

South Carolina Electric & Gas Company Virgil C. Summer Nuclear Station P O. Box 88 Jenkinsville, SC 29065 803) 345-5209

> July 11, 1995 RC-95-0185

Mr. S. Dembek Project Directorate II-1 Division of Reactor Projects - I/II Office of Nuclear Reactor Regulation Mail Stop 14820 (OWFN) U. S. Nuclear Regulatory Commission Washington, DC 20555

Dear Mr. Dembek:

Subject:

VIRGIL C. SUMMER NUCLEAR STATION

**DOCKET NO. 50/395** 

OPERATING LICENSE NO. NPF-12

AMENDMENT 95-02

FINAL SAFETY ANALYSIS REPORT (FSAR)

Per your phone conversation with Ms. Berley indicating that the previously transmitted FSAR Amendment 95-02 was destroyed prior to reaching your office, enclosed is a replacement set of FSAR Amendment 95-02 to the Final Safety Analysis Report (FSAR) for the Virgil C. Summer Nuclear Station. The remaining ten sets will be forwarded by copy of this letter to the Document Control Desk.

This FSAR Amendment is updated as of March 27, 1995; it constitutes the second update to the FSAR for 1995, including the required information in accordance with 10CFR50.71(e).

Please note that pages which are submitted as amendment numbers other than 95-02 are administrative in nature and do not constitute any technical changes.

If there are any questions, please contact Ms. Janis Berley at (803) 345-4248.

Very truly your:

R. M. Fowlkes

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**NUCLEAR EXCELLENCE - A SUMMER TRADITION!** 

# VIRGIL C. SUMMER NUCLEAR STATION FINAL SAFETY ANALYSIS REPORT - AMENDMENT 95-02 INSTRUCTION SHEET

This Instruction Sheet functions as a guide and checklist for inserting Amendment 95-02 into the Virgii C. Summer Final Safety Analysis Report. Please note that pages which are submitted as amendment numbers other than 95-02 are pages which have received corrections which are administrative in nature.

The following listed pages and figures of South Carolina Electric & Gas Company's Final Safety Analysis Report for the Virgil C. Sommer Nuclear Station are to be removed and replaced as indicated

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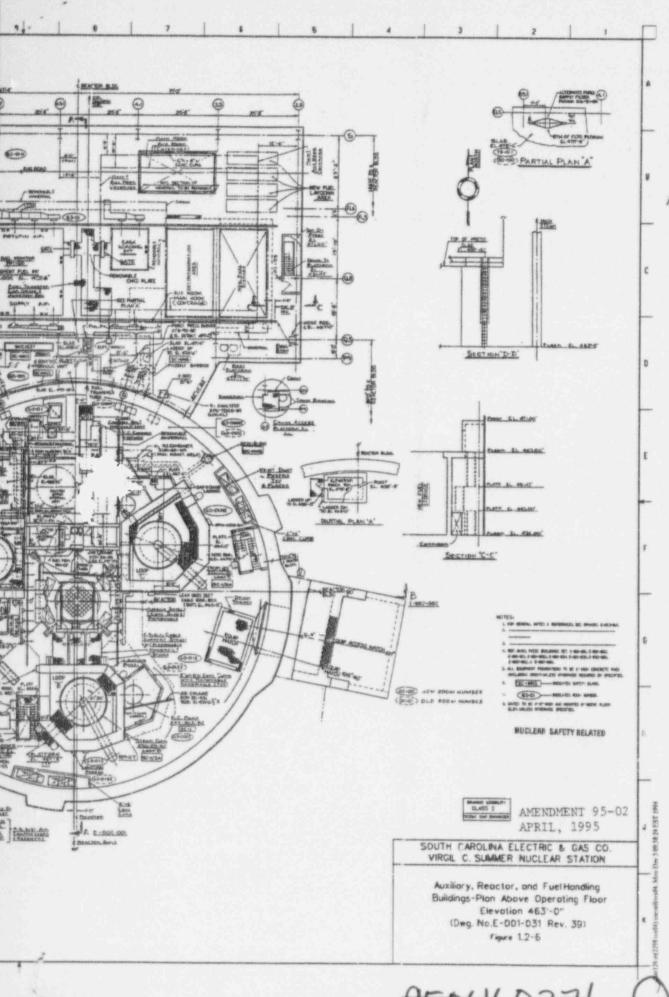
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### LIST OF EFFECTIVE PAGES (LEP)

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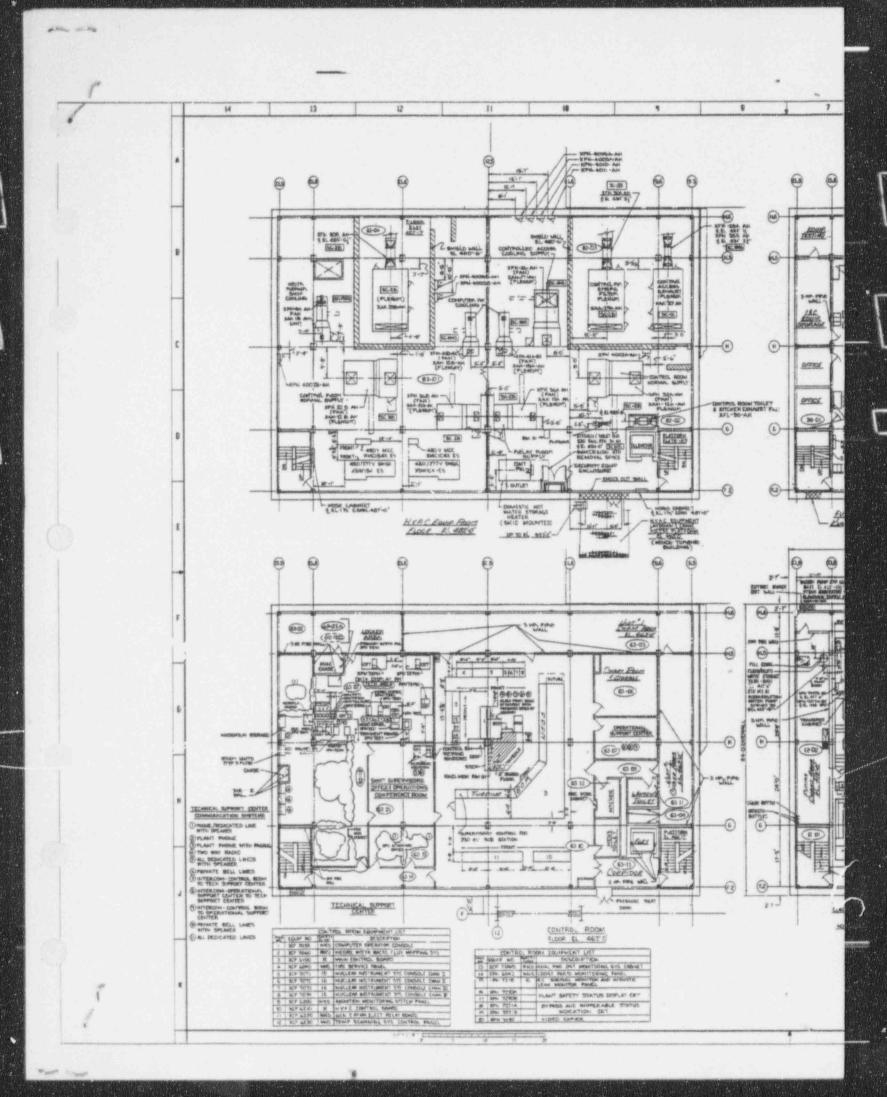
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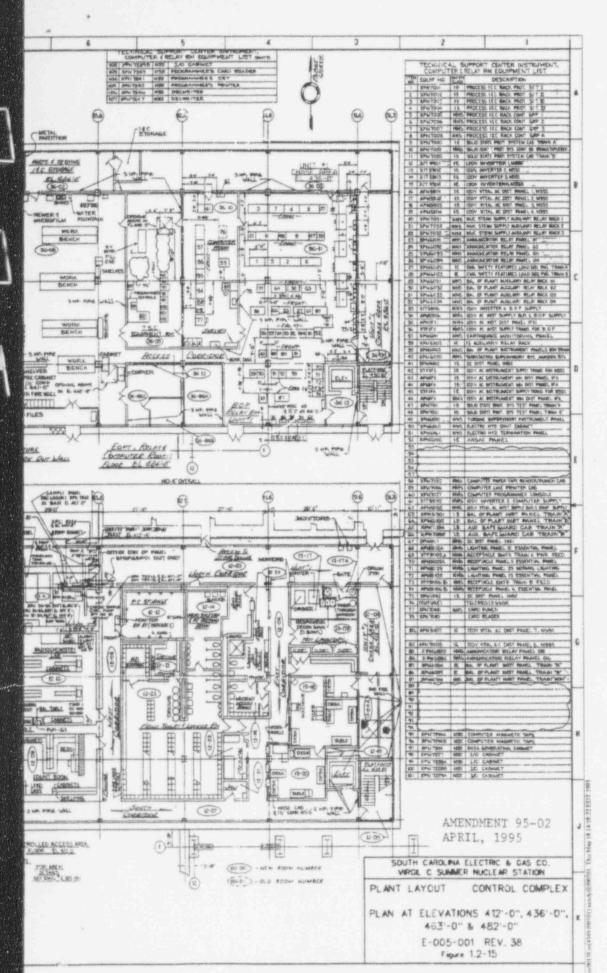
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# 5.5.7.3.3 Overpressurization Protection

Each inlet line to the RHRS is equipped with a pressure relief valve which protects the system from inadvertent overpressurization during plant cooldown or startup. Each valve has a relief flow capacity of 900 gpm at a set pressure of 450 psig. Analyses have been conducted to confirm the capabilty of the RHRS relief valve to prevent overpressurization of the RHRS. All credible events were examined for their potential to overpressurize the RHRS. These events included normal operating conditions, infrequency transients, and abnormal occurrences. The analyses confirmed that one relief valve has the capability to keep the RHRS maximum pressure within 10CFR50 Appendix G limits.

Each discharge line from the RHRS to the RCS is equipped with a pressure relief valve to relieve the maximum possible back-leakage through the valves separating the RHRS from the RCS. Each valve has a relief flow capacity of 20 gpm at a set pressure of 600 psig. These relief valves are located in the ECCS (see Figure 6.3-1).

The fluid discharged by the suction side relief valves is collected in the pressurizer relief tank. The fluid discharged by the discharge side relief valves is collected in the recycle holdup tanks of the boron recycle system.

# 5.5.7.3.4 Prevention of Exposure of the RHRS to Normal RCS Operating Pressure

The design of the RHRS includes two motor-operated gate isolation valves in series on each inlet line between the high pressure RCS and the lower pressure RHRS. They are closed during normal operation and are only opened for residual heat removal and RCS cold overpressure protection during a plant cooldown after the RCS pressure is reduced to approximately 425 psig or lower and the RCS temperature is reduced to approximately 350°F. During a plant startup the inlet isolation valves are shut after drawing a bubble in the pressurizer and prior to increasing RCS pressure above 425 psig. Power to the isolation valves is manually locked out during normal operation.

The two inlet isolation valves in each residual heat removal subsystem are independently and diversely interlocked with pressure signals to prevent their being opened whenever the RCS pressure is greater than approximately 425 psig. The autoclosure interlock of these valves has been removed as per WCAP-11835. An alarm has been added to alert the operator if the valves are not closed when the RCS pressure increases above the alarm 520 psig setpoint.

The use of two independently powered motor-operated valves in each of the two inlet lines, along with an independent and diverse pressure interlock to prevent them from being opened, and a RCS pressure high with RHR suction. Valves not closed alarm assures a design which meets applicable single failure criteria. Not only more than one single failure, but also different failure mechanisms, must be postulated to defeat the function of preventing possible exposure of the RHR system to normal RCS operating pressure. This protective interlock design, in combination with alarm, administrative controls and plant operating procedures, provide the means for accomplishing the protective function. For further information on the instrumentation and control features, see Section 7.6.2.

The RHR inlet isolation valves are provided with red-green position indicator lights on the main control board and a ESF monitor light for proper valve position. ESF monitor light is independent and diverse from valve position indication.

Isolation of the low pressure RHRS from the high pressure RCS is provided on the discharge side by two check valves in series. These check valves are located in the ECCS and their testing is described in Section 5.2.2.4.

#### 5.5.7.3.5 Shared Function

The safety function performed by the RHRS is not compromised by its normal function which is normal plant cooldown. The valves associated with the RHRS are normally aligned to allow immediate use of this system in its engineered safety features mode of operation. The system has been designed in such a manner that two redundant flow circuits are available, assuring the availability of at least one train for safety purposes.

The normal plant cooldown function of the RHRS is accomplished through a suction line arrangement which is independent of any safety function. The cold leg cooldown return lines are arranged in parallel redundant circuits and are utilized also as the low head injection lines to the RCS. Utilization of the same return circuits for cold leg cooldown lends assurance to the proper functioning of these lines for engineered safety features purposes.

#### 5.5.7.3.6 Radiological Consideration

The highest radiation levels experienced by the RHRS are those which would result from a loss of coolant accident. Following a loss of coolant accident, the RHRS is used as part of the ECCS. During the recirculation phase of emergency core cooling, the RHRS is designed to operate for up to a year pumping water from the reactor building sump, cooling it, and returning it to the reactor building to cool the core.

Since, except for some valves and piping, the RHRS is located outside the reactor building, most of the system is not subjected to the high levels of radioactivity in the reactor building post-accident environment.

## LIST OF EFFECTIVE PAGES (LEP)

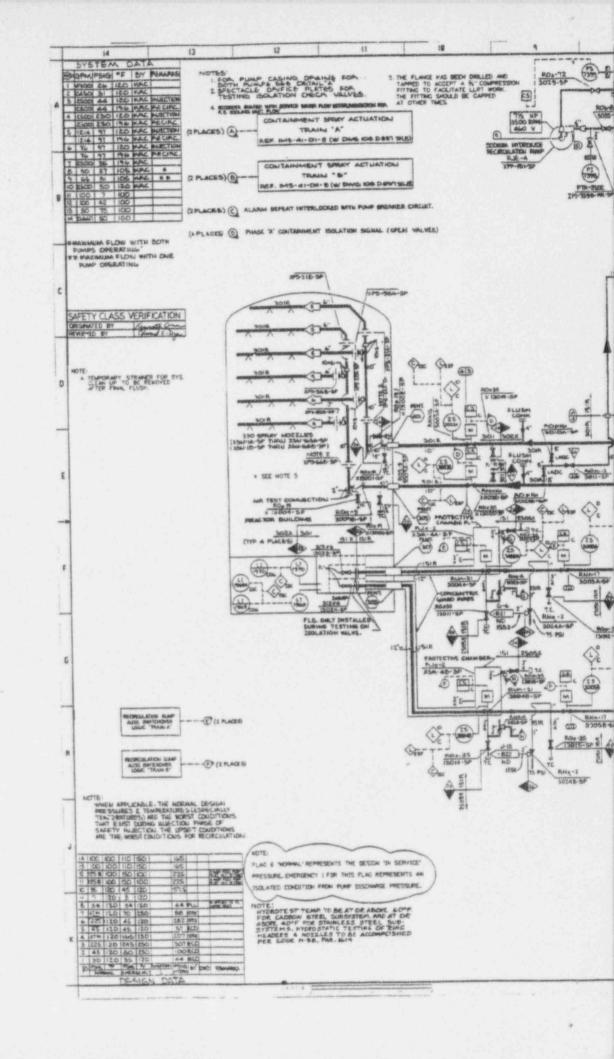
The following list delineates pages to Chapter 6 of the Virgil C. Summer Nuclear Station Final Safety Analysis Report which are currently in effect. The latest changes to pages and figures are indicated below by Amendment 94-09 in the Amendment column along with the amendment number and date for each page and figure included in the Final Safety Analysis Report.

