

James W Cook Vice President - Projects, Engineering and Construction

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April 20, 1984

84-04 #1

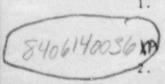
Mr J G Keppler US Nuclear Regulatory Commission Region III 799 Roosevelt Road Glen Ellyn, IL 60137

MIDLAND ENERGY CENTER PROJECT FINAL REPORT ON POTENTIALLY REPORTABLE CONDITIONS SEISMIC AND STRUCTURAL DESIGN CONCERNS FILE: 0.4.9.91 SERIAL: 28026

Jecause of discrepancies in the original seismic calculations, the following Safety Concerns and Reportability Evaluations (SCREs) were issued: SCRE 9 -Category I structures were analyzed with a nominal soil modulus without considering the variation of ±50% as required by the FSAR; SCRE 15 - for the seismic analysis of the diesel generator building, the material stiffness for soil under the building was assumed to be the same as undisturbed till material instead of fill material; and SCRE 42 - Use of Bechtel Computer Program CE-931 which overestimated the composite modal damping, which resulted in an underestimation of the building responses for the reactor and auxiliary buildings. In addition, SCRE 19 lists both seismic and structural concerns identified as a result of a CPCo review of the civil structural design calculations. The items on SCRE 19 were discussed with Messrs Landsman and Gardner of NRC Region III Inspection and Evaluation during a March 22, 1984 meeting with Bechtel and Consumers Power Company.

Attachment 1 provides a more detailed description and the circumstances under which the items were discovered. In each case, the original evaluation was that the discrepancies and concerns, respectively, were not reportable under 10CFR50.55(e), but that further evaluation would be necessary for confirmation.

In actuality, the engineering analysis supporting overall plant design and resolution of the SCREs has resulted in two basic categories in terms of making a final safety evaluation of the SCRE concerns.



Concerns identified in the SCREs, which in fact, have been analyzed
 to their original design basis and configuration and have been
 demonstrated to not be safety concerns, or

Equipment/system or structural modifications have occurred, (for various reasons) and the engineering analyses have not been performed to the original design basis and configuration. Thus the project has

not made an absolute confirmation as to nonreportability of subject SCRE concerns. This is specifically true of SCREs 9, 15, 42 and some of the items associated with SCRE 19.

Consumers Power has decided to classify these SCREs as potentially reportable. This is because conditions of the original plant design for category 2 above will remain indet. minate as to actual reportability.

These concerns are classified potentially reportable as no actual case has been identified where the original structure or components would not perform their intended function as required by the original design criteria. Changes in other loads, such as the dead loads, live loads, thermal loads, pipe break loads, etc, which are combined with the seismic loads, could have caused the increased stresses which required plant modification or equipment replacement. The effect of the specific discr/pant conditions identified in SCREs 9, 15, and 42, in contributing to the pred for equipment replacement or plant modification is not identifiable from che current plant design analysis. None of the SCRE 19 items have been classified as a nonconforming condition. Some of the analysis in current plant design which addresses items listed on SCRE 19 may have contributed to plant design changes. Of the 50 items originally identified in SCRE 19, only six are currently open. These will be resolved through ongoing analyses using current design criteria and thus, like the other SCRE concerns, initial evaluation of the nonreportability of the original conditions will not be verified.

To ensure all changes in seismic criteria and additional stresses are incorporated into the final plant configuration, the floor accelerations have been recalculated, and the structures have been reevaluated. Reevaluation of all piping systems, preparation of Seismic Qualification Review Team (SQRT) documentation involving review of all equipment seismic qualification, and a pump and valve operability review are tasks now in progress.

In conclusion, Consumers Power has decided to classify the subject SCREs as potentially reportable because systems have been changed and equipment has been replaced for reasons which a subject SCRE <u>may</u> have contributed to, and the concerns will not be analyzed to the original design. Since all required changes as documented in the SCREs have been incorporated into the latest calculations, the final plant design is assured to meet current design criteria and commitment to safety.

As can be seen from Attachment 1, each of the items was discovered through a design review process. The specific discrepancies identified are random and isolated. The review processes have provided a comprehensive look at the civil/structural design area. The review results have caused an increased awareness of design packaging and individual design detail necessary to produce acceptable design. It is felt that the past intensive overall reviews, in combination with our current Project Engineering design practices required by Engineering Department Procedures, MPQAD monitors and audits, and CPCo Engineering design overview provide an appropriate overall design review system. No additional specific corrective action is required. This is the

final report on this potentially reportable situation. If significant discrepancies are detected during the review programs, appropriate notification in accordance with IOCFR50.55(e) will be made.

ames W. Cook

JWC/PWJ/lr

CC: Document Control Desk, USNRC Washington, DC

> RJCook, NRC Resident Inspector Midland Nuclear Plant

DHood, USNRC Office of NRR Bethesda, MD

INPO Records Center

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Ms Lynne Bernabei Government Accountability Project 1901 Q Street, NW Washington, DC 20009

3/14/84

### ATTACHMENT 1

## SUMMARY OF SCRE CONCERNS AS ORIGINALLY ISSUED

SCRE 9 During the FSAR rereview, it was determined that there were some inconsistencies in the FSAR with regard to variations of soil modulus and effects on structural frequencies. With regard to structural adequacy, a check of seismic response forces within the major seismic Category 1 structures for a variation of soil modulus of ± 50% from the nominal value (22 x 10° 1b/ft<sup>2</sup>) as indicated by FSAR 2.5.4.7, is in process. Our opinion at this time is that the structures, in the configurations currently depicted in the FSAR, will be capable of carrying out their intended safety functions.

With regard to safety-related equipment within these structures, we have applied the option allowed in Section C.2 of Regulatory Guide 1.122, ie, to broaden the peaks associated with structural frequencies by  $\pm 15\%$ . In so doing, we have utilized the nominal value of soil modulus (ie,  $22 \times 10^{\circ}$  lb/ft<sup>2</sup>) for both the SSE and OBE. On this basis, for the structural configurations currently depicted in the FSAR, it is believed that the systems would be able to carry out their intended safety functions.

- SCRE 15 During the course of preparing for the structural and seismic design audit, it was discovered that in the original seismic analysis of the diesel generator building, the material stiffness of the site fill had been inadvertently chosen to be the same as the undisturbed till material.
- SCRE 19 During preparation for the NRC structural audit, it was established that various engineering activities related to plant design require additional attention to document full compliance with Project licensing and/or design criteria. The Bechtel prepared list does not include items covered by previous SCREs or existing MCARs. In addition, certain issues raised by Consumers Power Company during the audit preparation need to be integrated (as appropriate) into the listing.

None of the presently identified items are deemed reportable at this time due to the lack of any indicated safety impact. In all cases, appropriate anlayses will be conducted by Bechtel to determine the actual situation relative to potential impact on plant safety.

SCRE 42 During the January 29, 1982 seismic design status review meeting in Ann Arbor, Bechtel presented a floor response spectrum curve for the reactor building comparing the original spectra with the current spectra. The comparison indicates a degree of nonconservatism in the original spectra at certain frequencies. The nonconservatism in the original spectra appears to be the result of the original use of CE-931, which resulted in a composite modal damping which was too high. BLC-11329, dated August 14, 1981, stated that the use of CE-931 was not a safety problem due to other offsetting factors; however, the spectra comparison presented on January 29 indicates that CE-931 did, in fact, result in a spectra which was too low.

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The new seismic analysis which is underway will determine the adequacy of the reactor building design. Boottel advised during the January 29 meeting that the original design had sufficient margin relative to the nonconservative spectra; however, final determination regarding reportability cannot be made until the new analysis is complete.

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3.7.2.5, 3.7.2.9, and Appendix 3A Guide 1.122).	(Response to Reg DATE RECEIVED: 2/4/81
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INDIVIDUAL NOTIFIED: Ron Gardner	96502340 1
REFERENCE: O.C.R. Chron File No	28053



## SAFETY CONCERN A. J REPORTABILITY EVALUATION

PROJECTS, ENGINEERING AND CONSTRUCTION -OUALITY ASSURANCE DEPARTMENT SCRE NO: 9 PAGE 2

5. CONTINUED

currently depicted in the FSAR, will be capable of carrying out their intended safety functions.

With regard to safety-related equipment within these structures, we have applied the option allowed in Section C.2 of Regulatory Guide 1.122, ie, to broaden the peaks associated with structural frequencies by  $\pm$  15%. In so doing, we have utilized the nominal value of soil modulus (ie, 22 x 10 lb/ft<sup>2</sup>) for both the SSE and OBE. On this basis, for the structural configurations currently depicted in the FSAR, it is believed that the systems would be able to carry out their intended safety functions.

