170 0.37236e-03 0.37236e-03 0.37236e-03 0. e+00 0. e+00 0. e+0000
170 0.37237e-03 0.37237e-03 0.37237e-03 0. e+00 0. e+00 0. e+0000
180 0.37237e-03 0.37237e-03 0.37237e-03 0. e+00 0. e+00 0. e+0000
180 0.37236e-03 0.37236e-03 0.37236e-03 0. e+00 0. e+00 0. e+0000
190 0.37236e-03 0.37236e-03 0.37236e-03 0. e+00 0. e+00 0. e+0000
190 0.21181e-02 0.21181e-02 0.21181e-02 0. e+00 0. e+00 0. e+0000
200 0.21181e-02 0.21181e-02 0.21181e-02 0. e+00 0. e+00 0. e+0000

end
fini
ptre
newr, recl, pair, 8, 100
(2e15.7)
0. e+00 0. e+00
0.6500000e+03 0.1000000e-03
0.8800000e+03 0.1000000e-02
0.1000000e+04 0.2000000e-02
0.8800000e+03 0.3000000e-02
0.7800000e+03 0.5000000e-02
0.4300000e+03 0.2000000e-01
0.4300000e+03 0.1000000e+02
fini
thou, 792
2 191 3 1 0 0
ndyn
mass
dylo, 1, 1
recl 0 0. 0.500 2
20 19
tmo, rslt, 20, 0.2000e-01
auto, defl
inte, newm, 0.5000e-03, 0.e+00, 0.e+00, 0.1000e+00
stif
stif, upda
kinr, 12
elmr, 1, 2, 6, 3
kinr, 5
loop, 1500
zero, ltme
step

```

Table 2.3.11 (cont'd)

```
unba
auto,init
loop,20
stif
auto,load
load
disp
kinr,10
elmr,9,10
auto,merr,0.1000e+02,0.5000e+02
if,3,3,1,1
entr,1
auto,fact
kinr,1
if,3,2,2,3
entr,2
elmr,1
cont
goto,0
entr,3
auto,step,0.1000e-04,0.1000e-02,0.5000e+00,0.1000e+01
if,4,5,5,4
entr,4
inte,newm,,auto,0.e+00,0.e+00,0.e+00,0.1000e+00
entr,5
if,3,6,6,7
entr,6
kinr,12
elmr,5,2,6
kinr,5
stif,init
goto,8
entr,7
chou
elmr,1,2,4,6,11
kinr,4,9,11
wrou
zero,lr sb
unba
summ
elmr,3
kinr,3
stif,upda
auto,exit,0.3000e+00
if,5,8,8,0
entr,8
cont
fini
stop
```

D2.4 CLAMPED BEAM WITH IMPULSIVE LOADING

D2.4.1 PURPOSE

This example tests the BEAM element, by comparison with test results and previously reported analysis results. Large displacement and strain rate effects are considered, and the initial velocity loading option is tested.

D2.4.2 DESCRIPTION

Tests and analyses of a clamped-end beam under impulse (explosive) loading have been reported by Witmer et al [2.4.1]. Analyses of the same beam have been reported by Hibbitt and Karlsson [2.4.2].

The dimensions of the beam are shown in Fig. 2.4.1. Initial velocities as shown were produced by an explosive charge.

The beam was made of 6061-T6 aluminum alloy. The static Young's modulus reported in [2.4.1] was 10400 ksi ($7.171 \times 10^{10} \text{ N/m}^2$). For analysis, bilinear stress-strain relationships were assumed in both [2.4.1] and [2.4.2]. Very similar results were reported in [2.4.1] for (a) elastic-perfectly-plastic material with an extensional yield stress of 41.4 ksi ($2.854 \times 10^8 \text{ N/m}^2$) and (b) elastic-strain-hardening material with a yield stress of 40.5 ksi ($2.792 \times 10^8 \text{ N/m}^2$) and a strain hardening modulus of 76.1 ksi ($5.247 \times 10^8 \text{ N/m}^2$). The elastic-strain-hardening material was assumed for the WIPS analyses.

For the analyses in both [2.4.1] and [2.4.2], high strain rates were assumed to increase the yield stress according to the equation:

$$\sigma_y - \sigma_{y0} = \sigma_{y0} (|\dot{\epsilon}|/6500)^{0.25} \quad (2.4.1)$$

in which $\dot{\epsilon}$ = extensional strain rate; σ_{y0} = static yield stress; and σ_y = dynamic yield stress. For the WIPS analyses a trilinear approximation as shown in Table 2.4.1 was assumed.

The following WIPS analyses were performed:

- (1) Ten BEAM elements in half span, no strain rate effect, Newmark solution scheme
- (2) Ten BEAM elements in half span, no strain rate effect, Hilber-Hughes-Taylor (HHT) solution scheme.
- (3) Ten BEAM elements in half span, with strain rate effect, Newmark solution scheme.

In addition, an analysis with twenty BEAM elements in the half span and no strain rate effect was carried out to explore the effect of discretization. The results were not significantly different from those for Case 1 and are not reported here.

D2.4.3 WIPS ANALYSIS MODEL

D2.4.3.1 Geometry and Loading

The element subdivision and initial velocities for the 10-element analysis are shown in Fig. 2.4.2. The initial kinetic energy is the same as for the beam shown in Fig. 2.4.1. Only motion in the XY plane was permitted (i.e. no beam twist or lateral bending).

D2.4.3.2 BEAM Element Properties

For the assumed elastic-strain-hardening material, force-extension and moment-curvature relationships were calculated for the BEAM element cross section. The force-extension relationship has the same shape as the stress-strain curve, whereas the moment-curvature relationship is curvilinear. The two relationships were approximated using four linear segments each, as shown in Tables 2.4.2 and 2.4.3.

The procedure for determining strain rate properties for BEAM elements is described in the Theory Manual, Section B4.4.2. With this procedure and the dashpot stiffnesses shown in Table 2.4.1, the dimensionless properties shown in Table 2.4.4 were calculated.

D2.4.3.3 Analysis Control Parameters

For analysis with the Newmark scheme, the following parameters were specified:

Initial time step = 2×10^{-6} sec.

Minimum time step = 1×10^{-6} sec.

Maximum time step = 1×10^{-4} sec.

Initial $\beta/\Delta t$ = 0.1

Lower midstep tolerance = 0.5 k

Upper midstep tolerance = 2.5 k

The same parameters were used with the HHT scheme, except that the damping parameter was $\alpha = -0.1$.

D2.4.3.4 WIPS Input

Table 2.4.5 contains the WIPSLOG listing through the WIPS-DATA phase for Case 3. The procedures for the other cases were similar. Table 2.4.6 is a listing of the DATA file for Case 3.

D2.4.4 RESULTS

D2.4.4.1 No Strain Rate: Newmark Scheme

For the Newmark scheme and no strain rate, Fig. 2.4.3 compares the WIPS results for midspan deflection with the test results from [2.4.1] and the analysis results from [2.4.1] and [2.4.2]. The analysis in [2.4.1] used a finite difference scheme with 30 nodes in the half span. The analysis in [2.4.2] used a finite element model with 10 elements in the half span. It should be noted that during the test the beam twisted significantly because the explosion wavefront traveled laterally across the beam. Hence, there is some doubt whether the test and analysis results are directly comparable.

The three analyses differ significantly, that from [2.4.2] predicting the largest displacement and the WIPS analysis predicting the smallest displacement. None of the analyses agrees closely with the test results.

Because the displacements computed using WIPS were smaller than those reported in [2.4.1] and [2.4.2], an analysis was also carried out using very small numerical damping ($\beta/\Delta t$, = 0.002 rather than the default value of 0.1). The results differed only very slightly from those shown in Fig. 2.4.3. However, the number of time steps required for the solution increased dramatically (from 70 to 202 steps).

D2.4.4.2 No Strain Rate: HHT Scheme

Figure 2.4.4 compares the results for analyses with the Newmark and HHT schemes. The results are closely similar up to 0.5 milliseconds. The HHT analysis required 63 time steps for the solution.

D2.4.4.3 With Strain Rate

For the Newmark scheme with strain rate effects, Fig. 2.4.5 shows comparisons with experiment and the analyses reported in [2.4.1] and [2.4.2]. The WIPS analysis agrees quite closely with the analysis from [2.4.1]. Note, however, that the WIPS strain rate theory is not identical to that used in [2.4.1]. In particular, the strength increase in WIPS is based on plastic strain rate rather than total strain rate. This will tend to make the WIPS model somewhat more

flexible. The analysis required 63 time steps. The results of the WIPS analyses with and without strain rate effects are compared in Fig. 2.4.6.

D2.4.5 CONCLUSION

Compared with the two other reported analyses, the BEAM element in WIPS is slightly stiff. This is not due to the numerical damping scheme. For the case with no strain rate, the WIPS analyses and the two other reported analyses all differ from each other significantly. For the case with strain rate the WIPS analysis agrees quite closely with the analysis from [2.4.1] but differs significantly from the analysis in [2.4.2]. None of the analyses agrees closely with experiment. However, the experimental results are not necessarily reliable because of twisting of the beam.

Without further study it is not possible to say which of the analyses is the most accurate.

D2.4.6 REFERENCES

- 2.4.1 Witmer, E. A., Balmer, H. A., Leech, J. W., and Pian, T.H.H., "Large Dynamic Deformations of Beams, Rings, Plates, and Shells," *AIAA Journal*, Vol. 1, No. 8, pp. 1848-1857, 1963.
- 2.4.2 Hibbitt and Karlsson, "Analysis of Pipe Whip," Report No. EPRI NP-1208, Electric Power Research Institute, 1979.

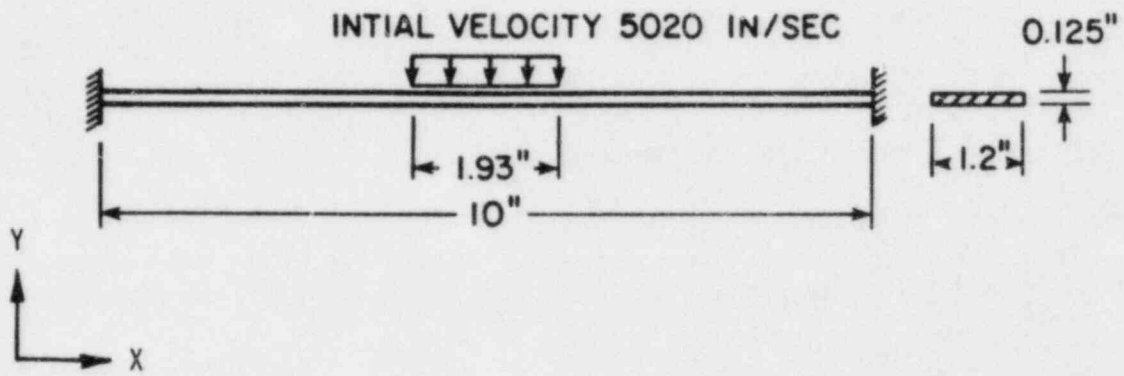


FIG. 2.4.1 IMPULSIVELY LOADED BEAM

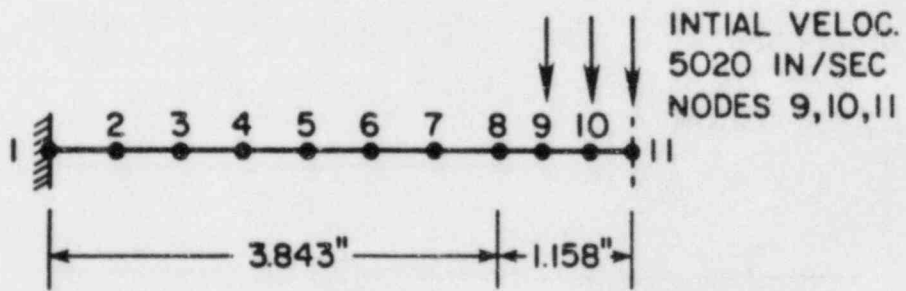


FIG. 2.4.2 ELEMENT SUBDIVISION

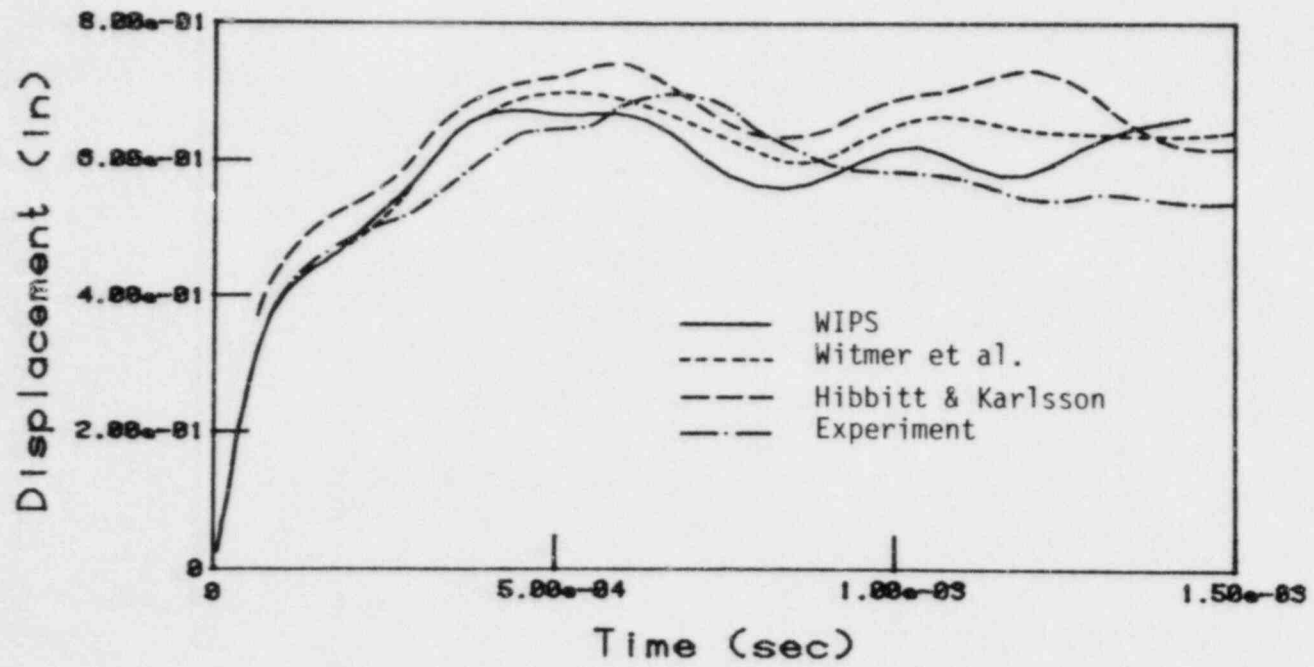


FIG. 2.4.3 DISPLACEMENT AT BEAM CENTER,
WITHOUT STRAIN RATE EFFECT.

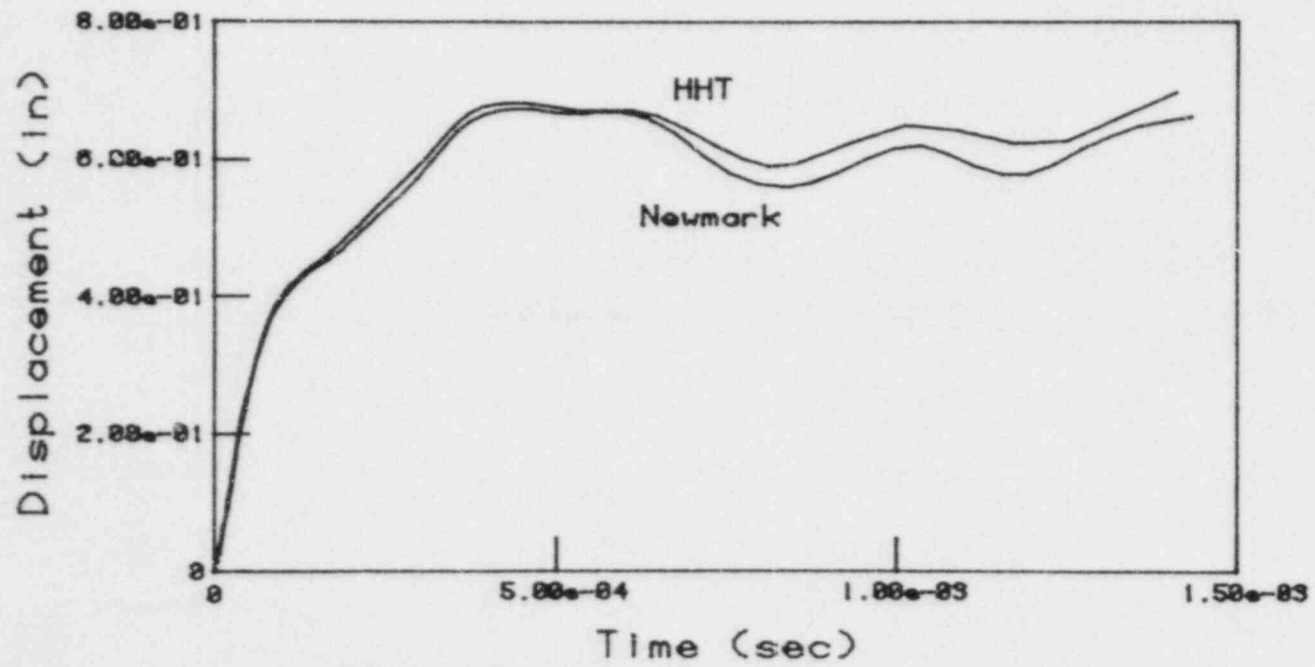


FIG. 2.4.4 DISPLACEMENT AT BEAM CENTER.
COMPARISON OF NEWMARK AND HHT SCHEMES.

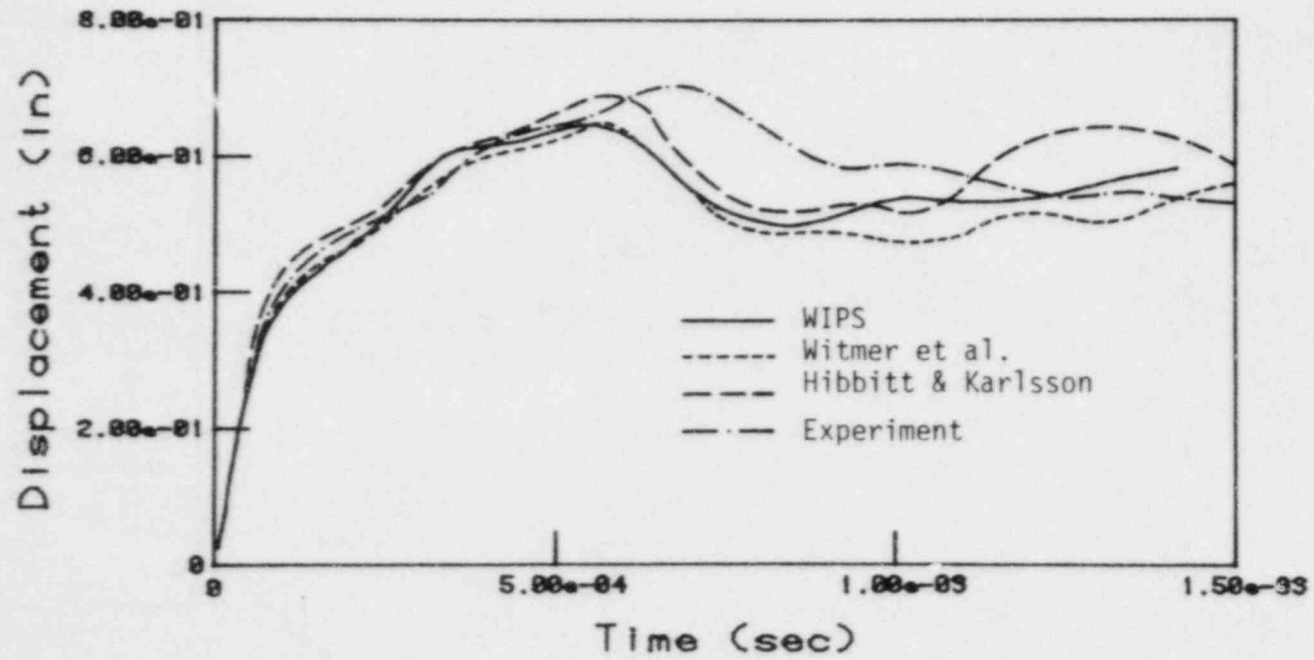


FIG. 2.4.5 DISPLACEMENT AT BEAM CENTER,
WITH STRAIN RATE EFFECT.

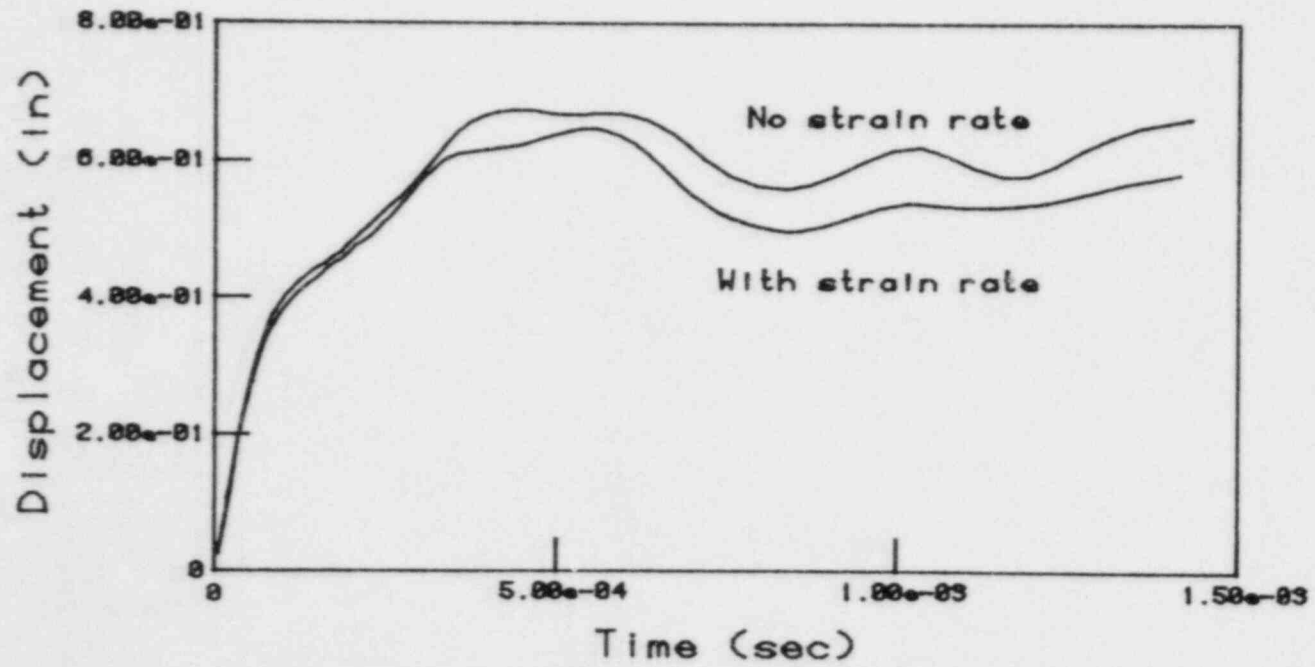


FIG. 2.4.6 DISPLACEMENT AT BEAM CENTER.
INFLUENCE OF STRAIN RATE ON RESULTS.

TABLE 2.4.1 - TRILINEAR APPROXIMATION FOR STRAIN RATE EFFECT		
Stress Increase (ksi)	Strain Rate (sec ⁻¹)	Dashpot Stiffness (k.sec/in ²)
0	0	2.0
8	4	0.0685
18	150	0.0108

TABLE 2.4.2 - STATIC FORCE-EXTENSION RELATIONSHIP FOR BEAM ELEMENT		
Force (k)	Axial Strain	Stiffness (k)
0	0	1560.00
6.075	0.00389	11.42
6.170	0.01121	11.41
6.634	0.05184	11.40

TABLE 2.4.3 - STATIC MOMENT-CURVATURE RELATIONSHIP FOR BEAM ELEMENT		
Moment (k.in)	Curvature (in ⁻¹)	Stiffness (k.in ²)
0	0	2.0310
0.156	0.0768	0.2290
0.189	0.2212	0.0150
0.201	1.0225	0.0149

TABLE 2.4.4 - DIMENSIONLESS STRAIN RATE RELATIONSHIP FOR BEAM ELEMENT	
Strength Increase Factor	Deformation Rate Factor
0	0
0.1869	1027
0.4206	38520
2.9370	2.607 × 10 ⁶

TABLE 2.4.5 - WIPSLOG LISTING. GEOM, BEAM, FREC, MODL AND DATA PHASES.

EXEC - WIPS EXECUTIVE
 Creating problem no. 1
 Problem description: Clamped beam with initial velocity. BEAM model.

NEXT WIPS-EXEC COMMAND : geom

GEOM - SPECIFICATION OF SYSTEM GEOMETRY

Define units

Length (ft,ln,m,mm) : ln
 Force (k,lb,kgf,kN) : k

Specify new GEOM data

START RUN NO. 1

Enter c.p. data in sequence along run

c.p. name and type : 1
 coord option : dl
 x,y,z :
 Any changes? :

c.p. name and type : 8
 no. of extra nodes : 6
 coord option :
 c.p. dx,dy,dz : ,3.843
 offset point defaults to preceding c.p.
 Any changes? :

c.p. name and type : 9
 no. of extra nodes :
 coord option :
 c.p. dx,dy,dz : ,.386
 offset point defaults to preceding c.p.
 Any changes? :

c.p. name and type : 11
 no. of extra nodes : 1
 coord option :
 c.p. dx,dy,dz : 1 5
 Any changes? :

c.p. name and type :
 Last c.p. in this run? : y
 Display GEOM data for this run? : y

GEOM DATA FOR RUN

run no.	c.l. name	c.p. type	bend radius	xtra nods	coord opt	c.p. i	c.p. j ?	coordinate data x,dx,p	y,dy	z,dz
1	1			0	dl			0.	0.	0.
	8			6	of	1		3.843	0.	0.
	9			0	of	8		0.386	0.	0.
	11			1	of	1		5.000	0.	0.

Table 2.4.5 (cont'd)

END OF DATA

START RUN NO. 2

Enter c.p. data in sequence along run

c.p. name and type :
Last run? : y

Display new GEOM data? :
Write in session log? :

Modify GEOM data? :

Save current GEOM data? : y
Comment for file catalog :
GEOM DATA SAVED. FILE NAME = GEOM0101

Produce COOR data? : y

Display COOR data? : y

COORD DATA

run no.	c.p. name	c.p. type	bend radius	node no.	x coord	y ? coord?	z coord
1				1	0.	0.	0.
	1			2	0.540	0.	0.
				3	1.090	0.	0.
				4	1.647	0.	0.
				5	2.196	0.	0.
				6	2.745	0.	0.
				7	3.294	0.	0.
	8			8	3.843	0.	0.
	9			9	4.220	0.	0.
				10	4.615	0.	0.
				11	5.000	0.	0.

Hit RETURN for more

11
END OF DATA

Plot geometry? :

Modify GEOM data? :

DATA COMPLETE FOR THIS SESSION
Save final GEOM data? : y
Comment for file catalog : 10 elements.
GEOM DATA SAVED. FILE NAME = GEOM0101
Save COOR data? : y
Comment for file catalog : 10 elements.
COORD DATA SAVED. FILE NAME = COOR0101

End of this GEOM session

Table 2.4.5 (cont'd)

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : beam

BEAM - SPECIFICATION OF BEAM PROPERTIES

Define units

Length (ft,in,m,mm) : in

Force (k,lb,kgf,kN) : k

Start new BEAM file

Specify a new property set? : y

SET NO. = 1

Property set description : 1.2x0.125, 40.5ksi, no strain rate.

Yield surface type (1-4) (dflt=1) : 2

Weight per unit length : 1.448e-5

Elastic stiffnesses

EAx,GAy,GAz : 1560 500 500

GJx,EIy,EIz : 2.031 2.031 2.031

Strengths at first yield

Fx,Mxx,Myy,Mzz : 6.075 .156 .156 .156

Stiffnesses after first yield

EA,GJx,EIy,EIz : 11.42 .229 .229 .229

Strengths at second yield

Fx,Mxx,Myy,Mzz : 6.17 .189 .189 .189

Stiffnesses after second yield

EA,GJx,EIy,EIz : 11.41 .015 .015 .015

Strengths at third yield

Fx,Mxx,Myy,Mzz : 11.4 .0149 .0149 .0149

*** error - must exceed previous values

Strengths at third yield

Fx,Mxx,Myy,Mzz : 6.634 .201 .201 .201

Stiffnesses after third yield

EA,GJx,EIy,EIz : 11.4 .0149 .0149 .0149

Strain rate factors (0-3, dflt=none) :

No strain rate effect

Use default tolerances? : y

Any errors? :

This set added to BEAM file

Specify a new property set? : y

SET NO. = 2

Property set description : 1.2x0.125, 40.5ksi, with strain rate.

Yield surface type (1-4) (dflt=1) : 2

Weight per unit length : 1.448e-5

Elastic stiffnesses

Table 2.4.5 (cont'd)

EAx,GAy,GAz : 1560 500 500
 GJx,EIy,EIz : 2.031 2.031 2.031
 Strengths at first yield
 Fx,Mxx,Myy,Mzz : 6.075 .156 .156 .156
 Stiffnesses after first yield
 EA,GJx,EIy,EIz : 11.42 .229 .229 .229
 Strengths at second yield
 Fx,Mxx,Myy,Mzz : 6.17 .189 .189 .189
 Stiffnesses after second yield
 EA,GJx,EIy,EIz : 11.41 .015 .015 .015
 Strengths at third yield
 Fx,Mxx,Myy,Mzz : 6.634 .201 .201 .201
 Stiffnesses after third yield
 EA,GJx,EIy,EIz : 11.4 .0149 .0149 .0149
 Strain rate factors (0-3, dflt=none) : 1027 38520 2.607e6
 Corresponding strength factors : .1869 .4206 2.937
 Use default tolerances? : y

Any errors? :

This set added to BEAM file

Specify a new property set? :

No. of property sets in BEAM file = 2

Display property set descriptions? : y

BEAM PROPERTY DESCRIPTIONS

Set No.	Description
1	1.2x0.125, 40.5ksi, no strain rate.
2	1.2x0.125, 40.5ksi, with strain rate.

Display new property set data? :

Write in session log? :

Display all property set data? : y

BEAM PROPERTY DATA

SET NO. 1. 1.2x0.125, 40.5ksi, no strain rate.

Data Type	Data 1	Data 2	Data 3	Data 4
Unit weight	0.1448e-04			
Elastic EAx,GAy,GAz	0.1560e+04	0.5000e+03	0.5000e+03	
GJx,EIy,EIz	0.2031e+01	0.2031e+01	0.2031e+01	
First yield				
Fx,Mxx,Myy,Mzz	0.6075e+01	0.1560e+00	0.1560e+00	0.1560e+00
EA,GJx,EIy,EIz	0.1142e+02	0.2290e+00	0.2290e+00	0.2290e+00
Second yield				
Fx,Mxx,Myy,Mzz	0.6170e+01	0.1890e+00	0.1890e+00	0.1890e+00
EA,GJx,EIy,EIz	0.1141e+02	0.1500e-01	0.1500e-01	0.1500e-01
Third yield				
Fx,Mxx,Myy,Mzz	0.6634e+01	0.2010e+00	0.2010e+00	0.2010e+00
EA,GJx,EIy,EIz	0.1140e+02	0.1490e-01	0.1490e-01	0.1490e-01

Table 2.4.5 (cont'd)

Stiffness tolerance 0.5000e-01
 Yield tolerance 0.2000e-01
 Unloading tolerance 0.2000e-01
 Hit RETURN for next set

SET NO. 2. 1.2x0.125, 40.5ksi, with strain rate.

Data Type	Data 1	Data 2	Data 3	Data 4
Unit weight	0.1448e-04			
Elastic EAx,GAy,GAz	0.1560e+04	0.5000e+03	0.5000e+03	
GJx,EIy,EIz	0.2031e+01	0.2031e+01	0.2031e+01	
First yield				
Fx,Mxx,Myy,Mzz	0.6075e+01	0.1560e+00	0.1560e+00	0.1560e+00
EA,GJx,EIy,EIz	0.1142e+02	0.2290e+00	0.2290e+00	0.2290e+00
Second yield				
Fx,Mxx,Myy,Mzz	0.6170e+01	0.1890e+00	0.1890e+00	0.1890e+00
EA,GJx,EIy,EIz	0.1141e+02	0.1500e-01	0.1500e-01	0.1500e-01
Third yield				
Fx,Mxx,Myy,Mzz	0.6634e+01	0.2010e+00	0.2010e+00	0.2010e+00
EA,GJx,EIy,EIz	0.1140e+02	0.1490e-01	0.1490e-01	0.1490e-01
Strain rate factors	0.1027e+04	0.3852e+05	0.2607e+07	
Strength factors	0.1869e+00	0.4206e+00	0.2937e+01	
Stiffness tolerance	0.5000e-01			
Yield tolerance	0.2000e-01			
Unloading tolerance	0.2000e-01			
Str. rate tolerance	0.5000e-01			

Hit RETURN for next set
 END OF DATA

New BEAM file created
 Comment for file catalog : 2 sets.

End this BEAM session? : y

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : frec

FREC - SPECIFY DYNAMIC FORCE RECORDS

Define units
 Length (ft,in,m,mm) : in
 Force (k,lb,kgf,kN) : k

Start new FREC file

Specify a new record? : y

RECORD NO. 1

Record name (4 characters) : rec1
 Description (max. 40 char.) : Dummy zero record.

Enter Time-Force pairs
 First pair automatically set to 0,0

Table 2.4.5 (cont'd)

```
Pair no. 2 : 10 0.
Pair no. 3 :
Last pair? : y
Any errors? :

Specify a new record? :

Display any records? : y
Record number (dflt=all) :

RECORD NO. 1. Name = rec1
      Time      Force
      0.         0.    e+00
      10.00000  0.    e+00
END OF RECORD

Write records in session log? :

End this FREC session? : y
New FREC file created
Comment for file catalog : 1 dummy record.

