

June 1, 1994

Docket No. 52-003

APPLICANT: Westinghouse Electric Corporation

FACILITY: AP600

SUBJECT: SUMMARY OF MEETING TO DISCUSS THE SHIELDING DESIGN AND LAYOUT OF THE MANAGEMENT MEETING WITH WESTINGHOUSE

On May 3, 1994, representatives of the Westinghouse Electric Corporation, Bechtel North American Power Corporation, and the Nuclear Regulatory Commission met to discuss the shielding design of the AP600. Enclosure 1 is a list of attendees. Enclosure 2 is the slide presentation.

Westinghouse discussed the containment source term assumptions, the release distribution outside of the containment, the radiation sources after an accident, and the shielding design for the sample station and the fuel transfer canal upender pit. The applicant traced the leakage paths that the AP600 design could have following a design basis accident.

(Original signed by)

Thomas J. Kenyon, Project Manager  
Standardization Project Directorate  
Associate Directorate for Advanced Reactors  
and License Renewal, NRR

Enclosures:  
As stated

cc w/enclosures:  
See next page

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| Docket File          | PDST R/F      | WRussell    | DCrutchfield  |
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| KShembarger          | PShea         | FHasselberg | TKenyon       |
| EJordan, 3701        | JMoore, 15B18 | WDean, EDO  | DCarter, 10D4 |
| ACRS (11) (w/o encl) |               |             |               |

|       |              |              |              |
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| OFC:  | LA:PDST:ADAR | PM:PDST:ADAR | SC:PDST:ADAR |
| NAME: | PShea        | TKenyon:sg   | RArchitzel   |
| DATE: | 05/26/94     | 05/26/94     | 05/26/94     |

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Westinghouse Electric Corporation

Docket No. 52-003

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WESTINGHOUSE AP600  
MEETING ATTENDEES  
MAY 3, 1994

| <u>Name</u>         | <u>Organization</u> |
|---------------------|---------------------|
| Dale Dexheimer      | Bechtel             |
| Jorge Schulz        | Bechtel             |
| Vijay Parameswaran  | Bechtel             |
| Naum Alper          | Westinghouse        |
| Heinrich Parin      | Bechtel             |
| Thomas Kenyon       | PDST                |
| Don Lindren         | W AP600             |
| James Sejvar        | W AP600             |
| D. Michael O'Connor | Bechtel             |
| Bryan Broadhead     | Oakridge Natl Lab.  |
| Dan Carter          | NRC/PRPB            |



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***AP600 RADIATION PROTECTION  
PRESENTATION***

***TO***

***UNITED STATES NUCLEAR  
REGULATORY COMMISSION***

***BECHTEL POWER CORPORATION  
SAN FRANCISCO, CA  
3 MAY 1994***

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# AGENDA

- Introduction M. O'Connor
- Containment Source Term J. Seyvar
- Outside Containment  
Release Distribution J. Schulz
- Post-Accident Radiation  
Source Descriptions D. Dexheimer
- Post-Accident Sample  
Station Shielding from  
Containment Source D. Dexheimer
- Fuel Transfer Canal  
Upriser Pit Shielding D. Dexheimer



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## ***AP600 POST-ACCIDENT SOURCES***

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- **CORE / CONTAINMENT INVENTORIES**
  - METHODS
  - ASSUMPTIONS
- **COMPARISON OF SOURCE TERM BASES**
  - TID
  - EPRI
  - NUREG
- **DOSE RATES INSIDE CONTAINMENT**
  - TID VERSUS EPRI SOURCES



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## POST-ACCIDENT SOURCE BASES

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- EXPECTED CASE
  - MINIMAL CORE DAMAGE
- DESIGN BASIS FOR ACCIDENT DOSE ANALYSES
  - TID-14844 — “CALCULATION OF DISTANCE FACTORS FOR POWER AND TEST REACTORS,” MARCH 1962
  - EPRI SOURCE TERM — “PASSIVE ALWR SOURCE TERM,” FEBRUARY 1991
  - NUREG-1465 — “ACCIDENT SOURCE TERMS FOR LIGHT-WATER NUCLEAR POWER PLANTS” (Draft Report For Comment), JUNE 1992

## METHODS

- CORE INVENTORIES BASED ON ORIGEN COMPUTER CODE ANALYSES
- ORNL-4628, "ORIGEN - THE ORNL ISOTOPE GENERATION AND DEPLETION CODE," MAY 1973
  - MATRIX EXPONENTIAL METHOD FOR SOLVING COUPLED, LINEAR, FIRST-ORDER ORDINARY DIFFERENTIAL EQUATIONS WITH CONSTANT COEFFICIENTS
  - GENERAL EXPRESSION

$$\frac{dX_i}{dt} = \sum_{j=1}^N l_{ij} \lambda_j X_j + \bar{\phi} \sum_{k=1}^N f_{ik} \sigma_k X_k - (\lambda_i + \bar{\phi} \sigma_i) X_i \quad (i = 1 \dots N)$$

where:

- $X_i$  is the atom density of nuclide  $i$
- $\lambda_i$  is the decay constant for nuclide  $i$
- $\sigma_i$  is the spectrum-averaged neutron absorption cross section of nuclide  $i$
- $l_{ij}$  and  $f_{ik}$  are the fractions of radioactive disintegration and neutron absorption by other nuclides which lead to the formation of species  $i$
- $\bar{\phi}$  is the average neutron flux
- $N$  is the number of nuclides





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## EPRI SOURCE TERMS - RELEASE SCENARIO

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|              |   |
|--------------|---|
| 0 - 1 HOUR   | NO FUEL DAMAGE OR<br>RELEASE OF CORE<br>ACTIVITY  |
| 1 - 5 HOURS  | <u>EARLY IN-VESSEL RELEASE</u><br><br>75% CORE MELT WITH<br>RELEASE OF 80% OF<br>NOBLE GASES, 38% OF<br>IODINES, 30% OF CESIUMS,<br>AND 8% OF TELLURIUM |
| 5 HOURS      | VESSEL FAILURE ASSUMED TO<br>OCCUR  |
| 5 - 24 HOURS | <u>LATE IN-VESSEL RELEASE</u><br><br>RELEASE OF 20% OF<br>NOBLE GASES, 17% OF<br>IODINES, 18% OF CESIUMS,<br>AND 3% OF TELLURIUM                        |
| 24 HOURS     | NO ADDITIONAL RELEASES  |



## TIMING OF EPRI AND NUREG-1465 RELEASES

|                | Gap Release |       | Early In-Vessel |       | Ex-Vessel |       | Late In-Vessel |       |
|----------------|-------------|-------|-----------------|-------|-----------|-------|----------------|-------|
|                | EPRI        | NUREG | EPRI            | NUREG | EPRI      | NUREG | EPRI           | NUREG |
| Duration (Hrs) | 0.5         |       | 1-5             | 1.3   |           | 2     | 5-24           | 10    |
| Noble Gas      | 0.05        |       | 0.8             | 0.95  |           | 0.0   | 0.2            | 0.0   |
| Iodine         | 0.05        |       | 0.38            | 0.35  |           | 0.29  | 0.17           | 0.07  |
| Cesium         | 0.05        |       | 0.3             | 0.25  |           | 0.39  | 0.18           | 0.06  |
| Tellurium      |             |       | 0.08            | 0.15  |           | 0.29  | 0.03           | 0.025 |
| Strontium      |             |       | 0.004           | 0.03  |           | 0.12  | -              | -     |
| Barium         |             |       | 0.004           | 0.04  |           | 0.10  | -              | -     |
| Ruthenium      |             |       | 0.004           | 0.008 |           | 0.004 | -              | -     |
| Cerium         |             |       | 0.004           | 0.01  |           | 0.02  | -              | -     |
| Lanthanum      |             |       | 0.004           | 0.002 |           | 0.015 | -              | -     |



## CORE RELEASES INTO CONTAINMENT

|                                     | TID-14844 | EPRI     | NRC Proposed      |           |
|-------------------------------------|-----------|----------|-------------------|-----------|
|                                     |           |          | NUREG             | 2/92 Memo |
| Duration                            | 0         | 1-24 hrs | ≥ 10 sec-13.3 hrs |           |
| Fraction of Core Inventory Released |           |          |                   |           |
| Noble Gas                           | 1.0       | 1.0      | 1.0               | 1.0       |
| Iodine                              | 0.5*      | 0.55     | 0.76 (0.5)**      | 0.40      |
| Others                              | 0.01      |          |                   |           |
| Cesium                              |           | 0.48     | 0.75 (0.4)        | 0.30      |
| Tellurium                           |           | 0.11     | 0.46 (0.2)        | 0.15      |
| Strontium                           |           | 0.004    | 0.15 (0.042)      | 0.03      |
| Barium                              |           | 0.004    | 0.14 (0.05)       | 0.04      |
| Ruthenium                           |           | 0.004    | 0.012 (0.0084)    | 0.008     |
| Cerium                              |           | 0.004    | 0.03 (0.012)      | 0.01      |
| Lanthanum                           |           | 0.004    | 0.017 (0.0035)    | 0.002     |