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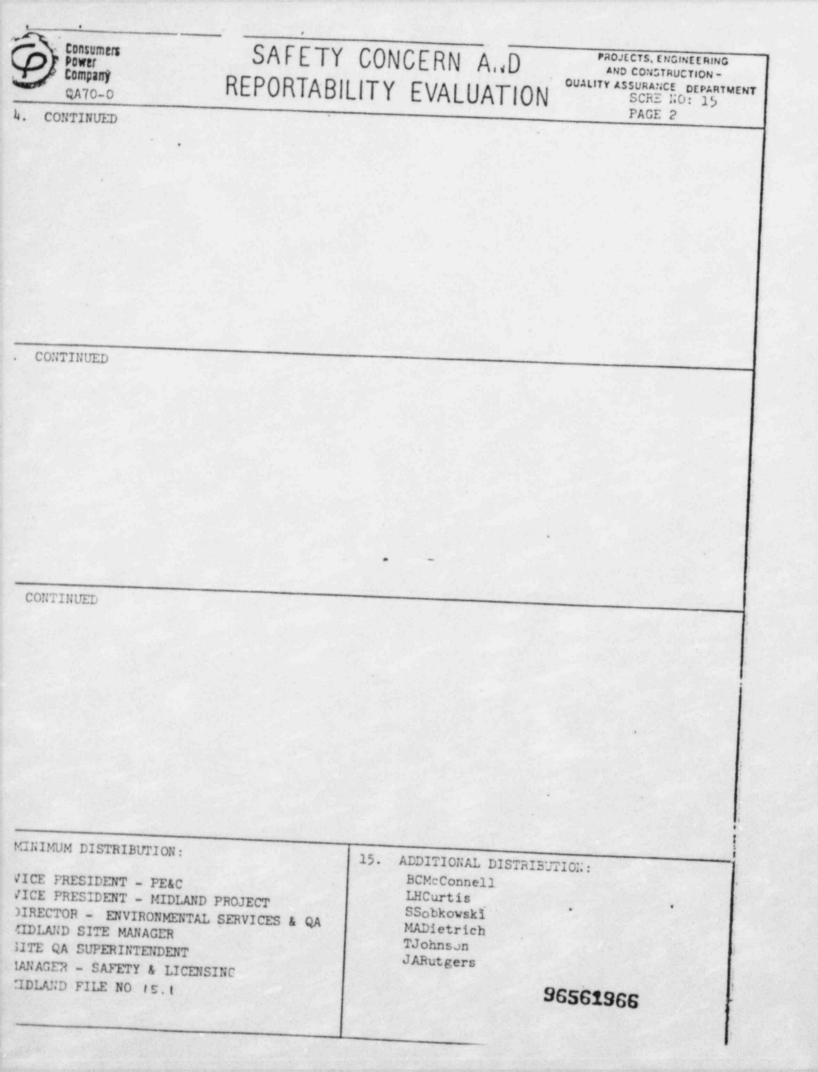
The SAR will be revised to reflect the actual design approach being used for structures and equipment.

#### Final Evaluation

See oral communication record of 3/15/84 for basis to declare this item potentially reportable. 3/22/84

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## Bechtel Associates Professional Corporation

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777 East Eisennower Parkway Ann Arbor, Michigan

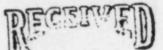
Mani Address: P.O. Box 1000, Ann Arbor, Michigan 48106 August 14, 1981

BLC- 11329

Consumers Power Company 1945 West Parnall Road Jackson, Michigan 49201

Attention: Mr. R.C. Bauman Design Production Manager





AUC 1 ) 1981 MIDLAND PROJECT MANASEMENT

Subject: Midland Plant Units 1 and 2 Consumers Power Company Bechtel Job 7220 Safety Implications -CE931 Program

This addresses the safety implications for the Midland Project of a concern regarcing the application of the CE931 program used in the seismic analysis of Seismic Category I structures. This concern is that the CE931 program may calculate composite modal damping that is too high in some cases. The CE931 program has been used in seismic analysis to calculate composite modal damping for all Seismic Category I structures on the Midland Project. However, investigations have shown that this concern is applicable only to the reactor buildings.

The concern for the reactor building is in damping for the rocking mode for both the east-west and north-south directions. The composite modal damping for this mode has been calculated in 1976 as approximately 12%. This value has been calculated in 1981 as approximately 5% for a slightly revised seismic model for the east-west direction. Using various verification techniques, we have concluded that approximately 5% is the correct damping for this application. Since the 1976 model yields lower responses than the 1981 model, the question of a potential safety concern arises for seismic qualifications performed using the 1976 seismic model.

Based upon our investigations, we believe that there is no identified safety deficiency for the following reasons;

- 1. The structure is partially embedded in soil. This effect will decrease response and was not considered in the 1976 analysis.
- Credit was not taken for soil material damping and SSE concrete material damping in the 1976 analysis.
- 3. CE931 calculated a compositive modal damping of 12%, however, a conservative limitation of 10% was used in the 1976 analysis to develop seismic response spectra and structural responses. This limitation is specified in BC-TOP-4-A and is referenced in the FSAR.

# Bechtel Associates Professional Corporation

## 039377

1.

August 14, 1981 The schedule impact of the resolution of this concern is shown in Schedule EPS-0119, Rev B. This impact is due to the abandonment of the CE-931 program and the substitution of the verified BSAP program in the application.

Very truly yours,

BLC-11329 Page 2

mf Jor L. H. Curtos

L.H. Curtis Project Engineer

SLS/kje(C) 7/23/7

cc: C.B. Miller T.J. Sullivan R.A. Wells



Written Response Requested: No

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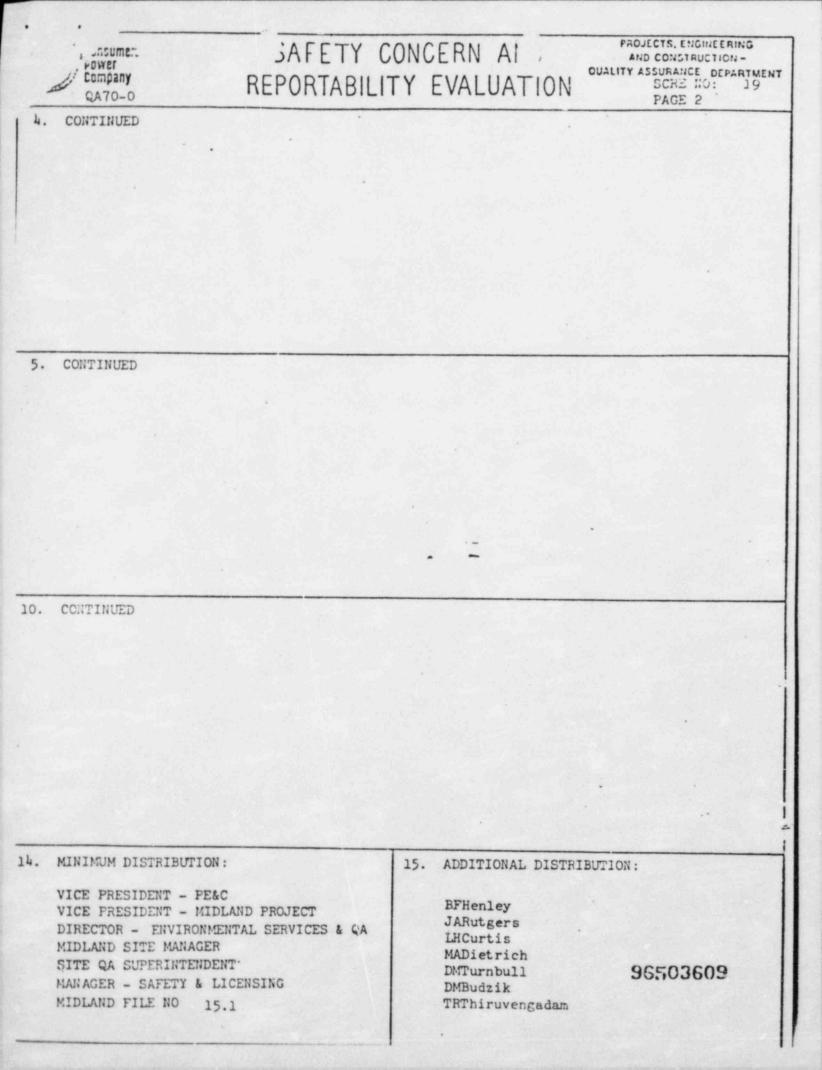
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CONSUMERS POWER COMPANY Projects, Engineering and Construction Midland Project Quality Assurance Department

