

# NUCLEAR POWER PLANT SYSTEM SOURCEBOOK

# BYRON 1 AND 2

50-454 and 50-455





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50-454 and 50-455

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# TABLE OF CONTENTS

Sectio		Page
1	SUMMARY DATA ON PLANT	1
2	IDENTIFICATION OF SIMILAR NUCLEAR POWER PLANTS	1
3	SYSTEM INFORMATION  3.1 Reactor Coolant System (RCS)  3.2 Auxiliary Feedwater (AFW) System and Secondary	2 7
	Steam Relief (SSR) System  3.3 Emergency Core Cooling System (ECCS)  3.4 Charging System (CVCS)  3.5 Containment Heat Removal Systems (PAHRS)  3.6 Instrumentation and Control System (I & C)  3.7 Electric Power System  3.8 Component Cooling System  3.9 Essential Service Water (ESW) System	13 20 30 35 41 45 60 65
4	PLANT INFORMATION 4.1 Site and Building Summary 4.2 Facility Layout Drawings 4.3 Section 4 References	72
5	BIBI IOGRAPHY FOR BYRON 1 AND 2	93
	APPENDIX A, Definition of Symbols Used in the System and Layout Drawings	94
	APPENDIX B, Definition of Terms Used in the Data Tables	101

# LIST OF FIGURES

Figure		Page
3-1	Cooling Water Systems Functional Diagram for Byron Units 1 and 2	6
3.1-1	Isometric View of a 4-Loop Westinghouse RCS	9
3.1-2	Byron Unit 1 Reactor Coolant System	10
3.1-3	Byron Unit 1 Reactor Coolant System Showing Component Locations	11
3.2-1	Byron Unit 1 Auxiliary Feedwater System	16
3.2-2	Byron Unit 1 Auxiliary Feedwater System Showing Component Locations	17
3.2-3	Byron Unit 1 Startup Feedwater System	18
3.3-1	Byron Unit 1 Safety Injection System	24
3.3-2	Byron Unit 1 Safety Injection System Showing Component Locations	25
3.3-3	Byron Unit 1 Residual Heat Removal System	26
3.3-4	Byron Unit 1 Residual Heat Removal System Showing Component Locations	27
3.4-1	Byron Unit 1 Charging System	32
3.4-2	Byron Unit 1 Charging System Showing Component Locations	33
3.5-1	Byron Unit 1 Containment Spray System	38
3.5-2	Byton Unit 1 Containment Spray System Showing Component Locations	39
3.7-1	Byron Unit 1 4160 and 480 VAC Electric Power Distribution System .	48
3.7-2	Byron Unit 1 4160 and 480 VAC Electric Power Distribution System Showing Component Locations	49
2.7-3	Byron Unit 1 125 VDC and 120 VAC Electric Power Distribution System	50
2.7-4	Byron Unit 1 125 VDC and 120 VAC Electric Power Distribution System Showing Component Locations	51
3.7-5	Byron Unit 1 Diesel Fuel Oil System	52

# LIST OF FIGURES (continued)

Figure		Page
3.8-1	Byron Unit 1 & 2 Component Cooling Water System	62
3.8-2	Byron Unit 1 & 2 Component Cooling Water System Showing Component Locations	63
3.9-1	Byron Unit 1 & 2 Essential Service Water System	67
3.9-2	Byron Unit 1 & 2 Essential Service Water System Showing Component Locations	69
4-1	General View of Byron Nuclear Station and Vicinity	73
4-2	Byron 1 & 2 Plot Plan	74
4-3	Byron Unit 1 Reactor, Auxiliary, and Turbine Building Elevation Drawing	75
4-4	Byron 1 & 2 Reactor, Auxiliary, and Fuel Handling Building Elevation Drawing	76
4-5	Byron 1 & 2 Station Arrangement, Elevation 330' of the Auxiliary Building	77
4-6	Byron 1 & 2 Station Arrangement, Elevation 346'	78
4-7	Byron 1 & 2 Station Arrangement, Elevation 364'	79
4-8	Byron 1 & 2 Station Arrangement, Elevation 383'	80
4-9	Byron 1 & 2 Station Arrangement, Elevation 401'	81
4-10	Byron 1 & 2 Station Arrangement, Elevation 426'	82
4-11	Byron 1 & 2 Station Arrangement, Elevation 451'	83
A-1	Key to Symbols in Fluid System Drawings	97
A-2	Key to Symbols in Electrical System Drawings	99
A-3	Key to Symbols in Facility Layout Drawings	100

# LIST OF TABLES

Table		Page
3-1	Summary of Byron 1 & 2 Systems Covered in this Report	3
3.1-1	Byron Reactor Coolant System Data Summary for Selected Components	12
3.2-1	Byton Auxiliary Feedwater System Data Summary for Selected Components	19
3.3-1	Byton Emergency Core Cooling System Data Summary for Selected Components	28
3.4-1	Byron Charging System Data Summary for Selected Components	34
3.5-1	Byron Containment Heat Removal System Data Summary for Selected Components	40
3.6-1	Byron Equipment Controls Available Outside the Control Room	44
3.7-1	Byton Electric Power System Data Summary for Selected Components	53
3.7-2	Partial Listing of Electrical Sources and Loads	55
3.8-1	Byron Component Cooling Water System Data Summary for Selected Components	64
3.9-1	Byron Essential Service Water System Data Summary for Selected Components	71
4-1	Definition of Byron 1 Building and Location Codes	84
4-2	Partial Listing of Components by Location at Byron	87
B-1	Component Type Codes	103

### CAUTION

The information in this report has been developed over an extended period of time based on a site visit, the Final Safety Analysis Report, system and layout drawings, and other published information. To the best of our knowledge, it accurately reflects the plant configuration at the time the information was obtained, however, the information in this document has not been independently verified by the licensee or the NRC.

#### NOTICE

This sourcebook will be periodically updated with new and/or replacement pages as appropriate to incorporate additional information on this reactor plant. Technical errors in this report should be brought to the attention of the following:

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Correction and other recommended changes should be submitted in the form of marked up copies of the affected text, tables or figures. Supporting documentation should be included if possible.

# BYRON 1 AND 2 RECORD OF REVISIONS

REVISION	ISSUE	COMMENTS
0	1/89	Original report

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#### BYRON 1 AND 2 SYSTEM SOURCEBOOK

This sourcebook contains summary information on Byron 1 and 2. Summary data on this plant are presented in Section 1, and similar nuclear power plants are identified in Section 2. Information on selected reactor plant systems is presented in Section 3, and the site and building layout is illustrated in Section 4. A bibliography of reports that describe features of this plant or site is presented in Section 5. Symbols used in the system and layout drawings are defined in Appendix A. Terms used in data tables are defined in Appendix B.

### SUMMARY DATA ON PLANT

Basic information on the Byron 1 & 2 nuclear power plant is listed below:

Docket number

- Operator

- Location

- Commercial operation date

Reactor type
 NSSS vendor

- Number of loops

- Power (MWt/MWe)

Architect-engineer

Containment type

50-454 (Unit 1), 50-455 (Unit 2) Commonwealth Edison Company

Byron, Illinois

9/85 (Unit 1), 8/87 (Unit 2)

PWR

Westinghouse

4

3411/1120

Sargent & Lundy

Reinforced concrete cylinder with steel

liner

### 2. IDENTIFICATION OF SIMILAR NUCLEAR POWER PLANTS

Each Byron unit has a Westinghouse PWR four-loop nuclear steam supply system (NSSS). Other four-loop Westinghouse plants in the United States include:

- Braidwood 1 and 2
- Callaway
- Catawba 1 and 2
- Comanche Peak 1 and 2
- Donald C. Cook 1 and 2 (ice condenser containment)
- Diablo Canyon 1 and 2
- Haddam Neck
- Indian Point 2 and 3
- McGuire 1 and 2 (ice condenser containment)
- Millstone 3
- Salem 1 and 2
- Seabrook 1
- Sequoyah 1 and 2 (ice condenser containment)
- Shearon Harris 1 and 2
- South Texas 1 and 2
- Trojan
- · Vogtle 1 and 2
- Watts Bar 1 and 2
- Wolf Creek
- Yankee Rowe
- Zion I and 2

Byron differs from the majority of Westinghouse plants in that the auxiliary feedwater system consists of one motor driven and one diesel driven pump, whereas other plants contain some number of motor driven and turbine driven pumps. Byron is similar to other plants in the number and type of charging and high pressure injection pumps.

Byron is a twin of the Braidwood plant. However, there are minor differences between the two plants. These differences are noted in the appropriate sections of this

report.

#### 3. SYSTEM INFORMATION

This section contains descriptions 5, selected systems at Byron 1 and 2 in terms of general function, operation, system success criteria, major components, and support system requirements. A summary of major systems at Byron 1 and 2 is presented in Table 3-1. In the "Report Section" column of this table, a section reference (i.e. 3.1, 3.2, etc.) is provided for all systems that are described in this report. An entry of "X" in this column means that the system is not described in this report. In the "FSAR Section Reference" column, a cross-reference is provided to the section of the Final Safety Analysis Report where additional information on each system can be found. Other sources of information on this plant are identified in the bibliography in Section 5.

Several cooling water systems are identified in Table 3-1. The functional relationships that exist among cooling water systems required for safe shutdown are shown in Figure 3-1. Details on the individual cooling water systems are provided in the report

sections identified in Table 3-1.

Table 3-1. Summary of Byron 1 & 2 Systems Covered in this Report

Concric System Name	Plant-Specific System_Name	Report Section	FSAR Section Reference
Reactor Heat Removal Systems Reactor Coolant System (RCS)	Same	3.1	5
- Auxiliary Feedwater (AFW) and Secondary Steam Relief (SSR) Systems	Same	3.2	10.4.9
- Emergency Core Cooling Systems (ECCS)	Same		
- High-Pressure Injection & Recirculation - Low-pressure Injection & Recirculation	Safety Injection System, Charging System Residual Heat Removal System	3.3 3.3 3.3	6.3 6.3 6.3
- Decay Heat Removal (DHR) System (Residual Heat Removal (RHR) System)	Residual Heat Removal (RHR) System	3.3	6.3
- Main Steam and Power Conversion Systems	Main Steam Supply System, Condensate and Feedwater System, Circulating Water System	X	10.3, 10.4
- Other Heat Removal Systems	None identified	X	
Reactor Coolant Inventory Control Systems - Chemical and Volume Control System (CVCS) (Charging System)	Same	3.4	9.3.4, 6.3
- ECCS	See ECCS, above		

Table 3-1. Summary of Byron 1 & 2 Systems Covered in this Report (Continued)

Generic System Name	Plant-Specific System Name	Report Section	FSAR Section Reference
Containment Systems			
- Containment	Same	X	6.2.1
- Containment Heat Removal Systems - Containment Spray System	Same	3.5	6.5.2
- Containment Fan Cooler System	Reactor Containment Fan Cooler Subsystem	3.5	9.4.8.1, 6.2.2
Containment Normal Ventilation Systems	Containment Ventilation System	X	9.4.8
- Combustible Gas Control Systems	Hydrogen Reconbiner System, Hydrogen Monitoring System, Hydrogen Mixing System, Post-LOCA Purge System	x	6.2.5
Reactor and Reactivity Control Systems Reactor Core	Same	X	4.0
- Control Rod System	Control Rod Drive System	X	4.6
- Boration Systems	See CVCS, above		
Instrumentation & Control (I&C) Systems			
Reactor Protection System (RPS)	Reactor Trip System	3.6	7.2
- Engineered Safety Feature Actuation System (ESFAS)	Same	3.6	7.3
- Remote Shutdown System	Various Remote Shutdown Panels	X	7.4

Table 3-1. Summary of Byron 1 & 2 Systems Covered in this Report (Continued)

		vstem Name	Plant-Specific System Name	Report Section	FSAR Section Reference
	1	Other I&C Systems  Other I&C Systems	ems (continued) Various systems	Х	7.5, 7.6, 7.7
	S	upport Systems Class 1E Electric Power System	Same	3.7	8.1, 8.3
		Non-Class 1E Electric Power System	Same	3.7	8.2, 8.3
		Diesel Generator Auxiliary Systems	Same	3.7	9.5.4 thru 9.5.8
		Component Cooling Water (CCW) System	Component Cooling System	3.8	9.2.2
On .		Service Water System (SWS)	Essential Service Water System, Non-essential Service Water System	3.9	9.2.1
		Other Cooling Water Systems	Plant Chilled Water System	X	9.2.7
	Ä.	Fire Protection Systems	Same	X	9.5.1
		Room Heating, Ventilating, and Air- Conditioning (HVAC) Systems	Same	X	9.4
		Instrument and Service Air Systems	Compressed Air Systems	X	9.3.1
		Refueling and Spent Fuel Systems	Spent Fuel Pit Cooling and Cleanup System, Fuel Handling System	X	9.1.3, 9.1.4
1/89		Radioactive Waste Systems	Radioactive Waste Management Systems	X	-11
9		Radiation Protection Systems	Same	x	12

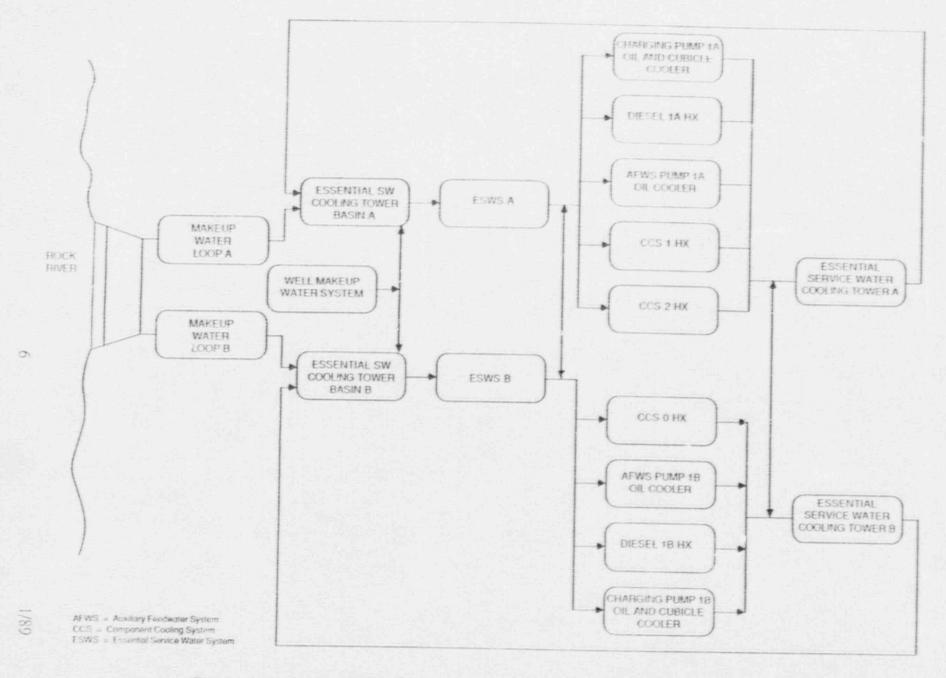


Figure 3-1. Cooling Water Systems Functional Diagram for Byron Units 1 and 2

## 3.1 REACTOR COOLANT SYSTEM (RCS)

3.1.1 System Function

The RCS transfers heat from the reactor core to the secondary coolant system via the steam generators. The RCS pressure boundary also establishes a boundary against the uncontrolled release of radioactive material from the reactor core and primary coolant.

3.1.2 System Definition

The RCS includes: (a) the reactor vessel, (b) reactor coolant loops, (c) reactor coolant pumps. (d) the primary side of the steam generators, (e) pressurizer, and (f) connected piping out to a suitable isolation valve boundary. An isometric drawing of a 4-loop Westinghouse RCS is shown in Figure 3.1-1. A simplified diagram of the RCS and important system interfaces is shown in Figure 3.1-2. A summary of data on selected RCS components is presented in Table 3.1-1.

3.1.3 System Operation

During power operation, circulation in the RCS is maintained by one reactor coolant pump in each of the four reactor coolant loops. RCS pressure is maintained within a prescribed band by the combined action of pressurizer heaters and pressurizer spray. RCS coolant inventory is measured by pressurizer water level which is maintained within a prescribed band by the chemical and volume control system (charging system).

At power, core heat is transferred to secondary coolant (feedwater) in the steam generators. The heat transfer path to the ultimate heat sink is completed by the a ain steam

and power conversion system and the circulating water system.

Following a transient or small LOCA (if RCS inventory is maintained), reactor core heat is still transferred to secondary coolant in the steam generators. Flow in the RCS is maintained by the reactor coolant pumps or by natural circulation. The heat transfer path to the ultimate heat sink can be established by using the secondary steam relief system (see Section 3.2) to vent main steam to atmosphere when the power conversion and circulating water systems are not available. If reactor core heat removal by this alternate path is not adequate, the RCS pressure will increase and a heat balance will be established in the RCS by venting steam or reactor coolant to the containment through the pressurizer relief valves. There are two power-operated relief valves and three safety valves on the pressurizer. A continued inability to establish adequate heat transfer to the steam generators will result in a LOCA-like condition (i.e., continuing loss of reactor coolant through the pressurizer relief valves). Repeated cycling of these relief valves has resulted in valve failure (i.e., relief valve stuck open).

Following a large LOCA, reactor core heat is dumped to the containment as reactor coolant and ECCS makeup water spills from the break. For a short-term period, the containment can act as a heat sink; however, the containment cooling systems must operate in order to complete a heat transfer path to the ultimate heat sink (see Section 3.5).

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3.1.4 System Success Criteria

The RCS success criteria can be described in terms of LOCA and transient mitigation, as follows:

- An unmitigatible LOCA is not initiated.

If a mitigatible LOCA is initiated, then LOCA mitigating systems are successful.

If a transient is initiated, then either:

RCS integrity is maintained and transient mingating systems are successful, or

RCS integrity is not maintained, leading to a LOCA-like condition (i.e. stuck-open safety or relief valve, reactor coolant pump seal failure), and LOCA mitigating systems are successful.

### 3.1.5 Component Information

#### A. RCS

Volume: 12,257 ft<sup>3</sup>, including pressurizer
 Normal operating pressure: 2250 psia

#### B. Pressurizer

1. Volume: 1800 ft3

### C. Safety Valves (3)

1. Set pressure: 2485 psig

2. Relief capacity: 420,000 lb/hr each

### D. Power-Operated Relief Valves (2)

1. Set pressure: 2335 psig

2. Relief capacity: 210,000 lb/hr each

#### E. Steam Generators

Type: Vertical shell and U-Tube
 Model: Westinghouse 51 Series

#### F. Pressurizer Heaters

1. Capacity: 1800 kW

## 3.1.6 Support Systems and Interfaces

#### A. Motive Power

 The pressurizer heaters are Class 1E AC loads that can be supplied from the standby diesel generators as described in Section 3.7.

2. The reactor coolant pumps are supplied from Non-Class 1E switchgear.

B. Reactor Coolant Pump Seal Injection Water System

The chemical and volume control system supplies seal water to cool the reactor coolant pump shaft seals and to maintain a controlled inleakage of seal water into the RCS. Loss of seal water flow may result in RCS leakage through the pump shaft seals which will resemble a small LOCA.

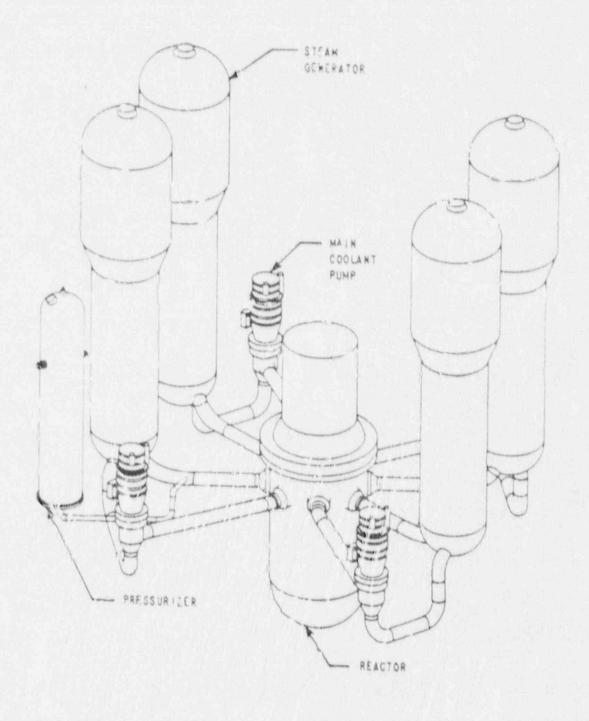


Figure 3.1-1. Isometric View of a 4-Loop Westinghouse RCS.

