



February 19, 1992
LD-92-026

Docket No. 52-002

U.S. Nuclear Regulatory Commission
Attn: Document Control Desk
Washington, DC 20555

Subject: Proprietary Information Transmittal

Reference: C-E Letter LD-92-023, dated February 18, 1992

Dear Sirs:

The response to Request for Additional Information (RAI) #722.22 (Reference letter) included a non-proprietary version of the attachments to that response. This letter transmits a copy of the proprietary version of those attachments. For convenience, the non-proprietary version is also enclosed.

The material enclosed as Attachments 1 and 2 to the response to RAI 722.22 is considered to be proprietary. As such, it is requested that the material be withheld from public disclosure in accordance with the provisions of 10 CFR 2.790 and that this material be appropriately safeguarded. The reasons for the classification of this material as proprietary are delineated in the enclosed affidavit.

If you have any questions, please contact Mr. Stan Ritterbusch of my staff at (203) 285-5206.

Very truly yours,

COMBUSTION ENGINEERING, INC.

C. B. Brinkman
Acting Director
Nuclear Systems Licensing

ser/lw
Enclosures: As Stated

Change: REC FOR 1 w/out Prop
DOB2
1/1

ABB Combustion Engineering Nuclear Power

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AFFIDAVIT PURSUANT

TO 10 CFR 2.790

Combustion Engineering, Inc.)
State of Connecticut)
County of Hartford) SS.:

I, C. B. Brinkman, depose and say that I am the Acting Director, Nuclear Systems Licensing, of Combustion Engineering, Inc., duly authorized to make this affidavit, and have reviewed or caused to have reviewed the information which is identified as proprietary and referenced in the paragraph immediately below. I am submitting this affidavit in conformance with the provisions of 10 CFR 2.790 of the Commission's regulations for withholding this information.

The information for which proprietary treatment is sought is contained in the following document:

Response to NRC Request for Additional Information #722.22
(Attachment to letter LD-92-023, dated February 18, 1992)

This document has been appropriately designated as proprietary.

I have personal knowledge of the criteria and procedures utilized by Combustion Engineering in designating information as a trade secret, privileged or as confidential commercial or financial information.

Pursuant to the provisions of paragraph (b) (4) of Section 2.790 of the Commission's regulations, the following is furnished for consideration by the Commission in determining whether the information sought to be withheld from public disclosure, included in

the above referenced document, should be withheld.

1. The information sought to be withheld from public disclosure, which is owned and has been held in confidence by Combustion Engineering, is MAAP computer code input listings and data files for System 80+™ severe accident analysis.
2. The information consists of test data or other similar data concerning a process, method or component, the application of which results in substantial competitive advantage to Combustion Engineering.
3. The information is of a type customarily held in confidence by Combustion Engineering and not customarily disclosed to the public. Combustion Engineering has a rational basis for determining the types of information customarily held in confidence by it and, in that connection, utilizes a system to determine when and whether to hold certain types of information in confidence. The details of the aforementioned system were provided to the Nuclear Regulatory Commission via letter DP-537 from F. M. Stern to Frank Schroeder dated December 2, 1974. This system was applied in determining that the subject document herein is proprietary.
4. The information is being transmitted to the Commission in confidence under the provisions of 10 CFR 2.790 with the

understanding that it is to be received in confidence by the Commission.

5. The information, to the best of my knowledge and belief, is not available in public sources, and any disclosure to third parties has been made pursuant to regulatory provisions or proprietary agreements which provide for maintenance of the information in confidence.
6. Public disclosure of the information is likely to cause substantial harm to the competitive position of Combustion Engineering because:
 - a. A similar product is manufactured and sold by major pressurized water reactor competitors of Combustion Engineering.
 - b. Development of this information by C-E required thousands of manhours and hundreds of thousands of dollars. To the best of my knowledge and belief, a competitor would have to undergo similar expense in generating equivalent information.
 - c. In order to acquire such information, a competitor would also require considerable time and inconvenience to develop the computer code model and design data in the MAAP code input listings and data files.
 - d. The information required significant effort and expense to obtain the licensing approvals necessary for application of

the information. Avoidance of this expense would decrease a competitor's cost in applying the information and marketing the product to which the information is applicable.

- e. The information consists of MAAP computer code input listings and data files for System 80+™ severe accident analysis, the application of which provides a competitive economic advantage. The availability of such information to competitors would enable them to modify their product to better compete with Combustion Engineering, take marketing or other actions to improve their product's position or impair the position of Combustion Engineering's product, and avoid developing similar data and analyses in support of their processes, methods or apparatus.
 - f. In pricing Combustion Engineering's products and services, significant research, development, engineering, analytical, manufacturing, licensing, quality assurance and other costs and expenses must be included. The ability of Combustion Engineering's competitors to utilize such information without similar expenditure of resources may enable them to sell at prices reflecting significantly lower costs.
- Use of the information by competitors in the international marketplace would increase their ability to market nuclear steam supply systems b, reducing the costs associated with their technology development. In addition, disclosure would have an adverse economic impact on Combustion

Engineering's potential for obtaining or maintaining
foreign licensees.

Further the deponent sayeth not.

Charles B. Brinkman

Charles B. Brinkman
Acting Director
Nuclear Systems Licensing

Sworn to before me
this 20th day of February, 1992

Laurie J. White
Notary Public

My commission expires: 3/31/94

QUESTION 722.22

Please provide MAAP input listings for a representative set of those accident scenarios used to develop the source term information for each release category. For several accident sequences which have relatively high frequencies of occurrence, provide MAAP output (in graphical form) showing: containment pressure (including partial pressures of steam and non-condensable gas); temperature of water and air space; distribution of core material and non-condensable gases in each compartment; mass of water in the IRWST and cavity; heat loss through the containment wall; fission product release fractions; and erosion depth of the basemat and the cavity wall. Include a basemat melt-through sequence (i.e., a dry cavity case) in these outputs.

RESPONSE 722.22

A listing of the MAAP_Parameter File which contains the plant design and operations data for the System 80+ design is provided in Attachment 1. The parameter file along with specific case data file are employed to perform MAAP analyses for specific accident scenarios used to develop the source term information. Case data file listings for a representative set of accident scenarios are provided in Attachment 2. These accident scenarios consist of the following Release Classes (RCs):

- RC 2.2 -- Small LOCA (0.02 sq ft) in hot leg with no safety injection and no emergency feedwater; containment isolation failure at the start of the transient.
- RC 2.4 -- Loss of Offsite Power transient with diesel generators available.
- RC 3.1 -- Total Loss of Feedwater transient with manual feed and bleed cooling of the RCS. Containment heat removal is assumed to be unavailable.
- RC 4.1 -- Large hot leg LOCA coincident with failure of safety injection.
- RC 5.1 -- Station Blackout with battery depletion at 8 hours.
- RC 6.2 -- Large cold leg LOCA with coincident failure of safety injection; no cavity flooding (dry cavity).
- RC 7.1 -- Station Blackout with battery depletion at 8 hours and late recovery of power and containment heat removal.

Readily available output parameters for the above accident scenarios are provided in Attachment 3. These include the containment pressure plot, tabular data for fission product release fractions, height of water level in the cavity and/or the IRWST, concrete erosion of the basemat, and mass of hydrogen generated.