## ORAL COMMUNICATIONS RECORD

Chron File No: 28053 Page 1 of 2

Date of Communication: 3/15/84 Time of Communication: 5:00 PM Prepared By: W R Bird MPQA Personnel Participating: W R Bird Other Party(s): Ron Gardner, NRC Region III

Projects and/or Subjects Discussed: POTENTIAL REPORTABLE ITEM CONCERNING STRUCTURAL DESIGN

Summary of Conversation: SCREs 9, 15, 19 and 42 represent conditions identified in the original seismic and structural design. Specifically:

- 9 Structures were analyzed with a nominal versus the FSAR Required ± 50% soils modulus.
- 15 Soil stiffness under the diesel generator building was assumed to be from undisturbed till versus fill in the seismic calculation.
- 19 Seismic and structural concerns from the Bechtel/CPCo review of civil structural design in 1981.
- 42 For the reactor building there was too high of a modal damping in computer code C∲-931.

The original conclusion as to reportability was that the conditions were not reportable but that further analysis was required to confirm. Our current deisgn is not representative of the original design conditions. Thus, at the point in time our design analysis is supporting final hardware. Thus we are not in a position to make a clear determination that all of the items represented by the SCREs were in fact not reportable. The basis for our immediate evaluation remain valid to support the belief that the items in fact do not represent a significant safety condition. However, criteria has changed and hardware has been modified. We are taking the position to declare these items potentially reportable in order to close them. A formal written report will be submitted by April 13, 1984. Closure will be through demonstrating that our final design meets the final design criteria.

## WRB/1r

CC: JWCook, P26-336B JEBrunner, M-1079 DMBudzik, P24-517A MADietrich, Midland GREagle, TASK AA RJErhardt, P14-113A LSGibson, P24-618A RCHollar, Bechtel PWJacobsen, P14-414 DTPerry, Midland EBPoser, Bechtel DLQuamme, Midland GLRichardson, Bechtel JARutgers, Bechtel RAWells, Midland NRC Resident Inspector, Midland RNGardner, NRC Region III



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April 20, 1984

84-04 #1

Mr J G Keppler US Nuclear Regulatory Commission Region III 799 Roosevelt Road Glen Ellyn, IL 60137

MIDLAND ENERGY CENTER PROJECT FINAL REPORT ON POTENTIALLY REPORTABLE CONDITIONS SEISMIC AND STRUCTURAL DESIGN CONCERNS FILE: 0.4.9.91 SERIAL: 28026

Because of discrepancies in the original seismic calculations, the following Safety Concerns and Reportability Evaluations (SCREs) were issued: SCRE 9 -Category I structures were analyzed with a nominal soil modulus without considering the variation of ±50% as required by the FSAR; SCRE 15 - for the seismic analysis of the diesel generator building, the material stiffness for soil under the building was assumed to be the same as undisturbed till material instead of fill material; and SCRE 42 - Use of Bechtel Computer Program CE-931 which overestimated the composite modal damping, which resulted in an underestimation of the building responses for the reactor and auxiliary buildings. In addition, SCRE 19 lists both seismic and structural concerns identified as a result of a CPCo review of the civil structural design calculations. The items on SCRE 19 were discussed with Messrs Landsman and Gardner of NRC Region III Inspection and Evaluation during a March 22, 1984 meeting with Bechtel and Consumers Power Company.

Attachment 1 provides a more detailed description and the circumstances under which the items were discovered. In each case, the original evaluation was that the discrepancies and concerns, respectively, were not reportable under 10CFR50.55(e), but that further evaluation would be necessary for confirmation.

In actualicy, the engineering analysis supporting overall plant design and resolution of the SCREs has resulted in two basic categories in terms of making a final safety evaluation of the SCRE concerns.

- Concerns identified in the SCREs, which in fact, have been analyzed to their original design basis and configuration and have been demonstrated to not be safety concerns, or
- 2. Equipment/system or structural modifications have occurred, (for various reasons) and the engineering analyses have not been performed to the original design basis and configuration. Thus the project has

OC0284-0041A-MP01

not made an absolute confirmation as to nonreportability of subject SCRE concerns. This is specifically true of SCREs 9, 15, 42 and some of the items associated with SCRE 19.

Consumers Power has decided to classify these SCREs as potentially reportable. This is because conditions of the original plant design for category 2 above will remain indeterminate as to actual reportability.

These concerns are classified potentially reportable as no actual case has been identified where the original structure or components would not perform their intended function as required by the original design criteria. Changes in other loads, such as the dead loads, live loads, thermal loads, pipe break loads, etc. which are combined with the seismic loads, could have caused the increased stresses which required plant modification or equipment replacement. The effect of the specific discrepant conditions identified in SCREs 9, 15, and 42, in contributing to the need for equipment replacement or plant modification is not identifiable from the current plant design analysis. None of the SCRE 19 items have been classified as a nonconforming condition. Some of the analysis in current plant design which addresses items listed on SCRE 19 may have contributed to plant design changes. Of the 50 items originally identified in SCRE 19, only six are currently open. These will be resolved through ongoing analyses using current design criteria and thus, like the other SCRE concerns, initial evaluation of the nonreportability of the original conditions will not be verified.

To ensure all changes in seismic criteria and additional stresses are incorporated into the final plant configuration, the floor accelerations have been recalculated, and the structures have been reevaluated. Reevaluation of all piping systems, preparation of Seismic Qualification Review Team (SQRT) documentation involving review of all equipment seismic qualification, and a pump and valve operability review are tasks now in progress.

In conclusion, Consumers Power has decided to classify the subject SCREs as potentially reportable because systems have been changed and equipment has been replaced for reasons which a subject SCRE may have contributed to, and the concerns will not be analyzed to the original design. Since all required changes as documented in the SCREs have been incorporated into the latest calculations, the final plant design is assured to meet current design criteria and commitment to safety.

As can be seen from Attachment 1, each of the items was discovered through a design review process. The specific discrepancies identified are random and isolated. The review processes have provided a comprehensive look at the civil/structural design area. The review results have caused an increased awareness of design packaging and individual design detail necessary to produce acceptable design. It is felt that the past intensive overall reviews, in combination with our current Project Engineering design practices required by Engineering Department Procedures, MPQAD monitors and audits, and CPCo Engineering design overview provide an appropriate overall design review system. No additional specific corrective action is required. This is the

final report on this potentially reportable situation. If significant discrepancies are detected during the review programs, appropriate notification in accordance with 10CFR50.55(e) will be made.

annes W. Croh

JWC/PWJ/1r

CC: Document Control Desk, USNRC Washington, DC

> RJCook, NRC Resident Inspector Midland Nuclear Plant

DHood, USNRC Office of NRR Bethesda, MD

INPO Records Center

SAFETY Company QA69-0 02816 REPORTABILI	CONCERN /	AIND ATION GUAL	PROJECTS, ENGINEERING AND CONSTRUCTION - ITY ASSURANCE DEPARTMEN PAGE 1
4. HOW WAS CONCERN IDENTIFIED, WHEN, WHERE?		TO MA	NAGER-MPQA
The issues covered by this SCRE were ide Bechtel and Consumers Power during prepa for the April 20 NRC structural audit. items may be identified during the audit	Aration Additional	SCRE NO: FILE NO:	LATION: Design Prod
		WHEN? BY WHON	The second se
(CONTINUE ON NEXT PAGE)	)	3. IS NRC WHEN? BY WHON	AWARE OF THIS? YES X NO
<ol> <li>BRIEF DESCRIPTION OF CONCERN - SYSTEM, CO (ATTACH SUPPORTING DOCUMENTS).</li> </ol>	OMPONENT, ACTIV	second	In case of the second party of the second
engineering activities related to plant document full compliance with Project li items were discussed with Bechtel on App Bechtel prepared list which does not ind existing MCAR's. In addition, certain i during the audit preparation need to be	icensing and/or ril 13 and are clude items cov issues raised b	design criter summarized on ered by previc y Consumers Po appropriate)	ria. These the attached ous SCRE's or ower Company
6. IMMEDIATE REPORTABILITY EVALUATION: a. REPORTABLE - GO TO 13 b. POTENTIALLY REFORTABLE - GO TO 13	EVALUATI	TION REPONSIBI	LE FOR FURTHER
C. NOT REPORTABLE, FURTHER EVALUATION d. NOT REPORTABLE		PORTABILITY EV CHECKED): TABLE b.	VALUATION NOT REPORTABLE
9. QA APPROVAL OF EVALUATION OF BLOCKS 1 TO 7:	MANAGER	Bud - MPQA	4/21/81 DATE
None of the presently identified items to the lack of any indicated safety imp	are deemed repo act. In all ca	ortable at this ses, appropris	ate analyses
will be conducted by Bechtel to determin potential impact on plant safety.		(CONTA)	NITE ON NEVT DAGE)
	12. FINAL QA		NUE ON NEXT PAGE)
potential impact on plant safety.	12. FINAL QA		NUE ON NEXT PAGE) NAGER MPQA/DATE:

6	Cansumer. Power Company QA70-0	028161	AFET	Y CONCE	RN AN	AND CONS	
4.	CONTINUED						
5.	CONTINUED						
10.	CONTINUED						
14.	MINIMUM DIS	TRIBUTION :		15.	ADDITIONAL DIS	TRIBUTION :	

 TODAY'S DATE 04/20/81
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IP TO:	***************************************	
	** **	
	** Rechtel Power Corporation **	
	** 777 E. Eis-shover Pkwy **	
	** Ann Arbor, Ml 49104 **	
	** ATTN: S. Strohl **	
	** 215 COURTER PT 1200 **	
	**	
	***************************************	

NOTES: 1) THIS MANKED COPY IS AN ATTACHMENT TO SCRE NO. 19. 2) CIRCLED ITEMS ARE COVERED BY THE SCRE WATED 4-20-81 3) OTHER ITEMS MAY BE ADDED TO SCRE NO.19 COVERAGE FOLLOWING ADDITIONAL CAR/ BECHTEL. REVIEW AND COMPLETION OF THE NACL HADDING

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## STRUCTUPAL AUDIT LIST OF ITEMS PUXILIARY PUILDING

Buxiliery_Building_	BRC Page EDa_	Ineppropriate or Caltted Celculations	Compliance with FSAR Commitments	General Condi- tion of Calca- lations	Signif- icence or Disposition	Cognizant Ebgibger_	Origi- nator/ Checker Group Lzeder_	S10188	5 6 7 8 10	•
Part 1 - General Analysis									17	
I. Basic Design Criteria	1								20 21	
A. Seiseic criterie	'	T.H. response spec- tra comparison to site spectra. (typical for all buildings)	BC-YGP-4 to 71 frequencies. Frequencies used may not be con- sistent.		Not significant	J.Chien	V.Tseng	Being genere (shoss dip m is FSAR)		0
8. Design loads	2			Feir				28	30 .	
II. Analysis Method	•						S.Foelber/ W.Tseng	- 6	33 34	
A. Seissic analysis		Model is being re- vised to consider the tornado missile shield and the con- nection of the con- trol tower to the main muxiliary building.	NCAR #7	6008	Change spectra	¥.Tseng	S.Foelber/ W.Tseng K.C.Hau	Revision in	36 37 38 39 40 41 42 43	
1. Asterial properties	•	1. Pasis for the fill parameters		Feir	Osknown	W.Tseng	K.C.H	1. Search in progress	-	
		2. As-built concrete modulus						2. Bo sction planned	51	
2. Time history, response spectru etc (general)	· <b>*</b> , <sup>€</sup>	The integration time interval used was .0' second instead of .005 second. (Typic for all buildings)		Feir	Not sign2ficent	¥.Tseng	% • C • H #u		54   55 56 57 58	)
3. Selection of , number of masses	. 6			Good		W.Tseng	K.C.Heu		61 62	

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### STRUCTUPAL AUDIT LIST OF ITEPS PUXILSARY BUILDING

Auxiliary_Puilding_	BPC Page Ega_	Ineppropriate or (mitted Calculationr	Compliance with ESAR Commitments	General Condi- tion of Calcu- lations	Signif- icance or Pisposition	Cognizant Enginger_	Origi- batoz/ Checker Group Lender_	Slatus	5 6 7 8 10	
6, Rodel responses	7		The combination of motions for the components tent with the FGAR. typical for all buildings)	Good	Not significant	W.Tseng	K.C.Het	SC# approved	6 67 68 69 70 71 72	
5. Soil-structure interaction	9	The ±50% varia- tion in soil proper- ties is slro iden- tified by CPCo and is addressed in SCRE 9. SCRE 9 elso addresses modifications of building res- ponse spectra. (typical for all buildings)	The effect of ±50% variation in the the soil properties was not considered	Fair	Significant if SAP change not (implemented		K.C.H	SCW approved calculations in progress		С
6. Hydrodynamic effect of spent fuel pool	10	Not considered in seismic analysis.		Poor	Not significant	V.Laksha1/ D.Magauson		Ca. seletions in progress	9°	
Se. Fuel pool valls and floors	17	Seismic effects not cospletely accounted for in design. Slosh height not calculated walls and slab appear to be designed for temperature effects only. Other loads not considered in combination.		Poor	Calculations meed to be redone	V.Lakshai/ D.Magnuson	S.Peri/ R.Tsao/ Y.Lem	Calculations in progress	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	)
7. Pesponse spectre (specific)	11			Good					108	

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STRUCTUPAL AUDIT LIST OF ITERS AUXILIARY BUILDING

&wxiliary_Building_	FADe Ega	Ineppropriate or Omitted Celculations	Compliance with FSAP Commitments	General Condi- tion of Calcu- lations	Signif- icance or Disposition	Cognizant Engineer_	Origi- netor/ Checker Group Lender_	5 7 	10
8. Vertical analysis	15	Floor flexibility wes not included in the calculations. (typical for all buildings)	FSAP does not address floor flexibility.	Fair	Study in progress	¥.Tseng	Fone	response	11 113 118 115 116
B. Stress analysis	12	A superseded sels- mic analysis was used for design.		Fair	Not signi- ficent			Calculations is progress	1 12 129
1. Shear walls and floors	) 12	The loading com- himetion including tornado wind was not checked.		Fair	Not signi- ficent	J.Ross/	P.Regu- pathy/ V.Verma/ K.Lam		125 C
Poundation set		<ol> <li>The dead load increased after the analysis was com- pleted.</li> <li>The loading combination including tor- tado wind was not checked.</li> </ol>	binations specified	Fair	Not signi- ficant	V. Terna/ Lakshai	P.Regu- pathy/ K.lam		1 131 132 133 134 135 136 137 138 139
C. Joint filler between buildings	18	**	**			J.Poss			142
D. Computer verifi-	16	Verification has not been completed for several programs. (typical for all buildings)	Ro FSAR commit- ment.		Not signi- ficent			11	1
E. Overell stability	18			Good		D.Regnuson	Lekshai	Celculation approved.	15 154

Sheet 3 4/18/81 15

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## STRUCTURAL AUDIT LIST OF ITERS PUTILIART PUILDING

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			STRUCTURAL AUDI PUXILIART	T LIST OF PUILDING				0	2 3
· _Auxiliary_Building_	BPC Pege Egs_	Ineppropriate or Omitted Celsulations	Compliance with FSAR Commitments	General Condi- tion of Celcu- lations	Signif- icance or Disposition	Cognizest Engineer_	Origi- mator/ Checker Group Lander_	2 8 I 6 i	5 6 7 8 10
F. Interaction with non-Category 1 structures	20	Auxiliary building calculations do not include interaction with turbine build- ing durine tormado and seispic events. Turbine building seispic analysis and tormado calcu- lations to be finalized.	Same as calcu- lations column	Not avsil- able	Calcula- tions neces- sery to show that turbine huilding will not demage sur- iliery building.	J.Ross	Lotshai	Turbine building calculations to be final- ized.	157 158 1 161 162 163 168 165 166 16'
G. Tornado aissiles	21					D. Regneson	Lekshei	Calculations complete	171
III. Conformence to Staff's Criteria (Deviations)	23								174 175 176
) Tart II - Ker_Designs									179 180
A. Exterior shear	28	<ol> <li>Falls were not designed for plate hending for seismic and tor- nado loads.</li> <li>Consider thermal gradient in design</li> </ol>		Feir	This will probably not be critical to design but calcu- lations need to be ande to check thi		P.Regu- pathy/ V.Verma/ K.Lam	Calculations in progress.	
B. Interior shear wells	25	Flexural design considers only con- partment presuri- zation. Seismic load was not in- cluded.	Missing losd com- bination pressure plus seismic	Poor Diffi- cult to follow	Calculations need to be made includ- ing seismic affects on wells. (tren verse bendim	<b>F</b> -	H.Tsao/ H.Kelley/ K.Lem	Calculations in progress	19 195 196 197 198 199
C. Main floors and roofs	26	Poof not checked for uplift during tornedo		Fair	Not signi- ficant	D.Magnuson	K.Len/ J.Arore	Calculations in progress	2   20 204