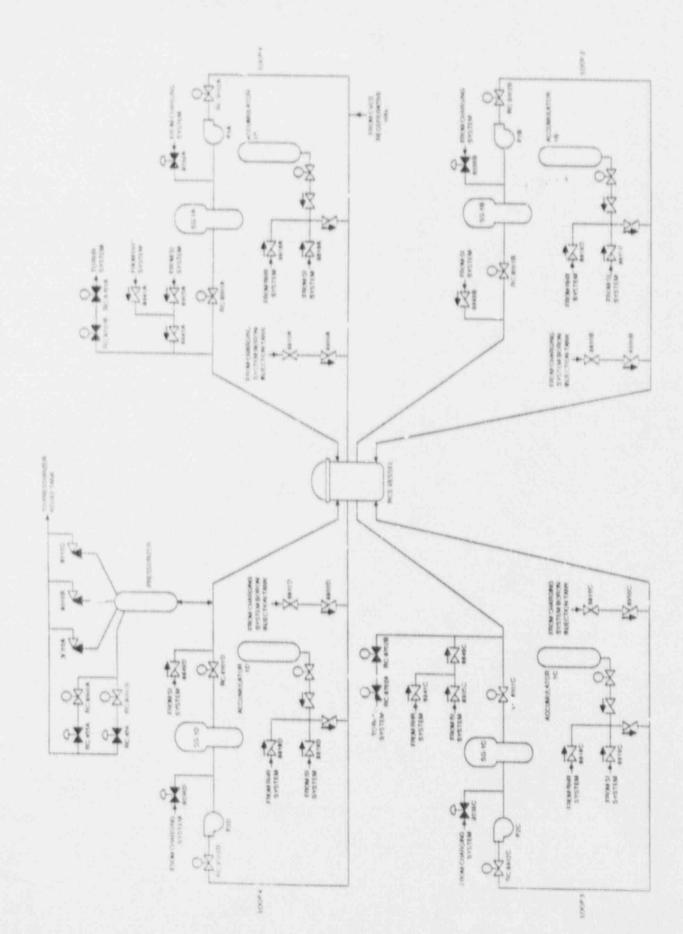


Figure 3.1-2. Byron Unit 1 Reactor Coolant System

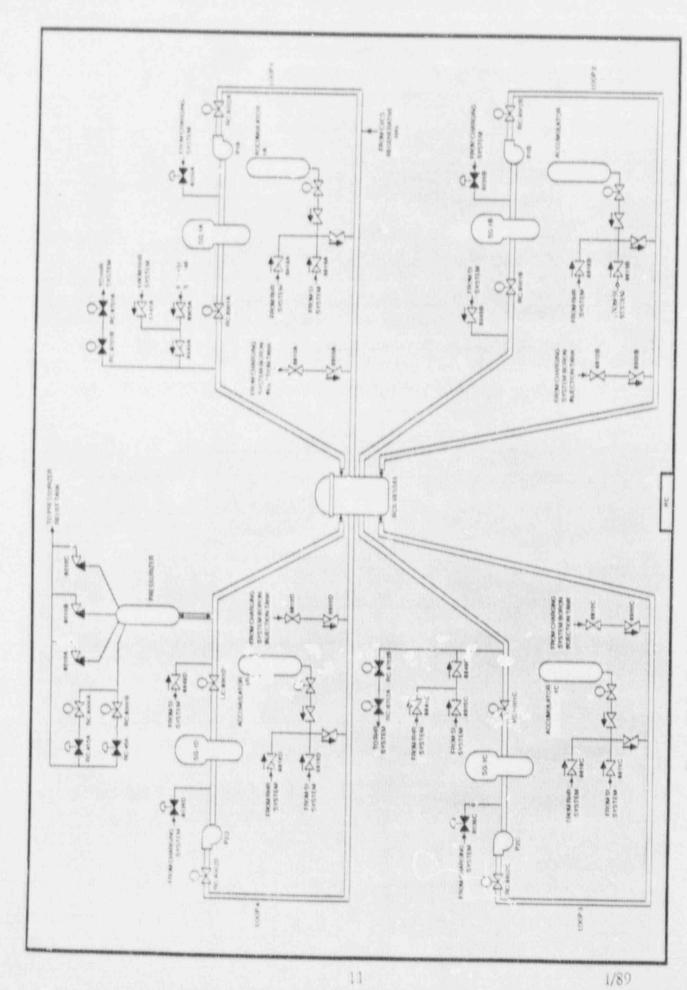


Figure 3.1-3. Byron Unit 1 Reactor Cowlant System Shewing Component Locations

Table 3.1-1. Byron Reactor Coolant System Data Summary for Selected Components

COMPONENT ID	CCMP.	LOCATION	POWER SOURCE	VOLTAGE	POWER SOURCE	EMERC.
RC-455A	NV	RC				
RC-456	NV	RC				
RC-8000A	MOV	RC	MCC-131X2	480	414PENRM	AC/A
RC-8000B	MOV	RC	MCC-102X2	480	426PENRM	AC/B
RC-8001A	MOV	RC	İ			
RC-8001B	MOV	HC .				
RC-8001C	MOV	RC				
RC-8001D	MOV	RC				
RC-8002A	MOV	RC				
RC-8002B	MOV	RC				
RC-8002C	MOV	RC				
RC-8002D	MOV	RC				
RC-8701A	MOV	RC	MCC-131X2	499	414PENRM	AC/A
RC-8701B	MOV	RC	MCC-132X2	480	426PENRM	AC/B
RC-8702A	MOV	RC	MCC-131X2	480	414PENRM	AC/A
RC-8702B	MOV	RC	MCC-132X2	480	426PENRM	AC/B
RCS-VESSEL	RV	RC				

#### 3.2 AUXILIARY FEEDWATER (AFW) SYSTEM AND SECONDARY STEAM RELIEF (SSR) SYSTEM

System Function

The AFW system provides a source of feedwater to the steam generators to remove heat from the reactor coola: system (RCS) when: (a) the main feedwater system is not available, and (b) RCS pressure is too high to permit heat removal by the residual heat removal (RHR) system. The SSR system provides a steam vent path from the steam generators to the atmosphere, thereby completing the heat transfer path to an ultimate heat sink when the main steam and power conversion systems are not available. Together, the AFW and SSR systems constitute an open-loop fluid system that provides to heat transfer from the RCS following transients and small-break LOCAs.

3.2.2 System Definition

The AFW system consists of one motor-driven pump and one diesel-driven pump. The normal water sources for the pumps is the condensate storage tank. An alternate source of water is the Essential Service Water system. Either pump can supply all four steam generators. Interfacing with the AFW system is the startup feedwater system. which consists 6; one startup feedwater pump supplied from the main condenser hotwell via the main condensate and feed booster pumps.

The SSR system includes five safety valves and one power-operated pressure

control valve on each of the four main steam lines.

Simplified drawings of the AFW and SSR systems are shown in Figures 3.2-1 and 3.2-2. The startup feedwater system is shown in Figure 3.2-3. A summary of data on selected AFW system components is presented in Table 3.2-1.

3.2.3 System Operation

During normal operation the AFW system is in standby, and is automotically actuated on either a low-low level in any steam generator, a safety injection signal, or a loss of power to the reactor coolant pumps. The system can also be manually started from the control room. Ordinarily, the AFW system is required to operate for about 5 hours to cool the unit down to 350°F, below which temperature the low pressure residual heat removal system operates.

Both AFW pumps are 1165 brake horsepower units. The diesel-driven AFW pump is capable of providing 840 gpm at 3350 feet head, which is nearly twice the sar acity required for system success. This pump is capable of supplying its own cooling and lubrication independently of AC power, but when AC power is available backup punips are provided for oil pressure, water jacket cooling, and room air cooling. The motor-driven AFW pump is capable of providing 890 gpm at 3350 feet of head. It requires essential service water for cooling (Ref. 1).

The primary suction source is the concensate storage tank. Redundant flow paths begin at the CST and meet at a header which supplies both pumps. No single valve can block the flow path. In the event of low suction pressure, there is automatic

switchover to service water as the AFW pump water source.

Flow from each AFW pump goes to all four steam generators through independent paths. Flow is regulated by eight manually controlled air-operated valves which fail open on loss of air.

3.2.4 System Success Criteria

For the decay heat removal function to be successful both the AFW system and the SSR system must operate successfully. The AFW success criteria are the following (Ref. 1 and 2):

> 1/89 13

- Either AFW pump can provide adequate flow.

- Water must be provided from the Condensate Storage Tank or Essential

Service Water System

Delivery requirements are 160 gpm to each of three steam generators or 240 gpm to each of two steam generators. This delivery must commence prior to the steam generators boiling dry (within 20 to 30 minutes)

The SSR system must operate to complete the heat transfer path to the environment. The number of safety valves which must open for the decay heat removal function is not known.

The startup feedwater system may be available as an alternate source of stean generator makeup if offsite power is available and the suction path from the main condenses hotwell via the condensate and feed booster pumps is functional.

## 3.2.5 Component Information

A. Motor-driven AFW pump 1A

1. Rated flow: 890 gpm @ 3350 ft. head (1452 psid)

2. Rated capacity: 175% (Ref. 1)

3. Type: Centrifugal

B. Diesel-driven AFW pump

1. Rated flow: 840 gpm @ 3350 ft. head (1452 psid)

2. Rated capacity: 185% (Ref. 1)

3. Type: Centrifugal

C. Startup Feedwater Pump

1. Rated flow: unknown

2. Type: Centrifugal

D. Condensate storage tank

1. Capacity: Unknown

2. Design Pressure: Atmospheric

E. Secondary steam relief valves

1. Five safety valves per main steam line

2. One power-operated pressure control valve per main steam line

## 3.2.6 Support Systems and Interfaces

## A. Control Signals

1. Automatic

- a. The AFW pumps are automatically actuated based on the following signals:
  - low-low water level in any one steam generator

safety injection signal

- loss of offsite power and station normal auxiliary power (blackout).
- b. The water source for the AFW pumps is automatically switched to the Essential Service Water system on low pump suction pressure.

- c. The AFW pumps are automatically tripped on low suction pressure.
- Remote manual
   The AFW system can be actuated by remote manual means from the main control room and from the remote shutdown control panel.

B. Motive power

- The AFW motor-driven pump and motor-operated valves are Class 1E AC loads that can be supplied from the standby diesel generators as described in Section 3.7. Redundant loads are supplied from separate load groups.
- 2. The AFW diesel-driven pump is supplied with fuel from a day tank.

#### C. Other

 Cooling for the motor-driven pump is provided by the essential service water system (see Section 3.9). Cooling for the diesel-driven pump is provided locally.

2. Pump cubicle coolers are cooled by essential service water (see Section

3.9)

 Each AFW pump has an auxiliary lube oil pump that provides lubrication prior to starting the pump. For a normal pump startup, the pump will start when an oil pressure interlock is satisfied. Under emergency start condition prelubrication is not required for AFW pump start (Ref. 2).

### 3.2.7 Section 3.2 References

- Youngblood, R. and Papazaglou, I.A., "Review of the Byron/Braidwood Units 1 and 2 Auxiliary Feedwater System Reliability Analysis, NUREG/CR-3096, BNL-NUREG-51633, Brookhaven National Laboratory, November 1983.
- 2. Byron/Braidwood Final Safety Analysis Report, Section 10.4.9.

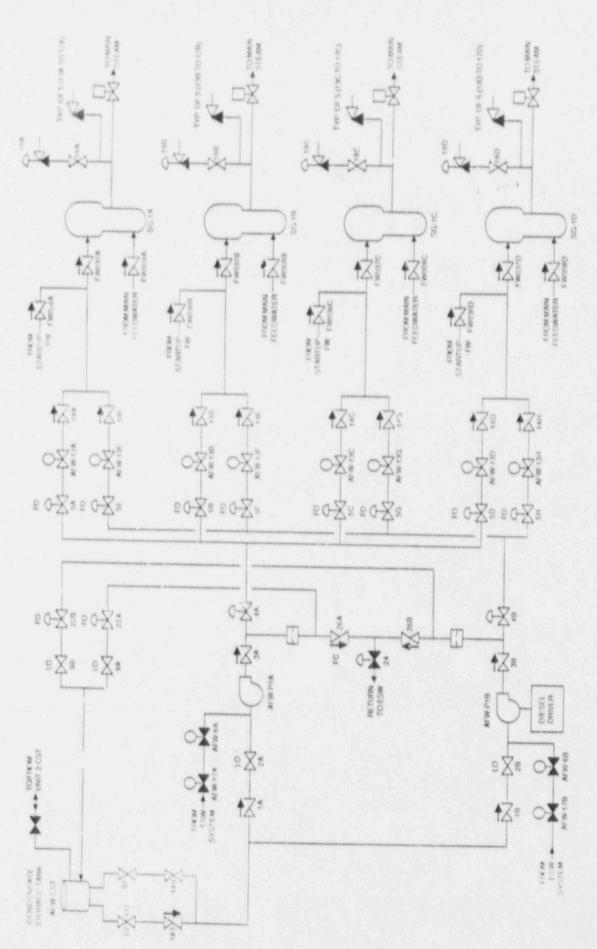


Figure 3.2-1. Byron Unit 1 Auxiliary Feedwater System

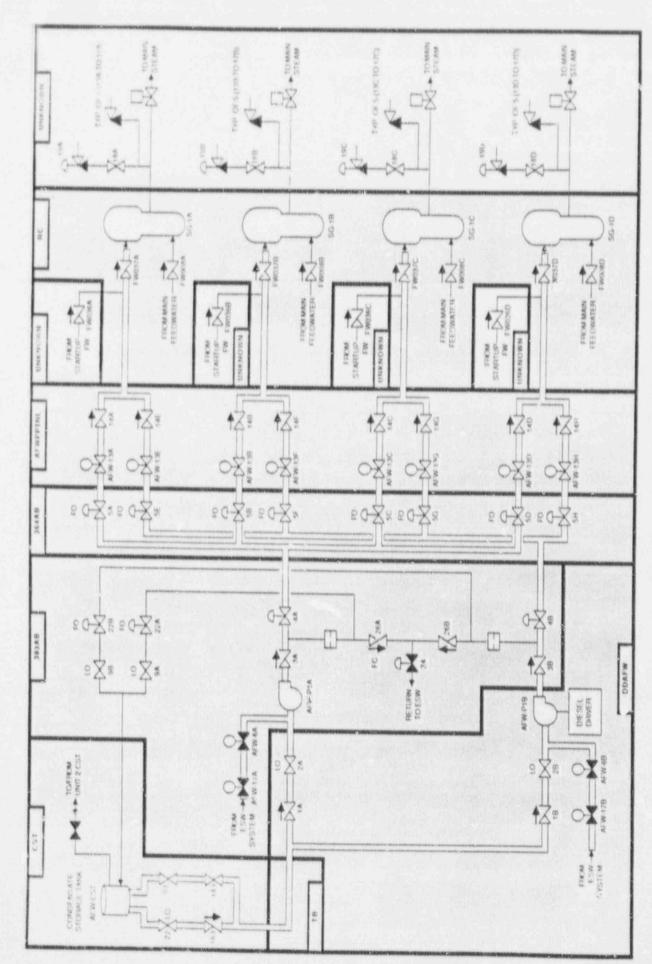


Figure 3.2-2. Byron Unit 1 Auxiliary Feedwater System Showing Component Locations

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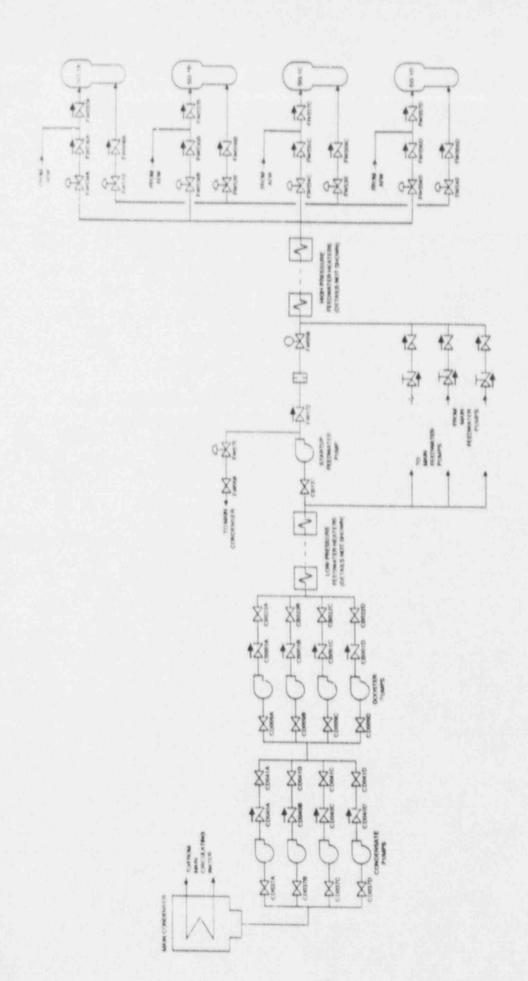


Figure 3.2-3. Byron Unit 1 Startup Feedwater System

Table 3.2-1. Byron Auxiliary Feedwater System Data Summary for Selected Components

COMPONENT ID	COMP. TYPE	LOCATION	POWER SOURCE	VOLTAGE	POWER SOURCE LOCATION	EMERG.
AFW-13A	MOA	AFWPPTNL	MCC-131X1	480	364PENRM	AC/A
AFW-13B	MOV	AFWPPTNL	MCC-131X1	480	364PENRM	AC/A
AFW-13C	MOV	AFWPPTNL	MCC-131X1	480	364PENRM	AC/A
AFW 13D	MOV	AFWPPTNL	MCC-131X1	480	364PENRM	AC/A
AFW-13E	MOV	AFWPPTNL	MCC-132X4	480	426PENRM	AC/B
AFW-13F	MOV	AFWPPINL	MCC-132X4	480	426PENRM	AC/B
AFW-13G	MOV	AFWPPTNL	MCC-132X4	480	426PENRM	AC/B
AFW-13H	VCM	AFWPPINE	MCC-132X4	480	42EPENRM	AC/B
AFW-17A	MOV	383AB	MCC-131X3	480	383AB	AC/A
AFW-17B	MOV	DDAFW	MCC-132X3	480	383AB	AC/B
AFW-6A	MOV	383AB	MCC-131X3	480	383AB	AC/A
AFW-6B	MOV	DDSFW	MCC-132X3	480	383AB	AC/B
AFW-CST	TANK	CST				
AFW-P1A	MDP	383AB	BUS-141	4160	ESF11	AC/A
AFW-P1B	DDP	DDAFW				
SG-1A	SG	RC				
SG-1B	SG	RC				
SG-1C	SG	RC				
SG-1D	SG	RC .				

## 3.3 EMERGENCY CORE COOLING SYSTEM (ECCS)

3.3.1 System Function

The ECCS is an integrated set of subsystems that perform emergency coolant injection and recirculation functions to maintain reactor core coolant inventory and adequate decay heat removal following a LOCA. The coolant injection function is performed during a relatively short-term period after LOCA initiation, followed by realignment to a recirculation mode of operation to maintain long-term, post-LOCA core cooling. Heat from the reactor core is transferred to the containment. The heat transfer path to the ultimate heat sink is completed by the containment cooling systems (see Section 3.5).

3.3.2 System Definition

The emergency coolant injection (ECI) function is performed by the following ECCS subsystems:

- Passive cold leg accumulators

Charging system (CVCS)
 Safety injection (SI) system

Residual heat removal (kHR) system

The charging function of the CVCS is described in Section 3.4.

The SI system provides high pressure coolant injection capability. The RHR pumps perform the low pressure injection function. The Refueling Water Storage Tank (RWST) is the water source for both the high and low pressure injection systems. Both systems inject coolant into all four RCS cold legs. The SI system can also inject into all four hot legs, while the RHR system can inject it to two hot legs.

After the injection phase is complete, recirculation (ECR) is performed by the RHR pumps drawing suction from the containment sump, and discharging into the RCS cold legs. Heat is transferred to the component cooling water system by the RHR heat exchangers. The RHR pumps can also deliver water to the suction of the SI and charging pumps during recirculation.

Simplified drawings of the safety injection system are so in Figures 3.3-1 and 3.3-2. The residual heat removal system is shown in Foures 3.3-3 and 3.3-4. Interfaces between the accumulators, the ECCS injection and recirculation subsystems, and the RCS are shown in Section 3.1. A summary of data on selected ECCS components is presented in Table 3.3-1.

3.3.3 System Operation

During normal operation, the ECCS is in standby. Following a LOCA, the four cold leg injection accumulators (one for each loop) supply borated water to the RCS as soon as RCS pressure drops below accumulator pressure (approximately 585 psig). A safety injection signal (SIS) automatically starts the two charging pumps, the two safety injection pumps, and the two RHR pumps, and aligns the charging pumps for injection. The charging pumps inject through the boron injection tank (BIT) into the four RCS cold legs. The SI and RHR pumps can inject into either the cold legs or the hot legs. All pumps are aligned to take suction on the RWST.

For small breaks, operator action can be taken to augment the RCS depressurization by utilizing the secondary steam dump capability and the auxiliary feedwater (AFW) system (i.e., depressurization due to rapid heat transfer from the RCS).

When the RWST water level drops to a prescribed low level setpoint, the RHR pumps are realigned to draw a suction from the containment sump and deliver water to the RCS cold legs. If depressurization of the RCS proceeds slowly, high pressure recirculation can be accomplished by manually aligning the discharge of the RHR pumps to

the suction of the charging and SI pumps. Approximately 18 hours after the accident, hot leg recirculation is initiated to ensure termination of boiling and preclude excessive boron concentration in the reactor vessel.

3.3.4 System Success Criteria

LOCA mitigation requires that both the emergency coolant injection and emergency coolant recirculation functions be accomplished. The success criteria for a large LOCA are the following (Ref. 1):

 3 of 4 accumulators provide makeup as RCS pressure drops below tank pressure.

- One safety injection pump injects its flow to the RCS.

One RHR pump delivers its flow to the RCS.

One centrifugal charging pump injects from the RWST into the RCS, and

 Coolant recirculation occurs on a low level signal from the RWST or by remote manual means.