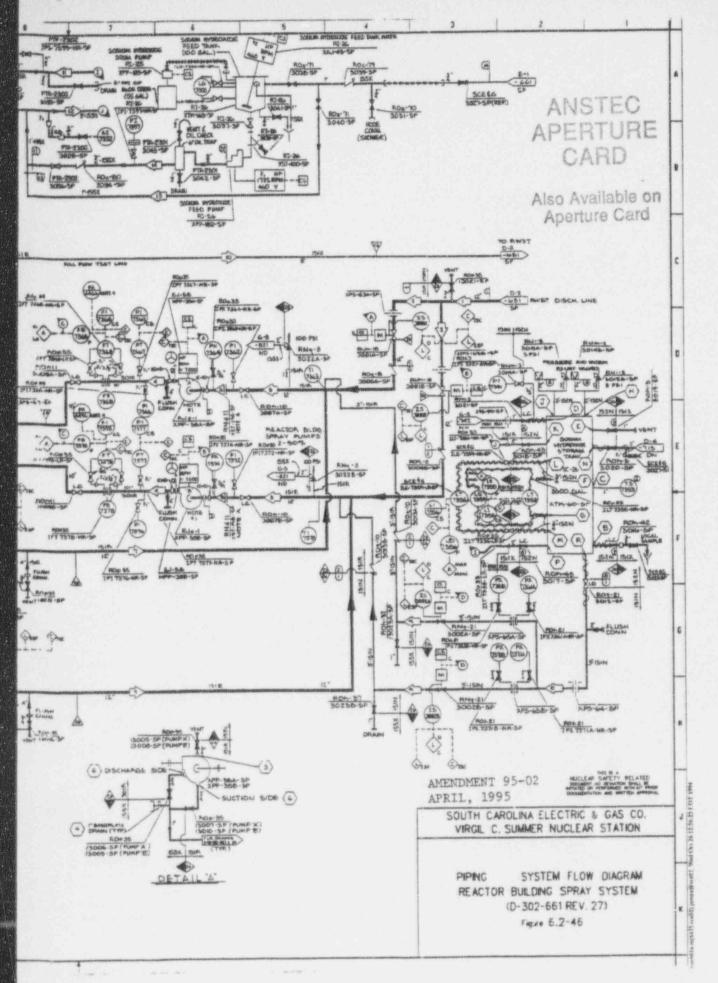
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The following list delineates pages to Chapter 7 of the Virgil C. Summer Nuclear Station Final Safety Analysis Report which are currently in effect. The latest changes to pages and figures are indicated below by Amendment 94-08 in the Amendment column along with the amendment number and date for each page and figure included in the Final Safety Analysis Report.

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# 7.7.3 TECHNICAL SUPPORT COMPLEX (TSC)

### 7.7.3.1 Description

In response to the recommendations issued post-TMI (e.g., NUREG-0578, NUREG-0585), South Carolina Gas and Electric will incorporate into the Virgil Summer Nuclear Power Plant a Technical Support Complex (TSC). This complex will improve the information available to operating and technical personnel. The 3 elements of the TSC are:

- ON-SITE Technical Support Center (OSTS).
- 2. Bypass and inoperable Status Indication (BISI)
- 3. Safety Parameter Display System (SPDS)

The ON-SITE Technical Support Center is at a location adjacent to but separate from the control room. Key plant information can be displayed in and transmitted from the OSTS to those technical personnel who are responsible for engineering support during post accident recovery. The center has the capability to receive, process, and display analog and digital signals from both the NSSS and BOP parts of the plant.

Bypass and Inoperable Status Indication provides the operator with a clear indication of the availability of plant safety systems. It provides the operator and OTSC personnel with a continuous systems level indication of bypasses or inoperable status of the systems comprising the Engineered Safety Features.

The purpose of the safety parameter display system (SPDS) is to assist operating personnel in evaluating the safety status of the plant. The SPDS provides a continuous indication of plant parameters or derived variables which are representative of the safety status of the plant during both normal and emergency use. The primary function of the SPDS is to aid in the rapid detection of abnormal operating conditions. Secondary functions include analyzing and diagnosing the abnormality, and providing an informational basis for corrective action execution.

The TSC is located in the Control Building, elevation 463'0", separate from but next to, the control room and is capable of accommodating a minimum of 25 persons (see Figure 1.2-15). Access to the control room is available through connecting doors between the TSC and the control room. Print storage and plant information will be available in the TSC. The TSC contains the following areas:

- Data Display Room This contains the communications and monitoring equipment necessary to provide the engineering and management support functions during an accident condition. The Communications, monitoring, and display equipment in this area includes:
  - Communications Network including plant telephones, dedicated lines to external parties, and radio systems.

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- SCE&G Co. Technical Area Office and communications facilities for SCE&G assigned personnel.
- 3. NRC Office Office and communications for five (5) NRC assigned personnel.
- 4. Operations Conference Room Conference Room facilities.
- 5. Westinghouse Office Office and communications facilities for plant personnel to communicate with Westinghouse.
- GAI Office Office and communications facilities for plant personnel to communicate with GAI.

The TSC is habitable to the same environmental conditions as the control room for postulated accident conditions. (The TSC has the same air supply and exhaust system as the control room, (see Section 9.4.1).

Installed radiation monitors (RM-G1 and RM-A1) will detect direct radiation and airborne radioactive contaminants for both the control room and the TSC. The monitors will alarm when high radiation levels are being approached. SCE&G Co. has established in the plant's emergency procedures the necessary precautionary protective measures to be taken for high levels of radiation.

# 7.7.3.2 Analysis

- The TSC is located on elevation 463'0" of the Control Building, which is a Seismic Category I structure.
- The environmental conditions within the TSC are the same as those in the control room.
- Installed radiation monitors (RM-G1 and RM-A1) will detect direct radiation and airborne radioactive contaminents for both the control room and the TSC. The monitors will alarm when high radiation levels are being approached.
- Equipment within the TSC is designed to assure reliability in the recovery of data.
- 5. The TSC and equipment located in the TSC are not required to initiate actuation of safety related systems. Loss of the TSC or any equipment within the TSC will not prevent safe shutdown of the plant.

# 7.7.4 CRITICAL SYSTEMS LEAK MONITORING SYSTEM

# 7.7.4.1 Description

An acoustical type leak monitoring system is provided to detect through the wall and valve seat leakage. Sensors for this system are located in the following locations:

a. Downstream of the pressurizer safety valves

- b. Downstream of the reactor vessel head vent valves
- c. On the feedwater lines to the steam generator
- d. On the emergency feedwater lines to the steam generator.

The sensors for the system are located inside the reactor building, with all conditioning components located outside.

A leak through a valve seat generates metal borne acoustic waves which are detected by acoustic transducers mounted on the piping adjacent to the valves. The transducers convert the acoustic waves into electrical signals which are amplified and then transmitted to the leak detection system.

The control room is provided with indication which relates to the size of the leak and an alarm which alerts the operator of the occurrence of a leak. The system is provided with multiple sensors to enable the plan operator to determine which pressurizer safety valve or reactor vessel head vent valve is open. Multiple sensors also aide in determining the approximate location of a through wall leak in the feedwater or emergency feedwater lines to the steam generators.

#### 7.7.4.2 Analysis

The critical systems leak monitoring system is powered from a vital instrument bus. The system will be qualified to IEJE 323 and IEEE 344. Seismic and environmental qualification is discussed in Section 3.10 and 3.11, respectively.

#### 7.7.5 REACTOR VESSEL LEVEL INSTRUMENTATION SYSTEM

This section deleted by Amendment 4.

## 7.7.6 CORE SUBCOOLING MONITOR

This section deleted by Amendment 1, August 1985.

# 7.7.7 REFERENCES

- Lipchak, J. B. and Stokes, R. A., "Nuclear Instrumentation System," WCAP-8255, January, 1974.
- "Calculation of Distance Factors for Power and Test Reactor Sites,"
   J. J. Dinunno, et. al, U. S. Atomic Energy Commission, Washington,
   D. C., March, 1962.

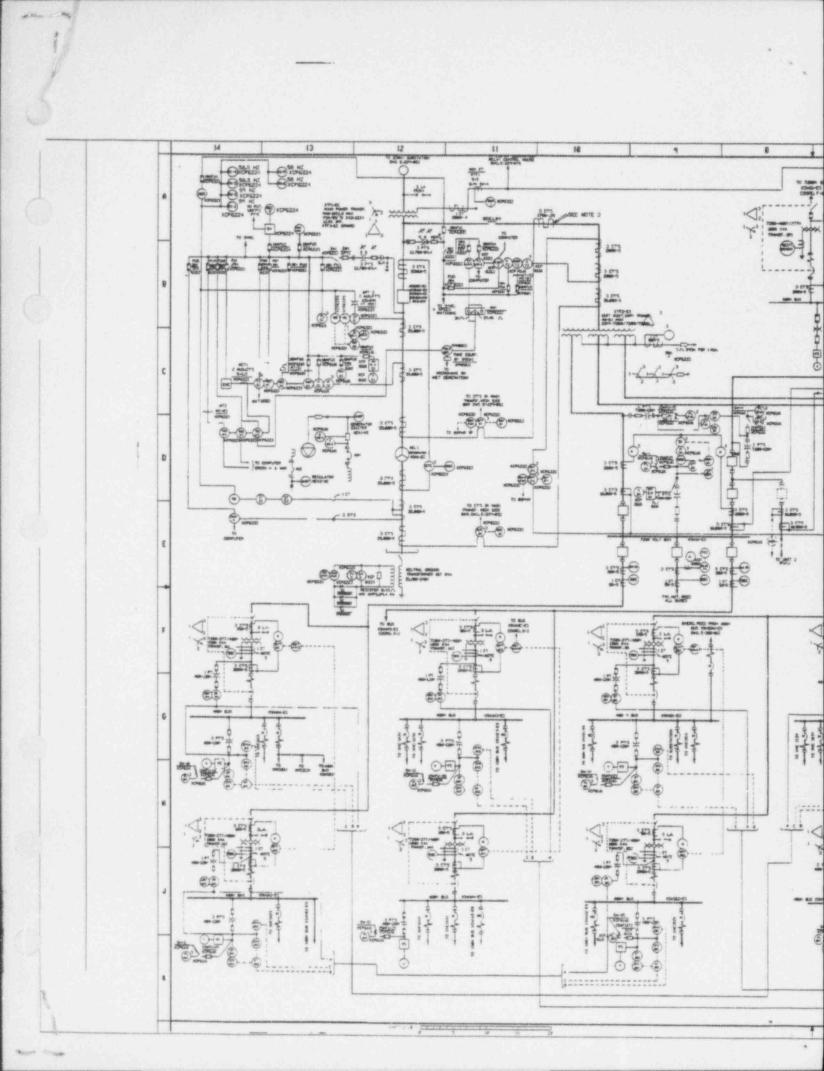
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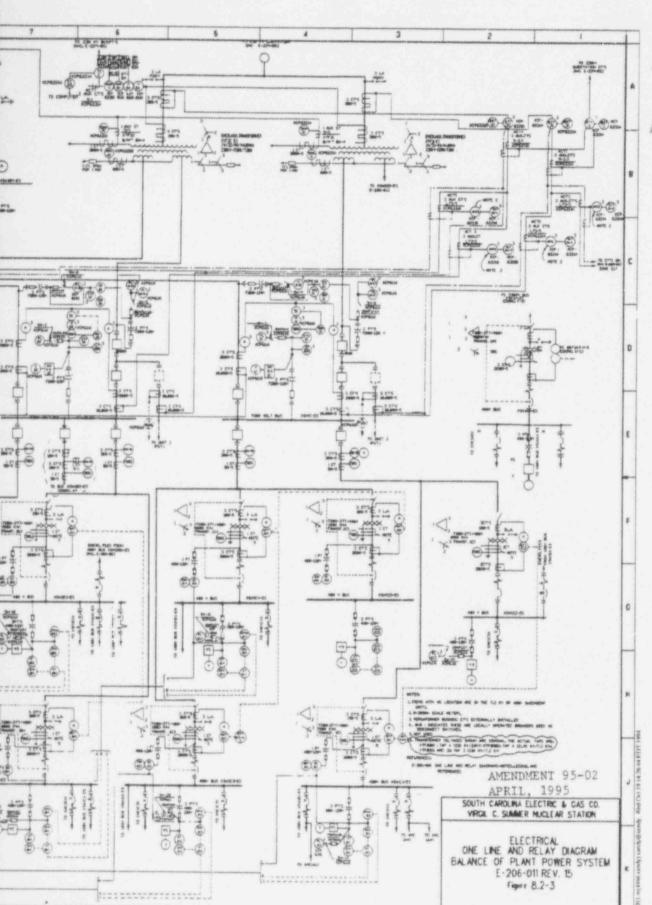
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## LIST OF EFFECTIVE PAGES (LEP)

The following list delineates pages to Chapter 8 of the Virgil C. Summer Nuclear Station Final Safety Analysis Report which are currently in effect. The latest changes to pages and figures are indicated below by Amendment 94-05 in the Amendment column along with the amendment number and date for each page and figure included in the Final Safety Analysis Report.

