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9502100114 950126
PDR ADOCK 07000687
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# 6.0 SUMMARY OF INTERIM SURVEY RESULTS

## 6.1 Area 1.0, Hold Up Tank Floor

### 6.1.1 General Information

The HUT floor survey area consisted of two survey units: 1.1 the concrete floor, and 1.2 the concrete cores from underneath the concrete floor area. The 1.1 floor survey unit was surveyed on an affected area basis with a one m by one m grid. Significant amounts of the concrete surface had to be removed to meet release criteria. Portions of the floor were completely removed down to the underlying bedrock to remove a contaminated pipe and potentially contaminated saw cut kerfs. The floor has a surface area of about 70 $m^2$ and includes the interior tank's floor, vestiges of the tank's walls and a concrete pad that was an extension of the HUT floor exterior to the tank. With a one m by one m grid, 85 direct beta and direct alpha surface contamination measurements were made (see Figure 1.1). Each grid block was then scanned for "hot spots" and then quantified and characterized as necessary. Very small residual deposits of soil were encountered on the floor and a single composite sample was taken. 85 gamma exposure measurements were taken about each grid block. Additionally, three in situ gamma spectra were taken with a portable GeLi detector where higher gamma exposure rates were encountered (see Figure 1.1 for locations).

Measurement and sampling results for the 1.1 survey unit are provided in four attached tables as follows:

Table 1.1-1; HUT Floor - gamma exposure rate data

Table 1.1-2; HUT Floor - direct beta surface contamination data

Table 1.1-3; HUT Floor - direct alpha surface contamination data

Table 1.1-4; HUT Floor - sediment sample analysis data

The 1.2 survey unit consisted of concrete cores that were drilled into the HUT floor at 30 locations (see Figure 1.2) to obtain material representative of the bedrock-concrete floor underside surface interface. The core surfaces were then measured for direct beta and alpha surface contamination. These cores were taken because of the possibility of contaminated water that had leaked from the HUT migrating under the HUT floor slab.

Measurement results for the 1.2 survey unit are provided in two attached tables as follows:

Table 1.2-1; HUT Floor - concrete floor core direct beta surface contamination data

Table 1.2-2; HUT Floor - concrete floor core direct alpha surface contamination data

## 6.1.2 RESULTS SUMMARY

### a Survey Unit: 1.1 HUT Floor Area Concrete

DIRECT SURVEY RESULTS

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | 2842 | 85 |
| Number of Meas: | 85 | 85 | 85 |
| Survey Unit Mean: | 9.4 | 6069 | 23 |
| True Mean, U alpha 95% C.L.: | 10.0 | 10885 | 50 |
| Criteria/Acceptable Y - N: | 5/*(c) | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | 245796 | 1367 |
| Criteria/Acceptable Y - N: | N.A. | 13500/*(c) | 5000/Yes |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | 22 | 297903.4 | 1707 |
| Criteria/Acceptable Y - N: | 10 | 40500/*(c) | 15000/Yes |
| Ref. Tables | 1.1-1 | 1.1-2 | 1.1-3 |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

(c) See results test

COMMENTS/SOIL - SEDIMENT RESULTS:

These results, without further analysis or explanation, would indicate that the acceptance criteria for gamma exposure rate and direct beta surface contamination have not been met for the HUT floor. However, as shown on Figure 1.3, an isodose plot of the gamma exposure rate data, two distinct sources of the elevated radioactivity are present.

The highest (22 uRem/hr) and most distinct spot is in the south-west corner, at grid block D-1, adjacent to the bedrock wall of the excavation. The other (17 uRem/hr), somewhat more dispersed, is located along the east bedrock wall of the excavation between grid blocks N-2 and R-7. Both of these locations have been identified as having deposits of natural Thorium ore, and thus can be attributed to causing the elevated gamma exposure rates (as well as elevated direct beta surface contamination results). These Th-232+D deposits can be observed as veins of a brownish-red crusty material. In situ gamma spectral data was obtained at three locations (grid blocks D-1, N-2 and Q-6) as shown on Figure 1.1. Analysis of these spectra indicates the presence of Th-232+D and U-238+D gamma rays. Additionally, the brownish-red material from the south-west corner was sampled and was laboratory analyzed by HPGe gamma spectral analysis. The results also indicated the presence of Th-232+D and U-238+D with a parent Th-232 concentration of approximately 1400 and 1600 pCi/gm respectively. Both the in situ and sample results showed no indication of the typical gamma rays at energies indicative of the reactor and/or hot labs radionuclide mixtures. Additionally, the composite soil sample taken from the HUT floor was found to be free of Cintichem reactor or hot laboratory mixture radionuclides.

Therefore, it can be concluded that the elevated gamma exposure rates and direct beta results are due solely to natural background and that the area meets acceptance criteria.

## 6.1.2 RESULTS SUMMARY

### b Survey Unit: 1.2 Bui Floor Area Cores

**DIRECT SURVEY RESULTS**

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | N.A | 4063 | 454 |
| Number of Meas: | N.A. | 100 | 100 |
| Survey Unit Mean: | N.A. | 2078 | 21 |
| True Mean, U alpha 95% C.L.: | N.A. | 2343 | 30 |
| Criteria/Acceptable Y - N: | N.A. | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | 10606 | 257 |
| Criteria/Acceptable Y - N: | N.A. | 13500/Yes | 5000/Yes |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | N.A. | None | None |
| Criteria/Acceptable Y - N: | N.A. | 40500/Yes | 15000/Yes |
| Ref. Tables | N.A. | 1.2-1 | 1.2-2 |

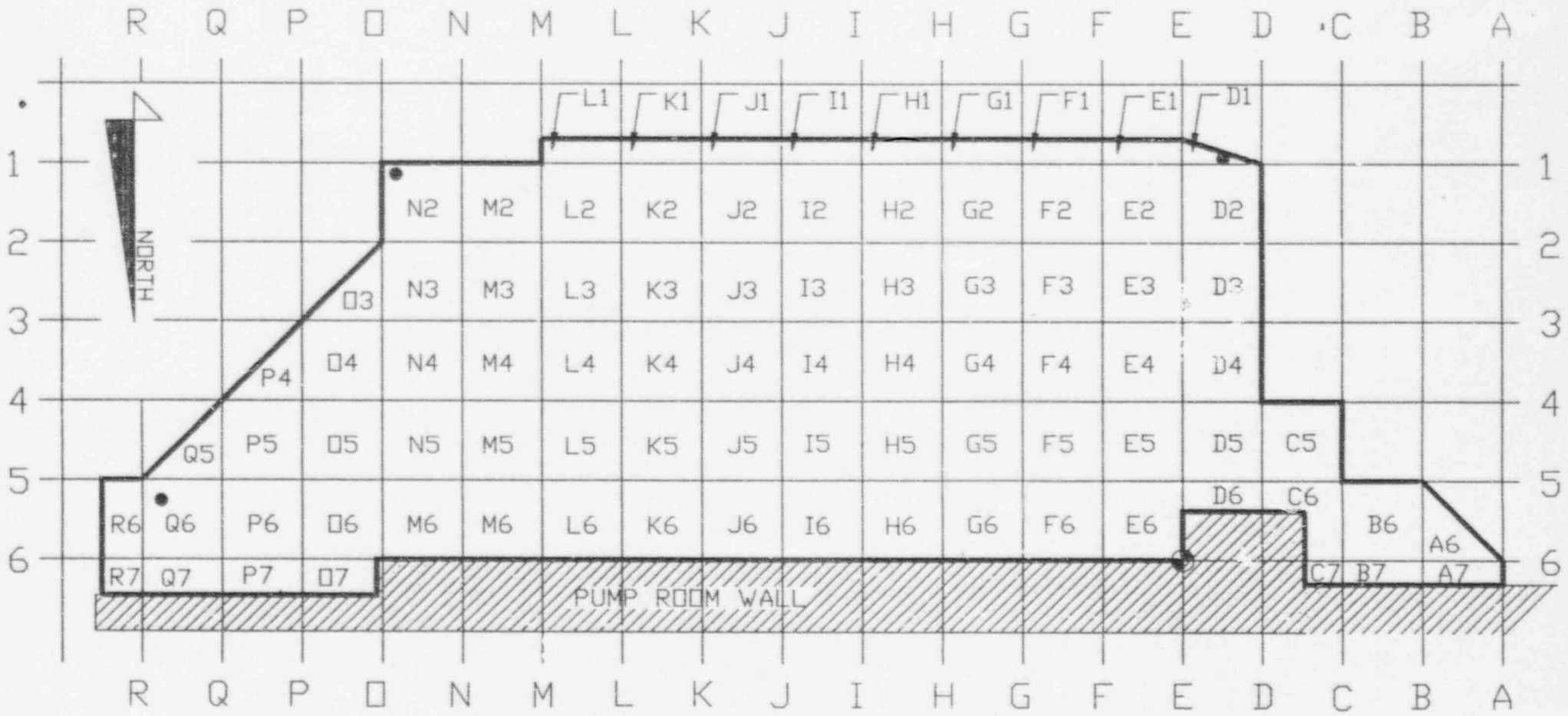
(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

**COMMENTS/SOIL - SEDIMENT RESULTS:**

None

1.1 FLOOR OF HUT




• LOCATION OF GeLi COUNT ON GRID
11/16/94

1.1 FLOOR OF HUT DWGS\2893.
1/12/95

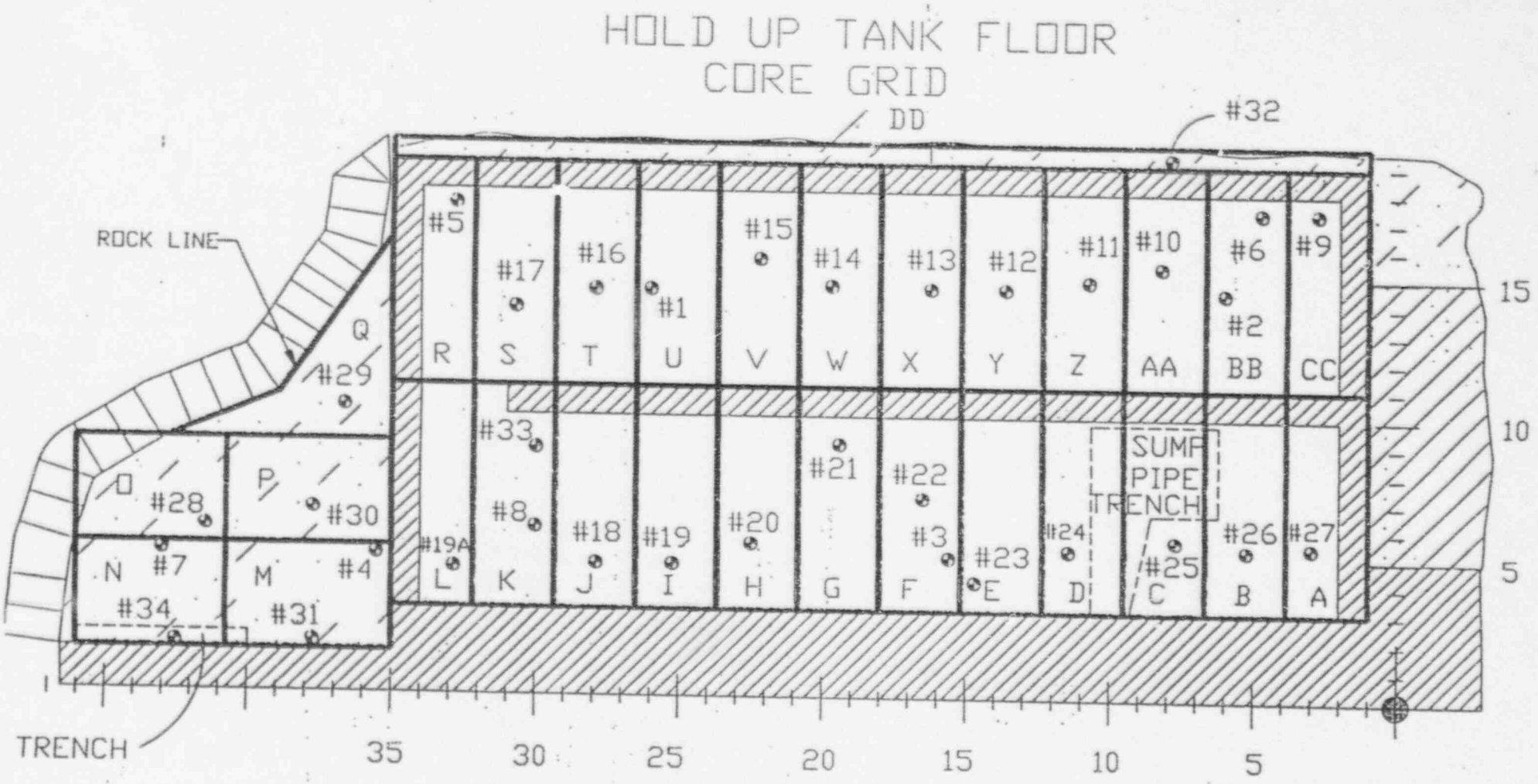
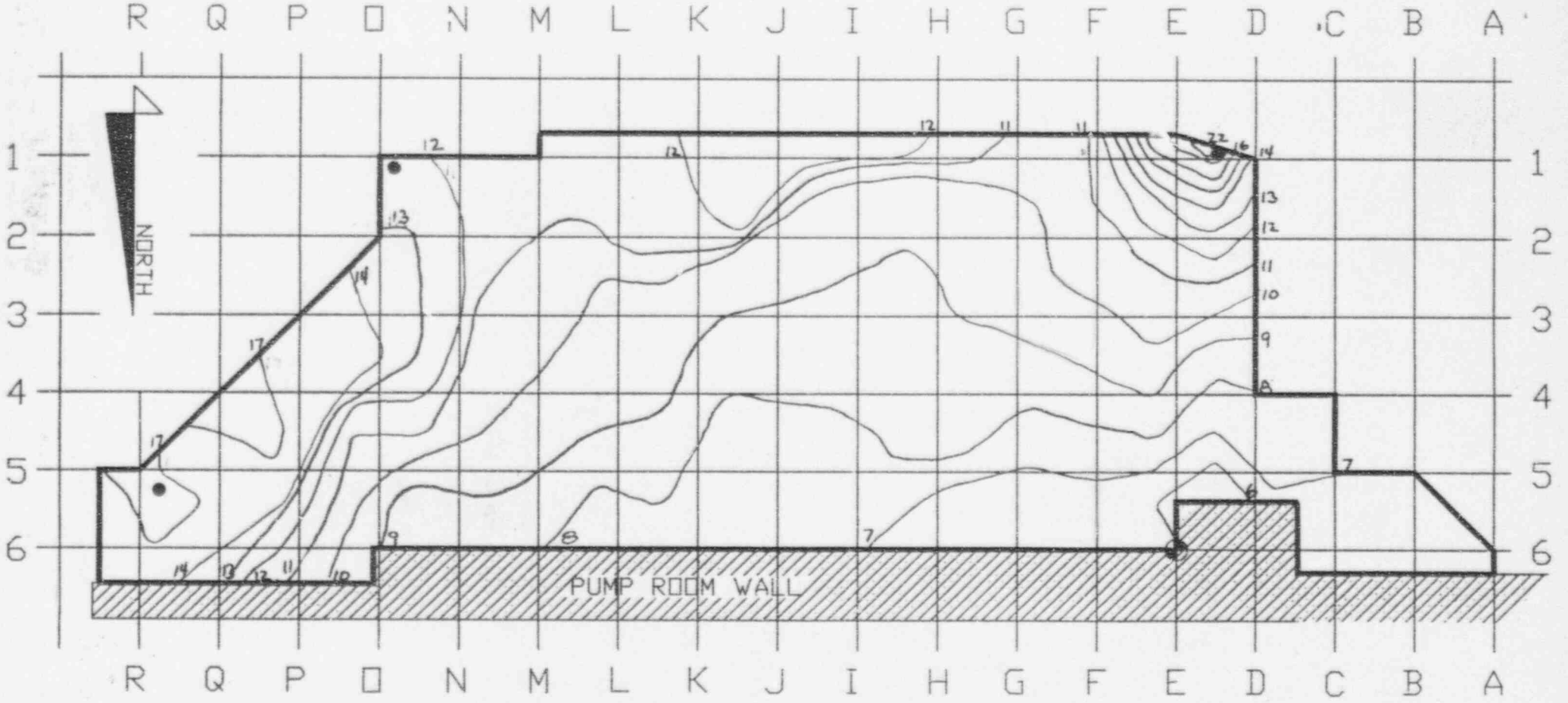



FIGURE 1.2

DWGS\2819B




• LOCATION OF GeLi COUNT ON GRID
11/16/94

1.3 FLOOR OF HUT
GAMMA ISO-DOSE PLOT

DWGS\2893
1/26/95

## 6.2 Area 2.0, South Exterior Wall of Reactor Building

Safe access to this area was found not to be possible with the current configuration of the area. Therefore, no radiological measurements have been made on the two survey unit areas; 2.1 above grade line wall surfaces and 2.2 below grade line wall surfaces. These surfaces will become more accessible as the HUT excavation becomes backfilled. Backfilling will provide a suitable surface upon which lift equipment can be staged adjacent to the building wall. These surfaces will be surveyed at that time and the data included as part of the final survey report.

## 6.3 Area 3.0, East/West Exterior Walls of Reactor Building

### 6.3.1 General Information

The east/west exterior reactor building wall survey consisted of two survey units: 3.1, the painted concrete east wall (an area about 260 $m^2$) and 3.2, the painted concrete west wall (an area about 50 $m^2$). Both of these walls were surveyed on an unaffected area basis. No decontamination work was required for these surfaces.

The 3.1 and 3.2 survey units each consisted of 36 and 30 individual sample/measurement points evenly distributed over the east and west reactor building walls respectively (see Figures 3.1 and 3.2). At each of these points, a direct measurement for beta and alpha surface contamination and a gamma exposure rate measurement at one meter from the wall's surface were made.

Measurement results for the 3.1 survey unit are provided in three attached tables as follows:

Table 3.1-1; East Exterior Wall Reactor Building - gamma exposure rate data

Table 3.1-2; East Exterior Wall Reactor Building - direct beta surface contamination data

Table 3.1-3; East Exterior Wall Reactor Building - direct alpha surface contamination data

Measurement results for the 3.2 survey unit are provided in three attached tables as follows:

Table 3.2-1; West Exterior Wall Reactor Building - gamma exposure rate data

Table 3.2-2; West Exterior Wall Reactor Building - direct beta surface contamination data

Table 3.2-3; West Exterior Wall Reactor Building - direct alpha surface contamination data

## 6.3.2 RESULTS SUMMARY

### a Survey Unit: 3.1 East Exterior Reactor Wall

DIRECT SURVEY RESULTS

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | 1927 | 60 |
| Number of Meas: | 36 | 36 | 36 |
| Survey Unit Mean: | 2.9 | 1053 | 12 |
| True Mean, U alpha 95% C.L.: | 3.6 | 1196 | 16 |
| Criteria/Acceptable Y - N: | 5/Yes | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Ind. Result (un-affected areas only) | 9.0 | 2291 | 42 |
| Criteria/Acceptable Y - N: | 10/Yes | 13500/Yes | 15000/Yes |
| Max. Hot Spot Scans (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Ref. Tables | 3.1-1 | 3.1-2 | 3.1-3 |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

COMMENTS/SOIL - SEDIMENT RESULTS:

None

## 6.3.2 RESULTS SUMMARY

### b Survey Unit: 3.2 West Exterior Wall of Reactor Building

DIRECT SURVEY RESULTS

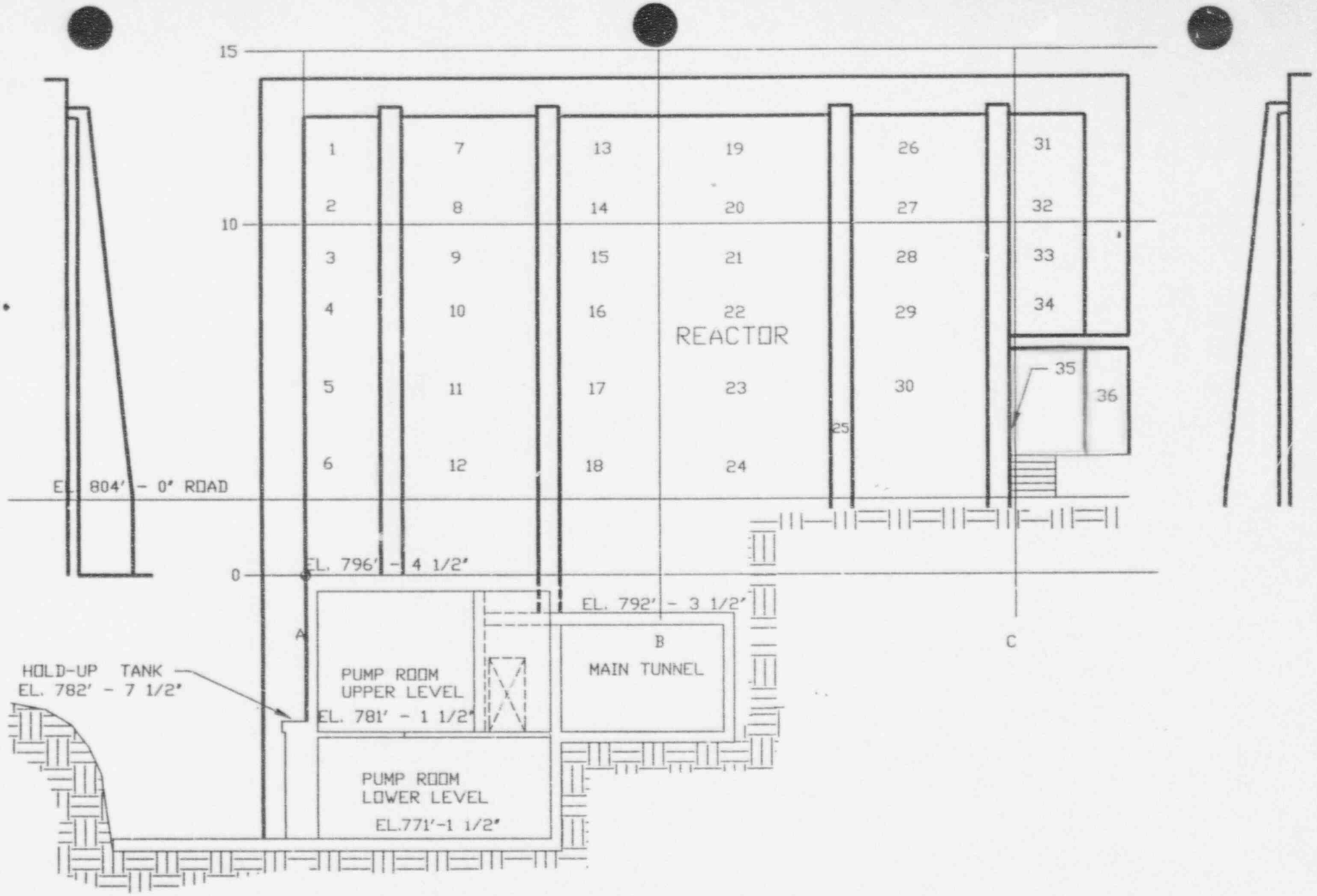
| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | 2168 | 28 |
| Number of Meas: | 30 | 30 | 30 |
| Survey Unit Mean: | 3.1 | 1483 | 4 |
| True Mean, U alpha 95% C.L.: | 3.5 | 1739 | 5 |
| Criteria/Acceptable Y - N: | 5/Yes | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Ind. Result (un-affected areas only) | 6 | 3838 | 23 |
| Criteria/Acceptable Y - N: | 10/Yes | 13500/Yes | 5000/Yes |
| Max. Hot Spot Scans (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Ref. Tables | 3.2-1 | 3.2-2 | 3.2-3 |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

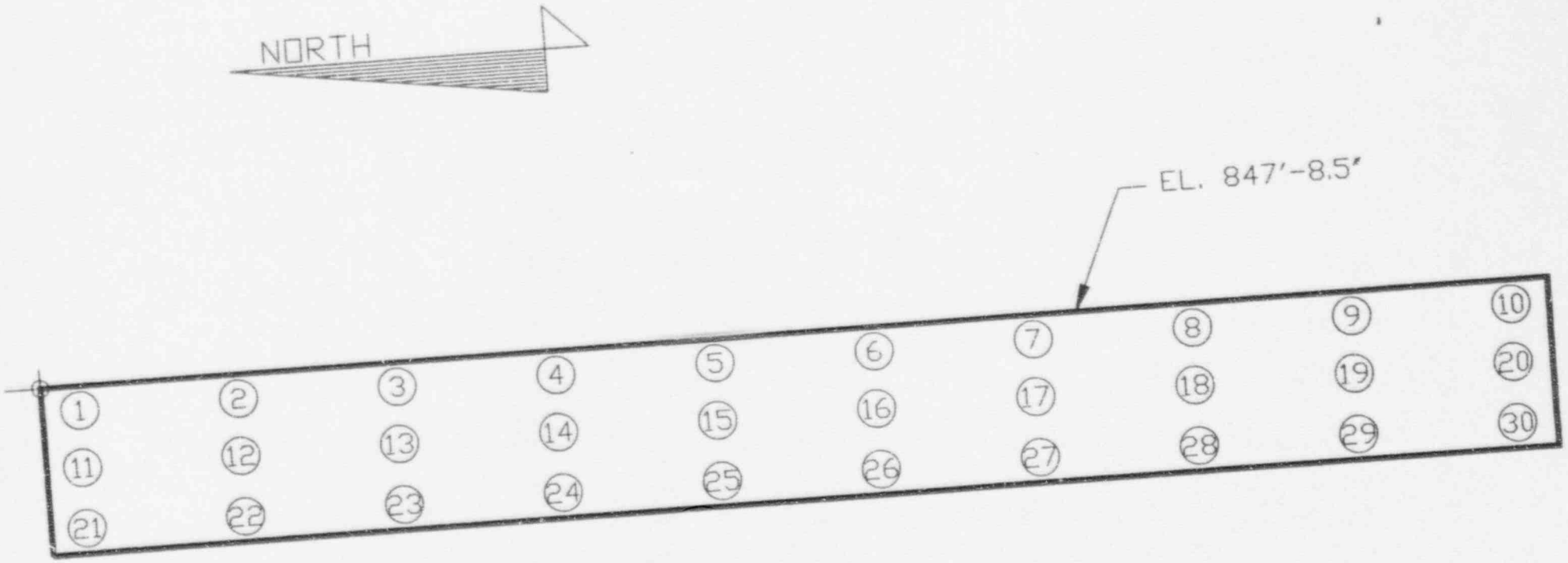
COMMENTS/SOIL - SEDIMENT RESULTS:

None




EAST ELEVATION

3.1 REACTOR EAST EXTERIOR WALL
1/11/95 DWGS\2856 A




3.2 REACTOR EXTERIOR WEST WALL

DWGS\2868A
1/23/95

## 6.4 Area 4.0 Roof of Reactor Building

### 6.4.1 General Information

The reactor building roof survey consisted of four survey units: 4.1, a layer of gravel and sediment, 4.2, a rubber membrane cover (under the gravel and sediment layer), and 4.3, an old roof surface (under the rubber membrane cover). The roof was surveyed on an unaffected area basis. The roof has a surface area of approximately 600 $m^2$. No decontamination work was required for this surface. Each survey unit consisted of 30 individual sample/measurement points, evenly distributed over the roof area. The 30 points for each of the survey units are at the same location, that is, superimposed upon one another (see Figure 4.1). Gamma exposure rate measurements were initially made at one meter above each of the 30 locations. Direct time-integrated measurements for beta and alpha surface contamination were then made at each location. After completion of the direct measurements, the gravel was removed from a 1 $m^2$ area, for each of the 30 locations, and the underlying sediment sampled. After sediment sampling, each of the 1 $m^2$ areas were cleared of remaining sediment and direct beta and alpha surface contamination measurements made on the rubber membrane. Adjacent to the membrane measurement points, 30 sections of the rubber membrane were excised to expose the original roof surface. Direct beta and alpha measurements for surface contamination were then made. Measurement and sampling results for the 4.1 survey unit are provided in the following four attached tables as follows:

Table 4.1-1; Reactor Building Roof - gamma exposure rate data

Table 4.1-2; Reactor Building Roof - gravel surface direct beta surface contamination data

Table 4.1-3; Reactor Building Roof - gravel surface direct alpha surface contamination data

Table 4.1-4; Reactor Building Roof - gravel surface isotopic sediment analysis data

Measurement results for the 4.2 survey unit are provided in the two attached tables as follows:

Table 4.2-1; Reactor Building Roof - rubber membrane direct beta surface contamination data

Table 4.2-2; Reactor Building Roof - rubber membrane direct alpha surface contamination data

Measurement results for the 4.3 survey unit are provided in the three attached tables as follows;

Table 4.3-1; Reactor Building Roof - original roof surface direct beta surface contamination data

Table 4.3-2; Reactor Building Roof - original roof surface direct alpha surface contamination data

Table 4.3-3; Reactor Building Roof - under membrane - gravel isotopic sediment analysis data

## 6.4.2 RESULTS SUMMARY

### a Survey Unit: 4.1 Reactor Building Roof - Gravel

**DIRECT SURVEY RESULTS**

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | 1831 | 36 |
| Number of Meas: | 30 | 30 | 30 |
| Survey Unit Mean: | 0.4 | 3336 | 10 |
| True Mean, U alpha 95% C.L.: | 1 | 3571 | 13 |
| Criteria/Acceptable Y - N: | 5/Yes | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Ind. Result (un-affected areas only) | 3 | 5431 | 34 |
| Criteria/Acceptable Y - N: | 10/Yes | 13500 | 15000/Yes |
| Max. Hot Spot Scans (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Ref. Tables | 4.1-1 | 4.1-2 | 4.1-3 |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

**COMMENTS/SOIL - SEDIMENT RESULTS:**

None

## 6.4.2 RESULTS SUMMARY

### b Survey Unit: 4.2 Reactor Building Roof - Membrane

**DIRECT SURVEY RESULTS**

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 $cm^2$ | dpm/100 $cm^2$ |
| MDA | N.A. | 1876 | 32 |
| Number of Meas: | N.A. | 30 | 30 |
| Survey Unit Mean: | N.A. | 866 | 11 |
| True Mean, U alpha 95% C.L.: | N.A. | 1048 | 14 |
| Criteria/Acceptable Y - N: | N.A. | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | 2269 | N.A. |
| Criteria/Acceptable Y - N: | N.A. | 13500/Yes | N.A. |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | 45 |
| Criteria/Acceptable Y - N: | N.A. | N.A. | 15000/Yes |
| Max. Hot Spot Scans (affected areas only) | N.A. | None | N.A. |
| Criteria/Acceptable Y - N: | N.A. | 40500/Yes | N.A. |
| Ref. Tables | N.A. | 4.2-1 | 4.2-2 |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

**COMMENTS/SOIL - SEDIMENT RESULTS:**

None

## 6.4.2 RESULTS SUMMARY

c Survey Unit: 4.3 Reactor Building Roof - Old Roof Surface

DIRECT SURVEY RESULTS

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | N.A. | 1876 | 32 |
| Number of Meas: | N.A. | 30 | 30 |
| Survey Unit Mean: | N.A. | 1003 | 3 |
| True Mean, U alpha 95% C.L.: | N.A. | 1156 | 4 |
| Criteria/Acceptable Y - N: | N.A. | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | 2080 | N.A. |
| Criteria/Acceptable Y - N: | N.A. | 13500/Yes | N.A. |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | 13 |
| Criteria/Acceptable Y - N: | N.A. | N.A. | 15000/Yes |
| Max. Hot Spot Scans (affected areas only) | N.A. | None | N.A. |
| Criteria/Acceptable Y - N: | N.A. | 40500/Yes | N.A. |
| Ref. Tables | N.A. | 4.3-1 | 4.3-2 |

(a) With a mean site background of 6 uRem/hr subtracted

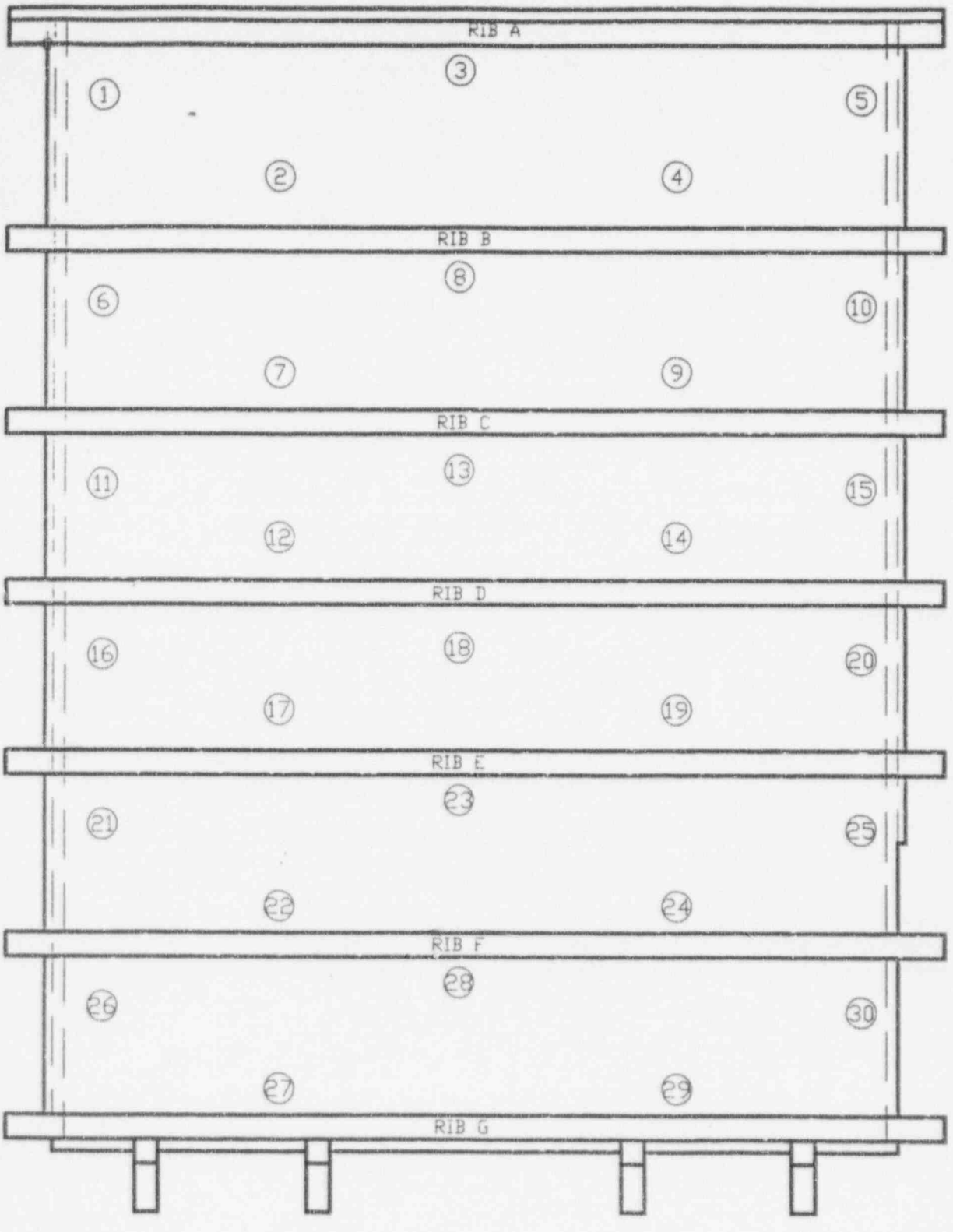
(b) Without subtraction of radioactivity due to natural radioactive material content

COMMENTS/SOIL - SEDIMENT RESULTS:

On Table 4.3-3 the three sediment samples were all found to have no positive gamma emitting radioactive materials above background.

# REACTOR ROOF

EL. 840' 0-1/2" AT CENTER PEAK
EL. 839' 3-1/2" AT N & S EDGES




4.1 GRAVEL & SEDIMENT
4.2 RUBBER MEMBRANE (UNDER GRAVEL)
4.3 OLD ROOF UNDER RUBBER MEMBRANE

DWGS\2858 A
1/23/95

## 6.5 South Exterior Wall of Pump Room

### 6.5.1 General Information

The pump room south exterior wall survey area consisted of three survey units: 5.1 the upper pump room wall (above the HUT roof elevation); 5.2, the lower pump room wall (below the HUT roof elevation); and 5.3, the HUT ledge (a vestige of the HUT roof interior surface between survey units 5.1 and 5.2). These survey units were surveyed on an affected area basis. The 5.2 survey unit wall was also the north interior wall of the Hold-up-Tank and was extensively contaminated prior to completion of the HUT removal task.

The 5.1 survey unit consisted of a tar coated 0.33m thick concrete wall with a surface area of about 60 $m^2$. This wall was above the elevation of the Hold-up-Tank and was initially covered by the soil overburden that was excavated to expose the HUT. This is the soil that comprises survey unit 8.1, which was found to be free of non-natural radioactive contamination. This wall did not require any decontamination work. The survey consisted of 91 measurement points located with a one meter by one meter grid. A measurement of gamma exposure rate and direct beta and alpha surface contamination was made on each grid block. Direct scans for beta and alpha surface contamination were made on 100% of the grid blocks' surface to locate potential "hot spots". If found, they were characterized and quantified.

Measurement results are provided in three attached tables as follows:

Table 5.1-1; Upper Pump Room Wall - gamma exposure rate data

Table 5.1-2; Upper Pump Room Wall - direct beta surface contamination data

Table 5.1-3; Upper Pump Room Wall - direct alpha surface contamination data

The 5.2 survey unit consisted of a bare, 3 foot thick concrete wall. This wall was the interior north wall of the Hold-up-Tank. This wall has a surface area of about 33 $m^2$. Extensive decontamination work has been performed on this wall. The entire wall was scabbled and entire sections have been cut out to remove contaminated cracks and embedments. Measurement points were located with a one meter by one meter grid. Gamma exposure rate, direct beta and direct alpha measurements were made at 63 locations which included the inside surfaces of the wall where sections of the wall were removed. Each grid block was scanned for beta and alpha "hot spots". "Hot spots", if found, were characterized and quantified as necessary.

Measurement results are provided in three attached tables as follows:

Table 5.2-1; Lower Pump Room Wall - gamma exposure rate data

Table 5.2-2; Lower Pump Room Wall - direct beta surface contamination data

Table 5.2-3; Lower Pump Room Wall - direct alpha surface contamination data

The HUT roof ledge is a 0.6 m wide by 0.33 m thick by 11 m long strip of concrete that rests on an 0.6 m wide shelf formed by the intersection of the lower and upper pump room walls. This strip of concrete is a vestige of the HUT roof that was segmented and removed. This survey unit, 5.3, consists of the lower surface of this HUT roof vestige that extends a few centimeters over the lower pump room wall.

The side and top of this concrete strip were included as a part of the other survey units. Decontamination work consisted of removing a contaminated grout fillet that sealed the interface between the lower pump room wall and HUT roof.

Measurements for direct beta and alpha surface contamination were made at 11 partial one meter grid blocks as shown on Figure 5.3. Gamma exposure rate measurements were not made as they would have been redundant to those performed for the 5.1 and 5.2 survey units. The surface was then scanned for beta and alpha contamination "hot spots" and characterized and quantified as necessary.

Measurement results are provided in two attached tables as follows:

Table 5.3-1; HUT Roof Ledge - direct beta surface contamination data

Table 5.3-2; HUT Roof Ledge - direct alpha surface contamination data

## 6.5.2 RESULTS SUMMARY

### a Survey Unit: 5.1 South Exterior Wall of Pump Room Above HUT Roof Elevation

**DIRECT SURVEY RESULTS**

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | 2122 | 56 |
| Number of Meas: | 91 | 91 | 91 |
| Survey Unit Mean: | 6.0 | 1960 | 9 |
| True Mean U alpha 95% C.L.: | 6.5 | 2254 | 12 |
| Criteria/Acceptable Y - N: | 5/*(c) | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | 7599 | 44 |
| Criteria/Acceptable Y - N: | N.A. | 13500/Yes | 5000/Yes |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | 12 | 8114 | 12 |
| Criteria/Acceptable Y - N: | 10/*(c) | 40500/Yes | 15000/Yes |
| Ref. Tables | 5.1-1 | 5.1-2 | 5.1-3 |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

(c) See results text

**COMMENTS/SOIL - SEDIMENT RESULTS:**

Gamma exposure rate results appear to exceed release criteria for the 5.1 survey unit. However, the direct beta surface contamination results indicate that this wall surface has little, if any, contamination on it that would cause the elevated exposure rates. Three in-situ gamma spectra were taken with a portable High Purity Germanium detector at locations for the 5.2 survey unit shown on Figure 5.2. Results indicate that the gamma

exposure rates are due to gamma rays from Th-232+D and U-238+D. No gamma rays from Co-60, Cs-137, Eu-152, Ag108m or any other gamma emitters from the reactor or hot laboratory radionuclide mixtures were found. Therefore, the elevated gamma exposure rates are attributed to natural background. The source of this higher background is the source same as for survey units 1.1, 5.1 and 6.1.

## 6.5.2 RESULTS SUMMARY

### b Survey Unit: 5.2 South Exterior Wall of Pump Room Below HUT Roof Elevation

**DIRECT SURVEY RESULTS**

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | 2529 | 51 |
| Number of Meas: | 63 | 63 | 63 |
| Survey Unit Mean: | 7.8 | 1629 | 8 |
| True Mean, U alpha 95% C.L.: | 9 | 1907 | 11 |
| Criteria/Acceptable Y - N: | 5/*(c) | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | 4375 | 62 |
| Criteria/Acceptable Y - N: | N.A. | 13500/Yes | 5000/Yes |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | 16 | 16325 | 30 |
| Criteria/Acceptable Y - N: | 10/*(c) | 40500/Yes | 15000/Yes |
| Ref. Tables | 5.2-1 | 5.2-2 | 5.2-3 |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

(c) See results text

**COMMENTS/SOIL - SEDIMENT RESULTS:**

As was the case for the 5.1 survey wall, gamma exposure rates are elevated in this area and would appear to exceed release criteria. Direct beta surface contamination measurements indicates that this surface is not the source of the elevated gamma exposure rates. As was previously stated for survey unit

5.1, in-situ gamma spectra were taken at three locations with the highest exposure rates, as shown on Figure 5.2. Results indicate that the elevated gamma exposure rates are due to gamma rays from Th-232+D and U-238+D. No gamma rays from Co-60, Cs-137, Eu-152, Ag-108m or any other gamma emitters from the reactor or hot laboratory radionuclide mixtures were found. Therefore, the elevated gamma exposure rates are attributed to natural background.

## 6.5.2 RESULTS SUMMARY

### c Survey Unit: 5.3 South Exterior Wall of Pump Room at HUT Roof Ledge

**DIRECT SURVEY RESULTS**

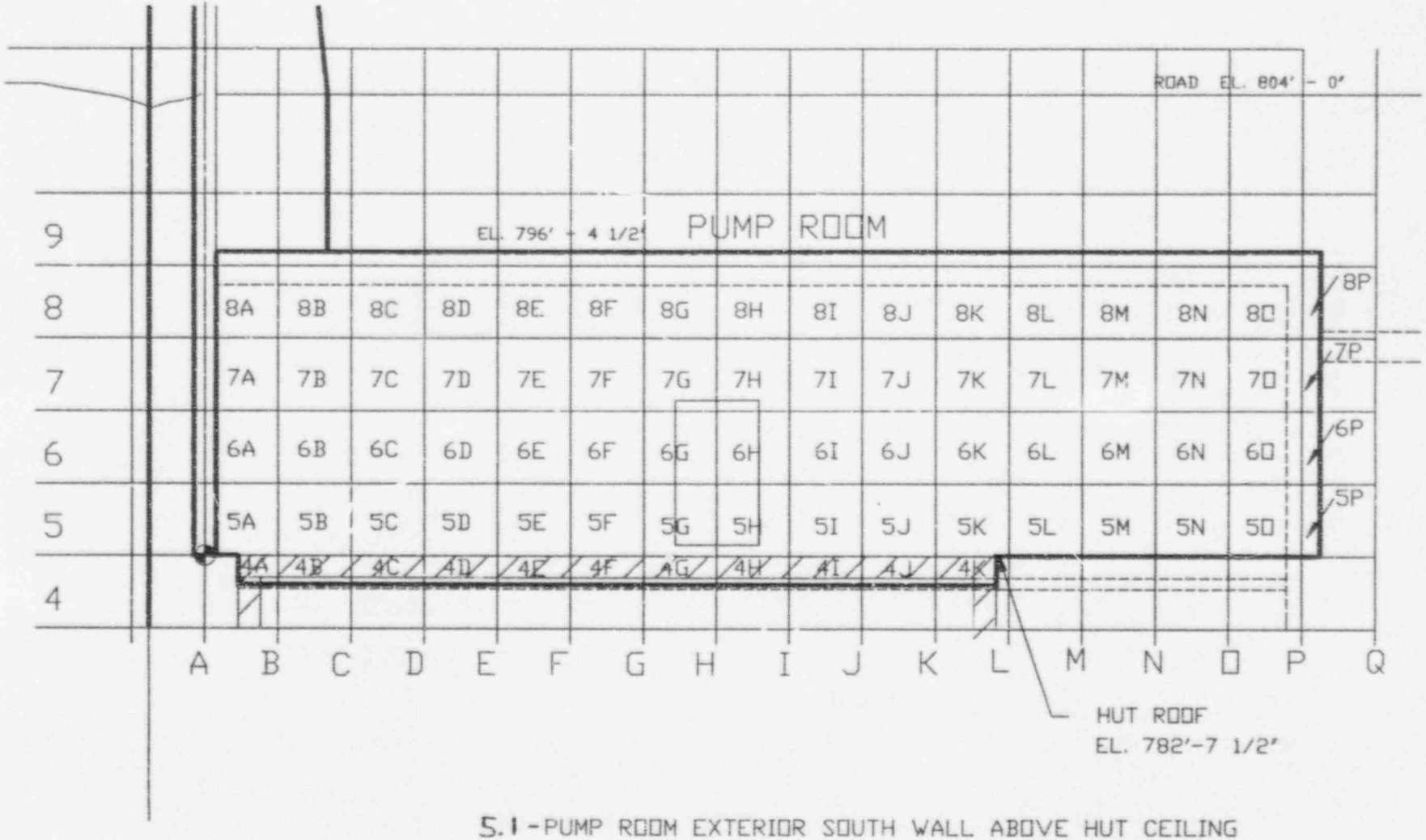
| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | N.A. | 2049 | 42 |
| Number of Meas: | N.A. | 11 | 11 |
| Survey Unit Mean: | N.A. | -102 | 4 |
| True Mean, U alpha 95% C.L.: | N.A. | 125 | 9 |
| Criteria/Acceptable Y - N: | N.A. | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | 413 | 22 |
| Criteria/Acceptable Y - N: | N.A. | 13500/Yes | 5000/Yes |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | N.A. | None | None |
| Criteria/Acceptable Y - N: | N.A. | 40500/Yes | 15000/Yes |
| Ref. Tables | N.A. | 5.3-1 | 5.3-2 |

(a) With a mean site background of 6 uRem/hr subtracted

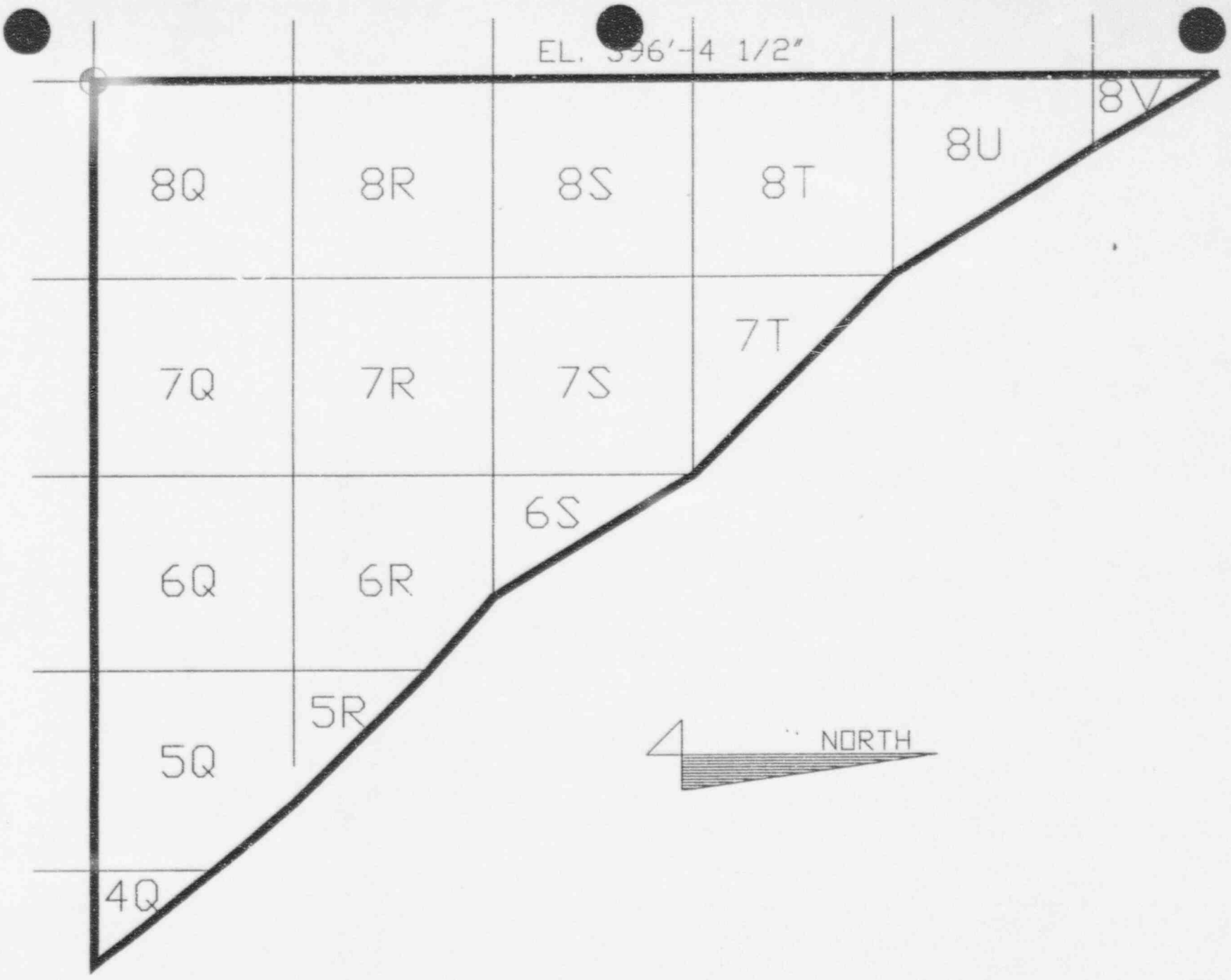
(b) Without subtraction of radioactivity due to natural radioactive material content

**COMMENTS/SOIL - SEDIMENT RESULTS:**

None

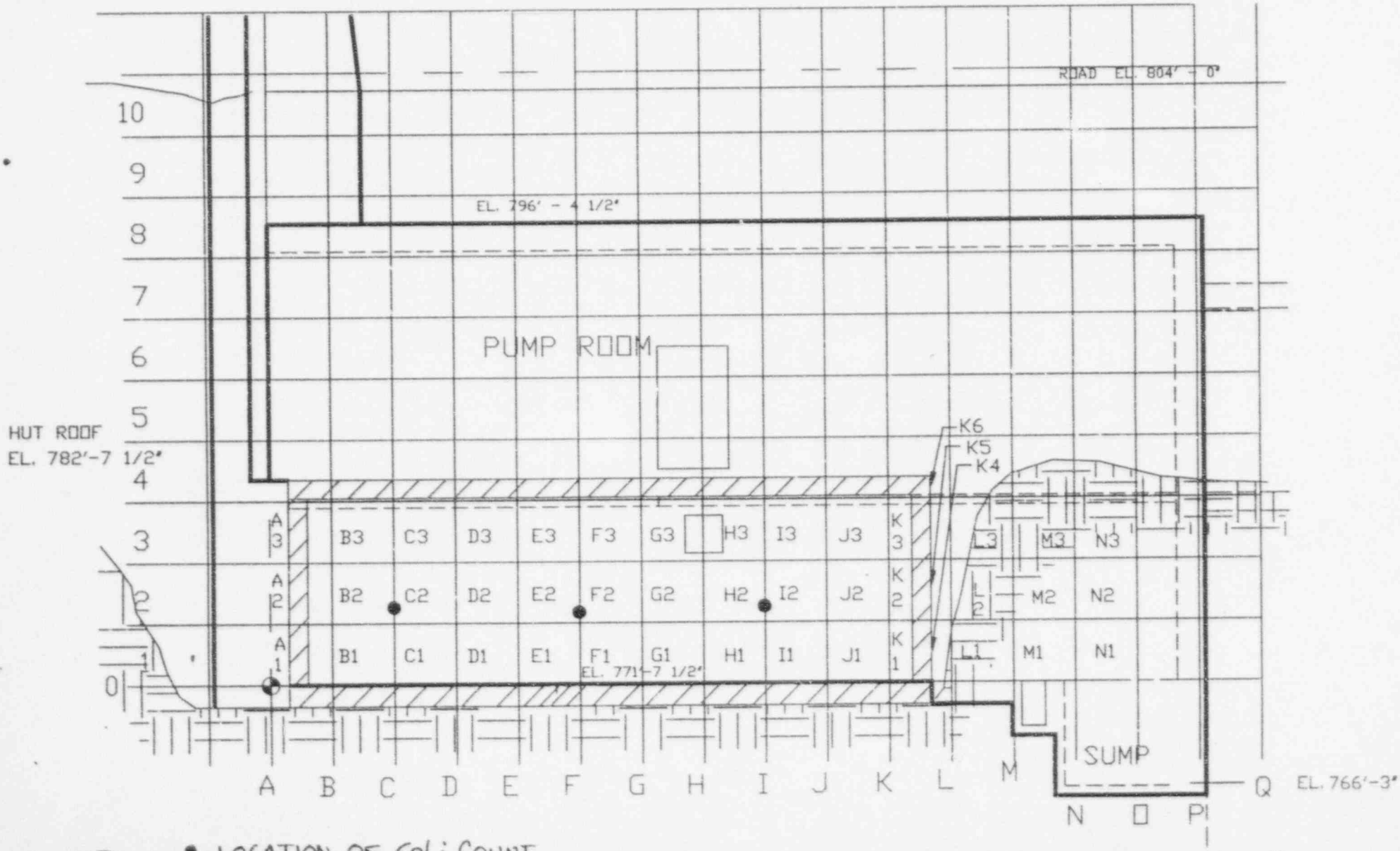



5.1 - PUMP ROOM EXTERIOR SOUTH WALL ABOVE HUT CEILING
DWGS\2896
1/13/95




5.1 EAST EXTERIOR PUMP ROOM WALL ABOVE HUT ROOF ELEV.

DWGS\2894

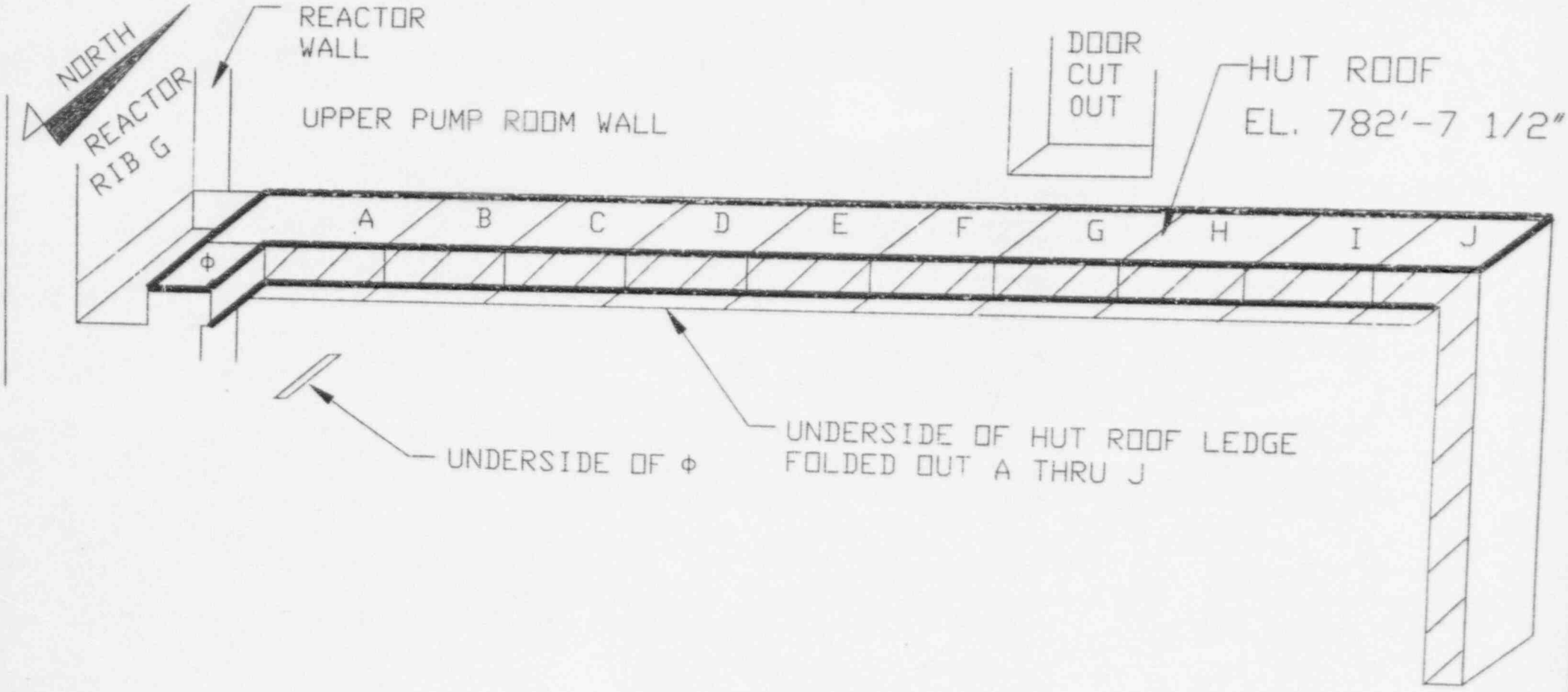



• LOCATION OF GeLi COUNT

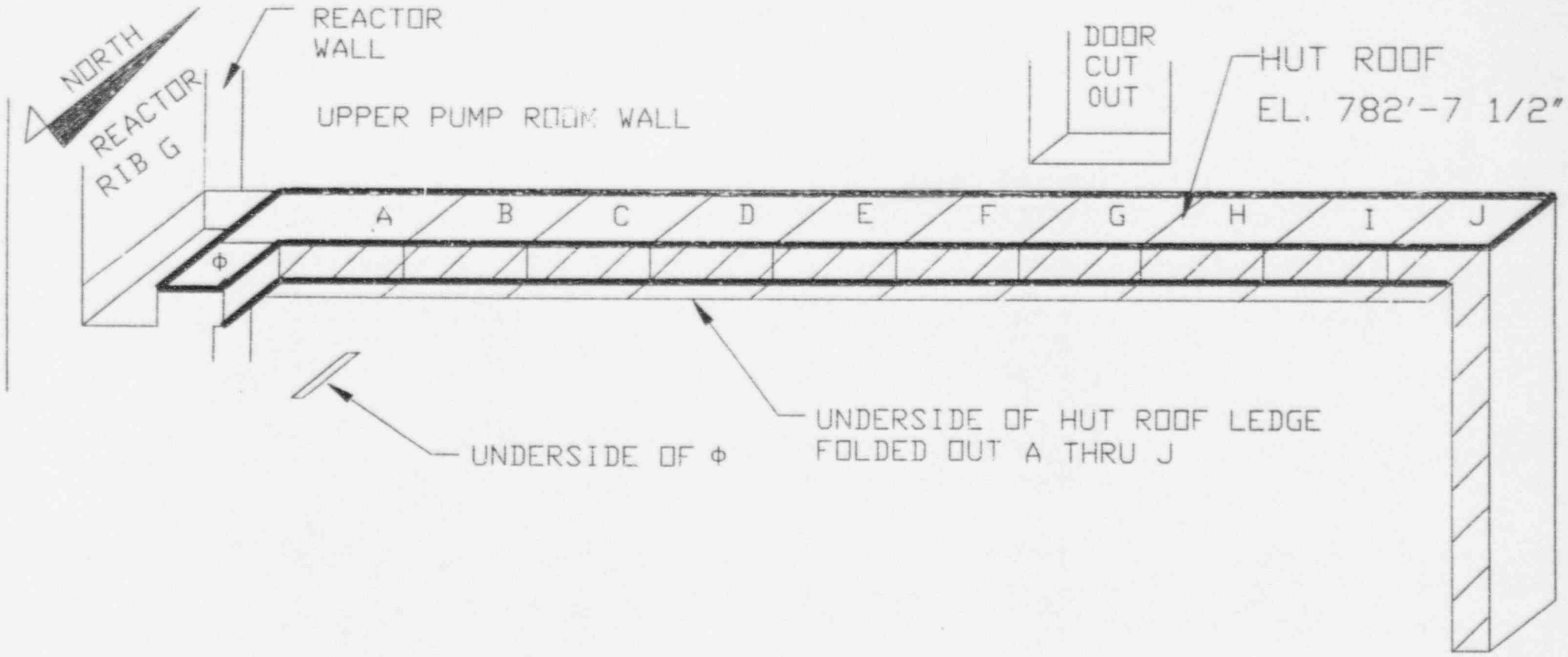
5.2 SOUTH EXTERIOR WALL OF PUMP ROOM

1/11/95

DWG\2859




5.3 HUT ROOF LEDGE




5.3 HUT ROOF LEDGE

## 6.6 Bedrock Wall of HUT Excavation

### 6.6.1 General Information

This survey area consisted of a single survey unit: 6.1, the bedrock wall that forms the east, west and south sides of the HUT excavation, from the HUT floor to about 3.5 M high (an elevation approximately equal to that of the HUT roof). This survey unit covers a "planer" area of about 85 $m^2$. The actual surface is comprised of an extremely jagged surface consisting primarily of bedrock outcroppings covered with deposits of rock dust, rubble and soil. The slope of this surface ranges from approximately vertical to 45°. Not all areas within this survey unit are safely accessible.

The survey consisted of 30 measurement points distributed over the bedrock surface, as evenly as was possible considering access limitations. The survey unit is considered an affected area and would normally have had the measurement points located with a one meter by one meter grid system. However, due to safety concerns, the grid could not be emplaced, and measurements were located where access could be made.

Direct beta and alpha measurements for surface contamination were made at each location, along with gamma exposure rates at one meter from the bedrock surface. Measurement locations are shown on Figure 6-1. Measurement results are presented in three attached tables as follows:

Table 6.1-1; Bedrock HUT Wall - gamma exposure rate data

Table 6.1-2; Bedrock HUT Wall - direct beta surface contamination data

Table 6.1-3; Bedrock HUT Wall - Direct alpha surface contamination data

## 6.6.2 RESULTS SUMMARY

### a Survey Unit: 6.1 Bedrock Wall of HUT Excavation - HUT Floor to Top of HUT Roof Elevation

DIRECT SURVEY RESULTS

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | 2773 | 83 |
| Number of Meas: | 30 | 30 | 30 |
| Survey Unit Mean: | 14.3 | 10145 | -32 |
| True Mean, U alpha 95% C.L.: | 16.4 | 12547 | -12 |
| Criteria/Acceptable Y - N: | 5/(c) | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Ind. Result (un-affected areas only) | 34 | 34300 | 166 |
| Criteria/Acceptable Y - N: | 10/(c) | 13500(c) | 15000/Yes |
| Max. Hot Spot Scans (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Ref. Tables | 6.1-1 | 6.1.2 | 6.1-3 |

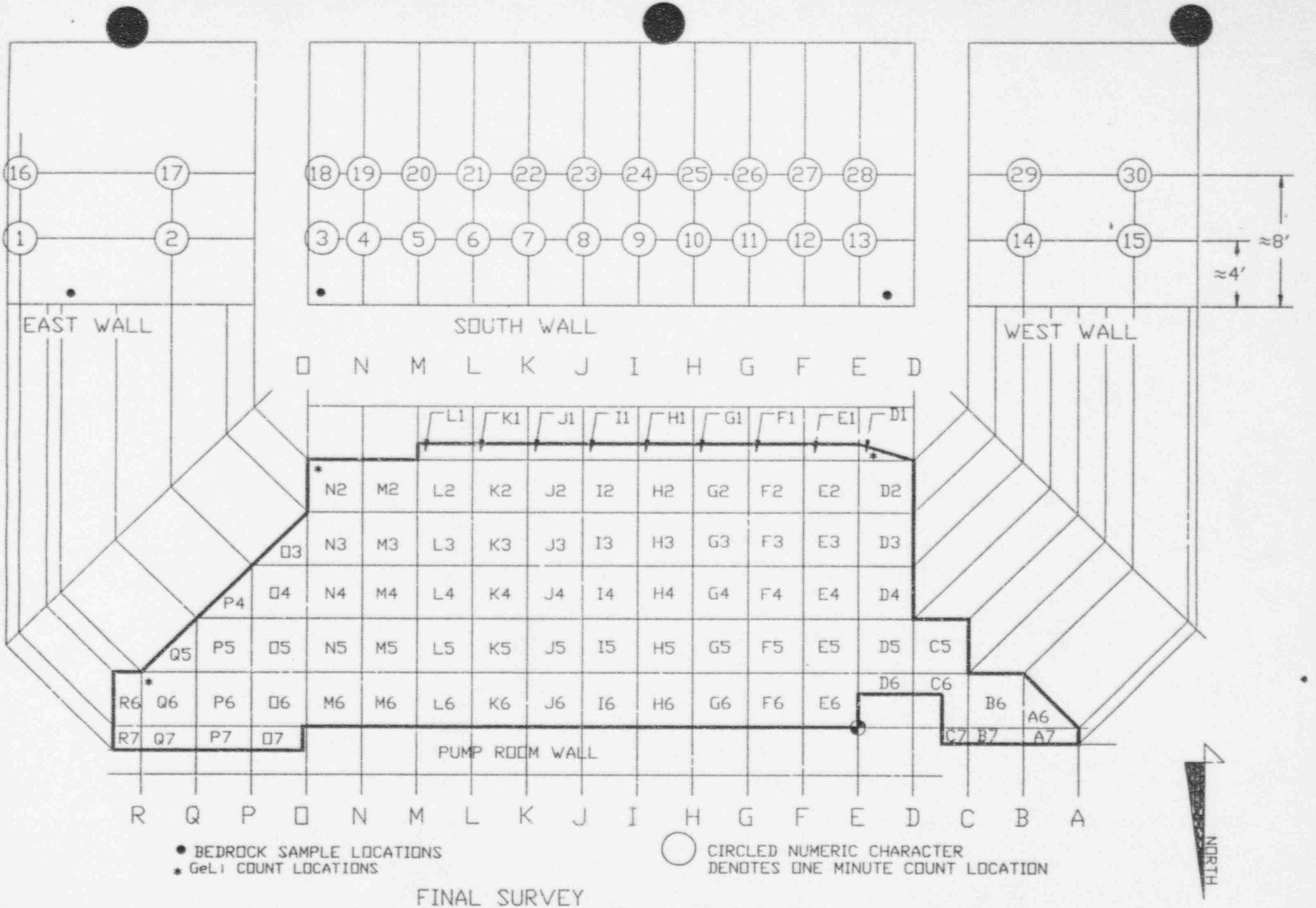
(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

(c) See results text

COMMENTS/SOIL - SEDIMENT RESULTS:

Gamma exposure rates were found to average 14 uRem/hr, with a maximum result of 34 uRem/hr. At first glance, these results appear to exceed the average and maximum criteria of 5 and 10 uRem/hr respectively. However, these results are corrected only for the average site background of 6 uRem/hr, exclusive of "hot spots" due to natural deposits of Th-232+D and U-238+D. Likewise, the direct beta surface contamination results also appear to be elevated.




● BEDROCK SAMPLE LOCATIONS
* GeLi COUNT LOCATIONS

○ CIRCLED NUMERIC CHARACTER DENOTES ONE MINUTE COUNT LOCATION

FINAL SURVEY
6.0 BEDROCK WALL OF HUT EXCAVATION
6.1 HUT FLOOR TO TOP OF HUT ROOF EXCAVATION

DWGS\2900
1/20/95

As previously described in section 6.1, the HUT floor survey unit, the general area contains significant deposits of natural Th-232+D and U-238+D which clearly are causing the elevated results. As such, these elevated results are attributed to natural background and therefore, the survey unit meets acceptance criteria.

## 6.7 Exterior Roof of Pump Room

### 6.7.1 General Information

The pump room roof survey consisted of a single survey unit: 7.1, a concrete surface with an area of about 100 $m^2$. This surface was surveyed on an affected-area basis. While this surface has not required any decontamination work, it was treated as an affected area because a primary water storage tank fill line that penetrated the pump room roof had previously been present. A concrete hole is currently located in grid boxes C2 and D2 (see Figure 7.0). Additionally, the pump room roof was used as a staging area for removal of the contaminated Hold-up Tank structure and soil.

A one meter by one meter grid was used to locate sample and/or measurement points, with 116 full or partial grid blocks being present (see Figure 7.0). Direct beta and alpha surface contamination measurements, as well as gamma exposure rate measurements, were made for each of the 116 grid blocks. Additionally, each grid block was scanned for "hot spots" and then quantified and characterized as necessary.

Measurement and sampling results for the 7.1 survey unit are provided in three attached tables as follows:

Table 7.1-1; Pump Room Roof - gamma exposure rate data

Table 7.1-2; Pump Room Roof - direct beta surface contamination data

Table 7.1-3; Pump Room Roof - direct alpha surface contamination data

Table 7.1-4; Pump Room Roof - soil surface isotopic sediment analysis data

## 6.7.2 RESULTS SUMMARY

### a Survey Unit: 7.1 Exterior Roof of Pump Room

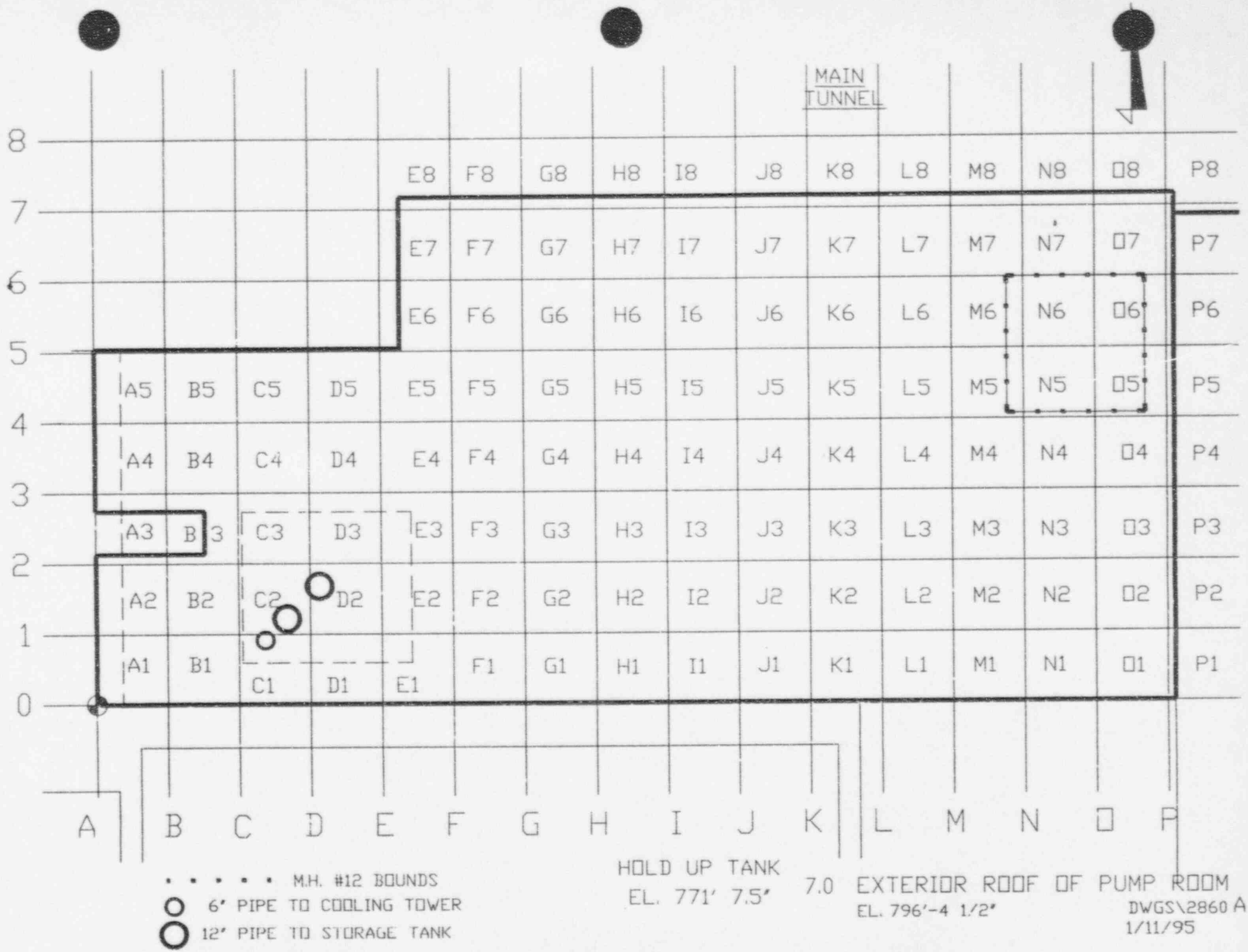
**DIRECT SURVEY RESULTS**

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | 2250 | 49 |
| Number of Meas: | 116 | 116 | 116 |
| Survey Unit Mean: | 2.5 | 964 | 15 |
| True Mean, U alpha 95% C.L.: | 2.8 | 1136 | 17 |
| Criteria/Acceptable Y - N: | 5/Yes | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | 4054 | 70 |
| Criteria/Acceptable Y - N: | N.A. | 13500/Yes | 5000/Yes |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | 6.0 | 16495 | 75 |
| Criteria/Acceptable Y - N: | 10/Yes | 40500/Yes | 15000/Yes |
| Ref. Tables | 7.1-1 | 7.1-2 | 7.1-3 |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

**COMMENTS/SOIL - SEDIMENT RESULTS:**


MAIN TUNNEL
8
7
6
5
4
3
2
1
0
A
B
C
D
E
F
G
H
I
J
K
L
M
N
O
P
E8 F8 G8 H8 I8 J8 K8 L8 M8 N8 O8 P8
E7 F7 G7 H7 I7 J7 K7 L7 M7 N7 O7 P7
E6 F6 G6 H6 I6 J6 K6 L6 M6 N6 O6 P6
A5 B5 C5 D5 E5 F5 G5 H5 I5 J5 K5 L5 M5 N5 O5 P5
A4 B4 C4 D4 E4 F4 G4 H4 I4 J4 K4 L4 M4 N4 O4 P4
A3 B3 C3 D3 E3 F3 G3 H3 I3 J3 K3 L3 M3 N3 O3 P3
A2 B2 C2 D2 E2 F2 G2 H2 I2 J2 K2 L2 M2 N2 O2 P2
A1 B1 C1 D1 E1 F1 G1 H1 I1 J1 K1 L1 M1 N1 O1 P1
M.H. #12 BOUNDS
6' PIPE TO COOLING TOWER
12' PIPE TO STORAGE TANK
HOLD UP TANK
EL. 771' 7.5"
7.0 EXTERIOR ROOF OF PUMP ROOM
EL. 796'-4 1/2"
DWGS\2860 A
1/11/95

## 6.8 Area 8.0, Grounds (South of Reactor Building Within RCA)

### 6.8.1 General Information

The grounds area survey consisted of six survey units: 8.1 the south soil spoils pile, 8.2 the asphalt driveway, 8.3 the HUT excavation surrounding soil/bedrock (above HUT roof and survey unit 6.1 elevations), 8.4 the concrete spillway behind (west) of the reactor building, 8.5 remaining ground surfaces west of the driveway (8.2) (exclusive of survey areas 10.0 Storage Tank Excavation and 11.0 Cooling Tower) and 8.6 ground surfaces east of the 8.2 driveway.

Survey units 8.1 and 8.2 were surveyed on an affected area basis. Survey unit 8.1, a spoils pile, is comprised of soil from the HUT excavation (an affected area). Survey unit 8.2, the driveway, has been used as a staging area for removal of the storage tank and decontamination and surveys of the exhaust stack and duct sections. Survey units 8.3, 8.4, 8.5 and 8.6 were surveyed on an unaffected area basis. These areas have not required any remediation nor have had any history of being used for storage of radioactive material.

Survey unit 8.1 consists of an approximately 400 $m^2$ area located at the south-west corner of the Cintichem RCA (see Figure 8.1). This area was used for storage of non-contaminated soil that was removed from the upper (above the HUT roof elevation) HUT excavation. This spoils pile contains approximately 660 $m^3$ of soil. This pile is represented by 70 composite soil samples, with aliquots taken from each of the 70 batches of soil that were placed upon the pile. Additionally, 20 gamma exposure rate measurements were made above the soil pile based upon 5 measurements per 100 $m^2$ grid block.

Measurement and sampling results are provided in two attached tables as follows:

Table 8.1-1 South Spoils Pile - gamma exposure rate data

Table 8.1-2 South Spoils Pile - soil sample data

The survey unit 8.2 survey consisted of the asphalt driveway that extends from the south RCA gate northeast to the HUT excavation. The driveway has a surface area of about 530 $m^2$. Measurement points were located with a one meter by one meter grid system and are shown on Figure 8.1. Six hundred-eighty-one (681) gamma exposure rate, direct beta and direct alpha surface contamination measurements were made on this surface.

Each of the one by one meter grid blocks were scanned for "hot spots" over one-hundred percent of the surface area, and then characterized and quantified as appropriate. Soil samples, from under the roadway surface, were obtained at eight locations where elevated gamma and/or beta activity was detected.

Measurement and sampling results are provided in four attached tables as follows:

Table 8.2-1; Driveway - gamma exposure rate data

Table 8.2-2; Driveway - direct beta surface contamination data

Table 8.2-3; Driveway - direct alpha surface contamination data

Table 8.2-4; Driveway - soil sample data

The 8.3 survey unit consists of the upper HUT excavation (i.e. above the HUT roof elevation, immediately above the 6.1 survey unit bedrock wall). This survey unit consists primarily of soil with bedrock outcroppings, with an approximate area of 640 $m^2$. Thirty sampling and measurement locations were evenly distributed over the survey unit as shown in Figure 8.2. At each of the 30 locations a gamma exposure rate was taken at one meter above the soil surface and a surface soil sample.

Measurement and sampling results are provided in two attached tables as follows:

Table 8.3-1; HUT Excavation - gamma exposure rate data

Table 8.3-2; HUT Excavation - soil sample data

The 8.4 survey unit consists of a concrete spillway located on the west side of the reactor building. The spillway is a water collection gutter for diverting runoff coming from the mountain that is west of the reactor building. The spillway has a surface area of approximately 80 $m^2$. The spillway is located approximately 20 meters above the HUT floor elevation. Measurements for gamma exposure rate, direct beta surface contamination and direct alpha surface contamination were made at 30 evenly distributed points on the spillway surface as shown on Figure 8.3. Additionally, deposits of sediment and/or soil were encountered on the surface and six samples were taken.

Measurement and sampling results are provided in four attached tables as follows:

Table 8.4-1; Spillway - gamma exposure rate data

Table 8.4-2; Spillway - direct beta surface contamination data

Table 8.4-3; Spillway - direct alpha surface contamination data

Table 8.4-4; Spillway - sediment sample data

The 8.5 survey unit consists of the ground area south of the HUT excavation excluding those areas covered under another survey unit (i.e. exclusive of survey units 8.1, 8.2, 8.3, 8.4, 8.6, 10.1, 10.2, 11.1 and 11.2). The 8.5 survey unit has an area of approximately 1000 $m^2$. The survey consisted of 30 evenly distributed measurement/sampling points, each at which a surface soil sample collected and a gamma exposure rate measurement taken. The locations of these points are shown on Figure 8.4.

Measurement and sampling results are provided in two attached tables as follows:

Table 8.5-1; General Grounds Area - gamma exposure rate data

Table 8.5-2; General Grounds Area - soil sample data

The 8.6 survey unit consists of a thin strip ground area east of the 8.2 survey unit driveway and west of the RCA fence. This survey unit has a surface area of about 190 $m^2$. The survey consisted of 30 evenly distributed measurement/sampling points, each at which a surface soil sample was collected and a gamma exposure rate measurement taken. The grid locations of these 30 points are shown on Figure 8.1.

Measurement and sampling results are provided in two attached tables as follows:

Table 8.6-1; East of Driveway Grounds - gamma exposure rate data

Table 8.6-2; East of Driveway Grounds - soil sample data

## 6.8.2 RESULTS SUMMARY

### a Survey Unit: 8.1 Grounds (South of Reactor Building within RCA) - Spoils Pile

**DIRECT SURVEY RESULTS**

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 $cm^2$ | dpm/100 $cm^2$ |
| MDA | 2 | N.A. | N.A. |
| Number of Meas: | 20 | N.A. | N.A. |
| Survey Unit Mean: | 2.3 | N.A. | N.A. |
| True Mean, U alpha 95% C.L.: | 2.8 | N.A. | N.A. |
| Criteria/Acceptable Y - N: | 5/Yes | N.A. | N.A. |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | 6.0 | N.A. | N.A. |
| Criteria/Acceptable Y - N: | 10/Yes | N.A. | N.A. |
| Ref. Tables | 8.1-1 | N.A. | N.A. |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

**COMMENTS/SOIL - SEDIMENT RESULTS:**

All 70 of the composite soil samples were found to be acceptable when compared to the soil release criteria. Eight samples were found to have detectable Sr-90, with a maximum concentration of 1.8 pCi/gm (10.3% of criteria). Forty-four samples were found

with detectable Cs-137 of which only one was found to be greater than the background level of 1.25 pCi/gm with a concentration of 1.83 pCi/gm above background. The sample with the highest overall concentration was found with 1.5 pCi/gm Sr-90 and 1.83 pCi/gm Cs-137 to yield a total sum-of-fractions of release criteria for positive results of 0.56.

## 6.8.2 RESULTS SUMMARY

### b Survey Unit: 8.2 Grounds (South of Reactor Building within RCA) - Driveway Asphalt

**DIRECT SURVEY RESULTS**

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | 2096 | 58 |
| Number of Meas: | 681 | 681 | 681 |
| Survey Unit Mean: | 1.7 | 1989 | 11 |
| True Mean, U alpha 95% C.L.: | 1.8 | 2067 | 11 |
| Criteria/Acceptable Y - N: | 5/Yes | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | 8730 | 50 |
| Criteria/Acceptable Y - N: | N.A. | 13500/Yes | 5000/Yes |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | 7.0 | 17114 | 41 |
| Criteria/Acceptable Y - N: | 10/Yes | 40500/Yes | 15000/Yes |
| Ref. Tables | 8.2-1 | 8.2-2 | 8.2-3 |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

**COMMENTS/SOIL - SEDIMENT RESULTS:**

The eight soil samples taken from under the driveway's asphalt layer were all found to meet soil release criteria. All samples were found with detectable radioactivity. Cs-137 was detected in seven of the samples, all at background levels. Sr-90 was detected in two samples with the highest concentration being 0.14 pCi/gm (< 1% of release criteria). Co-60 was found in one sample at a concentration 0.2 pCi/gm (22% of release criteria). The sample with Co-60 detected in it did not contain any other radionuclides above background.

## 6.8.2 RESULTS SUMMARY

### c Survey Unit: 8.3 Grounds South of Reactor Building within RCA HUT Excavation Soil Above HUT Roof Elevation

DIRECT SURVEY RESULTS

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | N.A. | N.A. |
| Number of Meas: | 30 | N.A. | N.A. |
| Survey Unit Mean: | 37 | N.A. | N.A. |
| True Mean, U alpha 95% C.L.: | 4.3 | N.A. | N.A. |
| Criteria/Acceptable Y - N: | 5/Yes | N.A. | N.A. |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | 10 | N.A. | N.A. |
| Criteria/Acceptable Y - N: | 10/(yes) | N.A. | N.A. |
| Ref. Tables | 8.3-1 | N.A. | N.A. |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

COMMENTS/SOIL - SEDIMENT RESULTS:

Gamma exposure rates were found to meet the average and maximum criteria with 3.6 uRem/hr and 10 uRem/hr being found. The true mean (u-sub-alpha) was calculated to be 4.3 uRem/hr. These results have been corrected for background by subtraction of the

average site background of 6 uRem/hr. While these results meet release criteria, they are clearly influenced by higher background levels caused by the natural Th-232+D and U-238+D deposits previously discussed in survey units 1.1 and 6.1. As such, the elevated gamma exposure rates reported herein are most likely due to a higher natural background.

All soil samples were found to meet soil release criteria. Only Cs-137 at background concentrations was found in three of the samples.

## 6.8.2 RESULTS SUMMARY

### d Survey Unit: 8.4 Grounds South of Reactor Building within RCA - Spillway Around Reactor Building

**DIRECT SURVEY RESULTS**

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | 2230 | 28 |
| Number of Meas: | 30 | 30 | 30 |
| Survey Unit Mean: | 3 | 596 | 17 |
| True Mean, U alpha 95% C.L.: | 3 | 972 | 20 |
| Criteria/Acceptable Y - N: | 5/Yes | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Ind. Result (un-affected areas only) | 6 | 3473 | 38 |
| Criteria/Acceptable Y - N: | 10/Yes | 13500/Yes | 15000/Yes |
| Max. Hot Spot Scans (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Ref. Tables | 8.4-1 | 8.4-2 | 8.4-3 |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

**COMMENTS/SOIL - SEDIMENT RESULTS:**

Five of the six sediment samples taken from the spillway surface were found with greater than background levels of Cs-137. Of the five samples, four exceed the release criteria, with a maximum concentration of 9.4 pCi/gm above background being found.

Therefore, this survey unit does not meet release criteria. At the present time, as with survey unit 9.1, it is not known if these levels are due to the concentrating of Cs-137 fallout from runoff off of the mountain or due to site contamination. As such, further investigations will be required for this area to determine if remediation is warranted. Survey unit 8.4 is therefore no longer included in this interim release process.

## 6.8.2 RESULTS SUMMARY

### e Survey Unit: 8.5 Grounds South of Reactor Building Within RCA

**DIRECT SURVEY RESULTS**

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | N.A. | N.A. |
| Number of Meas: | 30 | N.A. | N.A. |
| Survey Unit Mean: | 2 | N.A. | N.A. |
| True Mean, U alpha 95% C.L.: | 2 | N.A. | N.A. |
| Criteria/Acceptable Y - N: | 5/Yes | N.A. | N.A. |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Ind. Result (un-affected areas only) | 4 | N.A. | N.A. |
| Criteria/Acceptable Y - N: | 10/Yes | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Ref. Tables | 8.5-1 | N.A. | N.A. |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

**COMMENTS/SOIL - SEDIMENT RESULTS:**

Four soil samples were found with detectable radioactivity greater than background levels. One with Sr-90 (1 pCi/gm) and three with Cs-137 (0.44 to 0.84 pCi/gm). All four of these samples meet release criteria with the highest sum-of-fractions of release criteria for positive results being 0.22.

## 6.8.2 RESULTS SUMMARY

f Survey Unit: 8.6 Grounds South of Reactor Building within RCA - East of Driveway

DIRECT SURVEY RESULTS

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | N.A. | N.A. |
| Number of Meas: | 30 | N.A. | N.A. |
| Survey Unit Mean: | 2.8 | N.A. | N.A. |
| True Mean, U alpha 95% C.L.: | 3.3 | N.A. | N.A. |
| Criteria/Acceptable Y - N: | 5/Yes | N.A. | N.A. |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Ind. Result (un-affected areas only) | 6 | N.A. | N.A. |
| Criteria/Acceptable Y - N: | 10/Yes | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Ref. Tables | 8.6-1 | N.A. | N.A. |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

COMMENTS/SOIL - SEDIMENT RESULTS:

Three soil samples were found with detectable radioactivity above background, two samples with Cs-137 and one with Cs-137, Sr-90 and Co-60. The sample with the highest sum-of-fractions of release criteria for positive results was 0.73. Therefore, this survey unit meets soil release criteria.

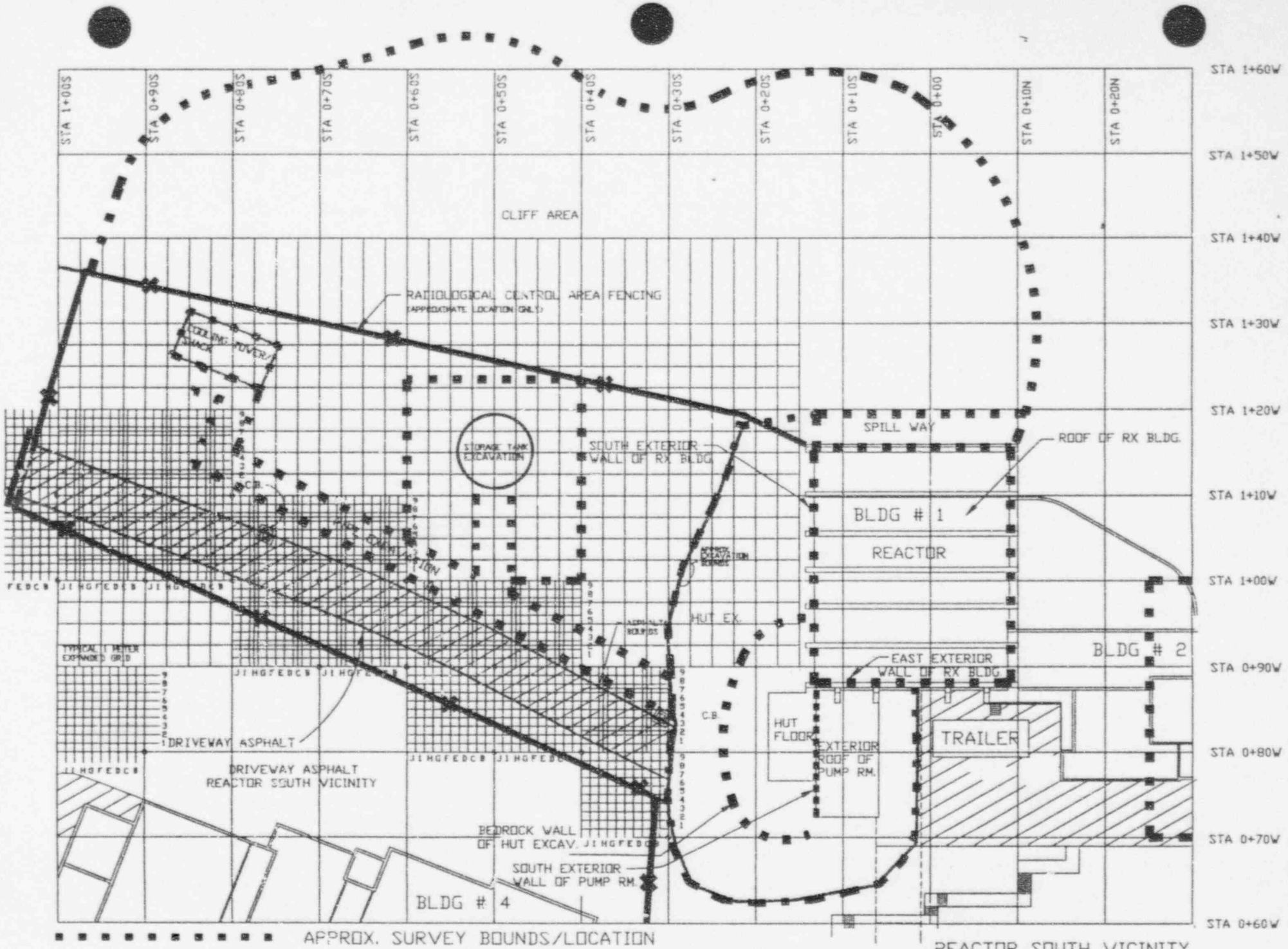
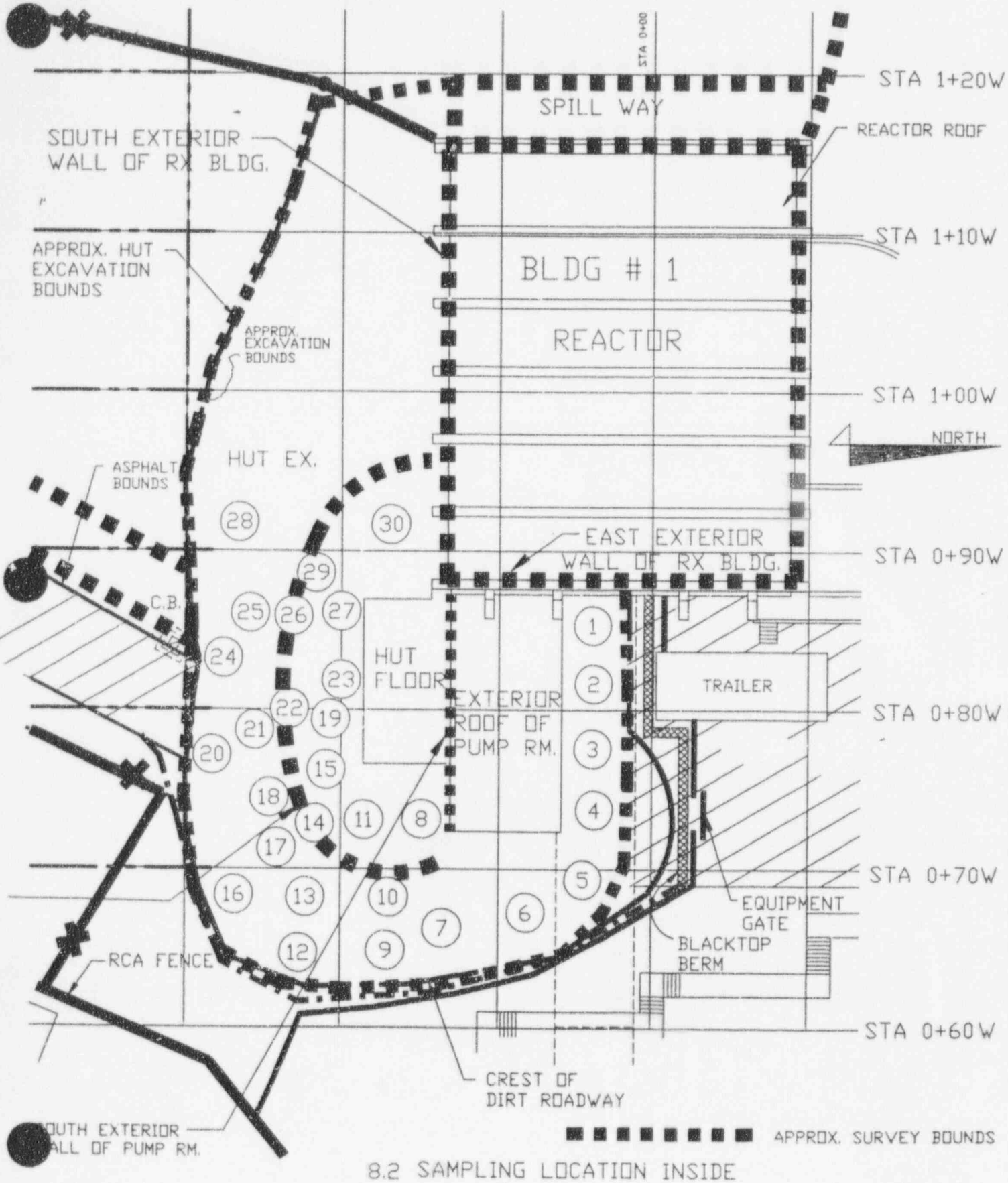


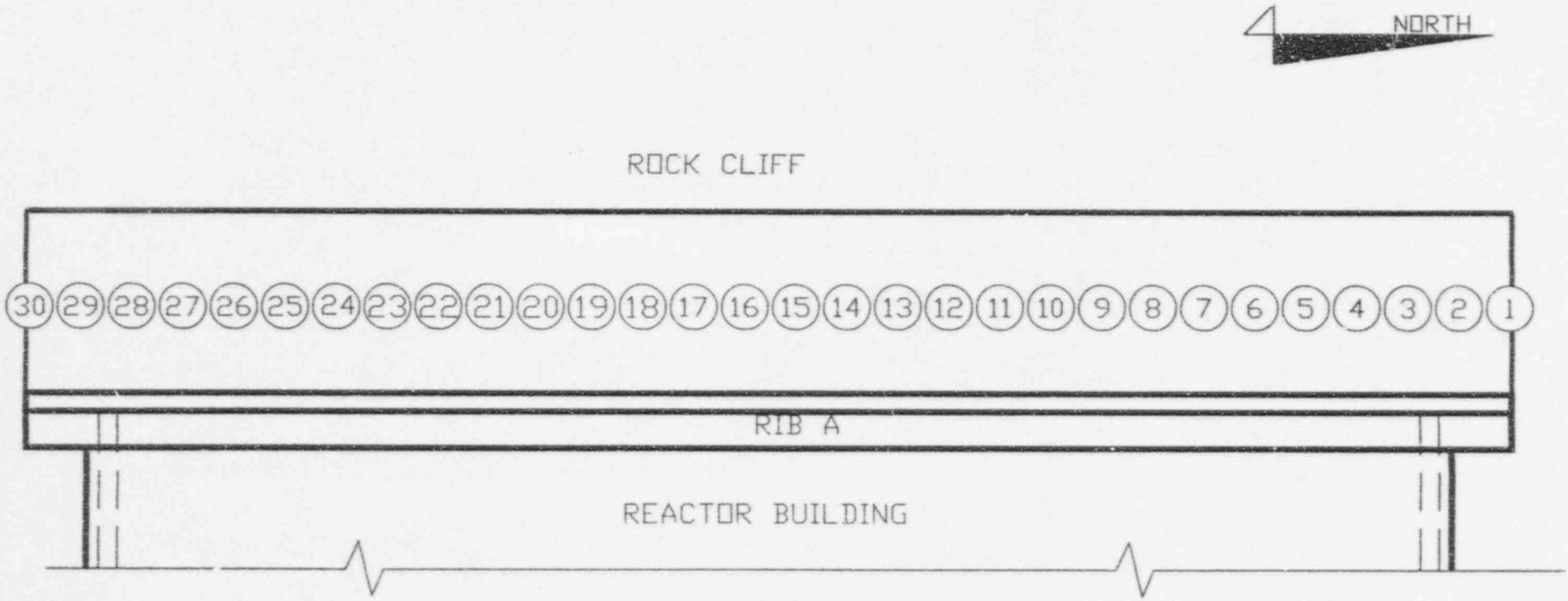

FIG. 8.1

REACTOR SOUTH VICINITY
FROM 2844
DWGS\2857A
10/26/94



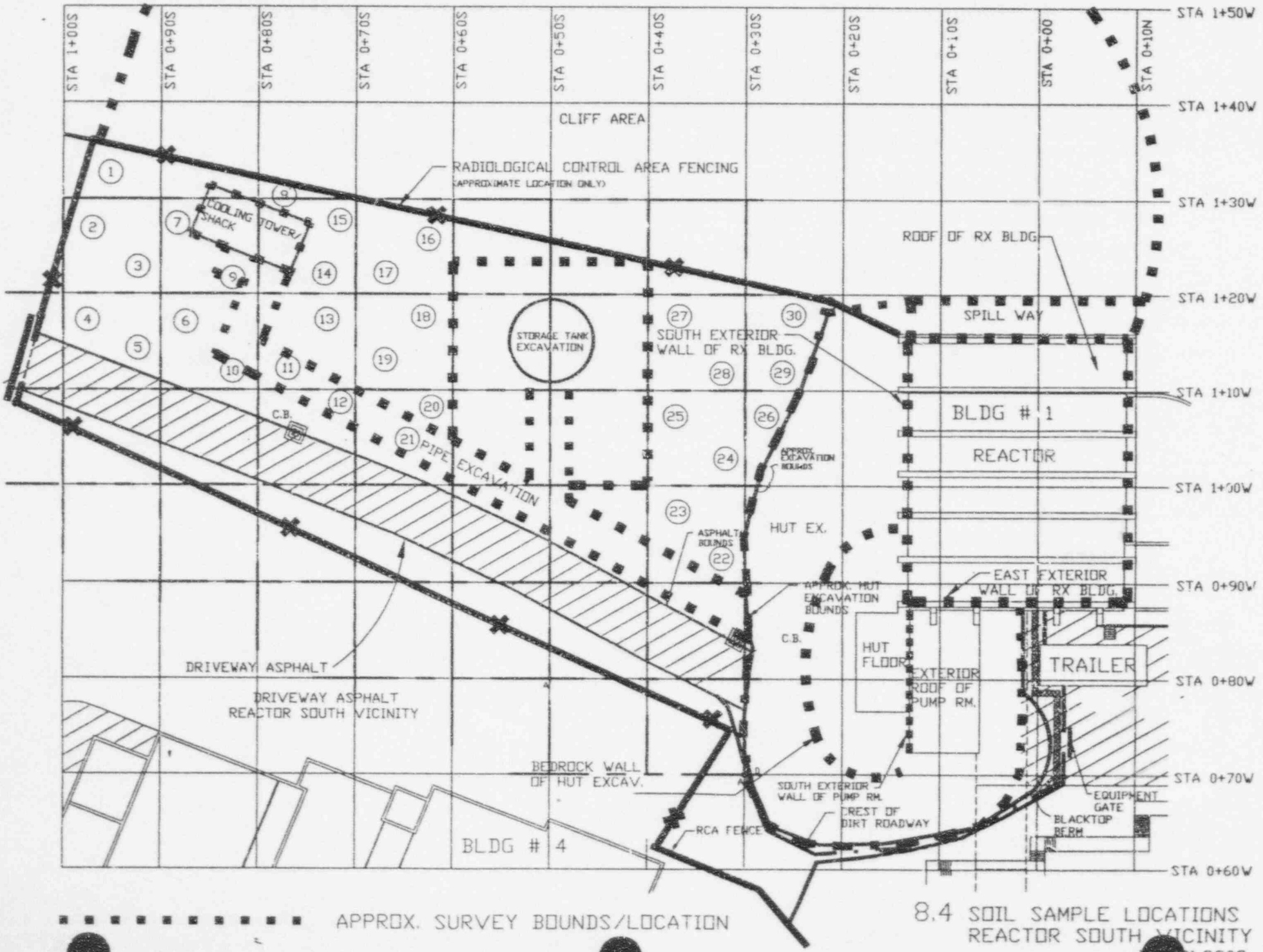

8.2 SAMPLING LOCATION INSIDE HUT EXCAVATION

DWGS\2903
1/26/95




8.3 SPILLWAY BEHIND REACTOR BUILDING

DW[illegible]2901
1/2[illegible]5




8.4 SOIL SAMPLE LOCATIONS
REACTOR SOUTH VICINITY

S\2902
1/24/95

## 6.9 Outside of RCA

### 6.9.1 General Information

This area has been deleted from the scope of this interim survey.

## 6.10 Storage Tank Excavation

### 6.10.1 General Information

The storage tank excavation area survey consisted of two survey units: 10.1 the concrete storage tank foundation ring and, 10.2 the soil within and adjacent to the storage tank foundation. Both of these survey units were surveyed on an affected area basis, in that the storage tank required dismantling and removal as radioactive waste. Additionally, a sump located in the tank floor on the east side and the associated tank fill line were found to have leaked. These were removed along with contaminated soil found under and around the sump and fill pipe. A portion of the concrete in the foundation ring adjacent to the sump was also removed as contaminated.

The 10.1 survey unit consisted of an approximately 0.23 m thick by 8.64 m diameter foundation ring, with an exposed surface area of about 30 $m^2$, with 35 individual measurement points for direct beta and alpha contamination determinations and gamma exposure rate. These locations are shown in Figure 10.1. Measurement results are provided in three attached tables as follows:

Table 10.1-1; Storage Tank Foundation - gamma exposure rate data

Table 10.1-2; Storage Tank Foundation - direct beta surface contamination data

Table 10.1-3; Storage Tank Foundation - direct alpha surface contamination data

The 10.2 survey unit consisted of the soil within the foundation ring, soil outside of the foundation ring, and soil within the trench from which the primary water fill line was removed. This area has a soil surface area of approximately 600 $m^2$. Gamma exposure rate measurements were taken at 34 locations along with corresponding soil samples. Figure 10-2 shows these locations relative to the storage tank foundation and site grid layout.

Measurement and sampling results are provided in two attached tables as follows:

Table 10.2-1; Storage Tank Excavation - gamma exposure rate above soil surface data

Table 10.2-2; Storage Tank Excavation - soil sample data

## 6.10.2 RESULTS SUMMARY

### a Survey Unit: 10.1 Storage Tank Excavation - Foundation

DIRECT SURVEY RESULTS

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | 1902 | 34 |
| Number of Meas: | 35 | 35 | 35 |
| Survey Unit Mean: | 1.7 | 3680 | 23 |
| True Mean, U alpha 95% C.L.: | 2.2 | 4012 | 29 |
| Criteria/Acceptable Y - N: | 5/Yes | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | 7548 | 69 |
| Criteria/Acceptable Y - N: | N.A. | 13500/Yes | 5000/Yes |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | 6.0 | None | None |
| Criteria/Acceptable Y - N: | 10/Yes | 40500/Yes | 15000/Yes |
| Ref. Tables | 10.1-1 | 10.1-2 | 10.1-3 |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

COMMENTS/SOIL - SEDIMENT RESULTS:

None

## 6.10.2 RESULTS SUMMARY

### b Survey Unit: 10.2 Storage Tank Excavation for Storage Tank and Pipe

**DIRECT SURVEY RESULTS**

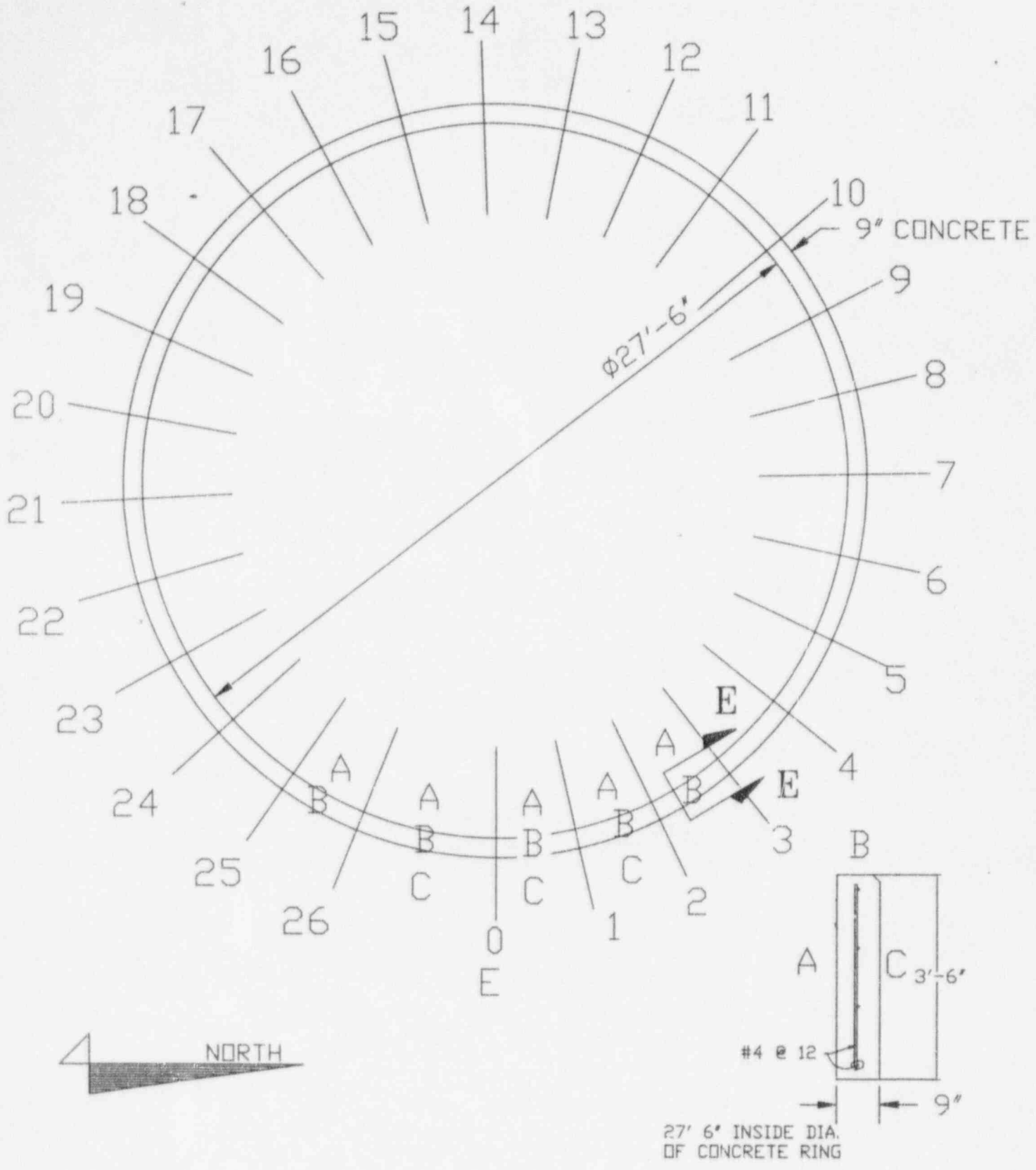
| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | N.A. | N.A. |
| Number of Meas: | 34 | N.A. | N.A. |
| Survey Unit Mean: | 0.3 | N.A. | N.A. |
| True Mean, U alpha 95% C.L.: | 0.7 | N.A. | N.A. |
| Criteria/Acceptable Y - N: | 5/Yes | N.A. | N.A. |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | 5.0 | N.A. | N.A. |
| Criteria/Acceptable Y - N: | 10/Yes | N.A. | N.A. |
| Ref. Tables | 10.2-1 | N.A. | N.A. |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

**COMMENTS/SOIL - SEDIMENT RESULTS:**

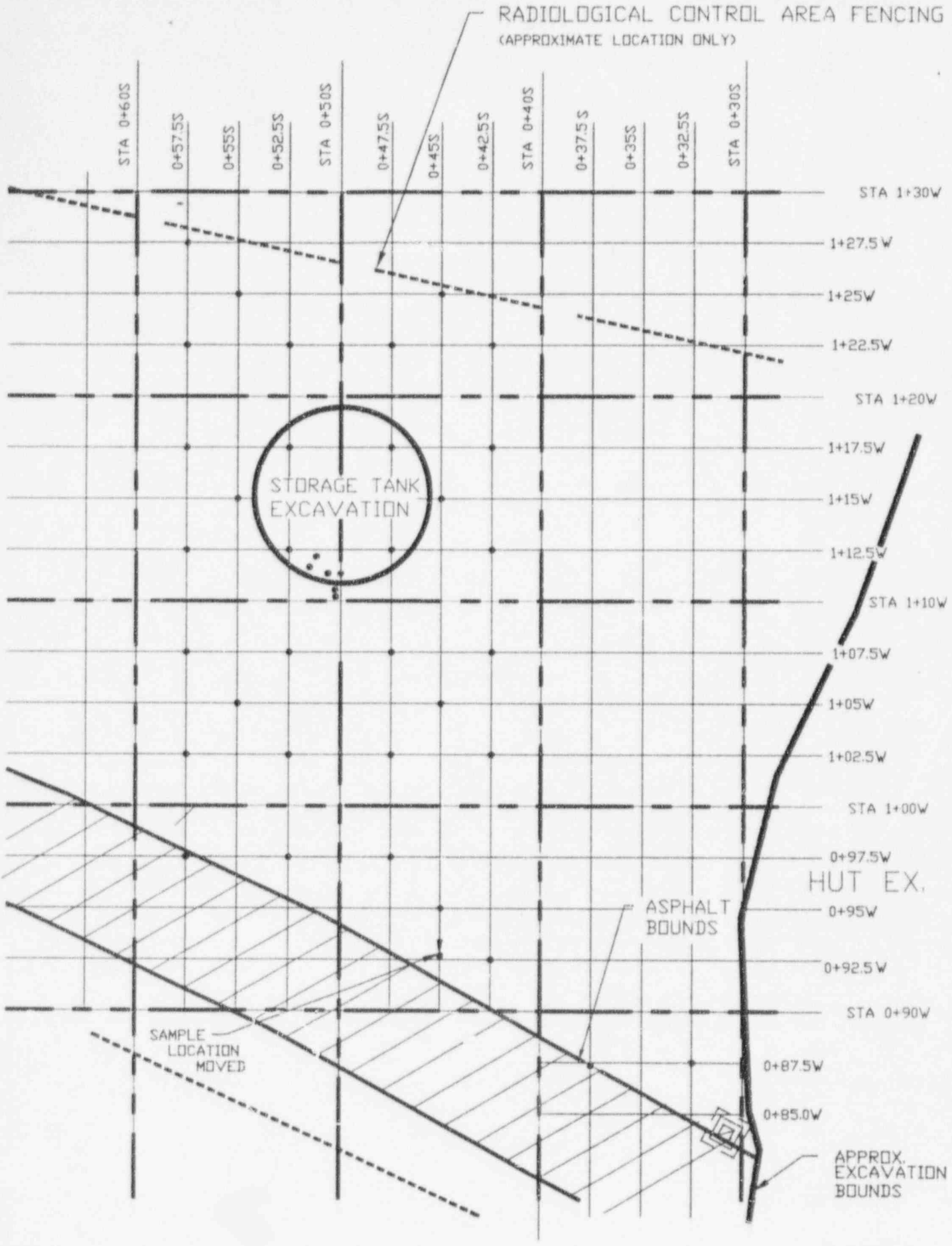
Only three of the 34 soil samples in this survey unit were found with detectable radionuclides (Cs-137 only) greater than background. The three positive results ranged from 0.6 to 1.58 pCi/gm Cs-137. The maximum result is approximately 42% of the 3.8 pCi/gm Cs-137 soil criteria. Therefore, as all sample results are less than acceptable criteria the survey unit is acceptable.




E - E

FOUNDATION SURVEY ON STORAGE TANK EXCAVATION

DWGS\2899
1/20/95




10.2 SAMPLE LOCATIONS
STORAGE TANK AREA

DWGS\2904
1/24/95

## 6.11 Cooling Tower/Shack

### 6.11.1 General Information

The cooling tower survey consists of two survey units: 11.1, the structure, and 11.2 surrounding area soil. The survey was conducted on an un-affected area basis. This structure has only come into contact with clean secondary side reactor heat exchanger cooling water. This was first determined after removal of the reactor heat exchanger, where no radioactive contamination was found within the secondary side heat exchanger shell.

