



UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D.C. 20585

VIRGINIA ELECTRIC AND POWER COMPANY

OLD DOMINION ELECTRIC COOPERATIVE

DOCKET NO. 50-338

NORTH ANNA POWER STATION, UNIT NO. 1

AMENDMENT TO FACILITY OPERATING LICENSE

Amendment No. 154  
License No. NPF-4

1. The Nuclear Regulatory Commission (the Commission) has found that:
  - A. The application for amendment by Virginia Electric and Power Company et al., (the licensee) dated January 8, 1992, as supplemented by letters dated January 31, February 10 and February 25, 1992, complies with the standards and requirements of the Atomic Energy Act of 1954, as amended (the Act), and the Commission's rules and regulations set forth in 10 CFR Chapter I;
  - B. The facility will operate in conformity with the application, the provisions of the Act, and the rules and regulations of the Commission;
  - C. There is reasonable assurance (i) that the activities authorized by this amendment can be conducted without endangering the health and safety of the public, and (ii) that such activities will be conducted in compliance with the Commission's regulations;
  - D. The issuance of this amendment will not be inimical to the common defense and security or to the health and safety of the public; and
  - E. The issuance of this amendment is in accordance with 10 CFR Part 51 of the Commission's regulations and all applicable requirements have been satisfied.

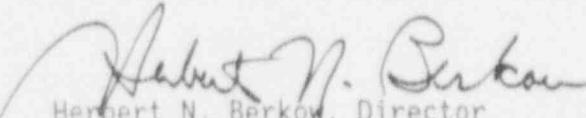
2. Accordingly, the license is amended by changes to the Technical Specifications as indicated in the attachment to this license amendment, and paragraph 2.D.(2) of Facility Operating License No. NPF-4 is hereby amended to read as follows:

(2) Technical Specifications

The Technical Specifications contained in Appendices A and B, as revised through Amendment No. 154, are hereby incorporated in the license. VEPCO shall operate the facility in accordance with the Technical Specifications.

3. This license amendment is effective as of its date of issuance.

FOR THE NUCLEAR REGULATORY COMMISSION



Herbert N. Berkow, Director  
Project Directorate II-2  
Division of Reactor Projects - I/II  
Office of Nuclear Reactor Regulation

Attachment:  
Changes to the Technical  
Specifications

Date of Issuance: March 3, 1992

ATTACHMENT TO LICENSE AMENDMENT NO. 154

TO FACILITY OPERATING LICENSE NO. NPF-4

DOCKET NO. 50-338

Replace the following pages of the Appendix "A" Technical Specifications with the enclosed pages as indicated. The revised pages are identified by amendment number and contain vertical lines indicating the area of change. The corresponding overleaf pages are also provided to maintain document completeness.

Remove Pages

2-1  
- -  
2-6  
2-9  
2-10  
3/4 2-15

Insert Pages

2-1  
2-2a  
2-6  
2-9  
2-10  
3/4 2-15

## 2.0 SAFETY LIMITS AND LIMITING SAFETY SYSTEM SETTINGS

### 2.1 SAFETY LIMITS

#### REACTOR CORE

2.1.1 The combination of THERMAL POWER, pressurizer pressure, and the highest operating loop coolant temperature ( $T_{avg}$ ) shall not exceed the limits shown in Figures 2.1-1\* for 3 loop operation and 2.1-2 and 2.1-3 for 2 loop operation.

APPLICABILITY: MODES 1 and 2.

#### ACTION:

Whenever the point defined by the combination of the highest operating loop average temperature and THERMAL POWER has exceeded the appropriate pressurizer pressure line, be in HOT STANDBY within 1 hour.

#### REACTOR COOLANT SYSTEM PRESSURE

2.1.2 The Reactor Coolant System pressure shall not exceed 2735 psig.

APPLICABILITY: MODES 1, 2, 3, 4 and 5.

#### ACTION:

MODES 1 and 2

Whenever the Reactor Coolant System pressure has exceeded 2735 psig, be in HOT STANDBY with the Reactor Coolant System pressure within its limit within 1 hour.

MODES 3, 4 and 5

Whenever the Reactor Coolant System pressure has exceeded 2735 psig, reduce the Reactor Coolant System pressure to within its limit within 5 minutes.

\* For the period of operation until steam generator replacement, the combination of THERMAL POWER, pressurizer pressure, and the highest operating loop coolant temperature ( $T_{avg}$ ) shall not exceed the limits shown in Figure 2.1-1a.