\* - INSTANTANEOUS PLATEOUT REDUCES THE FRACTION RELEASED FROM CONTAINMENT TO 0.25 (Reg. Guide 1.4)

\*\* - ( ) WITH DF OF 10 FROM POOL SCRUBBING ASSUMING 10 FT OF WATER OVER THE MOLTEN CORE ( NUREG-1465, Section 5.4)

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## CHEMICAL FORM OF IODINE

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- TID (REG. GUIDE 1.4) FOR AIRBORNE IODINE  
(25% OF TOTAL CORE INVENTORY)

ELEMENTAL - 91 %

ORGANIC - 4 %

PARTICULATE - 5 %

- EPRI

ELEMENTAL - 2.85 %

ORGANIC - 0.15 %

PARTICULATE - 97 %

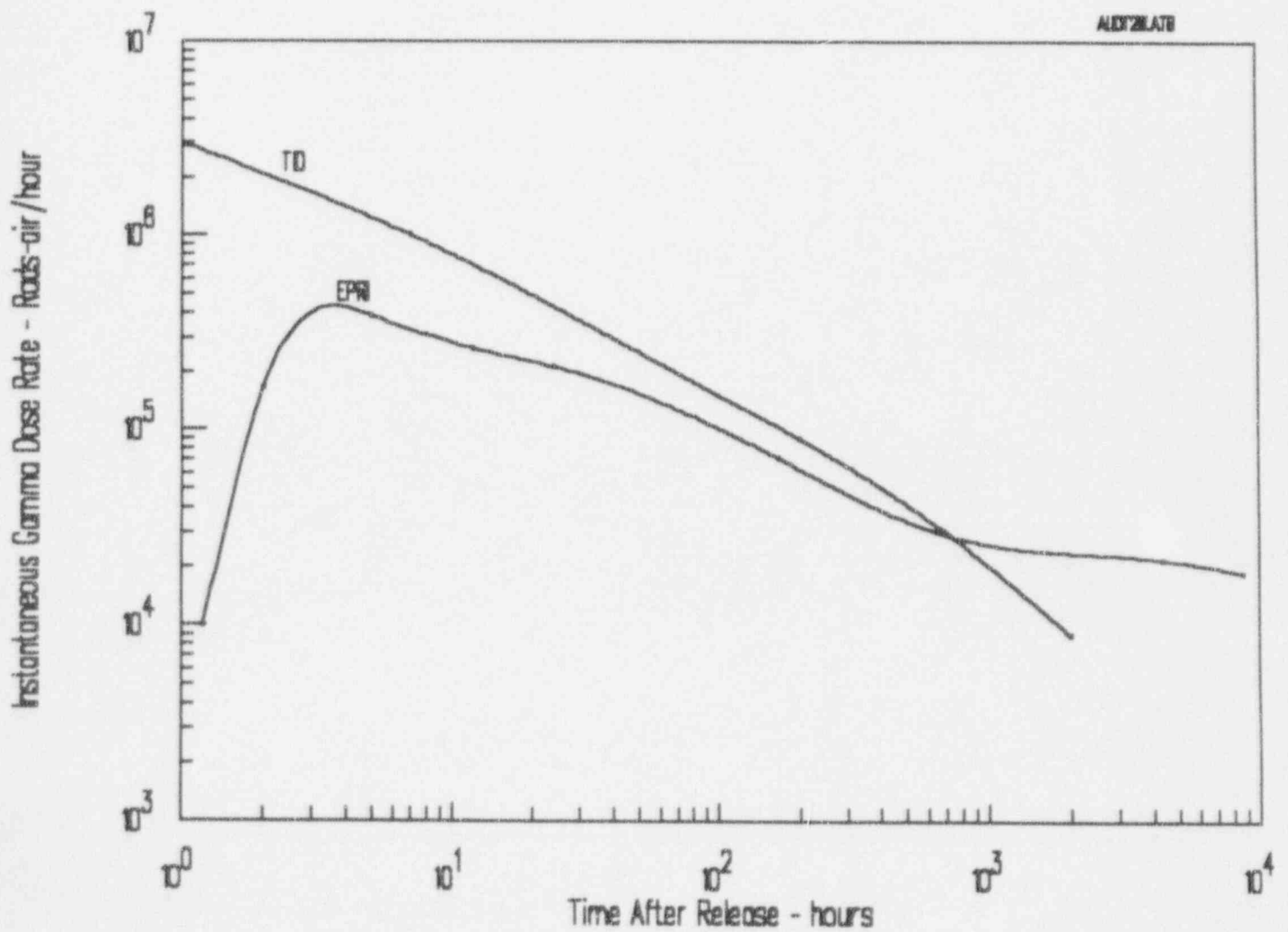
- NUREG

VOLATILE - 5 %

PARTICULATE - 95 %

- VOLATILE FRACTION ASSUMED TO BE 4.75%  
INORGANIC AND 0.25% ORGANIC PER DRAFT  
COMMISSION PAPER DATED FEBRUARY 1992

# CONTAINMENT DOSE RATE





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## REVISED SOURCE TERMS

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- LEVEL OF REALISM IS INCREASED OVER TID ASSUMPTIONS WITH RESPECT TO
  - TIMING
  - MAGNITUDE OF RELEASES
  - FORM OF IODINE
- DESIGN BASIS ACCIDENT RELEASES STILL CONSERVATIVE RELATIVE TO EXPECTED ACCIDENT RELEASES



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## ***OUTSIDE CONTAINMENT RELEASE DISTRIBUTION***

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- **POST-LOCA ACTIVITY DISTRIBUTION IN BUILDINGS**
  
- **POST-LOCA GAMMA EMISSION RATES**



## POST-LOCA ACTIVITY DISTRIBUTION BASES:

- **Thermal Power Level - 1972 MWT**  
(Ref: AP600 Radiation Analysis Design Manual Section 5.2.1)
- **The emission rates E in Mev/watt-sec for the equilibrium core for 6 isotope groups**  
(Ref: AP600 Radiation Analysis Design Manual Tables 5-5 to 5-10. Data for 64 hrs, 72 hrs, & 100 hrs are supplied by Westinghouse.)
- **Fraction of Core Fission Product Inventory Released to Containment by Isotope Group**

| <u>Isotope Group</u> | <u>0 - 1 hr</u> | <u>1 - 5 hrs</u> | <u>5 - 24 hrs</u> |
|----------------------|-----------------|------------------|-------------------|
| Noble Gases          | 0.0             | 2.0E-1/hr        | 1.05E-2/hr        |
| Iodines              | 0.0             | 9.5E-2/hr        | 8.95E-3/hr        |
| Cesium               | 0.0             | 7.5E-2/hr        | 9.47E-3/hr        |
| Tellurium            | 0.0             | 2.0E-2/hr        | 1.58E-3/hr        |
| Sr, Ba ,Ru           | 0.0             | 1.0E-3/hr        | 0.0               |
| Remaining Isotopes   | 0.0             | 1.0E-5/hr        | 0.0               |

(Ref: AP600 Radiation Analysis Design Manual Section 5.2)





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## POST-LOCA ACTIVITY DISTR BASES (CONT'D):

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- Assume no leakage from Auxiliary and Annex Buildings to outside air