The 11.1 survey unit cooling tower structure consists of a 10 m long by 4.5 m wide concrete basin, with a sloping floor 0.8 to 2.2 m deep, upon which sits the water distribution-cooling structure. The water distribution-cooling structure is 10 m long by 4.5 m wide by 3.1 m high and is constructed of a wooden framework; fiberglass siding, slates and grids; and wooden water distribution pipes. The cooling tower is in a structurally deteriorated condition. Therefore, access for survey purposes has been limited for safety reasons, to those surfaces that can be reached from outside the structure. The survey consisted of 30 evenly distributed measurement points on or in the structure, with direct beta and alpha, and gamma exposure rate measurements made at each point. Eight biased point measurement sets were made within a section of the upper tower where water distribution pipes could be cut open. A sample of the wooden pipes was removed for qualitative gamma spectral analysis. Measurement and sampling locations are shown on Figure 11-1.

Measurement and sampling results for the 11.1 survey unit are provided in four attached tables as follows:

Table 11.1-1; Cooling Tower Structure - gamma exposure rate data

Table 11.1-2; Cooling Tower Structure - direct beta surface contamination data

Table 11.1-3; Cooling Tower Structure - direct alpha surface contamination data

Table 11.1-4; Cooling Tower Structure - qualitative gamma spectral analysis of wooden pipe interior surface.

The 11.2 survey unit consisted of taking 30 soil samples from the ground immediately adjacent to the cooling tower structure which covered a soil area of about 100 $m^2$. The locations of these soil samples are shown in Figure 11-2. Gamma exposure rate measurements were not made above the soil sampling locations, as these would have been redundant with the 11.1 survey unit's gamma measurements that were made in the same general area. Sampling results are provided in Table 11.2-1.

## 6.11.2 RESULTS SUMMARY

### a Survey Unit: 11.1 Cooling Tower Shack - Concrete, Wood, Metal, Plastic

DIRECT SURVEY RESULTS

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | 1836 | 33 |
| Number of Meas: | 38 | 38 | 38 |
| Survey Unit Mean: | 1.24 | -58 | 23 |
| True Mean, U alpha 95% C.L.: | 1.72 | 259 | 27 |
| Criteria/Acceptable Y - N: | 5/Yes | 13500/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Ind. Result (un-affected areas only) | 6 | 3890 | 66 |
| Criteria/Acceptable Y - N: | 10/Yes | 13500/Yes | 15000/Yes |
| Max. Hot Spot Scans (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Ref. Tables | 11.1-1 | 11.1-2 | 11.1-3 |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

COMMENTS/SOIL - SEDIMENT RESULTS:

The qualitative gamma spectral analysis of the interior sections of the wooden pipe and plastic samples indicates that no radionuclides from the reactor or hot laboratory mixtures are present.

## 6.11.2 RESULTS SUMMARY

### b Survey Unit: 11.2 Cooling Tower Soil

**DIRECT SURVEY RESULTS**

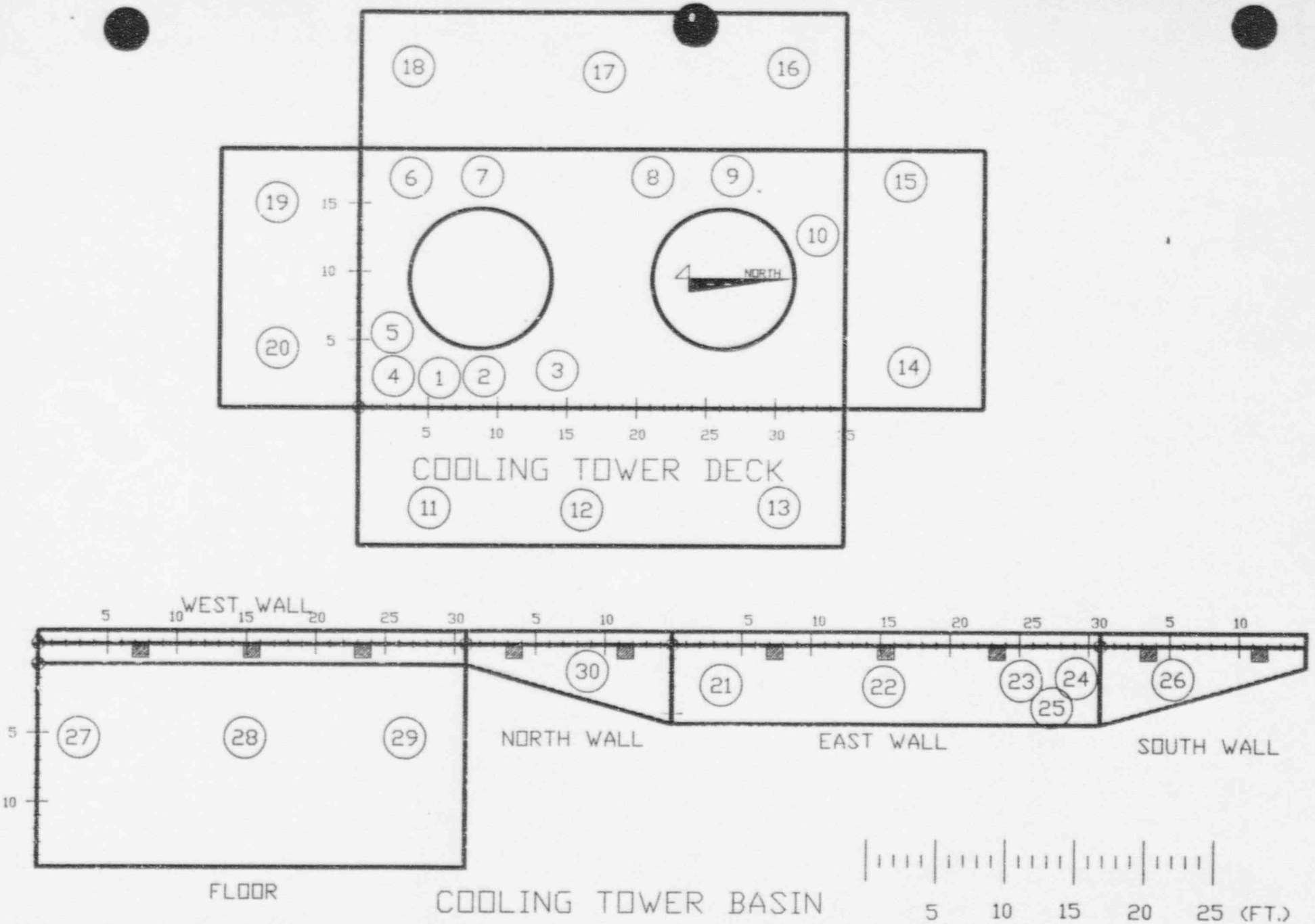
| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | N.A. | N.A. | N.A. |
| Number of Meas: | 0 | 0 | 0 |
| Survey Unit Mean: | N.A. | N.A. | N.A. |
| True Mean, U alpha 95% C.L.: | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Ref. Tables | N.A. | N.A. | N.A. |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

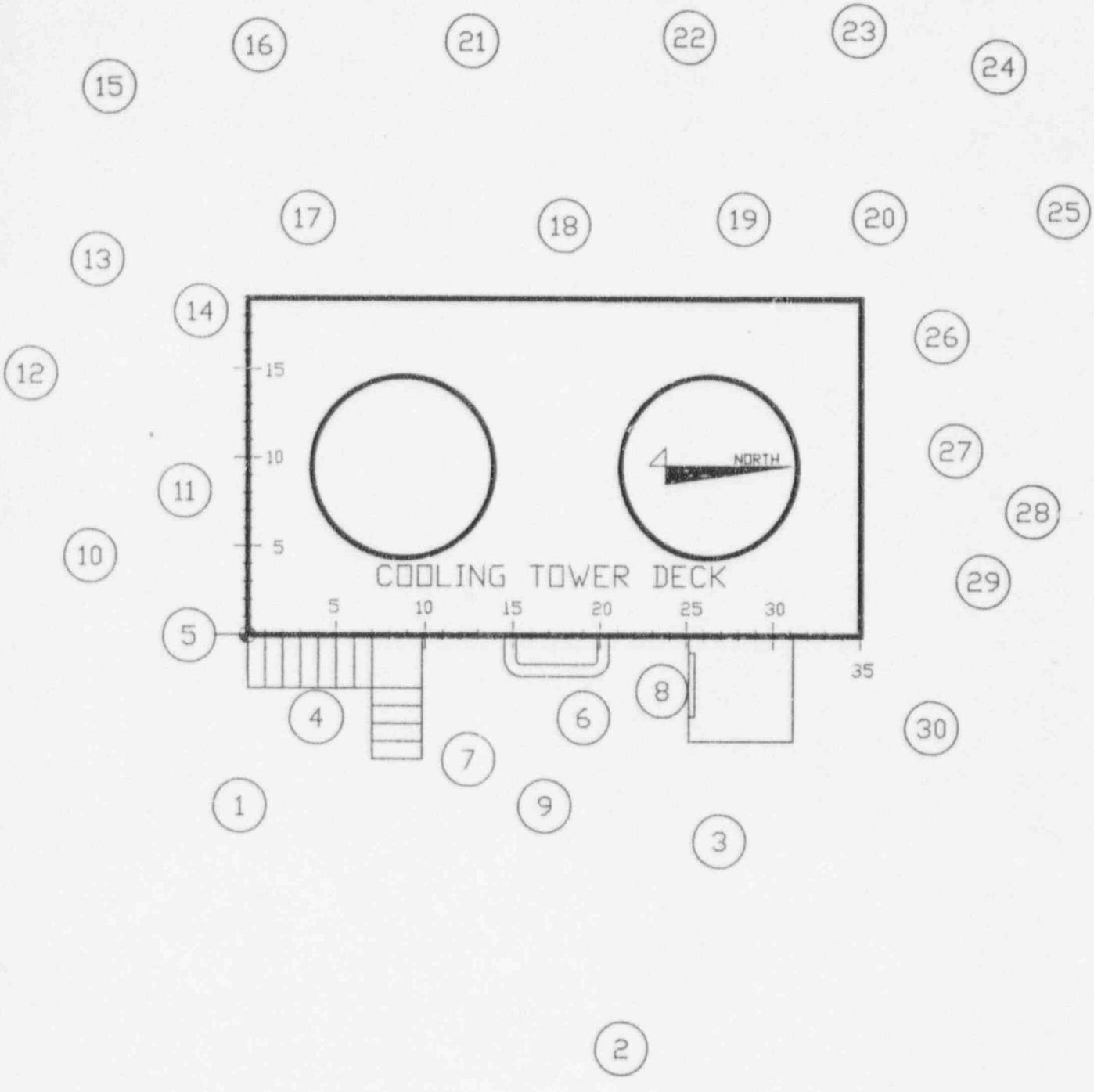
**COMMENTS/SOIL - SEDIMENT RESULTS:**

Soil sampling results indicate the presence of 7 samples with detectable and greater than background levels of radionuclides in the soil adjacent to the cooling tower structure. One sample with 0.18 pCi/gm Co-60, 0.13 pCi/gm Ag-108m and less than background amounts of Cs-137. The sum-of-fractions (SOF) of the soil release criteria for this sample is 0.34.




11.1 SAMPLE LOCATIONS
COOLING TOWER / STACK

DWGS\2907
1/25/95




11.2 SOIL SAMPLE LOCATIONS
COOLING TOWER / STACK AREA
DWGS\2908
1/25/95

The other six samples contained Cs-137 at concentrations greater than the background level of 1.25 pCi/gm. The Cs-137 concentration in these samples ranged from 0.09 to 2.15 pCi/gm above background. The corresponding SOF of the criteria would range from 0.02 to 0.57 for these samples.

The elevated levels of Cs-137 in these six soil samples may be due to Cs-137 background fallout being concentrated from surface water runoff from the mountain behind the cooling tower. None the less, whether fallout or not, the soil in this survey unit meets soil release criteria.

## 6.12 Area 12.0, 5K Tank Excavation

### 6.12.1 General Information

The 5K tank survey area consisted of two survey units: 12.1, the actual soil excavation pit area and; 12.2, a concrete tank foundation located in the approximate center of the excavation. These areas were surveyed on an affected area basis, in that a minor amount of soil contamination was initially found on the ground surface above and between the two 5K tanks. However, once this small amount of soil contamination was removed, no other contamination was encountered.

The 12.1 survey unit consisted of an area of about 600 $m^2$, and about 4.6 m deep, with 31 individual soil sample/gamma exposure rate locations. These locations are shown on Figure 12.1. In addition to the excavation pit, the clean soil that was excavated is located in a spoils pile north of the excavation pit. This spoils pile contains approximately 579 $m^3$ of soil and is represented by 78 soil samples that were taken during the excavation process. Measurement and sampling results for the 12.1 survey unit are provided in three attached tables as follows:

Table 12.1-1; 5K Area Excavation Pit - Gamma Exposure Rate Data

Table 12.1-2; 5K Area Excavation Pit Soil Sample Data

Table 12.1-3; 5K Area Excavation Spoils Soil Sample Data

The 12.2 survey unit consisted of a concrete foundation pad upon which the two - 5K tanks were located prior to removal. This pad has a surface area of approximately 22 $m^2$, with 34 gamma exposure rate measurement points and 128 direct beta and 128 alpha surface contamination measurement points. These locations are shown on Figure 12.2. Measurement and sampling results for the 12.2 survey unit are provided in the attached three tables as follows:

Table 12.2-1; 5K Tank Foundation - Gamma Exposure Rate Data

Table 12.2-2; 5K Tank Foundation - Direct Beta Surface Contamination Data

Table 12.2-3; 5K Tank Foundation - Direct Alpha Surface Contamination Data

## 6.12.2 RESULTS SUMMARY

### a Survey Unit: 12.1 5K Excavation

**DIRECT SURVEY RESULTS**

| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | N.A. | N.A. |
| Number of Meas: | 31 | N.A. | N.A. |
| Survey Unit Mean: | 2.5 | N.A. | N.A. |
| True Mean, U alpha 95% C.L.: | 2.9 | N.A. | N.A. |
| Criteria/Acceptable Y - N: | 5/Yes | N.A. | N.A. |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max Ind. Result (un-affected areas only) | 6 | N.A. | N.A. |
| Criteria/Acceptable Y - N: | 10/Yes | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Ref. Tables | 12.1-1 | N.A. | N.A. |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

**COMMENTS/SOIL - SEDIMENT RESULTS:**

Soil sample results for the excavation pit and spoils pile (see Tables 12.1-2 and 12.1-3 respectively) were found to meet soil release criteria. Note that Tables 12.1-2 and 12.1-3 include data for the most relevant radionuclides of interest, and not the complete results for all radionuclides for which analysis was performed. Those radionuclides not listed are those for which soil criteria was developed, but which have not been generally found in site soil and/or would not contribute significantly to the sum-of-fractions tally if found. The concentration

data shown in the tables have not been corrected for background due to fallout (1.25 pCi/gm Cs-137 at the 90% confidence level). However, the sum of the sum-of-fractions for each radionuclide has been corrected for fallout background. Soil in the excavated pit (Table 12.1-2) was found to contain only traces of Cs-137 at levels above MDA but less than the background level for 11 of the 30 samples. Therefore, there is no indication of any soil contamination being present. Also, for the spoils pile soil, only traces of Cs-137 were found in 38 of the 78 soil samples at levels above MDA but less than the background level. As such, the soil remaining in the excavation and in the spoils pile meet soil release criteria and are in fact indistinguishable from background.

## 6.12.2 RESULTS SUMMARY

### b Survey Unit: 12.2 5K Tank Foundation

**DIRECT SURVEY RESULTS**

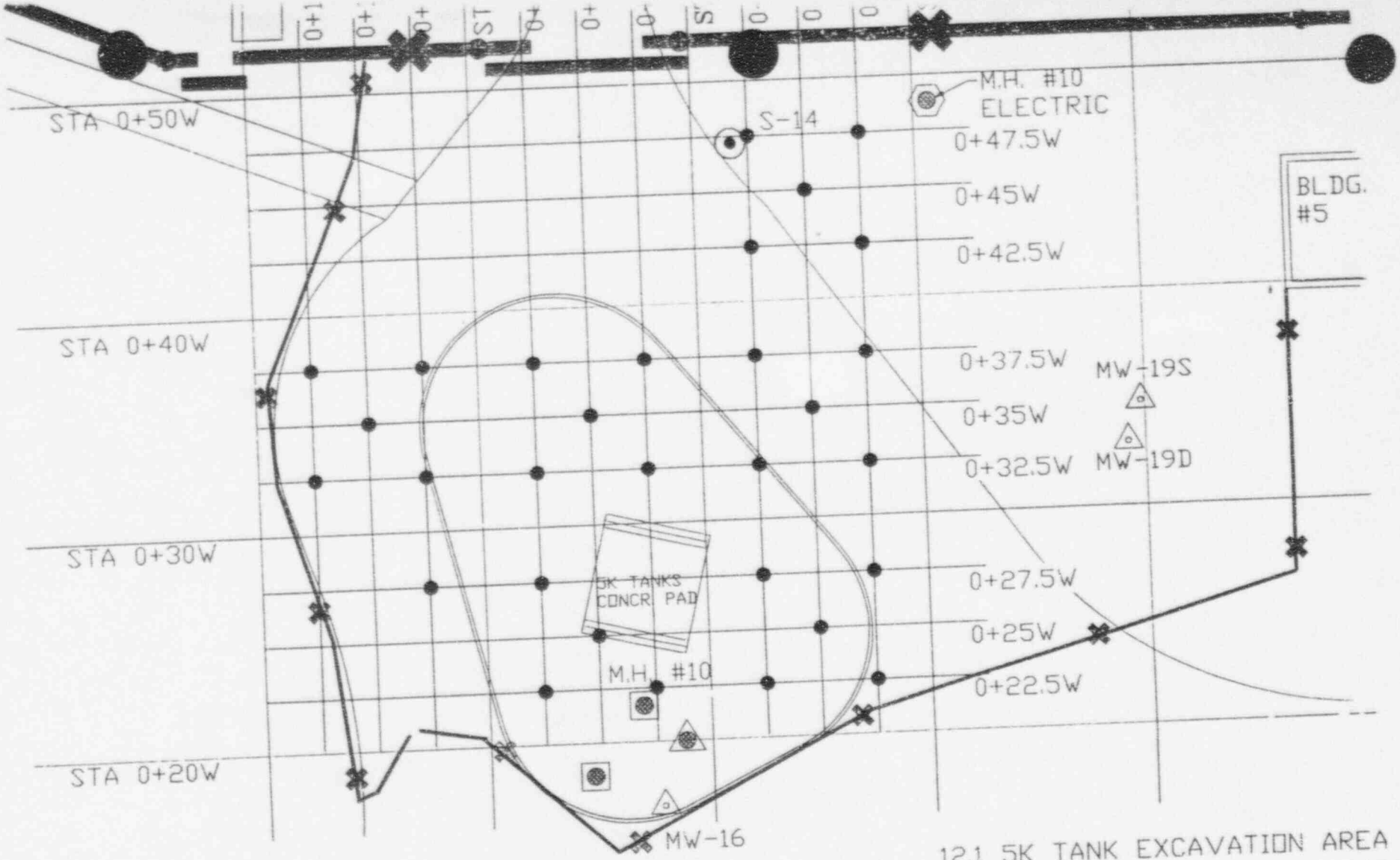
| Meas. Type: | Gamma Exposure Rate (a) | Direct Beta (b) | Direct Alpha (b) |
|---|---|---|---|
| Units | uRem/hr | dpm/100 cm² | dpm/100 cm² |
| MDA | 2 | 429 | 88 |
| Number of Meas: | 34 | 128 | 128 |
| Survey Unit Mean: | -0.15 | 567 | 6 |
| True Mean, U alpha 95% C.L.: | 0.15 | 594 | 7 |
| Criteria/Acceptable Y - N: | 5/Yes | 1301/Yes | 5000/Yes |
| Max Grid Block Wt. Mean: (affected areas only) | N.A. | 1292 | 46 |
| Criteria/Acceptable Y - N: | N.A. | 1301/Yes | 5000/Yes |
| Max Ind. Result (un-affected areas only) | N.A. | N.A. | N.A. |
| Criteria/Acceptable Y - N: | N.A. | N.A. | N.A. |
| Max. Hot Spot Scans (affected areas only) | 3 | None | None |
| Criteria/Acceptable Y - N: | 10/Yes | 3903/Yes | 15000/Yes |
| Ref. Tables | 12.2-1 | 12.2-2 | 12.2-3 |

(a) With a mean site background of 6 uRem/hr subtracted

(b) Without subtraction of radioactivity due to natural radioactive material content

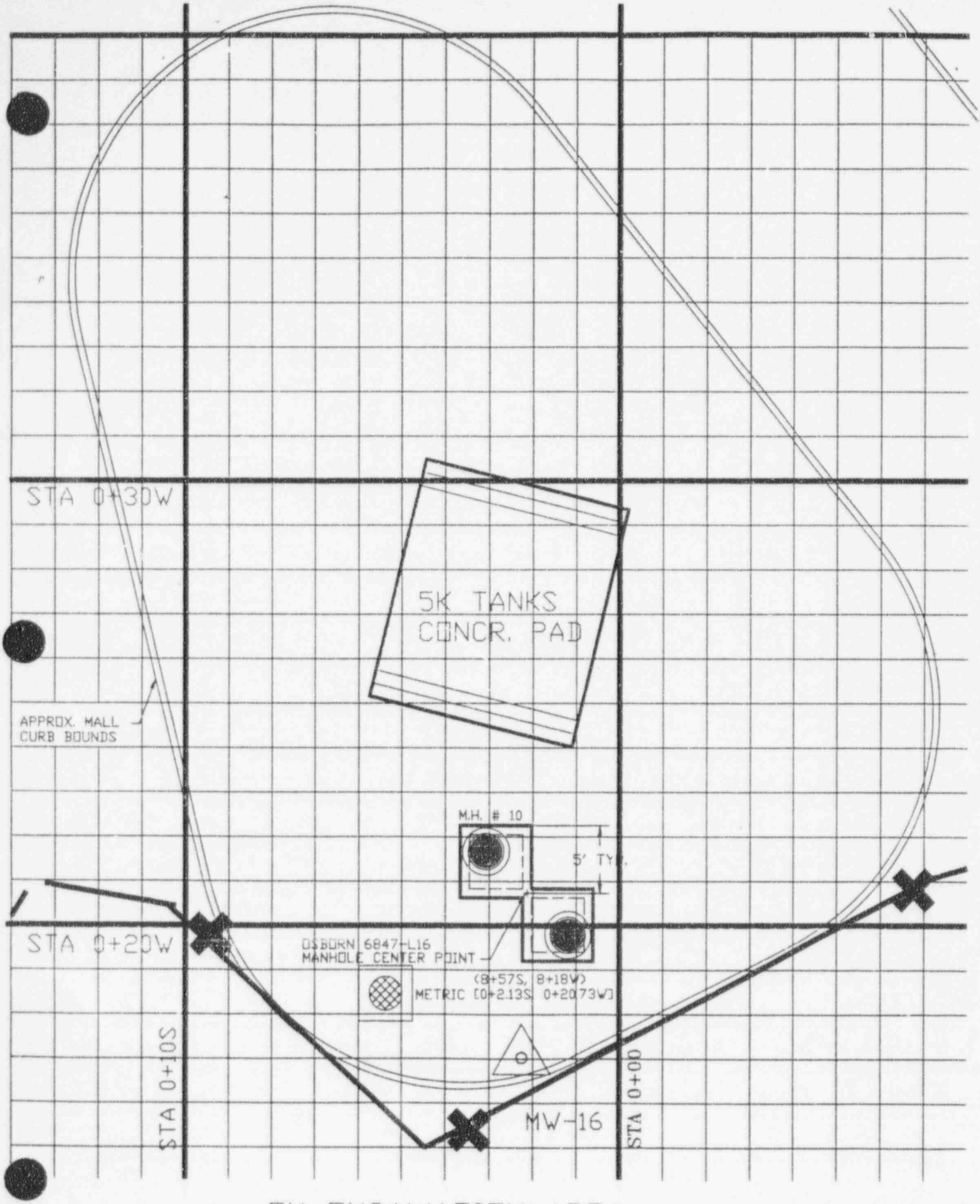
**COMMENTS/SOIL - SEDIMENT RESULTS:**

None




12.1 5K TANK EXCAVATION AREA

1/25/95 DWGS\2906




5K EXCAVATION AREA
FIGURE 12.2

DWGS\2883
1/26/95

TABLE 1.1-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:15 AM

FINAL SURVEY DATA SHEET

DATA FOR AFFECTED AREA DESCRIPTION:

HUT FLOOR AREA 1.1 FOR UREM POST REMEDIATION

RADIATION TYPE: GAMMA SURVEY IN UREM/HR

COMPLETION DATE: 11-9-94

TECHNICIANS: PS/CJ/TA

LOCATION: 1.0

GRID ID: 1.1

MEDIA TYPE: CONCRETE

# of POINTS: 85 (>60)

MATERIAL CODE

1=CONCRETE 5=PLASTIC

2=ROCK 6=SOIL

3=WOOD 7=ASPHALT

4=METAL 8=OTHER(SPECIFY):

NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | LIMIT |
|---|---|---|
| MAX | 22.00 FAIL | 10 |
| AVG | 9.38 FAIL | 5 |
| STD X | 3.64 | |
| MU SUB ALPHA | 10.03 FAIL | 5 |

| ID # | GRID COORIDINATES LETTER | NUMBER | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|---|
| 1.1 | A | 6 | 6 | 10 | 8 | 4 |
| 1.1 | A | 7 | 6 | 14 | 8 | 8 |
| 1.1 | B | 6 | 6 | 11 | 8 | 5 |
| 1.1 | B | 7 | 6 | 9 | 8 | 3 |
| 1.1 | C | 5 | 6 | 13 | 8 | 7 |
| 1.1 | C | 6 | 6 | 11 | 8 | 5 |
| 1.1 | C | 7 | 6 | 12 | 8 | 6 |
| 1.1 | D | 1 | 6 | 28 | 8 | 22 |
| 1.1 | D | 2 | 6 | 21 | 8 | 15 |
| 1.1 | D | 3 | 6 | 14 | 8 | 8 |
| 1.1 | D | 4 | 6 | 13 | 8 | 7 |
| 1.1 | D | 5 | 6 | 10 | 8 | 4 |
| 1.1 | D | 6 | 6 | 10 | 8 | 4 |
| 1.1 | E | 1 | 6 | 27 | 8 | 21 |
| 1.1 | E | 2 | 6 | 17 | 8 | 11 |
| 1.1 | E | 3 | 6 | 18 | 8 | 12 |
| 1.1 | E | 4 | 6 | 15 | 8 | 9 |
| 1.1 | E | 5 | 6 | 11 | 8 | 5 |
| 1.1 | E | 6 | 6 | 15 | 8 | 9 |
| 1.1 | F | 1 | 6 | 19 | 8 | 13 |
| 1.1 | F | 2 | 6 | 18 | 8 | 12 |
| 1.1 | F | 3 | 6 | 15 | 8 | 9 |
| 1.1 | F | 4 | 6 | 13 | 8 | 7 |
| 1.1 | F | 5 | 6 | 11 | 8 | 5 |
| 1.1 | F | 6 | 6 | 13 | 8 | 7 |
| 1.1 | G | 1 | 6 | 17 | 8 | 11 |
| 1.1 | G | 2 | 6 | 16 | 8 | 10 |
| 1.1 | G | 3 | 6 | 15 | 8 | 9 |
| 1.1 | G | 4 | 6 | 15 | 8 | 9 |
| 1.1 | G | 5 | 6 | 12 | 8 | 6 |
| 1.1 | G | 6 | 6 | 10 | 8 | 4 |
| 1.1 | H | 1 | 6 | 18 | 8 | 12 |

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TABLE 1.1-1

| | | | | | | |
|---|---|---|---|---|---|---|
| 1.1 | H | 2 | 6 | 14 | 8 | 8 |
| 1.1 | H | 3 | 6 | 14 | 8 | 8 |
| 1.1 | H | 4 | 6 | 15 | 8 | 9 |
| 1.1 | H | 5 | 6 | 13 | 8 | 7 |
| 1.1 | H | 6 | 6 | 10 | 8 | 4 |
| 1.1 | I | 1 | 6 | 18 | 8 | 12 |
| 1.1 | I | 2 | 6 | 15 | 8 | 9 |
| 1.1 | I | 3 | 6 | 15 | 8 | 9 |
| 1.1 | I | 4 | 6 | 13 | 8 | 7 |
| 1.1 | I | 5 | 6 | 13 | 8 | 7 |
| 1.1 | I | 6 | 6 | 13 | 8 | 7 |
| 1.1 | J | 1 | 6 | 18 | 8 | 12 |
| 1.1 | J | 2 | 6 | 18 | 8 | 12 |
| 1.1 | J | 3 | 6 | 13 | 8 | 7 |
| 1.1 | J | 4 | 6 | 13 | 8 | 7 |
| 1.1 | J | 5 | 6 | 13 | 8 | 7 |
| 1.1 | J | 6 | 6 | 13 | 8 | 7 |
| 1.1 | K | 1 | 6 | 17 | 8 | 11 |
| 1.1 | K | 2 | 6 | 17 | 8 | 11 |
| 1.1 | K | 3 | 6 | 16 | 8 | 10 |
| 1.1 | K | 4 | 6 | 15 | 8 | 9 |
| 1.1 | K | 5 | 6 | 14 | 8 | 8 |
| 1.1 | K | 6 | 6 | 12 | 8 | 6 |
| 1.1 | L | 1 | 6 | 17 | 8 | 11 |
| 1.1 | L* | 2 | 6 | 16 | 8 | 10 |
| 1.1 | L | 3 | 6 | 16 | 8 | 10 |
| 1.1 | L | 4 | 6 | 15 | 8 | 9 |
| 1.1 | L | 5 | 6 | 13 | 8 | 7 |
| 1.1 | L | 6 | 6 | 13 | 8 | 7 |
| 1.1 | M* | 2 | 6 | 17 | 8 | 11 |
| 1.1 | M* | 3 | 6 | 17 | 8 | 11 |
| 1.1 | M | 4 | 6 | 16 | 8 | 10 |
| 1.1 | M | 5 | 6 | 15 | 8 | 9 |
| 1.1 | M | 6 | 6 | 12 | 8 | 6 |
| 1.1 | N | 2 | 6 | 19 | 8 | 13 |
| 1.1 | N | 3 | 6 | 19 | 8 | 13 |
| 1.1 | N | 4 | 6 | 18 | 8 | 12 |
| 1.1 | N | 5 | 6 | 13 | 8 | 7 |
| 1.1 | N | 6 | 6 | 12 | 8 | 6 |
| 1.1 | O | 3 | 6 | 22 | 8 | 16 |
| 1.1 | O* | 4 | 6 | 17 | 8 | 11 |
| 1.1 | O | 5 | 6 | 16 | 8 | 10 |
| 1.1 | O | 6 | 6 | 15 | 8 | 9 |
| 1.1 | O | 7 | 6 | 12 | 8 | 6 |
| 1.1 | P | 4 | 6 | 23 | 8 | 17 |
| 1.1 | P | 5 | 6 | 20 | 8 | 14 |
| 1.1 | P | 6 | 6 | 17 | 8 | 11 |
| 1.1 | P | 7 | 6 | 16 | 8 | 10 |
| 1.1 | Q | 5 | 6 | 23 | 8 | 17 |
| 1.1 | Q | 6 | 6 | 20 | 8 | 14 |
| 1.1 | Q | 7 | 6 | 15 | 8 | 9 |
| 1.1 | R | 6 | 6 | 20 | 8 | 14 |
| 1.1 | R | 7 | 6 | 20 | 8 | 14 |

* : POST-REMEDIATION RESULTS

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TABLE 1.1-1

PRE-REMEDIATION RESULTS

| | | | | | | |
|---|---|---|---|---|---|---|
| 1.1 | L | 2 | 6 | 16 | 8 | 10 |
| 1.1 | M | 2 | 5 | 17 | 8 | 11 |
| 1.1 | M | 3 | 6 | 17 | 8 | 11 |
| 1.1 | D | 4 | 6 | 17 | 8 | 11 |

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TABLE 1.1-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:11 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
HUT FLOOR AREA 1.1 FOR BETA POST REMEDIATION

RADIATION TYPE: 1 BETA SCALING FACTOR = 0.3
COMPLETION DATE: 12-8-94
TECHNICIANS: PS/CD/TA
LOCATION: 1.0
GRID ID: 1.1
MEDIA TYPE: CONCRETE
# of POINTS: 85 (>60)
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2
REM.+ FIXED:

| | | LIMIT |
|---|---|---|
| MAX FOR IND GRID | 245796 FAIL | 13500 |
| AVG - SURVEY UNIT | 6069 PASS | 13500 |
| STD X | 26696 | |
| MU SUB ALPHA | 10885 PASS | 13500 |
| MAX HOT SPOT | 297903 FAIL | 40500 |

| ID # | GRID COORDINATES LETTER | NUMBER | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | SCAN MAX BETA COUNTS | TOTAL CONT. AREA CM^2 | MATERIAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. BETA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 MAX CM^2 | TEST | INST E CPM/C |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1.1 | A | 6 | 1 | 646.7 | 885 | 0 | 0 | 8 | 2291 | 4513 +/-1144 | | NA | | 0.1 |
| 1.1 | A | 7 | 3 | 618.4 | 1197 | 1666 | 1150 | 8 | 2177 | 11636 +/-1279 | | 19272 | | 0.18 |
| 1.1 | B | 6 | 1 | 646.7 | 785 | 0 | 0 | 8 | 2291 | 2619 +/-1082 | | NA | | 0.1 |
| 1.1 | B | 7 | 1 | 646.7 | 712 | 0 | 0 | 8 | 2291 | 1237 +/-1035 | | NA | | 0.1 |
| 1.1 | C | 5 | 5 | 649.9 | 781 | 0 | 0 | 8 | 2263 | 2447 +/-1064 | | NA | | 0.17 |
| 1.1 | C | 6 | 1 | 646.7 | 705 | 0 | 0 | 8 | 2291 | 1104 +/-1030 | | NA | | 0.1 |
| 1.1 | C | 7 | 1 | 646.7 | 733 | 0 | 0 | 8 | 2291 | 1634 +/-1048 | | NA | | 0.1 |
| 1.1 | D | 1 | 6 | 1077.6 | 3120 | 17361 | 8000 | 8 | 2842 | 245796 +/-2037 | FAIL | 297903 | FAIL | 0.18 |
| 1.1 | D | 2 | 4 | 703.1 | 2298 | 1218 | 800 | 8 | 2353 | 28170 +/-1781 | FAIL | 9615 | | 0.17 |
| 1.1 | D | 3 | 4 | 703.1 | 889 | 0 | 0 | 8 | 2353 | 3472 +/-1134 | | NA | | 0.17 |
| 1.1 | D | 4 | 4 | 703.1 | 962 | 0 | 0 | 8 | 2353 | 4835 +/-1176 | | NA | | 0.17 |
| 1.1 | D | 5 | 5 | 649.9 | 863 | 0 | 0 | 8 | 2263 | 3977 +/-1114 | | NA | | 0.17 |
| 1.1 | D | 6 | 5 | 649.9 | 833 | 0 | 0 | 8 | 2263 | 3417 +/-1096 | | NA | | 0.17 |
| 1.1 | E | 1 | 6 | 1077.6 | 1131 | 1902 | 480 | 8 | 2842 | 1654 +/-1262 | | 15082 | | 0.18 |
| 1.1 | E | 2 | 4 | 1042.1 | 1077 | 1554 | 800 | 8 | 2854 | 1364 +/-1258 | | 9559 | | 0.17 |
| 1.1 | E | 3 | 2 | 673.0 | 839 | 0 | 0 | 8 | 2258 | 3039 +/-1080 | | NA | | 0.18 |
| 1.1 | E | 4 | 2 | 673.0 | 757 | 0 | 0 | 8 | 2258 | 1538 +/-1030 | | NA | | 0.18 |
| 1.1 | E | 5 | 5 | 829.8 | 738 | 1347 | 177 | 8 | 2551 | -1512 +/-1048 | | 9653 | | 0.17 |
| 1.1 | E | 6 | 5 | 715.2 | 727 | 0 | 0 | 8 | 2372 | 220 +/-1034 | | NA | | 0.17 |
| 1.1 | F | 1 | 6 | 1077.6 | 1120 | 1566 | 300 | 8 | 2842 | 1020 +/-1256 | | 8935 | | 0.18 |
| 1.1 | F | 2 | 4 | 703.1 | 989 | 0 | 0 | 8 | 2353 | 5339 +/-1191 | | NA | | 0.17 |
| 1.1 | F | 3 | 2 | 673.0 | 808 | 1516 | 500 | 8 | 2258 | 3119 +/-1061 | | 15431 | | 0.18 |
| 1.1 | F | 4 | 2 | 673.0 | 827 | 0 | 0 | 8 | 2258 | 2819 +/-1073 | | NA | | 0.18 |
| 1.1 | F | 5 | 5 | 829.8 | 826 | 1580 | 200 | 8 | 2551 | 211 +/-1103 | | 14001 | | 0.17 |
| 1.1 | F | 6 | 5 | 829.8 | 767 | 1252 | 177 | 8 | 2551 | -1012 +/-1066 | | 7880 | | 0.17 |
| 1.1 | G | 1 | 6 | 1077.6 | 978 | 0 | 0 | 8 | 2842 | -1822 +/-1182 | | NA | | 0.18 |
| 1.1 | G | 2 | 4 | 703.1 | 919 | 0 | 0 | 8 | 2353 | 4032 +/-1151 | | NA | | 0.17 |
| 1.1 | G | 3 | 2 | 673.0 | 884 | 0 | 0 | 8 | 2258 | 3862 +/-1107 | | NA | | 0.18 |
| 1.1 | G | 4 | 2 | 673.0 | 959 | 0 | 0 | 8 | 2258 | 5235 +/-1149 | | NA | | 0.18 |
| 1.1 | G | 5 | 5 | 829.8 | 748 | 0 | 0 | 8 | 2551 | -1527 +/-1055 | | NA | | 0.17 |
| 1.1 | G | 6 | 5 | 829.8 | 754 | 1394 | 177 | 8 | 2551 | -1203 +/-1058 | | 10530 | | 0.17 |

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9502100114-04

TABLE 1.1-2

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1.1 | H | 1 | 6 | 1077.6 | 1089 | 0 | 0 | B | 2842 | 209 +/-1240 | NA | | 0.1 |
| 1.1 | H | 2 | 4 | 703.1 | 979 | 0 | 0 | B | 2353 | 5152 +/-1186 | NA | | 0.1 |
| 1.1 | H | 3 | 2 | 673.0 | 876 | 1175 | 100 | B | 2258 | 3771 +/-1102 | | 9189 | 0.1 |
| 1.1 | H | 4 | 2 | 673.0 | 727 | 1058 | 700 | B | 2258 | 1413 +/-1011 | | 7047 | 0.1 |
| 1.1 | H | 5 | 5 | 829.8 | 902 | 0 | 0 | B | 2551 | 1348 +/-1148 | NA | | 0.1 |
| 1.1 | H | 6 | 5 | 829.8 | 802 | 0 | 0 | B | 2551 | -519 +/-1088 | NA | | 0.1 |
| 1.1 | I | 1 | 6 | 1077.6 | 998 | 0 | 0 | B | 2842 | -1456 +/-1192 | NA | | 0.1 |
| 1.1 | I | 2 | 4 | 307.9 | 934 | 0 | 0 | B | 2519 | 2355 +/-1166 | NA | | 0.1 |
| 1.1 | I | 3 | 2 | 673.0 | 765 | 0 | 0 | B | 2258 | 1684 +/-1035 | NA | | 0.1 |
| 1.1 | I | 4 | 2 | 673.0 | 707 | 0 | 0 | B | 2258 | 622 +/- 998 | NA | | 0.1 |
| 1.1 | I | 5 | 5 | 829.8 | 750 | 1349 | 100 | B | 2551 | -1378 +/-1056 | | 9690 | 0.1 |
| 1.1 | I | 6 | 2 | 673.5 | 697 | 0 | 0 | B | 2259 | 430 +/- 992 | NA | | 0.1 |
| 1.1 | J | 1 | 6 | 920.0 | 1032 | 0 | 0 | B | 2630 | 2049 +/-1202 | NA | | 0.1 |
| 1.1 | J | 2 | 4 | 807.9 | 934 | 0 | 0 | B | 2519 | 2355 +/-1166 | NA | | 0.1 |
| 1.1 | J | 3 | 2 | 673.0 | 793 | 0 | 0 | B | 2258 | 2197 +/-1052 | NA | | 0.1 |
| 1.1 | J | 4 | 2 | 673.0 | 852 | 0 | 0 | B | 2258 | 3277 +/-1088 | NA | | 0.1 |
| 1.1 | J | 5 | 2 | 730.1 | 738 | 1306 | 400 | B | 2350 | 560 +/-1022 | | 10542 | 0.1 |
| 1.1 | J | 6 | 2 | 673.5 | 755 | 1866 | 100 | B | 2259 | 1695 +/-1029 | | 21829 | 0.1 |
| 1.1 | K | 1 | 6 | 920.0 | 1317 | 0 | 0 | B | 2630 | 7263 +/-1346 | NA | | 0.1 |
| 1.1 | K | 2 | 4 | 807.9 | 985 | 0 | 0 | B | 2519 | 3307 +/-1195 | NA | | 0.1 |
| 1.1 | K | 3 | 2 | 673.0 | 716 | 0 | 0 | B | 2258 | 787 +/-1004 | NA | | 0.1 |
| 1.1 | K | 4 | 2 | 673.0 | 739 | 0 | 0 | B | 2258 | 1208 +/-1019 | NA | | 0.1 |
| 1.1 | K | 5 | 1 | 659.9 | 793 | 1293 | 270 | B | 2314 | 2777 +/-1088 | | 11991 | 0. |
| 1.1 | K | 6 | 2 | 673.5 | 620 | 1336 | 100 | B | 2259 | -848 +/- 941 | | 12127 | 0.1 |
| 1.1 | L | 1 | 6 | 1046.0 | 1383 | 0 | 0 | B | 2801 | 6165 +/-1383 | NA | | 0.1 |
| 1.1 | L* | 2 | 5 | 844.1 | 976 | 0 | 0 | B | 2572 | 2462 +/-1191 | NA | | 0.1 |
| 1.1 | L | 3 | 2 | 673.0 | 911 | 1284 | 800 | B | 2258 | 4903 +/-1122 | | 11184 | 0.1 |
| 1.1 | L | 4 | 2 | 673.0 | 726 | 1424 | 900 | B | 2258 | 2120 +/-1011 | | 13747 | 0.1 |
| 1.1 | L | 5 | 2 | 730.1 | 817 | 1444 | 4000 | B | 2350 | 6182 +/-1070 | | 13068 | 0.1 |
| 1.1 | L | 6 | 2 | 730.1 | 975 | 0 | 0 | B | 2350 | 4483 +/-1161 | NA | | 0.1 |
| 1.1 | M* | 2 | 9 | 828.2 | 998 | 0 | 0 | B | 2509 | 3120 +/-1184 | NA | | 0.1 |
| 1.1 | M* | 3 | 5 | 873.6 | 1093 | 0 | 0 | B | 2616 | 4095 +/-1257 | NA | | 0.1 |
| 1.1 | M | 4 | 3 | 864.2 | 781 | 1498 | 500 | B | 2565 | -871 +/-1062 | | 11659 | 0.1 |
| 1.1 | M | 5 | 2 | 730.1 | 996 | 1362 | 8200 | B | 2350 | 10361 +/-1173 | | 11567 | 0.1 |
| 1.1 | M | 6 | 2 | 730.1 | 1264 | 1313 | 10000 | B | 2350 | 10670 +/-1312 | | 10670 | 0.1 |
| 1.1 | N | 2 | 4 | 807.9 | 1089 | 0 | 0 | B | 2519 | 5249 +/-1252 | NA | | 0.1 |
| 1.1 | N | 3 | 3 | 748.6 | 924 | 2427 | 4000 | B | 2390 | 14286 +/-1140 FAIL | | 30876 | 0.1 |
| 1.1 | N | 4 | 5 | 748.6 | 807 | 0 | 0 | B | 2425 | 1090 +/-1086 | NA | | 0.1 |
| 1.1 | N | 5 | 6 | 672.8 | 851 | 1642 | 200 | B | 2256 | 3550 +/-1087 | | 17731 | 0.1 |
| 1.1 | N | 6 | 6 | 672.8 | 1036 | 1403 | 500 | B | 2256 | 6980 +/-1191 | | 13359 | 0.1 |
| 1.1 | O | 3 | 3 | 864.2 | 968 | 0 | 0 | B | 2565 | 1909 +/-1171 | NA | | 0.1 |
| 1.1 | O* | 4 | 5 | 844.1 | 944 | 0 | 0 | B | 2572 | 1865 +/-1173 | NA | | 0.1 |
| 1.1 | O | 5 | 3 | 864.2 | 962 | 0 | 0 | B | 2565 | 1799 +/-1167 | NA | | 0.1 |
| 1.1 | O | 6 | 3 | 864.2 | 826 | 0 | 0 | B | 2565 | -703 +/-1089 | NA | | 0.1 |
| 1.1 | O | 7 | 3 | 864.2 | 783 | 0 | 0 | B | 2565 | -1494 +/-1063 | NA | | 0.1 |
| 1.1 | P | 4 | 3 | 864.2 | 1042 | 1311 | 300 | B | 2565 | 3419 +/-1211 | | 8219 | 0.1 |
| 1.1 | P | 5 | 3 | 864.2 | 1024 | 0 | 0 | B | 2565 | 2940 +/-1201 | NA | | 0.1 |
| 1.1 | P | 6 | 3 | 864.2 | 958 | 0 | 0 | B | 2565 | 1726 +/-1165 | NA | | 0.1 |
| 1.1 | P | 7 | 3 | 864.2 | 778 | 0 | 0 | B | 2565 | -1586 +/-1060 | NA | | 0.1 |
| 1.1 | Q | 5 | 3 | 864.2 | 1323 | 2060 | 2000 | B | 2565 | 11152 +/-1354 | | 21998 | 0.1 |
| 1.1 | Q | 6 | 3 | 864.2 | 1069 | 1677 | 400 | B | 2565 | 4215 +/-1226 | | 14952 | 0.1 |
| 1.1 | Q | 7 | 3 | 864.2 | 959 | 0 | 0 | B | 2565 | 1744 +/-1166 | NA | | 0.1 |
| 1.1 | R | 6 | 3 | 864.2 | 1939 | 0 | 0 | B | 2565 | 19772 +/-1623 FAIL | NA | | 0.1 |
| 1.1 | R | 7 | 3 | 864.2 | 1013 | 0 | 0 | B | 2565 | 2737 +/-1196 | NA | | 0.1 |

* = POST-REMEDIATION RESULTS

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TABLE 1.1-2

PRE-REMEDIATION RESULTS

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1.1 | L | 2 | 4 | 807.9 | 992 | 5686 | 300 | 8 | 2519 | 6068 +/-1199 | 91094 FAIL | 0.1 |
| 1.1 | M | 2 | 4 | 807.9 | 1091 | 2269 | 900 | 8 | 2519 | 7266 +/-1253 | 27285 | 0.1 |
| 1.1 | M | 3 | 2 | 673 | 985 | 3129 | 300 | 8 | 2258 | 6889 +/-1164 | 44957 FAIL | 0.1 |
| 1.1 | O | 4 | 3 | 864.2 | 925 | 2102 | 100 | 8 | 2565 | 1335 +/-1147 | 22770 | 0.1 |

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812

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9502100114 - 06

AR TABLE 1.1-3

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 08:34 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
HUT FLOOR AREA 1.1 FOR ALPHA POST REMEDIATION

RADIATION TYPE: 2 ALPHA
COMPLETION DATE: 11-9-94
TECHNICIANS: PS/CD/TA
LOCATION: 1.0
GRID ID: 1.1
MEDIA TYPE: CONCRETE
# of POINTS: 85 (>60)
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | | LIMIT |
|---|---|---|---|
| MAX FOR IND GRID | 1367 | PASS | 5000 |
| AVG - SURVEY UNIT | 23 | PASS | 5000 |
| STD X | 148 | | |
| MU SUB ALPHA | 50 | PASS | 5000 |
| MAX HOT SPOT | 1707 | PASS | 15000 |

| GRID COORIDINATES ID # | LETTER | NUMBER | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | SCAN MAX ALPHA COUNTS | TOTAL CONT. AREA CM^2 | MATER-IAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. ALPHA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 CM^2 | MAX TEST | INST CPM/ |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1.1 | A | 6 | 1 | 0.7 | 1 | 0 | 0 | 8 | 35 | 2 +/- 11 | NA | | | 0.18 |
| 1.1 | A | 7 | 3 | 0.9 | 2 | 0 | 1150 | 8 | 37 | 4 +/- 15 | NA | | | 0.19 |
| 1.1 | B | 6 | 1 | 0.7 | 4 | 0 | 0 | 8 | 35 | 17 +/- 21 | NA | | | 0.18 |
| 1.1 | B | 7 | 1 | 0.7 | 3 | 0 | 0 | 8 | 35 | 12 +/- 18 | NA | | | 0.18 |
| 1.1 | C | 5 | 5 | 2.1 | 3 | 0 | 0 | 8 | 52 | 5 +/- 19 | NA | | | 0.1 |
| 1.1 | C | 6 | 1 | 0.7 | 4 | 0 | 0 | 8 | 35 | 17 +/- 21 | NA | | | 0.18 |
| 1.1 | C | 7 | 1 | 0.7 | 2 | 0 | 0 | 8 | 35 | 7 +/- 15 | NA | | | 0.18 |
| 1.1 | D | 1 | 6 | 3.2 | 4 | 311 | 8000 | 8 | 61 | 1367 +/- 23 | | 1707 | | 0.18 |
| 1.1 | D | 2 | 4 | 2.6 | 6 | 7 | 800 | 8 | 51 | 17 +/- 24 | | 22 | | 0.20 |
| 1.1 | D | 3 | 4 | 2.6 | 2 | 0 | 0 | 8 | 51 | -3 +/- 15 | NA | | | 0.20 |
| 1.1 | D | 4 | 4 | 2.6 | 5 | 0 | 0 | 8 | 51 | 12 +/- 22 | NA | | | 0.20 |
| 1.1 | D | 5 | 5 | 2.1 | 4 | 0 | 0 | 8 | 52 | 10 +/- 22 | NA | | | 0.1 |
| 1.1 | D | 6 | 5 | 2.1 | 3 | 0 | 0 | 8 | 52 | 5 +/- 19 | NA | | | 0.1 |
| 1.1 | E | 1 | 6 | 3.2 | 10 | 8 | 480 | 8 | 61 | 37 +/- 35 | | 27 | | 0.18 |
| 1.1 | E | 2 | 4 | 1.5 | 4 | 4 | 800 | 8 | 42 | 12 +/- 20 | | 12 | | 0.20 |
| 1.1 | E | 3 | 2 | 0.6 | 1 | 0 | 0 | 8 | 32 | 2 +/- 10 | NA | | | 0.19 |
| 1.1 | E | 4 | 2 | 0.6 | 3 | 0 | 0 | 8 | 32 | 12 +/- 18 | NA | | | 0.19 |
| 1.1 | E | 5 | 5 | 1 | 1 | 8 | 177 | 8 | 40 | 1 +/- 11 | | 38 | | 0.1 |
| 1.1 | E | 6 | 5 | 0.7 | 0 | 0 | 0 | 8 | 36 | -4 +/- 3 | NA | | | 0.1 |
| 1.1 | F | 1 | 6 | 3.2 | 2 | 6 | 300 | 8 | 61 | -6 +/- 17 | | 16 | | 0.18 |
| 1.1 | F | 2 | 4 | 2.6 | 9 | 0 | 0 | 8 | 51 | 32 +/- 30 | NA | | | 0.20 |
| 1.1 | F | 3 | 2 | 0.6 | 3 | 4 | 500 | 8 | 32 | 13 +/- 18 | | 17 | | 0.19 |
| 1.1 | F | 4 | 2 | 0.6 | 3 | 0 | 0 | 8 | 32 | 12 +/- 18 | NA | | | 0.19 |
| 1.1 | F | 5 | 5 | 1 | 13 | 14 | 200 | 8 | 40 | 66 +/- 29 | | 71 | | 0.1 |
| 1.1 | F | 6 | 5 | 1 | 1 | 59 | 177 | 8 | 40 | 6 +/- 11 | | 317 | | 0.1 |
| 1.1 | G | 1 | 6 | 3.2 | 2 | 0 | 0 | 8 | 61 | -7 +/- 17 | NA | | | 0.18 |
| 1.1 | G | 2 | 4 | 2.6 | 2 | 0 | 0 | 8 | 51 | -3 +/- 15 | NA | | | 0.20 |
| 1.1 | G | 3 | 2 | 0.6 | 1 | 0 | 0 | 8 | 32 | 2 +/- 10 | NA | | | 0.19 |
| 1.1 | G | 4 | 2 | 0.6 | 3 | 0 | 0 | 8 | 32 | 12 +/- 18 | NA | | | 0.19 |
| 1.1 | G | 5 | 5 | 1 | 2 | 0 | 0 | 8 | 40 | 5 +/- 16 | NA | | | 0.1 |

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FF.
PM

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| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1.1 | G | 6 | 5 | 1 | 2 | 7 | 177 | B | 40 | 6 +/- | 16 | 33 | 0. |
| 1.1 | H | 1 | 6 | 3.2 | 1 | 0 | 0 | B | 61 | -12 +/- | 12 | NA | 0.1 |
| 1.1 | H | 2 | 4 | 2.6 | 2 | 0 | 0 | B | 51 | -3 +/- | 15 | NA | 0.2 |
| 1.1 | H | 3 | 2 | 0.6 | 5 | 3 | 100 | B | 32 | 22 +/- | 23 | 12 | 0.1 |
| 1.1 | H | 4 | 2 | 0.6 | 2 | 1 | 700 | B | 32 | 7 +/ | 14 | 2 | 0.1 |
| 1.1 | H | 5 | 5 | 1 | 2 | 0 | 0 | B | 40 | 5 +/- | 16 | NA | 0. |
| 1.1 | H | 6 | 5 | 1 | 2 | 0 | 0 | B | 40 | 5 +/- | 16 | NA | 0. |
| 1.1 | I | 1 | 6 | 3 2 | 1 | 0 | 0 | B | 61 | -12 +/- | 12 | NA | 0.1 |
| 1.1 | I | 2 | 4 | 2.8 | 2 | 0 | 0 | B | 52 | -4 +/- | 15 | NA | 0.2 |
| 1.1 | I | 3 | 2 | 0.6 | 5 | 0 | 0 | B | 32 | 23 +/- | 23 | NA | 0.1 |
| 1.1 | I | 4 | 2 | 0.6 | 1 | 0 | 0 | B | 32 | 2 +/- | 10 | NA | 0.1 |
| 1.1 | I | 5 | 5 | 1 | 4 | 3 | 100 | B | 40 | 16 +/- | 22 | 11 | 0. |
| 1.1 | I | 6 | 2 | 1.1 | 1 | 0 | 0 | B | 39 | -1 +/- | 11 | NA | 0.1 |
| 1.1 | J | 1 | 6 | 2.2 | 0 | 0 | 0 | B | 53 | -12 +/- | 5 | NA | 0.1 |
| 1.1 | J | 2 | 4 | 2.8 | 3 | 0 | 0 | B | 52 | 1 +/- | 18 | NA | 0.2 |
| 1.1 | J | 3 | 2 | 0.6 | 1 | 0 | 0 | B | 32 | 2 +/- | 10 | NA | 0.1 |
| 1.1 | J | 4 | 2 | 0.6 | 2 | 0 | 0 | B | 32 | 7 +/- | 14 | NA | 0.1 |
| 1.1 | J | 5 | 2 | 0.6 | 2 | 4 | 400 | B | 32 | 8 +/- | 14 | 17 | 0.1 |
| 1.1 | J | 6 | 2 | 1.1 | 1 | 5 | 100 | B | 39 | -0 +/- | 11 | 20 | 0.1 |
| 1.1 | K | 1 | 6 | 2.2 | 3 | 0 | 0 | B | 53 | 4 +/- | 20 | NA | 0.1 |
| 1.1 | K | 2 | 4 | 2.8 | 7 | 0 | 0 | B | 52 | 21 +/- | 26 | NA | 0.2 |
| 1.1 | K | 3 | 2 | 0.6 | 1 | 0 | 0 | B | 32 | 2 +/- | 10 | NA | 0.1 |
| 1.1 | K | 4 | 2 | 0.6 | 1 | 0 | 0 | B | 32 | 2 +/- | 10 | NA | 0.1 |
| 1.1 | K | 5 | 1 | 1.9 | 3 | 2 | 270 | B | 48 | 6 +/- | 18 | 1 | 0.1 |
| 1.1 | K | 6 | 2 | 1.1 | 1 | 2 | 100 | B | 39 | -0 +/- | 11 | 5 | 0.1 |
| 1.1 | L | 1 | 6 | 1.4 | 4 | 0 | 0 | B | 46 | 14 +/- | 22 | NA | 0.1 |
| 1.1 | L* | 2 | 50 | 1.8 | 0 | 0 | 0 | B | 48 | -10 +/- | 4 | NA | 0. |
| 1.1 | L | 3 | 2 | 0.6 | 3 | 3 | 800 | B | 32 | 12 +/- | 18 | 12 | 0.1 |
| 1.1 | L | 4 | 2 | 0.6 | 2 | 4 | 900 | B | 32 | 8 +/- | 14 | 17 | 0.1 |
| 1.1 | L | 5 | 2 | 0.6 | 0 | 4 | 4000 | B | 32 | 5 +/- | 2 | 17 | 0.1 |
| 1.1 | L | 6 | 2 | 0.6 | 0 | 0 | 0 | B | 32 | -3 +/- | 2 | NA | 0.1 |
| 1.1 | M* | 2 | 9 | 1.3 | 2 | 0 | 0 | B | 85 | 7 +/- | 30 | NA | 0. |
| 1.1 | M* | 3 | 50 | 1.4 | 2 | 0 | 0 | B | 44 | 3 +/- | 15 | NA | 0. |
| 1.1 | M | 4 | 3 | 3 | 1 | 3 | 500 | B | 56 | -10 +/- | 12 | 0 | 0.1 |
| 1.1 | M | 5 | 2 | 0.6 | 0 | 2 | 8200 | B | 32 | 5 +/- | 2 | 7 | 0.1 |
| 1.1 | M | 6 | 2 | 0.6 | 1 | 3 | 10000 | B | 32 | 12 +/- | 10 | 12 | 0.1 |
| 1.1 | N | 2 | 4 | 2.8 | 10 | 0 | 0 | B | 52 | 36 +/- | 31 | NA | 0.2 |
| 1.1 | N | 3 | 3 | 0.6 | 0.6 | 3 | 4000 | B | 33 | 5 +/- | 8 | 12 | 0.1 |
| 1.1 | N | 4 | 3 | 0.6 | 1 | 0 | 0 | B | 33 | 2 +/- | 10 | NA | 0.1 |
| 1.1 | N | 5 | 6 | 1.5 | 1 | 5 | 200 | B | 47 | -2 +/- | 12 | 19 | 0.1 |
| 1.1 | N | 6 | 6 | 1.5 | 2 | 5 | 500 | B | 47 | 4 +/- | 16 | 19 | 0.1 |
| 1.1 | O | 3 | 3 | 3 | 6 | 0 | 0 | B | 56 | 15 +/- | 25 | NA | 0.1 |
| 1.1 | O* | 4 | 50 | 1.8 | 2 | 0 | 0 | B | 48 | 1 +/- | 16 | NA | 0. |
| 1.1 | O | 5 | 3 | 3 | 0 | 0 | 0 | B | 56 | -15 +/- | 6 | NA | 0.1 |
| 1.1 | O | 6 | 3 | 3 | 5 | 0 | 0 | B | 56 | 10 +/- | 23 | NA | 0.1 |
| 1.1 | O | 7 | 3 | 3 | 9 | 0 | 0 | B | 56 | 31 +/- | 31 | NA | 0.1 |
| 1.1 | P | 4 | 3 | 3 | 3 | 2 | 300 | B | 56 | -0 +/- | 18 | -5 | 0.1 |
| 1.1 | P | 5 | 3 | 3 | 3 | 0 | 0 | B | 56 | 0 +/- | 18 | NA | 0.1 |
| 1.1 | P | 6 | 3 | 3 | 6 | 0 | 0 | B | 56 | 15 +/- | 25 | NA | 0.1 |
| 1.1 | P | 7 | 3 | 3 | 1 | 0 | 0 | B | 56 | -10 +/- | 12 | NA | 0.1 |
| 1.1 | Q | 5 | 3 | 3 | 12 | 11 | 2000 | B | 56 | 45 +/- | 35 | 41 | 0.1 |
| 1.1 | Q | 6 | 3 | 3 | 8 | 6 | 400 | B | 56 | 25 +/- | 29 | 15 | 0.1 |
| 1.1 | Q | 7 | 3 | 3 | 4 | 0 | 0 | B | 56 | 5 +/- | 21 | NA | 0.1 |
| 1.1 | R | 6 | 3 | 3 | 8 | 0 | 0 | B | 56 | 26 +/- | 29 | NA | 0.1 |
| 1.1 | R | 7 | 3 | 3 | 1 | 0 | 0 | B | 56 | -10 +/- | 12 | NA | 0.1 |

* : POST-REMEDIATION RESULTS

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TABLE 1.1-3

PRE-REMEDIATION RESULTS

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 1.1 | L | 2 | 4 | 2.8 | 5 | 0 | 300 | B | 52 | 10 +/- 22 | NA | 0.2 |
| 1.1 | M | 2 | 4 | 2.8 | 4 | 5 | 900 | B | 52 | 6 +/- 20 | 11 | 0.2 |
| 1.1 | M | 3 | 2 | 0.6 | 1 | 5 | 300 | B | 32 | 3 +/- 10 | 23 | 0.1 |
| 1.1 | O | 4 | 3 | 3 | 6 | 3 | 100 | B | 56 | 15 +/- 25 | 0 | 0.1 |

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TABLE 1.1-4

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:06 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 1.1 - HUT FLOOR SOIL FOR SUM OF THE FRACTIONS

RADIATION TYPE: SOIL-DATA FOR SUM OF THE FRACTIONS
COMPLETION DATE: 12-9-94
TECHNICIANS: TA
LOCATION: 1.0
GRID ID: 1.1
MEDIA TYPE: SOIL
# of POINTS: 1

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 0.26 | PASS | 1 |
| AVG | 0.26 | PASS | 1 |
| STD X | ERR | | |
| MU SUB ALPHA | ERR | ERR | 1 |

| | | ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED) | | | | | | | | ISOTOPES OF CO | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| ID # | GRID COORIDINATES OR OTHER ID | SR-90 | CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SOIL CODE | SR-90 | CO- |
| | | LIMIT 17 | LIMIT 0.9 | LIMIT 1.1 | LIMIT 1.8 | LIMIT 3.8 | LIMIT 63 | LIMIT 2 | | | |
| 1.1 | COMPOSITE OF HUT | 0.0585 < | 0.087 < | 0.033 < | 0.056 | 0.226 < | 0.348 < | 0.183 | 1 | 0.003441 < | |

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NCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| 60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| 0.096 < | 0.030 < | 0.031 | 0.000 < | 0.006 < | 0.092 | 0.257 |

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TABLE 1.2-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:13 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 1.1 - CORES FROM HOLDUP TANK FLOOR FOR BETA
DEEPEST CORE ONLY

RADIATION TYPE: 1 BETA SCALING FACTOR = 0.3
COMPLETION DATE: 9/93-6/94
TECHNICIANS: MANY
LOCATION: 1.0
GRID ID: 1.1
MEDIA TYPE: CONCRETE
# of POINTS: 100 (>60)
CT IN MINUTES: 0.2

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFIY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2
REM.+ FIXED:

| | | | LIMIT |
|---|---|---|---|
| MAX FOR IND GRID | 10606 | PASS | 13500 |
| AVG - SURVEY UNIT | 2078 | PASS | 13500 |
| STD X | 1592 | | |
| MU SUB ALPHA | 2343 | PASS | 13500 |
| MAX HOT SPOT | 0 | PASS | 40500 |

| ID # | CORE NUMBER | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 0.2 MINUTES | SCAN MAX BETA COUNTS | TOTAL CONT. AREA CM^2 | MATER-IAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. BETA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 CM^2 | MAX TEST |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 1.1 1 | | 1 | 4 | 181.0 | 226 | 0 | 0 | 8 | 2865 | 840 +/- 1240 | | NA |
| 1.1 2 | | 1 | 4 | 181.0 | 636 | 0 | 0 | 8 | 2865 | 8497 +/- 2070 | | NA |
| 1.1 3 | | 1 | 4 | 181.0 | 206 | 0 | 0 | 8 | 2865 | 467 +/- 1185 | | NA |
| 1.1 4 | | 1 | 4 | 181.0 | 246 | 0 | 0 | 8 | 2865 | 1214 +/- 1293 | | NA |
| 1.1 | | 2 | 4 | 181.0 | 216 | 0 | 0 | 8 | 2865 | 654 +/- 1213 | | NA |
| 1.1 5 | | 1 | 4 | 181.0 | 231 | 0 | 0 | 8 | 2865 | 934 +/- 1254 | | NA |
| 1.1 6 | | 1 | 4 | 181.0 | 221 | 0 | 0 | 8 | 2865 | 747 +/- 1227 | | NA |
| 1.1 7 | | 1 | 4 | 181.0 | 246 | 0 | 0 | 8 | 2865 | 1214 +/- 1293 | | NA |
| 1.1 | | 2 | 4 | 181.0 | 401 | 0 | 0 | 8 | 2865 | 4108 +/- 1646 | | NA |
| 1.1 9 | 0"-10" | 1 | 1 | 373.7 | 454 | 0 | 0 | 8 | 4063 | 1515 +/- 1783 | | NA |
| 1.1 (151.2 SQ IN) | | 2 | 1 | 373.7 | 564 | 0 | 0 | 8 | 4063 | 3598 +/- 1984 | | NA |
| 1.1 | | 3 | 1 | 373.7 | 474 | 0 | 0 | 8 | 4063 | 1894 +/- 1821 | | NA |
| 1.1 | | 4 | 1 | 373.7 | 484 | 0 | 0 | 8 | 4063 | 2083 +/- 1840 | | NA |
| 1.1 10 | 10"-19" | 1 | 1 | 373.7 | 459 | 0 | 0 | 8 | 4063 | 1610 +/- 1792 | | NA |
| 1.1 (138.6 SQ IN) | | 2 | 1 | 373.7 | 504 | 0 | 0 | 8 | 4063 | 2462 +/- 1877 | | NA |
| 1.1 | | 3 | 1 | 373.7 | 429 | 0 | 0 | 8 | 4063 | 1042 +/- 1734 | | NA |
| 1.1 | | 4 | 1 | 373.7 | 409 | 0 | 0 | 8 | 4063 | 663 +/- 1693 | | NA |
| 1.1 11 | 13"-17" | 1 | 1 | 373.7 | 584 | 0 | 0 | 8 | 4063 | 3977 +/- 2018 | | NA |
| 1.1 (75.6 SQ IN) | | 2 | 1 | 373.7 | 459 | 0 | 0 | 8 | 4063 | 1610 +/- 1792 | | NA |
| 1.1 | | 3 | 1 | 373.7 | 484 | 0 | 0 | 8 | 4063 | 2083 +/- 1840 | | NA |
| 1.1 | | 4 | 1 | 373.7 | 529 | 0 | 0 | 8 | 4063 | 2936 +/- 1922 | | NA |
| 1.1 12 | 12"-21" | 1 | 1 | 373.7 | 619 | 0 | 0 | 8 | 4063 | 4640 +/- 2077 | | NA |
| 1.1 (138.6 SQ IN) | | 2 | 1 | 373.7 | 559 | 0 | 0 | 8 | 4063 | 3504 +/- 1975 | | NA |
| 1.1 | | 3 | 1 | 373.7 | 539 | 0 | 0 | 8 | 4063 | 3125 +/- 1940 | | NA |
| 1.1 | | 4 | 1 | 373.7 | 499 | 0 | 0 | 8 | 4063 | 2367 +/- 1867 | | NA |

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| INST EFF. CPM/DPM |
|---|
| 0.1785 |
| 0.1785 |
| 0.1785 |
| 0.1785 |
| 0.1785 |
| 0.1785 |
| 0.1785 |
| 0.1785 |
| 0.1785 |
| 0.176 |
| 0.176 |
| 0.176 |
| 0.176 |
| 0.176 |
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| 0.176 |
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| 0.176 |
| 0.176 |
| 0.176 |
| 0.176 |
| 0.176 |
| 0.176 |
| 0.176 |
| 0.176 |

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TABLE I.2-I

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| 1.1 (88.2 SQ IN) | 2 | 4 | 335.9 | 351 | 0 | 0 | 8 | 3812 | 280 +/- 1548 | NA |
| 1.1 30 21"-23" | 1 | 5 | 329.8 | 425 | 0 | 0 | 8 | 3777 | 1773 +/- 1699 | NA |
| 1.1 (50.4 SQ IN) | 2 | 5 | 329.8 | 385 | 0 | 0 | 8 | 3777 | 1027 +/- 1618 | NA |
| 1.1 | 3 | 5 | 329.8 | 360 | 0 | 0 | 8 | 3777 | 560 +/- 1566 | NA |
| 1.1 | 4 | 5 | 329.8 | 375 | 0 | 0 | 8 | 3777 | 840 +/- 1597 | NA |
| 1.1 31 18"-27" | 1 | 5 | 329.8 | 390 | 0 | 0 | 8 | 3777 | 1120 +/- 1629 | NA |
| 1.1 (138.6 SQ IN) | 2 | 5 | 329.8 | 355 | 0 | 0 | 8 | 3777 | 467 +/- 1555 | NA |
| 1.1 32 0"-7" | 1 | 5 | 329.8 | 365 | 0 | 0 | 8 | 3777 | 653 +/- 1576 | NA |
| 1.1 (113.4 SQ IN) | 2 | 5 | 329.8 | 430 | 0 | 0 | 8 | 3777 | 1866 +/- 1709 | NA |
| 1.1 | 3 | 5 | 329.8 | 375 | 0 | 0 | 8 | 3777 | 840 +/- 1597 | NA |
| 1.1 | 4 | 5 | 329.8 | 475 | 0 | 0 | 8 | 3777 | 2706 +/- 1795 | NA |
| 1.1 33 0"-8" | 1 | 5 | 329.8 | 395 | 0 | 0 | 8 | 3777 | 1213 +/- 1639 | NA |
| 1.1 (126 SQ IN) | 2 | 5 | 329.8 | 430 | 0 | 0 | 8 | 3777 | 1866 +/- 1709 | NA |
| 1.1 | 3 | 5 | 329.8 | 370 | 0 | 0 | 8 | 3777 | 747 +/- 1587 | NA |
| 1.1 | 4 | 5 | 329.8 | 460 | 0 | 0 | 8 | 3777 | 2426 +/- 1767 | NA |
| 1.1 34 27"-43" | 1 | 2 | 294.9 | 265 | 0 | 0 | 8 | 3516 | -549 +/- 1320 | NA |
| 1.1 (226.8 SQ IN) | 2 | 2 | 294.9 | 390 | 0 | 0 | 8 | 3516 | 1739 +/- 1596 | NA |
| 1.1 | 3 | 2 | 294.9 | 405 | 0 | 0 | 8 | 3516 | 2014 +/- 1626 | NA |
| 1.1 | 4 | 2 | 294.9 | 355 | 0 | 0 | 8 | 3516 | 1098 +/- 1524 | NA |

# : RESURVEY DATA, SEE ORIGINAL SHEETS

NOTE: THE AREA UNDER THE CORE NUMBER IS THE SURFACE AREA OF THE CORE ITSELF.

NOTE: BACKGROUNDS ARE FROM THE CALIBRATION CONTROL CHARTS OF EACH INSTRUMENT.

0.1785
0.1786
0.1786
0.1786
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0.1786
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TABLE I.2-1

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| 1.1 13 12"-17.5" | 1 | 2 | 294.9 | 600 | 0 | 0 | 8 | 3516 | 5583 +/- 1975 | NA |
| 1.1 (94.5 SQ IN) | 2 | 2 | 294.9 | 330 | 0 | 0 | 8 | 3516 | 641 +/- 1470 | NA |
| 1.1 | 3 | 2 | 294.9 | 360 | 0 | 0 | 8 | 3516 | 1190 +/- 1534 | NA |
| 1.1 | 4 | 2 | 294.9 | 430 | 0 | 0 | 8 | 3516 | 2471 +/- 1675 | NA |
| 1.1 14 0"-13" | 1 | 1 | 373.7 | 459 | 0 | 0 | 8 | 4063 | 1610 +/- 1792 | NA |
| 1.1 (189 SQ IN) | 2 | 1 | 373.7 | 429 | 0 | 0 | 8 | 4063 | 1042 +/- 1734 | NA |
| 1.1 | 3 | 1 | 373.7 | 404 | 0 | 0 | 8 | 4063 | 568 +/- 1683 | NA |
| 1.1 | 4 | 1 | 373.7 | 934 | 0 | 0 | 8 | 4063 | 10606 +/- 2546 | NA |
| 1.1 15 0"-16" | 1 | 1 | 373.7 | 449 | 0 | 0 | 8 | 4063 | 1420 +/- 1773 | NA |
| 1.1 (226.8 SQ IN) | 2 | 1 | 373.7 | 554 | 0 | 0 | 8 | 4063 | 3409 +/- 1966 | NA |
| 1.1 | 3 | 1 | 373.7 | 594 | 0 | 0 | 8 | 4063 | 4167 +/- 2035 | NA |
| 1.1 16 12"-23" | 1 | 1 | 373.7 | 494 | 0 | 0 | 8 | 4063 | 2273 +/- 1858 | NA |
| 1.1 (163.8 SQ IN) | 2 | 1 | 373.7 | 529 | 0 | 0 | 8 | 4063 | 2936 +/- 1922 | NA |
| 1.1 17 21"-22" | 1 | 4 | 335.9 | 421 | 0 | 0 | 8 | 3812 | 1587 +/- 1692 | NA |
| 1.1 (37.8 SQ IN) | 2 | 4 | 335.9 | 461 | 0 | 0 | 8 | 3812 | 2334 +/- 1770 | NA |
| 1.1 18 0"-10" | 1 | 3 | 374.7 | 595 | 0 | 0 | 8 | 3952 | 4047 +/- 1978 | NA |
| 1.1 (151.2 SQ IN) | 2 | 3 | 374.7 | 435 | 0 | 0 | 8 | 3952 | 1104 +/- 1695 | NA |
| 1.1 | 3 | 3 | 374.7 | 475 | 0 | 0 | 8 | 3952 | 1840 +/- 1770 | NA |
| 1.1 | 4 | 3 | 374.7 | 485 | 0 | 0 | 8 | 3952 | 2024 +/- 1789 | NA |
| 1.1 19 0"-11" | 1 | 1 | 373.7 | 449 | 0 | 0 | 8 | 4063 | 1420 +/- 1773 | NA |
| 1.1 (163.8 SQ IN) | 2 | 1 | 373.7 | 524 | 0 | 0 | 8 | 4063 | 2841 +/- 1913 | NA |
| 1.1 | 3 | 1 | 373.7 | 524 | 0 | 0 | 8 | 4063 | 2841 +/- 1913 | NA |
| 1.1 | 4 | 1 | 373.7 | 389 | 0 | 0 | 8 | 4063 | 284 +/- 1652 | NA |
| 1.1 19A 0"-12" | 1 | 3 | 374.7 | 540 | 0 | 0 | 8 | 3952 | 3035 +/- 1886 | NA |
| 1.1 (176.4 SQ IN) | 2 | 3 | 374.7 | 500 | 0 | 0 | 8 | 3952 | 2299 +/- 1816 | NA |
| 1.1 | 3 | 3 | 374.7 | 535 | 0 | 0 | 8 | 3952 | 2943 +/- 1877 | NA |
| 1.1 | 4 | 3 | 374.7 | 535 | 0 | 0 | 8 | 3952 | 2943 +/- 1877 | NA |
| 1.1 20 0"-15" | 1 | 1 | 373.7 | 494 | 0 | 0 | 8 | 4063 | 2273 +/- 1858 | NA |
| 1.1 (214.2 SQ IN) | 2 | 1 | 373.7 | 539 | 0 | 0 | 8 | 4063 | 3125 +/- 1940 | NA |
| 1.1 | 3 | 1 | 373.7 | 469 | 0 | 0 | 8 | 4063 | 1799 +/- 1811 | NA |
| 1.1 | 4 | 1 | 373.7 | 539 | 0 | 0 | 8 | 4063 | 3125 +/- 1940 | NA |
| 1.1 21 17"-31" | 1 | 3 | 374.7 | 580 | 0 | 0 | 8 | 3952 | 3771 +/- 1954 | NA |
| 1.1 (201.6 SQ IN) | 2 | 3 | 374.7 | 540 | 0 | 0 | 8 | 3952 | 3035 +/- 1886 | NA |
| 1.1 | 3 | 3 | 374.7 | 470 | 0 | 0 | 8 | 3952 | 1748 +/- 1761 | NA |
| 1.1 22 12"-22" | 1 | 3 | 374.7 | 550 | 0 | 0 | 8 | 3952 | 3219 +/- 1903 | NA |
| 1.1 (151.2 SQ IN) | 2 | 3 | 374.7 | 375 | 0 | 0 | 8 | 3952 | 4 +/- 1577 | NA |
| 1.1 23 12.5"-21" | 1 | 4 | 335.9 | 596 | 0 | 0 | 8 | 3812 | 4855 +/- 2009 | NA |
| 1.1 (132.3 SQ IN) | 2 | 4 | 335.9 | 451 | 0 | 0 | 8 | 3812 | 2148 +/- 1751 | NA |
| 1.1 | 3 | 4 | 335.9 | 371 | 0 | 0 | 8 | 3812 | 654 +/- 1590 | NA |
| 1.1 24 21"-24"(63 SQ IN) | 1 | 4 | 335.9 | 531 | 0 | 0 | 8 | 3812 | 3641 +/- 1898 | NA |
| 1.1 25 13"-21" | 1 | 4 | 335.9 | 331 | 0 | 0 | 8 | 3812 | -93 +/- 1504 | NA |
| 1.1 (126 SQ IN) | 2 | 4 | 335.9 | 476 | 0 | 0 | 8 | 3812 | 2614 +/- 1798 | NA |
| 1.1 | 3 | 4 | 335.9 | 446 | 0 | 0 | 8 | 3812 | 2054 +/- 1741 | NA |
| 1.1 | 4 | 4 | 335.9 | 411 | 0 | 0 | 8 | 3812 | 1401 +/- 1673 | NA |
| 1.1 26 0"-13" | 1* | 4 | 335.9 | 446 | 0 | 0 | 8 | 3812 | 2054 +/- 1741 | NA |
| 1.1 (189 SQ IN) | 2* | 4 | 335.9 | 426 | 0 | 0 | 8 | 3812 | 1681 +/- 1702 | NA |
| 1.1 | 3* | 4 | 335.9 | 421 | 0 | 0 | 8 | 3812 | 1587 +/- 1692 | NA |
| 1.1 27 0"-10" | 1 | 2 | 294.9 | 450 | 0 | 0 | 8 | 3516 | 2837 +/- 1713 | NA |
| 1.1 (151.2 SQ IN) | 2 | 2 | 294.9 | 380 | 0 | 0 | 8 | 3516 | 1556 +/- 1576 | NA |
| 1.1 | 3 | 2 | 294.9 | 365 | 0 | 0 | 8 | 3516 | 1281 +/- 1545 | NA |
| 1.1 | 4 | 2 | 294.9 | 325 | 0 | 0 | 8 | 3516 | 549 +/- 1459 | NA |
| 1.1 28 15"20" | 1 | 4 | 335.9 | 396 | 0 | 0 | 8 | 3812 | 1120 +/- 1642 | NA |
| 1.1 (88.2 SQ IN) | 2 | 4 | 335.9 | 421 | 0 | 0 | 8 | 3812 | 1587 +/- 1692 | NA |
| 1.1 | 3 | 4 | 335.9 | 396 | 0 | 0 | 8 | 3812 | 1120 +/- 1642 | NA |
| 1.1 | 4 | 4 | 335.9 | 446 | 0 | 0 | 8 | 3812 | 2054 +/- 1741 | NA |
| 1.1 29 0"-5" | 1 | 4 | 335.9 | 396 | 0 | 0 | 8 | 3812 | 1120 +/- 1642 | NA |

0.1821
0.1821
0.1821
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0.176
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TABLE 1.2-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:12 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 1.1 - CORES FROM HOLDUP TANK FLOOR FOR ALPHA
DEEPEST CORE ONLY

| | | | |
|---|---|---|---|
| RADIATION TYPE: | 2 | | |
| COMPLETION DATE: | 9/93-6/94 | | |
| TECHNICIANS: | MANY | MATERIAL CODE | |
| LOCATION: | 1.0 | 1=CONCRETE | 5=PLASTIC |
| GRID ID: | 1.1 | 2=ROCK | 6=SOIL |
| MEDIA TYPE: | CONCRETE | 3=WOOD | 7=ASPHALT |
| # of POINTS: | 100 (>60) | 4=METAL | 8=OTHER(SPECIFIY): |
| CT IN MINUTES: | 0.2 | | NO MATERIAL BACKGROUND USED |

DPM/100CM^2

| REM.+ FIXED: | | | LIMIT |
|---|---|---|---|
| MAX FOR IND GRID | 257 | PASS | 5000 |
| AVG - SURVEY UNIT | 21 | PASS | 5000 |
| STD X | 57 | | |
| MU SUB ALPHA | 30 | PASS | 5000 |
| MAX HOT SPOT | 0 | PASS | 15000 |

| ID # | CORE NUMBER | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 0.2 MINUTES | SCAN MAX ALPHA COUNTS | TOTAL CONT. AREA CM^2 | MATERIAL CODE | MDA DPM/ 100 CM^2 | WGHTED AVG. ALPHA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 MAX CM^2 TEST |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 1.1 1 | | 1 | 6 | 0.9 | 0 | 0 | 0 | 8 | 433 | -17 +/- 3 | NA |
| 1.1 2 | | 1 | 6 | 0.9 | 5 | 0 | 0 | 8 | 433 | 76 +/- 54 | NA |
| 1.1 3 | | 1 | 6 | 0.9 | 0 | 0 | 0 | 8 | 433 | -17 +/- 3 | NA |
| 1.1 4 | | 1 | 6 | 0.9 | 0 | 0 | 0 | 3 | 433 | -17 +/- 3 | NA |
| 1.1 | | 2 | 6 | 0.9 | 0 | 0 | 0 | 8 | 433 | -17 +/- 3 | NA |
| 1.1 5 | | 1 | 6 | 0.9 | 0 | 0 | 0 | 8 | 433 | -17 +/- 3 | NA |
| 1.1 6 | | 1 | 6 | 0.9 | 5 | 0 | 0 | 8 | 433 | 76 +/- 54 | NA |
| 1.1 7 | | 1 | 6 | 0.9 | 0 | 0 | 0 | 8 | 433 | -17 +/- 3 | NA |
| 1.1 | | 2 | 6 | 0.9 | 0 | 0 | 0 | 8 | 433 | -17 +/- 3 | NA |
| 1.1 9 0"-10" | | 1 | 1 | 0.5 | 5 | 0 | 0 | 8 | 371 | 80 +/- 52 | NA |
| 1.1 (151.2 SQ IN) | | 2 | 1 | 0.5 | 6 | 0 | 0 | 8 | 371 | 98 +/- 57 | NA |
| 1.1 | | 3 | 1 | 0.5 | 15 | 0 | 0 | 8 | 371 | 257 +/- 90 | NA |
| 1.1 | | 4 | 1 | 0.5 | 10 | 0 | 0 | 8 | 371 | 169 +/- 74 | NA |
| 1.1 10 10"-19" | | 1 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 (138.6 SQ IN) | | 2 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 | | 3 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 | | 4 | 1 | 0.5 | 5 | 0 | 0 | 8 | 371 | 80 +/- 52 | NA |
| 1.1 11 13"-17" | | 1 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 (75.6 SQ IN) | | 2 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 | | 3 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 | | 4 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 12 12"-21" | | 1 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 (138.6 SQ IN) | | 2 | 1 | 0.5 | 5 | 0 | 0 | 8 | 371 | 80 +/- 52 | NA |
| 1.1 | | 3 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 | | 4 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 13 12"-17.5" | | 1 | 2 | 0.9 | 0 | 0 | 0 | 8 | 454 | -17 +/- 3 | NA |
| 1.1 (94.5 SQ IN) | | 2 | 2 | 0.9 | 0 | 0 | 0 | 8 | 454 | -17 +/- 3 | NA |

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| INST EFF. CPM/DPM |
|---|
| 0.1803 |
| 0.1803 |
| 0.1803 |
| 0.1803 |
| 0.1803 |
| 0.1803 |
| 0.1803 |
| 0.1803 |
| 0.1803 |
| 0.1879 |
| 0.1879 |
| 0.1879 |
| 0.1879 |
| 0.1879 |
| 0.1879 |
| 0.1879 |
| 0.1879 |
| 0.1879 |
| 0.1879 |
| 0.1879 |
| 0.1879 |
| 0.1879 |
| 0.1879 |
| 0.1879 |
| 0.1719 |
| 0.1719 |

TABLE I.2-2

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| 1.1 | 3 | 2 | 0.9 | 0 | 0 | 0 | 8 | 454 | -17 +/- 3 | NA |
| 1.1 | 4 | 2 | 0.9 | 0 | 0 | 0 | 8 | 454 | -17 +/- 3 | NA |
| 1.1 14 0"-13" | 1 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 (189 SQ IN) | 2 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 | 3 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 | 4 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 15 0"-16" | 1 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 (226.8 SQ IN) | 2 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 | 3 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 16 12"-23" | 1 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 (163.8 SQ IN) | 2 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 17 21"-22" | 1 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 (37.8 SQ IN) | 2 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 18 0"-10" | 1 | 3 | 0.5 | 10 | 0 | 0 | 8 | 348 | 158 +/- 69 | NA |
| 1.1 (151.2 SQ IN) | 2 | 3 | 0.5 | 5 | 0 | 0 | 8 | 348 | 75 +/- 49 | NA |
| 1.1 | 3 | 3 | 0.5 | 0 | 0 | 0 | 8 | 348 | -8 +/- 2 | NA |
| 1.1 | 4 | 3 | 0.5 | 5 | 0 | 0 | 8 | 348 | 75 +/- 49 | NA |
| 1.1 19 0"-11" | 1 | 1 | 0.5 | 5 | 0 | 0 | 8 | 371 | 80 +/- 52 | NA |
| 1.1 (163.8 SQ IN) | 2 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 | 3 | 1 | 0.5 | 5 | 0 | 0 | 8 | 371 | 80 +/- 52 | NA |
| 1.1 | 4 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 19A 0"-12" | 1 | 3 | 0.5 | 0 | 0 | 0 | 8 | 348 | -8 +/- 2 | NA |
| 1.1 (176.4 SQ IN) | 2 | 3 | 0.5 | 0 | 0 | 0 | 8 | 348 | -8 +/- 2 | NA |
| 1.1 | 3 | 3 | 0.5 | 0 | 0 | 0 | 8 | 348 | -8 +/- 2 | NA |
| 1.1 | 4 | 3 | 0.5 | 10 | 0 | 0 | 8 | 348 | 158 +/- 69 | NA |
| 1.1 20 0"-15" | 1 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 (214.2 SQ IN) | 2 | 1 | 0.5 | 5 | 0 | 0 | 8 | 371 | 80 +/- 52 | NA |
| 1.1 | 3 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 | 4 | 1 | 0.5 | 0 | 0 | 0 | 8 | 371 | -9 +/- 2 | NA |
| 1.1 21 17"-31" | 1 | 3 | 0.5 | 5 | 0 | 0 | 8 | 348 | 75 +/- 49 | NA |
| 1.1 (201.6 SQ IN) | 2 | 3 | 0.5 | 10 | 0 | 0 | 8 | 348 | 158 +/- 69 | NA |
| 1.1 | 3 | 3 | 0.5 | 5 | 0 | 0 | 8 | 348 | 75 +/- 49 | NA |
| 1.1 22 12"-22" | 1 | 3 | 0.5 | 0 | 0 | 0 | 8 | 348 | -8 +/- 2 | NA |
| 1.1 (151.2 SQ IN) | 2 | 3 | 0.5 | 5 | 0 | 0 | 8 | 348 | 75 +/- 49 | NA |
| 1.1 23 12.5"-21" | 1 | 4 | 0.6 | 5 | 0 | 0 | 8 | 392 | 80 +/- 53 | NA |
| 1.1 (132.3 SQ IN) | 2 | 4 | 0.6 | 5 | 0 | 0 | 8 | 392 | 80 +/- 53 | NA |
| 1.1 | 3 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 24 21"-24"(63 SQ IN) | 1 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 25 13"-21" | 1 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 (126 SQ IN) | 2 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 | 3 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 | 4 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 26 0"-13" | 1* | 4 | 0.6 | 5 | 0 | 0 | 8 | 392 | 80 +/- 53 | NA |
| 1.1 (189 SQ IN) | 2* | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 | 3* | 4 | 0.6 | 5 | 0 | 0 | 8 | 392 | 80 +/- 53 | NA |
| 1.1 27 0"-10" | 1 | 2 | 0.9 | 10 | 0 | 0 | 8 | 454 | 176 +/- 81 | NA |
| 1.1 (151.2 SQ IN) | 2 | 2 | 0.9 | 0 | 0 | 0 | 8 | 454 | -17 +/- 3 | NA |
| 1.1 | 3 | 2 | 0.9 | 5 | 0 | 0 | 8 | 454 | 80 +/- 57 | NA |
| 1.1 | 4 | 2 | 0.9 | 0 | 0 | 0 | 8 | 454 | -17 +/- 3 | NA |
| 1.1 28 15"20" | 1 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 (88.2 SQ IN) | 2 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 | 3 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 | 4 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 29 0"-5" | 1 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 (88.2 SQ IN) | 2 | 4 | 0.6 | 0 | 0 | 0 | 8 | 392 | -11 +/- 3 | NA |
| 1.1 30 21"-23" | 1 | 5 | 0.9 | 0 | 0 | 0 | 8 | 440 | -17 +/- 3 | NA |

0.1719
0.1719
0.1879
0.1879
0.1879
0.1879
0.1879
0.1879
0.1879
0.1879
0.1879
0.1836
0.1836
0.2
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0.2
0.1879
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0.2
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0.1836
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0.1719
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0.1836
0.1836
0.1836
0.1773

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TABLE 1.2-2

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| 1.1 (50.4 SQ IN) | 2 | 5 | 0.9 | 0 | 0 | 0 | 8 | 440 | -17 +/- 3 | NA |
| 1.1 | 3 | 5 | 0.9 | 5 | 0 | 0 | 8 | 440 | 77 +/- 55 | NA |
| 1.1 | 4 | 5 | 0.9 | 0 | 0 | 0 | 8 | 440 | -17 +/- 3 | NA |
| 1.1 31 18"-27" | 1 | 5 | 0.9 | 0 | 0 | 0 | 8 | 440 | -17 +/- 3 | NA |
| 1.1 (138.6 SQ IN) | 2 | 5 | 0.9 | 5 | 0 | 0 | 8 | 440 | 77 +/- 55 | NA |
| 1.1 32 0"-7" | 1 | 5 | 0.9 | 0 | 0 | 0 | 8 | 440 | -17 +/- 3 | NA |
| 1.1 (113.4 SQ IN) | 2 | 5 | 0.9 | 5 | 0 | 0 | 8 | 440 | 77 +/- 55 | NA |
| 1.1 | 3 | 5 | 0.9 | 0 | 0 | 0 | 8 | 440 | -17 +/- 3 | NA |
| 1.1 | 4 | 5 | 0.9 | 0 | 0 | 0 | 8 | 440 | -17 +/- 3 | NA |
| 1.1 33 0"-8" | 1 | 5 | 0.9 | 5 | 0 | 0 | 8 | 440 | 77 +/- 55 | NA |
| 1.1 (126 SQ IN) | 2 | 5 | 0.9 | 0 | 0 | 0 | 8 | 440 | -17 +/- 3 | NA |
| 1.1 | 3 | 5 | 0.9 | 0 | 0 | 0 | 8 | 440 | -17 +/- 3 | NA |
| 1.1 | 4 | 5 | 0.9 | 0 | 0 | 0 | 8 | 440 | -17 +/- 3 | NA |
| 1.1 34 27"-43" | 1 | 2 | 0.9 | 5 | 0 | 0 | 8 | 454 | 80 +/- 57 | NA |
| 1.1 (226.8 SQ IN) | 2 | 2 | 0.9 | 0 | 0 | 0 | 8 | 454 | -17 +/- 3 | NA |
| 1.1 | 3 | 2 | 0.9 | 0 | 0 | 0 | 8 | 454 | -17 +/- 3 | NA |
| 1.1 | 4 | 2 | 0.9 | 0 | 0 | 0 | 8 | 454 | -17 +/- 3 | NA |

# : RESURVEY DATA, SEE ORIGINAL SHEETS

NOTE: BACKGROUNDS ARE FROM CALIBRATION CONTROL CHARTS OF EACH INSTRUMENT

NOTE: THE AREA UNDER THE CORE NUMBER IS THE SURFACE AREA OF THE CORE ITSELF.

0.1773
0.1773
0.1773
0.1773
0.1773
0.1773
0.1773
0.1773
0.1773
0.1773
0.1773
0.1773
0.1719
0.1719
0.1719
0.1719

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TABLE 3.1-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
EAST EXTERIOR WALL - REACTOR BUILDING AREA 3.1 FOR UREM/HR

RADIATION TYPE: GAMMA SURVEY IN UREM/HR
COMPLETION DATE: 10-26-94
TECHNICIANS: JB/PK
LOCATION: 3.0
GRID ID: 3.1
MEDIA TYPE: CONCRETE
# of POINTS: 36

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | LIMIT |
|---|---|---|
| MAX | 9.00 PASS | 10 |
| AVG | 2.89 PASS | 5 |
| STD X | 2.48 | |
| MU SUB ALPHA | 3.59 PASS | 5 |

| ID # | INST. ID # | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|
| 3.1 | 1 | A | 6 | 7 | B | 1 |
| 3.1 | 2 | A | 6 | 15 | B | 9 |
| 3.1 | 3 | A | 6 | 13 | B | 7 |
| 3.1 | 4 | A | 6 | 12 | B | 6 |
| 3.1 | 5 | A | 6 | 8 | B | 2 |
| 3.1 | 6 | A | 6 | 12 | B | 6 |
| 3.1 | 7 | A | 6 | 7 | B | 1 |
| 3.1 | 8 | A | 6 | 8 | B | 2 |
| 3.1 | 9 | A | 6 | 8 | B | 2 |
| 3.1 | 10 | A | 6 | 7 | B | 1 |
| 3.1 | 11 | A | 6 | 11 | B | 5 |
| 3.1 | 12 | A | 6 | 5 | B | -1 |
| 3.1 | 13 | A | 6 | 8 | B | 2 |
| 3.1 | 14 | A | 6 | 10 | B | 4 |
| 3.1 | 15 | A | 6 | 8 | B | 2 |
| 3.1 | 16 | A | 6 | 9 | B | 3 |
| 3.1 | 17 | A | 6 | 8 | B | 2 |
| 3.1 | 18 | A | 6 | 9 | B | 3 |
| 3.1 | 19 | A | 6 | 7 | B | 1 |
| 3.1 | 20 | A | 6 | 8 | B | 2 |
| 3.1 | 21 | A | 6 | 12 | B | 6 |
| 3.1 | 22 | A | 6 | 10 | B | 4 |
| 3.1 | 23 | A | 6 | 8 | B | 2 |
| 3.1 | 24 | A | 6 | 11 | B | 5 |
| 3.1 | 25 | A | 6 | 6 | B | 0 |
| 3.1 | 26 | A | 6 | 7 | B | 1 |
| 3.1 | 27 | A | 6 | 7 | B | 1 |
| 3.1 | 28 | A | 6 | 6 | B | 0 |

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TABLE 3.1-I

| | | | | | | |
|---|---|---|---|---|---|---|
| 3.1 | 29 | A | 6 | 8 | 8 | 2 |
| 3.1 | 30 | A | 6 | 10 | 8 | 4 |
| 3.1 | 31 | A | 6 | 10 | 8 | 4 |
| 3.1 | 32 | A | 6 | 5 | 8 | -1 |
| 3.1 | 33 | A | 6 | 7 | 8 | 1 |
| 3.1 | 34 | A | 6 | 14 | 8 | 8 |
| 3.1 | 35 | A | 6 | 12 | 8 | 6 |
| 3.1 | 36 | A | 6 | 7 | 8 | 1 |

ANSTEC
APERTURE
CARD

Also Available on
Aperture Card

TABLE 3.1-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:23 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
EAST EXTERIOR WALL REACTOR - AREA 3.1 FOR BETA

RADIATION TYPE: 1 (1=BETA, 2=ALPHA)
COMPLETION
DATE: 10-25-94
TECHNICIANS: JB/PK
LOCATION: 3.0
GRID ID: 3.1
MEDIA TYPE: CONCRETE
# of POINTS: 36
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2
REM.+ FIXED:

| | | LIMIT | |
|---|---|---|---|
| MAX | 2291 PASS | 40500 | BETA SCALING FACTOR = 0.3 |
| AVG | 1053 PASS | 13500 | |
| STD X | 507 | | |
| MU SUB ALPHA | 1196 PASS | 13500 | |

| ID # | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | BETA FIXED GCPM | MATER-IAL CODE | MDA DPM/ 100 CM^2 | BETA FIXED DPM/ 100 CM^2 | STAT SIG ? | BETA EFF CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| 3.1 | 1 | 6 452.7 | 500 | 500 | 8 | 1860 | 865 | N | 0.1822 |
| 3.1 | 2 | 6 452.7 | 494 | 494 | 8 | 1860 | 756 | N | 0.1822 |
| 3.1 | 3 | 6 452.7 | 462 | 462 | 8 | 1860 | 170 | N | 0.1822 |
| 3.1 | 4 | 6 452.7 | 552 | 552 | 8 | 1860 | 1817 | N | 0.1822 |
| 3.1 | 5 | 6 452.7 | 538 | 538 | 8 | 1860 | 1561 | N | 0.1822 |
| 3.1 | 6 | 6 452.7 | 495 | 495 | 8 | 1860 | 774 | N | 0.1822 |
| 3.1 | 7 | 6 452.7 | 480 | 480 | 8 | 1860 | 499 | N | 0.1822 |
| 3.1 | 8 | 6 452.7 | 486 | 486 | 8 | 1860 | 609 | N | 0.1822 |
| 3.1 | 9 | 6 452.7 | 553 | 553 | 8 | 1860 | 1835 | N | 0.1822 |
| 3.1 | 10 | 6 452.7 | 543 | 543 | 8 | 1860 | 1652 | N | 0.1822 |
| 3.1 | 11 | 6 452.7 | 470 | 470 | 8 | 1860 | 317 | N | 0.1822 |
| 3.1 | 12 | 6 452.7 | 508 | 508 | 8 | 1860 | 1012 | N | 0.1822 |
| 3.1 | 13 | 6 452.7 | 475 | 475 | 8 | 1860 | 408 | N | 0.1822 |
| 3.1 | 14 | 6 452.7 | 484 | 484 | 8 | 1860 | 573 | N | 0.1822 |
| 3.1 | 15 | 6 452.7 | 474 | 474 | 8 | 1860 | 390 | N | 0.1822 |
| 3.1 | 16 | 6 452.7 | 505 | 505 | 8 | 1860 | 957 | N | 0.1822 |
| 3.1 | 17 | 6 452.7 | 507 | 507 | 8 | 1860 | 993 | N | 0.1822 |
| 3.1 | 18 | 6 452.7 | 504 | 504 | 8 | 1860 | 939 | N | 0.1822 |
| 3.1 | 19 | 1 440.8 | 524 | 524 | 8 | 1900 | 1522 | N | 0.1760 |
| 3.1 | 20 | 1 440.8 | 526 | 526 | 8 | 1900 | 1559 | N | 0.1760 |
| 3.1 | 21 | 1 440.8 | 485 | 485 | 8 | 1900 | 809 | N | 0.1760 |
| 3.1 | 22 | 1 440.8 | 484 | 484 | 8 | 1900 | 790 | N | 0.1760 |
| 3.1 | 23 | 1 440.8 | 521 | 521 | 8 | 1900 | 1467 | N | 0.1760 |
| 3.1 | 24 | 1 440.8 | 477 | 477 | 8 | 1900 | 662 | N | 0.1760 |
| 3.1 | 25 | 1 440.8 | 566 | 566 | 8 | 1900 | 2291 | Y | 0.1760 |
| 3.1 | 26 | 1 453.7 | 484 | 484 | 8 | 1927 | 554 | N | 0.1760 |

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Also Available on
Aperture Card

9502100114-19

TABLE 3.1-2

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.1 | 27 | 1 | 453.7 | 529 | 529 | B | 1927 | 1378 N | 0.1760 |
| 3.1 | 28 | 1 | 453.7 | 512 | 512 | B | 1927 | 1067 N | 0.1760 |
| 3.1 | 29 | 1 | 453.7 | 512 | 512 | B | 1927 | 1067 N | 0.1760 |
| 3.1 | 30 | 1 | 453.7 | 516 | 516 | B | 1927 | 1140 N | 0.1760 |
| 3.1 | 31 | 1 | 453.7 | 535 | 535 | B | 1927 | 1487 N | 0.1760 |
| 3.1 | 32 | 1 | 453.7 | 538 | 538 | B | 1927 | 1542 N | 0.1760 |
| 3.1 | 33 | 1 | 453.7 | 533 | 533 | B | 1927 | 1451 N | 0.1760 |
| 3.1 | 34 | 1 | 453.7 | 538 | 538 | B | 1927 | 1542 N | 0.1760 |
| 3.1 | 35 | 1 | 453.7 | 510 | 510 | B | 1927 | 1030 N | 0.1760 |
| 3.1 | 36 | 1 | 453.7 | 477 | 477 | B | 1927 | 426 N | 0.1760 |

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TABLE 3.1-3

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.1 | 27 | 1 | 3.4 | 3 | 3 | B | 60 | -2 N | 0.1896 |
| 3.1 | 28 | 1 | 3.4 | 3 | 3 | B | 60 | -2 N | 0.1896 |
| 3.1 | 29 | 1 | 3.4 | 2 | 2 | B | 60 | -7 N | 0.1896 |
| 3.1 | 30 | 1 | 3.4 | 2 | 2 | B | 60 | -7 N | 0.1896 |
| 3.1 | 31 | 1 | 3.4 | 7 | 7 | B | 60 | 19 N | 0.1896 |
| 3.1 | 32 | 1 | 3.4 | 5 | 5 | B | 60 | 8 N | 0.1896 |
| 3.1 | 33 | 1 | 3.4 | 5 | 5 | B | 60 | 8 N | 0.1896 |
| 3.1 | 34 | 1 | 3.4 | 4 | 4 | B | 60 | 3 N | 0.1896 |
| 3.1 | 35 | 1 | 3.4 | 2 | 2 | B | 60 | -7 N | 0.1896 |
| 3.1 | 36 | 1 | 3.4 | 3 | 3 | B | 60 | -2 N | 0.1896 |

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CARD

Also Available on
Aperture Card

TABLE 3.1-3

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:22 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
EAST EXTERIOR REACTOR WALL - AREA 3.1 FOR ALPHA

RADIATION TYPE: 2 (1=BETA, 2=ALPHA)
COMPLETION DATE: 10-26-94
TECHNICIANS: JB/PK
LOCATION: 3.0
GRID ID: 3.1
MEDIA TYPE: CONCRETE
# of POINTS: 36
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | LIMIT |
|---|---|---|
| MAX | 42 PASS | 15000 |
| AVG | 12 PASS | 5000 |
| STD X | 13 | |
| MU SUB ALPHA | 16 PASS | 5000 |

| ID # | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | ALPHA FIXED GCPM | MATER-IAL CODE | MDA DPM/ 100 CM^2 | ALPHA FIXED DPM/ 100 CM^2 | STAT SIG ? | ALPHA EFF. CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| 3.1 | 1 | 6 | 1.5 | 9 | 9 | 8 | 47 | 42 N | 0.1803 |
| 3.1 | 2 | 6 | 1.5 | 4 | 4 | 8 | 47 | 14 N | 0.1803 |
| 3.1 | 3 | 6 | 1.5 | 5 | 5 | 8 | 47 | 19 N | 0.1803 |
| 3.1 | 4 | 6 | 1.5 | 7 | 7 | 8 | 47 | 31 N | 0.1803 |
| 3.1 | 5 | 6 | 1.5 | 5 | 5 | 8 | 47 | 19 N | 0.1803 |
| 3.1 | 6 | 6 | 1.5 | 4 | 4 | 8 | 47 | 14 N | 0.1803 |
| 3.1 | 7 | 6 | 1.5 | 7 | 7 | 8 | 47 | 31 N | 0.1803 |
| 3.1 | 8 | 6 | 1.5 | 5 | 5 | 8 | 47 | 19 N | 0.1803 |
| 3.1 | 9 | 6 | 1.5 | 4 | 4 | 8 | 47 | 14 N | 0.1803 |
| 3.1 | 10 | 6 | 1.5 | 6 | 6 | 8 | 47 | 25 N | 0.1803 |
| 3.1 | 11 | 6 | 1.5 | 4 | 4 | 8 | 47 | 14 N | 0.1803 |
| 3.1 | 12 | 6 | 1.5 | 3 | 3 | 8 | 47 | 8 N | 0.1803 |
| 3.1 | 13 | 6 | 1.5 | 6 | 6 | 8 | 47 | 25 N | 0.1803 |
| 3.1 | 14 | 6 | 1.5 | 3 | 3 | 8 | 47 | 8 N | 0.1803 |
| 3.1 | 15 | 6 | 1.5 | 2 | 2 | 8 | 47 | 3 N | 0.1803 |
| 3.1 | 16 | 6 | 1.5 | 4 | 4 | 8 | 47 | 14 N | 0.1803 |
| 3.1 | 17 | 6 | 1.5 | 3 | 3 | 8 | 47 | 8 N | 0.1803 |
| 3.1 | 18 | 6 | 1.5 | 2 | 2 | 8 | 47 | 3 N | 0.1803 |
| 3.1 | 19 | 1 | 3.4 | 9 | 9 | 8 | 60 | 30 N | 0.1896 |
| 3.1 | 20 | 1 | 3.4 | 1 | 1 | 8 | 60 | -13 N | 0.1896 |
| 3.1 | 21 | 1 | 3.4 | 7 | 7 | 8 | 60 | 19 N | 0.1896 |
| 3.1 | 22 | 1 | 3.4 | 5 | 5 | 8 | 60 | 8 N | 0.1896 |
| 3.1 | 23 | 1 | 3.4 | 5 | 5 | 8 | 60 | 8 N | 0.1896 |
| 3.1 | 24 | 1 | 3.4 | 7 | 7 | 8 | 60 | 19 N | 0.1896 |
| 3.1 | 25 | 1 | 3.4 | 10 | 10 | 8 | 60 | 35 N | 0.1896 |
| 3.1 | 26 | 1 | 3.4 | 7 | 7 | 8 | 60 | 19 N | 0.1896 |

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TABLE 3.2-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:26 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
WEST EXTERIOR REACTOR WALL - AREA 3.2 FOR UREM

RADIATION TYPE: GAMMA SURVEY IN UREM/HR
COMPLETION DATE: 10-5-94
TECHNICIANS: JB/DR/PK
LOCATION: 3.0
GRID ID: 3.2
MEDIA TYPE: CONCRETE
# of POINTS: 30

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | LIMIT |
|---|---|---|
| MAX | 6.00 PASS | 10 |
| AVG | 3.10 PASS | 5 |
| STD X | 1.32 | |
| MU SUB ALPHA | 3.51 PASS | 5 |

| ID # | INST. ID # | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|
| 3.2 | 1 | A | 6 | 9 | 8 | 3 |
| 3.2 | 2 | A | 6 | 8 | 8 | 2 |
| 3.2 | 3 | A | 6 | 9 | 8 | 3 |
| 3.2 | 4 | A | 6 | 9 | 8 | 3 |
| 3.2 | 5 | A | 6 | 9 | 8 | 3 |
| 3.2 | 6 | A | 6 | 7 | 8 | 1 |
| 3.2 | 7 | A | 6 | 6 | 8 | 0 |
| 3.2 | 8 | A | 6 | 8 | 8 | 2 |
| 3.2 | 9 | A | 6 | 12 | 8 | 6 |
| 3.2 | 10 | A | 6 | 10 | 8 | 4 |
| 3.2 | 11 | A | 6 | 9 | 8 | 3 |
| 3.2 | 12 | A | 6 | 10 | 8 | 4 |
| 3.2 | 13 | A | 6 | 10 | 8 | 4 |
| 3.2 | 14 | A | 6 | 9 | 8 | 3 |
| 3.2 | 15 | A | 6 | 9 | 8 | 3 |
| 3.2 | 16 | A | 6 | 10 | 8 | 4 |
| 3.2 | 17 | A | 6 | 9 | 8 | 3 |
| 3.2 | 18 | A | 6 | 10 | 8 | 4 |
| 3.2 | 19 | A | 6 | 9 | 8 | 3 |
| 3.2 | 20 | A | 6 | 8 | 8 | 2 |
| 3.2 | 21 | A | 6 | 8 | 8 | 2 |
| 3.2 | 22 | A | 6 | 8 | 8 | 2 |
| 3.2 | 23 | A | 6 | 11 | 8 | 5 |
| 3.2 | 24 | A | 6 | 7 | 8 | 1 |
| 3.2 | 25 | A | 6 | 11 | 8 | 5 |
| 3.2 | 26 | A | 6 | 9 | 8 | 3 |
| 3.2 | 27 | A | 6 | 8 | 8 | 2 |
| 3.2 | 28 | A | 6 | 11 | 8 | 5 |
| 3.2 | 29 | A | 6 | 10 | 8 | 4 |
| 3.2 | 30 | A | 6 | 10 | 8 | 4 |

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CARD

Also Available on
Aperture Card

9502100114 - 23

TABLE 3.2-3

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:25 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
WEST EXTERIOR REACTOR WALL - AREA 3.2 FOR ALPHA

RADIATION TYPE: 2 (1=BETA, 2=ALPHA)
COMPLETION
DATE: 10-10-94
TECHNICIANS: JB/DR/PK
LOCATION: 3.0
GRID ID: 3.2
MEDIA TYPE: CONCRETE
# of POINTS: 30
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | LIMIT |
|---|---|---|
| MAX | 23 PASS | 15000 |
| AVG | 4 PASS | 5000 |
| STD X | 6 | |
| MU SUB ALPHA | 5 PASS | 5000 |

| ID # | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | ALPHA FIXED GCPM | MATER-IAL CODE | MDA DPM/ 100 CM^2 | ALPHA FIXED DPM/ 100 CM^2 | STAT SIG ? | ALPHA EFF. CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| 3.2 | 1 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 2 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 3 | 4 | 0.4 | 5 | 5 | 8 | 28 | 23 N | 0.2015 |
| 3.2 | 4 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 5 | 4 | 0.4 | 0 | 0 | 8 | 28 | -2 N | 0.2015 |
| 3.2 | 6 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 7 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 8 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 9 | 4 | 0.4 | 0 | 0 | 8 | 28 | -2 N | 0.2015 |
| 3.2 | 10 | 4 | 0.4 | 0 | 0 | 8 | 28 | -2 N | 0.2015 |
| 3.2 | 11 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 12 | 4 | 0.4 | 2 | 2 | 8 | 28 | 8 N | 0.2015 |
| 3.2 | 13 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 14 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 15 | 4 | 0.4 | 2 | 2 | 8 | 28 | 8 N | 0.2015 |
| 3.2 | 16 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 17 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 18 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 19 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 20 | 4 | 0.4 | 0 | 0 | 8 | 28 | -2 N | 0.2015 |
| 3.2 | 21 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 22 | 4 | 0.4 | 0 | 0 | 8 | 28 | -2 N | 0.2015 |
| 3.2 | 23 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 24 | 4 | 0.4 | 4 | 4 | 8 | 28 | 18 N | 0.2015 |
| 3.2 | 25 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 26 | 4 | 0.4 | 0 | 0 | 8 | 28 | -2 N | 0.2015 |
| 3.2 | 27 | 4 | 0.4 | 0 | 0 | 8 | 28 | -2 N | 0.2015 |
| 3.2 | 28 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| 3.2 | 29 | 4 | 0.4 | 3 | 3 | 8 | 28 | 13 N | 0.2015 |
| 3.2 | 30 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |

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TABLE 3.2-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:26 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
WEST EXTERIOR REACTOR WALL - AREA 3.2 FOR BETA

