(803) 831-3000

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DUKE POWER

February 28, 1992

Document Control Dock U. S. Kuclear Regulatory Commission Washington, D.C. 20555

Subject: (atawba Nuclear Station //ocket No. 50-414 LER 414/91-013, Revision 1

Gentlemen:

Attached is Licensce Event Report 414/91-013, Revision 1, concerning REACTOR TRIP DUE TO NC PUMP TRIP CAUSED BY EQUIPMENT FAILURE.

This event was considered to be of no significance with respect to the health and safety of the public.

Very truly yours,

W. R. McCollins

Station Managor

/lhe

Attachment

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xc: Mr. S. D. Ebneter Regional Administrator, Region II U. S. Nuclear Regulatory Commission 201 Marietta Street, NW, Suite 2900 Atlanta, GA 30323

> R. E. Martin U. S. Nuclear Regulatory Commission Office of Nuclear Reactor Pegulation Washington, D.C. 20555

Mr. W. T. Orders NRC Resident Inspector Catawba Nuclear Station

> PDR PDR

M & M Nuclear Insurers 1221 Avonues of the Americas New York, NY 10020

INPO Records Center Suite 1500 1100 Circle 70 Parkway Atlanta, GA 30339

1633

February 27, 1992

To: W. R. McCollum

Subject: LER 414/91-013, PIR 1-C91-0272, Revision 1; Reactor Trip Due To NC Pump Trip Caused By Equipment Failure

The following revisions have been made to IER 414/91-013.

1) LER Form Page 4 (Conclusion)

"SCRs will be tested during preventive maintenance relay testing." will be changed to "SCRs will be tested on a one time basis to ensure that lookage current is acceptable." The SCR manufacturer recommends one time only testing because forther testing could damage the SCRs. This action also applies to corrective action established for LER 414/91-008.

2) LFR Form Page 4

Delete the following from Conclusion, paragraph 5: "This report will be revised, if needed, based on the cutcome of this failure analysis. Part 21 reportability will be re-evaluated, if needed."

Add the following to the Conclusion, paragraph 5: "Following the analysis of the failed SCRs, Motorola has determined that the defect is not generic to these devices."

Add the following paragraph to Conclusion following paragraph 5: All spare SCRs (Motorola P/N SCR 1379H) were returned to ABB for testing and replacement. PD personnel will replace all questionable 3CRs with SCRs manufactured after 1982.

3) LER Form Page 5

Change Planned Corrective Action 1 to read: "All protective relay SCRs will be tested on a one time basis to ensure that leakage current is acceptable."

Delete Flanned Corrective Action 2. Motorola has determined that the defect is not generic.

S. T. Rose Chairman, Safety Review Group

STR/lhe

cc: LER/91-013 File

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other SCRs associated with the NC Pump supply and safety breakers have checked. Inspections of SCRs in other critical applications have been performed.

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BACKGROUND

The Reactor Coolant [EIIS:AB] (NC) System utilizes four loops to transport heat from the Reactor to four Steam Generators [EIIS:HX] (S/Gs). An NC Pump [EIIS:P] in each loop is powered by £900 V Switchgear [EIIS:SWGR] (located in the Turbine [EIIS:TRB] Building), via a 6900 V feeder breaker [EIIS:BRK] (11A-3, 1TB-3, 1TC-3, and 1TD-3) in series with a safety breaker. Erch safety breaker is located in its respective 6900 V NC Pump Switchgear, in either the 560 or 577 foot elevation Auxiliary Building [EIIS:NF] Unit 1 Electrical Penetration [EIIS:PEN] room. Each safety breaker is protected by a ground fault relay [EIIS:RLY] (50G) and an overcurrent relay (50/51). Actuation of either relay trips the safety breaker.

The overcurrent relay (ITE relay Type ITE51L) contains betw an instantaneous and a time delay circuit, each of which utilizes a Silicon Controlled Rectifier (SCR). The SCR acts as a solid state type contact in the relay trip logic. The overcurrent relay was manufactured by ITE Imperial Corporation, which is now ABB Power T & D Company, and the SCR is manufactured by Motorola.