- **Building Free Air Volumes in cubic feet:**

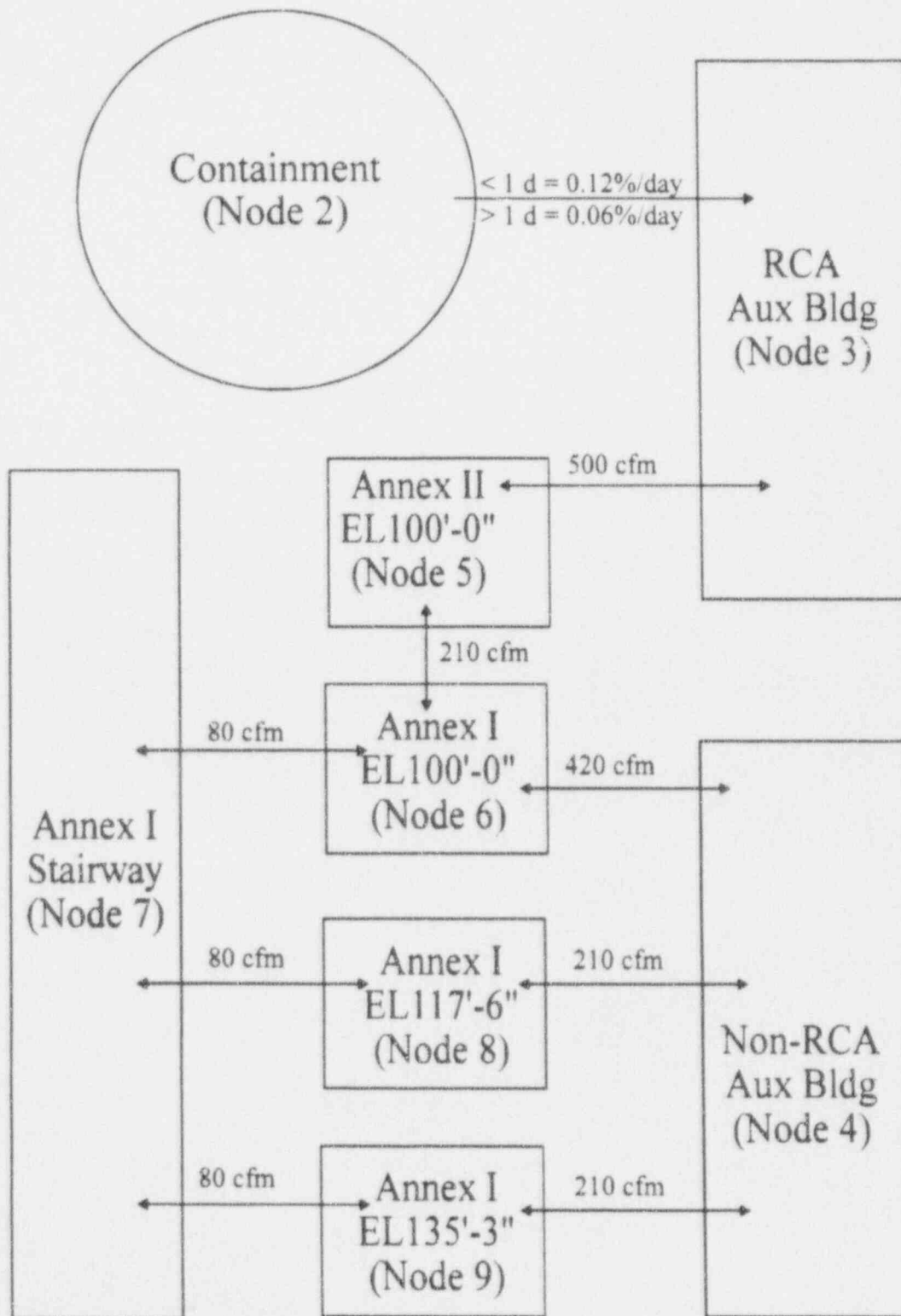
|                            |             |           |
|----------------------------|-------------|-----------|
| Containment                |             | 1,830,000 |
| RCA Auxiliary Building     |             | 616,500   |
| Non-RCA Auxiliary Building |             | 401,000   |
| Annex II Bldg              | Elev 100'0" | 101,500   |
| Annex I Bldg               | Elev 100'0" | 103,000   |
|                            | Elev 117'6" | 128,000   |
|                            | Elev 135'3" | 105,000   |
|                            | Stairwell   | 6,970     |







## LOCADOSE Model for Post Accident Activity Distribution



## POST-LOCA ACTIVITY DISTRIBUTION:

- Use LOCADOSE NE319 Release 3 to generate time dependent activity distribution fractions in each node for each isotope group with an initial unit activity.

Figure above presents a schematic diagram of the LOCADOSE Model used.

- Determine the total Post-Accident gamma emission rates  $E_{Tjk}$  in Mev/watt-sec by energy group as a function of time in each node.

$$E_{Tjk}(t) = \sum_{i=1}^6 f_{ik}(t) \times E_{ij}(t)$$

where:  $f_{ik}(t)$  = fraction of the activity of isotope group  $i$  in node  $k$  from the LOCADOSE runs at time  $t$

$E_{ij}(t)$  = gamma energy emission rate for isotope group  $i$  in energy group  $j$  from AP600 Radiation Analysis Manual Tables 5-5 to 5-10 at time  $t$

- Determine  $C_2$  multiplication factors (watt/cc) to convert total emission rates  $E_{Tjk}$  to volumetric gamma sources in Mev/cc-sec.

For all nodes except the environmental cloud:

$$C_2 = \frac{1972(\text{MW}) \times 10^6 (\text{W/MW})}{\text{Volume}_{\text{node}} (\text{ft}^3) \times 2,831.74 (\text{cc} / \text{ft}^3)}$$

## POST-LOCA ACTIVITY DISTRIBUTION (CONT'D):

- For the environmental cloud:

$$C_2 = \frac{\lambda_L(t) (1/\text{day}) \times 1972(\text{MW}) \times \chi/Q(t) (\text{sec}/\text{m}^3)}{24 \times 3600}$$

where:  $\lambda_L(t)$  = containment leakage rate at time t

\* $\chi/Q(t)$  = atmospheric dispersion factors at time t for the control room (shown below) are used

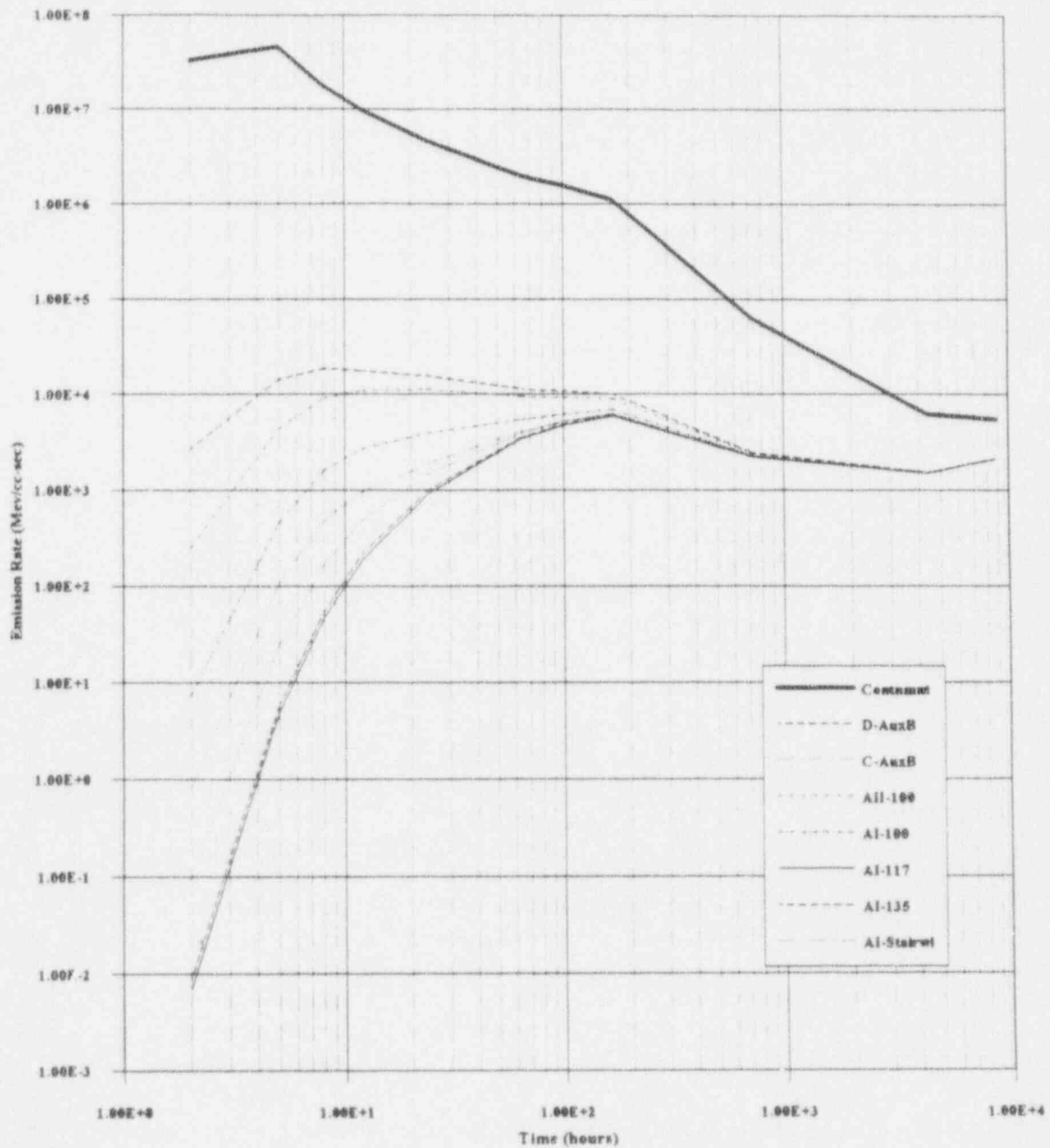
|              |                       |
|--------------|-----------------------|
| 0 - 2 hrs    | $2.18 \times 10^{-3}$ |
| 2 - 8 hrs    | $1.50 \times 10^{-3}$ |
| 8 - 24 hrs   | $1.30 \times 10^{-3}$ |
| 24 - 96 hrs  | $8.40 \times 10^{-4}$ |
| 96 - 720 hrs | $4.80 \times 10^{-4}$ |

\* Ref: AP600 Calc GW N1C 001 Rev A

The  $C_2$  factor is then applied to  $E_{Tjk}$  in Mev/watt-sec for the containment to get  $E_{Tjk}$  in Mev/cc-sec for the environmental cloud.