ATTACHMENT 1

LISTING OF MAAP PARAMETER FILE FOR THE SYSTEM 80+ DESIGN

THE FOLLOWING 16 PAGES CONTAIN COMBUSTION ENGINEERING
PROPRIETARY INFORMATION

ATTACHMENT 2

LISTING OF CASE DATA FILE FOR REPRESENTATIVE ACCIDENT SCENARIOS

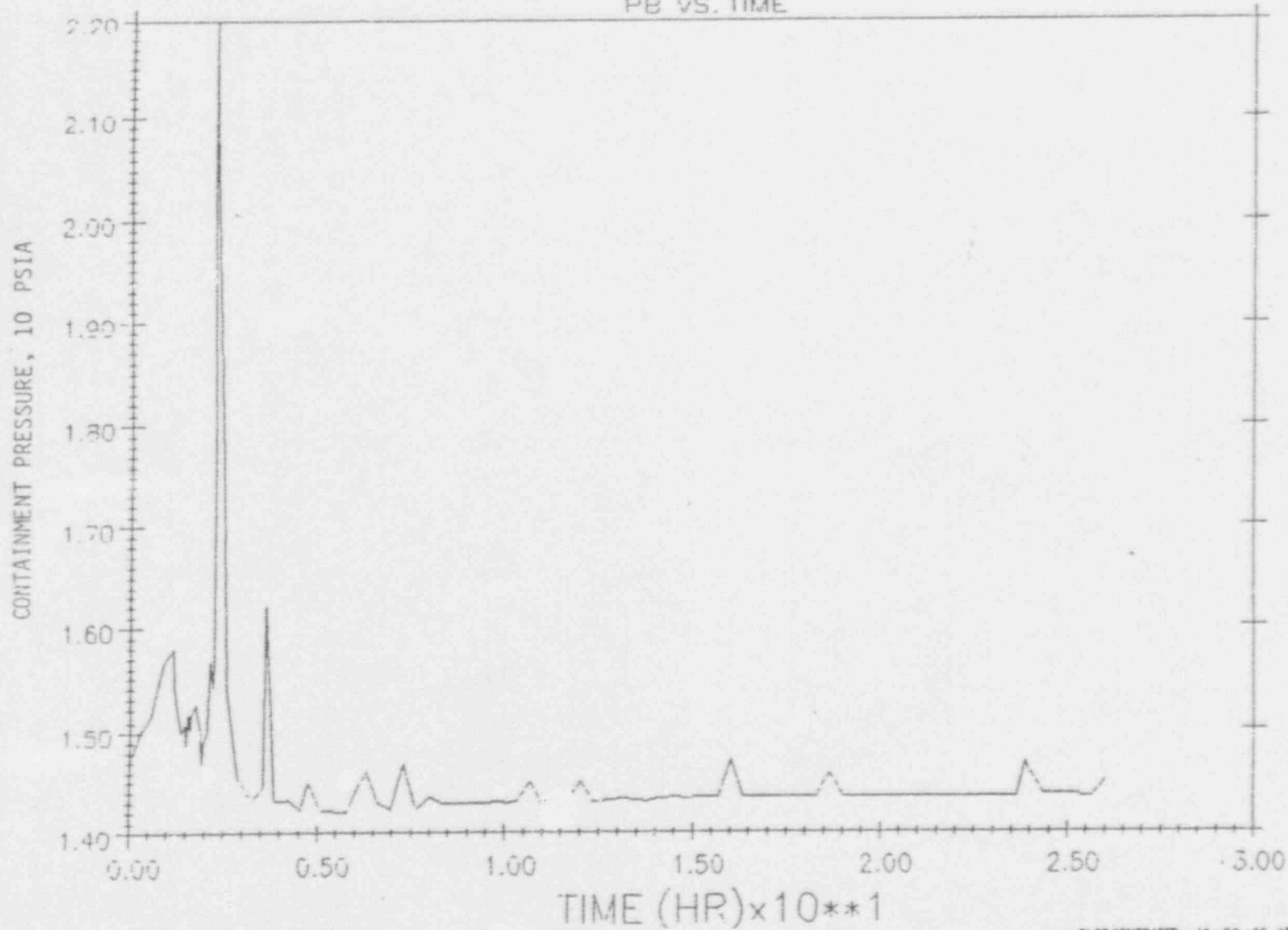
THE FOLLOWING 11 PAGES CONTAIN COMBUSTION ENGINEERING PROPRIETARY
INFORMATION

ATTACHMENT 3

MAAP OUTPUT FOR REPRESENTATIVE ACCIDENT SCENARIOS

SBL T=0 HOLE SF WET

PB VS. TIME



UO2,ACT GAS 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00
 AERO 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00
 DEP AERO/GAS 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00
 IN CORIUM 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00

LEAKED FROM CONTMT: GAS MASS(LB) AERBDOL MASS(LB) RELEASE FRACTION

| | | | | |
|----------|-------------|------------|------------|--|
| NOBL, IN | 1.5420E+03 | 2.0707E-01 | 9.8221E-01 | |
| CSI | -6.0273E-24 | 4.7800E+00 | 3.5310E-02 | |
| TEO2 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | |
| SR0 | 0.0000E+00 | 1.9777E-02 | 6.7704E-05 | |
| MOO2 | 0.0000E+00 | 4.1173E+00 | 3.3793E-03 | |
| CSOH | 1.3366E-06 | 2.0614E+01 | 2.6391E-02 | |
| BAO | 0.0000E+00 | 1.8091E-01 | 4.1245E-04 | |
| LA2O3 | 0.0000E+00 | 2.2504E-03 | 9.6522E-07 | |
| CEO2 | 0.0000E+00 | 2.5711E-02 | 2.7205E-05 | |
| SB | 8.6976E-08 | 7.5807E-01 | 8.6936E-02 | |
| TE2 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | |
| UO2,ACT | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | |

RELEASE CLASS 2.4

*Case 10
t=36 hours*

NO. ITERATIONS IN PRIM SYS TRANSPORT MODEL: 2 IN CONTMT GAS TRANSPORT MODEL: 1

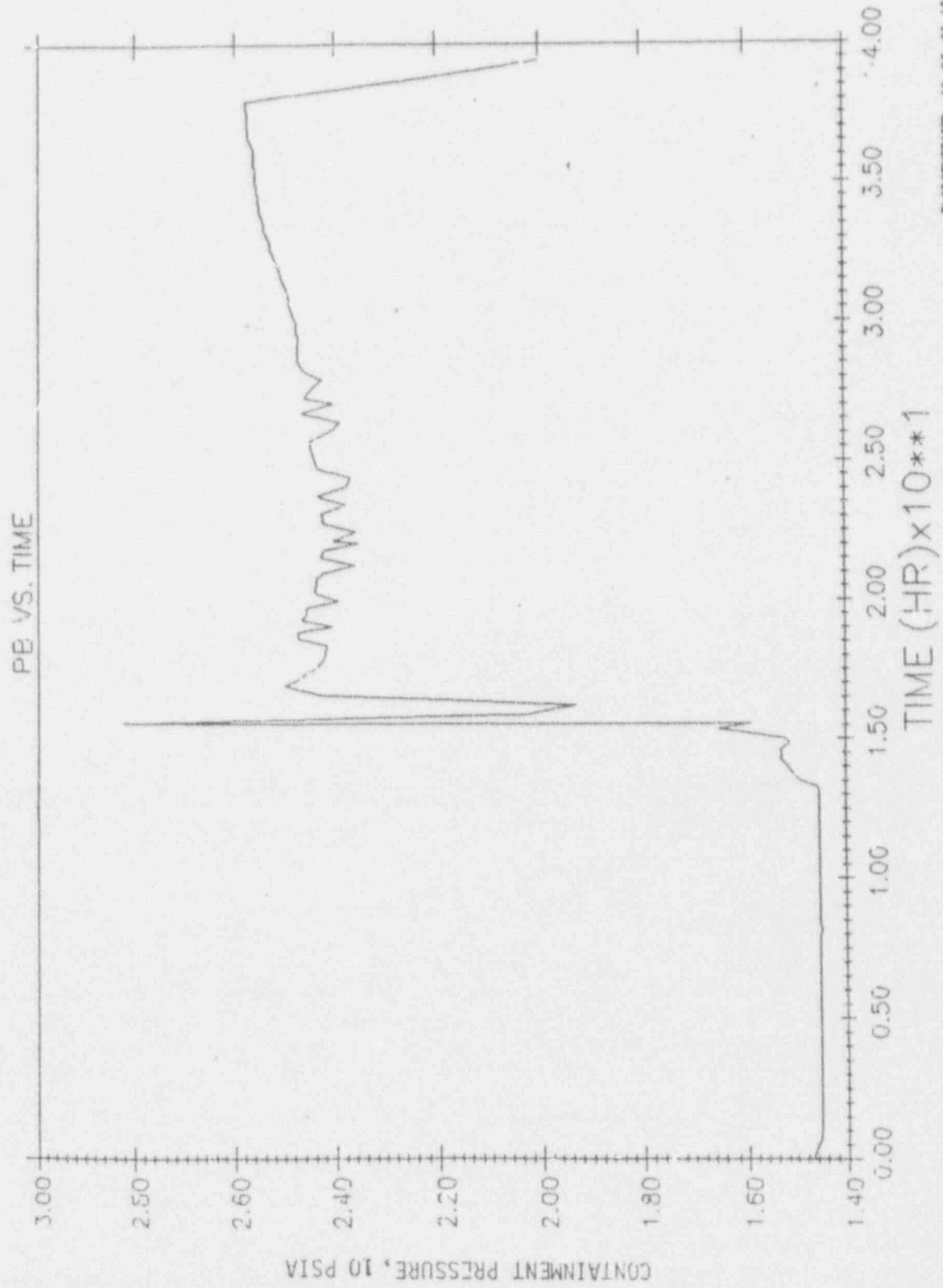
FISSIION PRODUCT MASS BALANCES:

BALANCE 1 = TOTAL MASS AS USED BY MAAP
BALANCE 2 = IN FUEL + INTEGRATED RELEASE FROM FUEL

| | NOBLES | CSI | TEO2 | SR0 | MOO2 | CSOH | BAO | LA2O3 | CEO2 | SB | TE2 | UO2 |
|----------|-----------|------------|-----------|-----------|-----------|--------------|-----|-------|------|----|-----|-----|
| BAL. 1: | 712.09875 | 61.06263 | 0.00000 | 133.53587 | 555.59937 | 354.29034 | | | | | | |
| BAL. 2: | 712.09991 | 61.06264 | 0.00000 | 133.53468 | 555.45697 | 354.29034 | | | | | | |
| INITIAL: | 712.09998 | 61.06259 | -0.60084 | 132.50000 | 552.63625 | 354.29031 | | | | | | |
| CORE: | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | | | | | | |
| CORIUM: | 0.00000 | 0.00000 | 0.00000 | 132.70961 | 427.19827 | 0.00000 | | | | | | |
| PB: | 1.36874 | 53.55337 | 0.00000 | 0.78049 | 120.31207 | 320.09421 | | | | | | |
| CONT: | 710.73004 | 7.50725 | 0.00000 | 0.04578 | 8.08900 | 34.19633 | | | | | | |
| INV REL: | 712.09991 | 61.06264 | 0.00000 | 0.82507 | 128.25867 | 354.29034 | | | | | | |
| EXV REL: | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | | | | | | |
| BAL. 1: | 200.42085 | 1065.85315 | 432.05881 | 4.17673 | 61.65564 | 113400.68750 | | | | | | |
| BAL. 2: | 200.40009 | 1065.84985 | 432.05746 | 4.17441 | 61.65564 | 113400.68750 | | | | | | |
| INITIAL: | 198.93653 | 1057.52490 | 428.68970 | 4.16393 | 61.17422 | 113392.09375 | | | | | | |
| CORE: | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | | | | | | |
| CORIUM: | 188.85867 | 1065.58472 | 430.90033 | 2.33961 | 61.65564 | 113400.68750 | | | | | | |
| PS: | 11.08803 | 0.26125 | 1.10423 | 0.83416 | 0.00000 | 0.00000 | | | | | | |