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : mod1

MODL - SPECIFICATION OF ANALYSIS MODEL

Define units
  Length (ft,in,m,mm) : in
  Force (k,lb,kgf,kN) : k

Sequence no. of COOR file : 1

Available element property sets
  Type      No. of Sets
  beam      2
Available substructure property sets
  None

DEFINE MODEL IN SEGMENTS

SEGMENT NO. 1

Pipe run no. : 1
First c.p. of segment : 1
Full 3D motion? :
Displacement plane (xy,yz or zx) : xy
Any substructures in this segment? :
Boundary condition code for first c.p. : 11111

Specify c.p.name + elem type + optional data
  1: 9 beam pr=2 ld=y
  2:
End of segment? : y
```

Table 2.4.5 (cont'd)

Display commands for this segment? : y

MODL COMMAND TABLE

SEGMENT NO.	1.	Run No. = 1					
c.p.	elem	optn	data	optn	data	optn	data
1		bcon	111111				
9	beam	prop	2				
		loc1	+	ldis	yes	this	yes
		wfac	1.0000				

Any changes? :

SEGMENT NO. 2

Pipe run no. : 1
 First c.p. of segment : 9
 Full 3D motion? :
 Displacement plane (xy,yz or zx) : xy
 Any substructures in this segment? :
 Boundary condition code for first c.p. :
 Symmetric - boundary code reset to 001110

Specify c.p.name + elem type + optional data

1: 11 beam

2:

End of segment? : y

Display commands for this segment? : y

MODL COMMAND TABLE

SEGMENT NO.	2.	Run No. = 1					
c.p.	elem	optn	data	optn	data	optn	data
9		bcon	1110				
11	beam	prop	2				
		loc1	+	ldis	yes	this	yes
		wfac	1.0000				

Any changes? : y

Re-enter data for this segment

SEGMENT NO. 2

Pipe run no. : 1
 First c.p. of segment : 9
 Full 3D motion? :
 Displacement plane (xy,yz or zx) : xy
 Any substructures in this segment? :
 Boundary condition code for first c.p. :
 Symmetric - boundary code reset to 001110

Specify c.p.name + elem type + optional data

1: 11 beam

2: 11, bc=101111

Table 2.4.5 (cont'd)

```

3:
End of segment? : y
Display commands for this segment? : y

MODL COMMAND TABLE

SEGMENT NO. 2. Run No. = 1
c.p. elem  optn  data      optn  data      optn  data
9
11  beam      bcon    1110
      prop      2
      loc1     +      ldis    yes      this    yes
      wfac    1.0000
11      bcon    101111
Any changes? :

SEGMENT NO. 3

Pipe run no. :
Last segment? : y

Any external substructures? :

Display commands for all segments? :
Write in session log? :

Produce MODL file? : y
Wait while data is processed

Specify initial velocities ? : y
Specify initial velocities for affected segments
Warning - only partial consistency check is performed on data
SEGMENT NO. : 2
Segment has transverse symmetry
Motion in xy plane only
Name of pivot point (dflt = no pivot) :
Specify global x+y velocities : 0 -5020
SEGMENT NO. :
Last affected segment ? : y
Wait while data is processed
Comment for file catalog : 10 elements, with strain rate.

MODL file saved. File name = MODL0101
End of this MODL session

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : list

Problem 1: Clamped beam with initial velocity. BEAM mode?

file  sequence      date                description
type  number
GDM   1   Fri Aug 13 14:45:24 1982  10 elements.

```

Table 2.4.5 (cont'd)

```

CODR      1  Fri Aug 13 14:45:24 1982  10 elements.
BEAM      Fri Aug 13 14:53:48 1982  2 sets.
FREC      Fri Aug 13 14:55:28 1982  1 dummy record.
MODL      1  Fri Aug 13 15:01:09 1982  10 elements, with strain rate.

```

NEXT WIPS-EXEC COMMAND : data

DATA - SET UP WIPS-ANAL INPUT DATA

Sequence no. of MODL file : 1

Problem description (4 lines)

```

Line 1 : Clamped Beam with Initial Velocity.          GHP 7/82
Line 2 :
Line 3 : 10 elements, with strain rate. 5020 velocity at 9,10,11.
Line 4 :

```

Set up PAUSE files at end of analysis ? :

```

Wait while files are processed
Initial velocities may be scaled if desired
Specify scale factor (dflt=1.0) :

```

Specify data for each loaded point

```

LOAD NO. 1
  Force record name : recl
  Name of loaded c.p. : 1
  Force direction (x,y,z or follower) : y
  Scale factor (+,- controls direction) : 1
  Time delay (sec) (dflt=0) :
LOAD NO. 2
  Force record name :
Last load? : y

```

```

Time steps : initial + max + min : 2e-6 1e-4 1e-6
Max steps + max total time : 200 .0015
Error tolerances : upper + lower : .5 .1

```

Results output intervals

```

Max. no. of steps : 1
Max. time (secs.) : 1
Integration scheme (newm or hllb)(dflt=newm) :
Damping factor (dflt=0.1) :
Factor for time step increase (dflt=2.0) :
Factor for time step decrease (dflt=0.5) :
Max. unbal. to reduce time step (dflt=no limit) : .5
Max. unbal. to stop analysis (dflt=no limit) : 10

```

DATA file set complete

```

Comment for file catalog : 10 elem, strain rate, Newmark 0.1
WIPS-ANAL DATA FILES SET UP. PARENT FILE NAME = DATA0101

```

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : list

Table 2.4.5 (cont'd)

Problem 1: Clamped beam with initial velocity. BEAM model.

file type	sequence number	date	description
GEOM	1	Fri Aug 13 14:45:24 1982	10 elements.
COORD	1	Fri Aug 13 14:45:24 1982	10 elements.
BEAM		Fri Aug 13 14:53:48 1982	2 sets.
FREC		Fri Aug 13 14:55:28 1982	1 dummy record.
MODL	1	Fri Aug 13 15:01:09 1982	10 elements, with strain rate.
DATA	1	Fri Aug 13 15:01:09 1982	10 elem, strain rate, Newmark 0.1
RESLT	1	Fri Aug 13 15:01:09 1982	10 elem, strain rate, Newmark 0.1
ECHO	1	Fri Aug 13 15:01:09 1982	10 elem, strain rate, Newmark 0.1
SLOG	1	Fri Aug 13 15:01:09 1982	10 elem, strain rate, Newmark 0.1

NEXT MIPS-EXEC COMMAND : quit

TABLE 2.4.6 - DATA FILE LISTING, CASE 3.

```

ECHD0101 SLOG0101 RSLT0101
star,
gbul
new,main,nonl,cart,0
substructure name = main
refn,12
  1 0.          e+00  0.          e+00  0.          e+00
  2 0.5490000e+00  0.          e+00  0.          e+00
  3 0.1098000e+01  0.          e+00  0.          e+00
  4 0.1647000e+01  0.          e+00  0.          e+00
  5 0.2196000e+01  0.          e+00  0.          e+00
  6 0.2745000e+01  0.          e+00  0.          e+00
  7 0.3294000e+01  0.          e+00  0.          e+00
  8 0.3843000e+01  0.          e+00  0.          e+00
  9 0.4229000e+01  0.          e+00  0.          e+00
 10 0.4614500e+01  0.          e+00  0.          e+00
 11 0.5000000e+01  0.          e+00  0.          e+00
9999
boun,12
  1 111111
  2 1110
  3 1110
  4 1110
  5 1110
  6 1110
  7 1110
  8 1110
  9 1110
 10 1110
 11 101111
9999 111111
enod,0
matl,2,64
0.200000000e+010.499999970e-010.          e+000.          e+000.          e+00
0.          e+000.199999996e-010.199999996e-010.203099990e+010.229000002e+00
0.149999997e-010.148999998e-010.156000003e+000.188999996e+000.201000005e+00
0.500000000e+030.203099990e+010.229000002e+000.149999997e-010.148999998e-01
0.156000003e+000.188999996e+000.201000005e+000.500000000e+030.203099990e+01
0.229000002e+000.149999997e-010.148999998e-010.156000003e+000.188999996e+00
0.201000005e+000.          e+000.156000000e+040.114200001e+020.114099998e+02
0.113999996e+020.607499981e+010.617000008e+010.663399982e+010.499999970e-01
0.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.144800006e-040.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+00
0.200000000e+010.499999970e-010.          e+000.          e+000.          e+00
0.          e+000.199999996e-010.199999996e-010.203099990e+010.229000002e+00
0.149999997e-010.148999998e-010.156000003e+000.188999996e+000.201000005e+00
0.500000000e+030.203099990e+010.229000002e+000.149999997e-010.148999998e-01
0.156000003e+000.188999996e+000.201000005e+000.500000000e+030.203099990e+01
0.229000002e+000.149999997e-010.148999998e-010.156000003e+000.188999996e+00
0.201000005e+000.          e+000.156000000e+040.114200001e+020.114099998e+02
0.113999996e+020.607499981e+010.617000008e+010.663399982e+010.499999970e-01
0.300000000e+010.102700000e+040.385200000e+050.260700000e+070.116900005e+00
0.420599997e+000.293700004e+010.144800006e-040.          e+000.          e+00

```

Table 2.4.6 (cont'd)

```

0.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+00
elem,1
  1  10  1
  1  0  0  0  1  2  2  1  1  1.00  1  0  1
0.          e+000.1000000000e+010.          e+000.          e+000.          e+00
0.          e+00
  2  0  0  0  2  3  2  1  1  1  0  1
0.549000025e+000.1000000000e+010.          e+000.          e+000.          e+00
0.          e+00
  3  0  0  0  3  4  2  1  1  1  0  1
0.109800005e+010.1000000000e+010.          e+000.          e+000.          e+00
0.          e+00
  4  0  0  0  4  5  2  1  1  1  0  1
0.164699996e+010.1000000000e+010.          e+000.          e+000.          e+00
0.          e+00
  5  0  0  0  5  6  2  1  1  1  0  1
0.219600010e+010.1000000000e+010.          e+000.          e+000.          e+00
0.          e+00
  6  0  0  0  6  7  2  1  1  1  0  1
0.274500012e+010.1000000000e+010.          e+000.          e+000.          e+00
0.          e+00
  7  0  0  0  7  8  2  1  1  1  0  1
0.329399991e+010.1000000000e+010.          e+000.          e+000.          e+00
0.          e+00
  8  0  0  0  8  9  2  1  1  1  0  1
0.384299994e+010.1000000000e+010.          e+000.          e+000.          e+00
0.          e+00
  9  0  0  0  9  10  2  1  1  1  0  1
0.422900009e+010.1000000000e+010.          e+000.          e+000.          e+00
0.          e+00
  10 0  0  0  10 11  2  1  1  1  0  1
0.461450005e+010.1000000000e+010.          e+000.          e+000.          e+00
0.          e+00

nord,opto
prof
end
fini
mode
tree,main
fini
mbui
new,main
pmas,13
  10 0.51755e-08 0.51755e-08 0.51755e-08 0.          e+00 C.          e+00 D.          e+0000
  20 0.10351e-07 0.10351e-07 0.10351e-07 0.          e+00 C.          e+00 D.          e+0000
  30 0.10351e-07 0.10351e-07 0.10351e-07 0.          e+00 C.          e+00 D.          e+0000
  40 0.10351e-07 0.10351e-07 0.10351e-07 0.          e+00 C.          e+00 D.          e+0000
  50 0.10351e-07 0.10351e-07 0.10351e-07 0.          e+00 C.          e+00 D.          e+0000
  60 0.10351e-07 0.10351e-07 0.10351e-07 0.          e+00 C.          e+00 D.          e+0000
  70 0.10351e-07 0.10351e-07 0.10351e-07 0.          e+00 C.          e+00 D.          e+0000
  80 0.88143e-08 0.88143e-08 0.88143e-08 0.          e+00 C.          e+00 D.          e+0000
  90 0.36389e-08 0.36389e-08 0.36389e-08 0.          e+00 C.          e+00 D.          e+0000
  90 0.36341e-08 0.36341e-08 0.36341e-08 0.          e+00 C.          e+00 D.          e+0000

```


Table 2.4.6 (cont'd)

```

100 0.72683e-08 0.72683e-08 0.72683e-08 0. e+00 0. e+00 0. e+0000
110 0.36341e-08 0.36341e-08 0.36341e-08 0. e+00 0. e+00 0. e+0000
110 0. e+00 0. e+00 0. e+00 0. e+00 0. e+0000
end
fini
ptre
newr, recl, pair, 2, 100
(2e15.7)
0. e+00 0. e+00
0. e+00 0.1000000e+02
fini
thou, 249
2 110 3 1 0 0
ndyn
velo, 1, 1
main 11
1 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00
2 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00
3 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00
4 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00
5 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00
6 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00
7 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00
8 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00 0. e+00
9 0. e+00-0.50200e+04 0. e+00 0. e+00 0. e+00 0. e+00
10 0. e+00-0.50200e+04 0. e+00 0. e+00 0. e+00 0. e+00
11 0. e+00-0.50200e+04 0. e+00 0. e+00 0. e+00 0. e+00
mass
dylo, 1, 1
recl 2 0. 1.000 1
1
time, rslt, 1, 0.1000e+01
auto, defl
inte, newm, 0.2000e-05, 0.e+00, 0.e+00, 0.1000e+00
stif
stif, upda
kinr, 12
elmr, 1, 2, 6, 3
kinr, 5
loop, 200
zero, ltme
step
unba
auto, linit
loop, 20
stif
auto, load
load
disp
kinr, 10
elmr, 9, 10
auto, nerr, 0.1000e+00, 0.5000e+00
lf, 3, 3, 1, 1
entr, 1
auto, fact
kinr, 1

```

Table 2.4.6 (cont'd)

```
if,3,2,2,3
entr,2
elwr,1
cont
goto,0
entr,3
auto,step,0.1000e-05,0.1000e-03,0.5000e+00,0.2000e+01
if,4,5,5,4
entr,4
inte,newm,,auto,0.e+00,0.e+00,0.e+00,0.1000e+00
entr,5
if,3,6,6,7
entr,6
kinr,12
elwr,5,2,t
kinr,5
stif,init
goto,8
entr,7
chou
elwr,1,2,4,6,11
kinr,4,9,11
wrou
zero,1rsb
unbs,chech,stop,0.5000e+00,0.1000e+02
if,3,3,9,9
entr,9
summ
elwr,3
kinr,3
stif,upda
auto,exit,0.1500e-02
if,5,8,8,0
entr,8
cont
fini
stop
```

D2.5 IMPULSIVELY LOADED RING

D2.5.1 PURPOSE

This example tests the BEAM and SHELL elements, by comparison with test results and previously reported analysis results. Large displacement and strain rate effects are considered, and the initial velocity loading option is tested.

D2.5.2 DESCRIPTION

Tests and analyses of a free ring under impulse (explosive) loading have been reported by Witmer et al [2.5.1]. Analyses of the same ring have been reported by Hibbitt and Karlsson [2.5.2].

The dimensions of the ring are shown in Fig. 2.5.1. Initial velocities as shown were produced by an explosive charge.

The beam was made of 6061-T6 aluminum alloy. The static Young's modulus reported in [2.5.2] was 10500 ksi (7.239×10^{10} N/m²). For analysis, a bilinear stress-strain relationship was assumed in [2.5.2], with a yield stress of 42.8 ksi (2.951×10^8 N/m²) and a strain hardening modulus of 78.7 ksi (5.426×10^8 N/m²). These values were used for the WIPS analysis.

For the analyses in both [2.5.1] and [2.5.2], high strain rates were assumed to increase the yield stress according to the equation:

$$\sigma_y - \sigma_o = \sigma_o (|\dot{\epsilon}|/6500)^{0.25} \quad (2.5.1)$$

in which $\dot{\epsilon}$ = extensional strain rate; σ_o = static yield stress; and σ_y = dynamic yield stress. The trilinear approximation used for the WIPS analysis is shown in Table 2.5.1.

WIPS analyses were performed as follows:

- (1) Eighteen BEAM elements in half ring, no strain rate effect.
- (2) Eighteen BEAM elements in half ring, with strain rate effect.
- (3) Eighteen SHELL elements in half ring, no strain rate effect, 5 integration points through thickness.
- (4) Eighteen SHELL elements in half ring, with strain rate effect, 5 integration points through thickness.

D2.5.3 WIPS ANALYSIS MODEL

D2.5.3.1 Geometry and Loading

The nodes and initial velocities for the BEAM model are shown in Fig. 2.5.1. The geometry and velocities for the SHELL model were essentially the same, but more nodes are needed to define the shell model (4 nodes, 2 each on the middle and outer surfaces, at each nodal cross section).

Only motion in the XY plane was permitted for the BEAM model, and only one-half of the ring was analyzed. Symmetry was similarly considered for the shell model. The geometry of the BEAM model was generated using the WIPS input modules. However, the geometry for the SHELL model could not be generated in this way, and it was necessary to set up the DATA file by hand.

D2.5.3.2 BEAM Element Properties

For the assumed elastic-strain-hardening material, force-extension and moment-curvature relationships were calculated for the BEAM element cross section. The force-extension relationship has the same shape as the stress-strain curve, whereas the moment-curvature

relationship is curvilinear. The two relationships were approximated using four linear segments each, as shown in Tables 2.5.2 and 2.5.3.

The procedure for determining strain rate properties for BEAM elements is described in the Theory Manual, Section B4.4.2. With this procedure and the dashpot stiffnesses shown in Table 2.5.1, the dimensionless properties shown in Table 2.5.4 were calculated.

D2.5.3.3 SHELL Element Properties

The shell material was specified to be bilinear, as indicated in Section D2.5.2, with strain rate effects as in Table 2.5.1. Five Gauss quadrature points were specified through the thickness in each element.

D2.5.3.4 Analysis Control Parameters

The Newmark solution scheme was used, with the following parameters.

Initial time step = 2×10^{-6} sec.

Minimum time step = 1×10^{-6} sec.

Maximum time step = 1×10^{-4} sec.

Initial $\beta/\Delta t$ = 0.1

Lower midstep tolerance = 0.5 k

Lower midstep tolerance = 2.5 k

D2.5.3.5 WIPS Input

Table 2.5.5 contains the WIPSLOG listing up to the WIPS-DATA phase for the BEAM model with strain rate effects. Table 2.5.6 is a listing of the DATA file for the corresponding analysis. Table 2.5.7 is a listing of the DATA file for the SHELL model with strain rate effects. The WIPSLOG and DATA file listings for the cases with no strain rate were similar.

The initial velocities for the BEAM model were not specified in the WIPS-MODL phase but instead were added by editing the DATA file. This was simpler than using the WIPS-MODL velocity option.

D2.5.4 RESULTS

D2.5.4.1 BEAM Model

For the BEAM model, Fig. 2.5.2 shows the variation with time of the computed diameter change for the first 2 milliseconds of response, plus analytical and experimental results as reported in [2.5.2].

Figure 2.5.3 shows the undeformed configuration and the computed deformed shapes at two different times, for the cases with and without strain rate effects (the shapes were drawn using WIPS-RSLT, then cut and pasted together). Analytical and experimental deformed shapes at similar times have been reported in [2.5.2]. Table 2.5.8 shows the value of a key parameter for the deformed shapes, namely the ratio of vertical to horizontal diameter.

Figure 2.5.3 and Table 2.5.8 indicate that when strain rate effects are included, the WIPS analysis and the analysis reported in [2.5.2] agree well with the experimental results up to the time of maximum diameter change at approximately 1.4 milliseconds. Beyond that time the WIPS analysis predicts a slower rate of diameter increase (i.e., a less rapid rebound) than either the experiment or the analysis of [2.5.2].

D2.5.4.2 SHELL Model

For the SHELL model, Fig. 2.5.4 shows the WIPS results for the first 2 milliseconds of response, plus analytical and experimental results as reported in [2.5.2]. The analysis in [2.5.2] used a beam type of model, with monitoring of stress-strain behavior at seven points through

the beam depth. This model is closer to the WIPS SHELL model than to the BEAM model. Table 2.5.9 compares the ratio of vertical to horizontal diameter for the analytical and experimental deformed shapes.

Figure 2.5.4 shows that the WIPS analysis including strain rate effects follows the experimental results closely up to approximately 1.1 milliseconds. Beyond that time, however, the WIPS analysis predicts much more rapid rebound than was observed in the experiment.

Figure 2.5.4 and Table 2.5.9 again show that when strain rate effects are ignored the analytical and experimental results differ substantially. In contrast with the BEAM model, however, the WIPS analysis results are in quite close agreement with the analysis results from [2.5.2].

D2.5.5 CONCLUSION

When strain rate effects are considered, the BEAM and SHELL models gave similar results up to a time of 1.1 milliseconds, and predicted maximum diameter changes which were close to those observed in the experiment. Beyond this, however, the results for this example are not encouraging, for the following reasons.

- (1) The magnitude of the strain rate effect was much larger for the SHELL model than for the BEAM model.
- (2) The SHELL model with strain rate effects showed a much more rapid rebound than was observed in the experiment and computed in the analysis of [2.5.2].

For the BEAM element, this example involves much higher strain rates and much larger deformations than will be present in typical pipe whip analyses. Because of this, it does not follow that the BEAM element is unsatisfactory for pipe whip analyses. The results do, however, suggest that before it is used for production analysis the BEAM element should be tested on additional examples which are more typical of pipe whip configurations.

For the SHELL element, the strain rates are still higher than would be expected in pipe whip applications, but are not completely unreasonable. This is because the SHELL element is intended primarily for analysis of pipe-to-pipe and pipe-to-wall impact. In such cases the impact velocity could approach the order of magnitude of the initial velocity in this example. The behavior of the SHELL element should thus be investigated in more detail before production impact analyses are performed.

It should be noted that analyses of shells with impact, large displacements, inelastic behavior and strain rate dependence are extremely complex by any standards. Any analytical studies of pipe-to-pipe or pipe-to-wall impact will be very expensive and will require very careful study to ensure that correct results are obtained. A part of such study should involve more detailed checking of the SHELL element.

D2.5.6 REFERENCES

- 2.5.1 Witmer, E. A., Balmer, H. A., Leech, J. W., and Pian, T.H.H., "Large Dynamic Deformations of Beams, Rings, Plates, and Shells," *AIAA Journal*, Vol. 1, No. 8, pp. 1848-1857, 1963.
- 2.5.2 Hibbitt and Karlsson, "Analysis of Pipe Whip," Report No. EPRI NP-1208, Electric Power Research Institute, 1979.

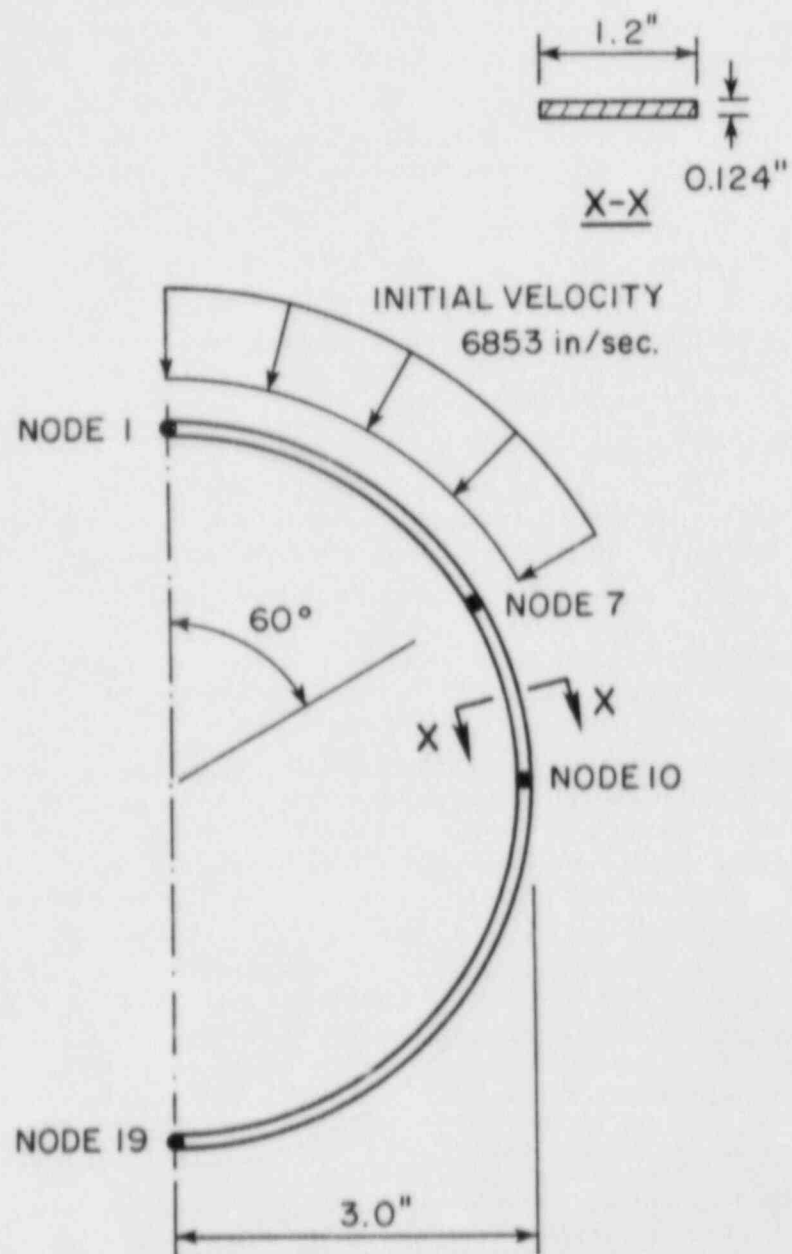


FIG. 2.5.1 RING WITH IMPULSIVE LOADING, DIMENSIONS AND INITIAL VELOCITY.

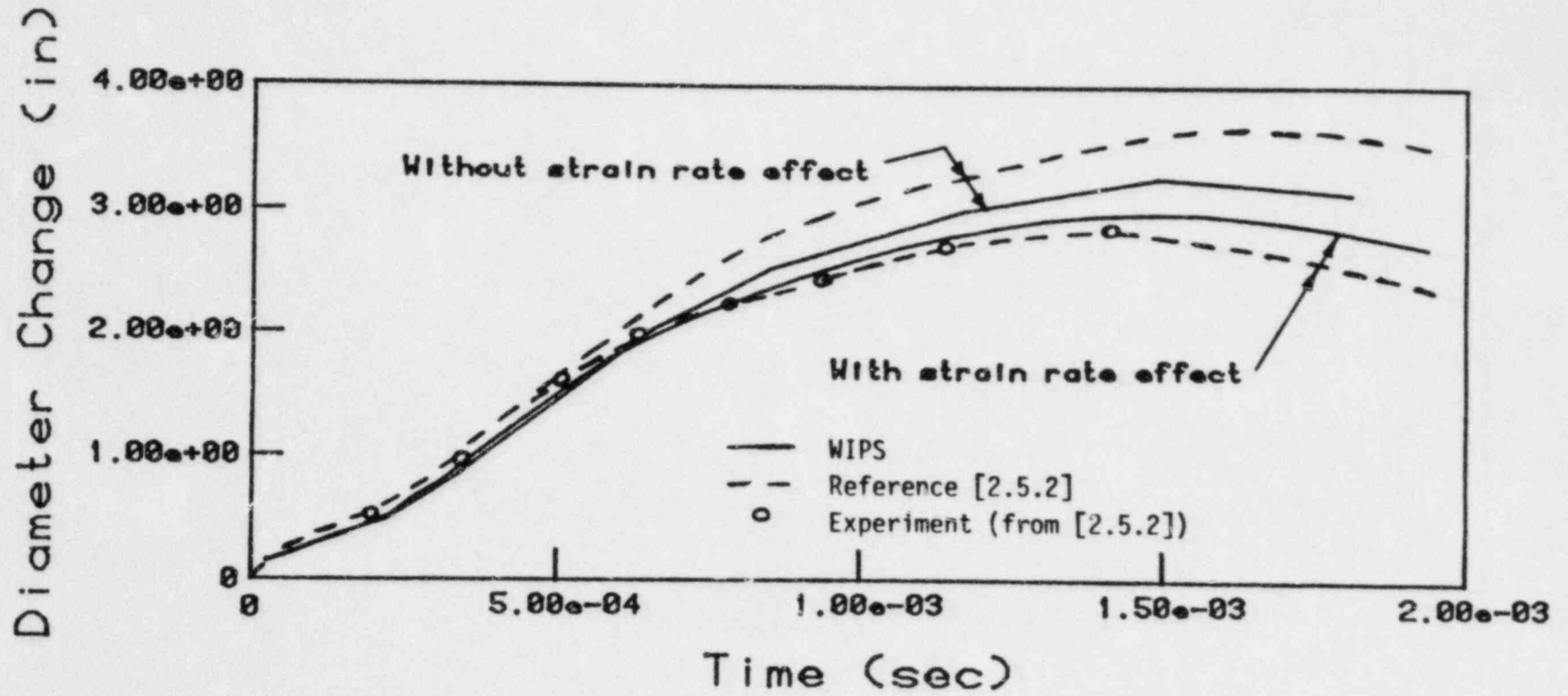


FIG. 2.5.2 CHANGE IN VERTICAL DIAMETER. BEAM MODEL.

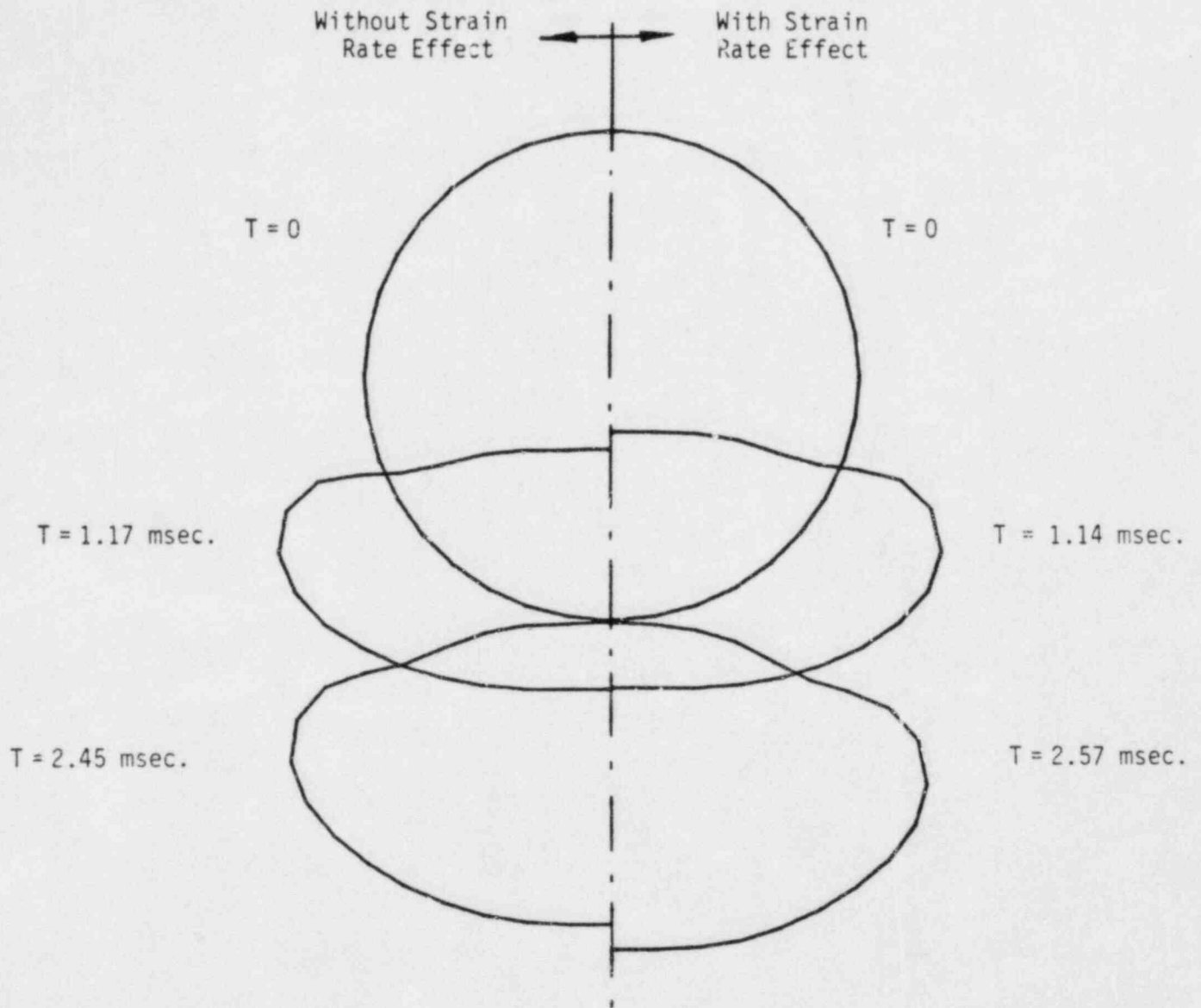


FIG. 2.5.3 DEFORMED SHAPES. BEAM MODEL.

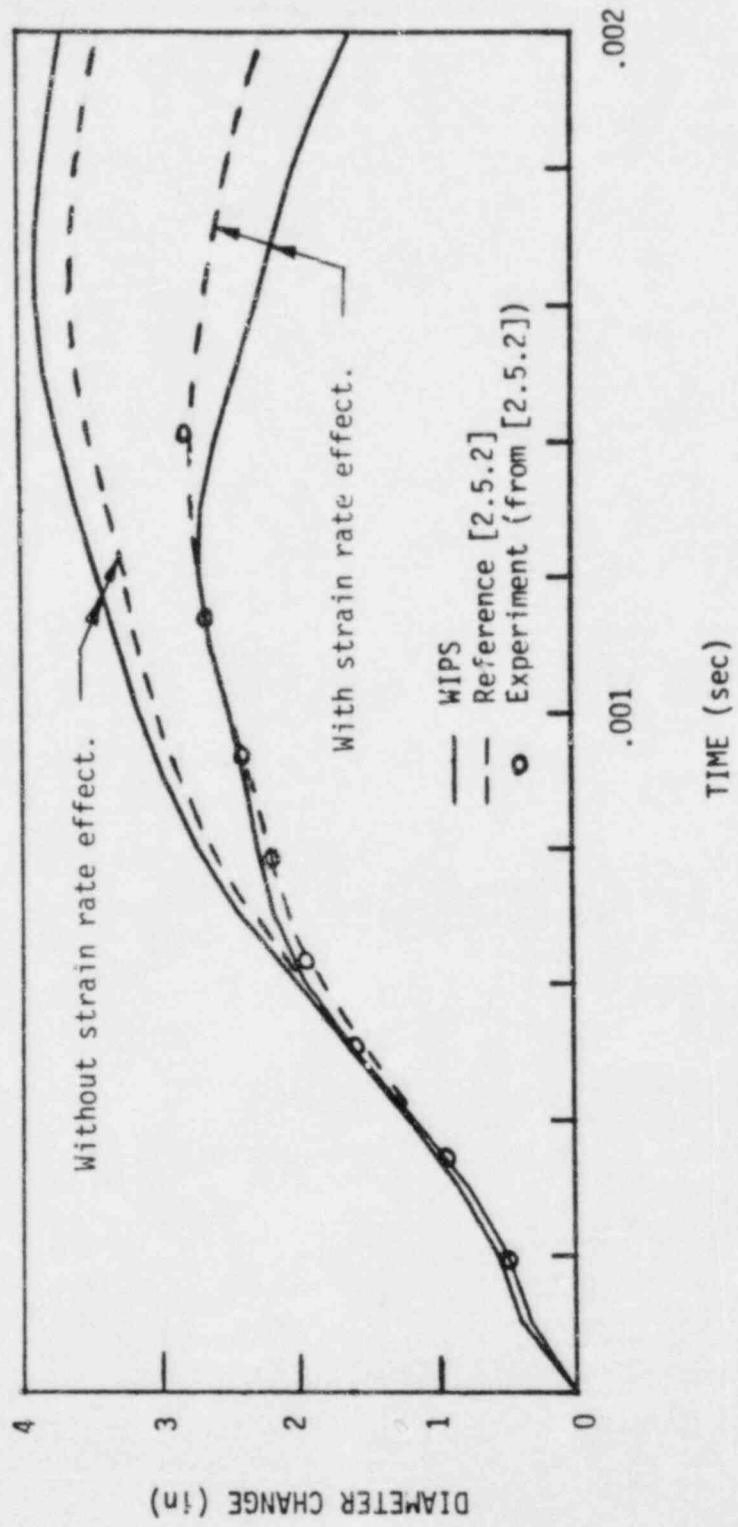


FIG. 2.5.4 CHANGE IN VERTICAL DIAMETER. SHELL MODEL.

TABLE 2.5.1 - TRILINEAR APPROXIMATION FOR STRAIN RATE EFFECT		
Stress Increase (ksi)	Strain Rate (sec ⁻¹)	Dashpot Stiffness (k.sec/in ²)
0	0	2.0
8	4	0.0685
18	150	0.0108

TABLE 2.5.2 - STATIC FORCE-EXTENSION RELATIONSHIP FOR BEAM ELEMENT		
Force (k)	Axial Strain	Stiffness (k)
0	0	1560.00
6.420	0.00412	11.81
6.503	0.01121	11.80
6.987	0.05226	11.79

TABLE 2.5.3 - STATIC MOMENT-CURVATURE RELATIONSHIP FOR BEAM ELEMENT		
Moment (k.in)	Curvature (in ⁻¹)	Stiffness (k.in ²)
0	0	2.0310
0.165	0.0812	0.2500
0.200	0.2212	0.0156
0.2125	1.0225	0.0155

TABLE 2.5.4 - DIMENSIONLESS STRAIN RATE RELATIONSHIP FOR BEAM ELEMENT	
Strength Increase Factor	Deformation Rate Factor
0	0
0.1869	972
0.4206	36450
2.9370	2.466 × 10 ⁶

TABLE 2.5.5 - WIPSLOG LISTING. ALL PHASES.

