

June 7, 1995

Mr. Robert Palla US Nuclear Regulatory Commission Washington, D. C. 20555

TRANSMITTAL OF INFORMATION DISCUSSING AP600 LEVEL 2 HUMAN ACTIONS - JLR-18-95

Dear Mr. Palla:

Please find enclosed a copy of information prepared by Dr. Harold S. Blackman discussing the manner in which Westinghouse quantified Level 2 human actions in the AP600 PRA. As indicated by Dr. Blackman, the Westinghouse assumptions appear optimistic. In fact, requantification calculations performed by Dr. Blackman indicate that failure probabilities may be as much as an order of magnitude higher. Base on the enclosed information, I would recommend that sensitivity calculations be performed to assess the importance of Westinghouse assumptions related to human actions. Perhaps these sensitivity studies could be included in the planned Westinghouse importance analyses or as part of the IRRAS Level 2 database verification work that we are discussing. If you have any questions about the enclosed information, please contact Dr. Blackman (208-526-0245) or me (208-526-2897).

Sincerely,

Dr. Joy L. Rempe

Nuclear Accident Analysis Technologies

Cas Renpe

Enclosure

cc:

S. F. Armour, DOE-ID, MS 1219

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Enclosure June 6, 1995 JLR-18-95 Page 1 of 22

Date:

June 5, 1995

To:

J. L. Rempe

From:

H. S. Blackman

Subject:

HUMAN ACTIONS IN LEVEL 2 AP600 PRA

The approach I have taken to comment on the human actions you identified in your memo of April 11 is as follows. I first reviewed the analysis conducted by Westinghouse for its appropriateness, then conducted one or two additional analyses based on the available information. In general, I found the following three items of concern across all of the failure rates calculated by Westinghouse.

- 1. Multiple Recovery Paths
- 2. No Diagnosis
- Non-Standard Quantification of THERP Trees

Multiple Recovery Paths

Westinghouse applies multiple recoveries for every human action in their analysis. This is of concern, as I believe it to be an unrealistic representation of operating conditions in real plants. It is especially optimistic given that no control room, no procedures, and no agreed upon operating philosophy exists (there is an apparent dichotomy between the SSAR and the PRA). That is, Westinghouse routinely applies recovery values for the shift technical advisor, the senior reactor operator, and also something unique to this work called "slack time". Time is the sole determining factor as to when these various recovery factors are applied. The conditions are as follows:

Time window > 10 minute and slack time >5 minutes- STA recovery applied Time window > 5 minutes and slack time > or = 0- SRO recovery applied Slack time > 1 hour - Special recovery applied

In general, where time available is less than 30 minutes Westinghouse does apply only recovery by the STA. In cases where time available exceeds one hour a third opportunity for recovery is provided, that Westinghouse terms "slack time". All of these recoveries are based upon a THERP value for "one-of-a-kind checking with alert factors". This value is intended for use in normal operating conditions, which is generally not the case in most of these recovery situations. This value is probably inappropriately used. I also have never seen this many recoveries credited in any past PRA. This is not to say that Westinghouse could not engineer the system so that three recoveries are possible, but it is to say that I have never seen that accomplished before.

No Diagnosis

Westinghouse asserts that the procedural system in place at current Westinghouse plants eliminates the need for diagnosis, and reduces the operator function to detection and action. The symptomed based procedures do indeed, function this way. Unfortunately operating experience has shown that operators do still diagnose and, in fact, will circumvent procedures, skip ahead to solutions (which I believe Westinghouse plants also allow) when

operators "know" what the event is. Conventional PRA's do include diagnosis for the operator, to account for the cognitive processing that does take place with the operator and to account for decisions that the operator may make, in spite of procedural systems etc. I have a great deal of reservation about the lack of any diagnose in the AP600 PRA. Westinghouse is putting enormous faith in their procedures, administrative controls, and operators which has not been borne out by experience.