The recirculation success criteria are not clearly defined in the FSAR.

Success Criteria for a small LOCA is not clearly defined in the FSAR, however it is noted that (Ref. 2):

- The Safety injection pump shutoff head is less than RCS normal operating pressure, therefore, a small LOCA must be of sufficient size to cause some RCS depressurization, or the RCS must be depressurized by other means if the safety injection pumps are to provide makeup. Options for depressurizing the RCS may include:
  - Opening power-operated relief valves on the pressurizer (two PORVs are available, see Section 3.1)
  - RCS cooldown (i.e. using the auxiliary feedwater system, see Section 3.2)
- The combined capacity of the two centrifugal charging pumps is 300 gpm (i.e. 150 gpm each) @ 5,800 ft. head. One charging pump can maintain normal operating pressure (2,250 psia) following a 0.375" equivalent diameter rupture (127 gpm leak/charging rate).

## 3.3.5 Component Information

A. Safety injection (high pressure) pumps 1A and 1B

1. Rated flow: 400 gpm @ 2540 ft head (1101 psid)

2. Rated capacity: 100%

3. Shutoff head: 3922 ft head (1700 psig)

4. Type: horizontal centrifugal

B. Residual heat removal (low pressure) pumps 1A and 1B 1. Rated flow: 3000 gpm @ 375 ft. head (163 psid)

2. Rated capacity: 100%

3. Shutoff head: 450 ft (195 psid)

4. Type: vertical centrifugal

- C. Cold leg injection accumulators (4)
  - 1. Accumulator volume: 1350 ft<sup>3</sup>
  - 2. Minimum water volume: 935 ft3
  - 3. Normal operating pressure: 585 psig
  - 4. Nominal boric acid concentration: 2000 ppm
- D. Refueling water storage tank
  - 1. Capacity: 458,000 gallons
  - Design Pressure: Atmospheric
     Minimum Boron Concentration: 1900 ppm
  - 4. Minimum water volume: 420,000 gallons
- E. RHR heat exchangers 1A and 1B
  - 1. Design duty: 28.95 x 106 Btu/hr
  - 2. Type: Vertical, shell and U-tube

### 3.3.6 Support Systems and Interfaces

- A. Control signals
  - 1. Automatic

The ECCS injection subsystems are automatically actuated by a safety injection signal (SIS). Conditions initiating an SIS trip are:

- a. Low pressurizer pressure
- b. High containment pressure
- c. Low steam line pressure
- d. Manual actuation

The SIS automatically initiates the following actions:

- starts the diesel generators
- starts the charging, SI, and RHR pumps
- aligns the charging pumps for injection

Switchover to the recirculation mode occurs automatically on low level in the RWST.

- 2. Remote manual
  - An SIS signal can be initiated by remote manual means from the main control room. The transition from the injection to the recirculation phase of ECCS operation can be initiated by remote manual means. Manual action is required to realign the charging and safety injection pumps for recirculation.
- B. Motive Power
  - The ECCS motor-driven pumps and motor-operated valves are Class 1E AC loads that can be supplied from the standby diesel generators as described in Section 3.7.

#### C. Other

1. Each SI and charging pump is cooled by the Essential Service Water system (see Section 3.9).

The RHR pumps and heat exchangers are cooled by the Component Cooling Water system (see Section 3.8).

3. Lubrication and ventilation are provided locally for the SI, RHR, and charging pumps and motors.

#### Section 3.3 References 3.3.7

- 1. Byron/Braidwood Final Safety Analysis Report, Section 6.3.2.
- 2. Byron/Braidwood Final Safety Analysis Report, Section 6.3.3.

23

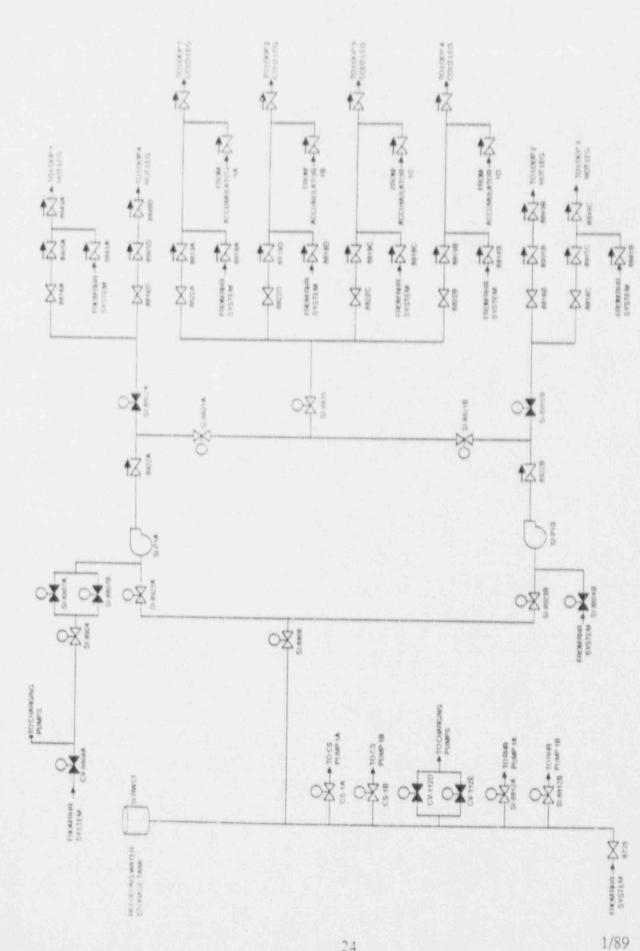


Figure 3.3-1. Byron Unit 1 Safety Injection System

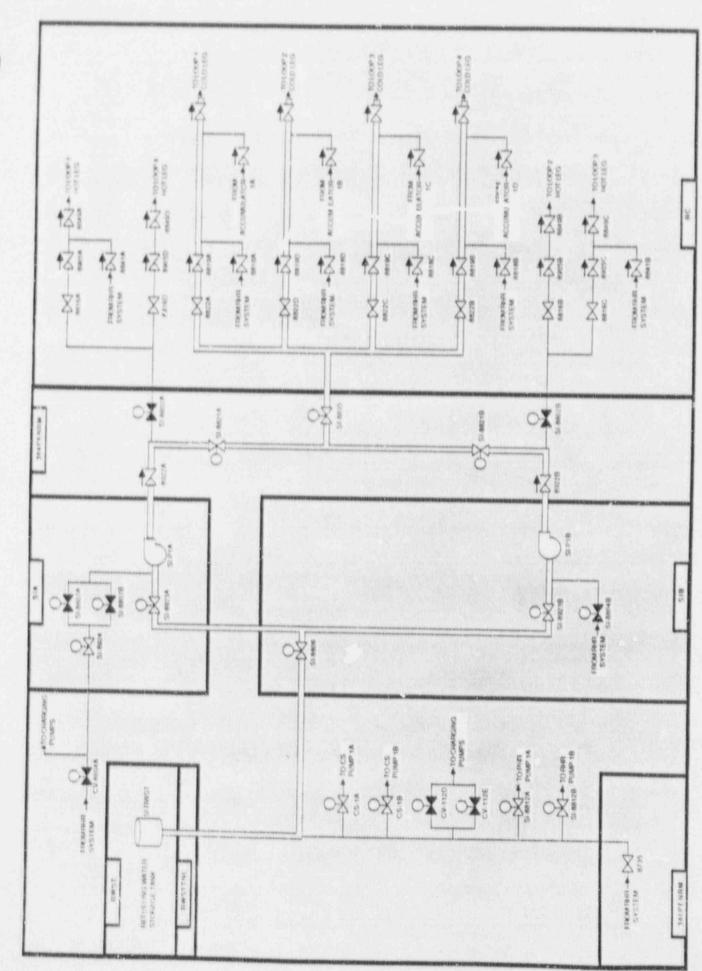


Figure 3.3-2. Byron Unit 1 Safety Injection System Showing Component Locations

1/89

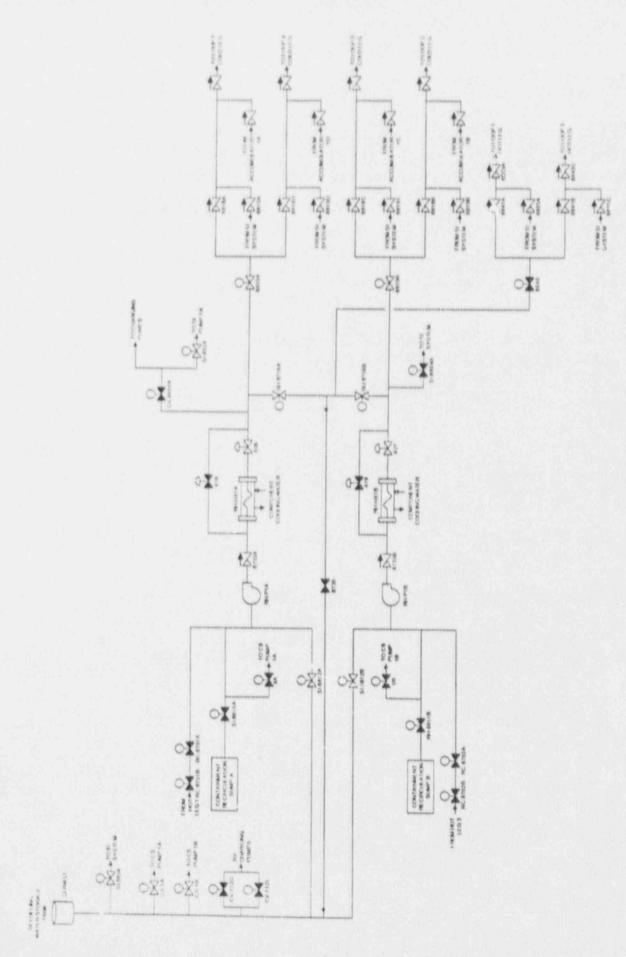


Figure 3.3-3. Byron Unit 1 Residual Heat Removal System

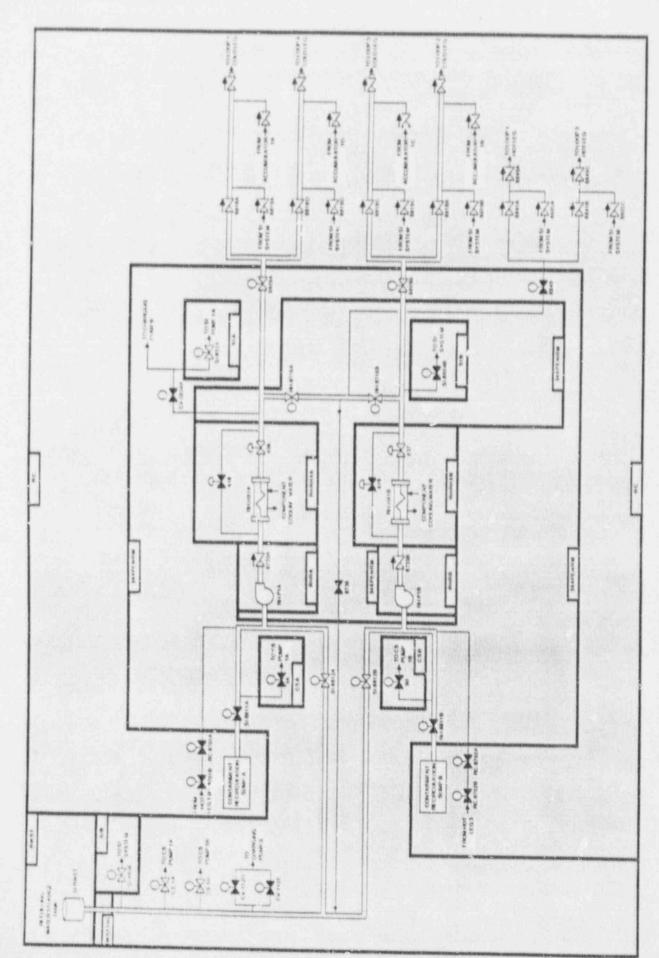


Figure 3.3-4. Byron Unit 1 Residual Heat Removal System Showing Component Locations

27

Table 3.3-1. Byron Emergency Core Cooling System Data Summary for Selected Components

COMPONENT ID	COMP. TYPE	LOCATION		VOLTAGE	POWER SOURCE	EMERG.
CV-8804A	MOV	364PENRM	MCC-131X1	489	364PENRM	AC/A
RH-8716A	MOV	346PENRM	MCC-131X1	480	364PENRM	AC/A
RH-8716A	MOV	346PENRM	MCC-131X1	480	364PENRM	AC/A
RH-8716B	MOV	346PENRM	MCC-132X4	480	426PENRM	AC/B
RH-8716B	MOV	346PENRM	MCC-132X4	486	426PENRM	AC/B
RH-HX1A	HX	RHRHXA				
RH-HX1B	HX	RHRHXB				
RH-P1A	MOP	RHRA	BUS-141	4160	ESF11	AC/A
RH-P1B	MDP	RHRB	BUS-142	4160	ESF12	AC/B
SI-8802A	MOV	364PENRM	MCC-121X1A	480	364PENRM	AC/A
SI-8802B	MOV	364PENRM	MCC-132X4A	480	426PENRM	AC/B
SI-8804B	MOV	SIB	MCC-132X4	480	426PENRM	AC/B
SI-8806	MOV	SIB	MCC-131X1	480	364PENRM	AC/A
SI-8807A	MOV	SIA	MCC-131X1	480	364PENRM	AC/A
SI-8807B	MOV	SIA	MCC-132X1	480	364AB	AC/B
SI-8811A	MOV	364PENRM	MCC-131X1	480	364PENRM	AC/A
SI-8811B	MOV	364PENRM	MCC-132X4A	480	426PENRM	AC/B
SI-8821A	MGV	364PENRM	MCC-131X1	480	364PENRM	AC/A
SI-8821A	MOV	364PENRM	MCS-131X1	480	364PENRM	AC/A
SI-8821B	MOV	364PENRM	MCC-132X4	480	426PENRM	AC/8
1-8821B	MOV	364PENRM	MCC-132X4	480	426PENRM	AC/B
SI-8835	MOV	364PENRM	MCC-131X1A	480	364PENRM	AC/A
SI-8923A	MOV	SIA	MCC-131X1	480	364PENRM	AC/A
SI-8923B	MOV	SIB	MCC-132X4	480	426PENRM	AC/B
61-8924	MOV	SIA	MCC-132X1		364AB	AC/B
SI-P1A	MDP	SIA	BUS-141		ESF11	AC/A
I-P1B	MDP	SIB	BUS-142		ESF12	
I-RWST	TANK	RWST		-100	COFIZ	AC/B

Table 3.3-1. Byron Emergency Core Cooling System Data Summary for Selected Components (Continued)

COMPONENT ID	COMP.	LOCATION	POL-ER SOURCE	VOLTAGE		
SUMP-A	SUMF	RC			LOCATION	LOAD GRP
SUMP-B	SUMP	RC				

# 3.4 CHARGING SYSTEM (CVCS)

3.4.1 System Function

The charging system is part of the Chemical and Volume Control System (CVCS). The CVCS is responsible for maintaining the proper water inventory in the Reactor Coolant System and maintaining water purity and the proper concentration of neutron absorbing and corrosion inhibiting chemicals in the reactor coolant. The makeup function of the CVCS is assumed to be required to maintain the plant in a long-term (8 hours) hot shutdown condition. The charging pumps also operate as part of the ECCS in the event of a LOCA.

3.4.2 System Definition

The CVCS provides a means for injection of control poison in the form of boric acid solution, chemical additions for corrosion control, and reactor coolant cleanup and degasification. This system also adds makeup water to the RCS, reprocesses water that is letdown from the RCS, provides seal water injection to the reactor coolant pump seals, and

performs an emergency core cooling function.

The CVCS consists of several subsystems: the charging, letdown, and seal water system, the reactor coolant purification and chemistry control system, the reactor makeup control system, and the boron thermal regeneration system. The functions of the CVCS are performed by the following components - the charging pumps, (two centrifugal, one positive displacement), boric acid transfer pumps, volume control tank, boric acid tanks, and various heat exchangers and demineralizers.

Simplified drawings of the CVCS, focusing on the charging portion of the system, are shown in Figures 3.4-1 and 3.4-2. A summary of data on selected charging

system somponents in presented in Table 3.4-1.

3.4.3 System Operation

During normal plant operation, one charging pump is running with its section aligned to the Volume Control Tank (VCT). The letdown flow from a RCS cold leg is cooled in the shell side of the regenerative heat exchanger, then directed to the VCT. The reactor makeup control system maintains the desired inventory in the VCT. The bulk of the charging flow is pumped back to the RCS through the tube side of the regenerative heat exchanger via two charging lines. Portions of the charging flow are directed to the reactor coolant pumps through a seal water injection filter, and to pressurizer spray.

The centrifugal charging pumps also provide high-head injection as part of the ECCS (see Section 3.3). During a LOCA the CVCS is isolated except for the centrifugal charging pumps and the piping in the safety injection path. The pumps take suction on the Refueling Water Storage Tank (RWST) and inject via the Boron Injection Tank into all four

cold legs.

The reciprocating (positive displacement) charging pump is also used to perform hydrostatic tests which verify the integrity of the RCS. The pump can pressurize the RCS to the maximum design test pressure.

3.4.4 Success Criteria

For post-transient makeup to the RCS the following charging system success criteria is assumed:

- A long-term water source must be available to the charging pumps.
- One of three charging pumps is available.
  A makeup path to the RCS is available.

For LOCA success criteria, see Section 3.3.4.

### 3.4.5 Component Information

A. Centrifugal charging pumps 1A and 1B

1. Rated flow: 150 @ 5800 ft head (2514 psid)

2. Rated capacity: 100%

3. Type: centrifugal

B. Reciprocating charging pump 1

Rated flow: 98 gpm
 Rated capacity: 100%

3. Type: positive displacement

### 3.4.6 Support Systems and Interfaces

#### A. Control Signals

1. Automatic

a. The centrifugal charging pumps are automatically actuated by a safety injection signal (SIS).

b. The reciprocating charging pump is tripped and the normal charging line

is isolated by an SIS.

2. Remote Manual

The charging pumps can be actuated by remote manual means from the control room.

B. Motive Power

1. The centrifugal charging pumps and motor operated valves of the CVCS are Class 1E AC loads that can be supplied from the standby diesel generators as described in Section 3.7.

C. Other

1. The centrifugal charging pumps are cooled by the Essential Service Water system (see Section 3.9).

2. Pump lubrication and ventilation are provided locally.

Figure 3.4-1. Byron Unit 1 Cnarging System

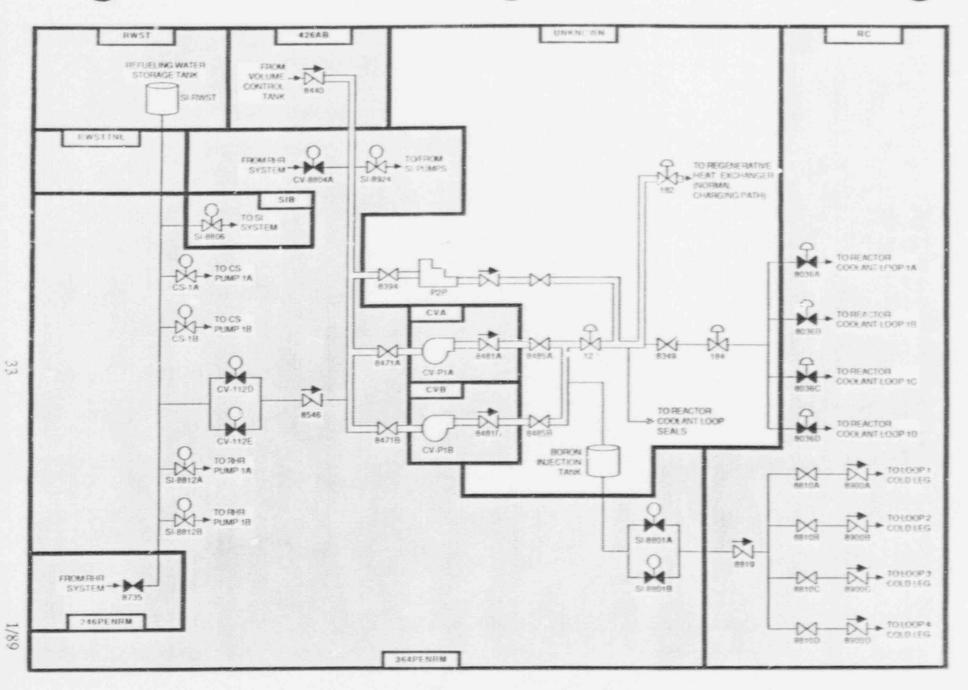


Figure 3.4-2. Byron Unit 1 Charging System Showing Component Locations

Table 3.4-1. Byron Charging System Data Summary for Selected Components

COMPONENT ID	COMP.	LOCATION	POWER SOURCE	VOLTAGE	POWER SOURCE LOCATION	EMERG.
CV-112D	MOV	364PENRM	MCC-131X1	480	364PENRM	AC/A
CV-112E	MOV	364PENRM	MCC-132X4	480	426PENRM	AC/B
CV-P1A	MDP	CVA	BUS-141	4160	ESF11	AC/A
CV-P1B	MDP	CVB	BUS-14?	4160	ESF12	AC/B
SI-8801A	MOV	364PENRM	MCC-131X1	480	364PENRM	AC/A
SI-8801B	MOV	364PENRM	MCC-132X5	480	426AB	AC/B
SI-RWST	TANK	RWST				

# 3.5 CONTAINMENT HEAT REMOVAL SYSTEM (PAHRS)

3.5.1 System Function

Containment heat removal systems perform the functions of containment heat removal and pressure control following a loss of coolant accident. In conjunction with the ECCS, the containment heat removal systems completes the post-LOCA heat transfer path from the reactor core to the ultimate heat sink. The Containment Spray System, which is one of the containment heat removal systems, also serves to remove elemental iodine from the containment atmosphere.