```
EXEC - WIPS EXECUTIVE
Creating problem no. 1
Problem description: Ring with Initial Velocity.

NEXT WIPS-EXEC COMMAND : geom

GEOM - SPECIFICATION OF SYSTEM GEOMETRY

Define units
Length (ft,in,m,mm) : in
Force (k,lb,kgf,kN) : k

Specify new GEOM data

SIAXI RING 4J. 1
Enter c.p. data in sequence along run

c.p. name and type : a
coord option : di
x,y,z : -1 2.9375
Any changes? :

c.p. name and type : 1
no. of extra nodes :
coord option : tn
*** error - this option can be used only with tn points
coord option :
c.p., dx,dy,dz :
offset point defaults to preceding c.p.
Any changes? : y
reenter data for this c.p.

c.p. name and type : 1 tn
no. of extra nodes :
coord option : tn
tn generated automatically
Any changes? :

c.p. name and type : t1 t1
bend radius : 2.9375
coord option : di
x,y,z : 2.9375 2.9375
Any changes? :

c.p. name and type : 10 tn
no. of extra nodes : 9
coord option : tn
tn generated automatically
Any changes? :

c.p. name and type : t2 t1
bend radius : 2.9375
coord option : di
x,y,z : 2.9375 -2.9375
Any changes? :
```

Table 2.5.5 (cont'd)

c.p. name and type : 19 tn
 no. of extra nodes : 9
 coord option : tn
 tn generated automatically
 Any changes? :

c.p. name and type : b
 no. of extra nodes :
 coord option : di
 x,y,z : -1 -2.9375
 Any changes? :

c.p. name and type :
 Last c.p. in this run? : y
 Display GEUM data for this run? : y

GEUM DATA FJR RUN

run no.	c.p. name	c.p. type	bend radius	xtra nodes	coord opt	c.p. i	c.p. j ?	coordinate x,dx,p	data y,dy	z,dz
1	a			0	di			-1.000	2.938	0.
	i	tn		0	tn			0.	0.	0.
	ti1	ti	2.938	0	di			2.938	2.938	0.
	10	tn		9	tn			0.	0.	0.
	ti2	ti	2.938	0	di			2.938	-2.938	0.
	19	tn		9	tn			0.	0.	0.
	b			0	di			-1.000	-2.938	0.

END OF DATA

START RUN NJ. 2
 Enter c.p. data in sequence along run

c.p. name and type :
 Last run? : y

Display new GEUM data? :
 Write in session log? :

Modify GEUM data? :

Save current GEUM data? : y
 Comment for file catalog :
 GEUM DATA SAVED. FILE NAME = GEUM0101

Produce COUR data? : y

Display COUR data? : y

COUR DATA

run no.	c.p. name	c.p. type	bend radius	node no.	x coord	y ? coord?	z coord
---------	-----------	-----------	-------------	----------	---------	------------	---------

Table 2.5.5 (cont'd)

1	a			1	-1.000	2.938	0.
	l	tn		2	0.	2.938	0.
	ti1	ti	2.938		2.938	2.938	0.
		center			0.	0.	0.
				3	0.510	2.893	0.
				4	1.005	2.760	0.
				5	1.459	2.544	0.
				6	1.888	2.250	0.
				7	2.250	1.888	0.
				8	2.544	1.467	0.
Hit RETURN for more							
				9	2.760	1.005	0.
				10	2.893	0.510	0.
	10	tn		11	2.938	0.	0.
	ti2	ti	2.938		2.938	-2.938	0.
		center			0.	0.	0.
				12	2.893	-0.510	0.
				13	2.760	-1.005	0.
				14	2.544	-1.459	0.
				15	2.250	-1.888	0.
				16	1.888	-2.250	0.
Hit RETURN for more							
				17	1.459	-2.544	0.
				18	1.005	-2.760	0.
				19	0.510	-2.893	0.
	19	tn		20	0.	-2.938	0.
	b			21	-1.000	-2.938	0.

END OF DATA

Plot geometry? :

Modify GEJM data? :

DATA COMPLETE FOR THIS SESSION

Save final GEJM data? : y

Comment for file catalog : Ring, C.p. a-1-19-b, nodes 1-21.

GEJM DATA SAVED. FILE NAME = GEJM0101

Save COUR data? : y

Comment for file catalog : From GEJM0101

COUR DATA SAVED. FILE NAME = COUR0101

End of this GEJM session

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : beam

BEAM - SPECIFICATION OF BEAM PROPERTIES

Define units

Length (ft, in, m, mm) : in

Force (k, lb, kgf, kN) : k

Start new BEAM file

Table 2.5.5 (cont'd)

```

Specify a new property set? : y

Set NO. = 1
Property set description : 1.290.125, 40.5ksi, no strain rate.

Yield surface type (1-4) (dfit=1) : 2
Weight per unit length : 1.448e-5

Elastic stiffnesses
  EA,GAY,GAZ : 1560 500 500
  GJX,Ely,Elz : 2.031 2.031 2.031
Strengths at first yield
  Fx,Mxx,Myy,Mzz : 6.075 .156 .156 .156
Stiffnesses after first yield
  EA,GJX,Ely,Elz : 11.42 .229 .229 .229
Strengths at second yield
  Fx,Mxx,Myy,Mzz : 6.17 .189 .189 .189
Stiffnesses after second yield
  EA,GJX,Ely,Elz : 11.41 .0149 .0149 .0149
Strengths at third yield
  Fx,Mxx,Myy,Mzz : 6.634 .201 .201 .201
Stiffnesses after third yield
  EA,GJX,Ely,Elz : 11.4 .01485 .01485 .01485
Strain rate factors (0-3, dfit=none) :
No strain rate effect
Use default tolerances? : y

Any errors? :

This set added to BEAM file

Specify a new property set? : y

Set NO. = 2
Property set description : 1.290.125, 40.5ksi, with strain rate.

Yield surface type (1-4) (dfit=1) : 2
Weight per unit length : 1.448e-5

Elastic stiffnesses
  EA,GAY,GAZ : 1560 500 500
  GJX,Ely,Elz : 2.031 2.031 2.031
Strengths at first yield
  Fx,Mxx,Myy,Mzz : 6.075 .156 .156 .156
Stiffnesses after first yield
  EA,GJX,Ely,Elz : 11.42 .229 .229 .229
Strengths at second yield
  Fx,Mxx,Myy,Mzz : 6.17 .189 .189 .189
Stiffnesses after second yield
  EA,GJX,Ely,Elz : 11.41 .0149 .0149 .0149
Strengths at third yield
  Fx,Mxx,Myy,Mzz : 6.634 .201 .201 .201
Stiffnesses after third yield
  EA,GJX,Ely,Elz : 11.4 .01485 .01485 .01485
Strain rate factors (0-3, dfit=none) : 1027 38520 2.607e6

```


Table 2.5.5 (cont'd)

Corresponding strength factors : .1869 .4205 2.937
 Use default tolerances? : y

Any errors? :

This set added to BEAM file

Specify a new property set? :

No. of property sets in BEAM file = 2

Display property set descriptions? : y

BEAM PROPERTY DESCRIPTIONS

Set No.	Description
1	1.2e0.125, 40.ksi, no strain rate.
2	1.2e0.125, 40.ksi, with strain rate.

Display new property set data? : y

BEAM PROPERTY DATA

SET NO. 1. 1.2e0.125, 40.ksi, no strain rate.

Data type	Data 1	Data 2	Data 3	Data 4
Unit weight	0.1448e-04			
Elastic EAx,GAy,GAz	0.1550e+04	0.5000e+03	0.5000e+03	
GJx,Ely,EIz	0.2031e+01	0.2031e+01	0.2031e+01	
First yield				
Fx,Mxx,Myy,Mzz	0.5075e+01	0.1560e+00	0.1560e+00	0.1560e+00
EA,GJx,Ely,EIz	0.1142e+02	0.2290e+00	0.2290e+00	0.2290e+00
Second yield				
Fx,Mxx,Myy,Mzz	0.5170e+01	0.1890e+00	0.1890e+00	0.1890e+00
EA,GJx,Ely,EIz	0.1141e+02	0.1490e-01	0.1490e-01	0.1490e-01
Third yield				
Fx,Mxx,Myy,Mzz	0.5534e+01	0.2010e+00	0.2010e+00	0.2010e+00
EA,GJx,Ely,EIz	0.1140e+02	0.1485e-01	0.1485e-01	0.1485e-01
Stiffness tolerance	0.5000e-01			
Yield tolerance	0.2000e-01			
Unloading tolerance	0.2000e-01			

Hit RETURN for next set

SET NO. 2. 1.2e0.125, 40.ksi, with strain rate.

Data type	Data 1	Data 2	Data 3	Data 4
Unit weight	0.1448e-04			
Elastic EAx,GAy,GAz	0.1550e+04	0.5000e+03	0.5000e+03	
GJx,Ely,EIz	0.2031e+01	0.2031e+01	0.2031e+01	
First yield				
Fx,Mxx,Myy,Mzz	0.5075e+01	0.1560e+00	0.1560e+00	0.1560e+00
EA,GJx,Ely,EIz	0.1142e+02	0.2290e+00	0.2290e+00	0.2290e+00
Second yield				
Fx,Mxx,Myy,Mzz	0.5170e+01	0.1890e+00	0.1890e+00	0.1890e+00
EA,GJx,Ely,EIz	0.1141e+02	0.1490e-01	0.1490e-01	0.1490e-01

Table 2.5.5 (cont'd)

```

Inhd yield
  Fx,Mxx,Myy,Mzz  0.6534e+01 0.2010e+00 0.2010e+00 0.2010e+00
  EA,GJx,Ely,Elz  0.1110e+02 0.1485e-01 0.1485e-01 0.1485e-01
Strain rate factors  0.1027e+04 0.3832e+05 0.2607e+07
Strength factors    0.1359e+00 0.4206e+00 0.2937e+01
Stiffness tolerance 0.5000e-01
Yield tolerance     0.2000e-01
Unloading tolerance 0.2000e-01
Str. rate tolerance 0.5000e-01
Hit RETURN for next set
END OF DATA

```

```

Display all property set data? :
Write in session log? :

```

```

New BEAM file created
Comment for file catalog : 2 sets

```

```

End this BEAM session? : y

```

```

EXEC - WIPS EXECUTIVE

```

```

NEXT WIPS-EXEC COMMAND : frec

```

```

FREC - SPECIFY DYNAMIC FORCE RECORDS

```

```

Define units
  Length (ft,in,m,mm) : in
  Force (k,lb,kgf,kN) : k

```

```

Start new FREC file

```

```

Specify a new record? : y

```

```

RECORD NO. 1

```

```

Record name (4 characters) : rec1
Description (max. 40 char.) : Junny zero record

```

```

Enter Time-Force pairs
First pair automatically set to 0,0

```

```

  Pair no. 2 : 10 0.
  Pair no. 3 :

```

```

Last pair? : y
Any errors? :

```

```

Specify a new record? :

```

```

Display any records? : y
Record number (dfmt=all) :

```

```

RECORD NO. 1. Name = rec1
  Time      Force
  0.         0.     e+00
  10.00000  0.     e+00
END OF RECORD

```


Table 2.5.5 (cont'd)

```

write records in session log? :

End this EXEC session? : y
New EXEC file created
Comment for file catalog : 1 record

NOTE: BOUNDARY CONDITION ERRORS WERE MADE IN THE FIRST MJDL
      AND DATA RUNS. THE CORRESPONDING PART OF THE WIPSLJG
      FILE HAS BEEN REMOVED.

EXEC - WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : modl

MJDL - SPECIFICATION OF ANALYSIS MODEL

Define units
  Length (ft,in,m,mm) : in
  Force (k,lb,kgf,kN) : k

Sequence no. of CUOK file : 1

Available element property sets
  Type      No. of Sets
  beam      2
Available substructure property sets
  None

DEFINE MODEL IN SEGMENTS

SEGMENT NO.  1

Pipe run no. : 1
First c.p. of segment : 1
Full 3D motion? :
Displacement plane (xy,yz or zx) : xy
Any substructures in this segment? :
Boundary condition code for first c.p. : 101111

Specify c.p.name + elem type + optional data
1: 19 beam pr=1 ld=y th=no
2: 19 zero bc=101111
3:

End of segment? : y
Display commands for this segment? : y

MJDL COMMAND TABLE

SEGMENT NO.  1.  Run No. =  1
  c.p.  elem  optn  data      optn  data      optn  data
  1
  19   beam      bcon  101111
      prop      1

```

Table 2.5.5 (cont'd)

```

          locl      +
          wfac      1.000
19      zero
          bcon      101111
Any changes? :
SEGMENT NU.  2
Pipe run no. :
Last segment? : y
Any external substructures? :
Display commands for all segments? :
Write in session log? :
Produce MUDL file? : y
Wait while data is processed
Specify initial velocities? :
Comment for file catalog : No strain rate. Velocities to be added.
MUDL file saved. File name = MUDL0102
End of this MUDL session

EXEC - WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : modl

MUDL - SPECIFICATION OF ANALYSIS MODEL
Define units
  Length (ft,in,m,mm) : in
  Force (k,lb,kgf,kN) : k
Sequence no. of COOR file : 1
Available element property sets
  Type      No. of Sets
  beam      2
Available substructure property sets
  None

DEFINE MODEL IN SEGMENTS
SEGMENT NU.  1
Pipe run no. : 1
First c.p. of segment : 1
Full 3D motion? :
Displacement plane (xy,yz or zx) : xy
Any substructures in this segment? :
Boundary condition code for first c.p. : 101111
Specify c.p.name + elem type + optional data

```

Table 2.5.5 (cont'd)

```

1: 19 beam pr=2 ld=y th=no
2: 19 zero bc=101111
3:
End of segment? : y
Display commands for this segment? : y

MUJL COMMAND TABLE

SEGMENT NU. 1. Run No. = 1
c.o. elem optn data optn data optn data
1
19 beam bcon 101111
prop 2
lcl + ldis yes this no
wfac 1.000
19 zero bcon 101111
Any changes? :

SEGMENT NU. 2

Pipe run no. :
Last segment? : y

Any external substructures? :

Display commands for all segments? :
Write in session log? :

Produce MUJL file? : y
Wait while data is processed

Specify initial velocities? :
Comment for file catalog : 4th strain rate. Velocities to be added.

MUJL file saved. File name = MUJL0103
End of this MUJL session

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : data

DATA - SET JP WIPS-ANAL INPJT DATA

Define units
Length (ft,in,m,mm) : in
Force (k,lb,kgf,kN) : k

Sequence no. of MUJL file : 2

Problem description (4 lines)
Line 1 : Ring with Initial Velocity. No strain rate. GHP 12/82.
Line 2 :
Line 3 :

```

Table 2.5.5 (cont'd)

```
Line 4 :

Set up PAUSE files at end of analysis ? :
Wait while files are processed

Specify data for each loaded point
LJAU NU. 1
  Force record name : recl
  Name of loaded c.p. : 1
  Force direction (x,y,z or follower) : y
  Scale factor (+,- controls direction) : 1
  Line delay (sec) (dfit=0) :
LJAU NU. 2
  Force record name :
Last load? : y

Time steps : initial + max + min : 2e-6 1e-4 1e-6
Max steps + max total time : 2000 2.9e-3
Error tolerances : upper + lower : .5 .1

Results output intervals
  Max. no. of steps : 10
  Max. time (secs.) : 1
Integration scheme (newn or hilb)(dfit=newn) :
Damping factor (dfit=0.1) :
Factor for time step increase (dfit=2.0) :
Factor for time step decrease (dfit=0.5) :
Max. unbal. to reduce time step (dfit=no limit) :
Max. unbal. to stop analysis (dfit=no limit) :

DATA file set complete
Comment for file catalog : No strain rate.
WIPS-ANAL DATA FILES SET UP. PARENT FILE NAME = DATA0102

EXEC = WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : data

DATA = SET UP WIPS-ANAL INPUT DATA

Define units
  Length (ft,in,m,mm) : in
  Force (k,lb,kgf,kN) : k

Sequence no. of MUOL file : 3

Problem description (4 lines)
Line 1 : Ring with Initial Velocity, With Strain Rate.          GHP 12/82
Line 2 :
Line 3 :
Line 4 :

Set up PAUSE files at end of analysis ? :
Wait while files are processed
```

Table 2.5.5 (cont'd)

```
Specify data for each loaded point
LJAU NU. 1
  Force record name : rec1
  Name of loaded c.p. : 1
  Force direction (x,y,z or follower) : y
  Scale factor (+,- controls direction) : 1
  Line delay (sec) (dfit=0) :
LJAU NU. 2
  Force record name :
Last load? : y

Time steps : initial + max + min : 2e-6 1e-4 1e-6
Max steps + max total time : 2000 2.9e-3
Error tolerances : upper + lower : .5 .1

Results output intervals
  Max. no. of steps : 10
  Max. time (secs.) : 1
Integration scheme (newn or hilb)(dfit=newn) :
Damping factor (dfit=0.1) :
Factor for time step increase (dfit=2.0) :
Factor for time step decrease (dfit=0.5) :
Max. unbal. to reduce time step (dfit=no limit) :
Max. unbal. to stop analysis (dfit=no limit) :

DATA file set complete
Comment for file catalog : with strain rate.
WIPS-ANAL DATA FILES SET UP. PARENT FILE NAME = DATA0103

EX=L - WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : quit
```

NOTE: THE INPUT DATA TO THIS POINT DOES NOT CONTAIN INITIAL VELOCITIES. THESE WERE ADDED "BY HAND" USING THE UNIX EDITOR.

TABLE 2.5.6 - DATA FILE LISTING. BEAM MODEL WITH STRAIN RATE EFFECTS.

```

ECHJ0103 SLUG0103 RSLT0103
star,
gbui
new,main,nonl,cart,0
substructure name = main
refn,20
  2 0. e+00 0.2937500e+01 0. e+00
  3 0.5100914e+00 0.2892873e+01 0. e+00
  4 0.1004684e+01 0.2750347e+01 0. e+00
  5 0.1464750e+01 0.2543750e+01 0. e+00
  6 0.1888188e+01 0.2250255e+01 0. e+00
  7 0.2250256e+01 0.1888189e+01 0. e+00
  8 0.2543750e+01 0.1464750e+01 0. e+00
  9 0.2750347e+01 0.1004684e+01 0. e+00
 10 0.2892873e+01 0.5100913e+00 0. e+00
 11 0.2937500e+01 0. e+00 0. e+00
 12 0.2892873e+01 -0.5100914e+00 0. e+00
 13 0.2750347e+01 -0.1004684e+01 0. e+00
 14 0.2543750e+01 -0.1464750e+01 0. e+00
 15 0.2250255e+01 -0.1888188e+01 0. e+00
 16 0.1888189e+01 -0.2250256e+01 0. e+00
 17 0.1464750e+01 -0.2543750e+01 0. e+00
 18 0.1004684e+01 -0.2750347e+01 0. e+00
 19 0.5100913e+00 -0.2892873e+01 0. e+00
 20 0. e+00 -0.2937500e+01 0. e+00
9999
bound,20
  2 101111
  3 1110
  4 1110
  5 1110
  6 1110
  7 1110
  8 1110
  9 1110
 10 1110
 11 1110
 12 1110
 13 1110
 14 1110
 15 1110
 16 1110
 17 1110
 18 1110
 19 1110
 20 101111
9999 111111
encl,0
mat1,2,64
0.20000000e+010.499999970e-010. e+000. e+000. e+00
0. e+000.199999996e-010.199999996e-010.203099990e+010.229000002e+00
0.148999999e-010.148479999e-010.156000003e+000.188999996e+000.201000005e+00
0.50000000e+030.203099990e+010.229000002e+000.148999993e-010.148479999e-01
0.156000003e+000.188999996e+000.201000005e+000.50000000e+030.203099990e+01
0.229000002e+000.148999998e-010.148479999e-010.156000003e+000.188999996e+00
0.201000005e+000. e+000.156000003e+040.114200001e+020.114099998e+02

```

Table 2.5.6 (cont'd)

0.	0.113774995e+020.	607479991e+010.	617000005e+010.	663399982e+010.	479999970e-01
0.	e+000.	e+000.	e+000.	e+000.	e+00
0.	e+000.	e+000.	144800003e-040.	e+000.	e+00
0.	e+000.	e+000.	e+000.	e+000.	e+00
0.	e+000.	e+000.	e+000.	e+000.	e+00
0.	e+000.	e+000.	e+000.	e+000.	e+00
0.	200000000e+010.	499999970e-010.	e+000.	e+000.	e+00
0.	e+000.	199999996e-010.	199999976e-010.	203079970e+010.	229000002e+00
0.	148999999e-010.	148479999e-010.	156070003e+000.	188999995e+000.	201000005e+00
0.	300000000e+030.	203099970e+010.	229000002e+000.	148999993e-010.	148479999e-01
0.	156000000e+000.	188999996e+000.	201000005e+000.	500000000e+030.	203099970e+01
0.	229000002e+000.	148999998e-010.	148479999e-010.	156000003e+000.	188999996e+00
0.	201000005e+000.	e+000.	156000000e+040.	114200001e+020.	114099998e+02
0.	113774995e+020.	607479991e+010.	617000005e+010.	663399982e+010.	479999970e-01
0.	300000000e+010.	102700000e+040.	385200000e+050.	260700000e+070.	136900005e+00
0.	420574997e+000.	293700004e+010.	144800003e-040.	e+000.	e+00
0.	e+000.	e+000.	e+000.	e+000.	e+00
0.	e+000.	e+000.	e+000.	e+000.	e+00
0.	e+000.	e+000.	e+000.	e+000.	e+00
e=1e-1					
0.	1	18	1		1.00
0.	1	0	0	0	2
0.	e+000.	e+00	e+000.	e+000.	1
0.	2	0	0	0	3
0.	e+000.	e+00	e+000.	e+000.	1
0.	3	0	0	0	4
0.	e+000.	e+00	e+000.	e+000.	1
0.	4	0	0	0	5
0.	e+000.	e+00	e+000.	e+000.	1
0.	5	0	0	0	6
0.	e+000.	e+00	e+000.	e+000.	1
0.	6	0	0	0	7
0.	e+000.	e+00	e+000.	e+000.	1
0.	7	0	0	0	8
0.	e+000.	e+00	e+000.	e+000.	1
0.	8	0	0	0	9
0.	e+000.	e+00	e+000.	e+000.	1
0.	9	0	0	0	10
0.	e+000.	e+00	e+000.	e+000.	1
0.	10	0	0	0	11
0.	e+000.	e+00	e+000.	e+000.	1
0.	11	0	0	0	12
0.	e+000.	e+00	e+000.	e+000.	1
0.	12	0	0	0	13
0.	e+000.	e+000.	e+000.	e+000.	1

Table 2.5.6 (cont'd)

```

    0.          e+00  0.1000000e+02
fini
thou,lbl
    2          152    3    1    0    0
ndyn
velo,l,l
main    7
    2  0.          e+00-.685300e+040.      e+000.      e+000.      e+000.      e+00
    3 -.119001e+04-.674839e+040.      e+000.      e+000.      e+000.      e+00
    4 -.234356e+04-.643971e+040.      e+000.      e+000.      e+000.      e+00
    5 -.342650e+04-.593437e+040.      e+000.      e+000.      e+000.      e+00
    6 -.440502e+04-.524970e+040.      e+000.      e+000.      e+000.      e+00
    7 -.524970e+04-.440502e+040.      e+000.      e+000.      e+000.      e+00
    8 -.419654e+04-.242290e+040.      e+000.      e+000.      e+000.      e+00
mass
dylc,l,l
recl    2    0.          1.00          1
    2
time,rslt,10,0.1000e+01
auto,defi
inte,newm,0.2000e-05,0.e+00,0.e+00,0.1000e+00
stir
stif,upda
k1nr,l2
e1nr,l,2,6,3
k1nr,b
loop,2000
zero,time
step
unba
auto,init
loop,20
stir
auto,load
load
disp
k1nr,10
e1nr,7,10
auto,terr,0.1000e+00,0.5000e+00
if,3,3,1,1
entr,1
auto,fact
k1nr,1
if,3,2,2,3
entr,2
e1nr,1
cont
goto,0
entr,3
auto,step,0.1000e-05,0.1000e-03,0.5000e+00,0.2000e+01
if,4,5,5,4
entr,4
inte,newm,,auto,0.e+00,0.e+00,0.e+00,0.1000e+00
entr,5
if,3,6,6,7
entr,6

```

Table 2.5.6 (cont'd)

```
klr,12
elr,5,2,6
klr,5
stf,init
goto,8
entr,7
chcu
elr,1,2,4,6,11
klr,4,9,11
wrcu
zerc,lr5b
unca
sunh
elr,3
klr,3
stf,upda
auto,exit,0.2400e-02
if,5,8,8,0
entr,5
cont
rini
stop
DATA0103
```

TABLE 2.5.7 - DATA FILE LISTING. SHELL MODEL WITH STRAIN RATE EFFECTS.

```

ECHESPOC  SLCGSR00  RSLTSR00  PAUSSR00  PAUZSR00
star,raus
qbui
new,ring,nonl,cart,0,100,100
      shell element example - free ring ... rate dependent mat1
refn,76
10.      e+000.293800000e+010.      e+00
20.      e+000.293800000e+01-.600000000e+00
30.      e+000.300000000e+01-.600000000e+00
40.      e+000.300000000e+010.      e+00
50.510178346e+000.289336518e+010.      e+00
60.510178346e+000.289336518e+01-.600000000e+00
70.520944533e+000.295442326e+01-.600000000e+00
80.520944533e+000.295442326e+010.      e+00
90.100485518e+010.276081692e+010.      e+00
100.100485518e+010.276081692e+01-.600000000e+00
110.102606043e+010.281907786e+01-.600000000e+00
120.102606043e+010.281907786e+010.      e+00
130.146900000e+010.254438264e+010.      e+00
140.146900000e+010.254438264e+01-.600000000e+00
150.150000000e+010.259807621e+01-.600000000e+00
160.150000000e+010.259807621e+010.      e+00
170.188851000e+010.225063857e+010.      e+00
180.188851000e+010.225063857e+01-.600000000e+00
190.192836283e+010.229813333e+01-.600000000e+00
200.192836283e+010.229813333e+010.      e+00
210.225063857e+010.188851000e+010.      e+00
220.225063857e+010.188851000e+01-.600000000e+00
230.229813333e+010.192836283e+01-.600000000e+00
240.229813333e+010.192836283e+010.      e+00
250.254438264e+010.146900000e+010.      e+00
260.254438264e+010.146900000e+01-.600000000e+00
270.259807621e+010.150000000e+01-.600000000e+00
280.259807621e+010.150000000e+010.      e+00
290.276081692e+010.100485518e+010.      e+00
300.276081692e+010.100485518e+01-.600000000e+00
310.281907786e+010.102606043e+01-.600000000e+00
320.281907786e+010.102606043e+010.      e+00
330.289336518e+010.510178346e+000.      e+00
340.289336518e+010.510178346e+00-.600000000e+00
350.295442326e+010.520944533e+00-.600000000e+00
360.295442326e+010.520944533e+000.      e+00
370.293800000e+010.540459853d-160.      e+00
380.293800000e+010.540459853d-16-.600000000e+00
390.300000000e+010.653975343d-16-.600000000e+00
400.300000000e+010.653975343d-160.      e+00
410.289336518e+01-.510178346e+000.      e+00
420.289336518e+01-.510178346e+00-.600000000e+00
430.295442326e+01-.520944533e+00-.600000000e+00
440.295442326e+01-.520944533e+000.      e+00
450.276081692e+01-.100485518e+010.      e+00
460.276081692e+01-.100485518e+01-.600000000e+00
470.281907786e+01-.102606043e+01-.600000000e+00
480.281907786e+01-.102606043e+010.      e+00
490.254438264e+01-.146900000e+010.      e+00
500.254438264e+01-.146900000e+01-.600000000e+00

```

Table 2.5.7 (cont'd)

```

51C.259807621e+01-.150000000e+01-.600000000e+00
52C.259807621e+01-.150000000e+010. e+00
53C.225063857e+01-.188851000e+010. e+00
54C.225063857e+01-.188851000e+01-.600000000e+00
55C.229813333e+01-.192836283e+01-.600000000e+00
56C.229813333e+01-.192836283e+010. e+00
57C.188851000e+01-.225063857e+010. e+00
58C.188851000e+01-.225063857e+01-.600000000e+00
59C.192836283e+01-.229813333e+01-.600000000e+00
60C.192836283e+01-.229813333e+010. e+00
61C.146900000e+01-.254438264e+010. e+00
62C.146900000e+01-.254438264e+01-.600000000e+00
63C.150000000e+01-.259807621e+01-.600000000e+00
64C.150000000e+01-.259807621e+010. e+00
65C.100485518e+01-.276081692e+010. e+00
66C.100485518e+01-.276081692e+01-.600000000e+00
67C.102606043e+01-.281907786e+01-.600000000e+00
68C.102606043e+01-.281907786e+010. e+00
69C.510178346e+00-.289336518e+010. e+00
70C.510178346e+00-.289336518e+01-.600000000e+00
71C.520944533e+00-.295442326e+01-.600000000e+00
72C.520944533e+00-.295442326e+010. e+00
73C.128091971d-15-.293800000e+010. e+00
74C.128091971d-15-.293800000e+01-.600000000e+00
75C.130795069d-15-.300000000e+01-.600000000e+00
76C.130795069d-15-.300000000e+010. e+00

```

bcun,10

5	000111	4	69
6	001111	4	70
7	001111	4	71
8	000111	4	72
1	100111		
2	101111		
3	101111	1	4
73	100111		
74	101111		
75	101111	1	76

enod,1

matl,1,36

```

1.0, 3.0, 0.1, 0.1, 0.3
9.66e-5, 0.1, 0.0, 0.0, 10.4e+3
79.7, 0.0, 0.0, 0.0, 0.0
42.8, 1.0e+10, 0.0, 0.0, 0.0
0.0, 2.0, 6.849e-2, 1.0769e-2, 8.0
18.0, 1.0e+10, 0.0, 0.0, 1.0
0.0, 0.0, -1.0, 0.0, 0.0
0.0

```

elem,1

20,18,1,5,2,3,,,1.0

1	0	0	0	1	5	6	2	4	8	7	31,1,1,5
2	0	0	0	5	9	10	6	8	12	11	71,1,0,5
3	0	0	0	9	13	14	10	12	16	15	111,1,0,5
4	0	0	0	13	17	18	14	16	20	19	151,1,0,5

Table 2.5.7 (cont'd)

5	0	0	0	17	21	22	18	20	24	23	191,1,0,5
6	0	0	0	21	25	26	22	24	28	27	231,1,0,5
7	0	0	0	25	29	30	26	28	32	31	271,1,0,5
8	0	0	0	29	33	34	30	32	36	35	311,1,0,5
9	0	0	0	33	37	38	34	36	40	39	351,1,1,5
10	0	0	0	37	41	42	38	40	44	43	391,1,0,5
11	0	0	0	41	45	46	42	44	48	47	431,1,0,5
12	0	0	0	45	49	50	46	48	52	51	471,1,0,5
13	0	0	0	49	53	54	50	52	56	55	511,1,0,5
14	0	0	0	53	57	58	54	56	60	59	551,1,0,5
15	0	0	0	57	61	62	58	60	64	63	591,1,0,5
16	0	0	0	61	65	66	62	64	68	67	631,1,0,5
17	0	0	0	65	69	70	66	68	72	71	671,1,0,5
18	0	0	0	69	73	74	70	72	76	75	711,1,0,5

nord
 prof
 end
 fini
 mbui
 new,ring
 pmas,3f

1	2.4032e-9	2.4032e-9	2.4032e-9
2	2.4032e-9	2.4032e-9	2.4032e-9
5	4.8065e-9	4.8065e-9	4.8065e-9
6	4.8065e-9	4.8065e-9	4.8065e-9
9	4.8065e-9	4.8065e-9	4.8065e-9
10	4.8065e-9	4.8065e-9	4.8065e-9
13	4.8065e-9	4.8065e-9	4.8065e-9
14	4.8065e-9	4.8065e-9	4.8065e-9
17	4.8065e-9	4.8065e-9	4.8065e-9
18	4.8065e-9	4.8065e-9	4.8065e-9
21	4.8065e-9	4.8065e-9	4.8065e-9
22	4.8065e-9	4.8065e-9	4.8065e-9
25	4.8065e-9	4.8065e-9	4.8065e-9
26	4.8065e-9	4.8065e-9	4.8065e-9
29	4.8065e-9	4.8065e-9	4.8065e-9
30	4.8065e-9	4.8065e-9	4.8065e-9
33	4.8065e-9	4.8065e-9	4.8065e-9
34	4.8065e-9	4.8065e-9	4.8065e-9
37	4.8065e-9	4.8065e-9	4.8065e-9

Table 2.5.7 (cont'd)

