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- Event Description: On June 12, 1995, the turbocharger (turbo) on the Emergency Diesel Generator (EDG) 2A failed due to the loss of a blade on the compressor impeller during operability testing. Repairs were made and the EDG was returned to service. On June 27, 1995, prior to confirmation of the results of the root cause analysis for the first failure, the turbo on the EDG 2B failed. Evaluation of the failed turbo (ABB Turbo Systems Model VTR-500) components indicated the two failures were identical. Turbos on the Unit 1 and 2 EDGs had been replaced as commercial grade components during each unit's previous refueling outage (1 and 2 EOC9). The EDG 2A and both Unit 1 EDGs were declared inoperable on June 28, 1995, at 1345, and a shutdown of both units was initiated. Following approval of a Notification Of Enforcement Discretion, shutdown of Unit 2 was halted at reduced power.
- Event Cause: This event is assigned an NRC cause code of Design Oversight. The significance of a design change to
 the turbo wall insert was misjudged during the Acceptable Substitute evaluation of the new turbos. The design change
 produced an unanticipated resonance induced vibration at surveillance test operating speeds, resulting in fatigue failure of
 a compressor impeller blade.
- Corrective Actions: The remaining compressor impellers (on EDGs 2B, 2A, 1A, and 1B) were evaluated and/or replaced. The wall inserts on EDGs 2B, 2A, 1A, and 1B were replaced, eliminating the potential for resonance induced vibration.

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Background										
 Background Emergency Diesel Genequipped with ABB Turn the compressor wall ins McGuire Nuclear Static Engineering personnel ABB Turbo Systems por 	bo Systems Model V sert to admit air to the on (MNS). were informed that p	TR-500 turbochargers (e compressor for rapid r	(turbo), v esponse	whick e. Th	h had a co he jet assi	ontinu st fea	uous slot m ature is not	use	ned in d at	n

- Due to the inability to procure parts per the 10CFR 50, Appendix B program, these turbos were procured through the commercial grade program from ABB Turbo Systems.
- · Engineering personnel requested a commercial grade evaluation on the new turbos.
- Component and Procurement Engineering personnel discussed and agreed upon the critical characteristics of the new turbos (per EPRI document "EPRI CGI Joint Utility Task Group Commercial Grade Item Evaluation for Turbocharger") and whether a functional test should be a requirement of the commercial grade evaluation.
- ABB Turbo Systems concluded that, based on past experience with the Model VTR-500 and VTR-304, the wall insert change was insignificant and no additional vendor proof testing was required.
- Component Engineering personnel determined that the 1 hour operability run of the EDGs following installation would
 provide an adequate in-situ performance test of the new turbos.
- Component Engineering and ABB Turbo Systems personnel agreed that testing the turbo in situ was preferable to a
 vendor test because it would eliminate the effect of slight differences in the design of other components, therefore
 resulting in a test using the exact configuration of the new turbos.
- Engineering personnel completed Acceptable Substitute documentation for the new turbos.
- One hour operability runs were performed on all 4 EDGs after installation of the new turbos.
- In addition, 24 hour runs were performed on EDGs 1A and 1B.

Description of Event

June 12, 1995

- EDG 2A turbo failed during monthly surveillance testing per procedure PT/2/A/4350/02A, Diesel Generator 2A Operability Test.
- Damage included a single failed compressor impeller blade section (approximately 2 square inches), a damaged bearing, and a damaged diffuser ring.
- Investigation of the failure mode was initiated and a preliminary root cause determined the cause to be infant mortality (a manufacturing defect in the compressor wheel or exhaust bearing that fails early in life).

June 13, 1995

Damaged components on EDG 2A were replaced.

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June 14, 1995

- The Plant Operations Review Committee (PORC) reviewed the initial failure analysis (including the potential for common mode failure, service history of the turbos, and the present operability evaluation for EDGs 1A, 1B, and 2B)related to the EDG 2A turbo failure.
- EDG 2A was returned to an operable status following a 1 hour operability run per procedure PT/2/A/4350/02A.