#### 3.5.2 System Definition

Containment heat removal systems include the following two systems:

Reactor Containment Fan Cooler (RCFC) System

Containment Spray (CS) System

The RCFC system provides the design heat removal capacity for the containment following a LOCA, assuming that core residual heat is released to the containment as steam. This is accomplished by the continuous recirculation of the airsteam mixture through cooling coils to transfer heat to essential service water. The RCFC system consists of two redundant trains, each powered from a separate bus. Each train consists of two 50% capacity fan cooler units.

The Containment Spray system is designed to remove fission products, primarily elemental iodine, from the containment atmosphere following a LOCA. The system also serves to reduce containment pressure and temperature during the injection phase of LOCA mitigation. The CS system consists of two independent trains, each containing a 100% capacity pump and three ring-type spray headers. During the injection phase of LOCA mitigation the CS pumps draw suction from the RWST. During recirculation the CS pumps draw from the containment sumps.

Simplified drawings of the Containment Spray system are shown in Figures 3.5-1 and 3.5-2. The interface between the containment fan cooler units and essential service water is shown on the ESW system drawings in Section 3.9. The interfaces are through motor operated valves CC-16A and CC-16B. A summary of data on selected containment spray system components is presented in Table 3.5-1.

3.5.3 System Operation

The Reactor Containment Fan Cooler system consists of two trains, each containing two 50% capacity fan cooler units. The RCFC is designed to commence operation approximately 45 seconds following the initiation of a safery injection signal. Heat is transferred through cooling coils to essential service water. During normal operation the RCFC fan motor operates in the high-speed mode. On initiation of post-LOCA mode of operation the motor will shift to low speed, resulting in lower air flow. The lower air flow compensates for the increase in containment air density resulting from the higher pressure following a LOCA (Ref. 1).

The Containment Spray system consists of two pumps, each supplying three spray headers located in the containment dome area. The spray system will be actuated by high-high containment pressure (approximately 23 psig). During the injection phase, water from the RWST is sprayed into the containment atmosphere by the CS pumps. Following the injection phase the spray pumps are realigned to draw suction from the

containment sump during recirculation.

3.5.4 System Success Criteria

The CS success criteria are not clearly defined in the FSAR in terms of containment heat removal. However, the following is noted (Ref. 1):

- Operation of one of the two independent CS trains will provide 100% of

system capacity.

Operation of one CS train will lower containment pressure enough so that containment design leakage is not exceeded, and enough iodine will be a moved to restrict the site boundary and offsite doses to below the limits of 10 CFR 100.

The RCFC success criteria are as follows (Ref. 2):

 One of two redundant trains is in operation approximately 45 seconds after a safety injection signal is initiated.

Partial CS and RCFS success criteria may exist, but are not defined in the FSAR.

#### 3.5.5 Component Information

A. Reactor Containment Fan Cooler Units 1A, 1B, 1C, and 1D

1. Fan Type: vane-axial

2. Raied capacity: 50%

3. Accident mode heat removal: 132 x 106 Btu/hr

B. Containment Spray Pump 1A

1. Rated flow: 3415 gpm @ 450 ft head (195 psid)

2. Rated capacity: 100%

3. Type: vertical centrifugal

C. Containment Spray Pump 1B

1. Rated flow: 3925 gpm @ 450 ft. head (195 psid)

2. Rated capacity: 100%

3. Type: vertical centrifugal

# 3.5.6 Support Systems and Interfaces

#### A. Control Signals

1. Automatic

The fan cooler units are automatically actuated by a safety injection signal. The containment spray system is automatically actuated on high-high containment pressure.

2. Remote manual

The RCFC and CS systems can be actuated by remote manual means from the control room.

B. Motive Power

 The RCFC units, CS pumps, and motor-operated valves are Class 1E AC loads that can be supplied from the standby diesel generators, as described in Section 3.7. Redundant loads are supplied from separate load groups.

- C Cooling Water
   The RCFC units are cooled by the Essential Service Water system (see Section 3.9).
- D. Other
  - 1. Lubrication, ventilation, and pump cooling are provided locally for the CS

#### Section 3.5 References 3.5.7

- 1. Byron/Braidwood Final Safety Analysis Report, 6.5.2.
- 2. Byron/Braidwood Final Safety Analysis Report, Section 6.2.2.

Figure 3.5-1. Byron Unit 1 Containment Spray System

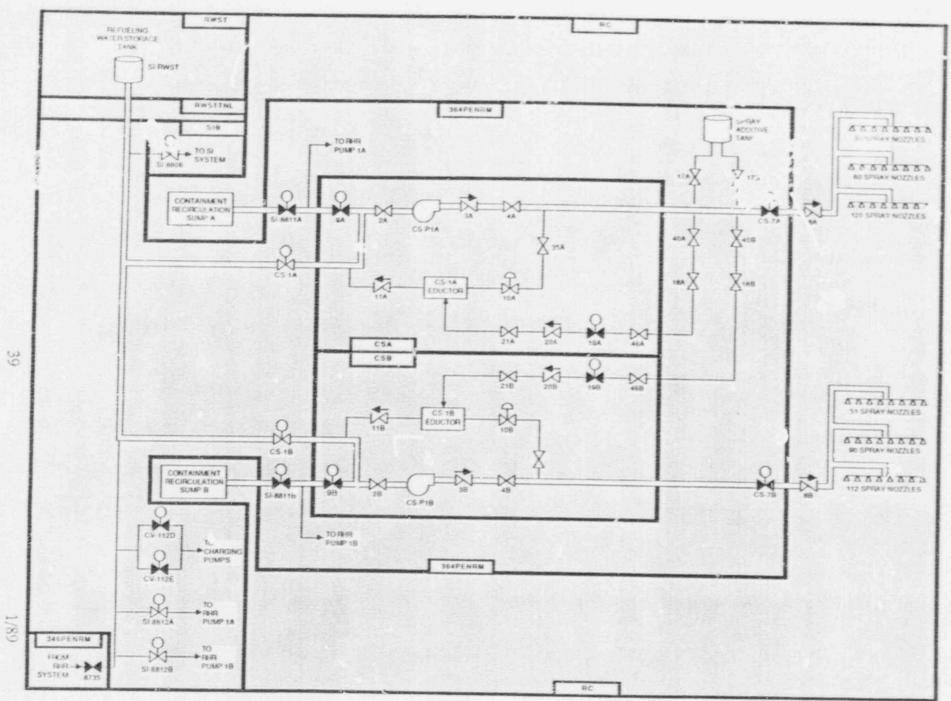


Figure 3.5-2. Byron Unit 1 Containment Spray System Showing Component Locations

Table 3.5-1. Byron Containment Heat Removal System Data Summary for Selected Components

COMPONENT ID	COMP. TYPE	LOCATION	POWER SOURCE	VOLTAGE	POWER SOURCE LOCATION	EMERG.
CC-16A	MOA	364PENRM	MCC-131X5	480	426AB	AG/A
CC-16B	MOV	364PENRM	MCC-132X4	480	426PENRM	AC/B
CC-27A	MOV	364PENRM	MCC-131X5	480	426AB	AC/A
CC-27B	MOV	364PENRM	MCC-132X4	480	426PENRM	AC/B
CC-FANA	ACU	RC .				
CC-FANB	ACU	RC				
CC-FANC	ACU	RC				
CC-FAND	ACU	RC				
CS-1A	MOV	364PENRM	MCC-131X1	480	364PENRM	AC/A
CS-1B	MOV	364PENRM	MCC-132X4A	480	426PENRM	AC/B
CS-7A	MOV	364PENRM	MCC-131X5	480	426AB	AC/A
CS-7B	MOV	364PENRM	MCC-132X4	480	426PENRM	AC/B
CS-P1A	MDP	CSA	BUS-141	4160	ESF11	AC/A
CS-P1B	MDP	CSB	BUS-142	4160	ESF12	AC/B

#### 3.6 INSTRUMENTATION AND CONTROL SYSTEMS (I & C)

3.6.1 System Function

The instrumentation and control systems consist of the Reactor Protection System (RPS), the Engineered Safety Features Actuation System (ESFAS), and systems for the display of plant information to the operators. The RPS and ESFAS monitor the reactor plant, and alert the operator to take corrective action before specified limits are exceeded. The RPS will initiate an automatic reactor trip (scram) to rapidly shutdown the reactor when plant conditions exceed one or more specified limits. The ESFAS will automatically actuate selected safety systems based on the specific limits or combinations of limits that are exceeded.

3.6.2

System Definition
The RPS includes sensor and transmitter units, logic units, and output trip relays that operate reactor trip circuit breakers to cause a reactor scram. The ESFAS includes independent sensor and transmitter units, logic units and relays that interface with the control circuits for the many different sets of components that can be actuated by the ESFAS. Operator instrumentation display systems consist of display panels in the control room that are powered by the 120 VAC electric power system (see Section 3.7). The remote shutdown capability is previded by the remote shutdown panel in conjunction with normal automatic systems and local controls outside the control room.

#### 3.6.3 System Operation

The Westinghouse RPS (or Reactor Trip System, RTS) has two to four redundant input instrument channels for each sensed parameter and two output actuation trains (A and B). The A and B logic trains independently generate a reactor trip command when prescribed parameters are outside the safe operating range. Either RPS train is capable of opening a separate and independent reactor trip circuit breaker to cause a scram. The manual scram A and B circuits bypass the RPS logic trains and send a reactor trip command directly to shunt trip circuitry in the reactor trip circuit breakers.

B. ESFAS

The ESFAS has three or four input instrument channels for each sensed parameter, and two output actuation trains (A and B). In general, each train controls equipment powered from different Class 1E AC electrical buses. An individual component usually receives an actuation signal from only one ESFAS train. The ESFAS generates the following signals: (a) reactor trip, provided one has not already been generated by the RPS, (b) safety injection signal (SIS), (3) containment isolation, (4) main steam line isolation, (5) main feedwater line isolation, (6) emergency diesel start, (7) control room isolation and (8) containment spray actuation. The control room operators can manually trip the various ESFAS logic subsystems. Details regarding ESFAS actuation logic are included in the system description for the actuated system.

#### C. Remote Shutdown

For equipment having controls outside the control room (which duplicate the functions inside the control room), the controls are provided with a selector switch which transfers control of the switchgear from the control room to a local station. Placing the local selector switch in the local operating position gives an annunciating alarm in the control room and turns off the indicating lights on the control room panel.

The mote shutdown panels are located at plant elevation 383 feet in the radwaste control area.

The main control room panels and the remote shutdown panels are located in separate physical locations, on separate elevations, with separate ventilation systems and multiple communication systems, and with lighted access routes between the two locations. Therefore, it is expected that no single credible event which will cause evacuation of the main control room will also cause remote shutdown panels to be inoperable. Equipment having controls available outside the control room are listed in Table 3.6-1 (Ref. 1).

## 3.6.4 System Success Criteria

#### A. RPS

In the analog portion, two to four redundant sensors and channels are used. The coincidence required to cause a trip varies from parameter to parameter. The channel's analog input is converted into a digital signal for the logic portion. The RPS uses hindrance logic (normal = 1, trip = 0) in both the input and output logic. Therefore, a channel will be in a trip state when input signals are lost, when control power is lost, or when the channel is temporarily removed from service for testing or maintenance (i.e. the channel has a fail-safe failure mode). A reactor scram will occur upon loss of control power to the RPS. A reactor scram usually is implemented by the scram circuit breakers which must open in response to a scram signal. There are two series scram circuit breakers in the power path to the scram rods. In this case, one of two circuit breakers must open. Details of the scram system for Byron have not been determined.

#### B. ESFAS

A single component usually receives a signal from only one ESFAS output train although both AFW pumps receive signals from both trains. ESFAS Trains A and B must be available in order to automatically actuate their respective components. ESFAS typically uses hindrance input logic (normal = 1, trip = 0) and transmission output logic (normal = 0, trip = 1). In this case, an input channel will be in a trip state when input signals are lost, when control power is lost, or when the channel is temporarily removed from service for testing or maintenance (i.e. the channel has a fail-safe failure mode). Control power is needed for the ESFAS output channels to send an actuation signal. Note that there may be some ESFAS actuation subsystems that utilize hindrance output logic. For these subsystems, loss of control power will cause system or component actuation, as is the case with the RPS. Details of the ESFAS system for Byron have not been determined.

### 3.6.5 Support Systems and Interfaces

#### A. Control Power

1. RPS

The RPS input instrument channels are powered from the 120 VAC instrument buses (see Section 3.7). It is assumed that the RPS A and B output logic trains are powered from separate 125 VDC distribution panels.

2. ESFAS

The ESFAS input instrument channels are powered from 120 VAC instrument buses. It is assumed that the ESFAS A and B output logic trains are powered from separate 125 VDC distr. ution panels.

Operator Instrumentation
 Operator instrumentation displays are powered from the 120 VAC instrument buses.

#### 3.6.6 Section 3.6 References

1. Byron/Braidwood Final Safety Analysis Report, Section 7.4.1.

# Table 3.6-1. Byron Equipment Controls Available Outside the Control Room

The following equipment can be controlled from local stations outside the main control room:

- Auxiliary Feedwater Pumps
- Centrifugal Charging Punips
- Boric Acid Transfer Pumps
- Essential Serv. Water Pump
- Component Cooling Water Pump
- Reactor Containment Fan Coolers
- Control Room Ventilation Unit including Control Room Air
- Inlet Dampers
- Primary Water Makeup Pumps
- Charging Flow Control Valve
- Letdown Orifice Isolation Valves
- Aux. Feedwater Control Valves
- Power-Operated Atmospheric Steam Relief
- Pressurizer Heater Control
- Emergency Boration Isolation Valve

#### 3.7 ELECTRIC POWER SYSTEM

3.7.1 System Function

The electric power system supplies power to various equipment and systems needed for normal operation and accident response. The onsite Class 1E electric power system supports the operation of safety class systems and instrumentation needed to establish and maintain a safe shutdown plant condition following an accident, when the normal electric power sources are not available.

3.7.2 System Definition

The onsite Class 1E electric power system consists of two 4160 switchgear buses, designated 141 and 142. There are two standby diesel generators connected to the buses. Diesel generator 1A is connected to bus 141, and diesel generator 1B is connected to bus 142. There are also four 480 VAC switchgear buses, designated 131X, 131Z, 132X, and 132Z. Buses 131X and 131Z are connected to 4160 bus 141 through transformers, and buses 132X and 132Z are connected to 4160 bus 142 through transformers. Buses 131Z and 132Z serve loads associated with the essential cooling towers. Various motor control centers (MCCs) receive their power from the 480 VAC buses.

Emergency power for vital instruments, control, and emergency lighting is supplied by two 125 VDC station batteries. The batteries energize two DC buses, designated 111 and 112. Four 120 VAC instrument buses are connected to the DC buses

through inverters, and to 480 VAC MCCs through transformers.

Simplified one-line diagrams of the electric power system are shown in Figures 3.7-1 through 3.7-4. A diagram of the diesel generator fuel oil system is shown in Figure 3.7-5. A summary of data on selected electric power system components is presented in Table 3.7-1. A partial listing of electrical sources and loads is presented in Table 3,7-2.

3.7.3 System Operation

During normal operation, the Class 1E electric power system is supplied from the 345 kV switchyard, directly to the two 4160 buses through two system auxiliary transformers. An alternate source of power is also from the 345 kV switchyard but through Unit 2's 4160 switchgear. The emergency sources of AC power are the diesel generators. The transfer from the preferred power source to the diesel generators is accomplished automatically by opening the normal source circuit breakers and then reenergizing the Class 1E portion of the electric power system from the diesel generators.

The DC power system normally is supplied through the battery chargers, with the batteries "floating" on the system, maintaining a full charge. Upon loss of AC power, the entire DC load draws from the batteries. The batteries are sized to supply the instrument inverters for up to 30 minutes, and other loads such as diesel generator control

power for up to 4 hours.

The 120 VAC vital buses normally receive power from the DC buses through

an inverter. An alternate source is from the 480 VAC system through transformers.

Redundant safeguards equipment such as motor driven pumps and motor operated valves are supplied by different VAC buses. For the purpose of discussion, this equipment has been grouped into "load groups". Load group "AC/A" contains components receiving electric power either directly or indirectly from 4160 bus 141. Load group "AC/B" contains components powered either directly or indirectly from 4160 bus 142. Components receiving DC power are assigned to load groups "DC/A" and "DC/B", based on the battery power source.

> 45 1/89

3.7.4 System Success Criteria

Basic system success criteria for mitigating transients and loss-of-coolant accidents are defined by front-line systems, which then create demands on support systems. Electric power system success criteria are defined as follows, without taking credit for cross-ties that may exist between independent load groups:

- Each Class 1E DC load group is supplied initially from its respective battery

 Each Class 1E AC load group is isolated from the non-Class 1E system and is supplied from its respective emergency power source (i.e. diesel generator)

Power distribution paths to essential loads are intact

Power to the battery chargers is restored before the batteries are exhausted

#### 3.7.5 Component Information

A. Standby diesel generators (2)

- 1. Maximum continuous rating: 5500 kW
- 2. 2 hour rating: 6050 kW
   3. Rated voltage: 4160 VAC
- 4. Manufacturer: unknown
- B. Batteries (2)

1. Rated voltage: 125 VDC

# 3.7.6 Support Systems and Interfaces

#### A. Control Signals

1. Automatic

The standby diesel generators are automatically started based on:

- Undervoltage on the normal bus

- Safety injection signal (SIS, see Section 3.3)

2. Remote manual

The diesel generators, can be started, and many distribution circuit breakers can be operated, from the main control room.

# B. Diesel Generator Auxiliary Systems

1. Diesel Cooling Water System

Heat is transferred from a jacket water system to the Essential Service Water system. Each diesel receives redundant cooling water supplies from the ESW "A" and "B" headers (see Section 3.9).

2. Diesel Starting System

Each diesel has an air starting system.

Diesei Fuel Oil Transfer and Storage System
 A 500 gallon "day tank" supplies the relatively short-term (approximately 72 minutes) fuel needs of each diesel. Each day tank is replenished from two 25,000 gallon storage tanks during engine operation.

4. Diesel Lubrication System

Each diesel generator has its own lubrication system.

Combustion Air Intake and Exhaust System
 This system supplies fresh air to the diesel intake, and directs the diesel exhaust outside of the diesel building.

6. Diesel Room Ventilation System

This system maintains the environmental conditions in the diesel room within limits for which the diesel generator and switchgear have been qualified. This system may be needed for long-term operation of the diesel generator.