Non Standard Quantification of THERF Trees

Although a small matter, Westinghouse has chosen to quantify only the main branches of the THERP trees for the HRA. This does not fully account for all the recovery paths, and success paths. Generally it does not make a huge difference in the calculated value, but none-the-less is less than accurate.

Recalculations

The Table below shows the recalculations performed. As previously mentioned, two levels of recalulations were performed, first was a reduction in the number of recoveries, and an increase in the assumed dependency. Second, for two cases, was a recalculation including a diagnosis task. Obviously, these values are generally higher in terms of the overall failure rate calculated. The column entitled AP600 shows the value provided by Westinghouse, the column AP600-THERP Tree is the recalculation including all recoveries and success paths, the column INEL modified represents the reduction of the number of recoveries and the increase in dependency from moderate to high, and the last column INEL New Model, includes a diagnosis task. I have attached the trees and tables for REN-MAN-02 and CIA-MAN-01 as examples for your review.

Human Error	AP600	AP600- THERP Tree	INEL Modified	INEL New - Model
REN-MAN-02	.0024	.0025	.0083	.027
REN-MAN-03	.0034		.0071	
VLN-MAN-01	.000162		.0015	
CID-MAN-01	.0012		.012	
CIA-MAN-01	.0059	.0059	.0075	.03
CIC-MAN-01	.00012		.012	
CIB-MAN-01	.00134		.00266	
CIB-MAN-00	.00184		.0036	
ADN-MAN-01	.000493		.0033	
ADN-REC-01				
LPM-MAN-01	.0022		.0042	
LPM-MAN-02	.0065		.0057	
LPM-MAN-03	.083		.6	

Of particular significance is the increase for the category titled INEL new model, which includes diagnosis. These represent an order of magnitude shift in the failure probability. I have included the trees and tables for both of these examples for your information.

Summary

I believe that the Westinghouse HRA is an optimistic analysis of the operator's role in the AP600 as compared to conventional PRAs. The analysis is a thorough, and

understandable one, however gives an inordinate amount of credit for recovery, and treats the operators as more of an autotron than a thinking human being. The use of certain values for recovery seem inappropriate and the actual quantification of the THERP trees is more of an estimate than a thorough quantification. The importance of time in the Westinghouse recovery methods does make the calculation of time windows particularly important, in that additional recoveries are based upon this value. The thermal-hydraulic run, and the code used, take on a greater importance for the HRA because of this reason. After having said all of this it is important to note that I have not rerun any of these numbers through the complete analysis and therefore have no idea whether any of these changes are risk significant.

INEL New Model

Table 3. ren-man-02

	Main Paths	Median CREP	Mesn CREP	Timer Factor	Remind HET	Nombel HIP Source	SES/DTN I	157 Medifie: 15F Method	Dependency Brief Typo
a/A-Crew falls to diagnose	0.00050	0.00050	0.00081	(5.0)	0.00010	Table 12-45	585	5.0	20
B- Operator selects wrong control (same as AP600)		0.013	0.021	(5.0)	0.0026		SBS	5.0	20
c/C-Second operator selects wrong control (same as AP600)	0.0066	0.51	0.51	(5.0)	0.0026		585	5.0	Ю
D-Operator omits 1/2 steps (same as AP600)		0.038	0.061	(5.0)	0.0076		585	5.0	ZD
(F- Second operator omits 1/2 steps (same as AP600)	0.019	0.52	0.53	(5.0)	0.0076		585	5,0	Ю
Main Paths Total P(f):	0.026		EF:	(5.0)	TotalP	P(f): 0.027			

Table 3b. ren-man-02

J	Failure Paths (> = 1E-6)	Calculations (Medians Displayed)	Median Results	Mean Results
1	A	0.0005	0.00050	0.00081
2	aBC	1.0 x 0.013 x 0.51	0.0066	0.011
3	aBcDE	1.0 x 0.013 x 0.49 x 0.038 x 0.52	0.00013	0.00033
1	abDE	1.0 x 0.99 x 0.038 x 0.52	0.019	0.032
		Total Failure Probability	0.027	0.044
		Error Factor	5.0	5.0