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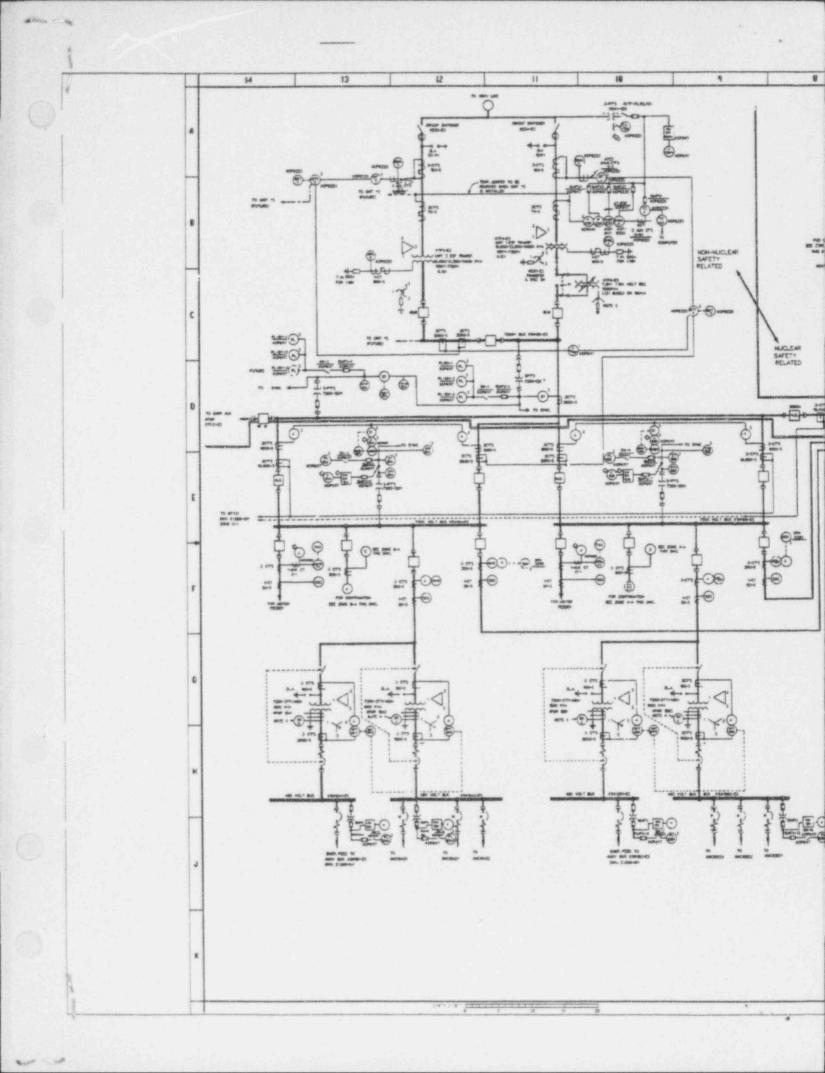


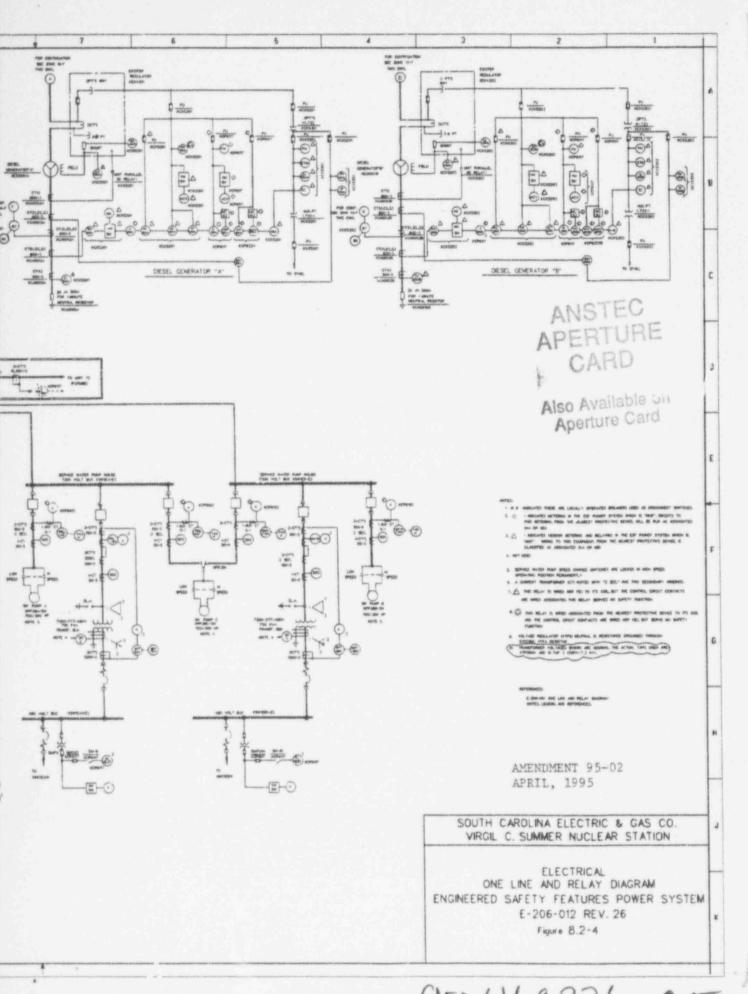


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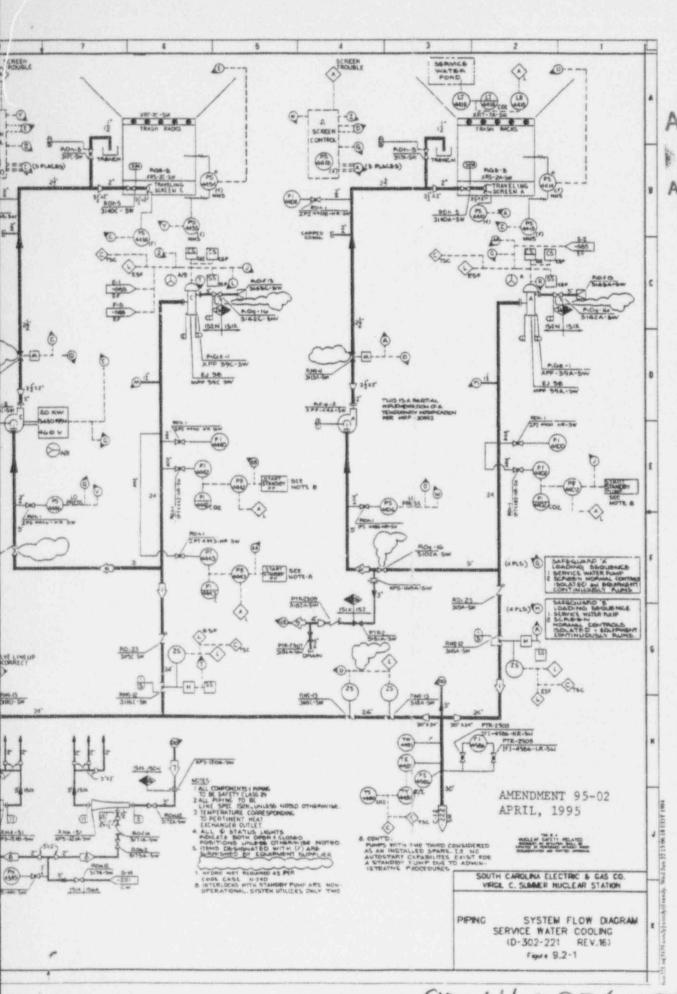
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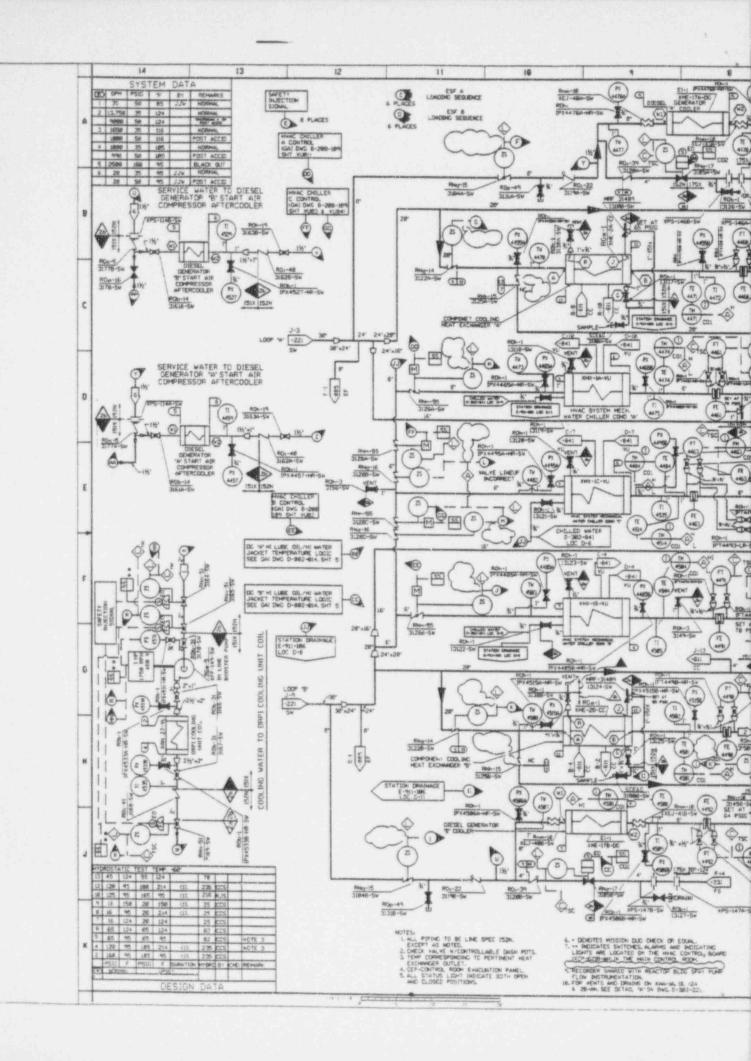
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Page 9.5-29	0	Aug. 1984			
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9.5-31 Fig. 9.5-1	95-02	Aug. 1984 Apr. 1995			
9.5-1a	5	Aug. 1989			
9.5-1b	93-10	Dec. 1993			
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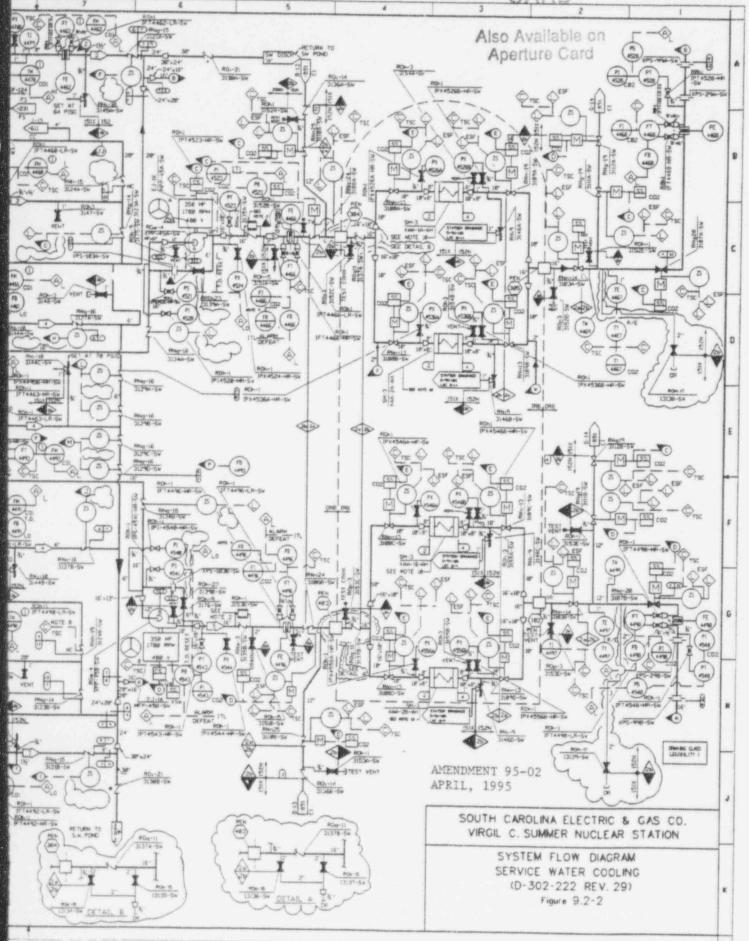
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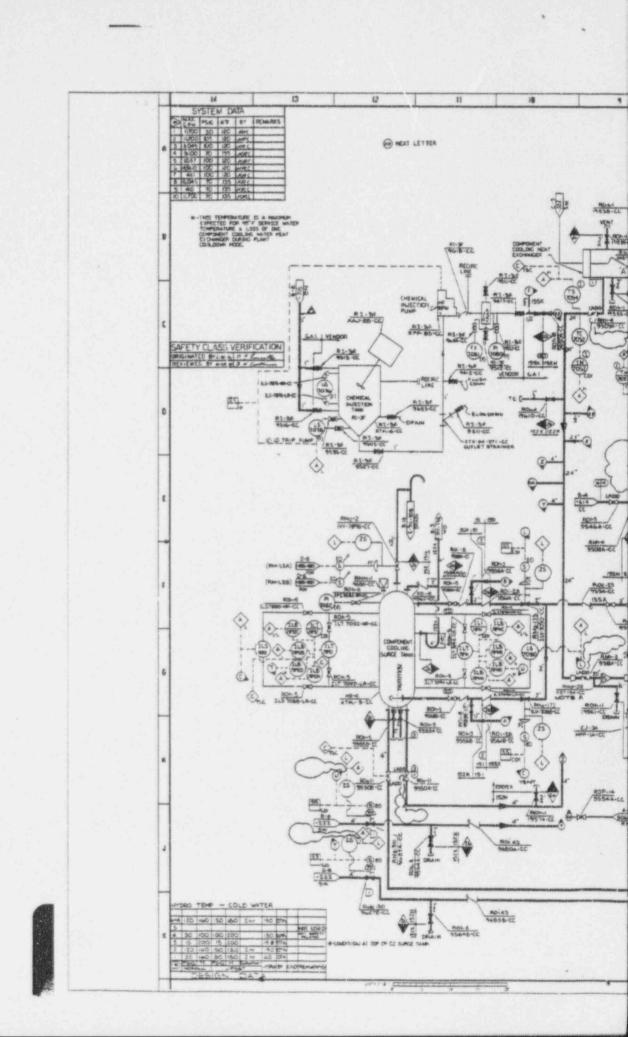
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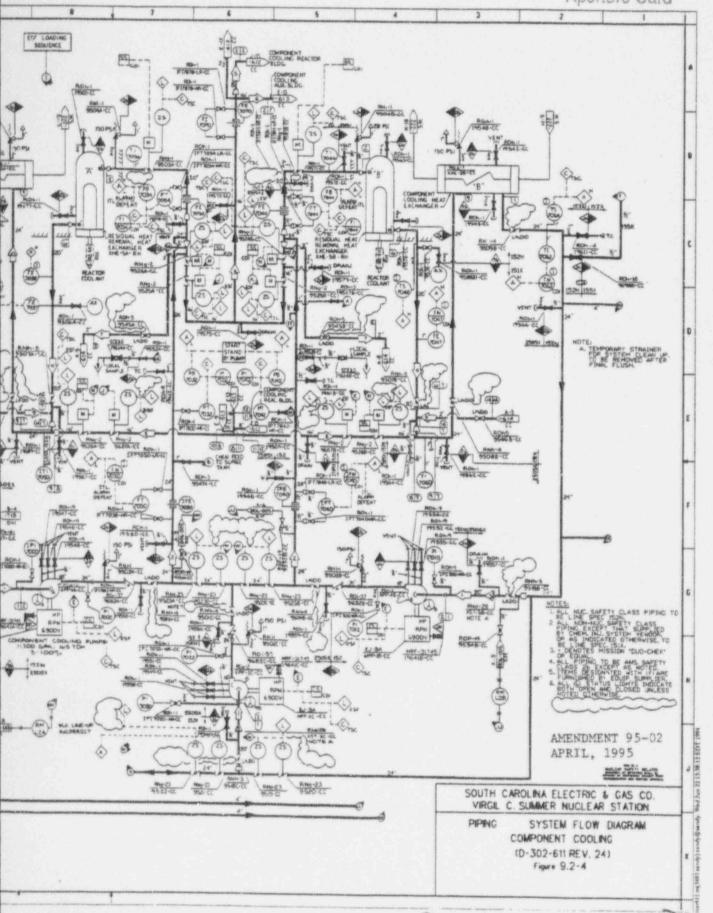
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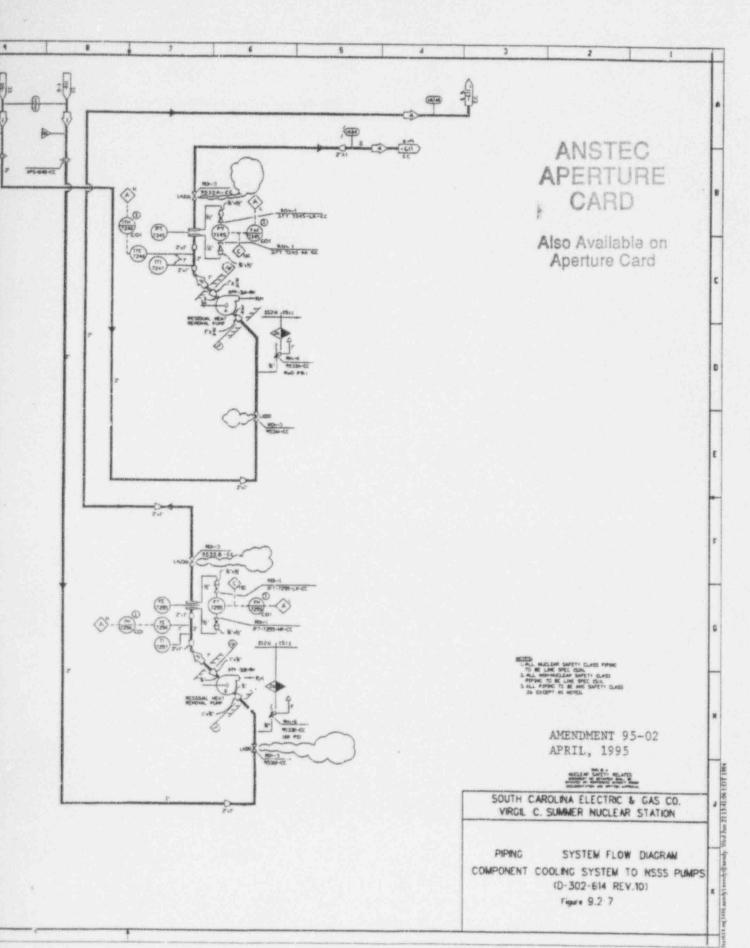
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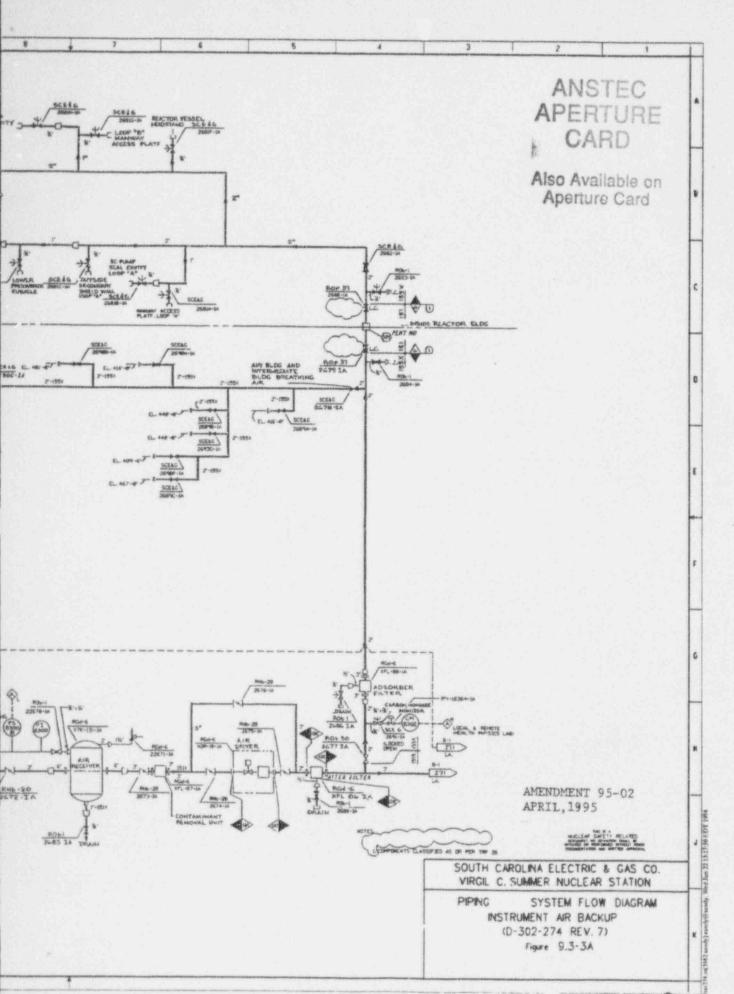
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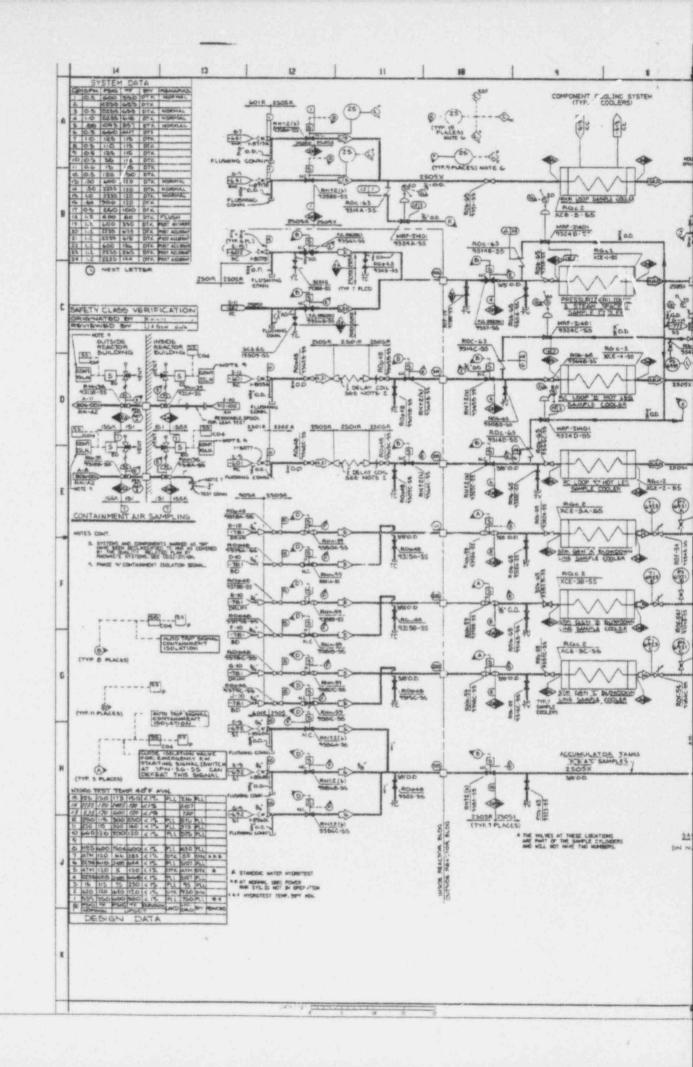
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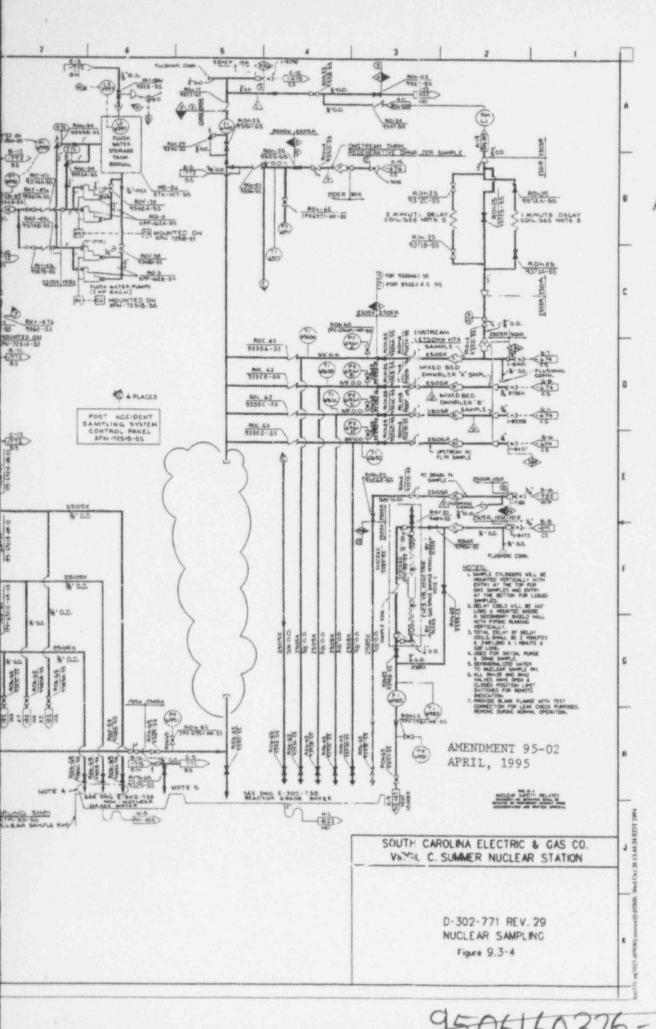
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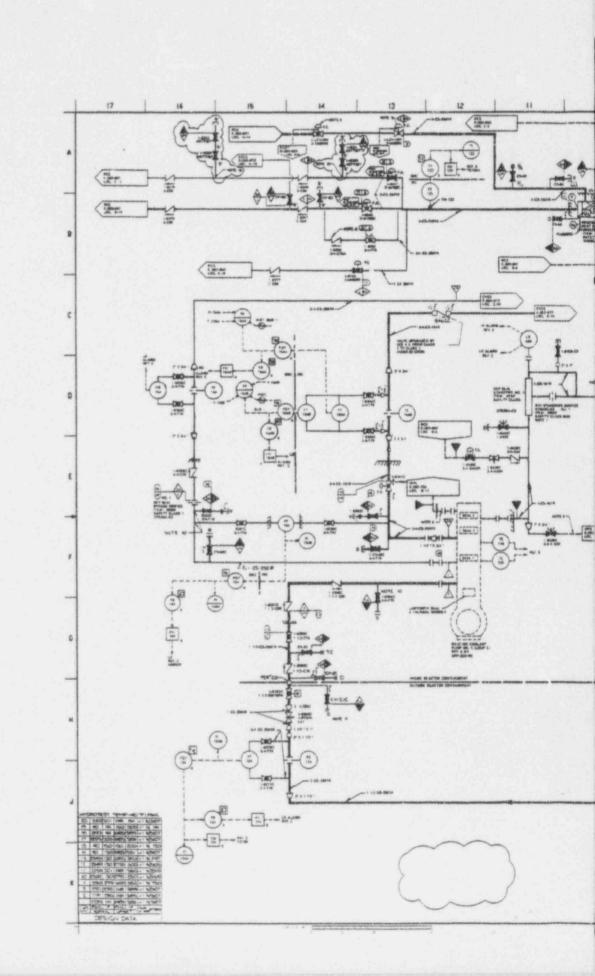