Sheet # #/18/81

#### STRUCTURAL AUDIT LIST OF ITERS PUXILIARY PUILDING

-	Availiary_Building_	NPC Fage Nga_	Inerrorriste cr Ceitted Calculationr	Compliance with FSAP COMMISSING	General Condi- tion of Calcu- lations	Signif- icance or Disposition	Cognizant Enginger_	Origi- nator/ Checker Group Leader_		5 6 7 e 10	
C	. Structural steel bracing	28	Cenerally designed for deal load and live loads only.	All the load cortinations given in the FCAR have not been considered.	Felr	Probebly not significent	D.Regnoson	K.lam/ J.Arora	Justificatio being pre- pared.	208 209 210 211	
E	. Foundation nat	20			Feir		Y.Yerns	Y.Yerme/ P.Regu- pathy/ K.Lem		218 215 216 217	
, "	. Rain frame concrete column design			MA.	#A					220 221	5
, ,	. Secondary floors	31	Same as sain floors.							224 225	
C	. Floor-wall junction datails	32					J.Ross			228	
1	Dynap'; effects of mechinery	33				Not signifi- cant (speeds higher than 30 Hz)				232 233 234 235	
	Added items not covered in audit		<ol> <li>Probable maximum flood elevation of 632°, instead of 635.5°</li> </ol>	Probable maximum flood elevation of 632' instead of elevation 635.5' was used in the analysis and design.	Fair	Fot signi- ficent 635.5 is wave runup	D. Nagn <b>ason</b>	D.Hagavson V-Latshai		237 238 239 240 241 242 243	

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14 15

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			STRUCTURAL AUDI	T LIST OF	TTEMS			0	287	12
			SEPVICE LATER	PUMF STH	ICTUPE			2	248	
								8		1.1
				General			Origi-		250	
	RPC	Inaprropriate		Condi-	Signif-		nator/	σ	251	
Service Water	Pade		Compliance with FSAR	tion of Calcu-	icance	C	Checker		252	
PERD_Strecture	HO1_		Consiteents	lations	Pisposition	Cognizent Engineer	Group	_States_	253	
Part I -									258	
feneral_Analisis									259	
1. Basic Design	1								261	
Criteria									262	
. Seissic criteris	1			Felr		J.Chein/	S.Sobtor-		264	
						P.Fujawa	ski/		265	
							C.Tuveson		266	5
8. Design loads )	2	Tornedo wind	300 sph tornsdo	Fair	Redo tor-	D.Griffith/	R.Rekin/	Tornado re-	1 26	i
		speed of 300 mph	wind used instead		nado enaly-	L.Ho	P.Goffes/	analysis	270	
		used to check missile local	of 360 mph wind.		618		P.Shen	complete		
		effects.					-		272 273	
II. Analysis Nethod									276	
. Seissic analyris			Fefer to aux	Feir					278	
1. Reteriel prop-		1. Concrete modulos			Not signi-	J.Chien				
erties	1.	(F ) bered on			ficent	J.Chien		Consider in current effe		
		f'c = 3,000 psi							283	
		instead of speci-							284	
		fied concrete strength of f*c =							285	
		4,000 psi.							286	
									207	
		<ol> <li>Analysis did not consider fill.</li> </ol>							289	
같은 생활을 통하는 것을 받는 것이?									290	
2. Time history,		Pefer to aux						1	293	1
etc (general)									298	
etc tyenetall									295	
3. Selection of	6			Good				1	298	
number of masses									299	
4. Rodal responses	7	Pefer to sur		Feir					302	
									302	

Sheet 6 4/18/81

		1	STRUCTUFAL AU SERVICE WATE	and the second second second				0	287	
S e les Seter Bits des Citer	Prge Eg.		Compliance with FSAR Commitments	Ceneral Condi- tion of Calcu- lations	Signif- icar or Disposition	Cognizent	Origi- nator/ Checker Group Leader_	2 8 - 6 -	250 251 252 253 255	
5. grodynamic	•	<ol> <li>Bydrodynamic effects are not considered.</li> </ol>		, <del>0</del> 0 T	Probably not significant			in corrent	305   306 307	
		<ol> <li>Torsionsl effect of combinations of bays filled or empty should be considered.</li> </ol>							309 310 311 312 313	
6. e spectra ic)	9			2018			F.Hsis/ K.Hsu/ G.Tuveson	New analysis not begun.	3 317 318	
The Investory reiseld	10	Prior Inch.						1.1.1.1	321	
C. Intern come	- 11								328 325	
al Sepana controle									328	
f. Intale ebructuse Abstrationete Reviced		initestary coloris anitestary colors in the inter the star or of the fi	Carlie 3.8-2. Till pe pat of iste abre selected ste included in the relations. Int all locking carticetions parches.	(10008- 91918 2010	Probably net		T.Kim/ P.Perikh/ M.Kumre (P.Shen)	is cerrent efforts	330 331 332 333 335 336 337 338	
(2. Thisky consists)									341	
3. Transa turn ann		tyler to y some		Tac. Di I		D.Griffith/ L.Ho M.Kuere/ (P.Shen)	Y.Kim/ P.Parikh/	.	342 345 346 347 348	)
C. Corpulat artificat		No. 1		bod		B.Mozafari			351 352	
D. Grecall stackitt		Fotor 10 chave		Incom- plete, fair		D.Griffith/ L.Ho	Y.Kim/ P.Parikh/ (.P.Shen)	1	355 356 357	
144 15		S CV					Sheet 7 4/18/81		14 15	

								A CONTRACTOR OF		
			STRUCTURAL AUDI SERVICE WATER	T LIST OF	ITERS CTURE			028	28	
Service Water	Proe Proe	Inappropriate or Omitted Calcylations	Compliance with FSAP Commitments	General Condi- tion of Calco- lations	Signif- icance or Disposition	Cognizent Engineet	Origi- betor/ Checker Group LendeL_		25 25 25 25 25	1 .
Interaction with son-Category I structures	19	Calculations have no been located for the interaction of the circulating water intake structure with SWPS.		No cel- cula- tion showing the in- teraction	Preliminary study shows no problem.			Perform sels analysis on circulating water struc- ture and check of structure	1	36 36 3
art II - Kar Designs									36	5
. Exterior shear walls	)'	1. Loads from Method I reismic analy- sir not consider- ed in design.	combinations in		Probably not significant	D.Griffith/ J.Gobster/ L.Ho	N.Mar1/ P.Parikh/ M.Kusra (P.Shen)			3
		<ol> <li>North and south walls not checked for tornado losis.</li> </ol>							37 37 37	17
		3. Temperature orad- ient acorss wells							38	
. Interior shear walls	22	Refer to A							38	
. Hain floors and	23	Refer to A						1	38	7
. Foundation set	28	Refer to A						1	39	0
<ul> <li>Floor-wall joint details</li> </ul>	25	Refer to A							39	
<ul> <li>Selesic restraint of pumps</li> </ul>	26								39 39	
1. Tanks			Section 3.8	Good		Rao/Dessi	Diesel oil tank: Reo/ A.Bando- podhyaya Pressuri- zation tenk: V.Patenkar/ C.Dirnbauer		401 401 401 401 401 401 401	1 2 3 4 5 6 7