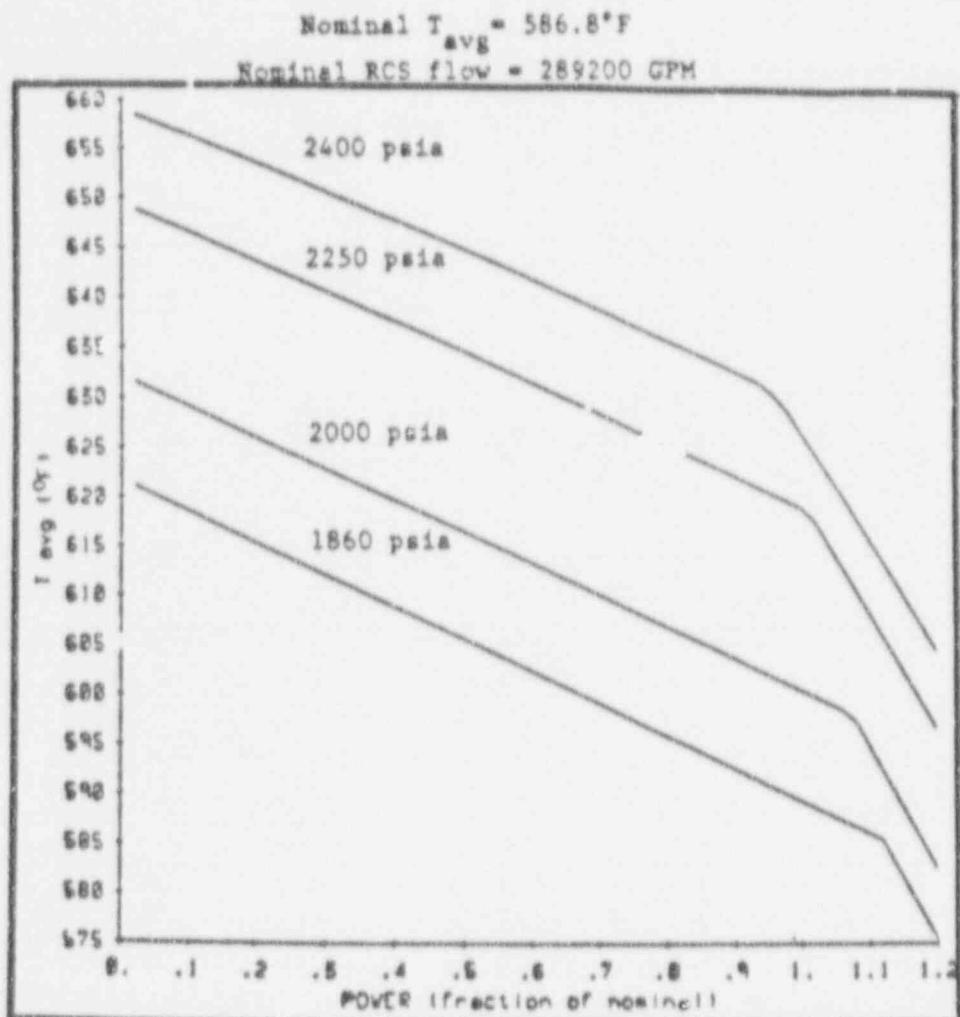


Figure 2.1-1 REACTOR CORE SAFETY LIMITS FOR THREE LOOP OPERATION

Nominal  $T_{avg}$  = 586.8°F  
Nominal RCS flow = 268,500 GPM

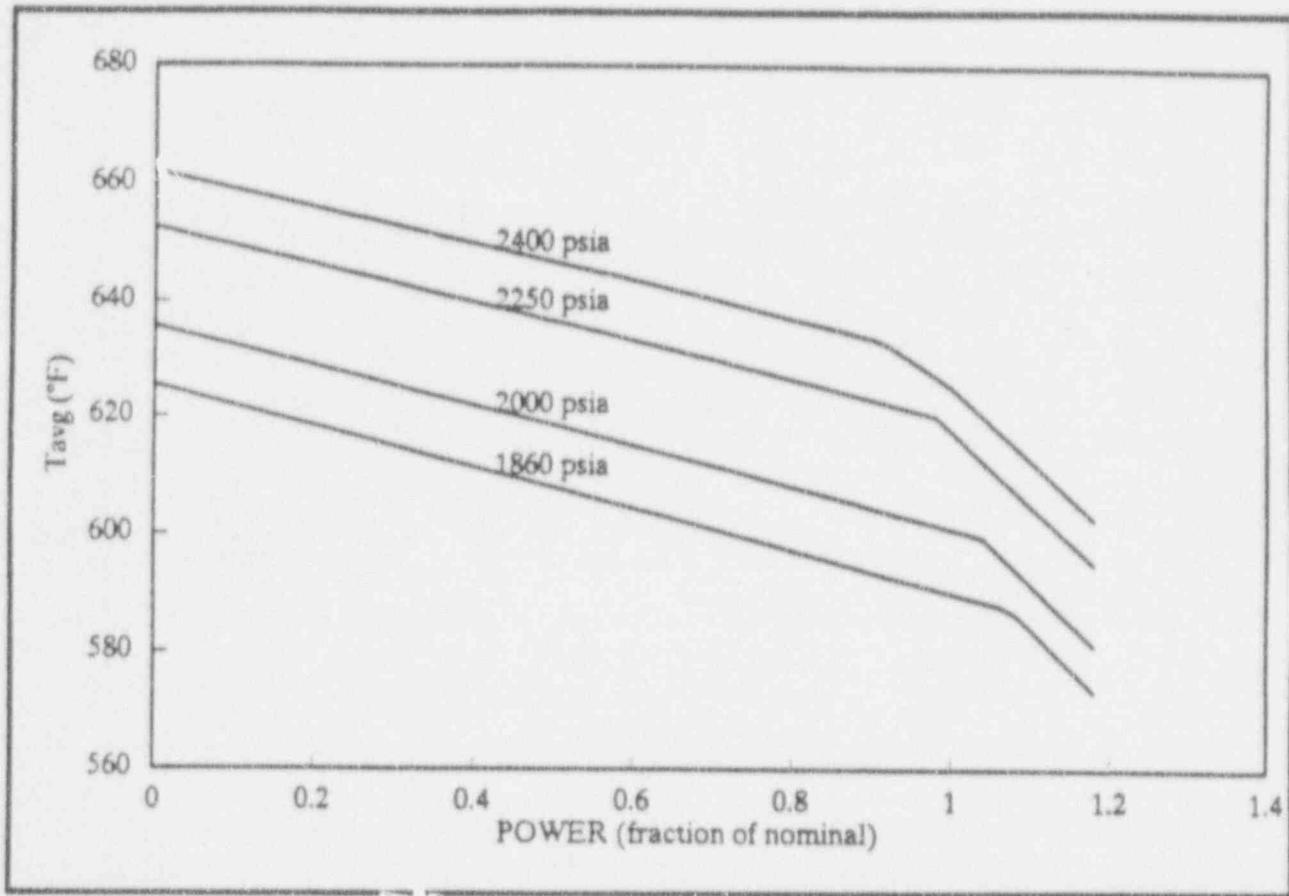


Figure 2.1-1a REACTOR CORE SAFETY LIMITS FOR THREE LOOP OPERATION FOR THE PERIOD OF OPERATION UNTIL STEAM GENERATOR REPLACEMENT

## SAFETY LIMITS AND LIMITING SAFETY SYSTEM SETTINGS

### 2.2 LIMITING SAFETY SYSTEM SETTINGS

#### REACTOR TRIP SYSTEM INSTRUMENTATION SETPOINTS

2.2.1 The reactor trip system instrumentation setpoints shall be set consistent with the Trip Setpoint values shown in Table 2.2-1.

APPLICABILITY: As shown for each channel in Table 3.3-1.

#### ACTION:

With a reactor trip system instrumentation setpoint less conservative than the value shown in the Allowable Values column of Table 2.2-1, declare the channel inoperable and apply the applicable ACTION statement requirement of Specification 3.3.1.1 until the channel is restored to OPERABLE status with its trip setpoint adjusted consistent with the Trip Setpoint value.

TABLE 2.2-1

## REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS

## FUNCTIONAL UNIT

TRIP SETPOINT	ALLOWABLE VALUES
1. Manual Reactor Trip	Not Applicable
2. Power Range, Neutron Flux	Low Setpoint - $\leq 25\%$ of RATED THERMAL POWER High Setpoint - $\leq 109\%^{**}$ of RATED THERMAL POWER
3. Power Range, Neutron Flux, High Positive Rate	$\leq 5\%$ of RATED THERMAL POWER with a time constant $\geq 2$ seconds
4. Power Range, Neutron Flux, High Negative Rate	$\leq 5\%$ of RATED THERMAL POWER with a time constant $\geq 2$ seconds
5. Intermediate Range, Neutron Flux	$\leq 25\%$ of RATED THERMAL POWER
6. Source Range, Neutron Flux	$\leq 10^5$ counts per second
7. Overtemperature $\Delta T$	See Note 1
8. Overpower $\Delta T$	See Note 2
9. Pressurizer Pressure--Low	$\geq 1870$ psig
10. Pressurizer Pressure--High	$\leq 2385$ psig
11. Pressurizer Water Level--High	$\leq 92\%$ of instrument span
12. Loss of Flow	$\geq 90\%$ of design flow per loop *
	$\geq 89\%$ of design flow per loop *

\* Design flow per loop is one-third of the minimum allowable Reactor Coolant System Total Flow Rate as specified in Table 3.2-1.