```

e 3E 4.8065e-9, 4.8065e-9, 4.8065e-9
41 4.8065e-9, 4.8065e-9, 4.8065e-9
42 4.8065e-9, 4.8065e-9, 4.8065e-9
45 4.8065e-9, 4.8065e-9, 4.8065e-9
46 4.8065e-9, 4.8065e-9, 4.8065e-9
49 4.8065e-9, 4.8065e-9, 4.8065e-9
50 4.8065e-9, 4.8065e-9, 4.8065e-9
53 4.8065e-9, 4.8065e-9, 4.8065e-9
54 4.8065e-9, 4.8065e-9, 4.8065e-9
57 4.8065e-9, 4.8065e-9, 4.8065e-9
58 4.8065e-9, 4.8065e-9, 4.8065e-9
61 4.8065e-9, 4.8065e-9, 4.8065e-9
62 4.8065e-9, 4.8065e-9, 4.8065e-9
65 4.8065e-9, 4.8065e-9, 4.8065e-9
66 4.8065e-9, 4.8065e-9, 4.8065e-9
69 4.8065e-9, 4.8065e-9, 4.8065e-9
70 4.8065e-9, 4.8065e-9, 4.8065e-9
73 2.4032e-9, 2.4032e-9, 2.4032e-9
74 2.4032e-9, 2.4032e-9, 2.4032e-9
end
fini
node
tree,rinc
fini
thou,741
100000000200000006860000300001
ndyn
mass
time,prir,1000,0.0001
velc,1,0
1,14
1 0. e+00-.685300e+040. e+000. e+000. e+000. e+00
2 0. e+00-.685300e+040. e+000. e+000. e+000. e+00
5 -.119001e+04-.674889e+040. e+000. e+000. e+000. e+00
6 -.119001e+04-.674889e+040. e+000. e+000. e+000. e+00
9 -.234386e+04-.643971e+040. e+000. e+000. e+000. e+00
10 -.234386e+04-.643971e+040. e+000. e+000. e+000. e+00
13 -.742650e+04-.593487e+040. e+000. e+000. e+000. e+00
14 -.342150e+04-.593487e+040. e+000. e+000. e+000. e+00
17 -.440502e+04-.524970e+040. e+000. e+000. e+000. e+00
18 -.440502e+04-.524970e+040. e+000. e+000. e+000. e+00
21 -.524970e+04-.440502e+040. e+000. e+000. e+000. e+00
22 -.524970e+04-.440502e+040. e+000. e+000. e+000. e+00
25 -.419659e+04-.242290e+040. e+000. e+000. e+000. e+00
26 -.419659e+04-.242290e+040. e+000. e+000. e+000. e+00
auto,defi
inte,rewr,0.2e-5,0.0,0.,0.1
stif
stif,upda
kinr,12
elmr,1,2,6,3
kinr,5
loop,1000
zero,ltme
step
unba

```

Table 2.5.7 (cont'd)

```
auto,init
lccp,30
stif
auto,load
load
disp
kinr,10
elmr,5,10
auto,nerr,0.5,2.5
if,3,3,1,1
entr,1
auto,fact
kinr,1
if,3,2,2,3
entr,2
elmr,1
cont
goto,0
entr,3
auto,step,1.0e-6,1.0e-4
if,4,5,5,4
entr,4
inte,newm,,auto,0.0,0.0,0.0,0.1
entr,5
if,3,6,6,7
entr,6
kinr,12
elmr,5,2,6
kinr,5
stif,init
goto,8
entr,7
chou
elmr,1,2,4,6,11
kinr,4,9,11
wrou
zero,lrsb
unba
if,3,3,9,9
entr,9
summ
elmr,3
kinr,3
stif,upda
auto,exit,0.0028
if,5,8,8,0
entr,8
cont
fini
stop
```


TABLE 2.5.8 - BEAM MODEL
RATIO OF VERTICAL DIAMETER TO HORIZONTAL DIAMETER

CASE	RATIO
Experiment [2.5.2] Time = 1.14 msec.	0.393
WIPS with strain rate Time = 1.14 msec.	0.391
Analysis with strain rate [2.5.2] Time = 1.14 msec.	0.406
WIPS without strain rate Time = 1.17 msec.*	0.358
Analysis without strain rate [2.5.2] Time = 1.14 msec.	0.333
Experiment [2.5.2] Time = 2.58 msec.	0.657
WIPS with strain rate Time = 2.57 msec.	0.519
Analysis with strain rate [2.5.2] Time = 2.58 msec.	0.613
WIPS without strain rate Time = 2.45 msec.*	0.466
Analysis without strain rate [2.5.2] Time = 2.58 msec.	0.423

*Results output was requested only every 20 steps. These were the closest available output times.

TABLE 2.5.9 - SHELL MODEL
RATIO OF VERTICAL DIAMETER TO HORIZONTAL DIAMETER

CASE	RATIO
Experiment [2.5.2] Time = 1.14 msec.	0.391
WIPS with strain rate Time = 1.10 msec.	0.431
Analysis with strain rate [2.5.2] Time = 1.14 msec.	0.406
WIPS with strain rate Time = 1.10 msec.	0.325
Analysis without strain rate [2.5.2] Time = 1.14 msec.	0.333
Experiment [2.5.2] Time = 2.58 msec.	0.657
WIPS with strain rate Time = 2.6 msec.	0.849
Analysis with strain rate [2.5.2] Time = 2.58 msec.	0.613
WIPS without strain rate Time = 2.6 msec.	0.395
Analysis without strain rate [2.5.2] Time = 2.58 msec.	0.423

D2.6 PIPE IMPACT ON INCLINED SLAB STRUCTURE

D2.6.1 PURPOSE

The purpose of this example is to test the SLAB substructure option, the impact analysis option, and three-dimensional motion of the PIPE element. Large displacement and contact friction effects are considered, but strain rate effects are ignored. The SLAB substructure is divided into only a small number of elements, to reduce the computation cost, and has been modelled assuming an elastic material.

The example has been chosen to test the computational procedure only. There are no test results or other analytical results available for comparison.

D2.6.2 DESCRIPTION

A pipe with the same geometry and properties as that in Section D2.3 has been assumed, except that full three-dimensional motion is allowed. A flat slab is located beneath the pipe, inclined at 45 degrees to the horizontal so that the pipe moves out-of-plane and slides over the slab after impact. The dimensions are shown in Fig. 2.6.1.

D2.6.3 WIPS ANALYSIS MODEL

D2.6.3.1 Pipe and Slab Properties

The pipe properties and pipe element subdivision were exactly as for the pipe considered in Section D2.3, ignoring strain rate effects. The slab was assumed to be of steel, 3 inches thick, with a very high yield strength. Boundary conditions for the slab were assumed arbitrarily to test the boundary condition specification in the WIPS-SLAB phase. A 3 x 5 finite element mesh was arbitrarily assumed. This mesh would be too coarse for a practical analysis. For sliding after impact, a coefficient of friction of 0.4 was specified.

D2.6.3.2 WIPS Input

Table 2.6.1 contains the WIPSLOG listings through the WIPS-DATA phase. Table 2.6.2 is a listing of the DATA file.

The data for this example was prepared on a VAX 11/780 computer at the University of California. A copy of the DATA file was then transferred by tape to the CRAY computer at Lawrence Livermore National Laboratory, and the analysis was performed on the CRAY. A formatted file containing the results output was produced (in fact, two files because the CRAY analysis was stopped and restarted). The output file was then transferred by tape back to the VAX, and incorporated into the RSLT file using the WIPS-MERG option. Finally, the results were processed on the VAX using WIPS-RSLT.

D2.6.4 RESULTS

D2.6.4.1 General

It is important to note that the purpose of this example is to test the impact analysis features of WIPS, not to obtain realistic results for pipe-to-slab impact. There are two features of the model which would be questionable in a practical impact analysis, namely (1) the coarseness of the finite element mesh and the assumption of elastic behavior for the SLAB substructure and (2) the fact that the pipe was modelled as a series of PIPE elements rather than with an ELBO substructure.

This second feature is particularly important when the calculated impact forces are considered. In an actual pipe-to-slab impact, substantial local deformation of the pipe will occur (and possibly also of the slab). This local deformation will have a major influence on the

impact forces. When a model using PIPE elements is used, local deformations of the pipe are ignored; and, as a consequence, the calculated impact forces are likely to be completely unrealistic (almost certainly much too large). Further, the calculated forces for such a model may depend on the integration time step used in the analysis, and possibly on other analysis assumptions. Impact analyses using PIPE or BEAM elements may predict the pipe motion with reasonable accuracy (although even this remains to be proved). They will not, however, predict accurate impact forces.

D2.6.4.2 Pipe Motion

The complete model is shown in Fig. 2.6.2, with the undeformed shape and the deformed shapes at two times after impact. At the second of these times the pipe had moved off the slab. In the following step the analysis stopped because of convergence problems. Fig. 2.6.3 shows a part of the model in more detail at three times during the interaction, beginning with the initial impact at 0.071 seconds. This figure shows that the pipe nodes cross boundaries in the slab mesh (the primary surface for the impact analysis).

The views in Figs. 2.6.2 and 2.6.3 are projections on the X-Y plane. Fig. 2.6.4 shows a part of the model (essentially the same part as in Fig. 2.6.3) but projected on the Y-Z plane. This figure indicates how the pipe translates and twists out of its original plane after it strikes the inclined slab. The lines representing the slab in this figure show the deformed positions of the slab center line at the four times.

D2.6.4.3 Impact Forces

Fig. 2.6.5 shows the variation with time of the calculated normal impact force, up to 0.1 seconds. Immediately after impact the variation is erratic and the calculated forces are very large. The pipe then bounces down the slab, successively separating and re-establishing contact. Further contact occurred at about 0.12 seconds, but is not shown on the graph.

D2.6.5 CONCLUSION

This example indicates that the contact analysis algorithm in WIPS performs as intended, preventing the secondary nodes (in this case the PIPE nodes) from penetrating the primary surface (the SLAB substructure). It must be emphasized, however, that contact analyses are extremely complex. Until more experience is gained, the results of contact analyses should be interpreted cautiously, particularly the calculated impact forces.

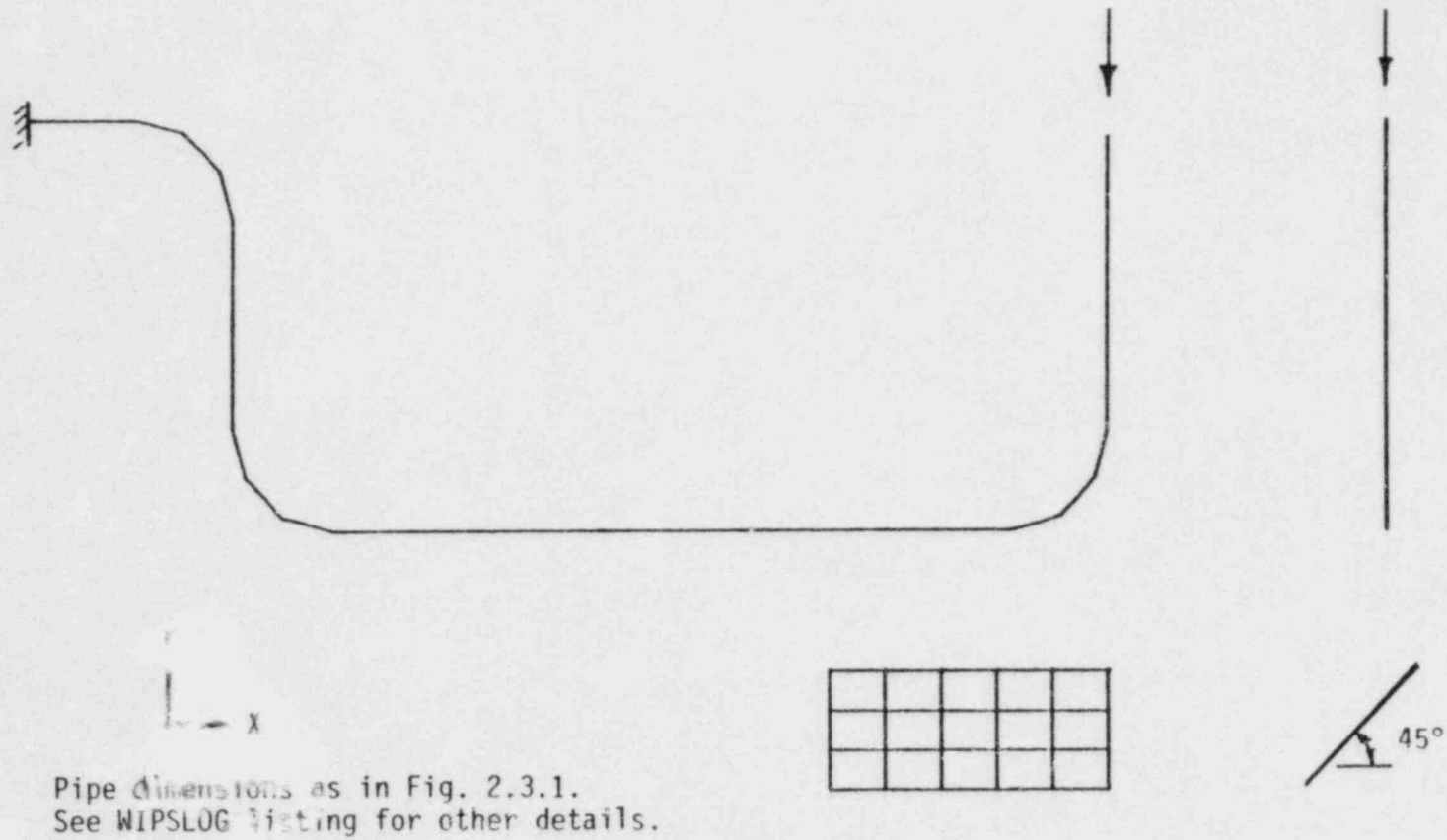


FIG. 2.6.1 PIPE IMPACTING INCLINED SLAB.

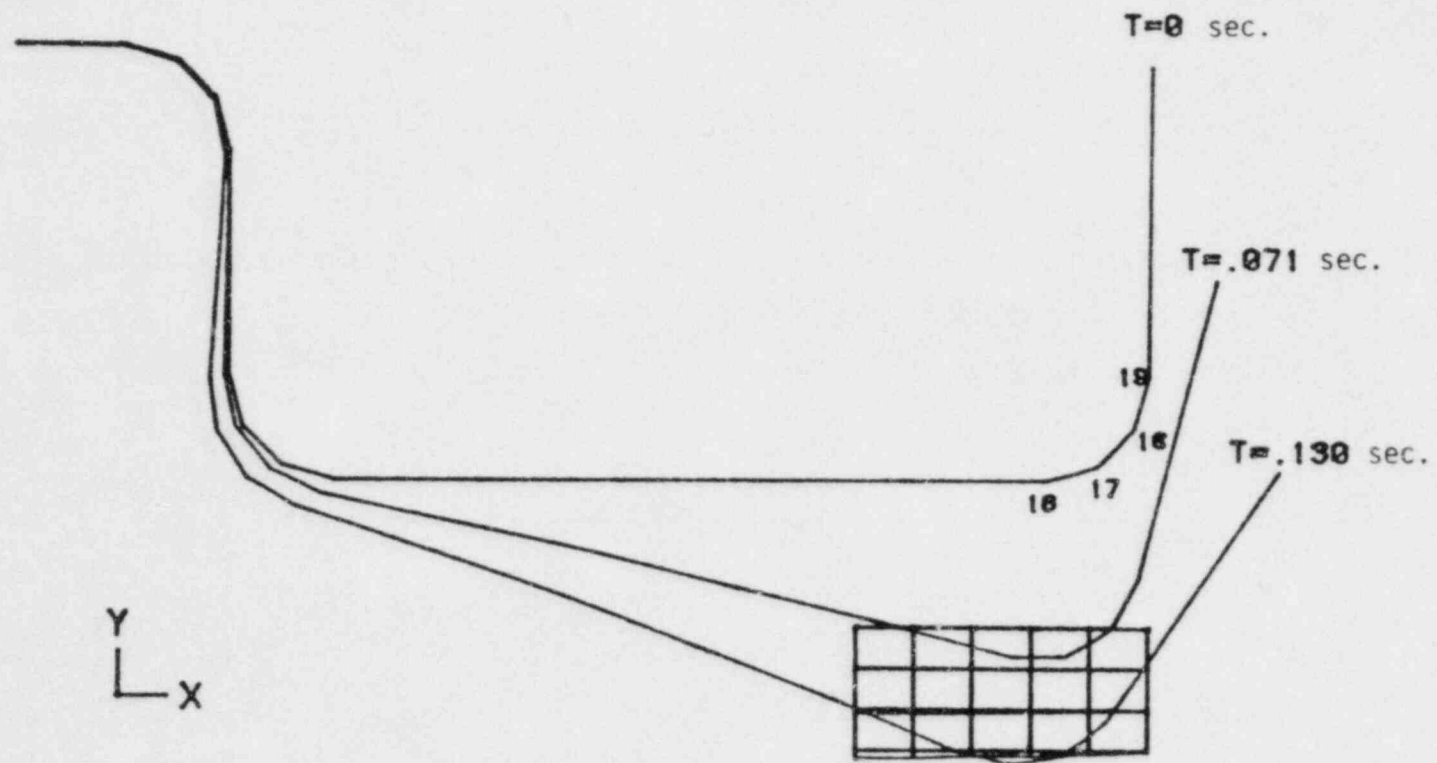


FIG. 2.6.2 DEFORMED PIPE AND SLAB. COMPLETE SYSTEM.

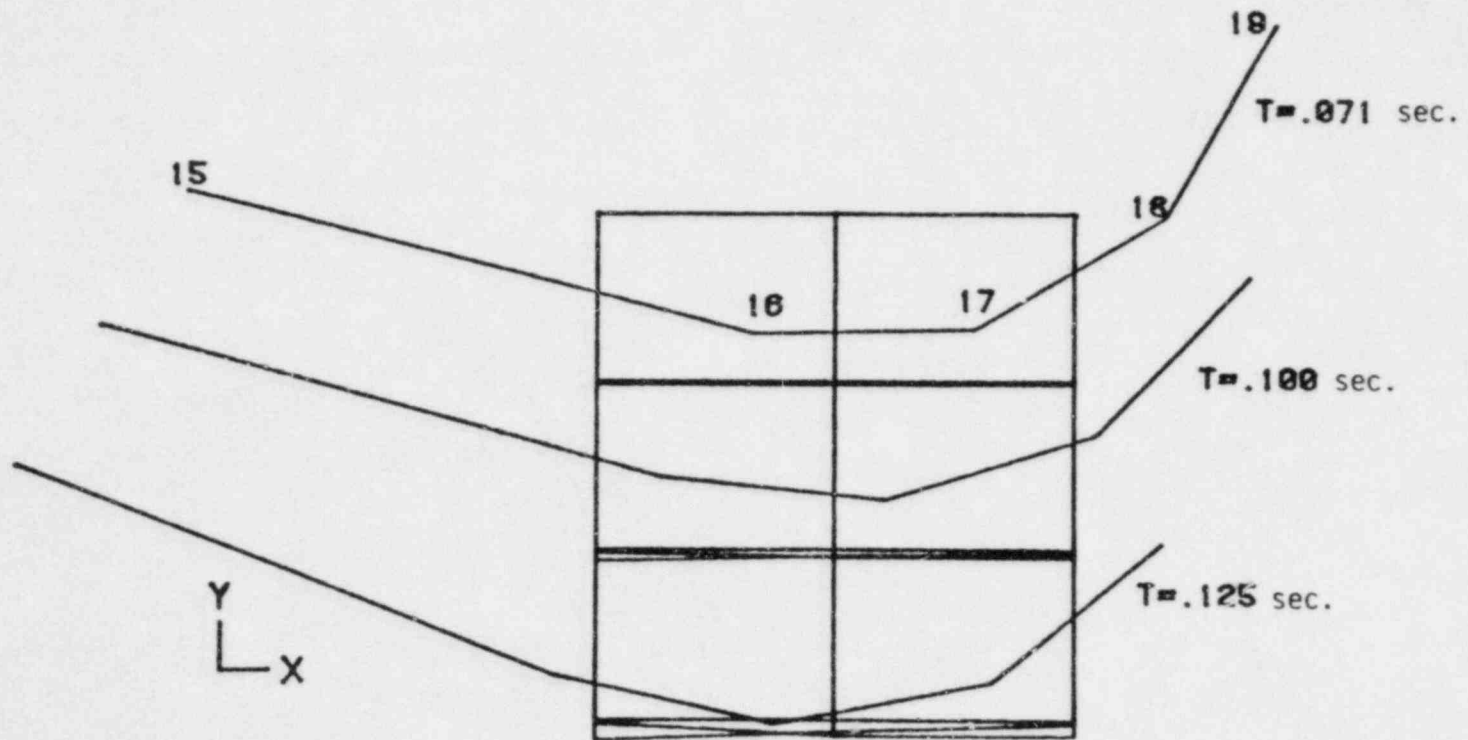


FIG. 2.6.3 DEFORMED PIPE AND SLAB. PART OF SYSTEM.

Only the part of the pipe from nodes 15-19 is shown (see node numbers in Part (b) of the figure).

Only one line of nodes near the slab center-line is shown.

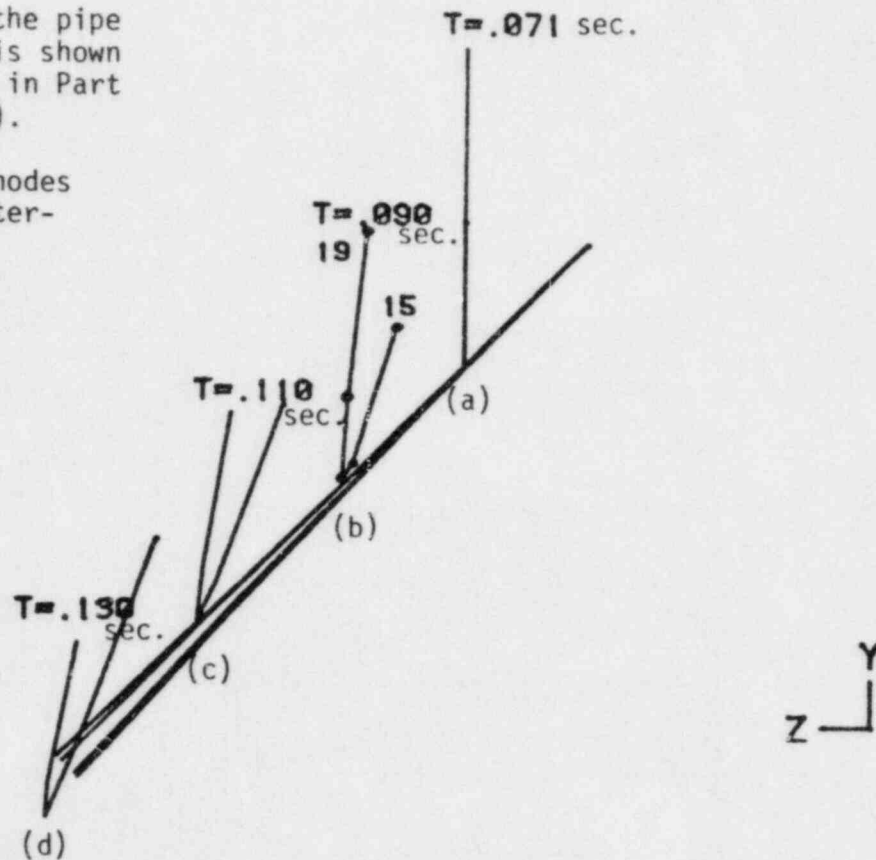


FIG. 2.6.4 DEFORMED PIPE AND SLAB. PART OF SYSTEM. END VIEW.

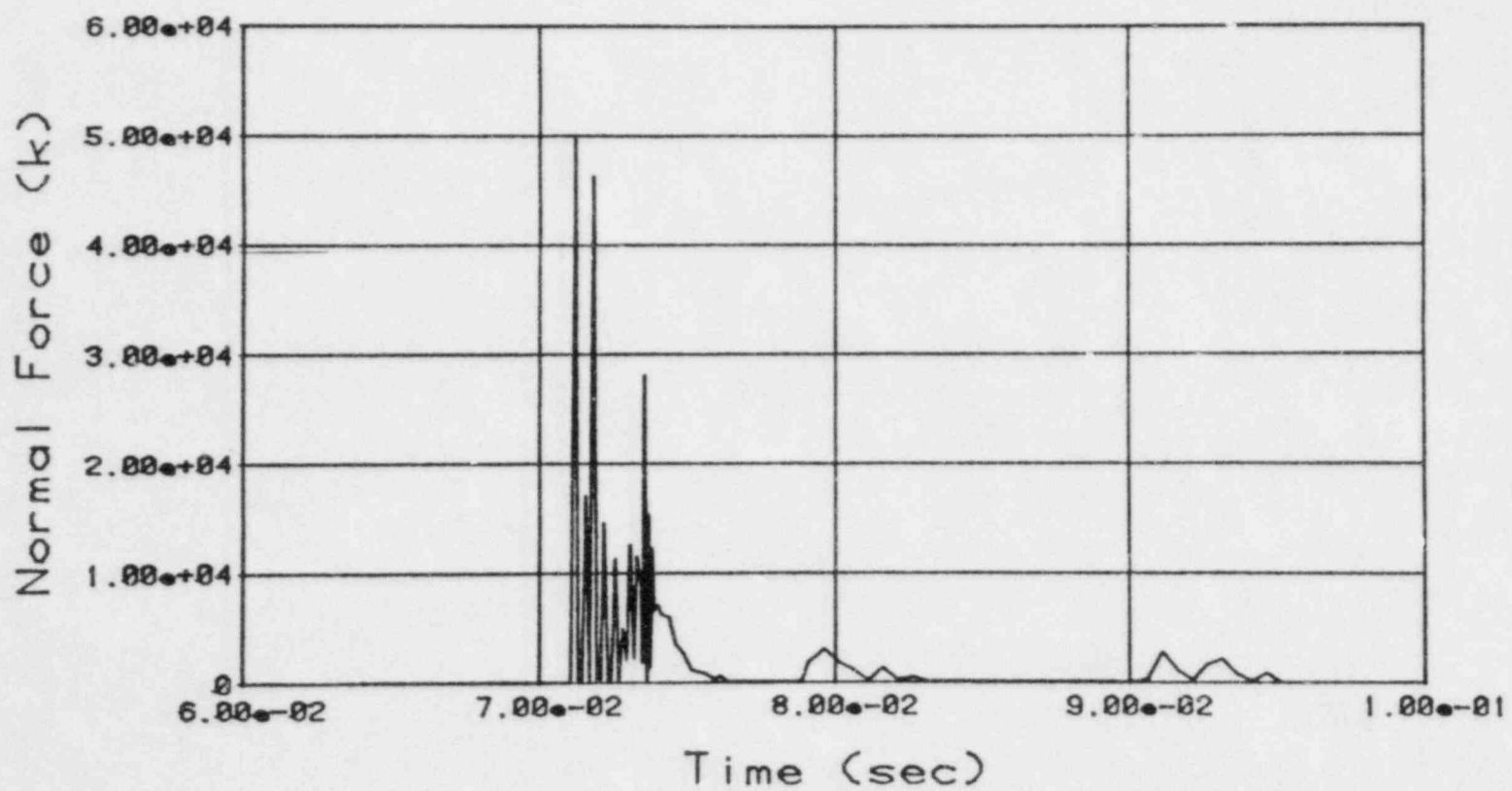


FIG. 2.6.5 IMPACT FORCE TIME HISTORY

TABLE 2.6.1 - WIPSLOG LISTINGS. GEOM, MATL, PIPE, SLAB,
FREC, MODL, AND DATA PHASES.

EXEC - WIPS EXECUTIVE
Creating problem no. 1
Problem description: Pipe impacting inclined slab.

NEXT WIPS-EXEC COMMAND : geom

GEOM - SPECIFICATION OF SYSTEM GEOMETRY

Define units
Length (ft, in, m, mm) : in
Force (k, lb, kgf, kN) : k

Specify new GEOM data

START RUN NO. 1
Enter c.p. data in sequence along run

c.p. name and type : 1
ccord option : di
x,y,z :
Any changes? :

c.p. name and type : 2 tn
nc. of extra nodes : 1
ccord option :
tn generate automatically
Any changes? :

c.p. name and type : t11 ti
bend radius : 36
ccord option :
c.p., dx,dy,dz : 1 7c
Any changes? :

c.p. name and type : 6 tn
nc. of extra nodes : 2
ccord option :
tn generate automatically
Any changes? :

c.p. name and type : 5 tn
nc. of extra nodes : 1
ccord option :
tn generated automatically
Any changes? :

c.p. name and type : t12 ti
bend radius : 36
ccord option :
c.p., dx,dy,dz : t11 0 -14b
Any changes? :

c.p. name and type : 11 tn
nc. of extra nodes : 2
ccord option :
tn generated automatically

Table 2.6.1 (cont'd)

Any changes? :

c.p. name and type : 16 tn
 no. of extra nodes : 4
 coord option :
 tn generated automatically
 Any changes? :

c.p. name and type : 17
 no. of extra nodes :
 coord option : cu
 c.p.i, c.p.j, proportion : 16 19 .33333
 Any changes? :

c.p. name and type : 18
 no. of extra nodes :
 coord option : cu
 c.p.i, c.p.j, proportion : 16 19 .66667
 Any changes? :

c.p. name and type : t13 ti
 bend radius : 36
 coord option :
 c.p.s dx,dy,dz : t12 315
 Any changes? :

c.p. name and type : 19 tn
 no. of extra nodes :
 coord option :
 tn generated automatically
 Any changes? :

c.p. name and type : 20
 no. of extra nodes :
 coord option :
 c.p.s dx,dy,dz : t13 0 142
 Any changes? :

c.p. name and type :
 Last c.p. in this run? : y
 Display GEOM data for this run? : y

GEOM DATA FOR RUN

run no.	c.p. name	c.p. type	bend radius	extra nodes	coord opt	c.p. i	c.p. j ?	coordinate data		
								x,dx,p	y,dy	z,dz
1										
	1			0	di			0.	0.	0.
	3	tn		1	tn			0.	0.	0.
	t11	ti	36.000	0	of	1		72.000	0.	0.
	6	tn		2	tn			0.	0.	0.
	8	tn		1	tn			0.	0.	0.
	t12	ti	36.000	0	of	t11		0.	-144.000	0.
	11	tn		2	tn			0.	0.	0.
	16	tn		4	tn			0.	0.	0.

Table 2.6.1 (cont'd)

```

17          0      cu  16  19      0.333      0.      0.
18          0      cu  16  19      0.667      0.      0.
Hit RETURN for more
  ti3      ti  36.000      0      ti2      315.000      0.      0.
19          0      tn          0.      0.      0.
20          0      of  ti3          0.      142.000      0.
END OF DATA

```

START RUN NO. 2
Enter c.p. data in sequence along run

c.p. name and type :
Last run? : y

Display new GLOM data? :
Write in session log? :

Modify GLOM data? :

Save current GLOM data? : y
Comment for file catalog :
GLOM DATA SAVED. FILE NAME = GLOM0101

Produce COOR data? : y

Display COOR data? : y

COOR DATA

run no.	c.p. name	c.p. type	send radius	node no.	x coord	y ? coord?	z coord
1	1			1	0.	0.	0.
	3	tn		2	18.000	0.	0.
	ti1	ti	36.000 center	3	36.000	0.	0.
				4	72.000	0.	0.
				5	36.000	-36.000	0.
	6	tn		6	54.000	-4.823	0.
				7	67.177	-18.000	0.
	8	tn		8	72.000	-36.000	0.
				9	72.000	-74.000	0.
	ti2	ti	36.000 center	10	72.000	-112.000	0.
				11	108.000	-148.000	0.
				12	76.823	-130.000	0.
	11	tn		13	90.000	-143.177	0.
				14	108.000	-148.000	0.
				15	156.600	-148.000	0.
				16	205.200	-148.000	0.
	16	tn		17	253.800	-148.000	0.
				18	302.400	-148.000	0.
				19	351.000	-148.000	0.

Table 2.6.1 (cont'd)

17			17	369.000	-143.177	0.
18			18	362.177	-130.000	0.
ti3	ti	36.000		367.000	-148.000	0.
		center		351.000	-112.000	0.
19	tn		19	387.000	-112.000	0.
20			20	387.000	-6.000	0.

END OF DATA

Plot geometry? :

Modify GEM data? :

DATA COMPLETE FOR THIS SESSION

Save final GEM data? : y

Comment for file catalog : Pipe as in Hibbitt Fig.4.12.

GEM DATA SAVED. FILE NAME = GEMM0101

Save COOR data? : y

Comment for file catalog : From GEMM0101.

COOR DATA SAVED. FILE NAME = COOR0101

End of this GEM session

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : matl

MATL - SPECIFICATION OF MATERIAL PROPERTIES

Define units

Length (ft,in,m,mm) : in

Force (k,lb,kgf,kN) :

Start new MATL file

Specify a new property set? : y

SET NO. = 1

Property set description : Hibbitt material, no strain rate.

Static moduli (min=2,max=5)

: 26700 219 2

Yield strengths (no. of moduli minus 1)

: 26.7 44

Strain rate stiffnesses (min=0,max=3)

:

No strain rate effect

Use default tolerances? : y

Poisson ratio (dflt = .3) :

Weight density (dflt=steel) :

Table 2.6.1 (cont'd)

```

Any errors? :
This set added to MATL file
Specify a new property set? :
No. of property sets in MATL file = 1
Display property set descriptions? : y
MATL PROPERTY DESCRIPTIONS
  Set No.  Type  Description
    1      BROZ  Hibbitt material, no strain rate.
Display new property set data? : y
MATL PROPERTY DATA
SET NO. 1.  Hibbitt material, no strain rate.

```

Matl Type	Data Type	Seqm No.	Modulus of Coefficient	Stress/Strain Limit
BROZ	static	1	0.2670e+05	0.2670e+02
		2	0.2190e+03	0.4400e+02
		3	0.2000e+01	
	ylt.tol.		0.2000e-01	
	ult.tol		0.5000e-01	
	rate tol		0.5000e-01	
	poisson		0.3000e+00	
	density		0.2840e-03	

```

Hit RETURN for next set
END OF DATA

Display all property set data? :
Write in session log? :

New MATL file created
Comment for file catalog :

End this MATL session? : y
EXEC - WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : matl

MATL - SPECIFICATION OF MATERIAL PROPERTIES
Define units
  Length (ft,in,m,cm) : in
  Force (k,lb,kgf,kN) : k

Existing MATL file being extended.
No. of existing property sets = 1

```

Table 2.6.1 (cont'd)

```

Specify a new property set? : y

SET NO. = 2
Property set description : Elastic material for slab.
  Static moduli (min=2,max=5)
  : 30000 300
  Yield strengths (no. of moduli minus 1)
  : 1e20
  Strain rate stiffnesses (min=0,max=3)
  :
  No strain rate effect
  Use default tolerances? :
  Yield tolerance (dfit=.02) : .02
  Stiffness tolerance (dfit=.05) : .05
  Poisson ratio (dfit = .3) :
  Weight density (dfit=steel) :

Any errors? :

This set added to MAIL file

Specify a new property set? :

No. of property sets in MAIL file = 2

Display property set descriptions? : y

MAIL PROPERTY DESCRIPTIONS

  Set No.  Type  Description
        1  mroz  Hibbitt material, no strain rate.
        2  mroz  Elastic material for slab.