Case 10

LOOP T=0 HOLE NOSP LATE WET



| | GAS MASS (LB) | AEROSOL MASS (LB) | RELEASE FRACTION |
|---------|---------------|-------------------|------------------|
| MOBL IN | 1. 5369E+03 | 8. 0695E+02 | 9. 7896E-01 |
| CSI | 3. 7522E-28 | 1. 3609E+01 | 1. 0109E-01 |
| TEO2 | 4. 0958E-34 | 1. 4456E-01 | 3. 5886E-04 |
| SRG | 0. 0000E+00 | 5. 4676E+00 | 1. 0717E-02 |
| MOO2 | 0. 0000E+00 | 8. 5031E-01 | 6. 9789E-04 |
| CSOH | 4. 8215E-05 | 8. 2226E+01 | 1. 0527E-01 |
| BAD | 0. 0000E+00 | 3. 3068E+00 | 7. 5391E-03 |
| LA203 | 0. 0000E+00 | 1. 0467E-01 | 4. 4895E-05 |
| CEO2 | 0. 0000E+00 | 9. 8831E-01 | 1. 0457E-03 |
| SB | 6. 3329E-06 | 1. 5089E+00 | 1. 6437E-01 |
| TE2 | 3. 5065E-04 | 7. 5413E+00 | 7. 0749E-02 |
| UO2.ACT | 0. 0000E+00 | 9. 7935E-01 | 3. 9176E-06 |

RELEASE CLASS 3.1

*(Age
t=60 hours)*

NO. ITERATIONS IN PRIM SYS TRANSPORT MODEL: 1 IN CONTHT GAS TRANSPORT MODEL: 7

FSSION PRODUCT MASS BALANCES:

BALANCE 1 = TOTAL MASS AS USED BY MAAP
BALANCE 2 = IN FUEL + INTEGRATED RELEASE FROM FUEL

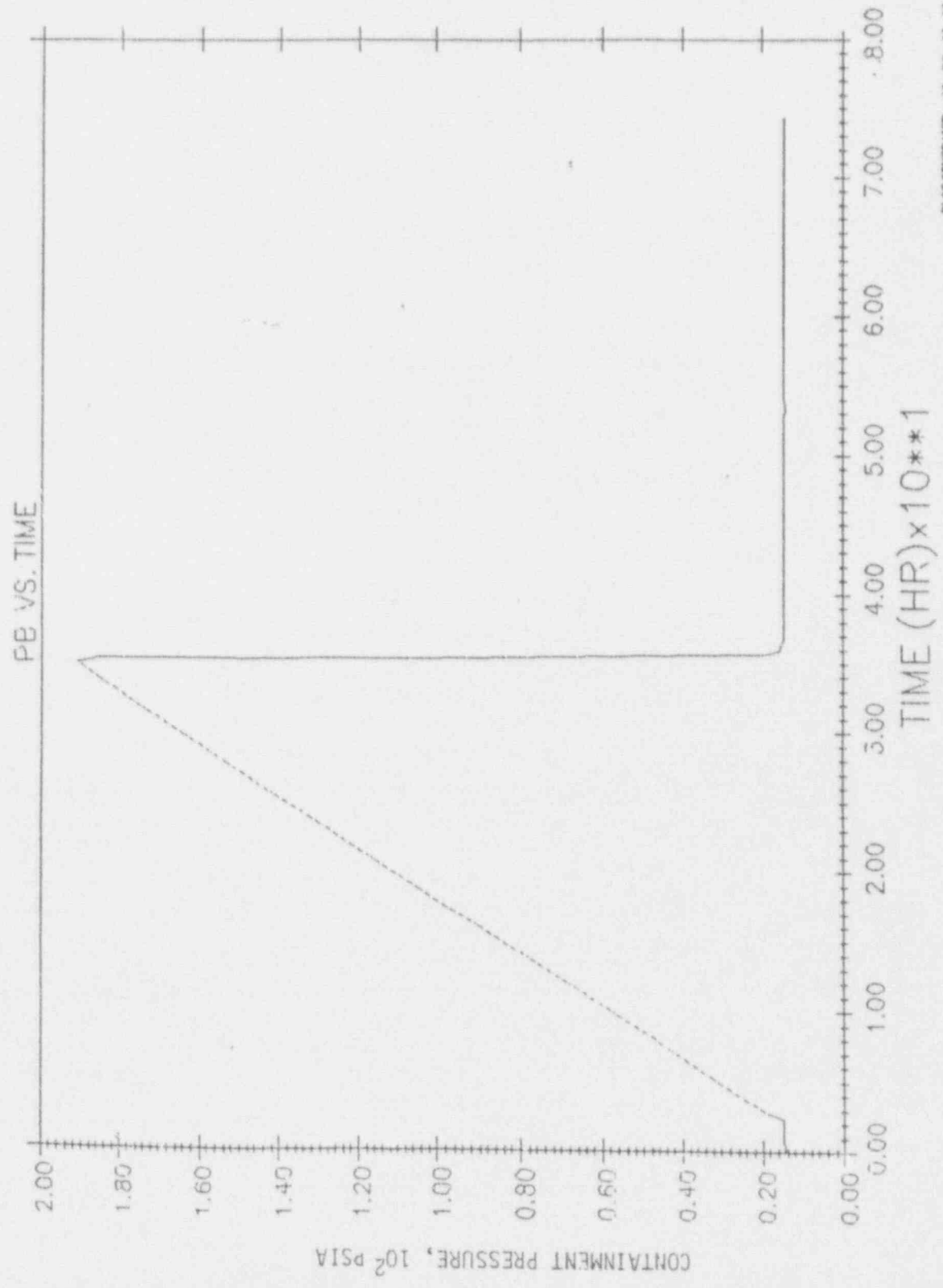
| | MOBLES | CSI | TEO2 | SRG | MOO2 | CEO2 | SB | TE2 | UO2 |
|----------|------------|------------|-----------|-----------|-----------|---------|---------|---------|---------|
| BAL 1: | 712.34180 | 61.06352 | 0.70777 | 133.38124 | 555.16205 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| BAL 2: | 712.33557 | 61.06355 | 0.70777 | 133.38077 | 555.08331 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| INITIAL: | 712.09998 | 61.06259 | 0.19845 | 132.50000 | 552.65625 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| CCRE: | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| CRORIUM: | 0.00000 | 0.00000 | 0.00000 | 97.90195 | 281.66031 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| PS: | 3.92870 | 52.34634 | 0.00114 | 2.19301 | 272.29065 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| CONT: | 708.41309 | 8.51698 | 0.70663 | 33.28629 | 1.21108 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| INV REL: | 712.33557 | 61.06355 | 0.00000 | 2.17233 | 273.42291 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| EXV REL: | 4641.00977 | 0.00000 | 0.70777 | 33.30649 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| BAL 1: | 500.17035 | 1064.59202 | 431.51526 | 4.17629 | 61.01521 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| BAL 2: | 200.16180 | 1064.59202 | 431.51517 | 4.17569 | 61.01535 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| INITIAL: | 198.93653 | 1057.52490 | 428.68570 | 4.16393 | 60.60712 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| CORE: | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| CRORIUM: | 141.30380 | 1063.24011 | 410.68532 | 0.33854 | 0.00604 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| PS: | 29.48168 | 0.77718 | 15.28076 | 2.60452 | 0.04928 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| CONT: | 19.38486 | 0.57568 | 5.56578 | 1.23322 | 60.95990 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| INV REL: | 29.57733 | 0.77729 | 15.27999 | 3.47814 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| EXV REL: | 19.28067 | 0.57551 | 5.56667 | 0.35901 | 61.00932 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |

ADDITIONAL FIGURES-OF-MERIT OF THIS RUN

RELEASE CLASS 3.1

Class

TRCP TRIP LATE WET



PLOT GENERATED - 16-JUL-80 16:28:37

| IN CORIUM | 0.0000E+00 | 0.0000E+00 | 2.2810E+03 |
|--------------|------------|------------|------------|
| CFUR GAS | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| AERO | 2.7345E-09 | 3.4056E-00 | 7.4173E-08 |
| DEP AERO/GAS | 9.3369E-09 | 5.1262E-07 | 7.1804E+00 |
| IN CORIUM | 0.0000E+00 | 0.0000E+00 | 7.7984E+02 |
| SR GAS | 5.4684E-14 | 8.6769E-14 | 3.0133E-04 |
| AERO | 1.9291E-06 | 2.1808E-04 | 1.3311E-14 |
| DEP AERO/GAS | 6.8445E-04 | 3.2682E-04 | 7.8911E-12 |
| IN CORIUM | 0.0000E+00 | 0.0000E+00 | 2.4697E-01 |
| TE2 GAS | 3.5837E-09 | 3.2914E-09 | 1.1515E-11 |
| AERO | 1.5863E-06 | 1.3476E-05 | 0.0000E+00 |
| DEP AERO/GAS | 5.8130E-06 | 2.6154E-04 | 0.0000E+00 |
| IN CORIUM | 0.0000E+00 | 0.0000E+00 | 1.1082E-04 |
| W02.ACT GAS | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| AERO | 1.9582E-06 | 2.4529E-05 | 5.3450E-05 |
| DEP AERO/GAS | 6.6796E-06 | 3.6739E-04 | 1.4573E+01 |
| IN CORIUM | 0.0000E+00 | 0.0000E+00 | 2.4978E+03 |

RELEASE FRACTION

| RELEASED FROM (CONTHT) | GAS MASS(LB) | AEROSOL MASS(LB) |
|------------------------|--------------|------------------|
| NR01.IN | 1.3762E+03 | 2.5627E+00 |
| CR1 | -1.3435E-20 | 9.9046E-02 |