Sheet 8 18 4/18/81 15

## STRUCTUPAL AUDIT LIST OF ITERS SFRVICE WATER PUMP STRUCTURE

Service Bater Pass_Structure	RRC Inservorrists Page or Ositted RosCalculations	Compliance with FSAR Commitments	General Condi- tion of Celcu- lations	Signif- icance or Disposition	Cognizent Engineer_	Origi- netor/ Checker Group Leader_	Status	250 251 252 253 255	
2. Piping		Section 3.8	Vendor calcu- latich for pipes Good		Reo/Desei		0281	8 11 8 12 8 13 8 18 8 18 8 16	
B. Seisnic Analysis							5	419	
2. Piping (concrete)	The stress commary for the diesel oil tanks is incomplete. Pressures not esses are given in P. 4R Table 3.9- 5.1, Sheet 5. Vertical earth- quake not con- sidered for diesel oil storage tank design. Flexibility of pipe bends was not con-		Vendor/ Good Feir free		G.Otal D.Reeves	R.Tseng/ G.Toveson	Co back to vendor. Bew Bew		1.
(concrete)	sidered in the analysis. Para- meters in analy- sis need to be re- vised: F for pipe and shear wave velocity.		field only.			C. Toveson	lations.	436 437 438 439 440 441 442 87	
C. Structurel Amelyain						,		. 846	
1. Tanks			Good			Vendor celcu- letions		448 449 450	
2. Piping (conc)	Missile impact wes considered for the steel ripe end not concrete ripe.		Good	Rot signi- cant	Rao/Desai	Vendor calcula- tlons/Reo	Update for concrete pip	1 452 458 455 456	

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Sheet 9 4/12/81

-										
			STRUCTUPAL AUDI SEPTICE WATER					28	247	
			SERAICE MAJER	FURP SIPU	CIUPE			-		1
				General Condi-	Signif-		Origi- mator/	on 	250-	••
		NFC Inappropriate	Compliance	tion of	icance		Checker		252	
•	Service Vater Pump_Structure	Page or Calivlations -	Consiteedis	Celcu- lations	Disposition	Cognizant Engineer_	Group Leader_	Status	255	
	D. Soil Settlesent								459	
•	C. Differential	Not considered.						Pevise desig	A63	
•	2. Seismic setti-	Not considered.							465	
•	Connections to structures	Not considered.							*:	
•	Category I	Not considered.							474 475 876	
	piping						1.1.1			
C	E. Damage to piping	#A for concrete Seisaic							479	
).	due to differential settlement	Category 1 pipe. Con- crete pipes are 40' away								
		from the structure and buried in natural soil.							482	
	Bert IT - Itens fot								486	
•	Covered in Questions Phich Should be Iden: Lified								*87 +88 489	
.70	Electrical Duct banks and conduit design	7		In revie					491	

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And a second second	
m	508
01	501
1.8.8	502
	508
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	\$15
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1	\$27
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	5 36 5 35 5 36
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	553 554 555
s. j :	354
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			STROCTURAL AUD					012	
Diesel 	89C 7499		Coopliance eith FSAD	Conerol Conei- tice of Celce- Lations	Signif- icance and Diampalilam	Cogn 1 sant	Origi- setur/ Checker Greep Lester	-114114	
(. Propose aroctic		Diemel pedestal spectra do not envelop horirontal building base aper- tra.		fair				Tendor regenilify	541 541 542 543 545
7. Vertical seissic	15								547
<ul> <li>Stress analysis</li> <li>Shear calls and floors</li> </ul>		Complete		Cood	•		T.Seens/ A.Bendyo- pedbysys/ P.Shen	851	572 573 578 578
2. Tenstation	"	Complete		6004	•		T.Reene/ A.Bendyo- pedbyoyo/ P.Sben	•	577 576 579 588
C. Joint filler be- tuess strectures		••				•		** **	58 584
D. Computer verifica-	16	Cooplete	Cood	**	B.Persfari	••	**		587
E. Gvorall atability	18				Good	401144	J.Cobater	T.Boang/ #A A.Bandyo- padhyaya/ P.Shon	592 593 594
. Interaction with mon-Catesory 1	20								597 578 599
6. Torsade elesiles		Pefet to estlicty building		Cood		J. 600 stor	T.Basso/ A.Basdyo- pedbyoys/ P.Shcs	1	603 603 604 605
III. Conference to Staff's Criteris (Devi: Lione)							•		808 809 818
370							Sheet 12		18 15

+			SWILL DU LICE I FOR I FICE UL LICE SWILL	17 11-1 0	ITERS			32	1
			L11-11 61818	#10# +n11	1110			81	
Assessive. Califias.	114	lastrorrists	Costilance uith 1'58	Ceneral Condi- ticn of Caicu- Latigat	Stentf- icence and Dissouities	Coostsaat Lastasst.	Orist- nator/ Chacter Gross	α.	
Met 11 - Gat. Pastana									
i. Literies these wills	:	femiete		Cood		J. Cobstor B. Basdys- padbysys/	T	Constate	
. Atorior shoor wills		Complete		6004	:		,		5555
C. Main flowers and		Complete			J	Personal yes	J.Gobster	T.Buang/ Complete h.Buadro- 027 pedhyora/ 028 P.Shen 029	
b. Steel atractural bracing		be attactural attal bractas has been		:	:	:	:	:	
E. Presentition				Card			T.Buss/	Caspiers	5555
f. his fras concrete release		Be concrete column column has been ared.		:	:	:	:	:	
4. Secondary floors		No percendary floor has been ared.					:	:	=
R. Plant-soll Joint dotaile		Charles.		3				Creasiate	1555
1. Pymanic offocto of sochinory	c	Canylate		3		:		Campiero	
37									

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Conteinernt_Puilding	PPC Insperopris Page or Critted EgsCelculation	with FSAR	General Condi- tion of Calcu- lations	Signif- icance and Disposition	Cognizant Engineer_	Origi- netor/ Checker Group Leader_	2 8 - 6	665 666 667 668 670	
Part I - General Analysis	'							674 675	
I. Besic Design								677	
A. Seissic criteria Criteria	1 Pefer to sor							680 681	
R. Design loads	2 1. Wind and tor loads are no addresred.		Fair	Not signi- ficant. Add cal- culation	Ader	T.Selys- neraney/ ene/ C.Tep	Calculations in progress.	16	K
	2. The 1974 FIN model has coments requir resolution a program must verified.	n- ing hd		Wind and tornado are not gover- ning loads.	Vel/Twan	R.Tuhol- ski/B.Dhar	Calculation to be per- formed.	1 6 690 691 692 693 694	
			Fair	Not signi-		#.Tehol-	Analysis to	1 69	
				ficent		ski/R.Dher	be reviewed.	1.6	
II. Analysis Method					3.1			702	
A. Seissic analysis								704	
1. Raterial proper- ties	) a 1. Cracked sect properties m used.		Good	Probably not significant			Po action planned	707 708 709	
	2. Tented concr modelus not							711 712	.)
2. Method of analy- sis (time histor response spectru etc)	7.)		Fair					715 716 717 718	
3. Selection of num ber of masses	D1. Backur reaul for reducing ber of MSSS marses is re quired.	nu#-	Felr	Not signi- ficant. Com pare frequen cies.			Not reduced in new cal- culations. Celcelations in progress	72 723	

Sheet	14	14
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Containment_Building	RRC Page Boa_	Inappropriate or Omitted Celculations	Compliance with FSAR Commitments	General Condi- tion of Calcu- lations	Signif- icance and Disposition	Cognizent Enginger_	Origi- mator/ Checker Group Lemist_	28 4/17/811 - 0 	665 666 667 668 670	
		<ol> <li>Applicability of specifying only translational and base rotational DDOF.</li> </ol>							728 729 730 731 732	
a. Rodal responses		Pefer to suz							735	
5. Soil strecture	) (	1. Refer to sox 2. Hydrodynali effects of e flooded re- fueling canal not considered.		Good	Could be nificent for equipment			Calcelations scheduled	738 742 743 744 745	
6. Pesponse spectro (specific)	• 11								748	
7. Vertical analys	18 16	Pefer to aux						1.1.1	752	
Polat crase	17	1. Rulti-modal response horizon- tal response change. program mout be		Feir	Probably not significant			discuss eith CPCo Verification of this assusption in progress.	756 757 758 760 762 762	
9. Buried piping	18	Fefer to buried piping							767	
B. Containment genera analysis	1 19								771 772	
1. Containsent she	11 19	tion of base say thre	R Tables 3.8-1 ough 3.8-17 tsin typo- phical errors.	Good	Verified by	Tel/ D.Tusn	K.Husag/ B.Dher			
					11/6/81 Review design calculations.				780	
							Sheet 15		14	