June 27, 1995

- Prior to confirmation of the results of the cause analysis for the EDG 2A turbo failure, EDG 2B turbocharger failed during monthly surveillance testing per procedure PT/2/A/4350/02B, Diesel Generator 2B Operability Test, at approximately 1030.
- The failure was identical to the earlier failure of the EDG 2A turbocharger.

June 28, 1995

- Due to the potential for a common mode failure, the EDG 2A and both Unit 1 EDGs were declared inoperable at 1345.
- Shutdown of Unit 1 was initiated at 1346.
- A Notification Of Unusual Event (NOUE) was declared for Units 1 and 2 at 1350.
- Shutdown of Unit 2 was initiated at 1415.
- The PORC reviewed a Notification Of Discretionary Enforcement (NOED) request for Unit 2, to change the required time to be in Mode 3 (Hot Standby) to 36 hours for Tech Spec 3.7.1.2b and 34 hours for Tech Spec 3.8.1.1f, to maintain an onsite power source while repair of the Unit 2 EDGs were completed.
- Approval of the NOED was requested from the NRC.
- Upon approval of the NOED at 1747, shutdown of Unit 2 was halted at approximately 28 percent.
- Unit 1 entered Mode 3 At 1841.

June 29, 1995

- Unit 1 entered Mode 4, Hot Shutdown, at 0127.
- EDG 2B repair/testing was completed, EDG 2B was restored to operable status, and Unit 2 was secured from the NOUE at 0727.
- Unit 1 entered Mode 5, Cold Shutdown, at 1830.
- An Independent Review Team consisting of personnel from McGuire Nuclear Station, the General Office, Catawba Nuclear Station, River Bend Nuclear Station, Surry Nuclear Station, and Brunswick Nuclear Station was formed to conduct an evaluation of the turbo failures.

June 30, 1995

EDG 2A repair/testing was completed and EDG 2A was restored to operable status at 0331.

July 1, 1995

- EDG 1A repair/testing was completed and EDG 1A was restored to operable status at 0302.
- The Unit 1 NOUE was terminated at 0415.

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July 2, 1995

- EDG 1B repair/testing was completed and EDG 1B was restored to operable status at 0936.
- The PORC reviewed the Operability Evaluation associated with returning the Unit 1 EDGs to service.

Conclusion

- This event is assigned an NRC cause code of Design Oversight, resulting in an unanticipated interaction of components. The significance of a design change to the turbo wall insert was misjudged during the Acceptable Substitute evaluation of the new turbos.
- Analysis of the failed EDG 2A and 2B turbo compressor impellers indicated the failures resulted from high cycle fatigue due to resonance induced vibration at an EDG load of 3700 to 4200 kW.
- This load range corresponds to a turbo speed of 12970 to 13410 RPM.
- Acoustic/vibration testing of the compressor blades revealed a natural frequency of approximately 3750 hertz.
- The natural frequency of the compressor blading, in conjunction with the 17 inlet nozzle wall insert (part number 77-SLHA11), resulted in a condition of resonance at or near the normal surveillance test operating speed (13500 RPM) of the turbos. This resulted in the fatigue failure of the compressor blading.
- Actual ESF EDG load (for a worst case loss of offsite power (LOOP)/ Large break Loss Of Coolant Accident (LOCA)) is 3508 kW as determined by calculation and supported by testing.
- For this load the maximum turbo speed would be 12600 RPM.
- Therefore, under ESF loads, the EDG turbos would not have been subject to the blade resonance fatigue failures.
- Dye penetrant inspection of the EDG 1A and 1B turbo compressor blades did not reveal any cracking.
- Since there were no cracks and no mechanism for crack initiation at ESF loads, the Unit 1 EDGs were past operable and capable of carrying the ESF loads.
- Even though both Unit 1 EDGs were declared inoperable (and Unit 1 was shutdown) on June 28, 1995, both EDGs
 remained available at all times except for the time period when each EDG was removed from service to implement
 corrective action to remove the 17 inlet nozzle wall inserts.
- · Therefore, there was no adverse impact to safety for Unit 1.
- Crack growth calculations by Failure Analysis Associates indicated that a crack would propagate from initiation to blade failure in 4 to 8 minutes.
- Since the surveillance test time in the load range where turbo failure could occur was greater than 8 minutes for EDGs 2A (40 minutes) and 2B (15 minutes), it is concluded that the turbo blade crack initiated and grew to failure during the surveillance test runs.
- Therefore, the Unit 2 EDGs were past operable for the entire period with the 17 inlet nozzle air assist design installed except for:

