

General Offices Selden Street, Berlin Connect ut

P.O. BOX 270 HARTFORD CONNECTICUT 06141-0220

Re: 10CFR50.73(a)(2)(v) January 20, 1992

U.S. Nuclear Regulatory Commission Document Control Desk Washington, D.C. 20555

Reference:

Facility Operating License No. NPF-49 Docket No. 50-423

Licensee Event Report 91-030-00

# Gentlemen:

This letter forwards Licensee Event Report 91-030-00 required to be submitted within thirty (30) days pursuant to 10CFR50.73(a)(2)(v), any event or condition th at alone could have prevented the fulfillment of the safety function of structures or systems that are needed to mitigate the consequences of an accident.

Very truly yours.

NORTHEAST NUCLEAR ENERGY COMPANY

Stephen E. Scace Director, Millstone Station

SES/GTB:lis

Attachment: LER 91-030-00

T. T. Martin, Region I Administrator

W. J. Raymond, Senior Resident Inspector, Millstone Unit Nos. 1, 2 and 3

V. L. Rooney, NRC Project Manager, Millstone Unit No. 3

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U.B. TRUCLEAR REQULATORY COMMISSION

APPROVED DMB NO. 3160-0108

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### Description of Even

On December 19, 1991, at 1300 hours, while shutdown in Mode 5 (Cold Shutdown), an engineering evaluation which was imitated in response to the failure of three normally energized auxiliary relays for safety related Motor Operated Valves (MOVs), concluded that the failures were due to thermal aging of the cold assembly and plastic parts near the cold. The tailed relays are Telemeranique (former ITE/Gould) model 110 control relays. The auxiliary relay failures were caused by the electric shorting of the relay coil due to insulation treakdown. As a result of the relay failures, the circuit control poer fuces blew. This caused a loss of control power and rendered the MOVs insperable. The affected MOVs were all powered from the Train 'B' Safety Related 480VAC bases. The event investigation revealed that the thermal aging condition existed for all normally energized 110 relays located in the Motor Control Centers (MCCs). The investigation concluded that a very high potential existed for additional relay failures due to the degree of thermal aging observed from other MCCs inspected.

The failures occurred at 0945 on November 23, 1991, during a Train 'B' Loss Of Power Test (LOP) conducted by the plant. As a result of the test, which imposed a transient on the Train 'B' 480VAC safety related buses and the subsequent re-energization of the buses by the auto start of the 'B' Emergency Diesel Generator, control power was lost to three safety related MOVs (3CCP'MOV227, 3MSS'MOV18B, 3; HS'LCV132E). After re-energizing the Train 'B' buses, a loss of control power alarm was received in the control room. The initial investigation determined that the loss of control power was due to the failure (i.e., shorting) of the 49X auxiliary relays which caused the control fuses to blow. The 49X relays are normally energized J10 relays which provide a motor thermal overload bypass function for the safety related MOVs and an alarm input for loss of control power for the circus. The failed relays were immediately replaced by plant maintenance electricians.

The Engineering investigation determined the following

- Inspection of the failed relays revealed that the movable plastic armature carrier which surrounds the
  core and roil, and the retainer for the magnet voke assembly, became discolored from blue to
  brown, embrittled and severely cracked. In addition, internal inspection of the coils revealed them
  to be chart, and having a burnt smell with physical arcing indications on the coil assemblies.
- A Review of LOP test data noted that the required 124 J10 relays had performed their safety functions for the 'B' Train test.
- 3. The failed J10 relays were mounted in small independent compartments located above breaker stacks in the Motor Control Centers. The failed J10 relays were mounted shoulder to shoulder, in a horizontal ganged arrangement on a universal mounting strip supplied and designed by the vendor. Tel mecanique. In all three cases, the relays mounted in the middle of the cluster failed.
- 4. A Review of electrical design drawings determined that all 49X and 74 auxiliary relays found in the NiCCs were normally energized 110 relays. The 74 function is used as an alarm input for loss of control power. In addition, two standard mounting arrangements were found to exist in the relay compartments for three or five relay configurations. The five relay arrangement had four ganged relays mounted shoulder to shoulder and one mounted individually.
- 5. A Review of the 's lemecanique technical data identified the tailed relays to be "ITE/Gould Model J10" control relays with "J20M" magnet block assemblies and standard G10JA126-120V, so evel coil assemblies. Per the equipment qualification report, the relays were qualified for the life of the plant. However, the qualification process did not account for their use in the ganged arrangement, as per the vendor design. The qualification testing described in the qualification test report did not account for the potential heat degradation from coil energization on "weak link" materials such as the plastic armature carrier. The failed coils had been in service, and normally energized for approximately seven years.

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- Additional J10 relays used in 49X and 74 applications where inspected in eight different Motor Control Centers. The inspections included both Salety and Non-Salety Related applications and in all cases moderate to significant thermal aging was observed. The relays were physically removed and the internal coil and plastic carriage assemblies were inspected. In all cases, there was discoloration of the plastic carrier assembly and varying degrees of cracking and embantlement. In addition, the surrounding relays in the ganged arrangement were inspected and Sound to have a significantly higher degree of discoloration on the inner shoulder (of the blue carrier) than on the outer shoulder, open to air.
- During the inspections of the additional 210 relays bus voltage was verified, both 480VAC line voltage and 120VAC control circuit voltage and in all cries the voltage was within acceptable limit for relay operation.
- It should be noted that discoloration was observed or the normally energized J10s which were free standing within the MCC cubicles, but to a significantly lesser degree.

Engineers I has postulated that the electrical stress of Jeenergizing and subsequently re-energizing the coils during the LOP Testing was sufficient to cause the weakened coil insulation to fail. There have not been any similar failures experienced at this plant in the past.