# POST-LOCA GAMMA EMISSION RATES



## ***AP600***

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- **Post-Accident Radiation Source Descriptions**



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## POST-ACCIDENT RADIATION SOURCES ON AGENDA

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- Unshielded Containment Cloud (UCC)
- Shielded Containment Cloud (SCC)
- Radiologically Controlled Areas of Auxiliary Building (RAC)
- Post-Accident Sample Piping (PAS)



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## UNSHIELDED CONTAINMENT CLOUD (UCC) GEOMETRY

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- Airborne sources uniformly distributed in containment air volume
- UCC for dose point locations inside containment
- Containment Cloud Geometry
  - Cylindrical cloud (IR = 65'-0")  
(BOT = 107'-2")  
(TOP = 256'-4")
  - Spaces below 107'-2" embedded in concrete slab
- Containment Internal Shield Geometry
  - Internal wall shielding - SG, refueling water storage tank and reactor cavity walls from El. 107'-2" to 135'-3"
  - Internal slab shielding - operating floor El. 135'-3"
- Dose Point Location
  - Containment dose point taken at middle of upper containment free volume El. 195'-9"

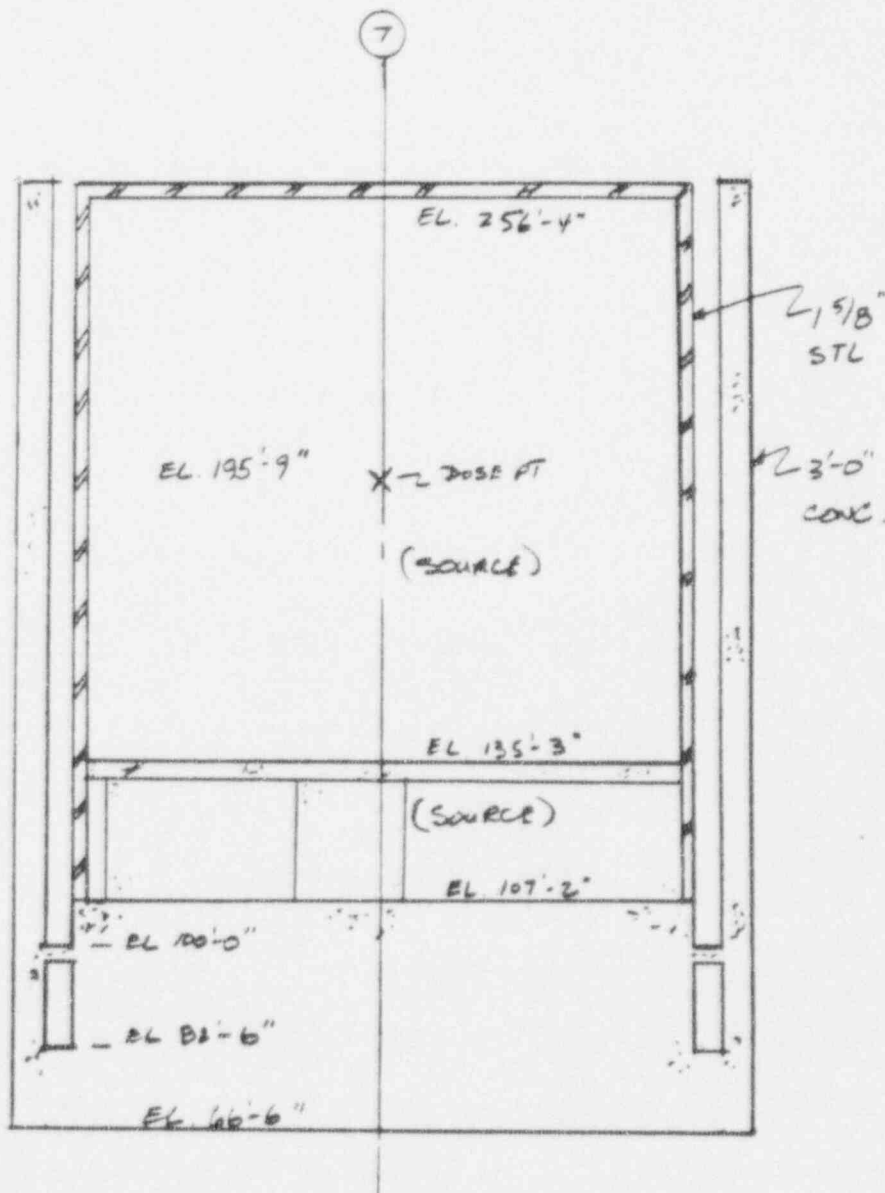
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## SHIELDED CONTAINMENT CLOUD (SCC) GEOMETRY

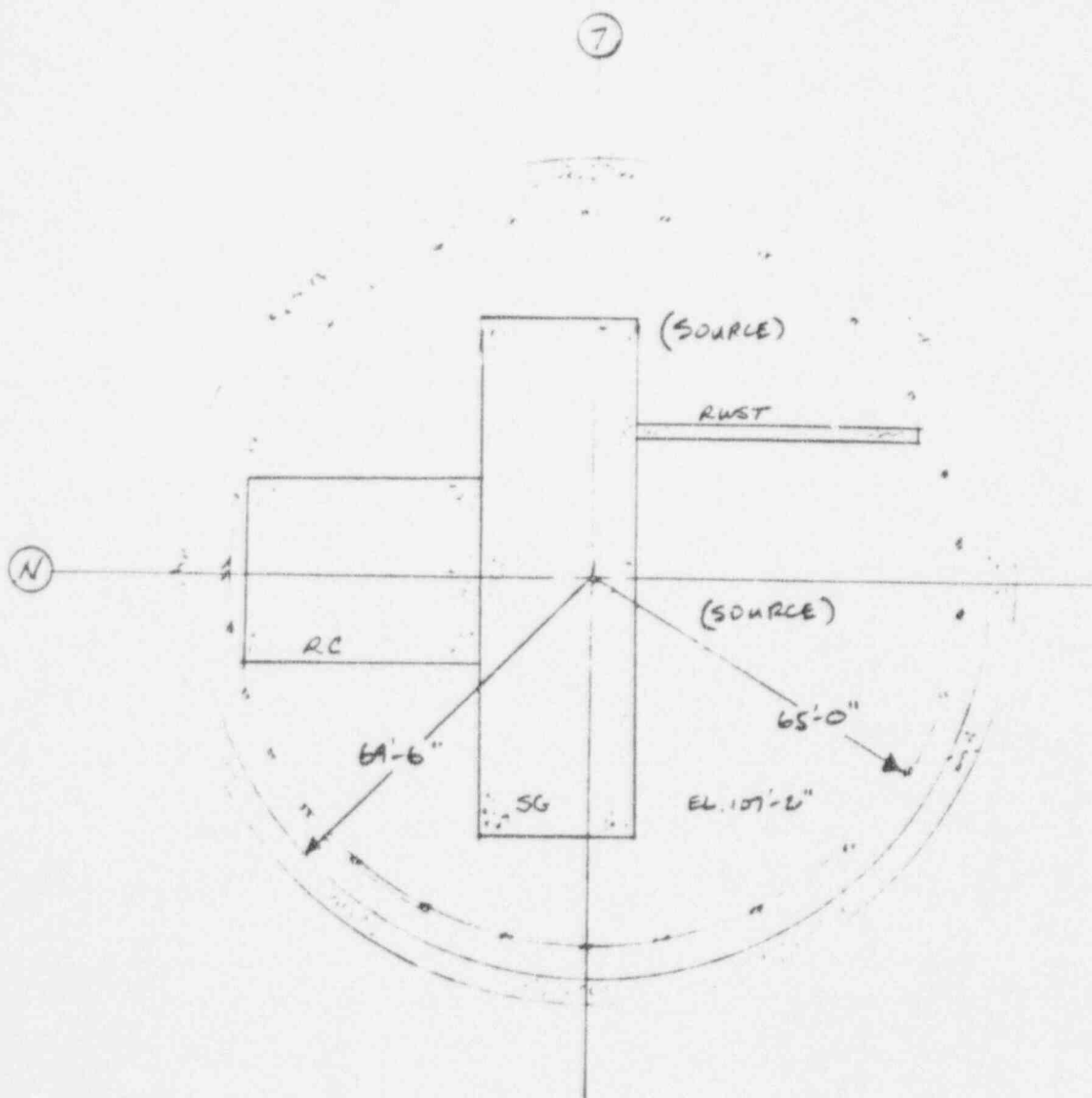
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- For dose point locations outside containment and not adjacent to containment penetrations
- Containment Cloud Geometry - same as UCC
- Containment External Shield Geometry
  - 1-5/8" containment steel liner (IR = 65'-0")
  - 3'-0" containment shield wall (IR = 69'-6")
- Dose Point Location
  - External dose point taken at their elevation and plant building or yard location