Figure 3.7-1. Byron Unit 1 4160 and 480 VAC Electric Power Distribution System

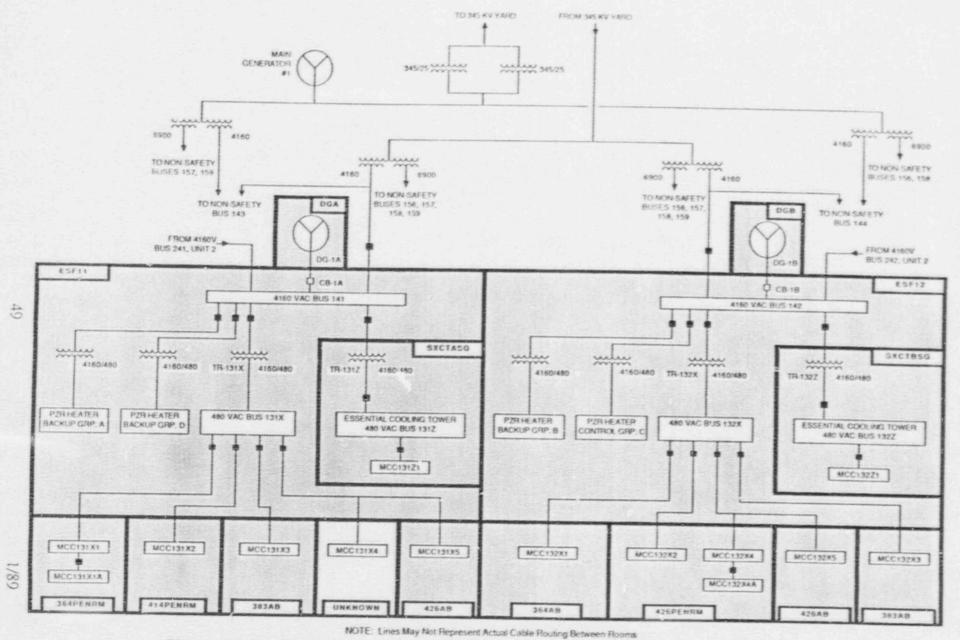


Figure 3.7-2. Byron Unit 1 4160 and 480 VAC Electric Power Distribution System Showing Component Locations

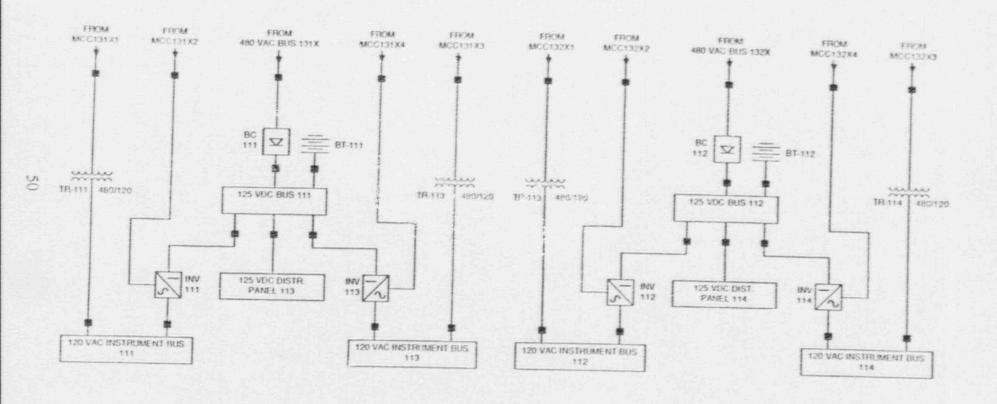


Figure 3.7-3. Byron Unit 1 125 VDC and 120 VAC Electric Power Distribution System

NOTE: Lines May Not Represent Actual Cable Routing Between Rooms

Figure 3.7-4. Byron Unit 1 125 VDC and 120 VAC Electric Power Distribution System **Showing Component Locations** 

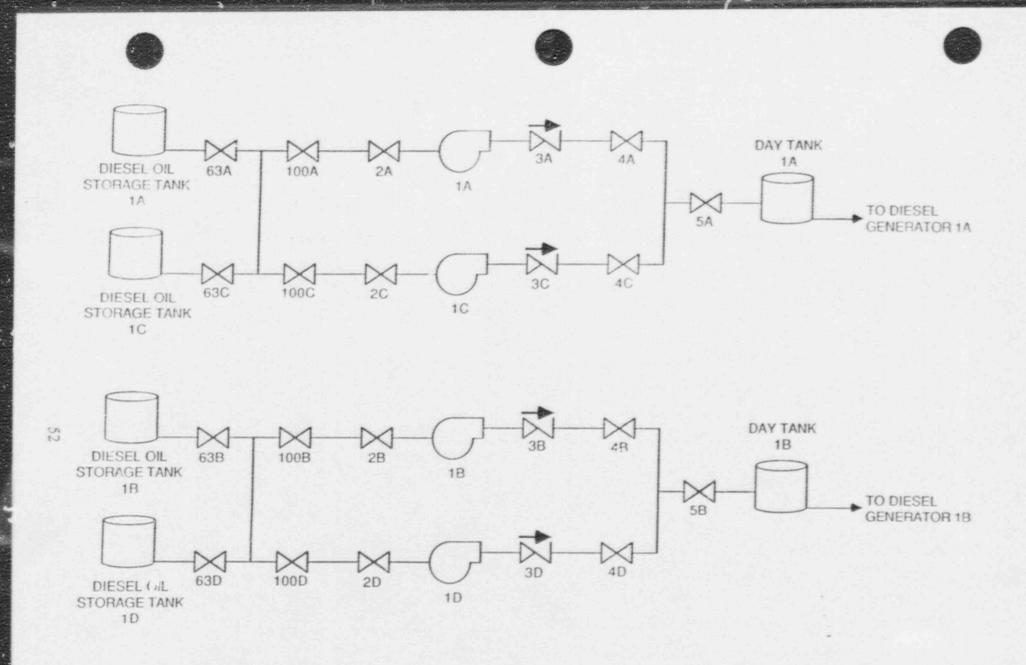


Figure 3.7-5. Byron Unit 1 Diesel Fuel Oil System

Table 3.7-1. Byron Electric Power System Data Summary for Selected Components

COMPONENT ID	COMP. TYPE	LOCATION	POWER SOURCE	VOLTAGE	POWER SOURCE	EMERG.
ACBUS-111	BUS	BATRM111	TR-111	120	BATRM111	LOAD GRP
ACBUS-111	BUS	BATHM111	INV-111	120	BATRM111	AC/A
ACBUS-112	BUS	BATRM112	TR-112	120	BATRM:112	AC/B
ACBUS-112	BUS	BATRM112	INV-112	120	BATRM112	AC/B
ACBUS-113	BUS	BATRM111	TR-113	120	BATRM111	AC/A
ACBUS-113	BUS	BATRM111	INV-113	120	BATRM111	AC/A
ACBUS-114	BUS	BATRM112	TR-114	120	BATRM112	AC/B
ACBUS-114	BUS	BATRM112	INV-114	120	BATRM112	AC/B
BC-111	BC	BATRM111	BUS-131X	125	ESF11	DC/A
BC-112	BC	BATRM112	BUS-132X	125	ESF12	DC/B
BT-111	BATT	BATRM111		125	20.12	DC/A
BT-112	BATT	BATRM112		125		DC/B
BUS-131X	BUS	ESF11	TR-131X	480	ESF11	AC/A
EUS-131Z	BUS	SXCTASG	TR-131Z	480	SXCTASG	AC/A
BUS-132X	BUS	ESF12	TR-132X	480	ESF12	AC/B
3US-132Z	BUS	SXCTBSG	TR-132Z	480	SXCTBSG	AC/B
BUS-141	BUS	ESF11	DG-1A	4160	DGA	
3US-142	BUS	ESF12	DG-1B	4160	DGB	AC/A
CB-1A	CB	ESF11	DG-1A	4160	DGA	AC/B
CB-1B	CB	ESF12	DG-1B		DGA DGB	AC/A
CBUS-111	BUS	BATRM111	BT-111			AC/B
CBUS-111	BUS	BATRM111	BC-111		BATRM111 BATRM111	DC/A
CBUS-112	BUS	BATRM112	BT-112		BATRM112	DC/A
CBUS-112	BUS	BATRM112	BC-112			DC/B
G-1A	DG	DGA	00 112		BATRM112	DC/B
)G-1B	DG	DGB		4160		AC/A
VV-111	INV	BATRM111	1000	4160		AC/B
	INV	BATRM111	MCC-131X2 DCBUS-111	120	414PENRM	DC/A

Table 3.7-1. Byron Electric Power System Data Summary for Selected Components (Continued)

COMPONENT ID	COMP. TYPE	LOCATION	POWER SOURCE	VOLTAGE	POWER SOURCE	EMERG.
INV-112	INV	BATRM112	MCC-132X2	120	426PENRM	DC/B
INV-112	INA	BATRM112	DCBUS-112	120	BATRM112	DC/B
INV-113	INV	BATRM111	MCC-131X4	120	UNKNOWN	DC/A
INV-113	INV	BATRM111	DCBUS-111	120	BATRM111	DC/A
INV-114	INV	BATRM112	MCC-132X4	120	426PENRM	DC/B
INV-114	INV	BATRM112	DCBUS-112	120	BA (RM112	DC/B
MCC-131X1	MCC	364PENRM	BUS-131X	480	ESF11	AC/A
MCC-131X1A	MCC	364PENRM	MCC-131X1	480	364PENRM	AC/A
MCC-131X2	MCC	414PENRM	BUS-131X	480	ESF11	AC/A
MCC-131X3	MCC	383AB	BUS-131X	480	ESF11	AC/A
MCC-131X4	MCC	UNKNOWN	BUS-131X	480	ESF11	AC/A
MCC-131X5	MCC	426AB	BUS-131X	480	ESF11	AC/A
MCC-132X1	MCC	364AB	BUS-132X	480	ESF12	AC/B
MCC-132X2	MCC	426PENRM	BUS-132X	480	ESF12	AC/B
ACC-132X3	MCC	383AB	BUS-132X	480	ESF12	AC/B
ACC-132X4	MCC	426PENRM	BUS-132X	480	ESF12	AC/B
ACC-132X4A	MCC	426PENRM	MCC-132X4	480	426PENRM	AC/B
ACC-132X5	MCC	426AB	BUS-132X	480	ESF12	
R-111	XFMR	BATRM111	MCC-131X1	120	364PENRM	AC/A
R-112	XFMR	BATRM112	MCC-132X1	120	364AB	AC/A
R-113	XFMR	BATRM111	MCC-131X3		383AB	
R-114	XFMR	BATRM112	MCC-132X3		383AB	AC/A
R-131X	XFMR	ESF11	BUS-141			AC/B
R-131Z	XFMR	SXCTASG	DUC 111		ESF11	AC/A
	XFMR	ESF12	DUIG		ESF11	AC/A
	XFMR	SXCTBSG	DUICALO	480	ESF12	AC/B

# TABLE 3.7-2. PARTIAL LISTING OF ELECTRICAL SOURCES AND LOADS AT BYRON

POWER	VOLTAGE	LOAD GRP	POWER SOURCE LOCATION	LOAD	COMPONENTID	COMP	COMPONEN
BC-111	125	DG/A	BATRM111	EP	D08US-111	BUS	BATRM111
BG-112	125	DC/B	BATRM112	EP	DOBUS-112	BUS	BATRM112
BT-111	125	DO/A	BATRM111	EP	DCBUS-111	BUS	BATRM111
BT-112	125	DO/B	BATRM112	EP	DOBUS-112	BUS	BATRM112
BUS-131X	125	DG/A	ESF11	ΕP	BC-111	BC	BATRM111
BUS-131X	480	AC/A	ESF11	EP	MCC-131X1	MCC	364PENRM
BUS-131X	480	AC/A	ESFII	EP	MCC-131X2	MGC	414PENRM
BUS-131X	480	AC/A	ESF11	EP	MCC-131X3	MCC	383AB
BUS-131X	480	AC/A	ESF11	EP	MCC-131X4	MCC	UNKNOWN
BUS-131X	480	AG/A	ESF11	EP	MCC-131X5		
BUS-131Z	480	AC/A	SWCTASG	ESW	ESW-CTFAN-A	MCC	426AB
BUS-132X	125	DC/B	ESF12	EP		ACU	SXCTA
BUS-132X	480	AC/B	ESF12		BC-112	BC	BATRM112
BUS-132X	480	AC/B	ESF12	EP	MGG-132X1	MCC	364AB
BUS-132X	480	AC/B	ESF12	EP	MCC-132X2	MCC	426PENAM
3US-132X	480	AC/B		EP	MCC-132X3	MGC	383AB
BUS-132X	480		ESF12	EP	MCC-132X4	MCC	426PENRM
BUS-132Z		AC/B	ESF12	EP	MCC-132X5	MCC	426AB
3US-141	480	AC/B	SWCTBSG	ESW	ESW-CTFAN-B	ACU	SXCTB
	4160	AC/A	ESF11	AFW	AFW-PIA	MDP	383AB
BUS-141	4160	2219	ESF11	cow	CCW-PO	MDP	364AB
3US-141	41SC	AC/A	ESF11	cvcs	CV-P1A	MDP	CVA
3US-141	4160	AC/A	ESF11	ECCS	RH-P1A	MDP	RHRA
BUS-141	4160	AC/A	ESF11	ECCS	SI-P1A	MOP	SIA
BUS 141	480	AC/A	ESF11	EP	TR-131X	XFMR	ESF11
3US-14*	480	AC/A	ESFII	EP	TR-131Z	XFMR	SXCTASG
BUS-141	4150	AC/A	ESF11	ESW	ESW-P1A	MDP	ESWPMPA
US-141	4160	AC/A	ESF11	PAHRS	CS-P1A	MDP	CSA
US-142	4160		ESF12	ccw	CCW-P0	MDP	
IUS-142	4160	AC/B	ESF12	CCW	CCW-P1B		364AB
US-142	4160	AC/B	ESF12	CVCS		MDP	364AB
US-142	4160	AC/B	ESF12		CV-P1B	MDP	CVB
		-		ECCS	RH-P1B	MOP	RHRB

# TABLE 3.7-2. PARTIAL LISTING OF ELECTRICAL SOURCES AND LOADS AT BYRON (CONTINUED)

POWER	VOLTAGE	EMERG LOAD GRP	POWER SOURCE LOCATION	SYSTEM	COMPONENT ID	TYPE	LOCATION
BUS-142	4160	AC/B	ESF12	ECOS	SI-P1B	MOP	SIB
BUS-142	480	AC/B	ESF12	EP	TR-132X	XFMR	ESF12
BUS-142	480	AC/B	ESF\2	EP	TR-132Z	XFMA	SXCTBSG
BUS-142	4160	AC/B	ESF12	ESW	ESW-P1B	MDP	ESWPMPB
BUS-142	4160	AG/B	ESF12	PAHRS	CS-P13	MOP	CSB
BUS141	4160	AG/A	ESF11	ccw	CCW-P1A	MOP	364AB
DOBUS-111	120	DC/A	BATRM111	EP	INV-111	INV	BATAMIII
DCBUS-111	120	DC/A	BATRMIII	EP	INV-113	INV	BATRM111
DCBUS-112	120	DC/8	BATRM112	EP	INV-112	INV	BATRM112
DCBUS-112	120	DC/8	BATRM112	EP	INV-114	INV	BATRM112
DG-1A	4160	AC/A	DGA	ĒΡ	BUS-141	BUS	ESF11
DG-1A	4160	AC/A	DGA	EP	CB-1A	СВ	ESF11
DG-18	4160	AC/B	DGB	EP	BUS-142	BUS	ESF12
DG-18	4160	AC/B	DG8	EP	CB-1B	СВ	ESF12
(NV-111	120	AO/A	BATRM111	EP	ACBUS-111	BUS	BATRM111
INV-112	120	AC/B	BATRM112	EP	ACBUS-112	BUS	BATRM112
INV-113	120	AC/A	BATAM111	EP	ACBUS-113	BUS	BATRM111
INV-114	120	AC/B	BATRM112	EP	ACBUS-114	BUS	BATRM112
MCC-131X1	480	AC/A	364PENRM	AFW	AFW-13A	MOV	AFWPPTNL
MCC-131X1	480	AC/A	364PENRM	AFW	AFW-138	MOV	AFWPPTNL
MCC-131X1	480	AC/A	364PENRM	AFW	AFW-13C	MOV	AFWPPTNL
MGC-131X1	480	AC/A	364PENRM	AFW	AFW-13D	MOV	AFWPPTNL
MCC-131X1	480	AC/A	364PENRM	cvcs	CV-112D	MOV	364PENRM
MCC-131X1	480	AC/A	364PENRM	CVCS	SI-8801A	MOV	364PENRM
MCC-131X1	480	AO/A	364PENRM	ECCS	CV-8804A	MOV	364PENRM
MCC-131X1	480	AC/A	364PENRM	ECCS	RH-8716A	MOV	346PENRM
M00-131X1	480	AG/A	364PENRM	ECCS	RH-8716A	MOV	346PENRM
MCC-131X1	480	AC/A	364PENRM	ECCS	SI-8806	MOV	SIB
MCC-131X1	480	AC A	364PENRM	ECCS	SI-8807A	MOV	SIA
	480	AC/A	364PENRM	ECCS	\$1-8811A	MOV	
MCC-131X1					SI-8821A	MOV	
MCC/131X1	480	AC/A	364PENRM	ECCS	31.9021W	MOY	Sour Elitain

# TABLE 3.7-2. PARTIAL LISTING OF ELECTRICAL SOURCES AND LOADS AT BYRON (CONTINUED)

POWER	VOLTAGE	LOAD GRP	POWER SOURCE LOCATION	LOAD SYSTEM	LOAD COMPONENT ID	COMP	COMPONEN
MCC-131X1	480	AC/A	364PENRM	ECCS	SI-8821A	MOV	364PENRM
MCC-131X1	480	AQ/A	364PENRM	ECCS	SI-8923A	MOV	SIA
MCC-131X1	480	AC/A	364PENRM	EP	MCC-131X1A	MGC	364PENRM
MCC-131X1	120	AC/A	364PENRM	EP	TR-111	XFMR	BATRMIII
MCC-131X1	480	AC/A	364PENRM	ESW	ESW-1-33	MOV	ESWPMPA
MCC-131X1	460	AC/A	364PENRM	ESW	ESW-1-33	MOV	ESWPMPA
MCC-131X1	480	AC/A	364PENRM	ESW	ESW-1-4	MOV	ESWPMPA
MCC-131X1	480	AQ/A	364PENAM	ESW	ESW-1-d	MOV	ESWPMPA
MCC-131X1	480	AO/A	364PENRM	PAHRS	CS-1A	MOV	364PENRM
MCC-131X1A	480	AC.A	364PENRM	Eccs	SI-8802A	MOV	364PENRM
MCC-131X1A	480	AC/A	364PENAM	ECCS	SI-8835	MOV	364PENRM
MCC-131X2	120	DG/A	414PENRM	ΕP	INV-111	INV	BATRMIII
MCC-131X2	480	AO/A	414PENRM	RCS	RC-8000A	MOV	RC
мсс татха	480	AC/A	414PENEM	RCS	RC-8701A	MOV	RC
MCC-131X2	480	AC/A	#14PENRM	ROS	RC-8702A	MOV	RC RC
MCC-131X3	480	AC/A	383AB	AFW	AFW-17A	MOV	383AB
MCC-131X3	480	AG/A	383AB	AFW	AFW-6A	MOV	383AB
MCC-131X3	480	AC/A	383AB	cow	00W-1-9473A	MOV	364AB
MCG-131X3	480	AG/A	383AB	cow	CCW-1-9473A	MOV	364AB
MCC-131X3	120	AC/A	383AB	EP	TR-113	XFMR	BATRMIII
MCC-131X3	480	AC/A	383AB	ESW	ESW-1-1A	MOV	SX1A
MCC-131X4	120	DC/A	UNKNOWN	EP		INV	BATRMIII
MCC-131X5	480	AC/A		PAHRS	CC-16A	MOV	364PENRM
MCC-131X5	480	AC/A		PAHRS	CC-27A	MOV	364PENAM
MCC-131X5	480	AO/A		PAHRS	CS-7A	MOV	364PENRM
MCC-132X1	480	AC/B		cow	CCW-1-9473B	MOV	
MCC-132X1	480			ccw	CCW-1-9473B		364AB
/CC-132X1				ECCS	SI-8807B	MOV	364AB
MCG-132X1				ECCS		MOV	SIA
MCG-132X1					SI-8924	MOV	SIA
MCC-132X1				ΕP		XFMR	BATRM112
	400	AQ/B	364AB	ESW	ESW-1-1B	MOV	SX1B

TABLE 3.7-2. PARTIAL LISTING OF ELECTRICAL SOURCES AND LOADS AT BYRON (CONTINUED)

POWER	VOLTAGE	EMERG LOAD GRP	POWER SOURCE LOCATION	LOAD	COMPONENTID	TYPE	COMPONEN' LOCATION
MGG-132X1	480	AC/B	364AB	ESW	ESW-1-34	MOV	ESWPMPB
MCC-132X1	480	AC/B	364AB	ESW	ESW-1-34	MOV	ESWPMPB
MCO-132X1	480	AC/B	364AB	ESW	ESW-1-5	MOV	ESWPMPB
MCC-132X1	480	AC/B	364AB	ESW	ESW-1-5	MOV	ESWPMPB
MCC-132X2	120	DC/B	426PENRM	EP	INV-112	INV	BATRM112
MCC-132X2	480	AC/B	426PENRM	RCS	RC-8000B	MOV	RC
MCC-132X2	480	AC/B	426PENRM	RCS	RC-8701B	MOV	RC
MCC-132X2	480	AC/B	426PENRM	RCS	RC-8702B	MOV	RO
MCC-132X3	480	AC/B	383AB	AFW	AFW-17B	MOV	DDAFW
M00-132X3	480	AC/B	383AB	AFW	AFW-68	MOV	DDAFW
MCC-132X3	120	AC/B	383AB	EP	TR-114	XFMR	BATRM112
MGG-132X4	480	AC/B	426PENRM	AFW	AFW-13E	MOV	AFWPPTNL
MO 0-132X4	480	AC/B	426PENRM	AFW	AFW-13F	MOV	AFWPPTNL
VCC-132X4	480	AC/B	426PENRM	AFW	AFW-13G	MOV	AFWPPTNL
MCC-132X4	480	AC/B	426PENRM	AFW	AFW-13H	MOV	AFWPPTNL
VGC-132X4	480	AC/B	426PENAM	cvcs	CV-112E	MOV	364PENRM
MCC-132X4	480	AC/B	426PENRM	ECCS	AH-8716B	MOV	346PENRM
VIO C-132X4	480	AC/B	426PENRM	ECCS	RH-8716B	MOV	346PENRM
MO C-132X4	480	AC/B	426PENRM	ECCS	SI-8804B	MOV	SIB
MCC-132X4	480	AC/B	426PENRM	ECCS	SI-8821B	MOV	364PENRM
MCC-132X4	480	AC/B	426PENRM	ECCS	SI-8821B	MOV	364PENRM
VICG-132X4	480	AC/B		ECCS	SI-8923B		
VCC-132X4	120	DC/B		EP			SIB
/ICC-132X4	480	AC/B			INV-114	INV	BATRM112
VCC-132X4	480	AC/B		EP	MCC-132X4A	MCC	426PENRM
VOC-132X4	480			PAHRS	CC-16B	MOV	364PENRM
MCC-132X4		AC/B		PAHRS	CC-27B	MOV	364PENRM
	480	AC/B		PAHRS	CS-7B	MOV	364PENRM
/CC-132X4A	480	AC/B		ECCS	SI-8802B	MOV	364PENRM
ACC-132X4A	480	AC/B	426PENRM	ECCS	SI-8811B	MOV	364PENRM
1CC-132X4A	480	AC/B	426PENRM	PAHAS	CS-1B	MOV	364PENRM
10 0 - 132X5	480	AC/B	426AB	cvcs	SI-8801B	MOV	364PENRM

# TABLE 3.7-2. PARTIAL LISTING OF ELECTRICAL SOURCE AND LOADS AT BYRON (CONTINUED)

POWER SOURCE	VOLTAGE	EMERG LOAD GRP	POWER SOURCE LOCATION	LOAD SYSTEM	LOAD COMPONENT ID	COMP	COMPONENT
MCC-231X3	480	AC/A	383AB	ccw	CCW-2-9473A	MOV	364AB
MQQ-232X1	480	AC/B	364AB	ccw	CCW-2-9473B	MOV	364AB
TR-111	120	AC/A	BATRM111	EP	ACBUS-111	BUS	BATRM111
TR-112	120	AC/B	BATRM112	EP	ACBUS-112	BUS	BATRM112
TR-113	120	AC/A	BATRMIII	EP	ACBUS-113	BUS	BATRM111
TR-114	120	AC/B	BATRM112	EP	ACBUS-114	BUS	BATRM112
TR-131X	480	AC/A	ESF11	EP	BUS-131X	BUS	ESF11
TR-1312	480	AC/A	SXCTASG	EP	BUS-131Z	BUS	SXCTASG
TR-132X	480	AC/B	ESF12	EP	BUS-132X	BUS	ESF12
TR-1322	480	AC/B	SXCTBSG	EP	BUS-132Z	BUS	SXCTBSG

#### COMPONENT COOLING SYSTEM 3.8

3.8.1 System Function

The Component Cooling system provides cooling water to various plant components in both units during normal operation, and plant shutdown. After an accident, the Component Cooling system acts as an intermediate system between the components being cooled and the Essential Service Water system. Separation is required to minimize the possible release of radioactive material. The Component Cooling System serves to remove residual and sensible heat from the RCS during plant shutdown by cooling the RHR heat exchangers.