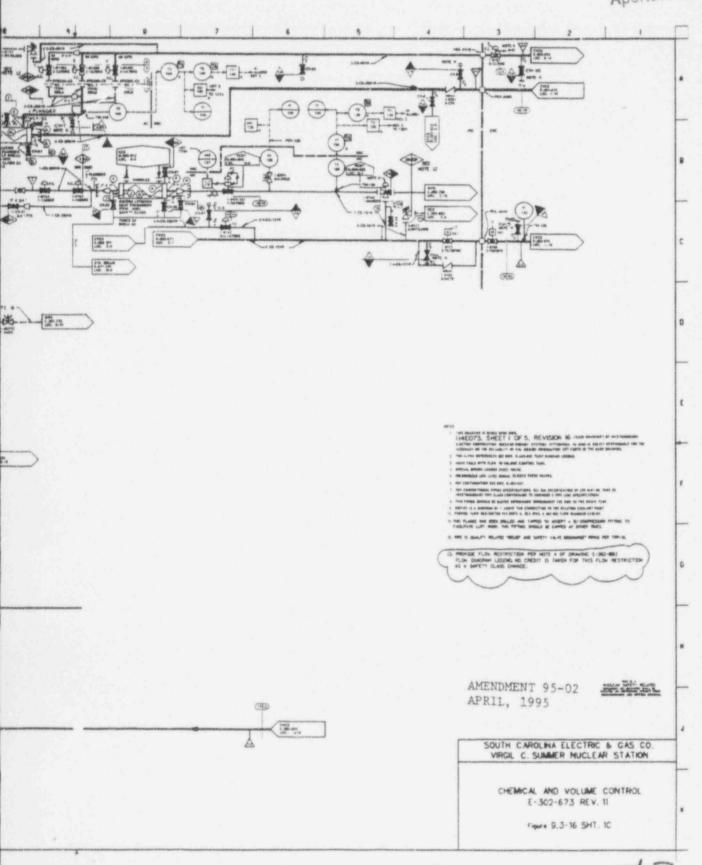


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- Two laboratory hood exhaust fans and a chemical storage area exhaust fan.
- Twelve electric unit heaters in the chemical storage and general floor areas.
- Ductwork connecting the air handling unit with the sample room and the water treating laboratory and for supply and exhaust of the laboratory hoods.
- 5. Instrumentation and control devices to perform the following functions:
  - a. Automatically operate the condensing unit and the air handling unit heating coil in response to a room thermostat.
  - b. Automatically place the outside, return and relief dampers under control of the outside and return mixture temperature controller or at a fixed minimum position in accordance with outside temperature.
  - Automatically prevent or permit the condensing unit to operate in accordance with outside temperature.
  - Control electric unit heaters with integral thermostats.
  - e. Automatically close hood inlet dampers when the entering air is below a set temperature.

The air handling unit operates continuously. The laboratory hood and chemical storage area exhaust fans are operated as required from local control stations. System components are supplied from non-Class 1E power sources.

#### 9.4.7.2.10 CRDM Cooling Water System

The main components of this system include:

- One CRDM cooler rack assembly which is an air to water heat exchanger.
- One CRDM cooling water industrial cooler, including two electric heaters, eight forced convection fans, and four circulation pumps.
- One expansion tank to control thermally induced water volume changes.
- Two 100% circulating water pumps, including a bypass line with a chemical feed tank.
- Four motor operated containment isolation valves, including two cneck valves on bypass lines on the Reactor Building Side.

The system is designed to remove heat from the containment air used to cool the Control Rod Drive Mechanism (CRDM) and dissipate this heat to the atmosphere via the Industrial Cooler.

The system can operate continuously while the plant is in operation. System components are powered from non-Class IE power sources, except for the motor operators on the containment isolation valves, which are supplied from the Class IE power sources.

#### 9.4.7.2.11 Turbine Building Switchgear Rooms Chilled Water System

The main components of this system include:

- 1. One air-cooled, electric motor drive, reciprocating water chiller.
- One primary water pump.
- 3. Two 100% capacity secondary water pumps.
- Chilled water piping system including a compression tank, an air separator, a chemical feed tank, and valves.
- Chilled Water Coils one coil in each of two redundant turbine building switchgear rooms air handling units. Each coil has two connections.
- 6. Instrumentation and control devices to perform the following functions:
  - a. Control the chiller. Included in a factory-furnished, factory-wired controls are a positive-acting timer to prevent short cycling of the compressors and to delay restart after shutdown, high and low pressure refrigerant safety pressurestats to stop the compressors, a multiple-step water temperature controller, a chilled water safety thermostat, circuit breakers, motor contactors, control relays, a control circuit ON-OFF switch, and a chilled water flow switch. The chiller is energized automatically when primary flow is established.
  - b. Control the primary pump. The pump is started by a remote manyal switch. The pump will shutdown on a chiller malfunction.
  - c. Control the secondary pumps. These pumps are redundant and each is wired to run only with its respective air handling unit. The active pump is controlled by one of three parallel-wired room thermostats.
  - d. Indicate locally the level of water in the compressor tank and alarm of low level in the control.
  - e. Alarm in the control room of low water flow.
  - f. Indicate locally the temperature of water entering and leaving the chiller and provide a computer high temperature alarm and CRT display in the control room of water leaving the chiller.
  - g. Indicate locally the pressure of water entering and leaving each pump.

