LIC-95-0045

ENCLOSURE

FORT CALHOUN STATION UNIT NO. 1

SIMULATION FACILITY PERFORMANCE TESTING REPORT

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Omaha Public Power District Fort Calhoun Station

Simulator Certification Renewal Submittal

Owner:	Omaha Public Power District
Operator:	Omaha Public Power District
Manufacturer:	Westinghouse Electric Corporation
Reference Plant:	Fort Calhoun Station, Unit 1
NSSS Vendor:	Combustion Engineering
Turbine Generator Vendor:	General Electric
Rating:	1500 MWth
Date Available for Training:	June 16, 1790
Initial Certification Date:	February 13, 1991

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Uncorrected Test Failures

The Certification program for the Fort Calhoun Station Simulator provides for the periodic performance of Certification Tests. Tests are performed either once per year, once per four years, or at special frequencies. The results of these tests are reviewed by a subject matter expert (SME) who places the test into one of three possible categories.

1. Category 1

Test Completed satisfactorily

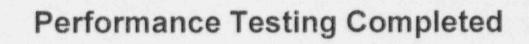
2. Category 2

Test Completed with deficiencies requiring correction, but not significant enough to impact test objectives

3. Category 3

Test Failed. Complete retest required

No tests are currently classified as Category 3; therefore, there are no uncorrected test failures requiring plans for remedy of failures. Some tests are classified as category 2 and are being addressed in accordance with the normal work planning and tracking system.



Test Number:	14.3.3
Test Name:	VERIFICATION OF SPARE COMPUTER TIME
Description:	This test verifies that the simulator is capable of running with enough spare duty cycle to provide real time simulation.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	Simulator duty cycle was measured for steady state and severe transient conditions. The first test initializes into 100% power conditions, Emergency Response Facilities (ERF) computer operating and no non-real time tasks active. The test was run for 15 minutes. Peak and steady state values for duty cycle were collected. The next two tests were multiple malfunction tests MM-1 and MM-3, which were selected as worst case, expending a maximum of calculation time, thus ensuring any less severe scenarios would not
	exceed spare time limits.

Test	Number:	14.4.4
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Test Name: ELEC1: JAL BUS TESTS

Description: This test verifies that the simulated plant electrical bus loads are connected to the correct bus.

Initial Conditions: BOL, 100% Power, Equilibrium Xenon

Test Precis: The simulated Electrical Distribution System was verified correct by the following methods. A database inspection was performed, and it was vified that all bus loads were connected to the correct bus.

The simulator was then run, each bus in turn deenergized, and it was verified that the components supplied by that bus deenergized by spot checking the loads.

Any Uncorrected Test Failures? No

Test	Number:	14.4.5

Test Name: PLANT AIR TESTS

Description: This test verifies that simulated air supplied components are connected to the correct air header.

Initial Conditions: BOL, 100% Power, Equilibrium Xenon

Test Precis: Simulated air system loads were verified correct by the following methods. A database inspection was performed, and it was verified that all air loads were connected to the correct header.

The simulator was then run, each air header was in turn depressurized and it was verified that the components supplied by that header went to their failed positions by spot checking the loads.

Any Uncorrected Test Failures? No

Test Number:	14.5.1.1.1
Test Name:	REACTOR COOLANT SYSTEM TESTING
Description:	To verify that operator conducted surveillance testing can be performed on the reactor coolant system (RCS), the following surveillances were performed:
	Pressurizer level instruments PORV block valves operation Low temperature-over pressure (LTOP) system RCS leak rate test Subcooled margin monitor
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	The pressurizer level instruments surveillance tests the pressurizer level control channels. By varying the pressurizer level transmitter signals, a check of the entire level control system was performed including all charging pump and pressurizer heater on and off signals, and all associated alarms.
	The power operated relief valve (PORV) block valve test stroked each PORV's block valve, and verified the proper operation and position indication of the valves.
	The low temperature-over pressure (LTOP) test was conducted by verifying the logic circuit indicators were enabled and the appropriate annunciators actuated.
	The RCS leak rate testing used the appropriate plant procedures to perform a water inventory balance.
	The subcooled margin monitor surveillance tested the A & B subcooled margin monitors and the A & B qualified safety parameter display system (QSPDS) calculations of P _{sat} , T _{sat}
	The results of the above surveillances showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station surveillance procedures for the RCS.
Simulator Respons	e Assessment: Plant procedures and best estimate
Any Uncorrected T	est Failures? No
Did this test reveal any exception to ANSI/ANS-3.5-1985? No	

Test Number: 14.5.1.1.4 CHEMICAL AND VOLUME CONTROL SYSTEM TESTING Test Name: To verify that operator conducted surveillance testing can be Description: performed on the chemical and volume control system (CVCS) BOL, 100% Power, Equilibrium Xenon Initial Conditions: Various CVCS containment isolation, safety related and non-safety Test Precis: related valves were stroked and compared to Fort Calhoun Station Unit 1 stroke time criteria. Various CVCS pumps were operated during the performance of surveillance tests, and their performance compared to the acceptance criteria of the tests performed. The results of the above surveillance showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station inservice surveillance test for the CVCS.

Simulator Response Assessment: Plant data and best estimate

Any Uncorrected Test Failures? No

Test Number:	14.5.1.1.5		
Test Name:	SAFETY INJECTION SYSTEM TESTING		
Description:	To verify that operator conducted surveillance testing can be performed on the safety injection system (SIS), The following surveillances were performed:		
	Safety injection valves in-service testing Safety injection/containment spray pumps and valves Shutdown cooling valve interlock test		
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon BOL, Cold Shutdown, RCS drained		
Test Precis:	For the safety injection valves in-service test, category A, B, and C safety related safety injection valves were stroked to verify operability. Valve stroke times were verified to be within the allowable band.		
	The safety injection/containment spray pumps and valves test was performed. Safety related valves were time stroked to verify operability. High and low pressure safety injection pump inservice inspections were performed on all safety injection pumps. Safety injection tank check valve test was performed		
	The shutdown cooling (SDC) valve Interlock test was performed. SDC suction valve controls, annunciators, automatic actions and overrides were tested and verified to actuate in response to varying the pressure transmitter inputs.		
	The results of the above surveillances showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station surveillance testing for the safety injection system.		
Simulator Respons	e Assessment: Plant data and best estimate		
Any Uncorrected T	est Failures? No		
Did this test reveal	Did this test reveal any exception to ANSI/ANS-3.5-1985? No		

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Test Number:	14.5.1.1.6
Test Name:	COMPONENT COOLING WATER SYSTEM TESTING
Description:	To verify that operator conducted surveillance testing can be performed on the component cooling water (CCW) system, the CCW pump inservice test surveillance was performed.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	Each component cooling water pump was run for five minutes, then suction and discharge pressure, and indicated pump flow rate were recorded. Total pump head was calculated, and compared to head versus flow pump curve for that pump.
	The results of the above surveillance showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station inservice surveillance test for the component cooling water system.
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Simulator Response Assessment: Plant data and best estimate

Any Uncorrected Test Failures? No

Test Number:	14.5.1.1.16
Test Name:	AUXILIARY FEEDWATER SYSTEM TESTING
Description:	To verify that operator conducted surveillance testing can be performed on the auxiliary feedwater (AFW) system, the following surveillances were performed:
	Auxiliary feedwater pumps inservice inspection Automatic initiation of auxiliary feedwater
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon BOL, Cold Shutdown, RCS Drained
Test Precis:	Auxiliary feedwater motor driven pump FW-6 and turbine driven pump FW-10 were run for an inservice inspection.
	Steam generators RC-2A and RC-2B, auxiliary feedwater initiation and override logic testing was performed.
	Logic matrices were then tested. In each matrix, the actuation alarm, emergency safeguards feature indicating lamp and matrix actuation relays were verified to actuate and reset.
	Functional testing verified auxiliary feedwater valves opening, pump starts, and auxiliary feedwater flow to the steam generators. Emergency safeguards features actuation system logic lamps and annunciators were verified to actuate. Operator overrides and reset of the initiation were verified.
	The results of the above surveillances showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station surveillance testing for the auxiliary feedwater system.
Simulator Response	Assessment: Plant data and best estimate
Any Uncorrected Te	est Failures? No

Test Number: 14.5.1.1.17

Test Name: RAW WATER SYSTEM TESTING

Description: To verify that operator conducted surveillance testing can be performed on the raw water system (RWS), the following surveillances were performed:

> Raw water system valve actuation Raw water valves inservice testing

Initial Conditions: BOL, 100% Power

Test Precis: The raw water system valve actuation test was performed. This test verified the ability to isolate any portion of the raw water system from the control room.

The raw water valves inservice quarterly test was performed.

The raw water inservice pump monthly test was performed. Pump differential pressures, currents and check valve operabilities were verified.

The results of the above surveillances showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station surveillance testing for the raw water system.

Simulator Response Assessment: Plant data and best estimate

Any Uncorrected Test Failures? No

Test	Number:	14.5.1.2.1

Test Name: REACTOR CORE TESTING

Description: To verify that operator conducted surveillance testing can be performed on the reactor core, the reactivity anomalies surveillance was performed.

Initial Conditions: BOL, 100% Power, Equilibrium Xenon

Test Precis: This test analyzed for reactivity deviations by performing a reactivity balance.

The results of the above surveillances showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station surveillance testing for the reactor core.

Simulator Response Assessment: Plant data and best estimate

Any Uncorrected Test Failures? No

Test Number:	14.5.1.2.2
Test Name:	CONTROL ROD DRIVE SYSTEM TESTING
Description:	To verify that operator conducted surveillance testing can be performed on the control rod drive mechanism (CRDM) system, the following surveillances were performed:
	Control element assemblies Secondary CEA position indicating, interlocks, alarms, and display system
Initial Conditions:	BOL, RCS Hot Shutdown, Borated
Test Precis:	The control element assemblies test verified CEA drive cystem interlocks, and alarms. The regulating group withdrawal prohibit, shutdown group insertion permissive, and regulating group upper and lower sequential permissives, were tested for trippable and non- trippable CEAs. The reactor protection system high power and high startup rate pre-trip rod withdrawal prohibit was tested. A reactor trip test was performed to verify all full length CEAs inserted. The manual individual exercise of CEAs was performed by inserting and withdrawing each regulating group and shutdown CEA 6 inches. Secondary CEA position indicating, interlocks, alarms, and display system testing was performed. Single CEA deviation, regulating group
	withdrawal prohibit, shutdown group insertion permissive, group out of sequence, and overlap, permissives, annunciators and setpoints were tested.
	The results of the above surveillances showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station surveillance testing for the CRDM System.
Simulator Respons	e Assessment: Plant data and best estimate
Any Uncorrected T	est Failures? No
Did this test reveal	any exception to ANSI/ANS-3.5-1985-1985? No

Test Number:	14.5.1.2.5
Test Name:	CONTAINMENT VENTILATION SYSTEM TESTING
Description:	To verify that operator conducted surveillance testing can be performed on the containment ventilation system, the following surveillances were performed:
	Containment air cooling and filtering system Containment hydrogen monitors Ventilating air valves inservice testing
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	Containment air cooling units were run, with the operational check of cooling unit dampers performed. Fan current and damper stroke times were satisfactory.
	Containment hydrogen monitors were placed in service.
	Containment pressure relief valves were time stroked shut, and closing times were verified to be within the allowable band. Containment radiation monitor isolation valves were time stroked shut and closing times were verified to be within the allowable band.
Simulator Response	Assessment: Plant data and best estimate
Any Uncorrected Test Failures? No	

Test Number:	14.5.1.2.9
Test Name:	DIESEL GENERATING SYSTEM TESTING
Description:	To verify that operator conducted surveillance testing can be performed on the diesel generating system, the diesel start and diesel fuel oil transfer pump surveillance was performed.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	The emergency diesel generators' responses to auto start signals were tested. The operation of the diesel fuel oil transfer pumps was tested.
	The results of the above surveillances showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station surveillance testing for the emergency diesel generator system.
Simulator Response	e Assessment: Plant data and best estimate

Test Number:	14.5.1.2.10
Test Name:	INPLANT ELECTRICAL DISTRIBUTION SYSTEM TESTING
Description:	To verify that operator conducted surveillance testing can be performed on the inplant electrical distribution system, the following surveillances were performed:
	13.8 KV emergency power DC transfer switches
Initial Conditions:	BOL Cold Shutdown, RCS drained
Test Precis:	This test verified that 13.8 KV emergency power was capable of performing its design function following the simultaneous loss of 345 KV, and 161 KV, off-site AC power and the failure of both on-site diesel generators (i.e., limited station blackout).
	DC transfer switch testing verified the proper transfer from the normal to emergency power supply for transferable inplant 125 vdc control busses.
	The results of the above surveillances showed the simulator capable of

performing within the acceptance criteria of the Fort Calhoun Station surveillance testing for the inplant electrical distribution system.

Simulator Response Assessment: Plant data and best estimate

Any Uncorrected Test Failures? No

Test Number:	14.5.1.2.13
Test Name:	DIESEL GENERATOR SEQUENCER TESTING
Description:	To verify that operator conducted surveillance testing can be performed on the D.G. sequencers, the automatic load sequencers surveillance was performed.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	This test verified the AC and DC engineered safeguards sequencer circuits and time setpoints. The ERF computer was used to capture the timer times for the equipment receiving a timer operate signal. Actuation signal times were verified to be within the allowable band.
	The results of the above surveillances showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station surveillance testing for the D.G sequencers.
Simulator Response	e Assessment: Plant data and best estimate

Test Number:	14.5.1.2.15
Test Name:	REACTOR PROTECTIVE SYSTEM TESTING
Description:	To verify that operator conducted surveillance testing can be performed on the reactor protective system (RPS), the following surveillances were performed:
	RPS normal operation RPS thermal margin/low pressure/T _{ext} Reactor coolant flow Thermal margin/low pressure channels High pressurizer pressure channels Steam generator level channels Steam generator pressure channels High containment pressure channels Turbine loss of load channels Manual trip channels RPS logic units Axial power distribution channels
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon BOL, RCS Hot Shutdown, Borated BOL, Cold Shutdown, RCS Drained
Test Precis:	Reactor protective system normal operation performed a switch alignment and lamp illumination verification.
	The thermal margin/Low pressure/ T_{cod} , channel check and calibration, was performed. This test ensured the four RPS channels T_{cod} were in the allowable band.
	The reactor coolant low glow, alarm and trip channel check was performed. This test verified the four RPS channels' RCS low flow pre- trip and trip logic actions, and annunciator setpoints for four pump operation to be in the allowable band.
	The thermal margin/Low pressure channels, alarm and trip channel check and calibration, was performed.
	Calculations using ${}_{\Delta}$ T power, nuclear power, T _{eve cet} , internal tilt, and correction factors, were performed for each channel. Testing verified the four RPS channels' thermal margin pre-trip and trip logic actions, and annunciator setpoints to be in the allowable band.

The high pressurizer pressure channels, alarm and trip channel check, was performed. This test verified the four RPS channels' high pressurizer pressure pre-trip and trip logic actions, and annunciator setpoints to be in the allowable band.

The steam generator level channels, alarm and trip channel check, was performed. This test verified the four RPS channels for each steam generator's level low pre-trip and trip logic actions, and annunciator setpoints to be in the allowable band.

The steam generator pressure channels, alarm and trip channel check, was performed. This test verified the four RPS channels for each steam generator's pressure and asymmetric steam generator low pretrip and trip logic actions, and annunciator setpoints to be in the allowable band.

The turbine loss of load channels, shutdown alarm and trip channel check, was performed. This test verified that with the turbine off line, the four RPS channels' turbine loss of load trip logic actions, subsequent trip, and annunciations, occurred at 15% nuclear power.

The high containment pressure channels, alarm and trip channel check, was performed. This test verified the four RPS channels for high containment pressure trip logic actions, and annunciation.

The manual trip channels, shutdown alarm and trip channel check, was performed.

The RPS logic units, operation of logic networks and clutch power contactors, was performed. RPS power supplies were tested for nominal voltage, current and ground indications. Each trip unit for each matrix coincidence trip logic combination was tested to actuate. Each matrix trip circuit was in turn, tested to trip each matrix relay, its clutch power supply, load contactor and actuate indicating lamps.

The axial power distribution channels, alarm and trip channel check and calibration was performed. This test verified the high power trip and also verified the four RPS channel's Internal and external axial power distribution, pre-trip and trip logic actions, and annunciator setpoints to be in the allowable band.

The results of the above surveillances showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station surveillance testing for the reactor protective system.

Simulator Response Assessment: Plant data and best estimate Any Uncorrected Test Failures? No Did this test reveal any exception to ANSI/ANS-3.5-1985? No

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Test Number:	14.5.1.2.16
Test Name:	ENGINEERED SAFEGUARDS SYSTEMS TESTING
Description.	To verify that operator conducted surveillance testing can be performed on the engineered safeguards system (ESF), the following surveillances were performed:
	Pressurizer pressure low signal Safety injection actuation Containment pressure high signal Containment spray logic Safety injection refueling water tank (SIRWT) low level signal Steam generator low pressure signal Recirculation actuation logic Offsite power low system
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon BOL, Cold Shutdown, RCS Drained
Test Precis:	The pressurizer pressure low signal (PPLS), alarm and trip channel check, was performed. This test verified the four RPS channels' pressurizer pressure low trip actions, indications and reset setpoints to be in the allowable band. The PPLS and blocking logic calibration refueling test was performed. This test was a functional check of the integrated ESF signals and resulting equipment actuation signals initiated by low pressurizer pressure transmitter signals. The PPLS block (override) actuation and annunciators were verified operable.
	The safety injection actuation signal test was performed. This test was a functional check of the train A integrated ESF signals and resulting equipment actuation signals. Train A PPLS, CPHS, SIAS, CIAS, VIAS lockout relays, containment isolation valves and ERF computer printouts were verified to actuate.