The P-8 permissive is in place when 2 out of 4 power range channels are greater than 48%. This permissive unblocks the 1 out of 4 loops loss of NC flow Reactor trip interlock.

EVENT DESCRIPTION

On June 20, 1991, Unit 1 was in Mode 1, Power Operation, at 71% power following a refueling outage. Power escalation was in progress. At 0823:11 hours, a Reactor trip occurred due to the "Low Flow P8 Permissive Trip", caused by the automatic trip of NC Pump 1A. Plant response was as expected. The Main Turbine tripped on Reactor trip. Operations personnel entered Emergency Procedures to respond to the trip. At 0823:23 hours, Feedwater Isolation occurred on Reactor trip with Low Tavg. (Low Tavg was due to low decay heat, as a result of a new core). Both motor (EIIS:MO) driven Auxiliary Feedwater [EIIS:BA] (CA) pumps [EIIS:P] automatically started, and supplied water to the Steam Generators. Neither the Pressurizer nor any of the Steam Generator Power Operated Relief Valves (PORVs) opened. None of the Pressurizer or Steam Generator code safety valves lifted. Banks 1 and 2 of the condenser steam dump valves actuated. A manual response required was the closing of valve SP34 (Steam Supply to the Feedwater Pump Turbines) to isolate steam drains which were causing excessive NC System cooldown. Letdown isolation occurred at 0828:40 hours as a result of Pressurizer level decreasing to approximately 17%, due to Low Tavg. (Low Tavg resulted from low decay heat, as a result of a new core.) Letdown was restored using the appropriate Abnormal Procedure. CA flows to Steam Generators C and D were slightly below the acceptance band, and Performance performed a subsequant flow balance. NC cooldown to 538 degrees F occurred, as a result of the lack

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of decay heat, loss of NC Pump 1A, CA flow to the Steam Generators, and the Auxiliary Steam header not being cross-tred to Unit 2. After CA was reset, and the Auxiliary Steam [EIIS:SA] (AS) header tied to Unit 2, Tavg began to increase. Other measures taken to increase Tavg included tripping Feedwater [EIIS:SJ] (CF) Pump 1B and isolating the atmospheric steam dumps. Appropriate notifications of the trip were made. Following the completion of all Emergency and Abnormal Procedures required, OP/1/A/6100/05, Unit Fast Recovery, was entered. CF flow to the Steam Generators was restored, and CA was shutdown and returned to standby. Operations personnel initiated work request 558160PS to investigate/repair the NC Pump trip.

At 1265 hours, on June 20, Power Delivery (PD) personnel identified the cause of the pump trip to be a degraded SCR associated with the NC Pump 1A safety breaker 50/51 XY2 overcurrent relay. The ECR in the time delay circuit of the overcurrent relay was degraded, resulting in the NC Pump 1A safety breaker tripping open. The degraded SCR was replaced. The SCRs for all other NC Pump overcurrent and ground fault relays, including both Units' supply and safety breakers, were also checked by FD personnel. A defective SCR in an NC Pump 1B 50G relay was found and replaced. The other relays, and associated SCRs, checked satisfactory.

By 0225 hours, on June 21, the Unit was returned to Mode 1. By 0545 hours, on June 21, the Unit was brough back on line.

SCRs for relay in critical applications were checked by PD personnel. These applications included Units 1 and 2 ETA and ETB (4160 Essertial Switchgear) normal incoming breakers, Units 1 and 2 Chemical and Volume Control [EIIS:CB] (NV) Pump motors A and B breakers, and Units 1 and 2 hotwell/condensate booster pump motors A, B, and C breakers. These inspections were complete by 1810 hours, on June 21. They were performed under work requests 269-278TRL.

CONCLUSION

This incident is attributed to an equipment failure. The SCR associated with the time delay circuit of the NC Pump 1A safety breaker 50/51 XYZ overcurrent relay was defective. Corrective actions included replacement of the SCR, inspections of other SCRs associated with NC Pump supply and safety breakers, and inspections of SCRs in other critical applications.