# CONTAINMENT CLOUD (SCC & UCC) SECTION



# CONTAINMENT CLOUD (SCC & UCC) PLAN AT 107'-2"



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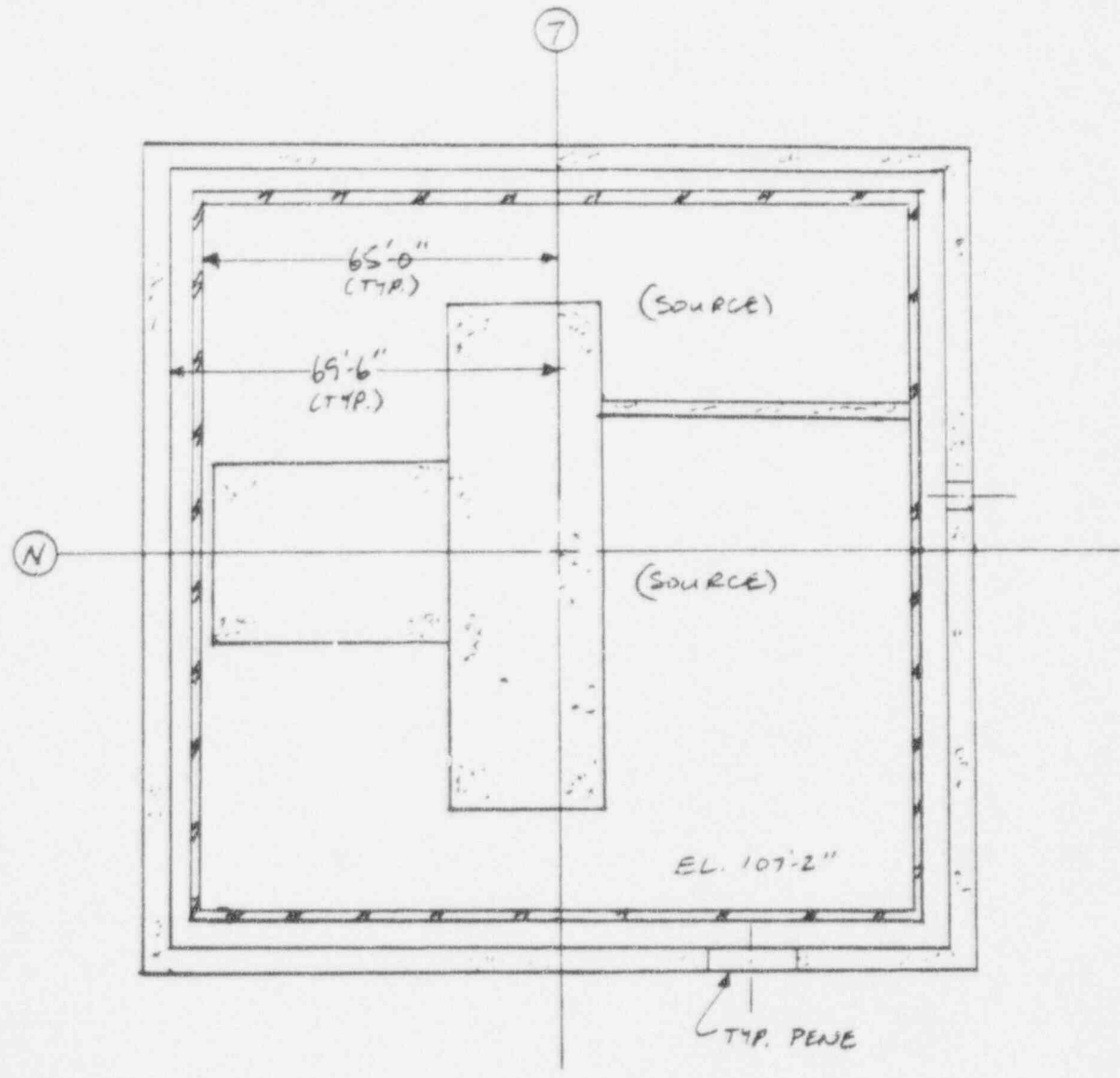
## CONTAINMENT PENETRATION STREAMING (CPS) GEOMETRY

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- For dose point locations outside containment and near to containment penetrations
- Containment Cloud Geometry - similar to UCC but using rectangular box versus cylinder
- Containment External Shield Geometry
  - 1-5/8" containment steel liner (Width=130'-0")
  - 3'-0" containment shield wall (Inner Width = 139'-0")
- Shield Building Penetration Geometry
  - Shield building penetrations (hatches, doors, etc.) to external areas modeled as air filled bodies



# CONTAINMENT CLOUD (SCC & CPS) PLAN AT 107'-2"



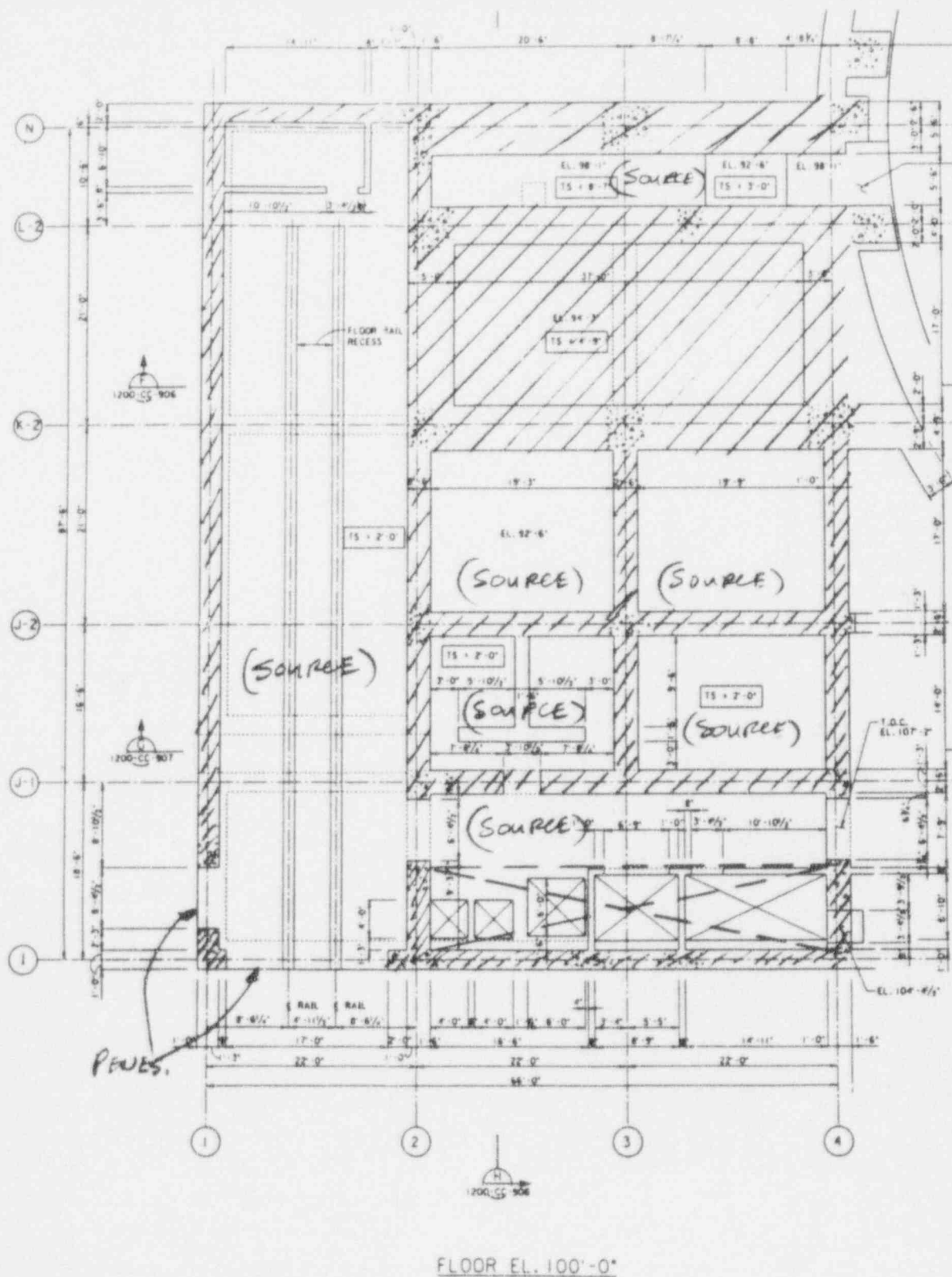
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## **Radiologically Controlled Areas of Auxiliary Building (RAC)**

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- **Building Cloud Sources**
  - Airborne sources uniformly distributed in the entire air volumes for auxiliary buildings and each air volume for Annex building HVAC regions
  - Location of building cloud boundaries shown on SAR Figures for Post-Accident Zoning
  - Room size clouds used for access areas and routes. (Internal building structural walls and slabs around vital access areas included in model)
  
- **Dose Point Locations**
  - Representative room dose rates at center at 3' from floor
  
- **Cumulative Dose Rates**
  - Building dose rates summed where appropriate with penetrations contributions from adjacent buildings (e.g. containment penetrations to auxiliary and annex buildings)
  - Peak dose rates at any Post-Accident time are then used to determine Zoning for each area.
  