3.8.2 System Definition

The Component Cooling system is a closed loop system consisting of five motor driven pumps, three heat exchangers, two surge tanks, and associated piping and valves. The system is designed to serve both units. The major heat loads in the plant can be divided into a Unit 1 loop and a Unit 2 loop, with each loop containing two pumps and one heat exchanger. An exception is the RHR heat exchangers and pumps, which are cooled by a common header which may be aligned with the Component Cooling pumps for Unit 1 or Unit 2, or isolated and supplied by the fifth pump and third heat exchanger, which are common to both units. These components are designated pump 0 and heat exchanger 0.

The heat exchangers transfer heat to the Essential Service Water system. The

surge tanks accommodate expansion, contraction, and in-leakage of water.

Simplified drawings of the Component Cooling system are shown in Figures 3.8-1 and 3.8-2. These drawings show some components from Unit 2. Unit 1 component IDs begin with "1", Unit 2 component IDs begin with "2". A summary of the data on selected Component Cooling system components is presented in Table 3.8-1.

3.8.3

System Operation
Three component cooling pumps, two component cooling heat exchangers, and the two surge tanks are sufficient for normal operation of the two units. The remaining two pumps and one heat exchanger serve as backups. Cooling water is circulated by the pumps through the shell side of the heat exchangers to the components being cooled, then back to the pump suction. Demineralized makeup water is added into the surge tanks as needed to maintain coolant inventory. A backup source of makeup water is the primary water storage tank.

Heat loads supported by the Component Cooling system include the following:

- RHR heat exchangers and pumps
- Spent fuel pit heat exchangers

Letdown heat exchanger

- Excess letdown heat exchanger

- Positive displacement charging pump

Component cooling is also provided for additional components, such as the reactor coolant pumps and components of the Chemical and Volume Control System.

3.8.4 System Success Criteria

Following a LOCA, the following success criteria apply to the Component Cooling System (Ref. 1):

> - Following a LOCA, Unit 1 equipment is normally isolated from Unit 2 equipment. Component Cooling System equipment in the unit experiencing the LOCA is then divided into two redundant trains each consisting of one

Component Cooling pump, one heat exchanger and half of the baffled surge tank. One Component Cooling train is adequate forestablishing a safe shutdown condition.

- Essential Service water must be supplied to the Component Cooling heat exchanger used for post-LOCA recovery.

#### 3.8.5 Component Information

- A. Component Cooling Pumps 1A, 1B, 2A, 2B, and 0 1. Rated flow: 4800 gpm @ 250 ft head (108 psid)
  2. Rated capacity: 33% (to supply both units)

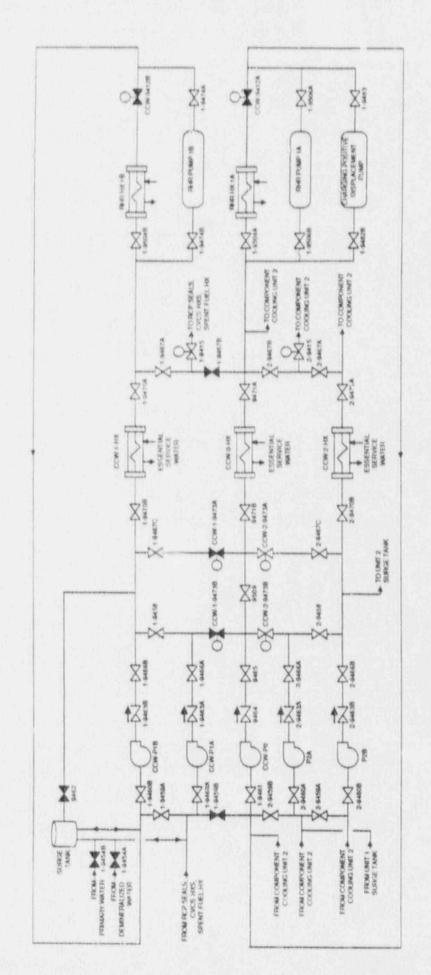
  - 3. Type: horizontal centrifugal
- B. Component Cooling Heat Exchangers 1 A, 1B, and 0
  - 1. Design duty: 40.87 x 106 Btu/hr
  - 2. Type: shell and straight tube

#### 3.8.6 Support Systems and Interfaces

- A. Control Signals
  - 1. Automatic
    - The Component Cooling pumps are not automatically actuated.
  - 2. Remote Manual The Component Cooling pumps can be actuated by remote manual means from the control room and from the remote shutdown control panel.
- B. Motive Power
  - 1. The Component Cooling motor-driven pumps and motor operated valves are Class 1E AC loads that can be supplied from the standby diesel generators as described in Section 3.7.
- C. Other
  - 1. The Component Cooling heat exchangers are cooled by the Essential Service Water system.
  - 2. Lubrication, ventilation, and cooling are provided locally for the Component Cooling pumps.

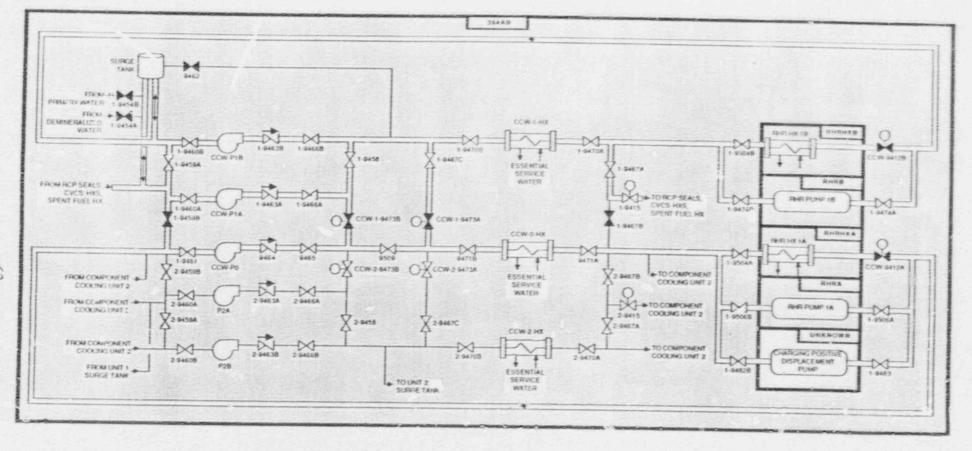
#### 3.8.7 Section 3.8 References

1. Byron/Braidwood Final Safety Analysis Report, Section 9.2.2.



NOTE: Details For Unit 2 Are Not included

Figure 3.8-1. Byron Unit 1 & 2 Component Cooling Water System



NOTE: Details For Lint 2 Are filet Included

Figure 3.8-2. Byron Unit 1 & 2 Component Cooling Water System Showing Component Locations

Table 3.8-1. Byron Component Cooling Water System Data Summary for Selected Components

COMPONENT ID	COMP.	LOCATION	POWER SOURCE	VOLTAGE	POWER SOURCE LOCATION	EMERG.
CCW-0-HX	HX	364AB				LUAD GIII
CCW-1-9473A	MOV	364AB	MCC-131X3	480	383AB	AC/A
CCW-1-9473A	MOV	364AB	MCC-131X3	480	383AB	AC/A
CCW-1-9473B	MOV	364AB	MCC-1: 2X1	480	364AB	AC/B
CCW-1-9473B	MOV	364AB	MCC- J2X1	480	364AB	AC/B
CCW-1-HX	HX	364AB				
CCW-2-9473A	MOV	364AB	MCC-231X3	480	383AB	AC/A
CCW-2-9473B	MOV	364AB	MCC-232X1	480	364AB	AC/B
CCW-9412A	MOV	364AB				
CCW-9412B	MOV	364AB				
CCW-P0	MDP	364AB	BUS-141	4160	ESF11	
CCW-P0	MDP	364AB	BUS-142	4160	ESF12	
CCW-P1A	MDP	364AB	BUS i41	4160	ESF11	AC/A
CCW-P1B	MDP	364AB	BUS-142	4160	ESF12	ACS -

#### ESSENTIAL SERVICE WATER (ESW) SYSTEM 3.9

3.9.1 System Function

The Essential Service Water System supplies cooling water from the ultimate heat sink to various heat loads in both the primary and secondary portions of the plant. The system is designed to provide a continuous flow of cooling water to those loads which are safety-related or essential to the safe shutdown of the reactor.

System Definition

The Essential Service Water System contains two headers, each supplied by a single motor-driven pump. The sources of water for the system are the two essential service water cooling towers. Strainers are provided to remove impurities from the raw water before it enters the ESW pumps. Heat is rejected to the cooling towers, which are designed to accommodate the ! at loads from both units simultaneously.

Simplified drawings of the ESW system are shown in Figures 3.9-1 and 3.9-2. These drawings show some components from Unit 2. Unit 1 component IDs begin with "1". Unit 2 component IDs begin with "2". A summary of data on selected ESW

components is presented in Table 3.9-1.

1.9.3 System Operation

During normal operation, one of the ESW pumps is in continuous operation providing pooling water to essential loads. Essential loads are those required for safe shutdown, and are therefore redundant and served by the corresponding channels of the ESW system. Heat loads supported by the ESW system include the following:

- Diesel generator coolers
- Containment fan coolers

Component Cooling System heat exchangers

AFW, ESW, SI, and centrifugal charging pump lube oil coolers

AFW. ESW, SI, RHR, CS, and centrifugal and positive displacement charging pump cubicle coolers.

The ESW also provides an assured supply of water to the Auxiliary Feedwater System. ESW header 1A supplies the motor-driven AFW pump 1A and ESW header 1B supplies the diesel-driven AFW pump 1B.

The essential service water cooling towers are cooled by fans.

3.9.4 System success Criteria

Following a LOCA the following success crimnia apply to the ESW system

(Ref 1):

- One out of two ESW pumps operates supplying cooling water to essential loads.

#### 3.9.5 Component Information

A. Service Water Pumps 1A and 1B

- 1. Rated flow: 24,000 gpm @ 180 ft head (78 psid)
- 2. Rated capacity: 100%
- 3. Type: horizontal centrifugal
- B. Ultimate Heat Sink Essential service water cooling towers (2)
- C. Cooling Tower Fans (2)

#### Support Systems and Interfaces 3.9.6

- A. Control Signals
  - 1. Automatic

- The ESW pumps are not automatically actuated.

  2. Remote Manual

  The ESW pumps can be actuated by remote manual means from the control room and from the remote shutdown control panel.
- B. Motive Power The ESW motor driven pumps, motor operated valves, and fans are Class 1E AC loads that can be supplied from he standby diesel generators as described in Section 3.7.
- - 1. Lubrication, ventilation, and cooling are provided locally for the ESW pumps.

#### 3.9.7 Section 3.9 References

1. Byron/Braidwood Final Safety Analysis Report, Section 9.2.1.

Figure 3.9.1 Byron Units 1 & 2 Essential Service Water System (Page 1 of 2)

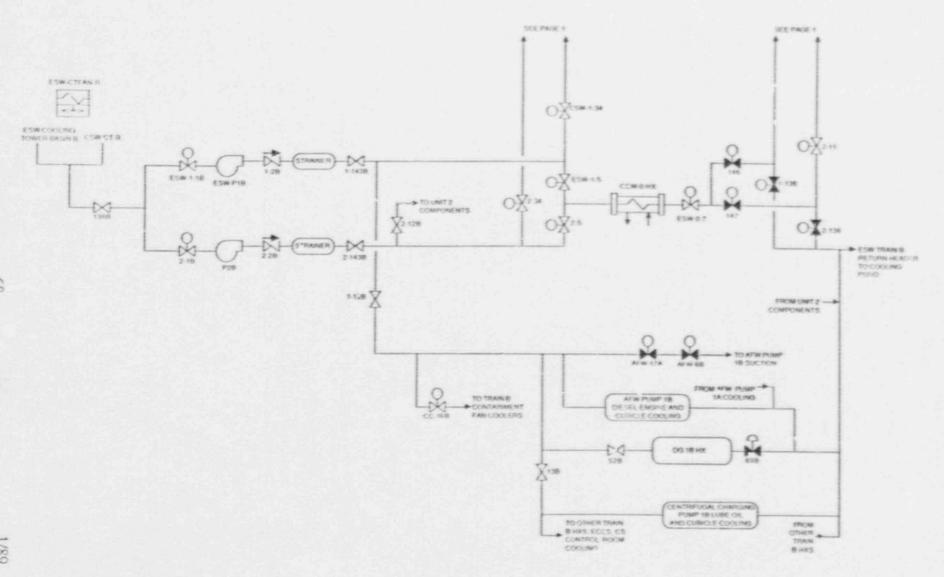


Figure 3.9-1. Byron Units 1 & 2 Essential Service Water System (Page 2 of 2)

Figure 3.9-2. Byron Units 1 & 2 Essential Service Water System Showing Component Locations (Page 1 of 2)

Figure 3.9-2. Byron Units 1 & 2 Essential Service Water System Showing Component Locations (Page 2 of 2)

Table 3.9-1. Byron Essential Service Water System Data Summary for Selected Components

COMPONENT ID	COMP. TYPE	LOCATION	POWER SOURCE	VOLTAGE	POWER SOURCE	EMERG.
ESW-0-7	MOV	346AB				
ESW-1-1A	MOV	SX1A	MCC-131X3	480	383AB	AC/A
ESW-1-1B	MOV	SX1B	MCC-132X1	480	364AB	AC/B
ESW-1-33	MOV	ESWPMPA	MCC-131X1	480	364PENRM	AC/A
ESW-1-33	MOV	ESWPMPA	MCC-131X1	480	364PENRM	AC/A
ESW-1-34	MOV	ESWPMPB	MCC-132X1	480	364AB	AC/B
ESW-1-34	MOV	ESWPMPB	MCC-132X1	489	364AB	AC/B
ESW-1-4	MOV	ESWPMPA	MCC-131X1	480	364PENRM	AC/A
ESW-1-4	MOV	ESWPMPA	MCC-131X1	480	364PENRM	AC/A
ESW-1-5	MOV	ESWPMPB	MCC-132X1	480	364AB	AC/B
ESW-1-5	MOV	ESWPMPB	MCC-132X1	480	364AB	AC/B
ESW-1-7	MOV	346AB				
ESW-CT-A	TANK	SXCTA		Pile II		
ESW-CT-B	TANK	SXCTB	LA LEVIE DE L'E			
ESW-CTFAN-A	ACU	SXCTA	BUS-131Z	480	SWCTASG	AC/A
ESW-CTFAN-B	ACU	SXCTB	BUS-132Z	480	SWCTBSG	AC/B
ESW-P1A	MDP	ESWPMPA	BUS-141	4160	ESF11	AC/A
ESW-P1B	MDP	ESWPMPB	BUS-142	4160	ESF12	AC/B

#### 4. PLANT INFORMATION

4.1 SITE AND BUILDING SUMMARY

The Byron Station, Units 1 and 2, is located in northern Illinois, 3.7 miles south-southwest of the town of Byron and 2.2 miles east of the Rock River. The site is in the approximate center of Ogle Courty in a predominately agricultural area. The site occupies approximately 1782 acres of land. Figure 4-1 is a general view of the plant and vicinity.

The major structures at this unit i clude the two containment buildings, a shared turbine building, a shared auxiliary building, a shared fuel building, and two cooling towers. A site plot plan is shown in Figure 4-2. Plant section drawings are

shown in Figures 4-3 and 4-4.

Each containment structure is a reinforced concrete cylinder with a steel liner. The containment contains the reactor vessel, reactor coolant pumps, steam generators, and pressurizer. Pumps, piping, and valving for the reactor coolant system is completely contained within the containment structure. Access to the building is via an equipment hatch or a personnel hatch. Piping and electrical penetration areas are on various levels of the auxiliary building.

The turbine building, located east of the containments, houses the turbine

generator and the associated power generating auxiliaries.

The auxiliary building is located to the east of and between the containments and contains much of the plant's safety related equipment, specifically the auxiliary feedwater pumps, high pressure injection pumps, RHR pumps and heat exchangers, containment spray pumps, charging pumps, component cooling water pumps and heat exchangers, and motor control centers supplying power to safety system components.

The fuel building is between the two containments and houses the spent fuel

pool.

The cooling towers are located east of the turbine building.

4.2 FACILITY LAYOUT DRAWINGS

Figures 4-5 through 4-11 are simplified building layout drawings for Byron 1 & 2. Details of the turbine building and many of the outlying buildings are not shown on these drawings. Major rooms, stairways, elevators, and doorways are shown in the simplified layout drawings, however, many interior walls have been omitted for clarity. Labels printed in uppercase correspond to the location codes listed in Table 4-1 and used in the component data listings and system drawings in Section 3. Some additional labels are included for information and are printed in lowercase type.

A listing of components by location is presented in Table 4-2. Components included in Table 4-2 are those found in the system data tables in Section 3, therefore this table is only a partial listing of the components and equipment that are located in a particular

room or area of the plant.

### 4.3 SECTION 4 REFERENCES

1. Heddleson, F.A., "Design Data and Safety Features of Commercial Nuclear Power Plants.", ORNL-NSIC-55, Volume IV, Oak Ridge National Laboratory, Nuclear Safety Information Center, March 1975.