Table 3a: HEPs for ren-man-02

HEP Factor HEP) (ER) (-								
g control (same as loops of same as loops (same as loops same as loops (same as loops same as loops (same as loops same as loops same as loops same as loops (same as loops same same as loops same as loops same same as loops same same as loops same same same same same same same sam	Human Action / Error	Nominal Median HEP	Error	Source/ THERP Table#	Step-by. Step or Dynamic	Modifier for PSFs	Modifier	THERP Depend- ency	Median CHEP (Mean CHEP)	Error	Error Type
0.0026 5.0 SBS 5.0 ZD 0.013 0.0026 5.0 SBS 5.0 HD 0.51 0.0076 5.0 SBS 5.0 HD 0.631 0.0076 5.0 SBS 5.0 HD 0.638 0.0076 5.0 SBS 5.0 HD 0.622 0.053 0.053 0.653 0.653 0.653	Orew fails to diagnose	0.00010	8.0	Table 12-4# 5	SBS	5.0		az az	0.00050	5.0	
6.0076 5.0 SBS 5.0 HD 0.51 6.0076 5.0 SBS 5.0 ZD 0.038 6.0076 5.0 SBS 5.0 HD 0.52 (0.051)	Operator selects wong control (same as AP600)	0.0026	5.0		SBS	5.0		CZ	(0.021)	5.0	
0.0076 5.0 SBS 5.0 ZD 0.038 0.0076 5.0 SBS 5.0 HD 0.52 (0.53)	Second operator selects wrong control (same as AP600)	0.0026	5.0		SBS	5.0		<u>A</u>	0.51	5.0	
0.0076 5.0 HD 0.52 (0.53)	Operator omits 1/2 steps (same as AP600)	6.0076	5.0		SBS	5.0		az za	0.038	8.0	
	Second operator omits 1/2 steps (same as AP600)	ALCOHOL STREET, STREET	5.0) car	SBS	5.0		Œ	0.52 (0.53)	5.0	

Table 2. ren-man-02

	Male Pette	Medias Off?	Mess CVEP	Emer Factor	Number 157	Rembazi HEP Source	MENDYN PSFM	MS/DYN FS Modifier PS Method	Department	Stree Type
a A-fail to respond to 1/5 alarens		0.040	0.065	(20)	0.0080		385 5	5.0	QZ	
b B- Sta falls to respond to 1/5 alarms		0.18	0.20	(2.0)	0.0080		288	3.0	QW	
C.SRO falls to respond to 1/5 alarms	0.0037	0.52	0.53	(8.0)	0.0080		SHS	5.0	9	
D-Select wrong control		0.013	1200	(3.0)	0.0026		S S S S S S S S S S S S S S S S S S S	5.0	æ	
e/f- 51 A fails		0.15	0.16	(2.0)	0.0026		5885	03	Q	
//-Stolails	1100.0	0.57	09'0	(3.8)	970'0		S#S	5.0	9	
Comit 1/2 steps		0.038	0.061	(20)	9700'0		388	5.0	02	
H-STAfalls		82.0	0.20	(15.0)	9.0076		285	05	S.	
A Stofalls	0.0032	0.52	0.53	(20)	9.00.0		383	2	£	
Male Parke Total PCD	0.0000		ŧ		Totaloff).	(). 0.0002				