- **Auxiliary Building Modeled as Air Filled Box with Internal Concrete Walls and Slabs**
  - Floor and wall openings modeled as air filled bodies

# TYPICAL RAC SOURCE-SHIELD GEOMETRY



LEGEND:

A. POST-ACCIDENT RADIATION ZONES:

| DESIGNATION | MAXIMUM DESIGN DOSE RATE | DESCRIPTION                       |
|-------------|--------------------------|-----------------------------------|
| 0           | $\leq 0.05$ mRem/hr      | NO RADIATION SOURCES              |
| I           | $\leq 0.25$ mRem/hr      | VERY LOW OR NO RADIATION SOURCES  |
| II          | $\leq 2.5$ mRem/hr       | LOW RADIATION SOURCES             |
| III         | $\leq 15.0$ mRem/hr      | LOW-TO-MODERATE RADIATION SOURCES |
| IV          | $\leq 100$ mRem/hr       | MODERATE RADIATION SOURCES        |
| V           | $\leq 1$ Rem/hr          | HIGH RADIATION SOURCES            |
| VI          | $\leq 10$ Rem/hr         | SAME AS ZONE V ABOVE              |
| VII         | $\leq 100$ Rem/hr        | SAME AS ZONE V ABOVE              |
| VIII        | $\leq 500$ Rad/hr        | SAME AS ZONE V ABOVE              |
| IX          | $> 500$ Rad/hr           | VERY HIGH RADIATION SOURCES       |

B. DRAWING SYMBOLS:

|     |  |
|-----|--|
| VI  | RADIATION ZONE NUMERAL AT POST-ACCIDENT PEAK |
| ECS | DOMINANT POST-ACCIDENT RADIATION SOURCE(S)   |

----- - NON-RADIOACTIVE AREA BOUNDARY

————— - RADIOACTIVE AREA BOUNDARY

----- - ANNEX AREA BOUNDARY

----- - RADIATION ZONE BOUNDARY

◇ - POST-ACCIDENT ACCESS ROUTE

C. POST-ACCIDENT SOURCES:

SYMBOL POST-ACCIDENT RADIATION SOURCE

ECS EXTERNAL CLOUD SHINE

NRA NON-RADIOACTIVE AUXILIARY BUILDING AREA CLOUD

RAC RADIOACTIVE AUXILIARY BUILDING AREA CLOUD

SCC SHIELDED CONTAINMENT CLOUD

UCC UNSHIELDED CONTAINMENT CLOUD

CPS CONTAINMENT AND PENETRATION RADIATION STREAMING

AXC ANNEX BUILDING AREA CLOUD

PAS POST-ACCIDENT SAMPLE PIPING

D. GENERAL DRAWING NOTES:

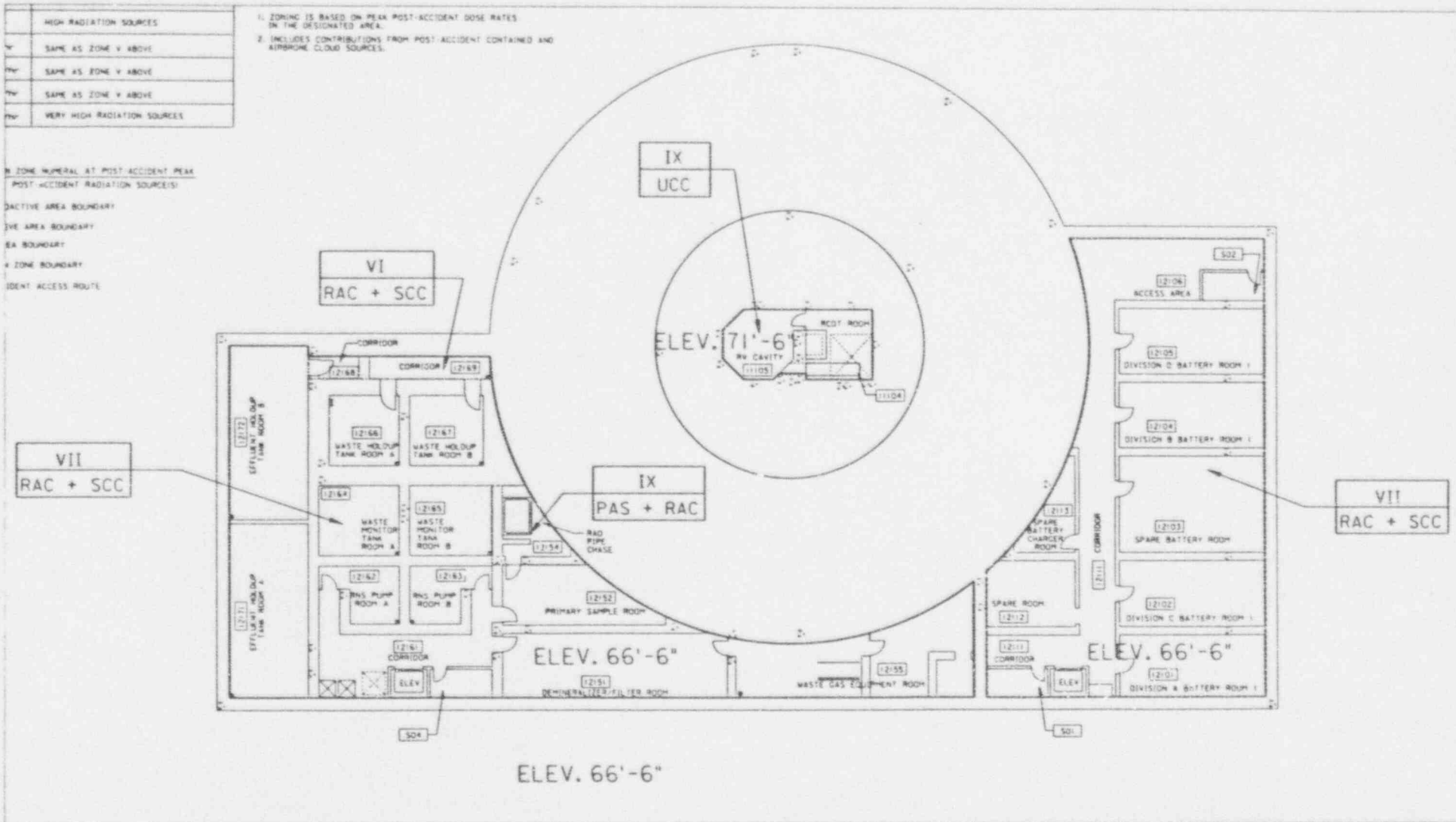
1. ZONING IS BASED ON PEAK POST-ACCIDENT DOSE RATES IN THE DESIGNATED AREA.
2. INCLUDES CONTRIBUTIONS FROM POST-ACCIDENT CONTAINED AND AIRBORNE CLOUD SOURCES.

|     |                             |
|-----|-----------------------------|
| III | HIGH RADIATION SOURCES      |
| IV  | SAME AS ZONE V ABOVE        |
| V   | SAME AS ZONE V ABOVE        |
| VI  | SAME AS ZONE V ABOVE        |
| VII | VERY HIGH RADIATION SOURCES |

1. ZONING IS BASED ON PEAK POST-ACCIDENT DOSE RATES IN THE DESIGNATED AREA.
2. INCLUDES CONTRIBUTIONS FROM POST-ACCIDENT CONTAINED AND AIRBORNE CLOUD SOURCES.

III ZONE NUMERAL AT POST-ACCIDENT PEAK POST-ACCIDENT RADIATION SOURCE(S)

DACTIVE AREA BOUNDARY  
 IVE AREA BOUNDARY  
 EA BOUNDARY  
 + ZONE BOUNDARY  
 | IDENT ACCESS ROUTE



|      |                             |
|------|-----------------------------|
| 1/IV | HIGH RADIATION SOURCES      |
| 2/IV | SAME AS ZONE V ABOVE        |
| 3/IV | SAME AS ZONE V ABOVE        |
| 4/IV | SAME AS ZONE V ABOVE        |
| 5/IV | VERY HIGH RADIATION SOURCES |

1. ZONING IS BASED ON PEAK POST-ACCIDENT DOSE RATES IN THE DESIGNATED AREA.
2. INCLUDES CONTRIBUTIONS FROM POST-ACCIDENT CONTAINED AND AIRBORNE CLOUD SOURCES.