Display new property set data? : y

MAIL PROPERTY DATA

SET NO.  2.  Elastic material for slab.

      Matl   Data   Seqm   Modulus or   Stress/Strain
      Type   Type   No.   Coefficient   Limit
      mroz
      static   1   0.3000e+05   0.1000e+21
              2   0.3000e+03
      ,ld,tol.   0.2000e-01
      ,lif,tol  0.5000e-01
      rate tol  0.      e+00
      poisson   0.3000e+00
      density   0.2840e-03

Hit RETURN for next set
END OF DATA

Display all property set data? :
Write in session log? :
  
```

Table 2.6.1 (cont'd)

```
Existing MATL file extended
Comment for file catalog :

End this MATL session? : y
EXEC = WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : quit
-----
EXEC = WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : pipe

PIPEL = SPECIFICATION OF PIPE PROPERTIES

Define units
  Length (ft,in,m,mm) : in
  Force (k,lb,kgf,kh) : k

No. of MATL property sets available = 2
Display material descriptions? : y

MATL PROPERTY DESCRIPTIONS
  Set No.  Type  Description
    1      mro2  Hibbitt material, no strain rate.
    2      mro2  Elastic material for slab.

Start new PIPEL file

Specify a new property set? : y

SET NO. = 1
Property set Description : 24sch100, no strain rate, small oval.
  Outside diameter : 24
  Wall thickness : .531
  Weight/unit length (dflt=pipe weight) :
  No. of X-section elements (dflt=12) :
  Material number : 1
  Large ovaling (yes or no)? (dflt=no) :
  Use default ovaling properties? : y

Any errors? :

This set added to PIPEL file

Specify a new property set? :

No. of property sets in PIPEL file = 1
Display property set descriptions? : y

PIPEL PROPERTY DESCRIPTIONS
  Set No.  Description
```

Table 2.6.1 (cont'd)

```

1 24sch100, no strain rate, small oval.
Display new property set data? : y
PIPE PROPERTY DATA
SLT NO. 1. 24sch100, no strain rate, small oval.

      Data      Seqm      Modulus or      Stress/Strain
      Type      No.      Data Value      Limit

      Outside diameter      0.2400e+02
      Wall thickness      0.5310e+00
      Unit weight      0.1112e-01
      No. of elements      12
      No. of slices      2
      Stress v strain      1 0.2670e+05      0.2670e+02
                          2 0.2190e+03      0.4400e+02
                          3 0.2000e+01
      Poisson ratio      0.3000e+00
      Large ovalling      no
      Ovalling ratios      1 0.3500e+00
                          2 0.8000e-01

Hit RETURN for next set
END OF DATA

Display all property set data? :
Write in session log? :

New PIPE file created
Comment for file catalog :

End this PIPE session? : y

EXEC - WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : quit

-----

EXEC - WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : slab

SLAB - SPECIFICATION OF SLAB PROPERTIES

Define units
Length (ft,in,mm) : in
Force (k,lb,kgf,kh) : k

No. of MAIL property sets available = 2
Display material descriptions? : y

MAIL PROPERTY DESCRIPTIONS
Set No. Type Description

```

Table 2.6.1 (cont'd)

```

1      MROX  Bidditt material, NO strain rate.
2      MROX  Elastic material for slab.

Start new SLAB file

Specify a new property set? : y

SET NO.  1

Substructure description : inclined slab
Length of side OA : 60
Length of side OB : 100
Outer strip widths (proportions of OA)
  Left strip :
  Right strip :
Outer strip widths (proportions of OB)
  Bottom strip : .2
  Top strip : .2
No. of subdivisions along OA
  Center strip : 3
No. of subdivisions along OB
  First strip : 1
  Center strip : 3
  Last strip : 1
Slab thickness : 3
No. of Gauss points thru thickness
  Center region : 2
  Outer regions : 2
Direction cosines of OA,OB
  OA (3 values) : 0 -1 1
  OB (3 values) : 1 0 0
Coords of point O (X,Y,Z values) : 267 -196 -10
Boundary codes (free,hing,clmp,syxy,syyz,or syzx)
  OA : free
  OB : hing
  OC : clmp
  AC : free
Material set number : z

Any errors? :

This set added to SLAB file

Specify a new property set? :

No. of property sets in SLAB file = 1

Display property set descriptions? : y

SLAB PROPERTY DESCRIPTIONS
  Set No.  Description
    1      inclined slab

Display new property data? : y

SLAB PROPERTY DATA

```


Table 2.6.1 (cont'd)

```

SET NO. 1. Inclined slab

                First      Center      Last
                Strip      Strip
widths along DA  0.      e+00  0.6000e+02  0.      e+00
widths along DB  0.2000e+02  0.6000e+02  0.2000e+02
Elements along UA  0      3      0
Elements along UB  1      3      1
Thicknesses      0.3000e+01  0.3000e+01  0.3000e+01
No. of Gauss. points  2      2      2

                X          Y          Z
Direction cosines
Edge DA         0.      e+00  -0.7071e+00  0.7071e+00
Edge DB         0.1000e+01  0.      e+00  0.      e+00
Coordinates of U  0.2070e+03  -0.1960e+03  -0.1000e+02

```

```

Boundary codes UA,BC = free, hing
Boundary codes UB,AC = clap, free
Hit RETURN for next set
END OF DATA

```

```

Display all property data? :
Write in session log? :

```

```

New SLAB file created
Comment for file catalog :

```

```

End this SLAB session? : y

```

```

EXEC - WIPS EXECUTIVE

```

```

NEXT WIPS-EXEC COMMAND : quit

```

```

-----
EXEC - WIPS EXECUTIVE

```

```

NEXT WIPS-EXEC COMMAND : frec

```

```

FREC - SPECIFY DYNAMIC FORCE RECORDS

```

```

Define units
Length (ft,in,mm) : in
Force (k,lb,kgf,kN) : k

```

```

Start new FREC file

```

```

Specify a new record? : y

```

```

RECORD NO. 1

```

```

Record name (4 characters) : rec1
Description (max. 40 char.) : Hibbitt record, max. 1000k.

```

```

Enter Time-Force pairs

```

Table 2.6.1 (cont'd)

First pair automatically set to 0,0

Pair no. 2 : .0001 650
 Pair no. 3 : .001 650
 Pair no. 4 : .002 1000
 Pair no. 5 : .003 650
 Pair no. 6 : .005 750
 Pair no. 7 : .02 430
 Pair no. 8 : 10 430
 Pair no. 9 :

Last pair? : ,
 Any errors? :

Specify a new record? :

Display any records? : y
 Record number (dfilt=all) :

RECORD NO.	1.	Name = rec1
	Time	Force
C.		e+00
C.00010		0.6500e+03
C.00100		0.8800e+03
C.00200		0.1000e+04
C.00300		0.8800e+03
C.00500		0.7800e+03
C.02000		0.4300e+03
1C.00000		0.4300e+03

END OF RECORD

Write records in session 10,? :

End this FREC session? : y
 New FREC file created
 Comment for file catalog :

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

 EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : read

MODEL - SPECIFICATION OF ANALYSIS MODEL

Define units

Length (ft,in,m,mm) : in
 Force (kylb,kgf,kN) : k

Sequence no. of CDR file : 1

Available element property sets
 Type No. of Sets

Table 2.6.1 (cont'd)

```

pipe          1
Available substructure property sets
Type      No. of Sets
slab      1

DEFINE MODEL 21 SEGMENTS

SEGMENT NO.  1

Pipe run no. : 1
First c.p. of segment : 1
Full 3D motion? : y
Boundary condition code for first c.p. : 11111

Specify c.p. name + elem type + optional data
1: 20 pipe pr=1 ld=y th=no
2:
End of segment? : y
Display commands for this segment? : y

MODEL COMMAND TABLE

SEGMENT NO.  1  c.p.  elem  data  optn  data  cptrn  data
1             20   pipe          bcon  11111
              prop      1
              loc1    auto  ldis   yes   this   no
              wfac    1.000

Any changes? :

SEGMENT NO.  2

Pipe run no. :
Last segment? : y

Any external substructures? : y
Specify substructure type + optional data
1: slab pr=1 ld=y th=no
More external substructures? :
Display commands for external substructures? : y

MODEL COMMAND TABLE

EXTERNAL SUBSTRUCTURES
type  optn  data  optn  data  cptrn  data
slab  prop  name  wfac  ldis  yes   this   no
      1   SC01  1.000  ldis  yes   this   no

Any changes? :

Display commands for all segments? :
Write in session log? :

```

Table 2.6.1 (cont'd)

```
Produce MODL file? : y
Wait while data is processed

Impact analysis required? : y
No. of impact surface pairs : 1

SURFACE PAIR NO. 1
Surface pair name : sur1

Define primary surface
  Substructure name : SC01
SLAB substructure, property set no. 1
  Divisions along CA = 3
  Divisions along CB = 5
Allowable grid range along CA = 1 thru 4
Allowable grid range along CB = 1 thru 6
Define grid ranges
  CA : 1 4
  CB : 1 6
Thickness from nodes to surface :

Define secondary nodes
  Substructure name (dflt = main) :
Main structure. Define c.p. ranges
  Run no., c.p.1, c.p.2 : 1 16 19
  Run no., c.p.1, c.p.2 :
Last range? : y
No. of impact nodes = 4
Thickness from nodes to surface :
Friction coefficient (dflt=zero) : .4
Sliding veloc. for full friction (dflt=50in/sec) : 100
Any errors? :

Specify initial velocities? :
Comment for file catalog : With inclined slab.

MODL file saved. File name = MODL0101
End of this MODL session

EXEC - WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : quit

-----

EXEC - WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : Data

DATA - SET UP WIPS-ANAL INPUT DATA

Define units
  Length (ft.,in.,mm) : in
  Force (k.,lb.,kgf.,kN) : k
```

Table 2 5.1 (cont'd)

```
Sequence no. of MOUT file : 1
Problem description (4 lines)
  Line 1 : Test of impact feature. Pipe as in Hibbitt Fig.4.12, with slab.
  Line 2 : Slab at 45 degree angle below elbow, approximately 50in clearance.
  Line 3 :
  Line 4 :

Set up PAUSE files at end of analysis ? :
Wait while files are processed

Specify data for each loaded point
LUAL NO. 1
  Force record name : r001
  Name of loaded c.p. : 20
  Force direction (x,y,z or follower) : foll
  Follower c.p. name : 1,
  Scale factor (+,- controls direction) : 1
  Time delay (sec) (dflt=0) :
LUAL NO. 2
  Force record name :
Last load? : ,

Time steps : initial + max + min : .0005 .001 .00001
Max steps + max total time : 200 .1
Error tolerances : upper + lower : 250 50

Results output intervals
  Max. no. of steps : 1
  Max. time (secs.) : 1
Integration scheme (newm or hilb)(dflt=newm) :
Damping factor (dflt=0.1) :
Factor for time step increase (dflt=2.0) :
Factor for time step decrease (dflt=0.5) :
Max. unbal. to reduce time step (dflt=no limit) :
Max. unbal. to stop analysis (dflt=no limit) :

DATA file set complete
Comment for file catalog : With inclined slab.
WIPS-ANAL DATA FILES SET UP. PARENT FILE NAME = DATA10,

EXEC = WIPS EXECUTIVE

NEXT WIPS=EXEC CUPHAND : quit

-----
```

TABLE 2.6.2 - LISTING OF DATA FILE.
PIPE IMPACTING INCLINED SLAB.

```

ECHO0101 SLAB0101 KSLT0101
star,
ygui
news001,noni,cart,0,49,15
slab substructure. name = s001
refn,49
10.287000000e+03-.198000000e+03-.100000000e+02
20.287000000e+03-.196939346e+03-.893933964e+01
30.287000000e+03-.212142136e+03.414213562e+01
40.287000000e+03-.211081482e+03.520279598e+01
50.287000000e+03-.226284271e+03.182842712e+02
60.287000000e+03-.225223618e+03.193449306e+02
70.287000000e+03-.240426407e+03.324264069e+02
80.287000000e+03-.239365753e+03.334870662e+02
90.307000000e+03-.198000000e+03-.100000000e+02
100.307000000e+03-.196939346e+03-.893933964e+01
110.307000000e+03-.212142136e+03.414213562e+01
120.307000000e+03-.211081482e+03.520279598e+01
130.307000000e+03-.226284271e+03.182842712e+02
140.307000000e+03-.225223618e+03.193449306e+02
150.307000000e+03-.240426407e+03.324264069e+02
160.307000000e+03-.239365753e+03.334870662e+02
170.327000000e+03-.198000000e+03-.100000000e+02
180.327000000e+03-.196939346e+03-.893933964e+01
190.327000000e+03-.212142136e+03.414213562e+01
200.327000000e+03-.211081482e+03.520279598e+01
210.327000000e+03-.226284271e+03.182842712e+02
220.327000000e+03-.225223618e+03.193449306e+02
230.327000000e+03-.240426407e+03.324264069e+02
240.327000000e+03-.239365753e+03.334870662e+02
250.347000000e+03-.198000000e+03-.100000000e+02
260.347000000e+03-.196939346e+03-.893933964e+01
270.347000000e+03-.212142136e+03.414213562e+01
280.347000000e+03-.211081482e+03.520279598e+01
290.347000000e+03-.226284271e+03.182842712e+02
300.347000000e+03-.225223618e+03.193449306e+02
310.347000000e+03-.240426407e+03.324264069e+02
320.347000000e+03-.239365753e+03.334870662e+02
330.367000000e+03-.198000000e+03-.100000000e+02
340.367000000e+03-.196939346e+03-.893933964e+01
350.367000000e+03-.212142136e+03.414213562e+01
360.367000000e+03-.211081482e+03.520279598e+01
370.367000000e+03-.226284271e+03.182842712e+02
380.367000000e+03-.225223618e+03.193449306e+02
390.367000000e+03-.240426407e+03.324264069e+02
400.367000000e+03-.239365753e+03.334870662e+02
410.387000000e+03-.198000000e+03-.100000000e+02
420.387000000e+03-.196939346e+03-.893933964e+01
430.387000000e+03-.212142136e+03.414213562e+01
440.387000000e+03-.211081482e+03.520279598e+01
450.387000000e+03-.226284271e+03.182842712e+02
460.387000000e+03-.225223618e+03.193449306e+02
470.387000000e+03-.240426407e+03.324264069e+02
480.387000000e+03-.239365753e+03.334870662e+02
9999
ECHO,34

```

Table 2.6.2 (cont'd)

```

1          000111      1  46
3          000111
4          000111
5          000111
6          000111
43         111111
44         000111
45         111111
46         000111
9          111111
10         111111
17         111111
18         111111
25         111111
26         111111
33         111111
34         111111
15         000111
16         000111
23         000111
24         000111
31         000111
32         000111
39         000111
40         000111
1          111111
2          111111
7          000111
8          000111
41         111111
42         111111
47         111111
48         000111
9999      011111
cnod,1
9999
enod,0
matl,1,36
0.100000000e+010.      e+000.199999999e-010.500000007e-010.299999982e+00
0.283999980e-030.      e+000.      e+000.      e+000.300000000e+05
0.300000000e+050.      e+000.      e+000.      e+000.      e+00
0.100000002e+210.999999932e+200.      e+000.      e+000.      e+000.      e+00
0.      e+000.      e+000.      e+000.      e+000.      e+00
0.      e+000.      e+000.      e+000.      e+000.      e+00
0.      e+000.      e+000.      e+000.      e+000.      e+000.100000000e+01
0.      e+00      e+00-.100000000e+010.      e+000.      e+00
elem,1
20  15  1  2  1  0      1.00
0.  1  0  0  0  1  3  11  9  2  4  12  10  1  1  0  2
0.  2  0  0  0  3  5  13  11  4  6  14  12  1  1  0  2
0.  3  0  0  0  5  7  15  13  6  8  16  14  1  1  0  2
0.  4  0  0  0  9  11  19  17  10  12  20  18  1  1  0  2
0.  0.  0.  0.  0.  0.  0.  0.  0.  0.  0.  0.  0.  0.  0.  0.  0.

```

Table 2.6.2 (cont'd)

0.	5	0	C	0	11	13	21	19	12	14	22	20	1	1	0	2
			e+000.				e+000.		e+00							
0.	6	0	C	0	13	15	23	21	14	16	24	22	1	1	0	2
			e+000.				e+000.		e+00							
0.	7	0	C	0	17	19	27	25	16	20	28	26	1	1	0	2
			e+000.				e+000.		e+00							
0.	8	0	C	0	19	21	29	27	20	22	30	28	1	1	0	2
			e+000.				e+000.		e+00							
0.	9	0	C	0	21	23	31	29	22	24	32	30	1	1	0	2
			e+000.				e+000.		e+00							
0.	10	0	C	0	25	27	35	33	26	28	36	34	1	1	0	2
			e+000.				e+000.		e+00							
0.	11	0	C	0	27	29	37	35	28	30	38	36	1	1	0	2
			e+000.				e+000.		e+00							
0.	12	0	C	0	29	31	39	37	30	32	40	38	1	1	0	2
			e+000.				e+000.		e+00							
0.	13	0	C	0	33	35	43	41	34	36	44	42	1	1	0	2
			e+000.				e+000.		e+00							
0.	14	0	C	0	35	37	45	43	36	38	46	44	1	1	0	2
			e+000.				e+000.		e+00							
0.	15	0	C	0	37	39	47	45	38	40	48	46	1	1	0	2
			e+000.				e+000.		e+00							

hard,
prof
end

new,main,nonl,cart,0,21,21

main structure

refn,21

1	0.	e+00	0.	e+00	0.	e+00
2	0.1800000e+02	0.	e+00	0.	e+00	0.
3	0.3600000e+02	0.	e+00	0.	e+00	0.
4	0.5400000e+02	-0.4023090e+01	0.	e+00	0.	e+00
5	0.6717671e+02	-0.1000000e+02	0.	e+00	0.	e+00
6	0.7200000e+02	-0.3000000e+02	0.	e+00	0.	e+00
7	0.7200000e+02	-0.7400000e+02	0.	e+00	0.	e+00
8	0.7200000e+02	-0.1120000e+03	0.	e+00	0.	e+00
9	0.7682310e+02	-0.1300000e+03	0.	e+00	0.	e+00
10	0.9000001e+02	-0.1431769e+03	0.	e+00	0.	e+00
11	0.1080000e+03	-0.1480000e+03	0.	e+00	0.	e+00
12	0.1566000e+03	-0.1480000e+03	0.	e+00	0.	e+00
13	0.2052000e+03	-0.1480000e+03	0.	e+00	0.	e+00
14	0.2538000e+03	-0.1480000e+03	0.	e+00	0.	e+00
15	0.3024000e+03	-0.1480000e+03	0.	e+00	0.	e+00
16	0.3510000e+03	-0.1480000e+03	0.	e+00	0.	e+00
17	0.3689999e+03	-0.1431770e+03	0.	e+00	0.	e+00
18	0.3821770e+03	-0.1299999e+03	0.	e+00	0.	e+00
19	0.3870000e+03	-0.1120000e+03	0.	e+00	0.	e+00
20	0.3870000e+03	-0.6000000e+01	0.	e+00	0.	e+00

9999

cons,1

s001 1
9999 9999

boun,2

1 111111
9999 111111

Table 2.6.2 (cont'd)

```

nord,opto
prof
end
fini
mode
tree,main
fini
moui
news,001
pas,25
  10 0.22187e-03 0.22187e-03 0.22187e-03 0. e+00 0. e+00 0. e+0000
  30 0.44375e-03 0.44375e-03 0.44375e-03 0. e+00 0. e+00 0. e+0000
  50 0.44375e-03 0.44375e-03 0.44375e-03 0. e+00 0. e+00 0. e+0000
  70 0.22187e-03 0.22187e-03 0.22187e-03 0. e+00 0. e+00 0. e+0000
  90 0.44375e-03 0.44375e-03 0.44375e-03 0. e+00 0. e+00 0. e+0000
 110 0.88750e-03 0.88750e-03 0.88750e-03 0. e+00 0. e+00 0. e+0000
 130 0.88750e-03 0.88750e-03 0.88750e-03 0. e+00 0. e+00 0. e+0000
 150 0.44375e-03 0.44375e-03 0.44375e-03 0. e+00 0. e+00 0. e+0000
 170 0.44375e-03 0.44375e-03 0.44375e-03 0. e+00 0. e+00 0. e+0000
 190 0.88750e-03 0.88750e-03 0.88750e-03 0. e+00 0. e+00 0. e+0000
 210 0.88750e-03 0.88750e-03 0.88750e-03 0. e+00 0. e+00 0. e+0000
 230 0.44375e-03 0.44375e-03 0.44375e-03 0. e+00 0. e+00 0. e+0000
 250 0.44375e-03 0.44375e-03 0.44375e-03 0. e+00 0. e+00 0. e+0000
 270 0.88750e-03 0.88750e-03 0.88750e-03 0. e+00 0. e+00 0. e+0000
 290 0.88750e-03 0.88750e-03 0.88750e-03 0. e+00 0. e+00 0. e+0000
 310 0.44375e-03 0.44375e-03 0.44375e-03 0. e+00 0. e+00 0. e+0000
 330 0.44375e-03 0.44375e-03 0.44375e-03 0. e+00 0. e+00 0. e+0000
 350 0.88750e-03 0.88750e-03 0.88750e-03 0. e+00 0. e+00 0. e+0000
 370 0.88750e-03 0.88750e-03 0.88750e-03 0. e+00 0. e+00 0. e+0000
 390 0.44375e-03 0.44375e-03 0.44375e-03 0. e+00 0. e+00 0. e+0000
 410 0.22187e-03 0.22187e-03 0.22187e-03 0. e+00 0. e+00 0. e+0000
 430 0.44375e-03 0.44375e-03 0.44375e-03 0. e+00 0. e+00 0. e+0000
 450 0.44375e-03 0.44375e-03 0.44375e-03 0. e+00 0. e+00 0. e+0000
 470 0.22187e-03 0.22187e-03 0.22187e-03 0. e+00 0. e+00 0. e+0000
99990 0.10000e+01
end
new,main
pas,20
  10 0.26060e-03 0.26060e-03 0.26060e-03 0. e+00 0. e+00 0. e+0000
  20 0.52119e-03 0.52119e-03 0.52119e-03 0. e+00 0. e+00 0. e+0000
  30 0.53039e-03 0.53039e-03 0.53039e-03 0. e+00 0. e+00 0. e+0000
  40 0.53958e-03 0.53958e-03 0.53958e-03 0. e+00 0. e+00 0. e+0000
  50 0.53958e-03 0.53958e-03 0.53958e-03 0. e+00 0. e+00 0. e+0000
  60 0.81994e-03 0.81994e-03 0.81994e-03 0. e+00 0. e+00 0. e+0000
  70 0.11003e-02 0.11003e-02 0.11003e-02 0. e+00 0. e+00 0. e+0000
  80 0.81994e-03 0.81994e-03 0.81994e-03 0. e+00 0. e+00 0. e+0000
  90 0.53958e-03 0.53958e-03 0.53958e-03 0. e+00 0. e+00 0. e+0000
 100 0.53958e-03 0.53958e-03 0.53958e-03 0. e+00 0. e+00 0. e+0000
 110 0.97340e-03 0.97340e-03 0.97340e-03 0. e+00 0. e+00 0. e+0000
 120 0.14072e-02 0.14072e-02 0.14072e-02 0. e+00 0. e+00 0. e+0000
 130 0.14072e-02 0.14072e-02 0.14072e-02 0. e+00 0. e+00 0. e+0000
 140 0.14072e-02 0.14072e-02 0.14072e-02 0. e+00 0. e+00 0. e+0000
 150 0.14072e-02 0.14072e-02 0.14072e-02 0. e+00 0. e+00 0. e+0000
 160 0.97340e-03 0.97340e-03 0.97340e-03 0. e+00 0. e+00 0. e+0000
 170 0.53958e-03 0.53958e-03 0.53958e-03 0. e+00 0. e+00 0. e+0000
 180 0.53958e-03 0.53958e-03 0.53958e-03 0. e+00 0. e+00 0. e+0000

```

Table 2.6.2 (cont'd)

```

190 0.18044e-02 0.18044e-02 0.18044e-02 0.      e+00 0.      e+00 0.      e+0000
200 0.15346e-02 0.15346e-02 0.15346e-02 0.      e+00 0.      e+00 0.      e+0000
end
fini
impa,1
sur1 1 0.40000000e+00 0.10000000e+03 0.      e+00 0.      e+00
s001 5 0.      0.      0.      0.      0.      0.      0.      0.      0.      0.
1 3 5 7
9 11 13 15
17 19 21 23
25 27 29 31
33 35 37 39
41 43 45 47
wain 4
16 17 18 19
fini
ptre
newr, recl, pair, 8, 100
(2e15.7)
0.      e+00 0.      e+00
0.6500000e+03 0.1000000e-03
0.8800000e+03 0.1000000e-02
0.1000000e+04 0.2000000e-02
0.8800000e+03 0.3000000e-02
0.7800000e+03 0.5000000e-02
0.4300000e+03 0.2000000e-01
0.4300000e+03 0.1000000e+02
fini
thou, 343
8 344 3 1 0 0
197 344 1 1 0 0
2 0 0
ndyn
mass
dylo, 1, 1
recl 0 0.      1.00 2
20 19
timo, rsl, 1, 0.1000e+01
auto, def
inte, newm, 0.5000e-03, 0.e+00, 0.e+00, 0.1000e+00
stif
stif, upda
kinr, 12
elmr, 1, 2, 6, 3
kinr, 5
loop, 200
zero, ltwe
impa, init, 0.e+00, 0.e+00
step
unba
auto, init
loop, 30
stif
auto, load
load
disp

```

Table 2.6.2 (cont'd)