RELEASE CLASS 4.1

Class
t=30 hours

| RELEASED FROM (CONTHT) | GAS MASS(LB) | AEROSOL MASS(LB) | RELEASE FRACTION |
|------------------------|--------------|------------------|------------------|
| NR02 | 1.4006E-20 | 3.1338E-01 | 1.8612E-33 |
| SR0 | -2.2016E-27 | 5.8031E-03 | 1.9866E-05 |
| NR02 | -3.1923E-26 | 7.6121E-03 | 6.2476E-06 |
| CR04 | 1.0256E-11 | 5.8558E-01 | 7.4971E-04 |
| NR02 | -9.9164E-30 | 6.6923E-03 | 1.5264E-05 |
| LA003 | 0.0000E+00 | 1.0795E-03 | 4.6301E-07 |
| CF02 | 0.0000E+00 | 3.9668E-03 | 4.1973E-06 |
| SR | 1.6292E-11 | 2.4522E-02 | 2.6713E-03 |
| TE2 | 2.5455E-07 | 1.2140E-01 | 9.0019E-04 |
| NR02.ACT | 0.0000E+00 | 1.1934E-02 | 4.7737E-08 |

NO. ITERATIONS IN PRIM SYS TRANSPORT MODEL: 4 IN CONTHT GAS TRANSPORT MODEL: 1

FISSION PRODUCT MASS BALANCES:

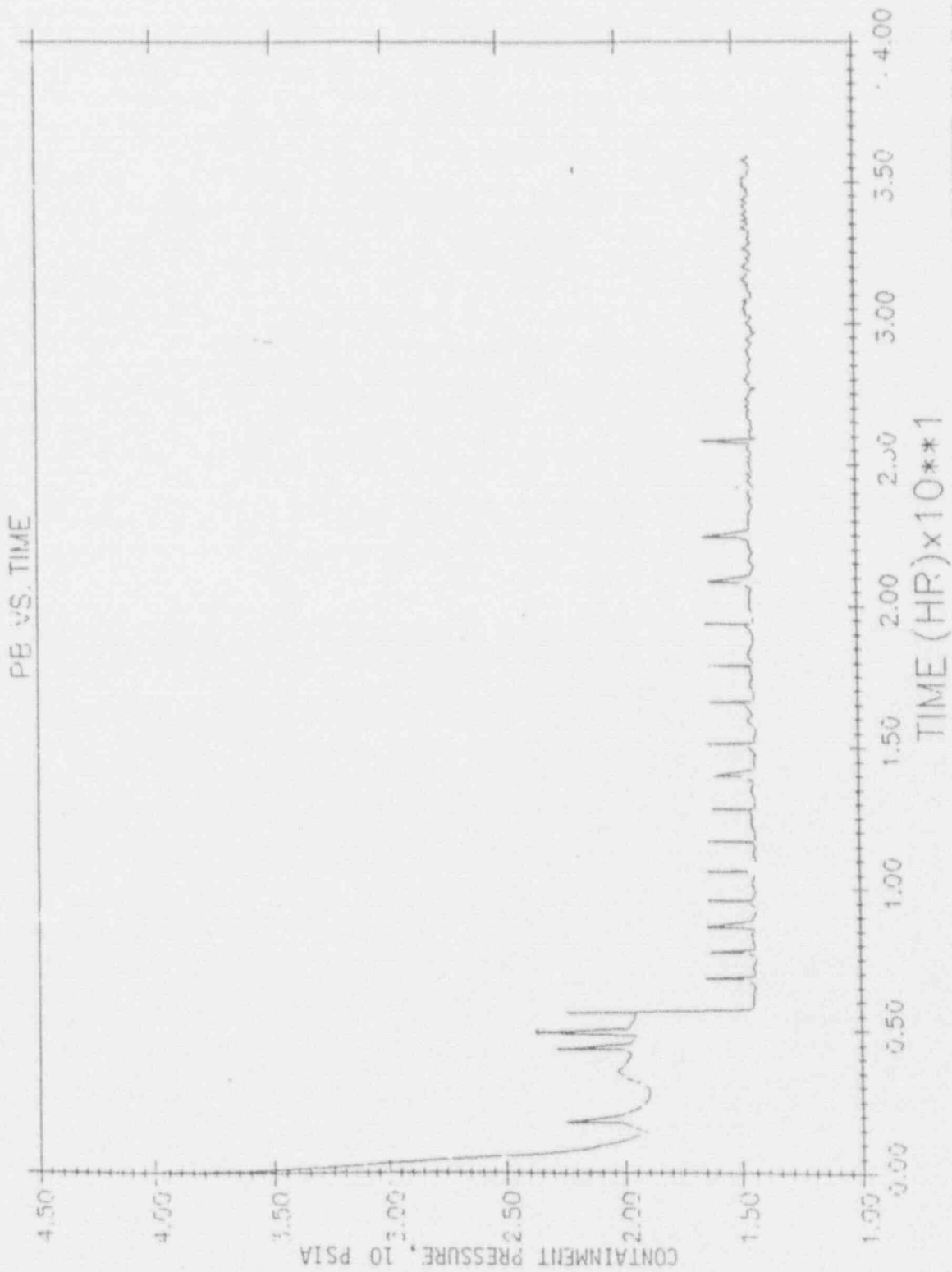
BALANCE 1 = TOTAL MASS AS USED BY MAAP
BALANCE 2 = IN FUEL + INTEGRATED RELEASE FROM FUEL

| | NR01 | SR0 | TE02 | SR02 | NR02 | CR04 |
|-------|-----------|----------|----------|-----------|-----------|-----------|
| BAL 1 | 712.09821 | 61.06258 | 54.79501 | 132.50014 | 552.64917 | 354.28506 |
| BAL 2 | 712.09869 | 61.06245 | 54.99578 | 132.50047 | 552.64978 | 354.29047 |

RELEASE CLASS 4.1

Case 6

4.91 CL EARLY FAIL DRY

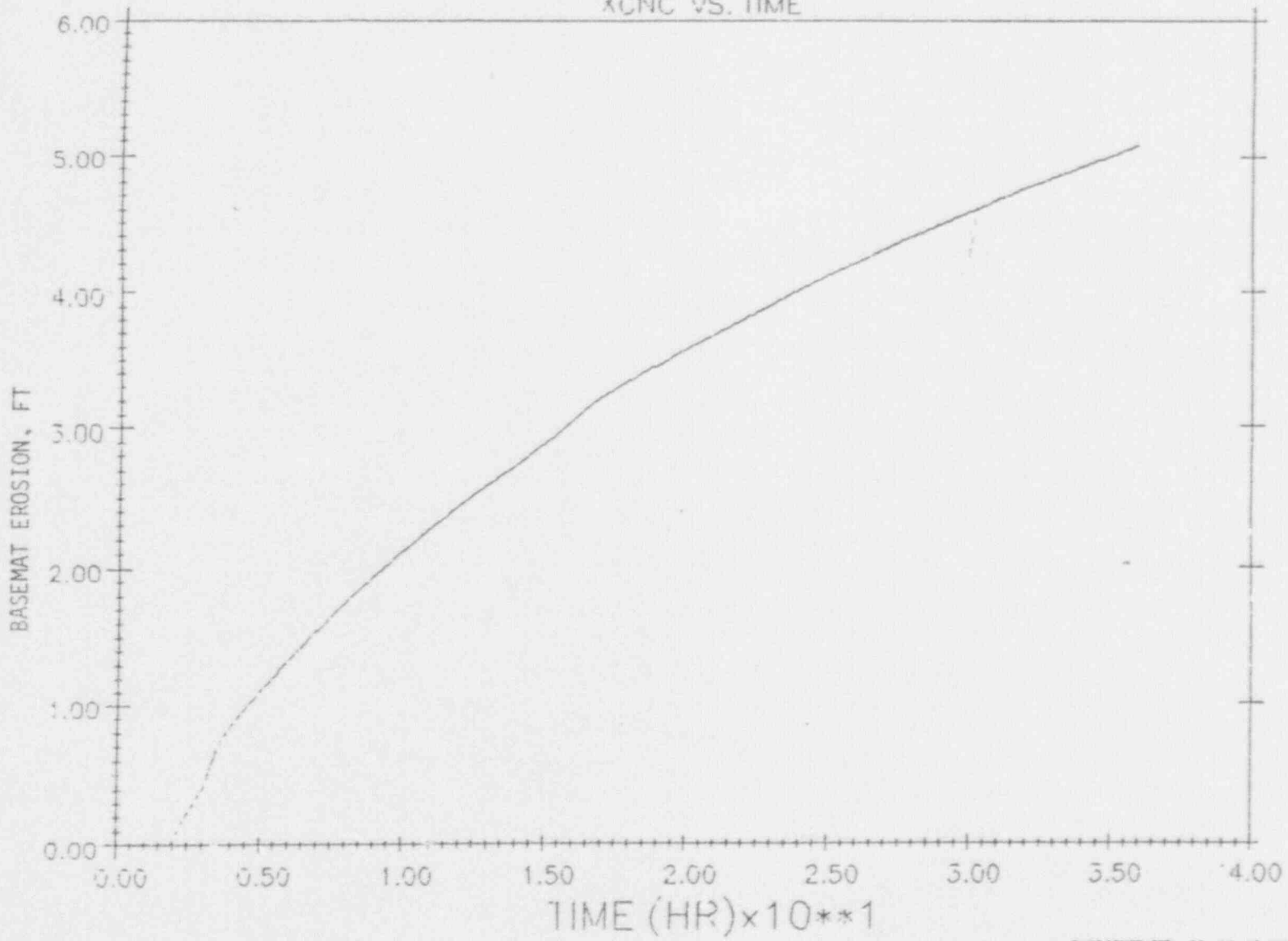


PLOT GENERATED - 28-JUL-80 09:38:38

Coal

4.91 CL EARLY FAIL DRY

XCNV VS. TIME



UO2, ACT GAS 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00
 AERO 2.6404E-03 1.1766E-03 3.5328E-05 2.7504E-03 0.0000E+00 0.0000E+00
 DEP AERO/GAS 6.6114E-01 1.2763E+00 9.9038E-02 1.3413E+00 0.0000E+00 0.0000E+00
 IN CORIUM 0.0000E+00 0.0000E+00 2.5000E+05