# II. Cause of Event

The root cause of the failure of the J10 relays is accelerated thermal aging of the coil and plastic parts near the coil due to prolonged overheaving. The problem is isolated to normally energized relays which are 'ganged' together.

After a review of the qualification test report documentation, it was discovered that the qualification test did not adequately test the normal!, energized relays mounted in the ganged arrangement.

The vendor had not considered the potential for accelerated aging and breakdown of the plastic components or the potential higher operating temperatures within the coil assemblies due to the standard "ganged" mounting configuration, per the vendors design.

It should be noted that Telemecanique did issue a 10CFR21 report to the NRC in October 1987, associated with overheating failures of special low voltage cuits for the J10 relays specifically at the Seabrook Nuclear Station. At that time no information was forwarded to Millstone. Part of their resolution was the changing of the armature carrier. Part Number #03938, to a remperature stabilized material which Telemecanique indicated would be adapted as a new standard to its relay line. It appears this has not happened and aging of the plastic components was not considered for the J19 relays in service.

#### III. Analysis of Event

This event is being reported in accordance with 10CFR50.73(a)(2)(v), as an event or condition which alone could have prevented the fulfillment of the safety function of structures or system that are needed to mitigate the consequences of an accident. As part of the required actions to response to the December 19, 1991 engineering evaluation conclusions, an immediate notification was performed pursuant to 10CFR50.72(b)(2)(iii).

The accreented thermal aging alone could have resulted in loss of equipment operations; due to the loss of control power. In the case of safety related MOVs with 49X relays, the valves would fail ""as is" and not perform any automatic or electrical manual instated operations. In the case of pumps and motions with 74 relays, the equipment would stop and would not respond to any automatic or manual control.

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The tailure mode of the relays caused motor operated valves in different systems to become inoperable. Results of the engineering investigation determined the accelerated aging of the 110 relays is considered to pose a significant safety consideration. Based on Engineering Judgment the potential for Loss OI Safety Function or System was possible if the plants electrical asstems had been challenged by a loss of power it should be noted that if relays had failed, the indure would have been detected by a loss of MCC control power alarm. The plant surveillance program, (i.e., the 18 month Loss OI Power Test) did detect the failures pro- to challenging the plant. The surveillance program mitigated the potential for greater failures to occur, during normal ident operation.

# 1V. Corrective Action

The immediate corrective action was to replace the three relays which failed during the Loss Of Power Texting. An Engineering investigation was initiated to determine the cause of the relay failures.

Upon completion of the Engineering investigation as documented in "Description of Event," the plant established a program which:

- Performed an inspection of all safety related J10 Relays, which included all MCCs and any other Cabinet/Panel which housed safety related J10s.
- 2. Performed 100% replacement of all the sidery related normally energized 49X and 74 relays.
- Evaluated and Replaced those J10 relays in non-safety related applications that could possibly challenge the plant.

Engineering has established a conservative life expectancy for the 110 relay of 5 years. This is based on the experience gained at Millstone. Engineering review of existing qualification report, information obtained from the Vender and another nuclear utility that had an analysis program associated with special 110 relays. In addition, a surveillance program is being developed which will sample and evaluate the 110 relays on a routine basis, with planned implementation prior to refueling outage No. 4.

A plant design change is being initiated for changing out the now no longer manufactured Telemecanique \$110 relays.

#### V. s.ddmoral Information

Telemecanique, the current manufacturer of the J10 telays has discontinued the manufacturing of these relays, as well as its 100 FR50 Appendix B program. They have provided no assistance in the evaluation of this incident, accelerated aging of components and indicated they no longer have the personnel to evaluate the insterial failures.

LER 86-051-00. LER 87-008-00. LER 87-034-00. "Reactor Trip Due To Low Steam Generator Level Caused By Failed Solenoid Valve" reported the failures of a solenoid valves. 3FW\$'SOV41 series, which supply control hydraulics for the feedwater isolation valves. The first event found no equipment problems and the cause was indeterminate. The subsequent events identified equipment problems. This was failure of qualified equipment within its qualification life. Subsequent investigation found a voltage problem and the coits assembles were replaced. These events are only related to this event by the fact that the failures were of qualified electrical devices and generic in nature. The failure mechanism of this event, accelerated thermal aging enhanced by the foounting transportent, a unrelated.

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LER 90-026-01, "Hydroger Monitor Temperature Profile/Operating Specification Income sency Dide to Inadequate Design Engineering Interface" reported the problem in maintaining the hydrogen monitor within calibration limits due to different temperature conditions found in the plant vice the equipment design temperature. A design modification was implemented to allow equipment operation under the temperature profile for the equipment location. This event is considered similar due to the impact that thermal conditions had on the plants safety related equipment, but would not have assisted in detecting or preventing this incident. This is due to the uniqueness of the confined thermal aging within the relay grouping, generated by the relays.

NPRDS was reviewed for similar failures of Telemecanique (ITE/Cimid) J10 Relays and no other incidents were reported.

Northeast Utilities has reviewed this incident with its other nuclear units (i.e., Millstone 1 & 2 and Connecticut Yarkee). The other units have evaluated their equipment and determined the problem is isolated to Unit 3. In addition, Seabrook Nuclear Station and Yankee Atomic Corp. have been contacted and informed about the event and the resultant investigation. Millstone 3 has also been in contact with INPO and has assisted in the preparation of a Significant Events Notification on this topic.

# EIIS Codes

System Low Voltage Power System, Class IE - ED

Components Relays - RLY

49X (thermal overload relay) 74 (control power relay)