EDG 2A:

- Inoperable on June 12, 1995, at 1520 (EDG start time of 2A failure run).
- Operable on June 14, 1995, at 1543 (Completion of 1 hour operability run, after repairs).
- Inoperable on June 29, 1995, at 0743 (Start time of wall insert replacement)
- Operable on June 30, 1995, at 0100 (following wall insert replacement and completion of a 1 hour operability run).

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EDG 2B

- Inoperable on June 27,1995, at 0948 (EDG start time of 2B failure run).
- · Operable on June 29, 1995, at 0605 (Completion of 1 hour operability run, after repairs).
- Since the Unit 2 EDGs would have performed satisfactorily under ESF loads and were only out of service one at a time for less than the 72 hours allowed by Technical Specifications, there was no adverse safety impact on Unit 2 due to turbo failures.
- This was the first Valid Failure in the last 20 Valid Tests and the second Valid Failure in the last 100 Valid Tests of EDG 2B. On a Unit basis, this was the fourth Valid Failure in the last 100 Valid Tests of EDGs 2A and 2B.
- Surveillance testing remains monthly per the requirements of Technical Specification 4.8-1 (Diesel Generator Test Schedule).
- A review of the Problem Investigation Process (PIP) data base for the past 24 months revealed three previous events which resulted from design oversight. Those events were documented in LERs 369/93-10, 369/94-01, and 369/94-02. None of these events involved the same equipment, systems, or vendors. Corrective actions for those events were specific to those events and would not have prevented this event. This event is not considered to be recurring.
- This event is Nuclear Plant Reliability Data System (NPRDS) reportable.
- This event did not result in any uncontrolled releases of radioactive material, personnel injuries, or radiation overexposures.
- The Independent Review Team identified several issues, some of which are included in the corrective actions. The team also identified the following strengths:
 - Management exercised appropriate conservative decision making following the EDG 2B turbo failure in declaring all EDGs inoperable. The decision to pursue discretionary enforcement to allow continued operation of Unit 2 was conservative from a nuclear safety perspective.
 - The overall response from all site groups following the EDG 2B turbo failure was timely, effective, and well
 coordinated in identifying and addressing the common mode failure. The challenging situation of a unit shutdown
 and cooldown in combination with a power reduction on the other unit while conducting analysis and repair work
 on the turbos was handled exceptionally well.

CORRECTIVE ACTION:

Immediate:

- EDG 2B was declared inoperable and an investigation was initiated to evaluate the potential of a common mode failure.
- 2. ABB Turbo Systems was contacted to assist in determining the root cause of the failures.
- 3. A third party consultant (Failure Analysis Associates), with expertise in rotating equipment failure analysis, was contracted to assist in determining the root cause of the failures.

