

Log # TXX-94172 File # 10035 Ref. # GL92-01R1

June 20, 1994

William J. Cahill, Jr.
Group Vice President

U. S. Nuclear Regulatory Commission Attn: Document Control Desk

Washington, DC 20555

SUBJECT:

COMANCHE PEAK STEAM ELECTRIC STATION (CPSES)

DOCKET NOS. 50-445 AND 50-446

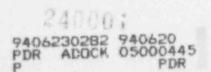
GENERIC LETTER (GL) 92-01, REVISION 1, "REACTOR VESSEL STRUCTURAL INTEGRITY," TEXAS UTILITIES ELECTRIC COMPANY, COMANCHE PEAK STEAM ELECTRIC STATION, UNIT NOS. 1 AND 2 (TAC NOS. M83451 AND M83452)

Gentlemen:

TU Electric received a letter from Mr. Tom Bergman dated May 11, 1994, on Generic Letter 92-01, Revision 1 which asked TU Electric to provide comments within 30 days from the date of the letter which has since expired on June 11, 1994. Per the phone conversation with Mr. Tom Bergman on June 14, 1994, TU Electric is sending this follow up letter.

TU Electric has reviewed the information provided in your letter dated May 11, 1994, regarding the data that has been entered into the Reactor Vessel Integrity Database (RVID). TU Electric has found the information to be correct and consistent with our data. TU Electric is sending you some clarifying information and missing data to add to your database and tables.

The references listed in the tables appear to be a portion of those provided in previous correspondence. The missing heat numbers for the plates in the beltline region are provided for inclusion in your database. The circumferential weld value for upper shelf energy (USE) is listed as 98 for the Unit 2 Reactor vessel. The 98 value appears to be a typo because 96 was the value provided in TU Electric's response to Generic Letter 88-11 (TXX-88882 dated December 30, 1988).



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TXX94172 Page 2 of 2 Questions concerning the clarifying information should be directed to Ray Adams, Licensing Engineer at 214-812-8826, Dan Hopkins at 817-897-6196, or Craig Harrington at 817-897-6705 in Design Engineering. Sincerely, William J. Cahill, Jr. D. R. Woodlan Docket Licensing Manager RJA/vld Enclosure c - Mr. L. J. Callan, Region IV Resident Inspectors, CPSES (2) Mr. T. A. Bergman, NRR

## Summary File for Pressurized Thermal Shock

Plant Name	Beltline Ident.	Hest No. Ident.	ID Neut. Fluence at EOL	1RT <sub>not</sub>	Method of Determin. IRT <sub>net</sub>	Chemistry Factor	Method of Determin. CF	<b>X</b> Cu	XNI
Comanche Peak 1 EOL: 2/8/2030	Int. shell R1107-1	C4-021-1	3.04E19	10°F	Plant specific	37	Table	0.06	0.65
	Int. shell/ R1107-2	67854-1	3.04819	-10°F	Plant specific	37	Table	0.06	0.64
	Int. shell R1107-3	C 4106-2	3.04219	10°F	Plant specific	31	Table	0.05	0.68
	Lower shell R1108-1	C4464-1	3.04E19	0°F	Plant specific	51	Table	0.08	0.64
	Lower shell R1108-2	c4533-2	3.04E19	20°F	Plant specific	31	Table	0.05	0.59
	Lower shell R1108-3	C4589-1	3.04£19	O°F	Plant specific	44	Table	0.07	0.64
	int. shell axial welds 101-124A/C	88112	3.04819	-70°F	Plant specific	43	Table	0.04	0.19
	Lower shell axial welds 101-142A/C	88112	3.04E19	-70°F	Plant specific	43	Table	0.04	0.19
	Circ. Weld 101-171	88112	3.04E19	-70°F	Plant specific	43	Table	0.04	0.19

The nickel content for all welds is from the average of 0.17 (GL 92-01 response dated July 2, 1992) and 0.2 (WCAP-13422).

