CRISIS MANAGEMENT PLAN

IMPLEMENTING PROCEDURE

EDA - 3

"Off-Site Dose Projections for
McGuire Nuclear Station"

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Approved By

01-16-92
Date

Rev. 10
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DUKE POWER COMPANY

Off-Site Dose Projection

for McGuire Nuclear Station

1.0 PURPOSE:

1.1 To describe a method for projecting dose commitment from a noble gas and/or iodine release, through the containment, the unit vent and/or the steam relief valves, during an emergency. Where appropriate, the Dose Assessment Coordinator, or designee, may deviate from this procedure due to varying plant conditions.

2.0 REFERENCES:

2.1 HP/0/B/1003/08, Determination of Radiation Monitor Setpoints (EMF's).

2.2 HP/0/B/1009/02, Alternative Method for Determining Dose Rate Within the Reactor Building.

2.3 HP/0/B/1009/10, Releases of Liquid Radioactive Material Exceeding Selected Licensee Commitments.

2.4 HP/1/B/1009/15 and HP/2/B/1009/15, Post-Accident Containment Air Sampling System Operating Procedures.

2.5 HP/0/B/1009/06, Procedure for Quantifying High Level Radioactivity Releases During Accident Conditions.

2.6 McGuire Nuclear Station Technical Specifications 3.6.1.2.

2.7 Offsite Dose Calculation Manual (ODCM).

2.8 Regulatory Guide 1.4, "Assumptions Used for Evaluating the Potential Radiological Consequences of a Loss of Coolant Accident for Pressurized Water Reactors".

2.9 Regulatory Guide 1.109, "Calculations of Annual Doses to Man from Routine Releases of Reactor Effluents for the Purpose of Evaluating Compliance with 10 CFR Part 50, Appendix I".

2.10 NuReg-0396, EPA 520/1-78-016, "Planning Basis for the Development of State and Local Government Radiological Emergency Response Plans in Support of Light Water Nuclear Power Plants".

2.11 NuReg-0654, FEMA-REP-1,Rev.1, "Criteria for Preparation and Evaluation of Radiological Emergency Response Plans and Preparedness in Support of Nuclear Power Plants".

2.12 Letter from F.G. Hudson; September 30, 1985, re: Release Rate Information from McGuire and Catawba Nuclear Station.

2.13 McGuire Nuclear Station Class A Computer Model Validation.

2.14 Selected Licensee Commitment Manual Section 16.11-6.

2.15 Letter from C.D. Ingram: June 7, 1989, re: Containment Design Leak Rate Validation.

3.0 **LIMITS AND PRECAUTIONS:**

3.1 This procedure is an alternative method of dose assessment to the Class A Atmospheric Dispersion Model computer code.

3.2 This procedure applies to releases made from McGuire Nuclear Station only. Many of the values contained in this procedure are site specific.

3.3 It is assumed that the whole body dose from an iodine release is very small compared to the thyroid dose; therefore, iodine whole body dose is not considered here.

3.4 This procedure considers all releases to be ground level releases and that all meteorological data are 15 minute averages.

3.5 Once a zone has been added to the list of affected zones, it shall not be removed except under the direction of the Dose Assessment Coordinator.

3.6 Once the Crisis Management Center (CMC) has been activated, the doses calculated by the Technical Support Center (TSC) dose assessment group, shall be compared with those calculated by the CMC before an evacuation recommendation is made.

3.7 EMF's 38, 39, and 40 will isolate on a phase A containment isolation (1 psig in containment). Therefore, EMF's 38L, 38H, 39L, 39H, 40 and 48 should not be considered valid when containment pressure is $\geq$ 1 psig.

3.8 The sample pump to EMF's 35, 36, and 37 will trip when there is a Trip 1 on EMF 36 HH. Therefore, EMF's 35L, 35H, 36L, 36H, and 37 should not be considered valid when EMF 36 HH is $\geq$ Trip 1 (usually set at 5-7 R/Hr).

4.0 **PROCEDURE:**

NOTE: Much of the information for the meteorology assessment can be obtained on the OAC, (Tech. Spec. 04 program). See Enclosure 5.14 for instructions.

4.1 Meteorology Assessment

4.1.1 Acquire the following information and record on the Dose Assessment Report and Meteorology Worksheet (Enclosures 5.1 and 5.2 respectively).

4.1.1.1 Lower tower wind speed (WS) in miles per hour.

4.1.1.1.1 Use upper tower wind speed if lower tower wind speed is not available.

4.1.1.2 Upper tower wind direction in degrees from North (North = 0).

4.1.1.2.1 Use lower tower wind direction if upper tower wind direction is not available.

4.1.1.2.2 If the wind speed or wind direction can not be obtained from plant systems, obtain them from the National Weather Service (phone 359-8284, or unlisted 359-8292). If the NWS information is unavailable, then obtain data from the CNS Control Room (8-831-2338).

4.1.1.3 Temperature gradient (ΔT) in degrees centigrade.

4.1.1.4 Using Enclosure 5.3, determine the stability class based on ΔT. If ΔT is unknown, then the following applies:

4.1.1.4.1 If between 1000 - 1600 hours, use stability class D;

4.1.1.4.2 If between 1600 - 1000 hours, use stability class G.

4.1.1.5 If necessary, use forecasted meteorological data for calculating doses due to changing meteorological conditions.

4.1.2 Determine the atmospheric dispersion parameters, $\overline{X/Q}$ (sec/m^3), for .5, 2, 5 and 10 miles (record on Enclosure 5.1).

4.1.2.1 Using ΔT, determine the two hour relative concentration value (C_H) from Enclosure 5.3.

4.1.2.2 Convert the C_H values to X/Q:

$$\overline{X/Q} = \frac{C_H}{WS}$$

4.1.3 Using Enclosure 5.4, circle on Enclosure 5.1 the protective action zones (PAZ), based upon wind speed and wind direction.

4.1.4 Recheck meteorological conditions approximately every 15 minutes to ensure that other zones have not been affected.

4.2 Source Term Assessment - Steam Relief Valves (Enclosure 5.5)

NOTE: Much of the information for Steam Relief Valve source term assessment can be obtained from the OAC (General 19 program). See Enclosure 5.14 for instructions.