RADIATION TYPE: 1 (1=BETA, 2=ALPHA)
COMPLETION DATE: 10-10-94
TECHNICIANS: JB/DR/PK
LOCATION: 3.0
GRID ID: 3.2
MEDIA TYPE: CONCRETE
# of POINTS: 30
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | | LIMIT | |
|---|---|---|---|---|
| MAX | 3838 | PASS | 40500 | BETA SCALING FACTOR = 0.3 |
| AVG | 1483 | PASS | 13500 | |
| STD X | 825 | | | |
| MU SUB ALPHA | 1739 | PASS | 13500 | |

| ID # | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | BETA FIXED GCPM | MATER-IAL CODE | MDA DPM/ 100 CM^2 | BETA FIXED DPM/ 100 CM^2 | STAT SIG ? | INST EFF CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| 3.2 | 1 | 4 | 594.5 | 679 | 679 | 8 | 2168 | 1578 N | 0.1785 |
| 3.2 | 2 | 4 | 594.5 | 629 | 629 | 8 | 2168 | 644 N | 0.1785 |
| 3.2 | 3 | 4 | 594.5 | 689 | 689 | 8 | 2168 | 1765 N | 0.1785 |
| 3.2 | 4 | 4 | 594.5 | 634 | 634 | 8 | 2168 | 738 N | 0.1785 |
| 3.2 | 5 | 4 | 594.5 | 636 | 636 | 8 | 2168 | 775 N | 0.1785 |
| 3.2 | 6 | 4 | 594.5 | 653 | 653 | 8 | 2168 | 1092 N | 0.1785 |
| 3.2 | 7 | 4 | 594.5 | 599 | 599 | 8 | 2168 | 84 N | 0.1785 |
| 3.2 | 8 | 4 | 594.5 | 656 | 656 | 8 | 2168 | 1148 N | 0.1785 |
| 3.2 | 9 | 4 | 594.5 | 688 | 688 | 8 | 2168 | 1746 N | 0.1785 |
| 3.2 | 10 | 4 | 594.5 | 650 | 650 | 8 | 2168 | 1036 N | 0.1785 |
| 3.2 | 11 | 4 | 594.5 | 644 | 644 | 8 | 2168 | 924 N | 0.1785 |
| 3.2 | 12 | 4 | 594.5 | 631 | 631 | 8 | 2168 | 682 N | 0.1785 |
| 3.2 | 13 | 4 | 594.5 | 642 | 642 | 8 | 2168 | 887 N | 0.1785 |
| 3.2 | 14 | 4 | 594.5 | 680 | 680 | 8 | 2168 | 1597 N | 0.1785 |
| 3.2 | 15 | 4 | 594.5 | 694 | 694 | 8 | 2168 | 1858 N | 0.1785 |
| 3.2 | 16 | 4 | 594.5 | 676 | 676 | 8 | 2168 | 1522 N | 0.1785 |
| 3.2 | 17 | 4 | 594.5 | 655 | 655 | 8 | 2168 | 1130 N | 0.1785 |
| 3.2 | 18 | 4 | 594.5 | 650 | 650 | 8 | 2168 | 1036 N | 0.1785 |
| 3.2 | 19 | 4 | 594.5 | 709 | 709 | 8 | 2168 | 2138 N | 0.1785 |
| 3.2 | 20 | 4 | 594.5 | 649 | 649 | 8 | 2168 | 1018 N | 0.1785 |
| 3.2 | 21 | 4 | 594.5 | 657 | 657 | 8 | 2168 | 1167 N | 0.1785 |
| 3.2 | 22 | 4 | 594.5 | 636 | 636 | 8 | 2168 | 775 N | 0.1785 |
| 3.2 | 23 | 4 | 594.5 | 751 | 751 | 8 | 2168 | 2923 Y | 0.1785 |
| 3.2 | 24 | 4 | 594.5 | 754 | 754 | 8 | 2168 | 2979 Y | 0.1785 |
| 3.2 | 25 | 4 | 594.5 | 800 | 800 | 8 | 2168 | 3838 Y | 0.1785 |
| 3.2 | 26 | 4 | 594.5 | 690 | 690 | 8 | 2168 | 1783 N | 0.1785 |
| 3.2 | 27 | 4 | 594.5 | 658 | 658 | 8 | 2168 | 1186 N | 0.1785 |
| 3.2 | 28 | 4 | 594.5 | 700 | 700 | 8 | 2168 | 1970 N | 0.1785 |
| 3.2 | 29 | 4 | 594.5 | 751 | 751 | 8 | 2168 | 2923 Y | 0.1785 |
| 3.2 | 30 | 4 | 594.5 | 678 | 678 | 8 | 2168 | 1559 N | 0.1785 |

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TABLE 4.1-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:29 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
REACTOR BUILDING ROOF - AREA 4.1 GRAVEL FOR BETA

RADIATION TYPE: 1 (1=BETA, 2=ALPHA)
COMPLETION DATE: 10-10-94
TECHNICIANS: RW/TA/DT
LOCATION: 4.0
GRID ID: 4.1
MEDIA TYPE: GRAVEL
# of POINTS: 30
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | LIMIT | |
|---|---|---|---|
| MAX | 5431 PASS | 40500 | |
| AVG | 3336 PASS | 13500 | BETA SCALING FACTOR = 0.3 |
| STD X | 757 | | |
| MU SUB ALPHA | 3571 PASS | 13500 | |

| ID # | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | BETA FIXED GCPM | MATER-IAL CODE | MDA DPM/ 100 CM^2 | BETA FIXED DPM/ 100 CM^2 | STAT SIG ? | BETA EFF. CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| 4.1 | 1 | 5 | 421 | 629 | 629 | 8 | 1831 | 3882 Y | 0.1786 |
| 4.1 | 2 | 5 | 421 | 608 | 608 | 8 | 1831 | 3490 Y | 0.1786 |
| 4.1 | 3 | 5 | 421 | 626 | 626 | 8 | 1831 | 3826 Y | 0.1786 |
| 4.1 | 4 | 5 | 421 | 598 | 598 | 8 | 1831 | 3303 Y | 0.1786 |
| 4.1 | 5 | 5 | 421 | 637 | 637 | 8 | 1831 | 4031 Y | 0.1786 |
| 4.1 | 6 | 5 | 421 | 574 | 574 | 8 | 1831 | 2856 Y | 0.1786 |
| 4.1 | 7 | 5 | 421 | 556 | 556 | 8 | 1831 | 2520 Y | 0.1786 |
| 4.1 | 8 | 5 | 421 | 581 | 581 | 8 | 1831 | 2986 Y | 0.1786 |
| 4.1 | 9 | 5 | 421 | 669 | 669 | 8 | 1831 | 4629 Y | 0.1786 |
| 4.1 | 10 | 5 | 421 | 601 | 601 | 8 | 1831 | 3359 Y | 0.1786 |
| 4.1 | 11 | 5 | 421 | 591 | 591 | 8 | 1831 | 3173 Y | 0.1786 |
| 4.1 | 12 | 5 | 421 | 613 | 613 | 8 | 1831 | 3583 Y | 0.1786 |
| 4.1 | 13 | 5 | 421 | 590 | 590 | 8 | 1831 | 3154 Y | 0.1786 |
| 4.1 | 14 | 5 | 421 | 617 | 617 | 8 | 1831 | 3658 Y | 0.1786 |
| 4.1 | 15 | 5 | 421 | 579 | 579 | 8 | 1831 | 2949 Y | 0.1786 |
| 4.1 | 16 | 5 | 421 | 626 | 626 | 8 | 1831 | 3826 Y | 0.1786 |
| 4.1 | 17 | 5 | 421 | 604 | 604 | 8 | 1831 | 3415 Y | 0.1786 |
| 4.1 | 18 | 5 | 421 | 712 | 712 | 8 | 1831 | 5431 Y | 0.1786 |
| 4.1 | 19 | 5 | 421 | 620 | 620 | 8 | 1831 | 3714 Y | 0.1786 |
| 4.1 | 20 | 5 | 421 | 648 | 648 | 8 | 1831 | 4237 Y | 0.1786 |
| 4.1 | 21 | 5 | 421 | 578 | 578 | 8 | 1831 | 2930 Y | 0.1786 |
| 4.1 | 22 | 5 | 421 | 580 | 580 | 8 | 1831 | 2968 Y | 0.1786 |
| 4.1 | 23 | 5 | 421 | 612 | 612 | 8 | 1831 | 3565 Y | 0.1786 |
| 4.1 | 24 | 5 | 421 | 575 | 575 | 8 | 1831 | 2874 Y | 0.1786 |
| 4.1 | 25 | 5 | 421 | 631 | 631 | 8 | 1831 | 3919 Y | 0.1786 |
| 4.1 | 26 | 5 | 421 | 516 | 516 | 8 | 1831 | 1773 N | 0.1786 |
| 4.1 | 27 | 5 | 421 | 569 | 569 | 8 | 1831 | 2762 Y | 0.1786 |
| 4.1 | 28 | 5 | 421 | 525 | 525 | 8 | 1831 | 1941 Y | 0.1786 |
| 4.1 | 29 | 5 | 421 | 587 | 587 | 8 | 1831 | 3098 Y | 0.1786 |
| 4.1 | 30 | 5 | 421 | 540 | 540 | 8 | 1831 | 2221 Y | 0.1786 |

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Also Available on
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9502100114-26

TABLE 4.1-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
REACTOR BUILDING ROOF - AREA 4.1 FOR UREM

RADIATION TYPE: GAMMA SURVEY IN UREM/HR
COMPLETION DATE: 10-10-94
TECHNICIANS: RW/DT/TA
LOCATION: 4.0
GRID ID: 4.1
MEDIA TYPE: SOIL
# of POINTS: 30

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | | LIMIT |
|---|---|---|---|
| MAX | 3 | PASS | 10 |
| AVG | 0.40 | PASS | 5 |
| STD X | 1 | | |
| MU SUB ALPHA | 1 | PASS | 5 |

| ID # | LOC# | INST. ID # | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|---|
| 4.1 | 1 | A | 6 | 9 | 8 | 3 |
| 4.1 | 2 | A | 6 | 8 | 8 | 2 |
| 4.1 | 3 | A | 6 | 5 | 8 | -1 |
| 4.1 | 4 | A | 6 | 7 | 8 | 1 |
| 4.1 | 5 | A | 6 | 5 | 8 | -1 |
| 4.1 | 6 | A | 6 | 6 | 8 | 0 |
| 4.1 | 7 | A | 6 | 6 | 8 | 0 |
| 4.1 | 8 | A | 6 | 7 | 8 | 1 |
| 4.1 | 9 | A | 6 | 8 | 8 | 2 |
| 4.1 | 10 | A | 6 | 7 | 8 | 1 |
| 4.1 | 11 | A | 6 | 7 | 8 | 1 |
| 4.1 | 12 | A | 6 | 6 | 8 | 0 |
| 4.1 | 13 | A | 6 | 6 | 8 | 0 |
| 4.1 | 14 | A | 6 | 6 | 8 | 0 |
| 4.1 | 15 | A | 6 | 8 | 8 | 2 |
| 4.1 | 16 | A | 6 | 5 | 8 | -1 |
| 4.1 | 17 | A | 6 | 7 | 8 | 1 |
| 4.1 | 18 | A | 6 | 8 | 8 | 2 |
| 4.1 | 19 | A | 6 | 6 | 8 | 0 |
| 4.1 | 20 | A | 6 | 7 | 8 | 1 |
| 4.1 | 21 | A | 6 | 6 | 8 | 0 |
| 4.1 | 22 | A | 6 | 6 | 8 | 0 |
| 4.1 | 23 | A | 6 | 5 | 8 | -1 |
| 4.1 | 24 | A | 6 | 4 | 8 | -2 |
| 4.1 | 25 | A | 6 | 5 | 8 | -1 |
| 4.1 | 26 | A | 6 | 8 | 8 | 2 |
| 4.1 | 27 | A | 6 | 7 | 8 | 1 |
| 4.1 | 28 | A | 6 | 3 | 8 | -3 |
| 4.1 | 29 | A | 6 | 7 | 8 | 1 |
| 4.1 | 30 | A | 6 | 7 | 8 | 1 |

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TABLE 4.1-3

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:28 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
REACTOR BUILDING ROOF - AREA 4.1 GRAVEL FOR ALPHA

RADIATION TYPE: 2 (1=BETA, 2=ALPHA)
COMPLETION DATE: 10-10-94
TECHNICIANS: RW/TA/DT
LOCATION: 4.0
GRID ID: 4.1
MEDIA TYPE: GRAVEL
# of POINTS: 30
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2
REM.+ FIXED:

| | | LIMIT |
|---|---|---|
| MAX | 34 PASS | 15000 |
| AVG | 10 PASS | 5000 |
| STD X | 9 | |
| MU SUB ALPHA | 13 PASS | 5000 |

| ID # | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | ALPHA FIXED GCPM | MATERIAL CODE | MDA DPM/ 100 CM^2 | ALPHA FIXED DPM/ 100 CM^2 | STAT SIG ? | ALPHA EFF CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| 4.1 | 1 | 5 | 0.7 | 3 | 3 | 8 | 36 | 13 N | 0.1830 |
| 4.1 | 2 | 5 | 0.7 | 2 | 2 | 8 | 36 | 7 N | 0.1830 |
| 4.1 | 3 | 5 | 0.7 | 2 | 2 | 8 | 36 | 7 N | 0.1830 |
| 4.1 | 4 | 5 | 0.7 | 2 | 2 | 8 | 36 | 7 N | 0.1830 |
| 4.1 | 5 | 5 | 0.7 | 5 | 5 | 8 | 36 | 23 N | 0.1830 |
| 4.1 | 6 | 5 | 0.7 | 2 | 2 | 8 | 36 | 7 N | 0.1830 |
| 4.1 | 7 | 5 | 0.7 | 1 | 1 | 8 | 36 | 2 N | 0.1830 |
| 4.1 | 8 | 5 | 0.7 | 1 | 1 | 8 | 36 | 2 N | 0.1830 |
| 4.1 | 9 | 5 | 0.7 | 1 | 1 | 8 | 36 | 2 N | 0.1830 |
| 4.1 | 10 | 5 | 0.7 | 1 | 1 | 8 | 36 | 2 N | 0.1830 |
| 4.1 | 11 | 5 | 0.7 | 2 | 2 | 8 | 36 | 7 N | 0.1830 |
| 4.1 | 12 | 5 | 0.7 | 1 | 1 | 8 | 36 | 2 N | 0.1830 |
| 4.1 | 13 | 5 | 0.7 | 2 | 2 | 8 | 36 | 7 N | 0.1830 |
| 4.1 | 14 | 5 | 0.7 | 3 | 3 | 8 | 36 | 13 N | 0.1830 |
| 4.1 | 15 | 5 | 0.7 | 4 | 4 | 8 | 36 | 18 N | 0.1830 |
| 4.1 | 16 | 5 | 0.7 | 3 | 3 | 8 | 36 | 13 N | 0.1830 |
| 4.1 | 17 | 5 | 0.7 | 1 | 1 | 8 | 36 | 2 N | 0.1830 |
| 4.1 | 18 | 5 | 0.7 | 2 | 2 | 8 | 36 | 7 N | 0.1830 |
| 4.1 | 19 | 5 | 0.7 | 3 | 3 | 8 | 36 | 13 N | 0.1830 |
| 4.1 | 20 | 5 | 0.7 | 2 | 2 | 8 | 36 | 7 N | 0.1830 |
| 4.1 | 21 | 5 | 0.7 | 5 | 5 | 8 | 36 | 23 N | 0.1830 |
| 4.1 | 22 | 5 | 0.7 | 5 | 5 | 8 | 36 | 23 N | 0.1830 |
| 4.1 | 23 | 5 | 0.7 | 5 | 5 | 8 | 36 | 23 N | 0.1830 |
| 4.1 | 24 | 5 | 0.7 | 4 | 4 | 8 | 36 | 18 N | 0.1830 |
| 4.1 | 25 | 5 | 0.7 | 1 | 1 | 8 | 36 | 2 N | 0.1830 |
| 4.1 | 26 | 5 | 0.7 | 3 | 3 | 8 | 36 | 13 N | 0.1830 |
| 4.1 | 27 | 5 | 0.7 | 3 | 3 | 8 | 36 | 13 N | 0.1830 |
| 4.1 | 28 | 5 | 0.7 | 1 | 1 | 8 | 36 | 2 N | 0.1830 |
| 4.1 | 29 | 5 | 0.7 | 1 | 1 | 8 | 36 | 2 N | 0.1830 |
| 4.1 | 30 | 5 | 0.7 | 7 | 7 | 8 | 36 | 34 N | 0.1830 |

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TABLE 4.1-4

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:09 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 4.1 - REACTOR ROOF GRAVEL FOR SUM OF THE FRACTIONS

RADIATION TYPE: SOIL DATA FOR SUM OF THE FRACTIONS
COMPLETION
DATE: 10-10-94
TECHNICIANS: RW/TA/DT
LOCATION: 4.0
GRID ID: 4.1
MEDIA TYPE: SOIL
# of POINTS: 30

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 0.36 | PASS | 1 |
| AVG | 0.25 | PASS | 1 |
| STD X | 0.07 | | |
| MU SUB ALPHA | 0.27 | PASS | 1 |

| | | ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED) | | | | | | | | ISOTOPES OF C |
|---|---|---|---|---|---|---|---|---|---|---|
| ID # | GRID COORIDINATES OR OTHER ID | SR-90 | CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SOIL CODE | SR-90 |
| | | LIMIT 17 | LIMIT 0.9 | LIMIT 1.1 | LIMIT 1.8 | LIMIT 3.8 | LIMIT 63 | LIMIT 2 | | |
| 4.1 | 1 | < 0.199 | < 0.108 | < 0.060 | < 0.067 | 0.236 | < 0.264 | < 0.139 | 1 | < 0.011706 |
| 4.1 | 2 | < 0.199 | < 0.099 | < 0.103 | < 0.065 | 0.343 | < 0.468 | < 0.172 | 1 | < 0.011706 |
| 4.1 | 3 | < 0.184 | < 0.135 | < 0.050 | < 0.077 | 0.525 | < 0.427 | < 0.210 | 1 | < 0.010824 |
| 4.1 | 4 | < 0.199 | < 0.041 | < 0.062 | < 0.071 | < 0.102 | < 0.176 | < 0.101 | 1 | < 0.011706 |
| 4.1 | 5 | < 0.191 | < 0.037 | 0.107 | < 0.047 | 0.292 | < 0.276 | < 0.056 | 1 | < 0.011235 |
| 4.1 | 6 | < 0.181 | < 0.054 | < 0.042 | < 0.047 | < 0.084 | < 0.332 | < 0.070 | 1 | < 0.010647 |
| 4.1 | 7 | < 0.191 | < 0.084 | < 0.070 | < 0.061 | < 0.109 | < 0.145 | < 0.183 | 1 | < 0.011235 |
| 4.1 | 8 | < 0.184 | < 0.118 | < 0.048 | < 0.072 | 0.124 | < 0.323 | < 0.077 | 1 | < 0.010824 |
| 4.1 | 9 | < 0.184 | < 0.080 | < 0.021 | < 0.059 | 0.191 | < 0.392 | < 0.087 | 1 | < 0.010824 |
| 4.1 | 10 | < 0.184 | < 0.052 | < 0.073 | < 0.080 | < 0.104 | < 0.296 | < 0.144 | 1 | < 0.010824 |
| 4.1 | 11 | < 0.184 | < 0.047 | < 0.066 | < 0.060 | 0.263 | < 0.410 | < 0.249 | 1 | < 0.010824 |
| 4.1 | 12 | < 0.184 | < 0.032 | < 0.064 | < 0.072 | 0.249 | < 0.167 | < 0.219 | 1 | < 0.010824 |
| 4.1 | 13 | < 0.209 | < 0.041 | < 0.079 | < 0.072 | < 0.088 | < 0.438 | < 0.203 | 1 | < 0.012294 |
| 4.1 | 14 | < 0.209 | < 0.078 | < 0.028 | < 0.069 | 0.424 | < 0.420 | < 0.200 | 1 | < 0.012294 |
| 4.1 | 15 | < 0.203 | < 0.038 | < 0.045 | < 0.059 | 0.236 | < 0.288 | < 0.227 | 1 | < 0.011941 |
| 4.1 | 16 | < 0.203 | < 0.043 | < 0.028 | < 0.072 | 0.170 | < 0.390 | < 0.091 | 1 | < 0.011941 |
| 4.1 | 17 | < 0.304 | < 0.090 | < 0.045 | < 0.077 | 0.268 | 0.511 | < 0.226 | 1 | < 0.017882 |
| 4.1 | *18 | < * | < * | < * | < * | < * | < * | < * | 1 | < 0 |
| 4.1 | 19 | < 0.181 | < 0.037 | < 0.074 | < 0.056 | 0.361 | < 0.396 | < 0.179 | 1 | < 0.010647 |
| 4.1 | 20 | < 0.191 | < 0.083 | < 0.030 | < 0.061 | 0.277 | < 0.460 | < 0.254 | 1 | < 0.011235 |
| 4.1 | 21 | < 0.191 | < 0.044 | < 0.022 | < 0.066 | 0.112 | < 0.146 | < 0.087 | 1 | < 0.011235 |
| 4.1 | 22 | < 0.181 | < 0.106 | < 0.075 | < 0.066 | 0.262 | < 0.292 | < 0.079 | 1 | < 0.010647 |
| 4.1 | 23 | < 0.181 | < 0.048 | < 0.063 | 0.050 | < 0.144 | < 0.333 | < 0.211 | 1 | < 0.010647 |
| 4.1 | 24 | < 0.203 | < 0.077 | < 0.039 | < 0.064 | 0.306 | < 0.281 | < 0.056 | 1 | < 0.011941 |
| 4.1 | 25 | < 0.203 | < 0.054 | < 0.040 | < 0.068 | 0.205 | < 0.335 | < 0.197 | 1 | < 0.011941 |
| 4.1 | 26 | < 0.203 | < 0.071 | < 0.067 | < 0.079 | 0.558 | < 0.172 | < 0.242 | 1 | < 0.011941 |
| 4.1 | 27 | < 0.203 | < 0.010 | < 0.029 | < 0.069 | 0.487 | < 0.428 | < 0.190 | 1 | < 0.011941 |
| 4.1 | 28 | < 0.198 | < 0.077 | < 0.060 | < 0.059 | 0.656 | < 0.409 | < 0.174 | 1 | < 0.011647 |
| 4.1 | 29 | < 0.17 | < 0.070 | < 0.043 | < 0.062 | 1.040 | < 0.407 | < 0.142 | 1 | < 0.010588 |
| 4.1 | 30 | < 0.18 | < 0.067 | < 0.027 | < 0.070 | 0.469 | < 0.433 | < 0.157 | 1 | < 0.010588 |

* = SAMPLE MISSING

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ONCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| -60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| 0.120 < | 0.054 < | 0.037 | 0.000 < | 0.004 < | 0.070 | 0.297 |
| 0.110 < | 0.094 < | 0.036 | 0.000 < | 0.007 < | 0.086 | 0.344 |
| 0.150 < | 0.046 < | 0.043 | 0.000 < | 0.007 < | 0.105 | 0.361 |
| 0.046 < | 0.056 < | 0.040 < | 0.000 < | 0.003 < | 0.051 | 0.207 |
| 0.041 | 0.097 < | 0.026 | 0.000 < | 0.004 < | 0.029 | 0.209 |
| 0.060 < | 0.038 < | 0.026 < | 0.000 < | 0.005 < | 0.035 | 0.175 |
| 0.093 < | 0.063 < | 0.034 < | 0.000 < | 0.002 < | 0.092 | 0.295 |
| 0.131 < | 0.044 < | 0.040 | 0.000 < | 0.005 < | 0.039 | 0.269 |
| 0.089 < | 0.019 < | 0.033 | 0.000 < | 0.006 < | 0.044 | 0.202 |
| 0.058 < | 0.066 < | 0.044 < | 0.000 < | 0.005 < | 0.072 | 0.256 |
| 0.052 < | 0.060 < | 0.033 | 0.000 < | 0.007 < | 0.125 | 0.287 |
| 0.035 < | 0.058 < | 0.040 | 0.000 < | 0.003 < | 0.110 | 0.256 |
| 0.046 < | 0.072 < | 0.040 < | 0.000 < | 0.007 < | 0.102 | 0.279 |
| 0.087 < | 0.025 < | 0.038 | 0.000 < | 0.007 < | 0.100 | 0.269 |
| 0.043 < | 0.041 < | 0.033 | 0.000 < | 0.005 < | 0.114 | 0.246 |
| 0.048 < | 0.025 < | 0.040 | 0.000 < | 0.006 < | 0.045 | 0.177 |
| 0.100 < | 0.041 < | 0.043 | 0.000 | 0.008 < | 0.113 | 0.322 |
| 0.000 < | 0.000 < | 0.000 < | 0.000 < | 0.000 < | 0.000 | 0.000 |
| 0.041 < | 0.067 < | 0.031 | 0.000 < | 0.006 < | 0.090 | 0.245 |
| 0.092 < | 0.027 < | 0.034 | 0.000 < | 0.007 < | 0.127 | 0.299 |
| 0.049 < | 0.020 < | 0.037 | 0.000 < | 0.002 < | 0.044 | 0.163 |
| 0.118 < | 0.068 < | 0.037 | 0.000 < | 0.005 < | 0.040 | 0.277 |
| 0.053 < | 0.057 | 0.028 | 0.000 < | 0.005 < | 0.106 | 0.260 |
| 0.086 < | 0.035 < | 0.036 | 0.000 < | 0.004 < | 0.028 | 0.200 |
| 0.060 < | 0.036 < | 0.038 | 0.000 < | 0.005 < | 0.099 | 0.250 |
| 0.079 < | 0.061 < | 0.044 | 0.000 < | 0.003 < | 0.121 | 0.319 |
| 0.011 < | 0.026 < | 0.038 | 0.000 < | 0.007 < | 0.095 | 0.189 |
| 0.086 < | 0.055 < | 0.033 | 0.000 < | 0.006 < | 0.087 | 0.279 |
| 0.077 < | 0.039 < | 0.034 | 0.000 < | 0.006 < | 0.071 | 0.239 |
| 0.075 < | 0.024 < | 0.039 | 0.000 < | 0.007 < | 0.079 | 0.234 |

TABLE 4.2-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:31 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
REACTOR BUILDING ROOF - AREA 4.2 RUBBER MEMBRANE FOR BETA

RADIATION TYPE: 1 (1=BETA, 2=ALPHA)
COMPLETION DATE: 10-11-94
TECHNICIANS: PS/TA/CD
LOCATION: 4.0
GRID ID: 4.2
MEDIA TYPE: MEMBRANE
# of POINTS: 30
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | | LIMIT | |
|---|---|---|---|---|
| MAX | 2269 | PASS | 40500 | |
| AVG | 866 | PASS | 13500 | BETA SCALING FACTOR = 0.3 |
| STD X | 587 | | | |
| MU SUB ALPHA | 1048 | PASS | 13500 | |

| ID # | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | BETA FIXED GCPM | MATER-IAL CODE | MDA DPM/ 100 CM^2 | BETA FIXED DPM/ 100 CM^2 | STAT SIG ? | BETA EFF. CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| 4.2 | 1 | 429.2 | 422 | 422 | 8 | 1876 | -136 | N | 0.176 |
| 4.2 | 2 | 429.2 | 475 | 475 | 8 | 1876 | 867 | N | 0.176 |
| 4.2 | 3 | 429.2 | 424 | 424 | 8 | 1876 | -98 | N | 0.176 |
| 4.2 | 4 | 429.2 | 467 | 467 | 8 | 1876 | 716 | N | 0.176 |
| 4.2 | 5 | 429.2 | 439 | 439 | 8 | 1876 | 186 | N | 0.176 |
| 4.2 | 6 | 429.2 | 480 | 480 | 8 | 1876 | 962 | N | 0.176 |
| 4.2 | 7 | 429.2 | 449 | 449 | 8 | 1876 | 375 | N | 0.176 |
| 4.2 | 8 | 429.2 | 438 | 438 | 8 | 1876 | 167 | N | 0.176 |
| 4.2 | 9 | 429.2 | 468 | 468 | 8 | 1876 | 735 | N | 0.176 |
| 4.2 | 10 | 429.2 | 465 | 465 | 8 | 1876 | 678 | N | 0.176 |
| 4.2 | 11 | 429.2 | 468 | 468 | 8 | 1876 | 735 | N | 0.176 |
| 4.2 | 12 | 429.2 | 468 | 468 | 8 | 1876 | 735 | N | 0.176 |
| 4.2 | 13 | 429.2 | 467 | 467 | 8 | 1876 | 716 | N | 0.176 |
| 4.2 | 14 | 429.2 | 434 | 434 | 8 | 1876 | 91 | N | 0.176 |
| 4.2 | 15 | 429.2 | 454 | 454 | 8 | 1876 | 470 | N | 0.176 |
| 4.2 | 16 | 429.2 | 488 | 488 | 8 | 1876 | 1114 | N | 0.176 |
| 4.2 | 17 | 429.2 | 530 | 530 | 8 | 1876 | 1909 | Y | 0.176 |
| 4.2 | 18 | 429.2 | 480 | 480 | 8 | 1876 | 962 | N | 0.176 |
| 4.2 | 19 | 429.2 | 471 | 471 | 8 | 1876 | 792 | N | 0.176 |
| 4.2 | 20 | 429.2 | 457 | 457 | 8 | 1876 | 527 | N | 0.176 |
| 4.2 | 21 | 429.2 | 549 | 549 | 8 | 1876 | 2269 | Y | 0.176 |
| 4.2 | 22 | 429.2 | 486 | 486 | 8 | 1876 | 1076 | N | 0.176 |
| 4.2 | 23 | 429.2 | 540 | 540 | 8 | 1876 | 2098 | Y | 0.176 |
| 4.2 | 24 | 429.2 | 471 | 471 | 8 | 1876 | 792 | N | 0.176 |
| 4.2 | 25 | 429.2 | 484 | 484 | 8 | 1876 | 1038 | N | 0.176 |
| 4.2 | 26 | 429.2 | 519 | 519 | 8 | 1876 | 1701 | N | 0.176 |
| 4.2 | 27 | 429.2 | 498 | 498 | 8 | 1876 | 1303 | N | 0.176 |
| 4.2 | 28 | 429.2 | 481 | 481 | 8 | 1876 | 981 | N | 0.176 |
| 4.2 | 29 | 429.2 | 500 | 500 | 8 | 1876 | 1341 | N | 0.176 |
| 4.2 | 30 | 429.2 | 475 | 475 | 8 | 1876 | 867 | N | 0.176 |

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TABLE 4.2-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:30 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
REACTOR BUILDING ROOF - AREA 4.2 RUBBER MEMBRANE FOR ALPHA

RADIATION TYPE: 2 (1=BETA, 2=ALPHA)
COMPLETION DATE: 10-11-94
TECHNICIANS: PS/TA/CD
LOCATION: 4.0
GRID ID: 4.2
MEDIA TYPE: MEMBRANE
# of POINTS: 30
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | LIMIT |
|---|---|---|
| MAX | 45 PASS | 15000 |
| AVG | 11 PASS | 5000 |
| STD X | 11 | |
| MU SUB ALPHA | 14 PASS | 5000 |

| ID # | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | ALPHA FIXED GCPM | MATER-IAL CODE | MDA DPM/ 100 CM^2 | ALPHA FIXED DPM/ 100 CM^2 | STAT SIG ? | ALPHA EFF CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| 4.2 | 1 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.2 | 2 | 0.5 | 0 | 0 | 8 | 32 | -3 | N | 0.1896 |
| 4.2 | 3 | 0.5 | 3 | 3 | 8 | 32 | 13 | N | 0.1896 |
| 4.2 | 4 | 0.5 | 4 | 4 | 8 | 32 | 18 | N | 0.1896 |
| 4.2 | 5 | 0.5 | 3 | 3 | 8 | 32 | 13 | N | 0.1896 |
| 4.2 | 6 | 0.5 | 3 | 3 | 8 | 32 | 13 | N | 0.1896 |
| 4.2 | 7 | 0.5 | 3 | 3 | 8 | 32 | 13 | N | 0.1896 |
| 4.2 | 8 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.2 | 9 | 0.5 | 3 | 3 | 8 | 32 | 13 | N | 0.1896 |
| 4.2 | 10 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.2 | 11 | 0.5 | 2 | 2 | 8 | 32 | 8 | N | 0.1896 |
| 4.2 | 12 | 0.5 | 3 | 3 | 8 | 32 | 13 | N | 0.1896 |
| 4.2 | 13 | 0.5 | 2 | 2 | 8 | 32 | 8 | N | 0.1896 |
| 4.2 | 14 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.2 | 15 | 0.5 | 2 | 2 | 8 | 32 | 8 | N | 0.1896 |
| 4.2 | 16 | 0.5 | 3 | 3 | 8 | 32 | 13 | N | 0.1896 |
| 4.2 | 17 | 0.5 | 4 | 4 | 8 | 32 | 18 | N | 0.1896 |
| 4.2 | 18 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.2 | 19 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.2 | 20 | 0.5 | 3 | 3 | 8 | 32 | 13 | N | 0.1896 |
| 4.2 | 21 | 0.5 | 6 | 6 | 8 | 32 | 29 | N | 0.1896 |
| 4.2 | 22 | 0.5 | 2 | 2 | 8 | 32 | 8 | N | 0.1896 |
| 4.2 | 23 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.2 | 24 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.2 | 25 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.2 | 26 | 0.5 | 9 | 9 | 8 | 32 | 45 | Y | 0.1896 |
| 4.2 | 27 | 0.5 | 8 | 8 | 8 | 32 | 40 | Y | 0.1896 |
| 4.2 | 28 | 0.5 | 2 | 2 | 8 | 32 | 8 | N | 0.1896 |
| 4.2 | 29 | 0.5 | 0 | 0 | 8 | 32 | -3 | N | 0.1896 |
| 4.2 | 30 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |

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TABLE 4.3-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:32 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
REACTOR BUILDING ROOF - AREA 4.3 BENEATH MEMBRANE FOR BETA

RADIATION TYPE: 1 (1=BETA, 2=ALPHA)
COMPLETION
DATE: 10-11-94
TECHNICIANS: PS/TA/CD
LOCATION: 4.0
GRID ID: 4.3
MEDIA TYPE: MEMBRANE
# of POINTS: 30
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2
REM.+ FIXED:

| | | | LIMIT | |
|---|---|---|---|---|
| MAX | 2080 | PASS | 40500 | |
| AVG | 1003 | PASS | 13500 | BETA SCALING FACTOR = 0.3 |
| STD X | 495 | | | |
| MU SUB ALPHA | 1156 | PASS | 13500 | |

| ID # | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | BETA FIXED GCPM | MATER-IAL CODE | MDA DPM/ 100 CM^2 | BETA FIXED DPM/ 100 CM^2 | STAT SIG ? | BETA EFF. CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| 4.3 | 1 | 429.2 | 455 | 455 | 8 | 1876 | 430 | N | 0.176 |
| 4.3 | 2 | 429.2 | 537 | 537 | 8 | 1876 | 1797 | N | 0.176 |
| 4.3 | 3 | 429.2 | 449 | 449 | 8 | 1876 | 330 | N | 0.176 |
| 4.3 | 4 | 429.2 | 490 | 490 | 8 | 1876 | 1013 | N | 0.176 |
| 4.3 | 5 | 429.2 | 437 | 437 | 8 | 1876 | 130 | N | 0.176 |
| 4.3 | 6 | 429.2 | 462 | 462 | 8 | 1876 | 547 | N | 0.176 |
| 4.3 | 7 | 429.2 | 507 | 507 | 8 | 1876 | 1297 | N | 0.176 |
| 4.3 | 8 | 429.2 | 479 | 479 | 8 | 1876 | 830 | N | 0.176 |
| 4.3 | 9 | 429.2 | 496 | 496 | 8 | 1876 | 1113 | N | 0.176 |
| 4.3 | 10 | 429.2 | 485 | 485 | 8 | 1876 | 930 | N | 0.176 |
| 4.3 | 11 | 429.2 | 478 | 478 | 8 | 1876 | 813 | N | 0.176 |
| 4.3 | 12 | 429.2 | 523 | 523 | 8 | 1876 | 1563 | N | 0.176 |
| 4.3 | 13 | 429.2 | 497 | 497 | 8 | 1876 | 1130 | N | 0.176 |
| 4.3 | 14 | 429.2 | 524 | 524 | 8 | 1876 | 1580 | N | 0.176 |
| 4.3 | 15 | 429.2 | 492 | 492 | 8 | 1876 | 1047 | N | 0.176 |
| 4.3 | 16 | 429.2 | 476 | 476 | 8 | 1876 | 780 | N | 0.176 |
| 4.3 | 17 | 429.2 | 469 | 469 | 8 | 1876 | 663 | N | 0.176 |
| 4.3 | 18 | 429.2 | 546 | 546 | 8 | 1876 | 1947 | Y | 0.176 |
| 4.3 | 19 | 429.2 | 483 | 483 | 8 | 1876 | 897 | N | 0.176 |
| 4.3 | 20 | 429.2 | 554 | 554 | 8 | 1876 | 2080 | Y | 0.176 |
| 4.3 | 21 | 429.2 | 472 | 472 | 8 | 1876 | 713 | N | 0.176 |
| 4.3 | 22 | 429.2 | 491 | 491 | 8 | 1876 | 1030 | N | 0.176 |
| 4.3 | 23 | 429.2 | 451 | 451 | 8 | 1876 | 363 | N | 0.176 |
| 4.3 | 24 | 429.2 | 517 | 517 | 8 | 1876 | 1463 | N | 0.176 |
| 4.3 | 25 | 429.2 | 480 | 480 | 8 | 1876 | 847 | N | 0.176 |
| 4.3 | 26 | 429.2 | 517 | 517 | 8 | 1876 | 1463 | N | 0.176 |
| 4.3 | 27 | 429.2 | 476 | 476 | 8 | 1876 | 780 | N | 0.176 |
| 4.3 | 28 | 429.2 | 485 | 485 | 8 | 1876 | 930 | N | 0.176 |
| 4.3 | 29 | 429.2 | 444 | 444 | 8 | 1876 | 247 | N | 0.176 |
| 4.3 | 30 | 429.2 | 509 | 509 | 8 | 1876 | 1330 | N | 0.176 |

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TABLE 4.3-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:32 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
REACTOR BUILDING ROOF - AREA 4.3 BENEATH MEMBRANE FOR ALPHA

RADIATION TYPE: 2 (1=BETA, 2=ALPHA)
COMPLETION DATE: 10-11-94
TECHNICIANS: PS/TA/CD
LOCATION: 4.0
GRID ID: 4.3
MEDIA TYPE: MEMBRANE
# of POINTS: 30
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | LIMIT |
|---|---|---|
| MAX | 13 PASS | 15000 |
| AVG | 3 PASS | 5000 |
| STD X | 5 | |
| MU SUB ALPHA | 4 PASS | 5000 |

| ID # | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | ALPHA FIXED GCPM | MATER-IAL CODE | MDA DPM/ 100 CM^2 | ALPHA FIXED DPM/ 100 CM^2 | STAT SIG ? | ALPHA EFF CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| 4.3 | 1 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.3 | 2 | 0.5 | 0 | 0 | 8 | 32 | -3 | N | 0.1896 |
| 4.3 | 3 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.3 | 4 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.3 | 5 | 0.5 | 0 | 0 | 8 | 32 | -3 | N | 0.1896 |
| 4.3 | 6 | 0.5 | 0 | 0 | 8 | 32 | -3 | N | 0.1896 |
| 4.3 | 7 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.3 | 8 | 0.5 | 0 | 0 | 8 | 32 | -3 | N | 0.1896 |
| 4.3 | 9 | 0.5 | 0 | 0 | 8 | 32 | -3 | N | 0.1896 |
| 4.3 | 10 | 0.5 | 3 | 3 | 8 | 32 | 13 | N | 0.1896 |
| 4.3 | 11 | 0.5 | 0 | 0 | 8 | 32 | -3 | N | 0.1896 |
| 4.3 | 12 | 0.5 | 3 | 3 | 8 | 32 | 13 | N | 0.1896 |
| 4.3 | 13 | 0.5 | 0 | 0 | 8 | 32 | -3 | N | 0.1896 |
| 4.3 | 14 | 0.5 | 3 | 3 | 8 | 32 | 13 | N | 0.1896 |
| 4.3 | 15 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.3 | 16 | 0.5 | 0 | 0 | 8 | 32 | -3 | N | 0.1896 |
| 4.3 | 17 | 0.5 | 0 | 0 | 8 | 32 | -3 | N | 0.1896 |
| 4.3 | 18 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.3 | 19 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.3 | 20 | 0.5 | 2 | 2 | 8 | 32 | 8 | N | 0.1896 |
| 4.3 | 21 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.3 | 22 | 0.5 | 2 | 2 | 8 | 32 | 8 | N | 0.1896 |
| 4.3 | 23 | 0.5 | 3 | 3 | 8 | 32 | 13 | N | 0.1896 |
| 4.3 | 24 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.3 | 25 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.3 | 26 | 0.5 | 0 | 0 | 8 | 32 | -3 | N | 0.1896 |
| 4.3 | 27 | 0.5 | 2 | 2 | 8 | 32 | 8 | N | 0.1896 |
| 4.3 | 28 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.3 | 29 | 0.5 | 1 | 1 | 8 | 32 | 3 | N | 0.1896 |
| 4.3 | 30 | 0.5 | 0 | 0 | 8 | 32 | -3 | N | 0.1896 |

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TABLE 4.3-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 09:30 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 4.3 - REACTOR ROOF UNDER RUBBER MEMBRANE FOR SUM OF THE FRACTIONS

RADIATION TYPE: DATA FOR SUM OF FRACTIONS
COMPLETION DATE: 10-28-94
TECHNICIANS: TA/CD/PS
LOCATION: 4.0
GRID ID: 4.3
MEDIA TYPE: SOIL/WOOD
# of POINTS: 3

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 0.29 | PASS | 1 |
| AVG | 0.20 | PASS | 1 |
| STD X | 0.07 | | |
| MU SUB ALPHA | 0.27 | PASS | 1 |

| | | | ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED) | | | | | | | | ISOTOPES OF C | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | GRID COORDINATES | | SR-90 | CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SOIL CODE | SR-90 | CO |
| ID # | OR OTHER ID | | LIMIT | LIMIT | LIMIT | LIMIT | LIMIT | LIMIT | LIMIT | | | |
| | | | 17 | 0.9 | 1.1 | 1.8 | 3.8 | 63 | 2 | | | |
| 4.3 | 25 | < | * | < 0.041 | < 0.019 | < 0.052 | < 0.082 | < 0.195 | < 0.136 | 1 | < | 0 < |
| 4.3 | 29 | < | * | < 0.035 | < 0.021 | < 0.061 | < 0.056 | < 0.216 | < 0.111 | 1 | < | 0 < |
| 4.3 | 30 | < | * | < 0.069 | < 0.038 | < 0.125 | < 0.131 | < 0.355 | < 0.201 | 1 | < | 0 < |

* = Sr-90 DATA NOT AVAILABLE

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NCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| 60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| 0.046 < | 0.017 < | 0.029 < | 0.000 < | 0.003 < | 0.068 | 0.163 |
| 0.039 < | 0.019 < | 0.034 | 0.000 < | 0.003 < | 0.056 | 0.151 |
| 0.076 < | 0.034 < | 0.069 < | 0.000 < | 0.006 < | 0.101 | 0.286 |

A.R.TABLE 5.1-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY, 1 OF 1 SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
ABOVE HUT ROOF ELEVATION - AREA 5.1 FOR MICROREM

RADIATION TYPE: GAMMA SURVEY IN UREM/HR
COMPLETION DATE: 10/31/94
TECHNICIANS: PS/TA/CD
LOCATION: 5.0
GRID ID: 5.1
MEDIA TYPE: CONCRETE
# of POINTS: 91

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | | LIMIT |
|---|---|---|---|
| MAX | 12.00 | FAIL | 10 |
| AVG | 6.03 | FAIL | 5 |
| STD X | 2.57 | | |
| MU SUB ALPHA | 6.48 | FAIL | 5 |

| GRID COORDINATES ID # | LETTER | # | LIST. ID # | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|---|---|
| 5.1 | A | 4 | A | 6 | 15 | 8 | 9 |
| 5.1 | A | 5 | A | 6 | 13 | 8 | 7 |
| 5.1 | A | 6 | A | 6 | 14 | 8 | 8 |
| 5.1 | A | 7 | A | 6 | 8 | 8 | 2 |
| 5.1 | A | 8 | A | 6 | 13 | 8 | 7 |
| 5.1 | B | [illegible] | A | 6 | 13 | 8 | 7 |
| 5.1 | B | [illegible] | A | 6 | 14 | 8 | 8 |
| 5.1 | B | 6 | A | 6 | 14 | 8 | 8 |
| 5.1 | B | 7 | A | 6 | 8 | 8 | 2 |
| 5.1 | B | 8 | A | 6 | 12 | 8 | 6 |
| 5.1 | C | 4 | A | 6 | 15 | 8 | 9 |
| 5.1 | C | 5 | A | 6 | 18 | 8 | 12 |
| 5.1 | C | 6 | A | 6 | 14 | 8 | 8 |
| 5.1 | C | 7 | A | 6 | 10 | 8 | 4 |
| 5.1 | C | 8 | A | 6 | 12 | 8 | 6 |
| 5.1 | D | 4 | A | 6 | 15 | 8 | 9 |
| 5.1 | D | 5 | A | 6 | 14 | 8 | 8 |
| 5.1 | D | 6 | A | 6 | 15 | 8 | 9 |
| 5.1 | D | 7 | A | 6 | 10 | 8 | 4 |
| 5.1 | D | 8 | A | 6 | 14 | 8 | 8 |
| 5.1 | E | 4 | A | 6 | 14 | 8 | 8 |
| 5.1 | E | 5 | A | 6 | 15 | 8 | 9 |
| 5.1 | E | 6 | A | 6 | 15 | 8 | 9 |
| 5.1 | E | 7 | A | 6 | 9 | 8 | 3 |
| 5.1 | E | 8 | A | 6 | 12 | 8 | 6 |
| 5.1 | F | 4 | A | 6 | 16 | 8 | 10 |
| 5.1 | F | 5 | A | 6 | 14 | 8 | 8 |
| 5.1 | F | 6 | A | 6 | 17 | 8 | 11 |
| 5.1 | F | 7 | A | 6 | 8 | 8 | 2 |
| 5.1 | F | 8 | A | 6 | 11 | 8 | 5 |
| 5.1 | G | 4 | A | 6 | 15 | 8 | 9 |
| 5.1 | G | 5 | A | 6 | 15 | 8 | 9 |

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TABLE 5.1-1

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 5.1 | G | 6 | A | 6 | 15 | B | 9 |
| 5.1 | G | 7 | A | 6 | 11 | B | 5 |
| 5.1 | G | 8 | A | 6 | 12 | B | 6 |
| 5.1 | H | 4 | A | 6 | 15 | B | 9 |
| 5.1 | H | 5 | A | 6 | 13 | B | 7 |
| 5.1 | H | 6 | A | 6 | 14 | B | 8 |
| 5.1 | H | 7 | A | 6 | 11 | B | 5 |
| 5.1 | H | 8 | A | 6 | 12 | B | 6 |
| 5.1 | I | 4 | A | 6 | 13 | B | 7 |
| 5.1 | I | 5 | A | 6 | 14 | B | 8 |
| 5.1 | I | 6 | A | 6 | 14 | B | 8 |
| 5.1 | I | 7 | A | 6 | 12 | B | 6 |
| 5.1 | I | 8 | A | 6 | 15 | B | 9 |
| 5.1 | J | 4 | A | 6 | 16 | B | 10 |
| 5.1 | J | 5 | A | 6 | 15 | B | 9 |
| 5.1 | J | 6 | A | 6 | 16 | B | 10 |
| 5.1 | J | 7 | A | 6 | 10 | B | 4 |
| 5.1 | J | 8 | A | 6 | 12 | B | 6 |
| 5.1 | K | 4 | A | 6 | 10 | B | 4 |
| 5.1 | K | 5 | A | 6 | 16 | B | 10 |
| 5.1 | K | 6 | A | 6 | 13 | B | 7 |
| 5.1 | K | 7 | A | 6 | 9 | B | 3 |
| 5.1 | K | 8 | A | 6 | 14 | B | 8 |
| 5.1 | L | 5 | A | 6 | 10 | B | 4 |
| 5.1 | L | 6 | A | 6 | 11 | B | 5 |
| 5.1 | L | 7 | A | 6 | 10 | B | 4 |
| 5.1 | L | 8 | A | 6 | 9 | B | 3 |
| 5.1 | M | 5 | A | | 11 | B | 5 |
| 5.1 | M | 6 | A | 6 | 8 | B | 2 |
| 5.1 | M | 7 | A | 6 | 12 | B | 6 |
| 5.1 | M | 8 | A | 6 | 9 | B | 3 |
| 5.1 | N | 5 | A | 6 | 10 | B | 4 |
| 5.1 | N | 6 | A | 6 | 12 | B | 6 |
| 5.1 | N | 7 | A | 6 | 11 | B | 5 |
| 5.1 | N | 8 | A | 6 | 11 | B | 5 |
| 5.1 | O | 5 | A | 6 | 13 | B | 7 |
| 5.1 | O | 6 | A | 6 | 11 | B | 5 |
| 5.1 | O | 7 | A | 6 | 9 | B | 3 |
| 5.1 | O | 8 | A | 6 | 12 | B | 6 |
| 5.1 | P | 5 | A | 6 | 10 | B | 4 |
| 5.1 | P | 6 | A | 6 | 12 | B | 6 |
| 5.1 | P | 7 | A | 6 | 8 | B | 2 |
| 5.1 | P | 8 | A | 6 | 10 | B | 4 |
| 5.1 | Q | 4 | A | 6 | 12 | B | 6 |
| 5.1 | Q | 5 | A | 6 | 14 | B | 8 |
| 5.1 | Q | 6 | A | 6 | 8 | B | 2 |
| 5.1 | Q | 7 | A | 6 | 14 | B | 8 |
| 5.1 | Q | 8 | A | 6 | 12 | B | 6 |
| 5.1 | R | 5 | A | 6 | 12 | B | 6 |
| 5.1 | R | 6 | A | 6 | 10 | B | 4 |
| 5.1 | R | 7 | A | 6 | 8 | B | 2 |
| 5.1 | R | 8 | A | 6 | 10 | B | 4 |
| 5.1 | S | 6 | A | 6 | 10 | B | 4 |
| 5.1 | S | 7 | A | 6 | 12 | B | 6 |
| 5.1 | S | 8 | A | 6 | 8 | B | 2 |
| 5.1 | T | 7 | A | 6 | 10 | B | 4 |
| 5.1 | T | 8 | A | 6 | 8 | B | 2 |
| 5.1 | U | 8 | A | 6 | 7 | B | 1 |
| 5.1 | V | 8 | A | 6 | 7 | B | 1 |

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RI TABLE 5.1-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:34 AM

FINAL SURVEY DATA SHEET

DATA FOR AFFECTED AREA DESCRIPTION:

ABOVE HUT ROOF ELEVATION - AREA 5.1 FOR BETA

RADIATION TYPE: 1 BETA SCALING FACTOR = 0.3

COMPLETION DATE: 10/31/94

TECHNICIANS: PS/TA/CD

LOCATION: 5.0

GRID ID: 5.1

MEDIA TYPE: CONCRETE

# of POINTS: 91 (>60)

CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | | LIMIT |
|---|---|---|---|
| MAX FOR IND GRID | 7599 | PASS | 13500 |
| AVG - SURVEY UNIT | 1960 | PASS | 13500 |
| STD X | 1685 | | |
| MU SUB ALPHA | 2254 | PASS | 13500 |
| MAX HOT SPOT | 8114 | PASS | 40500 |

WEIGHTED

| GRID ID # | COORDINATES LETTER | # | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | SCAN MAX BETA COUNTS | TOTAL CONT. AREA CM^2 | MATER-IAL CODE | MDA DPM/ 100 CM^2 | AVG. BETA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 CM^2 | MAX TEST | INST CPM/ |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.1 | A | 4 | 6 | 530.5 | 646 | 0 | 0 | 8 | 2009 | 2113 +/- 948 | NA | | | 0.1 |
| 5.1 | A | 5 | 6 | 530.5 | 557 | 0 | 0 | 8 | 2009 | 485 +/- 886 | NA | | | 0.1 |
| 5.1 | A | 6 | 6 | 530.5 | 591 | 0 | 0 | 8 | 2009 | 1107 +/- 910 | NA | | | 0.1 |
| 5.1 | A | 7 | 2 | 425.0 | 603 | 0 | 0 | 8 | 1804 | 3258 +/- 912 | NA | | | 0.1 |
| 5.1 | A | 8 | 6 | 456.4 | 619 | 0 | 0 | 8 | 1867 | 2975 +/- 924 | NA | | | 0.1 |
| 5.1 | B | 4 | 6 | 530.5 | 945 | 974 | 300 | 8 | 2009 | 7599 +/-1133 | | 8114 | | 0.1 |
| 5.1 | B | 5 | 6 | 530.5 | 559 | 0 | 0 | 8 | 2009 | 521 +/- 887 | NA | | | 0.1 |
| 5.1 | B | 6 | 6 | 530.5 | 554 | 0 | 0 | 8 | 2009 | 430 +/- 883 | NA | | | 0.1 |
| 5.1 | B | 7 | 2 | 425.0 | 604 | 0 | 0 | 8 | 1804 | 3277 +/- 912 | NA | | | 0.1 |
| 5.1 | B | 8 | 6 | 456.4 | 635 | 0 | 0 | 8 | 1867 | 3267 +/- 936 | NA | | | 0.1 |
| 5.1 | C | 4 | 6 | 530.5 | 745 | 0 | 0 | 8 | 2009 | 3924 +/-1013 | NA | | | 0.1 |
| 5.1 | C | 5 | 6 | 530.5 | 503 | 0 | 0 | 8 | 2009 | -503 +/- 846 | NA | | | 0.1 |
| 5.1 | C | 6 | 6 | 530.5 | 614 | 0 | 0 | 8 | 2009 | 1528 +/- 926 | NA | | | 0.1 |
| 5.1 | C | 7 | 2 | 425.0 | 613 | 0 | 0 | 8 | 1804 | 3441 +/- 919 | NA | | | 0.1 |
| 5.1 | C | 8 | 6 | 456.4 | 608 | 0 | 0 | 8 | 1867 | 2774 +/- 917 | NA | | | 0.1 |
| 5.1 | D | 4 | 6 | 530.5 | 756 | 0 | 0 | 8 | 2009 | 4126 +/-1020 | NA | | | 0.1 |
| 5.1 | D | 5 | 6 | 530.5 | 533 | 0 | 0 | 8 | 2009 | 46 +/- 868 | NA | | | 0.1 |
| 5.1 | D | 6 | 6 | 530.5 | 603 | 0 | 0 | 8 | 2009 | 1326 +/- 918 | NA | | | 0.1 |
| 5.1 | D | 7 | 2 | 425.0 | 638 | 0 | 0 | 8 | 1804 | 3899 +/- 936 | NA | | | 0.1 |
| 5.1 | D | 8 | 6 | 456.4 | 574 | 0 | 0 | 8 | 1867 | 2151 +/- 893 | NA | | | 0.1 |
| 5.1 | E | 4 | 6 | 530.5 | 785 | 0 | 0 | 8 | 2009 | 4656 +/-1038 | NA | | | 0.1 |
| 5.1 | E | 5 | 6 | 530.5 | 554 | 0 | 0 | 8 | 2009 | 430 +/- 883 | NA | | | 0.1 |
| 5.1 | E | 6 | 6 | 530.5 | 547 | 0 | 0 | 8 | 2009 | 302 +/- 878 | NA | | | 0.1 |
| 5.1 | E | 7 | 2 | 425.0 | 565 | 0 | 0 | 8 | 1804 | 2563 +/- 884 | NA | | | 0.1 |
| 5.1 | E | 8 | 6 | 456.4 | 620 | 0 | 0 | 8 | 1867 | 2993 +/- 925 | NA | | | 0.1 |
| 5.1 | F | 4 | 6 | 530.5 | 705 | 0 | 0 | 8 | 2009 | 3192 +/- 987 | NA | | | 0.1 |
| 5.1 | F | 5 | 6 | 530.5 | 583 | 0 | 0 | 8 | 2009 | 960 +/- 904 | NA | | | 0.1 |

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GPM

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TABLE 5.1-2

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.1 | F | 6 | 6 | 530.5 | 505 | 0 | 0 | 8 | 2009 | -467 +/- 847 | NA | 0.1 |
| 5.1 | F | 7 | 2 | 425.0 | 581 | 0 | 0 | 8 | 1804 | 2856 +/- 896 | NA | 0.1 |
| 5.1 | F | 8 | 6 | 456.4 | 630 | 0 | 0 | 8 | 1867 | 3176 +/- 932 | NA | 0.1 |
| 5.1 | G | 4 | 6 | 530.5 | 777 | 0 | 0 | 8 | 2009 | 4510 +/-1033 | NA | 0.1 |
| 5.1 | G | 5 | 6 | 530.5 | 594 | 0 | 0 | 8 | 2009 | 1162 +/- 912 | NA | 0.1 |
| 5.1 | G | 6 | 6 | 530.5 | 588 | 0 | 0 | 8 | 2009 | 1052 +/- 908 | NA | 0.1 |
| 5.1 | G | 7 | 2 | 425.0 | 655 | 0 | 0 | 8 | 1804 | 4210 +/- 948 | NA | 0.1 |
| 5.1 | G | 8 | 6 | 456.4 | 633 | 0 | 0 | 8 | 1867 | 3231 +/- 934 | NA | 0.1 |
| 5.1 | H | 4 | 6 | 530.5 | 804 | 0 | 0 | 8 | 2009 | 5004 +/-1050 | NA | 0.1 |
| 5.1 | H | 5 | 6 | 530.5 | 584 | 0 | 0 | 8 | 2009 | 979 +/- 905 | NA | 0.1 |
| 5.1 | H | 4 | 6 | 530.5 | 573 | 0 | 0 | 8 | 2009 | 778 +/- 897 | NA | 0.1 |
| 5.1 | H | 7 | 2 | 425.0 | 660 | 0 | 0 | 8 | 1804 | 4302 +/- 951 | NA | 0.1 |
| 5.1 | H | 8 | 6 | 456.4 | 600 | 0 | 0 | 8 | 1867 | 2627 +/- 911 | NA | 0.1 |
| 5.1 | I | 4 | 6 | 530.5 | 747 | 0 | 0 | 8 | 2009 | 3961 +/-1014 | NA | 0.1 |
| 5.1 | I | 5 | 6 | 530.5 | 558 | 0 | 0 | 8 | 2009 | 503 +/- 886 | NA | 0.1 |
| 5.1 | I | 6 | 6 | 530.5 | 629 | 0 | 0 | 8 | 2009 | 1802 +/- 936 | NA | 0.1 |
| 5.1 | I | 7 | 2 | 425.0 | 654 | 0 | 0 | 8 | 1804 | 4192 +/- 947 | NA | 0.1 |
| 5.1 | I | 8 | 6 | 456.4 | 607 | 0 | 0 | 8 | 1867 | 2755 +/- 916 | NA | 0.1 |
| 5.1 | J | 4 | 6 | 530.5 | 761 | 0 | 0 | 8 | 2009 | 4217 +/-1023 | NA | 0.1 |
| 5.1 | J | 5 | 6 | 530.5 | 571 | 0 | 0 | 8 | 2009 | 741 +/- 896 | NA | 0.1 |
| 5.1 | J | 6 | 6 | 530.5 | 633 | 0 | 0 | 8 | 2009 | 1875 +/- 939 | NA | 0.1 |
| 5.1 | J | 7 | 2 | 425.0 | 632 | 0 | 0 | 8 | 1804 | 3789 +/- 932 | NA | 0.1 |
| 5.1 | J | 8 | 6 | 456.4 | 647 | 0 | 0 | 8 | 1867 | 3487 +/- 944 | NA | 0.1 |
| 5.1 | K | 4 | 6 | 530.5 | 832 | 0 | 0 | 8 | 2009 | 5516 +/-1067 | NA | 0.1 |
| 5.1 | K | 5 | 6 | 530.5 | 518 | 0 | 0 | 8 | 2009 | -229 +/- 857 | NA | 0.1 |
| 5.1 | K | 6 | 6 | 530.5 | 558 | 0 | 0 | 8 | 2009 | 503 +/- 886 | NA | 0.1 |
| 5.1 | K | 7 | 2 | 425.0 | 567 | 0 | 0 | 8 | 1804 | 2599 +/- 886 | NA | 0.1 |
| 5.1 | K | 8 | 6 | 456.4 | 615 | 0 | 0 | 8 | 1867 | 2902 +/- 922 | NA | 0.1 |
| 5.1 | L | 5 | 2 | 421.5 | 552 | 0 | 0 | 8 | 1797 | 2389 +/- 875 | NA | 0.1 |
| 5.1 | L | 6 | 2 | 421.5 | 527 | 0 | 0 | 8 | 1797 | 1931 +/- 856 | NA | 0.1 |
| 5.1 | L | 7 | 2 | 421.5 | 457 | 0 | 0 | 8 | 1797 | 650 +/- 802 | NA | 0.1 |
| 5.1 | L | 8 | 2 | 421.5 | 543 | 0 | 0 | 8 | 1797 | 2224 +/- 868 | NA | 0.1 |
| 5.1 | M | 5 | 2 | 592.7 | 613 | 0 | 0 | 8 | 2122 | 372 +/- 930 | NA | 0.1 |
| 5.1 | M | 6 | 2 | 592.7 | 576 | 0 | 0 | 8 | 2122 | -306 +/- 904 | NA | 0.1 |
| 5.1 | M | 7 | 2 | 592.7 | 571 | 0 | 0 | 8 | 2122 | -397 +/- 901 | NA | 0.1 |
| 5.1 | M | 8 | 2 | 592.7 | 690 | 0 | 0 | 8 | 2122 | 1781 +/- 982 | NA | 0.1 |
| 5.1 | N | 5 | 2 | 592.7 | 637 | 0 | 0 | 8 | 2122 | 811 +/- 947 | NA | 0.1 |
| 5.1 | N | 6 | 2 | 592.7 | 544 | 0 | 0 | 8 | 2122 | -891 +/- 881 | NA | 0.1 |
| 5.1 | N | 7 | 2 | 592.7 | 630 | 0 | 0 | 8 | 2122 | 683 +/- 942 | NA | 0.1 |
| 5.1 | N | 8 | 2 | 592.7 | 595 | 0 | 0 | 8 | 2122 | 42 +/- 918 | NA | 0.1 |
| 5.1 | O | 5 | 2 | 592.7 | 566 | 0 | 0 | 8 | 2122 | -489 +/- 897 | NA | 0.1 |
| 5.1 | O | 6 | 2 | 592.7 | 633 | 0 | 0 | 8 | 2122 | 738 +/- 944 | NA | 0.1 |
| 5.1 | O | 7 | 2 | 592.7 | 571 | 0 | 0 | 8 | 2122 | -397 +/- 901 | NA | 0.1 |
| 5.1 | O | 8 | 6 | 643.3 | 556 | 0 | 0 | 8 | 2207 | -1597 +/- 893 | NA | 0.1 |
| 5.1 | P | 5 | 2 | 592.7 | 624 | 0 | 0 | 8 | 2122 | 573 +/- 938 | NA | 0.1 |
| 5.1 | P | 6 | 2 | 592.7 | 691 | 0 | 0 | 8 | 2122 | 1799 +/- 983 | NA | 0.1 |
| 5.1 | P | 7 | 2 | 592.7 | 624 | 0 | 0 | 8 | 2122 | 573 +/- 938 | NA | 0.1 |
| 5.1 | P | 8 | 6 | 643.3 | 575 | 0 | 0 | 8 | 2207 | -1250 +/- 907 | NA | 0.1 |
| 5.1 | Q | 4 | 6 | 495.0 | 671 | 0 | 0 | 8 | 1942 | 3220 +/- 963 | NA | 0.1 |
| 5.1 | Q | 5 | 6 | 495.0 | 737 | 0 | 0 | 8 | 1942 | 4427 +/-1006 | NA | 0.1 |
| 5.1 | Q | 6 | 6 | 495.0 | 588 | 0 | 0 | 8 | 1942 | 1701 +/- 905 | NA | 0.1 |
| 5.1 | Q | 7 | 6 | 495.0 | 646 | 0 | 0 | 8 | 1942 | 2763 +/- 946 | NA | 0.1 |
| 5.1 | Q | 8 | 6 | 495.0 | 596 | 0 | 0 | 8 | 1942 | 1848 +/- 911 | NA | 0.1 |
| 5.1 | R | 5 | 6 | 495.0 | 637 | 0 | 0 | 8 | 1942 | 2598 +/- 940 | NA | 0.1 |
| 5.1 | R | 6 | 6 | 495.0 | 584 | 0 | 0 | 8 | 1942 | 1628 +/- 903 | NA | 0.1 |
| 5.1 | R | 7 | 6 | 495.0 | 638 | 0 | 0 | 8 | 1942 | 2616 +/- 940 | NA | 0.1 |
| 5.1 | R | 8 | 6 | 495.0 | 581 | 0 | 0 | 8 | 1942 | 1575 +/- 900 | NA | 0.1 |
| 5.1 | S | 6 | 6 | 495.0 | 659 | 0 | 0 | 8 | 1942 | 3000 +/- 954 | NA | 0.1 |

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TABLE 5.1-2

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.1 | S | 7 | 6 | 495.0 | 595 | 0 | 0 | 8 | 1942 | 1829 +/- 910 | NA | 0.1 |
| 5.1 | S | 8 | 6 | 495.0 | 583 | 0 | 0 | 8 | 1942 | 1610 +/- 902 | NA | 0.1 |
| 5.1 | T | 7 | 6 | 495.0 | 586 | 0 | 0 | 8 | 1942 | 1665 +/- 904 | NA | 0.1 |
| 5.1 | T | 8 | 6 | 495.0 | 606 | 0 | 0 | 8 | 1942 | 2031 +/- 918 | NA | 0.1 |
| 5.1 | U | 8 | 6 | 495.0 | 554 | 0 | 0 | 8 | 1942 | 1079 +/- 881 | NA | 0.1 |
| 5.1 | V | 8 | 6 | 495.0 | 533 | 0 | 0 | 8 | 1942 | 695 +/- 865 | NA | 0.1 |

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TABLE 5.1-3

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:33 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
ABOVE HUT ROOF ELEVATION - AREA 5.1 FOR ALPHA

RADIATION TYPE: 2
COMPLETION
DATE: 10-31-94
TECHNICIANS: PS/TA/CD
LOCATION: 5.0
GRID ID: 5.1
MEDIA TYPE: CONCRETE
# of POINTS: 91 (>60)
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | LIMIT |
|---|---|---|
| MAX FOR IND GRID | 44 PASS | 5000 |
| AVG - SURVEY UNIT | 9 PASS | 5000 |
| STD X | 11 | |
| MU SUB ALPHA | 11 PASS | 5000 |
| MAX HOT SPOT | 12 PASS | 15000 |

| ID # | GRID COORDINATES LETTER | # | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | SCAN MAX ALPHA COUNTS | TOTAL CONT. AREA CM^2 | MATER-IAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. ALPHA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 CM^2 | MAX TEST | INST E CPM/D |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.1 | A | 4 | 6 | 1.8 | 3 | 0 | 0 | 8 | 50 | 7 +/- 19 | NA | | | 0.18 |
| 5.1 | A | 5 | 6 | 1.8 | 3 | 0 | 0 | 8 | 50 | 7 +/- 19 | NA | | | 0.18 |
| 5.1 | A | 6 | 6 | 1.8 | 2 | 0 | 0 | 8 | 50 | 1 +/- 16 | NA | | | 0.18 |
| 5.1 | A | 7 | 2 | 1.0 | 0 | 0 | 0 | 8 | 38 | -5 +/- 3 | NA | | | 0.19 |
| 5.1 | A | 8 | 6 | 2.5 | 4 | 0 | 0 | 8 | 56 | 8 +/- 22 | NA | | | 0.18 |
| 5.1 | B | 4 | 6 | 1.8 | 2 | 4 | 300 | 8 | 50 | 1 +/- 16 | | 12 | | 0.18 |
| 5.1 | B | 5 | 6 | 1.8 | 0 | 0 | 0 | 8 | 50 | -10 +/- 5 | NA | | | 0.18 |
| 5.1 | B | 6 | 6 | 1.8 | 2 | 0 | 0 | 8 | 50 | 1 +/- 16 | NA | | | 0.18 |
| 5.1 | B | 7 | 2 | 1.0 | 1 | 0 | 0 | 8 | 38 | 0 +/- 11 | NA | | | 0.19 |
| 5.1 | B | 8 | 6 | 2.5 | 1 | 0 | 0 | 8 | 56 | -8 +/- 12 | NA | | | 0.18 |
| 5.1 | C | 4 | 6 | 1.8 | 3 | 0 | 0 | 8 | 50 | 7 +/- 19 | NA | | | 0.18 |
| 5.1 | C | 5 | 6 | 1.8 | 3 | 0 | 0 | 8 | 50 | 7 +/- 19 | NA | | | 0.18 |
| 5.1 | C | 6 | 6 | 1.8 | 3 | 0 | 0 | 8 | 50 | 7 +/- 19 | NA | | | 0.18 |
| 5.1 | C | 7 | 2 | 1.0 | 1 | 0 | 0 | 8 | 38 | 0 +/- 11 | NA | | | 0.19 |
| 5.1 | C | 8 | 6 | 2.5 | 0 | 0 | 0 | 8 | 56 | -14 +/- 5 | NA | | | 0.18 |
| 5.1 | D | 4 | 6 | 1.8 | 3 | 0 | 0 | 8 | 50 | 7 +/- 19 | NA | | | 0.18 |
| 5.1 | D | 5 | 6 | 1.8 | 3 | 0 | 0 | 8 | 50 | 7 +/- 19 | NA | | | 0.18 |
| 5.1 | D | 6 | 6 | 1.8 | 1 | 0 | 0 | 8 | 50 | -4 +/- 12 | NA | | | 0.18 |
| 5.1 | D | 7 | 2 | 1.0 | 3 | 0 | 0 | 8 | 38 | 10 +/- 18 | NA | | | 0.19 |
| 5.1 | D | 8 | 2 | 2.5 | 2 | 0 | 0 | 8 | 56 | -2 +/- 16 | NA | | | 0.18 |
| 5.1 | E | 4 | 6 | 1.8 | 2 | 0 | 0 | 8 | 50 | 1 +/- 16 | NA | | | 0.18 |
| 5.1 | E | 5 | 6 | 1.8 | 2 | 0 | 0 | 8 | 50 | 1 +/- 16 | NA | | | 0.18 |
| 5.1 | E | 6 | 6 | 1.8 | 7 | 0 | 0 | 8 | 50 | 29 +/- 29 | NA | | | 0.18 |
| 5.1 | E | 7 | 2 | 1.0 | 1 | 0 | 0 | 8 | 38 | 0 +/- 11 | NA | | | 0.19 |
| 5.1 | E | 8 | 6 | 2.5 | 4 | 0 | 0 | 8 | 56 | 8 +/- 22 | NA | | | 0.18 |
| 5.1 | F | 4 | 6 | 1.8 | 2 | 0 | 0 | 8 | 50 | 1 +/- 16 | NA | | | 0.18 |
| 5.1 | F | 5 | 6 | 1.8 | 1 | 0 | 0 | 8 | 50 | -4 +/- 12 | NA | | | 0.18 |

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TABLE 5.1-3

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.1 | S | 7 | 6 | 0.9 | 2 | 0 | 0 | 8 | 39 | 6 +/- 16 | NA | 0.1 |
| 5.1 | S | 8 | 6 | 0.9 | 6 | 0 | 0 | 8 | 39 | 28 +/- 27 | NA | 0.1 |
| 5.1 | T | 7 | 6 | 0.9 | 2 | 0 | 0 | 8 | 39 | 6 +/- 16 | NA | 0.1 |
| 5.1 | T | 8 | 6 | 0.9 | 4 | 0 | 0 | 8 | 39 | 17 +/- 22 | NA | 0.1 |
| 5.1 | U | 8 | 6 | 0.9 | 3 | 0 | 0 | 8 | 39 | 12 +/- 19 | NA | 0.1 |
| 5.1 | V | 8 | 6 | 0.9 | 5 | 0 | 0 | 8 | 39 | 23 +/- 25 | NA | 0.1 |

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TABLE 5.1-3

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.1 | F | 6 | 6 | 1.8 | 2 | 0 | 0 | 8 | 50 | 1 +/- 16 | NA | 0.180 |
| 5.1 | F | 7 | 2 | 1.0 | 3 | 0 | 0 | 8 | 38 | 10 +/- 18 | NA | 0.195 |
| 5.1 | F | 8 | 6 | 2.5 | 1 | 0 | 0 | 8 | 56 | -8 +/- 12 | NA | 0.180 |
| 5.1 | G | 4 | 6 | 1.8 | 8 | 0 | 0 | 8 | 50 | 34 +/- 31 | NA | 0.180 |
| 5.1 | G | 5 | 6 | 1.8 | 4 | 0 | 0 | 8 | 50 | 12 +/- 22 | NA | 0.180 |
| 5.1 | G | 6 | 6 | 1.8 | 3 | 0 | 0 | 8 | 50 | 7 +/- 19 | NA | 0.180 |
| 5.1 | G | 7 | 2 | 1.0 | 6 | 0 | 0 | 8 | 38 | 26 +/- 25 | NA | 0.195 |
| 5.1 | G | 8 | 6 | 2.5 | 3 | 0 | 0 | 8 | 56 | 3 +/- 20 | NA | 0.180 |
| 5.1 | H | 4 | 6 | 1.8 | 5 | 0 | 0 | 8 | 50 | 18 +/- 25 | NA | 0.180 |
| 5.1 | H | 5 | 6 | 1.8 | 2 | 0 | 0 | 8 | 50 | 1 +/- 16 | NA | 0.180 |
| 5.1 | H | 6 | 6 | 1.8 | 3 | 0 | 0 | 8 | 50 | 7 +/- 19 | NA | 0.180 |
| 5.1 | H | 7 | 2 | 1.0 | 4 | 0 | 0 | 8 | 38 | 15 +/- 20 | NA | 0.195 |
| 5.1 | H | 8 | 6 | 2.5 | 4 | 0 | 0 | 8 | 56 | 8 +/- 22 | NA | 0.180 |
| 5.1 | I | 4 | 6 | 1.8 | 5 | 0 | 0 | 8 | 50 | 18 +/- 25 | NA | 0.180 |
| 5.1 | I | 5 | 6 | 1.8 | 5 | 0 | 0 | 8 | 50 | 18 +/- 25 | NA | 0.180 |
| 5.1 | I | 6 | 6 | 1.8 | 6 | 0 | 0 | 8 | 50 | 23 +/- 27 | NA | 0.180 |
| 5.1 | I | 7 | 2 | 1.0 | 4 | 0 | 0 | 8 | 38 | 15 +/- 20 | NA | 0.195 |
| 5.1 | I | 8 | 6 | 2.5 | 3 | 0 | 0 | 8 | 56 | 3 +/- 20 | NA | 0.180 |
| 5.1 | J | 4 | 6 | 1.8 | 2 | 0 | 0 | 8 | 50 | 1 +/- 16 | NA | 0.180 |
| 5.1 | J | 5 | 6 | 1.8 | 5 | 0 | 0 | 8 | 50 | 18 +/- 25 | NA | 0.180 |
| 5.1 | J | 6 | 6 | 1.8 | 4 | 0 | 0 | 8 | 50 | 12 +/- 22 | NA | 0.180 |
| 5.1 | J | 7 | 2 | 1.0 | 4 | 0 | 0 | 8 | 38 | 15 +/- 20 | NA | 0.195 |
| 5.1 | J | 8 | 6 | 2.5 | 4 | 0 | 0 | 8 | 56 | 8 +/- 22 | NA | 0.180 |
| 5.1 | K | 4 | 6 | 1.8 | 3 | 0 | 0 | 8 | 50 | 7 +/- 19 | NA | 0.180 |
| 5.1 | K | 5 | 6 | 1.8 | 4 | 0 | 0 | 8 | 50 | 12 +/- 22 | NA | 0.180 |
| 5.1 | K | 6 | 6 | 1.8 | 4 | 0 | 0 | 8 | 50 | 12 +/- 22 | NA | 0.180 |
| 5.1 | K | 7 | 2 | 1.0 | 1 | 0 | 0 | 8 | 38 | 0 +/- 11 | NA | 0.195 |
| 5.1 | K | 8 | 6 | 2.5 | 2 | 0 | 0 | 8 | 56 | -3 +/- 16 | NA | 0.180 |
| 5.1 | L | 5 | 2 | 1.1 | 3 | 0 | 0 | 8 | 39 | 10 +/- 18 | NA | 0.195 |
| 5.1 | L | 6 | 2 | 1.1 | 2 | 0 | 0 | 8 | 39 | 5 +/- 15 | NA | 0.195 |
| 5.1 | L | 7 | 2 | 1.1 | 1 | 0 | 0 | 8 | 39 | -1 +/- 11 | NA | 0.195 |
| 5.1 | L | 8 | 2 | 1.1 | 1 | 0 | 0 | 8 | 39 | -1 +/- 11 | NA | 0.195 |
| 5.1 | M | 5 | 2 | 1.4 | 2 | 0 | 0 | 8 | 42 | 3 +/- 15 | NA | 0.195 |
| 5.1 | M | 6 | 2 | 1.4 | 1 | 0 | 0 | 8 | 42 | -2 +/- 11 | NA | 0.195 |
| 5.1 | M | 7 | 2 | 1.4 | 2 | 0 | 0 | 8 | 42 | 3 +/- 15 | NA | 0.195 |
| 5.1 | M | 8 | 2 | 1.4 | 3 | 0 | 0 | 8 | 42 | 8 +/- 18 | NA | 0.195 |
| 5.1 | N | 5 | 2 | 1.4 | 1 | 0 | 0 | 8 | 42 | -2 +/- 11 | NA | 0.195 |
| 5.1 | N | 6 | 2 | 1.4 | 4 | 0 | 0 | 8 | 42 | 13 +/- 20 | NA | 0.195 |
| 5.1 | N | 7 | 2 | 1.4 | 3 | 0 | 0 | 8 | 42 | 8 +/- 18 | NA | 0.195 |
| 5.1 | N | 8 | 2 | 1.4 | 5 | 0 | 0 | 8 | 42 | 18 +/- 23 | NA | 0.195 |
| 5.1 | O | 5 | 2 | 1.4 | 3 | 0 | 0 | 8 | 42 | 8 +/- 18 | NA | 0.195 |
| 5.1 | O | 6 | 2 | 1.4 | 9 | 0 | 0 | 8 | 42 | 39 +/- 30 | NA | 0.195 |
| 5.1 | O | 7 | 2 | 1.4 | 2 | 0 | 0 | 8 | 42 | 3 +/- 15 | NA | 0.195 |
| 5.1 | O | 8 | 6 | 2.2 | 2 | 0 | 0 | 8 | 53 | -1 +/- 16 | NA | 0.185 |
| 5.1 | P | 5 | 2 | 1.4 | 2 | 0 | 0 | 8 | 42 | 3 +/- 15 | NA | 0.195 |
| 5.1 | P | 6 | 2 | 1.4 | 10 | 0 | 0 | 8 | 42 | 44 +/- 32 | NA | 0.195 |
| 5.1 | P | 7 | 2 | 1.4 | 2 | 0 | 0 | 8 | 42 | 3 +/- 15 | NA | 0.195 |
| 5.1 | P | 8 | 6 | 2.2 | 5 | 0 | 0 | 8 | 53 | 16 +/- 25 | NA | 0.185 |
| 5.1 | Q | 4 | 6 | 0.9 | 5 | 0 | 0 | 8 | 39 | 23 +/- 25 | NA | 0.185 |
| 5.1 | Q | 5 | 6 | 0.9 | 7 | 0 | 0 | 8 | 39 | 34 +/- 29 | NA | 0.185 |
| 5.1 | Q | 6 | 6 | 0.9 | 1 | 0 | 0 | 8 | 39 | 1 +/- 11 | NA | 0.185 |
| 5.1 | Q | 7 | 6 | 0.9 | 4 | 0 | 0 | 8 | 39 | 17 +/- 22 | NA | 0.185 |
| 5.1 | Q | 8 | 6 | 0.9 | 4 | 0 | 0 | 8 | 39 | 17 +/- 22 | NA | 0.185 |
| 5.1 | R | 5 | 6 | 0.9 | 5 | 0 | 0 | 8 | 39 | 23 +/- 25 | NA | 0.185 |
| 5.1 | R | 6 | 6 | 0.9 | 5 | 0 | 0 | 8 | 39 | 23 +/- 25 | NA | 0.185 |
| 5.1 | R | 7 | 6 | 0.9 | 2 | 0 | 0 | 8 | 39 | 6 +/- 16 | NA | 0.185 |
| 5.1 | R | 8 | 6 | 0.9 | 6 | 0 | 0 | 8 | 39 | 28 +/- 27 | NA | 0.185 |
| 5.1 | S | 6 | 6 | 0.9 | 3 | 0 | 0 | 8 | 39 | 12 +/- 19 | NA | 0.185 |

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TABLE 5.2-1

| | | | | | | |
|---|---|---|---|---|---|---|
| 5.2 G1 | INSIDE EAST | | 6 | 18 | 8 | 12 |
| 5.2 | G* | 3 | 6 | 13 | 8 | 7 |
| 5.2 | H | 1 | 6 | 13 | 8 | 7 |
| 5.2 | H* | 2 | 6 | 12 | 8 | 6 |
| 5.2 | H* | 3 | 6 | 12 | 8 | 6 |
| 5.2 H3 | INSIDE* | | 6 | 13 | 8 | 7 |
| 5.2 | I | 1 | 6 | 17 | 8 | 11 |
| 5.2 | I* | 2 | 6 | 15 | 8 | 9 |
| 5.2 I2 | INSIDE WEST | | 6 | 10 | 8 | 4 |
| 5.2 I2 | INSIDE EAST | | 6 | 13 | 8 | 7 |
| 5.2 I3 | INSIDE EAST | | 6 | 10 | 8 | 4 |
| 5.2 I3 | INSIDE WEST | | 6 | 12 | 8 | 6 |
| 5.2 | I* | 3 | 6 | 12 | 8 | 6 |
| 5.2 | J* | 1 | 6 | 11 | 8 | 5 |
| 5.2 | J* | 2 | 6 | 11 | 8 | 5 |
| 5.2 | J* | 3 | 6 | 14 | 8 | 8 |
| 5.2 | K* | 1 | 6 | 10 | 8 | 4 |
| 5.2 | K* | 2 | 6 | 8 | 8 | 2 |
| 5.2 | K | 3 | 6 | 19 | 8 | 13 |
| 5.2 | K | 4 | 6 | 16 | 8 | 10 |
| 5.2 | K | 5 | 6 | 16 | 8 | 10 |
| 5.2 | K | 6 | 6 | 14 | 8 | 8 |
| 5.2 | L | 1 | 6 | 18 | 8 | 12 |
| 5.2 | L | 2 | 6 | 13 | 8 | 7 |
| 5.2 | L | 3 | 6 | 12 | 8 | 6 |
| 5.2 | M | 1 | 6 | 19 | 8 | 13 |
| 5.2 | M | 2 | 6 | 19 | 8 | 13 |
| 5.2 | M | 3 | 6 | 18 | 8 | 12 |
| 5.2 | N | 1 | 6 | 22 | 8 | 16 |
| 5.2 | N | 2 | 6 | 20 | 8 | 14 |
| 5.2 | N | 3 | 6 | 19 | 8 | 13 |

* = POST-REMEDIATION RESULTS

PRE-REMEDIATION RESULTS

| | | | | | | |
|---|---|---|---|---|---|---|
| 5.2 | B | 1 | 6 | 15 | 8 | 9 |
| 5.2 | B | 2 | 6 | 13 | 8 | 7 |
| 5.2 | D | 1 | 6 | 11 | 8 | 5 |
| 5.2 | D | 3 | 6 | 12 | 8 | 6 |
| 5.2 | E | 1 | 6 | 13 | 8 | 7 |
| 5.2 | E | 3 | 6 | 15 | 8 | 9 |
| 5.2 | F | 2 | 6 | 16 | 8 | 10 |
| 5.2 | F | 3 | 6 | 16 | 8 | 10 |
| 5.2 | G | 1 | 6 | 11 | 8 | 5 |
| 5.2 | G | 3 | 6 | 13 | 8 | 7 |
| 5.2 | H | 2 | 6 | 12 | 8 | 6 |
| 5.2 H3 | INSIDE | | 6 | 14 | 8 | 8 |
| 5.2 | H | 3 | 6 | 13 | 8 | 7 |
| 5.2 | I | 2 | 6 | 14 | 8 | 8 |
| 5.2 | I | 3 | 6 | 19 | 8 | 13 |
| 5.2 | J | 1 | 6 | 15 | 8 | 9 |
| 5.2 | J | 2 | 6 | 17 | 8 | 11 |
| 5.2 | J | 3 | 6 | 16 | 8 | 10 |
| 5.2 | K | 1 | 6 | 16 | 8 | 10 |
| 5.2 | K | 2 | 6 | 16 | 8 | 10 |

ANSTEC
APERTURE
CARD

Also Available on
Aperture Card

TABLE 5.2-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
HUT WALL BELOW ROOF EXCAVATION AREA 5.2 FOR MICRO REM POST REMEDIATION

RADIATION TYPE: GAMMA SURVEY IN UREM/HR
COMPLETION
DATE: 10-31-94
TECHNICIANS: JB/PK
LOCATION: 5.0
GRID ID: 5.2
MEDIA TYPE: CONCRETE
# of POINTS: 63 (>60)

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | LIMIT |
|---|---|---|
| MAX | 16 FAIL | 10 |
| AVG | 7.84 FAIL | 5 |
| STD X | 4 | |
| MU SUB ALPHA | 9 FAIL | 5 |

| ID # | GRID COORDINATES LETTER | NUMBER | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|---|
| | W | S | | | | |
| 5.2 | A | 1 | 6 | 14 | 8 | 8 |
| 5.2 | A | 2 | 6 | 14 | 8 | 8 |
| 5.2 | A | 3 | 6 | 16 | 8 | 10 |
| 5.2 | B* | 1 | 6 | 12 | 8 | 6 |
| 5.2 | B* | 2 | 6 | 9 | 8 | 3 |
| 5.2 B2 | INSIDE WEST | | 6 | 13 | 8 | 7 |
| 5.2 B2 | INSIDE EAST | | 6 | 12 | 8 | 6 |
| 5.2 | B | 3 | 6 | 14 | 8 | 8 |
| 5.2 B3 | INSIDE EAST | | 6 | 17 | 8 | 11 |
| 5.2 B3 | INSIDE WEST | | 6 | 11 | 8 | 5 |
| 5.2 | C | 1 | 6 | 12 | 8 | 6 |
| 5.2 | C | 2 | 6 | 10 | 8 | 4 |
| 5.2 | C | 3 | 6 | 13 | 8 | 7 |
| 5.2 | D* | 1 | 6 | 12 | 8 | 6 |
| 5.2 | D | 2 | 6 | 11 | 8 | 5 |
| 5.2 | D* | 3 | 6 | 8 | 8 | 2 |
| 5.2 | E* | 1 | 6 | 7 | 8 | 1 |
| 5.2 E1 | INSIDE EAST | | 6 | 16 | 8 | 10 |
| 5.2 E1 | INSIDE WEST | | 6 | 17 | 8 | 11 |
| 5.2 | E | 2 | 6 | 15 | 8 | 9 |
| 5.2 E2 | INSIDE EAST | | 6 | 14 | 8 | 8 |
| 5.2 E2 | INSIDE WEST | | 6 | 19 | 8 | 13 |
| 5.2 | E* | 3 | 6 | 7 | 8 | 1 |
| 5.2 E3 | INSIDE EAST | | 6 | 13 | 8 | 7 |
| 5.2 E3 | INSIDE WEST | | 6 | 18 | 8 | 12 |
| 5.2 | F | 1 | 6 | 15 | 8 | 9 |
| 5.2 | F* | 2 | 6 | 13 | 8 | 7 |
| 5.2 | F* | 3 | 6 | 15 | 8 | 9 |
| 5.2 | G* | 1 | 6 | 8 | 8 | 2 |
| 5.2 | G | 2 | 6 | 11 | 8 | 5 |
| 5.2 G2 | INSIDE EAST | | 6 | 17 | 8 | 11 |
| 5.2 G3 | INSIDE WEST | | 6 | 20 | 8 | 14 |

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TABLE 5.2-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:37 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
HUT WALL BELOW ROOF EXCAVATION - AREA 5.2 FOR BETA POST REMEDIATION

RADIATION TYPE: 1 BETA SCALING FACTOR = 0.3
COMPLETION DATE: 11-4-94
TECHNICIANS: JB/DR
LOCATION: 5.0
GRID ID: 5.2
MEDIA TYPE: CONCRETE
# of POINTS: 63 (>60)
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2
REM.+ FIXED: LIMIT

| | | | |
|---|---|---|---|
| MAX FOR IND GRID | 4375 PASS | 13500 |
| AVG - SURVEY UNIT | 1629 PASS | 13500 |
| STD X | 1320 | |
| MU SUB ALPHA | 1907 PASS | 13500 |
| MAX HOT SPOT | 16325 PASS | 40500 |

| GRID ID # | COORDINATES LETTER | # | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | SCAN MAX BETA COUNTS | TOTAL CONT. AREA CM^2 | MATERIAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. BETA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 CM^2 | MAX TEST | INST CPM |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.2 | A | 1 | 4 | 723.3 | 772 | 1012 | 500 | B | 2386 | 1134 +/-1064 | | 5391 | | 0. |
| 5.2 | A | 2 | 4 | 697 | 728 | 0 | 0 | B | 2343 | 579 +/-1034 | NA | | | 0. |
| 5.2 | A | 3 | 4 | 697 | 732 | 973 | 300 | B | 2343 | 789 +/-1036 | | 5154 | | 0. |
| 5.2 | B* | 1 | 9 | 644.8 | 879 | 0 | 0 | B | 2220 | 4304 +/-1106 | NA | | | 0. |
| 5.2 | B* | 2 | 9 | 644.8 | 779 | 0 | 0 | B | 2220 | 2455 +/-1046 | NA | | | 0. |
| 5.2 B2 | INSIDE WEST | | 4 | 697 | 730 | 0 | 0 | B | 2343 | 616 +/-1035 | NA | | | 0. |
| 5.2 B2 | INSIDE EAST | | 4 | 697 | 762 | 0 | 0 | B | 2343 | 1214 +/-1056 | NA | | | 0. |
| 5.2 | B | 3 | 4 | 697 | 811 | 894 | 100 | B | 2343 | 2144 +/-1086 | | 3579 | | 0. |
| 5.2 B3 | INSIDE EAST | | 4 | 697 | 717 | 807 | 100 | B | 2343 | 390 +/-1027 | | 2054 | | 0. |
| 5.2 B3 | INSIDE WEST | | 4 | 697 | 706 | 0 | 0 | B | 2343 | 168 +/-1019 | NA | | | 0. |
| 5.2 | C | 1 | 4 | 723.3 | 826 | 868 | 200 | B | 2386 | 1934 +/-1097 | | 2702 | | 0. |
| 5.2 | C | 2 | 4 | 723.3 | 797 | 897 | 100 | B | 2386 | 1395 +/-1079 | | 3244 | | 0. |
| 5.2 | C | 3 | 4 | 697 | 769 | 811 | 100 | B | 2343 | 1352 +/-1060 | | 2129 | | 0. |
| 5.2 | D* | 1 | 9 | 644.8 | 670 | 0 | 0 | B | 2220 | 463 +/- 976 | NA | | | 0. |
| 5.2 | D | 2 | 4 | 723.3 | 744 | 0 | 0 | B | 2386 | 387 +/-1046 | NA | | | 0. |
| 5.2 | D* | 3 | 9 | 644.8 | 773 | 0 | 0 | B | 2220 | 2357 +/-1042 | NA | | | 0. |
| 5.2 | E* | 1 | 9 | 644.8 | 727 | 0 | 0 | B | 2220 | 1510 +/-1013 | NA | | | 0. |
| 5.2 E1 | INSIDE EAST | | 4 | 733.7 | 856 | 0 | 0 | B | 2403 | 2284 +/-1116 | NA | | | 0. |
| 5.2 E1 | INSIDE WEST | | 4 | 733.7 | 764 | 0 | 0 | B | 2403 | 566 +/-1059 | NA | | | 0. |
| 5.2 | E | 2 | 4 | 723.3 | 696 | 1074 | 400 | B | 2386 | -227 +/-1015 | | 6549 | | 0. |
| 5.2 E2 | INSIDE EAST | | 5 | 802.8 | 829 | 0 | 0 | B | 2510 | 489 +/-1103 | NA | | | 0. |
| 5.2 E2 | INSIDE WEST | | 5 | 802.8 | 770 | 0 | 0 | B | 2510 | -612 +/-1067 | NA | | | 0. |
| 5.2 | E* | 3 | 9 | 644.8 | 790 | 0 | 0 | B | 2220 | 2668 +/-1053 | NA | | | 0. |
| 5.2 E3 | INSIDE EAST | | 5 | 723.3 | 762 | 0 | 0 | B | 2385 | 722 +/-1057 | NA | | | 0. |
| 5.2 E3 | INSIDE WEST | | 5 | 723.3 | 759 | 0 | 0 | B | 2385 | 666 +/-1055 | NA | | | 0. |
| 5.2 | F | 1 | 5 | 723.3 | 816 | 1598 | 500 | B | 2385 | 2460 +/-1090 | | 16325 | | 0. |
| 5.2 | F* | 2 | 9 | 644.8 | 734 | 0 | 0 | B | 2220 | 1639 +/-1018 | NA | | | 0. |
| 5.2 | F* | 3 | 9 | 644.8 | 806 | 0 | 0 | B | 2220 | 2962 +/-1063 | NA | | | 0. |
| 5.2 | G* | 1 | 9 | 644.8 | 669 | 0 | 0 | B | 2220 | 445 +/- 975 | NA | | | 0. |

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TABLE 5.2-2

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.2 | G | 2 | 1 | 701.2 | 889 | 906 | 4000 | 8 | 2383 | 3686 +/-1150 | 3879 | 0 |
| 5.2 G2 INSIDE EAST | | | 1 | 745.3 | 757 | 0 | 0 | 8 | 2456 | 222 +/-1070 | NA | 0 |
| 5.2 G3 INSIDE WEST | | | 1 | 745.3 | 816 | 932 | 500 | 8 | 2456 | 1449 +/-1108 | 3536 | 0 |
| 5.2 G1 INSIDE EAST | | | 1 | 745.3 | 748 | 0 | 0 | 8 | 2456 | 51 +/-1065 | NA | 0 |
| 5.2 | G* | 3 | 9 | 644.8 | 770 | 0 | 0 | 8 | 2220 | 2301 +/-1040 | NA | 0. |
| 5.2 | H | 1 | 1 | 635 | 762 | 864 | 100 | 8 | 2271 | 2425 +/-1067 | 4337 | 0 |
| 5.2 | H* | 2 | 9 | 841.6 | 910 | 0 | 0 | 8 | 2529 | 1257 +/-1136 | NA | 0. |
| 5.2 | H* | 3 | 9 | 644.8 | 793 | 0 | 0 | 8 | 2220 | 2723 +/-1055 | NA | 0. |
| 5.2 H3 INSIDE* | | | 9 | 841.6 | 942 | 0 | 0 | 8 | 2529 | 1845 +/-1154 | NA | 0. |
| 5.2 | I | 1 | 1 | 635 | 852 | 892 | 3500 | 8 | 2271 | 4375 +/-1123 | 4867 | 0 |
| 5.2 | I* | 2 | 9 | 644.8 | 758 | 0 | 0 | 8 | 2220 | 2080 +/-1033 | NA | 0. |
| 5.2 I2 INSIDE WEST | | | 1 | 635 | 758 | 0 | 0 | 8 | 2271 | 2330 +/-1064 | NA | 0 |
| 5.2 I2 INSIDE EAST | | | 1 | 635 | 852 | 867 | 1000 | 8 | 2271 | 4138 +/-1123 | 4394 | 0 |
| 5.2 I3 INSIDE EAST | | | 1 | 635 | 829 | 0 | 0 | 8 | 2271 | 3674 +/-1109 | NA | 0 |
| 5.2 I3 INSIDE WEST | | | 1 | 635 | 684 | 0 | 0 | 8 | 2271 | 928 +/-1015 | NA | 0 |
| 5.2 | I* | 3 | 9 | 644.8 | 839 | 0 | 0 | 8 | 2220 | 3569 +/-1083 | NA | 0. |
| 5.2 | J* | 1 | 9 | 644.8 | 784 | 0 | 0 | 8 | 2220 | 2558 +/-1049 | NA | 0. |
| 5.2 | J* | 2 | 9 | 644.8 | 836 | 0 | 0 | 8 | 2220 | 3513 +/-1081 | NA | 0. |
| 5.2 | J* | 3 | 9 | 644.8 | 797 | 0 | 0 | 8 | 2220 | 2797 +/-1057 | NA | 0. |
| 5.2 | K* | 1 | 9 | 644.8 | 868 | 0 | 0 | 8 | 2220 | 4101 +/-1100 | NA | 0. |
| 5.2 | K* | 2 | 9 | 644.8 | 847 | 0 | 0 | 8 | 2220 | 3716 +/-1087 | NA | 0. |
| 5.2 | K | 3 | 1 | 701.2 | 812 | 1489 | 1000 | 8 | 2383 | 3381 +/-1103 | 14920 | 0 |
| 5.2 | K | 4 | 1 | 616.0 | 628 | 0 | 0 | 8 | 2237 | 227 +/- 975 | NA | 0 |
| 5.2 | K | 5 | 1 | 616 | 624 | 0 | 0 | 8 | 2237 | 152 +/- 972 | NA | 0 |
| 5.2 | K | 6 | 1 | 616 | 646 | 0 | 0 | 8 | 2237 | 568 +/- 987 | NA | 0 |
| 5.2 | L | 1 | 1 | 616 | 685 | 0 | 0 | 8 | 2237 | 1307 +/-1014 | NA | 0 |
| 5.2 | L | 2 | 1 | 616 | 655 | 0 | 0 | 8 | 2237 | 739 +/- 994 | NA | 0 |
| 5.2 | L | 3 | 1 | 616 | 680 | 0 | 0 | 8 | 2237 | 1212 +/-1011 | NA | 0 |
| 5.2 | M | 1 | 1 | 745.3 | 748 | 0 | 0 | 8 | 2456 | 51 +/-1065 | NA | 0 |
| 5.2 | M | 2 | 1 | 745.3 | 778 | 0 | 0 | 8 | 2456 | 619 +/-1084 | NA | 0 |
| 5.2 | M | 3 | 1 | 616 | 683 | 0 | 0 | 8 | 2237 | 1269 +/-1013 | NA | 0 |
| 5.2 | N | 1 | 1 | 745.3 | 804 | 0 | 0 | 8 | 2456 | 1112 +/-1100 | NA | 0 |
| 5.2 | N | 2 | 1 | 745.3 | 856 | 0 | 0 | 8 | 2456 | 2097 +/-1132 | NA | 0 |
| 5.2 | N | 3 | 1 | 745.3 | 688 | 0 | 0 | 8 | 2456 | -1085 +/-1025 | NA | 0 |

* : POST-REMEDIATION RESULTS

PRE-REMEDIATION RESULTS

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.2 | B | 1 | 4 | 723.3 | 803 | 2310 | 900 | 8 | 2386 | 4021 +/-1083 | 29630 | 0. |
| 5.2 | B | 2 | 4 | 697 | 707 | 1325 | 200 | 8 | 2343 | 418 +/-1020 | 11727 | 0. |
| 5.2 | D | 1 | 4 | 745.3 | 701 | 1231 | 200 | 8 | 2421 | -629 +/-1019 | 9070 | 0. |
| 5.2 | D | 3 | 4 | 723.3 | 723 | 902 | 200 | 8 | 2386 | 61 +/-1032 | 3337 | 0. |
| 5.2 | E | 1 | 4 | 723.3 | 741 | 1572 | 300 | 8 | 2386 | 796 +/-1044 | 15849 | 0. |
| 5.2 | E | 3 | 5 | 723.3 | 797 | 925 | 100 | 8 | 2385 | 1399 +/-1079 | 3764 | 0. |
| 5.2 | F | 2 | 5 | 723.3 | 812 | 1195 | 200 | 8 | 2385 | 1798 +/-1088 | 8804 | 0. |
| 5.2 | F | 3 | 5 | 723.3 | 808 | 987 | 100 | 8 | 2385 | 1614 +/-1085 | 4922 | 0. |
| 5.2 | G | 1 | 1 | 701.2 | 813 | 1253 | 1900 | 8 | 2383 | 3701 +/-1103 | 10451 | 0. |
| 5.2 | G | 3 | 1 | 745.3 | 785 | 924 | 1400 | 8 | 2456 | 1120 +/-1088 | 3384 | 0. |
| 5.2 | H | 2 | 1 | 635 | 833 | 6682 | 5100 | 8 | 2271 | 60246 +/-1111 FAIL | 114527 FAIL | 0. |
| 5.2 H3 INSIDE | | | 1 | 635 | 5789 | 7500 | 10000 | 8 | 2271 | 130019 +/-2840 FAIL | 130019 FAIL | 0. |
| 5.2 | H | 3 | 1 | 635 | 750 | 865 | 400 | 8 | 2271 | 2265 +/-1059 | 4356 | 0. |
| 5.2 | I | 2 | 1 | 635 | 783 | 6025 | 100 | 8 | 2271 | 3796 +/-1080 | 102083 FAIL | 0. |
| 5.2 | I | 3 | 1 | 635 | 876 | 923 | 300 | 8 | 2271 | 4591 +/-1138 | 5455 | 0. |
| 5.2 | J | 1 | 1 | 701.2 | 823 | 1050 | 1900 | 8 | 2383 | 3124 +/-1109 | 6606 | 0. |
| 5.2 | J | 2 | 1 | 701.2 | 804 | 1076 | 900 | 8 | 2383 | 2411 +/-1098 | 7098 | 0. |
| 5.2 | J | 3 | 1 | 701.2 | 924 | 947 | 300 | 8 | 2383 | 4233 +/-1170 | 4655 | 0. |
| 5.2 | K | 1 | 1 | 701.2 | 1128 | 1727 | 1000 | 8 | 2383 | 9218 +/-1285 | 19428 | 0. |
| 5.2 | K | 2 | 1 | 701.2 | 806 | 1123 | 700 | 8 | 2383 | 2405 +/-1099 | 7989 | 0. |

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R.A TABLE 5.2-3

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:36 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
HUT WALL BELOW ROOF EXCAVATION AREA 5.2 FOR ALPHA POST REMEDIATION

RADIATION TYPE: 2
COMPLETION
DATE: 10-31-94
TECHNICIANS: JB/PK
LOCATION: 5.0
GRID ID: 5.2
MEDIA TYPE: CONCRETE
# of POINTS: 63 (>60)
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | | LIMIT |
|---|---|---|---|
| MAX FOR IND GRID | 62 | PASS | 5000 |
| AVG - SURVEY UNIT | 8 | PASS | 5000 |
| STD X | 12 | | |
| MU SUB ALPHA | 11 | PASS | 5000 |
| MAX HOT SPOT | 30 | PASS | 15000 |

| ID # | GRID COORIDINATES W | S | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | SCAN MAX ALPHA COUNTS | TOTAL CONT. AREA CM^2 | MATERIAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. ALPHA FIXED DPM/ 100 CM^2 Avg. | AVG TEST | MAX PER 100 CM^2 | MAX TEST | INST CPM/ |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.2 | A | 1 | 4 | 0.8 | 3 | 2 | 500 | 8 | 34 | 11 +/- 17 | | 6 | | 0.2 |
| 5.2 | A | 2 | 4 | 0.8 | 8 | 0 | 0 | 8 | 34 | 36 +/- 28 | NA | | | 0.2 |
| 5.2 | A | 3 | 4 | 0.8 | 2 | 4 | 300 | 8 | 34 | 6 +/- 14 | | 16 | | 0.2 |
| 5.2 | B* | 1 | 9 | 2 | 4 | 0 | 0 | 8 | 51 | 11 +/- 22 | NA | | | 0.1 |
| 5.2 | B* | 2 | 9 | 2 | 4 | 0 | 0 | 8 | 51 | 11 +/- 22 | NA | | | 0.1 |
| 5.2 B2 INSIDE WEST | | | 4 | 0.8 | 0 | 0 | 0 | 8 | 34 | -4 +/- 3 | NA | | | 0.2 |
| 5.2 B2 INSIDE EAST | | | 4 | 0.8 | 3 | 0 | 0 | 8 | 34 | 11 +/- 17 | NA | | | 0.2 |
| 5.2 | B | 3 | 4 | 0.8 | 2 | 3 | 100 | 8 | 34 | 6 +/- 14 | | 11 | | 0.2 |
| 5.2 B3 INSIDE EAST | | | 4 | 0.8 | 0 | 3 | 100 | 8 | 34 | -4 +/- 3 | | 11 | | 0.2 |
| 5.2 B3 INSIDE WEST | | | 4 | 0.8 | 2 | 0 | 0 | 8 | 34 | 6 +/- 14 | NA | | | 0.2 |
| 5.2 | C | 1 | 4 | 0.8 | 4 | 3 | 200 | 8 | 34 | 16 +/- 20 | | 11 | | 0.2 |
| 5.2 | C | 2 | 4 | 0.8 | 0 | 2 | 100 | 8 | 34 | -4 +/- 3 | | 6 | | 0.2 |
| 5.2 | C | 3 | 4 | 0.8 | 1 | 4 | 100 | 8 | 34 | 1 +/- 10 | | 16 | | 0.2 |
| 5.2 | D* | 1 | 9 | 2 | 1 | 0 | 0 | 8 | 51 | -6 +/- 12 | NA | | | 0.1 |
| 5.2 | D | 2 | 4 | 0.8 | 1 | 0 | 0 | 8 | 34 | 1 +/- 10 | NA | | | 0.2 |
| 5.2 | D* | 3 | 9 | 2 | 2 | 0 | 0 | 8 | 51 | 0 +/- 16 | NA | | | 0.1 |
| 5.2 | E* | 1 | 9 | 2 | 2 | 0 | 0 | 8 | 51 | 0 +/- 16 | NA | | | 0.1 |
| 5.2 E1 INSIDE EAST | | | 5 | 1.1 | 0 | 0 | 0 | 8 | 41 | -6 +/- 4 | NA | | | 0.1 |
| 5.2 E1 INSIDE WEST | | | 5 | 1.1 | 3 | 0 | 0 | 8 | 41 | 10 +/- 19 | NA | | | 0.1 |
| 5.2 | E | 2 | 4 | 0.8 | 1 | 3 | 400 | 8 | 34 | 1 +/- 10 | | 11 | | 0.2 |
| 5.2 E2 INSIDE EAST | | | 5 | 0.1 | 1 | 0 | 0 | 8 | 23 | 5 +/- 11 | NA | | | 0.1 |
| 5.2 E2 INSIDE WEST | | | 5 | 0.1 | 8 | 0 | 0 | 8 | 23 | 43 +/- 30 | NA | | | 0.1 |
| 5.2 | E* | 3 | 9 | 2 | 3 | 0 | 0 | 8 | 51 | 6 +/- 19 | NA | | | 0.1 |
| 5.2 E3 INSIDE EAST | | | 5 | 0.8 | 1 | 0 | 0 | 8 | 38 | 1 +/- 11 | NA | | | 0.1 |
| 5.2 E3 INSIDE WEST | | | 5 | 0.8 | 3 | 0 | 0 | 8 | 38 | 12 +/- 19 | NA | | | 0.1 |
| 5.2 | F | 1 | 5 | 0.8 | 3 | 6 | 500 | 8 | 33 | 14 +/- 19 | | 30 | | 0.1 |
| 5.2 | F* | 2 | 9 | 2 | 3 | 0 | 0 | 8 | 51 | 6 +/- 19 | NA | | | 0.1 |
| 5.2 | F* | 3 | 9 | 2 | 4 | 0 | 0 | 8 | 51 | 11 +/- 22 | NA | | | 0.1 |
| 5.2 | G* | 1 | 9 | 2 | 1 | 0 | 0 | 8 | 51 | -6 +/- 12 | NA | | | 0.1 |

ANSTEC
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Also Available on
Aperture Card

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TABLE 5.2-3

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|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.2 | G | 2 | 1 | 0.4 | 3 | 4 | 4000 | 8 | 30 | 16 +/- 18 | | 19 | 0. |
| 5.2 G2 INSIDE EAST | | | 1 | 2.3 | 3 | 0 | 0 | 8 | 51 | 4 +/- 19 | NA | | 0. |
| 5.2 G3 INSIDE WEST | | | 1 | 2.3 | 5 | 1 | 500 | 8 | 51 | 13 +/- 24 | | -7 | 0. |
| 5.2 G1 INSIDE EAST | | | 1 | 2.3 | 14 | 0 | 0 | 8 | 51 | 62 +/- 39 | NA | | 0. |
| 5.2 | G* | 3 | 9 | 2 | 2 | 0 | 0 | 8 | 51 | 0 +/- 16 | NA | | 0. |
| 5.2 | H | 1 | 1 | 0.1 | 1 | 1 | 100 | 8 | 22 | 5 +/- 10 | | 5 | 0. |
| 5.2 | H* | 2 | 9 | 1.6 | 3 | 0 | 0 | 8 | 48 | 8 +/- 19 | NA | | 0. |
| 5.2 | H* | 3 | 9 | 2 | 7 | 0 | 0 | 8 | 51 | 28 +/- 29 | NA | | 0. |
| 5.2 H3 INSIDE* | | | 9 | 1.6 | 3 | 0 | 0 | 8 | 48 | 8 +/- 19 | NA | | 0. |
| 5.2 | I | 1 | 1 | 0.2 | 3 | 5 | 3500 | 8 | 25 | 18 +/- 18 | | 25 | 0. |
| 5.2 | I* | 2 | 9 | 2 | 4 | 0 | 0 | 8 | 51 | 11 +/- 22 | NA | | 0. |
| 5.2 I2 INSIDE WEST | | | 1 | 0.4 | 1 | 0 | 0 | 8 | 30 | 3 +/- 11 | NA | | 0. |
| 5.2 I2 INSIDE EAST | | | 1 | 0.4 | 0 | 1 | 1000 | 8 | 30 | -2 +/- 2 | | 3 | 0. |
| 5.2 I3 INSIDE EAST | | | 1 | 0.4 | 5 | 0 | 0 | 8 | 30 | 24 +/- 23 | NA | | 0. |
| 5.2 I3 INSIDE WEST | | | 1 | 0.4 | 3 | 0 | 0 | 8 | 30 | 14 +/- 18 | NA | | 0. |
| 5.2 | I* | 3 | 9 | 2 | 7 | 0 | 0 | 8 | 51 | 28 +/- 29 | NA | | 0. |
| 5.2 | J* | 1 | 9 | 2 | 1 | 0 | 0 | 8 | 51 | -6 +/- 12 | NA | | 0. |
| 5.2 | J* | 2 | 9 | 2 | 5 | 0 | 0 | 8 | 51 | 17 +/- 25 | NA | | 0. |
| 5.2 | J* | 3 | 9 | 2 | 4 | 0 | 0 | 8 | 51 | 11 +/- 22 | NA | | 0. |
| 5.2 | K* | 1 | 9 | 2 | 4 | 0 | 0 | 8 | 51 | 11 +/- 22 | NA | | 0. |
| 5.2 | K* | 2 | 9 | 2 | 4 | 0 | 0 | 8 | 51 | 11 +/- 22 | NA | | 0. |
| 5.2 | K | 3 | 1 | 0.4 | 3 | 3 | 1000 | 8 | 30 | 14 +/- 18 | | 14 | 0. |
| 5.2 | K | 4 | 1 | 0.2 | 4 | 0 | 0 | 8 | 25 | 20 +/- 21 | NA | | 0. |
| 5.2 | K | 5 | 1 | 0.2 | 3 | 0 | 0 | 8 | 25 | 15 +/- 18 | NA | | 0. |
| 5.2 | K | 6 | 1 | 0.2 | 0 | 0 | 0 | 8 | 25 | -1 +/- 1 | NA | | 0. |
| 5.2 | L | 1 | 1 | 0.2 | 1 | 0 | 0 | 8 | 25 | 4 +/- 10 | NA | | 0. |
| 5.2 | L | 2 | 1 | 0.2 | 2 | 0 | 0 | 8 | 25 | 9 +/- 15 | NA | | 0. |
| 5.2 | L | 3 | 1 | 0.2 | 2 | 0 | 0 | 8 | 25 | 9 +/- 15 | NA | | 0. |
| 5.2 | M | 1 | 1 | 2.7 | 3 | 0 | 0 | 8 | 55 | 2 +/- 19 | NA | | 0. |
| 5.2 | M | 2 | 1 | 2.3 | 2 | 0 | 0 | 8 | 51 | -2 +/- 15 | NA | | 0. |
| 5.2 | M | 3 | 1 | 0.2 | 3 | 0 | 0 | 8 | 25 | 15 +/- 18 | NA | | 0. |
| 5.2 | N | 1 | 1 | 2.3 | 1 | 0 | 0 | 8 | 51 | -7 +/- 11 | NA | | 0. |
| 5.2 | N | 2 | 1 | 2.3 | 0 | 0 | 0 | 8 | 51 | -12 +/- 5 | NA | | 0. |
| 5.2 | N | 3 | 1 | 2.3 | 0 | 0 | 0 | 8 | 51 | -12 +/- 5 | NA | | 0. |

* = POST-REMEDIATION RESULTS

PRE-REMEDIATION RESULTS

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.2 | B | 1 | 4 | 0.8 | 4 | 5 | 900 | 8 | 34 | 16 +/- 20 | | 21 | 0.2 |
| 5.2 | B | 2 | 4 | 0.8 | 3 | 4 | 200 | 8 | 34 | 11 +/- 17 | | 16 | 0.2 |
| 5.2 | D | 1 | 4 | 2.3 | 3 | 1 | 200 | 8 | 48 | 3 +/- 17 | | -6 | 0.2 |
| 5.2 | D | 3 | 4 | 0.8 | 2 | 1 | 200 | 8 | 34 | 6 +/- 14 | | 1 | 0.2 |
| 5.2 | E | 1 | 4 | 0.8 | 3 | 5 | 300 | 8 | 34 | 11 +/- 17 | | 21 | 0.2 |
| 5.2 | E | 3 | 5 | 0.8 | 3 | 4 | 100 | 8 | 38 | 12 +/- 19 | | 17 | 0 |
| 5.2 | F | 2 | 5 | 0.5 | 3 | 2 | 200 | 8 | 33 | 14 +/- 19 | | 8 | 0. |
| 5.2 | F | 3 | 5 | 0.5 | 5 | 4 | 100 | 8 | 33 | 25 +/- 24 | | 19 | 0. |
| 5.2 | G | 1 | 1 | 0.4 | 3 | 4 | 1900 | 8 | 30 | 15 +/- 18 | | 19 | 0.1 |
| 5.2 | G | 3 | 1 | 2.3 | 1 | 4 | 1400 | 8 | 51 | -5 +/- 11 | | 9 | 0.1 |
| 5.2 | H | 2 | 1 | 0.4 | 3 | 4 | 5100 | 8 | 30 | 16 +/- 18 | | 19 | 0.1 |
| 5.2 H3 INSIDE | | | 1 | 0.4 | 2 | 0 | 0 | 8 | 30 | 8 +/- 15 | NA | | 0.1 |
| 5.2 | H | 3 | 1 | 0.4 | 3 | 0 | 400 | 8 | 30 | 13 +/- 18 | NA | | 0.1 |
| 5.2 | I | 2 | 1 | 0.2 | 4 | 4 | 100 | 8 | 25 | 20 +/- 21 | | 20 | 0.1 |
| 5.2 | I | 3 | 1 | 0.4 | 1 | 4 | 300 | 8 | 30 | 4 +/- 11 | | 19 | 0.1 |
| 5.2 | J | 1 | 1 | 0.4 | 4 | 6 | 1900 | 8 | 30 | 21 +/- 21 | | 30 | 0.1 |
| 5.2 | J | 2 | 1 | 0.4 | 2 | 7 | 900 | 8 | 30 | 11 +/- 15 | | 35 | 0.1 |
| 5.2 | J | 3 | 1 | 0.4 | 3 | 5 | 300 | 8 | 30 | 14 +/- 18 | | 24 | 0.1 |
| 5.2 | K | 1 | 1 | 0.4 | 0 | 3 | 1000 | 8 | 30 | -1 +/- 2 | | 14 | 0.1 |
| 5.2 | K | 2 | 1 | 0.4 | 2 | 8 | 700 | 8 | 30 | 11 +/- 15 | | 40 | 0.1 |