ON ZONE NUMERAL AT POST-ACCIDENT PEAK  
AT POST-ACCIDENT RADIATION SOURCE(S)

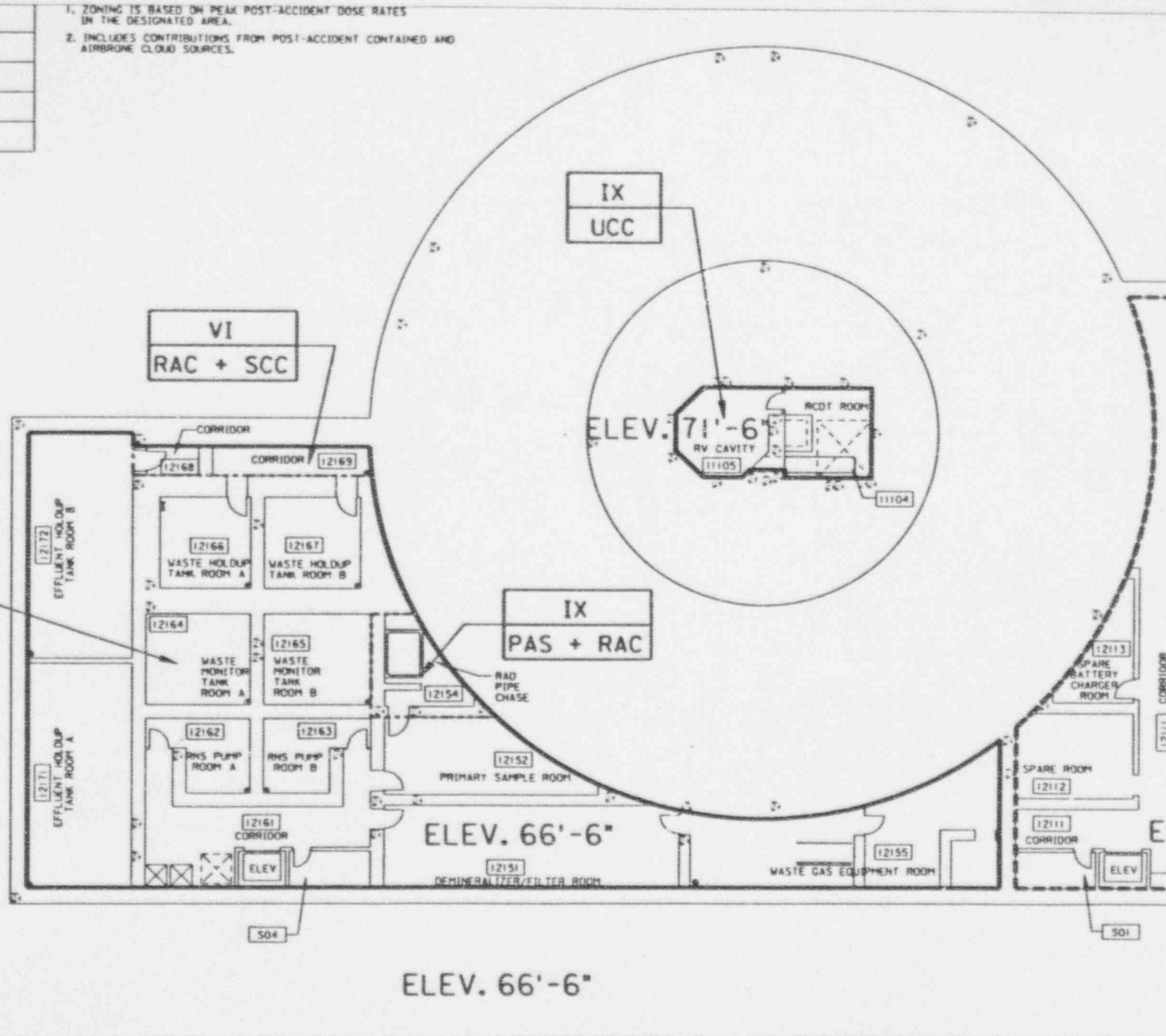
BOACTIVE AREA BOUNDARY

TIVE AREA BOUNDARY

REA BOUNDARY

ON ZONE BOUNDARY

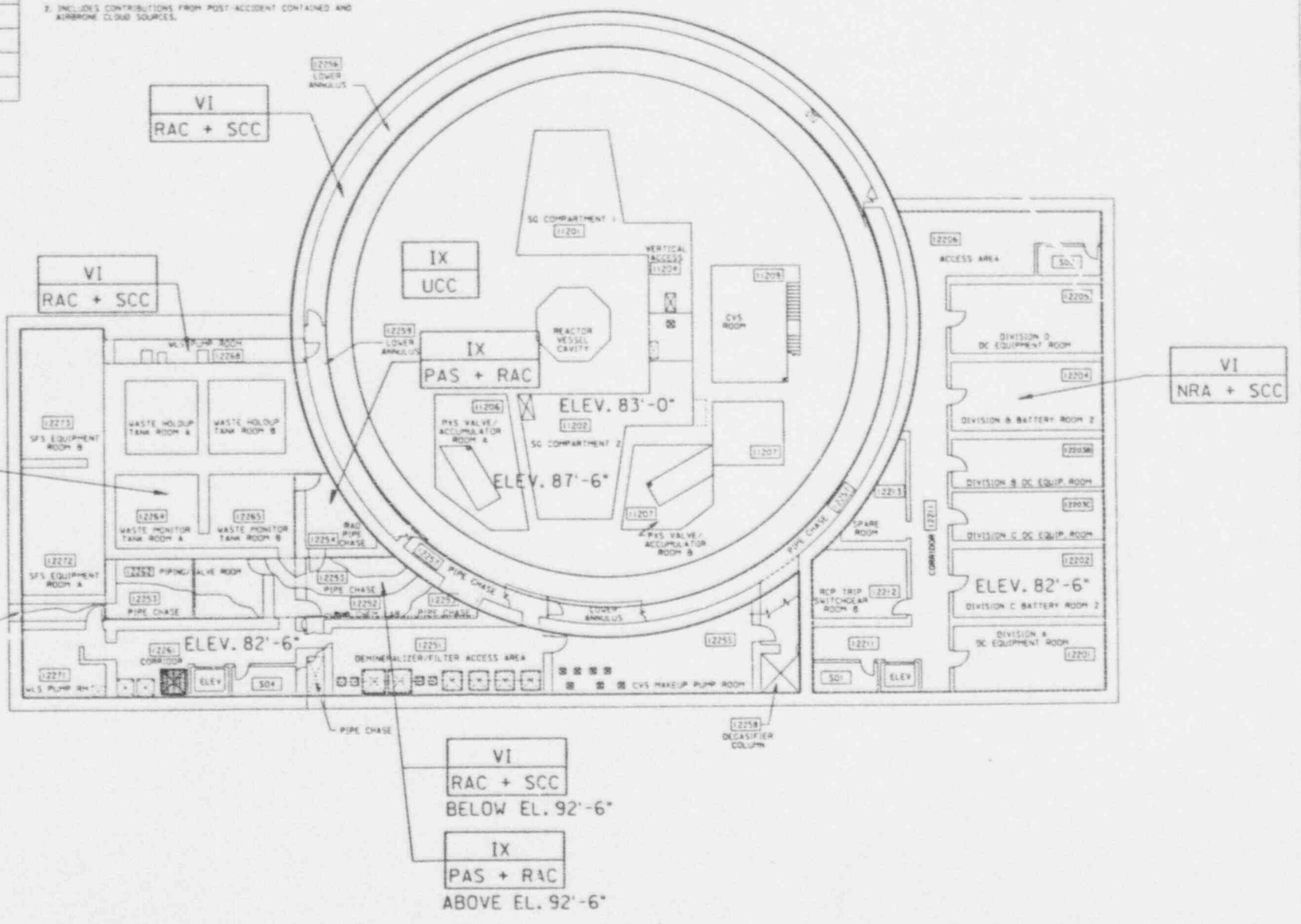
IDENT ACCESS ROUTE



SAME AS ZONE V ABOVE  
 SAME AS ZONE V ABOVE  
 SAME AS ZONE V ABOVE  
 VERY HIGH RADIATION SOURCES

2. INCLUDES CONTRIBUTIONS FROM POST-ACCIDENT CONTAINED AND AIRBORNE CLOUD SOURCES.

NUMERAL AT POST-ACCIDENT NEAR  
 ACCIDENT RADIATION SOURCE(S)  
 AREA BOUNDARY  
 A BOUNDARY  
 NEARY  
 BOUNDARY  
 ACCESS ROUTE



VI  
 RAC + SCC  
 BELOW EL. 92'-6"

IX  
 PAS + RAC  
 ABOVE EL. 92'-6"