4.2.1 Determine the Sub-Noble Gas Release Rates, SQ_{NG} (Ci/sec), by the following method:

4.2.1.1 For Unit 1 - EMF24, EMF25, EMF26 and EMF27
For Unit 2 - EMF10, EMF11, EMF12, and EMF13

$$SQ_{NG} = mR/hr \times \frac{1}{VOPEN} \times LBM \times CF$$

where:

mR/hr = EMF reading
Unit 1 = EMF's 24, 25, 26, 27
Unit 2 = EMF's 10, 11, 12, 13
VOPEN = time the valve is open in seconds
LBM = lbm released for the time the valve was open
CF = the correction factor per Enclosure 5.6

$$Units = \frac{Ci}{lbm\ mR/hr}$$

4.2.2 Determine the Noble Gas Release Rate, Q_{NG} (Ci/sec):

Q_{NG} = SQ_{NG} (1EMF24 or 2EMF10) +
SQ_{NG} (1EMF25 or 2EMF11) +
SQ_{NG} (1EMF26 or 2EMF12) +
SQ_{NG} (1EMF27 or 2EMF13)

4.2.3 Determine the Iodine release rate, Q_I (Ci/sec):

$$Q_I = Q_{NG} \times I/Xe\ ratio$$

where:

I/Xe ratio = ratio of I-131 eqv./Xe-133 eqv. from Enclosure 5.7

4.2.4 Record Q_{NG} and Q_I from the steam relief valves on Enclosure 5.1.

4.3 Source Term Assessment - Containment (Enclosure 5.8)

NOTE: Some of the information for Containment source term assessment can be obtained from the OAC (Tech Spec 04 program). See Enclosure 5.14 for instructions.

4.3.1 Determine the Noble Gas Release Rate, Q_{NG} (Ci/sec) based on one of the following methods:

NOTE: See Limit and Precaution 3.7.

4.3.1.1 Based on an EMF reading, where;

$$Q_{NG} = EMF \times CF \times LR$$

where:

EMF = 39(L), if EMF39(L) < 1E7 cpm,
EMF = 39(H), if EMF39(L) is offscale and EMF39(H) > 100 cpm,
EMF = 51A or 51B; if EMF39(H) is offscale

CF = the correction factor per Enclosure 5.9

LR = Leak Rate, (ml/hr) by one of the following methods:

Based on containment pressure:

LR = RLR (from Enclosure 5.10)

Based on an opening in containment:

LR = OIC (from Enclosure 5.11)

Based on design leak rate:

LR = 3.02E5 (reference 2.15) assuming bypass leakage of 0.07.

4.3.1.2 Based on PAGS sample or sample collected in accordance with reference 2.5, where;

$$Q_{NG} = Conc. \times CF \times LR$$

Where:

Conc = the Xe-133 equivalent concentration (μCi/ml) from Reference 2.4 or 2.5

CF = $2.78E\text{-}10 \ \frac{Ci\ hr}{sec\ \mu Ci}$

LR = leak rate, as determined in step 4.3.1.1 above

4.3.2 Determine the Iodine Release Rate Q_I (Ci/sec), based on one of the following methods:

4.3.2.1 Based on Q_{NG};

$$Q_I = Q_{NG} \times I/Xe\ ratio$$

where:

Q_{NG} = noble gas release rate as determined in Step 4.3.1 above

I/Xe ratio = ratio of I-131 eqv./Xe-133 eqv. from Enclosure 5.7.

4.3.2.2 Based on EMF40:

$$Q_I = \frac{\Delta CPM}{\Delta min} \times 6.54E\text{-}20 \frac{Ci\ hr\ min}{sec\ ml\ cpm} \times LR$$

where:

ΔCPM = reading from EMF40

Δmin = the time interval for EMF40 observation (normally 15 minutes)

LR = leak rate as determined in step 4.3.1.1 above

6.54E-20 = (4.0E-5 μCi/cpm x .1667 min/ft^3 x 3.53E-5 ft^3/ml x 1Ci/1E6 μCi x 1 hr/3600 sec)

4.0E-5 = correlation factor for EMF40 from Reference 2.1

.1667 min/ft^3 = inverse of EMF flow rate

4.3.2.3 Based on PAGS sample or sample collected in accordance with reference 2.5.

$$Q_I = Conc \times 2.78E\text{-}10 \frac{Ci\ hr}{sec\ \mu Ci} \times LR$$

where:

Conc = I-131 equivalent concentration (μCi/ml) from Reference 2.4 or reference 2.5

LR = leak rate as determined in step 4.3.1.1 above

4.3.3 Record Q_{NG} and Q_I from containment on Enclosure 5.1.

4.4 **Source Term Assessment - Unit Vent** (Enclosure 5.12)

NOTE: Some of the information for Unit Vent source term assessment can be obtained from the OAC (Tech Spec 04 program). See Enclosure 5.14 for instructions.

4.4.1 Determine the Noble Gas Release Rate, Q_{NG} (Ci/sec), based on one of the following methods:

4.4.1.1 Based on an EMF reading, where

NOTE: See Limit and Precaution 3.8.

$$Q_{NG} = EMF \times CF \times CFM$$

where:

EMF = 36(L) if EMF36(L) < 1E7 cpm

EMF = 36(H) if EMF36(L) is offscale and EMF36(H) is > 100 cpm

EMF = 36(HH) if EMF36(H) is offscale

CF = the correction factor per Enclosure 5.13

CFM = unit vent flow rate (ft^3/min)

4.4.1.2 Based on unit vent sample, where;

$$Q_{NG} = Conc \times CF \times CFM$$

where:

Conc = the Xe-133 equivalent concentration (μCi/ml) from Reference 2.5

CF = 4.72E-4 $\frac{Ci\ min\ ml}{sec\ ft^3\ \mu Ci}$

CFM = Unit vent flow (ft^3/min)

4.4.2 Determine the Iodine Release Rate Q_I (Ci/s, based on one of the following methods:

4.4.2.1 Based on Q_{NG};

$$Q_I = Q_{NG} \times I/Xe\ ratio$$

where:

Q_{NG} = noble gas release rate as determined in step 4.4.1 above

I/Xe ratio = ratio of I-131 eqv./Xe-133 eqv. from Enclosure 5.7

4.4.2.2 Based on EMF37:

$$Q_I = \frac{\Delta CPM}{\Delta min} \times 1.11E\text{-}13 \frac{Ci\ min\ min}{sec\ ft^3\ cpm} \times CFM$$

where:

ΔCPM = reading from EMF37

Δmin = the time interval for EMF37 observation (normally 15 minutes)

CFM = unit vent flow (ft^3/min)

1.11E-13 = (4.0E-5 μCi/cpm x .1667 min/ft^3 x 1 Ci/1E6 μCi x 1 min/60 sec)

4.0E-5 = correlation factor for EMF 37 from Reference 2.1

.1667 min/ft^3 = inverse of EMF flow rate

4.4.2.3 Based on unit vent sample:

$$Q_I = Conc \times 4.72E\text{-}4 \frac{Ci\ min\ ml}{sec\ ft^3\ \mu Ci} \times CFM$$

where:

Conc = I-131 equivalent concentration (μCi/ml) from Reference 2.5

CFM = unit vent flow rate (ft^3/min)

4.4.3 Record Q_{NG} and Q_I from the unit vent on Enclosure 5.1.

4.5 **Dose Assessment** (Enclosure 5.1)

4.5.1 Determine the total Noble Gas and Iodine Release Rates (TQ_{NG} and TQ_I) by summing Q_{NG} and Q_I from all releases.