Print Date: 18-MAY-95

Table 2a: HEPs for ren-man-02

	Human Action / Error	Nominal Median HEP		Source/ THERP Table #	Step-by- Step or Dynamic	Modifier for PSFs	Modifier Source	THERP Depend- ency	Median CHEP (Mean CHEP)	Error Factor	Error Type
	Fail to respond to 1/5 alarms	0.0080	5.0		SBS	5.0		ZD	0.040 (0.065)	5.0	
3	\$ta fails to respond to 1/5 alarms	0.0080	5.0		SBS	5.0		MD	0.18 (0.20)	5.0	
C	SRO falls to respond to 1/5 alarms	0.0080	5.0		SBS	5.0		HD	0.52 (0.53)	5.0	
)	Select wrong control	0.0026	5.0		SBS	5.0		ZD	0.013 (0.021)	5.0	
3	STA fails	0.0026	5.0		SBS	5.0		MD	0.15 (0.16)	5.0	
F	SRO fails	0.026	5.0		SBS	5.0		HD	0.57 (0.60)	5.0	
G	Omit 1/2 steps	0.0076	5.0		SBS	5.0		ZD	0.038 (0.061)	5.0	
Н	STA fails	0.0076	5.0		SBS	5.0		MD	0.18 (0.20)	5.0	
1	SRO fails	0.0076	5.0		SBS	5.0		HD	0.52 (0.53)	5.0	

Table 2b. ren-man-02

1	Failure Paths (> = 1E-6)	Calculations (Medians Displayed)	Median Results	Mean Results
1	ABC	0.04 x 0.18 x 0.52	0.0037	0.0068
1	ABcDEF	0.04 x 0.18 x 0.48 x 0.013 x 0.15 x 0.57	0.000003	0.000012
3	ABcdGHI	0.04 x 0.18 x 0.48 x 0.99 x 0.038 x 0.18 x 0.52	0.000012	0.000037
	AbDEF	0.04 x 0.82 x 0.013 x 0.15 x 0.57	0.000037	0.00011
	AbDeGHI	0.04 x 0.82 x 0.013 x 0.85 x 0.038 x 0.18 x 0.52	0.000001	0.000005
	AixIGHI	0.04 x 0.82 x 0.99 x 0.038 x 0.18 x 0.52	0.00011	0.00032
	aDEF	0.96 x 0.013 x 0.15 x 0.57	0.0011	0.0019
	«DE/GHI	0.96 x 0.013 x 0.15 x 0.44 x 0.038 x 0.18 x 0.52	0.000003	0.000008
)	sDeGHI	0.96 x 0.013 x 0.85 x 0.038 x 0.18 x 0.52	0.000037	0.00010
10	adGHI	0.96 x 0.99 x 0.038 x 0.18 x 0.52	0.0033	0.0058
	Prince of the second	Total Failure Probability	0.0083	0.015
		Error Factor	5.0	5.0

AP600 THERP Tree

Table 1. ren-man-02

	Main Poths	Medies CHEF	Mesn CHEP	Emerfactor	Nominal SEP Remissi SEP Seerce	SES/DYN PSF Modifier PSF Method	Dependency from Type
a/A-Fall to respond to 1/S alarms		0.040	0.065	(5.0)	0.0080	585 5.0	ZD
b\\ 8- Sta falls to respond to 1/5 alarms		0.41	0.65	(5.0)	0.081	585 5.0	ZD
c/C-SRO falls to respond to 1/5 alarms		0.13	0.17	(5.0)	0.081	SBS 1.0	LD
d/D-time credit	0.0011	0.54	0.57	(5,0)	0.081	585 1.0	НО
e E- Select wrong control		0.013	0.021	(5.0)	0.0026	585 5.0	70
f F- STA fails		0.41	0.65	(5.0)	0.081	585 5.0	ZD
g G-SRO fafts		0.13	0.17	(5.0)	0.081	585 1.0	LD
h/H-time credit	0.00035	0.54	0.57	(5.0)	0.081	585 1.0	НО
Omit 1/2 steps		0.038	0.061	(5.0)	0.0076	585 5.0	ZD
J- STA falis		0.41	0.65	(5.0)	0.081	585 5.0	20
K-SRO falls		0.13	0.17	(5.0)	0.081	\$85 1.0	10
1 L- time credit	0.00098	0.54	0.57	(5.0)	0.081	585 1.0	HD