Under normal conditions, the primary pump continuously circulates water in the primary pipe loop. This water is maintained at 45°F by the chiller which loads/unloads and cycles automatically under its self contained controls. The secondary pump circulates water between the primary loop and the chilled water coils identified in Section 9.4.4.2.1, subitem 4. It cycles upon demand of room thermostats.

Additionally, this system can provide chilled water to the CRDM Switchgear Room cooling coils via a booster pump in the event that chilled water is unavailable to these coils. This system can be provided chilled water from the non-nuclear safety related chilled water system. The system is non-nuclear safety class.

### 9.4.7.2.12 Non-nuclear Safety Related Chilled Water System

The main components of this system include:

- 1. One air-cooled, electric motor driven reciprocating water chiller.
- 2. Two 100% capacity chilled water circulating pumps.
- 3. One chilled water booster pump.
- Chilled water piping system including an atmospheric expansion tank, provisions for chemical sample and feed, and provisions for balancing the system.
- Chilled water cooling coils for the following areas:
  - a. CRDM Switchgear Room.
  - b. Controlled Access Area.
  - SAS/Computer Room.
  - d. Computer Room.
  - e. BOP Charger Area.
- 6. Instrumentation and control devices to perform the following functions:
  - a. Cause an alarm at a local panel and a common trouble alarm in the control room upon detection of either low chilled water flow, high chilled water temperature, or low expansion tank level.
  - b. Provide local indication of system flow.
  - c. Provide interlocks which shut the chiller down on low system flow.
  - d. Indicate water temperature locally at the pipe supply and return headers and at the inlet and outlet of each cooling coil.

- e. Provide thermowells for local testing in the supply and return headers at the chiller.
- f. Indicate water pressure locally at the suction and discharge of each pump.
- Provide the means for determining pressure drop across each system cooling coil.
- h. Provide local indication of expansion tank level.
- i. Provide a remote means for filling the system.
- Provide a local panel at the fill station to indicate "Normal," "Low," and "Fill Complete" expansion tank level with status lights.

Under normal conditions, the system provides chilled water via redundant circulating pumps to the cooling coils listed in Section 9.4.1.2.3, 9.4.1.2.4, 9.4.1.2.6, 9.4.6.2.1, and 9.4.6.2.3. The chiller loads/unloads and cycles automatically to maintain chilled water temperature at 45°F. This system can be aligned to provide a backup source of chilled water to the Turbine Building Switchgear Rooms cooling coils. In the event that chilled water is unavailable to the CRDM Switchgear Room cooling coils, the booster pump can be aligned to the Turbine Building Switchgear Rooms Chilled Water System to provide a backup source of cooling to the CRDM Switchgear Room.

## 9.4.7.3 Safety Evaluation

The service building ventilation system, industrial system, industrial cooling water system, substation relay house cooling system, penetration access areas ventilation system, miscellaneous pump room systems and lube oil room systems, water treating area laboratory heating and cooling system, and turbine building switchgear rooms chilled water system perform no safety function. The CRDM Cooling Water System performs no safety function except for the containment isolation valves where motor operators are supplied by Claus 1E power supplies. They do provide acceptable temperature levels in the various buildings.

Additionally, the substation battery room exhaust fan in the substation relay house cooling system prevents the occurrence of any appreciable hydrogen concentration in the battery room.

The diesel generator building ventilation system, service water pumphouse ventilation system, and chilled water system do perform safety functions since total loss of the heat removal capability of any one of these systems could produce conditions affecting the safety of the plant. These systems are designed with redundant equipment and piping systems and are so arranged, serviced, and maintained such that complete loss of system function or system cooling is highly unlikely. Each of the safety class systems is located in equipment rooms accessible for maintenance but not subject to floods, weather, external missiles, main steam line break effects, jet impingement,

#### TABLE 9.4-5 (Continued)

# DESIGN BASES FOR MISCELLANEOUS BUILDING VENTILATION AND COOLING SYSTEMS

System	System Function	Conditions Maintained	Safety	Seismic Category	
Chilled Water System	Provides continuous supply of chilled water to cooling coils for systems located in the control, auxiliary, intermediate, and turbine buildings.	Chilled water supplied at 45°F	2Ь		
Industrial Cooling Water System	Operates continuously when normal power is available to provide means for rejecting reactor building and boron thermal regeneration system heat loads.	85°F maximum discharge water temperature	NNS	None	
Substation Relay House Cooling System	Operates continuously to maintain relay room temperature and provide continuous exhaust of the substation battery room.	75°F	NNS	None	
Non-nuclear Safety Related Chilled Water System	Operates continuously when normal power is available to supply chilled water to cooling coils for systems located in the control and intermediate buildings.	Chilled water supplied at 45°F	NNS	None	

TABLE 9.4-6

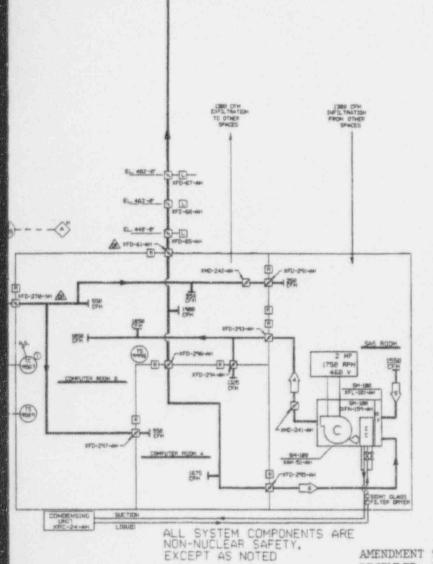
# REACTOR BUILDING COOLING AND FILTERING SYSTEMS FUNCTIONS, SAFETY CLASS AND SEISMIC CATEGORY

System	<u>Function</u>	Safety Class	Seismic Category
Reactor Building Cooling System	Normally: remove all reactor building heat, circulate cooled air to dome and into lower elevations. Post accident: depressurize and circulate.	<b>2</b> b	ľ
Reacto Building Purge Supply and Exhaust System	Supply tempered air to the reactor building and exhaust reactor building atmosphere through high efficiency filters to the purge exhaust vent.	NSS (2a for purge iso- lation valves only)	(plenums and purge isolation valves only)
Alternate Reactor Building Purge System	Supply filtered air to the reactor building and exhaust reactor building atmosphere through high efficiency filters to the purge exhaust vent.	NSS (2a for purge iso- lation valves only)	(purge iso- lation valves only)
Reactor Building Charcoal Cleanup System	Filter reactor building atmosphere for pre-access cleanup.	NNS	I (fans and plenums only)
Reactor Building Reactor Compart- ment Cooling System	Supply cooled air to the reactor compartment with resultant air flow around the vessel, nozzles, neutron detectors, and supports.	NNS	(fans only)
Reactor Building Secondary Compart- ment Cooling Sys- tem	Supply cooled air to the steam generators compartments.	NNS	None
Reactor Building Refueling Water Surface System	Maintain air flow across the refueling canal surface during refueling operations.	NNS	None
Reactor Building CRDM Shroud Cooling System	Draw cooled air through the shroud for heat removal.	NNS	1
Reactor Building Elevator Machine Room System	Draw air through the machine room for heat removal.	NNS	None

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- 5. COL. FACE DAMPERS FAIL OPEN AND COL. BYPASS DAMPERS FAIL CLOSED.
- 6. ALL EQUIPMENT IDENTIFIED AS OR TO BE PER TRP-3)

AMENDMENT 94-10 DECEMBER, 1994

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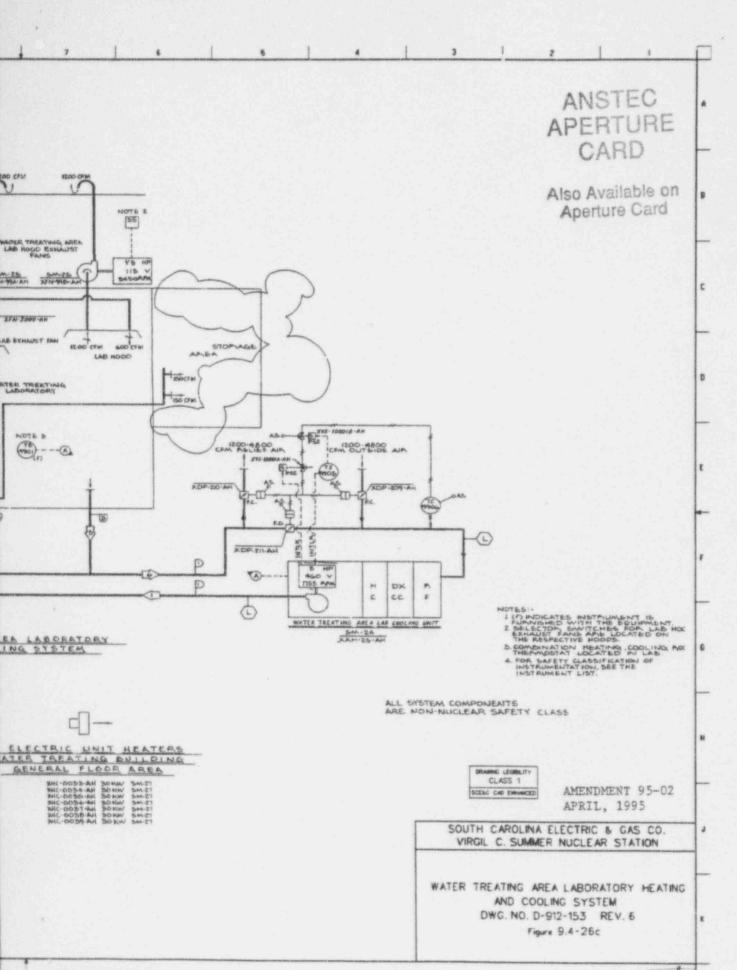
SOUTH CAROLINA ELECTRIC & GAS CO. VIRGIL C. SUMMER NUCLEAR STATION

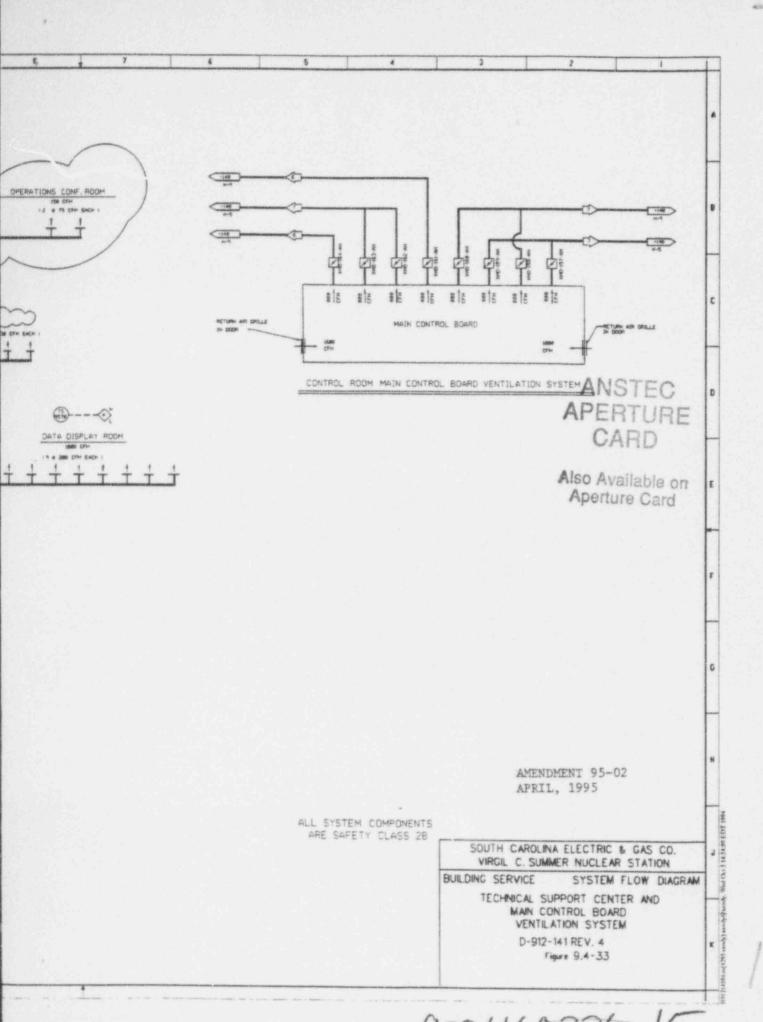
Building Service System Flow Diagram
Computer Rooms and SAS Room Cooling Unit
(Dwg. No. D-912-154 REV. 14)