4.5.2 Determine the Projected Whole Body Dose Rate, DRwb (Rem/hr), due to noble gases for .5, 2, 5 and 10 miles:

$$DRwb = \overline{X/Q} \times TQ_{NG} \times 33.6 \frac{Rem\ m^3}{hr\ Ci}$$

where:

33.6 is the adult whole body dose conversion factor from Reference 2.9 in $\frac{Rem\ m^3}{hr\ Ci}$

4.5.3 Determine the Projected Whole Body Dose, Dwb (rem), due to noble gases for .5, 2, 5 and 10 miles:

$$Dwb = DRwb \times 2\ hr$$

where:

dose is integrated over 2 hour time period

4.5.4 Determine the Projected Child Thyroid Dose Rate, DRct (Rem/hr), due to iodine for .5, 2, 5 and 10 miles:

$$DRct = \overline{X/Q} \times TQ_i \times 2.26E6\ \frac{Rem\ m^3}{hr\ Ci}$$

where:

2.26E6 is the child thyroid dose conversion factor from Reference 2.13 in $\frac{Rem\ m^3}{hr\ Ci}$

4.5.5 Determine the Projected Child Thyroid Dose, Dct (Rem), due to iodine for .5, 2, 5 and 10 miles:

$$Dct = DRct \times 2\ hr$$

where:

dose is integrated over 2 hour time period

4.6 Protective Action Recommendations (Enclosure 5.1, page 2 of 2):

4.6.1 Record the next sequential report number.

4.6.2 Determine release status by the following guidance criteria:

No Release - no potential release of activity generated by the event.

Potential Release - activity generated by the event that can potentially be released, but is not currently being released.

Release Within Normal Operating Limits - activity generated by the event currently or previously released within normal operating limits (below 1.711E-1 mrem/hr child thyroid and/or 1.008 E-2 mrem/hr whole body). Examples include containment pressure $\geq$ 1psig with increased reactor building activity, S/G tube leak, increased unit vent activity, and field team activity.

NOTE: No dose projections to the state/counties are required for this case.

Release Above Normal Operating Limits - activity generated by the event currently or previously released above normal operating limits (above 1.711E-1 mrem/hr child thyroid and/or 1.008E-2 mrem/hr whole body).

NOTE: Selected Licensee Commitment normal operating limits (most limiting values) are derived below.

$$1.711E\text{-}1\ mrem/hr = 1500\ mrem/yr \times yr/8766\ hr.$$

$$1.008E\text{-}2\ mrem/hr = 3E\text{-}7\ \frac{\mu Ci}{ml} \times 33.6\ \frac{rem/hr}{Ci/m^3} \times \frac{Ci}{1E6\mu Ci} \times \frac{1E6ml}{m^3} \times 1E3\ \frac{mrem}{rem}$$

4.6.3 Circle the PAZs and the actions for the current and previous protective action recommendations.

4.6.4 If the projected dose in a PAZ is < 1 Rem whole body and < 5 Rem thyroid, then recommend no protective action (action A).

4.6.5 If the projected dose in a PAZ is 1 to < 5 Rem whole body or 5 to < 25 Rem thyroid, then recommend evacuation of children and pregnant women (unless constraints make it impractical) and shelter others (actions C and D).

4.6.6 If the projected dose in a PAZ is $\geq$ 5 Rem whole body or $\geq$ 25 Rem thyroid, then recommend evacuation of affected zones and shelter all remaining zones (actions B and C).

4.6.7 If the dose rate at the site boundary is $\geq$ 5.0E-4 Rem/hr whole body, then recommend an Alert.

4.6.8 If the dose rate at the site boundary is $\geq$ .05 Rem/hr whole body or $\geq$ .25 Rem/hr thyroid, then recommend a Site Area Emergency.

4.6.9 If the dose rate at the site boundary is $\geq$ 1 Rem/hr whole body of $\geq$ 5 Rem/hr thyroid, then recommend a General Emergency.

4.6.10 Using data on Enclosure 5.1, pages 2 and 3, complete Enclosure 5.1, page 1 "Emergency Notification", items 5, 10, 11, 12, 13, 14, and 15.

NOTE: On item 13, list any whole body or child thyroid dose rate less than 0.0001 mrem/hr as "less than background" (where 0.0001 is an assumed value based on yearly effluent data). For integrated doses, use Enclosure 5.15 to calculate the total dose from all releases.

4.6.11 Submit the Emergency Notification form to the offsite communicator for radiological recommendations only.

5.0 ENCLOSURES:

5.1 Emergency Notification/Dose Assessment Report

5.2 Meteorology Worksheet

5.3 Two-hour Relative Concentration Factors (C_H)

5.4 Protective Action Zones Determination

5.5 Source Term Assessment - Steam Relief Valves

5.6 EMF24, EMF25, EMF26, EMF27 or EMF10, EMF11, EMF12, EMF13 Noble Gas Correction Factors (Steam Line Monitors)

5.7 I-131 eqv./Xe-133 eqv. Ratio

5.8 Source Term Assessment - Containment

5.9 Containment Monitors - Correction Factors

5.10 Containment Leakage Rate versus Pressure

5.11 Containment Leakage Rate versus Pressure and Size Opening

5.12 Source Term Assessment - Unit Vent

5.13 Unit Vent Monitors - Correction Factors

5.14 OAC Instructions

5.15 Integrated Dose Calculation

EMERGENCY NOTIFICATION

1. [A] THIS IS A DRILL [B] ACTUAL EMERGENCY [ ] INITIAL [ ] FOLLOW-UP* MESSAGE NUMBER _____

2. SITE: McGuire Nuclear Sta. UNIT: _____ REPORTED BY: _____

3. TRANSMITTAL TIME/DATE: _____ (Eastern) _____ mm / _____ dd / _____ yy CONFIRMATION PHONE NUMBER: 875-6044

4. AUTHENTICATION (If Required): _____ (Number) _____ (Codeword)

5. EMERGENCY CLASSIFICATION: (based on radiological conditions only)
[A] NOTIFICATION OF UNUSUAL EVENT [B] ALERT [C] SITE AREA EMERGENCY [D] GENERAL EMERGENCY

6. [A] Emergency Declaration At: [B] Termination At: TIME/DATE: _____ (Eastern) _____ mm / _____ dd / _____ yy (If B, go to item 15.)