Chemical composition (copper and nickel only) for all beltline materials, fluence, and IRT data are from WCAP-13422, which is not in the PR\_EDB. Surveillance materials copper, nickel, phosphorus, and sulfur data are from WCAP-13422.



E DUNIT I HEAT NUMBERS

# Summary File for Pressurized Thermal Shock

Plant Name	Beitline Ident.	Heat No. Ident.	ID Neut. Fluence at EOL	IRTnon	Method of Determin. IRT	Chemistry	Method of Determin. CF	*Cu	XNI
Comanche Peak 2	Int. shell A3807-1	C 55.21-1	3.04E19	-20°F	Plant specific	37	Table	0.06	0.64
EOL: 2/2/2033	Int. shell/ A3807-2	05522-2	3.04E19	10°F	Plant specific	37	Table	0.06	0.64
	Int. shell / A3807-3	B 9566-1	3.04E19	-20°F	Plant specific	31	Table	0.05	0.60
	Lower shell A3816-1	KKE 4 435-1	3.04E19	-30°F	Plant specific	31	Table	0.05	0.59
	Lower shell A3816-2	N214 437-1	3.04619	O°F	Plant specific	20	Table	0.03	0.65
	Lower shell A3816-3	NK64 433-1	3.04619	-40°F	Plant specific	26	Table	0.04	0.63
	int. shell axial welds	89833	3.04E19	-50°F	Plant specific	37.75	Table	0.07	0.05
	Lower shell exial welds	89833	3.04E19	-50°F	Plant specific	37.75	Table	0.07	0.05
	Circ. weld	89833	3.04E19	-60°F	Plant	34.05	Table	0.05	0.05

#### References:

The nickel content for the circ. weld is from the average of 0.03 (GL 92-01 Response dated July 2, 1992) and 0.07 (WCAP-10684).

The chemical composition, IRT<sub>met</sub>, and unirradiated upper shelf energy (UUSE) data are found in WCAP-10684, which is attached to December 16, 1985, letter from W. G. Counsil (TUECo) to V. S. Nooman (USNRC), subject: Fracture Toughness Properties of Unit 2 Reactor Vessel Materials

End of license (EOL) fluence datum is from WCAP-13422, which analyzes surveillance capsule U of Comanche Peak 1



UNIT 2 HEAT NUMBERS

# Summary File for Upper Shelf Energy

Plant Name	Beltline Ident.	Heat No.	Material Type	1/47 USE at EOL	1/4T Neutron Fluence at EOL	Unirrad. USE	Method of Determin. Unirrad. USE
Commonche Peak 2	Int. shell A3807-1		A 5338-1	84	1.812E19	108	Direct
EOL: 2/2/2033	int, shell A3807-2		A 533B-1	79	1.812E19	101	Direct
	Int. shell A3807-3		A 5338-1	82	1.812E19	105	Direct
	Lower shell A3816-1		A 5338-1	84	1.812E19	107	Direct
	Lower shell A3816-2		A 533B-1	83	1.812E19	106	Direct
	Lower shell A3816-3		A 5338-1	84	1.812E19	108	Direct
	int, shell axial welds	89833	Linde 0091, SAW	131	1.812E19	172	Direct
	Lower shell axial welds	89833	Linde 0091, SAW	131	1.812E19	172	Direct
	Circ. weld	89833	Linde 124, SAW	77	1.812E19	98	Surv. Weld

### References:

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The chemical composition and unirradiated upper shelf energy (UUSE) data are found in WCAP-10684, which is attached to December 16, 1985, letter from W. G. Counsil (TUECo) to V. S. Noonan (USNRC), subject: Fracture Toughness Properties of Unit 2 Reactor Vessel Materials

End of license (EDL) fluence datum is from WCAP-\*3422, which analyzes surveillance capsule U of Comanche Peak 1

GL 88-11 RESPONSE TXX-8882 MISTED VALUE AS 96.