LEAKED FROM CONTHT: GAS MASS(LB) AEROSOL MASS(LB) RELEASE FRACTION

NOBL, IN 1.5592E+03 3.0295E+01 7.9318E-01
 C91 8.1989E-06 5.2376E+00 3.8906E-02
 TE02 8.7014E-29 2.2399E+00 1.3307E-02
 SR0 0.0000E+00 1.0928E-02 3.7411E-05
 MO02 0.0000E+00 1.7760E-02 1.4577E-05
 CS0H 1.5077E-02 3.5562E+01 4.5549E-02
 GA0 0.0000E+00 3.6747E-02 9.3778E-05
 LA203 0.0300E+00 4.9348E-04 2.1166E-07
 CE02 0.0100E+00 2.3801E-03 2.5183E-06
 SP 8.9238E-03 1.9074E+00 2.0875E-01
 TE2 4.8811E-01 1.0952E+00 1.1740E-02
 UO2, ACT 0.0000E+00 2.5750E-02 1.0292E-07

RELEASE CLASS 5.1

Class 4
t = 140 hours

NO. ITERATIONS IN PRIM SYS TRANSPORT MODEL: 1 IN CONTHT GAS TRANSPORT MODEL: 3

FISSIOM PRODUCT MASS BALANCES:

BALANCE 1 = TOTAL MASS AS USED BY MAAP
 BALANCE 2 = IN FUEL + INTEGRATED RELEASE FROM FUEL

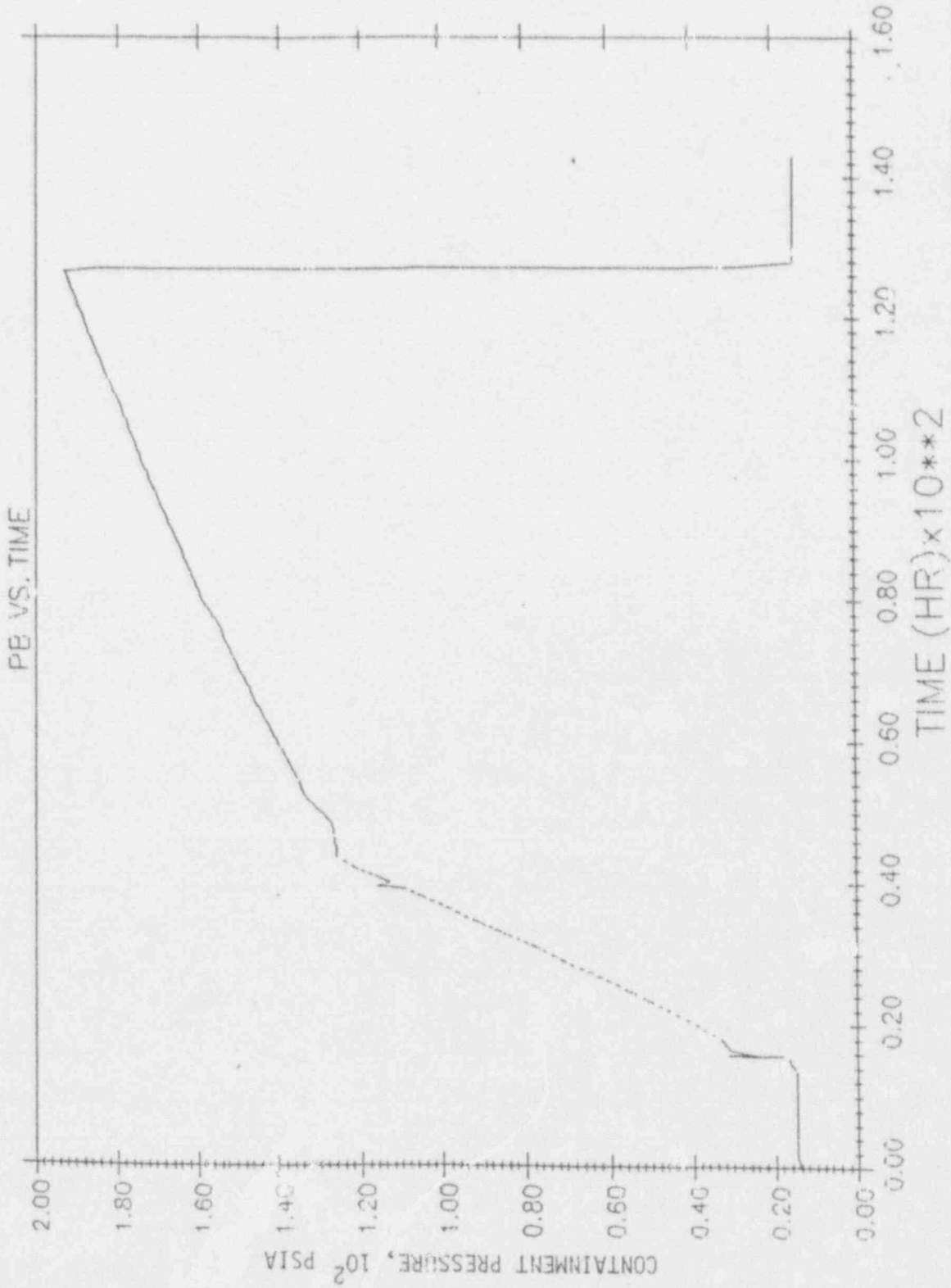
| | NOBLES | CS1 | TE02 | SR0 | MO02 | CS0H |
|----------|------------|----------|---------|-----------|-----------|-----------|
| BAL. 1: | 712.10083 | 61.06186 | 3.42127 | 133.30748 | 554.92566 | 354.29453 |
| BAL. 2: | 712.09961 | 61.06260 | 3.42127 | 133.30490 | 554.84570 | 354.29013 |
| INITIAL: | 712.09998 | 61.06259 | 2.94843 | 132.50000 | 552.65625 | 354.29031 |
| CORE: | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| CORIUM: | 0.00000 | 0.00000 | 0.00000 | 123.00731 | 427.78699 | 0.00000 |
| PS: | 0.14386 | 50.58181 | 0.00178 | 0.72725 | 122.35056 | 303.48398 |
| CONT: | 711.95697 | 10.48005 | 3.41949 | 9.57292 | 4.78812 | 50.81034 |
| INV REL: | 712.09961 | 61.06260 | 0.00000 | 0.74544 | 127.05857 | 354.29013 |
| EXV REL: | 6206.77490 | 0.00000 | 3.42127 | 9.55215 | 0.00014 | 0.00000 |

| | BA0 | LA203 | CE02 | SP | TE2 | UD2 |
|----------|-----------|------------|-----------|---------|----------|--------------|
| BAL. 1: | 200.14630 | 1063.86218 | 431.25928 | 4.17410 | 58.81182 | 113400.44531 |
| BAL. 2: | 200.13066 | 1063.86011 | 431.25839 | 4.17232 | 58.81169 | 113400.44531 |
| INITIAL: | 198.95653 | 1057.52490 | 426.68570 | 4.16393 | 58.43295 | 113392.09375 |
| CORE: | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| CORIUM: | 184.82861 | 1063.32910 | 428.95325 | 2.18885 | 8.90633 | 113398.89844 |
| PS: | 9.68557 | 0.27026 | 0.80507 | 0.26887 | 0.14393 | 0.00331 |
| CONT: | 5.63211 | 0.26283 | 1.50098 | 1.71637 | 49.76155 | 1.54676 |