Table 1a: HEPs for ren-man-02

	Human Action / Error	Nominal Median HEP		Source/ THERP Table #	Step-by- Step or Dynamic	Modifier for PSFs	Modifier Source	THERP Depend- ency	Median CHEP (Mean CHEP)	Error Factor	Error Type
۸.	Fail to respond to 1/5 alarms	0.0080	5.0		SBS	5.0		ZD	0.040 (0.065)	5.0	
В	\$ta fails to respond to 1/5 alarms	0.081	5.0		SBS	5.0		ZD	0.41 (0.65)	5.0	
С	SRO fails to respond to 1/5 alarms	0.081	5.0		SBS	1.0		LD	0.13 (0.17)	5.0	
D	time credit	0.081	5.0		SBS	1.0		HD	0.54 (0.57)	5.0	
E	Select wrong control	0.0026	5.0		SBS	5.0		ZD	0.013 (0.021)	5.0	
F	STA fails	0.081	5.0		SBS	5.0		ZD	0.41 (0.65)	5.0	
G	SRO fails	0.081	5.0		SBS	1.0		LD	0.13 (0.17)	5.0	
H	time credit	0.081	5.0		SBS	1.0		HD	0.54 (0.57)	5.0	
I	Omit 1/2 steps	0.0076	5.0		SBS	5.0		ZD	0.038 (0.061)	5.0	
J	STA fails	0.081	5.0		SBS	5.0		ZD	0.41 (0.65)	5.0	
K	SRO fails	0.081	5.0		SBS	1.0		LD	0.13 (0.17)	5.0	

Table 1a: HEPs for ren-man-02

Human Action / Error	Nominal Median HEP		Source/ THERP Table #		Modifier for PSFs	Modifier Source	THERP Depend- ency	Median CHEP (Mean CHEP)	Error Factor	Error Type
L time credit	0.081	5.0		SBS	1.0		HD	0.54 (0.57)	5.0	

Table1b. ren-man-02

	Calculations (Medians Displayed)	Median Results	Results
Failure Paths (> = 1E-6)		0.0011	0.0042
ABCD	0.04 x 0.41 x 0.13 x 0.54	0.000005	0.000047
ABcEFGH	0.04 x 0.41 x 0.87 x 0.013 x 0.41 x 0.13 x 0.54	0.000015	0.00013
ABcelJKL	0.04 x 0.41 x 0.87 x 0.99 x 0.038 x 0.41 x 0.13 x 0.54	0.00008	0.000030
4 AMEPGH	0.04 x 0.6 x 0.013 x 0.41 x 0.13 x 0.54	0.000025	0.000087
5 AbelJKL	0.04 x 0.6 x 0.99 x 0.038 x 0.41 x 0.13 x 0.54	0.00035	0.0013
6 NEFCH	0.96 x 0.013 x 0.41 x 0.13 x 0.54	0.000004	0.000042
7 aEFgIJKL	0.96 x 0.013 x 0.41 x 0.87 x 0.038 x 0.41 x 0.13 x 0.54	0.000007	0.000027
8 sENJKL	0.96 x 0.013 x 0.6 x 0.038 x 0.41 x 0.13 x 0.54	0.0010	0.0036
9 selJKL	0.96 x 0.99 x 0.038 x 0.41 x 0.13 x 0.54		0.0094
	Total Failure Probability	0.0025 5.0	5.0
	Error Factor		

Lable . Cla mano Louse cast	Natural Natural	Nedles CHF	Nedles CHE Mess CHE	they factor	Residue) NEP Newsimal NEP Secrets	MS-10TN 15F Modifier 75F Method	Department
A-Operator (sis to respond to V2 alarms-			0.013	(8.0)	0.00%	8.0	R
b & SAO fells to respond to 1/2 alarms	0.00080	0.30	91.0	(5.0)	0.0	93	2
C-Operator selects wrong control for 1/2		0.013	0.021	(8.0)	9.0026	5.0	2
valves- d. D-SRO selects wrong control for 1/2 valves-	0.001	0.10	0.16	(8.0)	6.30	10	R
(E- Operator omits step to close V2 valves—		0.038	0.061	(0'5)	9,0076	5.0	82
F St. O omits step to dose 1/2 valves-	0.0036	0.10	97.0	(8.0)	0.0	01	02
	A AACT		ti	(5.0)	E. (cm TotalP(f): 0.0059	6	