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TABLE 5.3-I

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:39 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
HUT ROOF LEDGE - AREA 5.3 FOR BETA

RADIATION TYPE: 1 BETA SCALING FACTOR = 0.3
COMPLETION DATE: 11-11-94
TECHNICIANS: JB
LOCATION: 5.0
GRID ID: 5.3
MEDIA TYPE: CONCRETE
# of POINTS: 11
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY);
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | | LIMIT |
|---|---|---|---|
| MAX FOR IND GRID | 413 | PASS | 13500 |
| AVG - SURVEY UNIT | -102 | PASS | 13500 |
| STD X | 417 | | |
| MU SUB ALPHA | 125 | PASS | 13500 |
| MAX HOT SPOT | 0 | PASS | 40500 |

| GRID COORDINATES ID # | LETTER | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | SCAN MAX BETA COUNTS | TOTAL CONT. AREA CM^2 | MATERIAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. BETA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 CM^2 | MAX TEST | INST |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.3 | D | 6 | 552.4 | 572 | 0 | 0 | B | 2049 | 359 +/- 898 | NA | | | 0.1 |
| 5.3 | A | 6 | 552.4 | 505 | 0 | 0 | B | 2049 | -867 +/- 849 | NA | | | 0.1 |
| 5.3 | B | 6 | 552.4 | 546 | 0 | 0 | B | 2049 | -117 +/- 879 | NA | | | 0.1 |
| 5.3 | C | 6 | 552.4 | 549 | 0 | 0 | B | 2049 | -62 +/- 881 | NA | | | 0.1 |
| 5.3 | D | 6 | 552.4 | 522 | 0 | 0 | B | 2049 | -556 +/- 862 | NA | | | 0.1 |
| 5.3 | E | 6 | 552.4 | 561 | 0 | 0 | B | 2049 | 157 +/- 890 | NA | | | 0.1 |
| 5.3 | F | 6 | 552.4 | 544 | 0 | 0 | B | 2049 | -154 +/- 878 | NA | | | 0.1 |
| 5.3 | G | 6 | 552.4 | 575 | 0 | 0 | B | 2049 | 413 +/- 900 | NA | | | 0.1 |
| 5.3 | H | 6 | 552.4 | 519 | 0 | 0 | B | 2049 | -611 +/- 859 | NA | | | 0.1 |
| 5.3 | I | 6 | 552.4 | 561 | 0 | 0 | B | 2049 | 157 +/- 890 | NA | | | 0.1 |
| 5.3 | J | 6 | 552.4 | 561 | 0 | 0 | B | 2049 | 157 +/- 890 | NA | | | 0.1 |

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TABLE 5.3-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:39 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
HUT ROOF LEDGE - AREA 5.3 FOR ALPHA

RADIATION TYPE: 2
COMPLETION
DATE: 11-11-94
TECHNICIANS: JB
LOCATION: 5.0
GRID ID: 5.3
MEDIA TYPE: CONCRETE
# of POINTS: 11
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | | LIMIT |
|---|---|---|---|
| MAX FOR IND GRID | 22 | PASS | 5000 |
| AVG - SURVEY UNIT | 4 | PASS | 5000 |
| STD X | 9 | | |
| MU SUB ALPHA | 9 | PASS | 5000 |
| MAX HOT SPOT | 0 | PASS | 15000 |

| ID # | GRID COORDINATES LETTER | # | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | SCAN MAX ALPHA COUNTS | TOTAL CONT. AREA CM^2 | MATERIAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. ALPHA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 CM^2 | MAX TEST | INST CPM/ |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 5.3 | O | | 6 | 1.1 | 2 | 0 | 0 | 8 | 42 | 5 +/- 16 | NA | | | 0.1 |
| 5.3 | A | | 6 | 1.1 | 5 | 0 | 0 | 8 | 42 | 22 +/- 25 | NA | | | 0.1 |
| 5.3 | B | | 6 | 1.1 | 1 | 0 | 0 | 8 | 42 | -1 +/- 11 | NA | | | 0.1 |
| 5.3 | C | | 6 | 1.1 | 4 | 0 | 0 | 8 | 42 | 16 +/- 22 | NA | | | 0.1 |
| 5.3 | D | | 6 | 1.1 | 0 | 0 | 0 | 8 | 42 | -6 +/- 4 | NA | | | 0.1 |
| 5.3 | E | | 6 | 1.1 | 2 | 0 | 0 | 8 | 42 | 5 +/- 16 | NA | | | 0.1 |
| 5.3 | F | | 6 | 1.1 | 2 | 0 | 0 | 8 | 42 | 5 +/- 16 | NA | | | 0.1 |
| 5.3 | G | | 6 | 1.1 | 1 | 0 | 0 | 8 | 42 | -1 +/- 11 | NA | | | 0.1 |
| 5.3 | H | | 6 | 1.1 | 0 | 0 | 0 | 8 | 42 | -6 +/- 4 | NA | | | 0.1 |
| 5.3 | I | | 6 | 1.1 | 2 | 0 | 0 | 8 | 42 | 5 +/- 16 | NA | | | 0.1 |
| 5.3 | J | | 6 | 1.1 | 1 | 0 | 0 | 8 | 42 | -1 +/- 11 | NA | | | 0.1 |

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TABLE 6.1-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:42 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
AREA 6.0 BEDROCK WALL OF HUT EXCAVATION - HUT FLOOR TO HUT ROOF ELEVATION

RADIATION TYPE:
COMPLETION
DATE: 01/19/95
TECHNICIANS: TA/JB/LD/PK
LOCATION: 6.0
GRID ID: 6.1
MEDIA TYPE: ROCK
# of POINTS: 30

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | | LIMIT |
|---|---|---|---|
| MAX: | 34.00 | FAIL | 10 |
| AVG: | 14.27 | FAIL | 5 |
| STD X: | 6.84 | | |
| MU SUB ALPHA: | 16.39 | FAIL | 5 |

| ID # | GRID COORDINATES | INST. ID # | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|---|
| 6.1 | 1 | A | 6 | 17 | 8 | 11 |
| 6.1 | 2 | A | 6 | 40 | 8 | 34 |
| 6.1 | 3 | A | 6 | 20 | 8 | 14 |
| 6.1 | 4 | A | 6 | 25 | 8 | 19 |
| 6.1 | 5 | A | 6 | 20 | 8 | 14 |
| 6.1 | 6 | A | 6 | 18 | 8 | 12 |
| 6.1 | 7 | A | 6 | 15 | 8 | 9 |
| 6.1 | 8 | A | 6 | 15 | 8 | 9 |
| 6.1 | 9 | A | 6 | 15 | 8 | 9 |
| 6.1 | 10 | A | 6 | 8 | 8 | 2 |
| 6.1 | 11 | A | 6 | 25 | 8 | 19 |
| 6.1 | 12 | A | 6 | 40 | 8 | 34 |
| 6.1 | 13 | A | 6 | 30 | 8 | 24 |
| 6.1 | 14 | A | 6 | 20 | 8 | 14 |
| 6.1 | 15 | A | 6 | 20 | 8 | 14 |
| 6.1 | 16 | A | 6 | 20 | 8 | 14 |
| 6.1 | 17 | A | 6 | 25 | 8 | 19 |
| 6.1 | 18 | A | 6 | 22 | 8 | 16 |
| 6.1 | 19 | A | 6 | 20 | 8 | 14 |
| 6.1 | 20 | A | 6 | 20 | 8 | 14 |
| 6.1 | 21 | A | 6 | 20 | 8 | 14 |
| 6.1 | 22 | A | 6 | 18 | 8 | 12 |
| 6.1 | 23 | A | 6 | 15 | 8 | 9 |
| 6.1 | 24 | A | 6 | 18 | 8 | 12 |
| 6.1 | 25 | A | 6 | 20 | 8 | 14 |
| 6.1 | 26 | A | 6 | 15 | 8 | 9 |
| 6.1 | 27 | A | 6 | 20 | 8 | 14 |
| 6.1 | 28 | A | 6 | 20 | 8 | 14 |
| 6.1 | 29 | A | 6 | 15 | 8 | 9 |
| 6.1 | 30 | A | 6 | 12 | 8 | 6 |

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TABLE 6.1-2

CINTICHEM DECOMMISSIONING PLAN 01/25/95 07:41 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 6.0 BEDROCK WALL OF HUT EXCAVATION - HUT FLOOR TO HUT ROOF ELEVATION

RADIATION TYPE: 1 BETA SCALING FACTOR = 0.3
COMPLETION DATE: 01/19/95
TECHNICIANS: TA/JB/LD/PK
LOCATION: 6.0
GRID ID: 6.1
MEDIA TYPE: ROCK
# of POINTS: 30 (>60)
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFIY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2
REM.+ FIXED:

| | | | LIMIT |
|---|---|---|---|
| MAX FOR IND GRID | 34300 | FAIL | 13500 |
| AVG - SURVEY UNIT | 10145 | PASS | 13500 |
| STD X | 7742 | | |
| MU SUB ALPHA | 12547 | PASS | 13500 |
| MAX HOT SPOT | 0 | PASS | 40500 |

| ID # | GRID CODRIDINATES | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | SCAN MAX BETA COUNTS | TOTAL CONT. AREA CM^2 | MATER-IAL CODE | MDA DPM | WEIGHTED AVG. BETA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 MAX CM^2 TEST | INST E CPM/D |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 6.1 | 1 | 11 | 961.8 | 1822 | 0 | 0 | 8 | 2773 | 16236 +/- 499 FAIL | NA | | 0.17 |
| 6.1 | 2 | 11 | 961.8 | 1840 | 0 | 0 | 8 | 2773 | 16576 +/- 501 FAIL | NA | | 0.17 |
| 6.1 | 3 | 11 | 961.8 | 2779 | 0 | 0 | 8 | 2773 | 34300 +/- 611 FAIL | NA | | 0.17 |
| 6.1 | 4 | 11 | 961.8 | 1651 | 0 | 0 | 8 | 2773 | 13009 +/- 476 FAIL | NA | | 0.17 |
| 6.1 | 5 | 11 | 961.8 | 1910 | 0 | 0 | 8 | 2773 | 17897 +/- 510 FAIL | NA | | 0.17 |
| 6.1 | 6 | 11 | 961.8 | 1489 | 0 | 0 | 8 | 2773 | 9951 +/- 454 FAIL | NA | | 0.17 |
| 6.1 | 7 | 11 | 961.8 | 1473 | 0 | 0 | 8 | 2773 | 9649 +/- 451 FAIL | NA | | 0.17 |
| 6.1 | 8 | 11 | 961.8 | 1269 | 0 | 0 | 8 | 2773 | 5798 +/- 421 FAIL | NA | | 0.17 |
| 6.1 | 9 | 11 | 961.8 | 1403 | 0 | 0 | 8 | 2773 | 8328 +/- 441 FAIL | NA | | 0.1 |
| 6.1 | 10 | 11 | 961.8 | 1451 | 0 | 0 | 8 | 2773 | 9234 +/- 448 FAIL | NA | | 0.17 |
| 6.1 | 11 | 11 | 961.8 | 1189 | 0 | 0 | 8 | 2773 | 4288 +/- 408 FAIL | NA | | 0.17 |
| 6.1 | 12 | 11 | 961.8 | 1118 | 0 | 0 | 8 | 2773 | 2948 +/- 397 FAIL | NA | | 0.17 |
| 6.1 | 13 | 11 | 961.8 | 1671 | 0 | 0 | 8 | 2773 | 13386 +/- 479 FAIL | NA | | 0.17 |
| 6.1 | 14 | 11 | 961.8 | 1050 | 0 | 0 | 8 | 2773 | 1665 +/- 386 FAIL | NA | | 0.17 |
| 6.1 | 15 | 11 | 961.8 | 736 | 0 | 0 | 8 | 2773 | -4262 +/- 329 | NA | | 0.17 |
| 6.1 | 16 | 9 | 831.2 | 1546 | 0 | 0 | 8 | 2513 | 13135 +/- 448 FAIL | NA | | 0.18 |
| 6.1 | 17 | 9 | 831.2 | 1974 | 0 | 0 | 8 | 2513 | 21000 +/- 503 FAIL | NA | | 0.18 |
| 6.1 | 18 | 9 | 831.2 | 1800 | 0 | 0 | 8 | 2513 | 17802 +/- 481 FAIL | NA | | 0.18 |
| 6.1 | 19 | 9 | 831.2 | 1919 | 0 | 0 | 8 | 2513 | 19989 +/- 496 FAIL | NA | | 0.18 |
| 6.1 | 20 | 9 | 831.2 | 1499 | 0 | 0 | 8 | 2513 | 12271 +/- 441 FAIL | NA | | 0.18 |
| 6.1 | 21 | 9 | 831.2 | 1352 | 0 | 0 | 8 | 2513 | 9570 +/- 420 FAIL | NA | | 0.18 |
| 6.1 | 22 | 9 | 831.2 | 1145 | 0 | 0 | 8 | 2513 | 5766 +/- 389 FAIL | NA | | 0.18 |
| 6.1 | 23 | 9 | 831.2 | 1514 | 0 | 0 | 8 | 2513 | 12547 +/- 443 FAIL | NA | | 0.18 |
| 6.1 | 24 | 9 | 831.2 | 1116 | 0 | 0 | 8 | 2513 | 5233 +/- 384 FAIL | NA | | 0.18 |
| 6.1 | 25 | 9 | 831.2 | 1299 | 0 | 0 | 8 | 2513 | 8596 +/- 412 FAIL | NA | | 0.18 |
| 6.1 | 26 | 9 | 831.2 | 1267 | 0 | 0 | 8 | 2513 | 8008 +/- 408 FAIL | NA | | 0.18 |
| 6.1 | 27 | 9 | 831.2 | 1262 | 0 | 0 | 8 | 2513 | 7916 +/- 407 FAIL | NA | | 0.18 |
| 6.1 | 28 | 9 | 831.2 | 1406 | 0 | 0 | 8 | 2513 | 10562 +/- 428 FAIL | NA | | 0.18 |
| 6.1 | 29 | 9 | 831.2 | 938 | 0 | 0 | 8 | 2513 | 1963 +/- 354 FAIL | NA | | 0.18 |
| 6.1 | 30 | 9 | 831.2 | 673 | 0 | 0 | 8 | 2513 | -2907 +/- 305 | NA | | 0.18 |

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TABLE 6.1-3

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:40 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 6.0 BEDROCK WALL OF HUT EXCAVATION - HUT FLOOR TO HUT ROOF ELEVATION

RADIATION TYPE: 2
COMPLETION DATE: 01/19/95
TECHNICIANS: TA/JB/LD/PK
LOCATION: 6.0
GRID ID: 6.1
MEDIA TYPE: ROCK
# of POINTS: 30 (>60)
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFIY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2
REM.+ FIXED:

| | | PASS | LIMIT |
|---|---|---|---|
| MAX FOR IND GRID | 166 | PASS | 5000 |
| AVG - SURVEY UNIT | -32 | PASS | 5000 |
| STD X | 64 | | |
| MU SUB ALPHA | -12 | PASS | 5000 |
| MAX HOT SPOT | 0 | PASS | 15000 |

| GRID COORDINATES ID # | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | SCAN MAX ALPHA COUNTS | TOTAL CONT. AREA CM^2 | MATER-IAL CODE | MDA DPM 100 CM^2 | WEIGHTED AVG. ALPHA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 MAX CM^2 TEST | INST CPM/ |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 6.1 1 | 11 | 7.2 | 6 | 0 | 0 | 8 | 83 | -7 +/- 28 | NA | | 0.1 |
| 6.1 2 | 11 | 7.2 | 10 | 0 | 0 | 8 | 83 | 51 +/- 35 | NA | | 0.1 |
| 6.1 3 | 11 | 7.2 | 11 | 0 | 0 | 8 | 83 | 69 +/- 37 | NA | | 0.1 |
| 6.1 4 | 11 | 7.2 | 6 | 0 | 0 | 8 | 83 | -22 +/- 28 | NA | | 0.1 |
| 6.1 5 | 11 | 7.2 | 8 | 0 | 0 | 8 | 83 | 15 +/- 32 | NA | | 0.1 |
| 6.1 6 | 11 | 7.2 | 10 | 0 | 0 | 8 | 83 | 51 +/- 35 | NA | | 0.1 |
| 6.1 7 | 11 | 7.2 | 4 | 0 | 0 | 8 | 83 | -59 +/- 23 | NA | | 0.1 |
| 6.1 8 | 11 | 7.2 | 1 | 0 | 0 | 8 | 83 | -113 +/- 14 | NA | | 0.1 |
| 6.1 9 | 11 | 7.2 | 3 | 0 | 0 | 8 | 83 | -77 +/- 21 | NA | | 0.1 |
| 6.1 10 | 11 | 7.2 | 6 | 0 | 0 | 8 | 83 | -22 +/- 28 | NA | | 0.1 |
| 6.1 11 | 11 | 7.2 | 3 | 0 | 0 | 8 | 83 | -77 +/- 21 | NA | | 0.1 |
| 6.1 12 | 11 | 7.2 | 2 | 0 | 0 | 8 | 83 | -95 +/- 18 | NA | | 0.1 |
| 6.1 13 | 11 | 7.2 | 5 | 0 | 0 | 8 | 83 | -40 +/- 26 | NA | | 0.1 |
| 6.1 14 | 11 | 7.2 | 8 | 0 | 0 | 8 | 83 | 15 +/- 32 | NA | | 0.1 |
| 6.1 15 | 11 | 7.2 | 4 | 0 | 0 | 8 | 83 | -59 +/- 23 | NA | | 0.1 |
| 6.1 16 | 9 | 7.0 | 2 | 0 | 0 | 8 | 83 | -92 +/- 18 | NA | | 0.1 |
| 6.1 17 | 9 | 7.0 | 5 | 0 | 0 | 8 | 83 | -37 +/- 26 | NA | | 0.1 |
| 6.1 18 | 9 | 7.0 | 16 | 0 | 0 | 8 | 83 | 166 +/- 44 | NA | | 0.1 |
| 6.1 19 | 9 | 7.0 | 5 | 0 | 0 | 8 | 83 | -37 +/- 26 | NA | | 0.1 |
| 6.1 20 | 9 | 7.0 | 3 | 0 | 0 | 8 | 83 | -74 +/- 21 | NA | | 0.1 |
| 6.1 21 | 9 | 7.0 | 6 | 0 | 0 | 8 | 83 | -18 +/- 28 | NA | | 0.1 |
| 6.1 22 | 9 | 7.0 | 5 | 0 | 0 | 8 | 83 | -37 +/- 26 | NA | | 0.1 |
| 6.1 23 | 9 | 7.0 | 9 | 0 | 0 | 8 | 83 | 37 +/- 34 | NA | | 0.1 |
| 6.1 24 | 9 | 7.0 | 8 | 0 | 0 | 8 | 83 | 18 +/- 32 | NA | | 0.1 |
| 6.1 25 | 9 | 7.0 | 5 | 0 | 0 | 8 | 83 | -37 +/- 26 | NA | | 0.1 |
| 6.1 26 | 9 | 7.0 | 4 | 0 | 0 | 8 | 83 | -55 +/- 24 | NA | | 0.1 |
| 6.1 27 | 9 | 7.0 | 3 | 0 | 0 | 8 | 83 | -74 +/- 21 | NA | | 0.1 |
| 6.1 28 | 9 | 7.0 | 1 | 0 | 0 | 8 | 83 | -111 +/- 14 | NA | | 0.1 |
| 6.1 29 | 9 | 7.0 | 2 | 0 | 0 | 8 | 83 | -92 +/- 18 | NA | | 0.1 |
| 6.1 30 | 9 | 7.0 | 1 | 0 | 0 | 8 | 83 | -111 +/- 14 | NA | | 0.1 |

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TABLE 7.1-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95

FINAL SURVEY DATA SHEET

DATA FOR UNAFFECTED AREA DESCRIPTION:

EXTERIOR ROOF OF PUMP ROOM - AREA 7.1 FOR UREM/HR

RADIATION TYPE: GAMMA SURVEY IN UREM/HR

COMPLETION DATE: 11/07/94

TECHNICIANS: JB/PK

LOCATION: 7.0

GRID ID: 7.1

MEDIA TYPE: CONCRETE

# of POINTS: 116

MATERIAL CODE

1=CONCRETE 5=PLASTIC

2=ROCK 6=SOIL

3=WOOD 7=ASPHALT

4=METAL 8=OTHER(SPECIFY):

NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | | LIMIT |
|---|---|---|---|
| MAX | 6.00 | PASS | 10 |
| AVG | 2.52 | PASS | 5 |
| STD X | 1.55 | | |
| MU SUB ALPHA | 2.76 | PASS | 5 |

| GRID ID # | COORIDINATES LETTER | # | INST. ID # | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|---|---|
| 7.1 | A | 1 | A | 6 | 8 | 8 | 2 |
| 7.1 | A | 2 | A | 6 | 7 | 8 | 1 |
| 7.1 | A | 3 | A | 6 | 12 | 8 | 6 |
| 7.1 | A | 4 | A | 6 | 7 | 8 | 1 |
| 7.1 | A | 5 | A | 6 | 8 | 8 | 2 |
| 7.1 | B | 1 | A | 6 | 8 | 8 | 2 |
| 7.1 | B | 2 | A | 6 | 8 | 8 | 2 |
| 7.1 | B | 3 | A | 6 | 9 | 8 | 3 |
| 7.1 | B | 4 | A | 6 | 11 | 8 | 5 |
| 7.1 | B | 5 | A | 6 | 8 | 8 | 2 |
| 7.1 | C | 1 | A | 6 | 9 | 8 | 3 |
| 7.1 | C | 2 | A | 6 | 9 | 8 | 3 |
| 7.1 | C | 3 | A | 6 | 10 | 8 | 4 |
| 7.1 | C | 4 | A | 6 | 7 | 8 | 1 |
| 7.1 | C | 5 | A | 6 | 8 | 8 | 2 |
| 7.1 | D | 1 | A | 6 | 12 | 8 | 6 |
| 7.1 | D | 2 | A | 6 | 8 | 8 | 2 |
| 7.1 | D | 3 | A | 6 | 9 | 8 | 3 |
| 7.1 | D | 4 | A | 6 | 5 | 8 | -1 |
| 7.1 | D | 5 | A | 6 | 7 | 8 | 1 |
| 7.1 | E | 1 | A | 6 | 9 | 8 | 3 |
| 7.1 | E | 2 | A | 6 | 7 | 8 | 1 |
| 7.1 | E | 3 | A | 6 | 11 | 8 | 5 |
| 7.1 | E | 4 | A | 6 | 11 | 8 | 5 |
| 7.1 | E | 5 | A | 6 | 8 | 8 | 2 |
| 7.1 | E | 6 | A | 6 | 9 | 8 | 3 |
| 7.1 | E | 7 | A | 6 | 10 | 8 | 4 |
| 7.1 | E | 8 | A | 6 | 9 | 8 | 3 |
| 7.1 | F | 1 | A | 6 | 7 | 8 | 1 |
| 7.1 | F | 2 | A | 6 | 8 | 8 | 2 |
| 7.1 | F | 3 | A | 6 | 8 | 8 | 2 |
| 7.1 | F | 4 | A | 6 | 9 | 8 | 3 |

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TABLE 7.1-1

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|---|---|---|---|---|---|---|---|
| 7.1 | F | 5 | A | 6 | 8 | B | 2 |
| 7.1 | F | 6 | A | 6 | 8 | B | 2 |
| 7.1 | F | 7 | A | 6 | 7 | B | 1 |
| 7.1 | F | 8 | A | 6 | 7 | B | 1 |
| 7.1 | G | 1 | A | 6 | 8 | B | 2 |
| 7.1 | G | 2 | A | 6 | 4 | B | -2 |
| 7.1 | G | 3 | A | 6 | 4 | B | -2 |
| 7.1 | G | 4 | A | 6 | 5 | B | -1 |
| 7.1 | G | 5 | A | 6 | 9 | B | 3 |
| 7.1 | G | 6 | A | 6 | 9 | B | 3 |
| 7.1 | G | 7 | A | 6 | 8 | B | 2 |
| 7.1 | G | 8 | A | 6 | 9 | B | 3 |
| 7.1 | H | 1 | A | 6 | 9 | B | 3 |
| 7.1 | H | 2 | A | 6 | 10 | B | 4 |
| 7.1 | H | 3 | A | 6 | 10 | B | 4 |
| 7.1 | H | 4 | A | 6 | 9 | B | 3 |
| 7.1 | H | 5 | A | 6 | 9 | B | 3 |
| 7.1 | H | 6 | A | 6 | 7 | B | 1 |
| 7.1 | H | 7 | A | 6 | 8 | B | 2 |
| 7.1 | H | 8 | A | 6 | 10 | B | 4 |
| 7.1 | I | 1 | A | 6 | 7 | B | 1 |
| 7.1 | I | 2 | A | 6 | 8 | B | 2 |
| 7.1 | I | 3 | A | 6 | 8 | B | 2 |
| 7.1 | I | 4 | A | 6 | 6 | B | 0 |
| 7.1 | I | 5 | A | 6 | 8 | B | 2 |
| 7.1 | I | 6 | A | 6 | 6 | B | 0 |
| 7.1 | I | 7 | A | 6 | 9 | B | 3 |
| 7.1 | I | 8 | A | 6 | 9 | B | 3 |
| 7.1 | J | 1 | A | 6 | 7 | B | 1 |
| 7.1 | J | 2 | A | 6 | 8 | B | 2 |
| 7.1 | J | 3 | A | 6 | 10 | B | 4 |
| 7.1 | J | 4 | A | 6 | 9 | B | 3 |
| 7.1 | J | 5 | A | 6 | 7 | B | 1 |
| 7.1 | J | 6 | A | 6 | 7 | B | 1 |
| 7.1 | J | 7 | A | 6 | 9 | B | 3 |
| 7.1 | J | 8 | A | 6 | 12 | B | 6 |
| 7.1 | K | 1 | A | 6 | 11 | B | 5 |
| 7.1 | K | 2 | A | 6 | 10 | B | 4 |
| 7.1 | K | 3 | A | 6 | 11 | B | 5 |
| 7.1 | K | 4 | A | 6 | 9 | B | 3 |
| 7.1 | K | 5 | A | 6 | 10 | B | 4 |
| 7.1 | K | 6 | A | 6 | 10 | B | 4 |
| 7.1 | K | 7 | A | 6 | 9 | B | 3 |
| 7.1 | K | 8 | A | 6 | 9 | B | 3 |
| 7.1 | L | 1 | A | 6 | 8 | B | 2 |
| 7.1 | L | 2 | A | 6 | 8 | B | 2 |
| 7.1 | L | 3 | A | 6 | 7 | B | 1 |
| 7.1 | L | 4 | A | 6 | 8 | B | 2 |
| 7.1 | L | 5 | A | 6 | 8 | B | 2 |
| 7.1 | L | 6 | A | 6 | 9 | B | 3 |
| 7.1 | L | 7 | A | 6 | 7 | B | 1 |
| 7.1 | L | 8 | A | 6 | 8 | B | 2 |
| 7.1 | M | 1 | A | 6 | 5 | B | -1 |
| 7.1 | M | 2 | A | 6 | 7 | B | 1 |
| 7.1 | M | 3 | A | 6 | 8 | B | 2 |
| 7.1 | M | 4 | A | 6 | 9 | B | 3 |
| 7.1 | M | 5 | A | 6 | 10 | B | 4 |
| 7.1 | M | 6 | A | 6 | 10 | B | 4 |
| 7.1 | M | 7 | A | 6 | 9 | B | 3 |
| 7.1 | M | 8 | A | 6 | 9 | B | 3 |

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TABLE 7.1-1

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 7.1 | N | 1 | A | 6 | 9 | B | 3 |
| 7.1 | N | 2 | A | 6 | 9 | B | 3 |
| 7.1 | N | 3 | A | 6 | 11 | B | 5 |
| 7.1 | N | 4 | A | 6 | 10 | B | 4 |
| 7.1 | N | 5 | A | 6 | 9 | B | 3 |
| 7.1 | N | 6 | A | 6 | 9 | B | 3 |
| 7.1 | N | 7 | A | 6 | 12 | B | 6 |
| 7.1 | N | 8 | A | 6 | 12 | B | 6 |
| 7.1 | O | 1 | A | 6 | 9 | B | 3 |
| 7.1 | O | 2 | A | 6 | 8 | B | 2 |
| 7.1 | O | 3 | A | 6 | 8 | B | 2 |
| 7.1 | O | 4 | A | 6 | 8 | B | 2 |
| 7.1 | O | 5 | A | 6 | 9 | B | 3 |
| 7.1 | O | 6 | A | 6 | 7 | B | 1 |
| 7.1 | O | 7 | A | 6 | 8 | B | 2 |
| 7.1 | O | 8 | A | 6 | 7 | B | 1 |
| 7.1 | P | 1 | A | 6 | 8 | B | 2 |
| 7.1 | P | 2 | A | 6 | 9 | B | 3 |
| 7.1 | P | 3 | A | 6 | 10 | B | 4 |
| 7.1 | P | 4 | A | 6 | 9 | B | 3 |
| 7.1 | P | 5 | A | 6 | 8 | B | 2 |
| 7.1 | P | 6 | A | 6 | 8 | B | 2 |
| 7.1 | P | 7 | A | 6 | 9 | B | 3 |
| 7.1 | P | 8 | A | 6 | 9 | B | 3 |

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ATTACHMENT 7.1-2

CIMTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:44 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
EXTERIOR ROOF OF SUMP ROOM - AREA 7.1 FOR BETA

RADIATION TYPE: 1 BETA SCALING FACTOR = 0.3
COMPLETION
DATE: 11/07/94
TECHNICIANS: JB/PK
LOCATION: 7.0
GRID ID: 7.1
MEDIA TYPE: CONCRETE
# of POINTS: 116 (>60)
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2
REM.+ FIXED:

| | | LIMIT |
|---|---|---|
| MAX FOR IND GRID | 4054 PASS | 13500 |
| AVG - SURVEY UNIT | 964 PASS | 13500 |
| STD X | 1115 | |
| MU SUB ALPHA | 1136 PASS | 13500 |
| MAX HOT SPOT | 16495 PASS | 40500 |

| GRID COORDINATES ID # | LETTER | # | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | SCAN MAX BETA COUNTS | TOTAL CONT. AREA CM^2 | MATER-IAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. BETA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 CM^2 | MAX TEST | INST CPM/ |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 7.1 | A | 1 | 6 | 526.6 | 600 | 0 | 0 | 8 | 2002 | 1343 +/- 916 | NA | | | 0.1 |
| 7.1 | A | 2 | 6 | 526.6 | 583 | 612 | 100 | 8 | 2002 | 1037 +/- 904 | | 1562 | | 0.1 |
| 7.1 | A | 3 | 6 | 526.6 | 684 | 697 | 100 | 8 | 2002 | 2882 +/- 973 | | 3117 | | 0.1 |
| 7.1 | A | 4 | 6 | 526.6 | 661 | 675 | 1000 | 8 | 2002 | 2484 +/- 958 | | 2715 | | 0.1 |
| 7.1 | A | 5 | 6 | 526.6 | 651 | 696 | 300 | 8 | 2002 | 2301 +/- 951 | | 3099 | | 0.1 |
| 7.1 | B | 1 | 6 | 542.7 | 575 | 0 | 0 | 8 | 2031 | 591 +/- 900 | NA | | | 0.1 |
| 7.1 | B | 2 | 6 | 526.6 | 600 | 628 | 100 | 8 | 2002 | 1348 +/- 916 | | 1855 | | 0.1 |
| 7.1 | B | 3 | 6 | 526.6 | 614 | 637 | 100 | 8 | 2002 | 1603 +/- 926 | | 2020 | | 0.1 |
| 7.1 | B | 4 | 6 | 526.6 | 660 | 682 | 4300 | 8 | 2002 | 2614 +/- 957 | | 2843 | | 0.1 |
| 7.1 | B | 5 | 6 | 526.6 | 608 | 0 | 0 | 8 | 2002 | 1489 +/- 922 | NA | | | 0.1 |
| 7.1 | C | 1 | 6 | 542.7 | 601 | 571 | 400 | 8 | 2031 | 1045 +/- 918 | | 518 | | 0.1 |
| 7.1 | C | 2 | 6 | 542.7 | 639 | 0 | 0 | 8 | 2031 | 1762 +/- 944 | NA | | | 0.1 |
| 7.1 | C | 3 | 6 | 542.7 | 599 | 0 | 0 | 8 | 2031 | 1030 +/- 917 | NA | | | 0.1 |
| 7.1 | C | 4 | 6 | 542.7 | 634 | 0 | 0 | 8 | 2031 | 1670 +/- 941 | NA | | | 0.1 |
| 7.1 | C | 5 | 6 | 526.6 | 654 | 659 | 2500 | 8 | 2002 | 2354 +/- 953 | | 2422 | | 0.1 |
| 7.1 | D | 1 | 6 | 542.7 | 635 | 0 | 0 | 8 | 2031 | 1689 +/- 941 | NA | | | 0.1 |
| 7.1 | D | 2 | 6 | 542.7 | 560 | 0 | 0 | 8 | 2031 | 317 +/- 889 | NA | | | 0.1 |
| 7.1 | D | 3 | 6 | 542.7 | 605 | 707 | 100 | 8 | 2031 | 1122 +/- 919 | | 3006 | | 0.1 |
| 7.1 | D | 4 | 6 | 526.6 | 618 | 630 | 700 | 8 | 2002 | 1688 +/- 929 | | 1892 | | 0.1 |
| 7.1 | D | 5 | 6 | 526.6 | 568 | 629 | 300 | 8 | 2002 | 791 +/- 893 | | 1873 | | 0.1 |
| 7.1 | E | 1 | 6 | 542.7 | 601 | 674 | 100 | 8 | 2031 | 1080 +/- 918 | | 2402 | | 0.1 |
| 7.1 | E | 2 | 6 | 542.7 | 648 | 0 | 0 | 8 | 2031 | 1926 +/- 950 | NA | | | 0.1 |
| 7.1 | E | 3 | 6 | 542.7 | 608 | 0 | 0 | 8 | 2031 | 1195 +/- 923 | NA | | | 0.1 |
| 7.1 | E | 4 | 6 | 669.3 | 597 | 0 | 0 | 8 | 2250 | -1323 +/- 924 | NA | | | 0.1 |
| 7.1 | E | 5 | 6 | 669.3 | 636 | 0 | 0 | 8 | 2250 | -609 +/- 951 | NA | | | 0.1 |
| 7.1 | E | 6 | 6 | 669.3 | 664 | 743 | 100 | 8 | 2250 | -83 +/- 969 | | 1348 | | 0.1 |
| 7.1 | E | 7 | 6 | 669.3 | 701 | 0 | 0 | 8 | 2250 | 580 +/- 994 | NA | | | 0.1 |
| 7.1 | E | 8 | 6 | 669.3 | 634 | 0 | 0 | 8 | 2250 | -646 +/- 949 | NA | | | 0.1 |
| 7.1 | F | 1 | 6 | 669.3 | 577 | 716 | 500 | 8 | 2250 | -1561 +/- 910 | | 854 | | 0.1 |

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EFF.
DPM

B22
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TABLE 7.1-2

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 7.1 | F | 2 | 6 | 669.3 | 642 | 0 | 0 | B | 2250 | -499 +/- 955 | NA | | 0.1 |
| 7.1 | F | 3 | 6 | 669.3 | 644 | 0 | 0 | B | 2250 | -463 +/- 956 | NA | | 0.1 |
| 7.1 | F | 4 | 6 | 669.3 | 569 | 0 | 0 | B | 2250 | -1835 +/- 904 | NA | | 0.1 |
| 7.1 | F | 5 | 6 | 669.3 | 590 | 798 | 200 | B | 2250 | -1375 +/- 919 | | 2355 | 0.1 |
| 7.1 | F | 6 | 6 | 669.3 | 608 | 786 | 100 | B | 2250 | -1089 +/- 932 | | 2135 | 0.1 |
| 7.1 | F | 7 | 6 | 669.3 | 651 | 0 | 0 | B | 2250 | -335 +/- 961 | NA | | 0.1 |
| 7.1 | F | 8 | 6 | 669.3 | 698 | 0 | 0 | B | 2250 | 525 +/- 992 | NA | | 0.1 |
| 7.1 | G | 1 | 6 | 559.4 | 629 | 0 | 0 | B | 2062 | 1273 +/- 938 | NA | | 0.1 |
| 7.1 | G | 2 | 6 | 669.3 | 598 | 765 | 100 | B | 2250 | -1274 +/- 925 | | 1751 | 0.1 |
| 7.1 | G | 3 | 6 | 669.3 | 618 | 0 | 0 | B | 2250 | -939 +/- 938 | NA | | 0.1 |
| 7.1 | G | 4 | 6 | 669.3 | 604 | 0 | 0 | B | 2250 | -1195 +/- 929 | NA | | 0.1 |
| 7.1 | G | 5 | 6 | 669.3 | 637 | 0 | 0 | B | 2250 | -591 +/- 951 | NA | | 0.1 |
| 7.1 | G | 6 | 6 | 590.9 | 718 | 690 | 100 | B | 2118 | 2320 +/-1000 | | 1813 | 0.1 |
| 7.1 | G | 7 | 2 | 565.8 | 633 | 691 | 200 | B | 2074 | 1251 +/- 942 | | 2292 | 0.1 |
| 7.1 | G | 8 | 2 | 565.8 | 622 | 0 | 0 | B | 2074 | 1029 +/- 935 | NA | | 0.1 |
| 7.1 | H | 1 | 6 | 559.4 | 606 | 0 | 0 | B | 2062 | 853 +/- 923 | NA | | 0.1 |
| 7.1 | H | 2 | 2 | 565.8 | 595 | 0 | 0 | B | 2074 | 535 +/- 916 | NA | | 0.1 |
| 7.1 | H | 3 | 2 | 565.8 | 603 | 0 | 0 | B | 2074 | 681 +/- 921 | NA | | 0.1 |
| 7.1 | H | 4 | 2 | 565.8 | 570 | 0 | 0 | B | 2074 | 77 +/- 898 | NA | | 0.1 |
| 7.1 | H | 5 | 2 | 565.8 | 583 | 0 | 0 | B | 2074 | 315 +/- 907 | NA | | 0.1 |
| 7.1 | H | 6 | 2 | 565.8 | 573 | 0 | 0 | B | 2074 | 132 +/- 900 | NA | | 0.1 |
| 7.1 | H | 7 | 2 | 565.8 | 693 | 0 | 0 | B | 2074 | 2328 +/- 982 | NA | | 0.1 |
| 7.1 | H | 8 | 2 | 565.8 | 671 | 0 | 0 | B | 2074 | 1926 +/- 968 | NA | | 0.1 |
| 7.1 | I | 1 | 6 | 559.4 | 680 | 0 | 0 | B | 2062 | 2206 +/- 973 | NA | | 0.1 |
| 7.1 | I | 2 | 2 | 565.8 | 616 | 0 | 0 | B | 2074 | 919 +/- 930 | NA | | 0.1 |
| 7.1 | I | 3 | 2 | 565.8 | 567 | 0 | 0 | B | 2074 | 22 +/- 896 | NA | | 0.1 |
| 7.1 | I | 4 | 2 | 565.8 | 558 | 0 | 0 | B | 2074 | -143 +/- 889 | NA | | 0.1 |
| 7.1 | I | 5 | 2 | 565.8 | 578 | 0 | 0 | B | 2074 | 223 +/- 904 | NA | | 0.1 |
| 7.1 | I | 6 | 2 | 565.8 | 596 | 0 | 0 | B | 2074 | 553 +/- 917 | NA | | 0.1 |
| 7.1 | I | 7 | 2 | 565.8 | 586 | 0 | 0 | B | 2074 | 370 +/- 909 | NA | | 0.1 |
| 7.1 | I | 8 | 2 | 565.8 | 593 | 0 | 0 | B | 2074 | 498 +/- 914 | NA | | 0.1 |
| 7.1 | J | 1 | 6 | 559.4 | 570 | 0 | 0 | B | 2062 | 194 +/- 897 | NA | | 0.1 |
| 7.1 | J | 2 | 2 | 565.8 | 614 | 0 | 0 | B | 2074 | 882 +/- 929 | NA | | 0.1 |
| 7.1 | J | 3 | 2 | 565.8 | 591 | 0 | 0 | B | 2074 | 461 +/- 913 | NA | | 0.1 |
| 7.1 | J | 4 | 2 | 565.8 | 605 | 0 | 0 | B | 2074 | 718 +/- 923 | NA | | 0.1 |
| 7.1 | J | 5 | 2 | 565.8 | 613 | 0 | 0 | B | 2074 | 864 +/- 928 | NA | | 0.1 |
| 7.1 | J | 6 | 2 | 565.8 | 591 | 0 | 0 | B | 2074 | 461 +/- 913 | NA | | 0.1 |
| 7.1 | J | 7 | 2 | 565.8 | 641 | 0 | 0 | B | 2074 | 1377 +/- 948 | NA | | 0.1 |
| 7.1 | J | 8 | 2 | 565.8 | 643 | 0 | 0 | B | 2074 | 1413 +/- 949 | NA | | 0.1 |
| 7.1 | K | 1 | 6 | 559.4 | 601 | 0 | 0 | B | 2062 | 761 +/- 919 | NA | | 0.1 |
| 7.1 | K | 2 | 2 | 565.8 | 658 | 0 | 0 | B | 2074 | 1688 +/- 959 | NA | | 0.1 |
| 7.1 | K | 3 | 2 | 565.8 | 575 | 0 | 0 | B | 2074 | 168 +/- 902 | NA | | 0.1 |
| 7.1 | K | 4 | 2 | 565.8 | 612 | 0 | 0 | B | 2074 | 846 +/- 928 | NA | | 0.1 |
| 7.1 | K | 5 | 2 | 565.8 | 588 | 0 | 0 | B | 2074 | 406 +/- 911 | NA | | 0.1 |
| 7.1 | K | 6 | 6 | 571.7 | 716 | 0 | 0 | B | 2084 | 2640 +/- 997 | NA | | 0.1 |
| 7.1 | K | 7 | 6 | 571.7 | 686 | 783 | 800 | B | 2084 | 2233 +/- 978 | | 3866 | 0.1 |
| 7.1 | K | 8 | 6 | 571.7 | 698 | 0 | 0 | B | 2084 | 2311 +/- 985 | NA | | 0.1 |
| 7.1 | L | 1 | 6 | 571.7 | 581 | 686 | 100 | B | 2084 | 189 +/- 906 | | 2091 | 0.1 |
| 7.1 | L | 2 | 6 | 571.7 | 582 | 0 | 0 | B | 2084 | 188 +/- 907 | NA | | 0.1 |
| 7.1 | L | 3 | 6 | 571.7 | 672 | 0 | 0 | B | 2084 | 1835 +/- 968 | NA | | 0.1 |
| 7.1 | L | 4 | 6 | 571.7 | 622 | 0 | 0 | B | 2084 | 920 +/- 934 | NA | | 0.1 |
| 7.1 | L | 5 | 6 | 571.7 | 632 | 0 | 0 | B | 2084 | 1103 +/- 941 | NA | | 0.1 |
| 7.1 | L | 6 | 6 | 571.7 | 640 | 0 | 0 | B | 2084 | 1250 +/- 947 | NA | | 0.1 |
| 7.1 | L | 7 | 6 | 571.7 | 712 | 715 | 200 | B | 2084 | 2568 +/- 994 | | 2622 | 0.1 |
| 7.1 | L | 8 | 6 | 571.7 | 672 | 0 | 0 | B | 2084 | 1835 +/- 968 | NA | | 0.1 |
| 7.1 | M | 1 | 6 | 559.4 | 587 | 0 | 0 | B | 2062 | 505 +/- 909 | NA | | 0.1 |
| 7.1 | M | 2 | 6 | 559.4 | 594 | 0 | 0 | B | 2062 | 633 +/- 914 | NA | | 0.1 |
| 7.1 | M | 3 | 6 | 559.4 | 546 | 0 | 0 | B | 2062 | -245 +/- 880 | NA | | 0.1 |
| 7.1 | M | 4 | 6 | 559.4 | 592 | 0 | 0 | B | 2062 | 596 +/- 913 | NA | | 0.1 |
| 7.1 | M | 5 | 6 | 559.4 | 655 | 0 | 0 | B | 2062 | 1749 +/- 956 | NA | | 0.1 |

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TABLE 7.1-2

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 7.1 | M | 6 | 6 | 559.4 | 781 | 0 | 0 | B | 2062 | 4054 +/-1037 | NA | | 0.1 |
| 7.1 | M | 7 | 6 | 559.4 | 627 | 0 | 0 | B | 2062 | 1237 +/- 937 | NA | | 0.1 |
| 7.1 | M | 8 | 6 | 559.4 | 654 | 0 | 0 | B | 2062 | 1731 +/- 955 | NA | | 0.1 |
| 7.1 | N | 1 | 6 | 559.4 | 644 | 0 | 0 | B | 2062 | 1548 +/- 949 | NA | | 0.1 |
| 7.1 | N | 2 | 6 | 559.4 | 573 | 0 | 0 | B | 2062 | 249 +/- 899 | NA | | 0.1 |
| 7.1 | N | 3 | 6 | 559.4 | 607 | 0 | 0 | B | 2062 | 871 +/- 923 | NA | | 0.1 |
| 7.1 | N | 4 | 6 | 559.4 | 634 | 0 | 0 | B | 2062 | 1365 +/- 942 | NA | | 0.1 |
| 7.1 | N | 5 | 6 | 559.4 | 664 | 0 | 0 | B | 2062 | 1914 +/- 962 | NA | | 0.1 |
| 7.1 | N | 6 | 6 | 559.4 | 660 | 0 | 0 | B | 2062 | 1840 +/- 959 | NA | | 0.1 |
| 7.1 | N | 7 | 6 | 559.4 | 732 | 1000 | 500 | B | 2062 | 3403 +/-1007 | | 8061 | 0.1 |
| 7.1 | N | 8 | 6 | 559.4 | 518 | 0 | 0 | B | 2062 | -757 +/- 859 | NA | | 0.1 |
| 7.1 | O | 1 | 6 | 559.4 | 6[illegible] | 0 | 0 | B | 2062 | 926 +/- 925 | NA | | 0.1 |
| 7.1 | O | 2 | 6 | 559.4 | 578 | 0 | 0 | B | 2062 | 340 +/- 903 | NA | | 0.1 |
| 7.1 | O | 3 | 6 | 559.4 | 616 | 0 | 0 | B | 2062 | 1035 +/- 930 | NA | | 0.1 |
| 7.1 | O | 4 | 6 | 559.4 | 603 | 0 | 0 | B | 2062 | 798 +/- 920 | NA | | 0.1 |
| 7.1 | O | 5 | 6 | 559.4 | 632 | 0 | 0 | B | 2062 | 1328 +/- 941 | NA | | 0.1 |
| 7.1 | O | 6 | 6 | 559.4 | 686 | 1461 | 100 | B | 2062 | 2458 +/- 977 | | 16495 | 0.1 |
| 7.1 | O | 7 | 6 | 559.4 | 694 | 0 | 0 | B | 2062 | 2462 +/- 982 | NA | | 0.1 |
| 7.1 | O | 8 | 6 | 559.4 | 678 | 785 | 100 | B | 2062 | 2189 +/- 971 | | 4127 | 0.1 |
| 7.1 | P | 1 | 6 | 559.4 | 643 | 0 | 0 | B | 2062 | 1529 +/- 948 | NA | | 0.1 |
| 7.1 | P | 2 | 6 | 559.4 | 607 | 0 | 0 | B | 2062 | 871 +/- 923 | NA | | 0.1 |
| 7.1 | P | 3 | 6 | 559.4 | 625 | 0 | 0 | B | 2062 | 1200 +/- 936 | NA | | 0.1 |
| 7.1 | P | 4 | 6 | 559.4 | 600 | 0 | 0 | B | 2062 | 743 +/- 918 | NA | | 0.1 |
| 7.1 | P | 5 | 6 | 559.4 | 652 | 0 | 0 | B | 2062 | 1694 +/- 954 | NA | | 0.1 |
| 7.1 | P | 6 | 6 | 559.4 | 576 | 702 | 100 | B | 2062 | 327 +/- 901 | | 2609 | 0.1 |
| 7.1 | P | 7 | 6 | 559.4 | 670 | 0 | 0 | B | 2062 | 2023 +/- 966 | NA | | 0.1 |
| 7.1 | P | 8 | 6 | 559.4 | 771 | 0 | 0 | B | 2062 | 3871 +/-1031 | NA | | 0.1 |

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TABLE 8.1-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:46 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
SPOILS PILE - AREA 8.1 FOR UREM/HR

RADIATION TYPE: GAMMA SURVEY IN UREM/HR
COMPLETION DATE: 10/25/94
TECHNICIANS: TA/CD/RW
LOCATION: 8.0
GRID ID: 8.1
MEDIA TYPE: SOIL
# of POINTS: 20

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | | LIMIT |
|---|---|---|---|
| MAX | 6.00 | PASS | 10 |
| AVG | 2.25 | PASS | 5 |
| STD X | 1.48 | | |
| MU SUB ALPHA | 2.82 | PASS | 5 |

| GRID ID # | COORIDINATES LETTER | # | INST. ID # | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|---|---|
| 8.1 | 1+37.5W | 1+17.5S | A | 6 | 10 | 8 | 4 |
| 8.1 | 1+37.5W | 1+12.5S | A | 6 | 10 | 8 | 4 |
| 8.1 | 1+35W | 1+15S | A | 6 | 8 | 8 | 2 |
| 8.1 | 1+32.5W | 1+17.5S | A | 6 | 7 | 8 | 1 |
| 8.1 | 1+32.5W | 1+12.5S | A | 6 | 8 | 8 | 2 |
| 8.1 | 1+47.5W | 1+17.5S | A | 6 | 8 | 8 | 2 |
| 8.1 | 1+47.5W | 1+12.5S | A | 6 | 10 | 8 | 4 |
| 8.1 | 1+45W | 1+15S | A | 6 | 7 | 8 | 1 |
| 8.1 | 1+42.5W | 1+17.5S | A | 6 | 8 | 8 | 2 |
| 8.1 | 1+42.5W | 1+12.5S | A | 6 | 8 | 8 | 2 |
| 8.1 | 1+37.5W | 1+27.5S | A | 6 | 10 | 8 | 4 |
| 8.1 | 1+37.5W | 1+22.5S | A | 6 | 7 | 8 | 1 |
| 8.1 | 1+35W | 1+25S | A | 6 | 8 | 8 | 2 |
| 8.1 | 1+32.5W | 1+27.5S | A | 6 | 7 | 8 | 1 |
| 8.1 | 1+32.5W | 1+22.5S | A | 6 | 6 | 8 | 0 |
| 8.1 | 1+47.5W | 1+27.5S | A | 6 | 7 | 8 | 1 |
| 8.1 | 1+47.5W | 1+22.5S | A | 6 | 9 | 8 | 3 |
| 8.1 | 1+45W | 1+25S | A | 6 | 7 | 8 | 1 |
| 8.1 | 1+42.5W | 1+27.5S | A | 6 | 12 | 8 | 6 |
| 8.1 | 1+42.5W | 1+22.5S | A | 6 | 8 | 8 | 2 |

ANSTEC
APERTURE
CARD

Also Available on
Aperture Card

TABLE 7.1-4

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:11 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 7.1 - EXTERIOR ROOF OF PUMP ROOM SOIL FOR SUM OF THE FRACTIONS

RADIATION TYPE: SOIL DATA FOR SUM OF THE FRACTIONS
COMPLETION
DATE: 11/07/94
TECHNICIANS: JB/PK
LOCATION: 7.0
GRID ID: 7.1
MEDIA TYPE: SOIL
# of POINTS: 2

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 0.27 | PASS | 1 |
| AVG | 0.24 | PASS | 1 |
| STD X | 0.05 | | |
| MU SUB ALPHA | 0.30 | PASS | 1 |

| | | ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED) | | | | | | | | ISOTOPES OF |
|---|---|---|---|---|---|---|---|---|---|---|
| ID # | GRID COORDINATES OR OTHER ID | SR-90 | CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SOIL CODE | SR-90 |
| | | LIMIT 17 | LIMIT 0.9 | LIMIT 1.1 | LIMIT 1.8 | LIMIT 3.8 | LIMIT 63 | LIMIT 2 | | |
| 7.1 | H8 | < 0.19 | < 0.064 | < 0.026 | < 0.042 | < 0.084 | < 0.320 | < 0.131 | 1 | < 0.011176 |
| 7.1 | J8 | < 0.19 | < 0.081 | < 0.055 | < 0.050 | < 0.064 | < 0.279 | < 0.177 | 1 | < 0.011176 |

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CONCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| 0.071 < | 0.023 < | 0.023 < | 0.000 < | 0.005 < | 0.066 | 0.199 |
| 0.090 < | 0.050 < | 0.028 < | 0.000 < | 0.004 < | 0.089 | 0.272 |

TABLE 7.1-3

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 7.1 | M | 6 | 6 | 1.4 | 14 | 0 | 0 | 8 | 46 | 70 +/- 41 | NA | | 0.1 |
| 7.1 | M | 7 | 6 | 1.4 | 3 | 0 | 0 | 8 | 46 | 9 +/- 19 | NA | | 0.1 |
| 7.1 | M | 8 | 6 | 1.4 | 6 | 0 | 0 | 8 | 46 | 26 +/- 27 | NA | | 0.1 |
| 7.1 | N | 1 | 6 | 1.4 | 4 | 0 | 0 | 8 | 46 | 14 +/- 22 | NA | | 0.1 |
| 7.1 | N | 2 | 6 | 1.4 | 2 | 0 | 0 | 8 | 46 | 3 +/- 16 | NA | | 0.1 |
| 7.1 | N | 3 | 6 | 1.4 | 4 | 0 | 0 | 8 | 46 | 14 +/- 22 | NA | | 0.1 |
| 7.1 | N | 4 | 6 | 1.4 | 9 | 0 | 0 | 8 | 46 | 42 +/- 33 | NA | | 0.1 |
| 7.1 | N | 5 | 6 | 1.4 | 6 | 0 | 0 | 8 | 46 | 26 +/- 27 | NA | | 0.1 |
| 7.1 | N | 6 | 6 | 1.4 | 4 | 0 | 0 | 8 | 46 | 14 +/- 22 | NA | | 0.1 |
| 7.1 | N | 7 | 6 | 1.4 | 5 | 7 | 500 | 8 | 46 | 21 +/- 25 | | 31 | 0.1 |
| 7.1 | N | 8 | 6 | 1.4 | 7 | 0 | 0 | 8 | 46 | 31 +/- 29 | NA | | 0.1 |
| 7.1 | O | 1 | 6 | 1.4 | 9 | 0 | 0 | 8 | 46 | 42 +/- 33 | NA | | 0.1 |
| 7.1 | O | 2 | 6 | 1.4 | 4 | 0 | 0 | 8 | 46 | 14 +/- 22 | NA | | 0.1 |
| 7.1 | O | 3 | 6 | 1.4 | 6 | 0 | 0 | 8 | 46 | 26 +/- 27 | NA | | 0.1 |
| 7.1 | O | 4 | 6 | 1.4 | 3 | 0 | 0 | 8 | 46 | 9 +/- 19 | NA | | 0.1 |
| 7.1 | O | 5 | 6 | 1.4 | 4 | 0 | 0 | 8 | 46 | 14 +/- 22 | NA | | 0.1 |
| 7.1 | O | 6 | 6 | 1.4 | 3 | 15 | 100 | 8 | 46 | 10 +/- 19 | | 75 | 0.1 |
| 7.1 | O | 7 | 6 | 1.4 | 5 | 0 | 0 | 8 | 46 | 20 +/- 25 | NA | | 0.1 |
| 7.1 | O | 8 | 6 | 1.4 | 9 | 5 | 100 | 8 | 46 | 42 +/- 33 | | 20 | 0.1 |
| 7.1 | P | 1 | 6 | 1.4 | 7 | 0 | 0 | 8 | 46 | 31 +/- 29 | NA | | 0.1 |
| 7.1 | P | 2 | 6 | 1.4 | 2 | 0 | 0 | 8 | 46 | 3 +/- 16 | NA | | 0.1 |
| 7.1 | P | 3 | 6 | 1.4 | 2 | 0 | 0 | 8 | 46 | 3 +/- 16 | NA | | 0.1 |
| 7.1 | P | 4 | 6 | 1.4 | 1 | 0 | 0 | 8 | 46 | -2 +/- 12 | NA | | 0.1 |
| 7.1 | P | 5 | 6 | 1.4 | 14 | 0 | 0 | 8 | 46 | 70 +/- 41 | NA | | 0.1 |
| 7.1 | P | 6 | 6 | 1.4 | 5 | 5 | 100 | 8 | 46 | 20 +/- 25 | | 20 | 0.1 |
| 7.1 | P | 7 | 6 | 1.4 | 4 | 0 | 0 | 8 | 46 | 14 +/- 22 | NA | | 0.1 |
| 7.1 | P | 8 | 6 | 1.4 | 6 | 0 | 0 | 8 | 46 | 26 +/- 27 | NA | | 0.1 |

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TABLE 7.1-3

| | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 7.1 | F | 2 | 6 | 1.2 | 5 | 0 | 0 | B | 43 | 21 +/- 25 | NA | | 0.1 |
| 7.1 | F | 3 | 6 | 1.2 | 4 | 0 | 0 | B | 43 | 16 +/- 22 | NA | | 0.1 |
| 7.1 | F | 4 | 6 | 1.2 | 3 | 0 | 0 | B | 43 | 10 +/- 19 | NA | | 0.1 |
| 7.1 | F | 5 | 6 | 1.2 | 3 | 5 | 200 | B | 43 | 10 +/- 19 | | 21 | 0.1 |
| 7.1 | F | 6 | 6 | 1.2 | 2 | 2 | 100 | B | 43 | 4 +/- 16 | | 4 | 0.1 |
| 7.1 | F | 7 | 6 | 1.2 | 1 | 0 | 0 | B | 43 | -1 +/- 12 | NA | | 0.1 |
| 7.1 | F | 8 | 6 | 1.2 | 3 | 0 | 0 | B | 43 | 10 +/- 19 | NA | | 0.1 |
| 7.1 | G | 1 | 6 | 1.4 | 5 | 0 | 0 | B | 46 | 20 +/- 25 | NA | | 0.1 |
| 7.1 | G | 2 | 6 | 1.2 | 2 | 3 | 100 | B | 43 | 4 +/- 16 | | 10 | 0.1 |
| 7.1 | G | 3 | 6 | 1.2 | 3 | 0 | 0 | B | 43 | 10 +/- 19 | NA | | 0.1 |
| 7.1 | G | 4 | 6 | 1.2 | 3 | 0 | 0 | B | 43 | 10 +/- 19 | NA | | 0.1 |
| 7.1 | G | 5 | 6 | 1.2 | 1 | 0 | 0 | B | 43 | -1 +/- 12 | NA | | 0.1 |
| 7.1 | G | 6 | 6 | 1.7 | 8 | 10 | 100 | B | 49 | 35 +/- 31 | | 46 | 0.1 |
| 7.1 | G | 7 | 2 | 1.7 | 3 | 7 | 200 | B | 45 | 7 +/- 18 | | 27 | 0.1 |
| 7.1 | G | 8 | 2 | 1.7 | 0 | 0 | 0 | B | 45 | -9 +/- 4 | NA | | 0.1 |
| 7.1 | H | 1 | 6 | 1.4 | 6 | 0 | 0 | B | 46 | 26 +/- 27 | NA | | 0.1 |
| 7.1 | H | 2 | 2 | 1.7 | 5 | 0 | 0 | B | 45 | 17 +/- 23 | NA | | 0.1 |
| 7.1 | H | 3 | 2 | 1.7 | 4 | 0 | 0 | B | 45 | 12 +/- 20 | NA | | 0.1 |
| 7.1 | H | 4 | 2 | 1.7 | 4 | 0 | 0 | B | 45 | 12 +/- 20 | NA | | 0.1 |
| 7.1 | H | 5 | 2 | 1.7 | 7 | 0 | 0 | B | 45 | 27 +/- 27 | NA | | 0.1 |
| 7.1 | H | 6 | 2 | 1.7 | 2 | 0 | 0 | B | 45 | 2 +/- 15 | NA | | 0.1 |
| 7.1 | H | 7 | 2 | 1.7 | 6 | 0 | 0 | B | 45 | 22 +/- 25 | NA | | 0.1 |
| 7.1 | H | 8 | 2 | 1.7 | 5 | 0 | 0 | B | 45 | 17 +/- 23 | NA | | 0.1 |
| 7.1 | I | 1 | 6 | 1.4 | 7 | 0 | 0 | B | 46 | 31 +/- 29 | NA | | 0.1 |
| 7.1 | I | 2 | 2 | 1.7 | 6 | 0 | 0 | B | 45 | 22 +/- 25 | NA | | 0.1 |
| 7.1 | I | 3 | 2 | 1.7 | 3 | 0 | 0 | B | 45 | 7 +/- 18 | NA | | 0.1 |
| 7.1 | I | 4 | 2 | 1.7 | 1 | 0 | 0 | B | 45 | -4 +/- 11 | NA | | 0.1 |
| 7.1 | I | 5 | 2 | 1.7 | 7 | 0 | 0 | B | 45 | 27 +/- 27 | NA | | 0.1 |
| 7.1 | I | 6 | 2 | 1.7 | 3 | 0 | 0 | B | 45 | 7 +/- 18 | NA | | 0.1 |
| 7.1 | I | 7 | 2 | 1.7 | 4 | 0 | 0 | B | 45 | 12 +/- 20 | NA | | 0.1 |
| 7.1 | I | 8 | 2 | 1.7 | 3 | 0 | 0 | B | 45 | 7 +/- 18 | NA | | 0.1 |
| 7.1 | J | 1 | 6 | 1.4 | 6 | 0 | 0 | B | 46 | 26 +/- 27 | NA | | 0.1 |
| 7.1 | J | 2 | 2 | 1.7 | 9 | 0 | 0 | B | 45 | 37 +/- 30 | NA | | 0.1 |
| 7.1 | J | 3 | 2 | 1.7 | 4 | 0 | 0 | B | 45 | 12 +/- 20 | NA | | 0.1 |
| 7.1 | J | 4 | 2 | 1.7 | 3 | 0 | 0 | B | 45 | 7 +/- 18 | NA | | 0.1 |
| 7.1 | J | 5 | 2 | 1.7 | 2 | 0 | 0 | B | 45 | 2 +/- 15 | NA | | 0.1 |
| 7.1 | J | 6 | 2 | 1.7 | 3 | 0 | 0 | B | 45 | 7 +/- 18 | NA | | 0.1 |
| 7.1 | J | 7 | 2 | 1.7 | 4 | 0 | 0 | B | 45 | 12 +/- 20 | NA | | 0.1 |
| 7.1 | J | 8 | 2 | 1.7 | 4 | 0 | 0 | B | 45 | 12 +/- 20 | NA | | 0.1 |
| 7.1 | K | 1 | 6 | 1.4 | 10 | 0 | 0 | B | 46 | 48 +/- 35 | NA | | 0.1 |
| 7.1 | K | 2 | 2 | 1.7 | 2 | 0 | 0 | B | 45 | 2 +/- 15 | NA | | 0.1 |
| 7.1 | K | 3 | 2 | 1.7 | 4 | 0 | 0 | B | 45 | 12 +/- 20 | NA | | 0.1 |
| 7.1 | K | 4 | 2 | 1.7 | 3 | 0 | 0 | B | 45 | 7 +/- 18 | NA | | 0.1 |
| 7.1 | K | 5 | 2 | 1.7 | 1 | 0 | 0 | B | 45 | -4 +/- 11 | NA | | 0.1 |
| 7.1 | K | 6 | 6 | 0.8 | 4 | 0 | 0 | B | 38 | 18 +/- 22 | NA | | 0.1 |
| 7.1 | K | 7 | 6 | 0.8 | 2 | 4 | 800 | B | 38 | 8 +/- 16 | | 18 | 0.1 |
| 7.1 | K | 8 | 6 | 0.8 | 0 | 0 | 0 | B | 38 | -4 +/- 3 | NA | | 0.1 |
| 7.1 | L | 1 | 6 | 0.8 | 2 | 2 | 100 | B | 38 | 7 +/- 16 | | 7 | 0.1 |
| 7.1 | L | 2 | 6 | 0.8 | 5 | 0 | 0 | B | 38 | 23 +/- 25 | NA | | 0.1 |
| 7.1 | L | 3 | 6 | 0.8 | 4 | 0 | 0 | B | 38 | 18 +/- 22 | NA | | 0.1 |
| 7.1 | L | 4 | 6 | 0.8 | 4 | 0 | 0 | B | 38 | 18 +/- 22 | NA | | 0.1 |
| 7.1 | L | 5 | 6 | 0.8 | 5 | 0 | 0 | B | 38 | 23 +/- 25 | NA | | 0.1 |
| 7.1 | L | 6 | 6 | 0.8 | 4 | 0 | 0 | B | 38 | 18 +/- 22 | NA | | 0.1 |
| 7.1 | L | 7 | 6 | 0.8 | 4 | 5 | 200 | B | 38 | 18 +/- 22 | | 23 | 0.1 |
| 7.1 | L | 8 | 6 | 0.8 | 3 | 0 | 0 | B | 38 | 12 +/- 19 | NA | | 0.1 |
| 7.1 | M | 1 | 6 | 1.4 | 1 | 0 | 0 | B | 46 | -2 +/- 12 | NA | | 0.1 |
| 7.1 | M | 2 | 6 | 1.4 | 5 | 0 | 0 | B | 46 | 20 +/- 25 | NA | | 0.1 |
| 7.1 | M | 3 | 6 | 1.4 | 2 | 0 | 0 | B | 46 | 3 +/- 16 | NA | | 0.1 |
| 7.1 | M | 4 | 6 | 1.4 | 4 | 0 | 0 | B | 46 | 14 +/- 22 | NA | | 0.1 |
| 7.1 | M | 5 | 6 | 1.4 | 12 | 0 | 0 | B | 46 | 59 +/- 38 | NA | | 0.1 |

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CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:43 AM

FINAL SURVEY DATA SHEET

DATA FOR AFFECTED AREA DESCRIPTION:

EXTERIOR ROOF OF PUMP ROOM - AREA 7.1 FOR ALPHA

RADIATION TYPE: 2

COMPLETION

DATE: 11-7-94

| | | | |
|---|---|---|---|
| TECHNICIANS: | PB/PK | MATERIAL CODE | |
| LOCATION: | 7.0 | 1=CONCRETE | 5=PLASTIC |
| GRID ID: | 7.1 | 2=ROCK | 6=SOIL |
| MEDIA TYPE: | CONCRETE | 3=WOOD | 7=ASPHALT |
| # of POINTS: | 116 (>60) | 4=METAL | 8=OTHER(SPECIFY): |
| CT IN MINUTES: | 1 | | NO MATERIAL BACKGROUND USED |

DPM/100CM^2

| REM.+ FIXED: | | | LIMIT |
|---|---|---|---|
| MAX FOR IND GRID | 70 | PASS | 5000 |
| AVG - SURVEY UNIT | 15 | PASS | 5000 |
| STD X | 14 | | |
| MU SUB ALPHA | 17 | PASS | 5000 |
| MAX HOT SPOT | 75 | PASS | 15000 |

| ID # | GRID CODRIDINATES LETTER | # | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | SCAN MAX ALPHA COUNTS | TOTAL CONT. AREA CM^2 | MATER-IAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. ALPHA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 CM^2 | MAX TEST | INST E CPM/D |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 7.1 | A | 1 | 6 | 1.1 | 2 | 0 | 0 | 8 | 42 | 5 +/- 16 | NA | | | 0.18 |
| 7.1 | A | 2 | 6 | 1.1 | 1 | 0 | 100 | 8 | 42 | -1 +/- 11 | NA | | | 0.18 |
| 7.1 | A | 3 | 6 | 1.1 | 1 | 2 | 100 | 8 | 42 | -0 +/- 11 | | 5 | | 0.18 |
| 7.1 | A | 4 | 2 | 1.1 | 0 | 2 | 1000 | 8 | 39 | -5 +/- 3 | | 5 | | 0.19 |
| 7.1 | A | 5 | 6 | 1.1 | 6 | 1 | 300 | 8 | 42 | 26 +/- 27 | | -1 | | 0.18 |
| 7.1 | B | 1 | 6 | 1.1 | 1 | 0 | 0 | 8 | 42 | -1 +/- 11 | NA | | | 0.18 |
| 7.1 | B | 2 | 6 | 1.1 | 4 | 4 | 100 | 8 | 42 | 16 +/- 22 | | 16 | | 0.18 |
| 7.1 | B | 3 | 6 | 1.1 | 5 | 5 | 100 | 8 | 42 | 22 +/- 25 | | 22 | | 0.18 |
| 7.1 | B | 4 | 6 | 1.1 | 1 | 6 | 4300 | 8 | 42 | 11 +/- 11 | | 27 | | 0.18 |
| 7.1 | B | 5 | 6 | 1.1 | 6 | 0 | 0 | 8 | 42 | 27 +/- 27 | NA | | | 0.18 |
| 7.1 | C | 1 | 6 | 1.1 | 3 | 3 | 400 | 8 | 42 | 11 +/- 19 | | 11 | | 0.18 |
| 7.1 | C | 2 | 6 | 1.1 | 0 | 0 | 0 | 8 | 42 | -6 +/- 4 | NA | | | 0.18 |
| 7.1 | C | 3 | 6 | 1.1 | 3 | 0 | 0 | 8 | 42 | 11 +/- 19 | NA | | | 0.18 |
| 7.1 | C | 4 | 6 | 1.1 | 4 | 0 | 0 | 8 | 42 | 16 +/- 22 | NA | | | 0.18 |
| 7.1 | C | 5 | 6 | 1.1 | 3 | 4 | 2500 | 8 | 42 | 12 +/- 19 | | 16 | | 0.18 |
| 7.1 | D | 1 | 6 | 1.1 | 5 | 0 | 0 | 8 | 42 | 22 +/- 25 | NA | | | 0.18 |
| 7.1 | D | 2 | 6 | 1.1 | 3 | 0 | 0 | 8 | 42 | 11 +/- 19 | NA | | | 0.18 |
| 7.1 | D | 3 | 6 | 1.1 | 4 | 5 | 100 | 8 | 42 | 16 +/- 22 | | 22 | | 0.18 |
| 7.1 | D | 4 | 6 | 1.1 | 2 | 5 | 700 | 8 | 42 | 6 +/- 16 | | 22 | | 0.18 |
| 7.1 | D | 5 | 6 | 1.1 | 3 | 1 | 300 | 8 | 42 | 10 +/- 19 | | -1 | | 0.18 |
| 7.1 | E | 1 | 6 | 1.1 | 3 | 2 | 100 | 8 | 42 | 10 +/- 19 | | 5 | | 0.18 |
| 7.1 | E | 2 | 6 | 1.1 | 5 | 0 | 0 | 8 | 42 | 22 +/- 25 | NA | | | 0.18 |
| 7.1 | E | 3 | 6 | 1.1 | 2 | 0 | 0 | 8 | 42 | 5 +/- 16 | NA | | | 0.18 |
| 7.1 | E | 4 | 6 | 1.2 | 5 | 0 | 0 | 8 | 43 | 21 +/- 25 | NA | | | 0.18 |
| 7.1 | E | 5 | 6 | 1.2 | 7 | 0 | 0 | 8 | 43 | 32 +/- 29 | NA | | | 0.18 |
| 7.1 | E | 6 | 6 | 1.2 | 1 | 1 | 100 | 8 | 43 | -1 +/- 12 | | -1 | | 0.18 |
| 7.1 | E | 7 | 6 | 1.2 | 2 | 0 | 0 | 8 | 43 | 4 +/- 16 | NA | | | 0.18 |
| 7.1 | E | 8 | 6 | 1.2 | 4 | 0 | 0 | 8 | 43 | 16 +/- 22 | NA | | | 0.18 |
| 7.1 | F | 1 | 6 | 1.2 | 2 | 1 | 500 | 8 | 43 | 4 +/- 16 | | -1 | | 0.18 |

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TABLE B.1-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:11 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA B.1 - SOUTH SPOILS PILE

RADIATION TYPE: SOIL DATA FOR SUM OF THE FRACTIONS
COMPLETION
DATE:
TECHNICIANS: ENV. DEPT.
LOCATION: B.0
GRID ID: B.1
MEDIA TYPE: SOIL
# of POINTS: 70

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 0.86 | PASS | 1 |
| AVG | 0.20 | PASS | 1 |
| STD X | 0.10 | | |
| MU SUB ALPHA | 0.22 | PASS | 1 |

| PDL ID # | DESCRIPTION | VOL IN CU FT | SR-90 LIMIT | CO-60 LIMIT | AG-108M LIMIT | CS-134 LIMIT | CS-137 LIMIT | CE-144 LIMIT | EU-152 LIMIT | SOIL CODE | SR-90 | CO |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | 17 | 0.9 | 1.1 | 1.8 | 3.8 | 63 | 2 | | | |
| | ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED) | | | | | | | | | | ISOTOPES OF C | |
| 396 | HUT LEVEL3 | 756 | < 0.050 | < 0.050 | * | < 0.060 | < 0.050 | < 0.300 | * | 1 | < 0.002941 | < |
| 397 | HUT LEVEL4 | 1323 | 0.065 | < 0.060 | * | < 0.060 | < 0.060 | < 0.400 | * | 1 | 0.003824 | < |
| 399 | HUT LEVEL5 | 1512 | < 0.050 | < 0.040 | * | < 0.050 | < 0.040 | < 0.200 | * | 1 | < 0.002941 | < |
| 406 | HUT LEVEL6 | 1701 | < 0.060 | < 0.030 | * | < 0.040 | < 0.040 | < 0.200 | * | 1 | < 0.003529 | < |
| 428 | HUT LEVEL4 | 3780 | 0.065 | < 0.060 | * | < 0.060 | < 0.060 | < 0.400 | * | 1 | 0.003824 | < |
| 437 | HUT LEVEL7 | 1620 | < 0.050 | < 0.050 | * | < 0.060 | < 0.050 | < 0.300 | * | 1 | < 0.002941 | < |
| 444 | HUT LEVEL2 | 4212 | 0.051 | < 0.030 | * | < 0.040 | < 0.040 | < 0.200 | * | 1 | 0.003 | < |
| 580 | UE-001 | 96 | < 0.200 | < 0.021 | < 0.013 | < 0.107 | 0.110 | < 0.360 | < 0.086 | 1 | < 0.011765 | < |
| 595 | UE-005 | 96 | 0.700 | < 0.027 | < 0.032 | < 0.123 | 0.508 | < 0.671 | < 0.113 | 1 | 0.041176 | < |
| 618 | UE-007 | 96 | < 0.200 | < 0.034 | < 0.033 | < 0.111 | < 0.065 | < 0.267 | < 0.112 | 1 | < 0.011765 | < |
| 5209 | STB-05 | 96 | < 0.220 | < 0.058 | < 0.041 | < 0.039 | 0.126 | < 0.299 | < 0.080 | 1 | < 0.012941 | < |
| 5208 | STB-04 | 96 | < 0.220 | < 0.053 | < 0.027 | < 0.056 | 0.133 | < 0.283 | < 0.107 | 1 | < 0.012941 | < |
| 5207 | STB-03 | 96 | < 0.220 | < 0.022 | < 0.037 | < 0.037 | < 0.035 | < 0.242 | 0.314 | 1 | < 0.012941 | < |
| 5206 | STB-02 | 96 | < 0.220 | < 0.022 | < 0.015 | < 0.042 | < 0.037 | < 0.217 | < 0.105 | 1 | < 0.012941 | < |
| 5205 | STB-01 | 96 | < 0.220 | < 0.089 | < 0.044 | < 0.133 | 0.107 | < 0.631 | < 0.049 | 1 | < 0.012941 | < |
| 5310 | STB-06 | 96 | < 0.220 | < 0.022 | < 0.022 | < 0.045 | < 0.055 | < 0.288 | < 0.069 | 1 | < 0.012941 | < |
| 5311 | STB-07 | 96 | < 0.220 | < 0.077 | < 0.021 | < 0.127 | 0.106 | < 0.604 | < 0.160 | 1 | < 0.012941 | < |
| 5312 | STB-08 | 96 | < 0.220 | < 0.031 | < 0.050 | < 0.132 | 0.104 | < 0.667 | < 0.130 | 1 | < 0.012941 | < |
| 5313 | STB-09 | 96 | < 0.220 | < 0.034 | < 0.050 | < 0.048 | 0.082 | < 0.337 | < 0.047 | 1 | < 0.012941 | < |
| 5314 | STB-010 | 96 | < 0.220 | < 0.036 | < 0.041 | < 0.135 | 0.077 | < 0.653 | < 0.094 | 1 | < 0.012941 | < |
| 5315 | STB-011 | 96 | < 0.220 | < 0.084 | < 0.038 | < 0.133 | < 0.096 | < 0.694 | < 0.079 | 1 | < 0.012941 | < |
| 5316 | STB-012 | 96 | < 0.220 | < 0.052 | < 0.029 | < 0.042 | < 0.066 | < 0.329 | < 0.117 | 1 | < 0.012941 | < |
| 5422 | STB-018 | 96 | < 0.220 | < 0.033 | < 0.031 | < 0.121 | 0.081 | < 0.634 | < 0.035 | 1 | < 0.012941 | < |
| 5423 | STB-019 | 96 | < 0.220 | < 0.061 | < 0.026 | < 0.045 | 0.110 | < 0.314 | < 0.101 | 1 | < 0.012941 | < |
| 5424 | STB-020 | 96 | < 0.220 | < 0.068 | < 0.024 | < 0.118 | 0.083 | < 0.669 | < 0.090 | 1 | < 0.012941 | < |
| 5317 | STB-013 | 96 | < 0.220 | < 0.045 | < 0.029 | < 0.038 | 0.113 | < 0.295 | < 0.117 | 1 | < 0.012941 | < |
| 5318 | STB-014 | 96 | < 0.220 | < 0.029 | < 0.027 | < 0.134 | 0.101 | < 0.656 | < 0.130 | 1 | < 0.012941 | < |
| 5319 | STB-015 | 96 | < 0.220 | < 0.025 | < 0.024 | < 0.038 | < 0.052 | < 0.186 | < 0.158 | 1 | < 0.012941 | < |
| 5420 | STB-016 | 96 | < 0.220 | < 0.043 | < 0.044 | < 0.037 | < 0.044 | < 0.290 | < 0.096 | 1 | < 0.012941 | < |
| 5421 | STB-017 | 96 | < 0.220 | < 0.037 | < 0.024 | < 0.130 | 0.078 | < 0.614 | < 0.114 | 1 | < 0.012941 | < |
| 5426 | STB-022 | 96 | < 0.220 | < 0.037 | < 0.032 | < 0.118 | 0.074 | < 0.630 | < 0.052 | 1 | < 0.012941 | < |
| 5425 | STB-021 | 96 | < 0.220 | < 0.045 | < 0.039 | < 0.042 | < 0.055 | < 0.267 | < 0.035 | 1 | < 0.012941 | < |

ANSTEC APERTURE CARD

Also Available on Aperture Card

ONCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| -60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| 0.056 | 0.000 < | 0.033 < | 0.000 < | 0.005 | 0.000 | 0.097 |
| 0.067 | 0.000 < | 0.033 < | 0.000 < | 0.006 | 0.000 | 0.110 |
| 0.044 | 0.000 < | 0.028 < | 0.000 < | 0.003 | 0.000 | 0.078 |
| 0.033 | 0.000 < | 0.022 < | 0.000 < | 0.003 | 0.000 | 0.062 |
| 0.067 | 0.000 < | 0.033 < | 0.000 < | 0.006 | 0.000 | 0.110 |
| 0.056 | 0.000 < | 0.033 < | 0.000 < | 0.005 | 0.000 | 0.097 |
| 0.033 | 0.000 < | 0.022 < | 0.000 < | 0.003 | 0.000 | 0.062 |
| 0.023 < | 0.012 < | 0.059 | 0.000 < | 0.006 < | 0.043 | 0.155 |
| 0.030 < | 0.029 < | 0.068 | 0.000 < | 0.011 < | 0.057 | 0.236 |
| 0.038 < | 0.030 < | 0.062 < | 0.000 < | 0.004 < | 0.056 | 0.202 |
| 0.064 < | 0.038 < | 0.021 | 0.000 < | 0.005 < | 0.040 | 0.181 |
| 0.059 < | 0.024 < | 0.031 | 0.000 < | 0.004 < | 0.054 | 0.185 |
| 0.025 < | 0.033 < | 0.020 < | 0.000 < | 0.004 | 0.157 | 0.252 |
| 0.025 < | 0.014 < | 0.023 < | 0.000 < | 0.003 < | 0.053 | 0.131 |
| 0.099 < | 0.040 < | 0.074 | 0.000 < | 0.010 < | 0.024 | 0.260 |
| 0.025 < | 0.020 < | 0.025 < | 0.000 < | 0.005 < | 0.034 | 0.121 |
| 0.086 < | 0.019 < | 0.071 | 0.000 < | 0.010 < | 0.080 | 0.278 |
| 0.035 < | 0.045 < | 0.073 | 0.000 < | 0.011 < | 0.065 | 0.242 |
| 0.038 < | 0.046 < | 0.026 | 0.000 < | 0.005 < | 0.023 | 0.152 |
| 0.040 < | 0.037 < | 0.075 | 0.000 < | 0.010 < | 0.047 | 0.222 |
| 0.093 < | 0.034 < | 0.074 < | 0.000 < | 0.011 < | 0.039 | 0.265 |
| 0.058 < | 0.026 < | 0.023 < | 0.000 < | 0.005 < | 0.059 | 0.184 |
| 0.037 < | 0.028 < | 0.067 | 0.000 < | 0.010 < | 0.018 | 0.173 |
| 0.068 < | 0.023 < | 0.025 | 0.000 < | 0.005 < | 0.051 | 0.184 |
| 0.076 < | 0.022 < | 0.066 | 0.000 < | 0.011 < | 0.045 | 0.231 |
| 0.050 < | 0.027 < | 0.021 | 0.000 < | 0.005 < | 0.059 | 0.173 |
| 0.032 < | 0.024 < | 0.074 | 0.000 < | 0.010 < | 0.065 | 0.219 |
| 0.027 < | 0.022 < | 0.021 < | 0.000 < | 0.003 < | 0.079 | 0.165 |
| 0.048 < | 0.040 < | 0.021 < | 0.000 < | 0.005 < | 0.068 | 0.174 |
| 0.041 < | 0.022 < | 0.072 | 0.000 < | 0.010 < | 0.057 | 0.215 |
| 0.041 < | 0.029 < | 0.066 | 0.000 < | 0.010 < | 0.026 | 0.185 |
| 0.050 < | 0.035 < | 0.023 < | 0.000 < | 0.004 < | 0.018 | 0.143 |

TABLE B.1-2

| | | |

| | | | | | | |
|---|---|---|---|---|---|---|
| 0.027 < | 0.015 < | 0.023 | 0.000 < | 0.003 < | 0.059 | 0.140 |
| 0.029 < | 0.021 < | 0.021 < | 0.000 < | 0.002 < | 0.049 | 0.135 |
| 0.055 < | 0.017 < | 0.072 < | 0.000 < | 0.011 < | 0.034 | 0.201 |
| 0.104 < | 0.022 < | 0.074 | 0.000 < | 0.010 < | 0.042 | 0.264 |
| 0.057 < | 0.034 < | 0.023 < | 0.000 < | 0.004 < | 0.083 | 0.214 |
| 0.027 < | 0.032 < | 0.025 < | 0.000 < | 0.003 < | 0.041 | 0.142 |
| 0.026 < | 0.028 < | 0.067 | 0.000 < | 0.010 < | 0.099 | 0.242 |
| 0.033 < | 0.024 < | 0.023 | 0.000 < | 0.004 < | 0.053 | 0.149 |
| 0.034 < | 0.037 < | 0.069 | 0.000 < | 0.006 < | 0.045 | 0.204 |
| 0.040 < | 0.017 < | 0.026 | 0.000 < | 0.004 < | 0.039 | 0.138 |
| 0.027 < | 0.042 < | 0.069 | 0.000 < | 0.010 < | 0.046 | 0.206 |
| 0.056 < | 0.034 < | 0.024 | 0.000 < | 0.004 < | 0.028 | 0.159 |
| 0.043 < | 0.023 < | 0.064 | 0.000 < | 0.010 < | 0.026 | 0.180 |
| 0.045 < | 0.055 < | 0.077 | 0.000 < | 0.011 < | 0.082 | 0.283 |
| 0.064 < | 0.035 < | 0.081 | 0.000 < | 0.012 < | 0.075 | 0.279 |
| 0.072 < | 0.017 < | 0.025 | 0.000 < | 0.003 < | 0.067 | 0.197 |
| 0.041 < | 0.011 < | 0.068 | 0.000 < | 0.009 < | 0.066 | 0.208 |
| 0.027 < | 0.015 < | 0.077 | 0.000 < | 0.011 < | 0.055 | 0.198 |
| 0.040 < | 0.022 < | 0.022 | 0.000 < | 0.005 < | 0.059 | 0.161 |
| 0.036 < | 0.033 < | 0.022 | 0.000 < | 0.003 < | 0.105 | 0.212 |
| 0.039 < | 0.014 < | 0.026 < | 0.000 < | 0.005 < | 0.035 | 0.132 |
| 0.022 < | 0.026 < | 0.023 | 0.000 < | 0.003 < | 0.062 | 0.148 |
| 0.027 < | 0.015 < | 0.023 | 0.000 < | 0.004 < | 0.056 | 0.138 |
| 0.049 < | 0.020 < | 0.072 | 0.000 < | 0.010 < | 0.039 | 0.204 |
| 0.035 < | 0.044 < | 0.070 | 0.000 < | 0.009 < | 0.024 | 0.195 |
| 0.023 < | 0.018 < | 0.068 | 0.000 < | 0.010 < | 0.027 | 0.160 |
| 0.076 < | 0.027 < | 0.069 < | 0.000 < | 0.010 < | 0.058 | 0.253 |
| 0.046 < | 0.015 < | 0.069 | 0.000 < | 0.011 < | 0.054 | 0.209 |
| 0.048 < | 0.026 < | 0.026 | 0.000 < | 0.004 < | 0.034 | 0.150 |
| 0.044 < | 0.014 < | 0.023 < | 0.000 < | 0.003 < | 0.038 | 0.136 |
| 0.029 < | 0.030 < | 0.071 | 0.000 < | 0.010 < | 0.042 | 0.195 |
| 0.027 < | 0.014 < | 0.021 < | 0.000 < | 0.002 < | 0.072 | 0.149 |
| 0.029 < | 0.018 < | 0.027 < | 0.000 < | 0.005 < | 0.061 | 0.246 |
| 0.042 < | 0.036 < | 0.026 | 0.000 < | 0.005 < | 0.028 | 0.225 |
| 0.089 < | 0.036 < | 0.077 | 0.482 < | 0.012 < | 0.073 | 0.856 |
| 0.049 < | 0.029 < | 0.073 | 0.000 < | 0.011 < | 0.094 | 0.268 |
| 0.149 < | 0.016 < | 0.071 < | 0.000 < | 0.011 < | 0.053 | 0.408 |
| 0.051 < | 0.041 < | 0.024 | 0.000 < | 0.004 < | 0.050 | 0.182 |

ANSTEC APERTURE CARD

Also Available on Aperture Card

TABLE B.2-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
DRIVEWAY - AREA B.2 FOR UREM

RADIATION TYPE: GAMMA SURVEY IN UREM/HR
COMPLETION
DATE: 10-17-94
TECHNICIANS: MANY
LOCATION: B.0
GRID ID: B.2
MEDIA TYPE: ASPHALT
# of POINTS: 681

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | | LIMIT |
|---|---|---|---|
| MAX | 7.00 | PASS | 10 |
| AVG | 1.67 | PASS | 5 |
| STD X | 1.79 | | |
| MU SUB ALPHA | 1.78 | PASS | 5 |

| ID # | GRID COORIDINATES W | S | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|---|
| B.2 | 0+91.5W | 0+39.5S | 6 | 6 | 8 | 0 |
| B.2 | 0+90.5W | 0+39.5S | 6 | 7 | 8 | 1 |
| B.2 | 0+89.5W | 0+39.5S | 6 | 7 | 8 | 1 |
| B.2 | 0+88.5W | 0+39.5S | 6 | 6 | 8 | 0 |
| B.2 | 0+90.5W | 0+38.5S | 6 | 8 | 8 | 2 |
| B.2 | 0+89.5W | 0+38.5S | 6 | 8 | 8 | 2 |
| B.2 | 0+88.5W | 0+38.5S | 6 | 8 | 8 | 2 |
| B.2 | 0+87.5W | 0+38.5S | 6 | 8 | 8 | 2 |
| B.2 | 0+89.5W | 0+37.5S | 6 | 7 | 8 | 1 |
| B.2 | 0+88.5W | 0+37.5S | 6 | 8 | 8 | 2 |
| B.2 | 0+87.5W | 0+37.5S | 6 | 7 | 8 | 1 |
| B.2 | 0+86.5W | 0+37.5S | 6 | 9 | 8 | 3 |
| B.2 | 0+85.5W | 0+37.5S | 6 | 9 | 8 | 3 |
| B.2 | 0+89.5W | 0+36.5S | 6 | 9 | 8 | 3 |
| B.2 | 0+88.5W | 0+36.5S | 6 | 7 | 8 | 1 |
| B.2 | 0+87.5W | 0+36.5S | 6 | 5 | 8 | -1 |
| B.2 | 0+86.5W | 0+36.5S | 6 | 6 | 8 | 0 |
| B.2 | 0+85.5W | 0+36.5S | 6 | 6 | 8 | 0 |
| B.2 | 0+88.5W | 0+35.5S | 6 | 9 | 8 | 3 |
| B.2 | 0+87.5W | 0+35.5S | 6 | 9 | 8 | 3 |
| B.2 | 0+86.5W | 0+35.5S | 6 | 6 | 8 | 0 |
| B.2 | 0+85.5W | 0+35.5S | 6 | 5 | 8 | -1 |
| B.2 | 0+84.5W | 0+35.5S | 6 | 8 | 8 | 2 |
| B.2 | 0+86.5W | 0+34.5S | 6 | 5 | 8 | -1 |
| B.2 | 0+85.5W | 0+34.5S | 6 | 6 | 8 | 0 |
| B.2 | 0+95.5W | 0+49.5S | 6 | 9 | 8 | 3 |
| B.2 | 0+94.5W | 0+49.5S | 6 | 7 | 8 | 1 |
| B.2 | 0+93.5W | 0+49.5S | 6 | 9 | 8 | 3 |
| B.2 | 0+92.5W | 0+49.5S | 6 | 8 | 8 | 2 |
| B.2 | 0+95.5W | 0+48.5S | 6 | 9 | 8 | 3 |
| B.2 | 0+94.5W | 0+48.5S | 6 | 8 | 8 | 2 |
| B.2 | 0+93.5W | 0+48.5S | 6 | 8 | 8 | 2 |

ANSTEC
APERTURE
CARD

Also Available on
Aperture Card

9502100114-67

TABLE B.2-1

| | | | | |
|---|---|---|---|---|
| B.2 0+92.5W 0+48.5S | 6 | 11 | 8 | 5 |
| B.2 0+95.5W 0+47.5S | 6 | 9 | 8 | 3 |
| B.2 0+94.5W 0+47.5S | 6 | 11 | 8 | 5 |
| B.2 0+93.5W 0+47.5S | 6 | 7 | 8 | 1 |
| B.2 0+92.5W 0+47.5S | 6 | 6 | 8 | 0 |
| B.2 0+94.5W 0+46.5S | 6 | 7 | 8 | 1 |
| B.2 0+93.5W 0+46.5S | 6 | 9 | 8 | 3 |
| B.2 0+92.5W 0+46.5S | 6 | 8 | 8 | 2 |
| B.2 0+91.5W 0+46.5S | 6 | 10 | 8 | 4 |
| B.2 0+90.5W 0+46.5S | 6 | 8 | 8 | 2 |
| B.2 0+94.5W 0+45.5S | 6 | 8 | 8 | 2 |
| B.2 0+93.5W 0+45.5S | 6 | 7 | 8 | 1 |
| B.2 0+92.5W 0+45.5S | 6 | 8 | 8 | 2 |
| B.2 0+91.5W 0+45.5S | 6 | 8 | 8 | 2 |
| B.2 0+90.5W 0+45.5S | 6 | 8 | 8 | 2 |
| B.2 0+89.5W 0+45.5S | 6 | 8 | 8 | 2 |
| B.2 0+94.5W 0+44.5S | 6 | 9 | 8 | 3 |
| B.2 0+93.5W 0+44.5S | 6 | 9 | 8 | 3 |
| B.2 0+92.5W 0+44.5S | 6 | 9 | 8 | 3 |
| B.2 0+91.5W 0+44.5S | 6 | 7 | 8 | 1 |
| B.2 0+90.5W 0+44.5S | 6 | 11 | 8 | 5 |
| B.2 0+89.5W 0+44.5S | 6 | 9 | 8 | 3 |
| B.2 0+88.5W 0+44.5S | 6 | 10 | 8 | 4 |
| B.2 0+94.5W 0+43.5S | 6 | 10 | 8 | 4 |
| B.2 0+93.5W 0+43.5S | 6 | 9 | 8 | 3 |
| B.2 0+92.5W 0+43.5S | 6 | 9 | 8 | 3 |
| B.2 0+91.5W 0+43.5S | 6 | 8 | 8 | 2 |
| B.2 0+90.5W 0+43.5S | 6 | 6 | 8 | 0 |
| B.2 0+89.5W 0+43.5S | 6 | 9 | 8 | 3 |
| B.2 0+88.5W 0+43.5S | 6 | 7 | 8 | 1 |
| B.2 0+93.5W 0+42.5S | 6 | 10 | 8 | 4 |
| B.2 0+92.5W 0+42.5S | 6 | 10 | 8 | 4 |
| B.2 0+91.5W 0+42.5S | 6 | 8 | 8 | 2 |
| B.2 0+90.5W 0+42.5S | 6 | 10 | 8 | 4 |
| B.2 0+89.5W 0+42.5S | 6 | 9 | 8 | 3 |
| B.2 0+88.5W 0+42.5S | 6 | 7 | 8 | 1 |
| B.2 0+93.5W 0+41.5S | 6 | 8 | 8 | 2 |
| B.2 0+92.5W 0+41.5S | 6 | 9 | 8 | 3 |
| B.2 0+91.5W 0+41.5S | 6 | 8 | 8 | 2 |
| B.2 0+90.5W 0+41.5S | 6 | 8 | 8 | 2 |
| B.2 0+89.5W 0+41.5S | 6 | 10 | 8 | 4 |
| B.2 0+88.5W 0+41.5S | 6 | 6 | 8 | 0 |
| B.2 0+92.5W 0+40.5S | 6 | 9 | 8 | 3 |
| B.2 0+91.5W 0+40.5S | 6 | 8 | 8 | 2 |
| B.2 0+90.5W 0+40.5S | 6 | 7 | 8 | 1 |
| B.2 0+89.5W 0+40.5S | 6 | 8 | 8 | 2 |
| B.2 0+88.5W 0+40.5S | 6 | 9 | 8 | 3 |
| B.2 0+99.5W 0+59.5S | 6 | 11 | 8 | 5 |
| B.2 0+98.5W 0+59.5S | 6 | 7 | 8 | 1 |
| B.2 0+97.5W 0+59.5S | 6 | 7 | 8 | 1 |
| B.2 0+96.5W 0+59.5S | 6 | 7 | 8 | 1 |
| B.2 0+95.5W 0+59.5S | 6 | 8 | 8 | 2 |
| B.2 0+94.5W 0+59.5S | 6 | 7 | 8 | 1 |
| B.2 0+93.5W 0+59.5S | 6 | 7 | 8 | 1 |
| B.2 0+98.5W 0+58.5S | 6 | 11 | 8 | 5 |
| B.2 0+97.5W 0+58.5S | 6 | 9 | 8 | 3 |
| B.2 0+96.5W 0+58.5S | 6 | 8 | 8 | 2 |
| B.2 0+95.5W 0+58.5S | 6 | 6 | 8 | 0 |
| B.2 0+94.5W 0+58.5S | 6 | 6 | 8 | 0 |
| B.2 0+93.5W 0+58.5S | 6 | 7 | 8 | 1 |

ANSTEC
APERTURE
CARD

Also Available on
Aperture Card

TABLE 8.2-1

| | | | | | |
|---|---|---|---|---|---|
| 8.2 | 0+98.5W | 0+57.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+97.5W | 0+57.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+96.5W | 0+57.5S | 6 | 8 | 8 | 2 |
| 8.2 | 0+95.5W | 0+57.5S | 6 | 8 | 8 | 2 |
| 8.2 | 0+94.5W | 0+57.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+93.5W | 0+57.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+98.5W | 0+56.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+97.5W | 0+56.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+96.5W | 0+56.5S | 6 | 3 | 8 | -3 |
| 8.2 | 0+95.5W | 0+56.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+94.5W | 0+56.5S | 6 | 3 | 8 | -3 |
| 8.2 | 0+93.5W | 0+56.5S | 6 | 12 | 8 | 6 |
| 8.2 | 0+97.5W | 0+55.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+96.5W | 0+55.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+95.5W | 0+55.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+94.5W | 0+55.5S | 6 | 4 | 8 | -2 |
| 8.2 | 0+93.5W | 0+55.5S | 6 | 4 | 8 | -2 |
| 8.2 | 0+97.5W | 0+54.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+96.5W | 0+54.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+95.5W | 0+54.5S | 6 | 4 | 8 | -2 |
| 8.2 | 0+94.5W | 0+54.5S | 6 | 4 | 8 | -2 |
| 8.2 | 0+93.5W | 0+54.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+92.5W | 0+54.5S | 6 | 9 | 8 | 3 |
| 8.2 | 0+97.5W | 0+53.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+96.5W | 0+53.5S | 6 | 4 | 8 | -2 |
| 8.2 | 0+95.5W | 0+53.5S | 6 | 4 | 8 | -2 |
| 8.2 | 0+94.5W | 0+53.5S | 6 | 3 | 8 | -3 |
| 8.2 | 0+93.5W | 0+53.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+92.5W | 0+53.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+97.5W | 0+52.5S | 6 | 3 | 8 | -3 |
| 8.2 | 0+96.5W | 0+52.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+95.5W | 0+52.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+94.5W | 0+52.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+93.5W | 0+52.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+92.5W | 0+52.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+96.5W | 0+51.5S | 6 | 8 | 8 | 2 |
| 8.2 | 0+95.5W | 0+51.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+94.5W | 0+51.5S | 6 | 4 | 8 | -2 |
| 8.2 | 0+93.5W | 0+51.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+92.5W | 0+51.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+96.5W | 0+50.5S | 6 | 9 | 8 | 3 |
| 8.2 | 0+95.5W | 0+50.5S | 6 | 4 | 8 | -2 |
| 8.2 | 0+94.5W | 0+50.5S | 6 | 4 | 8 | -2 |
| 8.2 | 0+93.5W | 0+50.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+92.5W | 0+50.5S | 6 | 6 | 8 | 0 |
| 8.2 | 1+0.5W | 0+60.5S | 6 | 9 | 8 | 3 |
| 8.2 | 0+99.5W | 0+60.5S | 6 | 8 | 8 | 2 |
| 8.2 | 0+98.5W | 0+60.5S | 6 | 11 | 8 | 5 |
| 8.2 | 0+97.5W | 0+60.5S | 6 | 9 | 8 | 3 |
| 8.2 | 0+96.5W | 0+60.5S | 6 | 10 | 8 | 4 |
| 8.2 | 0+95.5W | 0+60.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+94.5W | 0+60.5S | 6 | 9 | 8 | 3 |
| 8.2 | 0+93.5W | 0+60.5S | 6 | 10 | 8 | 4 |
| 8.2 | 1+0.5W | 0+61.5S | 6 | 4 | 8 | -2 |
| 8.2 | 0+99.5W | 0+61.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+98.5W | 0+61.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+97.5W | 0+61.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+96.5W | 0+61.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+95.5W | 0+61.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+94.5W | 0+61.5S | 6 | 6 | 8 | 0 |

ANSTEC
APERTURE
CARD

Also Available on
Aperture Card

TABLE 8.2-1

| | | | | | | |
|---|---|---|---|---|---|---|
| 8.2 | 0+93.5W | 0+61.5S | 6 | 8 | 8 | 2 |
| 8.2 | 1+0.5W | 0+62.5S | 6 | 8 | 8 | 2 |
| 8.2 | 0+99.5W | 0+62.5S | 6 | 10 | 8 | 4 |
| 8.2 | 0+98.5W | 0+62.5S | 6 | 8 | 8 | 2 |
| 8.2 | 0+97.5W | 0+62.5S | 6 | 8 | 8 | 2 |
| 8.2 | 0+96.5W | 0+62.5S | 6 | 11 | 8 | 5 |
| 8.2 | 0+95.5W | 0+62.5S | 6 | 11 | 8 | 5 |
| 8.2 | 0+94.5W | 0+62.5S | 6 | 12 | 8 | 6 |
| 8.2 | 0+93.5W | 0+62.5S | 6 | 6 | 8 | 0 |
| 8.2 | 1+0.5W | 0+63.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+99.5W | 0+63.5S | 6 | 10 | 8 | 4 |
| 8.2 | 0+98.5W | 0+63.5S | 6 | 10 | 8 | 4 |
| 8.2 | 0+97.5W | 0+63.5S | 6 | 11 | 8 | 5 |
| 8.2 | 0+96.5W | 0+63.5S | 6 | 9 | 8 | 3 |
| 8.2 | 0+95.5W | 0+63.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+94.5W | 0+63.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+93.5W | 0+63.5S | 6 | 7 | 8 | 1 |
| 8.2 | 1+0.5W | 0+64.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+99.5W | 0+64.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+98.5W | 0+64.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+97.5W | 0+64.5S | 6 | 4 | 8 | -2 |
| 8.2 | 0+96.5W | 0+64.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+95.5W | 0+64.5S | 6 | 5 | 8 | -1 |
| 8.2 | 1+2.5W | 0+65.5S | 6 | 10 | 8 | 4 |
| 8.2 | 1+1.5W | 0+65.5S | 6 | 5 | 8 | -1 |
| 8.2 | 1+0.5W | 0+65.5S | 6 | 9 | 8 | 3 |
| 8.2 | 0+99.5W | 0+65.5S | 6 | 10 | 8 | 4 |
| 8.2 | 0+98.5W | 0+65.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+97.5W | 0+65.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+96.5W | 0+65.5S | 6 | 9 | 8 | 3 |
| 8.2 | 0+95.5W | 0+65.5S | 6 | 8 | 8 | 2 |
| 8.2 | 1+2.5W | 0+66.5S | 6 | 9 | 8 | 3 |
| 8.2 | 1+1.5W | 0+66.5S | 6 | 8 | 8 | 2 |
| 8.2 | 1+0.5W | 0+66.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+99.5W | 0+66.5S | 6 | 10 | 8 | 4 |
| 8.2 | 0+98.5W | 0+66.5S | 6 | 8 | 8 | 2 |
| 8.2 | 0+97.5W | 0+66.5S | 6 | 12 | 8 | 6 |
| 8.2 | 0+96.5W | 0+66.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+95.5W | 0+66.5S | 6 | 7 | 8 | 1 |
| 8.2 | 1+2.5W | 0+67.5S | 6 | 7 | 8 | 1 |
| 8.2 | 1+1.5W | 0+67.5S | 6 | 6 | 8 | 0 |
| 8.2 | 1+0.5W | 0+67.5S | 6 | 7 | 8 | 1 |
| 8.2 | 0+99.5W | 0+67.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+98.5W | 0+67.5S | 6 | 8 | 8 | 2 |
| 8.2 | 0+97.5W | 0+67.5S | 6 | 8 | 8 | 2 |
| 8.2 | 0+96.5W | 0+67.5S | 6 | 7 | 8 | 1 |
| 8.2 | 1+3.5W | 0+67.5S | 6 | 9 | 8 | 3 |
| 8.2 | 1+2.5W | 0+68.5S | 6 | 6 | 8 | 0 |
| 8.2 | 1+1.5W | 0+68.5S | 6 | 10 | 8 | 4 |
| 8.2 | 1+0.5W | 0+68.5S | 6 | 6 | 8 | 0 |
| 8.2 | 0+99.5W | 0+68.5S | 6 | 8 | 8 | 2 |
| 8.2 | 0+98.5W | 0+68.5S | 6 | 9 | 8 | 3 |
| 8.2 | 0+97.5W | 0+68.5S | 6 | 5 | 8 | -1 |
| 8.2 | 0+96.5W | 0+68.5S | 6 | 8 | 8 | 2 |
| 8.2 | 1+3.5W | 0+68.5S | 6 | 7 | 8 | 1 |
| 8.2 | 1+2.5W | 0+68.5S | 6 | 6 | 8 | 0 |
| 8.2 | 1+1.5W | 0+69.5S | 6 | 9 | 8 | 3 |
| 8.2 | 1+0.5W | 0+69.5S | 6 | 11 | 8 | 5 |
| 8.2 | 0+99.5W | 0+69.5S | 6 | 8 | 8 | 2 |
| 8.2 | 0+98.5W | 0+69.5S | 6 | 9 | 8 | 3 |

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TABLE 8.2-1

| | | | | | |
|---|---|---|---|---|---|
| 8.2 0+97.5W | 0+69.5S | 6 | 10 | 8 | 4 |
| 8.2 0+96.5W | 0+69.5S | 6 | 7 | 8 | 1 |
| 8.2 1+3.5 | 0+70.5 | 6 | 9 | 8 | 3 |
| 8.2 1+2.5 | 0+70.5 | 6 | 9 | 8 | 3 |
| 8.2 1+1.5 | 0+70.5 | 6 | 8 | 8 | 2 |
| 8.2 1+0.5 | 0+70.5 | 6 | 10 | 8 | 4 |
| 8.2 0+99.5 | 0+70.5 | 6 | 8 | 8 | 2 |
| 8.2 0+98.5 | 0+70.5 | 6 | 9 | 8 | 3 |
| 8.2 0+97.5 | 0+70.5 | 6 | 10 | 8 | 4 |
| 8.2 1+4.5 | 0+71.5 | 6 | 9 | 8 | 3 |
| 8.2 1+3.5 | 0+71.5 | 6 | 7 | 8 | 1 |
| 8.2 1+2.5 | 0+71.5 | 6 | 7 | 8 | 1 |
| 8.2 1+1.5 | 0+71.5 | 6 | 5 | 8 | -1 |
| 8.2 1+0.5 | 0+71.5 | 6 | 5 | 8 | -1 |
| 8.2 0+99.5 | 0+71.5 | 6 | 6 | 8 | 0 |
| 8.2 0+98.5 | 0+71.5 | 6 | 7 | 8 | 1 |
| 8.2 0+97.5 | 0+71.5 | 6 | 8 | 8 | 2 |
| 8.2 1+4.5 | 0+72.5 | 6 | 5 | 8 | -1 |
| 8.2 1+3.5 | 0+72.5 | 6 | 9 | 8 | 3 |
| 8.2 1+2.5 | 0+72.5 | 6 | 6 | 8 | 0 |
| 8.2 1+1.5 | 0+72.5 | 6 | 7 | 8 | 1 |
| 8.2 1+0.5 | 0+72.5 | 6 | 12 | 8 | 6 |
| 8.2 0+99.5 | 0+72.5 | 6 | 9 | 8 | 3 |
| 8.2 0+98.5 | 0+72.5 | 6 | 8 | 8 | 2 |
| 8.2 0+97.5 | 0+72.5 | 6 | 11 | 8 | 5 |
| 8.2 1+4.5 | 0+74.5 | 6 | 6 | 8 | 0 |
| 8.2 1+3.5 | 0+74.5 | 6 | 6 | 8 | 0 |
| 8.2 1+2.5 | 0+74.5 | 6 | 7 | 8 | 1 |
| 8.2 1+1.5 | 0+74.5 | 6 | 6 | 8 | 0 |
| 8.2 1+0.5 | 0+74.5 | 6 | 8 | 8 | 2 |
| 8.2 0+99.5 | 0+74.5 | 6 | 10 | 8 | 4 |
| 8.2 0+98.5 | 0+74.5 | 6 | 8 | 8 | 2 |
| 8.2 1+5.5 | 0+75.5 | 6 | 9 | 8 | 3 |
| 8.2 1+4.5 | 0+75.5 | 6 | 7 | 8 | 1 |
| 8.2 1+3.5 | 0+75.5 | 6 | 10 | 8 | 4 |
| 8.2 1+2.5 | 0+75.5 | 6 | 6 | 8 | 0 |
| 8.2 1+1.5 | 0+75.5 | 6 | 6 | 8 | 0 |
| 8.2 1+0.5 | 0+75.5 | 6 | 8 | 8 | 2 |
| 8.2 0+99.5 | 0+75.5 | 6 | 8 | 8 | 2 |
| 8.2 0+98.5 | 0+75.5 | 6 | 5 | 8 | -1 |
| 8.2 1+5.5 | 0+76.5 | 6 | 6 | 8 | 0 |
| 8.2 1+4.5 | 0+76.5 | 6 | 7 | 8 | 1 |
| 8.2 1+3.5 | 0+76.5 | 6 | 3 | 8 | -3 |
| 8.2 1+2.5 | 0+76.5 | 6 | 10 | 8 | 4 |
| 8.2 1+1.5 | 0+76.5 | 6 | 9 | 8 | 3 |
| 8.2 1+0.5 | 0+76.5 | 6 | 8 | 8 | 2 |
| 8.2 0+99.5 | 0+76.5 | 6 | 8 | 8 | 2 |
| 8.2 0+98.5 | 0+76.5 | 6 | 8 | 8 | 2 |
| 8.2 1+5.5 | 0+77.5 | 6 | 8 | 8 | 2 |
| 8.2 1+4.5 | 0+77.5 | 6 | 7 | 8 | 1 |
| 8.2 1+3.5 | 0+77.5 | 6 | 8 | 8 | 2 |
| 8.2 1+2.5 | 0+77.5 | 6 | 10 | 8 | 4 |
| 8.2 1+1.5 | 0+77.5 | 6 | 7 | 8 | 1 |
| 8.2 1+0.5 | 0+77.5 | 6 | 9 | 8 | 3 |
| 8.2 0+99.5 | 0+77.5 | 6 | 8 | 8 | 2 |
| 8.2 0+98.5 | 0+77.5 | 6 | 11 | 8 | 5 |
| 8.2 1+5.5 | 0+78.5 | 6 | 6 | 8 | 0 |
| 8.2 1+4.5 | 0+78.5 | 6 | 6 | 8 | 0 |
| 8.2 1+3.5 | 0+78.5 | 6 | 5 | 8 | -1 |
| 8.2 1+2.5 | 0+78.5 | 6 | 7 | 8 | 1 |

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TABLE 8.2-1

| | | | | | |
|---|---|---|---|---|---|
| 8.2 1+1.5 | 0+78.5 | 6 | 7 | 8 | 1 |
| 8.2 1+0.5 | 0+78.5 | 6 | 6 | 8 | 0 |
| 8.2 0+99.5 | 0+78.5 | 6 | 4 | 8 | -2 |
| 8.2 1+6.5 | 0+79.5 | 6 | 5 | 8 | -1 |
| 8.2 1+5.5 | 0+79.5 | 6 | 8 | 8 | 2 |
| 8.2 1+4.5 | 0+79.5 | 6 | 6 | 8 | 0 |
| 8.2 1+3.5 | 0+79.5 | 6 | 5 | 8 | -1 |
| 8.2 1+2.5 | 0+79.5 | 6 | 12 | 8 | 6 |
| 8.2 1+1.5 | 0+79.5 | 6 | 8 | 8 | 2 |
| 8.2 1+0.5 | 0+79.5 | 6 | 9 | 8 | 3 |
| 8.2 0+99.5 | 0+79.5 | 6 | 8 | 8 | 2 |
| 8.2 1+2.5W | 0+89.5S | 6 | 10 | 8 | 4 |
| 8.2 1+3.5W | 0+89.5S | 6 | 7 | 8 | 1 |
| 8.2 1+4.5W | 0+89.5S | 6 | 6 | 8 | 0 |
| 8.2 1+5.5W | 0+89.5S | 6 | 5 | 8 | -1 |
| 8.2 1+6.5W | 0+89.5S | 6 | 7 | 8 | 1 |
| 8.2 1+7.5W | 0+89.5S | 6 | 7 | 8 | 1 |
| 8.2 1+8.5W | 0+89.5S | 6 | 6 | 8 | 0 |
| 8.2 1+2.5W | 0+88.5S | 6 | 9 | 8 | 3 |
| 8.2 1+3.5W | 0+88.5S | 6 | 8 | 8 | 2 |
| 8.2 1+4.5W | 0+88.5S | 6 | 7 | 8 | 1 |
| 8.2 1+5.5W | 0+88.5S | 6 | 8 | 8 | 2 |
| 8.2 1+6.5W | 0+88.5S | 6 | 8 | 8 | 2 |
| 8.2 1+7.5W | 0+88.5S | 6 | 6 | 8 | 0 |
| 8.2 1+8.5W | 0+88.5S | 6 | 8 | 8 | 2 |
| 8.2 1+2.5W | 0+87.5S | 6 | 7 | 8 | 1 |
| 8.2 1+3.5W | 0+87.5S | 6 | 8 | 8 | 2 |
| 8.2 1+4.5W | 0+87.5S | 6 | 6 | 8 | 0 |
| 8.2 1+5.5W | 0+87.5S | 6 | 8 | 8 | 2 |
| 8.2 1+6.5W | 0+87.5S | 6 | 7 | 8 | 1 |
| 8.2 1+7.5W | 0+87.5S | 6 | 10 | 8 | 4 |
| 8.2 1+8.5W | 0+87.5S | 6 | 11 | 8 | 5 |
| 8.2 1+1.5W | 0+86.5S | 6 | 9 | 8 | 3 |
| 8.2 1+2.5W | 0+86.5S | 6 | 9 | 8 | 3 |
| 8.2 1+3.5W | 0+86.5S | 6 | 5 | 8 | -1 |
| 8.2 1+4.5W | 0+86.5S | 6 | 6 | 8 | 0 |
| 8.2 1+5.5W | 0+86.5S | 6 | 8 | 8 | 2 |
| 8.2 1+6.5W | 0+86.5S | 6 | 8 | 8 | 2 |
| 8.2 1+7.5W | 0+86.5S | 6 | 12 | 8 | 6 |
| 8.2 1+8.5W | 0+86.5S | 6 | 9 | 8 | 3 |
| 8.2 1+1.5W | 0+85.5S | 6 | 5 | 8 | -1 |
| 8.2 1+2.5W | 0+85.5S | 6 | 9 | 8 | 3 |
| 8.2 1+3.5W | 0+85.5S | 6 | 7 | 8 | 1 |
| 8.2 1+4.5W | 0+85.5S | 6 | 11 | 8 | 5 |
| 8.2 1+5.5W | 0+85.5S | 6 | 7 | 8 | 1 |
| 8.2 1+6.5W | 0+85.5S | 6 | 10 | 8 | 4 |
| 8.2 1+7.5W | 0+85.5S | 6 | 7 | 8 | 1 |
| 8.2 1+1.5W | 0+84.5S | 6 | 7 | 8 | 1 |
| 8.2 1+2.5W | 0+84.5S | 6 | 8 | 8 | 2 |
| 8.2 1+3.5W | 0+84.5S | 6 | 11 | 8 | 5 |
| 8.2 1+4.5W | 0+84.5S | 6 | 6 | 8 | 0 |
| 8.2 1+5.5W | 0+84.5S | 6 | 7 | 8 | 1 |
| 8.2 1+6.5W | 0+84.5S | 6 | 7 | 8 | 1 |
| 8.2 1+7.5W | 0+84.5S | 6 | 6 | 8 | 0 |
| 8.2 1+1.5W | 0+83.5S | 6 | 7 | 8 | 1 |
| 8.2 1+2.5W | 0+83.5S | 6 | 8 | 8 | 2 |
| 8.2 1+3.5W | 0+83.5S | 6 | 8 | 8 | 2 |
| 8.2 1+4.5W | 0+83.5S | 6 | 6 | 8 | 0 |
| 8.2 1+5.5W | 0+83.5S | 6 | 4 | 8 | -2 |
| 8.2 1+6.5W | 0+83.5S | 6 | 5 | 8 | -1 |