The containment pressure high signal (CPHS), operation check was performed. The CPHS matrix logic was verified to deenergize by actuating pressure switch pairs. The CPHS calibration refueling surveillance was performed. This test was a functional check of the train A CPHS signal and resultant relay actuation signals initiated by high containment pressure transmitter inputs. CPHS, SIAS, CIAS, and VIAS relays were verified to actuate. The containment spray logic signal train A test was performed as a sub test of the safety injection actuation Test. This test verified the operability of the PPLS and CSAS relays. The containment spray actuation test was performed. PPLS, CPHS, SIAS, CIAS, VIAS lockout relays, breakers, and containment isolation valves were verified to actuate.

The safety injection refueling water tank (SIRWT) low level signal monthly channel check was performed. The matrix lamps were verified to deenergize by failing SIRWT level bistables. The SIRWT low level signal refueling surveillance was performed. This test was a functional check of the train A SIRWT low level circuitry and resulting relay actuation signals initiated by SIRWT level bistables. Matrix iamps and STLS relays were verified to actuate.

The steam generator low pressure signal (SGLS), indication and trip channel check was performed. This test verified the four RPS channels' steam generator pressure low trip actions, indications and reset setpoints to be in the allowable band. The SGLS and blocking logic calibration refueling test was performed. This test was a functional check of the ESF train A signals and resulting equipment actuation signals initiated by low steam generator pressure transmitter signals. SGLS alarm, lockout relays and valve actuations were verified to occur. The SGLS Block (override) and attendant annunciators were verified to be operable during each actuation.

The recirculation actuation logic (RAS) channel check was performed as a sub test of the safety injection actuation Test. This test verified the operability of the RAS relays, overrides, matrix lamps and isolation valves. The RAS logic and switch refueling test was performed. CPHS, SIAS, CIAS, VIAS, STLS and RAS lockout relays, breakers, and containment isolation valves were verified to actuate.

The offsite power low system (OPLS) channel check was performed. This test verified the individual operability of OPLS annunciators, matrix relay and sequencer indications for incoming transformers, busses and switchgear. The OPLS matrix refueling check was performed. This test was a functional check of OPLS matrix signals and resulting breaker actuations, crossties, load shed and equipment actuation signals initiated by test switch operation.

The results of the above surveillances showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station surveillance testing for the engineered safeguards system.

Simulator Response Assessment: Plant data and best estimate Did this test reveal any exception to ANSI/ANS-3.5-1985? No

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Test Number:	14.5.1.2.17
Test Name:	NUCLEAR INSTRUMENTATION SYSTEM TESTING
Description:	To verify that operator conducted surveillance testing can be performed on the nuclear instrumentation system (NIS), the following surveillances were performed:
	Power range safety channels Wide range logarithmic channels Rod drop indication
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon BOL, Cold Shutdown, RCS Drained
Test Precis:	The power range safety channels adjustment check and calibration was performed. This test compared plant computer calculated core power to RPS delta T and nuclear instrumentation power, and recalibrated those powers to calculated power as required. The power range safety channels monthly test was performed for eaci channel. Variable over power pre-trip and trip setpoints were verified with respect to linear and delta T power. Linear power upper and lower sub channels, linear power pre-trip and trip were verified.
	The wide range logarithmic channels functional check was performed.

The wide range logarithmic channels functional check was performed. The high DPM (start up rate of change) pre-trip and trip functions were verified to actuate

The rod drop indication check was performed. The results of the above surveillances showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station surveillance testing for the nuclear instrumentation system.

Simulator Response Assessment: Plant data and best estimate

Any Uncorrected Test Failures? No

Test Number:	14.5.1.2.18
Test Name:	INCORE NUCLEAR INSTRUMENTATION TESTING
Description:	To verify that operator conducted surveillance testing can be performed on incore instrumentation, the core exit thermocouples surveillance was performed.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	The core exit thermocouple (CET), channel check was performed. This test verified minimum QSPDS channel A & B valid quadrant CET operability criteria.
	The results of the above surveillance showed the simulator capable of performing within the acceptance criteria of the Fort Calhoun Station surveillance testing for the incore nuclear instrumentation system.
Simulator Response	e Assessment: Plant data and best estimate

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Test Number:	14.5.2.1
Test Name:	ROD WORTH TESTS
Description:	This test verifies that the control rod worths match the reference plant Technical Data Book values.
Initial Conditions:	BOL, reactor critical at approximately 1 MW, below point of adding heat MOL, reactor critical at approximately 1 MW, below point of adding
neat	EOL, reactor critical at approximately 1 MW, below point of adding heat
Test Precis:	All models are frozen with the exception of RFLUX2, RAUXIL, RXCTAH and NIS.
	The rod worths for each regulating group were determined by inserting each group and compensating for the reactivity insertion by dilution to maintain criticality.
	The data collected were plotted using the same axis as the curves in the Technical Data Book, and the curves were compared.
	The shutdown groups were measured in the same way, but the curves were not generated, as there are no curves in the Technical Data Book with which to compare. Total group worths were compared to the Technical Data Book specifications.
Simulator Response	e Assessment: Plant procedures and best estimate

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Test Number:	14.5.2.2	
Test Name:	BORON WORTH TESTS	
Description:	This test verifies that the boron worths match the reference plant Technical Data Book values.	
Initial Conditions:	BOL, reactor critical at approximately 1 MW, below point of adding heat MOL, reactor critical at approximately 1 MW, below point of adding	
neat	EOL, reactor critical at approximately 1 MW, below point of adding heat	
Test Precis:	All models are frozen with the exception of RFLUX2, RAUXIL, RXCTAH and NIS.	
	The boron worths for each core age were determined by running the program CORETEST, which was developed by Westinghouse Electric Inc. for use during factory acceptance testing of the Fort Calhoun Simulator.	
	The results of CORETEST were compared to the technical data book values.	
Simulator Respons	e Assessment: Plant procedures and best estimate	

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Test Name: ISOTHERMAL TEMPERATURE COEFFICIENT

Description: This test verifies that the isothermal temperature coefficient (ITC) matches the reference plant Technical Data Book value.

Initial Conditions: BOL, reactor critical at approximately 1 MW, below point of adding heat

Test Precis: All models are frozen with the exception of RFLUX2, and RXCTAH.

The core inlet and outlet enthalpies were then set to their initial conditions plus 2 btu/lbm and the resultant change in core reactivity was observed.

The reactivity change divided by the enthalpy change (directly convertible to a temperature change of 1.6 °F) results in the isothermal temperature coefficient.

Simulator Response Assessment: Plant Procedures and Best Estimate

Any Uncorrected Test Failures? No

Test Number:	14.5.2.4
Test Name:	POWER COEFFICIENT TEST
Description:	This test verifies that the power coefficient matches the reference plant Technical Data Book value.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	All models are frozen with the exception of RFLUX2, NIS and RXCTAH.
	Boron concentration is held constant as power is decreased by control rod insertion.
	The core inlet and outlet enthalpies are maintained at the proper values manually as power is reduced. When 10% power is reached, the rod worth curves are used to compute the total reactivity inserted to determine the power defect. The result is compared to the Technical Data Book values.
Simulator Response	e Assessment: Plant procedures and best estimate

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Test Number:	14.5.2.5
Test Name:	XENON TESTS
Description:	This test verifies that the Xenon concentration matches the reference plant Technical Data Book values.
Initial Conditions:	BOL, 100% Power Equilibrium Xenon BOL, 80% Power Equilibrium Xenon BOL, 50% Power Equilibrium Xenon BOL, 30% Power Equilibrium Xenon MOL, 100% Power Equilibrium Xenon MOL, 80% Power Equilibrium Xenon MOL, 50% Power Equilibrium Xenon EOL, 30% Power Equilibrium Xenon EOL, 100% Power Equilibrium Xenon EOL, 55% Power Equilibrium Xenon

Test Precis: The simulator was initialized into each initial condition listed and the Xenon concentration was compared to the Technical Data Book.

The simulator was tripped from 100% power MOL and Xenon plotted for 48 hours run time. The data collected were plotted and compared to the Technical Data Book curve.

A Xenon oscillation was initiated by dropping and then recovering a control rod. It was then verified that the Xenon oscillation produced could be damped by the use of control rods.

Simulator Response Assessment: Plant procedures and best estimate

Any Uncorrected Test Failures? No

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Test Number:	14.5.2.6
Test Name:	ESTIMATED CRITICAL POSITION TESTS
Description:	This test verifies that the estimated critical positions could be predicted within the tolerance of the Technical Data Book.
Initial Conditions:	BOL, 100% Power Equilibrium Xenon MOL, 100% Power Equilibrium Xenon EOL, 100% Power Equilibrium Xenon
Test Precis:	The simulator was initialized into each initial condition listed, tripped and restarted after calculating an Estimated Critical Conditions Worksheet. The results of the worksheets and simulator performance were compared to the Technical Data Book.
Simulator Response	e Assessment: Plant procedures and best estimate

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Test Number: 14.5.3.1

Test Name: NORMAL OPERATIONS TEST

Description: This test verifies the simulator capable of simulating real time plant operations of Fort Calhoun Station Unit 1.

Initial Conditions: BOL, 100% Power, Equilibrium Xenon

Test Precis: This test was performed with operating procedures and operating Instructions, using local operator actions (LOAs), where appropriate, and non-applicable plant specific tasks (notifications, approvals, manual valve lineups, etc.) annotated as not applicable (N/A).

The test was begun with a normal station shutdown to refueling conditions. Boration rates and amounts were verified to be consistent with plant references and operator experience.

Following shutdown cooling (SDC) initiation, a subsequent cooldown and drain down of the pressurizer to mid-loop conditions was conducted.

Pressurizer refill and bubble formation were completed. Pressurizer heatup rate and bubble formation were verified to be consistent with operator experience.

A plant heatup to normal operating pressure and temperature (NOP & NOT) was performed. Reactor coolant pump heat was used and verified to be consistent with plant data, and operator experience.

A dilution to reactor criticality was performed with dilution rate and amounts verified to be consistent with plant references and operator experience. Nuclear instrumentation response to the dilution and criticality was also verified to be consistent with operator experience.

The point of adding heat response was verified to be consistent with plant references and operator experience. Turbine warm-up and synchronization were performed. The rate of condenser vacuum rise was verified to be consistent with the vacuum pump(a) in service.

The main turbine warm up and roll was verified to be consistent with plant references and operator experience.

An increase in power to 100% was conducted and the feedwater pump capacity was verified to be consistent with plant references and operator experience.

Simulator Response Assessment:Plant data and best estimateAny Uncorrected Test Failures?NoDid this test reveal any exception to ANSI/ANS-3.5-1985?No

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Test Number:	14.5.3.2.1
Test Name:	STEADY STATE DRIFT TEST AT 100% POWER
Description:	This test verified the simulator computed values for 100% power were stable and met ANSI/ANS-3.5-1985 specifications.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	This test was performed by initializing into a 100% power steady state configuration, with controls in automatic, and acquiring data every three (3) minutes for one hour.
	Personnel monitored plant parameters on the instructor control CRT, on the control boards and on the simulator ERF. Following the test, captured data were examined for deviations.
Simulator Response	Assessment: Plant Data
Any Uncorrected Tes	Failures? No

Did this test reveal any exception to ANSI/ANS-3.5-1985? No

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Test Number: 14.5.3.2.2

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Test Name: STEADY STATE DRIFT TEST AT 80% POWER

Description: This test verified the simulator computed values for 80% power were stable and met ANSI/ANS-3.5-1985 specifications.

Initial Conditions: BOL, 80% Power, Equilibrium Xenon

Test Precis: This test was performed by initializing into an 80% power steady state configuration, with controls in automatic, and acquiring data every three (3) minutes for one hour.

Personnel monitored plant parameters on the instructor control CRT, on the control boards and on the simulator ERF. Following the test, captured data were examined for deviations.

Simulator Response Assessment: Plant Data

Any Uncorrected Test Failures? No

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Test Name: STEADY STATE DRIFT TEST AT 55% POWER

Description: This test verified the simulator computed values for 55% power were stable and met ANSI/ANS-3.5-1985 specifications.

Initial Conditions: BOL, 55% Power, Equilibrium Xenon

Test Precis: This test was performed by initializing into a 55% power steady state configuration, with controls in automatic, and acquiring data every three (3) minutes for one hour.

Personnel monitored plant parameters on the instructor control CRT, on the control boards and on the simulator ERF. Following the test, captured data were examined for deviations.

Simulator Response Assessment: Plant Data

Any Uncorrected Test Failures? No

Test Name:	STEADY STATE DRIFT TEST AT 30% POWER
Description:	This test verified the simulator computed values for 30% power were stable and met ANSI/ANS-3.5-1985 specifications.
Initial Conditions:	BOL, 30% Power, Equilibrium Xenon
Test Precis:	This test was performed by initializing into a 30% power steady state configuration, with controls in automatic, and acquiring data every three (3) minutes for one hour.
	Personnel monitored plant parameters on the instructor control CRT, on the control boards and on the simulator ERF. Following the test, captured data were examined for deviations.
Simulator Response	Assessment: Plant Data
Any Uncorrected Te	st Failures? No

Did this test reveal any exception to ANSI/ANS-3.5-1985? No

Test Number: 14.5.3.2.4

Test Number:	14.5.3.3.1	
Test Name:	STEADY STATE ACCURACY TEST AT 100% POWER	
Description:	This test verified the simulator computed values and meter indications for 100% power conditions.	
	The testing ensured critical and non critical parameters were accurate, and within tolerance when compared to Fort Calhoun Station Unit 1 at full power.	
	Principal mass and energy balance calculations were performed during this test.	
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon	
Test Precis:	This test was performed by initializing into a 100% power steady state configuration, with the controls in automatic. Steam flow was then adjusted to the values given as baseline data. Main condenser vacuum, circulating water temperature, and power factor were adjusted as required to maintain the baseline value.	
	The plant was allowed to stabilize, then computer as well as control board instrument data collection was performed.	
	Personnel performed the following mass and energy balances:	
	Indication of reactor power based on delta T Reactor power based on steam flow Core thermal power calculation Reactor coolant system leak rate calculation	
Simulator Response	Simulator Response Assessment: Plant data and best estimate	
Any Uncorrected Test Failures? No		

Did this test reveal any exception to ANSI/ANS-3.5-1985? No

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Test Number:	14.5.3.3.2	
Test Name:	STEADY STATE ACCURACY TEST AT 80% FOWER	
Description:	This test verified the simulator computed values and meter indications for 80% power conditions. The testing ensured critical and non critical parameters were accurate, and within tolerance when compared to Fort Calhoun Station Unit 1 at 80% of full power. Principal mass and energy balance calculations were performed during this test.	
Initial Conditions:	BOL, 80% Power, Equilibrium Xenon	
Test Precis:	This test was performed by initializing into a 80% power steady state configuration, with the controls in automatic. Steam flow was then adjusted to the values given as baseline data. Main condenser vacuum, circulating water temperature, and power factor were adjusted as required to maintain the baseline value.	
	The plant was allowed to stabilize, then computer as well as control board instrument data collection was performed.	
	Personnel performed the following mass and energy balances:	
	Indication of reactor power based on delta T Reactor power based on steam flow Core thermal power calculation Reactor coolant system leak rate calculation	
Simulator Response Assessment: Plant data and best estimate		

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Test Number:	14.5.3.3.3
Test Name:	STEADY STATE ACCURACY TEST AT 55% POWER
Description:	This test verified the simulator computed values and meter indications for 55% power conditions. The testing ensured critical and non critical parameters were accurate, and within tolerance when compared to Fort Calhoun Station Unit 1 at 55% of full power. Principal mass and energy balance calculations were performed during this test.
Initial Conditions:	BOL, 55% Power, Equilibrium Xenon
Test Precis:	This test was performed by initializing into a 55% power steady state configuration, with the controls in automatic. Steam flow was then adjusted to the values given as baseline data. Main condenser vacuum, circulating water temperature, and power factor were adjusted as required to maintain the baseline value.
	The plant was allowed to stabilize, then computer as well as control board instrument data collection was performed.
	Personnel performed the following mass and energy balances:
	Indication of Reactor power Based on delta T Reactor power Based on steam Flow Core thermal power Calculation Reactor Coolant system leak Rate Calculation
Simulator Respons	e Assessment: Plant data and best estimate

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Test Number:	14.5.3.3.4
Test Name:	STEADY STATE ACCURACY TEST AT 30% POWER
Description:	This test verifies the simulator computed values and meter indications for 30% power conditions. The testing ensured critical and non critical parameters were accurate, and within tolerance when compared to Fort Calhoun Station Unit 1 at 30% of full power. Principal mass and energy balance calculations were performed during this test.
Initial Conditions:	BOL, 30% Power, Equilibrium Xenon
Test Precis:	This test was performed by initializing into a 30% power steady state configuration, with the controls in automatic. Steam flow was then adjusted to the values given as baseline data. Main condenser vacuum, circulating water temperature, and power factor were adjusted as required to maintain the baseline value.
	The plant was allowed to stabilize, then computer as well as control boarJ instrument data collection was performed.
	Personnel performed the following mass and energy balances:
	Indication of reactor power based on delta T Reactor power based on steam flow Core thermal power Calculation Reactor coolant system leak rate calculation
Simulator Response	e Assessment: Plant data and best estimate

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Test Number:	14.5.4.1
Test Name:	MAXIMUM RATE POWER RAMP
Description:	This test verified the ability of the simulator to respond to a maximum rate down power in a realistic fashion.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	The test was performed by initializing into 100% power conditions, with the following systems in automatic:
	Pressurizer level control Pressurizer pressure control Letdown temperature control Volume control tank inlet control Steam generator level controls Steam dump and turbine bypass system control
	Data collection was initiated, then in accordance with AOP-5, a rapid load reduction to 20% power was performed at a 10% per minute

load reduction was initiated, then in accordance with AOP-5, a rapid load reduction to 20% power was performed at a 10% per minute ramp. Manual control of control rods, letdown pressure and main turbine control valves were the only manipulations performed.

Testing resulted in the reactor still critical, with no safety valves lifted, and in 10 minutes plant parameter trends were stabilizing.