RELEASE CLASS 5.1

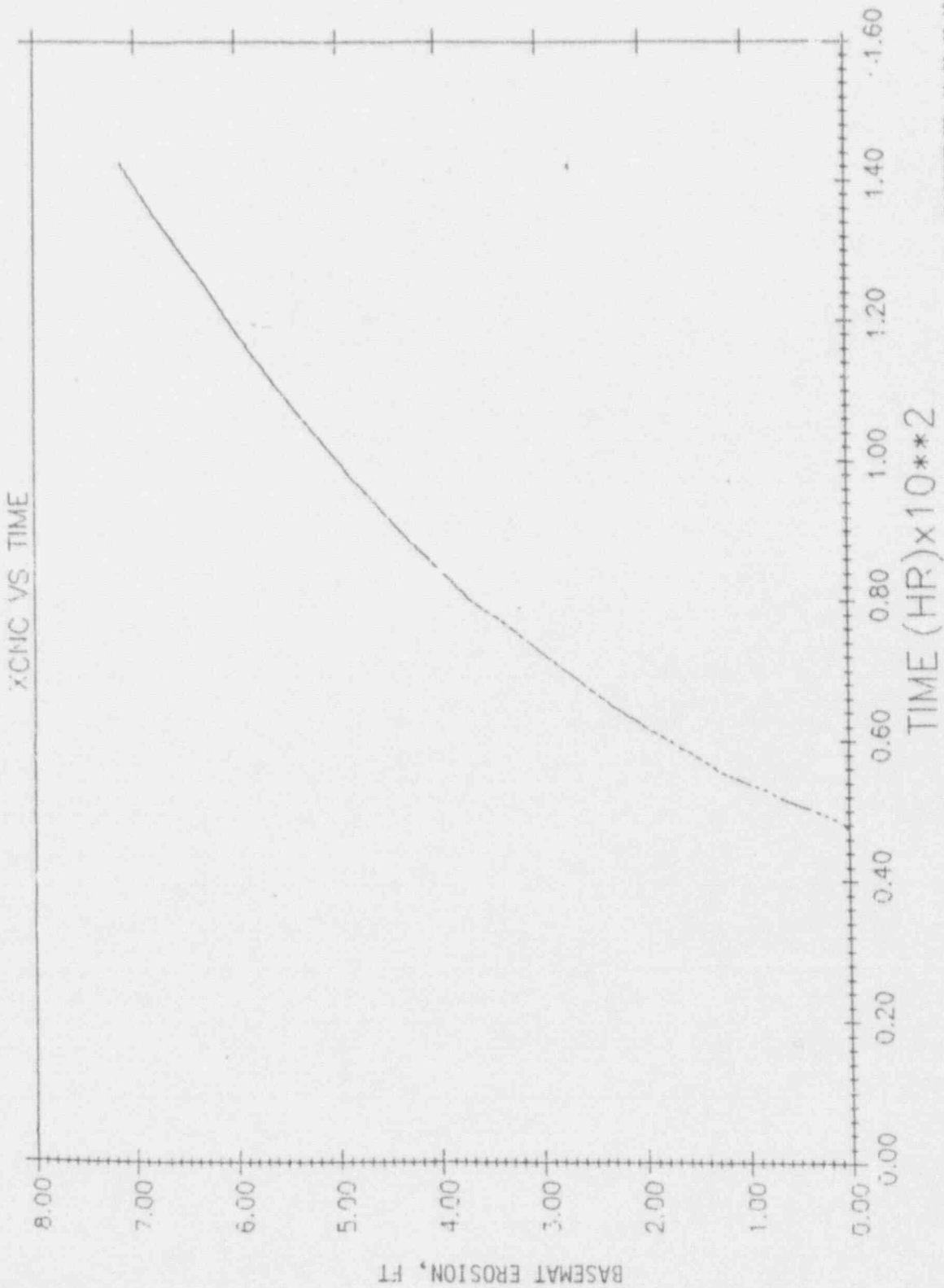
Case 4

LOOP DBL NOSPR LATE WET



RELEASE CLASS 5.3
Cont

LOOP DBL NOSPR LATE WET



PLOT GENERATED - 14-JUL-90 13:43:18

EFIN: (GAS) 0.0000E+00
 AERO 3.2043E-07
 DEP AERO/GAS 2.8727E-05
 IN CURTAIN 0.0000E+00

GUP 1.9654E-03
 GAS 0.6591E-13
 AERO -0.0470E-01
 DEP AERO/GAS 0.0000E+00
 IN CURTAIN

FE-2 3.0820E-01
 GAS 3.8986E-17
 AERO -0.0000E+00
 DEP AERO/GAS 0.0000E+00
 IN CURTAIN

FE-2 0.0000E+00
 GAS 3.0214E-04
 AERO 7.0425E-02
 DEP AERO/GAS 0.0000E+00
 IN CURTAIN

EFASED FROM CURTAIN: GAS MASS (LB) AEROSOL MASS (LB) RELEASE FRACTION
 NODS:IN 1.3097E+03 3.0063E+01 9.7308E-01
 (S) 1.1260E-04 2.9380E-01 2.1803E-02
 (FE-2) 1.9105E-09 3.0633E-01 1.8193E-03

SR0 0.0000E+00 1.4300E-02 4.9254E-09
 NODS 2.8669E-06 4.2447E-02 3.4830E-05
 CR0N 7.2339E-02 1.6200E+00 2.1792E-03
 NAO 0.0000E+00 1.9945E-02 4.5510E-09
 LA203 0.0000E+00 2.8349E-03 1.2158E-06
 (FE-2) 0.0000E+00 2.4225E-02 2.5630E-05
 SR 6.0594E-02 1.0117E-01 1.7616E-02
 FE-2 1.0817E+00 1.5005E+00 1.9369E-02
 UO2:ACT 0.0000E+00 1.3090E-02 5.2394E-08

RELEASE CLASS 6.2

*Case 2
 t=350 hours*

NUM. ITERATIONS IN PRIM SYS TRANSPORT MODEL: 2 IN CURTAIN GAS TRANSPORT MODEL: 1

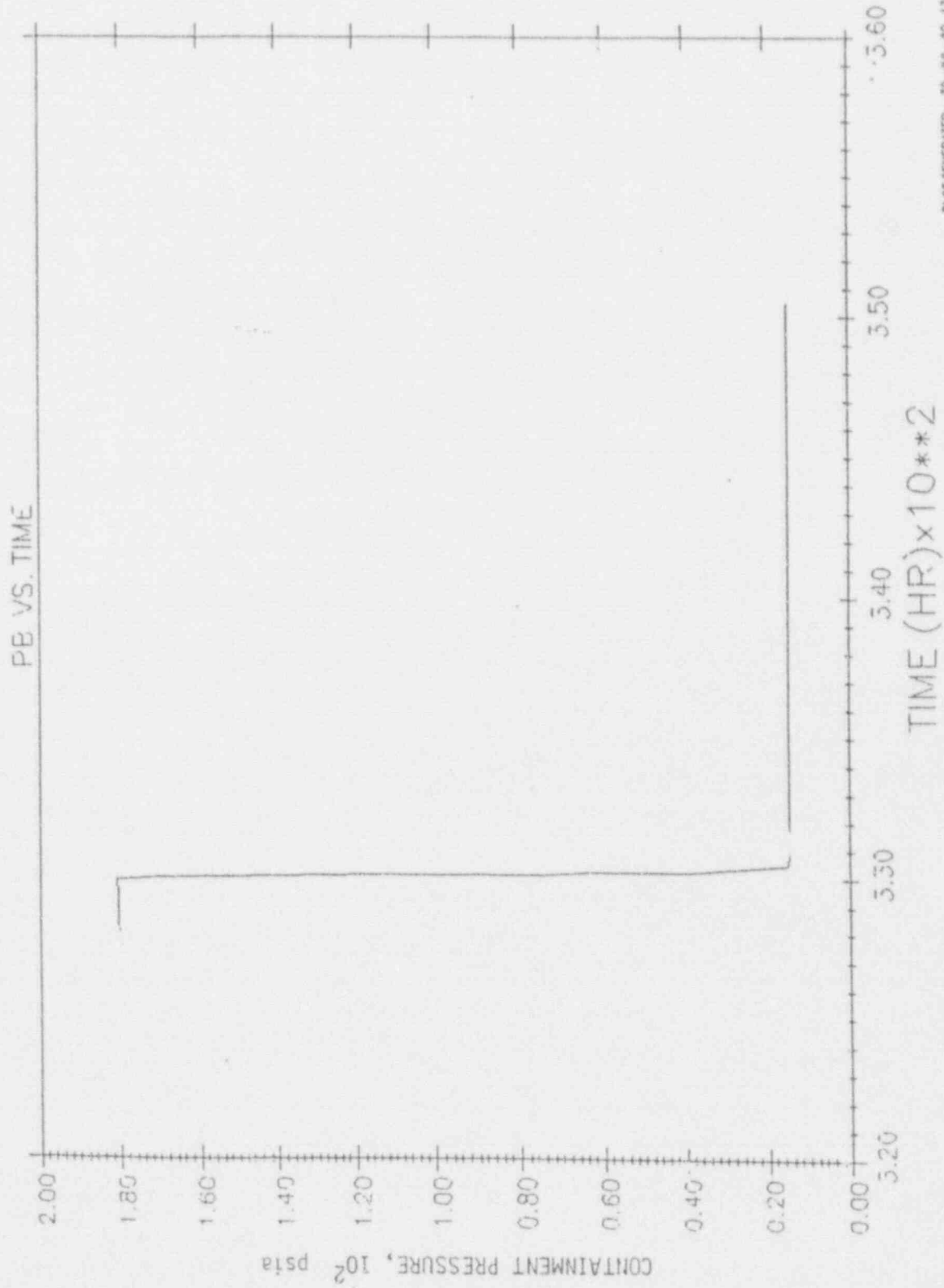
FISSION PRODUCT MASS BALANCES:

BALANCE 1 = TOTAL MASS AS USED BY HAAP
 BALANCE 2 = IN FUEL + INTEGRATED RELEASE FROM FUEL

| | MOXLES | CSI | TEO2 | SR0 | MOO2 | CR0N |
|---------|-----------|----------|----------|-----------|-----------|-----------|
| BAL. 1 | 711.09729 | 61.06078 | 71.44212 | 132.51192 | 552.61133 | 334.25281 |
| BAL. 2 | 711.09953 | 61.06053 | 71.44342 | 132.51312 | 552.61242 | 334.29053 |
| INITIAL | 711.09998 | 61.06057 | 71.44608 | 132.50000 | 552.65625 | 334.29031 |