7. EMERGENCY DESCRIPTION/REMARKS: _____

8. PLANT CONDITION: [A] IMPROVING [B] STABLE [C] DEGRADING

9. REACTOR STATUS: [A] SHUTDOWN: TIME/DATE: _____ (Eastern) _____ mm / _____ dd / _____ yy [B] _____ % POWER

10. EMERGENCY RELEASE(S):
[A] NONE (Go to item 14.) [B] POTENTIAL (Go to item 14.) [C] IS OCCURRING [D] HAS OCCURRED

**11. TYPE OF RELEASE: [ ] ELEVATED [X] GROUND LEVEL
[A] AIRBORNE: Started: _____ Time (Eastern) ____ / ____ / ____ Date Stopped: _____ Time (Eastern) ____ / ____ / ____ Date
[B] LIQUID: Started: _____ Time (Eastern) ____ / ____ / ____ Date Stopped: _____ Time (Eastern) ____ / ____ / ____ Date

**12. RELEASE MAGNITUDE: [X] CURIES PER SEC [ ] CURIES NORMAL OPERATING LIMITS: [ ] BELOW [ ] ABOVE
[A] NOBLE GASES _____ [B] IODINES _____
[C] IODINE/NOBLE GAS RATIO (if available) _____ [D] OTHER _____

**13. ESTIMATE OF PROJECTED OFFSITE DOSE: [ ] NEW [ ] UNCHANGED ESTIMATED DURATION: _____ HRS.

	Wholebody DOSE RATE (mrem/hr)	Child Thyroid DOSE RATE (mrem/hr)	Wholebody DOSE (mrem)	Child Thyroid DOSE (mrem)
SITE BOUNDARY				
2 MILES				
5 MILES				
10 MILES				

**14. METEOROLOGICAL DATA: [A] WIND DIRECTION (from) _____ ° [B] SPEED (mph) _____
[C] STABILITY CLASS _____ [D] PRECIPITATION (type) _____

15. RECOMMENDED PROTECTIVE ACTIONS: (based on radiological conditions only)
[A] NO RECOMMENDED PROTECTIVE ACTIONS
[B] EVACUATE _____
[C] SHELTER IN-PLACE _____
[D] OTHER _____

16. APPROVED BY: _____ (Name) _____ (Title) TIME/DATE: _____ (Eastern) _____ mm / _____ dd / _____ yy

* If items 8-14 have not changed, only items 1-7 and 15-16 are required to be completed.
**Information may not be available on initial notifications.

Form 34888 (R7-90)

McGUIRE NUCLEAR STATION
DOSE ASSESSMENT REPORT

Unit _____ Report # _____

Reactor Trip _____/_____ (date/time) Projection based on data on _____/_____ (date/time)

Prepared by: _____

Meteorology Assessment

[ ] Current [ ] Hypothetical

Wind Speed _____ mph Wind Direction _____ degrees from North
Temperature Gradient (ΔT) _____ C Stability Class A B C D E F G

Miles	0 - 2	2 - 5	5 - 10
PAZ	L B M C	N A D O R	E F G H I J K P Q S

Total Source Term Assessment

[ ] Current [ ] Hypothetical

Steam Relief Enclosure 5.5		Containment Enclosure 5.8		Unit Vent Enclosure 5.12		Total (Ci/sec)	
_____ Ci/sec	+	_____ Ci/sec	+	_____ Ci/sec	=	_____	= TQ_{NG}
_____ Ci/sec	+	_____ Ci/sec	+	_____ Ci/sec	=	_____	= TQ_{I}

Dose Assessment

$$\frac{C_H}{WS} = \overline{X/Q}$$

← Adult Whole Body ←

$$\left[\text{2 hr Dose (rem)} \cdots 2 \times \text{DRwb (rem/hr)} \cdots 33.6 \times \text{TQ}_{NG}\text{ (Ci/sec)} \times \overline{X/Q}\right]$$

_____	= 2 x	_____	= 33.6 x	TQ_{NG} _____	.5	_____		
_____	= 2 x	_____	= 33.6 x	_____	2	_____		
_____	= 2 x	_____	= 33.6 x	_____	5	_____		
_____	= 2 x	_____	= 33.6 x	_____	10	_____		
_____	= 2 x	_____	= 33.6 x	_____	1	_____		
_____	= 2 x	_____	= 33.6 x	_____	4	_____		
_____	= 2 x	_____	= 33.6 x	_____	7	_____		
_____	= 2 x	_____	= 33.6 x	_____	8	_____		

$\overline{X/Q}$ (sec/m³) Distance miles

→ Child Thyroid →

$$\left[\overline{X/Q} \times \text{TQ}_{I}\text{ (Ci/sec)} \times 2.26E6 \cdots \text{DRct (rem/hr)} \times 2 \cdots \text{2 hr Dose (rem)}\right]$$

TQ_{I} _____	x 2.26E6 =	_____	x 2 =	_____				
_____	x 2.26E6 =	_____	x 2 =	_____				
_____	x 2.26E6 =	_____	x 2 =	_____				
_____	x 2.26E6 =	_____	x 2 =	_____				
_____	x 2.26E6 =	_____	x 2 =	_____				
_____	x 2.26E6 =	_____	x 2 =	_____				
_____	x 2.26E6 =	_____	x 2 =	_____				
_____	x 2.26E6 =	_____	x 2 =	_____				

Field Data

Adult whole body

Location	Dose Rate Rem/hr	2hr Dose Rem
_____	_____	_____
_____	_____	_____
_____	_____	_____
_____	_____	_____