On May 29, 1991, the Unit 2 Reactor tripped on low flow due to a degraded SCR (see LER 414/91-008). This SCR was associated with a ground fault relay for 6900 volt switchgear feeder breaker 2TB-3 (for NC Pump 2B). Breaker 2TB-3 opened, causing NC Pump 2B to trip. Therefore, although there have not been any other incidents at Catawba during the past two years before these two events due to degraded SCRs, this is considered to be a recurring problem. A planned corrective action in LER 414/91-008 was for SCR testing to be added to

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existing preventive maintenance activities. SCRs will be tested on a one time basis to ensure that leakage current is acceptable.

Following the May 29 incident, a planned corrective action was made for PD personnel to test a sample group (30-40) of switchgear protective relays. Following the June 20 incident, the scope of this testing was greatly increased. As of July 15, 1991, 7 of 153 inservice relays tested have been found to have degraded SCRs (including those causing the two Deactor trips). Also, 2 out of 100 in stock have been found to be defective. Approximately 700 relays containing SCRs will be tested, some of which can only be tested off-line. On-line testing of relays for defective SCRs, where possible, is in progress. SCR failures will be trended to determine if a pattern is present. All switchgear protection relay SCRs will be tested by the end of the next three refueling outages on each Unit (one-third are tested each outage).

Industry-wide, the vendor has indicated a failure rate of less than 0.1% over the past 10 years. At Catawba, 11 SCR failures have been identified, previous to the May 29, 1991 incident. Previous relay test methods led to detection of friled (i.e. open) SCRs. The method now being used to test SCRs can detect degradation less severe than total SCR failure, which could result in tripping a relay. This testing should enable detection of degraded SCRs prior to failure.

The SCR failure is reportable to the Nuclear Reliability Database System (NFRDS). Following the analysis of the failed SCRs, Motorola has determined that the defect is not generic to these devices.

All spare SCRs (Motorola P/N SCR 1379H) were returned to ABB for testing and replacement. PD personnel will replace all questionable SCRs with SCRs manufactured after 1982.

CORRECTIVE ACTIONS

SUBSEQUENT

- Operations personnel entered Emergency Procedures to respond to the trip.
- Operations personnel took appropriate actions to respond to the NC cooldow ..
- Operations personnel entered the appropriate Abnormal Procedure to respond to the letdown isolation.
- 4) PD personnel investigated and replaced the defective SCR under work request 558160. .. Other NC Pump supply and safety breaker associated SCRs were checked.

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 PD personnel inspected SCRs in other critical applications. The scope of testing for defective SCRs was increased.

6) The defective SCRs were sent to Motorola for failure analysis.

PLANNED

 All protective relay SCRs will be tested on a one time basis to ensure that leakage current is acceptable.

SAFETY ANALYSIS

Plant response to the Reactor trip from 71% power was as expected. The Main Turbine tripped on Reactor trip, and feedwater isolation occurred on Reactor crip with Low Tavg. The motor driven CA pumps automatically started and supplied water to the Steam Generators. Flows to Steam Generators C and D were slightly below the acceptance band, and Performance performed a subsequent flow balance. None of the Pressuriter or Steam Generator PORVs opened, and none of the Pressurizer or Steam Generator code safety valves lifted. Banks 1 and 2 of the condenser steam cump valves actuated. Manual responses included manual Reactor trip, throttling CA flow, and closing valve SP34 (to isolate steam drains causing NC cooldown). Letdown was reestablished using the appropriate Abnormal Procedure following the letdown isolation. Prior to the transient, NC temperature was at 577 degrees F. NC System temperature cooled down to 538 degrees F during the transient as a result of the lack of decay heat, loss of NC Pump 1A, CA flow to the Steam Generators, and the Auxiliary Steam header not being cross-tied to Unit 2. NC cooldown did not exceed 100 degrees F in one hour. Heat removal was provided via the Steam Generators being fed by CA flow.

If the NC Pump trip had occurred at 100% power, plant safety aquipment was available to maintain critical parameters within their required values.

The health and safety of the public were not affected by this incident.