Table . cia-man01 (Base Case)

1	Failure Paths (> = 1E-6)	Calculations (Medians Displayed)	Median Results	Mean Results
1	AB	0.008 x 0.1	0.00080	0.0021
2	AbCD	0.008 x 0.9 x 0.013 x 0.1	0.000009	0.000037
3	AbcEF	0.008 x 0.9 x 0.99 x 0.038 x 0.1	0.000027	0.00011
	RCD	0.99 x 0.013 x 0.1	0.0013	0.0033
5	ACHEE	0.99 x 0.013 x 0.9 x 0.038 x 0.1	0.000044	0.00017
6	acEF	0.99 x 0.99 x 0.038 x 0.1	0.0037	0.0096
E		Total Failure Probability	0.0059	0.015
		Error Factor	5.0	5.0

Table : HEPs for cia-man01 (Base Case)

	Human Action / Error	Nominal Median HEP		Source/ THERP Table #	Step-by- Step or Dynamic	Modifier for PSFs	Modifier Source	THERP Depend- ency	Median CHEP (Mean CHEP)	Error Factor	Error Type
٨	Operator fails to respond to 1/2 siarms-	0.0016	5.0			5.0		ZD	0.0080 (0.013)	5.0	
В	SRO fails to respond to 1/2 alarms-	0.10	5.0			1.0		ZD	0.10 (0.16)	5.0	
С	Operator selects wrong control for 1/2 valves—	0.0026	5.0			5.0		ZD	0.013 (0.021)	5.0	
D	SRO selects wrong control for 1/2 valves—	0.10	5.0			1.0		ZD	0.10 (0.16)	5.0	
E	Operator omits step to close 1/2 valves—	0.0076	5.0			5.0		ZD	0.038 (0.061)	5.0	
F	SRO omits step to close 1/2 valves-	0.10	5.0			1.0		ZD	0.10 (0.16)	5.0	

Table . cia-man01(Base Case)

	Rate Pothe	Nesher OEP	Meyn (36)	Errer Factor	Secting 189 Seminal 189 Severa	SELDTH 15 Kadiller 15 Method	Department
A-Operator falls to respond to 1/2 alarms-			0.013	(5.0)	0.00%	5.0	Ø
b/8- SRO falls to respond to 1/2 slerms-	0.00.0	0.13	0.0	(0.2)	0.081	91	01
C-Operator selects wrong control for 1/2 valves-		81070	0.071	(8.0)	970070	5.0	92
D-SAO selects wrong control for V2 valves-	9100.0	6.8	0.7	(8.0)	190'0	2	9
e E- Operator omits step to dose 1/2 raives-		0.038	1907	(0.2)	6.6676	5.0	82
/ F- SAO omits step to dose 1/2 valves-	0.0046	0.13	Δ.0	(20)	0.061	2	9
Main Paths Total P(f);	0.0073		ä	(50)	Total P(f): 0.0075		

"..... 75 tilly 85

12.2	Human Action / Error	Nominal Median HEP	Error	Source/ THERP Table #	Step-by- Step or Dynamic	Modifier for PSFs	Modifier	THERP Dependency	Median CHEP (Mean CHEP)	Error	Error Type
<	Operator fails to respond to 1/2 alarms-	0.0016	5.0			5.0		92	0.0080	3.0	
20	SRO fails to respond to 1/2 alarms-	0.081	5.0			1.0		9	0.13 (0.17)	20	
0	Operator selects wrong control for 1/2 valves—	0.0026	20			\$0		92	(0.021)	5.9	
Q	SRO selects wrong control for 1/2 valves—	0.061	5.0			1.0		a	(0.13	5.0	
(m2	Operator omits step to close 1/2 valves- 0.0076	0.0076	5.0			2.0		220	(0.0038	5.0	
la.	SRO omits step to close 1/2 valves-	0.081	5.0			1.0		9	(0.13	5.0	