Simulator Response Assessment. Best Estimate

Any Uncorrected Test Failures? No

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Test Number:	14.5.4.2
Test Name:	MAIN TURBINE STOP AND CONTROL VALVE TEST
Description:	This test verified the ability of the simulator to respond to main turbine stop, intermediate and control valve testing in a realistic fashion.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	The test was performed by initializing into 100% power conditions, with the following systems in automatic:
	Pressurizer level control Pressurizer pressure control Letdown temperature control Volume control tank inlet control Steam generator level controls Steam dump and turbine bypass system control
	Data collection was initiated, then in accordance with OI-ST-10, testing of the main turbine stop valves was performed.
	Data collection was again initiated, then in accordance with OI-ST-10, testing of the main turbine intermediate valves was performed.

Testing continued with data collection, and then in accordance with OI-ST-10, tests of the main turbine intermediate valves IV-1 through 4 were performed.

Testing showed the integrated plant response to be realistic, self dampening and that station procedures could be used.

Simulator Response Assessment: Plant data and best estimate

Any Uncorrected Test Failures? No

Test Number:	14.5.4.3
Test Name:	INADVERTENT BORATION/DILUTION TEST
Description:	This test verified the ability of the simulator to respond to a dilution and boration event at full power in a realistic fashion.
nitial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	The test was performed by initializing into a 100% power configuration, with the following conditions:
	CEAs fully withdrawn Pressurizer level control in auto Pressurizer pressure control in auto CVCS in normal operation Steam generator level controls in auto Steam dump and turbine bypass system control in auto
	Data collection was initiated, then a continuous dilution was initiated by aligning demineralized water to the charging pump suctions and starting an additional two charging pumps.
	A reactor trip on thermal margin/Low pressure (TM/LP) or variable high power trip was verified to occur. Then the dilution was secured and the plant allowed to stabilize.
	The test continued following reinitialization to 100% power, and the initiation of data collection. A continuous boration was initiated by starting both boric acid pumps, aligning the discharge to the charging pump suctions and starting an additional two charging pumps.
	A reactor trip on thermal margin/Low pressure (TM/LP) was verified to occur. Then the boration was secured and the plant was allowed to stabilize.
	Testing showed the plant response to be realistic.
Simulator Respons	e Assessment: Best Estimate
Any Uncorrected T	est Failures? No
Did this test reveal	any exception to ANSI/ANS-3.5-1985? No

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Test Number:	14.5.4.4
Test Name	REACTOR TRIP AND RECOVERY TEST
Description:	This test verified the ability of the simulator to perform a reactor trip and subsequent restart in a realistic fashion.
Initial Conditions:	BOL, 80% Power, Equilibrium Xenon
Test Precis:	The test was performed by initializing into 80% of full rated power conditions, with the following systems in automatic:
	Pressurizer level control Pressurizer pressure control Letdown temperature control

Volume control tank inlet control

Steam generator level controls Steam dump and bypass system control Data collection was begun, and the reactor trip pushbutton was

depressed, initiating the transient. Operator control manipulations were performed to model as closely as possible the Fort Calhoun Station trip transient data being used. Following plant stabilization, simulator data and Fort Calhoun Station trip data were compared.

Using operating procedures, the reactor was started up and returned to nominal full power conditions.

Simulator Response Assessment: Plant data and Best Estimate

Any Uncorrected Test Failures? No

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Test Number:	14.5.4.5
Test Name:	DROPPED ROD TEST
Description:	This test verified the ability of the simulator to respond to a single dropped control element assembly (CEA) in a realistic fashion.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	The test was performed by initializing into 100% full rated power conditions, with the following systems in automatic:
	Pressurizer level control Pressurizer pressure control Letdown temperature control Volume control tank inlet control Steam generator level controls Steam dump and bypass system control
	Data collection was initiated, and CEA 40 was dropped. Changes s

Data collection was initiated, and CEA 40 was dropped. Changes such as lowered nuclear instrumentation readings in the affected quadrant, core power shift, with lowered reactor coolant system temperatures were verified to occur. Following plant stabilization, data analysis showed the plant response to be realistic.

Simulator Response Assessment: Best Estimate

Any Uncorrected Test Failures? No

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Test Number:	14.5.4.6
Test Name:	MANUAL REACTOR TRIP TEST
Description:	This test verified the ability of the simulator to conform to a baseline manual reactor trip in a realistic fashion.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	The test was performed by initializing into 100% power conditions, with systems verified to be in normal full power configuration. A five minute stability check was performed. Data collection was begun, and the reactor trip pushbutton was depressed, initiating the transient.
	Other than manual letdown pressure control, no operator control manipulations were performed. Hot standby conditions were verified maintained in automatic, and following stabilization, testing was concluded. Simulator data were then analyzed to verify acceptance criteria.
Simulator Response	e Assessment: Plant data and Best Estimate

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Test Number: 14.5.4.7 Test Name: SIMULTANEOUS TRIP OF MAIN FEEDWATER PUMPS TEST Description: This test verified the ability of the simulator to conform to a baseline simultaneous trip of all feedwater pumps in a realistic fashion. Initial Conditions: BOL, 100% Power, Equilibrium Xenon Test Precis: The test was performed by initializing into 100% power conditions, with systems verified to be in normal full power configuration. A five minute stability check was performed. Data collection was begun, and the main feedwater pumps were tripped simultaneously, initiating the transient. Other than manual letdown pressure control, no operator control manipulations were performed. Uncomplicated reactor trip criteria were verified maintained in automatic, and following trend stabilization, testing was concluded. Simulator data were then analyzed to determine if the acceptance criteria were met. Simulator Response Assessment: Best Estimate

Any Uncorrected Test Failures? No

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Test Number:	14.5.4.8
Test Name: TEST	SIMULTANEOUS CLOSURE OF MAIN STEAM ISOLATION VALVES
Description:	This test verified the ability of the simulator to conform to a baseline simultaneous closure of main steam isolation valves in a realistic fashion.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	The test was performed by initializing into 100% power conditions, with systems verified to be in normal full power configuration. A five minute stability check was performed. Data collection was begun, and the main steam isolation valves (MSIVs) were manually shut simultaneously, initiating the transient.
	Other than manual letdown pressure control, no operator control manipulations were performed. Uncomplicated reactor trip criteria were verified maintained in automatic, and following trend stabilization, testing was concluded. Simulator data were then analyzed to determine if the acceptance criteria were met.
Simulator Response	e Assessment: Best Estimate
Any Uncorrected Te	est Failures? No

Did this test reveal any exception to ANSI/ANS-3.5-1985? No

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Test Number: 14.5.4.9 SIMULTANEOUS TRIP OF ALL RCPs TEST Test Name: This test verified the ability of the simulator to conform to a baseline Description: simultaneous trip of all reactor coolant pumps in a realistic fashion. BOL. 100% Power, Equilibrium Xenon Initial Conditions: Test Precis: The test was performed by initializing into 100% power conditions, with systems verified to be in normal full power configuration. A five minute stability check was performed. Data collection was begun, the reactor coolant pumps were then tripped simultaneously, initiating the transient. Other than manual letdown pressure control, no operator control manipulations were performed. Uncomplicated reactor trip criteria were verified maintained in automatic, and following trend stabilization, testing was concluded. Simulator data were then analyzed to determine if the acceptance criteria were met.

Simulator Response Assessment: Best Estimate

Any Uncorrected Test Failures? No

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Test Number: 14.5.4.10

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Test Name: TRIP ANY RCP TEST

Description: This test verified the ability of the simulator to conform to a baseline trip of any single reactor coolant pump in a realistic fashion.

Initial Conditions: BOL, 100% Power, Equilibrium Xenon

Test Precis: The test was performed by initializing into 100% power conditions, with systems verified to be in normal full power configuration. A five minute stability check was performed. Data collection was begun, and one reactor coolant pump was tripped initiating the transient. Other than manual letdown pressure control, no operator control manipulations were performed. Uncomplicated reactor trip criteria were verified maintained in automatic, and following trend stabilization, testing was concluded. Simulator data were then analyzed to determine if the acceptance criteria were met.

Simulator Response Assessment: Best Estimate

Any Uncorrected Test Failures? No

Test Number: 14.5.4.11

Test Name: LOSS OF LOAD TEST

Description: This test verified the ability of the simulator to conform to a baseline main turbine trip in a realistic fashion.

Initial Conditions: BOL, 55% Power, Equilibrium Xenon

Test Precis: The test was performed by initializing into 55% power conditions, with systems verified to be in a normal configuration. A five minute stability check was performed. Data collection was begun, and the main turbine was manually tripped, initiating the transient. Other than manual letdown pressure control, no operator control manipulations were performed. Uncomplicated reactor trip criteria were verified maintained in automatic, and following trend stabilization, testing was concluded. Simulator data were then analyzed to determine if the acceptance criteria were met.

Simulator Response Assessment: Plant data and Best Estimate

Any Uncorrected Test Failures? No

ANSI/ANS-3.5-1985 Test Exception:

TRANSIENT TEST (APPENDIX B) B.2.2(6) TEST EXCEPTION

An exception to ANSI/ANS-3.5-1985 is taken for this test, due to Fort Calhoun Station Unit 1 plant configuration and operation.

Fort Calhoun Station system design criteria stipulate the automatic actuation of a turbine trip-unit trip interlock at 15% power. Station procedures require main generator synchronization at 12% power. Load is then applied to avoid a generator reverse power trip. Loading and its subsequent feedwater heater extraction steam load combine to raise power to above the level at which the loss of load trip is bypassed. Therefore, for the Fort Calhoun Station simulator, testing for main turbine trip (maximum power level which does not result in an immediate reactor trip) is not performed, as there is no power level at which this test is applicable.

Test Number:	14.5.4.12
Test Name:	MAXIMUM RATE POWER RAMP TEST
Description:	This test verified the ability of the simulator to conform to a baseline maximum rate power ramp in a realistic fashion.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	The test was performed by initializing into 100% power conditions, with systems verified to be in normal full power configuration. A five minute stability check was performed. Data collection was begun, and secondary load was rapidly lowered to 75% power, initiating the transient. Following a five minute stabilization, power was rapidly returned to 100% power. Operator control manipulations were performed. Normal full power conditions were verified, and following trend stabilization, testing was concluded. Simulator data were then analyzed to determine if the acceptance criteria were met.

Simulator Response Assessment: Best Estimate

Any Uncorrected Test Failures? No

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Test Number:	14.5.4.13
Test Name:	LOCA WITH LOSS OF ALL OFFSITE POWER TEST
Description:	This test verified the ability of the simulator to conform to a baseline maximum size reactor coolant system rupture combined with a loss of all offsite power in a realistic fashion.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	The test was performed by initializing into 100% power conditions, with systems verified to be in normal full power configuration. A five minute stability check was performed. Data collection was begun, and the simulator set to simultaneously insert a maximum size LOCA with a concurrent total loss of offsite power. No operator control manipulations were performed. Safety functions status checks were verified, and following stabilization, testing was concluded. The simulator data were then analyzed to determine if the acceptance criteria were met.

Simulator Response Assessment: Best Estimate

Any Uncorrected Test Failures? No

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Test Number:	14.5.4.14
Test Name:	EXCESS STEAM DEMAND TEST
Description:	This test verified the ability of the simulator to conform to a baseline maximum size unisolable main steam line rupture in a realistic fashion.
Initial Conditions:	BOL, 100% Power, Equilibrium Xenon
Test Precis:	The test was performed by initializing into 100% power conditions, with systems verified to be in normal full power configuration. A five minute stability check was performed. Data collection was begun, and the simulator set to insert a maximum sized unisolable steam line rupture. No operator control manipulations were performed. Safety functions status check was verified satisfied, and following trend stabilization, testing was concluded. The simulator data were then analyzed to determine if the acceptance criteria were met.
Simulator Response	e Assessment: Best Estimate

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14.5.4.15
SLOW RCS DEPRESSURIZATION TO SATURATION, NO HPSI TEST
This test verified the ability of the simulator to conform to a baseline slow primary system depressurization to saturated conditions using a pressurizer relief valve stuck open with actuation of high pressure ECCS inhibited, in a realistic fashion.
BOL, 100% Power, Equilibrium Xenon
The test was performed by initializing into 100% power conditions, with systems verified to be in normal full power configuration. A five minute stability check was performed. All high pressure safety injection and non-running charging pumps were disabled, and data collection was begun. Reactor coolant pumps were tripped in accordance with plant procedures, with no other operator control manipulations performed. Safety functions status check was verified challenged, and following trend stabilization, testing was concluded. The simulator data were then analyzed to determine if the acceptance criteria were met.

Simulator Response Assessment: Best Estimate

Any Uncorrected Test Failures? No

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Test Number:	14.5.5.1.4		
Malfunction Identifier:	AFW4		
Test Description:	Emergency feedwater storage tank leak. A variable size leak occurs on the discharge line upstream of FW-339.		
Initial Conditions:	100% Power, BOL		
	Options Available:	Options Used:	
	Magnitude 0-100% 100% = 8" Line Break	Magnitude 100%	
	Ramp Time 0-3600 s	Ramp Time 0 s	
	Delay Time 0-3600 s	Delay Time 0 s	
	Mode Direct/Remote/Conditional	Direct	
Test Precis:	Following malfunction actuation, observed: auxiliary feedwater storage tank level decreased continuously. LCV-1173 opens to fill tank from condensate system; LCV-1190 opens to make up to condenser from condensate storage tank; condensate storage tank level low, auxiliary feedwater tank high-low, auxiliary feedwater tank		

level low, auxiliary feedwater tank high-low, auxiliary feedwater tank low, emergency feedwater storage tank low-low alarms annunciate; LCV-1189 opens to fill auxiliary feedwater tank from demineralized water; waste disposal system malfunction alarm; spent regenerant tank overflows.

Operator starts demineralized water pumps and secures makeup to the auxiliary feedwater storage tank, then verifies sump level returns to normal after tank empties.

Any Uncorrected Test Failures? No

Test Number: 14.5.5.1.5 Test Description: Auxiliary Feedwater Activation Relay Failure AFW5 Malfunction Identifier: Auxiliary feedwater activation relay failure Test Description: Initial Conditions: 100% Power, BOL Options Used: Options Available: Selection A, B, C, D Selection A Energized/Deenergized Energized Ramp Time 0-3600 s Ramp Time 0 s Delay Time 0-3600 s Delay Time 0 s Mode Direct Direct/Remote/Conditional Test Parameters Monitored: None

Test Precis: Following malfunction actuation, observed: the correct channel matrix actuation relay light illuminated, along with the associated auxiliary feedwater system steam generator channel actuated alarm. Auxiliary feedwater feed valves opened and the auxiliary feedwater pumps started (both electric and steam driven). Verified auxiliary feedwater flow to both steam generators.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.2.2	
Malfunction Identifier:	CAS2	
Test Description:	Service air system leak. A variable siz service air line(s).	e leak occurs on the selected
Initial Conditions:	100% Power, BOL	
	Options Available:	Options Used:
	Selection A, B, C	Selection A
	Magnitude 0-100%	Magnitude 100
	Ramp Time 0-3600 s	Ramp Time 0 s
	Delay Time 0-3600 s	Delay Time 0 s
	Mode Direct/Remote/Conditional	Direct
Test Parameters Monit	ored: None	

Test Precis: Following malfunction actuation, observe: plant air pressure drop, standby compressor starts, air pressure low alarms actuate, at 80 psig service air header isolation valve PCV-1753 closes, instrument air pressure stabilizes; services air pressure fluctuates with PCV-1753. Operator isolates leak by closing manual isolation valve, then verifies that pressure stabilizes.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.2.3	
Malfunction Identifier:	CAS3	
Test Description:	Instrument air loop leak. A variabl Instrument air loop(s).	e size leak occurs on the selected
Initial Conditions:	100% Power, BOL	
	Options Available:	Options Used:
	Selection A, B, C	Selection B
	Delay Time 0-3600 s	Delay Time 0 s
	Mode Direct/Remote/Conditional	Direct
Test Parameters Monito	ored: None	

Test Precis: Following malfunction actuation, observe: air header pressure drops, standby compressor starts, air pressure low alarms actuate, operator isolates leak by closing isolation valve, then verifies that pressure recovers and stabilizes.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.2.4	
Malfunction Identifier:	CAS4	
Test Description:	Instrument air riser leak. A variable instrument air riser(s).	size leak occurs on the selected
Initial Conditions:	100% Power, BOL	
	Options Available:	Options Used:
	Selection A-J	Selection A
	Delay Time 0-3600 s	Delay Time 0 s
	Mode Direct/Remote/Conditional	Direct
Test Parameters Monit	ored: None	
Test Precis:	Following malfunction actuation, ob	serve: air riser pressure drops,

Test Precis: Following malfunction actuation, observe: air riser pressure drops, standby compressor starts, air pressure low alarms actuate, operator isolates leak by closing manual isolation valve, then verifies that pressure recovers and stabilizes.

Any Uncorrected Test Failures? No

Test Number: 14.5.5.3.4	Test	Number:	14	.5	5.	3.	4
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Malfunction Identifier: CCW4

Test Description:

Component cooling water (CCW) pump discharge header leak. A variable size leak occurs on the component cooling water pump discharge header.