4.91 CL LATE FAIL DRY

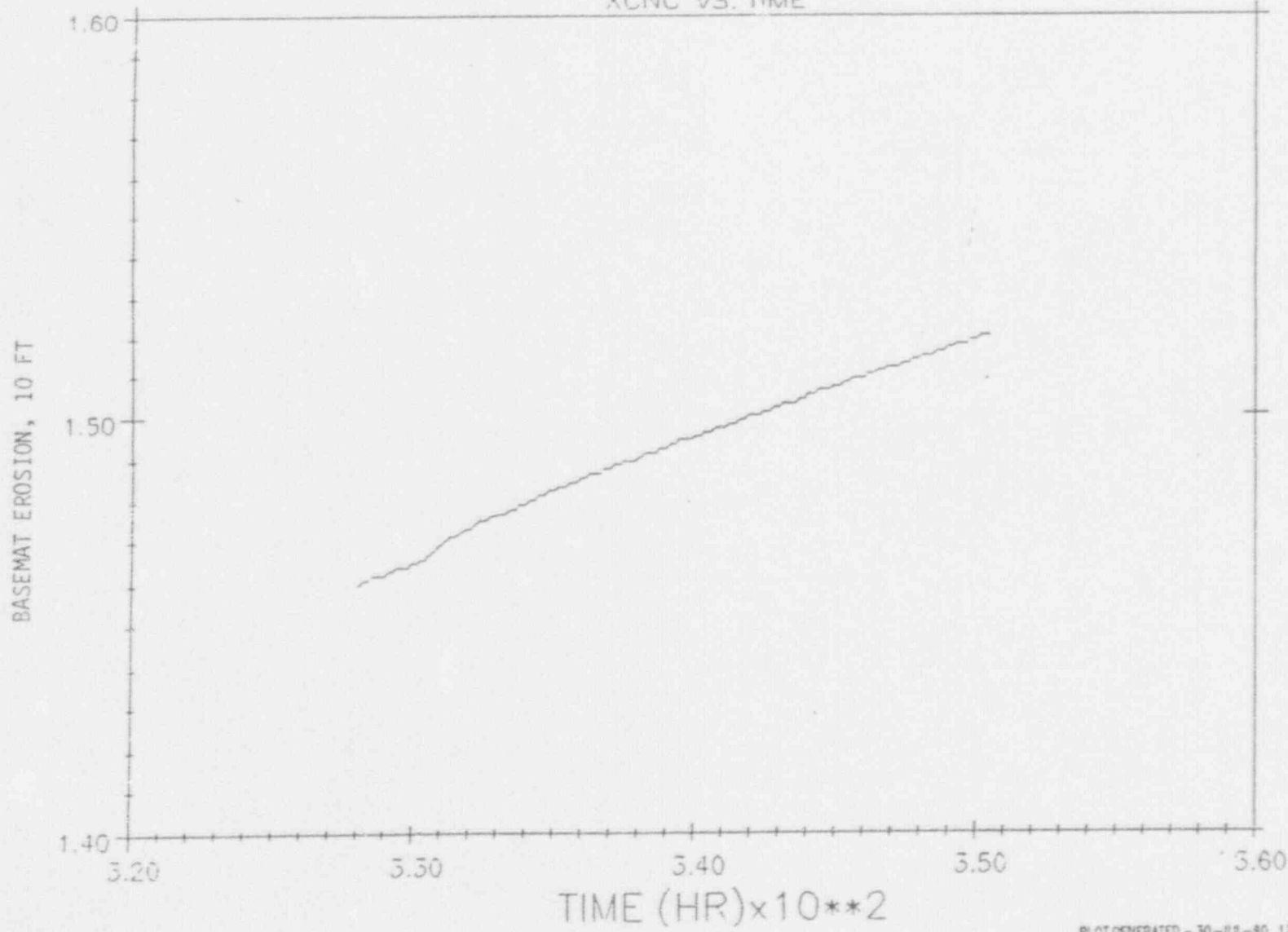
Case 2



4.91 CL LATE FAIL DRY

Case 2

XCNC VS. TIME



| | | | | | | | | | |
|--------------|-----------|------------|------------|-------------|-------------|------------|------------|------------|------------|
| CS01 | GAS | 4.5797E-09 | 4.2441E-09 | 1.0313E-09 | 6.8620E-08 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 2.3324E-09 |
| | AERO | 3.8066E-09 | 2.8389E-04 | 8.1273E-07 | 4.6026E-02 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 1.6080E-03 |
| DEP AERU/GAS | | 1.8717E-01 | 4.7017E-01 | 5.0894E+01 | 3.4836E+01 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 8.3424E+01 |
| | IN CORIUM | 0.0000E+00 | 0.0000E+00 | 0.0600E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| RAD | GAS | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| | AERO | 1.7719E-09 | 5.3920E-08 | 4.0645E-11 | 2.2235E-07 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| DEP AERU/GAS | | 7.8897E-09 | 2.1087E-06 | 3.4547E+00 | 2.4597E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 7.6378E-06 |
| | IN CORIUM | 0.0000E+00 | 0.0000E+00 | 4.1943E+02 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 6.5355E+00 |
| I A203 | GAS | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| | AERO | 0.6475E-10 | 2.3829E-09 | 3.0422E-12 | 1.0815E-08 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 3.3662E-07 |
| DEP AERU/GAS | | 3.8905E-09 | 1.0255E-07 | 1.2276E-01 | 8.0381E-02 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 2.5342E-01 |
| | IN CORIUM | 0.0000E+00 | 0.0000E+00 | 2.3672E+03 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| CF02 | GAS | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| | AERO | 5.4310E-09 | 1.4059E-08 | 1.7994E-11 | 6.7771E-08 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 1.9824E-06 |
| DEP AERU/GAS | | 2.4370E-08 | 6.4250E-07 | 8.3229E-01 | 4.3718E-01 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 1.5939E+00 |
| | IN CORIUM | 0.0000E+00 | 0.0000E+00 | 9.5520E+02 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| HP | GAS | 1.0509E-10 | 1.1851E-10 | 3.2676E-10 | 2.4920E-09 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 1.0825E-10 |
| | AERO | 3.7044E-05 | 2.7824E-06 | 7.6399E-09 | 4.4790E-04 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 1.8523E-05 |
| DEP AERU/GAS | | 1.8716E-04 | 4.2156E-03 | 5.1712E-01 | 6.4058E-01 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 1.5298E+00 |
| | IN CORIUM | 0.0000E+00 | 0.0000E+00 | 6.3828E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| TF02 | GAS | 6.2809E-07 | 5.4461E-07 | 1.0887E-08 | 5.6394E-06 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 2.5023E-07 |
| | AERO | 5.4672E-07 | 3.2711E-07 | -2.6166E-18 | -5.9242E-16 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 4.5037E-05 |
| DEP AERU/GAS | | 1.6926E-06 | 2.6864E-05 | 1.1839E+01 | 1.0466E+01 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 2.7872E+01 |
| | IN CORIUM | 0.0000E+00 | 0.0000E+00 | 8.6804E+01 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| VR02, ACT | GAS | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| | AERO | 4.2368E-09 | 1.1589E-09 | 1.4803E-11 | 5.2844E-08 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| DEP AERU/GAS | | 1.9020E-08 | 5.0105E-07 | 4.7991E-01 | 3.6704E-01 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 1.1110E+00 |
| | IN CORIUM | 0.0000E+00 | 0.0000E+00 | 2.5003E+05 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |

RELEASE FRACTION

| | | | |
|---------------------|---------------|-------------------|------------------|
| LEAKED FROM CONTAIN | GAS MASS (LB) | AEROSOL MASS (LB) | RELEASE FRACTION |
| NR01, IN | 4.7231E+01 | 2.0496E+00 | 3.0085E-02 |
| CF01 | 1.6483E-11 | 3.4513E-02 | 2.5638E-04 |
| TF02 | 0.0000E+00 | 0.0000E+00 | 0.0000E+00 |
| HP0 | 0.0000E+00 | 3.7072E-03 | 1.2698E-05 |
| HR02 | 0.0000E+00 | 2.4130E-02 | 1.9805E-05 |
| CS0H | 7.8389E-07 | 1.2468E-01 | 1.5962E-04 |
| RA0 | 0.0000E+00 | 2.6989E-03 | 6.1530E-06 |
| I A203 | 0.0000E+00 | 7.9140E-05 | 3.3945E-08 |
| CF02 | 0.0000E+00 | 4.1874E-04 | 4.4307E-07 |
| SB | 1.0143E-07 | 2.3289E-03 | 2.5372E-04 |
| TE2 | 1.4053E-05 | 6.7507E-03 | 6.4988E-05 |
| VR02, ACT | 0.0000E+00 | 2.9960E-04 | 1.1985E-07 |