Table . cia-man01 (Base Case)

]	Failure Paths (> = 1E-6)	Calculations (Medians Displayed)	Median Results	Mean Results
1	AB	0.008 x 0.13	0.0010	0.0022
2	AbCD	0.008 x 0.87 x 0.013 x 0.13	0.000012	0.000039
3	AbcEF	0.008 x 0.87 x 0.99 x 0.038 x 0.13	0.000033	0.00011
4	8CD	0.99 x 0.013 x 0.13	0.0016	0.0036
5	*CdEF	0.99 x 0.013 x 0.87 x 0.038 x 0.13	0.000054	0.00018
6	scEF	0.99 x 0.99 x 0.038 x 0.13	0.0047	0.010
		Total Failure Probability	0.0075	0.017
		Error Factor	5.0	5.0

INEL New Model

Table . cia-man01(Base Case)

	Main Paths	Reduc CRF	Mesa CHEP	Error Factor	Nominal IET Kominal IET Source	SES/STN PSF Nodifier PSF Method	Depandency
A-Crew falls to diagnose		0.48	0.78	(5.0)	0.48	1.0	ZD
b\\B- Crew falls to respond to 1/2 slarms	0.0038	0.0080	0.013	(5.0)	0.0016	5.0	20
C-Operator omits step to close 1/2 valves~		0.013	0.021	(5.0)	0.0026	5.0	ZD
d D-SRO omits step to close 1/2 valves-	0.0034	0.51	0.51	(5.0)	0.0076	5.0	Ю
AF- Operator selects wrong control for 1/2 valves-		0.038	0.061	(5.0)	0.0076	5.0	20
F- SRO selects wrong control for 1/2 valves-	0.0098	0.52	0.53	(5.0)	0.0076	5.0	но
Main Paths Total P(f):	0.017		EF:	(5.0)	Total P(f): 0.030		

Table . cia-man01 (Base Case)

1	Failure Paths (> = 1E-6)	Calculations (Medians Displayed)	Median Results	Mean Results
1	AB	0.48 x 0.008	0.0038	0.010
2	AbCD	0.48 x 0.99 x 0.013 x 0.51	0.0031	0.0082
3	AbOSEF	0.48 x 0.99 x 0.013 x 0.49 x 0.038 x 0.52	0.000060	0.00026
4	AbcEF	0.48 x 0.99 x 0.99 x 0.038 x 0.52	0.0093	0.024
5	I (C)	0.52 x 0.013 x 0.51	0.0034	0.0024
,	*CdEF	0.52 x 0.013 x 0.49 x 0.038 x 0.52	0.000066	0.000075
7	acEF	0.52 x 0.99 x 0.038 x 0.52	0.010	0.0071
		Total Failure Probability	0.030	0.053
		Error Factor	5.0	5.0

	Human Action / Error	Nominal Median HEP	Error	Source/ THERP Table #	Step-by- Step or Dynamic	Modifier for PSFs	Modifier	THERP Depend- ency	Median CHEP (Mean CHEP)	Error	Error Typa
<	Orew fails to diagnose	0.48	20			1.0		ß	0.48	5.0	
00	Grew fails to respond to 1/2 alarms	0.0016	5.0			5.0		23	0.0080 (0.013)	2.0	
0	Operator omits step to close 1/2 valves-	970070	5.0			5.0		az	(0.013	20	
0	SRO omits step to close 1/2 valves-	0.0026	5.0			20		H	0.51	8.0	
(m)	Operator selects wrong control for 1/2 valves—	970076	2.0			5.0		82	0.038	5.0	
£x.	SRO selects wrong control for 1/2 valves—	9.0076	5.0			5.0		Ð	0.52 (0.53)	80	