Initial Conditions:

100% Power, BOL Options Available:

Options Used:

Magnitude 0-100% 100% = 16" Line Break Magnitude: 100%

Ramp Time 0-3600s

Delay Time 0-3600 s Mode D Direct/Remote/Conditional Ramp Time: 60 s

Delay Time: 0 s

Test Parameters Monitored:

CCW system pressure CCW system flow CCW surge tank level Reactor coolant pump seal and lube oil temperatures Waste disposal system tank level alarms

Test Precis:

Following malfunction actuation, observed: component cooling water system pressure dropped, flow increased, surge tank level alarms actuated as level decreased, auto make-up system initiated filling surge tank. Components cooled by the component cooling water system showed flow decreases and temperature increases. Waste disposal system showed an increase in inventory due to the leakage. Raw water backup cooling was initiated to the components supplied and a temperature decrease was observed as the raw water cooling was placed in service.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.3	.5	
Malfunction Identifier:	CCW5		
Test Description:	Component cooling water heat exchanger tube leak. Tube failure occurs to a selectable degree in the selected heat exchanger.		
Initial Conditions:	100% P	ower, BCL	
	Options Available: Selection A, B, C, D		Options Used:
			Selected: A
	Magnitude 0 - 100%		Magnitude 100%
Test Parameters Monitored:		CCW system flow CCW surge tank level	
Test Precis:	water sy		erved: component cooling / increased, surge tank level

water system pressure dropped, flow increased, surge tank level alarms actuated as level decreased, auto make-up system initiated filling. Components cooled by the component cooling water system showed flow decreases and temperature increases.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.4.	1	
Malfunction Identifier:	CND1		
Test Description:	Loss of main condenser vacuum. Air leakage into the condenser causes pressure to rise.		
Initial Conditions:	100% Power, BOL		
	Options Available:		Options Used:
	Magnitude 0-100% 100% = Vac Bkr Open		Magnitude 100%
	Ramp Time 0-3600 s		Ramp Time 0 s
	Delay Ti	me 0-3600 s	Delay Time 0 s
	Mode Direct/Remote/Conditional		Direct
Test Parameters Monitored:		Condensers A and B pressures Condensers exhaust hood temperatures Reactor power Generator megawatts	
Test Precis:	Following malfunction actuation, observed: condenser A vacuum decreases faster than condenser B vacuum; standby vacuum pump starts with attendant alarm annunciation; exhaust high pressure alarms annunciate; exhaust hood temperature rises, generator output decreases, reactor trips approximately 15 minutes after		

Did this test reveal any exception to ANSI/ANS-3.5-1985? No

malfunction actuation.

Test Number:	14.5.5.4.	4	
Malfunction Identifier:	CND4		
Test Description:	Condensate pump bearing failure. The selected condensate pump(s) experiences bearing failure.		
Initial Conditions:	100% Power, BOL		
	Options	Available	Options Used:
	Selection A, B, C		Selection A
	Magnitud	de 0-100%	Magnitude 100%
	Ramp Time 0-3600 s Delay Time 0-3600 s		Ramp Time 0 s
			Delay Time 0 s
	Mode Direct/Remote/Conditional		Direct
Test Parameters Monitored:		Condensate pump A discharge pressure Condensate pump FW-2A current	
Test Precis:	Following malfunction actuation, observe: condensate pump A current rises sharply, then decreases to 0 after pump seizes; pump trips with attendant overload trip alarm; discharge pressure decreases to 0; standby condensate pump starts normally.		
Any Uncorrected Test F	Failures?	No	

Test Number:	14.5.5.4.5		
Malfunction Identifier:	CND5		
Test Description:	Condensate cooler tube leak. Tube failure occurs to a selectable degree in the condensate cooler.		
Initial Conditions:	100% Pc	ower, BOL	
	Options Available:		Options Used:
	Magnitude 0-100, 100% = 10% of Tubes		Magnitude 100%
	Ramp Time 0-3600 s Delay Time 0-3600 s		Ramp Time 0 s
			Delay Time 0 s
	Mode Direct/Remote/Conditional		Direct
Test Parameters Monitored:		Condenser hotwell level Condensate storage tank level Condensate cooler outlet header temperature Stator cooler inlet temperature	
Test Precis:	Following malfunction actuation, observed: condensate storage tank level decreased, and heat exchanger temperature irregularities on stator coolers and hydrogen coolers. Operator isolates and bypasses condensate cooler, then verifies that stator and hydrogen cooler temperatures stabilize at higher values.		
Any Uncorrected Test F	Failures?	No	

Test Number:	14.5.5.4.8		
Malfunction Identifier:	CND8		
Test Description:	Hotwell level control failure. The hotwell level controller fails to a selectable setpoint.		
Initial Conditions:	100% Power, BOL.		
	Options Available:	Options Used:	
	Selection 0-48"	Selection 48"	
	Ramp Time 0-3600 s	Ramp Time 0 s	
	Delay Time 0-3600 s	Delay Time 0 s	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monito	ored: Condenser hotwell level Condensate storage tank l	evel	
Test Precis:	Following malfunction actuation, observed: hotwell level increase, high level alarm annunciation level indication stabilized at 48", condensate storage tank level decreased.		
Any Uncorrected Test	Colluran2 No		

Test Number:	14.5.5.6.3		
Malfunction Identifier:	CRD3		
Test Description:	Failure of individual rod raise relay. The selected relay fails to the state selected.		
Initial Conditions:	100% Power, BOL		
	Options Available:	Options Used:	
	Selection 1-41	Selection 1	
	Magnitude D, E Deenergized/Energized	Magnitude E	
	Ramp Time	Ramp Time 0	
	Delay Time 0-3600 s	Delay Time 60 s	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monitor	ored: None		

Test Precis: Following malfunction actuation, observe group 4 rod 1 outward motion . Operator attempts to insert rods in manual group and manual individual modes and observes: rod deviation alarms, a rod block signal, and the withdraw lights for group 4 remain on. Rod outward motion stops when mode switch is taken to off.

Any Uncorrected Test Failures? No

Test Number. 14.5.5.0.4	Test	Number:	14.5.5.	6.4
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Test Description:

Failure of individual rod lower relay. The selected relay fails to the state selected.

Initial Conditions:

100% Power, BOL

Options Available:

Selection 1-41

Magnitude D, E Deenergized/Energized

Ramp Time

Delay Time 0-3600 s

Mode Direct/Remote/Conditional

None

Options Used:

Selection 1

Magnitude D

Ramp Time 0

Delay Time 0 s

Direct

Test Parameters Monitored:

Test Precis: Following malfunction actuation, insert group 4 rods and observe: group 4 lower lights on, rod 1 position indication not changing, group 4 rods (except rod 1) inserting.

> Operator selects manual Individual on rod mode selector switch and verifies that rod 1 will not insert. Operator verifies normal outward motion of rod 1

Any Uncorrected Test Failures? No

Test Number:	14	5	5	6	5	
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Test Description:

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Stuck rod. The selected rod sticks and does not move; it may be trippable.

Initial Conditions:

100% Power, BOL

Options Available:

Selection A-J

Magnitude T, U Trippable/Untrippable

Ramp Time

Ramp Time 0

Direct

Options Used:

Selection A

Magnitude U

Delay Time 0 s

Delay Time 0-3600 s

Mode Direct/Remote/Conditional

None

Test Parameters Monitored:

Test Precis:

Following malfunction actuation, select manual individual on rod mode selector switch, group 4 on rod group selector switch and rod 1 on rod selector switch, then attempt to move rod 1 with the In-Hold-Out switch. Verify that rod 1 does not move.

Operator trips the reactor and observes: rod 1 does not insert, reactor power decreases normally, rod position deviation low, lowlow, and reed switch alarms annunciate.

Any Uncorrected Test Failures? No

lest Number:	14	5	5	6	6	
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Test Description:

Initial Conditions:

100% Power, BOL

Options Available:

Selection 1-41

Magnitude D, E Deenergized/Energized

Ramp Time

Delay Time 0-3600 s

Mode Direct/Remote/Conditional Options Used:

Rod clutch failure. The selected rod falls into the core or fails to trip.

Selection 39

Magnitude D

Ramp Time 0

Delay Time 60 s

Direct

Test Parameters Monitored:

Linear range lower detector (A) Linear range lower detector (B) Linear range lower detector (C) Linear range lower detector (D) Linear range upper detector (A) Linear range upper detector (B) Linear range upper detector (C) Linear range upper detector (C)

Test Precin: Following malfunction actuation, observe: rod drop alarms (2), rod indication show a dropped rod, power dependent insertion limit group 4 alarms, flux decreases most on channel nearest dropped rod, and least on channel furthest from dropped rod. Operator observes lower flux near the dropped rod on the flux map on ERF computer.

Any Uncorrected Test Failures? No

Failure of clutch power supply. The selected power supply(ies) fails.

Initial Conditions:

Test Description:

100% power, BOL

Options Available:

Selection A-D

Delay Time 0-3600 s

Mode Direct/Remote/Conditional Selection A Delay Time 60 s Direct

Options Used:

Test Parameters Monitored: None

Test Precis:

Following malfunction actuation, observe: clutch #1 power supply current decreases to 0, DC power on light extinguishes, clutch #2 power supply current increases.

Operator then clears malfunction and observes: clutch power supply currents return to normal and DC power on light illuminates.

Any Uncorrected Test Failures? No

Test Number: 14.	5.	5	6.	8
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Test Description:

Rod ejection. The selected control element assembly (CEA) is ejected from the reactor vessel.

Initial Conditions: 30% Power, BOL

Options Available:

Options Used:

Selection 1-41

Selection 1

Magnitude 100%

Ramp Time 0 s

Delay Time 0

Direct

Magnitude 0-100% 100% = 2.75" Diameter Hole

Ramp Time

Delay Time 0-3600 s

Mode Direct/Remote/Conditional

Test Parameters Monitored:

Pressurizer level Linear range lower + upper detectors RCS global pressure Containment sump level Containment pressure Containment air particulate activity Containment air noble gas activity Fuel transfer canal area monitor Containment operating floor area monitor Containment air temperature Containment dew point

Test Precis: Following malfunction actuation, observed: reactor coolant system temperature increases indicative of positive reactivity addition, power dependent insertion limit group 4 and rod deviation alarms; pressurizer level decreases with channel X & Y alarms; reactor coolant system pressure drops with channel X & Y alarms; letdown goes to maximum; charging pumps start; containment sump level, temperature, dew point, pressure, and radiation levels rise; reactor trip, SIAS. Operator refers to EOP-3.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.7	.9	
Malfunction Identifier:	CVC9		
Test Description:			ainment. A variable size leak occurs charge header and FT-236.
Initial Conditions: 100% Power, BOL		ower, BOL	
	Options Available:		Options Used:
		de 0-100% 2" Line Break	Magnitude 100%
	Ramp Time 0-3600 s Delay Time 0-3600 s		Ramp Time 0 s
			Delay Time 0 s
	Mode Direct/R	emote/Conditional	Direct
Test Parameters Monitored:		temperature Charging temperatur	radiation monitor monitor level xchanger letdown outlet
Test Precis:	Following malfunction actuation, observe: volum decreases; charging flow-related alarms annun charging pumps start, discharge pressure decre		ed alarms annunciate; standby

decreases; charging flow-related alarms annunciate; standby charging pumps start, discharge pressure decreases; volume control tank auto makeup starts; pressurizer level and pressure decrease; volume control tank low, and low-low level alarms annunciate and charging pump suction switches to the SIRWT; when volume control tank isolates, its level rises; waste disposal system malfunction alarm annunciates; letdown temperature rises, alarms and TCV-202 closes; CRHS and VIAS actuate, main stack and process area monitor alarms annunciate.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.8.2	
Malfunction Identifier:	CWS2	
Test Description:	Main condenser tube leak. The fa degree in the selected bundle(s).	ilure occurs to a selectable
Initial Conditions:	100% Power	
	Options Available:	Options Used:
	Selection A-D	Selection A
	Magnitude 0-100% 100% = 10% Of The Tubes	Magnitude 100%
	Ramp Time 0-3600 s	Ramp Time 0
	Delay Time 0-3600 s	Delay Time 0
	Mode Direct/Remote/Conditional	Direct
Test Parameters Monit	ored: None	
Test Precis:	Following malfunction actuation, or pressure decreases and hotwell le	

est Precis: Following malfunction actuation, observe: condenser A outlet pressure decreases and hotwell level rises, hotwell high level alarm; condensate storage tank level rises; generator megawatts decrease with no rod movement or other operator actions.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.9.2			
Malfunction Identifier:	DSG2			
Test Description:	Diesel generator fuel transfer pumps discharge leak. A variat size leak occurs on the selected diesel's fuel transfer pumps' discharge.			
Initial Conditions:	100% Power, BOL			
	Options Available:	Options Used:		
	Selection A, B	Selection A		
	Magnitude 0-100% 100% = 1" Line Break	Magnitude 100		
	Ramp Time 0-3600 s	Ramp Time 0 s		
	Delay Time 0-3600 s	Delay Time 0 s		
	Mode Direct/Remote/Conditional	Direct		
Test Parameters Monit	ored: None			

Test Precis: Following malfunction actuation observe: fuel oil level in 300 gallon tank decreases, level rises in spent regenerant tank due to floor drain inflow.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.9.8				
Malfunction Identifier:	DSG8				
Test Description:	Diesel generator failure to start. The selected diesel ge cranks but fails to start.				
Initial Conditions:	100% Power, BOL				
	Options Available:	Options Used:			
	Selection A, B	Selection A			
	Delay Time 0-3600 s	Delay Time 0 s			
	Mode Direct/Remote/Conditional	Direct			
Test Parameters Monit	ored: None				

Test Precis: Following malfunction actuation, operator attempts to start DG-1 with emergency pushbutton and observes: start status light illuminates, then the diesel start fail and trouble alarms annunciate; the engine stopped status light illuminates.

Operator attempts to start diesel until starting air is exhausted.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.11.1	
Malfunction Identifier:	EDS1	
Test Description:	4160 VAC bus fault. The selected phase to ground fault on the bus.	bus(ses) is lost due to a single
Initial Conditions:	100% Power, BOL	
	C tions Available:	Options Used:
	Selection A-D	Selection C
	Delay Time 0-3600 s	Delay Time C s
	Mode Direct/Remote/Conditional	Direct

Test Parameters Monitored:

Breaker T1B-3B ammeter Breaker T1B-3C ammeter Transformer T1A3 current Bus 1B3A voltage Bus 1B3B voltage Bus 1B3C voltage Transformer T1A3 secondary wattage 4160V bus 1A3 voltage

Test Precis: Following malfunction actuation, observe: DG-1 start, breaker 1A33 trip and lockout, 86/1A33 alarm; lockout relay supervision tripped, diesel auto start demand, breaker off auto alarms; bus 1A3 voltage goes to 0; 4160 bus ground alarm comes in then clears; bus 1A3 low voltage and breaker auto trip alarms; transformer lockout relay 86-1A3-TFB picks up alarms; 4160 V bus 1A3 feeder auto trip, 480 V bus low voltage, breaker off auto, Diesel auto start demand alarms annunciate; 4160/480 V transformer voltages and currents go to 0; 4160V and 480V breakers trip with attendant alarms; power lost to busses 1A3, 1C3A, 1B3A-D, 1B3A-4A & 1B3C-4C; reactor trip with low flow alarm.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.11.2	
Malfunction Identifier:	EDS2	
Test Description:	480 VAC bus fault. The selected b phase to ground fault on the bus o	
Initial Conditions:	100% Power, BOL	
	Options Available:	Options Used:
	Selection A-I	Selection A
	Delay Time 0-3600 s	Delay Time 0 s
	Mode Direct/Remote/Conditional	Direct
Test Parameters Monit	tored: None	
Test Precis	Following actuation, observe segu	ential 480V bus alarms follower

Test Precis: Following actuation, observe sequential 480V bus alarms followed by respective breaker tripping, then phase current and voltage go to 0. Selected 480V load breakers trip open (charging pump, ventilation, and other operating loads on bus).

Any Uncorrected Test Failures? No

Test Number:	14.5.5.11.3				
Malfunction Identifier:	EDS3				
Test Description:	125 VDC bus fault. The selected bus(ses) is lost due to a short on the bus.				
Initial Conditions:	100% Power, BOL				
	Options Available	Options Used:			
	Selection A, B	Selection A			
	Ramp Time 0-3600 s	Ramp Time 0 s			
	Delay Time 0-3600 s	Delay Time 0 s			
	Mode Direct/Remote/Conditional	Direct			
Test Paramet Monito	bred: Battery 1 ammeter 125V DC charger 1 amm 125V DC bus #1 voltme				
Test Precis:	Following malfunction actuation, observe DC Bus #1 ground alarm. After approximately 15 seconds observe: DC bus 1 ground light illuminates, battery charger feeder trips, output current goes to 0; output current goes to maximum; bus current goes to 0; inverter A, C & 1 trouble, DC bus 1 low voltage, panel Al-41A undervoltage, 125 VDC ¿uxiliary supply not available-D2 alarms; normal source 125 VDC, bettery #1 (Normal) 125 VDC, DC distribution panel 1 lights out; power loss to 125 VDC loads and control power.				
Any Uncorrected Test Failures? No					

Did this test reveal any exception to ANSI/ANS-3.5-1985? No

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Test Number: 14.5.5.11.4 Malfunction Identifier: EDS4 Test Description: 120 VAC instrument bus fault. The selected bus(ses) is lost due single phase to ground fault on the bus. Initial Conditions: 100% Power Options Available: Options Used:	
Test Description: 120 VAC instrument bus fault. The selected bus(ses) is lost due single phase to ground fault on the bus. Initial Conditions: 100% Power Options Available: Options Used:	
Initial Conditions: 100% Power Options Available: Options Used:	
Options Available: Options Used:	e to
물건 것 같아요. 이 집에 가지 않는 것 같아요. 그 것 같아요. 이 집에 가지 않는 것 같아요. 그 것 같아요. 이 것	
Selection A-F Selection A	
Ramp Time 0-3600 s Ramp Time 0 s	
Delay Time 0-3600 s Delay Time 300 s	
Mode Direct Direct/Remote/Conditional	
Test Parameters Monitored: 120V AC inverter ammeter 120V AC bus A voltmeter	
Test Precis: Following malfunction actuation, observe bus ground light goes bright. After approximately five minutes observe: bus feeder breaker trips, invertor output current pegs high, then goes to 0, b voltage goes to 0, low voltage alarm annunciates, and loss of power to associated loads is experienced.	

이는 그는 것 같이 하는 것이 같아요.