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TABLE B.2-1

| | | | | | |
|---|---|---|---|---|---|
| B.2 1+7.5W | 0+83.5S | 6 | 10 | 8 | 4 |
| B.2 1+0.5W | 0+82.5S | 6 | 7 | 8 | 1 |
| B.2 1+1.5W | 0+82.5S | 6 | 6 | 8 | 0 |
| B.2 1+2.5W | 0+82.5S | 6 | 6 | 8 | 0 |
| B.2 1+3.5W | 0+82.5S | 6 | 11 | 8 | 5 |
| B.2 1+4.5W | 0+82.5S | 6 | 8 | 8 | 2 |
| B.2 1+5.5W | 0+82.5S | 6 | 9 | 8 | 3 |
| B.2 1+6.5W | 0+82.5S | 6 | 8 | 8 | 2 |
| B.2 1+0.5W | 0+81.5S | 6 | 7 | 8 | 1 |
| B.2 1+1.5W | 0+81.5S | 6 | 7 | 8 | 1 |
| B.2 1+2.5W | 0+81.5S | 6 | 7 | 8 | 1 |
| B.2 1+3.5W | 0+81.5S | 6 | 10 | 8 | 4 |
| B.2 1+4.5W | 0+81.5S | 6 | 9 | 8 | 3 |
| B.2 1+5.5W | 0+81.5S | 6 | 9 | 8 | 3 |
| B.2 1+6.5W | 0+81.5S | 6 | 8 | 8 | 2 |
| B.2 0+99.5W | 0+80.5S | 6 | 9 | 8 | 3 |
| B.2 1+0.5W | 0+80.5S | 6 | 11 | 8 | 5 |
| B.2 1+1.5W | 0+80.5S | 6 | 11 | 8 | 5 |
| B.2 1+2.5W | 0+80.5S | 6 | 11 | 8 | 5 |
| B.2 1+3.5W | 0+80.5S | 6 | 7 | 8 | 1 |
| B.2 1+4.5W | 0+80.5S | 6 | 7 | 8 | 1 |
| B.2 1+5.5W | 0+80.5S | 6 | 8 | 8 | 2 |
| B.2 1+6.5W | 0+80.5S | 6 | 10 | 8 | 4 |
| B.2 1+9.5W | 0+90.5S | 6 | 7 | 8 | 1 |
| B.2 1+8.5W | 0+90.5S | 6 | 6 | 8 | 0 |
| B.2 1+7.5W | 0+90.5S | 6 | 9 | 8 | 3 |
| B.2 1+6.5W | 0+90.5S | 6 | 8 | 8 | 2 |
| B.2 1+5.5W | 0+90.5S | 6 | 9 | 8 | 3 |
| B.2 1+4.5W | 0+90.5S | 6 | 9 | 8 | 3 |
| B.2 1+3.5W | 0+90.5S | 6 | 11 | 8 | 5 |
| B.2 1+9.5W | 0+91.5S | 6 | 7 | 8 | 1 |
| B.2 1+8.5W | 0+91.5S | 6 | 6 | 8 | 0 |
| B.2 1+7.5W | 0+91.5S | 6 | 6 | 8 | 0 |
| B.2 1+6.5W | 0+91.5S | 6 | 8 | 8 | 2 |
| B.2 1+5.5W | 0+91.5S | 6 | 8 | 8 | 2 |
| B.2 1+9.5W | 0+92.5S | 6 | 7 | 8 | 1 |
| B.2 1+8.5W | 0+92.5S | 6 | 9 | 8 | 3 |
| B.2 1+7.5W | 0+92.5S | 6 | 8 | 8 | 2 |
| B.2 1+6.5W | 0+92.5S | 6 | 4 | 8 | 2 |
| B.2 1+5.5W | 0+92.5S | 6 | 6 | 8 | 0 |
| B.2 1+4.5W | 0+92.5S | 6 | 8 | 8 | 2 |
| B.2 1+3.5W | 0+92.5S | 6 | 6 | 8 | 0 |
| B.2 1+10.5W | 0+93.5S | 6 | 11 | 8 | 5 |
| B.2 1+9.5W | 0+93.5S | 6 | 10 | 8 | 4 |
| B.2 1+8.5W | 0+93.5S | 6 | 7 | 8 | 1 |
| B.2 1+7.5W | 0+93.5S | 6 | 8 | 8 | 2 |
| B.2 1+6.5W | 0+93.5S | 6 | 9 | 8 | 3 |
| B.2 1+5.5W | 0+93.5S | 6 | 7 | 8 | 1 |
| B.2 1+4.5W | 0+93.5S | 6 | 9 | 8 | 3 |
| B.2 1+3.5W | 0+93.5S | 6 | 9 | 8 | 3 |
| B.2 1+10.5W | 0+94.5S | 6 | 10 | 8 | 4 |
| B.2 1+9.5W | 0+94.5S | 6 | 11 | 8 | 5 |
| B.2 1+8.5W | 0+94.5S | 6 | 11 | 8 | 5 |
| B.2 1+7.5W | 0+94.5S | 6 | 9 | 8 | 3 |
| B.2 1+6.5W | 0+94.5S | 6 | 7 | 8 | 1 |
| B.2 1+5.5W | 0+94.5S | 6 | 6 | 8 | 0 |
| B.2 1+4.5W | 0+94.5S | 6 | 8 | 8 | 2 |
| B.2 1+10.5W | 0+95.5S | 6 | 10 | 8 | 4 |
| B.2 1+9.5W | 0+95.5S | 6 | 6 | 8 | 0 |
| B.2 1+8.5W | 0+95.5S | 6 | 10 | 8 | 4 |

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TABLE 8.2-1

| | | | | | |
|---|---|---|---|---|---|
| 8.2 1+7.5W | 0+95.5S | 6 | 7 | 8 | 1 |
| 8.2 1+6.5W | 0+95.5S | 6 | 9 | 8 | 3 |
| 8.2 1+5.5W | 0+95.5S | 6 | 7 | 8 | 1 |
| 8.2 1+4.5W | 0+95.5S | 6 | 7 | 8 | 1 |
| 8.2 1+10.5W | 0+96.5S | 6 | 9 | 8 | 3 |
| 8.2 1+9.5W | 0+96.5S | 6 | 9 | 8 | 3 |
| 8.2 1+8.5W | 0+96.5S | 6 | 8 | 8 | 2 |
| 8.2 1+7.5W | 0+96.5S | 6 | 8 | 8 | 2 |
| 8.2 1+6.5W | 0+96.5S | 6 | 6 | 8 | 0 |
| 8.2 1+5.5W | 0+96.5S | 6 | 4 | 8 | -2 |
| 8.2 1+4.5W | 0+96.5S | 6 | 9 | 8 | 3 |
| 8.2 1+11.5W | 0+97.5S | 6 | 5 | 8 | -1 |
| 8.2 1+10.5W | 0+97.5S | 6 | 6 | 8 | 0 |
| 8.2 1+9.5W | 0+97.5S | 6 | 6 | 8 | 0 |
| 8.2 1+8.5W | 0+97.5S | 6 | 9 | 8 | 3 |
| 8.2 1+7.5W | 0+97.5S | 6 | 5 | 8 | -1 |
| 8.2 1+6.5W | 0+97.5S | 6 | 6 | 8 | 0 |
| 8.2 1+5.5W | 0+97.5S | 6 | 7 | 8 | 1 |
| 8.2 1+4.5W | 0+97.5S | 6 | 8 | 8 | 2 |
| 8.2 1+11.5W | 0+98.5S | 6 | 7 | 8 | 1 |
| 8.2 1+10.5W | 0+98.5S | 6 | 6 | 8 | 0 |
| 8.2 1+9.5W | 0+98.5S | 6 | 10 | 8 | 4 |
| 8.2 1+8.5W | 0+98.5S | 6 | 9 | 8 | 3 |
| 8.2 1+7.5W | 0+98.5S | 6 | 8 | 8 | 2 |
| 8.2 1+6.5W | 0+98.5S | 6 | 8 | 8 | 2 |
| 8.2 1+5.5W | 0+98.5S | 6 | 8 | 8 | 2 |
| 8.2 1+4.5W | 0+98.5S | 6 | 9 | 8 | 3 |
| 8.2 1+11.5W | 0+99.5S | 6 | 10 | 8 | 4 |
| 8.2 1+10.5W | 0+99.5S | 6 | 6 | 8 | 0 |
| 8.2 1+9.5W | 0+99.5S | 6 | 10 | 8 | 4 |
| 8.2 1+8.5W | 0+99.5S | 6 | 9 | 8 | 3 |
| 8.2 1+7.5W | 0+99.5S | 6 | 7 | 8 | 1 |
| 8.2 1+6.5W | 0+99.5S | 6 | 7 | 8 | 1 |
| 8.2 1+5.5W | 0+99.5S | 6 | 6 | 8 | 0 |
| 8.2 1+11.5 | 1+0.5 | 6 | 8 | 8 | 2 |
| 8.2 1+10.5 | 1+0.5 | 6 | 5 | 8 | -1 |
| 8.2 1+9.5 | 1+0.5 | 6 | 9 | 8 | 3 |
| 8.2 1+8.5 | 1+0.5 | 6 | 7 | 8 | 1 |
| 8.2 1+7.5 | 1+0.5 | 6 | 6 | 8 | 0 |
| 8.2 1+6.5 | 1+0.5 | 6 | 4 | 8 | -2 |
| 8.2 1+5.5 | 1+0.5 | 6 | 7 | 8 | 1 |
| 8.2 1+4.5 | 1+0.5 | 6 | 5 | 8 | -1 |
| 8.2 1+12.5 | 1+1.5 | 6 | 11 | 8 | 5 |
| 8.2 1+11.5 | 1+1.5 | 6 | 7 | 8 | 1 |
| 8.2 1+10.5 | 1+1.5 | 6 | 7 | 8 | 1 |
| 8.2 1+9.5 | 1+1.5 | 6 | 9 | 8 | 3 |
| 8.2 1+8.5 | 1+1.5 | 6 | 4 | 8 | -2 |
| 8.2 1+7.5 | 1+1.5 | 6 | 9 | 8 | 3 |
| 8.2 1+6.5 | 1+1.5 | 6 | 6 | 8 | 0 |
| 8.2 1+5.5 | 1+1.5 | 6 | 6 | 8 | 0 |
| 8.2 1+12.5 | 1+2.5 | 6 | 9 | 8 | 3 |
| 8.2 1+11.5 | 0+2.5 | 6 | 6 | 8 | 0 |
| 8.2 1+10.5 | 0+2.5 | 6 | 7 | 8 | 1 |
| 8.2 1+9.5 | 1+2.5 | 6 | 8 | 8 | 2 |
| 8.2 1+8.5 | 0+2.5 | 6 | 7 | 8 | 1 |
| 8.2 1+7.5 | 1+2.5 | 6 | 6 | 8 | 0 |
| 8.2 1+6.5 | 0+2.5 | 6 | 8 | 8 | 2 |
| 8.2 1+5.5 | 0+2.5 | 6 | 10 | 8 | 4 |
| 8.2 1+12.5 | 0+3.5 | 6 | 8 | 8 | 2 |
| 8.2 1+11.5 | 0+3.5 | 6 | 10 | 8 | 4 |

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TABLE B.2-1

| | | | | | |
|---|---|---|---|---|---|
| B.2 1+13.5 | 1+19.5 | 6 | 7 | 8 | 1 |
| B.2 1+12.5 | 1+19.5 | 6 | 10 | 8 | 4 |
| B.2 1+11.5 | 1+19.5 | 6 | 7 | 8 | 1 |
| B.2 1+10.5 | 1+19.5 | 6 | 8 | 8 | 2 |
| B.2 1+9.5 | 1+19.5 | 6 | 7 | 8 | 1 |
| B.2 1+19.5W | 1+20.5S | 6 | 8 | 8 | 2 |
| B.2 1+18.5W | 1+20.5S | 6 | 7 | 8 | 1 |
| B.2 1+17.5W | 1+20.5S | 6 | 9 | 8 | 3 |
| B.2 1+16.5W | 1+20.5S | 6 | 9 | 8 | 3 |
| B.2 1+15.5W | 1+20.5S | 6 | 8 | 8 | 2 |
| B.2 1+14.5W | 1+20.5S | 6 | 9 | 8 | 3 |
| B.2 1+13.5W | 1+20.5S | 6 | 9 | 8 | 3 |
| B.2 1+19.5W | 1+21.5S | 6 | 10 | 8 | 4 |
| B.2 1+18.5W | 1+21.5S | 6 | 9 | 8 | 3 |
| B.2 1+17.5W | 1+21.5S | 6 | 10 | 8 | 4 |
| B.2 1+16.5W | 1+21.5S | 6 | 8 | 8 | 2 |
| B.2 1+15.5W | 1+21.5S | 6 | 9 | 8 | 3 |
| B.2 1+14.5W | 1+21.5S | 6 | 8 | 8 | 2 |
| B.2 1+13.5W | 1+21.5S | 6 | 8 | 8 | 2 |
| B.2 1+20.5W | 1+22.5S | 6 | 7 | 8 | 1 |
| B.2 1+19.5W | 1+22.5S | 6 | 7 | 8 | 1 |
| B.2 1+18.5W | 1+22.5S | 6 | 6 | 8 | 0 |
| B.2 1+17.5W | 1+22.5S | 6 | 5 | 8 | -1 |
| B.2 1+16.5W | 1+22.5S | 6 | 7 | 8 | 1 |
| B.2 1+15.5W | 1+22.5S | 6 | 9 | 8 | 3 |
| B.2 1+14.5W | 1+22.5S | 6 | 9 | 8 | 3 |
| B.2 1+13.5W | 1+22.5S | 6 | 9 | 8 | 3 |
| B.2 1+20.5W | 1+23.5S | 6 | 8 | 8 | 2 |
| B.2 1+19.5W | 1+23.5S | 6 | 7 | 8 | 1 |
| B.2 1+18.5W | 1+23.5S | 6 | 5 | 8 | -1 |
| B.2 1+17.5W | 1+23.5S | 6 | 7 | 8 | 1 |
| B.2 1+16.5W | 1+23.5S | 6 | 8 | 8 | 2 |
| B.2 1+15.5W | 1+23.5S | 6 | 8 | 8 | 2 |
| B.2 1+14.5W | 1+23.5S | 6 | 7 | 8 | 1 |
| B.2 1+13.5W | 1+23.5S | 6 | 9 | 8 | 3 |
| B.2 1+20.5W | 1+24.5S | 6 | 7 | 8 | 1 |
| B.2 1+19.5W | 1+24.5S | 6 | 9 | 8 | 3 |
| B.2 1+18.5W | 1+24.5S | 6 | 11 | 8 | 5 |
| B.2 1+17.5W | 1+24.5S | 6 | 8 | 8 | 2 |
| B.2 1+16.5W | 1+24.5S | 6 | 8 | 8 | 2 |
| B.2 1+15.5W | 1+24.5S | 6 | 9 | 8 | 3 |
| B.2 1+14.5W | 1+24.5S | 6 | 10 | 8 | 4 |
| B.2 1+13.5W | 1+24.5S | 6 | 8 | 8 | 2 |
| B.2 1+20.5W | 1+25.5S | 6 | 7 | 8 | 1 |
| B.2 1+19.5W | 1+25.5S | 6 | 8 | 8 | 2 |
| B.2 1+18.5W | 1+25.5S | 6 | 6 | 8 | 0 |
| B.2 1+17.5W | 1+25.5S | 6 | 6 | 8 | 0 |
| B.2 1+16.5W | 1+25.5S | 6 | 6 | 8 | 0 |
| B.2 1+15.5W | 1+25.5S | 6 | 7 | 8 | 1 |
| B.2 1+14.5W | 1+25.5S | 6 | 5 | 8 | -1 |
| B.2 1+21.5W | 1+26.5S | 6 | 6 | 8 | 0 |
| B.2 1+20.5W | 1+26.5S | 6 | 8 | 8 | 2 |
| B.2 1+19.5W | 1+26.5S | 6 | 7 | 8 | 1 |
| B.2 1+18.5W | 1+26.5S | 6 | 7 | 8 | 1 |
| B.2 1+17.5W | 1+26.5S | 6 | 9 | 8 | 3 |
| B.2 1+16.5W | 1+26.5S | 6 | 6 | 8 | 0 |
| B.2 1+15.5W | 1+26.5S | 6 | 8 | 8 | 2 |
| B.2 1+14.5W | 1+26.5S | 6 | 6 | 8 | 0 |
| B.2 1+21.5W | 1+27.5S | 6 | 8 | 8 | 2 |
| B.2 1+20.5W | 1+27.5S | 6 | 6 | 8 | 0 |

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Aperture Card

TABLE 8.2-1

| | | | | | | |
|---|---|---|---|---|---|---|
| 8.2 | 1+10.5 | 1+11.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+9.5 | 1+11.5 | 6 | 10 | 8 | 4 |
| 8.2 | 1+8.5 | 1+11.5 | 6 | 11 | 8 | 5 |
| 8.2 | 1+7.5 | 1+11.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+14.5 | 1+12.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+13.5 | 1+12.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+12.5 | 1+12.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+11.5 | 1+12.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+10.5 | 1+12.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+9.5 | 1+12.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+8.5 | 1+12.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+15.5 | 1+13.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+14.5 | 1+13.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+13.5 | 1+13.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+12.5 | 1+13.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+11.5 | 1+13.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+10.5 | 1+13.5 | 6 | 10 | 8 | 4 |
| 8.2 | 1+9.5 | 1+13.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+8.5 | 1+13.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+15.5 | 1+14.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+14.5 | 1+14.5 | 6 | 10 | 8 | 4 |
| 8.2 | 1+13.5 | 1+14.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+12.5 | 1+14.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+11.5 | 1+14.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+10.5 | 1+14.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+9.5 | 1+14.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+8.5 | 1+14.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+15.5 | 1+15.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+14.5 | 1+15.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+13.5 | 1+15.5 | 6 | 5 | 8 | -1 |
| 8.2 | 1+12.5 | 1+15.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+11.5 | 1+15.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+10.5 | 1+15.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+9.5 | 1+15.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+15.5 | 1+16.5 | 6 | 10 | 8 | 4 |
| 8.2 | 1+14.5 | 1+16.5 | 6 | 5 | 8 | -1 |
| 8.2 | 1+13.5 | 1+16.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+12.5 | 1+16.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+11.5 | 1+16.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+10.5 | 1+16.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+9.5 | 1+16.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+8.5 | 1+16.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+15.5 | 1+17.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+14.5 | 1+17.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+13.5 | 1+17.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+12.5 | 1+17.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+11.5 | 1+17.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+10.5 | 1+17.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+9.5 | 1+17.5 | 6 | 5 | 8 | -1 |
| 8.2 | 1+16.5 | 1+18.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+15.5 | 1+18.5 | 6 | 5 | 8 | -1 |
| 8.2 | 1+14.5 | 1+18.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+13.5 | 1+18.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+12.5 | 1+18.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+11.5 | 1+18.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+10.5 | 1+18.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+9.5 | 1+18.5 | 6 | 10 | 8 | 4 |
| 8.2 | 1+16.5 | 1+19.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+15.5 | 1+19.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+14.5 | 1+19.5 | 6 | 8 | 8 | 2 |

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TABLE 8.2-1

| | | | | | |
|---|---|---|---|---|---|
| 8.2 1+10.5 | 0+3.5 | 6 | 10 | 8 | 4 |
| 8.2 1+9.5 | 0+3.5 | 6 | 6 | 8 | 0 |
| 8.2 1+8.5 | 0+3.5 | 6 | 12 | 8 | 6 |
| 8.2 1+7.5 | 0+3.5 | 6 | 7 | 8 | 1 |
| 8.2 1+6.5 | 0+3.5 | 6 | 12 | 8 | 6 |
| 8.2 1+5.5 | 0+3.5 | 6 | 8 | 8 | 2 |
| 8.2 1+12.5 | 1+4.5 | 6 | 11 | 8 | 5 |
| 8.2 1+11.5 | 1+4.5 | 6 | 6 | 8 | 0 |
| 8.2 1+10.5 | 1+4.5 | 6 | 12 | 8 | 6 |
| 8.2 1+9.5 | 1+4.5 | 6 | 8 | 8 | 2 |
| 8.2 1+8.5 | 1+4.5 | 6 | 7 | 8 | 1 |
| 8.2 1+7.5 | 1+4.5 | 6 | 8 | 8 | 2 |
| 8.2 1+6.5 | 1+4.5 | 6 | 8 | 8 | 2 |
| 8.2 1+12.5 | 1+5.5 | 6 | 8 | 8 | 2 |
| 8.2 1+11.5 | 1+5.5 | 6 | 10 | 8 | 4 |
| 8.2 1+10.5 | 1+5.5 | 6 | 6 | 8 | 0 |
| 8.2 1+9.5 | 1+5.5 | 6 | 8 | 8 | 2 |
| 8.2 1+8.5 | 1+5.5 | 6 | 9 | 8 | 3 |
| 8.2 1+7.5 | 1+5.5 | 6 | 8 | 8 | 2 |
| 8.2 1+6.5 | 1+5.5 | 6 | 8 | 8 | 2 |
| 8.2 1+12.5 | 1+6.5 | 6 | 7 | 8 | 1 |
| 8.2 1+11.5 | 1+6.5 | 6 | 10 | 8 | 4 |
| 8.2 1+10.5 | 1+6.5 | 6 | 5 | 8 | -1 |
| 8.2 1+9.5 | 1+6.5 | 6 | 7 | 8 | 1 |
| 8.2 1+8.5 | 1+6.5 | 6 | 11 | 8 | 5 |
| 8.2 1+7.5 | 1+6.5 | 6 | 10 | 8 | 4 |
| 8.2 1+6.5 | 1+6.5 | 6 | 8 | 8 | 2 |
| 8.2 1+13.5 | 1+7.5 | 6 | 6 | 8 | 0 |
| 8.2 1+12.5 | 1+7.5 | 6 | 7 | 8 | 1 |
| 8.2 1+11.5 | 1+7.5 | 6 | 9 | 8 | 3 |
| 8.2 1+10.5 | 1+7.5 | 6 | 7 | 8 | 1 |
| 8.2 1+9.5 | 1+7.5 | 6 | 9 | 8 | 3 |
| 8.2 1+8.5 | 1+7.5 | 6 | 8 | 8 | 2 |
| 8.2 1+7.5 | 1+7.5 | 6 | 12 | 8 | 6 |
| 8.2 1+6.5 | 1+7.5 | 6 | 7 | 8 | 1 |
| 8.2 1+13.5 | 1+8.5 | 6 | 12 | 8 | 6 |
| 8.2 1+12.5 | 1+8.5 | 6 | 4 | 8 | -2 |
| 8.2 1+11.5 | 1+8.5 | 6 | 7 | 8 | 1 |
| 8.2 1+10.5 | 1+8.5 | 6 | 6 | 8 | 0 |
| 8.2 1+9.5 | 1+8.5 | 6 | 5 | 8 | -1 |
| 8.2 1+8.5 | 1+8.5 | 6 | 8 | 8 | 2 |
| 8.2 1+7.5 | 1+8.5 | 6 | 11 | 8 | 5 |
| 8.2 1+13.5 | 1+9.5 | 6 | 9 | 8 | 3 |
| 8.2 1+12.5 | 1+9.5 | 6 | 10 | 8 | 4 |
| 8.2 1+11.5 | 1+9.5 | 6 | 5 | 8 | -1 |
| 8.2 1+10.5 | 1+9.5 | 6 | 9 | 8 | 3 |
| 8.2 1+9.5 | 1+9.5 | 6 | 13 | 8 | 7 |
| 8.2 1+8.5 | 1+9.5 | 6 | 9 | 8 | 3 |
| 8.2 1+7.5 | 1+9.5 | 6 | 10 | 8 | 4 |
| 8.2 1+13.5 | 1+10.5 | 6 | 11 | 8 | 5 |
| 8.2 1+12.5 | 1+10.5 | 6 | 7 | 8 | 1 |
| 8.2 1+11.5 | 1+10.5 | 6 | 10 | 8 | 4 |
| 8.2 1+10.5 | 1+10.5 | 6 | 9 | 8 | 3 |
| 8.2 1+9.5 | 1+10.5 | 6 | 10 | 8 | 4 |
| 8.2 1+8.5 | 1+10.5 | 6 | 7 | 8 | 1 |
| 8.2 1+7.5 | 1+10.5 | 6 | 6 | 8 | 0 |
| 8.2 1+14.5 | 1+11.5 | 6 | 8 | 8 | 2 |
| 8.2 1+13.5 | 1+11.5 | 6 | 10 | 8 | 4 |
| 8.2 1+12.5 | 1+11.5 | 6 | 8 | 8 | 2 |
| 8.2 1+11.5 | 1+11.5 | 6 | 10 | 8 | 4 |

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TABLE 8.2-1

| | | | | | | |
|---|---|---|---|---|---|---|
| 8.2 | 1+19.5W | 1+27.5S | 6 | 8 | 8 | 2 |
| 8.2 | 1+18.5W | 1+27.5S | 6 | 5 | 8 | -1 |
| 8.2 | 1+17.5W | 1+27.5S | 6 | 6 | 8 | 0 |
| 8.2 | 1+16.5W | 1+27.5S | 6 | 6 | 8 | 0 |
| 8.2 | 1+15.5W | 1+27.5S | 6 | 6 | 8 | 0 |
| 8.2 | 1+14.5W | 1+27.5S | 6 | 8 | 8 | 2 |
| 8.2 | 1+21.5W | 1+28.5S | 6 | 7 | 8 | 1 |
| 8.2 | 1+20.5W | 1+28.5S | 6 | 9 | 8 | 3 |
| 8.2 | 1+19.5W | 1+28.5S | 6 | 7 | 8 | 1 |
| 8.2 | 1+18.5W | 1+28.5S | 6 | 8 | 8 | 2 |
| 8.2 | 1+17.5W | 1+28.5S | 6 | 7 | 8 | 1 |
| 8.2 | 1+16.5W | 1+28.5S | 6 | 6 | 8 | 0 |
| 8.2 | 1+15.5W | 1+28.5S | 6 | 7 | 8 | 1 |
| 8.2 | 1+14.5W | 1+28.5S | 6 | 10 | 8 | 4 |
| 8.2 | 1+21.5W | 1+29.5S | 6 | 9 | 8 | 3 |
| 8.2 | 1+20.5W | 1+29.5S | 6 | 7 | 8 | 1 |
| 8.2 | 1+19.5W | 1+29.5S | 6 | 6 | 8 | 0 |
| 8.2 | 1+18.5W | 1+29.5S | 6 | 8 | 8 | 2 |
| 8.2 | 1+17.5W | 1+29.5S | 6 | 6 | 8 | 0 |
| 8.2 | 1+16.5W | 1+29.5S | 6 | 8 | 8 | 2 |
| 8.2 | 1+15.5W | 1+29.5S | 6 | 10 | 8 | 4 |
| 8.2 | 1+15.5 | 1+30.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+16.5 | 1+30.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+17.5 | 1+30.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+18.5 | 1+30.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+19.5 | 1+30.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+20.5 | 1+30.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+21.5 | 1+30.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+15.5 | 1+31.5 | 6 | 10 | 8 | 4 |
| 8.2 | 1+16.5 | 1+31.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+17.5 | 1+31.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+18.5 | 1+31.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+19.5 | 1+31.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+20.5 | 1+31.5 | 6 | 10 | 8 | 4 |
| 8.2 | 1+21.5 | 1+31.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+22.5 | 1+31.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+15.5 | 1+32.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+16.5 | 1+32.5 | 6 | 9 | 8 | 3 |
| 8.2 | 1+17.5 | 1+32.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+18.5 | 1+32.5 | 6 | 6 | 8 | 0 |
| 8.2 | 1+19.5 | 1+32.5 | 6 | 11 | 8 | 5 |
| 8.2 | 1+20.5 | 1+32.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+21.5 | 1+32.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+22.5 | 1+32.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+16.5 | 1+33.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+17.5 | 1+33.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+18.5 | 1+33.5 | 6 | 8 | 8 | 2 |
| 8.2 | 1+19.5 | 1+33.5 | 6 | 7 | 8 | 1 |
| 8.2 | 1+20.5 | 1+33.5 | 6 | 7 | 8 | 1 |

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TABLE 8.2-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:49 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
DRIVEWAY - AREA B.2 FOR BETA

RADIATION TYPE: 1 BETA SCALING FACTOR = 0.3
COMPLETION DATE: 10-17-94
TECHNICIANS: MANY
LOCATION: B.0
GRID ID: B.2
MEDIA TYPE: ASPHALT
# of POINTS: 681
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2
REM.+ FIXED:

| | | | LIMIT |
|---|---|---|---|
| MAX FOR IND GRID | 8730 | PASS | 13500 |
| AVG - SURVEY UNIT | 1989 | PASS | 13500 |
| STD X | 1231 | | |
| MU SUB ALPHA | 2067 | PASS | 13500 |
| MAX HOT SPOT | 17114 | PASS | 40500 |

| GRID ID # | COORDINATES LETTER | COORDINATES # | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | SCAN MAX BETA COUNTS | TOTAL CONT. AREA CM^2 | MATERIAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. BETA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 MAX CM^2 | TEST | INS CP |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| B.2 | 0+91.5W | 0+39.5S | 6 | 468.0 | 624 | 0 | 0 | 8 | 1890 | 2854 +/- 929 | NA | | | 0 |
| B.2 | 0+90.5W | 0+39.5S | 6 | 468.0 | 519 | 0 | 0 | 8 | 1890 | 933 +/- 853 | NA | | | 0 |
| B.2 | 0+89.5W | 0+39.5S | 6 | 468.0 | 618 | 0 | 0 | 8 | 1890 | 2744 +/- 925 | NA | | | 0 |
| B.2 | 0+88.5W | 0+39.5S | 6 | 468.0 | 654 | 0 | 0 | 8 | 1890 | 3403 +/- 949 | NA | | | 0 |
| B.2 | 0+90.5W | 0+38.5S | 6 | 468.0 | 513 | 0 | 0 | 8 | 1890 | 823 +/- 848 | NA | | | 0 |
| B.2 | 0+89.5W | 0+38.5S | 6 | 468.0 | 546 | 0 | 0 | 8 | 1890 | 1427 +/- 873 | NA | | | 0 |
| B.2 | 0+88.5W | 0+38.5S | 6 | 468.0 | 578 | 0 | 0 | 8 | 1890 | 2012 +/- 896 | NA | | | 0 |
| B.2 | 0+87.5W | 0+38.5S | 6 | 468.0 | 569 | 0 | 0 | 8 | 1890 | 1848 +/- 890 | NA | | | 0 |
| B.2 | 0+89.5W | 0+37.5S | 6 | 468.0 | 548 | 0 | 0 | 8 | 1890 | 1464 +/- 875 | NA | | | 0 |
| B.2 | 0+88.5W | 0+37.5S | 6 | 468.0 | 603 | 0 | 0 | 8 | 1890 | 2470 +/- 914 | NA | | | 0 |
| B.2 | 0+87.5W | 0+37.5S | 6 | 468.0 | 717 | 0 | 0 | 8 | 1890 | 4555 +/- 991 | NA | | | 0 |
| B.2 | 0+86.5W | 0+37.5S | 6 | 468.0 | 819 | 0 | 0 | 8 | 1890 | 6422 +/-1055 | NA | | | 0 |
| B.2 | 0+85.5W | 0+37.5S | 6 | 468.0 | 790 | 0 | 0 | 8 | 1890 | 5891 +/-1037 | NA | | | 0 |
| B.2 | 0+89.5W | 0+36.5S | 6 | 468.0 | 528 | 0 | 0 | 8 | 1890 | 1098 +/- 860 | NA | | | 0 |
| B.2 | 0+88.5W | 0+36.5S | 6 | 468.0 | 638 | 0 | 0 | 8 | 1890 | 3110 +/- 938 | NA | | | 0 |
| B.2 | 0+87.5W | 0+36.5S | 6 | 468.0 | 616 | 0 | 0 | 8 | 1890 | 2708 +/- 923 | NA | | | 0 |
| B.2 | 0+86.5W | 0+36.5S | 6 | 468.0 | 611 | 0 | 0 | 8 | 1890 | 2616 +/- 920 | NA | | | 0 |
| B.2 | 0+85.5W | 0+36.5S | 6 | 468.0 | 676 | 0 | 0 | 8 | 1890 | 3805 +/- 964 | NA | | | 0 |
| B.2 | 0+88.5W | 0+35.5S | 6 | 468.0 | 571 | 0 | 0 | 8 | 1890 | 1884 +/- 891 | NA | | | 0 |
| B.2 | 0+87.5W | 0+35.5S | 6 | 468.0 | 554 | 0 | 0 | 8 | 1890 | 1573 +/- 879 | NA | | | 0 |
| B.2 | 0+86.5W | 0+35.5S | 6 | 468.0 | 541 | 0 | 0 | 8 | 1890 | 1336 +/- 869 | NA | | | 0 |
| B.2 | 0+85.5W | 0+35.5S | 6 | 468.0 | 553 | 0 | 0 | 8 | 1890 | 1555 +/- 878 | NA | | | 0 |
| B.2 | 0+84.5W | 0+35.5S | 6 | 468.0 | 524 | 0 | 0 | 8 | 1890 | 1025 +/- 857 | NA | | | 0 |
| B.2 | 0+86.5W | 0+34.5S | 6 | 468.0 | 569 | 0 | 0 | 8 | 1890 | 1848 +/- 890 | NA | | | 0 |
| B.2 | 0+85.5W | 0+34.5S | 6 | 468.0 | 462 | 0 | 0 | 8 | 1890 | -110 +/- 809 | NA | | | 0 |

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TABLE B.2-2

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| B.2 0+95.5W | 0+49.5S | 1 | 471.4 | 542 | 0 | 0 | B | 1963 | 1337 +/- 901 | NA | |
| B.2 0+94.5W | 0+49.5S | 1 | 471.4 | 555 | 0 | 0 | B | 1963 | 1583 +/- 911 | NA | |
| B.2 0+93.5W | 0+49.5S | 1 | 471.4 | 630 | 0 | 0 | B | 1963 | 3004 +/- 966 | NA | |
| B.2 0+92.5W | 0+49.5S | 1 | 471.4 | 755 | 0 | 0 | B | 1963 | 5371 +/-1051 | NA | |
| B.2 0+95.5W | 0+48.5S | 1 | 471.4 | 563 | 0 | 0 | B | 1963 | 1735 +/- 917 | NA | |
| B.2 0+94.5W | 0+48.5S | 1 | 471.4 | 658 | 0 | 0 | B | 1963 | 3534 +/- 986 | NA | |
| B.2 0+93.5W | 0+48.5S | 1 | 471.4 | 593 | 0 | 0 | B | 1963 | 2303 +/- 939 | NA | |
| B.2 0+92.5W | 0+48.5S | 1 | 471.4 | 626 | 0 | 0 | B | 1963 | 2928 +/- 963 | NA | |
| B.2 0+95.5W | 0+47.5S | 1 | 471.4 | 614 | 0 | 0 | B | 1963 | 2701 +/- 954 | NA | |
| B.2 0+94.5W | 0+47.5S | 1 | 471.4 | 725 | 0 | 0 | B | 1963 | 4803 +/-1032 | NA | |
| B.2 0+93.5W | 0+47.5S | 1 | 471.4 | 621 | 0 | 0 | B | 1963 | 2833 +/- 960 | NA | |
| B.2 0+92.5W | 0+47.5S | 1 | 471.4 | 601 | 0 | 0 | B | 1963 | 2455 +/- 945 | NA | |
| B.2 0+94.5W | 0+46.5S | 1 | 471.4 | 588 | 0 | 0 | B | 1963 | 2208 +/- 936 | NA | |
| B.2 0+93.5W | 0+46.5S | 1 | 471.4 | 577 | 0 | 0 | B | 1963 | 2000 +/- 927 | NA | |
| B.2 0+92.5W | 0+46.5S | 1 | 471.4 | 545 | 0 | 0 | B | 1963 | 1394 +/- 903 | NA | |
| B.2 0+91.5W | 0+46.5S | 1 | 471.4 | 596 | 0 | 0 | B | 1963 | 2360 +/- 941 | NA | |
| B.2 0+90.5W | 0+46.5S | 1 | 471.4 | 549 | 0 | 0 | B | 1963 | 1470 +/- 906 | NA | |
| B.2 0+94.5W | 0+45.5S | 1 | 471.4 | 630 | 0 | 0 | B | 1963 | 3004 +/- 966 | NA | |
| B.2 0+93.5W | 0+45.5S | 1 | 471.4 | 603 | 0 | 0 | B | 1963 | 2492 +/- 947 | NA | |
| B.2 0+92.5W | 0+45.5S | 1 | 471.4 | 532 | 0 | 0 | B | 1963 | 1148 +/- 893 | NA | |
| B.2 0+91.5W | 0+45.5S | 1 | 471.4 | 591 | 0 | 0 | B | 1963 | 2265 +/- 938 | NA | |
| B.2 0+90.5W | 0+45.5S | 6 | 461.3 | 513 | 0 | 0 | B | 1877 | 946 +/- 848 | NA | 0 |
| B.2 0+89.5W | 0+45.5S | 6 | 461.3 | 634 | 0 | 0 | B | 1877 | 3160 +/- 935 | NA | 0 |
| B.2 0+94.5W | 0+44.5S | 6 | 461.3 | 528 | 0 | 0 | B | 1877 | 1220 +/- 859 | NA | 0 |
| B.2 0+93.5W | 0+44.5S | 6 | 461.3 | 645 | 0 | 0 | B | 1877 | 3361 +/- 943 | NA | 0 |
| B.2 0+92.5W | 0+44.5S | 6 | 461.3 | 564 | 0 | 0 | B | 1877 | 1879 +/- 886 | NA | 0 |
| B.2 0+91.5W | 0+44.5S | 6 | 461.3 | 515 | 0 | 0 | B | 1877 | 982 +/- 849 | NA | 0 |
| B.2 0+90.5W | 0+44.5S | 6 | 461.3 | 586 | 0 | 0 | B | 1877 | 2281 +/- 902 | NA | 0 |
| B.2 0+89.5W | 0+44.5S | 6 | 461.3 | 595 | 0 | 0 | B | 1877 | 2446 +/- 908 | NA | 0 |
| B.2 0+88.5W | 0+44.5S | 6 | 461.3 | 662 | 0 | 0 | B | 1877 | 3672 +/- 954 | NA | 0 |
| B.2 0+94.5W | 0+43.5S | 6 | 461.3 | 638 | 0 | 0 | B | 1877 | 3233 +/- 938 | NA | 0 |
| B.2 0+93.5W | 0+43.5S | 6 | 461.3 | 660 | 0 | 0 | B | 1877 | 3635 +/- 953 | NA | 0 |
| B.2 0+92.5W | 0+43.5S | 6 | 461.3 | 590 | 0 | 0 | B | 1877 | 2355 +/- 904 | NA | 0 |
| B.2 0+91.5W | 0+43.5S | 6 | 461.3 | 533 | 0 | 0 | B | 1877 | 1312 +/- 863 | NA | 0 |
| B.2 0+90.5W | 0+43.5S | 6 | 461.3 | 562 | 0 | 0 | B | 1877 | 1842 +/- 884 | NA | 0 |
| B.2 0+89.5W | 0+43.5S | 6 | 461.3 | 601 | 0 | 0 | B | 1877 | 2556 +/- 912 | NA | 0 |
| B.2 0+88.5W | 0+43.5S | 6 | 461.3 | 796 | 0 | 0 | B | 1877 | 6123 +/-1041 | NA | 0 |
| B.2 0+93.5W | 0+42.5S | 6 | 461.3 | 555 | 0 | 0 | B | 1877 | 1714 +/- 879 | NA | 0 |
| B.2 0+92.5W | 0+42.5S | 6 | 461.3 | 688 | 0 | 0 | B | 1877 | 4147 +/- 972 | NA | 0 |
| B.2 0+91.5W | 0+42.5S | 6 | 461.3 | 551 | 0 | 0 | B | 1877 | 1641 +/- 876 | NA | 0 |
| B.2 0+90.5W | 0+42.5S | 6 | 461.3 | 570 | 0 | 0 | B | 1877 | 1989 +/- 890 | NA | 0 |
| B.2 0+89.5W | 0+42.5S | 6 | 461.3 | 552 | 0 | 0 | B | 1877 | 1659 +/- 877 | NA | 0 |
| B.2 0+88.5W | 0+42.5S | 6 | 461.3 | 753 | 0 | 0 | B | 1877 | 5337 +/-1014 | NA | 0 |
| B.2 0+93.5W | 0+41.5S | 6 | 461.3 | 545 | 0 | 0 | B | 1877 | 1531 +/- 872 | NA | 0 |
| B.2 0+92.5W | 0+41.5S | 6 | 461.3 | 588 | 0 | 0 | B | 1877 | 2318 +/- 903 | NA | 0 |
| B.2 0+91.5W | 0+41.5S | 6 | 461.3 | 725 | 0 | 0 | B | 1877 | 4824 +/- 996 | NA | 0 |
| B.2 0+90.5W | 0+41.5S | 6 | 461.3 | 600 | 0 | 0 | B | 1877 | 2538 +/- 911 | NA | 0 |
| B.2 0+89.5W | 0+41.5S | 6 | 461.3 | 597 | 0 | 0 | B | 1877 | 2483 +/- 909 | NA | 0 |
| B.2 0+88.5W | 0+41.5S | 6 | 461.3 | 704 | 0 | 0 | B | 1877 | 4440 +/- 982 | NA | 0 |
| B.2 0+92.5W | 0+40.5S | 6 | 461.3 | 555 | 0 | 0 | B | 1877 | 1714 +/- 879 | NA | 0 |
| B.2 0+91.5W | 0+40.5S | 6 | 461.3 | 639 | 0 | 0 | B | 1877 | 3251 +/- 939 | NA | 0 |
| B.2 0+90.5W | 0+40.5S | 6 | 461.3 | 554 | 0 | 0 | B | 1877 | 1696 +/- 878 | NA | 0 |
| B.2 0+89.5W | 0+40.5S | 6 | 461.3 | 551 | 0 | 0 | B | 1877 | 1641 +/- 876 | NA | 0 |
| B.2 0+88.5W | 0+40.5S | 6 | 461.3 | 648 | 0 | 0 | B | 1877 | 3416 +/- 945 | NA | 0 |
| B.2 0+99.5W | 0+59.5S | 2 | 448.1 | 783 | 0 | 0 | B | 1851 | 6130 +/-1032 | NA | 0 |
| B.2 0+98.5W | 0+59.5S | 2 | 448.1 | 575 | 0 | 0 | B | 1851 | 2323 +/- 893 | NA | 0 |

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TABLE B.2-2

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|---|---|---|---|---|---|---|---|---|---|---|
| B.2 | 0+97.5W | 0+59.5S | 2 | 448.1 | 615 | 0 | 0 | 8 | 1851 | 3055 +/- 922 | NA |
| B.2 | 0+96.5W | 0+59.5S | 2 | 448.1 | 579 | 0 | 0 | 8 | 1851 | 2396 +/- 896 | NA |
| B.2 | 0+95.5W | 0+59.5S | 2 | 448.1 | 585 | 0 | 0 | 8 | 1851 | 2506 +/- 900 | NA |
| B.2 | 0+94.5W | 0+59.5S | 2 | 448.1 | 564 | 0 | 0 | 8 | 1851 | 2122 +/- 885 | NA |
| B.2 | 0+93.5W | 0+59.5S | 2 | 448.1 | 582 | 0 | 0 | 8 | 1851 | 2451 +/- 898 | NA |
| B.2 | 0+98.5W | 0+58.5S ** | 2 | 448.1 | 611 | 0 | 0 | 8 | 1851 | 2982 +/- 919 | NA |
| B.2 | 0+97.5W | 0+58.5S | 2 | 448.1 | 572 | 0 | 0 | 8 | 1851 | 2268 +/- 891 | NA |
| B.2 | 0+96.5W | 0+58.5S | 2 | 448.1 | 516 | 0 | 0 | 8 | 1851 | 1243 +/- 850 | NA |
| B.2 | 0+95.5W | 0+58.5S | 2 | 448.1 | 563 | 0 | 0 | 8 | 1851 | 2103 +/- 885 | NA |
| B.2 | 0+94.5W | 0+58.5S | 2 | 448.1 | 554 | 0 | 0 | 8 | 1851 | 1938 +/- 878 | NA |
| B.2 | 0+93.5W | 0+58.5S | 2 | 448.1 | 612 | 0 | 0 | 8 | 1851 | 3000 +/- 919 | NA |
| B.2 | 0+98.5W | 0+57.5S | 2 | 448.1 | 591 | 0 | 0 | 8 | 1851 | 2616 +/- 905 | NA |
| B.2 | 0+97.5W | 0+57.5S | 2 | 448.1 | 536 | 0 | 0 | 8 | 1851 | 1609 +/- 865 | NA |
| B.2 | 0+96.5W | 0+57.5S | 2 | 448.1 | 561 | 0 | 0 | 8 | 1851 | 2067 +/- 883 | NA |
| B.2 | 0+95.5W | 0+57.5S | 2 | 448.1 | 540 | 0 | 0 | 8 | 1851 | 1682 +/- 868 | NA |
| B.2 | 0+94.5W | 0+57.5S | 2 | 448.1 | 526 | 0 | 0 | 8 | 1851 | 1426 +/- 857 | NA |
| B.2 | 0+93.5W | 0+57.5S | 2 | 448.1 | 925 | 0 | 0 | 8 | 1851 | 8730 +/-1117 | NA |
| B.2 | 0+98.5W | 0+56.5S | 1 | 505.7 | 583 | 0 | 0 | 8 | 2032 | 1464 +/- 934 | NA |
| B.2 | 0+97.5W | 0+56.5S | 1 | 505.7 | 584 | 0 | 0 | 8 | 2032 | 1483 +/- 935 | NA |
| B.2 | 0+96.5W | 0+56.5S | 1 | 505.7 | 575 | 0 | 0 | 8 | 2032 | 1312 +/- 928 | NA |
| B.2 | 0+95.5W | 0+56.5S | 1 | 505.7 | 578 | 0 | 0 | 8 | 2032 | 1369 +/- 931 | NA |
| B.2 | 0+94.5W | 0+56.5S | 1 | 505.7 | 606 | 0 | 0 | 8 | 2032 | 1900 +/- 951 | NA |
| B.2 | 0+93.5W | 0+56.5S | 1 | 505.7 | 668 | 0 | 0 | 8 | 2032 | 3074 +/- 995 | NA |
| B.2 | 0+97.5W | 0+55.5S | 1 | 505.7 | 607 | 0 | 0 | 8 | 2032 | 1919 +/- 952 | NA |
| B.2 | 0+96.5W | 0+55.5S | 1 | 505.7 | 597 | 0 | 0 | 8 | 2032 | 1729 +/- 945 | NA |
| B.2 | 0+95.5W | 0+55.5S | 1 | 505.7 | 618 | 0 | 0 | 8 | 2032 | 2127 +/- 960 | NA |
| B.2 | 0+94.5W | 0+55.5S | 1 | 505.7 | 598 | 0 | 0 | 8 | 2032 | 1748 +/- 945 | NA |
| B.2 | 0+93.5W | 0+55.5S | 1 | 505.7 | 615 | 0 | 0 | 8 | 2032 | 2070 +/- 958 | NA |
| B.2 | 0+97.5W | 0+54.5S | 1 | 505.7 | 638 | 0 | 0 | 8 | 2032 | 2506 +/- 974 | NA |
| B.2 | 0+96.5W | 0+54.5S | 1 | 505.7 | 661 | 0 | 0 | 8 | 2032 | 2941 +/- 990 | NA |
| B.2 | 0+95.5W | 0+54.5S | 1 | 505.7 | 652 | 0 | 0 | 8 | 2032 | 2771 +/- 984 | NA |
| B.2 | 0+94.5W | 0+54.5S | 1 | 505.7 | 621 | 0 | 0 | 8 | 2032 | 2184 +/- 962 | NA |
| B.2 | 0+93.5W | 0+54.5S | 1 | 505.7 | 705 | 0 | 0 | 8 | 2032 | 3775 +/-1020 | NA |
| B.2 | 0+92.5W | 0+54.5S | 1 | 505.7 | 572 | 0 | 0 | 8 | 2032 | 1256 +/- 926 | NA |
| B.2 | 0+97.5W | 0+53.5S | 1 | 505.7 | 720 | 0 | 0 | 8 | 2032 | 4059 +/-1030 | NA |
| B.2 | 0+96.5W | 0+53.5S | 1 | 505.7 | 596 | 0 | 0 | 8 | 2032 | 1710 +/- 944 | NA |
| B.2 | 0+95.5W | 0+53.5S | 1 | 505.7 | 603 | 0 | 0 | 8 | 2032 | 1843 +/- 949 | NA |
| B.2 | 0+94.5W | 0+53.5S | 1 | 505.7 | 614 | 0 | 0 | 8 | 2032 | 2051 +/- 957 | NA |
| B.2 | 0+93.5W | 0+53.5S | 1 | 505.7 | 694 | 0 | 0 | 8 | 2032 | 3566 +/-1013 | NA |
| B.2 | 0+92.5W | 0+53.5S | 1 | 505.7 | 613 | 0 | 0 | 8 | 2032 | 2032 +/- 956 | NA |
| B.2 | 0+97.5W | 0+52.5S | 1 | 505.7 | 562 | 0 | 0 | 8 | 2032 | 1066 +/- 919 | NA |
| B.2 | 0+96.5W | 0+52.5S | 1 | 505.7 | 610 | 0 | 0 | 8 | 2032 | 1975 +/- 954 | NA |
| B.2 | 0+95.5W | 0+52.5S | 1 | 505.7 | 643 | 0 | 0 | 8 | 2032 | 2600 +/- 978 | NA |
| B.2 | 0+94.5W | 0+52.5S | 1 | 505.7 | 637 | 0 | 0 | 8 | 2032 | 2487 +/- 973 | NA |
| B.2 | 0+93.5W | 0+52.5S | 1 | 505.7 | 567 | 0 | 0 | 8 | 2032 | 1161 +/- 922 | NA |
| B.2 | 0+92.5W | 0+52.5S | 1 | 505.7 | 529 | 0 | 0 | 8 | 2032 | 441 +/- 894 | NA |
| B.2 | 0+96.5W | 0+51.5S | 1 | 505.7 | 589 | 0 | 0 | 8 | 2032 | 1578 +/- 939 | NA |
| B.2 | 0+95.5W | 0+51.5S | 1 | 505.7 | 562 | 0 | 0 | 8 | 2032 | 1066 +/- 919 | NA |
| B.2 | 0+94.5W | 0+51.5S | 1 | 505.7 | 596 | 0 | 0 | 8 | 2032 | 1710 +/- 944 | NA |
| B.2 | 0+93.5W | 0+51.5S | 1 | 505.7 | 574 | 0 | 0 | 8 | 2032 | 1294 +/- 928 | NA |
| B.2 | 0+92.5W | 0+51.5S | 1 | 505.7 | 633 | 0 | 0 | 8 | 2032 | 2411 +/- 971 | NA |
| B.2 | 0+96.5W | 0+50.5S | 6 | 468.3 | 537 | 0 | 0 | 8 | 1891 | 1257 +/- 866 | NA |
| B.2 | 0+95.5W | 0+50.5S | 6 | 468.3 | 546 | 0 | 0 | 8 | 1891 | 1422 +/- 873 | NA |
| B.2 | 0+94.5W | 0+50.5S | 6 | 468.3 | 574 | 0 | 0 | 8 | 1891 | 1934 +/- 893 | NA |
| B.2 | 0+93.5W | 0+50.5S | 6 | 468.3 | 636 | 0 | 0 | 8 | 1891 | 3068 +/- 937 | NA |
| B.2 | 0+92.5W | 0+50.5S | 6 | 468.3 | 649 | 0 | 0 | 8 | 1891 | 3306 +/- 946 | NA |

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|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 1+0.5W | 0+60.5S | 2 | 478 | 530 | 0 | 0 | 8 | 1911 | 952 +/- 862 | NA | 0 |
| 8.2 0+99.5W | 0+60.5S | 3 | 497 | 631 | 0 | 0 | 8 | 1957 | 2465 +/- 941 | NA | 0 |
| 8.2 0+98.5W | 0+60.5S | 3 | 497 | 652 | 0 | 0 | 8 | 1957 | 2851 +/- 955 | NA | 0 |
| 8.2 0+97.5W | 0+60.5S | 3 | 497 | 562 | 0 | 0 | 8 | 1957 | 1196 +/- 892 | NA | 0 |
| 8.2 0+96.5W | 0+60.5S | 3 | 497 | 580 | 0 | 0 | 8 | 1957 | 1527 +/- 905 | NA | 0 |
| 8.2 0+95.5W | 0+60.5S | 3 | 497 | 642 | 0 | 0 | 8 | 1957 | 2667 +/- 948 | NA | 0 |
| 8.2 0+94.5W | 0+60.5S | 3 | 497 | 637 | 0 | 0 | 8 | 1957 | 2575 +/- 945 | NA | 0 |
| 8.2 0+93.5W | 0+60.5S | 2 | 478 | 590 | 0 | 0 | 8 | 1911 | 2050 +/- 906 | NA | 0 |
| 8.2 1+0.5W | 0+61.5S | 2 | 478 | 514 | 0 | 0 | 8 | 1911 | 659 +/- 850 | NA | 0 |
| 8.2 0+99.5W | 0+61.5S | 3 | 497 | 859 | 0 | 0 | 8 | 1957 | 6659 +/-1087 | NA | 0 |
| 8.2 0+98.5W | 0+61.5S | 3 | 497 | 577 | 0 | 0 | 8 | 1957 | 1472 +/- 903 | NA | 0 |
| 8.2 0+97.5W | 0+61.5S | 3 | 497 | 631 | 0 | 0 | 8 | 1957 | 2465 +/- 941 | NA | 0 |
| 8.2 0+96.5W | 0+61.5S | 3 | 497 | 580 | 0 | 0 | 8 | 1957 | 1527 +/- 905 | NA | 0 |
| 8.2 0+95.5W | 0+61.5S | 3 | 497 | 596 | 0 | 0 | 8 | 1957 | 1821 +/- 916 | NA | 0 |
| 8.2 0+94.5W | 0+61.5S | 3 | 497 | 603 | 0 | 0 | 8 | 1957 | 1950 +/- 921 | NA | 0 |
| 8.2 0+93.5W | 0+61.5S | 2 | 478 | 602 | 0 | 0 | 8 | 1911 | 2270 +/- 915 | NA | 0 |
| 8.2 1+0.5W | 0+62.5S | 4 | 555 | 603 | 0 | 0 | 8 | 2096 | 896 +/- 939 | NA | 0 |
| 8.2 0+99.5W | 0+62.5S | 4 | 555 | 668 | 0 | 0 | 8 | 2096 | 2110 +/- 985 | NA | 0 |
| 8.2 0+98.5W | 0+62.5S | 4 | 555 | 695 | 0 | 0 | 8 | 2096 | 2614 +/-1003 | NA | 0 |
| 8.2 0+97.5W | 0+62.5S | 4 | 555 | 860 | 0 | 0 | 8 | 2096 | 5696 +/-1107 | NA | 0 |
| 8.2 0+96.5W | 0+62.5S | 4 | 555 | 827 | 0 | 0 | 8 | 2096 | 5079 +/-1087 | NA | 0 |
| 8.2 0+95.5W | 0+62.5S | 4 | 555 | 637 | 0 | 0 | 8 | 2096 | 1531 +/- 963 | NA | 0 |
| 8.2 0+94.5W | 0+62.5S | 2 | 478 | 634 | 0 | 0 | 8 | 1911 | 2856 +/- 937 | NA | 0 |
| 8.2 1+1.5W | 0+63.5S | 2 | 478 | 589 | 0 | 0 | 8 | 1911 | 2032 +/- 905 | NA | 0 |
| 8.2 1+0.5W | 0+63.5S | 4 | 555 | 548 | 0 | 0 | 8 | 2096 | -131 +/- 899 | NA | 0 |
| 8.2 0+99.5W | 0+63.5S | 4 | 555 | 560 | 0 | 0 | 8 | 2096 | 93 +/- 908 | NA | 0 |
| 8.2 0+98.5W | 0+63.5S | 4 | 555 | 563 | 0 | 0 | 8 | 2096 | 149 +/- 910 | NA | 0 |
| 8.2 0+97.5W | 0+63.5S | 4 | 555 | 555 | 0 | 0 | 8 | 2096 | 0 +/- 904 | NA | 0 |
| 8.2 0+96.5W | 0+63.5S | 4 | 555 | 624 | 0 | 0 | 8 | 2096 | 1289 +/- 954 | NA | 0 |
| 8.2 0+95.5W | 0+63.5S | 4 | 555 | 582 | 0 | 0 | 8 | 2096 | 504 +/- 924 | NA | 0 |
| 8.2 0+94.5W | 0+63.5S | 2 | 478 | 629 | 0 | 0 | 8 | 1911 | 2764 +/- 933 | NA | 0 |
| 8.2 1+1.5W | 0+64.5S | 2 | 478 | 574 | 0 | 0 | 8 | 1911 | 1757 +/- 895 | NA | 0 |
| 8.2 1+0.5W | 0+64.5S | 4 | 555 | 601 | 0 | 0 | 8 | 2096 | 859 +/- 938 | NA | 0 |
| 8.2 0+99.5W | 0+64.5S | 4 | 555 | 556 | 0 | 0 | 8 | 2096 | 19 +/- 905 | NA | 0 |
| 8.2 0+98.5W | 0+64.5S | 4 | 555 | 524 | 0 | 0 | 8 | 2096 | -579 +/- 881 | NA | 0 |
| 8.2 0+97.5W | 0+64.5S | 4 | 555 | 554 | 0 | 0 | 8 | 2096 | -19 +/- 904 | NA | 0 |
| 8.2 0+96.5W | 0+64.5S | 4 | 555 | 590 | 0 | 0 | 8 | 2096 | 654 +/- 930 | NA | 0 |
| 8.2 0+95.5W | 0+64.5S | 4 | 555 | 592 | 0 | 0 | 8 | 2096 | 691 +/- 931 | NA | 0 |
| 8.2 1+2.5W | 0+65.5S | 2 | 478 | 574 | 0 | 0 | 8 | 1911 | 1757 +/- 895 | NA | 0 |
| 8.2 1+1.5W | 0+65.5S | 3 | 520.2 | 610 | 0 | 0 | 8 | 2001 | 1652 +/- 928 | NA | 0 |
| 8.2 1+0.5W | 0+65.5S | 3 | 520.2 | 576 | 0 | 0 | 8 | 2001 | 1026 +/- 904 | NA | 0 |
| 8.2 0+99.5W | 0+65.5S | 3 | 520.2 | 587 | 0 | 0 | 8 | 2001 | 1229 +/- 911 | NA | 0 |
| 8.2 0+98.5W | 0+65.5S | 3 | 520.2 | 568 | 0 | 0 | 8 | 2001 | 879 +/- 898 | NA | 0 |
| 8.2 0+97.5W | 0+65.5S | 3 | 520.2 | 566 | 0 | 0 | 8 | 2001 | 843 +/- 896 | NA | 0 |
| 8.2 0+96.5W | 0+65.5S | 3 | 520.2 | 589 | 0 | 0 | 8 | 2001 | 1266 +/- 913 | NA | 0 |
| 8.2 0+95.5W | 0+65.5S | 2 | 478 | 617 | 0 | 0 | 8 | 1911 | 2544 +/- 925 | NA | 0 |
| 8.2 1+2.5W | 0+66.5S | 2 | 478 | 532 | 0 | 0 | 8 | 1911 | 988 +/- 864 | NA | 0 |
| 8.2 1+1.5W | 0+66.5S | 3 | 520.2 | 561 | 0 | 0 | 8 | 2001 | 751 +/- 893 | NA | 0 |
| 8.2 1+0.5W | 0+66.5S | 3 | 520.2 | 581 | 0 | 0 | 8 | 2001 | 1118 +/- 907 | NA | 0 |
| 8.2 0+99.5W | 0+66.5S | 3 | 520.2 | 607 | 0 | 0 | 8 | 2001 | 1597 +/- 926 | NA | 0 |
| 8.2 0+98.5W | 0+66.5S | 3 | 520.2 | 555 | 0 | 0 | 8 | 2001 | 640 +/- 888 | NA | 0 |
| 8.2 0+97.5W | 0+66.5S | 3 | 520.2 | 619 | 0 | 0 | 8 | 2001 | 1818 +/- 934 | NA | 0 |
| 8.2 0+96.5W | 0+66.5S | 3 | 520.2 | 551 | 0 | 0 | 8 | 2001 | 567 +/- 885 | NA | 0 |
| 8.2 0+95.5W | 0+66.5S | 3 | 520.2 | 552 | 0 | 0 | 8 | 2001 | 585 +/- 886 | NA | 0 |
| 8.2 1+2.5W | 0+67.5S | 4 | 475 | 565 | 0 | 0 | 8 | 1943 | 1681 +/- 906 | NA | 0 |
| 8.2 1+1.5W | 0+67.5S | 4 | 475 | 570 | 0 | 0 | 8 | 1943 | 1774 +/- 910 | NA | 0 |

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TABLE 8.2-2

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|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 1+0.5W | 0+67.5S | 4 | 475 | 608 | 0 | 0 | 8 | 1943 | 2484 +/- 937 | NA | 0 |
| 8.2 0+99.5W | 0+67.5S | 4 | 475 | 602 | 0 | 0 | 8 | 1943 | 2372 +/- 933 | NA | 0 |
| 8.2 0+98.5W | 0+67.5S | 4 | 475 | 575 | 0 | 0 | 8 | 1943 | 1867 +/- 913 | NA | 0 |
| 8.2 0+97.5W | 0+67.5S | 4 | 475 | 557 | 0 | 0 | 8 | 1943 | 1531 +/- 900 | NA | 0 |
| 8.2 0+96.5W | 0+67.5S | 2 | 478 | 597 | 0 | 0 | 8 | 1911 | 2178 +/- 911 | NA | 0 |
| 8.2 1+3.5W | 0+68.5S | 2 | 478 | 489 | 0 | 0 | 8 | 1911 | 201 +/- 831 | NA | 0 |
| 8.2 1+2.5W | 0+68.5S | 5 | 475 | 574 | 0 | 0 | 8 | 1942 | 1848 +/- 912 | NA | 0 |
| 8.2 1+1.5W | 0+68.5S | 5 | 475 | 602 | 0 | 0 | 8 | 1942 | 2370 +/- 932 | NA | 0 |
| 8.2 1+0.5W | 0+68.5S | 5 | 475 | 594 | 0 | 0 | 8 | 1942 | 2221 +/- 927 | NA | 0 |
| 8.2 0+99.5W | 0+68.5S | 5 | 475 | 601 | 0 | 0 | 8 | 1942 | 2352 +/- 932 | NA | 0 |
| 8.2 0+98.5W | 0+68.5S | 5 | 475 | 653 | 0 | 0 | 8 | 1942 | 3322 +/- 968 | NA | 0 |
| 8.2 0+97.5W | 0+68.5S | 5 | 475 | 615 | 0 | 0 | 8 | 1942 | 2613 +/- 942 | NA | 0 |
| 8.2 0+96.5W | 0+68.5S | 2 | 478 | 736 | 0 | 0 | 8 | 1911 | 4723 +/-1004 | NA | 0 |
| 8.2 1+3.5W | 0+69.5S | 2 | 478 | 553 | 0 | 0 | 8 | 1911 | 1373 +/- 879 | NA | 0 |
| 8.2 1+2.5W | 0+69.5S | 5 | 475 | 620 | 0 | 0 | 8 | 1942 | 2706 +/- 945 | NA | 0 |
| 8.2 1+1.5W | 0+69.5S | 5 | 475 | 584 | 0 | 0 | 8 | 1942 | 2034 +/- 919 | NA | 0 |
| 8.2 1+0.5W | 0+69.5S | 5 | 475 | 599 | 0 | 0 | 8 | 1942 | 2314 +/- 930 | NA | 0 |
| 8.2 0+99.5W | 0+69.5S | 5 | 475 | 587 | 0 | 0 | 8 | 1942 | 2090 +/- 921 | NA | 0 |
| 8.2 0+98.5W | 0+69.5S | 5 | 475 | 682 | 0 | 0 | 8 | 1942 | 3863 +/- 988 | NA | 0 |
| 8.2 0+97.5W | 0+69.5S | 5 | 475 | 635 | 0 | 0 | 8 | 1942 | 2986 +/- 956 | NA | 0 |
| 8.2 0+96.5W | 0+69.5S | 5 | 475 | 727 | 0 | 0 | 8 | 1942 | 4703 +/-1018 | NA | 0 |
| 8.2 1+3.5W | 0+70.5S | 3 | 558.6 | 554 | 0 | 0 | 8 | 2072 | -85 +/- 890 | NA | 0 |
| 8.2 1+2.5W | 0+70.5S | 4 | 475.0 | 579 | 0 | 0 | 8 | 1943 | 1942 +/- 916 | NA | 0 |
| 8.2 1+1.5W | 0+70.5S | 4 | 475.0 | 578 | 0 | 0 | 8 | 1943 | 1923 +/- 915 | NA | 0 |
| 8.2 1+0.5W | 0+70.5S | 4 | 475.0 | 622 | 0 | 0 | 8 | 1943 | 2745 +/- 947 | NA | 0 |
| 8.2 0+99.5W | 0+70.5S | 4 | 475.0 | 599 | 0 | 0 | 8 | 1943 | 2316 +/- 931 | NA | 0 |
| 8.2 0+98.5W | 0+70.5S | 4 | 475.0 | 614 | 0 | 0 | 8 | 1943 | 2596 +/- 941 | NA | 0 |
| 8.2 0+97.5W | 0+70.5S | 2 | 478.0 | 718 | 0 | 0 | 8 | 1911 | 4393 +/- 993 | NA | 0 |
| 8.2 1+4.5W | 0+71.5S | 2 | 478.0 | 577 | 0 | 0 | 8 | 1911 | 1812 +/- 897 | NA | 0 |
| 8.2 1+3.5W | 0+71.5S | 4 | 475.0 | 580 | 0 | 0 | 8 | 1943 | 1961 +/- 917 | NA | 0 |
| 8.2 1+2.5W | 0+71.5S | 4 | 475.0 | 588 | 0 | 0 | 8 | 1943 | 2110 +/- 923 | NA | 0 |
| 8.2 1+1.5W | 0+71.5S | 4 | 475.0 | 586 | 0 | 0 | 8 | 1943 | 2073 +/- 921 | NA | 0 |
| 8.2 1+0.5W | 0+71.5S | 4 | 475.0 | 637 | 0 | 0 | 8 | 1943 | 3025 +/- 958 | NA | 0 |
| 8.2 0+99.5W | 0+71.5S | 4 | 475.0 | 608 | 0 | 0 | 8 | 1943 | 2484 +/- 937 | NA | 0 |
| 8.2 0+98.5W | 0+71.5S | 3 | 475.0 | 610 | 0 | 0 | 8 | 1914 | 2483 +/- 925 | NA | 0 |
| 8.2 0+97.5W | 0+71.5S | 2 | 478.0 | 673 | 0 | 0 | 8 | 1911 | 3569 +/- 963 | NA | 0 |
| 8.2 1+4.5W | 0+72.5S | 2 | 478.0 | 554 | 0 | 0 | 8 | 1911 | 1391 +/- 880 | NA | 0 |
| 8.2 1+3.5W | 0+72.5S | 3 | 451.0 | 545 | 0 | 0 | 8 | 1866 | 1729 +/- 876 | NA | 0 |
| 8.2 1+2.5W | 0+72.5S | 3 | 451.0 | 606 | 0 | 0 | 8 | 1866 | 2851 +/- 920 | NA | 0 |
| 8.2 1+1.5W | 0+72.5S | 3 | 451.0 | 606 | 0 | 0 | 8 | 1866 | 2851 +/- 920 | NA | 0 |
| 8.2 1+0.5W | 0+72.5S | 3 | 451.0 | 554 | 0 | 0 | 8 | 1866 | 1895 +/- 883 | NA | 0 |
| 8.2 0+99.5W | 0+72.5S | 3 | 451.0 | 568 | 0 | 0 | 8 | 1866 | 2152 +/- 893 | NA | 0 |
| 8.2 0+98.5W | 0+72.5S | 3 | 451.0 | 653 | 0 | 0 | 8 | 1866 | 3716 +/- 953 | NA | 0 |
| 8.2 0+97.5W | 0+72.5S | 2 | 478.0 | 747 | 0 | 0 | 8 | 1911 | 4924 +/-1011 | NA | 0 |
| 8.2 1+4.5W | 0+74.5S | 3 | 558.6 | 620 | 0 | 0 | 8 | 2072 | 1130 +/- 937 | NA | 0 |
| 8.2 1+3.5W | 0+74.5S | 3 | 451.0 | 602 | 0 | 0 | 8 | 1866 | 2778 +/- 917 | NA | 0 |
| 8.2 1+2.5W | 0+74.5S | 3 | 451.0 | 513 | 0 | 0 | 8 | 1866 | 1141 +/- 852 | NA | 0 |
| 8.2 1+1.5W | 0+74.5S | 3 | 451.0 | 555 | 0 | 0 | 8 | 1866 | 1913 +/- 883 | NA | 0 |
| 8.2 1+0.5W | 0+74.5S | 3 | 451.0 | 551 | 0 | 0 | 8 | 1866 | 1840 +/- 880 | NA | 0 |
| 8.2 0+99.5W | 0+74.5S | 3 | 451.0 | 625 | 0 | 0 | 8 | 1866 | 3201 +/- 933 | NA | 0 |
| 8.2 0+98.5W | 0+74.5S | 3 | 558.6 | 620 | 0 | 0 | 8 | 2072 | 1130 +/- 937 | NA | 0 |
| 8.2 1+5.5W | 0+75.5S | 3 | 558.6 | 593 | 0 | 0 | 8 | 2072 | 633 +/- 918 | NA | 0 |
| 8.2 1+4.5W | 0+75.5S | 4 | 484.4 | 612 | 0 | 0 | 8 | 1962 | 2383 +/- 941 | NA | 0 |
| 8.2 1+3.5W | 0+75.5S | 4 | 484.4 | 628 | 0 | 0 | 8 | 1962 | 2682 +/- 952 | NA | 0 |
| 8.2 1+2.5W | 0+75.5S | 4 | 484.4 | 548 | 0 | 0 | 8 | 1962 | 1188 +/- 894 | NA | 0 |
| 8.2 1+1.5W | 0+75.5S | 4 | 484.4 | 573 | 0 | 0 | 8 | 1962 | 1655 +/- 912 | NA | 0 |

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TABLE B.2-2

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|---|---|---|---|---|---|---|---|---|---|---|---|
| B.2 1+0.5W | 0+75.5S | 4 | 484.4 | 571 | 0 | 0 | 8 | 1962 | 1617 +/- 911 | NA | 0 |
| B.2 0+99.5W | 0+75.5S | 4 | 484.4 | 606 | 0 | 0 | 8 | 1962 | 2271 +/- 936 | NA | 0 |
| B.2 0+98.5W | 0+75.5S | 3 | 558.6 | 790 | 0 | 0 | 8 | 2072 | 4257 +/-1049 | NA | 0 |
| B.2 1+5.5W | 0+76.5S | 3 | 558.6 | 556 | 0 | 0 | 8 | 2072 | -48 +/- 892 | NA | 0 |
| B.2 1+4.5W | 0+76.5S | 4 | 484.4 | 520 | 0 | 0 | 8 | 1962 | 665 +/- 873 | NA | 0 |
| B.2 1+3.5W | 0+76.5S | 4 | 484.4 | 554 | 0 | 0 | 8 | 1962 | 1300 +/- 898 | NA | 0 |
| B.2 1+2.5W | 0+76.5S | 4 | 484.4 | 611 | 0 | 0 | 8 | 1962 | 2364 +/- 940 | NA | 0 |
| B.2 1+1.5W | 0+76.5S | 4 | 484.4 | 572 | 0 | 0 | 8 | 1962 | 1636 +/- 912 | NA | 0 |
| B.2 1+0.5W | 0+76.5S | 4 | 484.4 | 617 | 0 | 0 | 8 | 1962 | 2476 +/- 944 | NA | 0 |
| B.2 0+99.5W | 0+76.5S | 4 | 484.4 | 646 | 0 | 0 | 8 | 1962 | 3018 +/- 965 | NA | 0 |
| B.2 0+98.5W | 0+76.5S | 3 | 558.6 | 723 | 0 | 0 | 8 | 2072 | 3024 +/-1006 | NA | 0 |
| B.2 1+5.5W | 0+77.5S | 3 | 558.6 | 582 | 0 | 0 | 8 | 2072 | 430 +/- 911 | NA | 0 |
| B.2 1+4.5W | 0+77.5S | 4 | 484.4 | 595 | 0 | 0 | 8 | 1962 | 2065 +/- 928 | NA | 0 |
| B.2 1+3.5W | 0+77.5S | 4 | 484.4 | 580 | 0 | 0 | 8 | 1962 | 1785 +/- 918 | NA | 0 |
| B.2 1+2.5W | 0+77.5S | 4 | 484.4 | 571 | 0 | 0 | 8 | 1962 | 1617 +/- 911 | NA | 0 |
| B.2 1+1.5W | 0+77.5S | 4 | 484.4 | 601 | 0 | 0 | 8 | 1962 | 2177 +/- 933 | NA | 0 |
| B.2 1+0.5W | 0+77.5S | 4 | 484.4 | 613 | 0 | 0 | 8 | 1962 | 2401 +/- 941 | NA | 0 |
| B.2 0+99.5W | 0+77.5S | 4 | 484.4 | 624 | 0 | 0 | 8 | 1962 | 2607 +/- 949 | NA | 0 |
| B.2 0+98.5W | 0+77.5S | 3 | 558.6 | 790 | 0 | 0 | 8 | 2072 | 4257 +/-1049 | NA | 0 |
| B.2 1+5.5W | 0+78.5S | 3 | 558.6 | 565 | 0 | 0 | 8 | 2072 | 118 +/- 898 | NA | 0 |
| B.2 1+4.5W | 0+78.5S | 4 | 484.4 | 712 | 0 | 0 | 8 | 1962 | 4250 +/-1009 | NA | 0 |
| B.2 1+3.5W | 0+78.5S | 3 | 466.6 | 661 | 0 | 0 | 8 | 1898 | 3576 +/- 939 | NA | 0 |
| B.2 1+2.5W | 0+78.5S | 3 | 466.6 | 571 | 0 | 0 | 8 | 1898 | 1921 +/- 896 | NA | 0 |
| B.2 1+1.5W | 0+78.5S | 3 | 466.6 | 535 | 0 | 0 | 8 | 1898 | 1258 +/- 870 | NA | 0 |
| B.2 0+99.5W | 0+78.5S | 3 | 466.6 | 558 | 0 | 0 | 8 | 1898 | 1681 +/- 887 | NA | 0 |
| B.2 0+98.5W | 0+78.5S | 3 | 558.6 | 665 | 0 | 0 | 8 | 2072 | 1957 +/- 968 | NA | 0 |
| B.2 1+6.5W | 0+78.5S | 3 | 558.6 | 597 | 0 | 0 | 8 | 2072 | 706 +/- 921 | NA | 0 |
| B.2 1+5.5W | 0+79.5S | 3 | 466.6 | 639 | 0 | 0 | 8 | 1898 | 3171 +/- 944 | NA | 0 |
| B.2 1+4.5W | 0+79.5S | 3 | 466.6 | 604 | 0 | 0 | 8 | 1898 | 2528 +/- 920 | NA | 0 |
| B.2 1+3.5W | 0+79.5S | 3 | 466.6 | 661 | 0 | 0 | 8 | 1898 | 3576 +/- 939 | NA | 0 |
| B.2 1+2.5W | 0+79.5S | 3 | 466.6 | 587 | 0 | 0 | 8 | 1898 | 2215 +/- 908 | NA | 0 |
| B.2 1+1.5W | 0+79.5S | 3 | 466.6 | 611 | 0 | 0 | 8 | 1898 | 2656 +/- 925 | NA | 0 |
| B.2 1+0.5W | 0+79.5S | 3 | 466.6 | 583 | 0 | 0 | 8 | 1898 | 2141 +/- 905 | NA | 0 |
| B.2 0+99.5W | 0+79.5S | 3 | 558.6 | 723 | 0 | 0 | 8 | 2072 | 3024 +/-1006 | NA | 0 |
| B.2 1+2.5W | 0+89.5S | 3 | 558.6 | 592 | 0 | 0 | 8 | 2072 | 614 +/- 918 | NA | 0 |
| B.2 1+3.5W | 0+89.5S | 4 | 499.7 | 553 | 0 | 0 | 8 | 1992 | 995 +/- 899 | NA | 0 |
| B.2 1+4.5W | 0+89.5S | 4 | 499.7 | 548 | 0 | 0 | 8 | 1992 | 902 +/- 895 | NA | 0 |
| B.2 1+5.5W | 0+89.5S | 4 | 499.7 | 555 | 0 | 0 | 8 | 1992 | 1033 +/- 900 | NA | 0 |
| B.2 1+6.5W | 0+89.5S | 4 | 499.7 | 564 | 0 | 0 | 8 | 1992 | 1201 +/- 907 | NA | 0 |
| B.2 1+7.5W | 0+89.5S | 4 | 499.7 | 628 | 0 | 0 | 8 | 1992 | 2396 +/- 953 | NA | 0 |
| B.2 1+8.5W | 0+89.5S | 3 | 558.6 | 665 | 0 | 0 | 8 | 2072 | 1957 +/- 968 | NA | 0 |
| B.2 1+2.5W | 0+88.5S | 3 | 558.6 | 535 | 0 | 0 | 8 | 2072 | -434 +/- 876 | NA | 0 |
| B.2 1+3.5W | 0+88.5S | 4 | 499.7 | 594 | 0 | 0 | 8 | 1992 | 1761 +/- 929 | NA | 0 |
| B.2 1+4.5W | 0+88.5S | 4 | 499.7 | 540 | 0 | 0 | 8 | 1992 | 753 +/- 889 | NA | 0 |
| B.2 1+5.5W | 0+88.5S | 4 | 499.7 | 563 | 0 | 0 | 8 | 1992 | 1182 +/- 906 | NA | 0 |
| B.2 1+6.5W | 0+88.5S | 4 | 499.7 | 609 | 0 | 0 | 8 | 1992 | 2041 +/- 940 | NA | 0 |
| B.2 1+7.5W | 0+88.5S | 4 | 499.7 | 635 | 0 | 0 | 8 | 1992 | 2527 +/- 958 | NA | 0 |
| B.2 1+8.5W | 0+88.5S | 3 | 558.6 | 566 | 0 | 0 | 8 | 2072 | 136 +/- 899 | NA | 0 |
| B.2 1+2.5W | 0+87.5S | 3 | 558.6 | 530 | 0 | 0 | 8 | 2072 | -526 +/- 873 | NA | 0 |
| B.2 1+3.5W | 0+87.5S | 4 | 499.7 | 531 | 0 | 0 | 8 | 1992 | 585 +/- 882 | NA | 0 |
| B.2 1+4.5W | 0+87.5S | 4 | 499.7 | 505 | 0 | 0 | 8 | 1992 | 99 +/- 862 | NA | 0 |
| B.2 1+5.5W | 0+87.5S | 4 | 499.7 | 591 | 0 | 0 | 8 | 1992 | 1705 +/- 927 | NA | 0 |
| B.2 1+6.5W | 0+87.5S | 4 | 499.7 | 536 | 0 | 0 | 8 | 1992 | 678 +/- 886 | NA | 0 |
| B.2 1+7.5W | 0+87.5S | 4 | 499.7 | 587 | 0 | 0 | 8 | 1992 | 1630 +/- 924 | NA | 0 |
| B.2 1+8.5W | 0+87.5S | 3 | 558.6 | 566 | 0 | 0 | 8 | 2072 | 136 +/- 899 | NA | 0 |
| B.2 1+1.5W | 0+86.5S | 3 | 558.6 | 765 | 0 | 0 | 8 | 2072 | 3797 +/-1033 | NA | 0 |

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| B.2 1+2.5W | 0+86.5S | 4 | 499.7 | 611 | 0 | 0 | 8 | 1992 | 2078 +/- 941 | NA | 0 |
| B.2 1+3.5W | 0+86.5S | 4 | 499.7 | 575 | 0 | 0 | 8 | 1992 | 1406 +/- 915 | NA | 0 |
| B.2 1+4.5W | 0+86.5S | 4 | 499.7 | 568 | 0 | 0 | 8 | 1992 | 1275 +/- 910 | NA | 0 |
| B.2 1+5.5W | 0+86.5S | 4 | 499.7 | 577 | 0 | 0 | 8 | 1992 | 1444 +/- 916 | NA | 0 |
| B.2 1+6.5W | 0+86.5S | 4 | 499.7 | 563 | 0 | 0 | 8 | 1992 | 1182 +/- 906 | NA | 0 |
| B.2 1+7.5W | 0+86.5S | 4 | 499.7 | 576 | 0 | 0 | 8 | 1992 | 1425 +/- 916 | NA | 0 |
| B.2 1+8.5W | 0+86.5S | 3 | 558.6 | 566 | 0 | 0 | 8 | 2072 | 136 +/- 899 | NA | 0 |
| B.2 1+1.5W | 0+85.5S | 3 | 558.6 | 604 | 0 | 0 | 8 | 2072 | 835 +/- 926 | NA | 0 |
| B.2 1+2.5W | 0+85.5S | 3 | 487.6 | 605 | 0 | 0 | 8 | 1939 | 2160 +/- 922 | NA | 0 |
| B.2 1+3.5W | 0+85.5S | 3 | 487.6 | 560 | 0 | 0 | 8 | 1939 | 1332 +/- 890 | NA | 0 |
| B.2 1+4.5W | 0+85.5S | 3 | 487.6 | 560 | 0 | 0 | 8 | 1939 | 1332 +/- 890 | NA | 0 |
| B.2 1+5.5W | 0+85.5S | 3 | 487.6 | 568 | 0 | 0 | 8 | 1939 | 1479 +/- 895 | NA | 0 |
| B.2 1+6.5W | 0+85.5S | 3 | 487.6 | 594 | 0 | 0 | 8 | 1939 | 1957 +/- 914 | NA | 0 |
| B.2 1+7.5W | 0+85.5S | 3 | 558.6 | 566 | 0 | 0 | 8 | 2072 | 136 +/- 899 | NA | 0 |
| B.2 1+1.5W | 0+84.5S | 3 | 487.6 | 576 | 0 | 0 | 8 | 1939 | 1626 +/- 901 | NA | 0 |
| B.2 1+2.5W | 0+84.5S | 3 | 487.6 | 614 | 0 | 0 | 8 | 1939 | 2325 +/- 928 | NA | 0 |
| B.2 1+3.5W | 0+84.5S | 3 | 487.6 | 551 | 0 | 0 | 8 | 1939 | 1166 +/- 883 | NA | 0 |
| B.2 1+4.5W | 0+84.5S | 3 | 487.6 | 537 | 0 | 0 | 8 | 1939 | 909 +/- 873 | NA | 0 |
| B.2 1+5.5W | 0+84.5S | 3 | 487.6 | 647 | 0 | 0 | 8 | 1939 | 2932 +/- 951 | NA | 0 |
| B.2 1+6.5W | 0+84.5S | 3 | 487.6 | 610 | 0 | 0 | 8 | 1939 | 2252 +/- 925 | NA | 0 |
| B.2 1+7.5W | 0+84.5S | 3 | 558.6 | 517 | 0 | 0 | 8 | 2072 | -765 +/- 863 | NA | 0 |
| B.2 1+1.5W | 0+83.5S | 3 | 558.6 | 663 | 0 | 0 | 8 | 2072 | 1921 +/- 967 | NA | 0 |
| B.2 1+2.5W | 0+83.5S | 3 | 487.6 | 621 | 0 | 0 | 8 | 1939 | 2454 +/- 933 | NA | 0 |
| B.2 1+3.5W | 0+83.5S | 3 | 487.6 | 594 | 0 | 0 | 8 | 1939 | 1957 +/- 914 | NA | 0 |
| B.2 1+4.5W | 0+83.5S | 3 | 487.6 | 529 | 0 | 0 | 8 | 1939 | 762 +/- 867 | NA | 0 |
| B.2 1+5.5W | 0+83.5S | 3 | 487.6 | 525 | 0 | 0 | 8 | 1939 | 688 +/- 864 | NA | 0 |
| B.2 1+6.5W | 0+83.5S | 3 | 487.6 | 641 | 0 | 0 | 8 | 1939 | 2822 +/- 947 | NA | 0 |
| B.2 1+7.5W | 0+83.5S | 3 | 558.6 | 554 | 0 | 0 | 8 | 2072 | -85 +/- 890 | NA | 0 |
| B.2 1+0.5W | 0+82.5S | 3 | 558.6 | 601 | 0 | 0 | 8 | 2072 | 780 +/- 924 | NA | 0 |
| B.2 1+1.5W | 0+82.5S | 3 | 487.6 | 635 | 0 | 0 | 8 | 1939 | 2712 +/- 943 | NA | 0 |
| B.2 1+2.5W | 0+82.5S | 3 | 487.6 | 630 | 0 | 0 | 8 | 1939 | 2620 +/- 939 | NA | 0 |
| B.2 1+3.5W | 0+82.5S | 3 | 487.6 | 607 | 0 | 0 | 8 | 1939 | 2196 +/- 923 | NA | 0 |
| B.2 1+4.5W | 0+82.5S | 3 | 487.6 | 547 | 0 | 0 | 8 | 1939 | 1093 +/- 880 | NA | 0 |
| B.2 1+5.5W | 0+82.5S | 3 | 487.6 | 635 | 0 | 0 | 8 | 1939 | 2712 +/- 943 | NA | 0 |
| B.2 1+6.5W | 0+82.5S | 3 | 558.6 | 584 | 0 | 0 | 8 | 2072 | 467 +/- 912 | NA | 0 |
| B.2 1+0.5W | 0+81.5S | 3 | 558.6 | 702 | 0 | 0 | 8 | 2072 | 2638 +/- 993 | NA | 0 |
| B.2 1+1.5W | 0+81.5S | 3 | 466.6 | 641 | 0 | 0 | 8 | 1898 | 3208 +/- 946 | NA | 0 |
| B.2 1+2.5W | 0+81.5S | 3 | 466.6 | 658 | 0 | 0 | 8 | 1898 | 3521 +/- 957 | NA | 0 |
| B.2 1+3.5W | 0+81.5S | 3 | 466.6 | 598 | 0 | 0 | 8 | 1898 | 2417 +/- 915 | NA | 0 |
| B.2 1+4.5W | 0+81.5S | 3 | 466.6 | 611 | 0 | 0 | 8 | 1898 | 2656 +/- 925 | NA | 0 |
| B.2 1+5.5W | 0+81.5S | 3 | 466.6 | 561 | 0 | 0 | 8 | 1898 | 1737 +/- 889 | NA | 0 |
| B.2 1+6.5W | 0+81.5S | 3 | 558.6 | 537 | 0 | 0 | 8 | 2072 | -397 +/- 878 | NA | 0 |
| B.2 0+99.5W | 0+80.5S | 3 | 558.6 | 677 | 0 | 0 | 8 | 2072 | 2178 +/- 976 | NA | 0 |
| B.2 1+0.5W | 0+80.5S | 3 | 466.6 | 665 | 0 | 0 | 8 | 1898 | 3650 +/- 962 | NA | 0 |
| B.2 1+1.5W | 0+80.5S | 3 | 466.6 | 579 | 0 | 0 | 8 | 1898 | 2068 +/- 902 | NA | 0 |
| B.2 1+2.5W | 0+80.5S | 3 | 466.6 | 591 | 0 | 0 | 8 | 1898 | 2288 +/- 910 | NA | 0 |
| B.2 1+3.5W | 0+80.5S | 3 | 466.6 | 573 | 0 | 0 | 8 | 1898 | 1957 +/- 898 | NA | 0 |
| B.2 1+4.5W | 0+80.5S | 3 | 466.6 | 607 | 0 | 0 | 8 | 1898 | 2583 +/- 922 | NA | 0 |
| B.2 1+5.5W | 0+80.5S | 3 | 466.6 | 641 | 0 | 0 | 8 | 1898 | 3208 +/- 946 | NA | 0 |
| B.2 1+6.5W | 0+80.5S | 3 | 558.6 | 553 | 0 | 0 | 8 | 2072 | -103 +/- 890 | NA | 0 |
| B.2 1+9.5W | 0+90.5S | 3 | 558.6 | 597 | 0 | 0 | 8 | 2072 | 706 +/- 921 | NA | 0 |
| B.2 1+8.5W | 0+90.5S | 4 | 499.7 | 624 | 0 | 0 | 8 | 1992 | 2321 +/- 950 | NA | 0 |
| B.2 1+7.5W | 0+90.5S | 4 | 499.7 | 568 | 0 | 0 | 8 | 1992 | 1275 +/- 910 | NA | 0 |
| B.2 1+6.5W | 0+90.5S | 4 | 499.7 | 573 | 0 | 0 | 8 | 1992 | 1369 +/- 914 | NA | 0 |
| B.2 1+5.5W | 0+90.5S | 4 | 499.7 | 590 | 0 | 0 | 8 | 1992 | 1686 +/- 926 | NA | 0 |
| B.2 1+4.5W | 0+90.5S | 4 | 499.7 | 573 | 0 | 0 | 8 | 1992 | 1369 +/- 914 | NA | 0 |

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TABLE B.2-2

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|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 1+9.5 | 1+13.5 | 2 | 461.1 | 567 | 0 | 0 | 8 | 1877 | 1938 +/- 888 | NA | 0 |
| 8.2 1+8.5 | 1+13.5 | 2 | 461.1 | 503 | 0 | 0 | 8 | 1877 | 767 +/- 841 | NA | 0 |
| 8.2 1+15.5 | 1+14.5 | 2 | 461.1 | 735 | 0 | 0 | 8 | 1877 | 5014 +/-1003 | NA | 0 |
| 8.2 1+14.5 | 1+14.5 | 2 | 461.1 | 605 | 0 | 0 | 8 | 1877 | 2634 +/- 915 | NA | 0 |
| 8.2 1+13.5 | 1+14.5 | 2 | 461.1 | 594 | 0 | 0 | 8 | 1877 | 2433 +/- 908 | NA | 0 |
| 8.2 1+12.5 | 1+14.5 | 2 | 461.1 | 599 | 0 | 0 | 8 | 1877 | 2524 +/- 911 | NA | 0 |
| 8.2 1+11.5 | 1+14.5 | 2 | 461.1 | 559 | 0 | 0 | 8 | 1877 | 1792 +/- 883 | NA | 0 |
| 8.2 1+10.5 | 1+14.5 | 2 | 461.1 | 513 | 0 | 0 | 8 | 1877 | 950 +/- 848 | NA | 0 |
| 8.2 1+9.5 | 1+14.5 | 2 | 461.1 | 612 | 0 | 0 | 8 | 1877 | 2762 +/- 920 | NA | 0 |
| 8.2 1+8.5 | 1+14.5 | 2 | 461.1 | 552 | 0 | 0 | 8 | 1877 | 1664 +/- 877 | NA | 0 |
| 8.2 1+15.5 | 1+15.5 | 2 | 461.1 | 671 | 0 | 0 | 8 | 1877 | 3842 +/- 961 | NA | 0 |
| 8.2 1+14.5 | 1+15.5 | 2 | 461.1 | 585 | 0 | 0 | 8 | 1877 | 2268 +/- 901 | NA | 0 |
| 8.2 1+13.5 | 1+15.5 | 2 | 461.1 | 484 | 0 | 0 | 8 | 1877 | 419 +/- 826 | NA | 0 |
| 8.2 1+12.5 | 1+15.5 | 2 | 461.1 | 532 | 0 | 0 | 8 | 1877 | 1298 +/- 863 | NA | 0 |
| 8.2 1+11.5 | 1+15.5 | 2 | 461.1 | 550 | 0 | 0 | 8 | 1877 | 1627 +/- 876 | NA | 0 |
| 8.2 1+10.5 | 1+15.5 | 2 | 461.1 | 529 | 0 | 0 | 8 | 1877 | 1243 +/- 860 | NA | 0 |
| 8.2 1+9.5 | 1+15.5 | 2 | 461.1 | 552 | 0 | 0 | 8 | 1877 | 1664 +/- 877 | NA | 0 |
| 8.2 1+15.5 | 1+16.5 | 2 | 461.1 | 612 | 0 | 0 | 8 | 1877 | 2762 +/- 920 | NA | 0 |
| 8.2 1+14.5 | 1+16.5 | 2 | 461.1 | 604 | 0 | 0 | 8 | 1877 | 2616 +/- 915 | NA | 0 |
| 8.2 1+13.5 | 1+16.5 | 2 | 461.1 | 536 | 0 | 0 | 8 | 1877 | 1371 +/- 866 | NA | 0 |
| 8.2 1+12.5 | 1+16.5 | 2 | 461.1 | 535 | 0 | 0 | 8 | 1877 | 1353 +/- 865 | NA | 0 |
| 8.2 1+11.5 | 1+16.5 | 2 | 461.1 | 571 | 0 | 0 | 8 | 1877 | 2012 +/- 891 | NA | 0 |
| 8.2 1+10.5 | 1+16.5 | 4 | 532.4 | 626 | 0 | 0 | 8 | 2054 | 1748 +/- 954 | NA | 0 |
| 8.2 1+9.5 | 1+16.5 | 4 | 532.4 | 578 | 0 | 0 | 8 | 2054 | 852 +/- 920 | NA | 0 |
| 8.2 1+8.5 | 1+16.5 | 4 | 532.4 | 589 | 0 | 0 | 8 | 2054 | 1057 +/- 928 | NA | 0 |
| 8.2 1+15.5 | 1+17.5 | 4 | 532.4 | 673 | 0 | 0 | 8 | 2054 | 2626 +/- 986 | NA | 0 |
| 8.2 1+14.5 | 1+17.5 | 4 | 532.4 | 584 | 0 | 0 | 8 | 2054 | 934 +/- 924 | NA | 0 |
| 8.2 1+13.5 | 1+17.5 | 4 | 532.4 | 667 | 0 | 0 | 8 | 2054 | 2614 +/- 982 | NA | 0 |
| 8.2 1+12.5 | 1+17.5 | 4 | 532.4 | 603 | 0 | 0 | 8 | 2054 | 1318 +/- 938 | NA | 0 |
| 8.2 1+11.5 | 1+17.5 | 4 | 532.4 | 587 | 0 | 0 | 8 | 2054 | 1020 +/- 926 | NA | 0 |
| 8.2 1+10.5 | 1+17.5 | 4 | 532.4 | 634 | 0 | 0 | 8 | 2054 | 1897 +/- 960 | NA | 0 |
| 8.2 1+9.5 | 1+17.5 | 4 | 532.4 | 595 | 0 | 0 | 8 | 2054 | 1169 +/- 932 | NA | 0 |
| 8.2 1+16.5 | 1+18.5 | 4 | 532.4 | 717 | 0 | 0 | 8 | 2054 | 3447 +/-1016 | NA | 0 |
| 8.2 1+15.5 | 1+18.5 | 4 | 532.4 | 595 | 0 | 0 | 8 | 2054 | 1169 +/- 932 | NA | 0 |
| 8.2 1+14.5 | 1+18.5 | 4 | 532.4 | 591 | 0 | 0 | 8 | 2054 | 1094 +/- 929 | NA | 0 |
| 8.2 1+13.5 | 1+18.5 | 4 | 532.4 | 634 | 0 | 0 | 8 | 2054 | 1897 +/- 960 | NA | 0 |
| 8.2 1+12.5 | 1+18.5 | 4 | 532.4 | 555 | 0 | 0 | 8 | 2054 | 422 +/- 903 | NA | 0 |
| 8.2 1+11.5 | 1+18.5 | 4 | 532.4 | 629 | 0 | 0 | 8 | 2054 | 1804 +/- 956 | NA | 0 |
| 8.2 1+10.5 | 1+18.5 | 4 | 532.4 | 678 | 0 | 0 | 8 | 2054 | 2719 +/- 990 | NA | 0 |
| 8.2 1+9.5 | 1+18.5 | 4 | 532.4 | 654 | 0 | 0 | 8 | 2054 | 2271 +/- 973 | NA | 0 |
| 8.2 1+16.5 | 1+19.5 | 4 | 532.4 | 738 | 0 | 0 | 8 | 2054 | 3839 +/-1030 | NA | 0 |
| 8.2 1+15.5 | 1+19.5 | 4 | 532.4 | 621 | 0 | 0 | 8 | 2054 | 1655 +/- 950 | NA | 0 |
| 8.2 1+14.5 | 1+19.5 | 4 | 532.4 | 694 | 0 | 0 | 8 | 2054 | 3018 +/-1001 | NA | 0 |
| 8.2 1+13.5 | 1+19.5 | 4 | 532.4 | 619 | 0 | 0 | 8 | 2054 | 1617 +/- 949 | NA | 0 |
| 8.2 1+12.5 | 1+19.5 | 4 | 532.4 | 645 | 0 | 0 | 8 | 2054 | 2103 +/- 967 | NA | 0 |
| 8.2 1+11.5 | 1+19.5 | 4 | 532.4 | 637 | 0 | 0 | 8 | 2054 | 1953 +/- 962 | NA | 0 |
| 8.2 1+10.5 | 1+19.5 | 4 | 532.4 | 668 | 0 | 0 | 8 | 2054 | 2532 +/- 983 | NA | 0 |
| 8.2 1+9.5 | 1+19.5 | 4 | 532.4 | 698 | 0 | 0 | 8 | 2054 | 3092 +/-1003 | NA | 0 |
| 8.2 1+19.5W | 1+20.5S | 3 | 503.5 | 615 | 0 | 0 | 8 | 1969 | 2051 +/- 930 | NA | 0 |
| 8.2 1+18.5W | 1+20.5S | 3 | 503.5 | 582 | 0 | 0 | 8 | 1969 | 1444 +/- 907 | NA | 0 |
| 8.2 1+17.5W | 1+20.5S | 3 | 503.5 | 670 | 0 | 0 | 8 | 1969 | 3063 +/- 968 | NA | 0 |
| 8.2 1+16.5W | 1+20.5S | 3 | 503.5 | 614 | 0 | 0 | 8 | 1969 | 2033 +/- 929 | NA | 0 |
| 8.2 1+15.5W | 1+20.5S | 3 | 503.5 | 636 | 0 | 0 | 8 | 1969 | 2437 +/- 945 | NA | 0 |
| 8.2 1+14.5W | 1+20.5S | 3 | 503.5 | 221 | 0 | 0 | 8 | 1969 | -5197 +/- 594 | NA | 0 |
| 8.2 1+13.5W | 1+20.5S | 3 | 503.5 | 646 | 0 | 0 | 8 | 1969 | 2621 +/- 951 | NA | 0 |
| 8.2 1+19.5W | 1+21.5S | 3 | 503.5 | 608 | 0 | 0 | 8 | 1969 | 1922 +/- 925 | NA | 0 |

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|---|---|---|---|---|---|---|---|---|---|---|---|
| B.2 1+11.5W | 1+6.5S | 3 | 477.3 | 569 | 0 | 0 | B | 1919 | 1687 +/- 895 | NA | |
| B.2 1+10.5W | 1+6.5S | 3 | 477.3 | 617 | 0 | 0 | B | 1919 | 2570 +/- 930 | NA | |
| B.2 1+9.5W | 1+6.5S | 3 | 477.3 | 579 | 0 | 0 | B | 1919 | 1871 +/- 903 | NA | |
| B.2 1+8.5W | 1+6.5S | 3 | 477.3 | 633 | 0 | 0 | B | 1919 | 2864 +/- 941 | NA | |
| B.2 1+7.5W | 1+6.5S | 3 | 477.3 | 601 | 0 | 0 | B | 1919 | 2276 +/- 918 | NA | |
| B.2 1+6.5W | 1+6.5S | 3 | 477.3 | 643 | 0 | 0 | B | 1919 | 3048 +/- 948 | NA | |
| B.2 1+13.5W | 1+7.5S | 4 | 423.4 | 688 | 0 | 0 | B | 1837 | 4941 +/- 989 | NA | |
| B.2 1+12.5W | 1+7.5S | 4 | 423.4 | 585 | 0 | 0 | B | 1837 | 3018 +/- 917 | NA | |
| B.2 1+11.5W | 1+7.5S | 4 | 423.4 | 556 | 0 | 0 | B | 1837 | 2476 +/- 895 | NA | |
| B.2 1+10.5W | 1+7.5S | 4 | 423.4 | 511 | 0 | 0 | B | 1837 | 1636 +/- 861 | NA | |
| B.2 1+9.5W | 1+7.5S | 4 | 423.4 | 562 | 0 | 0 | B | 1837 | 2588 +/- 900 | NA | |
| B.2 1+8.5W | 1+7.5S | 4 | 423.4 | 581 | 0 | 0 | B | 1837 | 2943 +/- 914 | NA | |
| B.2 1+7.5W | 1+7.5S | 4 | 423.4 | 600 | 0 | 0 | B | 1837 | 3298 +/- 928 | NA | |
| B.2 1+6.5W | 1+7.5S | 4 | 423.4 | 668 | 0 | 0 | B | 1837 | 4568 +/- 976 | NA | |
| B.2 1+13.5W | 1+8.5S | 4 | 423.4 | 585 | 0 | 0 | B | 1837 | 3018 +/- 917 | NA | |
| B.2 1+12.5W | 1+8.5S | 4 | 423.4 | 565 | 0 | 0 | B | 1837 | 2644 +/- 902 | NA | |
| B.2 1+11.5W | 1+8.5S | 4 | 423.4 | 587 | 0 | 0 | B | 1837 | 3055 +/- 918 | NA | |
| B.2 1+10.5W | 1+8.5S | 4 | 423.4 | 529 | 0 | 0 | B | 1837 | 1972 +/- 875 | NA | |
| B.2 1+9.5W | 1+8.5S | 4 | 423.4 | 557 | 0 | 0 | B | 1837 | 2495 +/- 896 | NA | |
| B.2 1+8.5W | 1+8.5S | 4 | 423.4 | 567 | 0 | 0 | B | 1837 | 2682 +/- 903 | NA | |
| B.2 1+7.5W | 1+8.5S | 4 | 423.4 | 575 | 0 | 0 | B | 1837 | 2831 +/- 909 | NA | |
| B.2 1+13.5W | 1+9.5S | 4 | 423.4 | 606 | 0 | 0 | B | 1837 | 3410 +/- 932 | NA | |
| B.2 1+12.5W | 1+9.5S | 4 | 423.4 | 533 | 0 | 0 | B | 1837 | 2047 +/- 878 | NA | |
| B.2 1+11.5W | 1+9.5S | 4 | 423.4 | 489 | 0 | 0 | B | 1837 | 1225 +/- 844 | NA | |
| B.2 1+10.5W | 1+9.5S | 4 | 423.4 | 538 | 0 | 0 | B | 1837 | 2140 +/- 882 | NA | |
| B.2 1+9.5W | 1+9.5S | 4 | 423.4 | 562 | 0 | 0 | B | 1837 | 2588 +/- 900 | NA | |
| B.2 1+8.5W | 1+9.5S | 4 | 423.4 | 616 | 0 | 0 | B | 1837 | 3597 +/- 939 | NA | |
| B.2 1+7.5W | 1+9.5S | 4 | 423.4 | 673 | 0 | 0 | B | 1837 | 4661 +/- 979 | NA | |
| B.2 1+13.5 | 1+10.5 | 4 | 423.4 | 625 | 0 | 0 | B | 1837 | 3765 +/- 946 | NA | |
| B.2 1+12.5 | 1+10.5 | 4 | 423.4 | 531 | 0 | 0 | B | 1837 | 2009 +/- 876 | NA | |
| B.2 1+11.5 | 1+10.5 | 4 | 423.4 | 534 | 0 | 0 | B | 1837 | 2065 +/- 879 | NA | |
| B.2 1+10.5 | 1+10.5 | 4 | 423.4 | 582 | 0 | 0 | B | 1837 | 2962 +/- 915 | NA | |
| B.2 1+9.5 | 1+10.5 | 4 | 423.4 | 563 | 0 | 0 | B | 1837 | 2607 +/- 901 | NA | |
| B.2 1+8.5 | 1+10.5 | 4 | 423.4 | 582 | 0 | 0 | B | 1837 | 2962 +/- 915 | NA | |
| B.2 1+7.5 | 1+10.5 | 4 | 423.4 | 640 | 0 | 0 | B | 1837 | 4045 +/- 956 | NA | |
| B.2 1+14.5 | 1+11.5 | 4 | 423.4 | 693 | 0 | 0 | B | 1837 | 5035 +/- 993 | NA | |
| B.2 1+13.5 | 1+11.5 | 4 | 423.4 | 567 | 0 | 0 | B | 1837 | 2682 +/- 903 | NA | |
| B.2 1+12.5 | 1+11.5 | 4 | 423.4 | 505 | 0 | 0 | B | 1837 | 1524 +/- 856 | NA | |
| B.2 1+11.5 | 1+11.5 | 4 | 423.4 | 588 | 0 | 0 | B | 1837 | 3074 +/- 919 | NA | |
| B.2 1+10.5 | 1+11.5 | 4 | 423.4 | 546 | 0 | 0 | B | 1837 | 2289 +/- 888 | NA | |
| B.2 1+9.5 | 1+11.5 | 4 | 423.4 | 514 | 0 | 0 | B | 1837 | 1692 +/- 863 | NA | |
| B.2 1+8.5 | 1+11.5 | 4 | 423.4 | 553 | 0 | 0 | B | 1837 | 2420 +/- 893 | NA | |
| B.2 1+7.5 | 1+11.5 | 2 | 461.1 | 596 | 0 | 0 | B | 1877 | 2469 +/- 909 | NA | |
| B.2 1+14.5 | 1+12.5 | 2 | 461.1 | 537 | 0 | 0 | B | 1877 | 1389 +/- 866 | NA | |
| B.2 1+13.5 | 1+12.5 | 2 | 461.1 | 514 | 0 | 0 | B | 1877 | 968 +/- 849 | NA | |
| B.2 1+12.5 | 1+12.5 | 2 | 461.1 | 545 | 0 | 0 | B | 1877 | 1536 +/- 872 | NA | |
| B.2 1+11.5 | 1+12.5 | 2 | 461.1 | 554 | 0 | 0 | B | 1877 | 1701 +/- 879 | NA | |
| B.2 1+10.5 | 1+12.5 | 2 | 461.1 | 526 | 0 | 0 | B | 1877 | 1188 +/- 858 | NA | |
| B.2 1+9.5 | 1+12.5 | 2 | 494.1 | 519 | 0 | 0 | B | 1942 | 456 +/- 855 | NA | |
| B.2 1+8.5 | 1+12.5 | 2 | 461.1 | 555 | 0 | 0 | B | 1877 | 1719 +/- 880 | NA | |
| B.2 1+15.5 | 1+13.5 | 2 | 461.1 | 677 | 0 | 0 | B | 1877 | 3952 +/- 965 | NA | |
| B.2 1+14.5 | 1+13.5 | 2 | 461.1 | 578 | 0 | 0 | B | 1877 | 2146 +/- 896 | NA | |
| B.2 1+13.5 | 1+13.5 | 2 | 461.1 | 517 | 0 | 0 | B | 1877 | 1023 +/- 851 | NA | |
| B.2 1+12.5 | 1+13.5 | 2 | 461.1 | 537 | 0 | 0 | B | 1877 | 1389 +/- 866 | NA | |
| B.2 1+11.5 | 1+13.5 | 2 | 461.1 | 551 | 0 | 0 | B | 1877 | 1646 +/- 877 | NA | |
| B.2 1+10.5 | 1+13.5 | 2 | 461.1 | 526 | 0 | 0 | B | 1877 | 1188 +/- 858 | NA | |