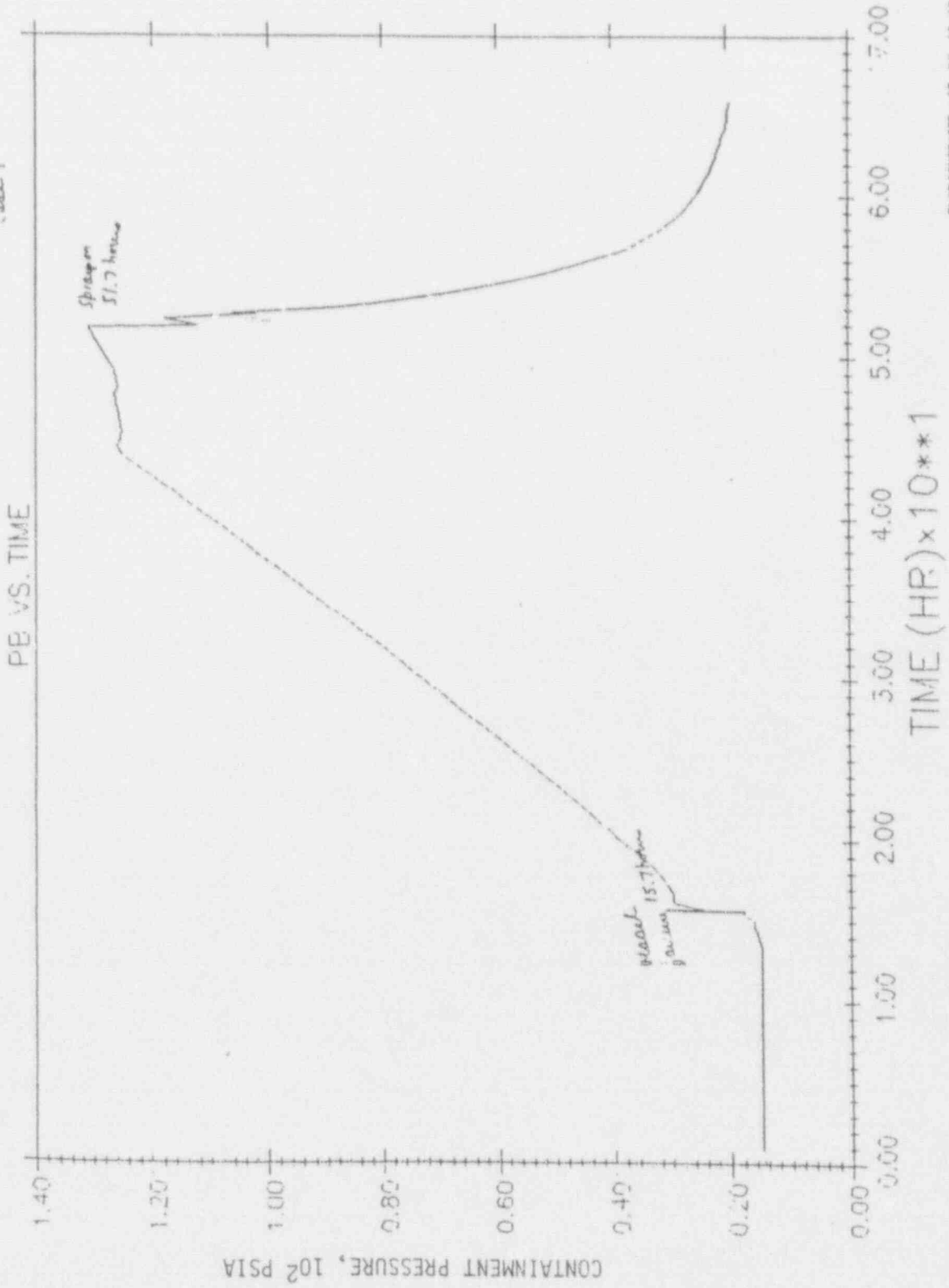
RELEASE CLASS 7.1

Case 1
t = 60 hours

RELEASE CLASS 7.1

LOOP DBL ISPR LATE WET

36 hour delay
can 1

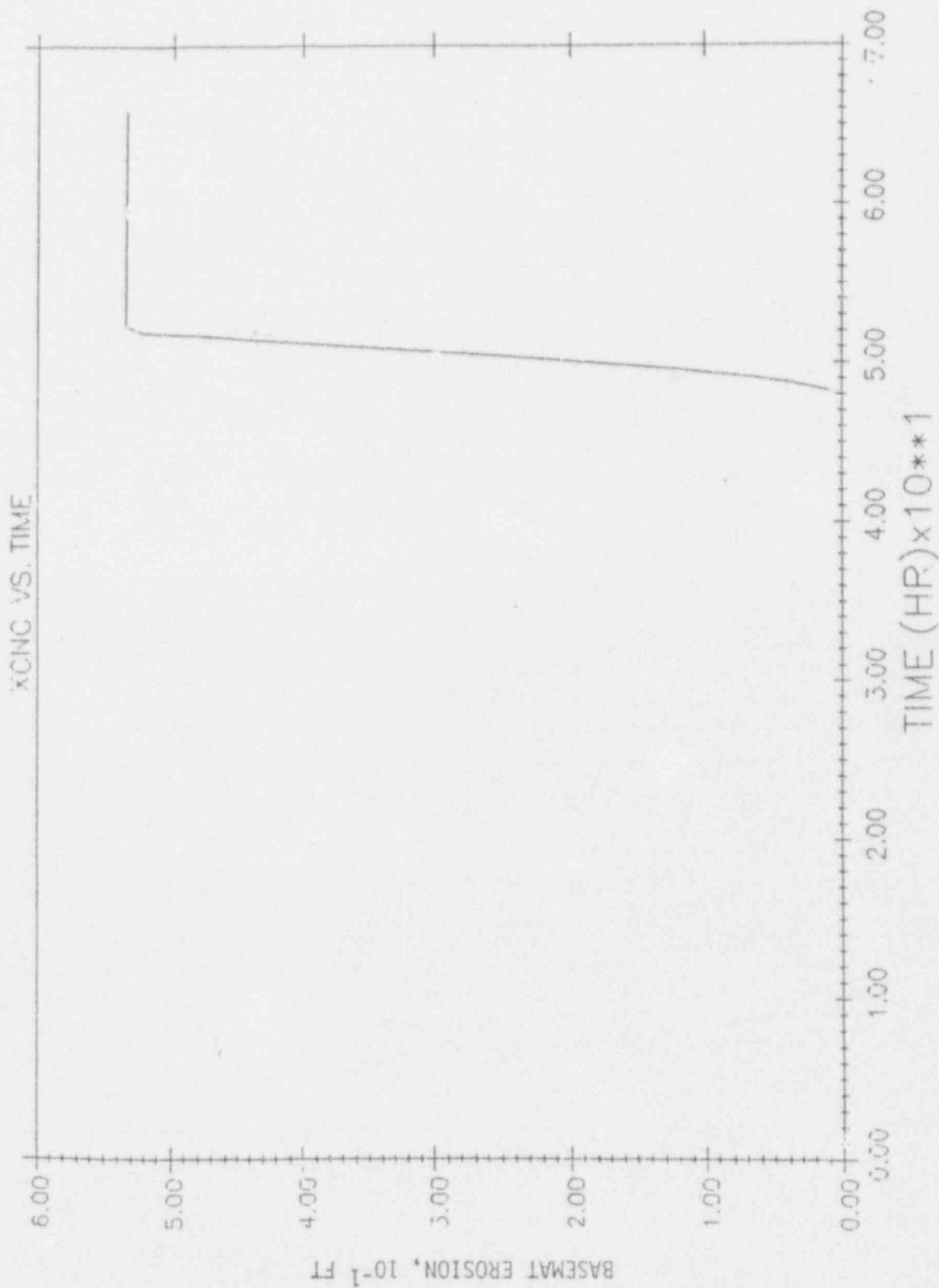


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RELEASE CLASS 7.1

LOOP DBL 1SPR LATE WET

$C_{max.1}$

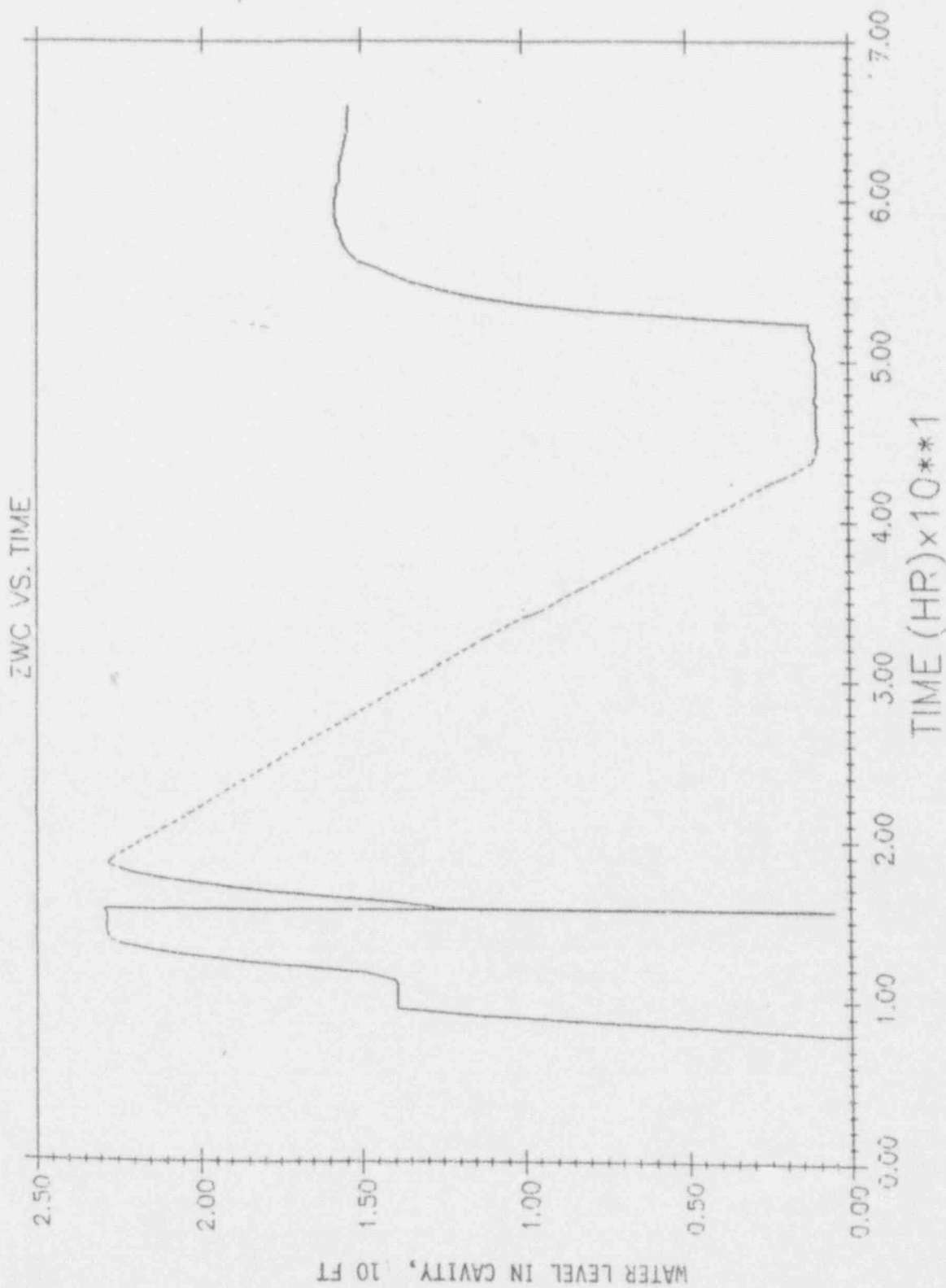


PLOT GENERATED - 27-JUL-68 - 090518

RELEASE CLASS 7.1

LOOP DBL 1SPR LATE WET

Case 1



PLOT GENERATED - 27-JUL-80 09:08:42