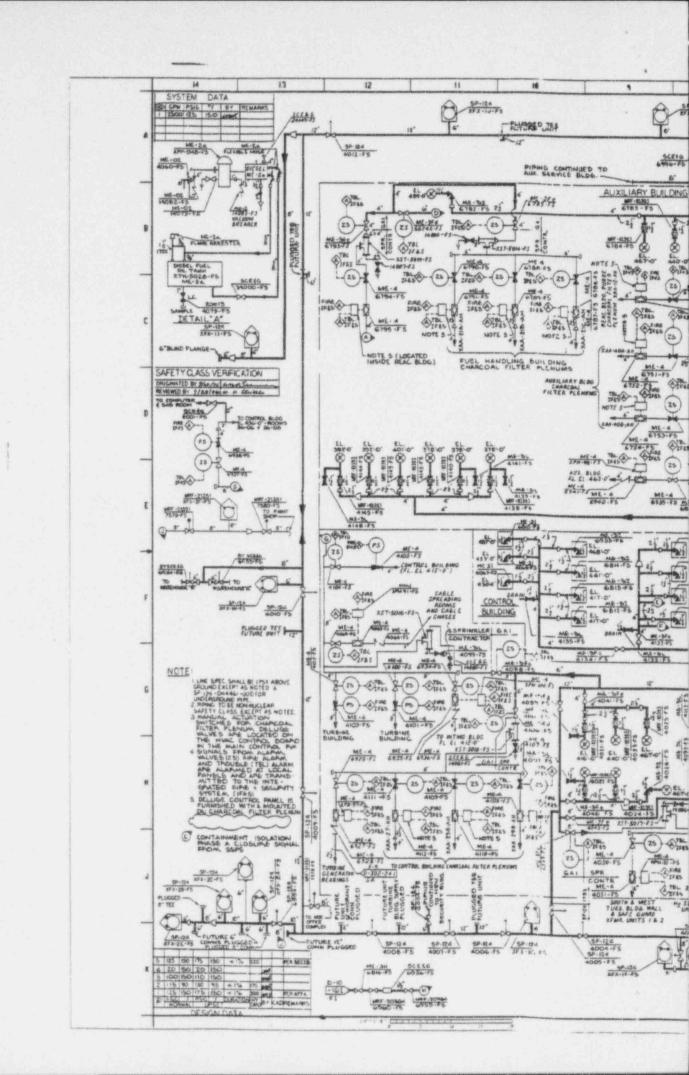
Figure 9.4-5

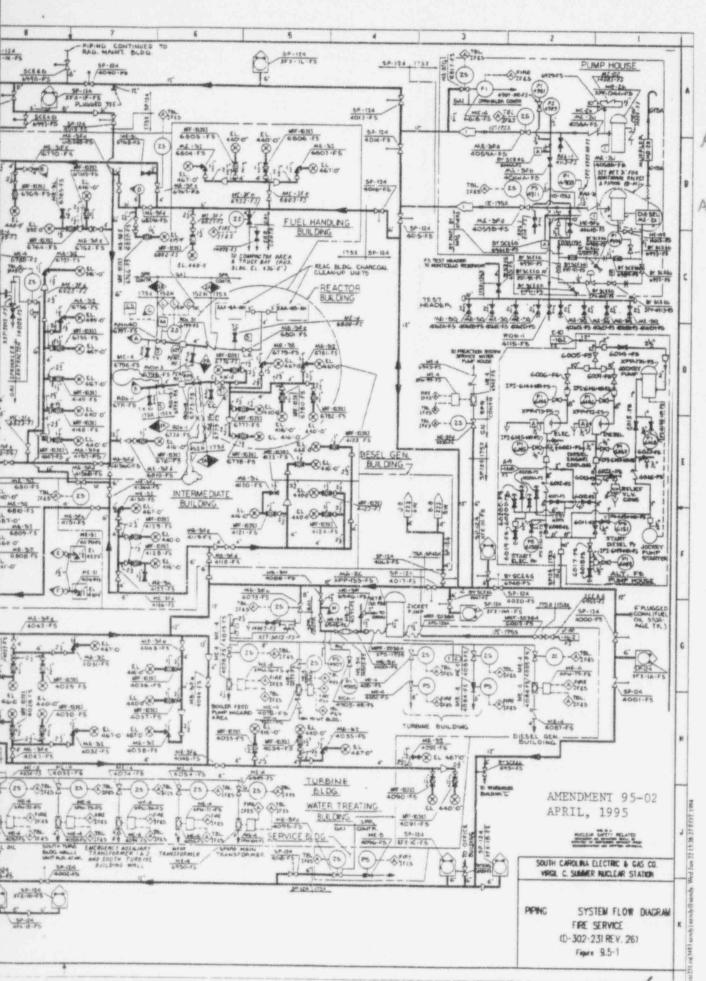
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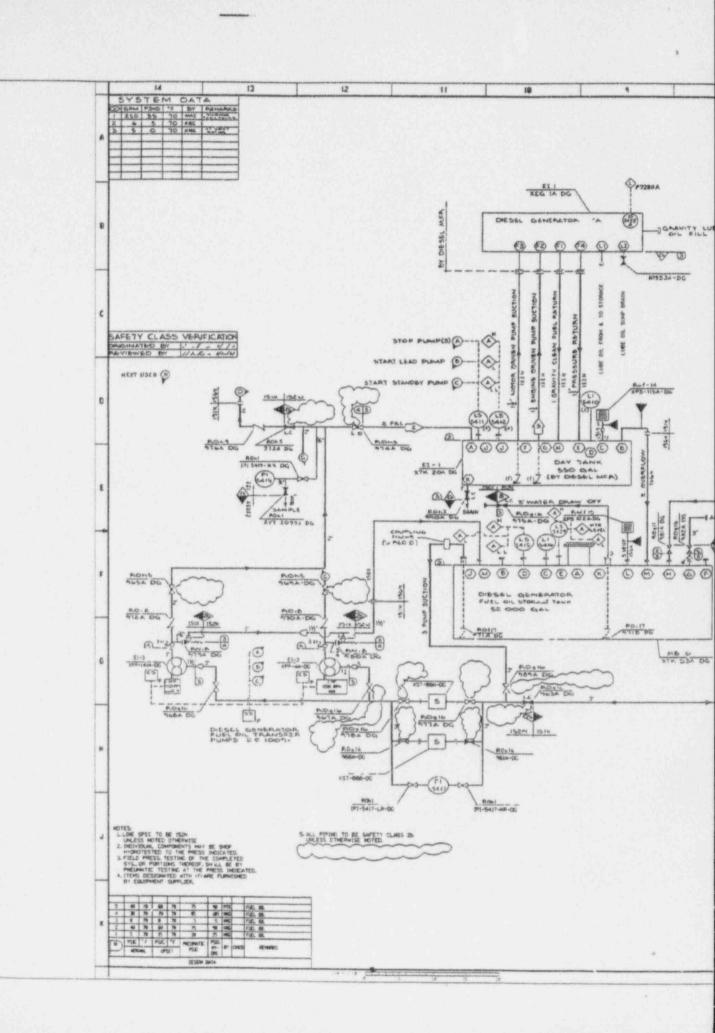


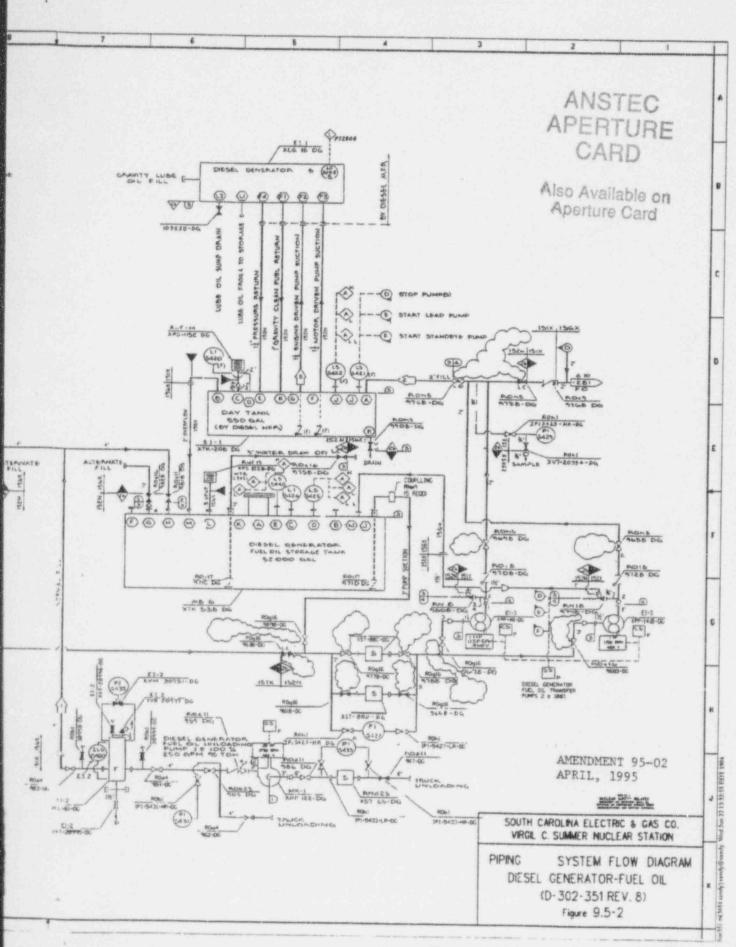


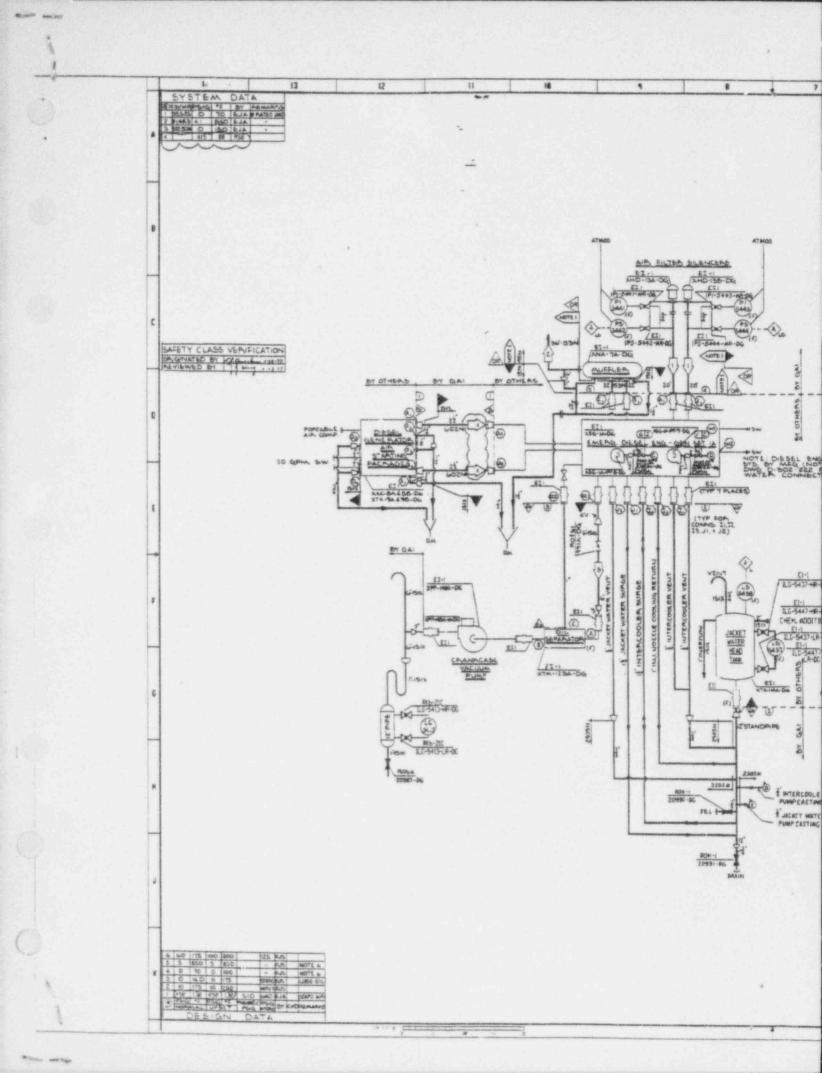


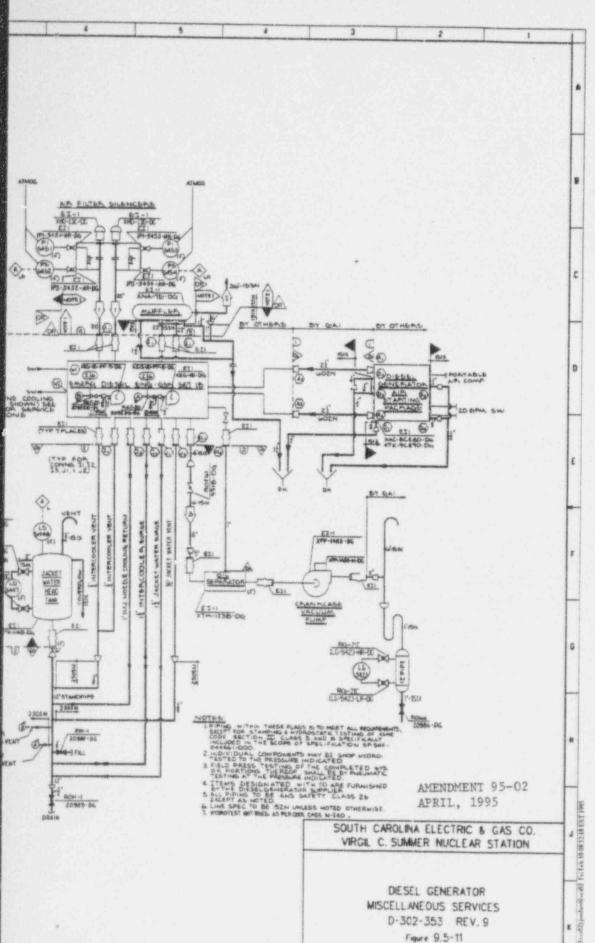


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Figure	<u>Title</u>
10.4-7	Circulating Water Cooling
10.4-7a	Condensate Polishing
10.4-8	Condensate
10.4-8a	Condensate Polishers Kidney Loop Operation
10.4-9	Condensate - Auxiliary Condensers and Blowdown Heat Exchangers
10.4-10	Feedwater (Non-Nuclear)
10.4-11	Feedwater (Non-Nuclear)
10.4-12	Feedwater (Nuclear)
10.4-13	Steam Generator Blowdown
10.4-14	Nuclear Blowdown Processing System Holdup Tank and Demineralizers
10.4-15	Nuclear Blowdown Processing System Spent Resin Storage Tank
10.4-16	Emergency Feedwater (Nuclear)
10.4-17	Liquid Effluents from Nuclear Plant to Fairfield Penstocks

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The following list delineates pages to Chapter 10 of the Virgil C. Summer Nuclear Station Final Safety Analysis Report which are currently in effect. The latest changes to pages and figures are indicated below by Amendment 94-10 in the Amendment column along with the amendment number and date for each page and figure included in the Final Safety Analysis Report.