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|---|---|---|---|---|---|---|---|---|---|---|---|
| B.2 1+5.5W | 0+98.5S | 4 | 464.2 | 569 | 0 | 0 | B | 1921 | 1957 +/- 908 | NA | |
| B.2 1+4.5W | 0+98.5S | 3 | 558.6 | 728 | 0 | 0 | B | 2072 | 3116 +/-1009 | NA | |
| B.2 1+11.5W | 0+99.5S | 3 | 558.6 | 596 | 0 | 0 | B | 2072 | 688 +/- 921 | NA | |
| B.2 1+10.5W | 0+99.5S | 4 | 464.2 | 576 | 0 | 0 | B | 1921 | 2088 +/- 913 | NA | |
| B.2 1+9.5W | 0+99.5S | 4 | 464.2 | 566 | 0 | 0 | B | 1921 | 1901 +/- 906 | NA | |
| B.2 1+8.5W | 0+99.5S | 4 | 464.2 | 583 | 0 | 0 | B | 1921 | 2218 +/- 918 | NA | |
| B.2 1+7.5W | 0+99.5S | 4 | 464.2 | 519 | 0 | 0 | B | 1921 | 1023 +/- 870 | NA | |
| B.2 1+6.5W | 0+99.5S | 4 | 464.2 | 540 | 0 | 0 | B | 1921 | 1415 +/- 886 | NA | |
| B.2 1+5.5W | 0+99.5S | 3 | 558.6 | 635 | 0 | 0 | B | 2072 | 1405 +/- 948 | NA | |
| B.2 1+11.5W | 1+0.5S | 4 | 464.2 | 673 | 0 | 0 | B | 1921 | 3899 +/- 982 | NA | |
| B.2 1+10.5W | 1+0.5S | 4 | 464.2 | 550 | 0 | 0 | B | 1921 | 1602 +/- 894 | NA | |
| B.2 1+9.5W | 1+0.5S | 4 | 464.2 | 573 | 0 | 0 | B | 1921 | 2032 +/- 911 | NA | |
| B.2 1+8.5W | 1+0.5S | 4 | 464.2 | 578 | 0 | 0 | B | 1921 | 2125 +/- 915 | NA | |
| B.2 1+7.5W | 1+0.5S | 4 | 464.2 | 557 | 0 | 0 | B | 1921 | 1733 +/- 899 | NA | |
| B.2 1+6.5W | 1+0.5S | 4 | 464.2 | 546 | 0 | 0 | B | 1921 | 1528 +/- 891 | NA | |
| B.2 1+5.5W | 1+0.5S | 4 | 464.2 | 553 | 0 | 0 | B | 1921 | 1658 +/- 896 | NA | |
| B.2 1+4.5W | 1+0.5S | 4 | 464.2 | 545 | 0 | 0 | B | 1921 | 1509 +/- 890 | NA | |
| B.2 1+12.5W | 1+1.5S | 3 | 477.3 | 688 | 0 | 0 | B | 1919 | 3876 +/- 978 | NA | |
| B.2 1+11.5W | 1+1.5S | 3 | 477.3 | 664 | 0 | 0 | B | 1919 | 3435 +/- 962 | NA | |
| B.2 1+10.5W | 1+1.5S | 3 | 477.3 | 621 | 0 | 0 | B | 1919 | 2643 +/- 932 | NA | |
| B.2 1+9.5W | 1+1.5S | 3 | 477.3 | 610 | 0 | 0 | B | 1919 | 2441 +/- 925 | NA | |
| B.2 1+8.5W | 1+1.5S | 3 | 477.3 | 577 | 0 | 0 | B | 1919 | 1834 +/- 901 | NA | |
| B.2 1+7.5W | 1+1.5S | 3 | 477.3 | 574 | 0 | 0 | B | 1919 | 1779 +/- 899 | NA | |
| B.2 1+6.5W | 1+1.5S | 3 | 477.3 | 577 | 0 | 0 | B | 1919 | 1834 +/- 901 | NA | |
| B.2 1+5.5W | 1+1.5S | 3 | 477.3 | 571 | 0 | 0 | B | 1919 | 1724 +/- 897 | NA | |
| B.2 1+12.5W | 1+2.5S | 3 | 477.3 | 747 | 1116 | 500 | B | 1919 | 5301 +/-1016 | 11749 | |
| B.2 1+11.5W | 1+2.5S | 3 | 477.3 | 598 | 0 | 0 | B | 1919 | 2220 +/- 916 | NA | |
| B.2 1+10.5W | 1+2.5S | 3 | 477.3 | 606 | 0 | 0 | B | 1919 | 2368 +/- 922 | NA | |
| B.2 1+9.5W | 1+2.5S | 3 | 477.3 | 562 | 0 | 0 | B | 1919 | 1558 +/- 890 | NA | |
| B.2 1+8.5W | 1+2.5S | 3 | 477.3 | 531 | 0 | 0 | B | 1919 | 988 +/- 867 | NA | |
| B.2 1+7.5W | 1+2.5S | 3 | 477.3 | 588 | 0 | 0 | B | 1919 | 2036 +/- 909 | NA | |
| B.2 1+6.5W | 1+2.5S | 3 | 477.3 | 537 | 0 | 0 | B | 1919 | 1098 +/- 872 | NA | |
| B.2 1+5.5W | 1+2.5S | 3 | 477.3 | 705 | 0 | 0 | B | 1919 | 4189 +/- 989 | NA | |
| B.2 1+12.5W | 1+3.5S | 3 | 477.3 | 701 | 0 | 0 | B | 1919 | 4115 +/- 987 | NA | |
| B.2 1+11.5W | 1+3.5S | 3 | 477.3 | 625 | 0 | 0 | B | 1919 | 2717 +/- 935 | NA | |
| B.2 1+10.5W | 1+3.5S | 3 | 477.3 | 593 | 0 | 0 | B | 1919 | 2128 +/- 913 | NA | |
| B.2 1+9.5W | 1+3.5S | 3 | 477.3 | 603 | 0 | 0 | B | 1919 | 2312 +/- 920 | NA | |
| B.2 1+8.5W | 1+3.5S | 3 | 477.3 | 584 | 0 | 0 | B | 1919 | 1963 +/- 906 | NA | |
| B.2 1+7.5W | 1+3.5S | 3 | 477.3 | 617 | 0 | 0 | B | 1919 | 2570 +/- 930 | NA | |
| B.2 1+6.5W | 1+3.5S | 3 | 477.3 | 519 | 0 | 0 | B | 1919 | 767 +/- 858 | NA | |
| B.2 1+5.5W | 1+3.5S | 3 | 477.3 | 627 | 0 | 0 | B | 1919 | 2754 +/- 937 | NA | |
| B.2 1+12.5W | 1+4.5S | 3 | 477.3 | 577 | 0 | 0 | B | 1919 | 1834 +/- 901 | NA | |
| B.2 1+11.5W | 1+4.5S | 3 | 477.3 | 654 | 0 | 0 | B | 1919 | 3251 +/- 955 | NA | |
| B.2 1+10.5W | 1+4.5S | 3 | 477.3 | 605 | 0 | 0 | B | 1919 | 2349 +/- 921 | NA | |
| B.2 1+9.5W | 1+4.5S | 3 | 477.3 | 576 | 0 | 0 | B | 1919 | 1816 +/- 900 | NA | |
| B.2 1+8.5W | 1+4.5S | 3 | 477.3 | 571 | 0 | 0 | B | 1919 | 1724 +/- 897 | NA | |
| B.2 1+7.5W | 1+4.5S | 3 | 477.3 | 610 | 0 | 0 | B | 1919 | 2441 +/- 925 | NA | |
| B.2 1+6.5W | 1+4.5S | 3 | 477.3 | 603 | 0 | 0 | B | 1919 | 2312 +/- 920 | NA | |
| B.2 1+12.5W | 1+5.5S | 3 | 477.3 | 594 | 0 | 0 | B | 1919 | 2147 +/- 913 | NA | |
| B.2 1+11.5W | 1+5.5S | 3 | 477.3 | 604 | 0 | 0 | B | 1919 | 2331 +/- 920 | NA | |
| B.2 1+10.5W | 1+5.5S | 3 | 477.3 | 607 | 0 | 0 | B | 1919 | 2386 +/- 923 | NA | |
| B.2 1+9.5W | 1+5.5S | 3 | 477.3 | 592 | 0 | 0 | B | 1919 | 2110 +/- 912 | NA | |
| B.2 1+8.5W | 1+5.5S | 3 | 477.3 | 582 | 0 | 0 | B | 1919 | 1926 +/- 905 | NA | |
| B.2 1+7.5W | 1+5.5S | 3 | 477.3 | 604 | 0 | 0 | B | 1919 | 2331 +/- 920 | NA | |
| B.2 1+6.5W | 1+5.5S | 3 | 477.3 | 583 | 0 | 0 | B | 1919 | 2000 +/- 908 | NA | |
| B.2 1+12.5W | 1+6.5S | 3 | 477.3 | 570 | 0 | 0 | B | 1919 | 1705 +/- 896 | NA | |

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TABLE 8.2-2

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 1+5.5W | 0+90.5S | 3 | 558.6 | 597 | 0 | 0 | 8 | 2072 | 706 +/- 921 | NA | 0 |
| 8.2 1+9.5W | 0+91.5S | 3 | 558.6 | 596 | 0 | 0 | 8 | 2072 | 688 +/- 921 | NA | 0 |
| 8.2 1+8.5W | 0+91.5S | 4 | 499.7 | 575 | 0 | 0 | 8 | 1992 | 1406 +/- 915 | NA | 0 |
| 8.2 1+7.5W | 0+91.5S | 4 | 499.7 | 606 | 0 | 0 | 8 | 1992 | 1985 +/- 937 | NA | 0 |
| 8.2 1+6.5W | 0+91.5S | 4 | 499.7 | 589 | 0 | 0 | 8 | 1992 | 1668 +/- 925 | NA | 0 |
| 8.2 1+5.5W | 0+91.5S | 3 | 558.6 | 574 | 0 | 0 | 8 | 2072 | 283 +/- 905 | NA | 0 |
| 8.2 1+9.5W | 0+92.5S | 3 | 558.6 | 656 | 0 | 0 | 8 | 2072 | 1792 +/- 962 | NA | 0 |
| 8.2 1+8.5W | 0+92.5S | 3 | 467.6 | 453 | 0 | 0 | 8 | 1900 | -269 +/- 806 | NA | 0 |
| 8.2 1+7.5W | 0+92.5S | 3 | 467.6 | 415 | 0 | 0 | 8 | 1900 | -968 +/- 775 | NA | 0 |
| 8.2 1+6.5W | 0+92.5S | 3 | 467.6 | 416 | 0 | 0 | 8 | 1900 | -949 +/- 776 | NA | 0 |
| 8.2 1+5.5W | 0+92.5S | 3 | 467.6 | 462 | 0 | 0 | 8 | 1900 | -103 +/- 813 | NA | 0 |
| 8.2 1+4.5W | 0+92.5S | 3 | 467.6 | 470 | 0 | 0 | 8 | 1900 | 44 +/- 820 | NA | 0 |
| 8.2 1+3.5W | 0+92.5S | 3 | 558.6 | 673 | 0 | 0 | 8 | 2072 | 2104 +/- 973 | NA | 0 |
| 8.2 1+10.5W | 0+93.5S | 3 | 558.6 | 538 | 0 | 0 | 8 | 2072 | -379 +/- 879 | NA | 0 |
| 8.2 1+9.5W | 0+93.5S | 3 | 467.6 | 527 | 0 | 0 | 8 | 1900 | 1093 +/- 864 | NA | 0 |
| 8.2 1+8.5W | 0+93.5S | 3 | 467.6 | 458 | 0 | 0 | 8 | 1900 | -177 +/- 810 | NA | 0 |
| 8.2 1+7.5W | 0+93.5S | 3 | 467.6 | 433 | 0 | 0 | 8 | 1900 | -636 +/- 790 | NA | 0 |
| 8.2 1+6.5W | 0+93.5S | 3 | 467.6 | 434 | 0 | 0 | 8 | 1900 | -618 +/- 791 | NA | 0 |
| 8.2 1+5.5W | 0+93.5S | 3 | 467.6 | 396 | 0 | 0 | 8 | 1900 | -1317 +/- 759 | NA | 0 |
| 8.2 1+4.5W | 0+93.5S | 3 | 467.6 | 401 | 0 | 0 | 8 | 1900 | -1225 +/- 763 | NA | 0 |
| 8.2 1+3.5W | 0+93.5S | 3 | 558.6 | 582 | 0 | 0 | 8 | 2072 | 430 +/- 911 | NA | 0 |
| 8.2 1+10.5W | 0+94.5S | 3 | 558.6 | 537 | 0 | 0 | 8 | 2072 | -397 +/- 878 | NA | 0 |
| 8.2 1+9.5W | 0+94.5S | 3 | 467.6 | 437 | 0 | 0 | 8 | 1900 | -563 +/- 793 | NA | 0 |
| 8.2 1+8.5W | 0+94.5S | 3 | 467.6 | 406 | 0 | 0 | 8 | 1900 | -1133 +/- 767 | NA | 0 |
| 8.2 1+7.5W | 0+94.5S | 3 | 467.6 | 419 | 0 | 0 | 8 | 1900 | -894 +/- 778 | NA | 0 |
| 8.2 1+6.5W | 0+94.5S | 3 | 467.6 | 428 | 0 | 0 | 8 | 1900 | -728 +/- 786 | NA | 0 |
| 8.2 1+5.5W | 0+94.5S | 4 | 499.4 | 625 | 0 | 0 | 8 | 1991 | 2345 +/- 951 | NA | 0 |
| 8.2 1+4.5W | 0+94.5S | 3 | 558.6 | 683 | 0 | 0 | 8 | 2072 | 2288 +/- 980 | NA | 0 |
| 8.2 1+10.5W | 0+94.5S | 3 | 558.6 | 519 | 0 | 0 | 8 | 2072 | -728 +/- 864 | NA | 0 |
| 8.2 1+9.5W | 0+95.5S | 4 | 499.4 | 659 | 0 | 0 | 8 | 1991 | 2980 +/- 975 | NA | 0 |
| 8.2 1+8.5W | 0+95.5S | 4 | 499.4 | 553 | 0 | 0 | 8 | 1991 | 1001 +/- 899 | NA | 0 |
| 8.2 1+7.5W | 0+95.5S | 4 | 499.4 | 562 | 0 | 0 | 8 | 1991 | 1169 +/- 905 | NA | 0 |
| 8.2 1+6.5W | 0+95.5S | 4 | 499.4 | 571 | 0 | 0 | 8 | 1991 | 1337 +/- 912 | NA | 0 |
| 8.2 1+5.5W | 0+95.5S | 4 | 499.4 | 583 | 0 | 0 | 8 | 1991 | 1561 +/- 921 | NA | 0 |
| 8.2 1+4.5W | 0+95.5S | 3 | 558.6 | 551 | 0 | 0 | 8 | 2072 | -140 +/- 888 | NA | 0 |
| 8.2 1+10.5W | 0+96.5S | 3 | 558.6 | 589 | 0 | 0 | 8 | 2072 | 559 +/- 916 | NA | 0 |
| 8.2 1+9.5W | 0+96.5S | 4 | 464.2 | 601 | 0 | 0 | 8 | 1921 | 2555 +/- 931 | NA | 0 |
| 8.2 1+8.5W | 0+96.5S | 4 | 464.2 | 567 | 0 | 0 | 8 | 1921 | 1920 +/- 907 | NA | 0 |
| 8.2 1+7.5W | 0+96.5S | 4 | 464.2 | 553 | 0 | 0 | 8 | 1921 | 1658 +/- 896 | NA | 0 |
| 8.2 1+6.5W | 0+96.5S | 4 | 464.2 | 517 | 0 | 0 | 8 | 1921 | 986 +/- 869 | NA | 0 |
| 8.2 1+5.5W | 0+96.5S | 4 | 464.2 | 580 | 0 | 0 | 8 | 1921 | 2162 +/- 916 | NA | 0 |
| 8.2 1+4.5W | 0+96.5S | 3 | 558.6 | 535 | 0 | 0 | 8 | 2072 | -434 +/- 876 | NA | 0 |
| 8.2 1+11.5W | 0+97.5S | 3 | 558.6 | 623 | 0 | 0 | 8 | 2072 | 1185 +/- 939 | NA | 0 |
| 8.2 1+10.5W | 0+97.5S | 4 | 464.2 | 651 | 0 | 0 | 8 | 1921 | 3488 +/- 967 | NA | 0 |
| 8.2 1+9.5W | 0+97.5S | 4 | 464.2 | 588 | 0 | 0 | 8 | 1921 | 2312 +/- 922 | NA | 0 |
| 8.2 1+8.5W | 0+97.5S | 4 | 464.2 | 574 | 0 | 0 | 8 | 1921 | 2050 +/- 912 | NA | 0 |
| 8.2 1+7.5W | 0+97.5S | 4 | 464.2 | 555 | 0 | 0 | 8 | 1921 | 1696 +/- 898 | NA | 0 |
| 8.2 1+6.5W | 0+97.5S | 4 | 464.2 | 533 | 0 | 0 | 8 | 1921 | 1285 +/- 881 | NA | 0 |
| 8.2 1+5.5W | 0+97.5S | 4 | 464.2 | 571 | 0 | 0 | 8 | 1921 | 1994 +/- 909 | NA | 0 |
| 8.2 1+4.5W | 0+97.5S | 3 | 558.6 | 657 | 0 | 0 | 8 | 2072 | 1810 +/- 963 | NA | 0 |
| 8.2 1+11.5W | 0+98.5S | 3 | 558.6 | 591 | 0 | 0 | 8 | 2072 | 596 +/- 917 | NA | 0 |
| 8.2 1+10.5W | 0+98.5S | 4 | 464.2 | 650 | 0 | 0 | 8 | 1921 | 3470 +/- 966 | NA | 0 |
| 8.2 1+9.5W | 0+98.5S | 4 | 464.2 | 632 | 0 | 0 | 8 | 1921 | 3134 +/- 953 | NA | 0 |
| 8.2 1+8.5W | 0+98.5S | 4 | 464.2 | 591 | 0 | 0 | 8 | 1921 | 2368 +/- 924 | NA | 0 |
| 8.2 1+7.5W | 0+98.5S | 4 | 464.2 | 593 | 0 | 0 | 8 | 1921 | 2405 +/- 926 | NA | 0 |
| 8.2 1+6.5W | 0+98.5S | 4 | 464.2 | 530 | 0 | 0 | 8 | 1921 | 1229 +/- 879 | NA | 0 |

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|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 | 1+18.5W | 1+21.5S | 3 | 503.5 | 577 | 0 | 0 | 8 | 1969 | 1352 +/- 903 | NA | 0 |
| 8.2 | 1+17.5W | 1+21.5S | 3 | 503.5 | 700 | 0 | 0 | 8 | 1969 | 3615 +/- 988 | NA | 0 |
| 8.2 | 1+16.5W | 1+21.5S | 3 | 503.5 | 587 | 0 | 0 | 8 | 1969 | 1536 +/- 910 | NA | 0 |
| 8.2 | 1+15.5W | 1+21.5S | 3 | 503.5 | 620 | 0 | 0 | 8 | 1969 | 2143 +/- 934 | NA | 0 |
| 8.2 | 1+14.5W | 1+21.5S | 3 | 503.5 | 611 | 0 | 0 | 8 | 1969 | 1978 +/- 927 | NA | 0 |
| 8.2 | 1+13.5W | 1+21.5S | 3 | 503.5 | 646 | 0 | 0 | 8 | 1969 | 2621 +/- 951 | NA | 0 |
| 8.2 | 1+20.5W | 1+22.5S | 3 | 503.5 | 542 | 0 | 0 | 8 | 1969 | 708 +/- 878 | NA | 0 |
| 8.2 | 1+19.5W | 1+22.5S | 3 | 503.5 | 561 | 0 | 0 | 8 | 1969 | 1058 +/- 892 | NA | 0 |
| 8.2 | 1+18.5W | 1+22.5S | 3 | 503.5 | 589 | 0 | 0 | 8 | 1969 | 1573 +/- 912 | NA | 0 |
| 8.2 | 1+17.5W | 1+22.5S | 3 | 503.5 | 569 | 0 | 0 | 8 | 1969 | 1205 +/- 897 | NA | 0 |
| 8.2 | 1+16.5W | 1+22.5S | 3 | 503.5 | 604 | 0 | 0 | 8 | 1969 | 1849 +/- 922 | NA | 0 |
| 8.2 | 1+15.5W | 1+22.5S | 3 | 503.5 | 592 | 0 | 0 | 8 | 1969 | 1628 +/- 914 | NA | 0 |
| 8.2 | 1+14.5W | 1+22.5S | 3 | 503.5 | 621 | 0 | 0 | 8 | 1969 | 2162 +/- 934 | NA | 0 |
| 8.2 | 1+13.5W | 1+22.5S | 3 | 503.5 | 721 | 0 | 0 | 8 | 1969 | 4001 +/-1001 | NA | 0 |
| 8.2 | 1+20.5W | 1+23.5S | 3 | 503.5 | 596 | 0 | 0 | 8 | 1969 | 1702 +/- 917 | NA | 0 |
| 8.2 | 1+19.5W | 1+23.5S | 3 | 503.5 | 601 | 0 | 0 | 8 | 1969 | 1794 +/- 920 | NA | 0 |
| 8.2 | 1+18.5W | 1+23.5S | 3 | 503.5 | 614 | 0 | 0 | 8 | 1969 | 2033 +/- 929 | NA | 0 |
| 8.2 | 1+17.5W | 1+23.5S | 3 | 503.5 | 537 | 0 | 0 | 8 | 1969 | 616 +/- 874 | NA | 0 |
| 8.2 | 1+16.5W | 1+23.5S | 3 | 503.5 | 654 | 0 | 0 | 8 | 1969 | 2769 +/- 957 | NA | 0 |
| 8.2 | 1+15.5W | 1+23.5S | 3 | 503.5 | 630 | 0 | 0 | 8 | 1969 | 2327 +/- 940 | NA | 0 |
| 8.2 | 1+14.5W | 1+23.5S | 3 | 503.5 | 639 | 0 | 0 | 8 | 1969 | 2493 +/- 947 | NA | 0 |
| 8.2 | 1+13.5W | 1+23.5S | 3 | 503.5 | 699 | 0 | 0 | 8 | 1969 | 3596 +/- 987 | NA | 0 |
| 8.2 | 1+20.5W | 1+24.5S | 3 | 503.5 | 605 | 0 | 0 | 8 | 1969 | 1867 +/- 923 | NA | 0 |
| 8.2 | 1+19.5W | 1+24.5S | 3 | 503.5 | 575 | 0 | 0 | 8 | 1969 | 1315 +/- 902 | NA | 0 |
| 8.2 | 1+18.5W | 1+24.5S | 3 | 503.5 | 647 | 0 | 0 | 8 | 1969 | 2640 +/- 952 | NA | 0 |
| 8.2 | 1+17.5W | 1+24.5S | 3 | 503.5 | 583 | 0 | 0 | 8 | 1969 | 1462 +/- 907 | NA | 0 |
| 8.2 | 1+16.5W | 1+24.5S | 3 | 503.5 | 649 | 0 | 0 | 8 | 1969 | 2677 +/- 954 | NA | 0 |
| 8.2 | 1+15.5W | 1+24.5S | 3 | 503.5 | 605 | 0 | 0 | 8 | 1969 | 1867 +/- 923 | NA | 0 |
| 8.2 | 1+14.5W | 1+24.5S | 3 | 503.5 | 616 | 0 | 0 | 8 | 1969 | 2070 +/- 931 | NA | 0 |
| 8.2 | 1+13.5W | 1+24.5S | 3 | 503.5 | 677 | 0 | 0 | 8 | 1969 | 3192 +/- 972 | NA | 0 |
| 8.2 | 1+20.5W | 1+25.5S | 3 | 503.5 | 584 | 0 | 0 | 8 | 1969 | 1481 +/- 908 | NA | 0 |
| 8.2 | 1+19.5W | 1+25.5S | 3 | 503.5 | 584 | 0 | 0 | 8 | 1969 | 1481 +/- 908 | NA | 0 |
| 8.2 | 1+18.5W | 1+25.5S | 3 | 503.5 | 588 | 0 | 0 | 8 | 1969 | 1554 +/- 911 | NA | 0 |
| 8.2 | 1+17.5W | 1+25.5S | 3 | 503.5 | 619 | 0 | 0 | 8 | 1969 | 2125 +/- 933 | NA | 0 |
| 8.2 | 1+16.5W | 1+25.5S | 3 | 503.5 | 552 | 0 | 0 | 8 | 1969 | 892 +/- 885 | NA | 0 |
| 8.2 | 1+15.5W | 1+25.5S | 3 | 503.5 | 584 | 0 | 0 | 8 | 1969 | 1481 +/- 908 | NA | 0 |
| 8.2 | 1+14.5W | 1+25.5S | 3 | 503.5 | 582 | 0 | 0 | 8 | 1969 | 1444 +/- 907 | NA | 0 |
| 8.2 | 1+21.5W | 1+26.5S | 6 | 509.5 | 532 | 0 | 0 | 8 | 1970 | 412 +/- 866 | NA | 0 |
| 8.2 | 1+20.5W | 1+26.5S | 6 | 509.5 | 563 | 0 | 0 | 8 | 1970 | 979 +/- 888 | NA | 0 |
| 8.2 | 1+19.5W | 1+26.5S | 6 | 509.5 | 677 | 0 | 0 | 8 | 1970 | 3064 +/- 967 | NA | 0 |
| 8.2 | 1+18.5W | 1+26.5S | 6 | 509.5 | 573 | 0 | 0 | 8 | 1970 | 1162 +/- 896 | NA | 0 |
| 8.2 | 1+17.5W | 1+26.5S | 6 | 509.5 | 544 | 0 | 0 | 8 | 1970 | 631 +/- 875 | NA | 0 |
| 8.2 | 1+16.5W | 1+26.5S | 6 | 509.5 | 672 | 0 | 0 | 8 | 1970 | 2973 +/- 964 | NA | 0 |
| 8.2 | 1+15.5W | 1+26.5S | 6 | 509.5 | 572 | 0 | 0 | 8 | 1970 | 1143 +/- 895 | NA | 0 |
| 8.2 | 1+14.5W | 1+26.5S | 6 | 509.5 | 578 | 0 | 0 | 8 | 1970 | 1253 +/- 899 | NA | 0 |
| 8.2 | 1+21.5W | 1+27.5S | 6 | 509.5 | 528 | 0 | 0 | 8 | 1970 | 338 +/- 863 | NA | 0 |
| 8.2 | 1+20.5W | 1+27.5S | 6 | 509.5 | 617 | 0 | 0 | 8 | 1970 | 1967 +/- 927 | NA | 0 |
| 8.2 | 1+19.5W | 1+27.5S | 6 | 509.5 | 646 | 0 | 0 | 8 | 1970 | 2497 +/- 947 | NA | 0 |
| 8.2 | 1+18.5W | 1+27.5S | 6 | 509.5 | 558 | 0 | 0 | 8 | 1970 | 887 +/- 885 | NA | 0 |
| 8.2 | 1+17.5W | 1+27.5S | 6 | 509.5 | 495 | 0 | 0 | 8 | 1970 | -265 +/- 838 | NA | 0 |
| 8.2 | 1+16.5W | 1+27.5S | 6 | 509.5 | 529 | 0 | 0 | 8 | 1970 | 357 +/- 864 | NA | 0 |
| 8.2 | 1+15.5W | 1+27.5S | 6 | 509.5 | 559 | 0 | 0 | 8 | 1970 | 906 +/- 886 | NA | 0 |
| 8.2 | 1+14.5W | 1+27.5S | 6 | 509.5 | 594 | 0 | 0 | 8 | 1970 | 1546 +/- 911 | NA | 0 |
| 8.2 | 1+21.5W | 1+28.5S | 6 | 509.5 | 575 | 0 | 0 | 8 | 1970 | 1198 +/- 897 | NA | 0 |
| 8.2 | 1+20.5W | 1+28.5S | 6 | 509.5 | 577 | 0 | 0 | 8 | 1970 | 1235 +/- 899 | NA | 0 |
| 8.2 | 1+19.5W | 1+28.5S | 6 | 509.5 | 639 | 0 | 0 | 8 | 1970 | 2369 +/- 942 | NA | 0 |

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|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 | 1+18.5W | 1+28.5S | 6 | 509.5 | 587 | 0 | 0 | B | 1970 | 1418 +/- 906 | NA | |
| 8.2 | 1+17.5W | 1+28.5S | 6 | 509.5 | 530 | 0 | 0 | B | 1970 | 375 +/- 864 | NA | |
| 8.2 | 1+16.5W | 1+28.5S | 6 | 509.5 | 628 | 0 | 0 | B | 1970 | 2168 +/- 934 | NA | |
| 8.2 | 1+15.5W | 1+28.5S | 6 | 509.5 | 555 | 0 | 0 | B | 1970 | 832 +/- 883 | NA | |
| 8.2 | 1+14.5W | 1+28.5S | 6 | 509.5 | 658 | 0 | 0 | B | 1970 | 2717 +/- 955 | NA | |
| 8.2 | 1+21.5W | 1+29.5S | 6 | 509.5 | 543 | 0 | 0 | B | 1970 | 613 +/- 874 | NA | |
| 8.2 | 1+20.5W | 1+29.5S | 6 | 509.5 | 591 | 0 | 0 | B | 1970 | 1491 +/- 909 | NA | |
| 8.2 | 1+19.5W | 1+29.5S | 6 | 509.5 | 630 | 0 | 0 | B | 1970 | 2205 +/- 936 | NA | |
| 8.2 | 1+18.5W | 1+29.5S | 6 | 509.5 | 530 | 0 | 0 | B | 1970 | 375 +/- 864 | NA | |
| 8.2 | 1+17.5W | 1+29.5S | 6 | 509.5 | 547 | 0 | 0 | B | 1970 | 686 +/- 877 | NA | |
| 8.2 | 1+16.5W | 1+29.5S | 6 | 509.5 | 541 | 0 | 0 | B | 1970 | 576 +/- 872 | NA | |
| 8.2 | 1+15.5W | 1+29.5S | 6 | 509.5 | 561 | 0 | 0 | B | 1970 | 942 +/- 887 | NA | |
| 8.2 | 1+15.5 | 1+30.5 | 1 | 469.4 | 640 | 0 | 0 | B | 1959 | 3231 +/- 973 | NA | |
| 8.2 | 1+16.5 | 1+30.5 | 1 | 469.4 | 583 | 0 | 0 | B | 1959 | 2152 +/- 932 | NA | |
| 8.2 | 1+17.5 | 1+30.5 | 1 | 469.4 | 579 | 0 | 0 | B | 1959 | 2076 +/- 929 | NA | |
| 8.2 | 1+18.5 | 1+30.5 | 1 | 469.4 | 596 | 874 | 351 | B | 1959 | 2583 +/- 941 | | 7663 |
| 8.2 | 1+19.5 | 1+30.5 | 1 | 469.4 | 667 | 0 | 0 | B | 1959 | 3742 +/- 992 | NA | |
| 8.2 | 1+20.5 | 1+30.5 | 1 | 469.4 | 623 | 0 | 0 | B | 1959 | 2909 +/- 961 | NA | |
| 8.2 | 1+21.5 | 1+30.5 | 1 | 469.4 | 584 | 0 | 0 | B | 1959 | 2170 +/- 932 | NA | |
| 8.2 | 1+15.5 | 1+31.5 | 1 | 469.4 | 664 | 0 | 0 | B | 1959 | 3686 +/- 990 | NA | |
| 8.2 | 1+16.5 | 1+31.5 | 1 | 469.4 | 602 | 1270 | 950 | B | 1959 | 3713 +/- 946 | | 15163 |
| 8.2 | 1+17.5 | 1+31.5 | 1 | 469.4 | 655 | 1373 | 1444 | B | 1959 | 5479 +/- 983 | | 17114 |
| 8.2 | 1+18.5 | 1+31.5 | 1 | 469.4 | 654 | 959 | 1170 | B | 1959 | 4172 +/- 983 | | 9273 |
| 8.2 | 1+19.5 | 1+31.5 | 1 | 469.4 | 615 | 0 | 0 | B | 1959 | 2758 +/- 955 | NA | |
| 8.2 | 1+20.5 | 1+31.5 | 1 | 469.4 | 668 | 0 | 0 | B | 1959 | 3761 +/- 993 | NA | |
| 8.2 | 1+21.5 | 1+31.5 | 1 | 469.4 | 579 | 0 | 0 | B | 1959 | 2076 +/- 929 | NA | |
| 8.2 | 1+22.5 | 1+31.5 | 1 | 469.4 | 553 | 0 | 0 | B | 1959 | 1583 +/- 909 | NA | |
| 8.2 | 1+15.5 | 1+32.5 | 1 | 469.4 | 625 | 0 | 0 | B | 1959 | 2947 +/- 962 | NA | |
| 8.2 | 1+16.5 | 1+32.5 | 1 | 469.4 | 565 | 0 | 0 | B | 1959 | 1811 +/- 918 | NA | |
| 8.2 | 1+17.5 | 1+32.5 | 1 | 469.4 | 559 | 0 | 0 | B | 1959 | 1697 +/- 914 | NA | |
| 8.2 | 1+18.5 | 1+32.5 | 1 | 469.4 | 611 | 0 | 0 | B | 1959 | 2682 +/- 952 | NA | |
| 8.2 | 1+19.5 | 1+32.5 | 1 | 469.4 | 588 | 0 | 0 | B | 1959 | 2246 +/- 935 | NA | |
| 8.2 | 1+20.5 | 1+32.5 | 1 | 469.4 | 592 | 0 | 0 | B | 1959 | 2322 +/- 938 | NA | |
| 8.2 | 1+21.5 | 1+32.5 | 1 | 469.4 | 636 | 0 | 0 | B | 1959 | 3155 +/- 970 | NA | |
| 8.2 | 1+22.5 | 1+32.5 | 1 | 469.4 | 622 | 910 | 500 | B | 1959 | 3163 +/- 960 | | 8345 |
| 8.2 | 1+16.5 | 1+33.5 | 1 | 469.4 | 672 | 0 | 0 | B | 1959 | 3837 +/- 995 | NA | |
| 8.2 | 1+17.5 | 1+33.5 | 1 | 469.4 | 605 | 0 | 0 | B | 1959 | 2568 +/- 948 | NA | |
| 8.2 | 1+18.5 | 1+33.5 | 1 | 469.4 | 500 | 0 | 0 | B | 1959 | 580 +/- 868 | NA | |
| 8.2 | 1+19.5 | 1+33.5 | 1 | 469.4 | 602 | 0 | 0 | B | 1959 | 2511 +/- 946 | NA | |
| 8.2 | 1+20.5 | 1+33.5 | 1 | 469.4 | 611 | 0 | 0 | B | 1959 | 2682 +/- 952 | NA | |

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Aperture Card

TABLE B.2-3

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| B.2 0+92.5 | 0+52.5 | 1 | 2.0 | 8 | 0 | 0 | B | 49 | 32 +/- 30 | NA | | 0 |
| B.2 0+93.5 | 0+52.5 | 1 | 2.0 | 6 | 0 | 0 | B | 49 | 21 +/- 26 | NA | | 0 |
| B.2 0+94.5 | 0+52.5 | 1 | 2.0 | 3 | 0 | 0 | B | 49 | 5 +/- 18 | NA | | 0 |
| B.2 0+95.5 | 0+52.5 | 1 | 2.0 | 3 | 0 | 0 | B | 49 | 5 +/- 18 | NA | | 0 |
| B.2 0+96.5 | 0+52.5 | 1 | 2.0 | 4 | 0 | 0 | B | 49 | 11 +/- 21 | NA | | 0 |
| B.2 0+97.5 | 0+52.5 | 1 | 2.0 | 4 | 0 | 0 | B | 49 | 11 +/- 21 | NA | | 0 |
| B.2 0+92.5 | 0+53.5 | 1 | 2.0 | 3 | 0 | 0 | B | 49 | 5 +/- 18 | NA | | 0 |
| B.2 0+93.5 | 0+53.5 | 1 | 2.0 | 10 | 0 | 0 | B | 49 | 42 +/- 33 | NA | | 0 |
| B.2 0+94.5 | 0+53.5 | 1 | 2.0 | 5 | 0 | 0 | B | 49 | 16 +/- 24 | NA | | 0 |
| B.2 0+95.5 | 0+53.5 | 1 | 2.0 | 7 | 0 | 0 | B | 49 | 26 +/- 28 | NA | | 0 |
| B.2 0+96.5 | 0+53.5 | 1 | 2.0 | 7 | 0 | 0 | B | 49 | 26 +/- 28 | NA | | 0 |
| B.2 0+97.5 | 0+53.5 | 1 | 2.0 | 5 | 0 | 0 | B | 49 | 16 +/- 24 | NA | | 0 |
| B.2 0+92.5 | 0+54.5 | 1 | 2.0 | 4 | 0 | 0 | B | 49 | 11 +/- 21 | NA | | 0 |
| B.2 0+93.5 | 0+54.5 | 1 | 2.0 | 5 | 0 | 0 | B | 49 | 16 +/- 24 | NA | | 0 |
| B.2 0+94.5 | 0+54.5 | 1 | 2.0 | 3 | 0 | 0 | B | 49 | 5 +/- 18 | NA | | 0 |
| B.2 0+95.5 | 0+54.5 | 1 | 2.0 | 5 | 0 | 0 | B | 49 | 16 +/- 24 | NA | | 0 |
| B.2 0+96.5 | 0+54.5 | 1 | 2.0 | 6 | 0 | 0 | B | 49 | 21 +/- 26 | NA | | 0 |
| B.2 0+97 | 0+54.5 | 1 | 2.0 | 6 | 0 | 0 | B | 49 | 21 +/- 26 | NA | | 0 |
| B.2 0+92.5 | 0+55.5 | 1 | 2.0 | 3 | 0 | 0 | B | 49 | 5 +/- 18 | NA | | 0 |
| B.2 0+94.5 | 0+55.5 | 1 | 2.0 | 5 | 0 | 0 | B | 49 | 16 +/- 24 | NA | | 0 |
| B.2 0+95.5 | 0+55.5 | 1 | 2.0 | 9 | 0 | 0 | B | 49 | 37 +/- 31 | NA | | 0 |
| B.2 0+96.5 | 0+55.5 | 1 | 2.0 | 4 | 0 | 0 | B | 49 | 11 +/- 21 | NA | | 0 |
| B.2 0+97.5 | 0+55.5 | 1 | 2.0 | 10 | 0 | 0 | B | 49 | 42 +/- 33 | NA | | 0 |
| B.2 0+93.5 | 0+56.5 | 1 | 2.0 | 1 | 0 | 0 | B | 49 | -5 +/- 11 | NA | | 0 |
| B.2 0+94.5 | 0+56.5 | 1 | 2.0 | 4 | 0 | 0 | B | 49 | 11 +/- 21 | NA | | 0 |
| B.2 0+95.5 | 0+56.5 | 1 | 2.0 | 3 | 0 | 0 | B | 49 | 5 +/- 18 | NA | | 0 |
| B.2 0+96.5 | 0+56.5 | 1 | 2.0 | 8 | 0 | 0 | B | 49 | 32 +/- 30 | NA | | 0 |
| B.2 0+97.5 | 0+56.5 | 1 | 2.0 | 9 | 0 | 0 | B | 49 | 37 +/- 31 | NA | | 0 |
| B.2 0+98.5 | 0+56.5 | 1 | 2.0 | 6 | 0 | 0 | B | 49 | 21 +/- 26 | NA | | 0 |
| B.2 0+93.5 | 0+57.5 | 2 | 0.7 | 1 | 0 | 0 | B | 34 | 2 +/- 10 | NA | | 0 |
| B.2 0+94.5 | 0+57.5 | 2 | 0.7 | 1 | 0 | 0 | B | 34 | 2 +/- 10 | NA | | 0 |
| B.2 0+95.5 | 0+57.5 | 2 | 0.7 | 1 | 0 | 0 | B | 34 | 2 +/- 10 | NA | | 0 |
| B.2 0+96.5 | 0+57.5 | 2 | 0.7 | 2 | 0 | 0 | B | 34 | 7 +/- 14 | NA | | 0 |
| B.2 0+97.5 | 0+57.5 | 2 | 0.7 | 3 | 0 | 0 | B | 34 | 12 +/- 18 | NA | | 0 |
| B.2 0+98.5 | 0+57.5 | 2 | 0.7 | 4 | 0 | 0 | B | 34 | 17 +/- 20 | NA | | 0 |
| B.2 0+93.5 | 0+58.5 | 2 | 0.7 | 5 | 0 | 0 | B | 34 | 22 +/- 23 | NA | | 0 |
| B.2 0+94.5 | 0+58.5 | 2 | 0.7 | 1 | 0 | 0 | B | 34 | 2 +/- 10 | NA | | 0 |
| B.2 0+95.5 | 0+58.5 | 2 | 0.7 | 4 | 0 | 0 | B | 34 | 17 +/- 20 | NA | | 0 |
| B.2 0+96.5 | 0+58.5 | 2 | 0.7 | 1 | 0 | 0 | B | 34 | 2 +/- 10 | NA | | 0 |
| B.2 0+97.5 | 0+58.5 | 2 | 0.7 | 1 | 0 | 0 | B | 34 | 2 +/- 10 | NA | | 0 |
| B.2 0+98.5 | 0+58.5 | 2 | 0.7 | 1 | 8 | 500 | B | 34 | 3 +/- 10 | | 37 | 0 |
| B.2 0+93.5 | 0+59.5 | 2 | 0.7 | 3 | 0 | 0 | B | 34 | 12 +/- 18 | NA | | 0 |
| B.2 0+94.5 | 0+59.5 | 2 | 0.7 | 0 | 0 | 0 | B | 34 | -4 +/- 3 | NA | | 0 |
| B.2 0+95.5 | 0+59.5 | 2 | 0.7 | 2 | 0 | 0 | B | 34 | 7 +/- 14 | NA | | 0 |
| B.2 0+96.5 | 0+59.5 | 2 | 0.7 | 4 | 0 | 0 | B | 34 | 17 +/- 20 | NA | | 0 |
| B.2 0+97.5 | 0+59.5 | 2 | 0.7 | 6 | 0 | 0 | B | 34 | 27 +/- 25 | NA | | 0 |
| B.2 0+98.5 | 0+59.5 | 2 | 0.7 | 7 | 0 | 0 | B | 34 | 32 +/- 27 | NA | | 0 |
| B.2 0+99.5 | 0+59.5 | 2 | 0.7 | 1 | 0 | 0 | B | 34 | 2 +/- 10 | NA | | 0 |
| B.2 1+0.5 | 0+60.5 | 2 | 1.2 | 4 | 0 | 0 | B | 40 | 14 +/- 20 | NA | | 0 |
| B.2 0+99.5 | 0+60.5 | 3 | 0.2 | 6 | 0 | 0 | B | 25 | 30 +/- 25 | NA | | 0 |
| B.2 0+98.5 | 0+60.5 | 3 | 0.2 | 3 | 0 | 0 | B | 25 | 14 +/- 18 | NA | | 0 |
| B.2 0+97.5 | 0+60.5 | 3 | 0.2 | 5 | 0 | 0 | B | 25 | 25 +/- 23 | NA | | 0 |
| B.2 0+96.5 | 0+60.5 | 3 | 0.2 | 2 | 0 | 0 | B | 25 | 9 +/- 14 | NA | | 0 |
| B.2 0+95.5 | 0+60.5 | 3 | 0.2 | 7 | 0 | 0 | B | 25 | 35 +/- 27 | NA | | 0 |
| B.2 0+94.5 | 0+60.5 | 3 | 0.2 | 3 | 0 | 0 | B | 25 | 14 +/- 18 | NA | | 0 |
| B.2 0+93.5 | 0+60.5 | 2 | 1.2 | 6 | 0 | 0 | B | 40 | 25 +/- 25 | NA | | 0 |
| B.2 1+0.5 | 0+61.5 | 2 | 1.2 | 1 | 0 | 0 | B | 40 | -1 +/- 11 | NA | | 0 |
| B.2 0+99.5 | 0+61.5 | 3 | 0.2 | 4 | 0 | 0 | B | 25 | 20 +/- 20 | NA | | 0 |
| B.2 0+98.5 | 0+61.5 | 3 | 0.2 | 7 | 0 | 0 | B | 25 | 35 +/- 27 | NA | | 0 |
| B.2 0+97.5 | 0+61.5 | 3 | 0.2 | 0 | 0 | 0 | B | 25 | -1 +/- 1 | NA | | 0 |

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|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 0+95.5 | 0+48.5 | 1 | 1.1 | 1 | 0 | 0 | B | 40 | -1 +/- 11 | NA | | 0. |
| 8.2 0+94.5 | 0+48.5 | 1 | 1.1 | 4 | 0 | 0 | B | 40 | 15 +/- 21 | NA | | 0. |
| 8.2 0+93.5 | 0+48.5 | 1 | 1.1 | 1 | 0 | 0 | B | 40 | -1 +/- 11 | NA | | 0. |
| 8.2 0+92.5 | 0+48.5 | 1 | 1.1 | 3 | 0 | 0 | B | 40 | 10 +/- 18 | NA | | 0. |
| 8.2 0+95.5 | 0+47.5 | 1 | 1.1 | 3 | 0 | 0 | B | 40 | 10 +/- 18 | NA | | 0. |
| 8.2 0+94.5 | 0+47.5 | 1 | 1.1 | 1 | 0 | 0 | B | 40 | -1 +/- 11 | NA | | 0. |
| 8.2 0+93.5 | 0+47.5 | 1 | 1.1 | 3 | 0 | 0 | B | 40 | 10 +/- 18 | NA | | 0. |
| 8.2 0+92.5 | 0+47.5 | 1 | 1.1 | 4 | 0 | 0 | B | 40 | 15 +/- 21 | NA | | 0. |
| 8.2 0+94.5 | 0+46.5 | 1 | 1.1 | 2 | 0 | 0 | B | 40 | 5 +/- 15 | NA | | 0. |
| 8.2 0+93.5 | 0+46.5 | 1 | 1.1 | 3 | 0 | 0 | B | 40 | 10 +/- 18 | NA | | 0. |
| 8.2 0+92.5 | 0+46.5 | 1 | 1.1 | 2 | 0 | 0 | B | 40 | 5 +/- 15 | NA | | 0. |
| 8.2 0+91.5 | 0+46.5 | 1 | 1.1 | 3 | 0 | 0 | B | 40 | 10 +/- 18 | NA | | 0. |
| 8.2 0+90.5 | 0+46.5 | 1 | 1.1 | 5 | 0 | 0 | B | 40 | 21 +/- 23 | NA | | 0. |
| 8.2 0+94.5 | 0+45.5 | 1 | 1.1 | 3 | 0 | 0 | B | 40 | 10 +/- 18 | NA | | 0. |
| 8.2 0+93.5 | 0+45.5 | 1 | 1.1 | 3 | 0 | 0 | B | 40 | 10 +/- 18 | NA | | 0. |
| 8.2 0+92.5 | 0+45.5 | 1 | 1.1 | 3 | 0 | 0 | B | 40 | 10 +/- 18 | NA | | 0. |
| 8.2 0+91.5 | 0+45.5 | 1 | 1.1 | 2 | 0 | 0 | B | 40 | 5 +/- 15 | NA | | 0. |
| 8.2 0+90.5 | 0+45.5 | 6 | 1.3 | 5 | 0 | 0 | B | 44 | 21 +/- 25 | NA | | 0. |
| 8.2 0+89.5 | 0+45.5 | 6 | 1.3 | 4 | 0 | 0 | B | 44 | 15 +/- 22 | NA | | 0. |
| 8.2 0+94.5 | 0+44.5 | 6 | 1.3 | 1 | 0 | 0 | B | 44 | -2 +/- 12 | NA | | 0. |
| 8.2 0+93.5 | 0+44.5 | 6 | 1.3 | 1 | 0 | 0 | B | 44 | -2 +/- 12 | NA | | 0. |
| 8.2 0+92.5 | 0+44.5 | 6 | 1.3 | 1 | 0 | 0 | B | 44 | -2 +/- 12 | NA | | 0. |
| 8.2 0+91.5 | 0+44.5 | 6 | 1.3 | 2 | 0 | 0 | B | 44 | 4 +/- 16 | NA | | 0. |
| 8.2 0+90.5 | 0+44.5 | 6 | 1.3 | 3 | 0 | 0 | B | 44 | 9 +/- 19 | NA | | 0. |
| 8.2 0+89.5 | 0+44.5 | 6 | 1.3 | 2 | 0 | 0 | B | 44 | 4 +/- 16 | NA | | 0. |
| 8.2 0+88.5 | 0+44.5 | 6 | 1.3 | 3 | 0 | 0 | B | 44 | 9 +/- 19 | NA | | 0. |
| 8.2 0+94.5 | 0+43.5 | 6 | 1.3 | 1 | 0 | 0 | B | 44 | -2 +/- 12 | NA | | 0. |
| 8.2 0+93.5 | 0+43.5 | 6 | 1.3 | 4 | 0 | 0 | B | 44 | 15 +/- 22 | NA | | 0. |
| 8.2 0+92.5 | 0+43.5 | 6 | 1.3 | 1 | 0 | 0 | B | 44 | -2 +/- 12 | NA | | 0. |
| 8.2 0+91.5 | 0+43.5 | 6 | 1.3 | 1 | 0 | 0 | B | 44 | -2 +/- 12 | NA | | 0. |
| 8.2 0+90.5 | 0+43.5 | 6 | 1.3 | 5 | 0 | 0 | B | 44 | 21 +/- 25 | NA | | 0. |
| 8.2 0+89.5 | 0+43.5 | 6 | 1.3 | 5 | 0 | 0 | B | 44 | 21 +/- 25 | NA | | 0. |
| 8.2 0+88.5 | 0+43.5 | 6 | 1.3 | 6 | 0 | 0 | B | 44 | 26 +/- 27 | NA | | 0. |
| 8.2 0+93.5 | 0+42.5 | 6 | 1.3 | 0 | 0 | 0 | B | 44 | -7 +/- 4 | NA | | 0. |
| 8.2 0+92.5 | 0+42.5 | 6 | 1.3 | 2 | 6 | 1677 | B | 44 | 8 +/- 16 | | 26 | 0. |
| 8.2 0+91.5 | 0+42.5 | 6 | 1.3 | 2 | 0 | 0 | B | 44 | 4 +/- 16 | NA | | 0. |
| 8.2 0+90.5 | 0+42.5 | 6 | 1.3 | 5 | 0 | 0 | B | 44 | 21 +/- 25 | NA | | 0. |
| 8.2 0+89.5 | 0+42.5 | 6 | 1.3 | 5 | 0 | 0 | B | 44 | 21 +/- 25 | NA | | 0. |
| 8.2 0+88.5 | 0+42.5 | 6 | 1.3 | 1 | 0 | 0 | B | 44 | -2 +/- 12 | NA | | 0. |
| 8.2 0+93.5 | 0+41.5 | 6 | 1.3 | 1 | 0 | 0 | B | 44 | -2 +/- 12 | NA | | 0. |
| 8.2 0+92.5 | 0+41.5 | 6 | 1.3 | 2 | 0 | 0 | B | 44 | 4 +/- 16 | NA | | 0. |
| 8.2 0+91.5 | 0+41.5 | 6 | 1.3 | 3 | 5 | 720 | B | 44 | 10 +/- 19 | | 21 | 0. |
| 8.2 0+90.5 | 0+41.5 | 6 | 1.3 | 2 | 0 | 0 | B | 44 | 4 +/- 16 | NA | | 0. |
| 8.2 0+89.5 | 0+41.5 | 6 | 1.3 | 6 | 0 | 0 | B | 44 | 26 +/- 27 | NA | | 0. |
| 8.2 0+88.5 | 0+41.5 | 6 | 1.3 | 4 | 0 | 0 | B | 44 | 15 +/- 22 | NA | | 0. |
| 8.2 0+92.5 | 0+40.5 | 6 | 1.3 | 0 | 0 | 0 | B | 44 | -7 +/- 4 | NA | | 0. |
| 8.2 0+91.5 | 0+40.5 | 6 | 1.3 | 0 | 0 | 0 | B | 44 | -7 +/- 4 | NA | | 0. |
| 8.2 0+90.5 | 0+40.5 | 6 | 1.3 | 3 | 0 | 0 | B | 44 | 9 +/- 19 | NA | | 0. |
| 8.2 0+89.5 | 0+40.5 | 6 | 1.3 | 2 | 0 | 0 | B | 44 | 4 +/- 16 | NA | | 0. |
| 8.2 0+88.5 | 0+40.5 | 6 | 1.3 | 3 | 0 | 0 | B | 44 | 9 +/- 19 | NA | | 0. |
| 8.2 0+92.5 | 0+50.5 | 6 | 2.1 | 6 | 0 | 0 | B | 52 | 22 +/- 27 | NA | | 0. |
| 8.2 0+93.5 | 0+50.5 | 6 | 2.1 | 6 | 0 | 0 | B | 52 | 22 +/- 27 | NA | | 0. |
| 8.2 0+94.5 | 0+50.5 | 6 | 2.1 | 3 | 0 | 0 | B | 52 | 5 +/- 19 | NA | | 0. |
| 8.2 0+95.5 | 0+50.5 | 6 | 2.1 | 1 | 0 | 0 | B | 52 | -6 +/- 12 | NA | | 0. |
| 8.2 0+96.5 | 0+50.5 | 6 | 2.1 | 4 | 0 | 0 | B | 52 | 11 +/- 22 | NA | | 0. |
| 8.2 0+92.5 | 0+51.5 | 1 | 2.0 | 9 | 0 | 0 | B | 49 | 37 +/- 31 | NA | | 0. |
| 8.2 0+93.5 | 0+51.5 | 1 | 2.0 | 5 | 0 | 0 | B | 49 | 16 +/- 24 | NA | | 0. |
| 8.2 0+94.5 | 0+51.5 | 1 | 2.0 | 3 | 0 | 0 | B | 49 | 5 +/- 18 | NA | | 0. |
| 8.2 0+95.5 | 0+51.5 | 1 | 2.0 | 3 | 0 | 0 | B | 49 | 5 +/- 18 | NA | | 0. |
| 8.2 0+96.5 | 0+51.5 | 1 | 2.0 | 4 | 0 | 0 | B | 49 | 11 +/- 21 | NA | | 0. |

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R.H.TABLE B.2-3

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:47 AM

FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 8.2 DRIVEWAY FOR ALPHA

RADIATION TYPE: 2
COMPLETION
DATE: 10-17-94
TECHNICIANS: MANY
LOCATION: 8.0
GRID ID: 8.2
MEDIA TYPE: ASPHALT
# of POINTS: 681
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2
REM.+ FIXED: LIMIT

| | | | |
|---|---|---|---|
| MAX FOR IND GRID | 50 | PASS | 5000 |
| AVG - SURVEY UNIT | 11 | PASS | 5000 |
| STD X | 11 | | |
| MU SUB ALPHA | 11 | PASS | 5000 |
| MAX HOT SPOT | 41 | PASS | 15000 |

| ID # | GRID COORDINATES W | S | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | SCAN MAX ALPHA COUNTS | TOTAL CONT. AREA CM^2 | MATERIAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. ALPHA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 CM^2 | MAX TEST | INST CPM |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 | 0+91.5W | 0+39.5S | 6 | 1 | 1 | 0 | 0 | 8 | 41 | 0 +/- 11 | NA | | | 0. |
| 8.2 | 0+90.5W | 0+39.5S | 6 | 1 | 2 | 0 | 0 | 8 | 41 | 6 +/- 16 | NA | | | 0. |
| 8.2 | 0+89.5W | 0+39.5S | 6 | 1 | 3 | 0 | 0 | 8 | 41 | 11 +/- 19 | NA | | | 0. |
| 8.2 | 0+88.5W | 0+39.5S | 6 | 1 | 2 | 0 | 0 | 8 | 41 | 6 +/- 16 | NA | | | 0. |
| 8.2 | 0+90.5W | 0+38.5S | 6 | 1 | 8 | 0 | 0 | 8 | 41 | 39 +/- 31 | NA | | | 0. |
| 8.2 | 0+89.5W | 0+38.5S | 6 | 1 | 3 | 0 | 0 | 8 | 41 | 11 +/- 19 | NA | | | 0. |
| 8.2 | 0+88.5W | 0+38.5S | 6 | 1 | 3 | 0 | 0 | 8 | 41 | 11 +/- 19 | NA | | | 0. |
| 8.2 | 0+87.5W | 0+38.5S | 6 | 1 | 2 | 0 | 0 | 8 | 41 | 6 +/- 16 | NA | | | 0. |
| 8.2 | 0+89.5W | 0+37.5S | 6 | 1 | 3 | 0 | 0 | 8 | 41 | 11 +/- 19 | NA | | | 0. |
| 8.2 | 0+88.5W | 0+37.5S | 6 | 1 | 2 | 0 | 0 | 8 | 41 | 6 +/- 16 | NA | | | 0. |
| 8.2 | 0+87.5W | 0+37.5S | 6 | 1 | 4 | 0 | 0 | 8 | 41 | 17 +/- 22 | NA | | | 0. |
| 8.2 | 0+86.5W | 0+37.5S | 6 | 1 | 2 | 0 | 0 | 8 | 41 | 6 +/- 16 | NA | | | 0. |
| 8.2 | 0+85.5W | 0+37.5S | 6 | 1 | 2 | 0 | 0 | 8 | 41 | 6 +/- 16 | NA | | | 0. |
| 8.2 | 0+89.5W | 0+36.5S | 6 | 1 | 4 | 0 | 0 | 8 | 41 | 17 +/- 22 | NA | | | 0. |
| 8.2 | 0+88.5W | 0+36.5S | 6 | 1 | 3 | 0 | 0 | 8 | 41 | 11 +/- 19 | NA | | | 0. |
| 8.2 | 0+87.5W | 0+36.5S | 6 | 1 | 3 | 0 | 0 | 8 | 41 | 11 +/- 19 | NA | | | 0. |
| 8.2 | 0+86.5W | 0+36.5S | 6 | 1 | 3 | 0 | 0 | 8 | 41 | 11 +/- 19 | NA | | | 0. |
| 8.2 | 0+85.5W | 0+36.5S | 6 | 1 | 2 | 0 | 0 | 8 | 41 | 6 +/- 16 | NA | | | 0. |
| 8.2 | 0+88.5W | 0+35.5S | 6 | 1 | 4 | 0 | 0 | 8 | 41 | 17 +/- 22 | NA | | | 0. |
| 8.2 | 0+87.5W | 0+35.5S | 6 | 1 | 2 | 0 | 0 | 8 | 41 | 6 +/- 16 | NA | | | 0. |
| 8.2 | 0+86.5W | 0+35.5S | 6 | 1 | 0 | 0 | 0 | 8 | 41 | -6 +/- 3 | NA | | | 0. |
| 8.2 | 0+85.5W | 0+35.5S | 6 | 1 | 1 | 0 | 0 | 8 | 41 | 0 +/- 11 | NA | | | 0. |
| 8.2 | 0+84.5W | 0+35.5S | 6 | 1 | 4 | 0 | 0 | 8 | 41 | 17 +/- 22 | NA | | | 0. |
| 8.2 | 0+86.5W | 0+34.5S | 6 | 1 | 4 | 0 | 0 | 8 | 41 | 17 +/- 22 | NA | | | 0. |
| 8.2 | 0+85.5W | 0+34.5S | 6 | 1 | 5 | 0 | 0 | 8 | 41 | 22 +/- 25 | NA | | | 0. |
| 8.2 | 0+95.5 | 0+49.5 | 1 | 1.1 | 4 | 0 | 0 | 8 | 40 | 15 +/- 21 | NA | | | 0. |
| 8.2 | 0+94.5 | 0+49.5 | 1 | 1.1 | 5 | 0 | 0 | 8 | 40 | 21 +/- 23 | NA | | | 0. |
| 8.2 | 0+93.5 | 0+49.5 | 1 | 1.1 | 3 | 0 | 0 | 8 | 40 | 10 +/- 18 | NA | | | 0. |
| 8.2 | 0+92.5 | 0+49.5 | 1 | 1.1 | 6 | 0 | 0 | 8 | 40 | 26 +/- 26 | NA | | | 0. |

ANSTEC
APERTURE
CARD

Also Available on
Aperture Card

| EFF. /DPM |
|---|
| .803 |
| 1803 |
| 1803 |
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TABLE 8.2-3

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|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 0+96.5 | 0+61.5 | 3 | 0.2 | 6 | 0 | 0 | 8 | 25 | 30 +/- 25 | NA | 0 |
| 8.2 0+95.5 | 0+61.5 | 3 | 0.2 | 1 | 0 | 0 | 8 | 25 | 4 +/- 10 | NA | 0 |
| 8.2 0+94.5 | 0+61.5 | 3 | 0.2 | 4 | 0 | 0 | 8 | 25 | 20 +/- 20 | NA | 0 |
| 8.2 0+93.5 | 0+61.5 | 2 | 1.2 | 1 | 0 | 0 | 8 | 40 | -1 +/- 11 | NA | 0 |
| 8.2 1+0.5 | 0+62.5 | 4 | 0.4 | 5 | 0 | 0 | 8 | 28 | 23 +/- 22 | NA | 0 |
| 8.2 0+99.5 | 0+62.5 | 4 | 0.4 | 0 | 0 | 0 | 8 | 28 | -2 +/- 2 | NA | 0 |
| 8.2 0+98.5 | 0+62.5 | 4 | 0.4 | 3 | 0 | 0 | 8 | 28 | 13 +/- 17 | NA | 0 |
| 8.2 0+97.5 | 0+62.5 | 4 | 0.4 | 2 | 0 | 0 | 8 | 28 | 8 +/- 14 | NA | 0 |
| 8.2 0+96.5 | 0+62.5 | 4 | 0.4 | 2 | 0 | 0 | 8 | 28 | 8 +/- 14 | NA | 0 |
| 8.2 0+95.5 | 0+62.5 | 4 | 0.4 | 2 | 0 | 0 | 8 | 28 | 8 +/- 14 | NA | 0 |
| 8.2 0+94.5 | 0+62.5 | 2 | 1.2 | 2 | 0 | 0 | 8 | 40 | 4 +/- 15 | NA | 0 |
| 8.2 1+1.5 | 0+63.5 | 2 | 1.2 | 1 | 0 | 0 | 8 | 40 | -1 +/- 11 | NA | 0 |
| 8.2 1+0.5 | 0+63.5 | 4 | 0.4 | 5 | 0 | 0 | 8 | 28 | 23 +/- 22 | NA | 0 |
| 8.2 0+99.5 | 0+63.5 | 4 | 0.4 | 4 | 0 | 0 | 8 | 28 | 18 +/- 20 | NA | 0 |
| 8.2 0+98.5 | 0+63.5 | 4 | 0.4 | 3 | 0 | 0 | 8 | 28 | 13 +/- 17 | NA | 0 |
| 8.2 0+97.5 | 0+63.5 | 4 | 0.4 | 5 | 0 | 0 | 8 | 28 | 23 +/- 22 | NA | 0 |
| 8.2 0+96.5 | 0+63.5 | 4 | 0.4 | 0 | 0 | 0 | 8 | 28 | -2 +/- 2 | NA | 0 |
| 8.2 0+95.5 | 0+63.5 | 4 | 0.4 | 2 | 0 | 0 | 8 | 28 | 8 +/- 14 | NA | 0 |
| 8.2 0+94.5 | 0+63.5 | 2 | 1.2 | 3 | 0 | 0 | 8 | 40 | 9 +/- 18 | NA | 0 |
| 8.2 1+1.5 | 0+64.5 | 2 | 1.2 | 0 | 0 | 0 | 8 | 40 | -6 +/- 3 | NA | 0 |
| 8.2 1+0.5 | 0+64.5 | 4 | 0.4 | 6 | 0 | 0 | 8 | 28 | 28 +/- 24 | NA | 0 |
| 8.2 0+99.5 | 0+64.5 | 4 | 0.4 | 3 | 0 | 0 | 8 | 28 | 13 +/- 17 | NA | 0 |
| 8.2 0+98.5 | 0+64.5 | 4 | 0.4 | 2 | 0 | 0 | 8 | 28 | 8 +/- 14 | NA | 0 |
| 8.2 0+97.5 | 0+64.5 | 4 | 0.4 | 2 | 0 | 0 | 8 | 28 | 8 +/- 14 | NA | 0 |
| 8.2 0+96.5 | 0+64.5 | 4 | 0.4 | 6 | 0 | 0 | 8 | 28 | 28 +/- 24 | NA | 0 |
| 8.2 0+95.5 | 0+64.5 | 4 | 0.4 | 0 | 0 | 0 | 8 | 28 | -2 +/- 2 | NA | 0 |
| 8.2 1+2.5 | 0+65.5 | 2 | 1.2 | 0 | 0 | 0 | 8 | 40 | -6 +/- 3 | NA | 0 |
| 8.2 1+1.5 | 0+65.5 | 3 | 0.0 | 4 | 0 | 0 | 8 | 14 | 21 +/- 20 | NA | 0 |
| 8.2 1+0.5 | 0+65.5 | 3 | 0.0 | 2 | 0 | 0 | 8 | 14 | 10 +/- 14 | NA | 0 |
| 8.2 0+99.5 | 0+65.5 | 3 | 0.0 | 3 | 0 | 0 | 8 | 14 | 15 +/- 18 | NA | 0 |
| 8.2 0+98.5 | 0+65.5 | 3 | 0.0 | 3 | 0 | 0 | 8 | 14 | 15 +/- 18 | NA | 0 |
| 8.2 0+97.5 | 0+65.5 | 3 | 0.0 | 2 | 0 | 0 | 8 | 14 | 10 +/- 14 | NA | 0 |
| 8.2 0+96.5 | 0+65.5 | 3 | 0.0 | 2 | 0 | 0 | 8 | 14 | 10 +/- 14 | NA | 0 |
| 8.2 0+95.5 | 0+65.5 | 2 | 1.2 | 9 | 0 | 0 | 8 | 40 | 40 +/- 30 | NA | 0 |
| 8.2 1+2.5 | 0+66.5 | 2 | 1.2 | 0 | 0 | 0 | 8 | 40 | -6 +/- 3 | NA | 0 |
| 8.2 1+1.5 | 0+66.5 | 3 | 0.0 | 6 | 0 | 0 | 8 | 14 | 31 +/- 25 | NA | 0 |
| 8.2 1+0.5 | 0+66.5 | 3 | 0.0 | 1 | 0 | 0 | 8 | 14 | 5 +/- 10 | NA | 0 |
| 8.2 0+99.5 | 0+66.5 | 3 | 0.0 | 2 | 0 | 0 | 8 | 14 | 10 +/- 14 | NA | 0 |
| 8.2 0+98.5 | 0+66.5 | 3 | 0.0 | 2 | 0 | 0 | 8 | 14 | 10 +/- 14 | NA | 0 |
| 8.2 0+97.5 | 0+66.5 | 3 | 0.0 | 7 | 0 | 0 | 8 | 14 | 36 +/- 27 | NA | 0 |
| 8.2 0+96.5 | 0+66.5 | 3 | 0.0 | 5 | 0 | 0 | 8 | 14 | 26 +/- 23 | NA | 0 |
| 8.2 0+95.5 | 0+66.5 | 3 | 0.0 | 3 | 0 | 0 | 8 | 14 | 15 +/- 18 | NA | 0 |
| 8.2 1+2.5 | 0+67.5 | 4 | 0.3 | 5 | 0 | 0 | 8 | 26 | 23 +/- 22 | NA | 0 |
| 8.2 1+1.5 | 0+67.5 | 4 | 0.3 | 2 | 0 | 0 | 8 | 26 | 8 +/- 14 | NA | 0 |
| 8.2 1+0.5 | 0+67.5 | 4 | 0.3 | 0 | 0 | 0 | 8 | 26 | -1 +/- 2 | NA | 0 |
| 8.2 0+99.5 | 0+67.5 | 4 | 0.3 | 1 | 0 | 0 | 8 | 26 | 3 +/- 10 | NA | 0 |
| 8.2 0+98.5 | 0+67.5 | 4 | 0.3 | 3 | 0 | 0 | 8 | 26 | 13 +/- 17 | NA | 0 |
| 8.2 0+97.5 | 0+67.5 | 4 | 0.3 | 4 | 0 | 0 | 8 | 26 | 18 +/- 20 | NA | 0 |
| 8.2 0+96.5 | 0+67.5 | 2 | 1.2 | 4 | 0 | 0 | 8 | 40 | 14 +/- 20 | NA | 0 |
| 8.2 1+3.5 | 0+68.5 | 2 | 1.2 | 2 | 0 | 0 | 8 | 40 | 4 +/- 15 | NA | 0 |
| 8.2 1+2.5 | 0+68.5 | 5 | 0.3 | 5 | 0 | 0 | 8 | 29 | 26 +/- 24 | NA | 0 |
| 8.2 1+1.5 | 0+68.5 | 5 | 0.3 | 0 | 0 | 0 | 0 | 29 | -2 +/- 2 | NA | 0 |
| 8.2 1+0.5 | 0+68.5 | 5 | 0.3 | 2 | 0 | 0 | 8 | 29 | 9 +/- 15 | NA | 0 |
| 8.2 0+99.5 | 0+68.5 | 5 | 0.3 | 3 | 0 | 0 | 8 | 29 | 15 +/- 19 | NA | 0 |
| 8.2 0+98.5 | 0+68.5 | 5 | 0.3 | 2 | 0 | 0 | 8 | 29 | 9 +/- 15 | NA | 0 |
| 8.2 0+97.5 | 0+68.5 | 5 | 0.3 | 3 | 0 | 0 | 8 | 29 | 15 +/- 19 | NA | 0 |
| 8.2 0+96.5 | 0+68.5 | 2 | 1.2 | 6 | 0 | 0 | 8 | 40 | 25 +/- 25 | NA | 0 |
| 8.2 1+3.5 | 0+69.5 | 2 | 1.2 | 2 | 0 | 0 | 8 | 40 | 4 +/- 15 | NA | 0 |
| 8.2 1+2.5 | 0+69.5 | 5 | 0.3 | 4 | 0 | 0 | 8 | 29 | 20 +/- 22 | NA | 0 |
| 8.2 1+1.5 | 0+69.5 | 5 | 0.3 | 3 | 0 | 0 | 8 | 29 | 15 +/- 19 | NA | 0 |

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TABLE 8.2-3

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|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 1+0.5 | 0+69.5 | 5 | 0.3 | 2 | 0 | 0 | 8 | 29 | 9 +/- 15 | NA | 0 |
| 8.2 0+99.5 | 0+69.5 | 5 | 0.3 | 1 | 0 | 0 | 8 | 29 | 4 +/- 11 | NA | 0 |
| 8.2 0+98.5 | 0+69.5 | 5 | 0.3 | 2 | 0 | 0 | 8 | 29 | 9 +/- 15 | NA | 0 |
| 8.2 0+97.5 | 0+69.5 | 5 | 0.3 | 1 | 0 | 0 | 8 | 29 | 4 +/- 11 | NA | 0 |
| 8.2 0+96.5 | 0+69.5 | 2 | 1.2 | 2 | 0 | 0 | 8 | 40 | 4 +/- 15 | NA | 0. |
| 8.2 1+3.5 | 0+70.5 | 3 | 1.4 | 5 | 0 | 0 | 8 | 42 | 19 +/- 23 | NA | 0. |
| 8.2 1+2.5 | 0+70.5 | 4 | 0.3 | 1 | 0 | 0 | 8 | 26 | 3 +/- 10 | NA | 0. |
| 8.2 1+1.5 | 0+70.5 | 4 | 0.3 | 5 | 0 | 0 | 8 | 26 | 23 +/- 22 | NA | 0. |
| 8.2 1+0.5 | 0+70.5 | 4 | 0.3 | 3 | 0 | 0 | 8 | 26 | 13 +/- 17 | NA | 0. |
| 8.2 0+99.5 | 0+70.5 | 4 | 0.3 | 4 | 0 | 0 | 8 | 26 | 18 +/- 20 | NA | 0. |
| 8.2 0+98.5 | 0+70.5 | 4 | 0.3 | 3 | 0 | 0 | 8 | 26 | 13 +/- 17 | NA | 0. |
| 8.2 0+97.5 | 0+70.5 | 2 | 1.2 | 5 | 0 | 0 | 8 | 40 | 19 +/- 23 | NA | 0. |
| 8.2 1+4.5 | 0+71.5 | 2 | 1.2 | 0 | 0 | 0 | 8 | 40 | -6 +/- 3 | NA | 0. |
| 8.2 1+3.5 | 0+71.5 | 4 | 0.3 | 0 | 0 | 0 | 8 | 26 | -1 +/- 2 | NA | 0. |
| 8.2 1+2.5 | 0+71.5 | 4 | 0.3 | 3 | 0 | 0 | 8 | 26 | 13 +/- 17 | NA | 0. |
| 8.2 1+1.5 | 0+71.5 | 4 | 0.3 | 3 | 0 | 0 | 8 | 26 | 13 +/- 17 | NA | 0. |
| 8.2 1+0.5 | 0+71.5 | 4 | 0.3 | 1 | 0 | 0 | 8 | 26 | 3 +/- 10 | NA | 0. |
| 8.2 0+99.5 | 0+71.5 | 4 | 0.3 | 3 | 0 | 0 | 8 | 26 | 13 +/- 17 | NA | 0. |
| 8.2 0+98.5 | 0+71.5 | 4 | 0.3 | 5 | 0 | 0 | 8 | 26 | 23 +/- 22 | NA | 0. |
| 8.2 0+97.5 | 0+71.5 | 2 | 1.2 | 3 | 0 | 0 | 8 | 40 | 9 +/- 18 | NA | 0. |
| 8.2 1+4.5 | 0+72.5 | 2 | 1.2 | 1 | 0 | 0 | 8 | 40 | -1 +/- 11 | NA | 0. |
| 8.2 1+3.5 | 0+72.5 | 3 | 0.5 | 5 | 0 | 0 | 8 | 31 | 23 +/- 25 | NA | 0. |
| 8.2 1+2.5 | 0+72.5 | 3 | 0.5 | 4 | 0 | 0 | 8 | 31 | 18 +/- 20 | NA | 0. |
| 8.2 1+1.5 | 0+72.5 | 3 | 0.5 | 4 | 0 | 0 | 8 | 31 | 18 +/- 20 | NA | 0. |
| 8.2 1+0.5 | 0+72.5 | 3 | 0.5 | 4 | 0 | 0 | 8 | 31 | 18 +/- 20 | NA | 0. |
| 8.2 0+99.5 | 0+72.5 | 3 | 0.5 | 1 | 0 | 0 | 8 | 31 | 3 +/- 10 | NA | 0. |
| 8.2 0+98.5 | 0+72.5 | 3 | 0.5 | 4 | 0 | 0 | 8 | 31 | 18 +/- 20 | NA | 0. |
| 8.2 0+97.5 | 0+72.5 | 2 | 1.2 | 6 | 0 | 0 | 8 | 40 | 25 +/- 25 | NA | 0. |
| 8.2 1+4.5 | 0+74.5 | 3 | 1.4 | 2 | 0 | 0 | 8 | 42 | 3 +/- 15 | NA | 0. |
| 8.2 1+3.5 | 0+74.5 | 3 | 0.5 | 1 | 0 | 0 | 8 | 31 | 3 +/- 10 | NA | 0. |
| 8.2 1+2.5 | 0+74.5 | 3 | 0.5 | 4 | 0 | 0 | 8 | 31 | 18 +/- 20 | NA | 0. |
| 8.2 1+1.5 | 0+74.5 | 3 | 0.5 | 7 | 0 | 0 | 8 | 31 | 34 +/- 27 | NA | 0. |
| 8.2 1+0.5 | 0+74.5 | 3 | 0.5 | 5 | 0 | 0 | 8 | 31 | 23 +/- 23 | NA | 0. |
| 8.2 0+99.5 | 0+74.5 | 3 | 0.5 | 5 | 0 | 0 | 8 | 31 | 23 +/- 23 | NA | 0. |
| 8.2 0+98.5 | 0+74.5 | 3 | 1.4 | 2 | 0 | 0 | 8 | 42 | 3 +/- 15 | NA | 0. |
| 8.2 1+5.5 | 0+75.5 | 3 | 1.4 | 3 | 0 | 0 | 8 | 42 | 8 +/- 18 | NA | 0. |
| 8.2 1+4.5 | 0+75.5 | 4 | 2.4 | 4 | 0 | 0 | 8 | 49 | 8 +/- 20 | NA | 0. |
| 8.2 1+3.5 | 0+75.5 | 4 | 2.4 | 8 | 0 | 0 | 8 | 49 | 28 +/- 28 | NA | 0. |
| 8.2 1+2.5 | 0+75.5 | 4 | 2.4 | 6 | 0 | 0 | 8 | 49 | 18 +/- 24 | NA | 0. |
| 8.2 1+1.5 | 0+75.5 | 4 | 2.4 | 2 | 0 | 0 | 8 | 49 | -2 +/- 15 | NA | 0. |
| 8.2 1+0.5 | 0+75.5 | 4 | 2.4 | 6 | 0 | 0 | 8 | 49 | 18 +/- 24 | NA | 0. |
| 8.2 0+99.5 | 0+75.5 | 4 | 2.4 | 3 | 0 | 0 | 8 | 49 | 3 +/- 18 | NA | 0. |
| 8.2 0+98.5 | 0+75.5 | 3 | 1.4 | 8 | 0 | 0 | 8 | 42 | 34 +/- 29 | NA | 0. |
| 8.2 1+5.5 | 0+76.5 | 3 | 1.4 | 2 | 0 | 0 | 8 | 42 | 3 +/- 15 | NA | 0. |
| 8.2 1+4.5 | 0+76.5 | 4 | 2.4 | 3 | 0 | 0 | 8 | 49 | 3 +/- 18 | NA | 0. |
| 8.2 1+3.5 | 0+76.5 | 4 | 2.4 | 6 | 0 | 0 | 8 | 49 | 18 +/- 24 | NA | 0. |
| 8.2 1+2.5 | 0+76.5 | 4 | 2.4 | 5 | 0 | 0 | 8 | 49 | 13 +/- 22 | NA | 0. |
| 8.2 1+1.5 | 0+76.5 | 4 | 2.4 | 3 | 0 | 0 | 8 | 49 | 3 +/- 18 | NA | 0. |
| 8.2 1+0.5 | 0+76.5 | 4 | 2.4 | 5 | 0 | 0 | 8 | 49 | 13 +/- 22 | NA | 0. |
| 8.2 0+99.5 | 0+76.5 | 4 | 2.4 | 4 | 0 | 0 | 8 | 49 | 8 +/- 20 | NA | 0. |
| 8.2 0+98.5 | 0+76.5 | 3 | 1.4 | 4 | 0 | 0 | 8 | 42 | 13 +/- 21 | NA | 0. |
| 8.2 1+5.5 | 0+77.5 | 3 | 1.4 | 1 | 0 | 0 | 8 | 42 | -2 +/- 11 | NA | 0. |
| 8.2 1+4.5 | 0+77.5 | 4 | 2.4 | 7 | 0 | 0 | 8 | 49 | 23 +/- 26 | NA | 0. |
| 8.2 1+3.5 | 0+77.5 | 4 | 2.4 | 2 | 0 | 0 | 8 | 49 | -2 +/- 15 | NA | 0. |
| 8.2 1+2.5 | 0+77.5 | 4 | 2.4 | 5 | 0 | 0 | 8 | 49 | 13 +/- 22 | NA | 0. |
| 8.2 1+1.5 | 0+77.5 | 4 | 2.4 | 3 | 0 | 0 | 8 | 49 | 3 +/- 18 | NA | 0. |
| 8.2 1+0.5 | 0+77.5 | 4 | 2.4 | 4 | 0 | 0 | 8 | 49 | 8 +/- 20 | NA | 0. |
| 8.2 0+99.5 | 0+77.5 | 4 | 2.4 | 3 | 0 | 0 | 8 | 49 | 3 +/- 18 | NA | 0. |
| 8.2 0+98.5 | 0+77.5 | 3 | 1.4 | 11 | 0 | 0 | 8 | 42 | 50 +/- 34 | NA | 0. |
| 8.2 1+5.5 | 0+78.5 | 3 | 1.4 | 1 | 0 | 0 | 8 | 42 | -2 +/- 11 | NA | 0. |

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TABLE B.2-3

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|---|---|---|---|---|---|---|---|---|---|---|---|
| B.2 1+4.5 | 0+78.5 | 4 | 2.4 | 4 | 0 | 0 | B | 49 | 8 +/- 20 | NA | 0 |
| B.2 1+3.5 | 0+78.5 | 3 | 1.1 | 5 | 0 | 0 | C | 39 | 20 +/- 23 | NA | 0 |
| B.2 1+2.5 | 0+78.5 | 3 | 1.1 | 2 | 0 | 0 | B | 39 | 5 +/- 15 | NA | 0 |
| B.2 1+1.5 | 0+78.5 | 3 | 1.1 | 4 | 0 | 0 | B | 39 | 15 +/- 21 | NA | 0 |
| B.2 1+0.5 | 0+78.5 | 3 | 1.1 | 3 | 0 | 0 | B | 39 | 10 +/- 18 | NA | 0 |
| B.2 0+99.5 | 0+78.5 | 3 | 1.4 | 6 | 0 | 0 | B | 42 | 24 +/- 25 | NA | 0 |
| B.2 1+6.5 | 0+79.5 | 3 | 1.4 | 3 | 0 | 0 | B | 42 | 8 +/- 18 | NA | 0 |
| B.2 1+5.5 | 0+79.5 | 3 | 1.1 | 3 | 0 | 0 | B | 39 | 10 +/- 18 | NA | 0 |
| B.2 1+4.5 | 0+79.5 | 3 | 1.1 | 10 | 0 | 0 | B | 39 | 46 +/- 32 | NA | 0 |
| B.2 1+3.5 | 0+79.5 | 3 | 1.1 | 5 | 0 | 0 | B | 39 | 20 +/- 23 | NA | 0 |
| B.2 1+2.5 | 0+79.5 | 3 | 1.1 | 6 | 0 | 0 | B | 39 | 25 +/- 25 | NA | 0 |
| B.2 1+1.5 | 0+79.5 | 3 | 1.1 | 4 | 0 | 0 | B | 39 | 15 +/- 21 | NA | 0 |
| B.2 1+0.5 | 0+79.5 | 3 | 1.1 | 3 | 0 | 0 | B | 39 | 10 +/- 18 | NA | 0 |
| B.2 0+99.5 | 0+79.5 | 3 | 1.4 | 6 | 0 | 0 | B | 42 | 24 +/- 25 | NA | 0 |
| B.2 1+6.5 | 0+80.5 | 3 | 1.4 | 5 | 0 | 0 | B | 42 | 19 +/- 23 | NA | 0 |
| B.2 1+5.5 | 0+80.5 | 3 | 1.1 | 1 | 0 | 0 | B | 39 | -1 +/- 11 | NA | 0 |
| B.2 1+4.5 | 0+80.5 | 3 | 1.1 | 9 | 0 | 0 | B | 39 | 41 +/- 31 | NA | 0 |
| B.2 1+3.5 | 0+80.5 | 3 | 1.1 | 6 | 0 | 0 | B | 39 | 25 +/- 25 | NA | 0 |
| B.2 1+2.5 | 0+80.5 | 3 | 1.1 | 5 | 0 | 0 | B | 39 | 20 +/- 23 | NA | 0 |
| B.2 1+1.5 | 0+80.5 | 3 | 1.1 | 4 | 0 | 0 | B | 39 | 15 +/- 21 | NA | 0 |
| B.2 1+0.5 | 0+80.5 | 3 | 1.1 | 5 | 0 | 0 | B | 39 | 20 +/- 23 | NA | 0 |
| B.2 0+99.5 | 0+80.5 | 3 | 1.4 | 1 | 0 | 0 | B | 42 | -2 +/- 11 | NA | 0 |
| B.2 1+6.5 | 0+81.5 | 3 | 1.4 | 3 | 0 | 0 | B | 42 | 8 +/- 18 | NA | 0 |
| B.2 1+5.5 | 0+81.5 | 3 | 1.1 | 0 | 0 | 0 | B | 39 | -5 +/- 3 | NA | 0 |
| B.2 1+4.5 | 0+81.5 | 3 | 1.1 | 4 | 0 | 0 | B | 39 | 15 +/- 21 | NA | 0 |
| B.2 1+3.5 | 0+81.5 | 3 | 1.1 | 3 | 0 | 0 | B | 39 | 10 +/- 18 | NA | 0 |
| B.2 1+2.5 | 0+81.5 | 3 | 1.1 | 1 | 0 | 0 | B | 39 | -1 +/- 11 | NA | 0 |
| B.2 1+1.5 | 0+81.5 | 3 | 1.1 | 3 | 0 | 0 | B | 39 | 10 +/- 18 | NA | 0 |
| B.2 1+0.5 | 0+81.5 | 3 | 1.4 | 5 | 0 | 0 | B | 42 | 19 +/- 23 | NA | 0 |
| B.2 1+6.5 | 0+82.5 | 3 | 1.4 | 2 | 0 | 0 | B | 42 | 3 +/- 15 | NA | 0 |
| B.2 1+5.5 | 0+82.5 | 3 | 0.6 | 5 | 0 | 0 | B | 33 | 23 +/- 23 | NA | 0 |
| B.2 1+4.5 | 0+82.5 | 3 | 0.6 | 3 | 0 | 0 | B | 33 | 12 +/- 18 | NA | 0 |
| B.2 1+3.5 | 0+82.5 | 3 | 0.6 | 2 | 0 | 0 | B | 33 | 7 +/- 15 | NA | 0 |
| B.2 1+2.5 | 0+82.5 | 3 | 0.6 | 1 | 0 | 0 | B | 33 | 2 +/- 10 | NA | 0 |
| B.2 1+1.5 | 0+82.5 | 3 | 0.6 | 4 | 0 | 0 | B | 33 | 18 +/- 20 | NA | 0 |
| B.2 1+0.5 | 0+82.5 | 3 | 1.4 | 7 | 0 | 0 | B | 42 | 29 +/- 27 | NA | 0 |
| B.2 1+7.5 | 0+83.5 | 3 | 1.4 | 0 | 0 | 0 | B | 42 | -7 +/- 4 | NA | 0 |
| B.2 1+6.5 | 0+83.5 | 6 | 0.6 | 3 | 0 | 0 | B | 35 | 13 +/- 19 | NA | 0 |
| B.2 1+5.5 | 0+83.5 | 3 | 0.6 | 3 | 0 | 0 | B | 33 | 12 +/- 18 | NA | 0 |
| B.2 1+4.5 | 0+83.5 | 3 | 0.6 | 2 | 0 | 0 | B | 33 | 7 +/- 15 | NA | 0 |
| B.2 1+3.5 | 0+83.5 | 3 | 0.6 | 4 | 0 | 0 | B | 33 | 18 +/- 20 | NA | 0 |
| B.2 1+2.5 | 0+83.5 | 3 | 0.6 | 1 | 0 | 0 | B | 33 | 2 +/- 10 | NA | 0 |
| B.2 1+1.5 | 0+83.5 | 3 | 1.4 | 3 | 0 | 0 | B | 42 | 8 +/- 18 | NA | 0 |
| B.2 1+7.5 | 0+84.5 | 3 | 1.4 | 3 | 0 | 0 | B | 42 | 8 +/- 18 | NA | 0 |
| B.2 1+6.5 | 0+84.5 | 3 | 0.6 | 5 | 0 | 0 | B | 33 | 23 +/- 23 | NA | 0 |
| B.2 1+5.5 | 0+84.5 | 3 | 0.6 | 4 | 0 | 0 | B | 33 | 18 +/- 20 | NA | 0 |
| B.2 1+4.5 | 0+84.5 | 3 | 0.6 | 3 | 0 | 0 | B | 33 | 12 +/- 18 | NA | 0 |
| B.2 1+3.5 | 0+84.5 | 3 | 0.6 | 4 | 0 | 0 | B | 33 | 18 +/- 20 | NA | 0 |
| B.2 1+2.5 | 0+84.5 | 3 | 0.6 | 2 | 0 | 0 | B | 33 | 7 +/- 15 | NA | 0 |
| B.2 1+1.5 | 0+84.5 | 3 | 1.4 | 2 | 0 | 0 | B | 42 | 3 +/- 15 | NA | 0 |
| B.2 1+7.5 | 0+85.5 | 3 | 1.4 | 3 | 0 | 0 | B | 42 | 8 +/- 18 | NA | 0 |
| B.2 1+6.5 | 0+85.5 | 3 | 0.6 | 5 | 0 | 0 | B | 33 | 23 +/- 23 | NA | 0 |
| B.2 1+5.5 | 0+85.5 | 3 | 0.6 | 3 | 0 | 0 | B | 33 | 12 +/- 18 | NA | 0 |
| B.2 1+4.5 | 0+85.5 | 3 | 0.6 | 3 | 0 | 0 | B | 33 | 12 +/- 18 | NA | 0 |
| B.2 1+3.5 | 0+85.5 | 3 | 0.6 | 7 | 0 | 0 | B | 33 | 33 +/- 27 | NA | 0 |
| B.2 1+2.5 | 0+85.5 | 3 | 0.6 | 0 | 0 | 0 | B | 33 | -3 +/- 2 | NA | 0 |
| B.2 1+1.5 | 0+85.5 | 3 | 1.4 | 5 | 0 | 0 | B | 42 | 19 +/- 23 | NA | 0 |
| B.2 1+8.5 | 0+86.5 | 3 | 1.4 | 3 | 0 | 0 | B | 42 | 8 +/- 18 | NA | 0 |
| B.2 1+7.5 | 0+86.5 | 4 | 1.6 | 3 | 0 | 0 | B | 43 | 7 +/- 17 | NA | 0 |
| B.2 1+6.5 | 0+86.5 | 4 | 1.6 | 3 | 0 | 0 | B | 41 | 8 +/- 17 | NA | 0 |

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TABLE 8.2-3

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|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 1+5.5 | 0+86.5 | 4 | 1.6 | 0 | 0 | 0 | 8 | 43 | -8 +/- 4 | NA | 0.20 |
| 8.2 1+4.5 | 0+86.5 | 4 | 1.6 | 2 | 0 | 0 | 8 | 43 | 2 +/- 14 | NA | 0.20 |
| 8.2 1+3.5 | 0+86.5 | 4 | 1.6 | 1 | 0 | 0 | 8 | 43 | -3 +/- 10 | NA | 0.20 |
| 8.2 1+2.5 | 0+86.5 | 4 | 1.6 | 2 | 0 | 0 | 8 | 43 | 2 +/- 14 | NA | 0.20 |
| 8.2 1+1.5 | 0+86.5 | 3 | 1.4 | 6 | 0 | 0 | 8 | 42 | 24 +/- 25 | NA | 0.19 |
| 8.2 1+8.5 | 0+87.5 | 3 | 1.4 | 3 | 0 | 0 | 8 | 42 | 8 +/- 18 | NA | 0.19 |
| 8.2 1+7.5 | 0+87.5 | 4 | 1.6 | 4 | 0 | 0 | 8 | 43 | 12 +/- 20 | NA | 0.20 |
| 8.2 1+6.5 | 0+87.5 | 4 | 1.6 | 4 | 0 | 0 | 8 | 43 | 12 +/- 20 | NA | 0.20 |
| 8.2 1+5.5 | 0+87.5 | 4 | 1.6 | 2 | 0 | 0 | 8 | 43 | 2 +/- 14 | NA | 0.20 |
| 8.2 1+4.5 | 0+87.5 | 4 | 1.6 | 2 | 0 | 0 | 8 | 43 | 2 +/- 14 | NA | 0.20 |
| 8.2 1+3.5 | 0+87.5 | 4 | 1.6 | 2 | 0 | 0 | 8 | 43 | 2 +/- 14 | NA | 0.20 |
| 8.2 1+2.5 | 0+87.5 | 3 | 1.4 | 4 | 0 | 0 | 8 | 42 | 13 +/- 21 | NA | 0.19 |
| 8.2 1+8.5 | 0+88.5 | 3 | 1.4 | 3 | 0 | 0 | 8 | 42 | 8 +/- 18 | NA | 0.19 |
| 8.2 1+7.5 | 0+88.5 | 4 | 0.3 | 3 | 0 | 0 | 8 | 26 | 13 +/- 17 | NA | 0.20 |
| 8.2 1+6.5 | 0+88.5 | 4 | 0.3 | 6 | 0 | 0 | 8 | 26 | 28 +/- 24 | NA | 0.20 |
| 8.2 1+5.5 | 0+88.5 | 4 | 0.3 | 6 | 0 | 0 | 8 | 26 | 28 +/- 24 | NA | 0.20 |
| 8.2 1+4.5 | 0+88.5 | 4 | 0.3 | 3 | 0 | 0 | 8 | 26 | 13 +/- 17 | NA | 0.20 |
| 8.2 1+3.5 | 0+88.5 | 4 | 0.3 | 5 | 0 | 0 | 8 | 26 | 23 +/- 22 | NA | 0.20 |
| 8.2 1+2.5 | 0+88.5 | 3 | 1.4 | 4 | 0 | 0 | 8 | 42 | 13 +/- 21 | NA | 0.19 |
| 8.2 1+8.5 | 0+89.5 | 3 | 1.4 | 2 | 0 | 0 | 8 | 42 | 3 +/- 15 | NA | 0.19 |
| 8.2 1+7.5 | 0+89.5 | 4 | 0.3 | 4 | 0 | 0 | 8 | 26 | 18 +/- 20 | NA | 0.20 |
| 8.2 1+6.5 | 0+89.5 | 4 | 0.3 | 1 | 0 | 0 | 8 | 26 | 3 +/- 10 | NA | 0.20 |
| 8.2 1+5.5 | 0+89.5 | 4 | 0.3 | 1 | 0 | 0 | 8 | 26 | 3 +/- 10 | NA | 0.20 |
| 8.2 1+4.5 | 0+89.5 | 4 | 0.3 | 4 | 0 | 0 | 8 | 26 | 18 +/- 20 | NA | 0.20 |
| 8.2 1+3.5 | 0+89.5 | 4 | 0.3 | 2 | 0 | 0 | 8 | 26 | 8 +/- 14 | NA | 0.20 |
| 8.2 1+2.5 | 0+89.5 | 3 | 1.4 | 3 | 0 | 0 | 8 | 42 | 8 +/- 18 | NA | 0.1 |
| 8.2 1+9.5 | 0+90.5 | 3 | 1.4 | 4 | 0 | 0 | 8 | 42 | 13 +/- 21 | NA | 0.19 |
| 8.2 1+8.5 | 0+90.5 | 4 | 0.3 | 0 | 0 | 0 | 8 | 26 | -1 +/- 2 | NA | 0.2 |
| 8.2 1+7.5 | 0+90.5 | 4 | 0.3 | 2 | 0 | 0 | 8 | 26 | 8 +/- 14 | NA | 0.2 |
| 8.2 1+6.5 | 0+90.5 | 4 | 0.3 | 3 | 0 | 0 | 8 | 26 | 13 +/- 17 | NA | 0.20 |
| 8.2 1+5.5 | 0+90.5 | 4 | 0.3 | 1 | 0 | 0 | 8 | 26 | 3 +/- 10 | NA | 0.2 |
| 8.2 1+4.5 | 0+90.5 | 4 | 0.3 | 3 | 0 | 0 | 8 | 26 | 13 +/- 17 | NA | 0.2 |
| 8.2 1+3.5 | 0+90.5 | 3 | 1.4 | 4 | 0 | 0 | 8 | 42 | 13 +/- 21 | NA | 0.1 |
| 8.2 1+9.5 | 0+91.5 | 3 | 1.4 | 3 | 0 | 0 | 8 | 42 | 8 +/- 18 | NA | 0.1 |
| 8.2 1+8.5 | 0+91.5 | 4 | 0.3 | 5 | 0 | 0 | 8 | 26 | 23 +/- 22 | NA | 0.2 |
| 8.2 1+7.5 | 0+91.5 | 4 | 0.3 | 4 | 0 | 0 | 8 | 26 | 18 +/- 20 | NA | 0.2 |
| 8.2 1+6.5 | 0+91.5 | 4 | 0.3 | 3 | 0 | 0 | 8 | 26 | 13 +/- 17 | NA | 0.2 |
| 8.2 1+5.5 | 0+91.5 | 3 | 1.4 | 5 | 0 | 0 | 8 | 42 | 19 +/- 23 | NA | 0.1 |
| 8.2 1+9.5 | 0+92.5 | 3 | 1.4 | 1 | 0 | 0 | 8 | 42 | -2 +/- 11 | NA | 0.1 |
| 8.2 1+8.5 | 0+92.5 | 3 | 0.5 | 7 | 0 | 0 | 8 | 31 | 34 +/- 27 | NA | 0.1 |
| 8.2 1+7.5 | 0+92.5 | 3 | 0.5 | 3 | 0 | 0 | 8 | 31 | 13 +/- 18 | NA | 0.1 |
| 8.2 1+6.5 | 0+92.5 | 3 | 0.5 | 2 | 0 | 0 | 8 | 31 | 8 +/- 14 | NA | 0.1 |
| 8.2 1+5.5 | 0+92.5 | 3 | 0.5 | 1 | 0 | 0 | 8 | 31 | 3 +/- 10 | NA | 0.1 |
| 8.2 1+4.5 | 0+92.5 | 3 | 0.5 | 1 | 0 | 0 | 8 | 31 | 3 +/- 10 | NA | 0.1 |
| 8.2 1+3.5 | 0+92.5 | 3 | 1.4 | 8 | 0 | 0 | 8 | 42 | 34 +/- 29 | NA | 0.1 |
| 8.2 1+10.5 | 0+93.5 | 3 | 1.4 | 1 | 0 | 0 | 8 | 42 | -2 +/- 11 | NA | 0. |
| 8.2 1+9.5 | 0+93.5 | 3 | 0.5 | 4 | 0 | 0 | 8 | 31 | 18 +/- 20 | NA | 0. |
| 8.2 1+8.5 | 0+93.5 | 3 | 0.5 | 4 | 0 | 0 | 8 | 31 | 18 +/- 20 | NA | 0.1 |
| 8.2 1+7.5 | 0+93.5 | 3 | 0.5 | 3 | 0 | 0 | 8 | 31 | 13 +/- 18 | NA | 0. |
| 8.2 1+6.5 | 0+93.5 | 3 | 0.5 | 1 | 0 | 0 | 8 | 31 | 3 +/- 10 | NA | 0. |
| 8.2 1+5.5 | 0+93.5 | 3 | 0.5 | 1 | 0 | 0 | 8 | 31 | 3 +/- 10 | NA | 0.1 |
| 8.2 1+4.5 | 0+93.5 | 3 | 0.5 | 0 | 0 | 0 | 8 | 31 | -3 +/- 2 | NA | 0. |
| 8.2 1+3.5 | 0+93.5 | 3 | 1.4 | 4 | 0 | 0 | 8 | 42 | 13 +/- 21 | NA | 0. |
| 8.2 1+10.5 | 0+94.5 | 3 | 1.4 | 3 | 0 | 0 | 8 | 42 | 8 +/- 18 | NA | 0. |
| 8.2 1+9.5 | 0+94.5 | 3 | 0.5 | 1 | 0 | 0 | 8 | 31 | 3 +/- 10 | NA | 0. |
| 8.2 1+8.5 | 0+94.5 | 3 | 0.5 | 0 | 0 | 0 | 8 | 31 | -3 +/- 2 | NA | 0. |
| 8.2 1+7.5 | 0+94.5 | 3 | 0.5 | 2 | 0 | 0 | 8 | 31 | 8 +/- 14 | NA | 0. |
| 8.2 1+6.5 | 0+94.5 | 3 | 0.5 | 5 | 0 | 0 | 8 | 31 | 23 +/- 23 | NA | 0. |
| 8.2 1+5.5 | 0+94.5 | 4 | 0.3 | 2 | 0 | 0 | 8 | 26 | 8 +/- 14 | NA | 0. |
| 8.2 1+4.5 | 0+94.5 | 3 | 1.4 | 8 | 0 | 0 | 8 | 42 | 34 +/- 29 | NA | 0. |

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TABLE B.2-3

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|---|---|---|---|---|---|---|---|---|---|---|---|
| B.2 1+10.5 | 0+95.5 | 3 | 1.4 | 5 | 0 | 0 | B | 42 | 19 +/- 23 | NA | 0. |
| B.2 1+9.5 | 0+95.5 | 4 | 0.3 | 3 | 0 | 0 | B | 26 | 13 +/- 17 | NA | 0. |
| B.2 1+8.5 | 0+95.5 | 4 | 0.3 | 3 | 0 | 0 | B | 26 | 13 +/- 17 | NA | 0. |
| B.2 1+7.5 | 0+95.5 | 4 | 0.3 | 4 | 0 | 0 | B | 26 | 18 +/- 20 | NA | 0. |
| B.2 1+6.5 | 0+95.5 | 4 | 0.3 | 3 | 0 | 0 | B | 26 | 13 +/- 17 | NA | 0. |
| B.2 1+5.5 | 0+95.5 | 4 | 0.3 | 2 | 0 | 0 | B | 26 | 8 +/- 14 | NA | 0. |
| B.2 1+4.5 | 0+95.5 | 3 | 1.4 | 2 | 0 | 0 | B | 42 | 3 +/- 13 | NA | 0. |
| B.2 1+10.5 | 0+96.5 | 3 | 1.4 | 0 | 0 | 0 | B | 42 | -7 +/- 4 | NA | 0. |
| B.2 1+9.5 | 0+96.5 | 4 | 1.5 | 6 | 0 | 0 | B | 42 | 22 +/- 24 | NA | 0. |
| B.2 1+8.5 | 0+96.5 | 4 | 1.5 | 9 | 0 | 0 | B | 42 | 37 +/- 29 | NA | 0. |
| B.2 1+7.5 | 0+96.5 | 4 | 1.5 | 5 | 0 | 0 | B | 42 | 17 +/- 22 | NA | 0. |
| B.2 1+6.5 | 0+96.5 | 4 | 1.5 | 4 | 0 | 0 | B | 42 | 12 +/- 20 | NA | 0. |
| B.2 1+5.5 | 0+96.5 | 4 | 1.5 | 4 | 0 | 0 | B | 42 | 12 +/- 20 | NA | 0. |
| B.2 1+4.5 | 0+96.5 | 3 | 1.4 | 5 | 0 | 0 | B | 42 | 19 +/- 23 | NA | 0. |
| B.2 1+11.5 | 0+97.5 | 3 | 1.4 | 0 | 0 | 0 | B | 42 | -7 +/- 4 | NA | 0. |
| B.2 1+10.5 | 0+97.5 | 4 | 1.5 | 3 | 0 | 0 | B | 42 | 7 +/- 17 | NA | 0. |
| B.2 1+9.5 | 0+97.5 | 4 | 1.5 | 3 | 0 | 0 | B | 42 | 7 +/- 17 | NA | 0. |
| B.2 1+8.5 | 0+97.5 | 4 | 1.5 | 5 | 0 | 0 | B | 42 | 17 +/- 22 | NA | 0. |
| B.2 1+7.5 | 0+97.5 | 4 | 1.5 | 2 | 0 | 0 | B | 42 | 2 +/- 14 | NA | 0. |
| B.2 1+6.5 | 0+97.5 | 4 | 1.5 | 3 | 0 | 0 | B | 42 | 7 +/- 17 | NA | 0. |
| B.2 1+5.5 | 0+97.5 | 4 | 1.5 | 5 | 0 | 0 | B | 42 | 17 +/- 22 | NA | 0. |
| B.2 1+4.5 | 0+97.5 | 3 | 1.4 | 6 | 0 | 0 | B | 42 | 24 +/- 25 | NA | 0. |
| B.2 1+11.5 | 0+98.5 | 3 | 1.4 | 5 | 0 | 0 | B | 42 | 19 +/- 23 | NA | 0. |
| B.2 1+10.5 | 0+98.5 | 4 | 1.5 | 3 | 0 | 0 | B | 42 | 7 +/- 17 | NA | 0. |
| B.2 1+9.5 | 0+98.5 | 4 | 1.5 | 3 | 0 | 0 | B | 42 | 7 +/- 17 | NA | 0. |
| B.2 1+8.5 | 0+98.5 | 4 | 1.5 | 6 | 0 | 0 | B | 42 | 22 +/- 24 | NA | 0. |
| B.2 1+7.5 | 0+98.5 | 4 | 1.5 | 1 | 0 | 0 | B | 42 | -2 +/- 10 | NA | 0. |
| B.2 1+6.5 | 0+98.5 | 4 | 1.5 | 2 | 0 | 0 | B | 42 | 2 +/- 14 | NA | 0. |
| B.2 1+5.5 | 0+98.5 | 4 | 1.5 | 3 | 0 | 0 | B | 42 | 7 +/- 17 | NA | 0. |
| B.2 1+4.5 | 0+98.5 | 3 | 1.4 | 3 | 0 | 0 | B | 42 | 8 +/- 18 | NA | 0. |
| B.2 1+11.5 | 0+99.5 | 3 | 1.4 | 2 | 0 | 0 | B | 42 | 3 +/- 15 | NA | 0. |
| B.2 1+10.5 | 0+99.5 | 4 | 1.5 | 2 | 0 | 0 | B | 42 | 2 +/- 14 | NA | 0. |
| B.2 1+9.5 | 0+99.5 | 4 | 1.5 | 2 | 0 | 0 | B | 42 | 2 +/- 14 | NA | 0. |
| B.2 1+8.5 | 0+99.5 | 4 | 1.5 | 3 | 0 | 0 | B | 42 | 7 +/- 17 | NA | 0. |
| B.2 1+7.5 | 0+99.5 | 4 | 1.5 | 0 | 0 | 0 | B | 42 | -7 +/- 4 | NA | 0. |
| B.2 1+6.5 | 0+99.5 | 4 | 1.5 | 2 | 0 | 0 | B | 42 | 2 +/- 14 | NA | 0. |
| B.2 1+5.5 | 0+99.5 | 3 | 1.4 | 4 | 0 | 0 | B | 42 | 13 +/- 21 | NA | 0. |
| B.2 1+11.5 | 1+0.5 | 4 | 1.5 | 4 | 0 | 0 | B | 42 | 12 +/- 20 | NA | 0. |
| B.2 1+10.5 | 1+0.5 | 4 | 1.5 | 4 | 0 | 0 | B | 42 | 12 +/- 20 | NA | 0. |
| B.2 1+9.5 | 1+0.5 | 4 | 1.5 | 1 | 0 | 0 | B | 42 | -2 +/- 10 | NA | 0. |
| B.2 1+8.5 | 1+0.5 | 4 | 1.5 | 4 | 0 | 0 | B | 42 | 12 +/- 20 | NA | 0. |
| B.2 1+7.5 | 1+0.5 | 4 | 1.5 | 4 | 0 | 0 | B | 42 | 12 +/- 20 | NA | 0. |
| B.2 1+6.5 | 1+0.5 | 4 | 1.5 | 2 | 0 | 0 | B | 42 | 2 +/- 14 | NA | 0. |
| B.2 1+5.5 | 1+0.5 | 4 | 1.5 | 3 | 0 | 0 | B | 42 | 7 +/- 17 | NA | 0. |
| B.2 1+4.5 | 1+0.5 | 4 | 1.5 | 3 | 0 | 0 | B | 42 | 7 +/- 17 | NA | 0. |
| B.2 1+12.5 | 1+1.5 | 3 | 3.4 | 9 | 0 | 0 | B | 58 | 29 +/- 31 | NA | 0. |
| B.2 1+11.5 | 1+1.5 | 3 | 3.4 | 4 | 0 | 0 | B | 58 | 3 +/- 21 | NA | 0. |
| B.2 1+10.5 | 1+1.5 | 3 | 3.4 | 3 | 0 | 0 | B | 58 | -2 +/- 18 | NA | 0. |
| B.2 1+9.5 | 1+1.5 | 3 | 3.4 | 2 | 0 | 0 | B | 58 | -7 +/- 15 | NA | 0. |
| B.2 1+8.5 | 1+1.5 | 3 | 3.4 | 6 | 0 | 0 | B | 58 | 13 +/- 25 | NA | 0. |
| B.2 1+7.5 | 1+1.5 | 3 | 3.4 | 6 | 0 | 0 | B | 58 | 13 +/- 25 | NA | 0. |
| B.2 1+6.5 | 1+1.5 | 3 | 3.4 | 7 | 0 | 0 | B | 58 | 19 +/- 27 | NA | 0. |
| B.2 1+5.5 | 1+1.5 | 3 | 3.4 | 4 | 0 | 0 | B | 58 | 3 +/- 21 | NA | 0. |
| B.2 1+12.5 | 1+2.5 | 3 | 3.4 | 3 | 10 | 500 | B | 58 | -0 +/- 18 | 34 | 0. |
| B.2 1+11.5 | 0+2.5 | 3 | 3.4 | 4 | 0 | 0 | B | 58 | 3 +/- 21 | NA | 0. |
| B.2 1+10.5 | 0+2.5 | 3 | 3.4 | 9 | 0 | 0 | B | 58 | 29 +/- 31 | NA | 0. |
| B.2 1+9.5 | 1+2.5 | 3 | 3.4 | 4 | 0 | 0 | B | 58 | 3 +/- 21 | NA | 0. |
| B.2 1+8.5 | 0+2.5 | 3 | 3.4 | 6 | 0 | 0 | B | 58 | 13 +/- 25 | NA | 0. |
| B.2 1+7.5 | 1+2.5 | 3 | 3.4 | 4 | 0 | 0 | B | 58 | 3 +/- 21 | NA | 0. |
| B.2 1+6.5 | 0+2.5 | 3 | 3.4 | 7 | 0 | 0 | B | 58 | 19 +/- 27 | NA | 0. |

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TABLE 8.2-3

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|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 1+5.5 | 0+2.5 | 3 | 3.4 | 7 | 0 | 0 | 8 | 58 | 19 +/- 27 | NA | 0. |
| 8.2 1+12.5 | 0+3.5 | 3 | 3.4 | 13 | 0 | 0 | 8 | 58 | 50 +/- 37 | NA | 0. |
| 8.2 1+11.5 | 0+3.5 | 3 | 3.4 | 5 | 0 | 0 | 8 | 58 | 8 +/- 23 | NA | 0. |
| 8.2 1+10.5 | 0+3.5 | 3 | 3.4 | 3 | 0 | 0 | 8 | 58 | -2 +/- 18 | NA | 0. |
| 8.2 1+9.5 | 0+3.5 | 3 | 3.4 | 7 | 0 | 0 | 8 | 58 | 19 +/- 27 | NA | 0. |
| 8.2 1+8.5 | 0+3.5 | 3 | 3.4 | 3 | 0 | 0 | 8 | 58 | -2 +/- 18 | NA | 0. |
| 8.2 1+7.5 | 0+3.5 | 3 | 3.4 | 5 | 0 | 0 | 8 | 58 | 8 +/- 23 | NA | 0. |
| 8.2 1+6.5 | 0+3.5 | 3 | 3.4 | 6 | 0 | 0 | 8 | 58 | 13 +/- 25 | NA | 0. |
| 8.2 1+5.5 | 0+3.5 | 3 | 3.4 | 7 | 0 | 0 | 8 | 58 | 19 +/- 27 | NA | 0. |
| 8.2 1+12.5 | 1+4.5 | 3 | 3.4 | 7 | 0 | 0 | 8 | 58 | 19 +/- 27 | NA | 0. |
| 8.2 1+11.5 | 1+4.5 | 3 | 3.4 | 5 | 0 | 0 | 8 | 58 | 8 +/- 23 | NA | 0. |
| 8.2 1+10.5 | 1+4.5 | 3 | 3.4 | 0 | 0 | 0 | 8 | 58 | -18 +/- 6 | NA | 0. |
| 8.2 1+9.5 | 1+4.5 | 3 | 3.4 | 7 | 0 | 0 | 8 | 58 | 19 +/- 27 | NA | 0. |
| 8.2 1+8.5 | 1+4.5 | 3 | 3.4 | 5 | 0 | 0 | 8 | 58 | 8 +/- 23 | NA | 0. |
| 8.2 1+7.5 | 1+4.5 | 3 | 3.4 | 3 | 0 | 0 | 8 | 58 | -2 +/- 18 | NA | 0. |
| 8.2 1+6.5 | 1+4.5 | 3 | 3.4 | 3 | 0 | 0 | 8 | 58 | -2 +/- 18 | NA | 0. |
| 8.2 1+12.5 | 1+5.5 | 3 | 3.4 | 9 | 0 | 0 | 8 | 58 | 29 +/- 31 | NA | 0. |
| 8.2 1+11.5 | 1+5.5 | 3 | 3.4 | 9 | 0 | 0 | 8 | 58 | 29 +/- 31 | NA | 0. |
| 8.2 1+10.5 | 1+5.5 | 3 | 3.4 | 6 | 0 | 0 | 8 | 58 | 13 +/- 25 | NA | 0. |
| 8.2 1+9.5 | 1+5.5 | 3 | 3.4 | 5 | 0 | 0 | 8 | 58 | 8 +/- 23 | NA | 0. |
| 8.2 1+8.5 | 1+5.5 | 3 | 3.4 | 7 | 0 | 0 | 8 | 58 | 19 +/- 27 | NA | 0. |
| 8.2 1+7.5 | 1+5.5 | 3 | 3.4 | 3 | 0 | 0 | 8 | 58 | -2 +/- 18 | NA | 0. |
| 8.2 1+6.5 | 1+5.5 | 3 | 3.4 | 2 | 0 | 0 | 8 | 58 | -7 +/- 15 | NA | 0. |
| 8.2 1+12.5 | 1+6.5 | 3 | 3.4 | 8 | 0 | 0 | 8 | 58 | 24 +/- 29 | NA | 0. |
| 8.2 1+11.5 | 1+6.5 | 3 | 3.4 | 5 | 0 | 0 | 8 | 58 | 8 +/- 23 | NA | 0. |
| 8.2 1+10.5 | 1+6.5 | 3 | 3.4 | 8 | 0 | 0 | 8 | 58 | 24 +/- 29 | NA | 0. |
| 8.2 1+9.5 | 1+6.5 | 3 | 3.4 | 7 | 0 | 0 | 8 | 58 | 19 +/- 27 | NA | 0. |
| 8.2 1+8.5 | 1+6.5 | 3 | 3.4 | 4 | 0 | 0 | 8 | 58 | 3 +/- 21 | NA | 0. |
| 8.2 1+7.5 | 1+6.5 | 3 | 3.4 | 10 | 0 | 0 | 8 | 58 | 34 +/- 33 | NA | 0. |
| 8.2 1+6.5 | 1+6.5 | 3 | 3.4 | 3 | 0 | 0 | 8 | 58 | -2 +/- 18 | NA | 0. |
| 8.2 1+13.5 | 1+7.5 | 4 | 1.4 | 2 | 0 | 0 | 8 | 41 | 3 +/- 14 | NA | 0.2 |
| 8.2 1+12.5 | 1+7.5 | 4 | 1.4 | 4 | 0 | 0 | 8 | 41 | 13 +/- 20 | NA | 0.2 |
| 8.2 1+11.5 | 1+7.5 | 4 | 1.4 | 4 | 0 | 0 | 8 | 41 | 13 +/- 20 | NA | 0.2 |
| 8.2 1+10.5 | 1+7.5 | 4 | 1.4 | 3 | 0 | 0 | 8 | 41 | 8 +/- 17 | NA | 0.2 |
| 8.2 1+9.5 | 1+7.5 | 4 | 1.4 | 3 | 0 | 0 | 8 | 41 | 8 +/- 17 | NA | 0.2 |
| 8.2 1+8.5 | 1+7.5 | 4 | 1.4 | 4 | 0 | 0 | 8 | 41 | 13 +/- 20 | NA | 0.2 |
| 8.2 1+7.5 | 1+7.5 | 4 | 1.4 | 0 | 0 | 0 | 8 | 41 | -7 +/- 4 | NA | 0.2 |
| 8.2 1+6.5 | 1+7.5 | 4 | 1.4 | 5 | 0 | 0 | 8 | 41 | 18 +/- 22 | NA | 0.2 |
| 8.2 1+13.5 | 1+8.5 | 4 | 1.4 | 10 | 0 | 0 | 8 | 41 | 43 +/- 31 | NA | 0.2 |
| 8.2 1+12.5 | 1+8.5 | 4 | 1.4 | 7 | 0 | 0 | 8 | 41 | 28 +/- 26 | NA | 0.2 |
| 8.2 1+11.5 | 1+8.5 | 4 | 1.4 | 4 | 0 | 0 | 8 | 41 | 13 +/- 20 | NA | 0.2 |
| 8.2 1+10.5 | 1+8.5 | 4 | 1.4 | 2 | 0 | 0 | 8 | 41 | 3 +/- 14 | NA | 0.2 |
| 8.2 1+9.5 | 1+8.5 | 4 | 1.4 | 1 | 0 | 0 | 8 | 41 | -2 +/- 10 | NA | 0.2 |
| 8.2 1+8.5 | 1+8.5 | 4 | 1.4 | 1 | 0 | 0 | 8 | 41 | -2 +/- 10 | NA | 0.2 |
| 8.2 1+7.5 | 1+8.5 | 4 | 1.4 | 2 | 0 | 0 | 8 | 41 | 3 +/- 14 | NA | 0.2 |
| 8.2 1+13.5 | 1+9.5 | 4 | 1.4 | 1 | 0 | 0 | 8 | 41 | -2 +/- 10 | NA | 0.2 |
| 8.2 1+12.5 | 1+9.5 | 4 | 1.4 | 7 | 0 | 0 | 8 | 41 | 28 +/- 26 | NA | 0.2 |
| 8.2 1+11.5 | 1+9.5 | 4 | 1.4 | 4 | 0 | 0 | 8 | 41 | 13 +/- 20 | NA | 0.2 |
| 8.2 1+10.5 | 1+9.5 | 4 | 1.4 | 0 | 0 | 0 | 8 | 41 | -7 +/- 4 | NA | 0.2 |
| 8.2 1+9.5 | 1+9.5 | 4 | 1.4 | 2 | 0 | 0 | 8 | 41 | 3 +/- 14 | NA | 0.2 |
| 8.2 1+8.5 | 1+9.5 | 4 | 1.4 | 3 | 0 | 0 | 8 | 41 | 8 +/- 17 | NA | 0.2 |
| 8.2 1+7.5 | 1+9.5 | 4 | 1.4 | 3 | 0 | 0 | 8 | 41 | 8 +/- 17 | NA | 0.2 |
| 8.2 1+13.5 | 1+10.5 | 4 | 1.4 | 4 | 0 | 0 | 8 | 41 | 13 +/- 20 | NA | 0.2 |
| 8.2 1+12.5 | 1+10.5 | 4 | 1.4 | 5 | 0 | 0 | 8 | 41 | 18 +/- 22 | NA | 0.2 |
| 8.2 1+11.5 | 1+10.5 | 4 | 1.4 | 3 | 0 | 0 | 8 | 41 | 8 +/- 17 | NA | 0.2 |
| 8.2 1+10.5 | 1+10.5 | 4 | 1.4 | 1 | 0 | 0 | 8 | 41 | -2 +/- 10 | NA | 0.2 |
| 8.2 1+9.5 | 1+10.5 | 4 | 1.4 | 2 | 0 | 0 | 8 | 41 | 3 +/- 14 | NA | 0.2 |
| 8.2 1+8.5 | 1+10.5 | 4 | 1.4 | 5 | 0 | 0 | 8 | 41 | 18 +/- 22 | NA | 0.2 |
| 8.2 1+7.5 | 1+10.5 | 4 | 1.4 | 2 | 0 | 0 | 8 | 41 | 3 +/- 14 | NA | 0.2 |
| 8.2 1+14.5 | 1+11.5 | 4 | 1.4 | 1 | 0 | 0 | 8 | 41 | -2 +/- 10 | NA | 0.2 |