\*\* The high trip setpoint for Power Range, Neutron Flux, shall be  $\leq 103\%$  RATED THERMAL POWER for the period of operation until steam generator replacement.

\*\*\* The allowable value for the high trip setpoint for Power Range, Neutron Flux, is required to be  $\leq 104\%$  RATED THERMAL POWER for the period of operation until steam generator replacement.

TABLE 2.2.1 (Continued)  
 REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINT  
 NOTATION (Continued)

Operation with 3 Loops		Operation with 2 Loops (no loops isolated)		Operation with 2 Loops (1 loop isolated)*	
K <sub>1</sub>	= 1.264 **	K <sub>1</sub>	= ( )	K <sub>1</sub>	= ( )
K <sub>2</sub>	= 0.0220	K <sub>2</sub>	= ( )	K <sub>2</sub>	= ( )
K <sub>3</sub>	= 0.001152	K <sub>3</sub>	= ( )	K <sub>3</sub>	= ( )

and  $f_1(\Delta t)$  is a function of the indicated difference between top and bottom detectors of the power-range nuclear ion chambers, with gains to be selected based on measured instrument response during plant startup tests such that:

- (i) for  $q_l - q_b$  between -44 percent and +3 percent,  $f_1(\Delta t) = 0$  (where  $q_l$  and  $q_b$  are percent RATED THERMAL POWER in the top and bottom halves of the core respectively, and  $q_l + q_b$  is total THERMAL POWER in percent of RATED THERMAL POWER).
  - (ii) for each percent that the magnitude of  $(q_l - q_b)$  exceeds -44 percent, the  $\Delta T$  trip setpoint shall be automatically reduced by 1.67 percent of its value at RATED THERMAL POWER.
  - (iii) for each percent that the magnitude of  $(q_l - q_b)$  exceeds +3 percent, the  $\Delta T$  trip setpoint shall be automatically reduced by 2.00 percent of its value at RATED THERMAL POWER.

\* Values dependent on NPPC approval of ECCS evaluation for these operating conditions.

\*\* The value for K<sub>1</sub> shall be equal to 1.132 for the period of operation until steam generator replacement.

TABLE 2.2-1 (Continued)  
 REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS  
 NOTATION (Continued)

Note 2:	Overpower $\Delta T \leq \Delta T_0 \left[ K_4 + K_5 \left( \frac{\tau_3 S}{1+\tau_3 S} \right) T - K_6 (T - T') - t_2(\Delta T) \right]$	
Where:	$\Delta T_0$	= indicated $\Delta T$ at RATED THERMAL POWER
	$T$	= Average temperature, °F
	$T'$	= Indicated $T_{avg}$ at RATED THERMAL POWER $\leq 586.8^{\circ}\text{F}$
	$K_4$	= 1.079 *
	$K_5$	= 0.02/°F for increasing average temperature
	$K_5$	= 0 for decreasing average temperatures
	$K_6$	= 0.00164 for $T > T'$ ; $K_6 = 0$ for $T \leq T'$
	$\frac{\tau_3 S}{1+\tau_3 S}$	= The function generated by the rate lag controller for $T_{avg}$ dynamic compensation
	$\tau_3$	= Time constant utilized in the rate lag controller for $T_{avg}$ $\tau_3 = 10$ secs.
	$S$	= Laplace transform operator ( $\text{sec}^{-1}$ )
	$t_2(\Delta T)$	= 0 for all $\Delta T$

Note 3: The channel's maximum trip point shall not exceed its computed trip point by more than 2 percent span.

\* The value for  $K_4$  shall be equal to 1.016 for the period of operation until steam generator replacement.

TABLE 3.2-1  
DNB PARAMETERS

<u>PARAMETER</u>	<u>3 Loops in Operation</u>	<u>2 Loops in Operation ** &amp; Loop Stop Valves Open</u>	<u>2 Loops in Operation ** &amp; Isolated Loop Stop Valves Closed</u>
Reactor Coolant System $T_{avg}$	$\leq 591^{\circ}\text{F}$		
Pressurizer Pressure	$\geq 2205 \text{ psig}^*$		
Reactor Coolant System Total Flow Rate	$\geq 284,000 \text{ gpm}^{***}$		

\* Limit not applicable during either a THERMAL POWER ramp increase in excess of 5% RATED THERMAL POWER per minute or a THERMAL POWER step increase in excess of 10% RATED THERMAL POWER.

\*\* Values dependent on NRC approval of ECCS evaluation for these conditions.

\*\*\* The value for the minimum allowable Reactor Coolant System Total Flow Rate is reduced to 268,500 gpm until steam generator replacement.

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NORTH ANNA - UNIT 1

3/4 2-16

Amendment No. 3,8,16,22,  
37,39,45,84, 105