```
iapa,anal
kinr,10
elmr,9,10
auto,terr,0.5000e+02,0.2500e+03
if,3,3,1,1
entr,1
auto,fact
kinr,1
iapa,upda,0
if,3,2,2,3
entr,2
elmr,1
cont
goto,0
entr,3
auto,step,0.1000e-04,0.1000e-02,0.5000e+00,0.2000e+01
if,4,5,5,4
entr,4
inte,newm,,auto,0.e+00,0.e+00,0.e+00,0.1000e+00
entr,5
if,3,6,6,7
entr,6
kinr,12
elmr,5,2,6
kinr,5
iapa,upda,1
stif,init
goto,8
entr,7
chou
iapa,mome
iapa,rslt
elmr,1,2,4,6,11
kinr,4,9,11
wrou
zero,1rsb
unba
summ
elmr,3
kinr,3
stif,upda
auto,exit,0.1000e+00
if,5,8,8,0
entr,8
cont
fini
stop
```

D2.7 ELBOW IMPACT ON RIGID STRUCTURE

D2.7.1 PURPOSE

The main purpose of this example is to test the ELBO substructure, impact analysis, and initial velocity options. A secondary purpose is to obtain an indication of the impact forces likely to be developed when a pipe elbow impacts on a rigid surface, allowing for local deformation of the elbow.

D2.7.2 DESCRIPTION

D2.7.2.1 ELBO and SLAB Substructures

In the example analyzed in Section D2.3, an unrestrained pipe underwent large displacements and then impacted an essentially rigid surface. The surface was modelled using very stiff GAPP elements, and it was noted that the computed impact force was probably not a realistic value.

In order to compute realistic impact forces for this type of problem, it is necessary to allow for local deformations of the pipe (and possibly of the impacted surface) near the point of contact. This can be done accurately only by modelling the pipe as a mesh of shell elements and performing an impact analysis.

With WIPS, it is possible to model the impacting pipe elbow as a substructure composed of SHELL elements. For the analysis described in this section, the elbow and short lengths of adjacent straight pipe were modelled, with 20 elements around the circumference and 16 elements longitudinally (10 in the elbow, 3 each in the adjacent lengths of straight pipe). For the analysis, only in-plane pipe motion was allowed, so that only one-half of the circumference was considered. The resulting mesh was thus 10 x 16. This is probably the coarsest mesh which can be expected to give reasonable results. For an accurate analysis a finer mesh is probably needed. The ELBO substructure is shown in Fig. 2.7.1.

The impacted surface can also be modelled using SHELL elements, as a SLAB substructure. For this analysis, only a 1 x 1 mesh was specified, producing a rigid surface.

D2.7.2.2 Piping Model

For parts of the pipe away from the impacting elbow, PIPE elements may be specified. It is possible to specify the same overall geometry as in Section D2.3. If this were done, however, a large amount of computer time would be required to perform the pre-impact analysis, yet the impacting elbow would undergo negligible deformation before impact.

For this reason, the specified geometry was somewhat different from that in Section D2.3. The geometry used is shown in Fig. 2.7.2. The choice was based on the following observations.

The analyses of Section D2.3 showed that before impact the pipe essentially hinged about the second elbow. These analyses also showed that the impacting pipe was inclined at approximately 24 degrees to the horizontal at impact, with an angular velocity of approximately 6.45 radians/second. The geometry was thus modified to place a hinged support at the approximate location of the plastic hinge; to locate a SLAB substructure just below the elbow, with a 24 degree inclination; and to specify an initial angular velocity of 6.45 radians/second about the hinge support. The geometry thus approximated the geometry of the Section D2.3 model just before impact.

D2.7.3 WIPS ANALYSIS MODEL

Table 2.7.1 shows the WIPSLOG listing for all phases of the data specification. This listing is largely self-explanatory. It may be noted that a time delay of -0.107 seconds (the time to impact calculated in Section D2.3) was specified in the WIPS-DATA phase. With this delay,

the jet force applied at time zero in the analysis corresponds to the force at the impact time. Table 2.7.2 shows the DATA file.

As with the example in Section D2.6, the DATA file was prepared on the University of California VAX computer and transferred to the Lawrence Livermore National Laboratory CRAY for execution.

D2.7.4 RESULTS

D2.7.4.1 General

As noted earlier in this section, the finite element mesh for the ELBO substructure was coarser than would probably be needed for an accurate analysis. Also, rate dependence in the pipe steel was not considered. Hence, this example serves primarily to confirm the contact analysis capabilities of WIPS, not to calculate correct impact forces.

Initial impact occurred at 0.0004 seconds, and the analysis was continued to .0048 seconds, for a total of some 30 time steps. Each time step required a number of substeps. In the last step the allowable substep limit was exceeded, and the analysis stopped. To continue the analysis it would be necessary to restart with a smaller time step or a larger substep limit.

D2.7.4.2 Elbow Deformations

Fig. 2.7.3 shows a side view of the elbow at the end of the analysis. Fig. 2.7.4 shows a cross section of the elbow near the center of the impacting region at initial impact and at three times after impact. These figures confirm that the elbow flattens against the rigid slab surface and show that the elbow separates from the surface in the center of the contact area. Qualitatively, this behavior is correct. More extensive studies are needed to determine whether WIPS produces quantitatively correct results.

D2.7.4.3 Impact Forces

Fig. 2.7.5 shows the variation with time of the calculated normal impact force (the sum over all contacting nodes at each time). The variation is rather erratic, suggesting that a shorter time step should have been used. As already noted, however, the calculated contact force is not necessarily realistic. The maximum value is much less than that calculated in Section D2.3.

D2.7.5 CONCLUSION

This example indicates that the contact analysis algorithm in WIPS performs as intended and that the shell element in ELBO substructures is capable of modelling large deformations of a pipe. Until more experience is gained, however, the results of analyses of this type should be interpreted cautiously for practical application.

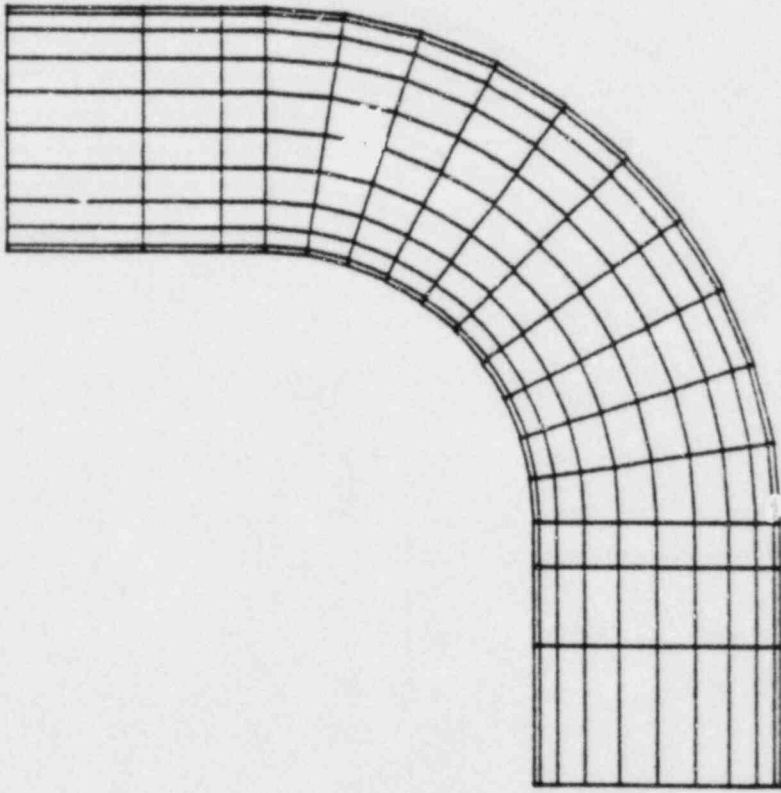


FIG. 2.7.1 ELBOW SUBSTRUCTURE.

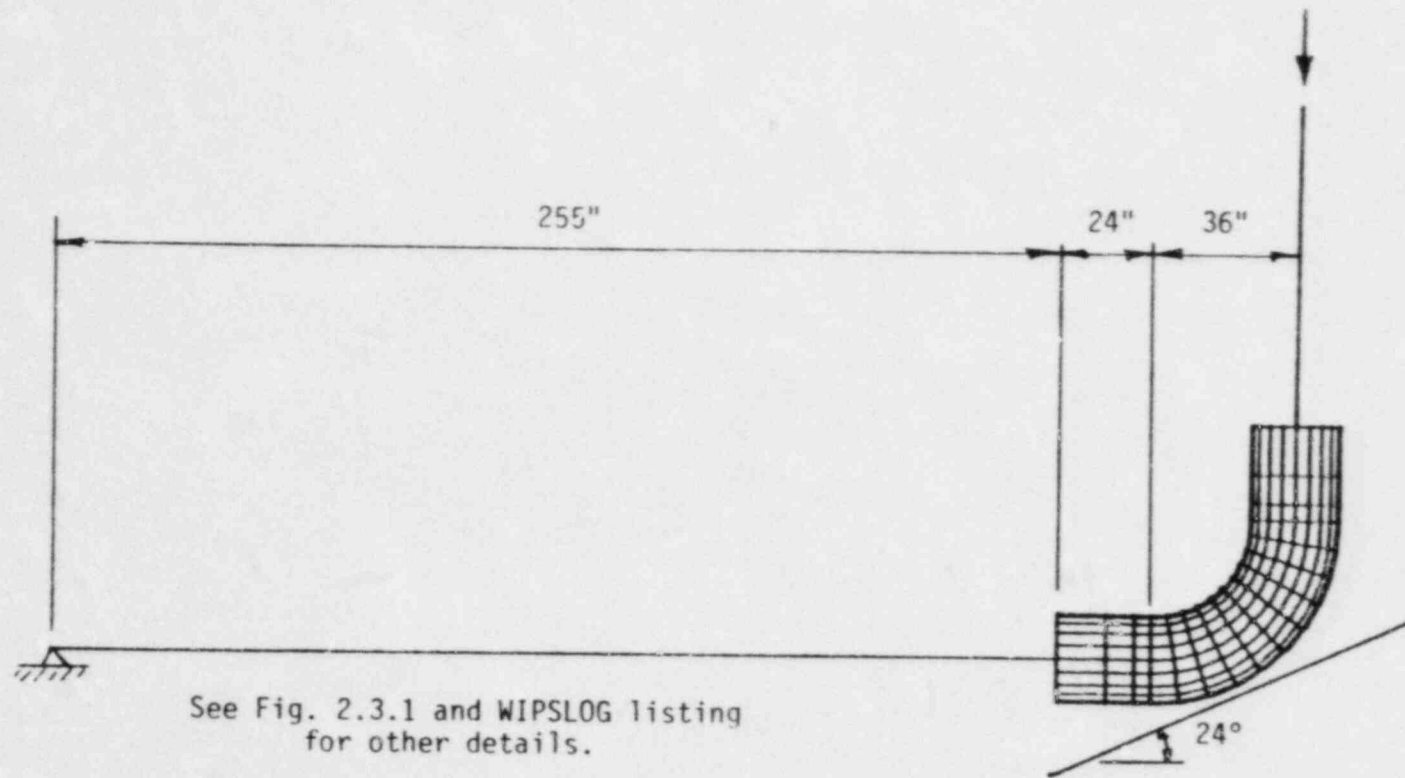


FIG. 2.7.2 PIPE WITH ELBOW AND SLAB SUBSTRUCTURES.

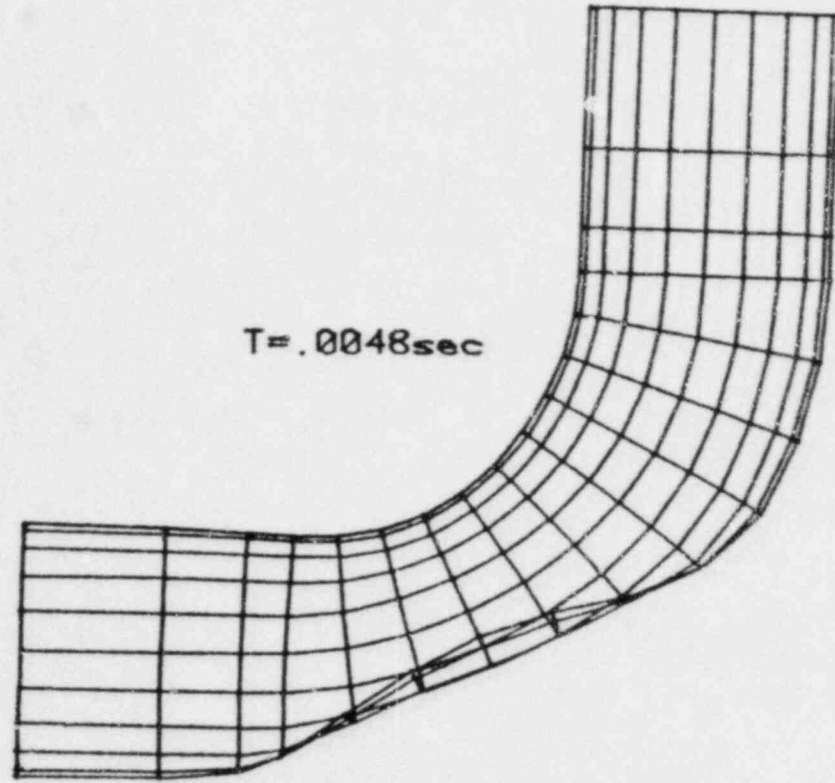


FIG. 2.7.3 DEFORMED ELBOW SUBSTRUCTURE.

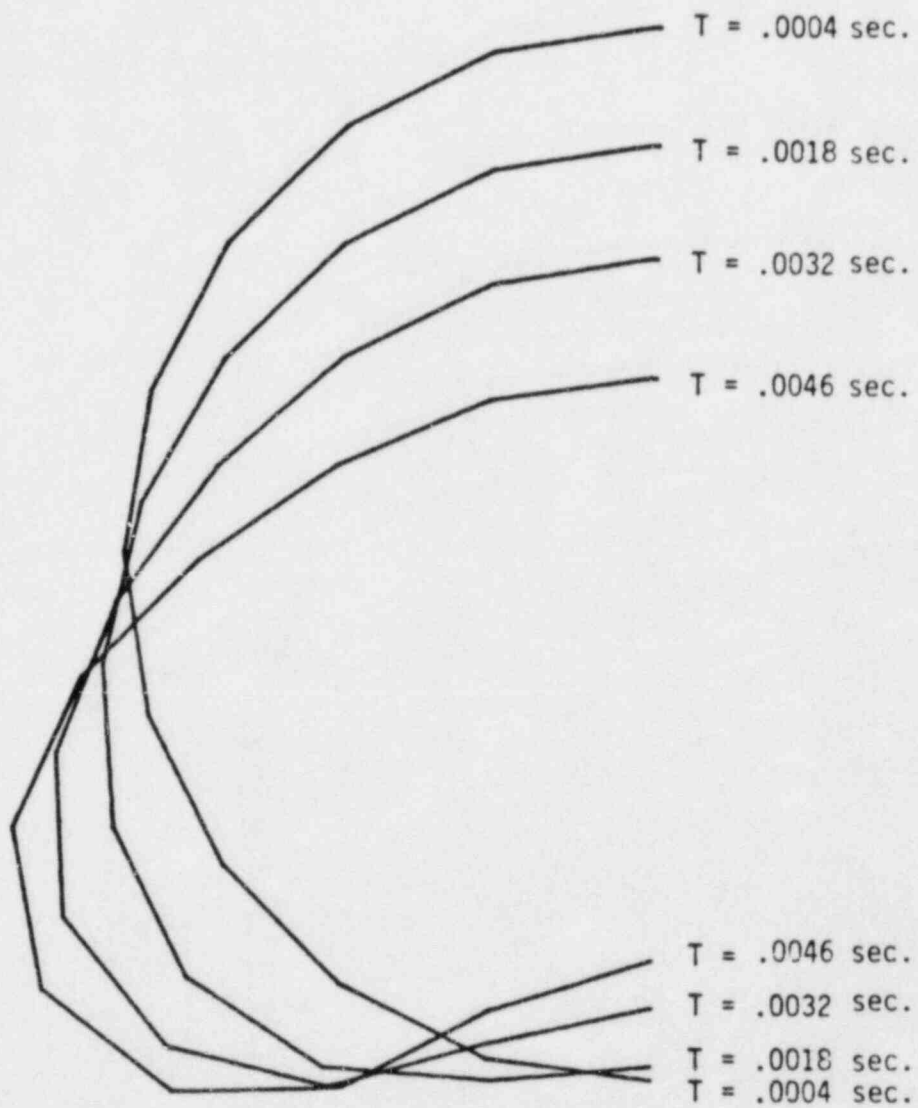


FIG. 2.7.4 CROSS SECTION DEFORMATIONS
NEAR CENTER OF CONTACT REGION

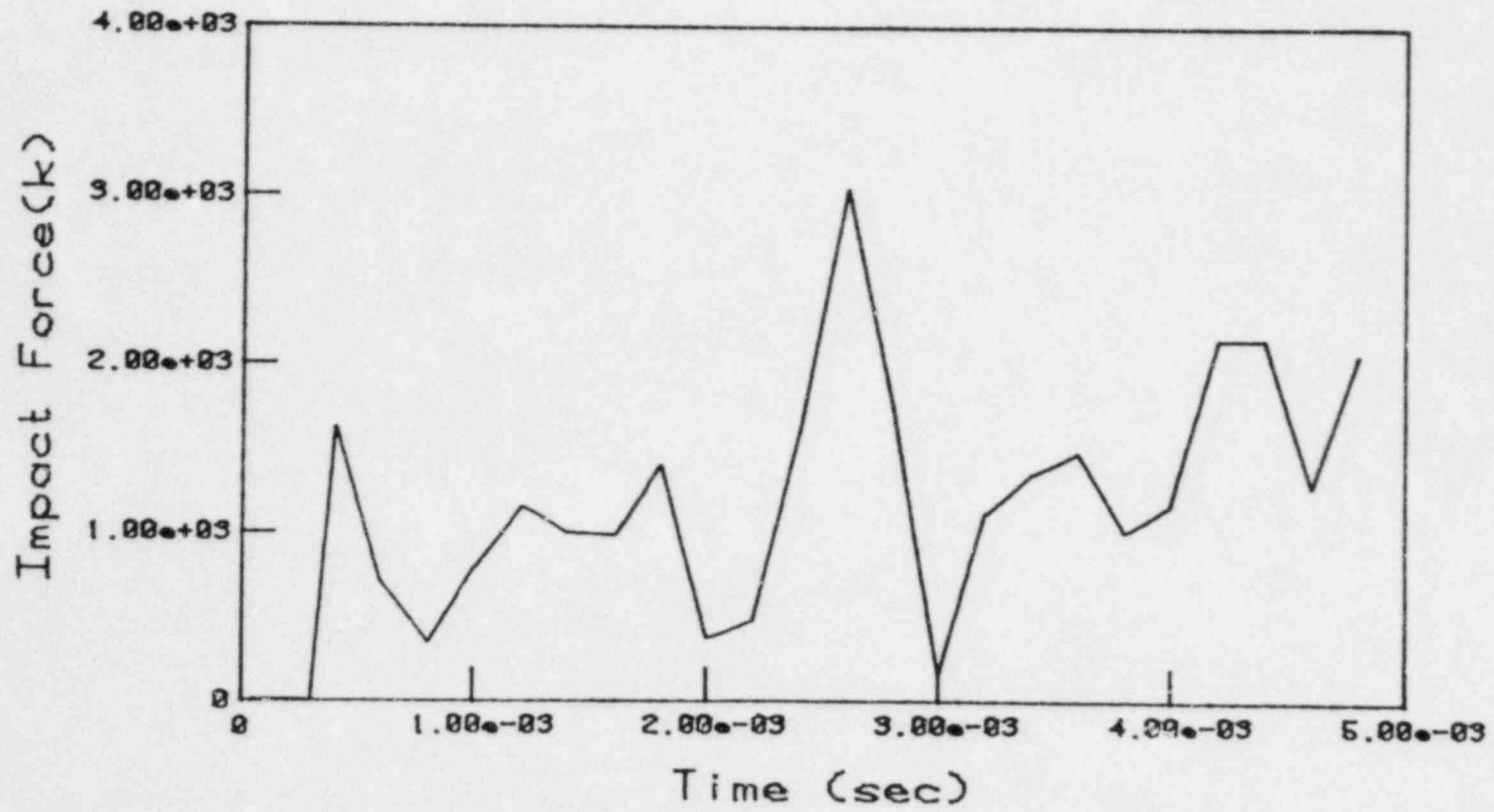


FIG. 2.7.5 IMPACT FORCE TIME HISTORY.

TABLE 2.7.1 - WIPSLOG LISTING - GEOM, MATL, PIPE, SLAB,
FREC, MODL, AND DATA PHASES

EXEC - WIPS EXECUTIVE
Creating problem no. 1
Problem description: Test case, EBBB substructure impact on rigid surface

NEXT WIPS-EXEC COMMAND : geom

GEOM - SPECIFICATION OF SYSTEM GEOMETRY

Define units
Length (ft, in, m, mm) : in
Force (k, lb, kgf, kN) : k

Specify new GEOM data

START RUN NO. 1
Enter c.p. data in sequence along run

c.p. name and type : 1
ccord option : di
x,y,z :
Any changes? :

c.p. name and type : 2
no. of extra nodes : 3
ccord option :
c.p. dx,dy,dz : 1,2,5
offset points defaults to preceding c.p.
Any changes? :

c.p. name and type : 3 to
no. of extra nodes :
ccord option :
to generate automatically
Any changes? :

c.p. name and type : ti ti
bend radius : 36
ccord option :
c.p. dx,dy,dz : 2,0,0
Any changes? :

c.p. name and type : 4 to
no. of extra nodes :
ccord option :
to generate automatically
Any changes? :

c.p. name and type : 5
no. of extra nodes :
ccord option :
c.p. dx,dy,dz : ti,0,0
Any changes? :

c.p. name and type : 6
no. of extra nodes :
ccord option :

Table 2.7.1 (cont'd)

c.p. dx,dy,z : rate
 offset point defaults to preceding c.p.
 Any changes? :

c.p. name and type :
 Last c.p. in this run? : y
 Display GEOM data for this run? : y

GEOM DATA FOR RUN

run no.	c.p. name	c.p. type	band radius	extra nodes	coord opt	c.p. i	c.p. i ?	coordinate data		
								x,0,0	y,dy	z,0z
1										
	1			0	di			0.	0.	0.
	2			0	cf	1		255.000	0.	0.
	3	tn		0	tn			0.	0.	0.
	ti	ti	36.000	0	cf	2		60.000	0.	0.
	4	tn		0	tn			0.	0.	0.
	5			0	cf	ti		0.	60.000	0.
	6			0	of	5		0.	62.000	0.

END OF DATA

START RUN NO. 2
 Enter c.p. data in sequence along run

c.p. name and type :
 Last run? : y

Display new GEOM data? :
 Write in session log? :

Modify GEOM data? :

Save current GEOM data? : y
 Comment for file catalog :
 GEOM DATA SAVED. FILE NAME = GEUMC101

Produce COOR data? : y

Display COOR data? : y

COOR DATA

run no.	c.p. name	c.p. type	band radius	node no.	COORD		
					x	y ?	z
1							
	1			1	0.	0.	0.
				2	63.750	0.	0.
				3	127.500	0.	0.
				4	191.250	0.	0.
	2			5	255.000	0.	0.
	3	tn		6	279.000	0.	0.
	ti	ti	36.000		315.000	0.	0.

Table 7.1 (cont'd)

		center		279.000	36.000	0.
4	in		7	315.000	36.000	0.
5			8	315.000	60.000	0.
HIL RETURN for more						
6			9	315.000	142.000	0.
END OF DATA						

Plot geometry? :

Modify GEM data? :

DATA COMPLETE FOR THIS SESSION!

Save final GEM data? : y

Comment for file catalog : For EEBD substructure

GEM DATA SAVED. FILE NAME = GEMG101

Save CGUR data? : y

Comment for file catalog : From GEMG101

CGUR DATA SAVED. FILE NAME = CGUR0101

End of this GEM session

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : matl

MATL - SPECIFICATION OF MATERIAL PROPERTIES

Define units

Length (ft, in, mm) : in

Force (k, lb, kgf, kN) : k

Start new MATL file

Specify a new property set? : y

SET NO. = 1

Property set description : Trilinear, no strain rate.

Stair moduli (min=2,max=5)

: 26700 210 20

Yield strengths (no. of moduli minus 1)

: 26.7 44

Strain rate stiffnesses (min=0,max=3)

:

No strain rate effect

Use default tolerances? :

Yield tolerance (dflt=.02) : .1

Stiffness tolerance (dflt=.05) : .1

Poisson ratio (dflt = .3) :

Weight density (dflt=steel) :

Any errors? :

This set added to MATL file

Specify a new property set? : y

Table 2.7.1 (cont'd)

```

SET NO. = 2
Property set description : Elastic
Static moduli (min=,max=5)
: 26700 26000
Yield strengths (no. of moduli minus 1)
: 1ee
Strain rate stiffnesses (min=0,max=3)
:
No strain rate effect
Use default tolerances? : y
Poisson ratio (dfit = .3) :
Weight density (dfit=steel) :
    
```

Any errors? :

This set added to MAIL file

Specify a new property set? :

No. of property sets in MAIL file = 2

Display property set descriptions? : y

MATL PROPERTY DESCRIPTIONS

```

Set No.  Type  Description
  1      mroz  Trilinear, no strain rate.
  2      mroz  Elastic
    
```

Display new property set data? : y

MATL PROPERTY DATA

SET NO. 1. Trilinear, no strain rate.

Matl Type	Data Type	Seam No.	Modulus or Coefficient	Stress/Strain Limit
mroz	static	1	0.2670e+05	0.2670e+02
		2	0.2190e+05	0.4400e+02
		3	0.2000e+02	
	ld.tol.		0.1000e+00	
	slf.tol		0.1000e+00	
	rate.tol		0. e+00	
	poisson		0.3000e+00	
	density		0.2840e-03	

Hit RETURN for next set

SET NO. 2. Elastic

Matl Type	Data Type	Seam No.	Modulus or Coefficient	Stress/Strain Limit
mroz	static	1	0.2670e+05	0.1000e+09
		2	0.2600e+05	

Table 2.7.1 (cont'd)

```

      ,E,tol,      0.2000e-01
      ,Kif,tol,    0.5000e-01
      ,rate,tol,   0.5000e-01
      ,viscos,     0.3000e+00
      ,density,    0.2590e-03
Hit RETURN for next set
END OF DATA

Display all property set data? :
Write in session log? :

New MAIL file created
Comment for file catalog : 2 materials

End this MAIL session? : y

EXEC - WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : elbc

ELBC - SPECIFICATION OF ELBC PROPERTIES

Define units
  Length (ft,in,mm) : in
  Force (k,lb,kgf,kh) : k

No. of MAIL property sets available = 2
Display material descriptions? : y

MAIL PROPERTY DESCRIPTIONS
  Set No. Type Description
    1  mrc Trilinear, no strain rate.
    2  mrc Elastic

Start new ELBC file

Specify a new property set? : y

SET NO. 1

Substructure description : 24in OD, 1.531 WT, 5K.
No. of circumf. divisions : 20
First Tangent
  Length : 24
  No. of divisions : 2
  Mesh factor : 1.75
  Outside diameter : 24
  Wall thickness : 1.531
  No. of integ. pts thru thickness : 5
Elbow
  End radius : 36
  End angle (deg) : 90
  No. of divisions : 10
  Outside diameter : 24
  Wall thickness : 1.531

```


Table 2.7.1 (cont'd)

```

    No. of integ. pts thru thickness : 5
Second tangent
    Length : 24
    No. of divisions : 5
    Mesh factor : 1.75
    Outside diameter : 24
    Wall thickness : 1.531
    No. of integ. pts thru thickness : 5
Material numbers (tangent, elbow, tangent) : 1 1 1

Any errors? :

This set added to ELBU file

Specify a new property set? :

No. of property sets in ELBU file = 1

Display property set descriptions? : y

ELBU PROPERTY DESCRIPTIONS
  Set No.  Description
      1    24in OD, 1.531 WT, SR.

Display new property data? : y

ELBU PROPERTY DATA

SET NO.  1.  24in OD, 1.531 WT, SR.
  Circumferential divisions = 20

      Tangent 1      Elbow      Tangent 2
Length      0.2400e+02      10      0.2400e+02
Divisions      5      10      5
Mesh factor    0.1750e+01      10      0.1750e+01
Diameter      0.2400e+02      0.2400e+02      0.2400e+02
Thickness     0.1531e+01      0.1531e+01      0.1531e+01
Bend radius   0.3600e+02
Angle (deg)   0.9000e+02
Integ. order   5      5      5
Material no.   1      1      1
Hit RETURN for next set
END OF DATA

Display all property data? :
Write in session log? :

New ELBU file created
Comment for file catalog : 1 set

End this ELBU session? : y

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : show

```

Table 2.7.1 (cont'd)

SLAB - SPECIFICATION OF SLAB PROPERTIES

Define units

Length (f, in, mm) : in
Force (k, lb, kgf, KN) : k

No. of MATL property sets available = 2
Display material descriptions? : y

MATL PROPERTY DESCRIPTIONS

Set No.	Type	Description
1	MP02	Trilinear, no strain rates
2	MP02	Elastic

Start new SLAB file

Specify a new property set? : y

SET NO. 1

Substructure description : Elastic, rigid because single element

Length of side OA : 100

Length of side OB : 100

Outer strip widths (proportions of OA)

Left strip :

Right strip :

Outer strip widths (proportions of OB)

Bottom strip :

Top strip :

No. of subdivisions along OA

Center strip : 1

No. of subdivisions along OB

Center strip : 1

Slab thickness : 2

No. of Gauss points thru thickness

Center region : 2

Outer regions : 2

Direction cosines of OA,OB

OA (3 values) : 0 0 1

OB (3 values) : .9135 .4067 0

Coords of point O (X,Y,Z values) : 253.45 -29.56 -50

Boundary codes (free, hinged, clamp, syxy, syyz, or syxz)

OA : hing

OB : hing

OC : hing

AC : free

Material set number : 2

Any errors? :

This set added to SLAB file

Specify a new property set? :

No. of property sets in SLAB file = 1

Table 2.7.1 (cont'd)

```

Display property set descriptions? : y
SLAB PROPERTY DESCRIPTIONS
Set No.  Description
  1      Elastic, rigid because single element

Display new property data? : y
SLAB PROPERTY DATA
SET NO.  1.  Elastic, rigid because single element
           First      Center      Last
           Strip      Strip      Strip
Widths along DA      0.      e+00      0.1000e+03      0.      e+00
Widths along DB      0.      e+00      0.1000e+03      0.      e+00
Elements along DA      0      1      0
Elements along DB      0      1      0
Thicknesses      0.2000e+01      0.2000e+01      0.2000e+01
No. of Gauss. points      2      2      2

           X      Y      Z
Direction cosines
  Edge DA      0.      e+00      0.      e+00      0.1000e+01
  Edge DB      0.9130e+00      0.4007e+00      0.      e+00
Coordinates of U      0.2534e+03      -0.2950e+02      -0.5000e+02

Boundary codes DA,DC = hing, hing
Boundary codes UB,AC = hing, free
Hit RETURN for next set
END OF DATA

Display all property data? :
Write in session log? :

New SLAB file created
Comment for file catalog : 1 set

End this SLAB session? : y

EXEC - WIPS EXECUTIVE
NEXT WIPS-EXEC COMMAND : free

FREE - SPECIFY DYNAMIC FORCE RECORDS

Define units
  Length (ft, in, mm) : in
  Force (k, lb, ksf, KN) : k

Start new FREE file

Specify a new record? : y
RECORD NO.  1

```

Table 2.7.1 (cont'd)

Record name (4 characters) : rec1
 Description (max. 40 char.) : Hibbitt record, max. 1000k.

Enter Time-Force pairs
 First pair automatically set to 0,0

Pair no. 2 : .0001 650
 Pair no. 3 : .001 120
 Pair no. 4 : .002 1000
 Pair no. 5 : .003 120
 Pair no. 6 : .005 720
 Pair no. 7 : .02 430
 Pair no. 8 : 10 430
 Pair no. 9 :

Last pair? : ,
 Any errors? :

Specify a new record? :

Display any records? : y
 Record number (dflt=all) :

RECORD NO.	1.	Name = rec1
Time		Force
0.	0.	e+00
0.00010	0.	6500e+03
0.00100	0.	8800e+03
0.00200	0.	1000e+04
0.00300	0.	8800e+03
0.00500	0.	7200e+03
0.02000	0.	4300e+03
10.00000	0.	4300e+03

END OF RECORD

Write records in session log? :

End this FREC session? : y
 New FREC file created
 Comment for file catalog : 1 record

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : pipe

PIPE - SPECIFICATION OF PIPE PROPERTIES

Define units
 Length (ft, in, mm) : in
 Force (k, lb, kgf, kN) : k

No. of MATL property sets available = 2
 Display material descriptions? : y

MATL PROPERTY DESCRIPTIONS
 Set No. Type Description
 1 mrc Trilinear, no strain rate.

Table 2.7.1 (cont'd)

```

2      NEW Elastic
Start new PIPE file
Specify a new property set? : y
SET NO. = 1
Property set description : 24in OD, 1.531in WT.
  Outside diameter : 24
  Wall thickness : 1.531
  Weight/unit length (dflt=pipe weight) :
  No. of X-section elements (dflt=12) :
  Material number : 1
  Large ovalling (yes or no)? (dflt=no) :
Use default ovalling properties? : y

Any errors? :

This set added to PIPE file
Specify a new property set? :

No. of property sets in PIPE file = 1
Display property set descriptions? : y
PIPE PROPERTY DESCRIPTIONS
  Set No.  Description
    1      24in OD, 1.531in WT.
Display new property set data? : y
PIPE PROPERTY DATA
SET NO.  1.  24in OD, 1.531in WT.

```

Data type	Seqm no.	Modulus or Data Value	Stress/Strain Limit
Outside diameter		0.2400e+02	
Wall thickness		0.1531e+01	
Unit weight		0.3069e-01	
No. of elements		12	
No. of slices		2	
Stress v strain	1	0.2670e+05	0.2670e+02
	2	0.2190e+03	0.4400e+02
	3	0.2000e+02	
Poisson ratio		0.3000e+00	
Large ovalling, ovalling ratios		no	
	1	0.3500e+00	
	2	0.3000e-01	

```

Hit RETURN for next set
END OF DATA

Display all property set data? :
write in session log? :

```

Table 2.7.1 (cont'd)

```

New PIPE file created
Comment for file catalog : isc

End this PIPE session? : y

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : w001

MODL - SPECIFICATION OF ANALYSIS MODEL

Define units
Length (ft, in, mm) : in
Force (k, lb, kgf, kN) : k

Sequence no. of CDDK file : 1

Available element property sets
Type      No. of Sets
pipe      1
Available substructure property sets
Type      No. of Sets
elbo      1
slab      1

DEFINE MODEL IN SEGMENTS

SEGMENT NO. 1

Pipe run no. : 1
First c.p. of segment : 1
Full 3D motion? :
Displacement plane (xy, yz or zx) : xy
Any substructures in this segment? : y
They must lie on +z or -z side of plane
Specify side (+ or -) : +
Boundary condition code for first c.p. : 11110

Specify c.p. name + elem. type + optional data
1: 2 pipe prop=1 ldis
1: 2 pipe prop
2: 2 pipe prop=1 ldis=yes this=no
2: 5 elbo prop=1 name=elbo this=no ldis=yes
3: 6 pipe
4:
End of segment? : y
Display commands for this segment? : y

MODL COMMAND TABLE

SEGMENT NO. 1  Run No. = 1
  c.p. elem.  Optn  data      Optn  data      Optn  data
  1
                beam  11110

```

Table 2.7.1 (cont'd)

```

2      pipe      prop      1
          locl      +
          wfac     1.000      ldis      yes      this      no

5      elbo      prop      1
          name     elbo      ldis      yes      this      no
          wfac     1.000

6      pipe      prop      1
          locl      +
          wfac     1.000

```

Hit RETURN for more
Any changes? :

SEGMENT NO. 2

Pipe run no. :
Last segment? : y

Any external substructures? : y
Specify substructure type + optional data
1 : slab prop=1 name=slab this=no
More external substructures? :
Display commands for external substructures? : y

MODEL COMMAND TABLE

```

EXTERNAL SUBSTRUCTURES
  type  optn  data  optn  data  optn  data
  slab
          prop      1
          name     slab      ldis      yes      this      no
          wfac     1.000

```

Any changes? : y
Redefine all external substructures

Any external substructures? : y
Specify substructure type + optional data
1 : slab prop=1 name=slab this=no ldis=no
More external substructures? :
Display commands for external substructures? : y

MODEL COMMAND TABLE

```

EXTERNAL SUBSTRUCTURES
  type  optn  data  optn  data  optn  data
  slab
          prop      1
          name     slab      ldis      no      this      no
          wfac     1.000

```

Any changes? :
Display commands for all segments? :
Write in session log? :

Table 2.7.1 (cont'd)

```
Produce MODL file? : y
wait while data is processed

Impact analysis required? : y
No. of impact surface pairs : 1

SURFACE PAIR NO. 1
Surface pair name : surf

Define primary surface
Substructure name : slab
SLAE substructure, property set no. 1
Divisions along UA = 1
Divisions along UB = 1
Allowable grid range along UA = 1 thru 2
Allowable grid range along UB = 1 thru 2
Define grid ranges
UA : 1 2
UB : 1 2
Thickness from nodes to surface : 1

Define secondary nodes
Substructure name (oflt = main) : elbow
ELBC substructure, property set no. 1
Circumf. divisions = 20
Longitl. divisions = 10 ( 3, 10, 3)
Only first circumferential half of mesh used
Allowable grid range = 1 thru 11
Allowable longitudinal grid range = 1 thru 17
Define grid ranges
Circumferential : 5 11
Longitudinal : 4 13
Thickness from nodes to surface : .765
Friction coefficient (oflt=zero) :
Sliding veloc. for full friction (dflt=50in/sec) :
Any errors? :

Specify initial velocities? : y
Specify initial velocities for affected segments
Warning - only partial consistency check is performed on data
SEGMENT NO. : 1
Segment has transverse symmetry
Motion in x-y plane only
Name of pivot point (dflt = no pivot) : 1
Pivot axis = global z
Angular velocity (rad/sec, r.h.s. rule) : -6.45
SEGMENT NO. :
Last affected segment? : y
wait while data is processed
Comment for file catalog : -6.45 rad/sec, zero friction.

MODL file saved. File name = MODL0101
End of this MODL session

EXEC = WIPS EXECUTIVE
```


Table 2.7.1 (cont'd)

NEXT WIPS-EXEC COMMAND : Data

DATA - SET UP WIPS-ANAL INPUT DATA

Define units

Length (ft, in, mm) : in
Force (k, lb, kgf, kh) : k

Sequence no. of MODEL file : 1

Problem description (4 lines)

Line 1 : Test of elbow substructure impact on rigid slab substructure.
Line 2 :
Line 3 : Geometry similar to Hibbitt unrestrained example. Initial geometry
Line 4 : set to just before impact. 1000in/sec approx. impact velocity.

Set up FAUSE files at end of analysis ? : y
Wait while files are processed
Initial velocities may be scaled if desired
Specify scale factor (dfit=1.0) :

Specify data for each loaded point

LOAD NO. 1
Force record name : rec1
Name of loaded c.p. : 0
Force direction (x,y,z or follower) : full
Follower c.p. name : 5
Scale factor (+x= controls direction) : .5
Time delay (sec) (dfit=0) : -.107

LOAD NO. 2
Force record name :
Last load? : ,

Time steps : initial + max + min : 2e-4 .001 2e-6
Max steps + max total time : 200 .02
Error tolerances : upper + lower : 250 50

Results output intervals

Max. no. of steps : 1
Max. time (secs.) : .1
Integration scheme (newb or hilb)(dfit=newb) :
Damping factor (dfit=0.1) :
Factor for time step increase (dfit=2.0) :
Factor for time step decrease (dfit=0.5) :
Max. unbal. to reduce time step (dfit=no limit) :
Max. unbal. to stop analysis (dfit=no limit) :

DATA file set complete
Comment for file catalog : 200 steps, max 20msec.
WIPS-ANAL DATA FILES SET UP. PARENT FILE NAME = DATA0101

EXEC - WIPS EXECUTIVE

NEXT WIPS-EXEC COMMAND : quit

TABLE 2.7.2 - LISTING OF DATA FILE. PIPE WITH ELBO
SUBSTRUCTURE IMPACTING RIGID SURFACE.