Subsequent:

1. The EDG 2B turbo rotor, air inlet casing/wall insert assembly, bearings, and lube oil pumps were replaced.

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2.	The EDG 2A turbo (with only 2 hours operation compressor impeller was dye penetrant tested		1995 repair) wall insert was replaced and the e bearings and lube oil pumps were also reused.					
З.	The EDG 1A turbo (with 40-50 hours operation and lube oil pumps were reused.	n since installation) w	all insert and rotor were replaced. The bearings					
4.	The EDG 1B turbo wall insert, rotor and turbin pumps were reused.	e side bearing were r	eplaced. The compressor side bearing and oil					
5.	A Nuclear Network Message was issued expla	aining the turbo failur	es experienced at MNS.					
6.	A metallurgical analysis, which included mater for the failed 2A & 2B compressor impeller, wa		nardness testing, was performed and documented s.					
7.	An independent third party failure analysis/revi	iew of the turbo failur	es was performed by Failure Analysis Associates.					
8.	Acoustic/vibration testing was conducted and o	documented on comp	pressor impeller blading.					
9.	An ABB Turbo Systems project team reviewed design was the cause of the failures.	I the acoustic test dat	ta and concurred that the 17 inlet nozzle wall insert					
10.	A Root Cause Fault Tree Analysis was comple	eted.	그 가슴을 잘 하는 것이 같다.					
11.	A Minor Modification was completed deleting u	use of the 17 inlet noz	zzle wall insert.					
12.	The D. C. Cook and Brunswick Nuclear Statio	ns were provided inf	ormation regarding the failures.					
	Planned:							
1.	Component Engineering personnel will comple September 1, 1995. This report will incorporat		oot Cause Analysis Report of the turbo failures by nal ABB Failure Analysis Report.					
2.	Engineering personnel will enhance the Acceptable Substitute and Modification Programs to address rotating equipment changes affecting natural frequency and critical speeds by December 1, 1995.							
3.	Engineering personnel will implement a more s 1, 1995 (McGuire Nuclear Station) and Februa		t failure root cause analysis process by December Generation Department).					
4.	Engineering personnel will evaluate a common determine if additional guidance is needed by I (Nuclear Generation Department).		process for safety significant components to (McGuire Nuclear Station) and February 1, 1996					
5.			re potential for modifications to be implemented npleted by December 1, 1995 (Unit 1) and March					

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SAFETY ANALYSIS:

The turbo is required for the EDG to operate at the necessary loading to support Engineered Safety Feature (ESF) loads. Loss of the turbo impacts the ability of the EDG to mitigate an accident. FSAR Chapter 15 contains the analysis of several accidents assuming the LOOP event. The primary event of interest is the LOOP event as an initiating event. The existing MNS PRA assumes the frequency of LOOP events to be 0.07 per year.

Based on industry data, LOOP to more than one unit occurs in only 17% of all LOOP events. At MNS, there is an additional margin of safety since there are two shared 4160V auxiliary transformers which can power the essential 4160V busses from either unit.

Assuming both EDGs fail following the occurrence of the LOOP and failures of power from the other unit, power run back, and recovery of offsite power, the unit could still be maintained in a safe shutdown condition with the use of the Standby Shutdown Facility (SSF), which can supply the reactor coolant pump seal injection and provide Steam Generator cooling by means of the turbine driven auxiliary feedwater pump. Thus a variety of means are available to mitigate a LOOP event even if the EDGs fail.

The Unit 1 EDGs were operable at all times except for the time period when each EDG was removed from service to implement corrective action to remove the 17 inlet nozzle wall inserts. For Unit 2, the EDGs were operable except for the time period when each EDG was inoperable due to the actual failure and associated repairs and the time period on EDG 2A during which corrective actions to replace the 17 inlet nozzle wall insert were being implemented. All repairs were completed within the 72 hour allowable outage time for each EDG. At no time were two EDGs inoperable at the same time.

Based on these time periods, the core damage probability as a result of the turbo failures is estimated to be approximately 2.3E -07.

During this period of reduced reliability of the McGuire emergency ac power system, no event requiring the use of the EDGs occurred at the McGuire site. Therefore, this event did not affect the health and safety of the public.