72 1/89

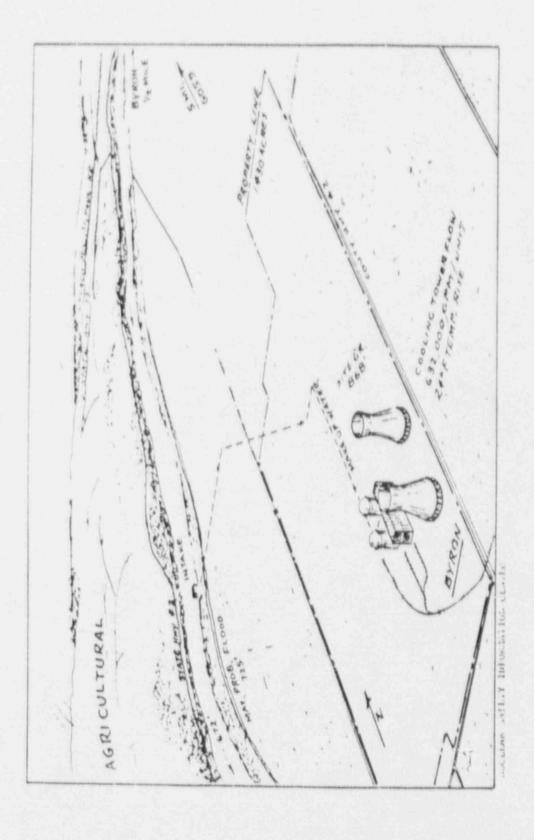


Figure 4-1. General View of Byron Station and Vicinity

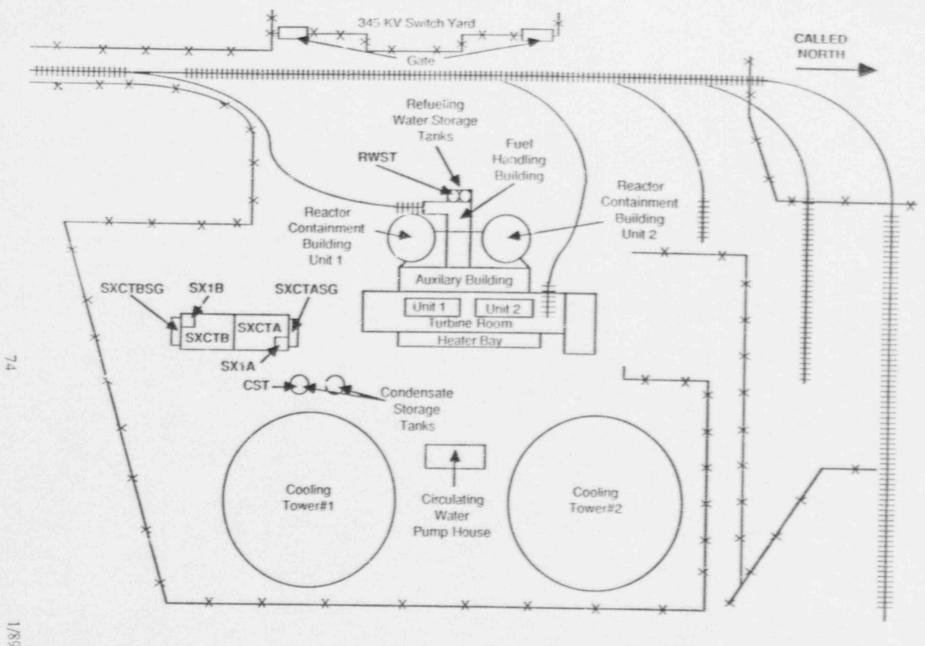


Figure 4-2. Byron 1 & 2 Plot Plan

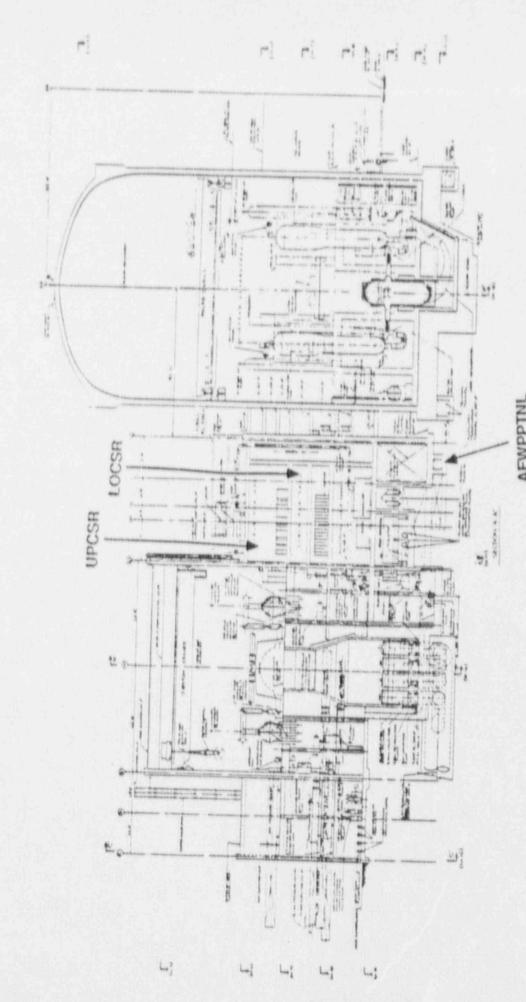


Figure 4-3. Byron Unit 1 Reactor, Auxiliary, and Turbine Building Elevation Drawing

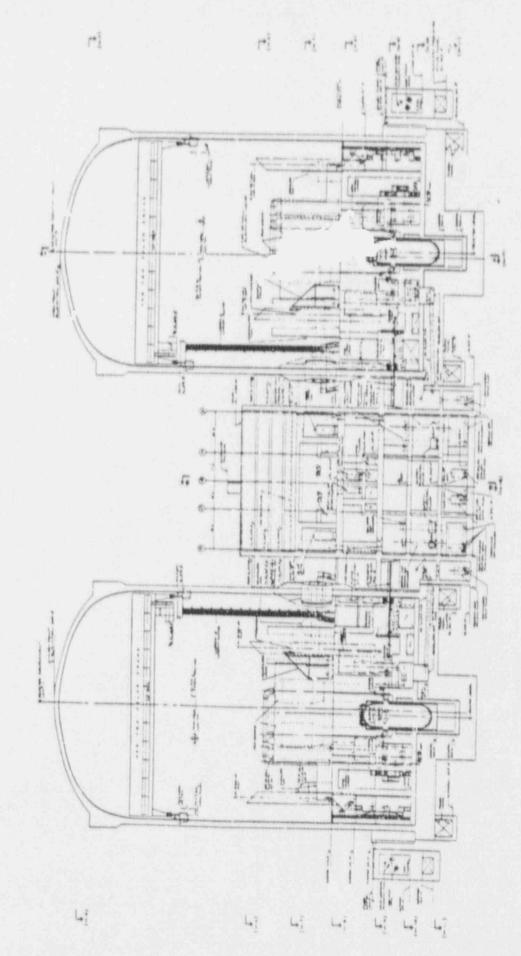


Figure 4-4. Byron 1 & 2 Reactor, Auxiliary, and Fuel Handling Building Elevation Drawing

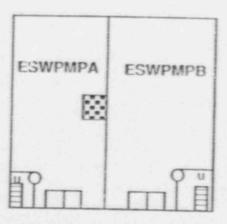


Figure 4-5. Byron 1 & 2 Station Arrangement, Elevation 330' of the Auxiliary Building

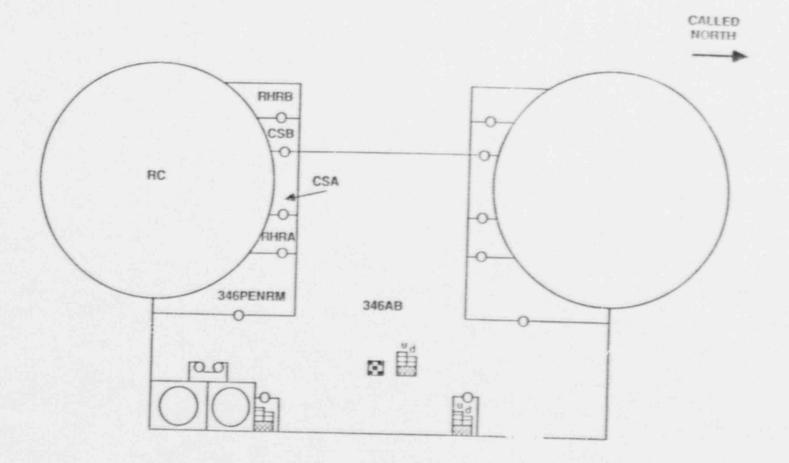


Figure 4-6. Byron 1 & 2 Station Arrangement, Elevation 346'

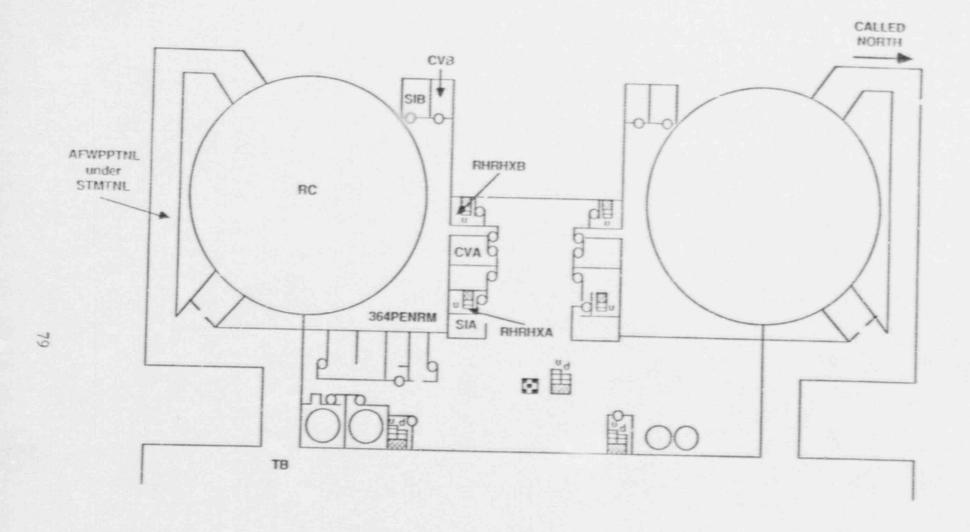


Figure 4-7. Byron 1 & 2 Station Arrangement, Elevation 364'

Figure 4-8. Byron 1 & 2 Station Arrangement, Elevation 383'

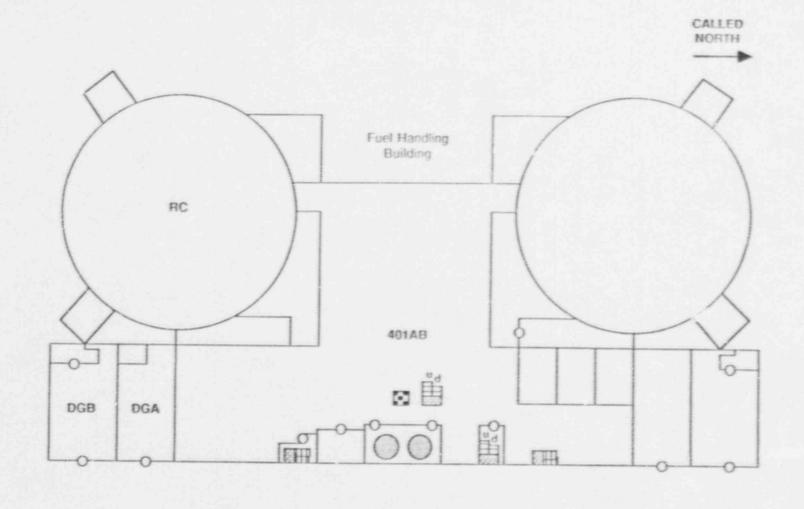


Figure 4-9. Byron 1 & 2 Station Arrangement, Elevation 401'

1/89

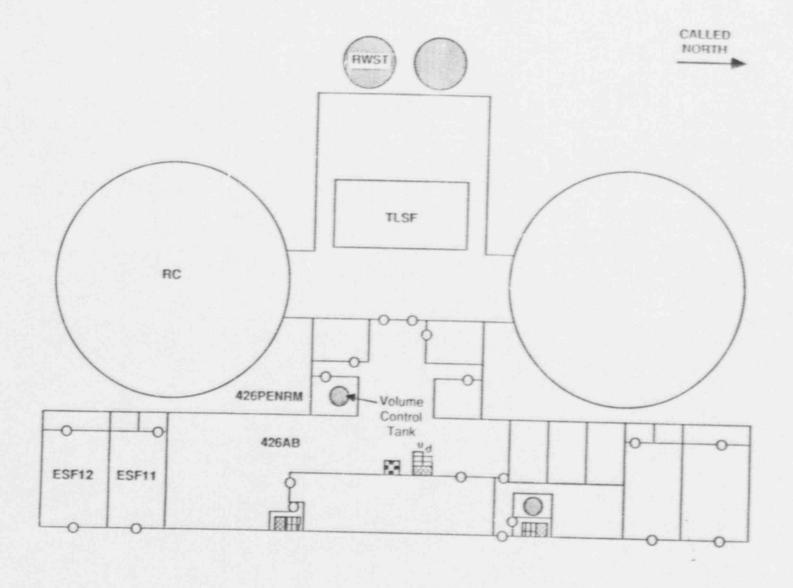


Figure 4-10. Byron 1 & 2 Station Arrangement, Elevation 426'

Figure 4-11. Byron 1 & 2 Station Arrangement, Elevation 451'

1/89

# Table 4-1. Definition of Byron 1 Building and Location Codes

	Codes	Descriptions
1.	346AB	Elevation 346' of the Auxiliary Building
2.	346PENRM	Penetration Area, located on the 346' elevation of the Auxiliary Building
3.	364AB	Elevation 364' of the Auxiliary Building
4.	364PENRM	Penetration Area, located on the 364' ele ion of the Auxiliary Building
5.	383AB	Elevation 383' of the Auxiliary Building
6.	401AB	Elevation 401' of the Auxiliary Building
7.	414PENRM	Penetration Area, located on the 414' of the Auxiliary Building
8.	426AB	Elevation 426' of the Auxiliary Building
9.	426PENRM	Penetration Area, located on the 426' of the Auxiliary Building
10.	AEER	Auxiliary Electric Equipment Room, located on the 451 elevation of the Auxiliary Building
11.	AFWPPTNL	Auxiliary Feedwater Pipe Tunnel under Main Steam Tunnel
12.	BATRM111	111 Battery Room, located on the 451' elevation of the Auxiliary Building
13.	BATRM112	112 Battery Room, located on the 451' elevation of the Auxiliary Building
14.	CR	Control Room, located on the 451' elevation of the Auxiliary Building
15.	CSA	Core Spray Pump A Room, located on the 346' elevation of the Auxiliary Building
16.	CSB	Core Spray Pump B Room, located on the 346' elevation of the Auxiliary Building
17.	CST	Condensate Storage Tank
18.	CVA	Centrifugal Charging Pump A Room, located on the 364' elevation of the Auxiliary Building
19	CVB	Centrifugal Charging Pump B Room, located on the 364' elevation of the Auxiliary Building

84

1/89

# Table 4-1. Definition of Byron 1 Building and Location Codes (Continued)

	Codes	Description
20.	DDAFW	Diesel Driven Auxiliary Feedwater Pump Room, located on the 38' elevation of the Auxiliary Building
21.	DGA	Diesel Generator 1A Room, located on the 401' elevation of the Auxiliary Building
22	DGAFUEL	Diesel Generator 1A Fuel Storage Room, located on the 383' elevation of the Auxiliary Building
23.	DGB	Diesel Generator 1B Room, located on the 401' elevation of the Auxiliary Building
24.	DGBFUEL	Diesel Generator 1B Fuel Storage Room, located on the 383' elevation of the Auxiliary Building
25.	ESF11	Division 11 ESF Switchgear Room, located on the 426' elevation of the Auxiliary Building
26.	ESF12	Division 12 ESF Switchgear Room, located on the 426' elevation of the Auxiliary Building
27.	ESWPMPA	Emergency Service Water A Pump Room, located on the 330' elevation of the Auxiliary Building
28.	ESWPMPB	Emergency Service Water B Pump Room, located on the 550' elevation of the Auxiliary Building
29.	LOCSR	Residual Heat Removal System "A" Pump Room, located on the 93' elevation of the Auxiliary Building - east side of the Reactor Containment Building
30.	RC	Reactor Containment Building
31.	RHRA	RHR Pump A Room, located on the 346' elevation of the Auxiliary Building
32.	RHRB	RHR Pump B Room, located on the 346' elevation of the Auxiliary Building
33.	RHRHXA	RHR Heat Exchanger A Room, located on the 364' elevation of the Auxiliary Building
34.	RHRHXB	RHR Heat Exchanger B Room, located on the 364' elevation of the Auxiliary Building
35.	RWST	Refueling Water Storage Tank

# Table 4-1. Definition of Byron 1 Building and Location Codes (Continued)

	Codes	Description
36.	RWSTINL	Tunnel from RWST, located on the 364' elevation of the Auxiliary Building
37.	RSCP	Remote Shutdown Control Panel, located on the 383' elevation of the Auxiliary Building
38.	SIA	Safety Injection Pump A Room, located on the 364' elevation of the Auxiliary Building
39.	SIB	Safety Injection Pump B Room, located on the 364' elevation of the Auxiliary Building
40.	STMTNL	Main Steam Tunnel, located on the 364' elevation - outboard side of Containment
41.	SX1A	Pit containing ESW Valve 1S001A on the 330' elevation of the Auxiliary Building
42.	SX1B	Pit containing ESW Valve 1S001B, located on the 330' elevation of the Auxiliary Building
43.	SXCTA	Emergency Service Water A Cooling Tower
44.	SXCTASG	Switchgear Room for the ESW A Cooling Tower
45.	TB	Turbine Building
46.	TLSF	Spent fuel pool operating floor, located on the 426' elevation of the Fuel Building
47.	UPCSR	Upper Cable Spreading Room, located on the 467' of the Auxiliary Building

TABLE 4-2. PARTIAL LISTING OF COMPONENTS BY LOCATION AT BYRON

LOCATION	SYSTEM	COMPONENTID	TYPE
346AB	ESW	ESW-1-7	MOV
346AB	ESW	ESW-0-7	MOV
346PENRM	ECCS	RH-8716A	MOV
346PENRM	ECCS	RH-8716A	MOV
346PENRM	ECCS	RH-8716B	MOV
346PENRM	ECCS	RH 8716B	MOV
364AB	ccw	CCW-1-9473A	MOV
364AB	ccw	CCW-1-9473A	MOV
364AD	ccw	CCW-1-9473B	MOV
364AB	ccw	CCW-1-9473B	MOV
364AB	cow	CCW-2-9473A	MOV
364AB	ccw	CCW-2-9473B	MOV
364AB	cow	CCW-PO	MDP
364AB	cow	CCW-P1A	MDP
364AB	ccw	GCW-P1B	MDP
364AB	ccw	CCW-9412A	MOV
364AB	ccw	CCW-94128	MOV
364AB	cow	COW-O-HX	HX
364AB	ccw	COW-17-IX	HX
364AB	CCW	COW-PO	MDP
364AB	SP	MCC-132X1	MCC
364PENRM	cvcs	CV-112D	MOV
364PENRM	oves	CV-112E	MOV
364PENRM	CVUS	SI-8801A	MOV
364PENRM	cvcs	SI-8801B	MOV
364PENRM	ECCS	CV-8804A	MOV
364PENRM	ECOS	SI-8811A	MOV
64PENRM	ECCS	SI-8811B	MOV
64PENRM	ECCS	SI-8821A	MOV
164PENRM	ECCS	SI-8821A	MOV
64PENAM	ECCS	SI-8821B	MOV
64PENRM	ECCS	SI-8821B	
64PENRM	ECCS		MOV
M. IFTIN	2005	SI-8835	MOV

TABLE 4-2. PARTIAL LISTING OF COMPONENTS BY LOCATION AT BYRON (CONTINUED)

LOCATION	SYSTEM	COMPONENTID	TYPE
364PENRM	ECCS	SI-8602A	MOV
364PENRM	ECCS	SI-8802B	MOV
364PENRM	EP	MCC-131X1	MOC
364PENRM	EP	MCC-131X1A	MCC
364PENRM	PAHRS	CO-16A	MOV
364PENRM	PAHRS	CC-27A	MOV
364PENAM	PAHRS	CC-16B	MOV
364PENRM	PAHAS	CC-27B	MOV
364PENAM	PAHRS	CS-1A	MOV
364PENRM	PAHAS	CS-7A	MOV
364PENRM	PAHRS	CS-1B	MOV
364PENRM	PAHAS	CS-7B	MOV
383AB	AFW	AFW-P1A	MDP
383AB	AFW	AFW-17A	MOV
383AB	AFW	AFW-6A	MOV
383AB	EP	MCC-131X3	MCC
383AB	EP	MCC-132X3	MCC
414PENAM	EF	MCC-131X2	MCC
426AB	EP	MCC-131X5	Mac
426AB	EP	MCC-132X5	MCC
426PENAM	EP	MCC-132X2	MCC
426PENAM	EP	MCC-132X4	MCC
426PENRM	EP	MCC-132X4A	
AFWPPTNL	AFW	AFW-13E	MCC
AFWPPTNL	AFW		MOV
AFWPPINL		AFW-13F	MOV
	AFW	AFW-13G	MOV
AFWPPTNL	AFW	AFW-13H	MOV
AFWPPTNL	AFW	AFW-13A	MOV
AFWPPTNL	AFW	AFW-13B	MOV
AFWPPTNL	AFW	AFW-13C	MOV
AFWEPTNL	AFW	AFW-13D	MOV
BATRMIII	EP	DCBUS-111	BUS
BATRMIII	EP	BC-111	BC

TABLE 4-2. PARTIAL LISTING OF COMPONENTS BY LOCATION AT BYRON (CONTINUED)

LOCATION	SYSTEM		TYPE
BATAMIII	EP	BT-111	BATT
BATRMIII	EP	DCBUS-111	BUS
BATRM111	EP	TR-111	XFMA
BATRMIII	EP	TR-113	XFMA
BATRMIII	EP	INV-111	INV
BATRMIII	EP	INV-111	INV
BATRIM111	EP	INV-113	INV
BATRM111	EP	INV-113	INV
BATRM111	EP	ACBUS-111	BUS
BATRMIII	EP	ACBUS-111	BUS
BATRMIII	EP	ACBUS-113	BUS
BATRMIII	EP	ACBUS-113	BUS
BATRM112	EP	DOBUS-112	BUS
BATAM112	EP	BC-112	BC
BATRM1'2	EP	BT-112	BATT
BATRM112	EP	DCBUS-112	BUS
BATRM112	EP	TA-112	XFMR
BATRM112	EP	TR-114	XFMR
BATRM112	EP	INV-112	INV
BATAM112	EP	INV-112	INV
BATRM112	EP	INV-114	INV
BATRM112	EP	INV-114	INV
BATRM112	EP	ACBUS-112	BUS
BATRM112	EP	ACBUS-112	BUS
BATAM112	EP	ACBUS-114	BUS
BATRM112	EP	ACBUS-114	BUS
OSA	PAHRS	CS-PIA	MDP
CSB	PAHRS	CS-P1B	MOP
CST	AFW	AFW-CST	TANK
OVA	cvcs	CV-P1A	MDP
OVB	ovos	CV-P1B	MDP
DDA: W	AFW	AFW-P1B	DDP
DDAFW	AFW	AFW-17B	MOV