```

ECH00101  SLE00101  FSLT0101  PAUL0101  PAUZO101
star,paus
gauj
new,elbo,nonl,curt,0,270,260
  elbow substructure. name = elbo
refn,376
  10.255000000e+030.112344799e+020.          e+00
  20.255000000e+030.120000000e+020.          e+00
  30.255000000e+030.106040447e+020.347165106e+01
  40.255000000e+030.114120787e+020.370820379e+01
  50.255000000e+030.908890152e+010.660347319e+01
  60.255000000e+030.970020427e+010.705342293e+01
  70.255000000e+030.660347414e+010.908890152e+01
  80.255000000e+030.705342288e+010.970820427e+01
  90.255000000e+030.347165227e+010.106840457e+02
  100.255000000e+030.370020475e+010.114120776e+02
  110.255000000e+030.848181173e-060.112344999e+02
  120.255000000e+030.905974044e-060.120000000e+02
  130.255000000e+03-.347165084e+010.106840447e+02
  140.255000000e+03-.370820332e+010.114120787e+02
  150.255000000e+03-.660347271e+010.908890152e+01
  160.255000000e+03-.705342245e+010.970820427e+01
  170.255000000e+03-.908890057e+010.660347462e+01
  180.255000000e+03-.970820230e+010.705342436e+01
  190.255000000e+03-.106840437e+020.347165442e+01
  200.255000000e+03-.114120700e+020.370820737e+01
  210.255000000e+03-.112344999e+020.437487552e-05
  220.255000000e+03-.120000000e+020.467297241e-05
  230.26764517.e+030.112344799e+020.          e+00
  240.26764517.e+030.120000000e+020.          e+00
  250.26764517.e+030.106040447e+020.347165106e+01
  260.26764517.e+030.114120787e+020.370820379e+01
  270.26764517.e+030.908890152e+010.660347319e+01
  280.26764517.e+030.970020427e+010.705342293e+01
  290.26764517.e+030.660347414e+010.908890152e+01
  300.26764517.e+030.705342388e+010.970820427e+01
  310.26764517.e+030.347165227e+010.106840457e+02
  320.26764517.e+030.370020475e+010.114120776e+02
  330.26764517.e+030.848181173e-060.112344999e+02
  340.26764517.e+030.905974044e-060.120000000e+02
  350.26764517.e+03-.347165084e+010.106840447e+02
  360.26764517.e+03-.370820332e+010.114120787e+02
  370.26764517.e+03-.660347271e+010.908890152e+01
  380.26764517.e+03-.705342245e+010.970820427e+01
  390.26764517.e+03-.908890057e+010.660347462e+01
  400.26764517.e+03-.970820230e+010.705342436e+01
  410.26764517.e+03-.106840437e+020.347165442e+01
  420.26764517.e+03-.114120700e+020.370820737e+01
  430.26764517.e+03-.112344799e+020.437487552e-05
  440.26764517.e+03-.120000000e+020.467297241e-05
  450.27487097.e+030.112344799e+020.          e+00
  460.27487097.e+030.120000000e+020.          e+00
  470.27487097.e+030.106040447e+020.347165106e+01
  480.27487097.e+030.114120787e+020.370820379e+01
  490.27487097.e+030.908890152e+010.660347319e+01
  500.27487097.e+030.970020427e+010.705342293e+01

```

Table 2.7.2 (cont'd)

510.27467097.e+030.660347414e+010.908890152e+01
 520.27467097.e+030.705342388e+010.970820427e+01
 530.27467097.e+030.347165227e+010.106846457e+02
 540.27467097.e+030.370820332e+010.114126778e+02
 550.27467097.e+030.848181172e-060.112344999e+02
 560.27467097.e+030.905974894e-060.120000000e+02
 570.27467097.e+030.347165084e+010.106846447e+02
 580.27467097.e+030.370820332e+010.114126767e+02
 590.27467097.e+030.660347271e+010.908890152e+01
 600.27467097.e+030.705342295e+010.970820427e+01
 610.27467097.e+030.908890057e+010.660347462e+01
 620.27467097.e+030.970820236e+010.705342436e+01
 630.27467097.e+030.106846437e+020.347165442e+01
 640.27467097.e+030.114126768e+020.370820757e+01
 650.27467097.e+030.112344999e+020.437487552e-05
 660.27467097.e+030.120000000e+020.467297241e-05
 670.279000000e+030.112344999e+020. e+00
 680.279000000e+030.120000000e+020. e+00
 690.279000000e+030.106846447e+020.347165106e+01
 700.279000000e+030.114126767e+020.370820379e+01
 710.279000000e+030.908890152e+010.660347319e+01
 720.279000000e+030.970820427e+010.705342293e+01
 730.279000000e+030.660347414e+010.908890152e+01
 740.279000000e+030.705342388e+010.970820427e+01
 750.279000000e+030.347165227e+010.106846457e+02
 760.279000000e+030.370820332e+010.114126778e+02
 770.279000000e+030.848181172e-060.112344999e+02
 780.279000000e+030.905974894e-060.120000000e+02
 790.279000000e+030.347165084e+010.106846447e+02
 800.279000000e+030.370820332e+010.114126767e+02
 810.279000000e+030.660347271e+010.908890152e+01
 820.279000000e+030.705342295e+010.970820427e+01
 830.279000000e+030.908890057e+010.660347462e+01
 840.279000000e+030.970820236e+010.705342436e+01
 850.279000000e+030.106846437e+020.347165442e+01
 860.279000000e+030.114126768e+020.370820757e+01
 870.279000000e+030.112344999e+020.437487552e-05
 880.279000000e+030.120000000e+020.467297241e-05
 890.282874175e+030.112344999e+020. e+00
 900.282754425e+030.122954798e+020. e+00
 910.282960205e+030.109983188e+020.347165106e+01
 920.282846313e+030.117153893e+020.370820379e+01
 930.283209819e+030.942022135e+010.660347319e+01
 940.283112948e+030.100318995e+020.705342293e+01
 950.283598605e+030.696539354e+010.908890152e+01
 960.283528229e+030.740980387e+010.970820427e+01
 970.284088502e+030.387212944e+010.106846457e+02
 980.284051544e+030.410576963e+010.114126778e+02
 990.284631658e+030.443219761e+000.112344999e+02
 1000.284631658e+030.443219761e+000.120000000e+02
 1010.285174715e+030.298569012e+010.106846447e+02
 1020.285211701e+030.321933031e+010.114126767e+02
 1030.285664642e+030.607895422e+010.908890152e+01
 1040.285735046e+030.652335454e+010.970820427e+01
 1050.286053467e+030.653578202e+010.660347462e+01
 1060.286150310e+030.914545918e+010.705342436e+01

Table 2.7.2 (cont'd)

1070.26530311e+03-.10109e79e+020.347165442e+01
 1080.26641697e+03-.108289490e+020.370820737e+01
 1090.26536905e+03-.106527655e+020.437487552e-05
 1100.26650881e+03-.114090415e+020.467297241e-05
 1110.26665291e+030.124466101e+020. e+00
 1120.26641642e+030.151740445e+020. e+00
 1130.26662287e+030.119236670e+020.347165106e+01
 1140.26559790e+030.126160680e+020.370820379e+01
 1150.267315979e+030.104060249e+020.660347319e+01
 1160.26712460e+030.109750171e+020.705342293e+01
 1170.26808404e+030.8042439e+010.908890152e+01
 1180.267944977e+030.647017097e+010.970820427e+01
 1190.269051619e+030.500370401e+010.106846457e+02
 1200.268978729e+030.528067912e+010.114126778e+02
 1210.29012460e+030.176195754e+010.112344959e+02
 1220.29012460e+030.176195754e+010.120000000e+02
 1230.291197415e+03-.153970941e+010.106846447e+02
 1240.29127050e+03-.176474404e+010.114126767e+02
 1250.292165192e+03-.451830364e+010.908890152e+01
 1260.292304200e+03-.444623661e+010.970820427e+01
 1270.292933225e+03-.688209152e+010.660347462e+01
 1280.29312460e+03-.747108172e+010.705342450e+01
 1290.29342630e+03-.69973259e+010.347165442e+01
 1300.293651307e+03-.909213352e+010.370820737e+01
 1310.293596203e+03-.642267704e+010.437487552e-05
 1320.293632825e+03-.965071100e+010.467297241e-05
 1330.290243317e+030.159337780e+020. e+00
 1340.268989570e+030.141158447e+020. e+00
 1350.290492910e+030.154638542e+020.347165106e+01
 1360.290162415e+030.140925379e+020.370820379e+01
 1370.291217377e+030.120220375e+020.660347319e+01
 1380.290936218e+030.125738401e+020.705342293e+01
 1390.292345704e+030.906750561e+010.908890152e+01
 1400.292141479e+030.102084141e+020.970820427e+01
 1410.293767570e+030.701703167e+010.106846457e+02
 1420.293660107e+030.722780180e+010.114126778e+02
 1430.295343656e+030.392370782e+010.112344959e+02
 1440.295343656e+030.392370782e+010.120000000e+02
 1450.295919769e+030.830503702e+000.106846447e+02
 1460.297027101e+030.610734049e+000.114126767e+02
 1470.298341505e+03-.145997000e+010.908890152e+01
 1480.298545817e+03-.236087799e+010.970820427e+01
 1490.299469940e+03-.417450237e+010.660347462e+01
 1500.299751079e+03-.472630405e+010.705342436e+01
 1510.300194397e+03-.559631920e+010.347165442e+01
 1520.300524902e+03-.624500179e+010.370820737e+01
 1530.300444001e+03-.608624450e+010.437487552e-05
 1540.300791505e+03-.678831055e+010.467297241e-05
 1550.293556750e+030.159042900e+020. e+00
 1560.293106842e+030.165035934e+020. e+00
 1570.293880005e+030.155194402e+020.347165106e+01
 1580.293452017e+030.101064404e+020.370820379e+01
 1590.29481790e+030.142284060e+020.660347319e+01
 1600.294453922e+030.147194922e+020.705342293e+01
 1610.295278819e+030.122177124e+020.908890152e+01
 1620.295014374e+030.12501729e+020.970820427e+01

Table 2.7.2 (cont'd)

1630.29511905e+030.968401527e+010.108e4e457e+02
 1640.29795001e+030.9e7559.01e+010.11412e770e+02
 1650.300160271e+030.88753955e+010.112344999e+02
 1660.300160271e+030.88753955e+010.120000000e+02
 1670.302200807e+030.406675579e+010.10684e447e+02
 1680.302339905e+030.387559077e+010.11412e767e+02
 1690.304041607e+030.15300886e+010.908890152e+01
 1700.304306105e+030.110005165e+010.970820427e+01
 1710.305502594e+030.477684498e+000.660347462e+01
 1720.30586600e+030.978710171e+000.705342430e+01
 1730.30644051e+030.17686817e+010.347165442e+01
 1740.306658409e+030.25765839e+010.370820737e+01
 1750.306763713e+030.221351051e+010.437487552e-05
 1760.307213604e+030.26328132e+010.467297241e-05
 1770.295511e71e+030.1e4081490e+020. e+00
 1780.295970501e+030.190294399e+020. e+00
 1790.296900605e+030.1e0993422e+020.347165106e+01
 1800.298385604e+030.1e6141415e+020.370820379e+01
 1810.29802901e+030.1e970781e+020.660347319e+01
 1820.2975911e5e+030.17408d955e+020.705342293e+01
 1830.299786499e+030.152135201e+020.908890152e+01
 1840.299468323e+030.15501e030e+020.970820427e+01
 1850.302001007e+030.129989072e+020.10684e457e+02
 1860.301833740e+030.131662560e+020.11412e770e+02
 1870.304455841e+030.1e5441599e+020.112344999e+02
 1880.304455841e+030.1e5441599e+020.120000000e+02
 1890.306910675e+030.8e8933163e+010.10684e447e+02
 1900.30707794e+030.79206383e+010.11412e767e+02
 1910.309125214e+030.5e7479925e+010.908890152e+01
 1920.309443319e+030.555663681e+010.970820427e+01
 1930.310882e00e+030.411733627e+010.660347462e+01
 1940.311320507e+030.3e7942381e+010.705342430e+01
 1950.312011047e+030.298097552e+010.347165442e+01
 1960.312525016e+030.247417831e+010.370820737e+01
 1970.312399641e+030.2e001e070e+010.437487552e-05
 1980.3129411e+030.2e5087794e+010.467297241e-05
 1990.299035700e+030.21443200e+020. e+00
 2000.29841641e+030.218931561e+020. e+00
 2010.299480509e+030.211200085e+020.347165106e+01
 2020.298691571e+030.15479374e+020.370820379e+01
 2030.300771545e+030.201820545e+020.660347319e+01
 2040.300270500e+030.205463720e+020.705342253e+01
 2050.302782205e+030.1e7.11571e+020.908890152e+01
 2060.302418274e+030.1e9056319e+020.970820427e+01
 2070.305315979e+030.1e8003190e+020.10684e457e+02
 2080.30512460e+030.17019361e+020.11412e770e+02
 2090.30812400e+030.148397341e+020.112344999e+02
 2100.30812460e+030.148397341e+020.120000000e+02
 2110.310933215e+030.1e799140e+020.10684e447e+02
 2120.31112460e+030.12e601067e+020.11412e767e+02
 2130.313466949e+030.1e9585101e+020.908890152e+01
 2140.31383090e+030.1e693536e+020.970820427e+01
 2150.31547767e+030.94974126e+010.660347462e+01
 2160.315978719e+030.91333911e+010.705342430e+01
 2170.316788677e+030.85594577e+010.347165442e+01
 2180.31735760e+030.81315507e+010.370820737e+01

Table 2.7.2 (cont'd)

2190.317213501e+030.623626041e+010.437487552e-05
 2200.317832815e+030.778631057e+010.467297241e-05
 2210.301066215e+030.247567005e+020. e+00
 2220.300384175e+030.251042509e+020. e+00
 2230.301556191e+030.245070724e+020.347165106e+01
 2240.300907471e+030.242375931e+020.370820379e+01
 2250.302977905e+030.237625195e+020.660347319e+01
 2260.302426175e+030.240637775e+020.705342293e+01
 2270.305192505e+030.226542587e+020.908890152e+01
 2280.304791595e+030.228585320e+020.970820427e+01
 2290.307982971e+030.212324429e+020.106846457e+02
 2300.307772217e+030.213098342e+020.114126776e+02
 2310.311076215e+030.196563454e+020.112349999e+02
 2320.311076205e+030.196563454e+020.120000000e+02
 2330.314169495e+030.180802491e+020.106846447e+02
 2340.314380200e+030.179728565e+020.114126767e+02
 2350.316959971e+030.166584320e+020.908890152e+01
 2360.317360871e+030.164541581e+020.970820427e+01
 2370.319174500e+030.155300713e+020.660347462e+01
 2380.319726315e+030.152489147e+020.705342436e+01
 2390.320596344e+030.148055191e+020.347165442e+01
 2400.321245015e+030.144750990e+020.370820737e+01
 2410.321086243e+030.145559902e+020.437487552e-05
 2420.321768311e+030.142084500e+020.467297241e-05
 2430.302553405e+030.263470440e+020. e+00
 2440.301825340e+030.265035972e+020. e+00
 2450.303076324e+030.261771297e+020.347165106e+01
 2460.302383942e+030.254021053e+020.370820379e+01
 2470.304593994e+030.276040191e+020.660347319e+01
 2480.304004974e+030.278753929e+020.705342293e+01
 2490.305957764e+030.269159794e+020.908890152e+01
 2500.306529645e+030.270550213e+020.970820427e+01
 2510.309936315e+030.259481945e+020.106846457e+02
 2520.309711304e+030.260212917e+020.114126776e+02
 2530.313238007e+030.248753940e+020.112349999e+02
 2540.313238007e+030.248753940e+020.120000000e+02
 2550.316539764e+030.238025970e+020.106846447e+02
 2560.316764740e+030.237294979e+020.114126767e+02
 2570.319518311e+030.228348103e+020.908890152e+01
 2580.319946259e+030.226757684e+020.970820427e+01
 2590.321882111e+030.220667790e+020.660347462e+01
 2600.322471100e+030.218753967e+020.705342436e+01
 2610.323399750e+030.215736599e+020.347165442e+01
 2620.324092115e+030.213486061e+020.370820737e+01
 2630.323922609e+030.214037457e+020.437487552e-05
 2640.324650711e+030.211671925e+020.467297241e-05
 2650.303460602e+030.321253270e+020. e+00
 2660.302704519e+030.322455780e+020. e+00
 2670.304003605e+030.320398140e+020.347165106e+01
 2680.303284607e+030.321537010e+020.370820379e+01
 2690.305579775e+030.317901840e+020.660347319e+01
 2700.304968109e+030.318670040e+020.705342293e+01
 2710.308034607e+030.314013780e+020.908890152e+01
 2720.307590211e+030.314717651e+020.970820427e+01
 2730.311127609e+030.309114531e+020.106846457e+02
 2740.310694210e+030.309464577e+020.114126776e+02

2750.	314550750E+030.	30358381E+020.	112344959E+02
2760.	314550750E+030.	30358381E+020.	120000000E+02
2770.	31795667E+030.	90050031E+020.	130846447E+02
2780.	31821930E+030.	9206786E+020.	14126767E+02
2790.	31079449E+030.	933594E+020.	14126767E+02
2800.	31523372E+030.	9206786E+020.	97020427E+01
2810.	32353372E+030.	8546527E+020.	66034746E+01
2820.	34145477E+030.	8849972E+020.	703347450E+01
2830.	345109E+030.	8096924E+020.	347165442E+01
2840.	325828449E+030.	85033345E+020.	3702077E+01
2850.	32552925E+030.	809085E+020.	43746752E-05
2860.	32640905E+030.	8911575E+020.	46729724E-05
2870.	30376550E+030.	3000000E+020.	E+00
2880.	3030000E+030.	3000000E+020.	E+00
2890.	304315309E+030.	3000000E+020.	34716510E+01
2900.	30358731E+030.	3000000E+020.	370207379E+01
2910.	30591110E+030.	3000000E+020.	660347319E+01
2920.	3052918E+030.	3000000E+020.	703347253E+01
2930.	30839652E+030.	3000000E+020.	908890152E+01
2940.	30794654E+030.	3000000E+020.	97020427E+01
2950.	31152831E+030.	3000000E+020.	10846437E+02
2960.	3112918E+030.	3000000E+020.	114126767E+02
2970.	31500000E+030.	3000000E+020.	12344999E+02
2980.	31500000E+030.	3000000E+020.	120000000E+02
2990.	318471649E+030.	3000000E+020.	10846447E+02
3000.	31870815E+030.	3000000E+020.	114126767E+02
3010.	32160345E+030.	3000000E+020.	908890152E+01
3020.	32053450E+030.	3000000E+020.	97020427E+01
3030.	32408885E+030.	3000000E+020.	66034746E+01
3040.	32470821E+030.	3000000E+020.	703347450E+01
3050.	32584660E+030.	3000000E+020.	347165442E+01
3060.	32612679E+030.	3000000E+020.	3702077E+01
3070.	326234497E+030.	3000000E+020.	43746752E-05
3080.	32700000E+030.	3000000E+020.	46729724E-05
3090.	30376550E+030.	3000000E+020.	E+00
3100.	3030000E+030.	3000000E+020.	E+00
3110.	304315309E+030.	3000000E+020.	34716510E+01
3120.	30358731E+030.	3000000E+020.	370207379E+01
3130.	30591110E+030.	3000000E+020.	660347319E+01
3140.	3052918E+030.	3000000E+020.	703347253E+01
3150.	30839652E+030.	3000000E+020.	908890152E+01
3160.	30794654E+030.	3000000E+020.	97020427E+01
3170.	31152831E+030.	3000000E+020.	10846447E+02
3180.	3112918E+030.	3000000E+020.	114126767E+02
3190.	31500000E+030.	3000000E+020.	12344999E+02
3200.	31500000E+030.	3000000E+020.	120000000E+02
3210.	318471649E+030.	3000000E+020.	10846447E+02
3220.	31870815E+030.	3000000E+020.	114126767E+02
3230.	32160345E+030.	3000000E+020.	908890152E+01
3240.	32053450E+030.	3000000E+020.	97020427E+01
3250.	32408885E+030.	3000000E+020.	66034746E+01
3260.	32470821E+030.	3000000E+020.	703347450E+01
3270.	32584660E+030.	3000000E+020.	347165442E+01
3280.	32612679E+030.	3000000E+020.	3702077E+01
3290.	326234497E+030.	3000000E+020.	43746752E-05
3300.	32700000E+030.	3000000E+020.	46729724E-05

Table 2.7.2 (cont'd)

3310.	303765500e+030.	473543431e+020.	e+00
3320.	303000000e+030.	473543431e+020.	e+00
3330.	304315309e+030.	473543431e+020.	347165108e+01
3340.	303587311e+030.	473543431e+020.	370820379e+01
3350.	305911100e+030.	473543431e+020.	660347319e+01
3360.	305291809e+030.	473543431e+020.	705342293e+01
3370.	308396515e+030.	473543431e+020.	908890152e+01
3380.	307946504e+030.	473543431e+020.	970820427e+01
3390.	311528311e+030.	473543431e+020.	106846457e+02
3400.	311291809e+030.	473543431e+020.	114126776e+02
3410.	315000000e+030.	473543431e+020.	112344999e+02
3420.	315000000e+030.	473543431e+020.	120000000e+02
3430.	318471649e+030.	473543431e+020.	106846447e+02
3440.	318708101e+030.	473543431e+020.	114126767e+02
3450.	321603405e+030.	473543431e+020.	908890152e+01
3460.	322053406e+030.	473543431e+020.	970820427e+01
3470.	324088805e+030.	473543431e+020.	660347462e+01
3480.	324708101e+030.	473543431e+020.	705342430e+01
3490.	325684600e+030.	473543431e+020.	347165442e+01
3500.	326412609e+030.	473543431e+020.	370820737e+01
3510.	326234407e+030.	473543431e+020.	437487552e-05
3520.	327000000e+030.	473543470e+020.	467297241e-05
3530.	303765503e+030.	600000030e+020.	e+00
3540.	303000000e+030.	600000000e+020.	e+00
3550.	304315309e+030.	600000030e+020.	347165108e+01
3560.	303587311e+030.	600000030e+020.	370820379e+01
3570.	305911100e+030.	600000030e+020.	660347319e+01
3580.	305291809e+030.	600000030e+020.	705342293e+01
3590.	308396515e+030.	600000030e+020.	908890152e+01
3600.	307946504e+030.	600000030e+020.	970820427e+01
3610.	311528311e+030.	600000030e+020.	106846457e+02
3620.	311291779e+030.	600000030e+020.	114126776e+02
3630.	315000000e+030.	600000030e+020.	112344999e+02
3640.	315000000e+030.	600000030e+020.	120000000e+02
3650.	318471649e+030.	600000030e+020.	106846447e+02
3660.	318708101e+030.	600000030e+020.	114126767e+02
3670.	321603405e+030.	600000030e+020.	908890152e+01
3680.	322053406e+030.	600000030e+020.	970820427e+01
3690.	324088805e+030.	600000030e+020.	660347462e+01
3700.	324708101e+030.	600000030e+020.	705342430e+01
3710.	325684600e+030.	600000030e+020.	347165442e+01
3720.	326412609e+030.	600000030e+020.	370820737e+01
3730.	326234407e+030.	600000030e+020.	437487552e-05
3740.	327000000e+030.	600000070e+020.	467297241e-05
99980.	255000000e+030.	c+000.	e+00
99990.	315000000e+030.	600000030e+020.	e+00
boun, 55			
1		000111	1 100
101		000111	1 200
201		000111	1 300
301		000111	1 374
2		001111	
22		001111	
23		001111	
24		001111	
43		001111	

Table 2.7.2 (cont'd)

44	001111
45	001111
46	001111
65	001111
66	001111
67	001111
68	001111
67	001111
66	001111
69	001111
90	001111
109	001111
110	001111
111	001111
112	001111
131	001111
132	001111
133	001111
134	001111
153	001111
154	001111
155	001111
156	001111
175	001111
176	001111
177	001111
178	001111
197	001111
198	001111
199	001111
200	001111
219	001111
220	001111
221	001111
222	001111
241	001111
242	001111
243	001111
244	001111
263	001111
264	001111
265	001111
266	001111
265	001111
286	001111
287	001111
288	001111
307	001111
308	001111
309	001111
310	001111
329	001111
330	001111
331	001111
332	001111
351	001111

Table 2.7.2 (cont'd)

```

352          001111
354          001111
374          001111
slav,22
  1 9948          111000
  3 9948          111000
  5 9948          111000
  7 9948          111000
  9 9948          111000
 11 9948          111000
 13 9948          111000
 15 9948          111000
 17 9948          111000
 19 9948          111000
 21 9948          111000
353 9949          111000
355 9949          111000
357 9949          111000
359 9949          111000
361 9949          111000
363 9949          111000
365 9949          111000
367 9949          111000
369 9949          111000
371 9949          111000
373 9949          111000
cnod,2
 9998
 9999
enod,0
matl,3,30
0.200000000e+000.          e+000.100000000e+000.100000000e+000.299999982e+00
0.283999980e-000.          e+000.          e+000.          e+000.257000000e+05
0.219000000e+000.200000000e+020.          e+000.          e+000.          e+00
0.267000000e+000.440000000e+020.999999932e+200.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.100000000e+01
0.          e+000.          e+00-.100000000e+010.          e+000.          e+00
0.          e+00
0.200000000e+000.          e+000.100000000e+000.100000000e+000.299999982e+00
0.283999980e-000.          e+000.          e+000.          e+000.257000000e+05
0.219000000e+000.200000000e+020.          e+000.          e+000.          e+00
0.267000000e+000.440000000e+020.999999932e+200.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.100000000e+01
0.          e+000.          e+00-.100000000e+010.          e+000.          e+00
0.          e+00
0.200000000e+000.          e+000.100000000e+000.100000000e+000.299999982e+00
0.283999980e-000.          e+000.          e+000.          e+000.257000000e+05
0.219000000e+000.200000000e+020.          e+000.          e+000.          e+00
0.267000000e+000.440000000e+020.999999932e+200.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.100000000e+01
0.          e+000.          e+00-.100000000e+010.          e+000.          e+00
0.          e+00
elem,1

```

Table 2.7.2 (cont'd)

20	1.00							1.00							
1	0	C	0	3	25	23	1	4	26	24	2	1	1	0	5
0.	e+00	C	0.	5	27	25	3	6	28	26	4	1	1	0	5
2	0	C	0	7	29	27	5	8	30	28	6	1	1	0	5
0.	e+00	C	0.	9	31	29	7	10	32	30	8	1	1	0	5
3	0	C	0	11	33	31	9	12	34	32	10	1	1	0	5
0.	e+00	C	0.	13	35	33	11	14	36	34	12	1	1	0	5
4	0	C	0	15	37	35	13	16	38	36	14	1	1	0	5
0.	e+00	C	0.	17	39	37	15	18	40	38	16	1	1	0	5
5	0	C	0	19	41	39	17	20	42	40	18	1	1	0	5
0.	e+00	C	0.	21	43	41	19	22	44	42	20	1	1	0	5
6	0	C	0	23	45	43	21	24	46	44	22	1	1	0	5
0.	e+00	C	0.	25	47	45	23	26	48	46	24	1	1	0	5
7	0	C	0	27	49	47	25	28	50	48	26	1	1	0	5
0.	e+00	C	0.	29	51	49	27	30	52	50	28	1	1	0	5
8	0	C	0	31	53	51	29	32	54	52	30	1	1	0	5
0.	e+00	C	0.	33	55	53	31	34	56	54	32	1	1	0	5
9	0	C	0	35	57	55	33	36	58	56	34	1	1	0	5
0.	e+00	C	0.	37	59	57	35	38	60	58	36	1	1	0	5
10	0	C	0	39	61	59	37	40	62	60	38	1	1	0	5
0.	e+00	C	0.	41	63	61	39	42	64	62	40	1	1	0	5
11	0	C	0	43	65	63	41	44	66	64	42	1	1	0	5
0.	e+00	C	0.	45	67	65	43	46	68	66	44	1	1	0	5
12	0	C	0	47	69	67	45	48	70	68	46	1	1	0	5
0.	e+00	C	0.	49	71	69	47	50	72	70	48	1	1	0	5
13	0	C	0	51	73	71	49	52	74	72	50	1	1	0	5
0.	e+00	C	0.	53	75	73	51	54	76	74	52	1	1	0	5
14	0	C	0	55	77	75	53	56	78	76	54	1	1	0	5
0.	e+00	C	0.	57	79	77	55	58	80	78	56	1	1	0	5
15	0	C	0	59	81	79	57	60	82	80	58	1	1	0	5
0.	e+00	C	0.	61	83	81	59	62	84	82	60	1	1	0	5
16	0	C	0	63	85	83	61	64	86	84	62	1	1	0	5
0.	e+00	C	0.	65	87	85	63	66	88	86	64	1	1	0	5
17	0	C	0	67	89	87	65	68	90	88	66	1	1	0	5
0.	e+00	C	0.	69	91	89	67	70	92	90	68	1	1	0	5
18	0	C	0	71	93	91	69	72	94	92	70	1	1	0	5
0.	e+00	C	0.	73	95	93	71	74	96	94	72	1	1	0	5
19	0	C	0	75	97	95	73	76	98	96	74	1	1	0	5
0.	e+00	C	0.	77	99	97	75	78	100	98	76	1	1	0	5
20	0	C	0	79	101	99	77	80	102	100	78	1	1	0	5
0.	e+00	C	0.	81	103	101	79	82	104	102	80	1	1	0	5
21	0	C	0	83	105	103	81	84	106	104	82	1	1	0	5
0.	e+00	C	0.	85	107	105	83	86	108	106	84	1	1	0	5
22	0	C	0	87	109	107	85	88	110	108	86	1	1	0	5
0.	e+00	C	0.	89	111	109	87	90	112	110	88	1	1	0	5
23	0	C	0	91	113	111	89	92	114	112	90	1	1	0	5
0.	e+00	C	0.	93	115	113	91	94	116	114	92	1	1	0	5
24	0	C	0	95	117	115	93	96	118	116	94	1	1	0	5
0.	e+00	C	0.	97	119	117	95	98	120	118	96	1	1	0	5
25	0	C	0	99	121	119	97	100	122	120	98	1	1	0	5
0.	e+00	C	0.	101	123	121	99	102	124	122	100	1	1	0	5
26	0	C	0	103	125	123	101	104	126	124	102	1	1	0	5
0.	e+00	C	0.	105	127	125	103	106	128	126	104	1	1	0	5
27	0	C	0	107	129	127	105	108	130	128	106	1	1	0	5
0.	e+00	C	0.	109	131	129	107	110	132	130	108	1	1	0	5
28	0	C	0	111	133	131	109	112	134	132	110	1	1	0	5
0.	e+00	C	0.	113	135	133	111	114	136	134	112	1	1	0	5

Table 2.7.2 (cont'd)

0.	e+00	0.	e+00	0.	e+00	81	84	86	84	82	1	1	0	5
29	0	0	83	85	83	81	84	86	84	82	1	1	0	5
0.	e+00	0.	e+00	0.	e+00	83	86	88	86	84	1	1	0	5
30	0	0	85	87	85	83	86	88	86	84	1	1	0	5
0.	e+00	0.	e+00	0.	e+00	87	90	92	90	88	2	1	0	5
31	0	0	89	91	89	87	90	92	90	88	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	89	92	94	92	90	2	1	0	5
32	0	0	91	93	91	89	92	94	92	90	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	91	94	96	94	92	2	1	0	5
33	0	0	93	95	93	91	94	96	94	92	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	93	96	98	96	94	2	1	0	5
34	0	0	95	97	95	93	96	98	96	94	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	95	98	100	98	96	2	1	0	5
35	0	0	97	99	97	95	98	100	98	96	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	97	100	102	100	98	2	1	0	5
36	0	0	99	101	99	97	100	102	100	98	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	99	102	104	102	100	2	1	0	5
37	0	0	101	103	101	99	102	104	102	100	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	101	104	106	104	102	2	1	0	5
38	0	0	103	105	103	101	104	106	104	102	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	103	106	108	106	104	2	1	0	5
39	0	0	105	107	105	103	106	108	106	104	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	105	108	110	108	106	2	1	0	5
40	0	0	107	109	107	105	108	110	108	106	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	107	110	112	110	108	2	1	0	5
41	0	0	109	111	109	107	110	112	110	108	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	109	112	114	112	110	2	1	0	5
42	0	0	111	113	111	109	112	114	112	110	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	111	114	116	114	112	2	1	0	5
43	0	0	113	115	113	111	114	116	114	112	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	113	116	118	116	114	2	1	0	5
44	0	0	115	117	115	113	116	118	116	114	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	115	118	120	118	116	2	1	0	5
45	0	0	117	119	117	115	118	120	118	116	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	117	120	122	120	118	2	1	0	5
46	0	0	119	121	119	117	120	122	120	118	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	119	122	124	122	120	2	1	0	5
47	0	0	121	123	121	119	122	124	122	120	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	121	124	126	124	122	2	1	0	5
48	0	0	123	125	123	121	124	126	124	122	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	123	126	128	126	124	2	1	0	5
49	0	0	125	127	125	123	126	128	126	124	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	125	128	130	128	126	2	1	0	5
50	0	0	127	129	127	125	128	130	128	126	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	127	130	132	130	128	2	1	0	5
51	0	0	129	131	129	127	130	132	130	128	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	129	132	134	132	130	2	1	0	5
52	0	0	131	133	131	129	132	134	132	130	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	131	134	136	134	132	2	1	0	5
53	0	0	133	135	133	131	134	136	134	132	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	133	136	138	136	134	2	1	0	5
54	0	0	135	137	135	133	136	138	136	134	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	135	138	140	138	136	2	1	0	5
55	0	0	137	139	137	135	138	140	138	136	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	137	140	142	140	138	2	1	0	5
56	0	0	139	141	139	137	140	142	140	138	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	139	142	144	142	140	2	1	0	5
57	0	0	141	143	141	139	142	144	142	140	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	141	144	146	144	142	2	1	0	5
58	0	0	143	145	143	141	144	146	144	142	2	1	0	5
0.	e+00	0.	e+00	0.	e+00	143	146	148	146	144	2	1	0	5

Table 2.7.2 (cont'd)

57	0	e+00	0.	e+00	0.	e+00	125	126	148	146	124	2	1	0	5
58	0	e+00	0.	e+00	0.	e+00	127	128	150	148	126	2	1	0	5
59	0	e+00	0.	e+00	0.	e+00	129	130	152	150	128	2	1	0	5
60	0	e+00	0.	e+00	0.	e+00	131	132	154	152	130	2	1	0	5
61	0	e+00	0.	e+00	0.	e+00	133	136	158	156	134	2	1	0	5
62	0	e+00	0.	e+00	0.	e+00	135	136	160	158	136	2	1	0	5
63	0	e+00	0.	e+00	0.	e+00	137	140	162	160	138	2	1	0	5
64	0	e+00	0.	e+00	0.	e+00	141	142	164	162	140	2	1	0	5
65	0	e+00	0.	e+00	0.	e+00	143	144	166	164	142	2	1	0	5
66	0	e+00	0.	e+00	0.	e+00	145	146	168	166	144	2	1	0	5
67	0	e+00	0.	e+00	0.	e+00	147	148	170	168	146	2	1	0	5
68	0	e+00	0.	e+00	0.	e+00	149	150	172	170	148	2	1	0	5
69	0	e+00	0.	e+00	0.	e+00	151	152	174	172	150	2	1	0	5
70	0	e+00	0.	e+00	0.	e+00	153	154	176	174	152	2	1	0	5
71	0	e+00	0.	e+00	0.	e+00	157	156	180	178	156	2	1	0	5
72	0	e+00	0.	e+00	0.	e+00	159	160	182	180	158	2	1	0	5
73	0	e+00	0.	e+00	0.	e+00	161	162	184	182	160	2	1	0	5
74	0	e+00	0.	e+00	0.	e+00	163	164	186	184	162	2	1	0	5
75	0	e+00	0.	e+00	0.	e+00	165	166	188	186	164	2	1	0	5
76	0	e+00	0.	e+00	0.	e+00	167	168	190	188	166	2	1	0	5
77	0	e+00	0.	e+00	0.	e+00	169	170	192	190	168	2	1	0	5
78	0	e+00	0.	e+00	0.	e+00	171	172	194	192	170	2	1	0	5
79	0	e+00	0.	e+00	0.	e+00	173	174	196	194	172	2	1	0	5
80	0	e+00	0.	e+00	0.	e+00	175	176	198	196	174	2	1	0	5
81	0	e+00	0.	e+00	0.	e+00	177	180	202	200	178	2	1	0	5
82	0	e+00	0.	e+00	0.	e+00	181	182	204	202	180	2	1	0	5
83	0	e+00	0.	e+00	0.	e+00	183	184	206	204	182	2	1	0	5
84	0	e+00	0.	e+00	0.	e+00	185	186	208	206	184	2	1	0	5

Table 2.7.2 (cont'd)

85	0	e+00	0.	187	209	207	185	186	210	200	188	2	1	0	5
86	0	e+00	0.	189	211	209	187	190	212	210	188	2	1	0	5
87	0	e+00	0.	191	213	211	189	192	214	212	190	2	1	0	5
88	0	e+00	0.	193	215	213	191	194	216	214	192	2	1	0	5
89	0	e+00	0.	195	217	215	193	196	218	216	194	2	1	0	5
90	0	e+00	0.	197	219	217	195	198	220	218	196	2	1	0	5
91	0	e+00	0.	199	221	219	197	202	224	222	200	2	1	0	5
92	0	e+00	0.	203	225	223	201	204	228	226	202	2	1	0	5
93	0	e+00	0.	205	227	225	203	206	230	228	204	2	1	0	5
94	0	e+00	0.	207	229	227	205	208	232	230	206	2	1	0	5
95	0	e+00	0.	209	231	229	207	210	234	232	208	2	1	0	5
96	0	e+00	0.	211	233	231	209	212	236	234	210	2	1	0	5
97	0	e+00	0.	213	235	233	211	214	238	236	212	2	1	0	5
98	0	e+00	0.	215	237	235	213	216	240	238	214	2	1	0	5
99	0	e+00	0.	217	239	237	215	218	242	240	216	2	1	0	5
100	0	e+00	0.	219	241	239	217	220	244	242	218	2	1	0	5
101	0	e+00	0.	223	245	243	221	224	248	246	222	2	1	0	5
102	0	e+00	0.	225	247	245	223	226	250	248	224	2	1	0	5
103	0	e+00	0.	227	249	247	225	228	252	250	226	2	1	0	5
104	0	e+00	0.	229	251	249	227	230	254	252	228	2	1	0	5
105	0	e+00	0.	231	253	251	229	232	256	254	230	2	1	0	5
106	0	e+00	0.	233	255	253	231	234	258	256	232	2	1	0	5
107	0	e+00	0.	235	257	255	233	236	260	258	234	2	1	0	5
108	0	e+00	0.	237	259	257	235	238	262	260	236	2	1	0	5
109	0	e+00	0.	239	261	259	237	240	264	262	238	2	1	0	5
110	0	e+00	0.	241	263	261	239	242	266	264	240	2	1	0	5
111	0	e+00	0.	243	265	263	241	244	268	266	242	2	1	0	5
112	0	e+00	0.	245	267	265	243	246	270	268	244	2	1	0	5

Table 2.7.2 (cont'd)

0.	e+00	0.	e+00	0.	e+00									
113	0	0	249	271	269	247	250	272	270	246	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
114	0	0	251	273	271	249	252	274	272	250	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
115	0	0	253	275	273	251	254	276	274	252	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
116	0	0	255	277	275	253	256	278	276	254	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
117	0	0	257	279	277	255	258	280	278	256	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
118	0	0	259	281	279	257	260	282	280	258	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
119	0	0	261	283	281	259	262	284	282	260	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
120	0	0	263	285	283	261	264	286	284	262	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
121	0	0	267	289	287	265	266	290	288	266	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
122	0	0	269	291	289	267	270	292	290	268	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
123	0	0	271	293	291	269	272	294	292	270	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
124	0	0	273	295	293	271	274	296	294	272	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
125	0	0	275	297	295	273	276	298	296	274	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
126	0	0	277	299	297	275	278	300	298	276	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
127	0	0	279	301	299	277	280	302	300	278	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
128	0	0	281	303	301	279	282	304	302	280	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
129	0	0	283	305	303	281	284	306	304	282	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
130	0	0	285	307	305	283	286	308	306	284	2	1	0	5
0.	e+00	0.	e+00	0.	e+00									
131	0	0	289	311	309	287	290	312	310	288	3	1	0	5
0.	e+00	0.	e+00	0.	e+00									
132	0	0	291	313	311	289	292	314	312	290	3	1	0	5
0.	e+00	0.	e+00	0.	e+00									
133	0	0	293	315	313	291	294	316	314	292	3	1	0	5
0.	e+00	0.	e+00	0.	e+00									
134	0	0	295	317	315	293	296	318	316	294	3	1	0	5
0.	e+00	0.	e+00	0.	e+00									
135	0	0	297	319	317	295	298	320	318	296	3	1	0	5
0.	e+00	0.	e+00	0.	e+00									
136	0	0	299	321	319	297	300	322	320	298	3	1	0	5
0.	e+00	0.	e+00	0.	e+00									
137	0	0	301	323	321	299	302	324	322	300	3	1	0	5
0.	e+00	0.	e+00	0.	e+00									
138	0	0	303	325	323	301	304	326	324	302	3	1	0	5
0.	e+00	0.	e+00	0.	e+00									
139	0	0	305	327	325	303	306	328	326	304	3	1	0	5
0.	e+00	0.	e+00	0.	e+00									
140	0	0	307	329	327	305	308	330	328	306	3	1	0	5

Table 2.7.2 (cont'd)

0.	e+00	0.	e+00	0.	e+00	309	310	314	330	310	3	1	0	5
141	0	0	311	333	331	309	310	314	330	310	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	311	314	336	334	312	3	1	0	5
142	0	0	312	335	333	311	314	336	334	312	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	313	316	338	336	314	3	1	0	5
143	0	0	313	337	335	313	316	338	336	314	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	315	316	340	338	316	3	1	0	5
144	0	0	315	339	337	315	316	340	338	316	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	317	320	342	340	318	3	1	0	5
145	0	0	317	341	339	317	320	342	340	318	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	321	322	344	342	320	3	1	0	5
146	0	0	321	343	341	319	322	344	342	320	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	323	324	346	344	322	3	1	0	5
147	0	0	323	345	343	321	324	346	344	322	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	325	326	348	346	324	3	1	0	5
148	0	0	325	347	345	323	326	348	346	324	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	327	328	350	348	326	3	1	0	5
149	0	0	327	349	347	325	328	350	348	326	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	329	330	352	350	328	3	1	0	5
150	0	0	329	351	349	327	330	352	350	328	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	331	334	356	354	332	3	1	0	5
151	0	0	331	353	351	331	334	356	354	332	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	333	336	358	356	334	3	1	0	5
152	0	0	333	355	353	333	336	358	356	334	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	335	336	360	358	336	3	1	0	5
153	0	0	335	357	355	335	336	360	358	336	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	337	340	362	360	338	3	1	0	5
154	0	0	337	359	357	337	340	362	360	338	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	339	342	364	362	340	3	1	0	5
155	0	0	339	361	359	339	342	364	362	340	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	341	344	366	364	342	3	1	0	5
156	0	0	341	363	361	341	344	366	364	342	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	343	346	368	366	344	3	1	0	5
157	0	0	343	365	363	343	346	368	366	344	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	345	348	370	368	346	3	1	0	5
158	0	0	345	367	365	345	348	370	368	346	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	347	350	372	370	348	3	1	0	5
159	0	0	347	369	367	347	350	372	370	348	3	1	0	5
0.	e+00	0.	e+00	0.	e+00	351	352	374	372	350	3	1	0	5
160	0	0	349	371	369	349	352	374	372	350	3	1	0	5
0.	e+00	0.	e+00	0.	e+00									