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Any Uncorrected Test Failures? No

Test Number:	14.5.5.11.6		
Malfunction Identifier:	EDS6		
Test Description:	480 VAC supply transformer fault. The selected 4160/480 VAC supply transformer is lost due to a single-phase to ground fault.		
Initial Conditions:	100% Power		
	Options Available:	Options Used:	
	Selection A-F	Selection A	
	Ramp Time 0-3600 s	Ramp Time 0 s	
	Delay Time 0-3600 s	Delay Time 0 s	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monit	ored: Transformer T1B-3A cur	rrent	
Test Precis:	Following malfunction actuation, observe: transformer high wind		

recis: Following malfunction actuation, observe: transformer high winding temperature alarm is received, transformer feeder breaker trips, transformer output voltage and current go to zero with associated alarms, and power is lost to loads supplied.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.11.11		
Malfunction Identifier:	EDS11		
Test Description:	Switchyard line fault. A single phase to ground fault occurs on phase A of the selected line.		
Initial Conditions:	100% Power, BOL		
	Options Available:	Options Used:	
	Selection A, B, C	Selection C	
	Delay Time 0-3600 s	Delay Time 0 s	
	Mode Direct/Remote/Conditional	Direct	

Test Parameters Monitored: None

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Test Precis: Following malfunction actuation, observe: relay 87 161 picks up causing lockout relay supervision tripped alarm; relay 86-161 trip with 161 KV alarm; relays 86-1 & 2/T1A-3 trip and DG-1 starts at idle, relays 86-1/T1A-4 & -2/T1A-4 trip, with DG-2 starting at idle and breakers 1A13 & 1A24 close with alarms; transformers T1A-4 & -3 watts, current, and voltage go to 0; T1A-1 & -2 wattage and current rise.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.11.12		
Malfunction Identifier:	EDS12		
Test Description:	Switchyard breaker fault. The selected breaker contacts weld shut or the selected breaker trip mechanism activates.		
Initial Conditions:	100% Power, BOL		
	Options Available:	Options Used:	
	Selection A, B, C	Selection A	
	Magnitude O, C Open, Fails To Open	Magnitude O	
	Delay Time 0-3600 s	Delay Time 0 s	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monit	ored: None		
Test Precis:	Following malfunction actuation, of with alarm. Operator opens breake		

with alarm. Operator opens breaker 3451-4 control switch and observes that alarm clears.

Any Uncorrected Test Failures? No

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Test Number:	14.5.5.12.1		
Malfunction Identifier:	EHC1		
Test Description:	Electrohydraulic fluid system leak. A variable size leak occurs on the electrohydraulic fluid accumulator inlet line.		
Initial Conditions:	100% Power		
	Options Available:		Options Used:
	Magnitude 0-100% 100% = Double Ended Shear		Magnitude 100
	Ramp Time 0-3600 s		Ramp Time 60 s
	Delay Tir	ne 0-3600 s	Delay Time 0 s
	Mode Direct/Re	emote/Conditional	Direct
Test Parameters Monito	ored:	Hydraulic fluid level in n Fluid actuator system (f Hydraulic fluid pump A Hydraulic fluid pump B	
Test Precis:	Following malfunction actuation, observe: electrohydraulic contro fluid pressure decreases, current rises, standby pump starts with alarm and pressure decreases more slowly; hydraulic oil press lo hydraulic power unit fluid level high-low alarms; turbine and react trip; EHC mechanical, emergency lights illuminate, hydraulic fluid pressure light goes out; all turbine stop, control and combined intercept valves close. After 5-10 minutes, observe hydraulic fluid pressure pump A & B stopped alarms.		rises, standby pump starts with re slowly; hydraulic oil press low, h-low alarms; turbine and reactor lights illuminate, hydraulic fluid stop, control and combined minutes, observe hydraulic fluid

Any Uncorrected Test Failures? No

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Test Number:	14.5.5.12.6		
Malfunction Identifier:	EHC6		
Test Description:	Load limit potentiometer failure. The load limit potentiometer's output fails to change in the selected deadband.		
Initial Conditions:	50% Power		
	Options Available:	Options Used:	
	Magnitude 0-5% Magnitude is % of potentiometer range	Magnitude 5%	
	Ramp Time 0-3600 s	Ramp Time 0 s	
	Delay Time 0-3600 s	Delay Time 0 s	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monito	ored: None		

Test Precis: Following actuation, operator slowly raises load with the load limiter and observes erratic potentiometer behavior. After load is raised past deadband selected; observe smooth potentiometer operation. Then lower load and observed erratic potentiometer operation when deadband is reached again.

Any Uncorrected Test Failures? No

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Test Number:	14.5.5.13.1		
Malfunction Identifier:	ESF1		
Test Description:	Steam generator low pressure logic matrix failure. The logic matrix for the selected train(s) fails to the selected condition(s).		
Initial Conditions:	100% Power, EOL		
	Options Available:	Options Used:	
	Selection A, B	Selection A	
	Magnitude T, F T= On (ACT), F=Off	Magnitude T	
	Delay Time 0-3600 s	Delay Time 0 s	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monit	ored: None		

Test Precis:

Following malfunction actuation, observe indications of SGLS & SGIS actuation; reactor trips, reactor coolant system temperature response tracks main steam safety valve cycling, pressurizer level response follows Tave, (program setpoint), pressurizer pressure and level alarms annunciate. Feedwater controller level alarms annunciate, steam generator pressures rise, steam generator levels decrease, steam generator feedwater and steam flows go to 0, feedwater pump discharge pressure rises and suction flow decreases, feedwater recirculation valves open. Condensate pumps discharge low flow alarms annunciate. Observe the following: reactor coolant system temperature and pressure stabilize at temperature corresponding to main steam safety valve setpoints, steam generator levels decrease, auxiliary feedwater actuation system actuation with appropriate alarms and actions. Observe proper auxiliary feedwater flow to steam generators. Verify proper cycling of auxiliary feedwater valves and attendant alarms as steam generator levels vary between actuation and reset setpoints.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.13.2		
Malfunction Identifier:	ESF2		
Test Description:	Containment high pressure logic matrix failure. The logic matrix for the selected train(s) fails to the selected condition(s).		
Initial Conditions:	100% Power, BOL		
	Options available:	Options Used:	
	Selection A, B	Selection A	
	Magnitude T, F T= On (ACT), F=Off	Magnitude T	
	Delay Time 0-3600 s	Delay Time 0	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monit	ored: None		
Test Precis:	Following malfunction actuation, o		

is: Following malfunction actuation, observe: CPHS, SIAS, and 480V load shed actuate with associated alarms and indications; SGIS actuates with associated valve closures and alarm annunciation; reactor trip alarms. Diesel generators start, load sequencers S1-1 & S2-2 actuate with associated alarm annunciation; CIAS and VIAS actuate with associated alarms.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.13.5		
Malfunction Identifier:	ESF5		
Test Description:	Pressurizer low pressure logic matrix failure. The logic matrix for the selected train(s) fails to the selected condition(s).		
Initial Conditions:	100% Power, BOL		
	Options Available:	Options Used:	
	Selection A, B	Selection A	
	Magnitude T, F T= On (ACT), F=Off	Magnitude T	
	Delay Time 0-3600 s	Delay Time 0 s	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monito	ored: None		
Test Precis:	Following malfunction actuation, observe: PPLS actuates with associated alarm annunciation; SIAS, diesel generator start, and CIAS signals received, sequencers S1-1 and S2-2 actuate.		

Any Uncorrected Test Failures? No

Test Number:	14.5.5.13.10		
Malfunction Identifier:	ESF10		
Test Description:	Safety injection actuation signal failure. The actuation signal for the selected train(s) fails to the selected condition(s).		
Initial Conditions:	100% Power, BOL		
	Options Available:	Options Used:	
	Selection A, B	Selection A	
	Magnitude T, F T= On (ACT), F=Off	Magnitude T	
	Delay Time 0-3600 s	Delay Time 0 s	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monit	ored: None		
Test Precis:	Following malfunction actuation, observe: SIAS will actuate with annunciation on panels AI-30A/B and the ERF. Valves will go to their accident positions, 480V load shed will initiate and emergency		

boration will commence. SIAS actuation will also cause VIAS actuation.

Any Uncorrected Test Failures? No

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Test Number:	14.5.5.13.12		
Malfunction Identifier:	ESF12		
Test Description:	OPLS logic matrix failure. The logic matrix for the selected train(s) fails to the selected condition(s).		
Initial Conditions:	100% Power, BOL		
	Options Available:	Options Used:	
	Selection A, B	Selection A	
	Magnitude T, F T = On (ACT), F=Off	Magnitude T	
	Delay Time 0-3600 s	Delay Time 0 s	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monit	ored: None		
Test Desein			

Test Precis: Following malfunction actuation, observe: 86A/OPLS trips with alarm; breakers 1A13 & 1A33 trip, DG-1 starts and accelerates to 900 rpm, bus 1A3 load sheds; breakers 1A24 & 1A44 trip, DG-2 starts and accelerates to 900 rpm, bus 1A4 load sheds; supply breakers to MCC-3B2, -3B3, -3C-4C-1 deenergize; associated loads trip.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.14	4.2	
Malfunction Identifier:	FDW2		
Test Description:	Main feedwater header leak. A variable size leak occurs on the main feedwater header.		riable size leak occurs on the
Initial Conditions:	50% Pov	ver	
	Options	Available:	Options Used:
	Magnitude 0-100% Magnitude 100% = 18" Diameter Break		Magnitude 50%
	Ramp Time 0-3600 s		Ramp Time 600 s
	Delay Tir	me 0-3600 s	Delay Time 0 s
	Mode Direct/Re	emote/Conditional	Direct
Test Parameters Monitored:		Main feedwater pump(Main feedwater pump(Steam generator levels Main feedwater header	s) discharge pressure s
Test Precis:	Following actuation, observe: heater 6 A/B outlet, feedwater pump discharge pressures decrease; feedwater pump suction flow rises; steam generator feedwater flows and levels decrease; feedwater control steam generator low alarms annunciate, turbine building sump high level alarms annunciate, reactor trip.		
Any Uncorrected Test F	Failures?	No	

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Test Number:	14.5.5.14.3			
Malfunction Identifier:	FDW3			
Test Description:	Main feedwater line leak upstream of the flow control valve. A variable size leak occurs on the selected feed line(s) between the flow element and the flow control valve.			
Initial Conditions:	100% Po	wer, BOL		
	Options A	vailable:	Options Used:	
	Selection	A, B	Selection A	
		e 0-100% 6'' Diameter Break	Magnitude 10%	
	Ramp Tin	ne 0-3600 s	Ramp Time 0 s	
	Delay Tin	ne 0-3600 s	Delay Time 0 s	
	Mode Direct/Re	mote/Conditional	Direct	
Test Parameters Monito	ored:	Steam generator levels Main feedwater flows Feedwater regulating valve	s' positions	

Test Precis: Following malfunction actuation, observe: steam generator RC-2A feedwater flow rises, level decreases, feedwater regulating valve A position increases, low level alarm annunciates, steam generator B level decreases slower than steam generator A, steam generator A low level causes reactor trip.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.14.5			
Malfunction Identifier:	FDW5			
Test Description:	Main feedwater line leak inside containment. A variable size leak occurs on the selected feed line(s) downstream of the check valve.			
Initial Conditions:	100% Pc			
	Options	Available:	Options Used:	
	Selection	n A, B	Selection A	
	Magnitude 0-100% 100% = 16" Diameter Break Ramp Time 0-3600 s Delay Time 0-3600 s		Magnitude 100%	
			Ramp Time 0 s	
			Delay Time 0 s	
	Mode Direct/Remote/Conditional		Direct	
Test Parameters Monito	ored:	Steam generator steam, A steam generator level RCS pressure and temp Containment pressure a	/pressure peratures	
Test Precis:	Following malfunction actuation, observe: steam generator feedwater flow rises, steam generator RC-2A pressure & level decrease; steam generator RC-2A low level alarm annunciates; reactor trips; steam generator low level, low pressure channel pre- trip & trip alarms annunciate. steam generator 2A steam flow, pressure and level decrease to 0 and SGIS actuates as steam generator boils dry. Containment sump high level alarm			

annunciates. RCS temperature & pressure, and pressurizer level decrease; SIAS actuates at 1600 psia.

Containment high pressure alarms annunciate and CPHS actuates.

Any Uncorrected Test Failures? No

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Test Number:	14.5.5.16.1				
Malfunction Identifie	r: FWH1	FWH1			
Test Description:		Feedwater heater tube leak. Tube failure occurs to a selectat degree in the selected heater(s).			
Initial Conditions:	100% Power, BO	100% Power, BOL			
	Options Available	Options Used;			
	Selection A-L	Selection K (6A)			
	Magnitude 0-100 100% = 10% Of 1				
	Ramp Time 0-36	00 s Ramp Time 0 s			
	Delay Time 0-360	00 s Delay Time 0 s			
	Mode Direct/Remote/Co	Direct	Direct		
Test Parameters M		generator transmitted levels (NR)			

Condenser steam pressure Gross generator electrical power output (MW) Heater 6A level control Heater 5A level control Second stage extraction pressure Heater 6A drain temperature.

Test Precis: Following malfunction actuation, observe: heater 6A level and extraction pressure rising, drain temperature decreases; heater 5A level rises rapidly; steam generator level decreasing and feedwater flow rising; hotwell level rising, heater 6A extraction valve closes, and condenser vacuum decreasing due to 6A high level dump; standby vacuum pumps start; heater 6A high-low level alarm; generator megawatts decrease.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.17	.1	
Malfunction Identifier:	GEN!		
Test Description:		egulator failure. The voltage i o the setpoint selected.	regulator changes the output
Initial Conditions :	100% Po	wer	
	Options /	Available:	Options Used:
	Selection A=Auto F	A, B Regulator, B=Manual	Selection A
		le 80-120% Rated Voltage	Magnitude 120%
	Ramp Tir	ne 0-3600 s	Ramp Time 60 s
	Delay Tir	ne 0-3600 s	Delay Time 0 s
	Mode Direct/Re	emote/Conditional	Direct
Test Parameters Monito	red:	Generator field ammeter Power factor meter Generator output imaginary Main generator current Generator field voltage met	
Test Precis:	Following malfunction actuation, observe: generator picks reactive load; leading power factor rises; voltage regulator voltage rises; field current and voltage, and generator outp current rise with field overvoltage alarm. After 10 seconds, regulator trips to manual mode with alarm; parameters effect return to pre-malfunction conditions, except the voltage reg		es; voltage regulator transfer e, and generator output m. After 10 seconds, voltage arm; parameters effected

Any Uncorrected Test Failures? No

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Did this test reveal any exception to ANSI/ANS-3.5-1985? No

transfer volt meter.

Test Number: 14.5.5.17.4

Malfunction Identifier: GEN4

Test Description:

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Field breaker failure. The field breaker fails to the position selected.

Initial Conditions:

Approximately 12% reactor power, turbine at 1800 RPM

Options available:

Magnitude O, C Open, Closed

Mode

Magnitude O

Delay Time 0

Options Used:

Delay Time 0-3600 s

Direct/Remote/Conditional

Direct

Test Parameters Monitored:

None

Test Precis:

Following malfunction actuation, operator starts up generator and observes: field breaker does not close, field breaker mismatch light illuminates, and exciter field breaker tripped alarm annunciates. Operator returns field breaker control switch to OFF and observes that above alarms and indications return to normal.

Any Uncorrected Test Failures? No

Test I	Number:	14.	5.	5.	18	3.	1

Malfunction Identifier: MSS1

Test Description:

Main steam line leak inside containment. A variable size leak occurs on the selected steam line inside containment.

Initial Conditions:

100% Power, BOL

Options Available:

Selection A, B

Magnitude 0-100% 100% = 28" Diameter Break

Delay Time 0 s

Direct

Magnitude 100%

Options Used:

Selection A

Ramp Time 60 s

Delay Time 0-3600 s

Ramp Time 0-3600 s

Mode Direct/Remote/Conditional

Test Parameters Monitored:

Steam generator wide range levels Total containment pressure RCS global pressure Steam generator steam pressures Containment temperature Wide range cold leg temperatures Wide range hot leg temperatures Auxiliary feedwater flows to steam generators Feedwater flows to steam generators Steam line flows to main steam header

Test Precis:

Following malfunction actuation, observe: steam generator RC-2A steam pressure drops, steam temperature and flow decrease; RC-2B, main steam, and turbine first stage pressure and temperature decrease; steam generator levels and RCS temperature decrease; T_{ref}/T_{avg} deviation alarms annunciate; RCS pressure decreases with alarms; pressurizer heaters energize; letdown flow decreases to minimum; pressurizer level channel X & Y alarms; steam generator low ievel alarms; containment pressure rises with alarms; reactor trips, CPHS, SIAS, VIAS, CIAS, SGLS, AFWS all actuate with alarms, actions, and indications; containment sump level rises with attendant alarms. Following AFWS, operator verifies no auxiliary feedwater flow to steam generator RC-2A; RC-2B level recovers, RC-2B pressure rises to main steam safety valve setpoint.