Child thyroid

Location	Dose Rate Rem/hr	2hr Dose Rem
_____	_____	_____
_____	_____	_____
_____	_____	_____
_____	_____	_____

[ ] Emergency [ ] Drill

McGUIRE NUCLEAR STATION
DOSE ASSESSMENT REPORT

The Emergency Condition ***Report #*** _____

_____ (a) No release - no potential release of activity generated by the event.
_____ (b) Potential release - activity generated by the event that can potentially be released, but is not currently being released.
_____ (c) Release (within normal operating limits) - activity generated by the event currently or previously released within normal operating limits. (below 1.711 E-1 mrem/hr child thyroid and/or 1.008E-2 mrem/hr whole body)
Started _____ Stopped _____ In progress _____
_____ (d) Release (above normal operating limits) - activity generated by the event, currently or previously released above normal operating limits (above 1.711E-1 mrem/hr child thyroid and/or 1.008E-2 mrem/hr whole body).
Started _____ Stopped _____ In progress _____

The following protective actions are recommended:

MILES	PAZ	CURRENT ACTIONS	PREVIOUS ACTIONS
0 - 2	L,B,M,C	A B C D	A B C D
2 - 5	N,A,D,O,P	A B C D	A B C D
5 - 10	E,F,G,H,I,J,K,P,Q,S	A B C D	A B C D

A) Monitor environmental radiation levels. No specific actions. (<1 Rem Whole Body and <5 Rem Thyroid)
B) Evacuate affected zones and seek shelter if immediate evacuation is not possible. Shelter all remaining zones. Monitor environmental radiation levels Control access. (≥ 5 Rem Whole Body or ≥ 25 Rem Thyroid)
C) Remain indoors with windows closed, turn off air conditioners and other ventilation, monitor EBS stations. Control access. (Action D also) (1 to <5 Rem Whole Body or 5 to <25 Rem Thyroid)
D) Pregnant women and children evacuate (unless constraints make it impractical) and go to designated shelter. (1 to <5 Rem Whole Body or 5 to <25 Rem Thyroid)
* - based on field data

Emergency Classification based on <u>Radiological Data</u>

[ ] Recommend Alert
(Dose rate at 0.5 miles is > .5 mR/hr Whole Body)

[ ] Recommend Site Area Emergency
(Dose rate at 0.5 miles is > .05 Rem/hr Whole Body or > .25 Rem/hr Thyroid)

[ ] Recommend General Emergency
(Dose rate at 0.5 miles is > 1 Rem/hr Whole Body or > 5 Rem/hr Thyroid)

Comments:

_____
_____
_____

Doses concur with CMC? (Yes/No/NA)

_____ _____ / _____
Dose Assessment Coordinator Date/Time

[ ] Emergency
[ ] Drill

McGUIRE NUCLEAR STATION
METEOROLOGY

Unit: _____ Report #: _____

Reactor Trip: ____/____

Prepared by: _____

Wind speed (WS) _____ mph

Wind direction _____ °N

ΔT _____ °C

Default Data

	Wind speed (WS) _____	mph
1000 to 1600 hrs.	Wind direction _____	°N
	Stability Class ___D___	°C
	Wind speed (WS) _____	mph
1600 to 1000 hrs.	Wind direction _____	°N
	Stability Class ___G___	°C

NOTE: If the wind speed or wind direction cannot be obtained from plant systems, obtain them from the National Weather Service, 359-8284 or unlisted 359-8292. If NWS information is unavailable, then obtain data from the Catawba Nuclear Station Control Room, 8-831-2338.

McGUIRE NUCLEAR STATION
TWO-HOUR RELATIVE CONCENTRATION FACTORS (C_H)

Temperature Gradiant	Stability Class	Distance (Miles)										
		.5	1	2	3	4	5	6	7	8	9	10
1) $\Delta T < -.6$	A	1.4E-5	1.2E-6	5.9E-7	4.1E-7	3.2E-7	2.5E-7	2.0E-7	1.9E-7	1.8E-7	1.6E-7	1.5E-7
2) $-.6 \leq \Delta T < -.5$	C	1.5E-4	4.5E-5	1.3E-5	6.3E-6	3.9E-6	2.7E-6	1.9E-6	1.4E-6	1.1E-6	8.3E-7	7.8E-7
3) $-.5 \leq \Delta T < -.2$	D	3.8E-4	1.4E-4	4.9E-5	2.7E-5	1.7E-5	1.2E-5	9.2E-6	7.3E-6	6.0E-6	5.0E-6	4.3E-6
4) $-.2 \leq \Delta T < +.4$	E	6.9E-4	2.5E-4	9.6E-5	5.5E-5	3.5E-5	2.5E-5	2.0E-5	1.6E-5	1.3E-5	1.1E-5	9.7E-6
5) $+.4 \leq \Delta T < +1.2$	F	1.1E-3	5.1E-4	2.0E-4	1.2E-4	8.2E-5	6.3E-5	5.1E-5	4.3E-5	3.8E-5	3.3E-5	3.0E-5
6) $+1.2 \leq \Delta T$	G	1.8E-3	1.1E-3	4.3E-4	2.7E-4	2.0E-4	1.7E-4	1.3E-4	1.2E-4	8.6E-5	7.8E-5	7.3E-5

NOTE: If ΔT is unavailable use: 1000–1600 hours Use Stability Class D

1600–1000 hours Use Stability Class G

There is no B Stability Class for McGuire.

McGUIRE NUCLEAR STATION
PROTECTIVE ACTION ZONES DETERMINATION

Determine the affected zones (based on wind direction) from the table below and record on Enclosure 5.1.