```

nord.
prof
end
new,slab,nonl,court,0,9,1
slab substructure. name = slab
refn,9
10.253449507e+03=-1.295593991e+02=-.500000000e+02
20.253043274e+03=-1.26464481e+02=-.500000000e+02
30.253449907e+03=-1.295593991e+02=.500000000e+02
40.253043274e+03=-1.26464481e+02=.500000000e+02
50.344505145e+03=.11122752e+02=-.500000000e+02
60.344399411e+03=.12053461e+02=-.500000000e+02
70.344035145e+03=.11122752e+02=.500000000e+02
80.344399411e+03=.12053461e+02=.500000000e+02

```

Table 2.7.2 (cont'd)

```

9999
bcun,10
  1          000111    1    6
  1          111111
  2          000111
  3          111111
  4          000111
  5          111111
  6          000111
  7          111111
  8          000111
9999          0.1111
cnod,1
9999
erod,0
matl,1,36
0.100000000e+00.          e+00.199999999e-010.499999970e-010.299999982e+00
0.2839999480e-010.499999970e-010.          e+000.          e+000.257000000e+05
0.266000000e+010.          e+000.          e+000.          e+000.          e+00
0.100000000e+00.999999932e+200.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.          e+00
0.          e+000.          e+000.          e+000.          e+000.100000000e+01
0.          e+000.          e+00-.100000000e+010.          e+000.          e+00
0.          e+00
elem,1
  20      1      2      1      0          1.00
  1      0      0      0      1      3      7      5      2      4      8      6      1      0      0      2
0.          e+000.          e+000.          e+00
ncrd,
prof
end
new,main,nonl,cart,0,10,10
main structure
refn,8
  1  0.          e+00  0.          e+00  0.          e+00
  2  0.5375000e+02  0.          e+00  0.          e+00
  3  0.1275000e+03  0.          e+00  0.          e+00
  4  0.1912500e+03  0.          e+00  0.          e+00
  5  0.2550000e+03  0.          e+00  0.          e+00
  8  0.3150000e+03  0.2000000e+02  0.          e+00
  9  0.3150000e+03  0.1420000e+03  0.          e+00
9999
cons,1
elbo  2
9999  5
9999  8
cons,1
slab  1
9999 9999
bcun,8
  1          111110
  2          1110
  3          1110
  4          1110
  5          1110

```


Table 2.7.2 (cont'd)

```

3670 0.25267e-04 0.25267e-04 0.25267e-04 0. e+00 0. e+00 0. e+0000
3690 0.25267e-04 0.25267e-04 0.25267e-04 0. e+00 0. e+00 0. e+0000
3710 0.25267e-04 0.25267e-04 0.25267e-04 0. e+00 0. e+00 0. e+0000
3730 0.12634e-04 0.12634e-04 0.12634e-04 0. e+00 0. e+00 0. e+0000
end
new,slab
pwas,5
10 0.36979e-02 0.36979e-02 0.36979e-02 0. e+00 0. e+00 0. e+0000
30 0.36979e-02 0.36979e-02 0.36979e-02 0. e+00 0. e+00 0. e+0000
50 0.36979e-02 0.36979e-02 0.36979e-02 0. e+00 0. e+00 0. e+0000
70 0.36979e-02 0.36979e-02 0.36979e-02 0. e+00 0. e+00 0. e+0000
99990 0.10000e+01
end
new,train
pwas,7
10 0.12736e-02 0.12736e-02 0.12736e-02 0. e+00 0. e+00 0. e+0000
20 0.25477e-02 0.25477e-02 0.25477e-02 0. e+00 0. e+00 0. e+0000
30 0.25477e-02 0.25477e-02 0.25477e-02 0. e+00 0. e+00 0. e+0000
40 0.25477e-02 0.25477e-02 0.25477e-02 0. e+00 0. e+00 0. e+0000
50 0.12736e-02 0.12736e-02 0.12736e-02 0. e+00 0. e+00 0. e+0000
80 0.16385e-02 0.16385e-02 0.16385e-02 0. e+00 0. e+00 0. e+0000
90 0.16385e-02 0.16385e-02 0.16385e-02 0. e+00 0. e+00 0. e+0000
end
fini
inpa,1
sur1 1 0. e+00 0.5000000e+02 0.1000000e+01 0.7649999e+00
slab 1 -
1 3
5 7
eloo 70
75 77 79 81 83 85 87 89 91 93 95 97 99 101 103 105 107 109 111 113 115 117 119 121
123 125 127 129 131 133 135 137 139 141 143 145 147 149 151 153 155 157 159 161 163 165 167 169
171 173 175 177 179 181 183 185 187 189 191 193 195 197 199 201 203 205 207 209 211 213 215 217
219 221 223 225 227 229 231 233 235 237 239 241 243 245 247 249 251 253 255 257 259 261 263 265
275 277 279 281 283 285
fini
ptre
new,rec1,par,5,100
(2e15.7)
0. e+00 0. e+00
0.6500000e+01 0.1000000e-03
0.8800000e+01 0.1000000e-02
0.1000000e+04 0.2000000e-02
0.8800000e+01 0.3000000e-02
0.7800000e+01 0.5000000e-02
0.4300000e+01 0.2000000e-01
0.4300000e+01 0.1000000e+02
fini
thou,1234
8 1235 1 1 0 0
83 1235 1 1 0 0
1203 1235 1 1 0 0
2 - 0 0
ndyn
velo,2,1
slbo 376

```


Table 2.7.2 (cont'd)

1	0.72463e+02-0.16440e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
2	0.49375e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
3	0.58916e+02-0.16440e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
4	0.46958e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
5	0.58623e+02-0.16440e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
6	0.39945e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
7	0.42592e+02-0.16440e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
8	0.29022e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
9	0.22392e+02-0.16440e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
10	0.15258e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
11	0.54708e-05-0.16440e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
12	0.37277e-06	0.	e+00	0.	e+00	0.	e+00	0.	e+00
13	-0.22392e+02-0.16440e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
14	-0.15258e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
15	-0.42592e+02-0.16440e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
16	-0.29022e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
17	-0.58623e+02-0.16440e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
18	-0.39945e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
19	-0.68916e+02-0.16440e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
20	-0.46958e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
21	-0.72463e+02-0.16440e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
22	-0.49375e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
23	-0.72463e+02-0.17263e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
24	-0.49375e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
25	-0.68916e+02-0.17263e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
26	-0.46958e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
27	-0.58623e+02-0.17263e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
28	-0.39945e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
29	-0.42592e+02-0.17263e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
30	-0.29022e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
31	-0.22392e+02-0.17263e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
32	-0.15258e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
33	-0.54708e-05-0.17263e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
34	-0.37277e-06	0.	e+00	0.	e+00	0.	e+00	0.	e+00
35	-0.22392e+02-0.17263e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
36	-0.15258e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
37	-0.42592e+02-0.17263e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
38	-0.29022e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
39	-0.58623e+02-0.17263e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
40	-0.39945e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
41	-0.68916e+02-0.17263e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
42	-0.46958e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
43	-0.72463e+02-0.17263e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
44	-0.49375e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
45	-0.72463e+02-0.17729e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
46	-0.49375e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
47	-0.68916e+02-0.17729e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
48	-0.46958e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
49	-0.58623e+02-0.17729e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
50	-0.39945e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
51	-0.42592e+02-0.17729e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
52	-0.29022e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
53	-0.22392e+02-0.17729e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
54	-0.15258e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
55	-0.54708e-05-0.17729e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
56	-0.37277e-06	0.	e+00	0.	e+00	0.	e+00	0.	e+00

Table 2.7.2 (cont'd)

57	-0.22392e+02-0.17729e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
58	-0.15258e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
59	-0.42592e+02-0.17729e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
60	-0.29022e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
61	-0.58623e+02-0.17729e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
62	-0.39945e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
63	-0.58916e+02-0.17729e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
64	-0.46958e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
65	-0.72463e+02-0.17729e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
66	-0.49375e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
67	-0.72463e+02-0.17995e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
68	-0.49375e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
69	-0.58916e+02-0.17995e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
70	-0.46958e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
71	-0.58623e+02-0.17995e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
72	-0.39945e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
73	-0.42592e+02-0.17995e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
74	-0.29022e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
75	-0.22392e+02-0.17995e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
76	-0.15258e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
77	-0.54708e-05-0.17995e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
78	-0.37277e-06	0.	e+00	C.	e+00	J.	e+00	0.	e+00
79	-0.22392e+02-0.17995e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
80	-0.15258e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
81	-0.42592e+02-0.17995e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
82	-0.29022e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
83	-0.58623e+02-0.17995e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
84	-0.39945e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
85	-0.58916e+02-0.17995e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
86	-0.46958e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
87	-0.72463e+02-0.17995e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
88	-0.49375e+01	0.	e+00	C.	e+00	J.	e+00	0.	e+00
89	-0.74429e+02-0.18245e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
90	-0.48767e+01	0.77232e+00	C.	e+00	J.	e+00	0.	e+00	e+00
91	-0.70926e+02-0.18251e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
92	-0.46380e+01	0.73460e+00	C.	e+00	J.	e+00	0.	e+00	e+00
93	-0.60760e+02-0.18267e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
94	-0.39453e+01	0.62496e+00	C.	e+00	J.	e+00	0.	e+00	e+00
95	-0.44927e+02-0.18292e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
96	-0.28564e+01	0.45411e+00	C.	e+00	J.	e+00	0.	e+00	e+00
97	-0.24975e+02-0.18324e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
98	-0.15070e+01	0.23676e+00	C.	e+00	J.	e+00	0.	e+00	e+00
99	-0.28588e+01-0.18352e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
100	-0.38445e-06	0.	e+00	C.	e+00	J.	e+00	0.	e+00
101	-0.19258e+02-0.18394e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
102	-0.15070e+01-0.18376e+00	C.	e+00	J.	e+00	0.	e+00	0.	e+00
103	-0.39209e+02-0.18425e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
104	-0.28664e+01-0.45411e+00	C.	e+00	J.	e+00	0.	e+00	0.	e+00
105	-0.55043e+02-0.18450e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
106	-0.39453e+01-0.62496e+00	C.	e+00	J.	e+00	0.	e+00	0.	e+00
107	-0.65209e+02-0.18467e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
108	-0.46380e+01-0.73460e+00	C.	e+00	J.	e+00	0.	e+00	0.	e+00
109	-0.68712e+02-0.18472e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
110	-0.48767e+01-0.77232e+00	C.	e+00	J.	e+00	0.	e+00	0.	e+00
111	-0.80281e+02-0.18487e+04	C.	e+00	J.	e+00	0.	e+00	0.	e+00
112	-0.46958e+01	0.5257e+01	C.	e+00	J.	e+00	0.	e+00	e+00

Table 2.7.2 (cont'd)

113	0.76906e+02-0.16500e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
114	0.44650e+01-0.14511e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
115	0.67119e+02-0.16571e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
116	0.37990e+01-0.12344e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
117	0.51872e+02-0.16062e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
118	0.27601e+01-0.89099e+00	C.	e+00	0.	e+00	0.	e+00	0.	e+00
119	0.32651e+02-0.16044e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
120	0.14511e+01-0.47143e+00	C.	e+00	0.	e+00	0.	e+00	0.	e+00
121	0.11365e+02-0.16713e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
122	0. e+00	C.	e+00	0.	e+00	0.	e+00	0.	e+00
123	-0.99315e+01-0.18781e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
124	-0.14511e+01-0.47143e+00	C.	e+00	0.	e+00	0.	e+00	0.	e+00
125	-0.29143e+02-0.16045e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
126	-0.27601e+01-0.89099e+00	C.	e+00	0.	e+00	0.	e+00	0.	e+00
127	-0.44389e+02-0.16044e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
128	-0.37990e+01-0.12344e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
129	-0.54176e+02-0.16920e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
130	-0.44650e+01-0.14511e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
131	-0.57551e+02-0.16927e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
132	-0.46958e+01-0.15257e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
133	0.89873e+02-0.16701e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
134	0.43993e+01-0.22410e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
135	0.86713e+02-0.16737e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
136	0.41840e+01-0.21520e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
137	0.77542e+02-0.16784e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
138	0.35591e+01-0.16135e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
139	0.53258e+02-0.16850e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
140	0.25859e+01-0.13176e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
141	0.45260e+02-0.16940e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
142	0.13595e+01-0.69267e+00	C.	e+00	0.	e+00	0.	e+00	0.	e+00
143	0.25308e+02-0.19050e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
144	0. e+00	C.	e+00	0.	e+00	0.	e+00	0.	e+00
145	0.53567e+01-0.19151e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
146	-0.13595e+01-0.69267e+00	C.	e+00	0.	e+00	0.	e+00	0.	e+00
147	-0.12642e+02-0.19243e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
148	-0.25859e+01-0.13174e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
149	-0.26926e+02-0.19310e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
150	-0.35591e+01-0.16135e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
151	-0.36096e+02-0.19363e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
152	-0.41840e+01-0.21510e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
153	-0.39256e+02-0.19379e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
154	-0.43993e+01-0.22410e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
155	0.10297e+03-0.16934e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
156	0.39945e+01-0.29022e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
157	0.10010e+03-0.16955e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
158	0.37990e+01-0.27603e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
159	0.91774e+02-0.19010e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
160	0.32316e+01-0.23481e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
161	0.78804e+02-0.19110e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
162	0.23479e+01-0.17050e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
163	0.52462e+02-0.19229e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
164	0.12344e+01-0.39010e+00	C.	e+00	0.	e+00	0.	e+00	0.	e+00
165	0.44346e+02-0.19360e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
166	0.30756e-05	C.	e+00	0.	e+00	0.	e+00	0.	e+00
167	0.26231e+02-0.19492e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
168	-0.12344e+01-0.39010e+00	C.	e+00	0.	e+00	0.	e+00	0.	e+00

Table 2.7.2 (cont'd)

169	0.98883e+01-0.29611e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
170	-0.23879e+01-0.17066e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
171	-0.30511e+01-0.19705e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
172	-0.32316e+01-0.23479e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
173	-0.11408e+02-0.19765e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
174	-0.37990e+01-0.27001e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
175	-0.14277e+02-0.19186e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
176	-0.39945e+01-0.29022e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
177	0.11925e+03-0.19125e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
178	0.34913e+01 0.34913e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
179	0.11674e+03-0.19150e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
180	0.33205e+01 0.33205e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
181	0.10946e+03-0.29223e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
182	0.28245e+01 0.28245e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
183	0.98127e+02-0.19320e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
184	0.20522e+01 0.20522e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
185	0.33843e+02-0.19479e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
186	0.10789e+01 0.10789e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
187	0.68010e+02-0.29037e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
188	0. e+00 0. e+00	0.	e+00	0.	e+00	0.	e+00	0.	e+00
189	0.52170e+02-0.19706e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
190	-0.10789e+01-0.10789e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
191	0.37892e+02-0.19439e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
192	-0.20521e+01-0.20520e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
193	0.26557e+02-0.20052e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
194	-0.28245e+01-0.28246e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
195	0.19279e+02-0.20125e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
196	-0.33204e+01-0.33203e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
197	0.16771e+02-0.20150e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
198	-0.34913e+01-0.34913e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
199	0.13831e+03-0.19280e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
200	0.29022e+01 0.3944e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
201	0.13622e+03-0.19316e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
202	0.27601e+01 0.37490e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
203	0.13017e+03-0.19400e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
204	0.23479e+01 0.32317e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
205	0.12075e+03-0.19529e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
206	0.17059e+01 0.23479e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
207	0.10886e+03-0.19693e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
208	0.89682e+00 0.12344e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
209	0.95716e+02-0.19674e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
210	0. e+00 0. e+00	0.	e+00	0.	e+00	0.	e+00	0.	e+00
211	0.82555e+02-0.20055e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
212	-0.89682e+00-0.12344e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
213	0.70681e+02-0.20219e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
214	-0.17059e+01-0.23479e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
215	0.61256e+02-0.20340e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
216	-0.23479e+01-0.32317e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
217	0.55206e+02-0.20431e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
218	-0.27601e+01-0.37490e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
219	0.53124e+02-0.20460e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
220	-0.29022e+01-0.3944e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
221	0.15958e+03-0.25419e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
222	0.22416e+01 0.45490e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
223	0.15807e+03-0.19400e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
224	0.21319e+01 0.41040e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00

Table 2.7.2 (cont'd)

225	0.15340e+03-0.19540e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
226	0.18135e+01-0.21590e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
227	0.14612e+03-0.19685e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
228	0.13176e+01-0.25079e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
229	0.13695e+03-0.19685e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
230	0.59257e+00-0.25594e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
231	0.12578e+03-0.20064e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
232	0.	e+00	0.	e+00	0.	e+00	0.	e+00	0.
233	0.11662e+03-0.20204e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
234	-0.59257e+00-0.15594e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
235	0.10745e+03-0.20444e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
236	-0.13176e+01-0.25079e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
237	0.10017e+03-0.20387e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
238	-0.18135e+01-0.21590e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
239	0.95496e+02-0.20670e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
240	-0.21319e+01-0.41640e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
241	0.93856e+02-0.20710e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
242	-0.22416e+01-0.45990e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
243	0.18284e+03-0.19515e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
244	0.15258e+01-0.46920e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
245	0.18174e+03-0.19540e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
246	0.14511e+01-0.44059e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
247	0.17856e+03-0.19640e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
248	0.12344e+01-0.37992e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
249	0.17301e+03-0.19799e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
250	0.89682e+00-0.27001e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
251	0.16737e+03-0.19991e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
252	0.47148e+00-0.14511e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
253	0.16045e+03-0.20204e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
254	0.	e+00	0.	e+00	0.	e+00	0.	e+00	0.
255	0.15353e+03-0.20417e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
256	-0.47148e+00-0.14511e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
257	0.14726e+03-0.20007e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
258	-0.89682e+00-0.27001e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
259	0.14233e+03-0.20761e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
260	-0.12344e+01-0.37992e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
261	0.13915e+03-0.20059e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
262	-0.14511e+01-0.44059e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
263	0.13805e+03-0.20693e+04	0.	e+00	0.	e+00	0.	e+00	0.	e+00
264	-0.15258e+01-0.46950e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
265	0.20721e+03-0.19573e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
266	0.77239e+00-0.48767e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
267	0.20566e+03-0.19608e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
268	0.73458e+00-0.46381e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
269	0.20505e+03-0.19710e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
270	0.62488e+00-0.39452e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
271	0.20254e+03-0.19308e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
272	0.45400e+00-0.26064e+01	0.	e+00	0.	e+00	0.	e+00	0.	e+00
273	0.19936e+03-0.20060e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
274	0.23868e+00-0.15070e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
275	0.19588e+03-0.20289e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
276	0.	e+00	0.	e+00	0.	e+00	0.	e+00	0.
277	0.19237e+03-0.20510e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
278	-0.23868e+00-0.15070e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
279	0.18921e+03-0.20710e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
280	-0.45401e+00-0.26060e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00

Table 2.7.2 (cont'd)

281	0.166710e+03-0.200000e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
282	-0.524950e+00-0.39474e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
283	0.165100e+03-0.200970e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
284	-0.734590e+00-0.46379e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
285	0.164540e+03-0.210050e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
286	-0.772390e+00-0.463767e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
287	0.232200e+03-0.255950e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
288	-0.245050e-04-0.493750e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
289	0.232200e+03-0.256200e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
290	0. e+00 0.463600e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
291	0.232200e+03-0.257310e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
292	0. e+00 0.394940e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
293	0.232200e+03-0.258920e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
294	0. e+00 0.290220e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
295	0.232200e+03-0.260940e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
296	0. e+00 0.152570e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
297	0.232200e+03-0.263100e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
298	0. e+00 0. e+00	C.	e+00	0.	e+00	0.	e+00	0.	e+00
299	0.232200e+03-0.265410e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
300	0. e+00 0.152570e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
301	0.232200e+03-0.267430e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
302	0. e+00 0.290220e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
303	0.232200e+03-0.269040e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
304	0. e+00 0.394940e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
305	0.232200e+03-0.210070e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
306	0. e+00 0.463500e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
307	0.232200e+03-0.210420e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
308	0.246050e-04-0.493750e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
309	0.258830e+03-0.255930e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
310	-0.246050e-04-0.493750e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
311	0.258830e+03-0.256200e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
312	0. e+00 0.463600e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
313	0.258830e+03-0.257310e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
314	0. e+00 0.394940e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
315	0.258830e+03-0.258920e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
316	0. e+00 0.290220e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
317	0.258830e+03-0.260940e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
318	0. e+00 0.152570e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
319	0.258830e+03-0.263100e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
320	0. e+00 0. e+00	C.	e+00	0.	e+00	0.	e+00	0.	e+00
321	0.258830e+03-0.265410e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
322	0. e+00 0.152570e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
323	0.258830e+03-0.267430e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
324	0. e+00 0.290220e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
325	0.258830e+03-0.269040e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
326	0. e+00 0.394940e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
327	0.258830e+03-0.210070e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
328	0. e+00 0.463500e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
329	0.258830e+03-0.210420e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
330	0.246050e-04-0.493750e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
331	0.305440e+03-0.255930e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
332	-0.246050e-04-0.493750e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
333	0.305440e+03-0.256200e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
334	0. e+00 0.463600e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00
335	0.305440e+03-0.257310e+04	C.	e+00	0.	e+00	0.	e+00	0.	e+00
336	0. e+00 0.394940e+01	C.	e+00	0.	e+00	0.	e+00	0.	e+00

Table 2.7.2 (cont'd)

337	0.30544e+03-0.2904e+04	e+00	0.	e+00	0.	e+00	0.	e+00
338	0.	e+00	0.2902e+01	e+00	0.	e+00	0.	e+00
339	0.30544e+03-0.20094e+04	e+00	0.	e+00	0.	e+00	0.	e+00
340	0.	e+00	0.1527e+01	e+00	0.	e+00	0.	e+00
341	0.30544e+03-0.20310e+04	e+00	0.	e+00	0.	e+00	0.	e+00
342	0.	e+00	0.	e+00	0.	e+00	0.	e+00
343	0.30544e+03-0.20094e+04	e+00	0.	e+00	0.	e+00	0.	e+00
344	0.	e+00	0.1527e+01	e+00	0.	e+00	0.	e+00
345	0.30544e+03-0.20740e+04	e+00	0.	e+00	0.	e+00	0.	e+00
346	0.	e+00	0.2902e+01	e+00	0.	e+00	0.	e+00
347	0.30544e+03-0.20904e+04	e+00	0.	e+00	0.	e+00	0.	e+00
348	0.	e+00	0.3994e+01	e+00	0.	e+00	0.	e+00
349	0.30544e+03-0.21007e+04	e+00	0.	e+00	0.	e+00	0.	e+00
350	0.	e+00	0.40950e+01	e+00	0.	e+00	0.	e+00
351	0.30544e+03-0.2104e+04	e+00	0.	e+00	0.	e+00	0.	e+00
352	0.24605e-04-0.49375e+01	e+00	0.	e+00	0.	e+00	0.	e+00
353	0.38700e+03-0.19590e+04	e+00	0.	e+00	0.	e+00	0.	e+00
354	-0.24605e-04-0.49375e+01	e+00	0.	e+00	0.	e+00	0.	e+00
355	0.38700e+03-0.19620e+04	e+00	0.	e+00	0.	e+00	0.	e+00
356	0.	e+00	0.40960e+01	e+00	0.	e+00	0.	e+00
357	0.38700e+03-0.19721e+04	e+00	0.	e+00	0.	e+00	0.	e+00
358	0.	e+00	0.3994e+01	e+00	0.	e+00	0.	e+00
359	0.38700e+03-0.19892e+04	e+00	0.	e+00	0.	e+00	0.	e+00
360	0.	e+00	0.2902e+01	e+00	0.	e+00	0.	e+00
361	0.38700e+03-0.20094e+04	e+00	0.	e+00	0.	e+00	0.	e+00
362	0.	e+00	0.15259e+01	e+00	0.	e+00	0.	e+00
363	0.38700e+03-0.20310e+04	e+00	0.	e+00	0.	e+00	0.	e+00
364	0.	e+00	0.	e+00	0.	e+00	0.	e+00
365	0.38700e+03-0.20541e+04	e+00	0.	e+00	0.	e+00	0.	e+00
366	0.	e+00	0.15257e+01	e+00	0.	e+00	0.	e+00
367	0.38700e+03-0.20743e+04	e+00	0.	e+00	0.	e+00	0.	e+00
368	0.	e+00	0.2902e+01	e+00	0.	e+00	0.	e+00
369	0.38700e+03-0.20904e+04	e+00	0.	e+00	0.	e+00	0.	e+00
370	0.	e+00	0.3994e+01	e+00	0.	e+00	0.	e+00
371	0.38700e+03-0.21007e+04	e+00	0.	e+00	0.	e+00	0.	e+00
372	0.	e+00	0.40960e+01	e+00	0.	e+00	0.	e+00
373	0.38700e+03-0.2104e+04	e+00	0.	e+00	0.	e+00	0.	e+00
374	0.24605e-04-0.49375e+01	e+00	0.	e+00	0.	e+00	0.	e+00
9998	0.	e+00	0.16440e+04	e+00	0.	e+00	0.	e+00
9999	0.38700e+03-0.20310e+04	e+00	0.	e+00	0.	e+00	0.	e+00
main	7							
1	0.	e+00	0.	e+00	0.	e+00	-0.64500e+01	
2	0.	e+00	-0.41119e+03	e+00	0.	e+00	0.	e+00
3	0.	e+00	-0.32230e+03	e+00	0.	e+00	0.	e+00
4	0.	e+00	-0.12330e+04	e+00	0.	e+00	0.	e+00
5	0.	e+00	-0.16440e+04	e+00	0.	e+00	0.	e+00
8	0.38700e+03-0.20310e+04	e+00	0.	e+00	0.	e+00	0.	e+00
9	0.91590e+03-0.20310e+04	e+00	0.	e+00	0.	e+00	0.	e+00
mass								
dylo,1,1								
recl	0-0.107	3.500	2					
9	9							
time,rslt,1,0.100e+00								
auto,defi								
inte,newm,0.200e+03,3.e+00,0.e+00,0.1000e+00								
stif								

Table 2.7.2 (cont'd)

```

stif,upda
kinr,12
elmr,1,2,6,3
kinr,5
loop,200
zero,ltrae
inpa,init,,0.e+00,0.e+00
step
wrba
auto,init
loop,30
stif
auto,load
load
disp
inpa,anal
kinr,10
elmr,9,10
auto,terr,0.5000e+02,0.2500e+03
if,3,3,1,1
entr,1
auto,fact
kinr,1
inpa,upda,0
if,3,2,2,3
entr,2
elmr,1
cont
goto,0
entr,3
auto,step,0.2000e-05,0.1000e-04,0.5000e+00,0.2000e+01
if,4,5,5,4
entr,4
inte,newm,,auto,0.e+00,0.e+00,0.e+00,0.1000e+00
entr,5
if,3,6,6,7
entr,6
kinr,12
elmr,5,2,6
kinr,5
inpa,upda,1
stif,init
goto,8
entr,7
chou
inpa,none
iapa,rslt
elmr,1,2,4,5,1
kinr,4,9,11
wrou
zero,lrsb
unta
sumb
elmr,3
kinr,3
stif,upda

auto,exit,0.2000e-01
if,5,8,8,0
entr,b
cont
fini
paus

```

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WIPS (Whip and Impact of Piping Systems) is a special purpose computer code for the structural analysis of pipe whip dynamic effects following a postulated pipe rupture. WIPS has been developed primarily to provide support for the pipe whip analysis procedures described in Section 3.6.2 of the U.S. Nuclear Regulatory Commission Standard Review Plan.

This report summarizes the purpose and scope of the WIPS development effort, identifying those clauses in the standard Review Plan which refer to pipe whip analysis, and indicating how the WIPS code can be used to provide supporting data. Detailed information on use of the code is contained in accompanying reports which cover (1) use instructions, (2) theory, (3) programming procedures, and (4) verification examples.

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