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Conisinnent_Puilding	RPC Inappropriate Fage or Caltured ForCalculations	Compliance with FSAR Commitments	General Condi- tion of Calcu- lations	Signif- icance and Disposition	Cognizent Ebgigert_	Origi- metor/ Checket Group Leader_	*/17/818	665 . 666 667 658 670	
	<ol> <li>Siring celcu- letion hes not been checked.</li> </ol>			Not signi- ficant	G.Kwong		In progress	783   78 785	
	5. FINEL analysis of shell does not include stiff- nesses of inter- nel structures			Not signi- ficant knows.	D.Tuan	"	Justificatio in progress	n   78 790 791 792	1
	4. Primary load Ro alone was not checked	t required	**	Probably not significant	D.Tuen	**	Celculations scheduled	1 · 795 796	1
	5. Deviations from design criteris e) membrane comp. stress b) radial tension in dome c) allow. reinf. stress d) allow. effec- tive tendon stresses	)		Probably not significant	D. Tuan	F.7al bosk i	Celculations scheduled	1 7 000 001 012 003 004 005 005 005 005 005 005 005	
	<ol> <li>Section resultant at Section 3 of ring girder (056) has to be checked.</li> </ol>			Celcu- lation to be checked			Check schedu	1ed 813 814 815	
2 Containsent Internals	20		Bed					821 822	
	1. Loads from PV were not included in FINEL enely- sis of primery shield well.			Calculation is being revised.	D.Chow	,	Being per- formed	825 826 827 828 829	
	2. Seismic load not checked for lay- down area and sump wall.		Feir	Wot sign1f1- cant	W.Hagedorn		To be f eddressed	832 833 834 835	
						Sheet 16 4/18/81		18 15	

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-				CCRTFINHEN					028	663
• •	Contelevent_Building	RPC Page Ega_	Inappropriate or Daitted Calcylations	Compliance with FSAP Commitments	General Condi- tion of Calcu- lations	Signif- icence and Disposition	Cognizant Enginetr_	Origi- mator/ Checker Group Leader_	07 4/17/018-	665 666 667 668 670
			3. Primary shield well loads in the FSAR have not been veri- fied.			Additional calculation might be required.	C.Boyak		New calcu- lations com- pleted	840 841 842
			<ol> <li>Pinned houndary condition is</li> </ol>			Rodify model	D.Chow		Fatare work	1 88 846
2	3. Foundation set	)	8. Soil property (F) sariation not evaluated.			Probably not significant			Calcelation scheduled	1°
• •	C. Compater program verification	23	A number of computer programs have not been verified.	FSAR Subsection 3.8.1.4.8 and Ap- pendix 3C do not list all of the programs used for analysis of the containment.		Verified by 11/81.	D.Toen/ T.Tseng	"		854 855 856 857 858 859 860
•	D. Overell stebility	24	Seissic separation of basement not con- sidered.	Calculations sup- porting FSAP Table 2.5-14, bearing pressure, cannot be located.		Not sign1- ficent	D.Tuan	E.Rueng/ B.Dher	in progress	863 1 86 865 866 867
•	E. Interaction with mon-Category 1 structures	26	<ol> <li>Interaction be- tween tendon ac- cers shaft and containment.</li> </ol>	See BBC Page 2		Not signi- ficant (no interaction)			New calcula- tions com- plete	871 872 873

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			STRUCTUFAL AUDI CONTAINPEN					028	667
	NFC Page	Inappropriate or Calitad	Compliance with FSBR	General Condi- tion of Calcu-	Signif- icence and	Cognizant	Origi- nator/ Checker Group	e/17/018	665 665 667 668
, III. Conformance to Deviations	27	Colculations		lations	Pierositien	Epgineer_	Leader_	_Status_	67C 876 877
Pert 11 - Laz Designs	· ·	1. à full celculation for liner plate		Fair	Add celcu- letion.	D.Tuen	C.Ten	Calculations scheduled	879 1 8 892 . 883
	>	has not been loce ted (Compare to BC-TOR:11 2. No celculations			Provide			Celculations	···· _·
	C	located for some rene- trations in liner.	)		calculations			1	889 890
•		3. Calculations are required for the by 3me under the line. plate.			Provide cal- lation cover sheet and reference staff report.	T.Brozo		Calculations scheduled	894 895 896 897 898
. Ratch design	31	<ol> <li>Liner plate effect not con- sidered.</li> </ol>		Fair	Not signi- ficant.	¥e1	J.Shi/ B.Thoski/ C.Ten	by MCAR 51	901 902 903
•		<ol> <li>Tangential shear has not been checked.</li> </ol>			Bot signi- ficent			Calculations scheduled	907 908
		3. Shear reinforcing appears low		`	Ray be sig- nificant			Celculations in progress	
C. Bass slab	34	1. There is no bearing calculs- tion located.		Poor/ Average	<b>Tel</b>			Calculations in progress	1 9 91 917
D. Well-base slab , junction	37	See chell response		Poor/ Average		Vel	J.Sh1/ J.Hink	·	920 921

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Containment Building	BRC Page Bga_	Inappropriate or Omitted Calculations	Compliance with FSAR Commitments	General Condi- tion of Calcu- laiions	Signif- icance and Disposition	Cognizent Engligger_	Origi- sator/ Checker Group Lesder_	4/17/818	665 666 668 670
E. Resbrane shear	*0	The equipment hatch area has not been evaluated for mem- brane shear.	The equipment hatch area has not been evalua- ted for membrane shear. (FSAR Subsection 3.8.1.5.1.4)		May be sig- nificant			Calculations in progress D 2 8	92 928 927 928 929 930
F. Dose-to-cylinder junction	*2	See shell response		Feir	Not signi- ficest	Vel	J.Sh1/		933 934
C. Primery shield wall base sat junction	••	1. No verification of rebar adequacy at junction.		Poor	Calculation is being developed.	D.Chos	C.Tes/ J.Hink		937 938 939
H. Operating floors	87	<ol> <li>Seisaic load was not considered.</li> </ol>		Fair	Vertical-met governing; Morisontal- may be sig- nificant.				
1. Polar crane sup- ports		<ol> <li>Consideration of seismic loads is not clear.</li> </ol>		Fair	Probably not significant			Calculations in progress	9 98 950
		2. Global effect on shell is not clear.			Not signifi- cant			Calculations in progress	953 958 955
		3. Containment move- ment due to pres- mure and tempera- ture has not been considered.			To be re- viewed in future.				959 960 961
J. Reactor vessel	51								964
R. Stess generato sayr sapport	)57	1. The calculation for the 24"-con- crete slat is not available.	Revise FSAR to state that bolts do not take shear		Not sifnifi- cant.	D.Chow/ D.Tusn	M.Elgaaly/ J.Hink		969 970
L. Coolent pump support	t 55	1. HCAP 45 - anchor bolt		(**)	Cese by case eval- ustion.	N.Hagedorn	K.Sandeki/	1	973 974 975

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Containment_Building	BPC Page Ega_	Insppropriate or Omitted Calculations	Compliance with FSAR Commitments	General Condi- tion of Calcu- lations	Signif- icance and Disposition	Cognizent Englinger_	Origi- netor/ Checker Group Lender_	4/17/818 	_	665 666 668 670	
		<ol> <li>Snubber spring rate do not consider coll condition or as- built pin to pin lengths.</li> </ol>			Probably not significant				1	978 979 980 981 982	
R. Secondary shield wells	57	Computer run needs addi- tional checking.		Poor	8.Tuen	B.Ragedorn/ B.Dher	C.Chang/	Check cel lation	1	985 986 987	
. Other steel struc- teres	),	Seismic loads were B not considered on all pletforms.		Fe1: (27)	Not control- ling load.	W.Hagedorn/ D.Tuen	J.Hink/ G.Tuveson/ H.Elgeely/ B.Dhsr/ D.Tuen	Redo cale lations		91 992 993 994	Ĩ
0. Post-tensioning system	61	Neither Sechtel sor 1 wendor calcs include pressurization effects.	<ul> <li>Preliminary calculations indicate that the allowalles in FSJ Subsections 3.8.1 and 3.8.1.5.2 for stressing tendom</li> </ul>	1.5.1 r pre-	Signifi- cance um- knowa	Vel/ T.Bronze	N.Duchom/ N.Bemoit/ G.Untnown		02816	997 998 999 1000 1001 1002 1003	
			concrete are excu under pressure conditions.		Calculation is being checked.					1008 1005 1006 1007 1008 1009	
		2	• Pretensioning tendons stress level exceeds 0.7 fu fellow- able in accor- dance with FSAR Subsections 3.8.1.5.1.8 and		Not signi- ficent			Bevise F		1 10 101? 101. 1015 1016 1017 1018 1019	)
			3.8.1.5.2.7) et transfer.					1.10%	1	1020	