NOTE: If wind speed is less than or equal to 5 mph – the affected zones for 0 – 5 miles shall be L,B,M,C,N,A,D,O,R

Wind Direction (Degrees from North)	0 – 5 Miles	5 – 10 Miles
0 – 22.5	L,B,M,C,D,O,R	E,S,F
22.6 – 45.0	L,B,M,C,D,O,R	E,Q,S
45.1 – 67.5	L,B,M,C,D,O,R	E,Q,S
67.6 – 90.0	L,B,M,C,D,O,R,N	P,Q,S
90.1 – 112.5	L,B,M,C,O,R,N	K,P,Q,S
112.6 – 135.0	L,B,M,C,O,N,R,A	I,K,P,Q,S
135.1 – 157.5	L,B,M,C,O,A,N	I,K,P,Q
157.6 – 180.0	L,B,M,C,A,N	I,J,K,P
180.1 – 202.5	L,B,M,C,A,N	G,H,I,J,K,P
202.6 – 225.0	L,B,M,C,A,N,D	G,H,I,J,K,P
225.1 – 247.5	L,B,M,C,A,D	F,G,H,I,J
247.6 – 270.0	L,B,M,C,A,D	F,G,H,I,J
270.1 – 292.5	L,B,M,C,A,D	E,F,G,H,J
292.6 – 315.0	L,B,M,C,A,D	E,F,G
315.1 – 337.5	L,B,M,C,D,R	E,F,G
337.6 – 359.9	L,B,M,C,D,R	E,F,S

McGUIRE NUCLEAR STATION
SOURCE TERM ASSESSMENT - STEAM RELIEF VALVES

Report # _____

Reactor Trip: _____/_____ (date/time)

Projection based on data on: _____/_____ (date/time)

Calculations based on _____ Melted Core _____ LOCA

NOBLE GAS

based on EMF24 or EMF10

_____ mR/hr × $\frac{1}{\text{_____ sec}}$ × _____ lbm × $\frac{\text{_____ Ci}}{\text{lbm mR/hr}}$ = _____ Ci/sec

+

based on EMF25 or EMF11

_____ mR/hr × $\frac{1}{\text{_____ sec}}$ × _____ lbm × $\frac{\text{_____ Ci}}{\text{lbm mR/hr}}$ = _____ Ci/sec

+

based on EMF26 or EMF12

_____ mR/hr × $\frac{1}{\text{_____ sec}}$ × _____ lbm × $\frac{\text{_____ Ci}}{\text{lbm mR/hr}}$ = _____ Ci/sec

+

based on EMF27 or EMF13

_____ mR/hr × $\frac{1}{\text{_____ sec}}$ × _____ lbm × $\frac{\text{_____ Ci}}{\text{lbm mR/hr}}$ = _____ Ci/sec

Total from all Steam Relief Valves, Q_{NG} = _____ Ci/sec

* from Enclosure 5.6

IODINE

From all Steam Relief Valves

Q_I

_____ Ci/sec(Q_{NG}) × _____ *I-131 eqv./Xe-133 eqv. ratio* (*Enclosure 5.7*) = _____ Ci/sec

☐ Emergency ☐ Drill

Prepared By: _____

McGUIRE NUCLEAR STATION
STEAM LINE MONITOR
NOBLE GAS CORRECTION FACTOR
EMF24, EMF25, EMF26, EMF27, or
EMF10, EMF11, EMF12, EMF13

Time Since Trip (hrs)	Correction Factor
≥ 0	6.3820×10^{-3}
≥ 2	1.1255×10^{-2}
≥ 4	1.2763×10^{-2}
≥ 8	1.4736×10^{-2}
≥ 24	1.6476×10^{-2}
≥ 48	1.6476×10^{-2}
≥ 100	1.6476×10^{-2}
≥ 250	1.6476×10^{-2}
≥ 500	1.6476×10^{-2}
≥ 720	1.6476×10^{-2}

* *units in* $\frac{Ci}{lbm\ mR/hr}$

* *Enclosure 5.6 is the correlation factor per Reference* 2.13 $\times$ 2.83E4 $\frac{ml}{ft^3} \times .41\ \frac{ft^3}{lbm} \times \frac{Ci}{1E6\ \mu Ci} \times \frac{1R}{1000\ mR}$

.41 = *specific volume of steam per Reference* 2.13.

McGUIRE NUCLEAR STATION
I-131 eqv./Xe-133 eqv. Ratio

NOTE: For containment releases in which I/Xe ratio is utilized to determine I-131 equiv. concentration, apply the appropriate correction from the table below.

Time Since Trip (hrs)	Column 1 Ratio based on LOCA	Column 2 Ratio based on Melted Core
≥ 0	2.91E-3	2.24E-3
≥ 2	3.61E-3	9.66E-3
≥ 4	4.05E-3	1.59E-2
≥ 8	4.64E-3	2.85E-2
≥ 24	5.08E-3	7.52E-2
≥ 48	5.11E-3	1.11E-1
≥ 100	5.42E-3	1.33E-1
≥ 250	7.00E-3	1.80E-1
≥ 500	1.09E-2	2.90E-1
≥ 720	1.53E-2	4.33E-1

* Enclosure 5.7 is from Reference 2.13.

NOTE: For vent releases in which I/Xe ratio is utilized to determine I-131 equiv. concentration, apply the appropriate correction from the table below:

1. LOCA, use column 1 (based on LOCA).
2. LOCA through charcoal filters, divide column 1 value by 100.
3. Core damage, use column 2 (based on Core Melt).
4. Core damage through charcoal filters, divide column 2 values by 100.
5. Tube rupture, use 1.53E-5. (Column 1 value at ≥ 720 hrs. divided by 1000).
6. New fuel accident (< 100 hours old), use 2.217E-4. (Column 2 value at ≥ 100 hrs. divided by 600).
7. Old fuel accident (≥ 100 hours old), use 7.217E-4. (Column 2 value at ≥ 720 hrs. divided by 600).
8. Gas decay tank, assume no radioiodine released, only noble gases are considered to be released from gas tank.

NOTE: For steam release in which I/Xe ratio is utilized to determine I-131 equiv. concentration, apply the appropriate correction from the table below:

1. Design basis primary coolant, divide column 1 value by 100.
2. Iodine spiked primary coolant, use column 1.
3. Core damage, divide column 2 value by 100.

McGUIRE NUCLEAR STATION
SOURCE TERM ASSESSMENT - CONTAINMENT

Report # _____

Reactor Trip _____/_____ (date/time)

Projection based on date on _____/_____ (date/time)

Calculations based on _____ Melted Core _____ LOCA
Containment pressure _____ psig
LR = _____ ml/hr
LR based on: (circle one) Realistic Leak Rate | Opening in Containment Opening size: _____ | Design Leak Rate 3.02E6 assuming bypass leakage of 0.07

NOBLE GAS

based on (check one)

EMF39 (L) ☐ if < 1E7 cpm | EMF39(H) ☐ if > 100 cpm | EMF51 ☐ if 39(H) is offscale