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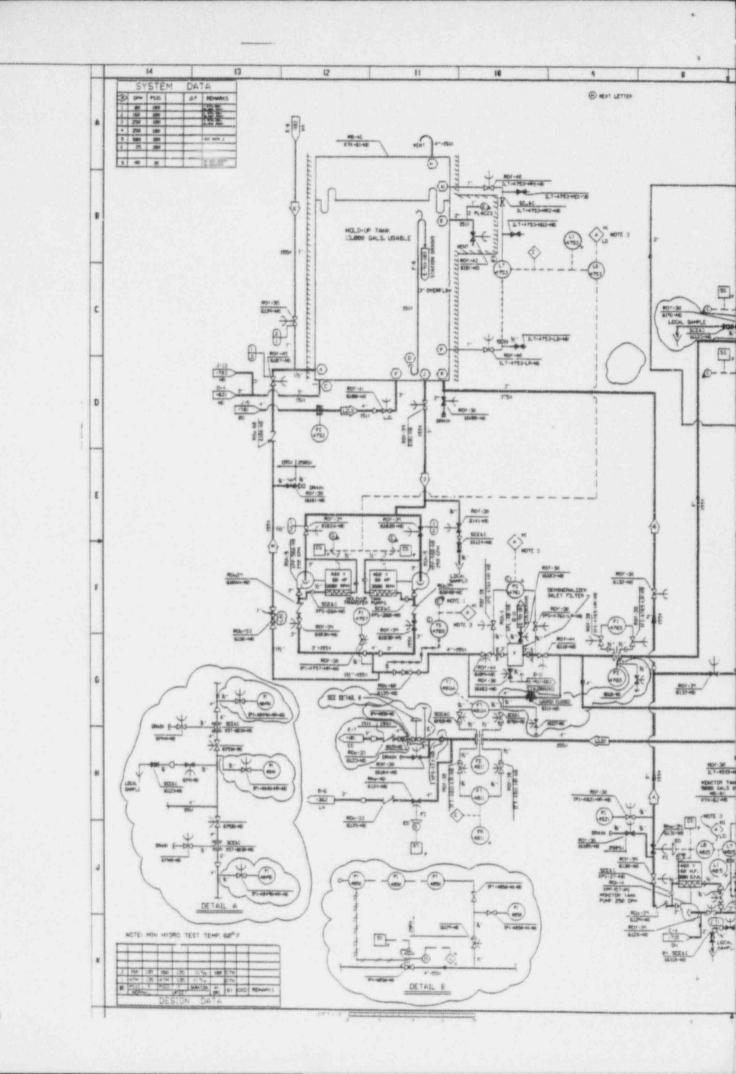
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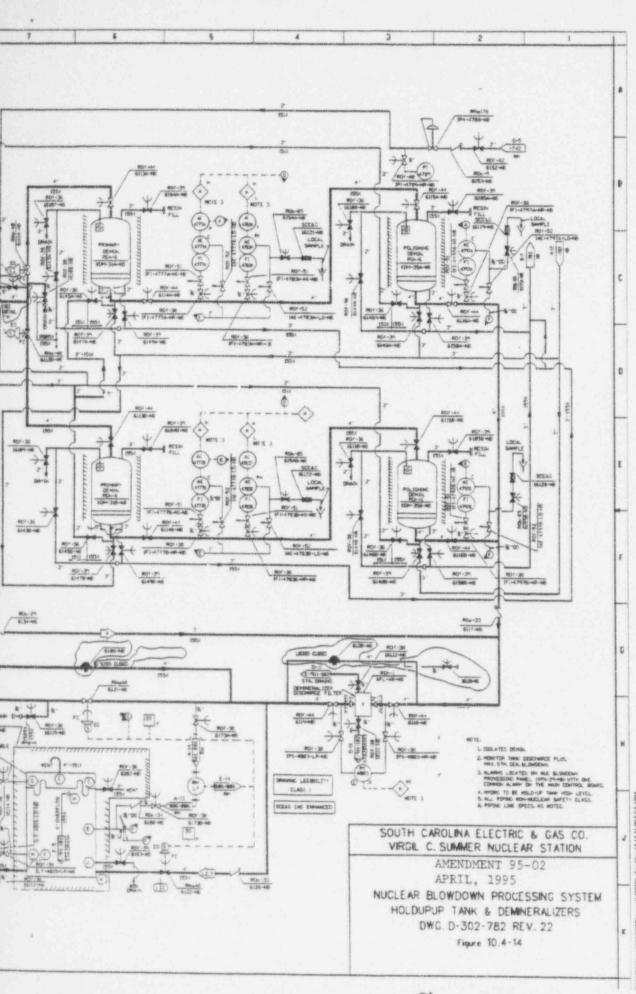
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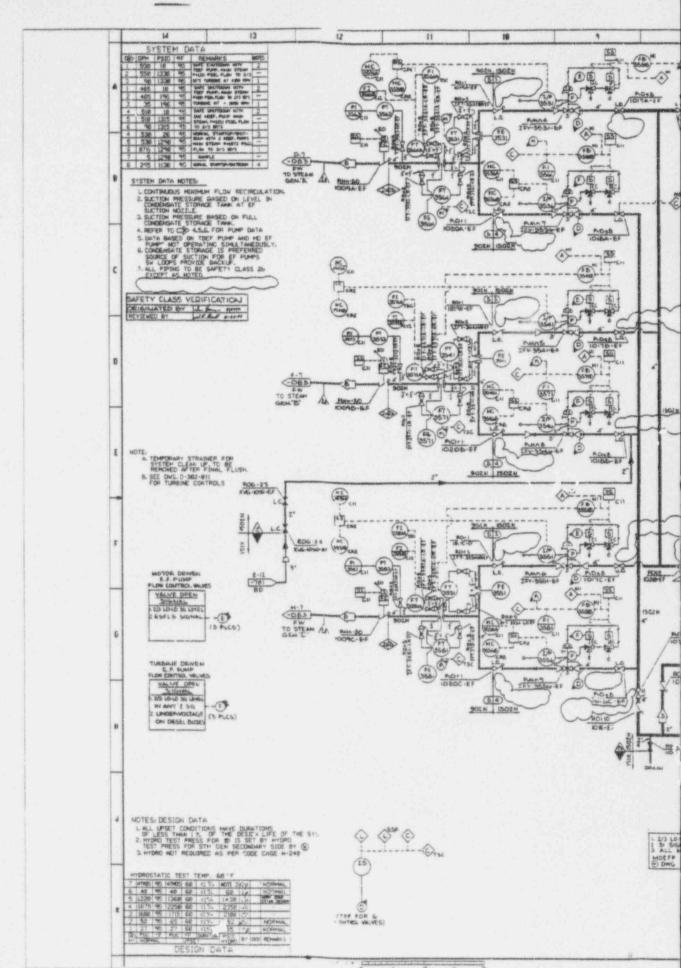
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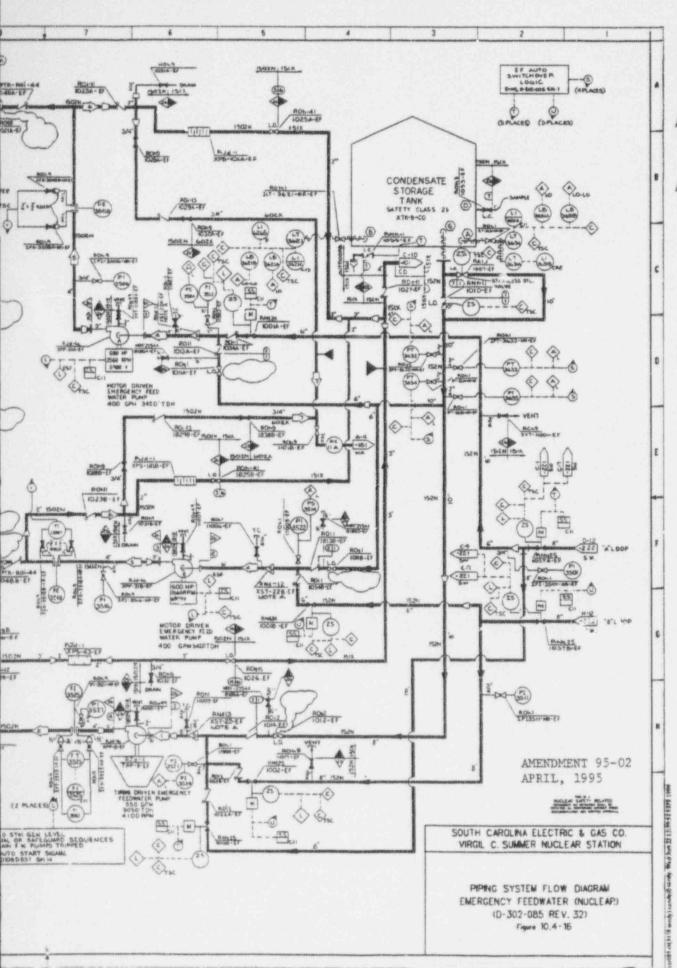
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#### 11.5.6 STORAGE

Compactable waste, filled containers of compacted waste, and spent filter cartridges are stored in the shielded areas of the radwaste area or in a location determined by the Manager of Health Physics and Radwaste Services. Contaminated hardware and tools may also be stored in these rooms. Solidified waste, after solidification is complete, and dewatered resins, once dewatering is complete, may be shipped off-site for immediate burial at a licensed facility. Primary spent resins will normally have at least a one month decay period while being held in the spent resin storage tank. Evaporator bottoms and secondary blowdown resins do not normally require a decay period.

If solidified waste and/or dewatered resins require storage for any reason, they will be stored in the radiation control area outside the truck access on the storage pad (see Figure 1.2-25) or in a location determined by the Manager of Health Physics and Radwaste Services. The storage pad is approximately 40 feet wide by 120 feet long and is sloped toward a hold-up trench. Waste stored in the storage area will be shielded as required by portable shields and/or casks used for shipment.

Storage areas for solidified waste, dewatered resins, and compacted waste are sufficient, based on the estimates presented in Section 11.5.4, to accommodate greater than 30 days waste generation.

#### 11.5.7 SHIPMENT

Shipment, in accordance with applicable regulations, is made as necessary-dependent upon operational considerations and storage area availability.

The primary activity determination method will be to sample the waste stream (resins and liquid waste) during transfer to a process container and analyze the sample using the appropriate counting instrumentation. An isotopic determination is made of the radionuclides present and the activity of each. Summation of the individual activities is used to calculate the Curie content of the processed container.

For cases where the primary method cannot be used, an alternate technique will be implemented. The alternate method entails using the dose rate of the packaged waste in order to calculate the Curie content. The calculation considers the waste characteristics, geometry of the waste package, characteristics of the container and solidification media (if applicable), and the average gamma energy. For spent cartridge filters, this alternate method will be used to determine the Curie content. The appropriate counting instrumentation is used to analyze samples taken from the process stream to identify resonauclides present and the average gamma energy.

#### 11.5.8 POTENTIAL FOR RELEASES

### 11.5.8.1 Potential for Release during Container Filling

The filling operation may be terminated via visual inspection using a remote monitor/television camera. Termination is accomplished by closing valves MOV-2 and MOV-5.

There is no airborne release to the atmosphere in the fill areas. Air in the container and gas, if any, from the waste entering the container are vented to the building exhaust, through a local filter, or through a portable ventilation unit. Only one line feeds waste to the container. This is flushed with water as the final phase of the fill cycle.

If leaks of any kind or spills are observed, the operation in progress can be immediately terminated. Any spill which may occur will be contained by permanent curbing in the solidification area.

Except for the curb in the solidification area, there are no physical barriers in the immediate fill areas to contain spills. Spills from the shipping container would need to be drained to a specific location or container as determined by the type of material spilled.

The floor surfaces have a special nonporous finish to permit decontamination of the surface, if required.

## 11.5.8.2 Potential for Release from Storage Tanks

## 11.5.8.2.1 Waste Evaporator Concentrate: Tank

Essentially all radioactive gases are stripped from the concentrates in the waste evaporator. A normally closed vent is ducted to the auxiliary building exhaust system. A water seal, set for 2 feet of water, vents to the waste evaporator concentrates tank cubicle which is serviced by the auxiliary building exhaust system.

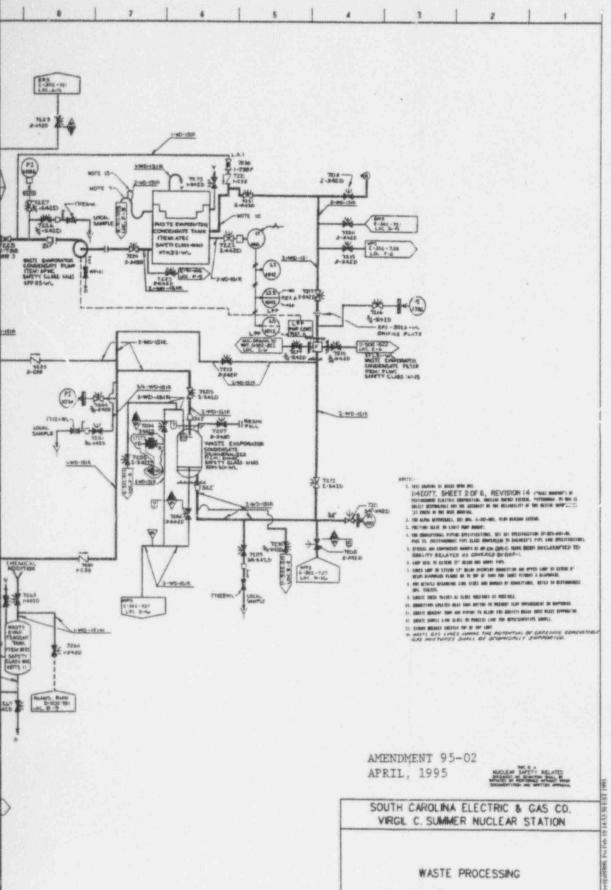
Overflow is not anticipated since waste evaporator concentrates tank capacity is sufficient for storage of the expected volume of concentrates generated by one year of normal operation. However, an overflow is directed to the waste holdup tank. Level indicators actuate alarms at the solid waste system control panel prior to tank overflow.

Floor drains in the cubicles for this tank and for the waste evaporator concentrates tank transfer pump drain to the floor drain tank. By appropriate valving, the concentrates can be pumped from the floor drain tank to either the waste holdup tank, waste evaporator, waste evaporator concentrates tank, or directly to the drumming station area for solidification.

#### 11.5.8.2.2 Chemical Drain Tank

This tank is vented to the building exhaust system. A high level alarm is provided on the solid waste system control panel. Overflow, or leakage, if it occurs, is directed to the auxiliary building sump by a floor drain. The

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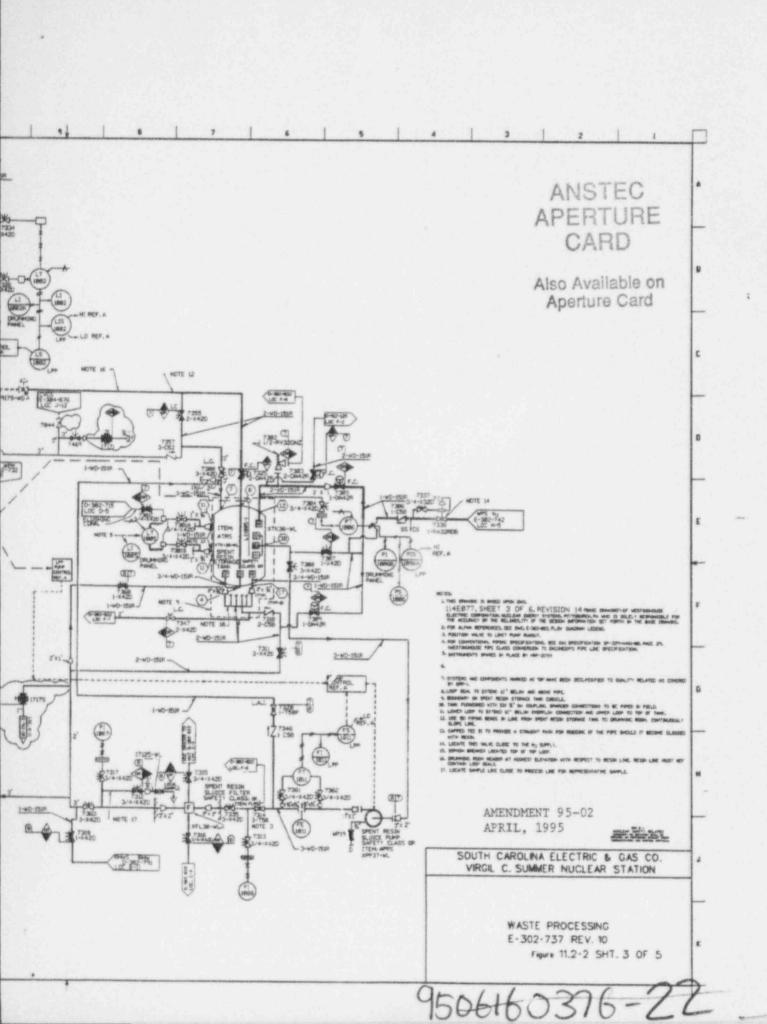


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#### LIST OF EFFECTIVE PAGES (LEP)

The following list delineates pages to Chapter 12 of the Virgil C. Summer Nuclear Station Final Safety Analysis Report which are currently in effect. The latest changes to pages and figures are indicated below by Amendment 94-10 in the Amendment column along with the amendment number and date for each page and figure included in the Final Safety Analysis Report.