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TABLE 8.2-3

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|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 | 1+16.5 | 1+19.5 | 4 | 1.7 | 1 | 0 | 0 | B | 44 | -3 +/- 11 | NA | 0. |
| 8.2 | 1+15.5 | 1+19.5 | 4 | 1.7 | 9 | 0 | 0 | B | 44 | 36 +/- 29 | NA | 0. |
| 8.2 | 1+14.5 | 1+19.5 | 4 | 1.7 | 1 | 0 | 0 | B | 44 | -3 +/- 11 | NA | 0. |
| 8.2 | 1+13.5 | 1+19.5 | 4 | 1.7 | 0 | 0 | 0 | B | 44 | -8 +/- 4 | NA | 0. |
| 8.2 | 1+12.5 | 1+19.5 | 4 | 1.7 | 8 | 0 | 0 | B | 44 | 31 +/- 28 | NA | 0. |
| 8.2 | 1+11.5 | 1+19.5 | 4 | 1.7 | 3 | 0 | 0 | B | 44 | 6 +/- 17 | NA | 0. |
| 8.2 | 1+10.5 | 1+19.5 | 4 | 1.7 | 4 | 0 | 0 | B | 44 | 11 +/- 20 | NA | 0. |
| 8.2 | 1+9.5 | 1+19.5 | 4 | 1.7 | 5 | 0 | 0 | B | 44 | 16 +/- 22 | NA | 0. |
| 8.2 | 1+19.5 | 1+20.5 | 3 | 1.9 | 6 | 0 | 0 | B | 47 | 21 +/- 25 | NA | 0. |
| 8.2 | 1+18.5 | 1+20.5 | 3 | 1.9 | 5 | 0 | 0 | B | 47 | 16 +/- 23 | NA | 0. |
| 8.2 | 1+17.5 | 1+20.5 | 3 | 1.9 | 3 | 0 | 0 | B | 47 | 6 +/- 18 | NA | 0. |
| 8.2 | 1+16.5 | 1+20.5 | 3 | 1.9 | 3 | 0 | 0 | B | 47 | 6 +/- 18 | NA | 0. |
| 8.2 | 1+15.5 | 1+20.5 | 3 | 1.9 | 3 | 0 | 0 | B | 47 | 6 +/- 18 | NA | 0. |
| 8.2 | 1+14.5 | 1+20.5 | 3 | 1.9 | 3 | 0 | 0 | B | 47 | 6 +/- 18 | NA | 0. |
| 8.2 | 1+13.5 | 1+20.5 | 3 | 1.9 | 6 | 0 | 0 | B | 47 | 21 +/- 25 | NA | 0. |
| 8.2 | 1+19.5 | 1+21.5 | 3 | 1.9 | 4 | 0 | 0 | B | 47 | 11 +/- 21 | NA | 0. |
| 8.2 | 1+18.5 | 1+21.5 | 3 | 1.9 | 0 | 0 | 0 | B | 47 | -10 +/- 4 | NA | 0. |
| 8.2 | 1+17.5 | 1+20.5 | 3 | 1.9 | 1 | 0 | 0 | B | 47 | -5 +/- 11 | NA | 0. |
| 8.2 | 1+16.5 | 1+20.5 | 3 | 1.9 | 5 | 0 | 0 | B | 47 | 16 +/- 23 | NA | 0. |
| 8.2 | 1+15.5 | 1+21.5 | 3 | 1.9 | 4 | 0 | 0 | B | 47 | 11 +/- 21 | NA | 0. |
| 8.2 | 1+14.5 | 1+21.5 | 3 | 1.9 | 1 | 0 | 0 | B | 47 | -5 +/- 11 | NA | 0. |
| 8.2 | 1+13.5 | 1+21.5 | 3 | 1.9 | 5 | 0 | 0 | B | 47 | 16 +/- 23 | NA | 0. |
| 8.2 | 1+20.5 | 1+22.5 | 3 | 1.9 | 3 | 0 | 0 | B | 47 | 6 +/- 18 | NA | 0. |
| 8.2 | 1+19.5 | 1+22.5 | 3 | 1.9 | 1 | 0 | 0 | B | 47 | -5 +/- 11 | NA | 0. |
| 8.2 | 1+18.5 | 1+22.5 | 3 | 1.9 | 2 | 0 | 0 | B | 47 | 1 +/- 15 | NA | 0. |
| 8.2 | 1+17.5 | 1+22.5 | 3 | 1.9 | 2 | 0 | 0 | B | 47 | 1 +/- 15 | NA | 0. |
| 8.2 | 1+16.5 | 1+22.5 | 3 | 1.9 | 3 | 0 | 0 | B | 47 | 6 +/- 18 | NA | 0. |
| 8.2 | 1+15.5 | 1+22.5 | 3 | 1.9 | 2 | 0 | 0 | B | 47 | 1 +/- 15 | NA | 0. |
| 8.2 | 1+14.5 | 1+22.5 | 3 | 1.9 | 3 | 0 | 0 | B | 47 | 6 +/- 18 | NA | 0. |
| 8.2 | 1+13.5 | 1+22.5 | 3 | 1.9 | 6 | 0 | 0 | B | 47 | 21 +/- 25 | NA | 0. |
| 8.2 | 1+20.5 | 1+23.5 | 3 | 1.9 | 4 | 0 | 0 | B | 47 | 11 +/- 21 | NA | 0. |
| 8.2 | 1+19.5 | 1+23.5 | 3 | 1.9 | 7 | 0 | 0 | B | 47 | 26 +/- 27 | NA | 0. |
| 8.2 | 1+18.5 | 1+23.5 | 3 | 1.9 | 1 | 0 | 0 | B | 47 | -5 +/- 11 | NA | 0. |
| 8.2 | 1+17.5 | 1+23.5 | 3 | 1.9 | 2 | 0 | 0 | B | 47 | 1 +/- 15 | NA | 0. |
| 8.2 | 1+16.5 | 1+23.5 | 3 | 1.9 | 4 | 8 | 500 | B | 47 | 12 +/- 21 | 31 | 0. |
| 8.2 | 1+15.5 | 1+23.5 | 3 | 1.9 | 8 | 5 | 300 | B | 47 | 31 +/- 29 | 16 | 0. |
| 8.2 | 1+14.5 | 1+23.5 | 3 | 1.9 | 6 | 0 | 0 | B | 47 | 21 +/- 25 | NA | 0. |
| 8.2 | 1+13.5 | 1+23.5 | 3 | 1.9 | 1 | 0 | 0 | B | 47 | -5 +/- 11 | NA | 0. |
| 8.2 | 1+20.5 | 1+24.5 | 3 | 1.9 | 1 | 0 | 0 | B | 47 | -5 +/- 11 | NA | 0. |
| 8.2 | 1+19.5 | 1+24.5 | 3 | 1.9 | 1 | 0 | 0 | B | 47 | -5 +/- 11 | NA | 0. |
| 8.2 | 1+18.5 | 1+24.5 | 3 | 1.9 | 2 | 0 | 0 | B | 47 | 1 +/- 15 | NA | 0. |
| 8.2 | 1+17.5 | 1+24.5 | 3 | 1.9 | 4 | 0 | 0 | B | 47 | 11 +/- 21 | NA | 0. |
| 8.2 | 1+16.5 | 1+24.5 | 3 | 1.9 | 7 | 0 | 0 | B | 47 | 26 +/- 27 | NA | 0. |
| 8.2 | 1+15.5 | 1+24.5 | 3 | 1.9 | 0 | 0 | 0 | B | 47 | -10 +/- 4 | NA | 0. |
| 8.2 | 1+14.5 | 1+24.5 | 3 | 1.9 | 2 | 0 | 0 | B | 47 | 1 +/- 15 | NA | 0. |
| 8.2 | 1+13.5 | 1+24.5 | 3 | 1.9 | 3 | 0 | 0 | B | 47 | 6 +/- 18 | NA | 0. |
| 8.2 | 1+20.5 | 1+25.5 | 3 | 1.9 | 1 | 0 | 0 | B | 47 | -5 +/- 11 | NA | 0. |
| 8.2 | 1+19.5 | 1+25.5 | 3 | 1.9 | 2 | 0 | 0 | B | 47 | 1 +/- 15 | NA | 0. |
| 8.2 | 1+18.5 | 1+25.5 | 3 | 1.9 | 1 | 0 | 0 | B | 47 | -5 +/- 11 | NA | 0. |
| 8.2 | 1+17.5 | 1+25.5 | 3 | 1.9 | 2 | 0 | 0 | B | 47 | 1 +/- 15 | NA | 0. |
| 8.2 | 1+16.5 | 1+25.5 | 3 | 1.9 | 6 | 0 | 0 | B | 47 | 21 +/- 25 | NA | 0. |
| 8.2 | 1+15.5 | 1+25.5 | 3 | 1.9 | 4 | 0 | 0 | B | 47 | 11 +/- 21 | NA | 0. |
| 8.2 | 1+14.5 | 1+25.5 | 3 | 1.9 | 3 | 0 | 0 | B | 47 | 6 +/- 18 | NA | 0. |
| 8.2 | 1+21.5 | 1+26.5 | 6 | 0.5 | 1 | 0 | 0 | B | 33 | 3 +/- 11 | NA | 0. |
| 8.2 | 1+20.5 | 1+26.5 | 6 | 0.5 | 0 | 0 | 0 | B | 33 | -3 +/- 2 | NA | 0. |
| 8.2 | 1+19.5 | 1+26.5 | 6 | 0.5 | 4 | 0 | 0 | B | 33 | 19 +/- 22 | NA | 0. |
| 8.2 | 1+18.5 | 1+26.5 | 6 | 0.5 | 2 | 0 | 0 | B | 33 | 8 +/- 16 | NA | 0. |
| 8.2 | 1+17.5 | 1+26.5 | 6 | 0.5 | 2 | 0 | 0 | B | 33 | 8 +/- 16 | NA | 0. |
| 8.2 | 1+16.5 | 1+26.5 | 6 | 0.5 | 0 | 0 | 0 | B | 33 | -3 +/- 2 | NA | 0. |
| 8.2 | 1+15.5 | 1+26.5 | 6 | 0.5 | 3 | 0 | 0 | B | 33 | 14 +/- 19 | NA | 0. |

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TABLE 8.2-3

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|---|---|---|---|---|---|---|---|---|---|---|---|
| 8.2 1+13.5 | 1+11.5 | 4 | 1.4 | 5 | 0 | 0 | 8 | 41 | 18 +/- 22 | NA | 0. |
| 8.2 1+12.5 | 1+11.5 | 4 | 1.4 | 1 | 0 | 0 | 8 | 41 | -2 +/- 10 | NA | 0. |
| 8.2 1+11.5 | 1+11.5 | 4 | 1.4 | 5 | 0 | 0 | 8 | 41 | 18 +/- 22 | NA | 0. |
| 8.2 1+10.5 | 1+11.5 | 4 | 1.4 | 2 | 0 | 0 | 8 | 41 | 3 +/- 14 | NA | 0. |
| 8.2 1+9.5 | 1+11.5 | 4 | 1.4 | 3 | 0 | 0 | 8 | 41 | 8 +/- 17 | NA | 0. |
| 8.2 1+8.5 | 1+11.5 | 4 | 1.4 | 3 | 0 | 0 | 8 | 41 | 8 +/- 17 | NA | 0. |
| 8.2 1+7.5 | 1+11.5 | 2 | 0.4 | 4 | 0 | 0 | 8 | 29 | 18 +/- 20 | NA | 0. |
| 8.2 1+14.5 | 1+12.5 | 2 | 0.4 | 0 | 0 | 0 | 8 | 29 | -2 +/- 2 | NA | 0. |
| 8.2 1+13.5 | 1+12.5 | 2 | 0.4 | 2 | 0 | 0 | 8 | 29 | 8 +/- 14 | NA | 0. |
| 8.2 1+12.5 | 1+12.5 | 2 | 0.4 | 0 | 0 | 0 | 8 | 29 | -2 +/- 2 | NA | 0. |
| 8.2 1+11.5 | 1+12.5 | 2 | 0.4 | 2 | 0 | 0 | 8 | 29 | 8 +/- 14 | NA | 0. |
| 8.2 1+10.5 | 1+12.5 | 2 | 0.4 | 1 | 0 | 0 | 8 | 29 | 3 +/- 10 | NA | 0. |
| 8.2 1+9.5 | 1+12.5 | 2 | 1.2 | 2 | 0 | 0 | 8 | 40 | 4 +/- 15 | NA | 0. |
| 8.2 1+8.5 | 1+12.5 | 2 | 0.4 | 0 | 0 | 0 | 8 | 29 | -2 +/- 2 | NA | 0. |
| 8.2 1+15.5 | 1+13.5 | 2 | 0.4 | 1 | 0 | 0 | 8 | 29 | 3 +/- 10 | NA | 0. |
| 8.2 1+14.5 | 1+13.5 | 2 | 0.4 | 1 | 0 | 0 | 8 | 29 | 3 +/- 10 | NA | 0. |
| 8.2 1+13.5 | 1+13.5 | 2 | 0.4 | 1 | 0 | 0 | 8 | 29 | 3 +/- 10 | NA | 0. |
| 8.2 1+12.5 | 1+13.5 | 2 | 0.4 | 3 | 0 | 0 | 8 | 29 | 13 +/- 17 | NA | 0. |
| 8.2 1+11.5 | 1+13.5 | 2 | 0.4 | 1 | 0 | 0 | 8 | 29 | 3 +/- 10 | NA | 0. |
| 8.2 1+10.5 | 1+13.5 | 2 | 0.4 | 3 | 0 | 0 | 8 | 29 | 13 +/- 17 | NA | 0. |
| 8.2 1+9.5 | 1+13.5 | 2 | 0.4 | 1 | 0 | 0 | 8 | 29 | 3 +/- 10 | NA | 0. |
| 8.2 1+8.5 | 1+13.5 | 2 | 0.4 | 0 | 0 | 0 | 8 | 29 | -2 +/- 2 | NA | 0. |
| 8.2 1+15.5 | 1+14.5 | 2 | 0.4 | 3 | 0 | 0 | 8 | 29 | 13 +/- 17 | NA | 0. |
| 8.2 1+14.5 | 1+14.5 | 2 | 0.4 | 1 | 0 | 0 | 8 | 29 | 3 +/- 10 | NA | 0. |
| 8.2 1+13.5 | 1+14.5 | 2 | 0.4 | 0 | 0 | 0 | 8 | 29 | -2 +/- 2 | NA | 0. |
| 8.2 1+12.5 | 1+14.5 | 2 | 0.4 | 3 | 0 | 0 | 8 | 29 | 13 +/- 17 | NA | 0. |
| 8.2 1+11.5 | 1+14.5 | 2 | 0.4 | 5 | 0 | 0 | 8 | 29 | 24 +/- 23 | NA | 0. |
| 8.2 1+10.5 | 1+14.5 | 2 | 0.4 | 0 | 0 | 0 | 8 | 29 | -2 +/- 2 | NA | 0. |
| 8.2 1+9.5 | 1+14.5 | 2 | 0.4 | 0 | 0 | 0 | 8 | 29 | -2 +/- 2 | NA | 0. |
| 8.2 1+8.5 | 1+14.5 | 2 | 0.4 | 0 | 0 | 0 | 8 | 29 | -2 +/- 2 | NA | 0. |
| 8.2 1+15.5 | 1+15.5 | 2 | 0.4 | 5 | 0 | 0 | 8 | 29 | 24 +/- 23 | NA | 0. |
| 8.2 1+14.5 | 1+15.5 | 2 | 0.4 | 4 | 0 | 0 | 8 | 29 | 18 +/- 20 | NA | 0. |
| 8.2 1+13.5 | 1+15.5 | 2 | 0.4 | 0 | 0 | 0 | 8 | 29 | -2 +/- 2 | NA | 0. |
| 8.2 1+12.5 | 1+15.5 | 2 | 0.4 | 1 | 0 | 0 | 8 | 29 | 3 +/- 10 | NA | 0. |
| 8.2 1+11.5 | 1+15.5 | 2 | 0.4 | 1 | 0 | 0 | 8 | 29 | 3 +/- 10 | NA | 0. |
| 8.2 1+10.5 | 1+15.5 | 2 | 0.4 | 3 | 0 | 0 | 8 | 29 | 13 +/- 17 | NA | 0. |
| 8.2 1+9.5 | 1+15.5 | 2 | 0.4 | 2 | 0 | 0 | 8 | 29 | 8 +/- 14 | NA | 0. |
| 8.2 1+15.5 | 1+16.5 | 2 | 0.4 | 1 | 0 | 0 | 8 | 29 | 3 +/- 10 | NA | 0. |
| 8.2 1+14.5 | 1+16.5 | 2 | 0.4 | 5 | 0 | 0 | 8 | 29 | 24 +/- 23 | NA | 0. |
| 8.2 1+13.5 | 1+16.5 | 2 | 0.4 | 1 | 0 | 0 | 8 | 29 | 3 +/- 10 | NA | 0. |
| 8.2 1+12.5 | 1+16.5 | 2 | 0.4 | 3 | 0 | 0 | 8 | 29 | 13 +/- 17 | NA | 0. |
| 8.2 1+11.5 | 1+16.5 | 2 | 0.4 | 2 | 0 | 0 | 8 | 29 | 8 +/- 14 | NA | 0. |
| 8.2 1+10.5 | 1+16.5 | 4 | 1.7 | 3 | 0 | 0 | 8 | 44 | 6 +/- 17 | NA | 0. |
| 8.2 1+9.5 | 1+16.5 | 4 | 1.7 | 4 | 0 | 0 | 8 | 44 | 11 +/- 20 | NA | 0. |
| 8.2 1+8.5 | 1+16.5 | 4 | 1.7 | 0 | 0 | 0 | 8 | 44 | -8 +/- 4 | NA | 0. |
| 8.2 1+15.5 | 1+17.5 | 4 | 1.7 | 3 | 0 | 0 | 8 | 44 | 6 +/- 17 | NA | 0. |
| 8.2 1+14.5 | 1+17.5 | 4 | 1.7 | 4 | 0 | 0 | 8 | 44 | 11 +/- 20 | NA | 0. |
| 8.2 1+13.5 | 1+17.5 | 4 | 1.7 | 4 | 0 | 0 | 8 | 44 | 11 +/- 20 | NA | 0. |
| 8.2 1+12.5 | 1+17.5 | 4 | 1.7 | 2 | 0 | 0 | 8 | 44 | 1 +/- 14 | NA | 0. |
| 8.2 1+11.5 | 1+17.5 | 4 | 1.7 | 2 | 0 | 0 | 8 | 44 | 1 +/- 14 | NA | 0. |
| 8.2 1+10.5 | 1+17.5 | 4 | 1.7 | 3 | 0 | 0 | 8 | 44 | 6 +/- 17 | NA | 0. |
| 8.2 1+9.5 | 1+17.5 | 4 | 1.7 | 3 | 0 | 0 | 8 | 44 | 6 +/- 17 | NA | 0. |
| 8.2 1+16.5 | 1+18.5 | 4 | 1.7 | 4 | 0 | 0 | 8 | 44 | 11 +/- 20 | NA | 0. |
| 8.2 1+15.5 | 1+18.5 | 4 | 1.7 | 4 | 0 | 0 | 8 | 44 | 11 +/- 20 | NA | 0. |
| 8.2 1+14.5 | 1+18.5 | 4 | 1.7 | 1 | 0 | 0 | 8 | 44 | -3 +/- 11 | NA | 0. |
| 8.2 1+13.5 | 1+18.5 | 4 | 1.7 | 1 | 0 | 0 | 8 | 44 | -3 +/- 11 | NA | 0. |
| 8.2 1+12.5 | 1+18.5 | 4 | 1.7 | 2 | 0 | 0 | 8 | 44 | 1 +/- 14 | NA | 0. |
| 8.2 1+11.5 | 1+18.5 | 4 | 1.7 | 6 | 0 | 0 | 8 | 44 | 21 +/- 24 | NA | 0. |
| 8.2 1+10.5 | 1+18.5 | 4 | 1.7 | 6 | 0 | 0 | 8 | 44 | 21 +/- 24 | NA | 0. |
| 8.2 1+9.5 | 1+18.5 | 4 | 1.7 | 0 | 0 | 0 | 8 | 44 | -8 +/- 4 | NA | 0. |

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TABLE B.2-3

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|---|---|---|---|---|---|---|---|---|---|---|---|---|
| B.2 1+14.5 | 1+26.5 | 6 | 0.5 | 5 | 0 | 0 | 8 | 33 | 25 +/- 24 | NA | | 0. |
| B.2 1+21.5 | 1+27.5 | 6 | 0.5 | 6 | 0 | 0 | 8 | 33 | 31 +/- 27 | NA | | 0. |
| B.2 1+20.5 | 1+27.5 | 6 | 0.5 | 2 | 0 | 0 | 8 | 33 | 8 +/- 16 | NA | | 0. |
| B.2 1+19.5 | 1+27.5 | 6 | 0.5 | 3 | 0 | 0 | 8 | 33 | 14 +/- 19 | NA | | 0. |
| B.2 1+18.5 | 1+27.5 | 6 | 0.5 | 2 | 0 | 0 | 8 | 33 | 8 +/- 16 | NA | | 0. |
| B.2 1+17.5 | 1+27.5 | 6 | 0.5 | 2 | 0 | 0 | 8 | 33 | 8 +/- 16 | NA | | 0. |
| B.2 1+16.5 | 1+27.5 | 6 | 0.5 | 1 | 0 | 0 | 8 | 33 | 3 +/- 11 | NA | | 0. |
| B.2 1+15.5 | 1+27.5 | 6 | 0.5 | 1 | 0 | 0 | 8 | 33 | 3 +/- 11 | NA | | 0. |
| B.2 1+14.5 | 1+27.5 | 6 | 0.5 | 8 | 0 | 0 | 8 | 33 | 42 +/- 31 | NA | | 0. |
| B.2 1+21.5 | 1+18.5 | 6 | 0.5 | 3 | 0 | 0 | 8 | 33 | 14 +/- 19 | NA | | 0. |
| B.2 1+20.5 | 1+28.5 | 6 | 0.5 | 1 | 0 | 0 | 8 | 33 | 3 +/- 11 | NA | | 0. |
| B.2 1+19.5 | 1+28.5 | 6 | 0.5 | 2 | 0 | 0 | 8 | 33 | 8 +/- 16 | NA | | 0. |
| B.2 1+18.5 | 1+28.5 | 6 | 0.5 | 1 | 0 | 0 | 8 | 33 | 3 +/- 11 | NA | | 0. |
| B.2 1+17.5 | 1+28.5 | 6 | 0.5 | 4 | 0 | 0 | 8 | 33 | 19 +/- 22 | NA | | 0. |
| B.2 1+16.5 | 1+28.5 | 6 | 0.5 | 6 | 0 | 0 | 8 | 33 | 31 +/- 27 | NA | | 0. |
| B.2 1+15.5 | 1+28.5 | 6 | 0.5 | 2 | 0 | 0 | 8 | 33 | 8 +/- 16 | NA | | 0. |
| B.2 1+14.5 | 1+28.5 | 6 | 0.5 | 9 | 0 | 0 | 8 | 33 | 47 +/- 33 | NA | | 0. |
| B.2 1+21.5 | 1+29.5 | 6 | 0.5 | 0 | 0 | 0 | 8 | 33 | -3 +/- 2 | NA | | 0. |
| B.2 1+20.5 | 1+29.5 | 6 | 0.5 | 2 | 0 | 0 | 8 | 33 | 8 +/- 16 | NA | | 0. |
| B.2 1+19.5 | 1+29.5 | 6 | 0.5 | 3 | 0 | 0 | 8 | 33 | 14 +/- 19 | NA | | 0. |
| B.2 1+18.5 | 1+29.5 | 6 | 0.5 | 3 | 0 | 0 | 8 | 33 | 14 +/- 19 | NA | | 0. |
| B.2 1+17.5 | 1+29.5 | 6 | 0.5 | 0 | 0 | 0 | 8 | 33 | -3 +/- 2 | NA | | 0. |
| B.2 1+16.5 | 1+29.5 | 6 | 0.5 | 1 | 0 | 0 | 8 | 33 | 3 +/- 11 | NA | | 0. |
| B.2 1+15.5 | 1+29.5 | 6 | 0.5 | 3 | 0 | 0 | 8 | 33 | 14 +/- 19 | NA | | 0. |
| B.2 1+15.5 | 1+30.5 | 1 | 1.3 | 3 | 0 | 0 | 8 | 42 | 9 +/- 18 | NA | | 0. |
| B.2 1+16.5 | 1+30.5 | 1 | 1.3 | 2 | 0 | 0 | 8 | 42 | 4 +/- 15 | NA | | 0. |
| B.2 1+17.5 | 1+30.5 | 1 | 1.3 | 1 | 0 | 0 | 8 | 42 | -2 +/- 11 | NA | | 0. |
| B.2 1+18.5 | 1+30.5 | 1 | 1.3 | 2 | 3 | 351 | 8 | 42 | 4 +/- 15 | | 9 | 0. |
| B.2 1+19.5 | 1+30.5 | 1 | 1.3 | 2 | 0 | 0 | 8 | 42 | 4 +/- 15 | NA | | 0. |
| B.2 1+20.5 | 1+30.5 | 1 | 1.3 | 0 | 0 | 0 | 8 | 42 | -7 +/- 4 | NA | | 0. |
| B.2 1+21.5 | 1+30.5 | 1 | 1.3 | 2 | 0 | 0 | 8 | 42 | 4 +/- 15 | NA | | 0. |
| B.2 1+15.5 | 1+31.5 | 1 | 1.3 | 9 | 0 | 0 | 8 | 42 | 41 +/- 31 | NA | | 0. |
| B.2 1+16.5 | 1+31.5 | 1 | 1.3 | 4 | 3 | 950 | 8 | 42 | 14 +/- 21 | | 9 | 0. |
| B.2 1+17.5 | 1+31.5 | 1 | 1.3 | 3 | 4 | 1444 | 8 | 42 | 10 +/- 18 | | 14 | 0. |
| B.2 1+18.5 | 1+31.5 | 1 | 1.3 | 1 | 6 | 1170 | 8 | 42 | 2 +/- 11 | | 25 | 0. |
| B.2 1+19.5 | 1+31.5 | 1 | 1.3 | 3 | 0 | 0 | 8 | 42 | 9 +/- 18 | NA | | 0. |
| B.2 1+20.5 | 1+31.5 | 1 | 1.3 | 3 | 0 | 0 | 8 | 42 | 9 +/- 18 | NA | | 0. |
| B.2 1+21.5 | 1+31.5 | 1 | 1.3 | 2 | 0 | 0 | 8 | 42 | 4 +/- 15 | NA | | 0. |
| B.2 1+22.5 | 1+31.5 | 1 | 1.3 | 3 | 0 | 0 | 8 | 42 | 9 +/- 18 | NA | | 0. |
| B.2 1+15.5 | 1+32.5 | 1 | 1.3 | 3 | 0 | 0 | 8 | 42 | 9 +/- 18 | NA | | 0. |
| B.2 1+16.5 | 1+32.5 | 1 | 1.3 | 2 | 0 | 0 | 8 | 42 | 4 +/- 15 | NA | | 0. |
| B.2 1+17.5 | 1+32.5 | 1 | 1.3 | 4 | 0 | 0 | 8 | 42 | 14 +/- 21 | NA | | 0. |
| B.2 1+18.5 | 1+32.5 | 1 | 1.3 | 4 | 0 | 0 | 8 | 42 | 14 +/- 21 | NA | | 0. |
| B.2 1+19.5 | 1+32.5 | 1 | 1.3 | 2 | 0 | 0 | 8 | 42 | 4 +/- 15 | NA | | 0. |
| B.2 1+20.5 | 1+32.5 | 1 | 1.3 | 2 | 0 | 0 | 8 | 42 | 4 +/- 15 | NA | | 0. |
| B.2 1+21.5 | 1+32.5 | 1 | 1.3 | 2 | 0 | 0 | 8 | 42 | 4 +/- 15 | NA | | 0. |
| B.2 1+22.5 | 1+32.5 | 1 | 1.3 | 3 | 9 | 500 | 8 | 42 | 11 +/- 18 | | 41 | 0. |
| B.2 1+16.5 | 1+33.5 | 1 | 1.3 | 4 | 0 | 0 | 8 | 42 | 14 +/- 21 | NA | | 0. |
| B.2 1+17.5 | 1+33.5 | 1 | 1.3 | 6 | 0 | 0 | 8 | 42 | 25 +/- 26 | NA | | 0. |
| B.2 1+18.5 | 1+33.5 | 1 | 1.3 | 1 | 0 | 0 | 8 | 42 | -2 +/- 11 | NA | | 0. |
| B.2 1+19.5 | 1+33.5 | 1 | 1.3 | 3 | 0 | 0 | 8 | 42 | 9 +/- 18 | NA | | 0. |
| B.2 1+20.5 | 1+33.5 | 1 | 1.3 | 3 | 0 | 0 | 8 | 42 | 9 +/- 18 | NA | | 0. |

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ANSTEC
APERTURE
CARD

Also Available on
Aperture Card

TABLE B.2-4

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:12 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 8.2 - GROUNDS SOUTH OF REACTOR DRIVEWAY SOIL FOR SUM OF THE FRACTIONS

RADIATION TYPE: SOIL DATA FOR SUM OF THE FRACTIONS
COMPLETION DATE: 10/12/ - 10/20/94
TECHNICIANS: TA/JB/CD/PK/DR/PS
LOCATION: 8.0
GRID ID: 8.2
MEDIA TYPE: SOIL
# of POINTS: 8

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 0.32 | PASS | 1 |
| AVG | 0.22 | PASS | 1 |
| STD X | 0.05 | | |
| MU SUB ALPHA | 0.25 | PASS | 1 |

ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED) ISOTOPES OF C

| ID # | GRID COORDINATES OR OTHER ID | | SR-90 | CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SOIL CODE | SR-90 | C |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | S | W | LIMIT 17 | LIMIT 0.9 | LIMIT 1.1 | LIMIT 1.8 | LIMIT 3.5 | LIMIT 63 | LIMIT 2 | | | |
| 8.2 | 0+42.5 | 0+92.5 | < 0.201 | < 0.037 | < 0.042 | < 0.060 | 0.183 | < 0.290 | < 0.097 | 1 | < 0.011824 | < |
| 8.2 | 1+32.5 | 1+22.5 | < 0.176 | < 0.059 | < 0.031 | < 0.083 | 0.213 | < 0.359 | < 0.095 | 1 | < 0.010353 | < |
| 8.2 | 1+23.5 | 1+15.5 | 0.139 | < 0.056 | < 0.047 | < 0.066 | 0.189 | < 0.405 | < 0.115 | 1 | 0.008176 | < |
| 8.2 | 1+31.5 | 1+16.5 | 0.091 | < 0.063 | < 0.025 | < 0.057 | < 0.117 | < 0.269 | < 0.201 | 1 | 0.005371 | < |
| 8.2 | 0+41.5 | 0+91.5 | < 0.201 | < 0.103 | < 0.044 | < 0.061 | 0.194 | < 0.379 | < 0.091 | 1 | < 0.011824 | < |
| 8.2 | 0+58.5 | 0+98.5 | < 0.190 | 0.211 | < 0.021 | < 0.043 | 0.262 | < 0.152 | < 0.056 | 1 | < 0.011176 | |
| 8.2 | 1+2.5 | 1+12.5 | < * | < 0.049 | < 0.043 | < 0.058 | 0.199 | < 0.242 | < 0.063 | 1 | < 0 | < |
| 8.2 | 1+31.5/1+30.5 | 1+18.5 | < 0.176 | < 0.060 | < 0.039 | < 0.057 | 0.156 | < 0.382 | < 0.163 | 1 | < 0.010353 | < |

* : Sr-90 RESULT NOT GIVEN DUE TO INSUFFICIENT SAMPLE SIZE

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CONCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| O-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| 0.041 < | 0.038 < | 0.033 | 0.000 < | 0.005 < | 0.049 | 0.177 |
| 0.066 < | 0.028 < | 0.046 | 0.000 < | 0.006 < | 0.048 | 0.204 |
| 0.062 < | 0.043 < | 0.037 | 0.000 < | 0.006 < | 0.058 | 0.213 |
| 0.070 < | 0.022 < | 0.031 < | 0.000 < | 0.004 < | 0.101 | 0.234 |
| 0.114 < | 0.040 < | 0.034 | 0.000 < | 0.006 < | 0.045 | 0.252 |
| 0.234 < | 0.019 < | 0.024 | 0.000 < | 0.002 < | 0.028 | 0.319 |
| 0.055 < | 0.039 < | 0.032 | 0.000 < | 0.004 < | 0.032 | 0.161 |
| 0.067 < | 0.036 < | 0.032 | 0.000 < | 0.006 < | 0.082 | 0.232 |

A.R.TABLE 8.3-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95

FINAL SURVEY DATA SHEET

DATA FOR UNAFFECTED AREA DESCRIPTION:

HUT EXCAVATION BEDROCK - AREA 8.3 FOR UREM

RADIATION TYPE: GAMMA SURVEY IN UREM/HR

COMPLETION -

DATE: 11-18-94

TECHNICIANS: JB/PK

LOCATION: 8.0

GRID ID: 8.3

MEDIA TYPE: SOIL/ROCK

# of POINTS: 30

MATERIAL CODE

1=CONCRETE 5=PLASTIC

2=ROCK 6=SOIL

3=WOOD 7=ASPHALT

4=METAL 8=OTHER(SPECIFY):

NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | LIMIT |
|---|---|---|
| MAX | 10.00 PASS | 10 |
| AVG | 3.67 PASS | 5 |
| STD X | 1.90 | |
| MU SUB ALPHA | 4.26 PASS | 5 |

| ID # | INST. ID # | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|
| 8.3 | 1 | A | 6 | 11 | 8 | 5 |
| 8.3 | 2 | A | 6 | 9 | 8 | 3 |
| 8.3 | 3 | A | 6 | 11 | 8 | 5 |
| 8.3 | 4 | A | 6 | 7 | 8 | 1 |
| 8.3 | 5 | A | 6 | 8 | 8 | 2 |
| 8.3 | 6 | A | 6 | 9 | 8 | 3 |
| 8.3 | 7 | A | 6 | 8 | 8 | 2 |
| 8.3 | 8 | A | 6 | 9 | 8 | 3 |
| 8.3 | 9 | A | 6 | 8 | 8 | 2 |
| 8.3 | 10 | A | 6 | 10 | 8 | 4 |
| 8.3 | 11 | A | 6 | 10 | 8 | 4 |
| 8.3 | 12 | A | 6 | 12 | 8 | 6 |
| 8.3 | 13 | A | 6 | 8 | 8 | 2 |
| 8.3 | 14 | A | 6 | 11 | 8 | 5 |
| 8.3 | 15 | A | 6 | 12 | 8 | 6 |
| 8.3 | 16 | A | 6 | 10 | 8 | 4 |
| 8.3 | 17 | A | 6 | 9 | 8 | 3 |
| 8.3 | 18 | A | 6 | 9 | 8 | 3 |
| 8.3 | 19 | A | 6 | 12 | 8 | 6 |
| 8.3 | 20 | A | 6 | 10 | 8 | 4 |
| 8.3 | 21 | A | 6 | 9 | 8 | 3 |
| 8.3 | 22 | A | 6 | 8 | 8 | 2 |
| 8.3 | 23 | A | 6 | 16 | 8 | 10 |
| 8.3 | 24 | A | 6 | 8 | 8 | 2 |
| 8.3 | 25 | A | 6 | 8 | 8 | 2 |
| 8.3 | 26 | A | 6 | 7 | 8 | 1 |
| 8.3 | 27 | A | 6 | 10 | 8 | 4 |
| 8.3 | 28 | A | 6 | 12 | 8 | 6 |
| 8.3 | 29 | A | 6 | 10 | 8 | 4 |
| 8.3 | 30 | A | 6 | 9 | 8 | 3 |

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TABLE 8.3-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:12 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 8.3 - HUT EXCAVATION BEDROCK ABOVE HUT ROOF SOIL FOR SUM OF THE FRACTIONS

RADIATION TYPE: SOIL DATA FOR SUM OF THE FRACTIONS
COMPLETION DATE: 11-18-94
TECHNICIANS: JB/PK
LOCATION: 8.0
GRID ID: 8.3
MEDIA TYPE: SOIL
# of POINTS: 30

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 0.30 | PASS | 1 |
| AVG | 0.20 | PASS | 1 |
| STD X | 0.04 | | |
| MU SUB ALPHA | 0.21 | PASS | 1 |

ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED) ISOTOPES OF

| ID # | GRID COORDINATES OR OTHER ID | SR-90 | CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SOIL CODE | SR-90 |
|---|---|---|---|---|---|---|---|---|---|---|
| | | LIMIT 17 | LIMIT 0.9 | LIMIT 1.1 | LIMIT 1.8 | LIMIT 3.8 | LIMIT 63 | LIMIT 2 | | |
| 8.3 | 1 | < 0.193 | < 0.0407 | < 0.019 | < 0.050 | < 0.059 | < 0.180 | < 0.067 | 1 | < 0.011353 < |
| 8.3 | 2 | < 0.193 | < 0.059 | < 0.028 | < 0.056 | < 0.055 | < 0.313 | < 0.137 | 1 | < 0.011353 < |
| 8.3 | 3 | < 0.193 | < 0.038 | < 0.045 | < 0.047 | < 0.056 | < 0.421 | < 0.151 | 1 | < 0.011353 < |
| 8.3 | 4 | < 0.193 | < 0.020 | < 0.042 | < 0.056 | < 0.118 | < 0.358 | < 0.132 | 1 | < 0.011353 < |
| 8.3 | 5 | < 0.210 | < 0.036 | < 0.039 | < 0.046 | < 0.257 | < 0.340 | < 0.121 | 1 | < 0.012353 < |
| 8.3 | 6 | < 0.210 | < 0.057 | < 0.047 | < 0.047 | < 0.207 | < 0.319 | < 0.081 | 1 | < 0.012353 < |
| 8.3 | 7 | < 0.210 | < 0.097 | < 0.023 | < 0.053 | < 0.081 | < 0.134 | < 0.164 | 1 | < 0.012353 < |
| 8.3 | 8 | < 0.210 | < 0.063 | < 0.037 | < 0.068 | < 0.057 | < 0.374 | < 0.124 | 1 | < 0.012353 < |
| 8.3 | 9 | < 0.210 | < 0.044 | < 0.029 | < 0.058 | < 0.051 | < 0.139 | < 0.098 | 1 | < 0.012353 < |
| 8.3 | 10 | < 0.210 | < 0.036 | < 0.035 | < 0.060 | < 0.070 | < 0.279 | < 0.082 | 1 | < 0.012353 < |
| 8.3 | 11 | < 0.210 | < 0.067 | < 0.065 | < 0.057 | < 0.037 | < 0.287 | < 0.075 | 1 | < 0.012353 < |
| 8.3 | 12 | < 0.204 | < 0.022 | < 0.047 | < 0.046 | < 0.057 | < 0.348 | < 0.060 | 1 | < 0.012 < |
| 8.3 | 13 | < 0.204 | < 0.065 | < 0.045 | < 0.042 | < 0.059 | < 0.174 | < 0.059 | 1 | < 0.012 < |
| 8.3 | 14 | < 0.204 | < 0.060 | < 0.026 | < 0.057 | < 0.084 | < 0.354 | < 0.124 | 1 | < 0.012 < |
| 8.3 | 15 | < 0.204 | < 0.084 | < 0.021 | < 0.058 | < 0.050 | < 0.243 | < 0.176 | 1 | < 0.012 < |
| 8.3 | 16 | < 0.204 | < 0.032 | < 0.086 | < 0.042 | < 0.029 | < 0.137 | < 0.064 | 1 | < 0.012 < |
| 8.3 | 17 | < 0.204 | < 0.068 | < 0.028 | < 0.055 | < 0.091 | < 0.169 | < 0.098 | 1 | < 0.012 < |
| 8.3 | 18 | < 0.204 | < 0.087 | < 0.047 | < 0.052 | < 0.024 | < 0.264 | < 0.069 | 1 | < 0.012 < |
| 8.3 | 19 | < 0.204 | < 0.026 | < 0.057 | < 0.051 | < 0.039 | < 0.399 | < 0.151 | 1 | < 0.012 < |
| 8.3 | 20 | < 0.204 | < 0.033 | < 0.019 | < 0.053 | < 0.075 | < 0.463 | < 0.163 | 1 | < 0.012 < |
| 8.3 | 21 | < 0.204 | < 0.053 | < 0.026 | < 0.041 | < 0.129 | < 0.127 | < 0.067 | 1 | < 0.012 < |
| 8.3 | 22 | < 0.204 | < 0.097 | < 0.017 | < 0.053 | < 0.046 | < 0.251 | < 0.106 | 1 | < 0.012 < |
| 8.3 | 23 | < 0.204 | < 0.085 | < 0.039 | < 0.066 | < 0.043 | < 0.361 | < 0.090 | 1 | < 0.012 < |
| 8.3 | 24 | 0.078 | < 0.035 | < 0.055 | 0.049 | 0.166 | < 0.362 | < 0.126 | 1 | 0.004565 < |
| 8.3 | 25 | < 0.204 | < 0.036 | < 0.040 | < 0.053 | < 0.065 | < 0.362 | < 0.075 | 1 | < 0.012 < |
| 8.3 | 26 | < 0.202 | < 0.048 | < 0.034 | < 0.050 | < 0.041 | < 0.258 | < 0.081 | 1 | < 0.011882 < |
| 8.3 | 27 | < 0.202 | < 0.063 | < 0.042 | < 0.046 | < 0.027 | < 0.356 | < 0.069 | 1 | < 0.011882 < |
| 8.3 | 28 | < 0.202 | < 0.035 | < 0.049 | < 0.066 | 1.160 | < 0.271 | < 0.244 | 1 | < 0.011882 < |
| 8.3 | 29 | < 0.202 | < 0.092 | < 0.040 | < 0.076 | 0.724 | < 0.511 | < 0.192 | 1 | < 0.011882 < |
| 8.3 | 30 | < 0.202 | < 0.054 | < 0.038 | < 0.052 | < 0.248 | < 0.435 | < 0.210 | 1 | < 0.011882 < |

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CONCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| O-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| 0.045 < | 0.017 < | 0.028 < | 0.000 < | 0.003 < | 0.033 | 0.137 |
| 0.065 < | 0.025 < | 0.031 < | 0.000 < | 0.005 < | 0.069 | 0.207 |
| 0.042 < | 0.041 < | 0.026 < | 0.000 < | 0.007 < | 0.076 | 0.202 |
| 0.023 < | 0.038 < | 0.031 < | 0.000 < | 0.006 < | 0.066 | 0.175 |
| 0.040 < | 0.035 < | 0.025 < | 0.000 < | 0.005 < | 0.061 | 0.178 |
| 0.064 < | 0.042 < | 0.026 < | 0.000 < | 0.005 < | 0.040 | 0.190 |
| 0.107 < | 0.021 < | 0.029 < | 0.000 < | 0.002 < | 0.082 | 0.254 |
| 0.070 < | 0.035 < | 0.038 < | 0.000 < | 0.006 < | 0.062 | 0.223 |
| 0.049 < | 0.026 < | 0.032 < | 0.000 < | 0.002 < | 0.049 | 0.171 |
| 0.040 < | 0.032 < | 0.033 < | 0.000 < | 0.004 < | 0.041 | 0.163 |
| 0.074 < | 0.059 < | 0.032 < | 0.000 < | 0.005 < | 0.037 | 0.220 |
| 0.024 < | 0.042 < | 0.025 < | 0.000 < | 0.006 < | 0.030 | 0.139 |
| 0.072 < | 0.041 < | 0.023 < | 0.000 < | 0.003 < | 0.030 | 0.180 |
| 0.067 < | 0.024 < | 0.032 < | 0.000 < | 0.006 < | 0.062 | 0.202 |
| 0.094 < | 0.019 < | 0.032 < | 0.000 < | 0.004 < | 0.088 | 0.249 |
| 0.036 < | 0.078 < | 0.024 < | 0.000 < | 0.002 < | 0.032 | 0.184 |
| 0.076 < | 0.025 < | 0.031 < | 0.000 < | 0.003 < | 0.049 | 0.195 |
| 0.096 < | 0.043 < | 0.029 < | 0.000 < | 0.004 < | 0.034 | 0.218 |
| 0.029 < | 0.052 < | 0.028 < | 0.000 < | 0.006 < | 0.076 | 0.204 |
| 0.036 < | 0.017 < | 0.029 < | 0.000 < | 0.007 < | 0.082 | 0.184 |
| 0.058 < | 0.024 < | 0.023 < | 0.000 < | 0.002 < | 0.033 | 0.152 |
| 0.107 < | 0.016 < | 0.029 < | 0.000 < | 0.004 < | 0.053 | 0.221 |
| 0.095 < | 0.035 < | 0.037 < | 0.000 < | 0.006 < | 0.045 | 0.229 |
| 0.039 < | 0.050 < | 0.027 | 0.000 < | 0.006 < | 0.063 | 0.190 |
| 0.040 < | 0.036 < | 0.029 < | 0.000 < | 0.006 < | 0.037 | 0.161 |
| 0.054 < | 0.031 < | 0.028 < | 0.000 < | 0.004 < | 0.041 | 0.169 |
| 0.070 < | 0.038 < | 0.025 < | 0.000 < | 0.006 < | 0.034 | 0.185 |
| 0.039 < | 0.045 < | 0.037 | 0.000 < | 0.004 < | 0.122 | 0.258 |
| 0.102 < | 0.036 < | 0.042 | 0.000 < | 0.008 < | 0.096 | 0.296 |
| 0.060 < | 0.034 < | 0.029 < | 0.000 < | 0.007 < | 0.105 | 0.247 |

TABLE 8.4-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:56 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
SPILLWAY BEHIND REACTOR BUILDING - AREA 8.4 FOR MICRO REM

RADIATION TYPE: GAMMA SURVEY IN UREM/HR
COMPLETION
DATE: 10-5-94
TECHNICIANS: JB/DR/PK
LOCATION: 8.0
GRID ID: 8.4
MEDIA TYPE: CONCRETE
# of POINTS: 30

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | LIMIT |
|---|---|---|
| MAX | 6 PASS | 10 |
| AVG | 3 PASS | 5 |
| STD X | 1 | |
| MU SUB ALPHA | 3 PASS | 5 |

| ID # | INST. ID # | AREA BKG UREM/HR | AREA READING UREM/HR | MATER-IAL CODE | NET UREM/HR |
|---|---|---|---|---|---|
| 8.4 | 1 | 4 | 6 | 8 | 2 |
| 8.4 | 2 | 4 | 6 | 7 | 8 | 1 |
| 8.4 | 3 | 4 | 6 | 7 | 8 | 1 |
| 8.4 | 4 | 4 | 6 | 10 | 8 | 4 |
| 8.4 | 5 | 4 | 6 | 8 | 8 | 2 |
| 8.4 | 6 | 4 | 6 | 9 | 8 | 3 |
| 8.4 | 7 | 4 | 6 | 10 | 8 | 4 |
| 8.4 | 8 | 4 | 6 | 10 | 8 | 4 |
| 8.4 | 9 | 4 | 6 | 9 | 8 | 3 |
| 8.4 | 10 | 4 | 6 | 10 | 8 | 4 |
| 8.4 | 11 | 4 | 6 | 10 | 8 | 4 |
| 8.4 | 12 | 4 | 6 | 7 | 8 | 1 |
| 8.4 | 13 | 4 | 6 | 12 | 8 | 6 |
| 8.4 | 14 | 4 | 6 | 11 | 8 | 5 |
| 8.4 | 15 | 4 | 6 | 9 | 8 | 3 |
| 8.4 | 16 | 4 | 6 | 8 | 8 | 2 |
| 8.4 | 17 | 4 | 6 | 10 | 8 | 4 |
| 8.4 | 18 | 4 | 6 | 6 | 8 | 0 |
| 8.4 | 19 | 4 | 6 | 8 | 8 | 2 |
| 8.4 | 20 | 4 | 6 | 8 | 8 | 2 |
| 8.4 | 21 | 4 | 6 | 9 | 8 | 3 |
| 8.4 | 22 | 4 | 6 | 8 | 8 | 2 |
| 8.4 | 23 | 4 | 6 | 9 | 8 | 3 |
| 8.4 | 24 | 4 | 6 | 8 | 8 | 2 |
| 8.4 | 25 | 4 | 6 | 9 | 8 | 3 |
| 8.4 | 26 | 4 | 6 | 11 | 8 | 5 |
| 8.4 | 27 | 4 | 6 | 10 | 8 | 4 |
| 8.4 | 28 | 4 | 6 | 9 | 8 | 3 |
| 8.4 | 29 | 4 | 6 | 7 | 8 | 1 |
| 8.4 | 30 | 4 | 6 | 10 | 8 | 4 |

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CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:54 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
SPILLWAY BEHIND REACTOR BUILDING - 8.4 FOR BETA

RADIATION TYPE: 1 (1=BETA, 2=ALPHA)
COMPLETION DATE: 10-10-94
TECHNICIANS: JB/DR/PK
LOCATION: 8.0
GRID ID: 8.4
MEDIA TYPE: CONCRETE
# of POINTS: 30
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | LIMIT |
|---|---|---|
| MAX | 3473 PASS | 40500 |
| AVG | 596 PASS | 13500 |
| STD X | 1209 | |
| MU SUB ALPHA | 972 PASS | 13500 |

| ID # | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | BETA FIXED GCPM | MATER-IAL CODE | MDA DPM/ 100 CM^2 | BETA FIXED DPM/ 100 CM^2 | STAT SIG ? | INST EFF. CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| 8.4 | 1 | 4 | 630 | 632 | 632 | 8 | 2230 | 37 N | 0.1785 |
| 8.4 | 2 | 4 | 630 | 652 | 652 | 8 | 2230 | 411 N | 0.1785 |
| 8.4 | 3 | 4 | 630 | 683 | 683 | 8 | 2230 | 990 N | 0.1785 |
| 8.4 | 4 | 4 | 630 | 727 | 727 | 8 | 2230 | 1811 N | 0.1785 |
| 8.4 | 5 | 4 | 630 | 657 | 657 | 8 | 2230 | 504 N | 0.1785 |
| 8.4 | 6 | 4 | 630 | 635 | 635 | 8 | 2230 | 93 N | 0.1785 |
| 8.4 | 7 | 4 | 630 | 816 | 816 | 8 | 2230 | 3473 Y | 0.1785 |
| 8.4 | 8 | 4 | 630 | 789 | 789 | 8 | 2230 | 2969 Y | 0.1785 |
| 8.4 | 9 | 4 | 630 | 747 | 747 | 8 | 2230 | 2185 N | 0.1785 |
| 8.4 | 10 | 4 | 630 | 683 | 683 | 8 | 2230 | 990 N | 0.1785 |
| 8.4 | 11 | 4 | 630 | 689 | 689 | 8 | 2230 | 1102 N | 0.1785 |
| 8.4 | 12 | 4 | 630 | 638 | 638 | 8 | 2230 | 149 N | 0.1785 |
| 8.4 | 13 | 4 | 630 | 698 | 698 | 8 | 2230 | 1270 N | 0.1785 |
| 8.4 | 14 | 4 | 630 | 670 | 670 | 8 | 2230 | 747 N | 0.1785 |
| 8.4 | 15 | 4 | 630 | 582 | 582 | 8 | 2230 | -896 N | 0.1785 |
| 8.4 | 16 | 4 | 630 | 649 | 649 | 8 | 2230 | 355 N | 0.1785 |
| 8.4 | 17 | 4 | 630 | 640 | 640 | 8 | 2230 | 187 N | 0.1785 |
| 8.4 | 18 | 4 | 630 | 772 | 772 | 8 | 2230 | 2652 Y | 0.1785 |
| 8.4 | 19 | 4 | 630 | 715 | 715 | 8 | 2230 | 1587 N | 0.1785 |
| 8.4 | 20 | 4 | 630 | 689 | 689 | 8 | 2230 | 1102 N | 0.1785 |
| 8.4 | 21 | 4 | 630 | 607 | 607 | 8 | 2230 | -430 N | 0.1785 |
| 8.4 | 22 | 4 | 630 | 595 | 595 | 8 | 2230 | -654 N | 0.1785 |
| 8.4 | 23 | 4 | 630 | 595 | 595 | 8 | 2230 | -654 N | 0.1785 |
| 8.4 | 24 | 4 | 630 | 582 | 582 | 8 | 2230 | -896 N | 0.1785 |
| 8.4 | 25 | 4 | 630 | 613 | 613 | 8 | 2230 | -317 N | 0.1785 |
| 8.4 | 26 | 4 | 630 | 575 | 575 | 8 | 2230 | -1027 N | 0.1785 |
| 8.4 | 27 | 4 | 630 | 554 | 554 | 8 | 2230 | -1419 N | 0.1785 |
| 8.4 | 28 | 4 | 630 | 639 | 639 | 8 | 2230 | 168 N | 0.1785 |
| 8.4 | 29 | 4 | 630 | 697 | 697 | 8 | 2230 | 1251 N | 0.1785 |
| 8.4 | 30 | 4 | 630 | 638 | 638 | 8 | 2230 | 149 N | 0.1785 |

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CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:53 AM

FINAL SURVEY DATA SHEET

DATA FOR UNAFFECTED AREA DESCRIPTION:

SPILLWAY BEHIND REACTOR BUILDING - B.4 FOR ALPHA

RADIATION TYPE: 2 (1=BETA, 2=ALPHA)

COMPLETION

DATE: 10-10-94

TECHNICIANS: JB/DR/PK

LOCATION: B.0

GRID ID: B.4

MEDIA TYPE: CONCRETE

# of POINTS: 30

CT IN MINUTES: 1

MATERIAL CODE

1=CONCRETE 5=PLASTIC

2=ROCK 6=SOIL

3=WOOD 7=ASPHALT

4=METAL 8=OTHER(SPECIFY):

NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | LIMIT |
|---|---|---|
| MAX | 38 PASS | 15000 |
| AVG | 17 PASS | 5000 |
| STD X | 11 | |
| MU SUB ALPHA | 20 PASS | 5000 |

| ID # | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | ALPHA FIXED GCPM | MATER-IAL CODE | MDA DPM/ 100 CM^2 | ALPHA FIXED DPM/ 100 CM^2 | STAT SIG ? | ALPHA EFF. CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| B.4 | 1 | 4 | 0.4 | 6 | 6 | 8 | 28 | 28 N | 0.2015 |
| B.4 | 2 | 4 | 0.4 | 0 | 0 | 8 | 28 | -2 N | 0.2015 |
| B.4 | 3 | 4 | 0.4 | 2 | 2 | 8 | 28 | 8 N | 0.2015 |
| B.4 | 4 | 4 | 0.4 | 3 | 3 | 8 | 28 | 13 N | 0.2015 |
| B.4 | 5 | 4 | 0.4 | 0 | 0 | 8 | 28 | -2 N | 0.2015 |
| B.4 | 6 | 4 | 0.4 | 8 | 8 | 8 | 28 | 38 Y | 0.2015 |
| B.4 | 7 | 4 | 0.4 | 6 | 6 | 8 | 28 | 28 N | 0.2015 |
| B.4 | 8 | 4 | 0.4 | 5 | 5 | 8 | 28 | 23 N | 0.2015 |
| B.4 | 9 | 4 | 0.4 | 5 | 5 | 8 | 28 | 23 N | 0.2015 |
| B.4 | 10 | 4 | 0.4 | 4 | 4 | 8 | 28 | 18 N | 0.2015 |
| B.4 | 11 | 4 | 0.4 | 8 | 8 | 8 | 28 | 38 Y | 0.2015 |
| B.4 | 12 | 4 | 0.4 | 3 | 3 | 8 | 28 | 13 N | 0.2015 |
| B.4 | 13 | 4 | 0.4 | 3 | 3 | 8 | 28 | 13 N | 0.2015 |
| B.4 | 14 | 4 | 0.4 | 2 | 2 | 8 | 28 | 8 N | 0.2015 |
| B.4 | 15 | 4 | 0.4 | 4 | 4 | 8 | 28 | 18 N | 0.2015 |
| B.4 | 16 | 4 | 0.4 | 5 | 5 | 8 | 28 | 23 N | 0.2015 |
| B.4 | 17 | 4 | 0.4 | 6 | 6 | 8 | 28 | 28 N | 0.2015 |
| B.4 | 18 | 4 | 0.4 | 4 | 4 | 8 | 28 | 18 N | 0.2015 |
| B.4 | 19 | 4 | 0.4 | 8 | 8 | 8 | 28 | 38 Y | 0.2015 |
| B.4 | 20 | 4 | 0.4 | 3 | 3 | 8 | 28 | 13 N | 0.2015 |
| B.4 | 21 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| B.4 | 22 | 4 | 0.4 | 2 | 2 | 8 | 28 | 8 N | 0.2015 |
| B.4 | 23 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| B.4 | 24 | 4 | 0.4 | 1 | 1 | 8 | 28 | 3 N | 0.2015 |
| B.4 | 25 | 4 | 0.4 | 2 | 2 | 8 | 28 | 8 N | 0.2015 |
| B.4 | 26 | 4 | 0.4 | 5 | 5 | 8 | 28 | 23 N | 0.2015 |
| B.4 | 27 | 4 | 0.4 | 3 | 3 | 8 | 28 | 13 N | 0.2015 |
| B.4 | 28 | 4 | 0.4 | 7 | 7 | 8 | 28 | 33 Y | 0.2015 |
| B.4 | 29 | 4 | 0.4 | 4 | 4 | 8 | 28 | 18 N | 0.2015 |
| B.4 | 30 | 4 | 0.4 | 2 | 2 | 8 | 28 | 8 N | 0.2015 |

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R.H.TABLE 8.4-4

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:13 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 8.4 - SPILLWAY BEHIND REACTOR BUILDING SOIL FOR SUM OF THE FRACTIONS

RADIATION TYPE: SOIL DATA FOR SUM OF THE FRACTIONS
COMPLETION DATE: 10-10-94
TECHNICIANS: JB/DR/PK
LOCATION: 8.0
GRID ID: 8.4
MEDIA TYPE: SOIL
# of POINTS: 6

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 2.88 | FAIL | 1 |
| AVG | 1.52 | FAIL | 1 |
| STD X | 0.79 | | |
| MU SUB ALPHA | 2.07 | FAIL | 1 |

ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED)

| ID # | GRID COORIDINATES OR OTHER ID | SR-90 | CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SOIL CODE | ISOTOPES OF SR-90 |
|---|---|---|---|---|---|---|---|---|---|---|
| | | LIMIT 17 | LIMIT 0.9 | LIMIT 1.1 | LIMIT 1.8 | LIMIT 3.8 | LIMIT 63 | LIMIT 2 | | |
| 8.4 | 2 | < 0.619 | < 0.151 | < 0.149 | < 0.223 | < 0.692 | < 0.902 | < 0.335 | 1 | < 0.036412 < |
| 8.4 | 6 | < 0.461 | < 0.081 | < 0.084 | < 0.104 | 6.450 | < 0.256 | < 0.184 | 1 | < 0.027118 < |
| 8.4 | 12 | < 0.495 | < 0.064 | < 0.073 | < 0.065 | 3.330 | < 0.373 | < 0.182 | 1 | < 0.029118 < |
| 8.4 | 20 | < 0.341 | < 0.099 | < 0.093 | < 0.080 | 10.600 | < 0.447 | < 0.299 | 1 | < 0.020059 < |
| 8.4 | 25 | < 0.336 | < 0.112 | < 0.107 | < 0.110 | 5.650 | < 0.748 | < 0.293 | 1 | < 0.019765 < |
| 8.4 | 26 | < 0.193 | < 0.070 | < 0.081 | < 0.070 | 5.720 | < 0.309 | < 0.114 | 1 | < 0.011353 < |

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CONCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| O-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| 0.168 < | 0.135 < | 0.124 < | 0.000 < | 0.014 < | 0.168 | 0.645 |
| 0.090 < | 0.077 < | 0.058 | 1.368 < | 0.004 < | 0.092 | 1.716 |
| 0.071 < | 0.066 < | 0.036 | 0.547 < | 0.006 < | 0.091 | 0.847 |
| 0.110 < | 0.084 < | 0.044 | 2.461 < | 0.007 < | 0.150 | 2.876 |
| 0.124 < | 0.097 < | 0.061 | 1.158 < | 0.012 < | 0.147 | 1.619 |
| 0.077 < | 0.073 < | 0.039 | 1.176 < | 0.005 < | 0.057 | 1.439 |

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RETABLE 8.5-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:58 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
GROUNDS SOUTH OF REACTOR BUILDING WITHIN RCA - AREA 8.5 FOR UREM

RADIATION TYPE: GAMMA SURVEY IN UREM/HR
COMPLETION DATE: 10-6-94
TECHNICIANS: JB/DR/PK
LOCATION: 8.0
GRID ID: 8.5
MEDIA TYPE: SOIL
# of POINTS: 30

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | LIMIT |
|---|---|---|
| MAX | 4 PASS | 10 |
| AVG | 2 PASS | 5 |
| STD X | 1 | |
| MU SUB ALPHA | 2 PASS | 5 |

| ID # | | INST. ID.# | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|---|
| 8.5 | 1 | A | 6 | 8 | 8 | 2 |
| 8.5 | 2 | A | 6 | 7 | 8 | 1 |
| 8.5 | 3 | A | 6 | 6 | 8 | 0 |
| 8.5 | 4 | A | 6 | 7 | 8 | 1 |
| 8.5 | 5 | A | 6 | 7 | 8 | 1 |
| 8.5 | 6 | A | 6 | 9 | 8 | 3 |
| 8.5 | 7 | A | 6 | 7 | 8 | 1 |
| 8.5 | 8 | A | 6 | 7 | 8 | 1 |
| 8.5 | 9 | A | 6 | 10 | 8 | 4 |
| 8.5 | 10 | A | 6 | 8 | 8 | 2 |
| 8.5 | 11 | A | 6 | 8 | 8 | 2 |
| 8.5 | 12 | A | 6 | 8 | 8 | 2 |
| 8.5 | 13 | A | 6 | 9 | 8 | 3 |
| 8.5 | 14 | A | 6 | 6 | 8 | 0 |
| 8.5 | 15 | A | 6 | 9 | 8 | 3 |
| 8.5 | 16 | A | 6 | 9 | 8 | 3 |
| 8.5 | 17 | A | 6 | 6 | 8 | 0 |
| 8.5 | 18 | A | 6 | 6 | 8 | 0 |
| 8.5 | 19 | A | 6 | 7 | 8 | 1 |
| 8.5 | 20 | A | 6 | 6 | 8 | 0 |
| 8.5 | 21 | A | 6 | 7 | 8 | 1 |
| 8.5 | 22 | A | 6 | 9 | 8 | 3 |
| 8.5 | 23 | A | 6 | 9 | 8 | 3 |
| 8.5 | 24 | A | 6 | 8 | 8 | 2 |
| 8.5 | 25 | A | 6 | 7 | 8 | 1 |
| 8.5 | 26 | A | 6 | 8 | 8 | 2 |
| 8.5 | 27 | A | 6 | 8 | 8 | 2 |
| 8.5 | 28 | A | 6 | 5 | 8 | -1 |
| 8.5 | 29 | A | 6 | 9 | 8 | 3 |
| 8.5 | 30 | A | 6 | 7 | 8 | 1 |

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TABLE B.5-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:13 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA B.5 - GROUNDS SOUTH OF REACTOR BUILDING WITHIN RCA SOIL FOR SUM OF THE FRACTIONS

RADIATION TYPE: SOIL DATA FOR SUM OF THE FRACTIONS
COMPLETION DATE: 10-6-94
TECHNICIANS: JB/DR/PK
LOCATION: B.0
GRID ID: B.5
MEDIA TYPE: SOIL
# of POINTS: 30

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 0.51 | PASS | 1 |
| AVG | 0.25 | PASS | 1 |
| STD X | 0.09 | | |
| MU SUB ALPHA | 0.28 | PASS | 1 |

ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED)

| ID # | GRID COORIDINATES OR OTHER ID | SR-90 | CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SOIL CODE | ISOTOPES OF SR-90 |
|---|---|---|---|---|---|---|---|---|---|---|
| | | LIMIT 17 | LIMIT 0.9 | LIMIT 1.1 | LIMIT 1.8 | LIMIT 3.8 | LIMIT 63 | LIMIT 2 | | |
| B.5 | 1 | < 0.202 | < 0.037 | < 0.022 | < 0.060 | < 0.072 | < 0.336 | < 0.044 | 1 | < 0.011882 < |
| B.5 | 2 | < 0.18 | < 0.062 | < 0.026 | < 0.066 | < 0.110 | < 0.316 | < 0.122 | 1 | < 0.010588 < |
| B.5 | 3 | < 0.18 | < 0.048 | < 0.047 | < 0.062 | < 0.079 | < 0.140 | < 0.176 | 1 | < 0.010588 < |
| B.5 | 4 | 1.01 | < 0.059 | < 0.047 | < 0.089 | 0.466 | < 0.359 | < 0.301 | 1 | 0.059412 < |
| B.5 | 5 | < 0.18 | < 0.071 | < 0.048 | < 0.046 | < 0.138 | < 0.216 | < 0.107 | 1 | < 0.010588 < |
| B.5 | 6 | < 0.18 | < 0.039 | < 0.048 | < 0.047 | 0.100 | < 0.187 | < 0.074 | 1 | < 0.010588 < |
| B.5 | 7 | < 0.18 | < 0.040 | < 0.072 | < 0.068 | 0.503 | < 0.355 | < 0.107 | 1 | < 0.010588 < |
| B.5 | 8 | < 0.18 | < 0.059 | < 0.098 | < 0.093 | 0.913 | < 0.180 | < 0.179 | 1 | < 0.010588 < |
| B.5 | 9 | < 0.18 | < 0.073 | < 0.042 | < 0.066 | 0.184 | < 0.322 | < 0.207 | 1 | < 0.010588 < |
| B.5 | 10 | < 0.18 | < 0.060 | < 0.034 | < 0.074 | < 0.121 | < 0.455 | < 0.097 | 1 | < 0.010588 < |
| B.5 | 11 | < 0.176 | < 0.036 | < 0.031 | < 0.063 | < 0.088 | < 0.340 | < 0.100 | 1 | < 0.010353 < |
| B.5 | 12 | < 0.252 | < 0.044 | < 0.037 | < 0.060 | 0.756 | < 0.483 | < 0.153 | 1 | < 0.014824 < |
| B.5 | 13 | < 0.182 | < 0.047 | < 0.035 | < 0.067 | 0.377 | < 0.317 | < 0.129 | 1 | < 0.010706 < |
| B.5 | 14 | < 0.17 | < 0.039 | < 0.058 | < 0.081 | 0.265 | < 0.406 | < 0.186 | 1 | < 0.01 < |
| B.5 | 15 | < 0.17 | < 0.029 | < 0.039 | < 0.063 | < 0.085 | < 0.351 | < 0.095 | 1 | < 0.01 < |
| B.5 | 16 | < 0.202 | < 0.097 | < 0.030 | < 0.085 | 0.968 | < 0.322 | < 0.289 | 1 | < 0.011882 < |
| B.5 | 17 | < 0.203 | < 0.041 | < 0.026 | < 0.072 | 0.914 | < 0.287 | < 0.154 | 1 | < 0.011941 < |
| B.5 | 18 | < 0.169 | < 0.074 | < 0.045 | < 0.062 | 0.478 | < 0.345 | < 0.075 | 1 | < 0.009941 < |
| B.5 | 19 | < 0.174 | < 0.047 | < 0.033 | < 0.073 | 0.620 | < 0.248 | < 0.062 | 1 | < 0.010235 < |
| B.5 | 20 | < 0.203 | < 0.044 | < 0.050 | < 0.057 | 0.298 | < 0.411 | < 0.163 | 1 | < 0.011941 < |
| B.5 | 21 | < 0.183 | < 0.073 | < 0.029 | < 0.083 | 0.689 | < 0.272 | < 0.173 | 1 | < 0.010765 < |
| B.5 | 22 | < 0.183 | < 0.059 | < 0.022 | < 0.064 | < 0.134 | < 0.414 | < 0.746 | 1 | < 0.010765 < |
| B.5 | 23 | < 0.203 | < 0.073 | < 0.042 | < 0.054 | 0.271 | < 0.347 | < 0.093 | 1 | < 0.011941 < |
| B.5 | 24 | < 0.183 | < 0.083 | < 0.051 | < 0.059 | < 0.151 | < 0.216 | < 0.170 | 1 | < 0.010765 < |
| B.5 | 25 | < 0.203 | < 0.094 | < 0.039 | < 0.056 | 0.677 | < 0.278 | < 0.139 | 1 | < 0.011941 < |
| B.5 | 26 | < 0.203 | < 0.044 | < 0.020 | < 0.057 | < 0.093 | < 0.371 | < 0.091 | 1 | < 0.011941 < |
| B.5 | 27 | < 0.203 | < 0.070 | < 0.050 | < 0.085 | 1.770 | < 0.338 | < 0.107 | 1 | < 0.011941 < |
| B.5 | 28 | < 0.203 | < 0.052 | < 0.051 | < 0.073 | 1.690 | < 0.191 | < 0.091 | 1 | < 0.011941 < |
| B.5 | 29 | < 0.203 | < 0.054 | < 0.030 | < 0.061 | 0.361 | < 0.215 | < 0.118 | 1 | < 0.011941 < |
| B.5 | 30 | < 0.22 | < 0.073 | < 0.044 | < 0.070 | 2.090 | < 0.152 | < 0.200 | 1 | < 0.012941 < |

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CONCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| O-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| 0.041 < | 0.020 < | 0.033 < | 0.000 < | 0.005 < | 0.022 | 0.134 |
| 0.069 < | 0.023 < | 0.037 < | 0.000 < | 0.005 < | 0.061 | 0.205 |
| 0.053 < | 0.043 < | 0.034 < | 0.000 < | 0.002 < | 0.088 | 0.231 |
| 0.066 < | 0.043 < | 0.049 | 0.000 < | 0.006 < | 0.151 | 0.373 |
| 0.079 < | 0.044 < | 0.026 | 0.000 < | 0.003 < | 0.054 | 0.216 |
| 0.043 < | 0.043 < | 0.026 | 0.000 < | 0.003 < | 0.037 | 0.163 |
| 0.044 < | 0.065 < | 0.038 | 0.000 < | 0.006 < | 0.054 | 0.217 |
| 0.066 < | 0.089 < | 0.052 | 0.000 < | 0.003 < | 0.090 | 0.309 |
| 0.081 < | 0.038 < | 0.037 | 0.000 < | 0.005 < | 0.104 | 0.274 |
| 0.066 < | 0.031 < | 0.041 < | 0.000 < | 0.007 < | 0.048 | 0.204 |
| 0.040 < | 0.028 < | 0.035 < | 0.000 < | 0.005 < | 0.050 | 0.168 |
| 0.049 < | 0.033 < | 0.034 | 0.000 < | 0.008 < | 0.077 | 0.215 |
| 0.052 < | 0.032 < | 0.037 | 0.000 < | 0.005 < | 0.065 | 0.201 |
| 0.043 < | 0.053 < | 0.045 | 0.000 < | 0.006 < | 0.093 | 0.251 |
| 0.032 < | 0.035 < | 0.035 < | 0.000 < | 0.006 < | 0.047 | 0.166 |
| 0.108 < | 0.027 < | 0.047 | 0.000 < | 0.005 < | 0.145 | 0.344 |
| 0.046 < | 0.023 < | 0.040 | 0.000 < | 0.005 < | 0.077 | 0.203 |
| 0.082 < | 0.041 < | 0.034 | 0.000 < | 0.005 < | 0.038 | 0.210 |
| 0.052 < | 0.030 < | 0.040 | 0.000 < | 0.004 < | 0.031 | 0.168 |
| 0.048 < | 0.045 < | 0.032 | 0.000 < | 0.007 < | 0.082 | 0.225 |
| 0.081 < | 0.026 < | 0.046 | 0.000 < | 0.004 < | 0.087 | 0.255 |
| 0.065 < | 0.020 < | 0.036 < | 0.000 < | 0.007 < | 0.373 | 0.511 |
| 0.081 < | 0.038 < | 0.030 | 0.000 < | 0.006 < | 0.046 | 0.213 |
| 0.092 < | 0.046 < | 0.033 < | 0.000 < | 0.003 < | 0.085 | 0.270 |
| 0.104 < | 0.036 < | 0.031 | 0.000 < | 0.004 < | 0.070 | 0.257 |
| 0.049 < | 0.018 < | 0.032 < | 0.000 < | 0.006 < | 0.045 | 0.162 |
| 0.078 < | 0.045 < | 0.047 | 0.137 < | 0.005 < | 0.054 | 0.378 |
| 0.057 < | 0.047 < | 0.040 | 0.116 < | 0.003 < | 0.045 | 0.321 |
| 0.060 < | 0.027 < | 0.034 | 0.000 < | 0.003 < | 0.059 | 0.196 |
| 0.081 < | 0.040 < | 0.039 | 0.221 < | 0.002 < | 0.100 | 0.496 |

TABLE 8.6-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:59 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
GROUND EAST OF ROADWAY - AREA 8.6 FOR UREM/HR

| | | | |
|---|---|---|---|
| RADIATION TYPE: | GAMMA SURVEY IN UREM/HR | | |
| COMPLETION DATE: | 10-18-94 | | |
| TECHNICIANS: | TA/CD/PS | MATERIAL CODE | |
| LOCATION: | 8.0 | 1=CONCRETE | 5=PLASTIC |
| GRID ID: | 8.6 | 2=ROCK | 6=SOIL |
| MEDIA TYPE: | SOIL | 3=WOOD | 7=ASPHALT |
| # of POINTS: | 30 | 4=METAL | 8=OTHER(SPECIFY): |
| | | | NO MATERIAL BACKGROUND USED |

| MICRO REM PER HOUR: | | | LIMIT |
|---|---|---|---|
| MAX: | 6.00 | PASS | 10 |
| AVG: | 2.80 | PASS | 5 |
| STD X: | 1.56 | | |
| MU SUB ALPHA: | 3.28 | PASS | 5 |

| ID # | GRID POINT W | S | INST. ID # | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|---|---|
| 8.6 | 1+14.5 | 1+31.5 | A | 6 | 11 | 8 | 5 |
| 8.6 | 1+13.5 | 1+28.5 | A | 6 | 12 | 8 | 6 |
| 8.6 | 1+12.5 | 1+24.5 | A | 6 | 9 | 8 | 3 |
| 8.6 | 1+12.5 | 1+21.5 | A | 6 | 10 | 8 | 4 |
| 8.6 | 1+11.5 | 1+18.5 | A | 6 | 9 | 8 | 3 |
| 8.6 | 1+10.5 | 1+15.5 | A | 6 | 7 | 8 | 1 |
| 8.6 | 1+9.5 | 1+12.5 | A | 6 | 8 | 8 | 2 |
| 8.6 | 1+8.5 | 1+9.5 | A | 6 | 11 | 8 | 5 |
| 8.6 | 1+6.5 | 1+6.5 | A | 6 | 12 | 8 | 6 |
| 8.6 | 1+7.5 | 1+3.5 | A | 6 | 10 | 8 | 4 |
| 8.6 | 1+5.5 | 1+0.5 | A | 6 | 10 | 8 | 4 |
| 8.6 | 1+6.5 | 0+97.5 | A | 6 | 7 | 8 | 1 |
| 8.6 | 1+5.5 | 0+94.5 | A | 6 | 6 | 8 | 0 |
| 8.6 | 1+4.5 | 0+92.5 | A | 6 | 7 | 8 | 1 |
| 8.6 | 1+2.5 | 0+89.5 | A | 6 | 7 | 8 | 1 |
| 8.6 | 1+1.5 | 0+86.5 | A | 6 | 9 | 8 | 3 |
| 8.6 | 1+0.5 | 0+83.5 | A | 6 | 8 | 8 | 2 |
| 8.6 | 0+99.5 | 0+81.5 | A | 6 | 9 | 8 | 3 |
| 8.6 | 0+98.5 | 0+79.5 | A | 6 | 8 | 8 | 2 |
| 8.6 | 0+97.5 | 0+75.5 | A | 6 | 8 | 8 | 2 |
| 8.6 | 0+96.5 | 0+72.5 | A | 6 | 9 | 8 | 3 |
| 8.6 | 0+95.5 | 0+69.5 | A | 6 | 7 | 8 | 1 |
| 8.6 | 0+94.5 | 0+65.5 | A | 6 | 10 | 8 | 4 |
| 8.6 | 0+94.5 | 0+63.5 | A | 6 | 8 | 8 | 2 |
| 8.6 | 0+93.5 | 0+60.5 | A | 6 | 10 | 8 | 4 |
| 8.6 | 0+90.5 | 0+53.5 | A | 6 | 10 | 8 | 4 |
| 8.6 | 0+89.5 | 0+49.5 | A | 6 | 8 | 8 | 2 |
| 8.6 | 0+87.5 | 0+44.5 | A | 6 | 8 | 8 | 2 |
| 8.6 | 0+84.5 | 0+38.5 | A | 6 | 9 | 8 | 3 |
| 8.6 | 0+83.5 | 0+34.5 | A | 6 | 7 | 8 | 1 |

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TABLE 8.6-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:14 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 8.6 - GROUND EAST OF ROADWAY SOIL FOR SUM OF THE FRACTIONS

RADIATION TYPE: SOIL DATA FOR SUM OF THE FRACTIONS
COMPLETION DATE: 10-18-94
TECHNICIANS: TA/CD/PS
LOCATION: 8.0
GRID ID: 8.6
MEDIA TYPE: SOIL
# of POINTS: 30

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 0.90 | PASS | 1 |
| AVG | 0.26 | PASS | 1 |
| STD X | 0.14 | | |
| MU SUB ALPHA | 0.31 | PASS | 1 |

ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED) ISOTOPES OF

| ID # | GRID COORDINATES OR OTHER ID | | | SR-90 | CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SOIL CODE | SR-90 | C |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | LIMIT 17 | LIMIT 0.9 | LIMIT 1.1 | LIMIT 1.8 | LIMIT 3.8 | LIMIT 63 | LIMIT 2 | | | |
| 8.6 | 1+14.5 | 1+31.5 | 1 | < 0.201 | < 0.079 | < 0.053 | < 0.063 | 1.260 | < 0.402 | < 0.096 | 1 | < 0.011824 | < |
| 8.6 | 1+13.5 | 1+28.5 | 2 | < 0.201 | < 0.057 | < 0.049 | < 0.066 | 0.960 | < 0.182 | < 0.161 | 1 | < 0.011824 | < |
| 8.6 | 1+12.5 | 1+24.5 | 3 | < 0.201 | < 0.041 | < 0.030 | < 0.069 | 1.030 | < 0.069 | < 0.091 | 1 | < 0.011824 | < |
| 8.6 | 1+12.5 | 1+21.5 | 4 | < 0.217 | < 0.064 | < 0.025 | < 0.073 | 1.130 | < 0.366 | < 0.129 | 1 | < 0.012765 | < |
| 8.6 | 1+11.5 | 1+18.5 | 5 | < 0.217 | < 0.064 | < 0.024 | < 0.067 | 1.110 | < 0.039 | < 0.060 | 1 | < 0.012765 | < |
| 8.6 | 1+10.5 | 1+15.5 | 6 | < 0.217 | < 0.037 | < 0.044 | < 0.064 | 1.270 | < 0.459 | < 0.097 | 1 | < 0.012765 | < |
| 8.6 | 1+9.5 | 1+12.5 | 7 | < 0.217 | < 0.047 | < 0.035 | < 0.056 | 1.180 | < 0.358 | < 0.102 | 1 | < 0.012765 | < |
| 8.6 | 1+8.5 | 1+9.5 | 8 | < 0.217 | < 0.048 | < 0.032 | < 0.067 | 1.250 | < 0.354 | < 0.252 | 1 | < 0.012765 | < |
| 8.6 | 1+6.5 | 1+6.5 | 9 | < 0.217 | < 0.048 | < 0.031 | < 0.067 | 0.940 | < 0.298 | < 0.104 | 1 | < 0.012765 | < |
| 8.6 | 1+7.5 | 1+3.5 | 10 | < 0.217 | < 0.033 | < 0.047 | < 0.070 | 0.832 | < 0.522 | < 0.131 | 1 | < 0.012765 | < |
| 8.6 | 1+5.5 | 1+0.5 | 11 | < 0.217 | < 0.041 | < 0.067 | < 0.059 | 0.661 | < 0.201 | < 0.165 | 1 | < 0.012765 | < |
| 8.6 | 1+6.5 | 0+97.5 | 12 | < 0.191 | < 0.042 | < 0.046 | < 0.066 | 0.518 | < 0.449 | < 0.147 | 1 | < 0.011235 | < |
| 8.6 | 1+5.5 | 0+94.5 | 13 | < 0.191 | < 0.044 | < 0.042 | < 0.075 | 0.793 | < 0.396 | < 0.155 | 1 | < 0.011235 | < |
| 8.6 | 1+4.5 | 0+92.5 | 14 | < 0.191 | < 0.038 | < 0.036 | < 0.076 | 0.734 | < 0.545 | < 0.748 | 1 | < 0.011235 | < |
| 8.6 | 1+2.5 | 0+89.5 | 15 | < 0.191 | < 0.094 | < 0.033 | < 0.069 | 0.883 | < 0.430 | < 0.178 | 1 | < 0.011235 | < |
| 8.6 | 1+1.5 | 0+86.5 | 16 | < 0.178 | < 0.049 | < 0.077 | < 0.063 | 0.939 | < 0.339 | < 0.078 | 1 | < 0.010471 | < |
| 8.6 | 1+0.5 | 0+83.5 | 17 | < 0.191 | < 0.041 | < 0.045 | < 0.080 | 1.200 | < 0.335 | < 0.232 | 1 | < 0.011235 | < |
| 8.6 | 0+99.5 | 0+81.5 | 18 | < 0.178 | < 0.042 | < 0.048 | < 0.079 | 1.510 | < 0.392 | < 0.203 | 1 | < 0.010471 | < |
| 8.6 | 0+98.5 | 0+79.5 | 19 | < 0.191 | < 0.059 | < 0.074 | < 0.057 | 1.190 | < 0.197 | < 0.122 | 1 | < 0.011235 | < |
| 8.6 | 0+97.5 | 0+75.5 | 20 | < 0.191 | < 0.080 | < 0.065 | < 0.065 | 1.190 | < 0.309 | < 0.165 | 1 | < 0.011235 | < |
| 8.6 | 0+96.5 | 0+72.5 | 21 | 0.284 | < 0.430 | < 0.034 | < 0.058 | 2.150 | < 0.190 | < 0.214 | 1 | 0.016706 | |
| 8.6 | 0+95.5 | 0+69.5 | 22 | < 0.176 | < 0.051 | < 0.034 | < 0.078 | 0.475 | < 0.439 | < 0.107 | 1 | < 0.010353 | < |
| 8.6 | 0+94.5 | 0+65.5 | 23 | < 0.176 | < 0.093 | < 0.122 | < 0.066 | 0.513 | < 0.141 | < 0.124 | 1 | < 0.010353 | < |
| 8.6 | 0+94.5 | 0+63.5 | 24 | < 0.191 | < 0.114 | < 0.034 | < 0.054 | 0.461 | < 0.251 | < 0.091 | 1 | < 0.011235 | < |
| 8.6 | 0+93.5 | 0+60.5 | 25 | < 0.191 | < 0.091 | < 0.022 | < 0.058 | 0.396 | < 0.335 | < 0.128 | 1 | < 0.011235 | < |
| 8.6 | 0+90.5 | 0+53.5 | 26 | < 0.191 | < 0.047 | < 0.087 | < 0.063 | 0.733 | < 0.445 | < 0.238 | 1 | < 0.011235 | < |
| 8.6 | 0+89.5 | 0+49.5 | 27 | < 0.191 | < 0.035 | < 0.065 | < 0.070 | 1.410 | < 0.276 | < 0.060 | 1 | < 0.011235 | < |
| 8.6 | 0+87.5 | 0+44.5 | 28 | < 0.176 | < 0.052 | < 0.027 | < 0.073 | 0.305 | < 0.141 | < 0.201 | 1 | < 0.010353 | < |
| 8.6 | 0+84.5 | 0+38.5 | 29 | < 0.176 | < 0.055 | < 0.038 | < 0.081 | 0.771 | < 0.369 | < 0.091 | 1 | < 0.010353 | < |
| 8.6 | 0+83.5 | 0+34.5 | 30 | < 0.176 | < 0.048 | < 0.024 | < 0.058 | 0.184 | < 0.321 | < 0.068 | 1 | < 0.010353 | < |

ANSTEC
APERTURE
CARD

Also Available on
Aperture Card

CONCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| D-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| 0.087 < | 0.048 < | 0.035 | 0.003 < | 0.006 < | 0.048 | 0.240 |
| 0.063 < | 0.045 < | 0.036 | 0.000 < | 0.003 < | 0.081 | 0.239 |
| 0.046 < | 0.027 < | 0.038 | 0.000 < | 0.001 < | 0.045 | 0.170 |
| 0.071 < | 0.022 < | 0.040 | 0.000 < | 0.006 < | 0.065 | 0.217 |
| 0.071 < | 0.021 < | 0.037 | 0.000 < | 0.001 < | 0.030 | 0.173 |
| 0.041 < | 0.040 < | 0.036 | 0.005 < | 0.007 < | 0.049 | 0.191 |
| 0.052 < | 0.031 < | 0.031 | 0.000 < | 0.006 < | 0.051 | 0.184 |
| 0.053 < | 0.029 < | 0.037 | 0.000 < | 0.006 < | 0.126 | 0.263 |
| 0.053 < | 0.028 < | 0.037 | 0.000 < | 0.005 < | 0.052 | 0.188 |
| 0.036 < | 0.043 < | 0.039 | 0.000 < | 0.008 < | 0.066 | 0.205 |
| 0.046 < | 0.061 < | 0.033 | 0.000 < | 0.003 < | 0.083 | 0.239 |
| 0.047 < | 0.042 < | 0.037 | 0.000 < | 0.007 < | 0.074 | 0.218 |
| 0.048 < | 0.038 < | 0.042 | 0.000 < | 0.006 < | 0.078 | 0.223 |
| 0.043 < | 0.033 < | 0.042 | 0.000 < | 0.009 < | 0.374 | 0.511 |
| 0.104 < | 0.030 < | 0.038 | 0.000 < | 0.007 < | 0.089 | 0.280 |
| 0.055 < | 0.070 < | 0.035 | 0.000 < | 0.005 < | 0.039 | 0.215 |
| 0.046 < | 0.041 < | 0.044 | 0.000 < | 0.005 < | 0.116 | 0.264 |
| 0.047 < | 0.044 < | 0.044 | 0.068 < | 0.006 < | 0.102 | 0.321 |
| 0.066 < | 0.068 < | 0.032 | 0.000 < | 0.003 < | 0.061 | 0.240 |
| 0.089 < | 0.059 < | 0.036 | 0.000 < | 0.005 < | 0.083 | 0.282 |
| 0.478 < | 0.031 < | 0.032 | 0.237 < | 0.003 < | 0.107 | 0.905 |
| 0.057 < | 0.031 < | 0.044 | 0.000 < | 0.007 < | 0.054 | 0.203 |
| 0.104 < | 0.111 < | 0.037 | 0.000 < | 0.002 < | 0.062 | 0.326 |
| 0.127 < | 0.031 < | 0.030 | 0.000 < | 0.004 < | 0.045 | 0.249 |
| 0.101 < | 0.020 < | 0.032 | 0.000 < | 0.005 < | 0.064 | 0.234 |
| 0.052 < | 0.079 < | 0.035 | 0.000 < | 0.007 < | 0.119 | 0.303 |
| 0.039 < | 0.059 < | 0.039 | 0.042 < | 0.004 < | 0.030 | 0.225 |
| 0.058 < | 0.025 < | 0.040 | 0.000 < | 0.002 < | 0.101 | 0.236 |
| 0.062 < | 0.035 < | 0.045 | 0.000 < | 0.006 < | 0.045 | 0.203 |
| 0.053 < | 0.021 < | 0.032 | 0.000 < | 0.005 < | 0.034 | 0.156 |

TABLE 10.1-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:09 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
STORAGE TANK FOUNDATION - AREA 10.1 FOR UREM/POST REMEDIATION

RADIATION TYPE: GAMMA SURVEY IN UREM/HR
COMPLETION DATE: 10-10-94
TECHNICIANS: RW/DT/TA
LOCATION: 10.0
GRID ID: 10.1
MEDIA TYPE: CONCRETE
# of POINTS: 35

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | LIMIT |
|---|---|---|
| MAX: | 6.00 PASS | 10 |
| AVG: | 1.71 PASS | 5 |
| STD X: | 1.67 | |
| MU SUB ALPHA: | 2.19 PASS | 5 |

| ID # | GRID COORDINATES | INST. ID # | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|---|
| 10.1 | 0 | 10A | A | 6 | 8 | 8 | 2 |
| 10.1 | 0 | 10B | A | 6 | 9 | 8 | 3 |
| 10.1 | 0 | 10C | A | 6 | 10 | 8 | 4 |
| 10.1 | 10 | 20A | A | 6 | 7 | 8 | 1 |
| 10.1 | 10 | 20B | A | 6 | 8 | 8 | 2 |
| 10.1 | 10 | 20C | A | 6 | 7 | 8 | 1 |
| 10.1 | 20 | 30A | A | 6 | 7 | 8 | 1 |
| 10.1 | 20 | 30B | A | 6 | 12 | 8 | 6 |
| 10.1 | 30 | 40 | A | 6 | 9 | 8 | 3 |
| 10.1 | 40 | 50 | A | 6 | 7 | 8 | 1 |
| 10.1 | 50 | 60 | A | 6 | 6 | 8 | 0 |
| 10.1 | 60 | 70 | A | 6 | 10 | 8 | 4 |
| 10.1 | 70 | 80 | A | 6 | 7 | 8 | 1 |
| 10.1 | 80 | 90 | A | 6 | 6 | 8 | 0 |
| 10.1 | 90 | 100 | A | 6 | 8 | 8 | 2 |
| 10.1 | 100 | 110 | A | 6 | 10 | 8 | 4 |
| 10.1 | 110 | 120 | A | 6 | 5 | 8 | -1 |
| 10.1 | 120 | 130 | A | 6 | 6 | 8 | 0 |
| 10.1 | 130 | 140 | A | 6 | 8 | 8 | 2 |
| 10.1 | 140 | 150 | A | 6 | 5 | 8 | -1 |
| 10.1 | 150 | 160 | A | 6 | 7 | 8 | 1 |
| 10.1 | 160 | 170 | A | 6 | 6 | 8 | 0 |
| 10.1 | 170 | 180 | A | 6 | 7 | 8 | 1 |
| 10.1 | 180 | 190 | A | 6 | 7 | 8 | 1 |
| 10.1 | 190 | 200 | A | 6 | 8 | 8 | 2 |
| 10.1 | 200 | 210 | A | 6 | 8 | 8 | 2 |
| 10.1 | 210 | 220 | A | 6 | 9 | 8 | 3 |
| 10.1 | 220 | 230 | A | 6 | 7 | 8 | 1 |
| 10.1 | 230 | 240 | A | 6 | 7 | 8 | 1 |
| 10.1 | 240 | 250 | A | 6 | 6 | 8 | 0 |
| 10.1 | 250 | 260A | A | 6 | 7 | 8 | 1 |
| 10.1 | 250 | 260B | A | 6 | 7 | 8 | 1 |

ANSTEC
APERTURE
CARD

Also Available on
Aperture Card

TABLE 10.1-2

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 10.1 | 250 | 260B* | 3 | 461.3 | 674 | 0 | 0 | 8 | 1887 | 3913 +/- 968 | NA |
| 10.1 | 260 | 0A* | 3 | 461.3 | 729 | 0 | 0 | 8 | 1887 | 4925 +/-1004 | NA |
| 10.1 | 260 | 0B* | 3 | 461.3 | 650 | 0 | 0 | 8 | 1887 | 3471 +/- 951 | NA |
| 10.1 | 260 | 0C* | 3 | 461.3 | 809 | 0 | 0 | 8 | 1887 | 6396 +/-1054 | NA |

* : POST-REMEDIATION RESULTS

PRE REMEDIATION RESULTS

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 10.1 | 250 | 260A | 3 | 468.7 | 633 | 0 | 0 | 8 | 1902 | 3022 +/- 940 | NA |
| 10.1 | 250 | 260B | 3 | 468.7 | 683 | 0 | 0 | 8 | 1902 | 3942 +/- 974 | NA |
| 10.1 | 260 | 0A | 3 | 468.7 | 683 | 0 | 0 | 8 | 1902 | 3942 +/- 974 | NA |
| 10.1 | 260 | 0B | 3 | 468.7 | 715 | 0 | 0 | 8 | 1902 | 4531 +/- 995 | NA |
| 10.1 | 260 | 0C | 3 | 468.7 | 696 | 917 | 300 | 8 | 1902 | 4303 +/- 983 | 8247 |

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ANSTEC
APERTURE
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Also Available on
Aperture Card

TABLE 10.1-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:08 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
STORAGE TANK FOUNDATION - AREA 10.1 FOR BETA POST REMEDIATION

RADIATION TYPE: 1 BETA SCALING FACTOR = 0.3
COMPLETION DATE: 10-10-94
TECHNICIANS: RK/DT/TA
LOCATION: 10.0
GRID ID: 10.1
MEDIA TYPE: CONCRETE
# of POINTS: 35
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2
REM.+ FIXED:

| | | | LIMIT |
|---|---|---|---|
| MAX FOR IND GRID | 7548 | PASS | 13500 |
| AVG - SURVEY UNIT | 3680 | PASS | 13500 |
| STD X | 1160 | | |
| MU SUB ALPHA | 4012 | PASS | 13500 |
| MAX HOT SPOT | 0 | PASS | 40500 |

| ID # | GRID COORDINATES | | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ MINUTES | SCAN MAX BETA COUNTS | TOTAL CONT. AREA CM^2 | MATERIAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. BETA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 CM^2 TEST | INS CP |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 10.1 | 0 | 10A | 3 | 468.7 | 879 | 0 | 0 | 8 | 1902 | 7548 +/-1097 | NA | | 0 |
| 10.1 | 0 | 10B | 3 | 468.7 | 641 | 0 | 0 | 8 | 1902 | 3170 +/- 946 | NA | | 0 |
| 10.1 | 0 | 10C | 3 | 468.7 | 657 | 0 | 0 | 8 | 1902 | 3464 +/- 957 | NA | | 0 |
| 10.1 | 10 | 20A | 3 | 468.7 | 653 | 0 | 0 | 8 | 1902 | 3390 +/- 954 | NA | | 0 |
| 10.1 | 10 | 20B | 3 | 468.7 | 677 | 0 | 0 | 8 | 1902 | 3832 +/- 970 | NA | | 0 |
| 10.1 | 10 | 20C | 3 | 468.7 | 629 | 0 | 0 | 8 | 1902 | 2949 +/- 937 | NA | | 0 |
| 10.1 | 20 | 30A | 3 | 468.7 | 632 | 0 | 0 | 8 | 1902 | 3004 +/- 939 | NA | | 0 |
| 10.1 | 20 | 30B | 3 | 468.7 | 698 | 0 | 0 | 8 | 1902 | 4218 +/- 984 | NA | | 0 |
| 10.1 | 30 | 40 | 3 | 468.7 | 832 | 0 | 0 | 8 | 1902 | 6683 +/-1069 | NA | | 0 |
| 10.1 | 40 | 50 | 3 | 468.7 | 730 | 0 | 0 | 8 | 1902 | 4807 +/-1005 | NA | | 0 |
| 10.1 | 50 | 60 | 3 | 468.7 | 595 | 0 | 0 | 8 | 1902 | 2323 +/- 913 | NA | | 0 |
| 10.1 | 60 | 70 | 3 | 468.7 | 675 | 0 | 0 | 8 | 1902 | 3795 +/- 969 | NA | | 0 |
| 10.1 | 70 | 80 | 3 | 468.7 | 663 | 0 | 0 | 8 | 1902 | 3574 +/- 961 | NA | | 0 |
| 10.1 | 80 | 90 | 3 | 468.7 | 693 | 0 | 0 | 8 | 1902 | 4126 +/- 981 | NA | | 0 |
| 10.1 | 90 | 100 | 3 | 468.7 | 656 | 0 | 0 | 8 | 1902 | 3446 +/- 956 | NA | | 0 |
| 10.1 | 100 | 110 | 3 | 468.7 | 622 | 0 | 0 | 8 | 1902 | 2820 +/- 932 | NA | | 0 |
| 10.1 | 110 | 120 | 3 | 468.7 | 616 | 0 | 0 | 8 | 1902 | 2710 +/- 928 | NA | | 0 |
| 10.1 | 120 | 130 | 3 | 468.7 | 619 | 0 | 0 | 8 | 1902 | 2765 +/- 930 | NA | | 0 |
| 10.1 | 130 | 140 | 3 | 468.7 | 629 | 0 | 0 | 8 | 1902 | 2949 +/- 937 | NA | | 0 |
| 10.1 | 140 | 150 | 3 | 468.7 | 651 | 0 | 0 | 8 | 1902 | 3354 +/- 952 | NA | | 0 |
| 10.1 | 150 | 160 | 3 | 468.7 | 640 | 0 | 0 | 8 | 1902 | 3151 +/- 945 | NA | | 0 |
| 10.1 | 160 | 170 | 3 | 468.7 | 600 | 0 | 0 | 8 | 1902 | 2415 +/- 917 | NA | | 0 |
| 10.1 | 170 | 180 | 3 | 468.7 | 668 | 0 | 0 | 8 | 1902 | 3666 +/- 964 | NA | | 0 |
| 10.1 | 180 | 190 | 3 | 468.7 | 636 | 0 | 0 | 8 | 1902 | 3078 +/- 942 | NA | | 0 |
| 10.1 | 190 | 200 | 3 | 468.7 | 641 | 0 | 0 | 8 | 1902 | 3170 +/- 946 | NA | | 0 |
| 10.1 | 200 | 210 | 3 | 468.7 | 610 | 0 | 0 | 8 | 1902 | 2599 +/- 924 | NA | | 0 |
| 10.1 | 210 | 220 | 3 | 468.7 | 660 | 0 | 0 | 8 | 1902 | 3519 +/- 959 | NA | | 0 |
| 10.1 | 220 | 230 | 3 | 468.7 | 684 | 0 | 0 | 8 | 1902 | 3961 +/- 975 | NA | | 0 |
| 10.1 | 230 | 240 | 3 | 468.7 | 641 | 0 | 0 | 8 | 1902 | 3170 +/- 946 | NA | | 0 |
| 10.1 | 240 | 250 | 3 | 468.7 | 650 | 0 | 0 | 8 | 1902 | 3335 +/- 952 | NA | | 0 |
| 10.1 | 250 | 260 | 3 | 468.7 | 631 | 0 | 0 | 8 | 1902 | 3122 +/- 938 | NA | | 0 |

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TABLE 10.1-1

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 10.1 | 260 | 0A* | A | 6 | 8 | 8 | 2 |
| 10.1 | 260 | 0B* | A | 6 | 9 | 8 | 3 |
| 10.1 | 260 | 0C* | A | 6 | 12 | 8 | 6 |

* = POS-REMEDIATION RESULTS

PRE-REMEDIATION RESULTS

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 10.1 | 250 | 260A | A | 6 | 7 | 8 | 1 |
| 10.1 | 250 | 260B | A | 6 | 7 | 8 | 1 |
| 10.1 | 260 | 0A | A | 6 | 8 | 8 | 2 |
| 10.1 | 260 | 0B | A | 6 | 9 | 8 | 3 |
| 10.1 | 260 | 0C | A | 6 | 9 | 8 | 3 |

ANSTEC
APERTURE
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Also Available on
Aperture Card

TABLE 10.2-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:06 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 10.2 - STORAGE TANK EXCAVATION SOIL FOR SUM OF THE FRACTIONS

RADIATION TYPE: SOIL DATA FOR SUM OF THE FRACTIONS
COMPLETION DATE: 10-7-94
TECHNICIANS: TA/CD/PS
LOCATION: 10.0
GRID ID: 10.2
MEDIA TYPE: SOIL
# of POINTS: 40

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 0.62 | PASS | 1 |
| AVG | 0.26 | PASS | 1 |
| STD X | 0.09 | | |
| MU SUB ALPHA | 0.28 | PASS | 1 |

ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED) ISOTOPES OF

| ID # | GRID COORIDINATES OR OTHER ID S | W | SR-90 LIMIT 17 | CO-60 LIMIT 0.9 | AG-108M LIMIT 1.1 | CS-134 LIMIT 1.8 | CS-137 LIMIT 3.8 | CE-144 LIMIT 63 | EU-152 LIMIT 2 | SOIL CODE | SR-90 | C |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 10.2 | 0+57.5 | 1+27.5 | 0.611 | 0.085 | 0.075 | 0.063 | 1.810 | 0.447 | 0.194 | 1 | 0.035941 | < |
| 10.2 | 0+55 | 1+25 | 0.583 | 0.047 | 0.028 | 0.071 | 2.830 | 0.389 | 0.086 | 1 | 0.034294 | < |
| 10.2 | 0+57.5 | 1+22.5 | < 0.202 | 0.042 | 0.029 | 0.066 | 0.193 | 0.407 | 0.143 | 1 | < 0.011882 | < |
| 10.2 | 0+52.5 | 1+22.5 | < 0.202 | 0.060 | 0.042 | 0.064 | 0.447 | 0.245 | 0.176 | 1 | < 0.011882 | < |
| 10.2 | 0+45 | 1+25 | < 0.202 | 0.046 | 0.037 | 0.080 | 1.810 | 0.295 | 0.188 | 1 | < 0.011882 | < |
| 10.2 | 0+47.5 | 1+22.5 | < 0.202 | 0.073 | 0.044 | 0.056 | 0.582 | 0.444 | 0.078 | 1 | < 0.011882 | < |
| 10.2 | 0+42.5 | 1+22.5 | < 0.202 | 0.043 | 0.064 | 0.065 | 0.591 | 0.231 | 0.099 | 1 | < 0.011882 | < |
| 10.2 | 0+57.5 | 1+17.5 | < 0.203 | 0.049 | 0.037 | 0.058 | 0.386 | 0.424 | 0.186 | 1 | < 0.011941 | < |
| 10.2 | 0+52.5 | 1+17.5 | < 0.203 | 0.097 | 0.073 | 0.067 | 1.260 | 0.315 | 0.177 | 1 | < 0.011941 | < |
| 10.2 | 0+55 | 1+15 | < 0.203 | 0.026 | 0.027 | 0.045 | 0.152 | 0.217 | 0.132 | 1 | < 0.011941 | < |
| 10.2 | 0+57.5 | 1+12.5 | < 0.19 | 0.061 | 0.039 | 0.040 | 0.242 | 0.281 | 0.057 | 1 | < 0.011176 | < |
| 10.2 | 0+52.5 | 1+12.5 | < 0.16 | 0.041 | 0.030 | 0.053 | 0.103 | 0.391 | 0.151 | 1 | < 0.009412 | < |
| 10.2 | 0+47.5 | 1+17.5 | < 0.203 | 0.071 | 0.042 | 0.040 | 0.187 | 0.242 | 0.152 | 1 | < 0.011941 | < |
| 10.2 | 0+42.5 | 1+17.5 | < 0.201 | 0.067 | 0.045 | 0.063 | 0.194 | 0.370 | 0.131 | 1 | < 0.011824 | < |
| 10.2 | 0+45 | 1+15 | < 0.202 | 0.129 | 0.118 | 0.084 | 0.090 | 0.195 | 0.183 | 1 | < 0.011882 | < |
| 10.2 | 0+47.5 | 1+12.5 | < 0.193 | 0.042 | 0.019 | 0.071 | < 0.106 | 0.169 | 0.130 | 1 | < 0.011353 | < |
| 10.2 | 0+42.5 | 1+12.5 | < 0.202 | 0.050 | 0.050 | 0.053 | 0.252 | 0.360 | 0.137 | 1 | < 0.011882 | < |
| 10.2 | 0+57.5 | 1+7.5 | < 0.202 | 0.033 | 0.035 | 0.068 | 0.202 | 0.373 | 0.585 | 1 | < 0.011882 | < |
| 10.2 | 0+52.5 | 0+7.5 | < 0.202 | 0.044 | 0.036 | 0.061 | < 0.033 | 0.413 | 0.125 | 1 | < 0.011882 | < |
| 10.2 | 0+55 | 1+05 | < 0.202 | 0.089 | 0.047 | 0.059 | 0.219 | 0.243 | 0.068 | 1 | < 0.011882 | < |
| 10.2 | 0+57.5 | 1+2.5 | 0.346 | 0.102 | 0.028 | 0.075 | 0.589 | 0.329 | 0.212 | 1 | 0.020353 | < |
| 10.2 | 0+52.5 | 1+2.5 | < 0.193 | 0.064 | 0.043 | 0.068 | < 0.063 | 0.298 | 0.108 | 1 | < 0.011353 | < |
| 10.2 | 0+47.5 | 1+7.5 | < 0.202 | 0.073 | 0.048 | 0.066 | < 0.076 | 0.353 | 0.166 | 1 | < 0.011882 | < |
| 10.2 | 0+42.5 | 1+7.5 | < 0.193 | 0.059 | 0.035 | 0.061 | 0.213 | 0.398 | 0.096 | 1 | < 0.011353 | < |
| 10.2 | 0+45 | 1+5 | < 0.19 | 0.095 | 0.051 | 0.067 | < 0.129 | 0.327 | 0.121 | 1 | < 0.011176 | < |
| 10.2 | 0+47.5 | 1+2.5 | < 0.193 | 0.042 | 0.040 | 0.058 | < 0.129 | 0.431 | 0.130 | 1 | < 0.011353 | < |
| 10.2 | 0+42.5 | 1+2.5 | 0.246 | 0.076 | 0.050 | 0.064 | 0.215 | 0.368 | 0.120 | 1 | 0.014471 | < |
| 10.2 | 0+57.5 | 0+97.5 | < 0.202 | 0.044 | 0.059 | 0.062 | < 0.122 | 0.316 | 0.212 | 1 | < 0.011882 | < |
| 10.2 | 0+52.5 | 0+97.5 | < 0.16 | 0.052 | 0.021 | 0.059 | < 0.064 | 0.387 | 0.114 | 1 | < 0.009412 | < |
| 10.2 | 0+47.5 | 0+97.5 | < 0.16 | 0.059 | 0.039 | 0.070 | < 0.087 | 0.363 | 0.169 | 1 | < 0.009412 | < |
| 10.2 | 0+45 | 0+95 | < 0.16 | 0.034 | 0.033 | 0.048 | < 0.039 | 0.314 | 0.127 | 1 | < 0.009412 | < |
| 10.2 | 0+42.5 | 0+92.5 | < 0.16 | 0.049 | 0.030 | 0.060 | < 0.043 | 0.373 | 0.129 | 1 | < 0.009412 | < |

CONCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| O-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| 0.094 < | 0.068 < | 0.035 | 0.147 < | 0.007 < | 0.097 | 0.484 |
| 0.052 < | 0.025 < | 0.040 | 0.416 < | 0.006 < | 0.043 | 0.617 |
| 0.047 < | 0.027 < | 0.036 | 0.000 < | 0.006 < | 0.072 | 0.200 |
| 0.067 < | 0.038 < | 0.035 | 0.000 < | 0.00[illegible] < | 0.088 | 0.244 |
| 0.051 < | 0.034 < | 0.045 | 0.147 < | 0.005 < | 0.094 | 0.387 |
| 0.081 < | 0.040 < | 0.031 | 0.000 < | 0.007 < | 0.039 | 0.211 |
| 0.048 < | 0.059 < | 0.036 | 0.000 < | 0.004 < | 0.050 | 0.207 |
| 0.055 < | 0.034 < | 0.032 | 0.000 < | 0.007 < | 0.093 | 0.232 |
| 0.108 < | 0.066 < | 0.037 | 0.003 < | 0.005 < | 0.089 | 0.320 |
| 0.029 < | 0.025 < | 0.025 | 0.000 < | 0.003 < | 0.066 | 0.160 |
| 0.068 < | 0.036 < | 0.022 | 0.000 < | 0.004 < | 0.028 | 0.170 |
| 0.046 < | 0.027 < | 0.030 | 0.000 < | 0.006 < | 0.076 | 0.194 |
| 0.079 < | 0.039 < | 0.022 | 0.000 < | 0.004 < | 0.076 | 0.231 |
| 0.074 < | 0.041 < | 0.035 | 0.000 < | 0.006 < | 0.066 | 0.233 |
| 0.143 < | 0.107 < | 0.047 | 0.000 < | 0.003 < | 0.092 | 0.404 |
| 0.047 < | 0.017 < | 0.039 < | 0.000 < | 0.003 < | 0.065 | 0.182 |
| 0.055 < | 0.045 < | 0.029 | 0.000 < | 0.006 < | 0.069 | 0.215 |
| 0.036 < | 0.032 < | 0.038 | 0.000 < | 0.006 < | 0.293 | 0.417 |
| 0.048 < | 0.032 < | 0.034 < | 0.000 < | 0.007 < | 0.063 | 0.195 |
| 0.099 < | 0.043 < | 0.033 | 0.000 < | 0.004 < | 0.034 | 0.225 |
| 0.113 < | 0.025 < | 0.041 | 0.000 < | 0.005 < | 0.106 | 0.312 |
| 0.071 < | 0.039 < | 0.038 < | 0.000 < | 0.005 < | 0.054 | 0.218 |
| 0.081 < | 0.044 < | 0.037 < | 0.000 < | 0.006 < | 0.083 | 0.262 |
| 0.065 < | 0.032 < | 0.034 | 0.000 < | 0.006 < | 0.048 | 0.197 |
| 0.106 < | 0.047 < | 0.037 < | 0.000 < | 0.005 < | 0.061 | 0.266 |
| 0.047 < | 0.036 < | 0.032 < | 0.000 < | 0.007 < | 0.065 | 0.199 |
| 0.084 < | 0.045 < | 0.035 | 0.000 < | 0.006 < | 0.060 | 0.245 |
| 0.048 < | 0.054 < | 0.034 < | 0.000 < | 0.005 < | 0.106 | 0.259 |
| 0.058 < | 0.019 < | 0.033 < | 0.000 < | 0.006 < | 0.057 | 0.183 |
| 0.066 < | 0.035 < | 0.039 < | 0.000 < | 0.006 < | 0.085 | 0.240 |
| 0.038 < | 0.030 < | 0.027 < | 0.000 < | 0.005 < | 0.064 | 0.173 |
| 0.055 < | 0.028 < | 0.033 < | 0.000 < | 0.006 < | 0.065 | 0.195 |

ANSTEC APERTURE CARD

Also Available on Aperture Card

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:10 AM

FINAL SURVEY DATA SHEET

DATA FOR UNAFFECTED AREA DESCRIPTION:

STORAGE TANK EXCAVATION - AREA 10.2 FOR UREM/HR

RADIATION TYPE: GAMMA SURVEY IN UREM/HR

COMPLETION DATE: 10-7-94

TECHNICIANS: TA/CD/PS

LOCATION: 10.0

GRID ID: 10.2

MEDIA TYPE: SOIL

# of POINTS: 34

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | | LIMIT |
|---|---|---|---|
| MAX: | 5.00 | PASS | 10 |
| AVG: | 0.26 | PASS | 5 |
| STD X: | 1.36 | | |
| MU SUB ALPHA: | 0.66 | PASS | 5 |

| ID # | GRID POINT S | GRID POINT W | INST. ID # | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|---|---|
| 10.2 | 0+57.5 | 1+27.5 | A | 6 | 7 | 8 | 1 |
| 10.2 | 0+55 | 1+25 | A | 6 | 6 | 8 | 0 |
| 10.2 | 0+57.5 | 1+22.5 | A | 6 | 7 | 8 | 1 |
| 10.2 | 0+52.5 | 1+22.5 | A | 6 | 6 | 8 | 0 |
| 10.2 | 0+45 | 1+25 | A | 6 | 6 | 8 | 0 |
| 10.2 | 0+47.5 | 1+22.5 | A | 6 | 7 | 8 | 1 |
| 10.2 | 0+42.5 | 1+22.5 | A | 6 | 6 | 8 | 0 |
| 10.2 | 0+57.5 | 1+17.5 | A | 6 | 5 | 8 | -1 |
| 10.2 | 0+52.5 | 1+17.5 | A | 6 | 5 | 8 | -1 |
| 10.2 | 0+55 | 1+15 | A | 6 | 7 | 8 | 1 |
| 10.2 | 0+57.5 | 1+12.5 | A | 6 | 5 | 8 | -1 |
| 10.2 | 0+52.5 | 1+12.5 | A | 6 | 5 | 8 | -1 |
| 10.2 | 0+47.5 | 1+17.5 | A | 6 | 6 | 8 | 0 |
| 10.2 | 0+42.5 | 1+17.5 | A | 6 | 5 | 8 | -1 |
| 10.2 | 0+45 | 1+15 | A | 6 | 6 | 8 | 0 |
| 10.2 | 0+47.5 | 1+12.5 | A | 6 | 7 | 8 | 1 |
| 10.2 | 0+42.5 | 1+12.5 | A | 6 | 5 | 8 | -1 |
| 10.2 | 0+57.5 | 1+7.5 | A | 6 | 5 | 8 | -1 |
| 10.2 | 0+52.5 | 0+7.5 | A | 6 | 8 | 8 | 2 |
| 10.2 | 0+55 | 1+05 | A | 6 | 7 | 8 | 1 |
| 10.2 | 0+57.5 | 1+2.5 | A | 6 | 6 | 8 | 0 |
| 10.2 | 0+52.5 | 1+2.5 | A | 6 | 6 | 8 | 0 |
| 10.2 | 0+47.5 | 1+7.5 | A | 6 | 5 | 8 | -1 |
| 10.2 | 0+42.5 | 1+7.5 | A | 6 | 6 | 8 | 0 |
| 10.2 | 0+45 | 1+5 | A | 6 | 6 | 8 | 0 |
| 10.2 | 0+47.5 | 1+2.5 | A | 6 | 6 | 8 | 0 |
| 10.2 | 0+42.5 | 1+2.5 | A | 6 | 5 | 8 | -1 |
| 10.2 | 0+57.5 | 0+97.5 | A | 6 | 6 | 8 | 0 |
| 10.2 | 0+52.5 | 0+97.5 | A | 6 | 7 | 8 | 1 |
| 10.2 | 0+47.5 | 0+97.5 | A | 6 | 7 | 8 | 1 |
| 10.2 | 0+45 | 0+95 | A | 6 | 10 | 8 | 4 |
| 10.2 | 0+42.5 | 0+92.5 | A | 6 | 11 | 8 | 5 |
| 10.2 | 0+37.5 | 0+87.5 | A | 6 | 6 | 8 | 0 |
| 10.2 | 0+32.5 | 0+87.5 | A | 6 | 5 | 8 | -1 |