Any Uncorrected Test Failures? No

41

Test Number:	14.5.5.18.3			
Malfunction Identifier:	MSS3			
Test Description:	Main steam line leak outside containment (non- isolable). A variable size leak occurs on the selected steam line outside of containment.			
Initial Conditions:	100% Power, BOL			
	Options Available	Options Used:		
	Selection A, B	Selection A		
	Magnitude 0-100% 100% = 28" Diameter Brea	Magnitude 100 k		
	Ramp Time 0-3600 s	Ramp Time 600 s		
	Delay Time 0-3600 s	Delay Time 0 s		
	Mode Direct/Remote/Conditional	Direct		
Test Parameters Monito	RCS temperatur	r pressures and levels res and pressure tdown system pressures and flows		
Test Precis:	Following malfunction actua	ation, observe: steam generator RC-2		

Following malfunction actuation, observe: steam generator RC-2A steam pressure, temperature, and flow decrease; RC-2B pressure and temperature decrease, flow rises; main steam and turbine first stage pressure decrease; RC-2A level swells, then decreases with low level alarm; RC-2B level, RCS temperature and pressure decrease; T.,/Tax deviation and pressurizer pressure channel X & Y alarms; pressurizer backup heaters energize; TM/LP pre-trip and trip, subcooled margin low, high power pre-trip and trip alarms; reactor trip; pressurizer SI signal low-low alarms; PPLS actuation , and ERF indications; pressurizer level drops, letdown flow goes to minimum, high-low channel X & Y alarms, standby charging pumps start; volume control tank level decreases with suction switch over to SIRWT, VCT low-low level alarms; pressurizer low-low channel X & Y alarms, backup heaters de-energize; SIAS, VIAS, CIAS, SGLS, and AFWS actuations with actions and alarms; auxiliary feedwater flow to RC-2B; reactor coolant pumps cavitate; pressurizer and RC-2B levels recover; RC-2B pressure rises to main steam safety valve setpoint. Operator stops reactor coolant pumps when cavitation is observed

Any Uncorrected Test Failures? No

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Test Number:	14.5.5.18.5			
Malfunction Identifier:	MSS5			
Test Description:	Main steam isolation valve (MSIV) failure. The selected MSIV(s) fails closed.			
Initial Conditions:	100% Power, BOL			
	Options Available:	Options Used:		
	Selection A, B	Selection A		
	Delay Time 0-3600 s	Delay Time 0 s		
	Mode Direct/Remote/Conditional	Direct		

Test Parameters Monitored:

None

Test Precis:

Following malfunction actuation, observe: steam generator RC-2A steam pressure increases; reactor coolant system temperatures increase due to loss of heat sink. Pressurizer pressure and level increase, pressurizer spray valves open. Reactor trip due to ASGT.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.18.6			
Malfunction Identifier:	MSS6			
Test Description:	Main steam line to turbine driven auxiliary feedwater pump (TDAFWP) leak. A variable size leak occurs on the selected line(s) supplying the TDAFWP between the stop valve & check valve.			
Initial Conditions:	100% Power, BOL			
	Options Available:	Options Used:		
	Selection A, B	Selection A		
	Magnitude 0-100% 100% = 2" Diameter Break	Magnitude 100		
	Ramp Time 0-3600 s	Ramp Time 0 s		
	Delay Time 0-3600 s	Delay Time 0 s		
	Mode Direct/Remote/Conditional	Direct		

Test Parameters Monitored: None

Test Precis: Following malfunction actuation, observe the FW-10 red light on and the auxiliary oil pump stops, when steam driven pump is supplied from unaffected steam line. Operator closes HC-1045B and observes FW-10 red light off, recirculation valves open, FW-10 running alarm clears, recirculation flow = 0. (pump stops). Operator opens HC-1045B, resets trip latch and YCV-1045, then observes: FW-10 red light on then off, recirculation valve opens, FW-10 running alarm.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.18	.7		
Malfunction Identifier:	MSS7			
Test Description:	Main steam header leak. A variable size leak occurs on the common main steam header.			
Initial Conditions:	100% Power, BOL			
	Options A	vailable:	Options Used:	
		e 0-100% 6'' Diameter Break	Magnitude 10%	
	Ramp Tin	ne 0-3600 s	Ramp Time 600 s	
	Delay Time 0-3600 s		Delay Time 0 s	
	Mode Direct/Remote/Conditional		Direct	
Test Parameters Monit	ored:	RCS pressure Generator megawatts Steam generator steam	n flows	
Test Precis:	main stea decrease	m header pressures dec , RCS cold leg temperatu	bserve steam generator and crease. Generator megawatts ures decrease as steam urbine building sump level	

generator steam flows increase. Turbine building sump level increases. RCS T_{ave} decreases, reactor power increases. Condensate storage tank level decreases.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.19.2	
Malfunction Identifier:	NIS2	
Test Description:	Wide range power supply failure. The selected channel(s) fails.	selected power supply for the
Initial Conditions:	Cold Shutdown Conditions, BOL	
	Options Available:	Options Used:
	Selected Channel A - H	Selected Channel: A
	Delay Time 0-3600 s	Delay Time 0 s
	Mode Direct/Remote/Conditional	Direct
Test Parameters Monito	ored: None	
Test recis	Selected drawer power on light goes	out all indications go to zero

Test recis: Selected drawer power on light goes out, all indications go to zero, high voltage meter goes to zero, nuclear Instrumentation channel inoperative annunciator alarms, extended range circuit deenergizes.

Any Uncorrected Test Failures? No

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Test Number:	14.5.5.19.7		
Malfunction Identifier:	NIS7		
Test Description:	Power range power supply failure. The high voltage power supply for the selected channel(s) fails.		
Initial Conditions:	100% Power, BOL		
	Options Available:	Options Used:	
	Selection A-F	Selection E	
	Delay Time 0-3600 s	Delay Time 60 s	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monit	ored: None		

Test Precis: Following malfunction actuation, observe: high voltage detector meter fails to 0, bistable trip light illuminates, nuclear instrumentation channel inoperative alarm, upper and lower power level meters fail to 0, rod drop bistable trip with alarms, level 1 trip light goes out, power on light remains lit.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.20.4	4	
Malfunction Identifier:	PRS4		
Test Description:		er steam space leak. A d of the pressurizer.	variable size leak occurs from the
Initial Conditions:	100% Pow	ver, BOL	
	Options Av	vailable:	Options Used:
	Magnitude 100% = 8"	0-100% Diameter Hole	Magnitude 100
	Ramp Tim	e 0-3600 s	Ramp Time 60 s
	Delay Time	e 0-3600 s	Delay Time 0 s
	Mode Direct/Ren	note/Conditional	Direct
Test Parameters Monit	ored:	Containment pressure RCS global pressure	•
Test Precis:			observe: pressurizer pressure sup heaters energize; charging

cis: Following malfunction actuation, observe: pressurizer pressure decreases, level increases, backup heaters energize; charging flow, containment pressure, temperature, activity, dew point, and sump level rise.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.20.5				
Malfunction Identifier:	PRS5				
Test Description:	Pressurizer power operated relief valve (PORV) failure. The selected PORV(S) fails to the position selected.				
Initial Conditions:	100% Po	wer, BOL			
	Options A	vailable:	Options Used:		
	Selection	A, B	Selection A		
	Fail Posit	ion 0-100%	Magnitude 100%		
	Ramp Tin	ne 0-3600 s	Ramp Time 60 s Delay Time 0 s		
	Delay Tin	ne 0-3600 s			
	Mode Direct/Remote/Conditional		Direct		
Test Parameters Monito	red:	Total containment pressure RCS global pressure Pressurizer level Pressurizer quench tank lev Pressurizer quench tank pr Containment temperature	vel		
Test Precis:	alarm ind PORV dis pressuriz level char alarms ar low-low p pressure, disc blow	ressure alarms; PPLS actuat	izer pressure decreases; ad alarm annunciates; rization rate rises, high-low ad subcooled margin low M/LP with alarms; pressurizer tes; pressurizer quench tank with attendant alarms, rupture ure drop; containment		

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Test Number:	14.5.5.20	0.9	
Malfunction Identifier:	PRS9		
Test Description:		zer level instrumentation taj surizer instrument tap.	o leak. A variable size leak on
Initial Conditions:	100% Po	wer, BOL	
	Options /	Available:	Options Used:
	Selection	A-D	Selection A
		ie 0-100% 1" Diameter Hole	Magnitude 20%
	Ramp Tir	me 0-3600 s	Ramp Time 60 s
	Delay Tir	ne 0-3600 s	Delay Time 0 s
	Mode Direct/Re	emote/Conditional	Direct
Test Parameters Monito	ored:	RCS global pressure Pressurizer pressure	

Test Precis: Following malfunction actuation, observe: pressurizer pressure decreases to lower limit, low-low pressure alarms, channel A TM/LP trip with (3) alarms, PPLS matrix lights change state. Operator bypasses trip unit and verifies yellow light on.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.2	1.1			
Malfunction Identifier:	RCP1				
Test Description:	Reactor coolant pump (RCP) lube oil cooler leak. A variable size leak occurs between component cooling water and the lube oil systems of the selected reactor coolant pump upper lube oil cooler.				
Initial Conditions:	100% P	ower, BOL			
	Options	Available:	Options Used:		
	Selectio	n A-D	Selection A		
	Magnitude 0-100% 100% = 10% of tubes Ramp Time 0-3600 s		Magnitude 100%		
			Ramp Time 60 s		
	Delay Ti	ime 0-3600 s	Delay Time 0 s		
	Mode Direct/R	emote/Conditional	Direct		
Test Parameters Monit	ored:	RCP upper oil reservoir le RCP speed RCP lower thrust bearing RCP upper thrust bearing	temperature		

RCP speed RCP lower thrust bearing temperature RCP upper thrust bearing temperature RCP upper bearing temperature Lube oil cooler flow RCP reverse flow switch Vibration

Test Precis:

Following malfunction actuation, lube oil leaks into the component cooling water system. Observe: component cooling water from RCP-3A lube oil cooler high temperature alarm; lube oil flow and reservoir level decrease with attendant alarms; reactor coolant pump bearing temperatures rise; lube oil levels fluctuate; reactor coolant pump high vibration alarm; reactor coolant pump trips with attendant alarm; reactor trip.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.2	1.3		
Malfunction Identifier:	RCP3			
Test Description:		tor coolant pump (RCP) guide bearing failure. The selected ng(s) fails.		
Initial Conditions:	100% Po	ower, BOL		
	Options	Available:	Options Used:	
	Selection	n A-H	Selection B	
	Magnitude 0-100% Ramp Time 0-3600 s Delay Time 0-3600 s Mode Direct/Remote/Conditional		Magnitude 100%	
			Ramp Time 60 s	
			Delay Time 0 s	
			Direct	
Test Parameters Monitored:		RCP speed (RPM) RCP upper guide bearing temperature RCP current RCP vibration		
Test Precis:	Following malfunction actuation, observe: RCP-3A upper guide bearing temperature rises with attendant alarm, RCP-3A high vibration alarm, pump seizes. Reactor trips due to low RCS flow.			

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Test Number:	14.5.5.2	10	
		1.5	
Malfunction Identifier:	RCP9		
Test Description:	Reactor coolant pump (RCP) lower seal failure. The lower seal or the selected RCP(s) fails.		
Initial Conditions:	100% P	ower, BOL	
	Options	Available:	Options Used:
	Selectio	n A-D	Selection A
	Magnitude 0-100% 100% = Complete Seal Fail Ramp Time 0-3600 s		Magnitude 100%
			Ramp Time 60 s
	Delay Ti	ime 0-3600 s	Delay Time 0 s
	Mode Direct/Remote/Conditional		Direct
Test Parameters Monit	ored:	RC-3A controlled bleed- RC-3A middle seal press RC-3A upper seal press RC-3A seal bleedoff tem RCP 3A main header flo	sure ure iperature
Test Precis:	pressure upper se	e rises from 1400 to 2100 p	serve: RCP-3A middle seal inlet sia with attendant ERF alarm; s and seai bleedoff flow may nnunciates.

Test Number:	14	5	5.	22.	1	

Malfunction Identifier: RCS1

Test Description:

RCS loop leak. A variable size leak occurs on the selected RCS loop(s).

Initial Conditions:

100% Power, BOL

Options Available:

Selection A-H

Magnitude 0-100% 100% = Line Diameter

Ramp Time 0-3600 s

Magnitude 10%

Options Used:

Selection C

Ramp Time 0 s

Delay Time 0 s

Delay Time 0-3600 s

Mode Direct/Remote/Conditional Direct

Test Parameters Monitored:

Reactor vessel mixture level HPSI flow indication LPSI flow indication Pressurizer level SI-6AB/C/D level Indication SIRWT level Pressurizer pressure Wide range containment pressure Containment air temperature Core exit thermocouple

Test Precis:

Following mainunction actuation, observe: RCS pressure drops rapidly with low pressure channel X & Y alarms; TM/LP pre-trip and subcooled margin low alarms; reactor trips on TM/LP with attendant alarms and indications. Operator verifies reactor trip response, then observes: (4) pressurizer low-low pressure alarms; PPLS actuation with attendant alarms and actions; pressurizer level drops rapidly with channel X & Y alarms, reactor vessel decreases; pressurizer backup heaters de-energize; containment pressure rises with attendant alarms; CPHS actuation with attendant actions and alarms; reactor coolant pumps cavitate; safety injection tanks inject with attendant alarms; containment activity rises and CRHS actuates with attendant alarms and actions; SIAS, VIAS, CIAS, CSAS, SGIS actuate with attendant alarms and actions; containment sump/water level rises with attendant alarms; containment dew point rises; HPSI/LPSI pressure and flows; containment spray flow causes containment pressure decrease; SIRWT level decreases with alarms and actions; RAS actuates with alarms and actions.

Any Uncorrected Test Failures? No

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т	est Number:	14.5.5.22.3			
N	alfunction Identifier:	RCS3			
Т	est Description:	Fuel failure. Fuel rods fail causing the activity to increase.	reactor coolant system		
Ir	nitial Conditions:	100% Power, BOL			
		Options Available:	Options Used:		
		Magnitude 0-2%	Magnitude 2%		
		Ramp Time 0-3600 s	Ramp Time 60 s		
		Delay Time 0-3600 s	Delay Time		
		Mode Direct/Remote/Conditional	Direct		
Test Parameters Monitor		tored: CCW header radiation monitor			
Т	est Precis:	Following malfunction actuation, obser Operator inserts a letdown heat excha that the component cooling water radia rapidly and process radiation high alar	nger tube leak and observes ation monitor signal rises		

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Test Number:	14.5.5.24.1	
Malfunction Identifier:	RPS1	
Test Description:	Failure of interposing relay. The selector to the position selected.	cted interposing relay(s) fails
Initial Conditions:	100% Power, BOL	
	Options Available:	Options Used:
	Selection A-D	Selection A
	Magnitude D, E Deenergized, Energized	wagnitude D
	Ramp Time	Ramp Time 0 s
	Delay Time 0-3600 s	Delay Time 0
	Mode Direct/Remote/Conditional	Direct

Test Parameters Monitored:

2."

None

Test Precis: Following malfunction actuation, observe that the interposing relays de-energize causing a half-trip as indicated by: control power ground, PS1 & PS3 AC trouble, AC on, and DC on lights extinguish; M1 coil voltage goes to 0, trip channel 1 light comes on; output ammeters for PS1 & PS3 decrease, output current meters for PS2 & PS4 rise.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.24.2	
Malfunction Identifier:	RPS2	
Test Description:	Reactor protection system (RPS) po selected ladder logic power supply(ie	
Initial Conditions:	100% Power, BOL	
	Options Available:	Options Used:
	Selection A-L	Selection A
	Ramp Time	Ramp Time 0 s
	Delay Time 0-3600 s	Delay Time
	Mode Direct/Remote/Conditional	Direct
Test Parameters Monit	ored: None	
Test Precis:	Following malfunction actuation, obs	erve: power supply light o

Test Precis: Following malfunction actuation, observe: power supply light on RPS power supply drawer goes out, AB-1 & -2 matrix relays deenergize and status lights go out, a half-trip will occur with attendant indications.

Operator performs surveillance test on high pressurizer pressure channels for selected channel, but does not bypass trip unit; and observes TU-8A trip 2 & 3 lights illuminate, but trip 1 light does not.

Any Uncorrected Test Failures? No

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Test Number:	14.5.5.24.3		
Malfunction Identifier:	RPS3		
Test Description:	Failure of axial power distribution (APD) positive limit calculator. The selected axial power distribution positive limit calculator fails.		
Initial Conditions:	100% Power, BOL		
	Options Available:	Options Used:	
	Selection A-L	Selection A	
	Selected Output Range 50-150% of Normal Output	Selected 50%	
	Ramp Time	Ramp Time 0 s	
	Delay Time 0-3600 s	Delay Time	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monit	ored: None		

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Following malfunction actuation, observe: APD positive limit meter Test Precis: decreases by selected output range. Operator places the meter input selector switch to the positive limit position and verifies that RPS voltmeter reads the same as the value selected for the malfunction.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.25.2	
Malfunction Identifier:	RRS2	
Test Description:	Main feedwater master controller failure. The steam generator level input for the selected master level controller(s) fails to the selected value.	
Initial Conditions:	100% Power, BOL	
	Options Available:	Options Used:
	Selection A, B	Selection A
	Magnitude 0-100% Percent of Input Value	Magnitude 50
	Ramp Time	Ramp Time 0 s
	Delay Time 0-3600 s	Delay Time
	Mode Direct/Remote/Conditional	Direct

Test Parameters Monitored: None

Test Precis: Following malfunction actuation, observe: main feedwater controller output responds in the proper direction based upon the difference in the magnitude selected and the steam generator level (original input signal).

Operator switches selected controller to manual and raises steam generator level while observing low level alarm clears.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.25.7			
Malfunction Identifier:	RRS7			
Test Description:	Steam dump quick opening solenoid valve failure. The quick opening solenoid valve fails to the position selected.			
Initial Conditions:	100% Power, BOL			
	Options Available:	Options Used:		
	Selection A-E	Selection A		
	Magnitude D, E Deenergized, Energized	Magnitude E		
	Delay Time 0-3600 s	Delay Time		
	Mode Direct/Remote/Conditional	Direct		
Test Parameters Monitor	ored: None			
Test Precis:	Following malfunction actuation, observe: TCV-909-1 red light on TCV-909-2, -3, -4 green lights on; steam generators RC-2A and RC-2B steam flows and levels rise; reactor to turbine power mismatch as nuclear power rises and turbine power decreases.			