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Page/Fig. No.	Amend. No.	Date	Page/Fig. No.	Amend. No.	Date
Fig. 12.1-2  12.1-2a  12.1-3  12.1-4  12.1-5(1 of 2)  12.1-5(2 of 2)  12.1-6  12.1-7  12.1-8  12.1-10  12.1-11  12.1-11a  12.1-12  12.1-13  12.1-14  12.1-15  12.1-16  12.1-17  12.1-18  12.1-19  12.1-19  12.1-20  12.1-21  12.1-22  Page 12.2-1  12.2-2  12.2-3  12.2-4  12.2-5  12.2-6  12.2-7  12.2-8  12.2-10  12.2-11  12.2-12  12.2-13  12.2-14  12.2-15  12.2-16  12.2-17  12.2-18  12.2-19  12.2-19  12.2-19  12.2-20  12.2-21  12.2-21  12.2-22  12.2-23  12.2-24  Fig. 12.2-1	93-10 93-10 93-10 93-10 93-10 95-02 95-02 95-02	Aug. 1986 Aug. 1986 Aug. 1988 Aug. 1988 Aug. 1988 Aug. 1989 Aug. 1988 Aug. 1989 Aug. 1989 Aug. 1989 Aug. 1989 Aug. 1989 Aug. 1989 Aug. 1984 Aug. 1988	Fig. 12.2-2 12.2-3 12.2-4 Page 12.3-1 12.3-3 12.3-4 12.3-5 12.3-6 12.3-7 12.3-8 12.3-10 12.3-11 12.3-12 12.3-14 12.3-15 12.3-16 12.3-17 12.3-18 12.3-19 12.3-20 Fig. 12.3-1 Page 12A-1 12A-2 12A-3 12A-4 12A-5 12A-6 12A-7 12A-8 12A-9 12A-10 12A-11 12A-12 12A-13 12A-14 12A-15 12A-10 12A-11 12A-12 12A-13 12A-14 12A-15 12A-10 12A-11 12A-12 12A-13 12A-14 12A-15 12A-10 12A-11 12A-12 12A-13 12A-11 12A-12 12A-13 12A-14 12A-15 12A-16 12A-17 12A-18 12A-19 12A-20 12A-21 12A-22 12A-23 12A-24 12A-25	0 0 0 0 94-01 94-01 94-01 94-01 94-01 94-01 94-01 94-01 94-01 94-01 94-01 94-01 94-01	Aug. 1984 Aug. 1984 Jan. 1994 Jan. 1984 Aug. 1988
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12A.4-8	2	Aug. 1986

In the control complex, the sampling room could be considered as a source of airborne activity. This air is monitored for airborne activity as discussed in Section 12.2.4.2.7.

Periodic surveillance of accessible areas, in accordance with Sections 12.1.5 and 12.3.2, will be performed.

Reliable power for the fixed instrumentation is obtained from the diesel backed, 120 volt instrument buses. Associated sample pumps obtain power from the 480 volt diesel backed buses. This assures continuity of operation in the event of a loss of offsite power. Measured activity levels are indicated and recorded on the radiation monitoring system control panel located in the control room. Local indication is provided for each channel. A differential pressure switch is provided on the particulate and iodine collection filter holders to cause an alarm on filter blockage. Another differential pressure switch is provided across the two filter holders (except on RMA-4) to cause an alarm on loss of flow. The loss of flow alarm for RMA-4 originates from the flow indication device (photohelic). The movable monitors have local indication, recording and alarms. Detectors have remotely actuated check sources to provide functional verification. In addition, each channel is calibrated routinely by exposure to a calibrated source traceable either directly or indirectly to NBS for verification against its initial calibration. Calibration of the monitors is performed following any required maintenance of the detectors. Measurements have an accuracy of  $\pm 25$  percent of the true value. Precision is  $\pm 15$  percent at all levels. Each ratemeter is equipped with two adjustable alarm levels (alert and high) and a channel failure/or loss of power alarm. These alarms, associated with the fixed monitors, are annunciated on the radiation monitoring system control panel in the control room. Channels which have interlock functions with other systems (see Figure 11.4-1) are provided with a bypass switch for use during maintenance or testing. Use of this switch is annunciated.

## 12.2.4.2.1 Control Room Supply Air, Channel RM-A1

This channel monitors the particulate, iodine and gaseous activity of air supplied to the control room. A sample of air is taken from the air supply duct through an isokinetic sampler nozzle and is drawn successively through a particulate sampler, an iodine sampler, and a gas sampler. The particulate sampler is equipped with a fixed filter which is continuously monitored by a lead shielded scintillator detector. The iodine sampler is similar to the particulate sampler except that an activated charcoal cartridge is used instead of a fixed filter. The fixed filter and the charcoal filter are designed to be removable for laboratory analysis. The sensitive volume of the gas sampler is shielded with lead and monitored by a scintillation detector. The approximate sensitivity and range of this channel are as follows:

- Particulate, 10-11 to 10-7 μCi/cc based upon Cs-137.
- 2. Gas, 2 x 10-6 to 2 x 10-2 µCi/cc based upon Kr-85.
- 3. Iodine, 3 x 10-11 to 10-7 μCi/cc based upon I-131.

A high activity alarm from the gas channel automatically places the control room, computer room, relay room and instrument repair room ventilation systems in the recirculation mode, starts the control room emergency ventilation system and closes the outside air dampers. The iodine and particulate channels provide high activity alarms to alert operating personnel. The high alarm setpoints are established on the basis of the requirements of 10 CFR 20 and the sensitivity of the detection channels.

#### 12.2.4.2.2 Reactor Building Air Sample Line, Channel RM-A2

This channel monitors the particulate, iodine and gaseous activity level of the air inside the reactor building and is located inside the auxiliary building. Reactor building air drawn from and returned through reactor building penetrations is monitored by RM-A2. The readout of the monitor is used to detect leaks in systems containing primary coolant. Channel ranges are similar to those of Channel RM-A1. The sensitivity of this monitor provides the capability to detect 10-MPC-hours of particulate and iodine radioactivity.

The monitor air sample and return lines /re isolated (closed) upon occurrence of a containment isolation signal (Phase A). Post accident, this monitor can be used as a reactor building air sampling station, provided that reactor building pressure and temperature have been reduced sufficiently to allow opening of the sample line isolation valves. This monitor is also designed to withstand seismic conditions as recommended by Regulatory Guide 1.45.

The monitor design is similar to that of RM-Al, except that a moving particulate filter is used. An additional sample pump is also provided to allow operation when one pump is undergoing maint nance.

A high activity alarm from the gas channel initiates closure of the reactor building purge valves (see Figure 11.4-1).

High alarm setpoints are based upon plant operating requirements, sensitivity and measured normal background. The particulate alarm setpoints may be readjusted as a function of primary coolant activity, leakages or plant conditions.

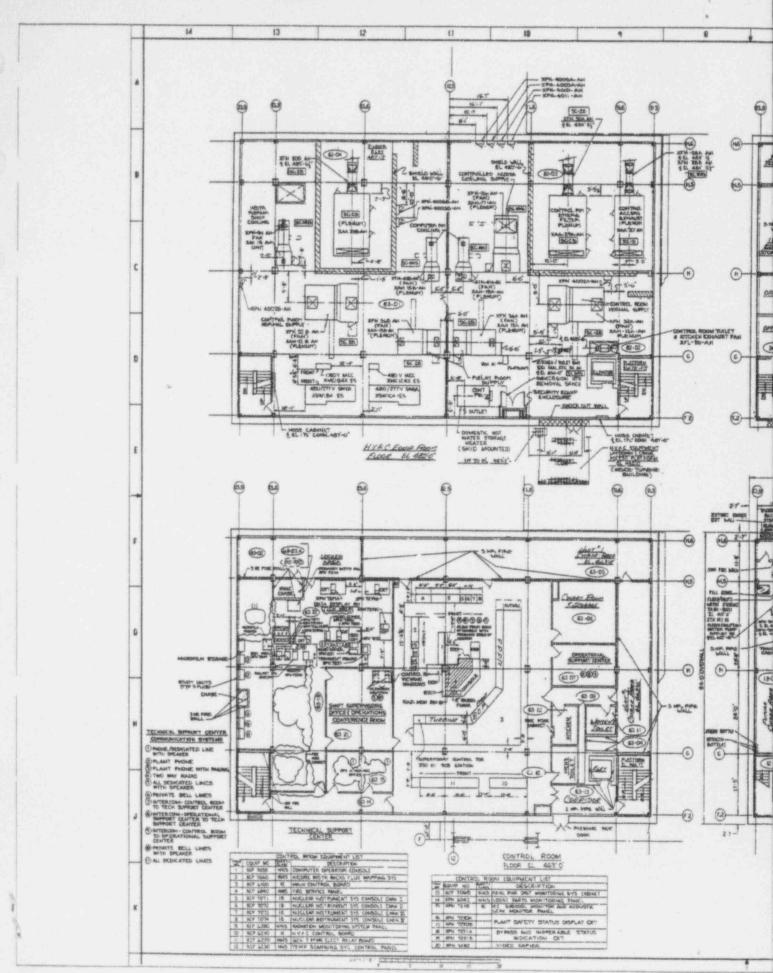
A fixed alarm setpoint is not applicable to particulate radiation monitoring for reactor coolant leak detection. The activity of the reactor coolant and background radiation must be taken into consideration.

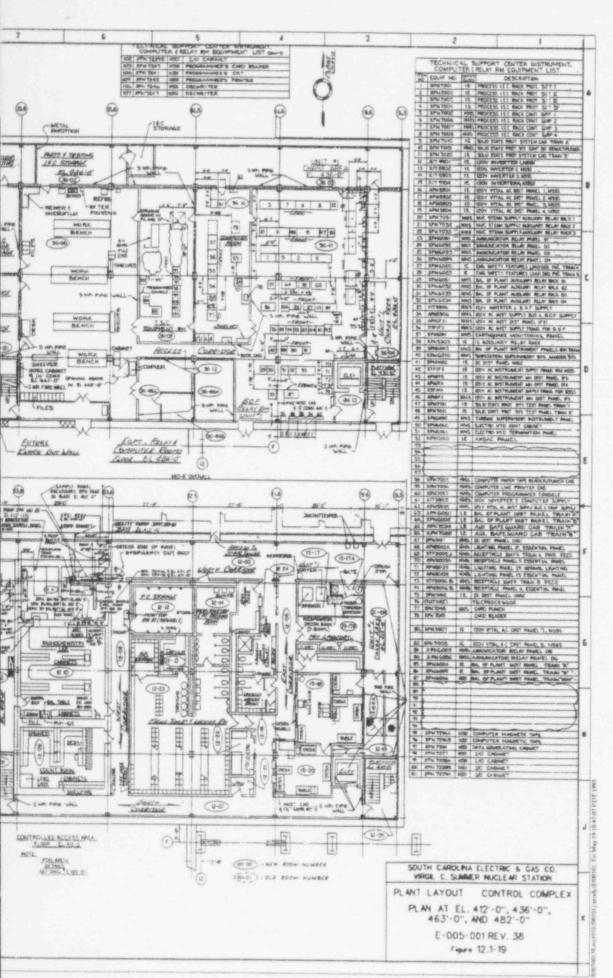
The particulate channel of radiation monitor RM-A2 will be operated with an initial setpoint of not less than twice background and may subsequently be readjusted based upon the results of periodic analysis of reactor coolant activity.

This setpoint is expressed as follows:

\* 
$$[(B_1) * (C_1 R_1 K_1)] \ge Setpoint \ge 2B_1^*$$
 Eq. 12.2-1

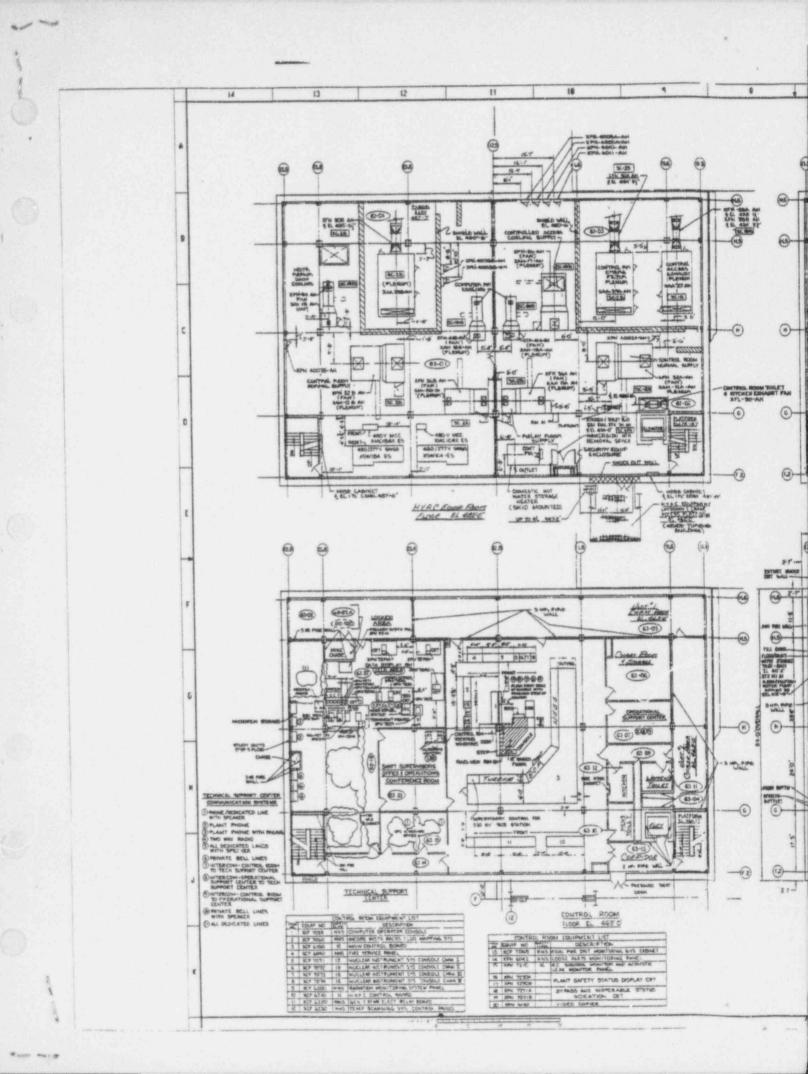
<sup>\*</sup>This setpoint may be adjusted greater than this expression to compensate for high containment equilibrium activity but no more than twice the operational equilibrium (same for in gas channel).

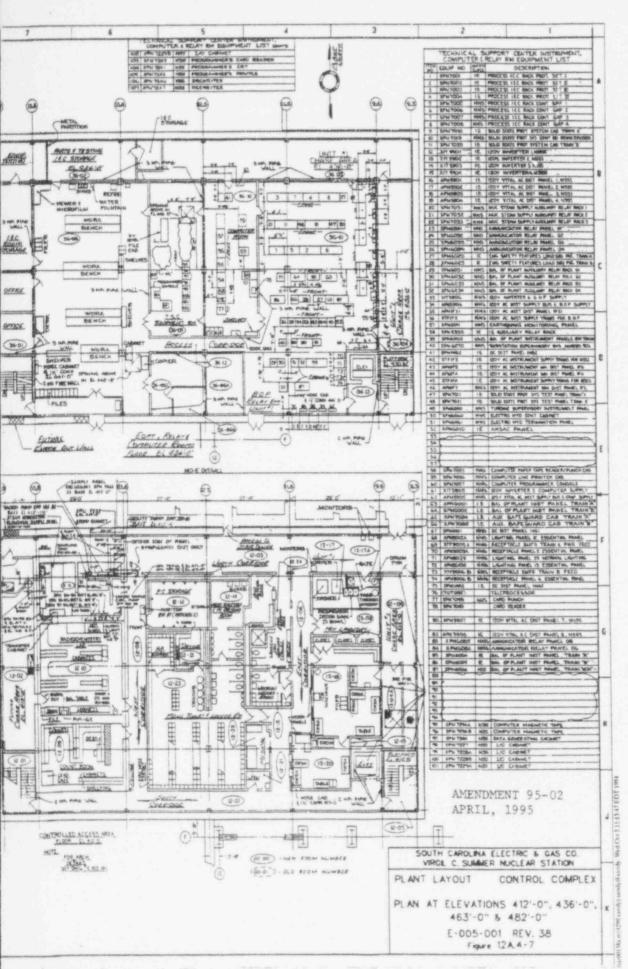




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