EMF		CF		LR		Q_{NG}
_____ cpm or R/hr	x	_____ (Encl. 5.9)	x	_____ ml/hr	=	_____ Ci/sec

based on PAGS sample

_____ $\mu Ci/ml$ x 2.78E-10 $\frac{Ci\ hr}{sec\ \mu Ci}$ x _____ ml/hr = _____ Ci/sec

IODINE

based on

Q_{NG}						Q_I
_____ Ci/sec	x	_____		I-131 eqv./Xe-133 eqv. ratio (Encl. 5.7)	=	_____ Ci/sec

based on EMF40

				LR		
$\frac{\_\_\_\_\ \Delta cpm}{\_\_\_\_\ \Delta min}$	x	6.54E-20 $\frac{Ci\ hr\ min}{sec\ ml\ cpm}$	x	_____ ml/hr	=	_____ Ci/sec

based on PAGS sample

_____ $\mu Ci/ml$ x 2.78E-10 $\frac{Ci\ hr}{sec\ \mu Ci}$ x _____ ml/hr = _____ Ci/sec

☐ Emergency ☐ Drill Prepared By: _____

McGUIRE NUCLEAR STATION
CONTAINMENT MONITORS NOBLE GAS CORRECTION FACTORS

EMF39L

Time Since Trip (hrs)	Correction Factor Based on LOCA	Correction Factor Based on Melted Core
≥ 0	6.394E-18	6.672E-17
≥ 2	6.394E-18	4.448E-17
≥ 4	6.394E-18	3.058E-17
≥ 8	6.394E-18	2.113E-17
≥ 24	6.394E-18	1.112E-17
≥ 48	6.394E-18	1.056E-17
≥ 100	6.394E-18	1.390E-17
≥ 250	6.394E-18	1.446E-17
≥ 500	6.394E-18	9.730E-18
≥ 720	6.394E-18	6.394E-18

Units in $\frac{Ci\ hr}{sec\ ml\ cpm}$

EMF39H

Time Since Trip (hrs)	Correction Factor Based on LOCA	Correction Factor Based on Melted Core
≥ 0	5.56E-14	1.429E-13
≥ 2	5.56E-14	1.003E-13
≥ 4	5.56E-14	1.232E-13
≥ 8	5.56E-14	1.195E-13
≥ 24	5.56E-14	7.339E-14
≥ 48	5.56E-14	6.060E-14
≥ 100	5.56E-14	5.699E-14
≥ 250	5.56E-14	5.588E-14
≥ 500	5.56E-14	5.560E-14
≥ 720	5.56E-14	5.560E-14

Units in $\frac{Ci\ hr}{sec\ ml\ cpm}$

EMF51 A or B

Time Since Trip (hrs)	Correction Factor Based on LOCA	Correction Factor Based on Melted Core
≥ 0	3.781E-10	1.150E-9
≥ 2	3.114E-10	5.894E-10
≥ 4	2.780E-10	4.726E-10
≥ 8	2.446E-10	3.392E-10
≥ 24	2.335E-10	1.990E-10
≥ 48	2.335E-10	1.668E-10
≥ 100	2.335E-10	1.612E-10
≥ 250	2.335E-10	1.557E-10
≥ 500	2.335E-10	1.251E-10
≥ 720	2.335E-10	1.056E-10

Units in $\frac{Ci\ hr}{sec\ ml\ R/hr}$

* Enclosure 5.9 is the correlation factor per Reference 2.13 $\times \frac{hr}{3600\ sec} \times \frac{Ci}{1E6\ \mu Ci}$

McGUIRE NUCLEAR STATION
CONTAINMENT LEAKAGE RATE VERSUS PRESSURE

PSiG	ml/hr
$\geq$ 0	1.460E4
$\leq$ 2	3.175E4
$\geq$ 4	5.821E4
$\leq$ 8	9.779E4
$\geq$ 10	1.114E5
$\leq$ 11	1.164E5
$\geq$ 12	1.199E5
$\leq$ 13	1.235E5
$\geq$ 14	1.260E5
= 15	1.285E5
> 15	Use design leak rate (3.02E5 mℓ/hr)

* Enclosure 5.10 is the realistic leakage rate (m^3/sec per Reference 2.12 and 2.15) x 1E6 ml/m^3 x 3600 sec/hr x 0.07 (0.07 per Reference 2.6).

McGUIRE NUCLEAR STATION
CONTAINMENT LEAKAGE RATE VERSUS PRESSURE AND SIZE OPENING

For 1" diameter opening					
PSIG	ml/hr	PSIG	ml/hr	PSIG	ml/hr
>1.25	2.209E8	> 5.0	3.908E8	> 12.5	5.862E8
>2.50	2.889E8	> 7.5	4.588E8	> 15.0	6.287E8
>3.75	3.483E8	> 10.0	5.268E8		
For 2" diameter opening					
PSIG	ml/hr	PSIG	ml/hr	PSIG	ml/hr
> 1.25	8.4[illegible]E8	> 5.0	1.512E9	> 12.5	2.243E9
> 2.50	1.1[illegible]E9	> 7.5	1.784E9	> 15.0	2.464E9
> 3.75	1.342E9	> 10.0	2.022E9		
For 4" diameter opening					
PSIG	ml/hr	PSIG	ml/hr	PSIG	ml/hr
> 1.25	3.144E9	> 5.0	5.692E9	> 12.5	8.496E9
> 2.50	4.248E9	> 7.5	6.797E9	> 15.0	9.176E9
> 3.75	5.098E9	> 10.0	7.731E9		
For 6" diameter opening					
PSIG	ml/hr	PSIG	ml/hr	PSIG	ml/hr
> 1.25	7.137E9	> 5.0	1.291E10	> 12.5	1.937E10
> 2.50	9.516E9	> 7.5	1.529E10	> 15.0	2.124E10
> 3.75	1.138E10	> 10.0	1.716E10		
For 8" diameter opening					
PSIG	ml/hr	PSIG	ml/hr	PSIG	ml/hr
> 1.25	1.257E10	> 5.0	2.243E10	> 12.5	3.381E10
> 2.50	1.648E10	> 7.5	2.634E10	> 15.0	[illegible]68E10
> 3.75	1.971E10	> 10.0	3.042E10		
For 12" diameter opening					
PSIG	ml/hr	PSIG	ml/hr	PSIG	ml/hr
> 1.25	2.719E10	> 5.0	5.012E10	> 12.5	7.476E10
> 2.50	3.733E10	> 7.5	5.947E10	> 15.0	8.156E10
> 3.75	4.452E10	> 10.0	6.712E10		
For 18" diameter opening					
PSIG	ml/hr	PSIG	ml/hr	PSIG	ml/hr
> 1.25	5.522E10	> 5.0	1.003E11	> 12.5	1.529E11
> 2.50	7.476E10	> 7.5	1.199E11	> 15.0	1.665E11
> 3.75	8.836E10	> 10.0	1.351E11		
For 34" diameter opening					
PSIG	ml/hr	PSIG	ml/hr	PSIG	ml/hr
> 1.25	1.869E11	> 5.0	3.398E11	> 12.5	5.132E11
> 2.50	2.583E11	> 7.5	4.078E11	> 15.0	5.607E11
> 3.75	3.093E11	> 10.0	4.588E11		
For Personnel Hatch Opening					
PSIG	ml/hr	PSIG	ml/hr	PSIG	ml/hr
> 1.25	2.379E12	> 5.0	4.090E12	> 12.5	6.967E12
> 2.50	3.398E12	> 7.5	5.573E12	> 15.0	7.646E12
> 3.75	4.111E12	> 10.0	6.372E12		
For Equipment Hatch Opening					
PSIG	ml/hr	PSIG	ml/hr	PSIG	ml/hr
> 1.25	1.121E13	> 5.0	2.022E13	> 12.5	3.059E13
> 2.50	1.478E13	> 7.5	2.379E13	> 15.0	3.398E13
> 3.75	1.767E13	> 10.0	2.719E13		