Operator closes air to solenoid for TCV-909-1 and observes: green indication light on, RC-2A and RC-2B steam flows decrease, reactor to turbine power mismatch disappears, generator megawatts return to normal.

on;

Any Uncorrected Test Failures? No

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Test Number:14.5.5.26.3Malfunction Identifier:RWS3Test Description:Raw water supply line break. A variable size leak occurs on the selected raw water line downstream of the flow element.Initial Conditions:100% Power, BOLOptions Available:Options Used: Selection A, BSelection A, BSelection AMagnitude 0-100% 100% = 16" Pipe BreakMagnitude 100%Delay Time 0-3600 sDelay Time 60 sDelay Time 0-3600 sDelay Time 0 sMode Direct/Remote/ConditionalDirectTest Parameters Monitored:CCW heat exchanger temperatures Raw water system header flowsTest Precis:Following malfunction actuation, observe: raw water supply flow rises, supply header low pressure alarm annunciates, component cooling water heat exchanger outlet temperature rises, raw water supply pressure decreases, raw water-cooled loads heat up, wast				
Test Description: Raw water supply line break. A variable size leak occurs on the selected raw water line downstream of the flow element. Initial Conditions: 100% Power, BOL Dptions Available: Options Used: Selection A, B Selection A Magnitude 0-100% Magnitude 100% 100% = 16" Pipe Break Ramp Time 0-3600 s Ramp Time 60 s Delay Time 0-3600 s Delay Time 0 s Direct Mode Direct Direct Test Parameters Monitored: CCW heat exchanger temperatures Raw water system pressure Letdown heat exchanger outlet temperature SRaw water system header flows Test Precis: Following malfunction actuation, observe: raw water supply flow rises, supply header low pressure alarm annunciates, component rise, supply pressure decreases, raw water-cooled loads heat up, waster supply pressure decreases, raw water-cooled loads heat up, waster	Test Number:	14.5.5.26.3		
Initial Conditions: 100% Power, BOL Initial Conditions: 100% Power, BOL Options Available: Options Used: Selection A, B Selection A Magnitude 0-100% Magnitude 100% 100% = 16" Pipe Break Magnitude 100% Ramp Time 0-3600 s Ramp Time 60 s Delay Time 0-3600 s Delay Time 0 s Mode Direct Direct/Remote/Conditional Direct Test Parameters Monitored: CCW heat exchanger temperatures Raw water system pressure Letdown heat exchanger outlet temperature Containment cooler outlet temperature Raw water system header flows Test Precis: Following malfunction actuation, observe: raw water supply flow rises, supply header low pressure alarm annunciates, component cooling water heat exchanger outlet temperature rises, raw water supply pressure decreases, raw water-cooled loads heat up, wast	Malfunction Identifier:	RWS3		
Options Available: Options Used: Selection A, B Selection A Magnitude 0-100% Magnitude 100% 100% = 16" Pipe Break Magnitude 100% Ramp Time 0-3600 s Ramp Time 60 s Delay Time 0-3600 s Delay Time 0 s Mode Direct Direct/Remote/Conditional Direct Test Parameters Monitored: CCW heat exchanger temperatures Raw water system pressure Letdown heat exchanger outlet temperatures Raw water system header lows Test Precis: Following malfunction actuation, observe: raw water supply flow rises, supply header low pressure alarm annunciates, component cooling water heat exchanger outlet temperature rises, raw water supply pressure decreases, raw water-cooled loads heat up, waster	Test Description:			
Selection A, B Selection A Magnitude 0-100% 100% = 16" Pipe Break Magnitude 100% Ramp Time 0-3600 s Ramp Time 60 s Delay Time 0-3600 s Delay Time 0 s Mode Direct Direct/Remote/Conditional Direct Test Parameters Monitored: CCW heat exchanger temperatures Raw water system pressure Letdown heat exchanger outlet temperatures Raw water system header flows Test Precis: Following malfunction actuation, observe: raw water supply flow rises, supply header low pressure alarm annunciates, component cooling water heat exchanger outlet temperature rises, raw water supply pressure decreases, raw water-cooled loads heat up, wast	Initial Conditions:	100% Po	wer, BOL	
Magnitude 0-100% 100% = 16" Pipe Break Magnitude 100% Ramp Time 0-3600 s Ramp Time 60 s Delay Time 0-3600 s Delay Time 0 s Mode Direct/Remote/Conditional Direct Test Parameters Monitored: CCW heat exchanger temperatures Raw water system pressure Letdown heat exchanger outlet temperatures Raw water system header flows Test Precis: Following malfunction actuation, observe: raw water supply flow rises, supply header low pressure alarm annunciates, component cooling water heat exchanger outlet temperature rises, raw water supply pressure decreases, raw water-cooled loads heat up, wast		Options A	Available:	Options Used:
100% = 16" Pipe Break Ramp Time 0-3600 s Ramp Time 60 s Delay Time 0-3600 s Delay Time 0 s Mode Direct Direct/Remote/Conditional Direct Test Parameters Monitored: CCW heat exchanger temperatures Raw water system pressure Letdown heat exchanger outlet temperatures Raw water system header flows Test Precis: Following malfunction actuation, observe: raw water supply flow rises, supply header low pressure alarm annunciates, component cooling water heat exchanger outlet temperature rises, raw water supply pressure decreases, raw water-cooled loads heat up, waster		Selection	А, В	Selection A
Delay Time 0-3600 s Delay Time 0 s Mode Direct Direct/Remote/Conditional Direct Test Parameters Monitored: CCW heat exchanger temperatures Raw water system pressure Letdown heat exchanger outlet temperatures Raw water system header flows Test Precis: Following malfunction actuation, observe: raw water supply flow rises, supply header low pressure alarm annunciates, component cooling water heat exchanger outlet temperature rises, raw water supply pressure decreases, raw water-cooled loads heat up, wast				Magnitude 100%
Mode Direct Direct/Remote/Conditional Direct Test Parameters Monitored: CCW heat exchanger temperatures Raw water system pressure Letdown heat exchanger outlet temperatures Raw water system header outlet temperatures Raw water system header flows Test Precis: Following malfunction actuation, observe: raw water supply flow rises, supply header low pressure alarm annunciates, component cooling water heat exchanger outlet temperature rises, raw water supply pressure decreases, raw water-cooled loads heat up, wast		Ramp Tir	ne 0-3600 s	Ramp Time 60 s
Direct/Remote/Conditional Test Parameters Monitored: CCW heat exchanger temperatures Raw water system pressure Letdown heat exchanger outlet temperature Containment cooler outlet temperatures Raw water system header flows Test Precis: Following malfunction actuation, observe: raw water supply flow rises, supply header low pressure alarm annunciates, component cooling water heat exchanger outlet temperature rises, raw water supply pressure decreases, raw water-cooled loads heat up, wast		Delay Tin	ne 0-3600 s	Delay Time 0 s
Raw water system pressure Letdown heat exchanger outlet temperature Containment cooler outlet temperatures Raw water system header flows Test Precis: Following malfunction actuation, observe: raw water supply flow rises, supply header low pressure alarm annunciates, component cooling water heat exchanger outlet temperature rises, raw water supply pressure decreases, raw water-cooled loads heat up, wast			emote/Conditional	Direct
rises, supply header low pressure alarm annunciates, component cooling water heat exchanger outlet temperature rises, raw water supply pressure decreases, raw water-cooled loads heat up, wast	Test Parameters Monito	ored:	Raw water system pressu Letdown heat exchanger of Containment cooler outlet	re outlet temperature temperatures
disposal trouble alarm annunciates.	Test Precis:	rises, sup cooling w supply pr	oply header low pressure ala vater heat exchanger outlet t	arm annunciates, component temperature rises, raw water

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Test Number:14.5.5.27.2Malfunction Identifier:SDC2Test Description:Shutdown cooling heat exchanger inlet header leak. A variable size leak occurs on the shutdown cooling heat exchangers' inlet header between SI-169 & SI-170.Initial Conditions:COLD S/D, BOLInitial Conditions:Options Available: Magnitude 0-100% 100% = 12" pipe breakOptions Used: Magnitude 100% 100% = 12" pipe breakMode Direct/Remote/ConditionalDelay Time 0-3600 sRamp Time 60 sTest Parameters Monitored:Shutdown cooling flow Pressurizer level RCS temperatures RCS pressureDirectTest Precis:Following malfunction actuation, observe: shutdown cooling flow and pressure, and pressurizer level decrease; waste disposal system Malfunction alarm. CRHS, and VIAS actuation with attendant alarms and indications; high activity and radiation levels and alarms, RCS temperature fiese pressurizer pressure and temperature decrease along saturation curve.				
Test Description:Shutdown cooling heat exchanger inlet header leak. A variable size leak occurs on the shutdown cooling heat exchangers' inlet header between SI-169 & SI-170.Initial Conditions:COLD S/D, BOLInitial Conditions:COLD S/D, BOLOptions Available:Options Used:Magnitude 0-100%Magnitude 100%100% = 12" pipe breakRamp Time 0-3600 sDelay Time 0-3600 sDelay Time 60 sDelay Time 0-3600 sDelay Time 0 sModeDirectDirect/Remote/ConditionalDirectTest Parameters Monitored:Shutdown cooling flow Pressurizer level RCS temperatures RCS pressureTest Precis:Following malfunction actuation, observe: shutdown cooling flow and pressure, and pressurizer level decrease; waste disposal system Malfunction alarm; CRHS, and VIAS actuation with attendant alarms and indications; high activity and radiation levels and alarms; RCS temperature rises; pressurizer pressure and	Test Number:	14.5.5.27.2		
leak occurs on the shutdown cooling heat exchangers' inlet header between SI-169 & SI-170. Initial Conditions: COLD S/D, BOL <u>Options Available:</u> <u>Options Used:</u> Magnitude 0-100% Magnitude 100% 100% = 12" pipe break Magnitude 100% Ramp Time 0-3600 s Ramp Time 60 s Delay Time 0-3600 s Delay Time 0 s Mode Direct Test Parameters Monitored: Shutdown cooling flow Pressurizer level RCS temperatures RCS pressure Test Precis: Following malfunction actuation, observe: shutdown cooling flow and pressure, and pressurizer level decrease; waste disposal system Malfunction alarm; CRHS, and VIAS actuation with attendant alarms and indications; high activity and radiation levels and alarms; RCS temperature rises; pressurizer pressurizer pressure and	Malfunction Identifier:	SDC2		
Options Available:Options Used:Magnitude 0-100% 100% = 12" pipe breakMagnitude 100%Ramp Time 0-3600 sRamp Time 60 sDelay Time 0-3600 sDelay Time 0 sMode Direct/Remote/ConditionalDirectTest Parameters Monitored:Shutdown cooling flow Pressurizer level RCS temperatures RCS pressureShutdown cooling flow and pressurizer level decrease; waste disposal system Malfunction alarm; CRHS, and VIAS actuation with attendant alarms and indications; high activity and radiation levels and alarms; RCS temperature rises; pressurizer pressure and	Test Description:	leak occurs on the shutdown cooling heat exchangers' inlet header		
Magnitude 0-100% 100% = 12" pipe break Magnitude 100% Ramp Time 0-3600 s Ramp Time 60 s Delay Time 0-3600 s Delay Time 0 s Mode Direct Direct/Remote/Conditional Direct Test Parameters Monitored: Shutdown cooling flow Pressurizer level RCS temperatures RCS pressure Shutdown cooling flow Test Precis: Following malfunction actuation, observe: shutdown cooling flow and pressure, and pressurizer level decrease; waste disposal system Malfunction alarm; CRHS, and VIAS actuation with attendant alarms and indications; high activity and radiation levels and alarms; RCS temperature rises; pressurizer pressure and	Initial Conditions:	COLD S/	D, BOL	
100% = 12" pipe break Ramp Time 0-3600 s Ramp Time 60 s Delay Time 0-3600 s Delay Time 0 s Mode Direct Direct/Remote/Conditional Direct Test Parameters Monitored: Shutdown cooling flow Pressurizer level RCS temperatures RCS pressure Test Precis: Following malfunction actuation, observe: shutdown cooling flow and pressurizer level decrease; waste disposal system Malfunction alarm; CRHS, and VIAS actuation with attendant alarms and indications; high activity and radiation levels and alarms; RCS temperature rises; pressurizer pressure and		Options /	Available:	Options Used:
Delay Time 0-3600 s Delay Time 0 s Mode Direct Direct/Remote/Conditional Direct Test Parameters Monitored: Shutdown cooling flow Pressurizer level RCS temperatures RCS pressure RCS pressure Test Precis: Following malfunction actuation, observe: shutdown cooling flow and pressure, and pressurizer level decrease; waste disposal system Malfunction alarm; CRHS, and VIAS actuation with attendant alarms and indications; high activity and radiation levels and alarms; RCS temperature rises; pressurizer pressure and				Magnitude 100%
Mode Direct/Remote/Conditional Direct Test Parameters Monitored: Shutdown cooling flow Pressurizer level RCS temperatures RCS pressure Test Precis: Following malfunction actuation, observe: shutdown cooling flow and pressure, and pressurizer level decrease; waste disposal system Malfunction alarm; CRHS, and VIAS actuation with attendant alarms and indications; high activity and radiation levels and alarms; RCS temperature rises; pressurizer pressure and		Ramp Tir	me 0-3600 s	Ramp Time 60 s
Direct/Remote/Conditional Test Parameters Monitored: Shutdown cooling flow Pressurizer level RCS temperatures RCS pressure Test Precis: Following malfunction actuation, observe: shutdown cooling flow and pressure, and pressurizer level decrease; waste disposal system Malfunction alarm; CRHS, and VIAS actuation with attendant alarms and indications; high activity and radiation levels and alarms; RCS temperature rises; pressurizer pressure and		Delay Time 0-3600 s		Delay Time 0 s
Pressurizer level RCS temperatures RCS pressure Test Precis: Following malfunction actuation, observe: shutdown cooling flow and pressure, and pressurizer level decrease; waste disposal system Malfunction alarm; CRHS, and VIAS actuation with attendant alarms and indications; high activity and radiation levels and alarms; RCS temperature rises; pressurizer pressure and			emote/Conditional	Direct
and pressure, and pressurizer level decrease; waste disposal system Malfunction alarm; CRHS, and VIAS actuation with attendant alarms and indications; high activity and radiation levels and alarms; RCS temperature rises; pressurizer pressure and	Test Parameters Monito	ored:	Pressurizer level RCS temperatures	
	Test Precis:	and pressure, and pressurizer level decrease; waste disposal system Malfunction alarm; CRHS, and VIAS actuation with attendant alarms and indications; high activity and radiation leve and alarms; RCS temperature rises; pressurizer pressure and		ecrease; waste disposal d VIAS actuation with n activity and radiation levels pressurizer pressure and

Test Number:	14.5.5.30	.1	
Malfunction Identifier:	SGN1		
Test Description:		nerator tube rupture. the selected steam g	Tube failure occurs to a selectable generator(s).
Initial Conditions:	100% Po	wer, BOL	
	Options A	Available:	Options Used:
	Selection	А, В	Selection A
	Magnitud 100% = 1	e 0-100% 0 tubes	Magnitude 10%
	Ramp Tin	ne 0-3600 s	Ramp Time 0 s
	Delay Tin	ne 0-3600 s	Delay Time 0 s
	Mode Direct/Re	mote/Conditional	Direct
Test Parameters Monito	ored:	RCS global pressur Steam generator A Condenser off gas r RCS hot leg temper	wide range level nge pressure de range pressures re pressure in level reference leg radiation

Test Precis:

Following malfunction actuation, observe: pressurizer level and pressure decrease, backup heaters energize; high-low, then lowlow channel X & Y level alarms annunciate, backup heaters trip, pressurizer off-normal channel X & Y alarms; condenser off-gas radiation rises; letdown flow stops; steam generator RC-2A level and pressure rise, feedwater flow decreases; RC-2A high level alarm; reactor trip; steam generator blow down monitor alarms; PPLS, SIAS, CIAS, and VIAS actuate with alarms and indications; pressurizer level rises due to safety injection flow, then backup heaters energize, RCS pressure rises to 1300 psia where leak flow and SI flow are balanced.

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Test Number: 14.5.5.30.2

Malfunction Identifier: SGN2

Test Description:

Reference leg leak. A variable size leak occurs at the top of the selected reference leg(s).

Initial Conditions: 100% Power, BOL

Options Available:

Selection A-D

Magnitude 0-100% 100% = 3/8" line break

Ramp Time 0-3600 s

Delay Time 0-3600 s

Mode Direct/Remote/Conditional

None

Selection A Magnitude 100%

Options Used:

Ramp Time 60 s

- searcher - searcher - searcher

Delay Time 0 s

Direct

Test Parameters Monitored:

Test Precis:

Following malfunction actuation, observe: Steam generator RC-2A control channel level indicator level rises, feedwater regulating valve closes, reducing flow; RC-2A actual level decreases with low level alarm; RC-2A pressure drops with attendant alarms and channel A ASGT trip; containment dew point and sump level rise.

Operator manually controls RC-2A level, bypasses steam generator pressure trip A, observes bypass alarm annunciates and low pressure trip alarm and trip lights clear; channel A ASGT trip lights remain on.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.3	81.5	
Malfunction Identifier:	SIS5		
Test Description:		njection tank gas space leak. a gas space of the selected ta	
Initial Conditions:	100% P	ower, BOL	
	Options	Available:	Options Used:
	Selectio	n A-D	Selection A
		ide 0-100% 1" Diameter Hole	Magnitude 100%
	Ramp Time 0-3600 s Delay Time 0-3600 s		Ramp Time 60 s
			Delay Time 0 s
	Mode Direct/F	emote/Conditional	Direct
Test Parameters Monito	ored:	Safety injection tank press Safety injection tank level Containment pressure	ure

Test Precis: Following malfunction actuation, observe: SI tank 6A pressure drops, SI-6A high-low pressure, then at 243 psig SI-6A low pressure alarms annunciate.

Any Uncorrected Test Failures? No

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Test Number:	14.5.5.32.3	
Malfunction Identifier:	GEN6	
Test Description:	Stator cooling water pump suction occurs on the suction line of the supump(s) downstream of the isolation	elected stator cooling water
Initial Conditions:	100% Power, BOL	
	Options Available:	Options Used:
	Selection A and/or B	Selection used: A
	Magnitude 0-100% 100% = Double ended shear of suction piping	Magnitude 100%
	Ramp Time 0-3600 s	Ramp Time 60 s
	Delay Time 0-3600 s	Delay Time 0 s
	Mode Direct/Remote/Conditional	Direct
Test Parameters Monit	ored: Stator cooling inlet tem Stator cooling outlet ter Stator winding tempera Stator cooling water pre Turbine building sump I	nperature tures essure
Test Precis:	Following malfunction actuation, o	bserve: stator cooling system

st Precis: Following malfunction actuation, observe: stator cooling system flow and pressure decrease, standby pump starts with associated alarms, standby pump trips and approximately 70 seconds later, turbine trips, followed by reactor trip. Turbine building sump level increases, generator stator winding temperatures increase.