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## STRUCTURAL AUDIT LIST OF ITEMS POPATED WATER STOFAGE TARE

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Borated Water	F Ge			ompliance with FSAR geniteents	General Condi- tion of Calcu- lations	Signif- icance and Disposition	Cognizant Engineer_	Origi- netor/ Checker Group Leader_	States		1028 1029 1030 1031 103
Part 1 - Ga eral Analy:			Tes		Good		Reo/Desai	Rao/ A. Bando- pedhysys/ G. Udogi	Complete		1037 1038 1039 1040
1. Pasic Design Criter-	,										1042
A. Seispic design cri- teris	'	Fone					AcConnel/ Mozeferi/	Banby/ Dunnelly/		1	1046 17 1049 1050
O B. Design loads	2				Good		Reo/Desai	Rao/Bando/ Udogi		1	1051 1058 1055
TBL 3-17 O 11. Analysis Pethod									028		1056
A. Seissic analysis	•	Dynamic analysis was performed using TID-7024 techniques.			Tank fair Foundation		Otel Pierce	Banby/Don- nelly/Hush		1	1062 1063
o (. Material proper-	•	<ol> <li>soil structure interaction</li> <li>Shear modulus, sutgrade reactions and bearing</li> </ol>			Not signi ficant				Calcs in progress	1	1066 1069 1069 1070
•		capabilities of soil were taken from unchecked and unargrowed calculations.								1	1074 1075 1076
O 2. Time history, re- sponse spectrum, etc (general)	6	Not performed	8/3		B/A		R/A	*/1	•	1	1079 1080 1081
3. Selection of num- ber of masses	6	Pased on TID-7020	•		Tenk - no		Otel Pierce	#/A N/A			1085
<ul> <li>Rodal response</li> </ul>	7	8/8	K/A		#/A		B/A	K/A		'	1085

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STRUCTURAL AUDIT LIST OF ITEMS ECRATED WATER STORAGE TABE

Borated Bater Storage_Tank	BPC Page Ega_	Inspropriate or Omitted Calculations		Compliance with FSAR Commitments	Ceneral Condi- tion of Calcu- lations	Signif- icance and Discosition	Cognizant Engineer_	Origi- nator/ Checker Group Lender_	_Status_		1028 1029 1030 1031 103	
5. Soll structure	9	Pefer to sux			8/8		#/8	B/A		1	1091	
6. Besponse spectra (specific)	11							Bandy/Rc- Connel	Complete		1094 1095	
7. Vertical seismic	15				Tenk - s	parse	Otal	Bandy/Bc- Connel	Complete		1098	
					Foundati	on - good	Pierce	Bandy/Mc- Connel	Complete		1100	g
. Stress analysis											118	-
. 1. Steel tank	12	Vendor Jesign	Tes		Good		Rao/Desai	Tobdor	Complete	1	1106	
detion	13				Good		Reo/Desei	Bandy/ Udog1/Reo	Complete		1109	
C. Joint filler be- tween structures	18		8/8						281		1113	
D. Computer verifica- tion	16								6	۱	1117	
E. Overell stability	18				Good		Rao/Dessi	Bandy/ Udog1/Bao	Complete	1	1121 1122	
F. Interaction with mon-Category I structures	20										1125 1126 1127	
. C. Torasdo sissiles	21										1130	
111. Conformance to Staff's Criteria (De- vistions)	23										113. 1134 1135	~
B Part II - Kar Desists											1138	
A. Steel tank					Good		Rao/Desai	Vendor/ Rec	Complete	1	1140	
B. Foundation					Good		Pao/Dessi	Pandy/ Udog1/Reo	Complete	1	1183 1188	

1025

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## STRUCTURAL AUDIT LIST OF ITERS POPATED WATER STORAGE TARK

	Porated Vater	RPC Page Bos	Inarpropriate or Omitted 	Compliance with FSAR Coemitmenia	General Condi- tion of Calcu- lations	Signif- icance and Disposition	Cognizent Englagez.	Origi- metor/ Checker Grosp Leader_	Status	1029 1029 1030 1031 103
	rt III - Justifica: pa of Proposed Pe: LE								02	1187 1188 1189
·	Effects of thrs crecks	26							18	1152
	Test Procedere to Evaluate Settlement Effects	26							6 -	1156 1157 115P
E Co	rt IV - Iteas Fot Inred_is_Ouestions at_Should_be_Iden= fied									1161 1162 1163 1164

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STPUCTURAL AUDIT LIST OF ITEMS POPATED WATER STORAGE TANK

					General			Origi-		1020 .
					Cond1-	Signif-		hator/		1025
			**********	Compliance	tion of	icence		Checker		1030.
		RBC	Inerpropriate .	with FSAR	Calcu-	and	Cognizant	Group		1031
	rated Bater	Page	or Deittes		lations	Disposition	Enginger	Leader_	States	103
	torage_Task	E91	Celculations	Cossileenis	TETTANS	EVERXNY PARM	BRIDSING.			
										1167
BOTES	•									
613	Calculation 021	overturn	ing and sliding 5.F.	check.						1169
	Calculation 0248									1170
	Calculation 025	fandante	r isolation valve che	aber						1171
1.43	Calculation 026	containa	ent shell and base sl	ab analysis (FINE)	1)					1172
128-120-120-1			and analysis for sale	Pair inadian (1585)					and the second second	1173
B (4)	Calculation 056	continat	ion of Q26 and Q27 to	develop FSAR Tabl	les 2.8-1	and 3.8-17 (fc	or additions	1 relavant	calculations	11
	see MRC page 2)	Cospins	ton of gro and gro o							
								- 11 - 12 - 12 - 12 - 12 - 12 - 12 - 12	the second of the	1176
D 1483	(Pro optioner all	-1411	calculations 2148 st	. MRC page 44)(for	secondar	y shield well	calculation	033, 034	A, and Q35A	11-
										11 -
	see ant page 51)	-	dation sat reinforce	ent design (for a	tditional	relevant calcu	lations see	BRC page	19 calculatio	8 026
		V-8 1000	detion set terminister							
(10)	and Q27) (for Q24k mee RS									1181
									0	1182
		100, an	0 000						N	1183
	Question 51, Q51	s, and bu	at hatch reinforcese	at design					00	1984
(12)		Lana Ann	stanl acuinsant hatr	N 7220-508-17, 772	0-508-18					1185
			and the sat rainfo	rcesent decidn						1186
	Calculation Q4 a	Ind fins 1	nforcement (see MPC	secos 19 and 21 fo	r calculat	ions Q4, Q4A.	026, 027, 1	and OSb)	5	1187
(1 5 5	Calculation 010	wall rei	ulating Q10, Q26, C2	T ant O & see MRC	pages 2.	19, 24, 21, 3	4, and 371			1188
			are tius 610' 610'	· · · · · · · · · · · · · · · · · · ·						1189
	Calculation 014									1190
(1+)			. C18C. Q18G-1 struc	toral steal, concr.	ete. stuel	plate and gr	sting			1191
	Celculation 01/1	0, 01/1-	concrete, reinforces	ant (recent) dirds	rs. bracke	ts. concrete,	and reinf.	at bracket	t locations	1192
	Calculations 050	0, 05-64	concrete, reinforces	the						1193
(	Calculation 012	(014) 0	144-6 (new) 023P-10 0	THE .						1198
		lculetio	on 012							1195
. (24)	Calculation 012	a abbet	033, 034A, 055A-geo	A condition. Calc	alating Of	2 stress aupp	og boop-ra	adition (co	osponents	1196
(88)	Calculations Q1	3-a (CPDC)	013, 0344, 0004-900	a condition. care	a a a cana a a					1197
•	of snubbers, su	pport and	thor bolts, rear brac	Rets, tubind, res.		ditton				1108
(24)	Calculations 03	3, 0344,	and Q35A wall reinfo	rcement and detail	35-28 037	064. 0200-2		ctural ste	el. fen	1
(27)			065, 2188-1 0138-5 t							1200
	supports etc, ci	ore flood	surport, pipe restr t tensioning design a	aint, jet bartlets		lattone 7220-	C2-89. 7220	-C2-50, an	4 7220-C2-56-4	· boot
	Calculation Of,	Q6a post	t tensioning design a	ud lubar-boot. In	rico carco					1 1202
(	Calculation 07.	07a but	tress reinforcement 1	elsäy						1.11.1

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