* Enclosure 5.11 is the containment leakage for an opening size in standard cubic feet per min (scfm) x 2.8[illegible]4 ml/ft^3 x 60 min/hr.

McGUIRE NUCLEAR STATION
SOURCE TERM ASSESSMENT – UNIT VENT

Report # _____

Reactor Trip _____ _____ (date/time)

Projection based on date on _____ / _____ (date/time)

Calculations based on _____ Melted Core _____ LOCA

CFM = _____ ft^3/min

NOBLE GAS

based on (check one)

EMF36 (L) ☐ if < 1E7 cpm

EMF36(H) ☐ if > 100 cpm

EMF36(HH) ☐ if 36(H) is offscale

EMF		CF		CFM		Q_{NG}
_____ cpm or R/hr	x	_____ (Encl. 5.13)	x	_____ $\frac{ft^3}{min}$	=	_____ $\frac{Ci}{sec}$

based on Unit Vent Sample

_____ $\mu Ci/ml$	x	4.72E-4 $\frac{Ci\ min\ ml}{sec\ ft^3\ \mu Ci}$	x	_____ $\frac{ft^3}{min}$	=	_____ $\frac{Ci}{sec}$

IODINE

based on

Q_{NG}						Q_I
_____ $\frac{Ci}{sec}$	x	_____		I-131 eq./Xe-133 eqv. ratio (Encl. 5.7)	=	_____ $\frac{Ci}{sec}$

based on EMF37

				CFM		
_____ $\frac{\Delta cpm}{\Delta min}$	x	1.11E-13 $\frac{Ci\ min\ min}{sec\ ft^3\ cpm}$	x	_____ $\frac{ft^3}{min}$	=	_____ $\frac{Ci}{sec}$

based on Unit Vent Sample

_____ $\mu Ci/ml$	x	4.72E-4 $\frac{Ci\ min\ ml}{sec\ ft^3\ \mu Ci}$	x	_____ $\frac{ft^3}{min}$	=	_____ $\frac{Ci}{sec}$

☐ Emergency ☐ Drill Prepared By: _____

McGUIRE NUCLEAR STATION
UNIT VENT MONITORS NOBLE GAS CORRECTION FACTORS

Correction Factors for Melted Core
Accidents with or without charcoal

Time Since Trip (hrs)	EMF36L based on Melted Core $\left(\frac{Ci\ min}{sec\ ft^3\ cpm}\right)$	EMF36H based on Melted Core $\left(\frac{Ci\ min}{sec\ ft^3\ cpm}\right)$	EMF 36HH based on Melted Core $\left(\frac{Ci\ min}{sec\ ft^3\ R/hr}\right)$
≥ 0	1.133E-10	2.426E-7	1.887E-3
≥ 2	7.552E-11	1.704E-7	1.179E-3
≥ 4	5.192E-11	2.091E-7	9.905E-4
≥ 8	3.587E-11	2.030E-7	6.367E-4
≥ 24	1.888E-11	1.246E-7	2.931E-4
≥ 48	1.794E-11	1.029E-7	2.405E-4
≥ 100	2.360E-11	9.676E-8	2.358E-4
≥ 250	2.454E-11	9.481E-8	2.358E-4
≥ 500	1.652E-11	9.440E-8	2.358E-4
≥ 720	1.086E-11	9.440E-8	2.358E-4

Correction Factors for All Other Accidents

Accident	EMF 36L $\left(\frac{Ci\ min}{sec\ ft^3\ cpm}\right)$	EMF36H $\left(\frac{Ci\ min}{sec\ ft^3\ cpm}\right)$	EMF 36HH $\left(\frac{Ci\ min}{sec\ ft^3\ R/hr}\right)$
New Fuel (<100 hrs old)	2.360E-11	9.676E-8	2.358E-4
All Other Accidents *	1.086E-11	9.440E-8	2.358E-4

* Accidents include LOCA with or without charcoal, Tube Rupture, WGDT, and Old Fuel (≥ 100 hours old).

* Enclosure 5.13 is the correlation factor per Reference 2.13 x

$$2.83E4\ \frac{ml}{ft^3} \times \frac{min}{60\ sec} \times \frac{Ci}{1E6\ \mu Ci}$$

INSTHUCTIONS ON HOW TO OBTAIN DATA FROM THE OPERATOR AID COMPUTER OAC

1) ***Tech Spec 04 Program (Plant Data and Status Summary)***

   a) At the OAC in the TSC or Computer Room, press [Tech Spec] 04

   b) Then press [Print] and [Enter]

   c) The report will print out

2) ***General 19 Program (Main Steam Release Program)***

   a) At the OAC in the TSC or Computer, Room press [General] 19

   b) Then press [Print] and [Enter]

   c) Using the arrow pointer keys, highlight "Main Steam Release" and press enter.

   d) The report will print out

INTEGRATED DOSE CALCULATION

Duration (hrs)										
L										
B										
M										
C										
N										
A										
D										
O										
R										
E										
G										
H										
I										
J										
K										
P										
Q										
S										

Instructions:

1) Add the doses from previous releases to the projected release.

2) Add the times of previous releases to the time of the projected release.