Any Uncorrected Test Failures? No

Test Number.	14.5.5.33.1		
Malfunction Identifier:	TUR1		
Test Description:	Main turbine lube oil reservoir leak. A variable size leak occurs at the base of the main turbine lube oil reservoir.		
Initial Conditions:	100% Power		
	Options available:	Options Used:	
	Magnitude 0-100% 100% = 1" Line Break	Magnitude 100%	
	Ramp Time 0-3600 s	Ramp Time 0	
	Delay Time 0-3600 s	Delay Time 0	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monitor	ored: None		
Test Precis:	Following malfunction actuation, obs decreasing, turbine oil tank level hig low alarms; motor suction, emergen	h-low and bearing oil pressure	

low alarms; motor suction, emergency bearing, and turning gear oil pumps running with attendant alarms; after oil tank empties, oil pumps cavitate, then trip with attendant alarms; turbine vibration alarm and trip; turbine coasts down quickly

Any Uncorrected Test Failures? No

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Test Number:	14.5.5.33.5		
Malfunction Identifier:	TUR5		
Test Description:	Main turbine high vibration. The selected bearing experiences excessive vibration of the magnitude selected.		
Initial Conditions:	100% Power, BOL		
	Options Available:	Options Used:	
	Selection A-J	Selection C	
	Magnitude 0-20 mils	Magnitude 10m	
	Ramp Time 0-3600 s	Ramp Time 900 s	
	Delay Time 0-3600 s	Delay Time 0 s	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monit	ored: Bearings 1 through 6 vibra Bearings 1 through 6 oil or		
Test Precis:	Following malfunction actuation, observe: turbine vibration alarm annunciates as vibration readings rise on bearings (highest to lowest) 3, 2, 4, 5, 1, and 6; turbine trip when vibration is greater than 10 mils; vibration decrease except through resonance speeds.		

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Test Number:	14.5.5.33.6	
Malfunction Identifier:	TUR6	
Test Description:	Turning gear failure. The turning g	ear fails to engage when needed.
Initial Conditions: rpm	Any condition that has the main turbine rotating at greater than 300	
	Options Available:	Options Used:
	Delay Time 0-3600 s	Delay Time 0
	Mode Direct/Remote/Conditiona!	Direct
Test Parameters Monitor	ored: None	

Test Precis: Following malfunction actuation, operator follows OI-ST-3, Turbine Generator Shutdown, observes bearing oil pressure stable and the turning gear oil pump starts. At 200 rpm, operator starts bearing lift pumps and observes listed normal indications. At 0 rpm, operator observes turning gear not started, then attempts manual start. Turning gear stopped or disengaged alarm annunciates

Plant is recovered when operator clears malfunction, starts turning gear motor and observes alarm clears.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.34.2		
Malfunction Identifier:	WDS2		
Test Description:	Gas decay tank leak. A variable s B.	size leak occurs on gas decay tank	
Initial Conditions:	100% Power, BOL		
	Options Available:	Options Used:	
	Magnitude 0-100% 100% = 1.5" diameter hole	Magnitude 100	
	Ramp Time 0-3600 s	Ramp Time 60 s	
	Delay Time 0-3600 s	Delay Time 0 s	
	Mode Direct/Remote/Conditional	Direct	
Test Parameters Monit	ored: Stack gas iodine monit Stack gas air particula Waste gas decay tank	te monitor	
Test Precis:	Following maifunction actuation, observe: high activity indicated in the main stack with alarms, CRHS and VIAS actuations with actions and alarms; process monitor meters and recorders indicate high; stack monitor alarms and indications; corridor area monitors read high; tank WD-29B pressure decreased. After isolating tank and compressor rooms, observe radiation readings decrease.		
Any Uncorrected Test I	Failures? No		

Did this test reveal any exception to ANSI/ANS-3.5-1985? No

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Test Number:	14.5.5.35.1	
Malfunction Identifier:	MM-1	
Test Description:	Loss of coolant accident with loss of generator failure. Multiple malfunctio	
Initial Conditions:	100% Power, BOL	
	Malfunctions used	Malfunction Selections
	RCS Loop Leak	14% Magnitude, 10 second ramp time
	Diesel Fail to start	A selected
	Switchyard Line Faults	A, B and C conditional upon Reactor Trip

Test Parameters Monitored:

Pressurizer pressure Steam generator pressures Reactor vessel level Core exit thermocouple temperatures RCS temperatures HPSI and LPSI flows Safety injection tank levels Auxiliary feedwater flows RCS subcooling

Test Precis: Upon activation of the RCS loop leak malfunction, the loss of offsite power occurs, reactor coolant pumps trip, main feedwater pumps trip, a bubble forms in the reactor vessel head, the RCS hot legs reach saturation conditions. The secondary safety valves lift, SIAS is actuated, the pressurizer empties, one diesel generator does not start, HPSI flow initiates via one train, the core uncovers, then is reflooded.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.35.2	
Malfunction Identifier:	MM-2	
Test Description:	Inadvertent opening of a pressu (PORV) with a loss of offsite pow failure. multiple malfunction	
Initial Conditions:	100% Power, BOL	
	Malfunctions used	Malfunction Selections
	Global Failure of PORV	100% Open
	Diesel Fail to start	A selected
	Switchyard Line Faults	A, B and C conditional upon reactor trip
Test Parameters Monit	ored: Pressurizer pressure Steam generator pres Reactor vessel level Core exit thermocoup RCS temperatures HPSI and LPSI flows	ssures ple temperatures

Safety injection tank levels Auxiliary feedwater flows RCS subcooling

Test Precis:

Upon activation of the global failure for the PORV, the reactor trips on low RCS pressure, a loss of offsite power occurs, reactor coolant pumps trip, main feedwater pumps trip, a bubble forms in the reactor vessel head, the RCS hot legs reach saturation conditions. SIAS is actuated, one diesel generator does not start, HPSI flow initiates via one train, steam flows out of the PORV and the core remains covered for the duration of the event.

Any Uncorrected Test Failures? No

Test Number: 14.5.5.35.3

Malfunction Identifier: MM-3

Test Description:

Inadvertent opening of a pressurizer pilot operated relief valve (PORV) with a loss of all feedwater, offsite power, one HPSI pump, and one ECCS train. Multiple malfunction

Initial Conditions:

100% Power, BOL

Malfunctions used

Failure of PORV

Malfunction Selections

100% Open, 60 second ramp time

Failure of ALL Feedwater Pumps Conditional upon failure of PORV

Failure to start

Failure of 2 of 3 HPSI Pumps

Failure of one ECCS Train to actuate

Switchyard Line Faults

13

Malfunctions ESF-1 through

A, B and C conditional upon Reactor Trip

Test Parameters Monitored:

Pressurizer pressure Steam generator pressures Reactor vessel level Core exit thermocouple temperatures RCS temperatures HPSI and LPSI flows Safety injection tank levels Auxiliary feedwater flows RCS subcooling

Test Precis: Upon activation of the loss of the main feedwater pumps, the reactor trips on low steam generator level, followed by the loss of all off-site power. All reactor coolant pumps trip, secondary safety valves open, SIAS actuates on the one remaining operable train. A bubble forms in the reactor vessel head, the RCS hot legs approach saturation conditions.

Any Uncorrected Test Failures? No

Test Number:	14.5.5.35.4	
Malfunction Identifier:	MM-4	
Test Description:	Loss of all feedwater, offsite power, of ECCS train. Multiple malfunction	one HPSI pump, and one
Initial Conditions:	100% Power, BOL	
	Malfunctions used	Malfunction Selections
	Failure of ALL Feedwater Pumps	Direct activation
	Failure of 1 HPSI Pump	Failure to start
	Failure of one entire ECCS Train to actuate	Malfunctions ESF-1 through 13
	Switchyard Line Faults	A, B and C conditional upon reactor trip
Test Parameters Monito	bred: Pressurizer pressure Steam generator pressure Reactor vessel level Core exit thermocouple te RCS temperatures HPSI and LPSI flows Safety injection tank levels Auxiliary feedwater flows RCS subcooling	mperatures
Test Precis:	Upon activation of the main feedwate flow is lost, and the steam generator causing a reactor trip on low steam g off-site power causes all reactor cool safety valves open to control steam g circulation is established, and the ver allow bubble formation. RCS temperator conditions. Due to the inventory in the temperatures remain fairly stable for	levels decrease rapidly, enerator level. The loss of all ant pumps to trip. Secondary generator pressure. Natural ssel level does not decrease to atures do not reach saturation e steam generators, the RCS
Any Uncorrected Test F	Failures? No	

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Test Number:	14.5.5.35.5	
Malfunction Identifier:	MM-5	
Test Description:	Loss of coolant accident (LOCA) w isolated, a loss of offsite power, an Multiple malfunction.	
Initial Conditions:	100% Power, BOL	
	Malfunctions used	Malfunction Selections
	RCS Loop Leak	RCS1C, 2.75% Magnitude, 10 sec ramp
	Failure of MSIV for A Steam Generator	Fail Closed upon RCS Leak actuation
	Failure of Auxiliary FW valve for "B" Steam Generator	Fail Closed
	Switchyard Line Faults	A, B and C conditional upon Reactor Trip
	Diesel Generator 1 Failure	Fail to start

Failure of all Charging Pumps

Fail to start/run

Test Parameters Monitored:

Pressurizer pressure Steam generator pressures Reactor Vessel level Core exit thermocouple temperatures RCS temperatures HPSI and LPSI flows Safety injection tank levels Auxiliary feedwater flows RCS subcooling

Test Precis: Upon activation of the LOCA, the main steam isolation valve for B steam generator closes, the secondary safety valves open on B steam generator, the reactor trips, followed by a loss of all off-site power, loss of all reactor coolant pumps, all main feedwater pumps, SIAS actuation and the formation of a bubble in the reactor vessel head. HPSI initiates, the pressurizer empties, but the core is not uncovered.

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Testing Program Changes

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Changes to the performance testing program for the second four-year interval as compared to the first four-year interval are as follows.

The following tests were deleted from the certification testing program for the listed reasons:

- 14.4.4 Electrical Bus Test
- 14.4.5 Air System Test

The above two tests were deleted because they are handler tests that were developed for the factory acceptance testing program prior to simulator shipment from the vendor. Changes to the configuration of the simulator are handled through the maintenance and modification process, making the performance of these tests redundant to the maintenance and modification process.

- 14.5.1.2.1 Reactor Core
- 14.5.1.2.18 Incore Nuclear Instrumentation System
- 14.5.2.1 Rod Worth Test
- 14.5.2.2 Boron Worth Test
- 14.5.2.3 Isothermal Moderator Temp. Coefficient Test
- 14.5.2.4 Power Coefficient Test
- 14.5.2.5 Xenon Test

The above core tests were deleted because they are not needed to meet the requirements of ANSI/ANS-3.5-1985 3.1.1 (9). These tests do not use installed instrumentation. They are performed once per core update by the software engineer responsible for the core model to ensure the data from the simulator matches the reference plant Technical Data Book.

- 14.5.3.2.2 Steady State Drift @ 80%
- 14.5.3.2.3 Steady State Drift @ 50%
- 14.5.3.2.4 Steady State Drift @ 30%

The above Steady State Drift tests are not required by ANSI/ANS-3.5-1985. They were part of the original factory acceptance test plan.

14.5.4.1 Maximum Rate Power Ramp

This test was redundant to test 14.5.4.12

- 14.5.4.2 Main Turbine Stop and Control Valve Testing
- 14.5.5.12.1 EHC Fluid System Leak on Accumulator

The above tests are not required by ANSI/ANS-3.5-1985. They were part of the original factory acceptance test plan.

14.5.5.2.2 Service Air System Leak

The above test was eliminated because it is redundant to 14.5.5.2.3 and 14.5.5.2.4

- 14.5.5.21.9 Reactor Coolant Pump Lower Seal failure
- 14.5.5.32.3 Stator Cooling Water Pump Suction Line Leak
- 14.5.5.33.1 Main Turbine Lube Oil Reservoir Leak
- 14.5.5.33.6 Turning Gear Failure
- 14.5.5.34.2 Gas decay Tank Leak
- 14.5.5.4.4 Condensate Pump Bearing Failure
- 14.5.5.9.2 Diesel Generator Fuel Transfer Pump Discharge Leak
- 14.5.4.3 Inadvertent Boration Dilution

The above tests are not required by ANSI/ANS-3.5-1985. They were part of the original factory acceptance test plan.

Testing Program 1995—1998

The performance test schedule for the next four-year interval is as follows. Note that Cycle 1 refers to tests due in the first year of the four year testing program (i.e., 1995), Cycle 2 refers to 1996, and so forth. "All" refers to tests due each year of the four year program. There are currently 101 Test procedures in the Certification Testing Program.

Test No.	Test Title		cle
14.3.3	Verification of Spare Computer Time	All	
14.5.3.1	Normal Operations Test	All	
14.5.3.2.1	Steady State Drift @ 100%	All	
14.5.3.3.1	Steady State Accuracy 100%	All	
14.5.3.3.2	Steady State Accuracy 80%	All	
14.5.3.3.3	Steady State Accuracy 50%	All	
14.5.3.3.4	Steady State Accuracy 30%	All	
14.5.4.10	Trip Any RCP Test	All	
14.5.4.11	Loss Of Load	All	
14.5.4.12	Maximum Rate Power Ramp (100-75-100)	All	
14.5.4.13	LOCA With Loss of All Offsite Power	All	
14.5.4.14	Excess Steam Demand	All	
14.5.4.15	Slow RCS Depress To Sat - No HPSI	All	
14.5.4.4	Reactor Trip and Recovery	All	
14.5.4.5	Dropped Rod	All	
14.5.4.6	Reactor Trip Test	All	
14.5.4.7	Simultaneous Trip of MFW Pumps Test	All	
14.5.4.8	Simultaneous Closure of MSIVs Test	All	
14.5.4.9	Simultaneous Trip of All RCPs Test	All	E
14.5.1.1.16	Auxiliary Feedwater System	1	
14.5.1.1.6	Component Cooling Water	1.1.1	
14.5.1.2.10	Inplant Electrical Distribution		
14.5.1.2.15	Reactor Protection System	1	
14.5.1.2.9	Diesel Generator	1	
14.5.5.1.4	Emergency Feedwater Storage Tank Leak	1	
14.5.5.1.5	Auxiliary Feedwater Activation Relay Failure	1	
14.5.5.11.1	4160 VAC Bus Fault	1	
14.5.5.11.11	Switchyard Line Fault	1	
14.5.5.11.12	Switchyard Breaker Fault	1	
14.5.5.11.2	480 VAC Bus Fault	1	
14.5.5.11.3	125 VDC Bus Fault	1	
14.5.5.11.4	120 VAC Instrument Bus Failure	1	
14.5.5.11.6	480 VAC Supply Transformer Fault	1.	
14.5.5.24.1	Failure of Interposing Relay	1	
14.5.5.24.2	RPS Power Supply Failure	1	
14.5.5.24.3	Failure of APD Positive Limit Calculator	1	
14.5.5.25.2	Main Feedwater Master Controller Failure	1	
14.5.5.25.7	Steam Dump Quick Opening Solenoid Failure	1	
14.5.5.3.4	CCW Pump Discharge Header Leak	1	
14.5.5.3.5	CCW Heat Exchanger Tube Leak	1	
14.5.5.9.8	Diesel Generator Failure to Start	1	

Test No.	Test Title	Cycle
14.5.1.1.1	Reactor Coolant System	2
	Raw Water System	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
14.5.1.1.4	Chemica: and Volume Control	2
14.5.2.6	ECP Test	2
	Feedwater Heater Tube Leak	2
	Wide Range Power Supply Failure	2
	Pressurizer Steam Space Leak	2
14.5.5.20.5	Pressurizer PORV Failure	2
14.5.5.20.9	Pressurizer Level Instrumentation Failure	2
	RCP Lube Oil Cooler Leak	2
	RCP Guide Bearing Failure	2
14.5.5.22.1	RCS Loop Leak	2
14.5.5.22.3		2
14.5.5.26.3		2
14.5.5.7.9	Raw Water Supply Line Break Charging Line Leak Outside Containment	2
14.5.5.8.2	Main Condenser Tube Leak	2
		2 2 2 3
14.5.1.1.5	Safety Injection System	3
	D-G Sequencer	3
14.5.1.2.16	Engineered Safeguards System	
14.5.5.13.1	SGLS Logic Matrix Failure	3
14.5.5.13.10	SIAS Logic Actuation Signal Failure	3
	OPLS Logic Matrix Failure	3 3 3
	CPHS Logic Matrix Failure	3
14.5.5.13.5	PPLS Logic Matrix Failure	3 3 3 3 3
14.5.5.18.1	Main Steam Line Break Inside Containment	3
14.5.5.18.3	Main Steam Line Break outside Containment	3
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ABBREVIATIONS & ACRONYMS

AFAS	Auxiliary feedwater actuation signal
AFW	Auxiliary feedwater
AOP	Abnormal operating procedure
APD	Axial power distribution
ASGT	Asymmetric steam generator trip
ASI	Axial shape index
BOL	Beginning of (core) life
CCW	Component cooling water
CEA	Control element assembly
CIAS	Containment isolation actuation signal
CPHS	Containment pressure high signal
CRHS	Containment radiation high signal
CSAS	Containment spray actuation signal
DG	Diesel generator
ECCS	Emergency core cooling system
EOL	End of (core) life
EOP	Emergency operating procedure
ERF	Emergency response facility
HCV	Hand control valve
HPSI	High pressure safety injection
LCV	Level control valve
LOA	Local operator action
LPSI	Low pressure safety injection
MOL	Middle of (core) life
MSSV	Main steam safety valve
MVAR	Mega volt-ampere reactive
MW	Megawatt
OI	Operating instruction
OP	Operating procedure
PCV	Pressure control valve
PORV	Power operated relief valve
PPLS	Pressurizer pressure low signal
RAS	Recirculation actuation signal
RCP	Reactor coolant pump
RCS	Reactor coolant system
RPS	Reactor protection system
SDBP	Steam dump and (turbine) bypass system
SDC	Shutdown cooling
SG	Steam generator
SGIS	Steam generator isolation signal
SGLS	Steam generator low (pressure) signal
SI	Safety injection
SIAS	Safety injection actuation signal
SIRWT	Safety injection refueling water storage tank
STLS	Storage tank (SIRWT) low (level) signal
TCV	Temperature control valve
TM/LP	Thermal margin/low pressure
TU	(RPS) Trip unit
VCT	Volume control tank
VIAS	Ventilation isolation actuation signal
V MO	a simulation restation detailon eigna

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