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R A TABLE 10.1-3

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:07 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
STORAGE TANK FOUNDATION - AREA 10.1 FOR ALPHA POST REMEDIATION

RADIATION TYPE: 2 ALPHA
COMPLETION
DATE: 10-10-94
TECHNICIANS: RW/DT/TA
LOCATION: 10.0
GRID ID: 10.1
MEDIA TYPE: CONCRETE
# of POINTS: 35
CT IN MINUTES: 1

MATERIAL CODE
1:CONCRETE 5:PLASTIC
2:ROCK 6:SOIL
3:WOOD 7:ASPHALT
4:METAL 8:OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | LIMIT |
|---|---|---|
| MAX FOR IND GRID | 69 PASS | 5000 |
| AVG - SURVEY UNIT | 23 PASS | 5000 |
| STD X | 20 | |
| MU SUB ALPHA | 29 PASS | 5000 |
| MAX HOT SPOT | 0 PASS | 15000 |

| ID # | GRID COORDINATES W | S | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | SCAN MAX ALPHA COUNTS | TOTAL CONT. AREA CM^2 | MATER-IAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. ALPHA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 MAX CM^2 TEST | IN C |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 10.1 | 0 | 10A | 3 | 0.7 | 4 | 0 | 0 | 8 | 34 | 17 +/- 20 | | NA | |
| 10.1 | 0 | 10B | 3 | 0.7 | 11 | 0 | 0 | 8 | 34 | 53 +/- 34 | | NA | |
| 10.1 | 0 | 10C | 3 | 0.7 | 10 | 0 | 0 | 8 | 34 | 48 +/- 32 | | NA | |
| 10.1 | 10 | 20A | 3 | 0.7 | 6 | 0 | 0 | 8 | 34 | 27 +/- 25 | | NA | |
| 10.1 | 10 | 20B | 3 | 0.7 | 13 | 0 | 0 | 8 | 34 | 64 +/- 37 | | NA | |
| 10.1 | 10 | 20C | 3 | 0.7 | 5 | 0 | 0 | 8 | 34 | 22 +/- 23 | | NA | |
| 10.1 | 20 | 30A | 3 | 0.7 | 3 | 0 | 0 | 8 | 34 | 12 +/- 18 | | NA | |
| 10.1 | 20 | 30B | 3 | 0.7 | 14 | 0 | 0 | 8 | 34 | 69 +/- 38 | | NA | |
| 10.1 | 30 | 40 | 3 | 0.7 | 9 | 0 | 0 | 8 | 34 | 43 +/- 30 | | NA | |
| 10.1 | 40 | 50 | 3 | 0.7 | 4 | 0 | 0 | 8 | 34 | 17 +/- 20 | | NA | |
| 10.1 | 50 | 60 | 3 | 0.7 | 5 | 0 | 0 | 8 | 34 | 22 +/- 23 | | NA | |
| 10.1 | 60 | 70 | 3 | 0.7 | 14 | 0 | 0 | 8 | 34 | 69 +/- 38 | | NA | |
| 10.1 | 70 | 80 | 3 | 0.7 | 4 | 0 | 0 | 8 | 34 | 17 +/- 20 | | NA | |
| 10.1 | 80 | 90 | 3 | 0.7 | 4 | 0 | 0 | 8 | 34 | 17 +/- 20 | | NA | |
| 10.1 | 90 | 100 | 3 | 0.7 | 6 | 0 | 0 | 8 | 34 | 27 +/- 25 | | NA | |
| 10.1 | 100 | 110 | 3 | 0.7 | 2 | 0 | 0 | 8 | 34 | 7 +/- 15 | | NA | |
| 10.1 | 110 | 120 | 3 | 0.7 | 2 | 0 | 0 | 8 | 34 | 7 +/- 15 | | NA | |
| 10.1 | 120 | 130 | 3 | 0.7 | 1 | 0 | 0 | 8 | 34 | 2 +/- 10 | | NA | |
| 10.1 | 130 | 140 | 3 | 0.7 | 5 | 0 | 0 | 8 | 34 | 22 +/- 23 | | NA | |
| 10.1 | 140 | 150 | 3 | 0.7 | 0 | 0 | 0 | 8 | 34 | -4 +/- 3 | | NA | |
| 10.1 | 150 | 160 | 3 | 0.7 | 3 | 0 | 0 | 8 | 34 | 12 +/- 18 | | NA | |
| 10.1 | 160 | 170 | 3 | 0.7 | 1 | 0 | 0 | 8 | 34 | 2 +/- 10 | | NA | |
| 10.1 | 170 | 180 | 3 | 0.7 | 5 | 0 | 0 | 8 | 34 | 22 +/- 23 | | NA | |
| 10.1 | 180 | 190 | 3 | 0.7 | 2 | 0 | 0 | 8 | 34 | 7 +/- 15 | | NA | |
| 10.1 | 190 | 200 | 3 | 0.7 | 0 | 0 | 0 | 8 | 34 | -4 +/- 3 | | NA | |
| 10.1 | 200 | 210 | 3 | 0.7 | 1 | 0 | 0 | 8 | 34 | 2 +/- 10 | | NA | |
| 10.1 | 210 | 220 | 3 | 0.7 | 7 | 0 | 0 | 8 | 34 | 33 +/- 27 | | NA | |
| 10.1 | 220 | 230 | 3 | 0.7 | 11 | 0 | 0 | 8 | 34 | 53 +/- 34 | | NA | |
| 10.1 | 230 | 240 | 3 | 0.7 | 9 | 0 | 0 | 8 | 34 | 43 +/- 30 | | NA | |
| 10.1 | 240 | 250 | 3 | 0.7 | 4 | 0 | 0 | 8 | 34 | 17 +/- 20 | | NA | |
| 10.1 | 250 | 260* | 4 | 0.7 | 3 | 0 | 0 | 8 | 33 | 11 +/- 17 | | NA | |

ST EFF.
PM/DPM

.1937
.1937
.1937

TABLE 10.1-3

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 10.1 | 250 | 260B* | 4 | 0.7 | 4 | 0 | 0 | 8 | 33 | 16 +/- 20 | NA |
| 10.1 | 260 | 0A* | 4 | 0.7 | 5 | 0 | 0 | 8 | 33 | 21 +/- 22 | NA |
| 10.1 | 260 | 0B* | 4 | 0.7 | 2 | 0 | 0 | 8 | 33 | 6 +/- 14 | NA |
| 10.1 | 260 | 0C* | 4 | 0.7 | 3 | 0 | 0 | 8 | 33 | 11 +/- 17 | NA |

* : POST-REMEDIATION RESULTS

PRE-REMEDIATION RESULTS

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 10.1 | 250 | 260A | 3 | 0.7 | 5 | 0 | 0 | 8 | 34 | 22 +/- [illegible] | NA |
| 10.1 | 250 | 260B | 3 | 0.7 | 11 | 0 | 0 | 8 | 34 | 53 +/- 34 | NA |
| 10.1 | 260 | 0A | 3 | 0.7 | 5 | 0 | 0 | 8 | 34 | 22 +/- 23 | NA |
| 10.1 | 260 | 0B | 3 | 0.7 | 7 | 0 | 0 | 8 | 34 | 33 +/- 27 | NA |
| 10.1 | 260 | 0C | 3 | 0.7 | 4 | 7 | 300 | 8 | 34 | 18 +/- 20 | 33 |

0.2015
0.2015
0.2015
0.2015

0.1937
0.1937
0.1937
0.1937
0.1937

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TABLE 10.2-2

| | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 10.2 | 0+37.5 | 0+87.5 | < | 0.16 | < | 0.036 | < | 0.030 | < | 0.063 | < | 0.070 | < | 0.415 | < | 0.137 | 1 | < | 0.009412 | < |
| 10.2 | 0+32.5 | 0+87.5 | < | 0.202 | < | 0.037 | < | 0.035 | < | 0.063 | < | 0.050 | < | 0.149 | < | 0.133 | 1 | < | 0.011882 | < |
| 10.2 | BG | 0+51.5 | 1+11.5 | | 0.738 | < | 0.057 | < | 0.034 | < | 0.051 | < | 0.052 | < | 0.098 | < | 0.118 | 1 | | 0.043412 | < |
| 10.2 | BG | 0+50+1FT | 1+10+3F | | 0.501 | < | 0.080 | < | 0.052 | < | 0.056 | | 0.082 | < | 0.321 | < | 0.113 | 1 | | 0.029471 | < |
| 10.2 | BG | 1+10-2FT | 0+50+1F | | 0.344 | < | 0.055 | < | 0.045 | < | 0.081 | < | 0.063 | < | 0.291 | < | 0.136 | 1 | | 0.020235 | < |
| 10.2 | BG | 1+10+1FT | 0+50+2F | | 0.484 | < | 0.072 | < | 0.070 | < | 0.056 | < | 0.108 | < | 0.218 | < | 0.158 | 1 | | 0.028471 | < |
| 10.2 | BG | 1+10+1FT | 0+50 | < | 0.19 | < | 0.078 | < | 0.026 | < | 0.063 | < | 0.066 | < | 0.174 | < | 0.081 | 1 | < | 0.011176 | < |
| 10.2 | BG | 1+10-1FT | 0+50+1F | | 0.857 | < | 0.138 | < | 0.086 | < | 0.075 | < | 0.100 | < | 0.312 | < | 0.079 | 1 | | 0.050412 | < |

| | | | | | | |
|---|---|---|---|---|---|---|
| 0.040 < | 0.027 < | 0.035 < | 0.000 < | 0.007 < | 0.069 | 0.187 |
| 0.041 < | 0.031 < | 0.035 < | 0.000 < | 0.002 < | 0.067 | 0.188 |
| 0.063 < | 0.030 < | 0.028 < | 0.000 < | 0.002 < | 0.059 | 0.226 |
| 0.089 < | 0.047 < | 0.031 | 0.000 < | 0.005 < | 0.057 | 0.258 |
| 0.062 < | 0.041 < | 0.045 < | 0.000 < | 0.005 < | 0.068 | 0.240 |
| 0.080 < | 0.064 < | 0.031 < | 0.000 < | 0.003 < | 0.079 | 0.285 |
| 0.086 < | 0.024 < | 0.035 < | 0.000 < | 0.003 < | 0.040 | 0.199 |
| 0.153 < | 0.078 < | 0.041 < | 0.000 < | 0.005 < | 0.040 | 0.368 |

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Aperture Card

TABLE 11.1-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:18 AM

FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
COOLING TOWER AREA 11.1 FOR UREM

RADIATION TYPE: GAMMA SURVEY IN UREM/HR
COMPLETION DATE: 10-27-94
TECHNICIANS: JB/PK
LOCATION: 11.0
GRID ID: 11.1
MEDIA TYPE: WOOD, CONC., METAL, PLAS.
# of POINTS: 38

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | LIMIT |
|---|---|---|
| MAX | 6.00 PASS | 10 |
| AVG | 1.24 PASS | 5 |
| STD X | 1.78 | |
| RU SUB ALPHA | 1.72 PASS | 5 |

| ID # | INST. ID # | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|
| 11.1 | 1 | A | 6 | 6 | 8 | 0 |
| 11.1 | 2 | A | 6 | 8 | 8 | 2 |
| 11.1 | 3 | A | 6 | 5 | 8 | -1 |
| 11.1 | 4 | A | 6 | 4 | 8 | -2 |
| 11.1 | 5 | A | 6 | 7 | 8 | 1 |
| 11.1 | 6 | A | 6 | 7 | 8 | 1 |
| 11.1 | 7 | A | 6 | 9 | 8 | 3 |
| 11.1 | 8 | A | 6 | 7 | 8 | 1 |
| 11.1 | 9 | A | 6 | 8 | 8 | 2 |
| 11.1 | 10 | A | 6 | 6 | 8 | 0 |
| 11.1 | 11 | A | 6 | 6 | 8 | 0 |
| 11.1 | 12 | A | 6 | 7 | 8 | 1 |
| 11.1 | 13 | A | 6 | 6 | 8 | 0 |
| 11.1 | 14 | A | 6 | 6 | 8 | 0 |
| 11.1 | 15 | A | 6 | 6 | 8 | 0 |
| 11.1 | 16 | A | 6 | 7 | 8 | 1 |
| 11.1 | 17 | A | 6 | 5 | 8 | -1 |
| 11.1 | 18 | A | 6 | 4 | 8 | -2 |
| 11.1 | 19 | A | 6 | 6 | 8 | 0 |
| 11.1 | 20 | A | 6 | 7 | 8 | 1 |
| 11.1 | 21 | A | 6 | 5 | 8 | -1 |
| 11.1 | 22 | A | 6 | 8 | 8 | 2 |
| 11.1 | 23 | A | 6 | 12 | 8 | 6 |
| 11.1 | 24 | A | 6 | 9 | 8 | 3 |
| 11.1 | 25 | A | 6 | 10 | 8 | 4 |
| 11.1 | 26 | A | 6 | 9 | 8 | 3 |
| 11.1 | 27 | A | 6 | 9 | 8 | 3 |
| 11.1 | 28 | A | 6 | 8 | 8 | 2 |
| 11.1 | 29 | A | 6 | 9 | 8 | 3 |
| 11.1 | 30 | A | 6 | 7 | 8 | 1 |
| 11.1 | *31 | A | 6 | 9 | 8 | 3 |
| 11.1 | *32 | A | 6 | 8 | 8 | 2 |

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Aperture Card

TABLE 11.1-1

| | | | | | | |
|---|---|---|---|---|---|---|
| 11.1 | #33 | A | 6 | 5 | 8 | -1 |
| 11.1 | #34 | A | 6 | 7 | 8 | 1 |
| 11.1 | #35 | A | 6 | 6 | 8 | 0 |
| 11.1 | #36 | A | 6 | 8 | 8 | 2 |
| 11.1 | #37 | A | 6 | 9 | 8 | 3 |
| 11.1 | #38 | A | 6 | 10 | 8 | 4 |

# = BIASED LOCATIONS-

ANSTEC
APERTURE
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CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:17 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
COOLING TOWER STACK AREA 11.1 FOR BETA

RADIATION TYPE: 1 (1=BETA, 2=ALPHA)
COMPLETION -
DATE: 10-26-94
TECHNICIANS: JB/DR/PK
LOCATION: 11.0
GRID ID: 11.1
MEDIA TYPE: WOOD, CONC., METAL, PLAS.
# of POINTS: 38
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | | LIMIT | |
|---|---|---|---|---|
| MAX | 3890 | PASS | 40500 | BETA SCALING FACTOR = 0.3 |
| AVG | -58 | PASS | 13500 | |
| STD X | 1158 | | | |
| MU SUB ALPHA | 259 | PASS | 13500 | |

| ID # | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | BETA FIXED GCPM | MATER-IAL CODE | MDA DPM | BETA FIXED DPM/ 100 CM^2 | STAT SIG ? | BETA EFF CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| 11.1 | 1 | 422.7 | 386 | 386 | 8 | 1836 | -685 | N | 0.1785 |
| 11.1 | 2 | 422.7 | 363 | 363 | 8 | 1836 | -1115 | N | 0.1785 |
| 11.1 | 3 | 422.7 | 450 | 450 | 8 | 1836 | 510 | N | 0.1785 |
| 11.1 | 4 | 422.7 | 413 | 413 | 8 | 1836 | -181 | N | 0.1785 |
| 11.1 | 5 | 422.7 | 431 | 431 | 8 | 1836 | 155 | N | 0.1785 |
| 11.1 | 6 | 422.7 | 430 | 430 | 8 | 1836 | 136 | N | 0.1785 |
| 11.1 | 7 | 422.7 | 426 | 426 | 8 | 1836 | 62 | N | 0.1785 |
| 11.1 | 8 | 422.7 | 398 | 398 | 8 | 1836 | -461 | N | 0.1785 |
| 11.1 | 9 | 422.7 | 423 | 423 | 8 | 1836 | 6 | N | 0.1785 |
| 11.1 | 10 | 422.7 | 443 | 443 | 8 | 1836 | 379 | N | 0.1785 |
| 11.1 | 11 | 422.7 | 378 | 378 | 8 | 1836 | -835 | N | 0.1785 |
| 11.1 | 12 | 422.7 | 365 | 365 | 8 | 1836 | -1077 | N | 0.1785 |
| 11.1 | 13 | 422.7 | 359 | 359 | 8 | 1836 | -1190 | N | 0.1785 |
| 11.1 | 14 | 422.7 | 412 | 412 | 8 | 1836 | -200 | N | 0.1785 |
| 11.1 | 15 | 422.7 | 355 | 355 | 8 | 1836 | -1264 | N | 0.1785 |
| 11.1 | 16 | 422.7 | 376 | 376 | 8 | 1836 | -872 | N | 0.1785 |
| 11.1 | 17 | 422.7 | 359 | 359 | 8 | 1836 | -1190 | N | 0.1785 |
| 11.1 | 18 | 422.7 | 363 | 363 | 8 | 1836 | -1115 | N | 0.1785 |
| 11.1 | 19 | 422.7 | 392 | 392 | 8 | 1836 | -573 | N | 0.1785 |
| 11.1 | 20 | 422.7 | 349 | 349 | 8 | 1836 | -1376 | N | 0.1785 |
| 11.1 | 21 | 422.7 | 631 | 631 | 8 | 1836 | 3890 | Y | 0.1785 |
| 11.1 | 22 | 422.7 | 387 | 387 | 8 | 1836 | -667 | N | 0.1785 |
| 11.1 | 23 | 422.7 | 369 | 369 | 8 | 1836 | -1003 | N | 0.1785 |
| 11.1 | 24 | 422.7 | 432 | 432 | 8 | 1836 | 174 | N | 0.1785 |
| 11.1 | 25 | 422.7 | 427 | 427 | 8 | 1836 | 80 | N | 0.1785 |
| 11.1 | 26 | 422.7 | 453 | 453 | 8 | 1836 | 566 | N | 0.1785 |
| 11.1 | 27 | 422.7 | 463 | 463 | 8 | 1836 | 753 | N | 0.1785 |
| 11.1 | 28 | 422.7 | 519 | 519 | 8 | 1836 | 1798 | N | 0.1785 |
| 11.1 | 29 | 422.7 | 562 | 562 | 8 | 1836 | 2601 | Y | 0.1785 |
| 11.1 | 30 | 422.7 | 508 | 508 | 8 | 1836 | 1693 | N | 0.1785 |

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CARD

Also Available on
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TABLE 11.1-2

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 11.1 | #31 | 6 | 397.9 | 330 | 330 | 8 | 1747 | -1268 N | 0.1822 |
| 11.1 | #32 | 6 | 397.9 | 428 | 428 | 8 | 1747 | 562 N | 0.1822 |
| 11.1 | #33 | 6 | 397.9 | 363 | 363 | 8 | 1747 | -652 N | 0.1822 |
| 11.1 | #34 | 6 | 397.9 | 344 | 344 | 8 | 1747 | -1007 N | 0.1822 |
| 11.1 | #35 | 6 | 397.9 | 448 | 448 | 8 | 1747 | 936 N | 0.1822 |
| 11.1 | #36 | 6 | 397.9 | 455 | 455 | 8 | 1747 | 1066 N | 0.1822 |
| 11.1 | #37 | 6 | 397.9 | 417 | 417 | 8 | 1747 | 357 N | 0.1822 |
| 11.1 | #38 | 6 | 397.9 | 339 | 339 | 8 | 1747 | -1100 N | 0.1822 |

# : BIASED LOCATIONS

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TABLE 11.1-3

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:16 AM
FINAL SURVEY DATA SHEET
DATA FOR UNAFFECTED AREA DESCRIPTION:
COOLING TOWER AREA 11.1 FOR ALPHA

RADIATION TYPE: 2 (1=BETA, 2=ALPHA)
COMPLETION
DATE: 10-27-94
TECHNICIANS: JB/PX
LOCATION: 11.0
GRID ID: 11.1
MEDIA TYPE: WOOD, CONC,METAL PLAS.
# of POINTS: 38
CT IN MINUTES: 1

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

DPM/100CM^2
REM.: FIXED: LIMIT
MAX 66 PASS 15000
AVG 23 PASS 5000
STD X 16
MU SUB ALPHA 27 PASS 5000

| ID # | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | ALPHA FIXED GCPM | MATER-IAL CODE | MDA DPM/ 100 CM^2 | ALPHA FIXED DPM/ 100 CM^2 | STAT SIG ? | ALPHA EFF CPM/DPM |
|---|---|---|---|---|---|---|---|---|---|
| 11.1 | 1 | 4 | 0.7 | 8 | 8 | 8 | 33 | 36 Y | 0.2015 |
| 11.1 | 2 | 4 | 0.7 | 4 | 4 | 8 | 33 | 16 N | 0.2015 |
| 11.1 | 3 | 4 | 0.7 | 9 | 9 | 8 | 33 | 41 Y | 0.2015 |
| 11.1 | 4 | 4 | 0.7 | 6 | 6 | 8 | 33 | 26 N | 0.2015 |
| 11.1 | 5 | 4 | 0.7 | 7 | 7 | 8 | 33 | 31 N | 0.2015 |
| 11.1 | 6 | 4 | 0.7 | 7 | 7 | 8 | 33 | 31 N | 0.2015 |
| 11.1 | 7 | 4 | 0.7 | 7 | 7 | 8 | 33 | 31 N | 0.2015 |
| 11.1 | 8 | 4 | 0.7 | 10 | 10 | 8 | 33 | 46 Y | 0.2015 |
| 11.1 | 9 | 4 | 0.7 | 11 | 11 | 8 | 33 | 51 Y | 0.2015 |
| 11.1 | 10 | 4 | 0.7 | 7 | 7 | 8 | 33 | 31 N | 0.2015 |
| 11.1 | 11 | 4 | 0.7 | 1 | 1 | 8 | 33 | 1 N | 0.2015 |
| 11.1 | 12 | 4 | 0.7 | 3 | 3 | 8 | 33 | 11 N | 0.2015 |
| 11.1 | 13 | 4 | 0.7 | 2 | 2 | 8 | 33 | 6 N | 0.2015 |
| 11.1 | 14 | 4 | 0.7 | 3 | 3 | 8 | 33 | 11 N | 0.2015 |
| 11.1 | 15 | 4 | 0.7 | 3 | 3 | 8 | 33 | 11 N | 0.2015 |
| 11.1 | 16 | 4 | 0.7 | 1 | 1 | 8 | 33 | 1 N | 0.2015 |
| 11.1 | 17 | 4 | 0.7 | 3 | 3 | 8 | 33 | 11 N | 0.2015 |
| 11.1 | 18 | 4 | 0.7 | 3 | 3 | 8 | 33 | 11 N | 0.2015 |
| 11.1 | 19 | 4 | 0.7 | 2 | 2 | 8 | 33 | 6 N | 0.2015 |
| 11.1 | 20 | 4 | 0.7 | 4 | 4 | 8 | 33 | 16 N | 0.2015 |
| 11.1 | 21 | 4 | 0.7 | 10 | 10 | 8 | 33 | 46 Y | 0.2015 |
| 11.1 | 22 | 4 | 0.7 | 8 | 8 | 8 | 33 | 36 Y | 0.2015 |
| 11.1 | 23 | 4 | 0.7 | 1 | 1 | 8 | 33 | 1 N | 0.2015 |
| 11.1 | 24 | 4 | 0.7 | 4 | 4 | 8 | 33 | 16 N | 0.2015 |
| 11.1 | 25 | 4 | 0.7 | 5 | 5 | 8 | 33 | 21 N | 0.2015 |
| 11.1 | 26 | 4 | 0.7 | 14 | 14 | 8 | 33 | 66 Y | 0.2015 |
| 11.1 | 27 | 4 | 0.7 | 1 | 1 | 8 | 33 | 1 N | 0.2015 |
| 11.1 | 28 | 4 | 0.7 | 10 | 10 | 8 | 33 | 46 Y | 0.2015 |
| 11.1 | 29 | 4 | 0.7 | 8 | 8 | 8 | 33 | 36 Y | 0.2015 |
| 11.1 | 30 | 4 | 0.7 | 3 | 3 | 8 | 33 | 11 N | 0.2015 |

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CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:07 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 11.1 - BIASED GRAB SAMPLES FROM COOLING TOWER

RADIATION TYPE: DATA FOR SUM OF THE FRACTIONS
COMPLETION
DATE: 10-28-94
TECHNICIANS: JB\PK
LOCATION: 11.0
GRID ID: 11.1
MEDIA TYPE: WOOD/PLASTIC
# of POINTS: 2

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 0.20 | PASS | 1 |
| AVG | 0.12 | PASS | 1 |
| STD X | 0.11 | | |
| MU SUB ALPHA | 0.26 | PASS | 1 |

| | | | ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED) | | | | | | | | ISOTOPES OF |
|---|---|---|---|---|---|---|---|---|---|---|---|
| ID # | GRID COORIDINATES OR OTHER ID | SR-90 | CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SOIL CODE | SR-90 | |
| | | LIMIT | LIMIT | LIMIT | LIMIT | LIMIT | LIMIT | LIMIT | | | |
| | | 17 | 0.9 | 1.1 | 1.8 | 3.8 | 63 | 2 | | | |
| 11.1 | BG WOOD | < * | < 0.009 | < 0.010 | < 0.013 | < 0.017 | < 0.080 | < 0.026 | 1 | < 0 | < |
| 11.1 | BG PLASTIC | < * | < 0.060 | < 0.046 | < 0.052 | < 0.067 | < 0.467 | < 0.114 | 1 | < 0 | < |

* : Sr-90 RESULTS NOT GIVE DUE TO SOLID SAMPLES OF WOOD AND PLASTIC

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CONCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| 0.010 < | 0.009 < | 0.007 < | 0.000 < | 0.001 < | 0.013 | 0.040 |
| 0.067 < | 0.042 < | 0.029 < | 0.000 < | 0.007 < | 0.057 | 0.202 |

TABLE 11.1-3

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 11.1 | #31 | 6 | 0.3 | 1 | 1 | B | 29 | 4 N | 0.1803 |
| 11.1 | #32 | 6 | 0.3 | 6 | 6 | B | 29 | 32 Y | 0.1803 |
| 11.1 | #33 | 6 | 0.3 | 6 | 6 | B | 29 | 32 Y | 0.1803 |
| 11.1 | #34 | 6 | 0.3 | 7 | 7 | B | 29 | 37 Y | 0.1803 |
| 11.1 | #35 | 6 | 0.3 | 4 | 4 | B | 29 | 21 N | 0.1803 |
| 11.1 | #36 | 6 | 0.3 | 2 | 2 | B | 29 | 9 N | 0.1803 |
| 11.1 | #37 | 6 | 0.3 | 1 | 1 | B | 29 | 4 N | 0.1803 |
| 11.1 | #38 | 6 | 0.3 | 3 | 3 | B | 29 | 15 N | 0.1803 |

# : BIASED LOCATIONS

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CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:07 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 11.1 - COOLING TOWER SOIL FOR SUM OF THE FRACTIONS

RADIATION TYPE: SOIL DATA FOR SUM OF THE FRACTIONS
COMPLETION -
DATE: 10-27-94
TECHNICIANS: JB/PK
LOCATION: 11.0
GRID ID: 11.1
MEDIA TYPE: SOIL
# of POINTS: 30

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 1.08 | FAIL | 1 |
| AVG | 0.33 | PASS | 1 |
| STD X | 0.19 | | |
| MU SUB ALPHA | 0.39 | PASS | 1 |

| | | ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED) | | | | | | | | ISOTOPES OF |
|---|---|---|---|---|---|---|---|---|---|---|
| ID # | GRID COORIDINATES OR OTHER ID | SR-90 LIMIT 17 | CO-60 LIMIT 0.9 | AG-108M LIMIT 1.1 | CS-134 LIMIT 1.8 | CS-137 LIMIT 3.8 | CE-144 LIMIT 65 | EU-152 LIMIT 2 | SOIL CODE | SR-90 |
| 11.1 | 1 | 0.249 < | 0.117 < | 0.058 < | 0.046 < | 0.113 < | 0.203 < | 0.170 | 1 | 0.014647 < |
| 11.1 | 2 | < 0.19 < | 0.042 < | 0.041 < | 0.066 | 0.223 < | 0.185 < | 0.144 | 1 | < 0.011176 < |
| 11.1 | 3 | < 0.19 < | 0.039 < | 0.031 < | 0.066 | 0.195 < | 0.134 < | 0.080 | 1 | < 0.011176 < |
| 11.1 | 4 | 1.03 < | 0.171 < | 0.118 < | 0.142 | 0.879 < | 0.274 < | 0.179 | 1 | 0.060588 < |
| 11.1 | 5 | < 0.19 < | 0.065 < | 0.062 < | 0.056 | 0.602 < | 0.256 < | 0.108 | 1 | < 0.011176 < |
| 11.1 | 6 | < 0.19 < | 0.059 < | 0.057 < | 0.068 | 1.110 < | 0.187 < | 0.171 | 1 | < 0.011176 < |
| 11.1 | 7 | 0.194 | 0.181 | 0.151 < | 0.057 | 1.220 < | 0.212 < | 0.163 | 1 | 0.011412 |
| 11.1 | 8 | < 0.19 < | 0.040 < | 0.049 < | 0.055 | 0.241 < | 0.167 < | 0.105 | 1 | < 0.011176 < |
| 11.1 | 9 | < 0.195 < | 0.084 < | 0.053 < | 0.073 | 0.460 < | 0.489 < | 0.180 | 1 | < 0.011471 < |
| 11.1 | 10 | < 0.195 < | 0.067 < | 0.043 < | 0.052 | 0.434 < | 0.328 < | 0.202 | 1 | < 0.011471 < |
| 11.1 | 11 | 1.04 < | 0.088 < | 0.046 < | 0.072 | 1.410 < | 0.225 < | 0.161 | 1 | 0.061176 < |
| 11.1 | 12 | < 0.195 < | 0.040 < | 0.051 < | 0.066 | 0.414 < | 0.266 < | 0.126 | 1 | < 0.011471 < |
| 11.1 | 13 | < 0.195 < | 0.056 < | 0.042 < | 0.060 | 0.576 < | 0.203 < | 0.165 | 1 | < 0.011471 < |
| 11.1 | 14 | < 0.195 < | 0.064 < | 0.072 < | 0.069 | 0.545 < | 0.205 < | 0.206 | 1 | < 0.011471 < |
| 11.1 | 15 | < 0.195 < | 0.083 < | 0.073 < | 0.079 | 2.200 < | 0.202 < | 0.151 | 1 | < 0.011471 < |
| 11.1 | 16 | < 0.195 < | 0.059 < | 0.039 < | 0.085 | 0.514 < | 0.284 < | 0.230 | 1 | < 0.011471 < |
| 11.1 | 17 | 0.199 < | 0.038 < | 0.068 < | 0.068 | 0.328 < | 0.361 < | 0.162 | 1 | 0.011706 < |
| 11.1 | 18 | 0.276 < | 0.047 < | 0.073 < | 0.077 | 0.770 < | 0.396 < | 0.096 | 1 | 0.016235 < |
| 11.1 | 19 | 0.315 < | 0.041 < | 0.030 < | 0.066 | 0.595 < | 0.423 < | 0.099 | 1 | 0.018529 < |
| 11.1 | 20 | 0.343 < | 0.045 < | 0.058 < | 0.060 | 0.540 < | 0.325 < | 0.064 | 1 | 0.020176 < |
| 11.1 | 21 | 0.285 < | 0.057 < | 0.025 < | 0.078 | 0.580 < | 0.276 < | 0.215 | 1 | 0.016765 < |
| 11.1 | 22 | 0.53 < | 0.063 < | 0.097 < | 0.081 | 2.890 < | 0.251 < | 0.101 | 1 | 0.031176 < |
| 11.1 | 23 | 0.728 < | 0.107 < | 0.091 < | 0.108 | 3.430 < | 0.451 < | 0.393 | 1 | 0.042824 < |
| 11.1 | 24 | 0.429 < | 0.048 < | 0.066 < | 0.082 | 2.090 < | 0.495 < | 0.105 | 1 | 0.025235 < |
| 11.1 | 25 | 0.408 < | 0.057 < | 0.097 < | 0.106 | 1.340 < | 0.501 < | 0.185 | 1 | 0.024 < |
| 11.1 | 26 | 0.214 < | 0.059 < | 0.061 < | 0.090 | 1.050 < | 0.353 < | 0.135 | 1 | 0.012588 < |
| 11.1 | 27 | < 0.18 < | 0.070 < | 0.036 < | 0.075 | 0.518 < | 0.212 < | 0.167 | 1 | < 0.010588 < |
| 11.1 | 28 | < 0.18 < | 0.047 < | 0.106 < | 0.092 < | 0.124 < | 0.356 < | 0.204 | 1 | < 0.010588 < |
| 11.1 | 29 | < 0.18 < | 0.084 < | 0.056 < | 0.081 | 0.853 < | 0.233 < | 0.287 | 1 | < 0.010588 < |
| 11.1 | 30 | 0.192 < | 0.050 < | 0.043 < | 0.082 | 0.781 < | 0.344 < | 0.217 | 1 | 0.011294 < |

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CONCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| 0.130 < | 0.053 < | 0.025 < | 0.000 < | 0.003 < | 0.085 | 0.311 |
| 0.047 < | 0.037 < | 0.037 | 0.000 < | 0.003 < | 0.072 | 0.207 |
| 0.043 < | 0.028 < | 0.037 | 0.000 < | 0.002 < | 0.040 | 0.162 |
| 0.190 < | 0.107 < | 0.079 | 0.000 < | 0.004 < | 0.090 | 0.531 |
| 0.073 < | 0.056 < | 0.031 | 0.000 < | 0.004 < | 0.054 | 0.229 |
| 0.065 < | 0.052 < | 0.038 | 0.000 < | 0.003 < | 0.086 | 0.254 |
| 0.201 | 0.137 < | 0.032 | 0.000 < | 0.003 < | 0.082 | 0.466 |
| 0.045 < | 0.045 < | 0.031 | 0.000 < | 0.003 < | 0.053 | 0.186 |
| 0.093 < | 0.048 < | 0.041 | 0.000 < | 0.008 < | 0.090 | 0.291 |
| 0.075 < | 0.039 < | 0.029 | 0.000 < | 0.005 < | 0.101 | 0.260 |
| 0.098 < | 0.042 < | 0.040 | 0.042 < | 0.004 < | 0.081 | 0.367 |
| 0.045 < | 0.046 < | 0.036 | 0.000 < | 0.004 < | 0.063 | 0.206 |
| 0.063 < | 0.038 < | 0.033 | 0.000 < | 0.003 < | 0.083 | 0.231 |
| 0.071 < | 0.065 < | 0.038 | 0.000 < | 0.003 < | 0.103 | 0.293 |
| 0.092 < | 0.066 < | 0.044 | 0.250 < | 0.003 < | 0.076 | 0.542 |
| 0.065 < | 0.036 < | 0.047 | 0.000 < | 0.005 < | 0.115 | 0.279 |
| 0.042 < | 0.062 < | 0.038 | 0.000 < | 0.006 < | 0.081 | 0.240 |
| 0.053 < | 0.066 < | 0.043 | 0.000 < | 0.006 < | 0.048 | 0.231 |
| 0.045 < | 0.027 < | 0.036 | 0.000 < | 0.007 < | 0.049 | 0.184 |
| 0.050 < | 0.053 < | 0.033 | 0.000 < | 0.005 < | 0.032 | 0.193 |
| 0.063 < | 0.023 < | 0.043 | 0.000 < | 0.004 < | 0.108 | 0.258 |
| 0.070 < | 0.088 < | 0.045 | 0.432 < | 0.004 < | 0.051 | 0.720 |
| 0.119 < | 0.082 < | 0.060 | 0.574 < | 0.007 < | 0.197 | 1.082 |
| 0.053 < | 0.060 < | 0.046 | 0.221 < | 0.008 < | 0.053 | 0.466 |
| 0.063 < | 0.088 < | 0.059 | 0.024 < | 0.008 < | 0.093 | 0.358 |
| 0.065 < | 0.056 < | 0.050 | 0.000 < | 0.006 < | 0.068 | 0.256 |
| 0.077 < | 0.033 < | 0.042 | 0.000 < | 0.003 < | 0.084 | 0.249 |
| 0.052 < | 0.096 < | 0.051 < | 0.000 < | 0.006 < | 0.102 | 0.318 |
| 0.093 < | 0.051 < | 0.045 | 0.000 < | 0.004 < | 0.144 | 0.347 |
| 0.055 < | 0.039 < | 0.045 | 0.000 < | 0.005 < | 0.109 | 0.265 |

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:19 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
SK TANK EXCAVATION AREA 12.1 FOR UREM

RADIATION TYPE: GAMMA SURVEY IN UREM/HR
COMPLETION -
DATE: 11-22-94
TECHNICIANS: TA/CD
LOCATION: 12.0
GRID ID: 12.1
MEDIA TYPE: SOIL
# of POINTS: 31

MATERIAL CODE
1=CONCRETE 5=PLASTIC
2=ROCK 6=SOIL
3=WOOD 7=ASPHALT
4=METAL 8=OTHER(SPECIFY):
NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | | LIMIT |
|---|---|---|---|
| MAX | 6.00 | PASS | 10 |
| AVG | 2.45 | PASS | 5 |
| STD X | 1.41 | | |
| MU SUB ALPHA | 2.88 | PASS | 5 |

| ID # | GRID COORIDINATES W | N | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|---|
| 12.1 | 0+47.5 | 0+2.5N | 6 | 8 | 8 | 2 |
| 12.1 | 0+47.5 | 0+7.5N | 6 | 9 | 8 | 3 |
| 12.1 | 0+45 | 0+5N | 6 | 10 | 8 | 4 |
| 12.1 | 0+42.5 | 0+2.5N | 6 | 7 | 8 | 1 |
| 12.1 | 0+42.5 | 0+7.5N | 6 | 8 | 8 | 2 |
| 12.1 | 0+37.5 | 0+12.5S | 6 | 10 | 8 | 4 |
| 12.1 | 0+32.5 | 0+12.5S | 6 | 9 | 8 | 3 |
| 12.1 | 0+37.5 | 0+17.5S | 6 | 7 | 8 | 1 |
| 12.1 | 0+35 | 0+15S | 6 | 6 | 8 | 0 |
| 12.1 | 0+32.5 | 0+17.5S | 6 | 6 | 8 | 0 |
| 12.1 | 0+37.5 | 0+7.5S | 6 | 8 | 8 | 2 |
| 12.1 | 0+37.5 | 0+2.5S | 6 | 8 | 8 | 2 |
| 12.1 | 0+35 | 0+5S | 6 | 9 | 8 | 3 |
| 12.1 | 0+32.5 | 0+7.5S | 6 | 8 | 8 | 2 |
| 12.1 | 0+32.5 | 0+2.5S | 6 | 9 | 8 | 3 |
| 12.1 | 0+32.5 | 0+2.5N | 6 | 10 | 8 | 4 |
| 12.1 | 0+37.5 | 0+2.5N | 6 | 8 | 8 | 2 |
| 12.1 | 0+37.5 | 0+7.5N | 6 | 8 | 8 | 2 |
| 12.1 | 0+35 | 0+5N | 6 | 7 | 8 | 1 |
| 12.1 | 0+32.5 | 0+7.5N | 6 | 8 | 8 | 2 |
| 12.1 | 0+27.5 | 0+12.5S | 6 | 7 | 8 | 1 |
| 12.1 | 0+27.5 | 0+7.5S | 6 | 11 | 8 | 5 |
| 12.1 | 0+27.5 | 0+2.5S | 6 | 8 | 8 | 2 |
| 12.1 | 0+25 | 0+5S | 6 | 12 | 8 | 6 |
| 12.1 | 0+22.5 | 0+7.5S | 6 | 10 | 8 | 4 |
| 12.1 | 0+22.5 | 0+2.5S | 6 | 9 | 8 | 3 |
| 12.1 | 0+27.5 | 0+2.5N | 6 | 10 | 8 | 4 |
| 12.1 | 0+25 | 0+5N | 6 | 9 | 8 | 3 |
| 12.1 | 0+22.5 | 0+2.5N | 6 | 9 | 8 | 3 |
| 12.1 | 0+27.5 | 0+7.5N | 6 | 7 | 8 | 1 |
| 12.1 | 0+22.5 | 0+7.5N | 6 | 7 | 8 | 1 |

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A.R. TABLE 12.1-2

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:08 AM
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 12.1 - 5K TANK EXCAVATION SOIL FOR SUM OF THE FRACTIONS

RADIATION TYPE: SOIL DATA FOR SUM OF THE FRACTIONS
COMPLETION -
DATE: 11/17/94
TECHNICIANS: TA/CD/JB/PK
LOCATION: 12.0
GRID ID: 12.1
MEDIA TYPE: SOIL
# of POINTS: 30

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 0.43 | PASS | 1 |
| AVG | 0.21 | PASS | 1 |
| STD X | 0.06 | | |
| MU SUB ALPHA | 0.22 | PASS | 1 |

| ID # | GRID CODRIDINATES OR OTHER ID | | ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND INCLUDED) SR-90 | CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SOIL CODE | ISOTOPES SR-90 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | W | N/S | LIMIT 17 | LIMIT 0.9 | LIMIT 1.1 | LIMIT 1.8 | LIMIT 3.8 | LIMIT 63 | LIMIT 2 | | |
| 12.1 | 0+47.5 | 0+2.5N | < 0.218 | < 0.032 | < 0.055 | < 0.053 | < 0.031 | < 0.272 | < 0.118 | 1 | < 0.012824 |
| 12.1 | 0+47.5 | 0+7.5N | < 0.218 | < 0.099 | < 0.053 | < 0.057 | < 0.097 | < 0.301 | < 0.077 | 1 | < 0.012824 |
| 12.1 | 0+45 | 0+5N | < 0.218 | < 0.036 | < 0.062 | < 0.057 | 0.676 | < 0.287 | < 0.089 | 1 | < 0.012824 |
| 12.1 | 0+42.5 | 0+2.5N | < 0.218 | < 0.134 | < 0.138 | < 0.0[illegible] | 0.397 | < 0.419 | < 0.209 | 1 | < 0.012824 |
| 12.1 | 0+42.5 | 0+7.5N | < 0.218 | < 0.029 | < 0.020 | < 0.048 | 0.[illegible]77 | < 0.186 | < 0.107 | 1 | < 0.012824 |
| 12.1 | 0+37.5 | 0+12.5S | < 0.218 | < 0.044 | < 0.030 | < 0.062 | 0.354 | < 0.350 | < 0.202 | 1 | < 0.012824 |
| 12.1 | 0+32.5 | 0+12.5S | < 0.183 | < 0.032 | < 0.047 | < 0.062 | < 0.068 | < 0.323 | < 0.075 | 1 | < 0.010765 |
| 12.1 | 0+37.5 | 0+17.5S | < 0.199 | < 0.050 | < 0.049 | < 0.067 | 0.853 | < 0.428 | < 0.149 | 1 | < 0.011706 |
| 12.1 | 0+35 | 0+15S | < 0.199 | < 0.040 | < 0.033 | < 0.052 | < 0.077 | < 0.260 | < 0.076 | 1 | < 0.011706 |
| 12.1 | 0+32.5 | 0+17.5S | < 0.199 | < 0.046 | < 0.056 | < 0.066 | 0.778 | < 0.215 | < 0.170 | 1 | < 0.011706 |
| 12.1 | 0+37.5 | 0+7.5S | < 0.183 | < 0.042 | < 0.072 | < 0.061 | < 0.297 | < 0.445 | < 0.199 | 1 | < 0.010765 |
| 12.1 | 0+37.5 | 0+2.5S | < 0.183 | < 0.035 | < 0.045 | < 0.058 | < 0.070 | < 0.316 | < 0.075 | 1 | < 0.010765 |
| 12.1 | 0+35 | 0+5S | < 0.183 | < 0.046 | < 0.034 | < 0.045 | 0.201 | < 0.397 | < 0.141 | 1 | < 0.010765 |
| 12.1 | 0+32.5 | 0+7.5S | < 0.203 | < 0.050 | < 0.027 | < 0.068 | 0.141 | < 0.439 | < 0.154 | 1 | < 0.011941 |
| 12.1 | 0+32.5 | 0+2.5S | < 0.203 | < 0.037 | < 0.051 | < 0.071 | < 0.125 | < 0.346 | < 0.121 | 1 | < 0.011941 |
| 12.1 | 0+32.5 | 0+2.5N | < 0.203 | < 0.046 | < 0.[illegible]9 | < 0.053 | < 0.067 | < 0.323 | < 0.111 | 1 | < 0.011941 |
| 12.1 | 0+37.5 | 0+2.5N | < 0.218 | < 0.083 | < 0.053 | < 0.062 | < 0.073 | < 0.129 | < 0.096 | 1 | < 0.012824 |
| 12.1 | 0+37.5 | 0+7.5N | < 0.218 | < 0.068 | < 0.040 | < 0.059 | < 0.045 | < 0.260 | < 0.[illegible]5 | 1 | < 0.012824 |
| 12.1 | 0+35 | 0+5N | < 0.218 | < 0.032 | < 0.018 | < 0.048 | < 0.154 | < 0.263 | < 0.197 | 1 | < 0.012824 |
| 12.1 | 0+32.5 | 0+7.5N | < 0.199 | < 0.029 | < 0.047 | < 0.051 | 0.173 | < 0.251 | < 0.062 | 1 | < 0.011706 |
| 12.1 | 0+27.5 | 0+12.5S | < 0.199 | < 0.038 | < 0.030 | < 0.080 | 0.491 | < 0.330 | < 0.123 | 1 | < 0.011706 |
| 12.1 | 0+27.5 | 0+7.5S | < 0.203 | < 0.052 | < 0.036 | < 0.053 | < 0.065 | < 0.276 | < 0.136 | 1 | < 0.011941 |
| 12.1 | 0+25 | 0+5S | < 0.203 | < 0.071 | < 0.042 | < 0.049 | < 0.065 | < 0.343 | < 0.165 | 1 | < 0.011941 |
| 12.1 | 0+22.5 | 0+7.5S | < 0.177 | < 0.025 | < 0.048 | < 0.056 | < 0.074 | < 0.361 | < 0.147 | 1 | < 0.010412 |
| 12.1 | 0+22.5 | 0+2.5S | < 0.177 | < 0.032 | < 0.032 | < 0.065 | < 0.107 | < 0.363 | < 0.075 | 1 | < 0.010412 |
| 12.1 | 0+27.5 | 0+2.5N | < 0.203 | < 0.041 | < 0.030 | < 0.070 | < 0.092 | < 0.240 | < 0.096 | 1 | < 0.011941 |
| 12.1 | 0+25 | 0+5N | < 0.177 | < 0.036 | < 0.047 | < 0.053 | 0.122 | < 0.271 | < 0.062 | 1 | < 0.010412 |
| 12.1 | 0+22.5 | 0+2.5N | < 0.177 | < 0.032 | < 0.055 | < 0.052 | < 0.233 | < 0.292 | < 0.114 | 1 | < 0.010412 |
| 12.1 | 0+27.5 | 0+7.5N | < 0.199 | < 0.090 | < 0.037 | < 0.048 | < 0.092 | < 0.279 | < 0.180 | 1 | < 0.011706 |
| 12.1 | 0+22.5 | 0+7.5N | < 0.199 | < 0.041 | < 0.022 | < 0.059 | < 0.097 | < 0.294 | < 0.071 | 1 | < 0.011706 |

OF CONCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|
| < 0.036 | < 0.050 | < 0.029 | 0.000 | < 0.004 | < 0.059 | 0.191 |
| < 0.109 | < 0.048 | < 0.031 | 0.000 | < 0.005 | < 0.039 | 0.245 |
| < 0.040 | < 0.056 | < 0.032 | 0.000 | < 0.005 | < 0.045 | 0.190 |
| < 0.149 | < 0.125 | < 0.036 | 0.000 | < 0.007 | < 0.105 | 0.434 |
| < 0.033 | < 0.018 | < 0.027 | 0.000 | < 0.003 | < 0.054 | 0.147 |
| < 0.049 | < 0.028 | < 0.034 | 0.000 | < 0.006 | < 0.101 | 0.230 |
| < 0.035 | < 0.043 | < 0.034 | 0.000 | < 0.005 | < 0.037 | 0.165 |
| < 0.055 | < 0.044 | < 0.037 | 0.000 | < 0.007 | < 0.075 | 0.230 |
| < 0.044 | < 0.030 | < 0.029 | 0.000 | < 0.004 | < 0.038 | 0.156 |
| < 0.051 | < 0.051 | < 0.037 | 0.000 | < 0.003 | < 0.085 | 0.239 |
| < 0.047 | < 0.065 | < 0.034 | 0.000 | < 0.007 | < 0.100 | 0.263 |
| < 0.039 | < 0.041 | < 0.032 | 0.000 | < 0.005 | < 0.038 | 0.166 |
| < 0.051 | < 0.031 | < 0.025 | 0.000 | < 0.006 | < 0.071 | 0.195 |
| < 0.055 | < 0.024 | < 0.038 | 0.000 | < 0.007 | < 0.077 | 0.213 |
| < 0.041 | < 0.046 | < 0.039 | 0.000 | < 0.005 | < 0.061 | 0.204 |
| < 0.051 | < 0.017 | < 0.029 | 0.000 | < 0.005 | < 0.056 | 0.171 |
| < 0.093 | < 0.048 | < 0.035 | 0.000 | < 0.002 | < 0.048 | 0.238 |
| < 0.076 | < 0.036 | < 0.033 | 0.000 | < 0.004 | < 0.052 | 0.213 |
| < 0.025 | < 0.016 | < 0.026 | 0.000 | < 0.004 | < 0.099 | 0.193 |
| < 0.032 | < 0.042 | < 0.029 | 0.000 | < 0.004 | < 0.031 | 0.149 |
| < 0.042 | < 0.027 | < 0.044 | 0.000 | < 0.005 | < 0.062 | 0.192 |
| < 0.058 | < 0.033 | < 0.029 | 0.000 | < 0.004 | < 0.068 | 0.204 |
| < 0.079 | < 0.038 | < 0.027 | 0.000 | < 0.005 | < 0.083 | 0.245 |
| < 0.028 | < 0.043 | < 0.031 | 0.000 | < 0.006 | < 0.074 | 0.192 |
| < 0.035 | < 0.029 | < 0.036 | 0.000 | < 0.006 | < 0.037 | 0.154 |
| < 0.046 | < 0.028 | < 0.039 | 0.000 | < 0.004 | < 0.048 | 0.176 |
| < 0.040 | < 0.043 | < 0.029 | 0.000 | < 0.004 | < 0.031 | 0.158 |
| < 0.036 | < 0.050 | < 0.029 | 0.000 | < 0.005 | < 0.057 | 0.186 |
| < 0.100 | < 0.034 | < 0.027 | 0.000 | < 0.004 | < 0.090 | 0.266 |
| < 0.045 | < 0.020 | < 0.033 | 0.000 | < 0.005 | < 0.035 | 0.149 |

ANSTEC APERTURE CARD
Also Available on Aperture Card

RETABLE 12.1-3

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95
FINAL SURVEY DATA SHEET 08:08 AM
DATA FOR AFFECTED AREA DESCRIPTION:
SOIL SAMPLES FROM 5K MALL LANDFILL AREA

RADIATION TYPE: SOIL DATA FOR SUM OF THE FRACTIONS

| | |
|---|---|
| COMPLETION DATE: | 12/07/94 |
| TECHNICIANS: | ENV. |
| LOCATION: | 12.0 |
| GRID ID: | 12.1 |
| MEDIA TYPE: | SOIL |
| # of POINTS: | 78 |

| SOIL DATA IN SUM OF FRACTIONS: | | | LIMIT |
|---|---|---|---|
| MAX | 0.23 | PASS | 1 |
| AVG | 0.16 | PASS | 1 |
| S.D X | 0.03 | | |
| MU SUB ALPHA | 0.17 | PASS | 1 |

ISOTOPES OF CONCERN IN PCI/G (WITH BACKGROUND IN

| ID # | GRID COORIDINATES OR OTHER ID | SR-90 | CO-60 | AG-108M | CS-134 | CS-137 | CE- |
|---|---|---|---|---|---|---|---|
| | | LIMIT 17 | LIMIT 0.9 | LIMIT 1.1 | LIMIT 1.8 | LIMIT 3.8 | L |
| | 5K | | | | | | |
| 12.1 005 | | < 0.127 | < 0.02 | < 0.027 | < 0.045 | < 0.018 | < 0. |
| 12.1 006 | | < 0.127 | < 0.025 | < 0.017 | < 0.043 | 0.230 | < 0 |
| 12.1 007 | | < 0.127 | < 0.048 | < 0.020 | < 0.048 | < 0.020 | < 0 |
| 12.1 008 | | < 0.127 | < 0.069 | < 0.032 | 0.066 | 0.190 | < 0 |
| 12.1 009 | | < 0.127 | < 0.063 | < 0.019 | < 0.036 | 0.340 | < 0 |
| 12.1 010 | | < 0.127 | < 0.070 | < 0.022 | < 0.047 | 0.170 | < 0 |
| 12.1 011 | | < 0.127 | < 0.029 | < 0.029 | < 0.041 | 0.310 | < 0 |
| 12.1 012 | | < 0.127 | < 0.034 | < 0.025 | < 0.031 | 0.210 | < 0 |
| 12.1 013 | | < 0.127 | < 0.060 | < 0.031 | < 0.040 | 0.240 | < 0 |
| 12.1 014 | | < 0.127 | < 0.022 | < 0.031 | < 0.042 | 0.200 | < 0 |
| 12.1 015 | | < 0.127 | < 0.028 | < 0.014 | < 0.047 | 0.190 | < 0 |
| 12.1 016 | | < 0.127 | < 0.026 | < 0.034 | < 0.043 | 0.230 | < 0. |
| 12.1 017 | | < 0.127 | < 0.033 | < 0.026 | < 0.038 | 0.200 | < 0. |
| 12.1 018 | | < 0.127 | < 0.028 | < 0.042 | < 0.037 | 0.170 | < 0. |
| 12.1 019 | | < 0.127 | < 0.029 | < 0.034 | < 0.043 | 0.240 | < 0. |
| 12.1 020 | | < 0.127 | < 0.045 | < 0.031 | < 0.039 | 0.230 | < 0. |
| 12.1 021 | | < 0.127 | < 0.045 | < 0.018 | < 0.039 | 0.310 | < 0. |
| 12.1 022 | | < 0.127 | < 0.035 | < 0.027 | < 0.038 | 0.210 | < 0. |
| 12.1 023 | | < 0.127 | < 0.064 | < 0.020 | < 0.041 | 0.280 | < 0. |
| 12.1 024 | | < 0.127 | < 0.058 | < 0.037 | < 0.038 | 0.290 | < 0. |
| 12.1 104 | | < 0.249 | < 0.022 | < 0.039 | < 0.043 | 0.320 | < 0. |
| 12.1 108 | | < 0.249 | < 0.025 | < 0.019 | < 0.046 | 0.290 | < 0. |
| 12.1 112 | | 0.712 | < 0.035 | < 0.027 | < 0.045 | 0.160 | < 0. |
| 12.1 115 | | 0.712 | < 0.074 | < 0.016 | < 0.045 | 0.160 | < 0. |
| 12.1 118 | | 0.712 | < 0.030 | < 0.023 | < 0.044 | < 0.073 | < 0. |
| 12.1 121 | | < 0.283 | < 0.055 | < 0.035 | < 0.039 | < 0.069 | < 0. |
| 12.1 124 | | < 0.283 | < 0.030 | < 0.024 | < 0.039 | 0.150 | < 0. |
| 12.1 128 | | 0.089 | < 0.038 | < 0.033 | < 0.034 | 0.120 | < 0. |
| 12.1 131 | | 0.089 | < 0.051 | < 0.029 | < 0.036 | < 0.055 | < 0. |
| 12.1 134 | | 0.089 | < 0.046 | < 0.019 | < 0.043 | 0.120 | < 0. |
| 12.1 136 | | 0.089 | < 0.045 | < 0.031 | < 0.054 | 0.140 | < 0. |
| 12.1 140 | | 0.089 | < 0.052 | < 0.016 | < 0.044 | < 0.056 | < 0. |

ANSTEC
APERTURE
CARD

Also Available on
Aperture Card

CLUDED) ISOTOPES OF CONCERN IN FRACTION OF LIMIT (WITH Cs-137 BACKGROUND OF 1.25 pCi/gm SUBTRACTED)

| 144 MIT 63 | EU-152 LIMIT 2 | SOIL CODE | SR-90 | CO-60 | AG-108M | CS-134 | CS-137 | CE-144 | EU-152 | SUM |
|---|---|---|---|---|---|---|---|---|---|---|
| 290 < | 0.062 | 1 | < 0.007471 < | 0.022 < | 0.025 < | 0.025 < | 0.000 < | 0.005 < | 0.031 | 0.115 |
| 230 < | 0.130 | 1 | < 0.007471 < | 0.028 < | 0.015 < | 0.024 | 0.000 < | 0.004 < | 0.065 | 0.143 |
| 240 < | 0.077 | 1 | < 0.007471 < | 0.053 < | 0.018 < | 0.027 < | 0.000 < | 0.004 < | 0.039 | 0.148 |
| 200 < | 0.042 | 1 | < 0.007471 < | 0.077 < | 0.029 | 0.037 | 0.000 < | 0.003 < | 0.021 | 0.174 |
| 100 < | 0.130 | 1 | < 0.007471 < | 0.070 < | 0.017 < | 0.020 | 0.000 < | 0.002 < | 0.065 | 0.181 |
| 150 < | 0.120 | 1 | < 0.007471 < | 0.078 < | 0.020 < | 0.026 | 0.000 < | 0.002 < | 0.060 | 0.194 |
| 290 < | 0.120 | 1 | < 0.007471 < | 0.032 < | 0.026 < | 0.023 | 0.000 < | 0.005 < | 0.060 | 0.153 |
| 210 < | 0.092 | 1 | < 0.007471 < | 0.038 < | 0.023 < | 0.017 | 0.000 < | 0.003 < | 0.046 | 0.135 |
| 250 < | 0.097 | 1 | < 0.007471 < | 0.067 < | 0.028 < | 0.022 | 0.000 < | 0.004 < | 0.049 | 0.177 |
| 210 < | 0.078 | 1 | < 0.007471 < | 0.024 < | 0.028 < | 0.023 | 0.000 < | 0.003 < | 0.039 | 0.126 |
| 130 < | 0.083 | 1 | < 0.007471 < | 0.031 < | 0.013 < | 0.026 | 0.000 < | 0.002 < | 0.042 | 0.121 |
| 260 < | 0.073 | 1 | < 0.007471 < | 0.029 < | 0.031 < | 0.024 | 0.000 < | 0.004 < | 0.037 | 0.132 |
| 210 < | 0.055 | 1 | < 0.007471 < | 0.037 < | 0.024 < | 0.021 | 0.000 < | 0.003 < | 0.028 | 0.120 |
| 210 < | 0.091 | 1 | < 0.007471 < | 0.031 < | 0.038 < | 0.021 | 0.000 < | 0.003 < | 0.046 | 0.146 |
| 130 < | 0.140 | 1 | < 0.007471 < | 0.032 < | 0.031 < | 0.024 | 0.000 < | 0.002 < | 0.070 | 0.167 |
| 210 < | 0.047 | 1 | < 0.007471 < | 0.050 < | 0.028 < | 0.022 | 0.000 < | 0.003 < | 0.024 | 0.134 |
| 110 < | 0.045 | 1 | < 0.007471 < | 0.050 < | 0.016 < | 0.022 | 0.000 < | 0.002 < | 0.023 | 0.120 |
| 280 < | 0.053 | 1 | < 0.007471 < | 0.039 < | 0.025 < | 0.021 | 0.000 < | 0.004 < | 0.027 | 0.123 |
| 170 < | 0.130 | 1 | < 0.007471 < | 0.071 < | 0.018 < | 0.023 | 0.000 < | 0.003 < | 0.065 | 0.187 |
| 240 < | 0.110 | 1 | < 0.007471 < | 0.064 < | 0.034 < | 0.021 | 0.000 < | 0.004 < | 0.055 | 0.185 |
| 320 < | 0.095 | 1 | < 0.014647 < | 0.024 < | 0.035 < | 0.024 | 0.000 < | 0.005 < | 0.048 | 0.151 |
| 180 < | 0.050 | 1 | < 0.014647 < | 0.028 < | 0.017 < | 0.026 | 0.000 < | 0.003 < | 0.025 | 0.113 |
| 180 < | 0.043 | 1 | 0.041882 < | 0.039 < | 0.025 < | 0.025 | 0.000 < | 0.003 < | 0.022 | 0.155 |
| 140 < | 0.130 | 1 | 0.041882 < | 0.082 < | 0.015 < | 0.025 | 0.000 < | 0.002 < | 0.065 | 0.231 |
| 140 < | 0.100 | 1 | 0.041882 < | 0.033 < | 0.021 < | 0.024 < | 0.000 < | 0.002 < | 0.050 | 0.173 |
| 210 < | 0.110 | 1 | < 0.016647 < | 0.061 < | 0.032 < | 0.022 < | 0.000 < | 0.003 < | 0.055 | 0.190 |
| 210 < | 0.100 | 1 | < 0.016647 < | 0.033 < | 0.022 < | 0.022 | 0.000 < | 0.003 < | 0.050 | 0.147 |
| 190 < | 0.110 | 1 | 0.005235 < | 0.042 < | 0.030 < | 0.019 | 0.000 < | 0.003 < | 0.055 | -4 |
| 260 < | 0.055 | 1 | 0.005235 < | 0.057 < | 0.026 < | 0.020 < | 0.000 < | 0.004 < | 0.028 | 0.140 |
| 240 < | 0.120 | 1 | 0.005235 < | 0.051 < | 0.017 < | 0.024 | 0.000 < | 0.004 < | 0.060 | 0.161 |
| 320 < | 0.066 | 1 | 0.005235 < | 0.050 < | 0.028 < | 0.030 | 0.000 < | 0.005 < | 0.033 | 0.151 |
| 240 < | 0.130 | 1 | 0.005235 < | 0.058 < | 0.015 < | 0.024 < | 0.000 < | 0.004 < | 0.065 | 0.171 |

9502100114-134

TABLE 12.1-3

| | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 12.1 143 | | 0.089 | < | 0.050 | < | 0.032 | < | 0.037 | < | 0.064 | < | 0 |
| 12.1 146 | | 0.089 | < | 0.041 | < | 0.048 | < | 0.047 | | 0.120 | < | 0 |
| 12.1 150 | < | 0.174 | < | 0.027 | < | 0.018 | < | 0.039 | < | 0.060 | < | 0 |
| 12.1 152 | < | 0.174 | < | 0.063 | < | 0.022 | < | 0.049 | < | 0.024 | < | 0 |
| 12.1 155 | < | 0.174 | < | 0.059 | < | 0.047 | < | 0.054 | < | 0.043 | < | 0 |
| 12.1 158 | < | 0.174 | < | 0.027 | < | 0.024 | < | 0.038 | < | 0.022 | < | 0 |
| 12.1 159 | < | 0.208 | < | 0.022 | < | 0.031 | < | 0.039 | < | 0.056 | < | 0 |
| 12.1 160 | < | 0.208 | < | 0.065 | < | 0.034 | < | 0.036 | < | 0.050 | < | 0 |
| 12.1 161 | < | 0.208 | < | 0.033 | < | 0.035 | < | 0.043 | < | 0.050 | < | 0 |
| 12.1 162 | < | 0.208 | < | 0.066 | < | 0.025 | < | 0.044 | < | 0.068 | < | 0 |
| 12.1 163 | < | 0.208 | < | 0.034 | < | 0.015 | < | 0.036 | < | 0.043 | < | 0 |
| 12.1 164 | < | 0.208 | < | 0.019 | < | 0.037 | < | 0.041 | < | 0.053 | < | 0 |
| 12.1 165 | < | 0.208 | < | 0.032 | < | 0.023 | < | 0.039 | < | 0.054 | < | 0 |
| 12.1 166 | < | 0.208 | < | 0.049 | < | 0.042 | < | 0.046 | < | 0.064 | < | 0 |
| 12.1 167 | < | 0.208 | < | 0.099 | < | 0.021 | < | 0.040 | | 0.150 | < | 0 |
| 12.1 168 | < | 0.208 | < | 0.022 | < | 0.021 | < | 0.037 | < | 0.057 | < | 0 |
| 12.1 169 | < | 0.208 | < | 0.051 | < | 0.038 | < | 0.047 | < | 0.026 | < | 0 |
| 12.1 170 | < | 0.208 | < | 0.066 | < | 0.047 | < | 0.035 | | 0.280 | < | 0 |
| 12.1 171 | < | 0.208 | < | 0.038 | < | 0.042 | < | 0.041 | < | 0.057 | < | 0 |
| 12.1 172 | < | 0.191 | < | 0.049 | < | 0.023 | < | 0.045 | < | 0.072 | < | 0 |
| 12.1 173 | < | 0.191 | < | 0.047 | < | 0.031 | < | 0.043 | < | 0.054 | | 0 |
| 12.1 174 | < | 0.191 | < | 0.040 | < | 0.038 | < | 0.041 | < | 0.051 | < | 0 |
| 12.1 175 | < | 0.191 | < | 0.061 | < | 0.033 | < | 0.041 | < | 0.044 | < | 0 |
| 12.1 176 | < | 0.191 | < | 0.053 | < | 0.039 | < | 0.046 | < | 0.086 | < | 0 |
| 12.1 177 | < | 0.191 | < | 0.037 | < | 0.019 | < | 0.045 | | 0.068 | < | 0 |
| 12.1 178 | < | 0.191 | < | 0.029 | < | 0.028 | < | 0.039 | | 0.071 | < | 0 |
| 12.1 179 | < | 0.191 | < | 0.027 | < | 0.043 | < | 0.050 | < | 0.058 | < | 0 |
| 12.1 180 | < | 0.191 | < | 0.021 | < | 0.028 | < | 0.044 | | 0.069 | < | 0 |
| 12.1 181 | < | 0.191 | < | 0.054 | < | 0.031 | < | 0.047 | | 0.140 | < | 0 |
| 12.1 182 | < | 0.191 | < | 0.020 | < | 0.027 | < | 0.046 | < | 0.065 | < | 0 |
| 12.1 183 | < | 0.191 | < | 0.038 | < | 0.055 | < | 0.044 | | 0.330 | < | 0 |
| 12.1 184 | < | 0.191 | < | 0.038 | < | 0.014 | < | 0.045 | | 0.087 | < | 0 |
| 12.1 185 | < | 0.191 | < | 0.048 | < | 0.022 | < | 0.046 | < | 0.055 | < | 0 |
| 12.1 186 | < | 0.191 | < | 0.027 | < | 0.033 | < | 0.040 | < | 0.041 | < | 0 |
| 12.1 187 | < | 0.191 | < | 0.046 | < | 0.042 | < | 0.044 | < | 0.024 | < | 0 |
| 12.1 188 | < | 0.191 | < | 0.024 | < | 0.022 | < | 0.037 | < | 0.045 | < | 0 |
| 12.1 189 | < | 0.191 | < | 0.028 | < | 0.024 | < | 0.044 | < | 0.047 | < | 0 |
| 12.1 190 | < | 0.191 | < | 0.033 | < | 0.023 | < | 0.042 | < | 0.053 | < | 0 |
| 12.1 191 | < | 0.191 | < | 0.051 | < | 0.022 | < | 0.040 | < | 0.075 | < | 0 |
| 12.1 192 | < | 0.191 | < | 0.023 | < | 0.035 | < | 0.045 | | 0.079 | < | 0 |
| 12.1 193 | < | 0.191 | < | 0.053 | < | 0.012 | < | 0.039 | < | 0.045 | < | 0 |
| 12.1 194 | < | 0.191 | < | 0.048 | < | 0.026 | < | 0.041 | < | 0.065 | < | 0 |
| 12.1 195 | < | 0.191 | < | 0.019 | < | 0.022 | < | 0.038 | | 0.150 | < | 0 |
| 12.1 196 | < | 0.191 | < | 0.049 | < | 0.030 | < | 0.044 | | 0.120 | < | 0 |
| 12.1 197 | < | 0.191 | < | 0.036 | < | 0.043 | < | 0.041 | < | 0.040 | < | 0 |
| 12.1 198 | < | 0.191 | < | 0.110 | < | 0.023 | < | 0.038 | < | 0.039 | < | 0 |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| .180 | < 0.039 | 1 | 0.005235 < | 0.056 < | 0.029 < | 0.021 < | 0.000 < | 0.003 < | 0.010 | 0.133 |
| .270 | < 0.150 | 1 | 0.005235 < | 0.046 < | 0.044 < | 0.026 | 0.000 < | 0.004 < | 0.075 | 0.200 |
| .300 | < 0.071 | 1 | < 0.010235 < | 0.030 < | 0.016 < | 0.022 < | 0.000 < | 0.005 < | 0.036 | 0.119 |
| .250 | < 0.049 | 1 | < 0.010235 < | 0.070 < | 0.020 < | 0.027 < | 0.000 < | 0.004 < | 0.025 | 0.156 |
| .150 | < 0.110 | 1 | < 0.010235 < | 0.066 < | 0.043 < | 0.030 < | 0.000 < | 0.002 < | 0.055 | 0.206 |
| .110 | < 0.130 | 1 | < 0.012235 < | 0.030 < | 0.022 < | 0.021 < | 0.000 < | 0.002 < | 0.065 | 0.150 |
| .230 | < 0.140 | 1 | < 0.012235 < | 0.024 < | 0.028 < | 0.022 < | 0.000 < | 0.004 < | 0.070 | 0.160 |
| .210 | < 0.083 | 1 | < 0.012235 < | 0.072 < | 0.031 < | 0.020 < | 0.000 < | 0.003 < | 0.042 | 0.180 |
| .140 | < 0.061 | 1 | < 0.012235 < | 0.037 < | 0.032 < | 0.024 < | 0.000 < | 0.002 < | 0.031 | 0.137 |
| .220 | < 0.110 | 1 | < 0.012235 < | 0.073 < | 0.023 < | 0.024 < | 0.000 < | 0.003 < | 0.055 | 0.191 |
| .210 | < 0.092 | 1 | < 0.012235 < | 0.038 < | 0.014 < | 0.020 < | 0.000 < | 0.003 < | 0.046 | 0.133 |
| .150 | < 0.110 | 1 | < 0.012235 < | 0.021 < | 0.034 < | 0.023 < | 0.000 < | 0.002 < | 0.055 | 0.147 |
| .220 | < 0.110 | 1 | < 0.012235 < | 0.036 < | 0.021 < | 0.022 < | 0.000 < | 0.003 < | 0.055 | 0.149 |
| .180 | < 0.089 | 1 | < 0.012235 < | 0.054 < | 0.038 < | 0.026 < | 0.000 < | 0.003 < | 0.045 | 0.178 |
| .190 | < 0.110 | 1 | < 0.012235 < | 0.110 < | 0.019 < | 0.022 | 0.000 < | 0.003 < | 0.055 | 0.222 |
| .210 | < 0.096 | 1 | < 0.012235 < | 0.024 < | 0.019 < | 0.021 < | 0.000 < | 0.003 < | 0.048 | 0.126 |
| .290 | < 0.140 | 1 | < 0.012235 < | 0.057 < | 0.035 < | 0.026 < | 0.000 < | 0.005 < | 0.070 | 0.204 |
| .240 | < 0.130 | 1 | < 0.012235 < | 0.073 < | 0.043 < | 0.019 | 0.000 < | 0.004 < | 0.065 | 0.217 |
| .250 | < 0.140 | 1 | < 0.012235 < | 0.042 < | 0.038 < | 0.023 < | 0.000 < | 0.004 < | 0.070 | 0.189 |
| .270 | < 0.160 | 1 | < 0.011235 < | 0.054 < | 0.021 < | 0.025 < | 0.000 < | 0.004 < | 0.080 | 0.196 |
| .420 | < 0.110 | 1 | < 0.011235 < | 0.052 < | 0.028 < | 0.024 < | 0.000 | 0.007 < | 0.055 | 0.177 |
| .110 | < 0.087 | 1 | < 0.011235 < | 0.044 < | 0.035 < | 0.023 < | 0.000 < | 0.002 < | 0.044 | 0.158 |
| .290 | < 0.150 | 1 | < 0.011235 < | 0.068 < | 0.030 < | 0.023 < | 0.000 < | 0.005 < | 0.075 | 0.211 |
| .130 | < 0.080 | 1 | < 0.011235 < | 0.059 < | 0.035 < | 0.026 < | 0.000 < | 0.002 < | 0.040 | 0.173 |
| .200 | < 0.130 | 1 | < 0.011235 < | 0.041 < | 0.017 < | 0.025 | 0.000 < | 0.003 < | 0.065 | 0.163 |
| .220 | < 0.093 | 1 | < 0.011235 < | 0.032 < | 0.025 < | 0.022 | 0.000 < | 0.003 < | 0.047 | 0.141 |
| .230 | < 0.120 | 1 | < 0.011235 < | 0.030 < | 0.039 < | 0.028 < | 0.000 < | 0.004 < | 0.060 | 0.172 |
| .300 | < 0.079 | 1 | < 0.011235 < | 0.023 < | 0.025 < | 0.024 | 0.000 < | 0.005 < | 0.040 | 0.129 |
| .310 | < 0.130 | 1 | < 0.011235 < | 0.060 < | 0.028 < | 0.026 | 0.000 < | 0.005 < | 0.065 | 0.195 |
| .270 | < 0.087 | 1 | < 0.011235 < | 0.022 < | 0.025 < | 0.026 < | 0.000 < | 0.004 < | 0.044 | 0.131 |
| .300 | < 0.200 | 1 | < 0.011235 < | 0.042 < | 0.050 < | 0.024 | 0.000 < | 0.005 < | 0.100 | 0.233 |
| .300 | < 0.089 | 1 | < 0.011235 < | 0.042 < | 0.013 < | 0.025 | 0.000 < | 0.005 < | 0.045 | 0.140 |
| .190 | < 0.061 | 1 | < 0.011235 < | 0.053 < | 0.020 < | 0.026 < | 0.000 < | 0.003 < | 0.031 | 0.144 |
| .190 | < 0.091 | 1 | < 0.011235 < | 0.030 < | 0.030 < | 0.022 < | 0.000 < | 0.003 < | 0.046 | 0.142 |
| .170 | < 0.110 | 1 | < 0.011235 < | 0.051 < | 0.038 < | 0.024 < | 0.000 < | 0.003 < | 0.055 | 0.183 |
| .026 | < 0.120 | 1 | < 0.011235 < | 0.027 < | 0.020 < | 0.021 < | 0.000 < | 0.000 < | 0.060 | 0.139 |
| .240 | < 0.130 | 1 | < 0.011235 < | 0.031 < | 0.022 < | 0.024 < | 0.000 < | 0.004 < | 0.065 | 0.157 |
| .240 | < 0.090 | 1 | < 0.011235 < | 0.037 < | 0.021 < | 0.023 < | 0.000 < | 0.004 < | 0.045 | 0.141 |
| .200 | < 0.140 | 1 | < 0.011235 < | 0.057 < | 0.020 < | 0.022 < | 0.000 < | 0.003 < | 0.070 | 0.183 |
| .260 | < 0.096 | 1 | < 0.011235 < | 0.026 < | 0.032 < | 0.025 | 0.000 < | 0.004 < | 0.048 | 0.146 |
| .240 | < 0.110 | 1 | < 0.011235 < | 0.059 < | 0.011 < | 0.022 < | 0.000 < | 0.004 < | 0.055 | 0.162 |
| .110 | < 0.094 | 1 | < 0.011235 < | 0.053 < | 0.024 < | 0.023 < | 0.000 < | 0.002 < | 0.047 | 0.160 |
| .260 | < 0.054 | 1 | < 0.011235 < | 0.021 < | 0.020 < | 0.021 | 0.000 < | 0.004 < | 0.027 | 0.105 |
| .270 | < 0.070 | 1 | < 0.011235 < | 0.054 < | 0.027 < | 0.024 | 0.000 < | 0.004 < | 0.035 | 0.157 |
| .240 | < 0.120 | 1 | < 0.011235 < | 0.040 < | 0.039 < | 0.023 < | 0.000 < | 0.004 < | 0.060 | 0.177 |
| .220 | < 0.059 | 1 | < 0.011235 < | 0.122 < | 0.021 < | 0.021 < | 0.000 < | 0.003 < | 0.030 | 0.208 |

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ATTACHMENT 12.2-1

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:21 AM

FINAL SURVEY DATA SHEET

DATA FOR AFFECTED AREA DESCRIPTION:

MALL AREA 5K TANK PLATFORM FOR UREM - AREA 12.2

RADIATION TYPE: GAMMA SURVEY IN UREM/HR

COMPLETION DATE: 11-17-94

TECHNICIANS: TA/CD/JB/PK

LOCATION: 12.0

GRID ID: 12.2

MEDIA TYPE: CONCRETE

# of POINTS: 34

1

MATERIAL CODE

1=CONCRETE 5=PLASTIC

2=ROCK 6=SOIL

3=WOOD 7=ASPHALT

4=METAL 8=OTHER(SPECIFY):

NO MATERIAL BACKGROUND USED

| MICRO REM PER HOUR: | | | LIMIT |
|---|---|---|---|
| MAX | 3.00 | PASS | 10 |
| AVG | -0.15 | PASS | 5 |
| STD X | 1.02 | | |
| MU SUB ALPHA | 0.15 | PASS | 5 |

| GRID COORIDINATES ID # W | N/S | AREA BKG UREM/HR | AREA READING UREM/HR | MATERIAL CODE | NET UREM/HR |
|---|---|---|---|---|---|
| 12.2 0+27.5W | 0+4.5S | 6 | 6 | 8 | 0 |
| 12.2 0+26.5 | 0+4.5S | 6 | 6 | 8 | 0 |
| 12.2 0+25.5 | 0+4.5S | 6 | 6 | 8 | 0 |
| 12.2 0+24.5 | 0+4.5S | 6 | 5 | 8 | -1 |
| 12.2 0+29.5 | 0+3.5S | 6 | 5 | 8 | -1 |
| 12.2 0+28.5 | 0+3.5S | 6 | 6 | 8 | 0 |
| 12.2 0+27.5 | 0+3.5S | 6 | 6 | 8 | 0 |
| 12.2 0+26.5 | 0+3.5S | 6 | 5 | 8 | -1 |
| 12.2 0+25.5 | 0+3.5S | 6 | 7 | 8 | 1 |
| 12.2 0+24.5 | 0+3.5S | 6 | 5 | 8 | -1 |
| 12.2 0+29.5 | 0+2.5S | 6 | 5 | 8 | -1 |
| 12.2 0+28.5 | 0+2.5S | 6 | 6 | 8 | 0 |
| 12.2 0+27.5 | 0+2.5S | 6 | 7 | 8 | 1 |
| 12.2 0+26.5 | 0+2.5S | 6 | 6 | 8 | 0 |
| 12.2 0+25.5 | 0+2.5S | 6 | 6 | 8 | 0 |
| 12.2 0+24.5 | 0+2.5S | 6 | 5 | 8 | -1 |
| 12.2 0+29.5 | 0+1.5S | 6 | 4 | 8 | -2 |
| 12.2 0+28.5 | 0+1.5S | 6 | 6 | 8 | 0 |
| 12.2 0+27.5 | 0+1.5S | 6 | 6 | 8 | 0 |
| 12.2 0+26.5 | 0+1.5S | 6 | 5 | 8 | -1 |
| 12.2 0+25.5 | 0+1.5S | 6 | 7 | 8 | 1 |
| 12.2 0+24.5 | 0+1.5S | 6 | 7 | 8 | 1 |
| 12.2 0+29.5 | 0+0.5S | 6 | 6 | 8 | 0 |
| 12.2 0+28.5 | 0+0.5S | 6 | 5 | 8 | -1 |
| 12.2 0+27.5 | 0+0.5S | 6 | 6 | 8 | 0 |
| 12.2 0+26.5 | 0+0.5S | 6 | 5 | 8 | -1 |
| 12.2 0+25.5 | 0+0.5S | 6 | 7 | 8 | 1 |
| 12.2 0+24.5 | 0+0.5S | 6 | 5 | 8 | -1 |
| 12.2 0+29.5 | 0+0.5N | 6 | 6 | 8 | 0 |
| 12.2 0+28.5 | 0+0.5N | 6 | 5 | 8 | -1 |
| 12.2 0+27.5 | 0+0.5N | 6 | 7 | 8 | 1 |
| 12.2 0+26.5 | 0+0.5N | 6 | 4 | 8 | -2 |
| 12.2 0+25.5 | 0+0.5N | 6 | 7 | 8 | 1 |
| 12.2 0+24.5 | 0+0.5N | 6 | 9 | 8 | 3 |

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CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:21 AM

FINAL SURVEY DATA SHEET

DATA FOR AFFECTED AREA DESCRIPTION:

AREA 12.2 - MALL 5K CONCRETE TANK BASE FOR BETA

RADIATION TYPE: 1 BETA SCALING FACTOR = 0.974

COMPLETION DATE: 11-17-94

TECHNICIANS: TA/CD/JB/PK MATERIAL CODE

LOCATION: 12.0 1=CONCRETE 5=PLASTIC

GRID ID: 12.2 2=ROCK 6=SOIL

MEDIA TYPE: CONCRETE 3=WOOD 7=ASPHALT

# of POINTS: 129 4=METAL 8=OTHER(SPECIFY):

CT IN MINUTES: 1 NO MATERIAL BACKGROUND USED

DPM/100CM^2

REM.+ FIXED: LIMIT

MAX FOR IND GRID 1292 PASS 1301

AVG - SURVEY UNIT 567 PASS 1301

STD X 185

MU SUB ALPHA 594 PASS 1301

MAX HOT SPOT 0 PASS 3903

| ID # | GRID COORIDINATES W | S | INST. ID # | BETA INST. AREA BKG CPM | BETA FIXED COUNTS/ 1 MINUTES | SCAN MAX BETA COUNTS | TOTAL CONT. AREA CM^2 | MATER- IAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. BETA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 MAX CM^2 TEST | IN C |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 12.2 | 0+27.5 | 0+4.5S1 | 6 | 478.0 | 709 | 0 | 0 | 8 | 398 | 881 +/- 206 | NA | | |
| 12.2 | 0+26.5 | 0+4.5S1 | 3 | 529.5 | 708 | 0 | 0 | 8 | 425 | 691 +/- 209 | NA | | |
| | | | 2 | 3 | 529.5 | 705 | 0 | 0 | 8 | 425 | 679 +/- 209 | NA | |
| 12.2 | 0+25.5 | 0+4.5S1 | 6 | 478.0 | 723 | 0 | 0 | 8 | 404 | 948 +/- 211 | NA | | |
| | | | 2 | 3 | 529.5 | 681 | 0 | 0 | 8 | 429 | 593 +/- 208 | NA | |
| | | | 3 | 3 | 529.5 | 665 | 0 | 0 | 8 | 429 | 546 +/- 206 | NA | |
| 12.2 | 0+24.5 | 0+4.5S1 | 3 | 529.5 | 662 | 0 | 0 | 8 | 429 | 519 +/- 205 | NA | | |
| 12.2 | 0+29.5 | 0+3.5S1 | 9 | 492.9 | 715 | 0 | 0 | 8 | 410 | 860 +/- 210 | NA | | |
| | | | 2 | 9 | 492.9 | 678 | 0 | 0 | 8 | 415 | 725 +/- 207 | NA | |
| 12.2 | 0+28.5 | 0+3.5S1 | 6 | 478.0 | 647 | 0 | 0 | 8 | 398 | 645 +/- 197 | NA | | |
| | | | 2 | 9 | 492.9 | 632 | 0 | 0 | 8 | 410 | 538 +/- 198 | NA | |
| | | | 3 | 9 | 492.9 | 623 | 0 | 0 | 8 | 410 | 503 +/- 197 | NA | |
| | | | 4 | 9 | 492.9 | 726 | 0 | 0 | 8 | 410 | 802 +/- 211 | NA | |
| 12.2 | 0+27.5 | 0+3.5S1 | 6 | 478.0 | 680 | 0 | 0 | 8 | 404 | 782 +/- 205 | NA | | |
| | | | 2 | 9 | 492.9 | 634 | 0 | 0 | 8 | 404 | 538 +/- 195 | NA | |
| | | | 3 | 9 | 492.9 | 585 | 0 | 0 | 8 | 410 | 356 +/- 191 | NA | |
| | | | 4 | 3 | 529.5 | 708 | 0 | 0 | 8 | 425 | 691 +/- 209 | NA | |
| | | | 5 | 9 | 492.9 | 621 | 0 | 0 | 8 | 410 | 496 +/- 196 | NA | |
| 12.2 | 0+26.5 | 0+3.5S1 | 6 | 478.0 | 704 | 0 | 0 | 8 | 404 | 875 +/- 208 | NA | | |
| | | | 2 | 3 | 529.5 | 649 | 0 | 0 | 8 | 425 | 462 +/- 201 | NA | |
| | | | 3 | 3 | 529.5 | 587 | 0 | 0 | 8 | 425 | 223 +/- 192 | NA | |
| | | | 4 | 3 | 529.5 | 711 | 0 | 0 | 8 | 418 | 692 +/- 207 | NA | |
| | | | 5 | 3 | 529.5 | 714 | 0 | 0 | 8 | 429 | 722 +/- 212 | NA | |
| 12.2 | 0+25.5 | 0+3.5S1 | 6 | 478.0 | 680 | 0 | 0 | 8 | 409 | 791 +/- 207 | NA | | |
| | | | 2 | 3 | 529.5 | 605 | 0 | 0 | 8 | 418 | 288 +/- 192 | NA | |
| | | | 3 | 3 | 529.5 | 655 | 0 | 0 | 8 | 429 | 491 +/- 204 | NA | |
| | | | 4 | 3 | 529.5 | 650 | 0 | 0 | 8 | 429 | 472 +/- 203 | NA | |
| | | | 5 | 3 | 529.5 | 672 | 0 | 0 | 8 | 429 | 558 +/- 207 | NA | |
| 12.2 | 0+24.5 | 0+3.5S1 | 3 | 529.5 | 684 | 0 | 0 | 8 | 429 | 605 +/- 208 | NA | | |
| | | | 2 | 3 | 529.5 | 679 | 0 | 0 | 8 | 418 | 570 +/- 202 | NA | |
| 12.2 | 0+29.5 | 0+2.5S1 | 6 | 478.0 | 658 | 0 | 0 | 8 | 409 | 705 +/- 204 | NA | | |
| | | | 2 | 9 | 492.9 | 645 | 0 | 0 | 8 | 415 | 595 +/- 202 | NA | |

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TABLE 12.2-2

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | | 3 | 9 | 492.9 | 610 | 0 | 0 | 8 | 415 | 458 +/- 197 | NA |
| 12.2 0+28.5 | 0+2.5S1 | 6 | 478.0 | 647 | 0 | 0 | 8 | 409 | 661 +/- 202 | NA |
| | | 2 | 9 | 492.9 | 669 | 0 | 0 | 8 | 404 | 672 +/- 200 | NA |
| | | 3 | 9 | 492.9 | 613 | 0 | 0 | 8 | 415 | 470 +/- 197 | NA |
| | | 4 | 9 | 492.9 | 645 | 0 | 0 | 8 | 415 | 595 +/- 202 | NA |
| | | 5 | 9 | 492.9 | 626 | 0 | 0 | 8 | 415 | 521 +/- 199 | NA |
| 12.2 0+27.5 | 0+2.5S1 | 6 | 478.0 | 688 | 0 | 0 | 8 | 409 | 822 +/- 208 | NA |
| | | 2 | 9 | 492.9 | 635 | 0 | 0 | 8 | 404 | 542 +/- 196 | NA |
| | | 3 | 9 | 492.9 | 650 | 0 | 0 | 8 | 415 | 615 +/- 203 | NA |
| | | 4 | 9 | 492.9 | 624 | 0 | 0 | 8 | 415 | 513 +/- 199 | NA |
| | | 5 | 9 | 492.9 | 568 | 0 | 0 | 8 | 415 | 294 +/- 191 | NA |
| 12.2 0+26.5 | 0+2.5S1 | 6 | 478.0 | 601 | 0 | 0 | 8 | 409 | 481 +/- 195 | NA |
| | | 2 | 9 | 492.9 | 590 | 0 | 0 | 8 | 415 | 380 +/- 194 | NA |
| | | 3 | 9 | 492.9 | 626 | 0 | 0 | 8 | 415 | 521 +/- 199 | NA |
| | | 4 | 9 | 492.9 | 598 | 0 | 0 | 8 | 404 | 401 +/- 190 | NA |
| | | 5 | 9 | 492.9 | 586 | 0 | 0 | 8 | 415 | 364 +/- 193 | NA |
| 12.2 0+25.5 | 0+2.5S1 | 6 | 478.0 | 620 | 0 | 0 | 8 | 409 | 556 +/- 198 | NA |
| | | 2 | 9 | 492.9 | 563 | 0 | 0 | 8 | 415 | 274 +/- 190 | NA |
| | | 3 | 9 | 492.9 | 630 | 0 | 0 | 8 | 404 | 523 +/- 195 | NA |
| | | 4 | 9 | 492.9 | 589 | 0 | 0 | 8 | 415 | 220 +/- 188 | NA |
| | | 5 | 9 | 492.9 | 617 | 0 | 0 | 8 | 415 | 486 +/- 198 | NA |
| 12.2 0+24.5 | 0+2.5S1 | 9 | 492.9 | 636 | 0 | 0 | 8 | 415 | 560 +/- 201 | NA |
| | | 2 | 9 | 492.9 | 644 | 0 | 0 | 8 | 415 | 591 +/- 202 | NA |
| 12.2 0+29.5 | 0+1.5S1 | 6 | 478.0 | 586 | 0 | 0 | 8 | 398 | 412 +/- 188 | NA |
| | | 2 | 9 | 492.9 | 674 | 0 | 0 | 8 | 415 | 709 +/- 206 | NA |
| | | 3 | 9 | 492.9 | 643 | 0 | 0 | 8 | 415 | 588 +/- 202 | NA |
| | | 4 | 9 | 492.9 | 636 | 0 | 0 | 8 | 415 | 560 +/- 201 | NA |
| 12.2 0+28.5 | 0+1.5S1 | 6 | 478.0 | 641 | 0 | 0 | 8 | 409 | 638 +/- 201 | NA |
| | | 2 | 9 | 492.9 | 576 | 0 | 0 | 8 | 404 | 317 +/- 187 | NA |
| | | 3 | 9 | 492.9 | 598 | 0 | 0 | 8 | 415 | 411 +/- 195 | NA |
| | | 4 | 9 | 492.9 | 620 | 0 | 0 | 8 | 415 | 497 +/- 198 | NA |
| | | 5 | 9 | 492.9 | 641 | 0 | 0 | 8 | 415 | 580 +/- 202 | NA |
| 12.2 0+27.5 | 0+1.5S1 | 6 | 478.0 | 620 | 0 | 0 | 8 | 409 | 556 +/- 198 | NA |
| | | 2 | 9 | 492.9 | 584 | 0 | 0 | 8 | 404 | 347 +/- 188 | NA |
| | | 3 | 9 | 492.9 | 631 | 0 | 0 | 8 | 415 | 541 +/- 200 | NA |
| | | 4 | 9 | 492.9 | 622 | 0 | 0 | 8 | 415 | 505 +/- 199 | NA |
| | | 5 | 9 | 492.9 | 615 | 0 | 0 | 8 | 415 | 478 +/- 198 | NA |
| 12.2 0+26.5 | 0+1.5S1 | 6 | 478.0 | 648 | 0 | 0 | 8 | 409 | 665 +/- 202 | NA |
| | | 2 | 9 | 492.9 | 621 | 0 | 0 | 8 | 404 | 489 +/- 194 | NA |
| | | 3 | 9 | 492.9 | 629 | 0 | 0 | 8 | 415 | 533 +/- 200 | NA |
| | | 4 | 9 | 492.9 | 577 | 0 | 0 | 8 | 415 | 329 +/- 192 | NA |
| | | 5 | 9 | 492.9 | 654 | 0 | 0 | 8 | 404 | 614 +/- 198 | NA |
| 12.2 0+25.5 | 0+1.5S1 | 6 | 478.0 | 618 | 0 | 0 | 8 | 409 | 548 +/- 198 | NA |
| | | 2 | 9 | 492.9 | 646 | 0 | 0 | 8 | 415 | 599 +/- 202 | NA |
| | | 3 | 9 | 492.9 | 579 | 0 | 0 | 8 | 404 | 328 +/- 187 | NA |
| | | 4 | 9 | 492.9 | 634 | 0 | 0 | 8 | 415 | 552 +/- 201 | NA |
| | | 5 | 9 | 492.9 | 585 | 0 | 0 | 8 | 415 | 360 +/- 193 | NA |
| 12.2 0+24.5 | 0+1.5S1 | 6 | 478.0 | 635 | 0 | 0 | 8 | 409 | 615 +/- 200 | NA |
| | | 2 | 9 | 492.9 | 567 | 0 | 0 | 8 | 415 | 290 +/- 190 | NA |
| | | 3 | 9 | 492.9 | 629 | 0 | 0 | 8 | 404 | 519 +/- 195 | NA |
| 12.2 0+29.5 | 0+0.5S1 | 6 | 478.0 | 705 | 0 | 0 | 8 | 409 | 889 +/- 210 | NA |
| | | 2 | 9 | 492.9 | 698 | 0 | 0 | 8 | 415 | 803 +/- 210 | NA |
| | | 3 | 9 | 492.9 | 594 | 0 | 0 | 8 | 415 | 396 +/- 195 | NA |
| 12.2 0+28.5 | 0+0.5S1 | 6 | 478.0 | 587 | 0 | 0 | 8 | 409 | 427 +/- 193 | NA |
| | | 2 | 9 | 492.9 | 593 | 0 | 0 | 8 | 404 | 382 +/- 189 | NA |
| | | 3 | 9 | 492.9 | 618 | 0 | 0 | 8 | 415 | 490 +/- 198 | NA |
| | | 4 | 9 | 492.9 | 621 | 0 | 0 | 8 | 415 | 501 +/- 199 | NA |
| | | 5 | 9 | 492.9 | 577 | 0 | 0 | 8 | 415 | 329 +/- 192 | NA |
| 12.2 0+27.5 | 0+0.5S1 | 6 | 478.0 | 630 | 0 | 0 | 8 | 409 | 595 +/- 200 | NA |
| | | 2 | 9 | 492.9 | 628 | 0 | 0 | 8 | 404 | 515 +/- 195 | NA |

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TABLE 12.2-2

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | | 3 | 9 | 492.9 | 620 | 0 | 0 | 8 | 415 | 497 +/- 198 | NA |
| | | 4 | 9 | 492.9 | 611 | 0 | 0 | 8 | 415 | 462 +/- 197 | NA |
| | | 5 | 9 | 492.9 | 567 | 0 | 0 | 8 | 415 | 290 +/- 190 | NA |
| 12.2 0+26.5 | 0+0.5S1 | 6 | 478.0 | 584 | 0 | 0 | 8 | 409 | 415 +/- 193 | NA |
| | | 2 | 9 | 492.9 | 583 | 0 | 0 | 8 | 404 | 344 +/- 188 | NA |
| | | 3 | 9 | 492.9 | 574 | 0 | 0 | 8 | 415 | 317 +/- 192 | NA |
| | | 4 | 9 | 492.9 | 555 | 0 | 0 | 8 | 415 | 243 +/- 189 | NA |
| | | 5 | 9 | 492.9 | 620 | 0 | 0 | 8 | 415 | 497 +/- 198 | NA |
| 12.2 0+25.5 | 0+0.5S1 | 6 | 478.0 | 640 | 0 | 0 | 8 | 398 | 618 +/- 196 | NA |
| | | 2 | 9 | 492.9 | 640 | 0 | 0 | 8 | 415 | 576 +/- 201 | NA |
| | | 3 | 9 | 492.9 | 628 | 0 | 0 | 8 | 415 | 529 +/- 200 | NA |
| | | 4 | 9 | 492.9 | 560 | 0 | 0 | 8 | 415 | 263 +/- 189 | NA |
| | | 5 | 9 | 492.9 | 646 | 0 | 0 | 8 | 415 | 599 +/- 202 | NA |
| 12.2 0+24.5 | 0+0.5S1 | 6 | 478.0 | 641 | 0 | 0 | 8 | 398 | 622 +/- 196 | NA |
| | | 2 | 9 | 492.9 | 611 | 0 | 0 | 8 | 415 | 462 +/- 197 | NA |
| | | 3 | 9 | 492.9 | 684 | 0 | 0 | 8 | 415 | 748 +/- 208 | NA |
| | | 4 | 9 | 492.9 | 547 | 0 | 0 | 8 | 415 | 212 +/- 187 | NA |
| 12.2 0+29.5 | 0+0.5N1 | 6 | 478.0 | 731 | 0 | 0 | 8 | 409 | 990 +/- 214 | NA |
| | | 2 | 9 | 454.0 | 655 | 0 | 0 | 8 | 388 | 767 +/- 198 | NA |
| | | 3 | 9 | 454.0 | 728 | 0 | 0 | 8 | 398 | 1072 +/- 213 | NA |
| | | 4 | 9 | 454.0 | 614 | 0 | 0 | 8 | 398 | 626 +/- 197 | NA |
| | | 5 | 9 | 454.0 | 607 | 0 | 0 | 8 | 388 | 584 +/- 191 | NA |
| 12.2 0+28.5 | 0+0.5N1 | 6 | 478.0 | 699 | 0 | 0 | 8 | 409 | 865 +/- 210 | NA |
| | | 2 | 9 | 454.0 | 645 | 0 | 0 | 8 | 398 | 748 +/- 202 | NA |
| | | 3 | 9 | 454.0 | 784 | 0 | 0 | 8 | 398 | 1292 +/- 221 | NA |
| | | 4 | 9 | 454.0 | 618 | 0 | 0 | 8 | 398 | 642 +/- 198 | NA |
| | | 5 | 9 | 454.0 | 619 | 0 | 0 | 8 | 398 | 646 +/- 198 | NA |
| 12.2 0+27.5 | 0+0.5N1 | 6 | 478.0 | 594 | 0 | 0 | 8 | 409 | 454 +/- 194 | NA |
| | | 2 | 9 | 454.0 | 664 | 0 | 0 | 8 | 398 | 822 +/- 204 | NA |
| | | 3 | 9 | 454.0 | 621 | 0 | 0 | 8 | 398 | 654 +/- 198 | NA |
| 12.2 0+26.5 | 0+0.5N1 | 6 | 478.0 | 640 | 0 | 0 | 8 | 409 | 634 +/- 201 | NA |
| | | 2 | 9 | 454.0 | 630 | 0 | 0 | 8 | 398 | 689 +/- 199 | NA |
| | | 3 | 9 | 454.0 | 620 | 0 | 0 | 8 | 398 | 650 +/- 198 | NA |
| 12.2 0+25.5 | 0+0.5N1 | 9 | 454.0 | 645 | 0 | 0 | 8 | 398 | 748 +/- 202 | NA | |
| | | 2 | 9 | 454.0 | 661 | 0 | 0 | 8 | 398 | 810 +/- 204 | NA |
| 12.2 0+24.5 | 0+0.5N1 | 9 | 454.0 | 651 | 0 | 0 | 8 | 398 | 771 +/- 202 | NA | |

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TABLE 12.2-3

CINTICHEM DECOMMISSIONING PLAN 25-Jan-95 07:20 AM
FINAL SURVEY DATA SHEET
DATA FOR AFFECTED AREA DESCRIPTION:
AREA 12.2 - MALL 5K CONCRETE TANK BASE FOR ALPHA

RADIATION TYPE: 2 ALPHA
COMPLETION -
DATE: 11-17-94
TECHNICIANS: TA/CD/JB/PK MATERIAL CODE
LOCATION: 12.0 1:CONCRETE 5:PLASTIC
GRID ID: 12.2 2:ROCK 6:SOIL
MEDIA TYPE: CONCRETE 3:WOOD 7:ASPHALT
# of POINTS: 128 (>60) 4:METAL 8:OTHER(SPECIFY):
CT IN MINUTES: 1 NO MATERIAL BACKGROUND USED

DPM/100CM^2

| REM.+ FIXED: | | | LIMIT |
|---|---|---|---|
| MAX FOR IND GRID | 46 | PASS | 5000 |
| AVG - SURVEY UNIT | 6 | PASS | 5000 |
| STD X | 11 | | |
| MU SUB ALPHA | 7 | PASS | 5000 |
| MAX HOT SPOT | 0 | PASS | 15000 |

| ID # | GRID COORDINATES W | S | INST. ID # | ALPHA INST. AREA BKG CPM | ALPHA FIXED COUNTS/ 1 MINUTES | SCAN MAX ALPHA COUNTS | TOTAL CONT. AREA CM^2 | MATERIAL CODE | MDA DPM/ 100 CM^2 | WEIGHTED AVG. ALPHA FIXED DPM/ 100 CM^2 | AVG TEST | MAX PER 100 MAX CM^2 TEST |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 12.2 | 0+27.5 | 0+4.5S | 1 | 0.6 | 4 | 0 | 0 | 8 | 35 | 19 +/- 22 | NA | |
| 12.2 | 0+26.5 | 0+4.5S | 1 | 2.1 | 10 | 0 | 0 | 8 | 49 | 41 +/- 32 | NA | |
| | | | 2 | 2.1 | 2 | 0 | 0 | 8 | 49 | -1 +/- 15 | NA | |
| 12.2 | 0+25.5 | 0+4.5S | 1 | 0.6 | 2 | 0 | 0 | 8 | 35 | 8 +/- 16 | NA | |
| | | | 2 | 2.1 | 6 | 0 | 0 | 8 | 49 | 20 +/- 25 | NA | |
| | | | 3 | 2.1 | 3 | 0 | 0 | 8 | 49 | 5 +/- 18 | NA | |
| 12.2 | 0+24.5 | 0+4.5S | 1 | 2.1 | 5 | 0 | 0 | 8 | 49 | 15 +/- 23 | NA | |
| 12.2 | 0+29.5 | 0+3.5S | 1 | 1.7 | 9 | 0 | 0 | 8 | 49 | 40 +/- 33 | NA | |
| | | | 2 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA | |
| 12.2 | 0+28.5 | 0+3.5S | 1 | 0.6 | 2 | 0 | 0 | 8 | 35 | 8 +/- 16 | NA | |
| | | | 2 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA | |
| | | | 3 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA | |
| | | | 4 | 1.7 | 4 | 0 | 0 | 8 | 49 | 13 +/- 22 | NA | |
| 12.2 | 0+27.5 | 0+3.5S | 1 | 0.6 | 2 | 0 | 0 | 8 | 35 | 8 +/- 16 | NA | |
| | | | 2 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA | |
| | | | 3 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA | |
| | | | 4 | 2.1 | 3 | 0 | 0 | 8 | 49 | 5 +/- 18 | NA | |
| | | | 5 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA | |
| 12.2 | 0+26.5 | 0+3.5S | 1 | 0.6 | 4 | 0 | 0 | 8 | 35 | 19 +/- 22 | NA | |
| | | | 2 | 2.1 | 7 | 0 | 0 | 8 | 49 | 25 +/- 27 | NA | |
| | | | 3 | 2.1 | 3 | 0 | 0 | 8 | 49 | 5 +/- 18 | NA | |
| | | | 4 | 2.1 | 11 | 0 | 0 | 8 | 49 | 46 +/- 34 | NA | |
| | | | 5 | 2.1 | 4 | 0 | 0 | 8 | 49 | 10 +/- 21 | NA | |
| 12.2 | 0+25.5 | 0+3.5S | 1 | 0.6 | 0 | 0 | 0 | 8 | 35 | -3 +/- 3 | NA | |
| | | | 2 | 2.1 | 0 | 0 | 0 | 8 | 49 | -11 +/- 5 | NA | |
| | | | 3 | 2.1 | 5 | 0 | 0 | 8 | 49 | 15 +/- 23 | NA | |
| | | | 4 | 2.1 | 2 | 0 | 0 | 8 | 49 | -1 +/- 15 | NA | |
| | | | 5 | 2.1 | 5 | 0 | 0 | 8 | 49 | 15 +/- 23 | NA | |
| 12.2 | 0+24.5 | 0+3.5S | 1 | 2.1 | 3 | 0 | 0 | 8 | 56 | 5 +/- 18 | NA | |

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| NST EFF. CPM/DPM |
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| 0.1803 |
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TABLE 12.2-3

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | | 2 | 3 | 2.1 | 4 | 0 | 0 | 8 | 62 | 10 +/- 21 | NA |
| 12.2 | 0+29.5 | 0+2.5S1 | 6 | 0.6 | 8 | 0 | 0 | 8 | 88 | 41 +/- 31 | NA |
| | | 2 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| | | 3 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| 12.2 | 0+28.5 | 0+2.5S1 | 6 | 0.6 | 5 | 0 | 0 | 8 | 35 | 24 +/- 24 | NA |
| | | 2 | 9 | 1.7 | 3 | 0 | 0 | 8 | 49 | 7 +/- 19 | NA |
| | | 3 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 4 | 9 | 1.7 | 5 | 0 | 0 | 8 | 49 | 18 +/- 25 | NA |
| | | 5 | 9 | 1.7 | 3 | 0 | 0 | 8 | 49 | 7 +/- 19 | NA |
| 12.2 | 0+27.5 | 0+2.5S1 | 6 | 0.6 | 2 | 0 | 0 | 8 | 35 | 8 +/- 16 | NA |
| | | 2 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 3 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| | | 4 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 5 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| 12.2 | 0+26.5 | 0+2.5S1 | 6 | 0.6 | 4 | 0 | 0 | 8 | 35 | 19 +/- 22 | NA |
| | | 2 | 9 | 1.7 | 3 | 0 | 0 | 8 | 49 | 7 +/- 19 | NA |
| | | 3 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 4 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| | | 5 | 9 | 1.7 | 0 | 0 | 0 | 8 | 49 | -9 +/- 4 | NA |
| 12.2 | 0+25.5 | 0+2.5S1 | 6 | 0.6 | 2 | 0 | 0 | 8 | 35 | 8 +/- 16 | NA |
| | | 2 | 9 | 1.7 | 3 | 0 | 0 | 8 | 49 | 7 +/- 19 | NA |
| | | 3 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| | | 4 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 5 | 9 | 1.7 | 0 | 0 | 0 | 8 | 49 | -9 +/- 4 | NA |
| 12.2 | 0+24.5 | 0+2.5S1 | 9 | 1.7 | 6 | 0 | 0 | 8 | 49 | 24 +/- 27 | NA |
| | | 2 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| 12.2 | 0+29.5 | 0+1.5S1 | 6 | 0.6 | 1 | 0 | 0 | 8 | 35 | 2 +/- 11 | NA |
| | | 2 | 9 | 1.7 | 4 | 0 | 0 | 8 | 49 | 13 +/- 22 | NA |
| | | 3 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 4 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| 12.2 | 0+28.5 | 0+1.5S1 | 6 | 0.6 | 0 | 0 | 0 | 8 | 35 | -3 +/- 3 | NA |
| | | 2 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 3 | 9 | 1.7 | 3 | 0 | 0 | 8 | 49 | 7 +/- 19 | NA |
| | | 4 | 9 | 1.7 | 5 | 0 | 0 | 8 | 49 | 18 +/- 25 | NA |
| | | 5 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| 12.2 | 0+27.5 | 0+1.5S1 | 6 | 0.6 | 3 | 0 | 0 | 8 | 35 | 13 +/- 19 | NA |
| | | 2 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 3 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 4 | 9 | 1.7 | 3 | 0 | 0 | 8 | 49 | 7 +/- 19 | NA |
| | | 5 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| 12.2 | 0+26.5 | 0+1.5S1 | 6 | 0.6 | 2 | 0 | 0 | 8 | 35 | 8 +/- 16 | NA |
| | | 2 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| | | 3 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| | | 4 | 9 | 1.7 | 3 | 0 | 0 | 8 | 49 | 7 +/- 19 | NA |
| | | 5 | 9 | 1.7 | 5 | 0 | 0 | 8 | 49 | 18 +/- 25 | NA |
| 12.2 | 0+25.5 | 0+1.5S1 | 6 | 0.6 | 3 | 0 | 0 | 8 | 35 | 13 +/- 19 | NA |
| | | 2 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 3 | 9 | 1.7 | 0 | 0 | 0 | 8 | 49 | -9 +/- 4 | NA |
| | | 4 | 9 | 1.7 | 0 | 0 | 0 | 8 | 49 | -9 +/- 4 | NA |
| | | 5 | 9 | 1.7 | 5 | 0 | 0 | 8 | 49 | 18 +/- 25 | NA |
| 12.2 | 0+24.5 | 0+1.5S1 | 6 | 0.6 | 3 | 0 | 0 | 8 | 35 | 13 +/- 19 | NA |
| | | 2 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| | | 3 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| 12.2 | 0+29.5 | 0+0.5S1 | 6 | 0.6 | 3 | 0 | 0 | 8 | 35 | 13 +/- 19 | NA |
| | | 2 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 3 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| 12.2 | 0+28.5 | 0+0.5S1 | 6 | 0.6 | 2 | 0 | 0 | 8 | 35 | 8 +/- 16 | NA |
| | | 2 | 9 | 1.7 | 0 | 0 | 0 | 8 | 49 | -9 +/- 4 | NA |
| | | 3 | 9 | 1.7 | 0 | 0 | 0 | 8 | 49 | -9 +/- 4 | NA |
| | | 4 | 9 | 1.7 | 0 | 0 | 0 | 8 | 49 | -9 +/- 4 | NA |

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TABLE 12.2-3

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | 5 | 9 | 1.7 | 0 | 0 | 0 | 8 | 49 | -9 +/- 4 | NA |
| 12.2 0+27.5 | 0+0.5S1 | 6 | 0.6 | 6 | 0 | 0 | 8 | 35 | 30 +/- 27 | NA | |
| | | 2 | 9 | 1.7 | 3 | 0 | 0 | 8 | 49 | 7 +/- 19 | NA |
| | | 3 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| | | 4 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 5 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| 12.2 0+26.5 | 0+0.5S1 | 6 | 0.6 | 3 | 0 | 0 | 8 | 35 | 13 +/- 19 | NA | |
| | | 2 | 9 | 1.7 | 3 | 0 | 0 | 8 | 49 | 7 +/- 19 | NA |
| | | 3 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 4 | 9 | 1.7 | 1 | 0 | 0 | 8 | 49 | -4 +/- 12 | NA |
| | | 5 | 9 | 1.7 | 3 | 0 | 0 | 8 | 49 | 7 +/- 19 | NA |
| 12.2 0+25.5 | 0+0.5S1 | 6 | 0.6 | 5 | 0 | 0 | 8 | 35 | 24 +/- 24 | NA | |
| | | 2 | 9 | 1.7 | 4 | 0 | 0 | 8 | 49 | 13 +/- | NA |
| | | 3 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/ | NA |
| | | 4 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| | | 5 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| 12.2 0+24.5 | 0+0.5S1 | 6 | 0.6 | 5 | 0 | 0 | 8 | 35 | 24 +/- 24 | NA | |
| | | 2 | 9 | 1.7 | 2 | 0 | 0 | 8 | 49 | 2 +/- 16 | NA |
| | | 3 | 9 | 1.7 | 4 | 0 | 0 | 8 | 49 | 13 +/- 22 | NA |
| | | 4 | 9 | 1.7 | 3 | 0 | 0 | 8 | 49 | 7 +/- 19 | NA |
| 12.2 0+29.5 | 0+0.5N1 | 6 | 0.6 | 2 | 0 | 0 | 8 | 35 | 8 +/- 16 | NA | |
| | | 2 | 9 | 2 | 2 | 0 | 0 | 8 | 51 | 0 +/- 16 | NA |
| | | 3 | 9 | 2 | 4 | 0 | 0 | 8 | 51 | 11 +/- 22 | NA |
| | | 4 | 9 | 2 | 0 | 0 | 0 | 8 | 51 | -11 +/- 5 | NA |
| | | 5 | 9 | 2 | 1 | 0 | 0 | 8 | 51 | -6 +/- 12 | NA |
| 12.2 0+28.5 | 0+0.5N1 | 6 | 0.6 | 2 | 0 | 0 | 8 | 35 | 8 +/- 16 | NA | |
| | | 2 | 9 | 2 | 1 | 0 | 0 | 8 | 51 | -6 +/- 12 | NA |
| | | 3 | 9 | 2 | 2 | 0 | 0 | 8 | 51 | 0 +/- 16 | NA |
| | | 4 | 9 | 2 | 3 | 0 | 0 | 8 | 51 | 6 +/- 19 | NA |
| | | 5 | 9 | 2 | 3 | 0 | 0 | 8 | 51 | 6 +/- 19 | NA |
| 12.2 0+27.5 | 0+0.5N1 | 6 | 0.6 | 0 | 0 | 0 | 8 | 35 | -3 +/- 3 | NA | |
| | | 2 | 9 | 2 | 6 | 0 | 0 | 8 | 51 | 22 +/- 27 | NA |
| | | 3 | 9 | 2 | 2 | 0 | 0 | 8 | 51 | 0 +/- 16 | NA |
| 12.2 0+26.5 | 0+0.5N1 | 6 | 0.6 | 4 | 0 | 0 | 8 | 35 | 19 +/- 22 | NA | |
| | | 2 | 9 | 2 | 1 | 0 | 0 | 8 | 51 | -6 +/- 12 | NA |
| | | 3 | 9 | 2 | 3 | 0 | 0 | 8 | 51 | 6 +/- 19 | NA |
| 12.2 0+25.5 | 0+0.5N1 | 9 | 2 | 1 | 0 | 0 | 8 | 51 | -6 +/- 12 | NA | |
| | | 2 | 9 | 2 | 1 | 0 | 0 | 8 | 51 | -6 +/- 12 | NA |
| 12.2 0+24.5 | 0+0.5N1 | 9 | 2 | 5 | 0 | 0 | 8 | 51 | 17 +/- 25 | NA | |

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