TABLE 4-2. PARTIAL LISTING OF COMPONENTS BY LOCATION AT BYRON (CONTINUED)

LOCATION	SYSTEM	COMPONENTID	TYPE
DDAFW	AFW	AFW-6B	MOV
DGA	EP	DG-1A	50
DGB	EP	DG-18	DG
ESF11	EP	BUS-141	BUS
ESF11	EP	BUS-131X	BUS
ESF11	EP	TR-131X	XFMR
ESF11	EP	CB-1A	СВ
ESF12	EP	BUS-142	BUS
ESF12	EP	BUS-132X	BUS
ESF12	EP	TR-132X	XFMR
ESF12	EP	CB-1B	CB
ESWPMPA	ESW	ESW-1-33	MOV
ESWPMPA	ESW	ESW-1-33	MOV
ESWPMPA	ESW	ESW-1-4	MOV
ESWPMPA	ESW	ESW-1-4	MOV
ESWPMPA	ESW	ESW-PIA	MDP
ESWPMPB	ESW	ESW-1-34	MOV
ESWPMPB	ESW	ESW-1-34	MOV
ESWPMPB	ESW	ESW-1-5	MOV
ESWPMPB	ESW	ESW-1-5	MOV
ESWPMPB	ESW	ESW-P1B	MDP
90	AFW	SG-1A	SG
RO	AFW	SG-18	SG
RO	AFW	SG-10	SG
AC .	AFW	SG-1D	SG
40	ECCS	SUMP-A	SUMP
10	ECCS	SUMP-B	SUMP
RC	PAHRS	CC-FANA	
RC .	PAHRS	OC-FANC	ACU
6			AQU
	PAHRS	OC-FANB	ACU
i,	PAHRS	CC-FAND	ACU
	ACS	ACS-VESSEL	RV
0	ROS	RC-455A	NV

TABLE 4-2. PARTIAL LISTING OF COMPONENTS BY LOCATION AT BYRON (CONTINUED)

LOCATION		COMPONENTID	TYPE
AC .	ROS	RC-456	NV
RO	RCS	RC-8000A	MOV
AC .	RCS	AC-8000B	MOV
AC .	ROS	RC-6701A	MCV
RC .	RCS	RC-8701B	MOV
RC	ROS	AC-8702A	MOV
RO	ROS	AC-87020	MOV
RC	ROS	RC-8001A	MOV
RC	RCS	RC-8002A	MOV
RQ	HCS	RC-60013	MOV
RO	ROS	RC-8002B	MÓV
RO	RCS	RC-8001C	MOV
RO	RCS	RC-8002C	MOV
RC	RCS	RC-8001D	MOV
RC	ACS	RC-8002D	MOV
RHRA	ECCS	RH-PTA	MOP
RHRB	ECCS	AH-P1B	MOP
RHRHXA	ECCS	RH-HX1A	HX
RHAHXB	ECOS	RH-HX1B	HX
RWST	cvcs	SFAWST	TANK
RWST	ECCS	SI-AWST	TANK
SIA	ECCS	SI-8923A	MOV
SIA	ECCS	SI-P1A	MDP
SIA	ECCS	SI-8807A	MOV
SIA	ECCS	SI-8807B	MOV
SIA	ECCS	\$1-8924	MOV
SIB	EGOS	SI-8804B	MOV
SIB	ECOS	\$1-8806	MOV
918	ECOS	S1-8923B	MOV
SIB	ECCS	SI-P1B	MOP
SX1A -	ESW	ESW-1-1A	MOV
X1B	ESW	ESW-1-18	NOV
XCTA	ESW	ESW-CT-A	TANK

TABLE 4-2. PARTIAL LISTING OF COMPONENTS BY LOCATION AT BYRON (CONTINUED)

LOCATIC	SYSTEM	COMPONENTID	COMP
SXCIA	ESW	ESW-CTFAN-A	ACU
SXCTASG	EP	BUS-131Z	BUS
SXCTASG	EP	TR-131Z	XFMR
SXCTB	ESW	ESW-CT-B	TANK
SXCTB	ESW	ESW-CTFAN-B	ACU
SXCTBSG	EP	BUS-132Z	BUS
SXCTBSG	EP	TR-132Z	XFMA
UNKNOWN	EP	MCC-131X4	MCC

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- NUREG-75/023, "Safety Evaluation Report on Byron Station, Units 1 and 2, and The Braidwood Station, Units 1 and 2," USNRC, April 1975.
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- 3 NUREG-0876, "Safety Evaluation Report Related to the Operation of Byron Station, Units 1 and 2," USNRC, March 1982
- NUREG-1113, "Technical Specifications for Byron Station, Units 1 and 2," USNRC.
- Youngblood, R. and Papazoglou, I.A., "Review of the Byron/Braidwood Units 1 and 2 Auxiliary Feedwater System Reliability Analysis," NUREG/CR-3096, Brookhaven National Laboratory, November 1983.
- Cho, N.Z. et. al., "Analysis of Allowed Outage Times at Byre: Generating Station," NUREG/CR-4404, Brookhaven National Laboratory, June 1986.

#### APPENDIX A DEFINITION OF SYMBOLS USED IN THE SYSTEM AND LAYOUT DRAWINGS

### A1. SYSTEM DRAWINGS

## A1.1 Fluid System Drawings

The simplified system drawings are accurate representations of the major flow paths in a system and the important interfaces with other fluid systems. As a general rule, small fluid lines that are not essential to the bar 'c operation of the system are not shown in these drawings. Lines of this type include instrumentation lines, vent lines, drain lines, and other lines that are less than 1/3 the diameter of the connecting major flow path. There usually are two versions of each fluid system drawing; a simplified system drawing, and a comparable drawing showing component locations. The drawing conventions used in the fluid system drawings are the following:

Flow generally is left to right.

- Water sources are located on the left and water "users" (i.e., heat loads) or discharge paths are located on the right.

One exception is the return flow path in closed loop systems which is right

Another exception is the Reactor Coolant System (RCS) drawing which is "vessel-centered", with the primary loops on both sides of the vessel.

Horizontal lines always dominate and break vertical lines.

Component symbols used in the fluid system drawings are defined in Figure A-1

Most valve and pump symbols are designed to allow the reader to distinguish among similar components based on their support system requirements (i.e., electric power for a motor or solenoid, steam to drive a turbine, pneu natic or hydraulic source for valve operation, etc.)

Valve symbols allow the reader to distinguish among valves that allow flow in either direction, check (non-return) valves, and valves that perform an overpressure protection function. No attempt has been made to define the specific type of valve (i.e., as a globe, gate, butterfly, or other specific type of valve).

Pump symbols distinguish between centrifugal and positive displacement pumps and between types of pump drives (i.e., motor, turbine, or engine).

Locations are identified in terms of plant location codes defined in Section 4 of this Sourcebook.

Location is indicated by shaded "zones" that are not intended to represent the actual room geometry.

Locations of discrete components represent the actual physical location of

the component.

Piping locations between discrete components represent the plant areas through which the piping passes (i.e. including pipe tunnels and underground pipe runs).

Component locations that are not known are indicated by placing the

components in an unshaded (white) zone,

The primary flow path in the system is highlighted (i.e., bold white line) in the location version of the fluid system drawings.

#### A1.2 Electrical System Drawings

The electric power system drawings focus on the Class 1E portions of the plant's electric power system. Separate drawings are provided for the AC and DC portions of the Class 1E system. There often are two versions of each electrical system drawing; a simplified system drawing, and a comparable drawing showing component locations. The drawing conventions used in the electrical system drawings are the following:

- Flow generally is top to bottom

 In the AC power drawings, the interface with the switchyard and/or offsite grid is shown at the top of the drawing.

In the DC power drawings, the batteries and the interface with the AC power system are shown at the top of the drawing.

Vertical lines dominate and break horizontal lines.

- Component symbols used in the electrical system drawings are defined in Figure A-2.
- Locations are identified in terms of plant location codes defined in Section 4 of this Sourcebook.

 Locations are indicated by shaded "zones" that are not intended to represent the actual room geometry.

Locations of discrete components represent the actual physical location of

the component.

 The electrical connections (i.e., cable runs) between discrete components, as shown on the electrical system drawings, DO NOT represent the actual cable routing in the plant

Component locations that are not known are indicated by placing the

discrete components in an unshaded (white) zone.

#### A2. SITE AND LAYOUT DRAWINGS

## A2.1 Site Drawings

A general view of each reactor site and vicinity is presented along with a simplified site plan showing the arrangement of the major buildings, tanks, and other features of the site. The general view of the reactor site is obtained from ORNL-NSIC-55 (Ref. 1). The site drawings are approximately to scale, but should not be used to estimate distances on the site. As-built scale drawings should be consulted for this purpose.

Labels printed in bold uppercase correspond to the location codes defined in Section 4 and used in the component data listings and system drawings in Section 3. Some

additional labels are included for information and are printed in lowercase type.

## A2.2 Layout Drawings

Simplified building layout drawings are developed for the portions of the plant that contain components and systems that are described in Section 3 of this Sourcebook. Generally, the following buildings are included: reactor building, auxiliary building, fuel building, diesel building, and the intake structure or pumphouse. Layout drawings generally are not developed for other buildings.

Symbols used in the simplified layout drawings re defined in Figure A-3. Major rooms, stairways, elevators, and doorways are shown in the simplified layout drawings however, many interior walls have been omitted for clarity. The building layout drawings,

are approximately to scale, should not be used to estimate room size or distances. As-built

scale drawings for should be consulted his purpose.

Labels printed in uppercase bolded also correspond to the location codes defined in Section 4 and used in the component data listings and system drawings in Section 3. Some additional labels are included for information and are printed in lowercase type.

#### A3. APPENDIX A REFERENCES

 Heddleson, F.A., "Design Data and Safety Features of Commercial Nuclear Power Plants.", ORNL-NSIC-55, Volumes 1 to 4, Oak Ridge National Laboratory, Nuclear Safety Information Center, December 1973 (Vol.1), January 1972 (Vol. 2), April 1974 (Vol. 3), and March 1975 (Vol. 4)

96 1/89

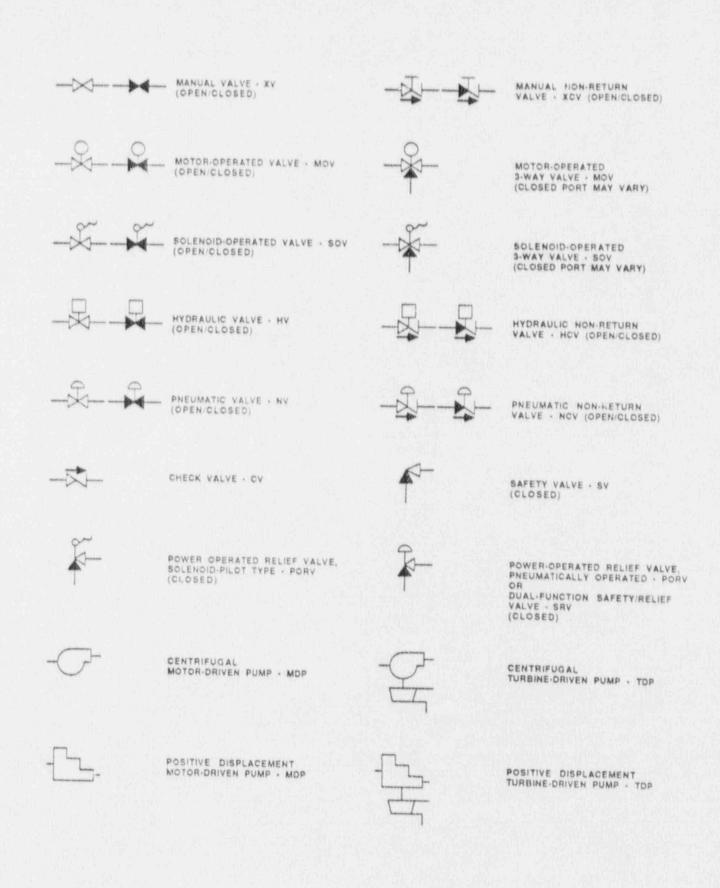


Figure A-1. Key To Symbols In Fluid System Drawings

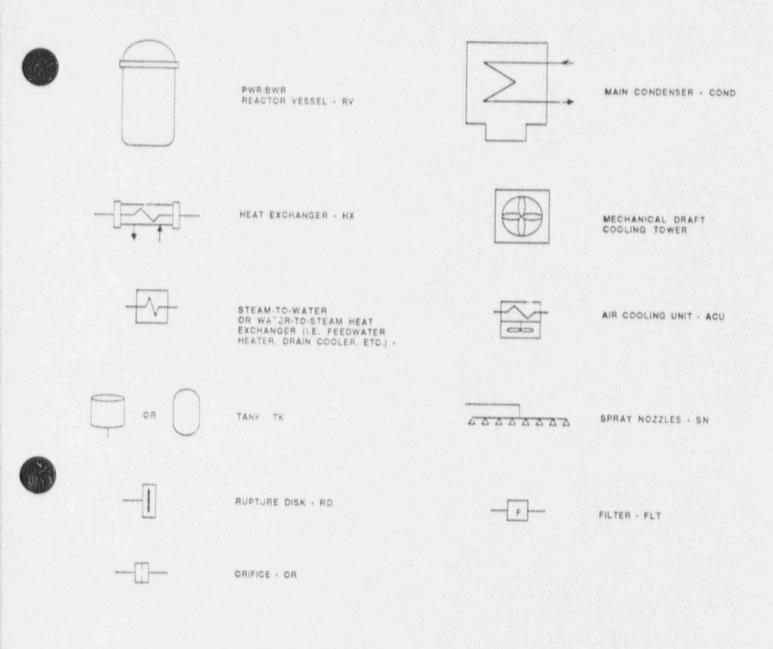


Figure A-1. Key To Symbols In Fluid System Drawings (Continued)

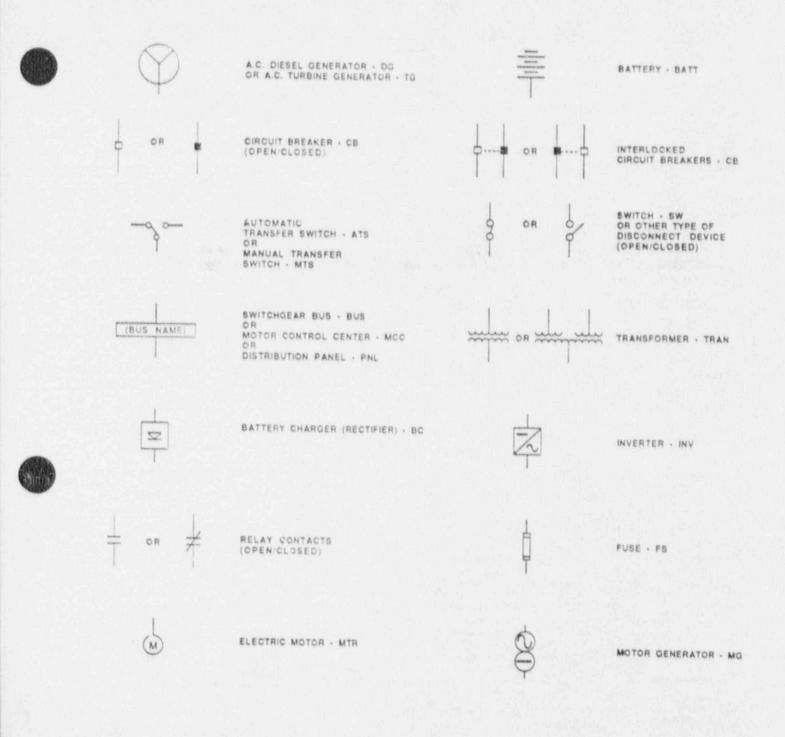


Figure A-2. Key To Symbols In Electrical System Drawings

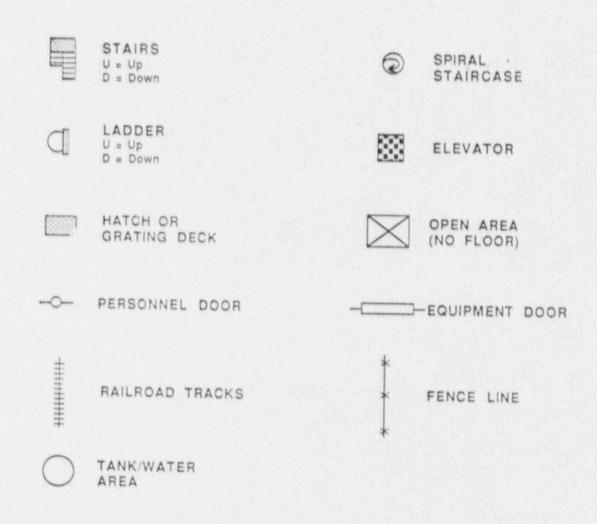


Figure A-3. Key To Symbols In Facility Layout Drawings

# DEFINITION OF TERMS USED IN THE DATA TABLES

Terms appearing in the data tables in Sections 3 and 4 of this Sourcebook are defined as follows:

SYSTEM (also LOAD SYSTEM) - All components associated with a particular system description in the Sourcebook have the same system code in the data base. System codes used in this Sourcebook are the following:

Code	Definition
RCS AFW ECCS CVCS PAHRS	Reactor Coolant System Auxiliary Feedwater System Emergency Core Cooling System Charging System Containment Heat Removal Systems (including containment spray system and fan coolers)
I&C EP CCW ESW	Instrumentation and Control Systems Electric Power System Component Cooling Water System Essential Service Water System

COMPONENT ID (also LOAD COMPONENT ID) - The component identification (ID) code in a data table matches the component ID that appears in the corresponding system drawing. The component ID generally begins with a system preface followed by a component number. The system preface is not necessarily the same as the system code described above. For component IDs, the system preface corresponds to what the plant calls the component (e.g. HPI, RHR). An example is HPI-730, denoting valve number 730 in the high pressure injection system, which is part of the ECCS. The component number is a contraction of the component number appearing in the plant piping and instrumentation drawings (P&IDs) and electrical one-line system drawings.

LOCATION (also COMPONENT LOCATION and POWER SOURCE LOCATION) - Refer to the location codes defined in Section 4.

COMPONENT TYPE (COMP TYPE) - Refer to Table B-1 for a list of component type codes.

POWER SOURCE - The component ID of the power source is listed in this field (see COMPONENT ID, above). In this data base, a "power source" for a particular component (i.e. a load or a distribution component) is the next higher electrical distribution or generating component in a distribution system. A single component may have more than one power source (i.e. a DC bus powered from a battery and a battery charger).

POWER SOURCE VOLTAGE (also VOLTAGE) - The voltage "seen" by a load of a power source is entered in this field. The downstream (output) voltage of a transformer, inverter, or battery charger is used.

EMERGENCY LOAD GROUP (EMERG LOAD GROUP) - AC and DC load groups (or electrical divisions) are defined as appropriate to the plant. Generally, AC load groups are identified as AC/A. AC/B, etc. The emergency load group for a third-of-a-kind load (i.e. a "swing" load) that can be powered from either of two AC load groups would be identified as AC/AB. DC load group follows similar naming conventions.

102 1/89

# TABLE B-1. COMPONENT TYPE CODES

COMPONENT	COMP TYPE
VALVES:  Motor-operated valve Pneumatic (air-operated) valve Hydraulic valve Solenoid-operated valve Manual valve Check valve Pneumatic non-return valve Hydraulic non-return valve Safety valve Dual function safety/relief valve Power-operated relief valve (pneumatic or solenoid-operated)	MOV NV or AOV HV SOV XV CV NCV HCV SV SRV PORV
PUMPS:  Motor-driven pump (centrifugal or PD) Turbine-driven pump (centrifugal of PD) Diesel-driven pump (centrifugal of PD)	MDP TDP DDP
OTHER FLUID SYSTEM COMPONENTS: Reactor vessel Steam generator (U-tube or once-through) Heat exchanger (water-to-water HX, or water-to-air HX) Cooling tower Tank Sump Rupture disk Orifice Filter or strainer Spray nozzle Heaters (i.e. pressurizer heaters)	RV SG HX CT TANK or TK SUMP RD ORIF FLT SN HTR
VENTILATION SYSTEM COMPONENTS: Fan (motor-driven, any type) Air cooling unit (air-to-water HX, usually including a fan) Condensing (air-conditioning) unit	FAN ACU or FCU COND
EMERGENCY POWER SOURCES: Diesel generator Gas turbine generator Battery	DG GT BATT

## TABLE B-1. COMPONENT TYPE CODES (Continued)

## COMPONENT COMP TYPE

## ELECTRIC POWER DISTRIBUTION EQUIPMENT:

Bus or switchgear	BUS
Motor control center	MCC
Distribution panel or cabinet	PNL or CAB
Transformer	TRAN or XFMR
Battery charger (rectifier)	BC or RECT
Inverter	INV
Uninterruptible power supply (a unit that may include battery, battery charger, and inverter)	UPS
Motor generator	MG
Circuit breaker	CB
Switch	SW
Automatic transfer switch	ATS
Manual transfer switch	MTS