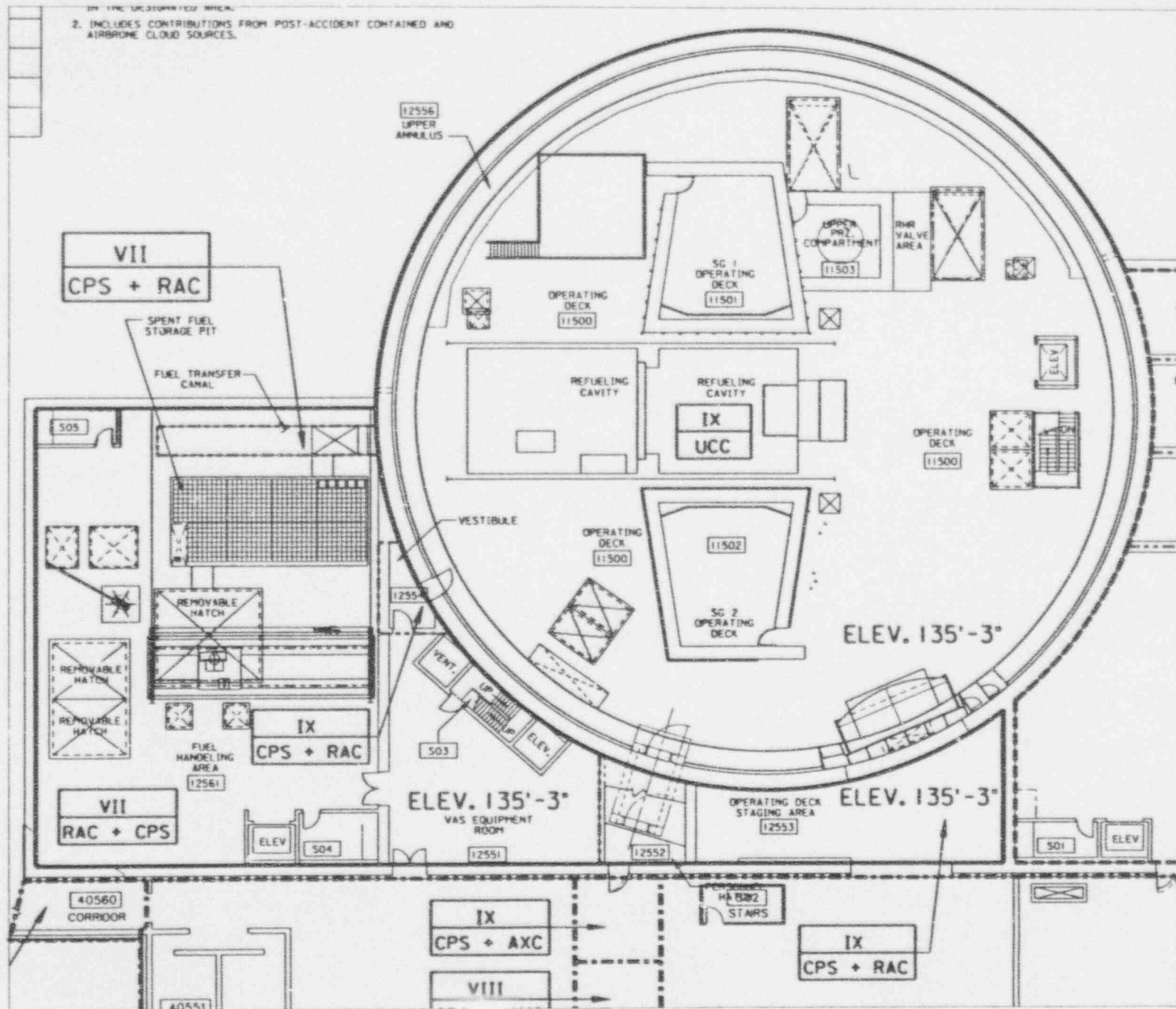








2. INCLUDES CONTRIBUTIONS FROM POST-ACCIDENT CONTAINED AND AIRBORNE CLOUD SOURCES.



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## **PASS PIPING SOURCE DESCRIPTION (PAS)**

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- **Liquid source term based on Post-Accident core release activity distributed uniformly throughout the reactor coolant system volume 7,354 ft<sup>3</sup>**
- **Liquid activity model is same as time dependent release model for containment previously discussed and includes**
  - 100% Noble gases
  - 55% Iodine
  - 48% Cesium
  - 11% Tellurium
  - 0.4% Sr, Ba, Ru
  - 0.004% Others

(Ref: AP600 Radiation Analysis Design Manual Section 5.2 and Tables 5-5 to 5-10)

- **Liquid sample dose rates are not additive to building airborne since same activity source**
- **Containment atmosphere sample activity same as containment airborne activity previously discussed**
- **Sample pipes located in a single Auxiliary Building pipe chase.**
  - 3/8" liquid sample inlet pipe
  - 3/8" containment atmosphere sample inlet pipe
  - 1" sample return pipe



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## ***AP600***

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- **Post-Accident Sample Station Shielding from Containment Source**





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## **CONTAINMENT SHIELDING TO PASS ROOM**

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- **Major Containment Shields**

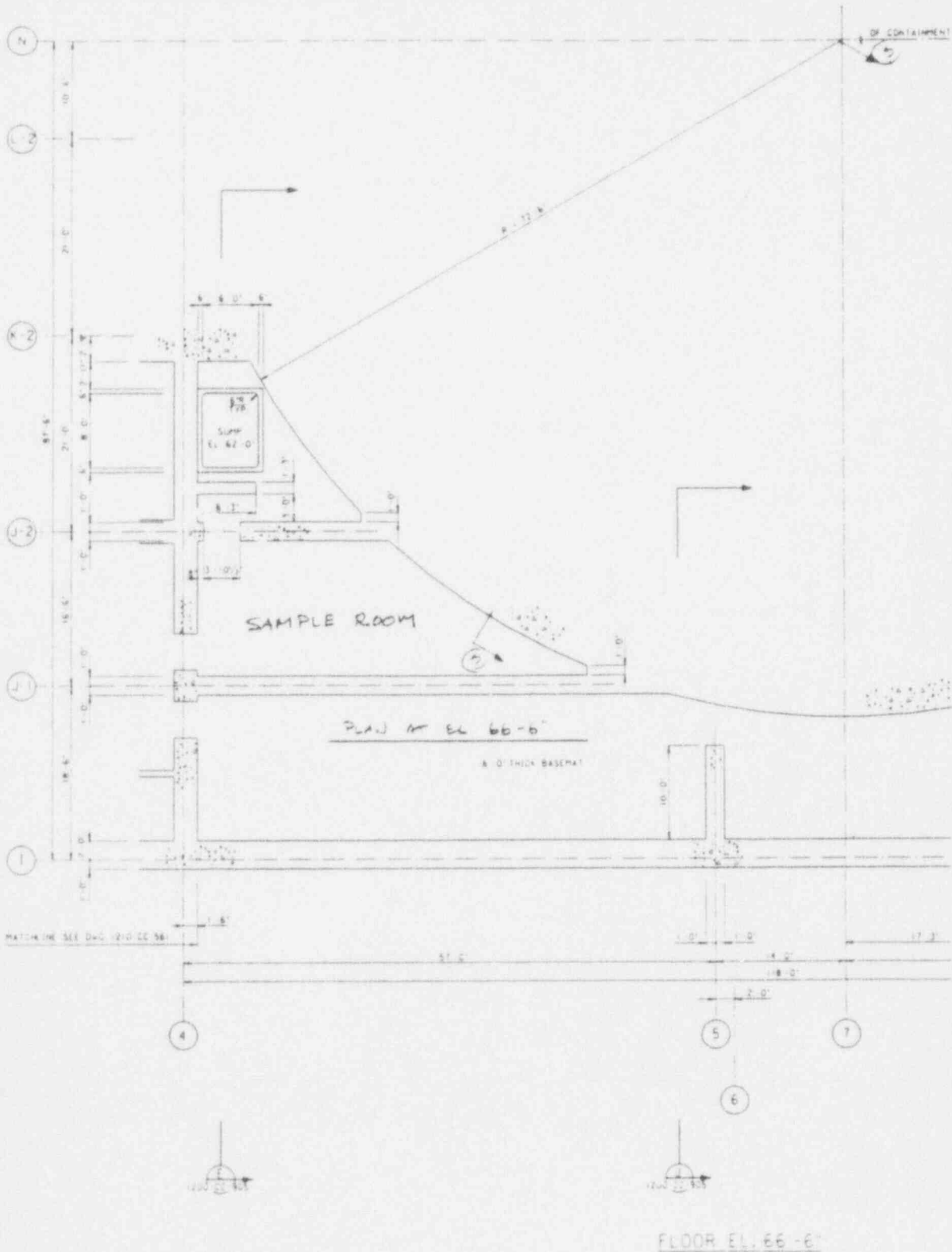
- 1-5/8" containment steel liner (ID = 65'-0")
- 3'-0" containment shield building wall (ID = 69'-6")
- containment concrete fill to El. 107'-2"
- containment shield building concrete fill to El. 82'-6"
- equipment hatch 6" steel door shielding

- **Major Auxiliary Building Shields**

- 2'-0" concrete floor slab El. 107'-2"
- 2'-0" concrete floor slab El. 92'-6"
- 0'-9" concrete floor slab El. 82'-6"



# CONTAINMENT-PASS ROOM SHIELDING-66'-6"

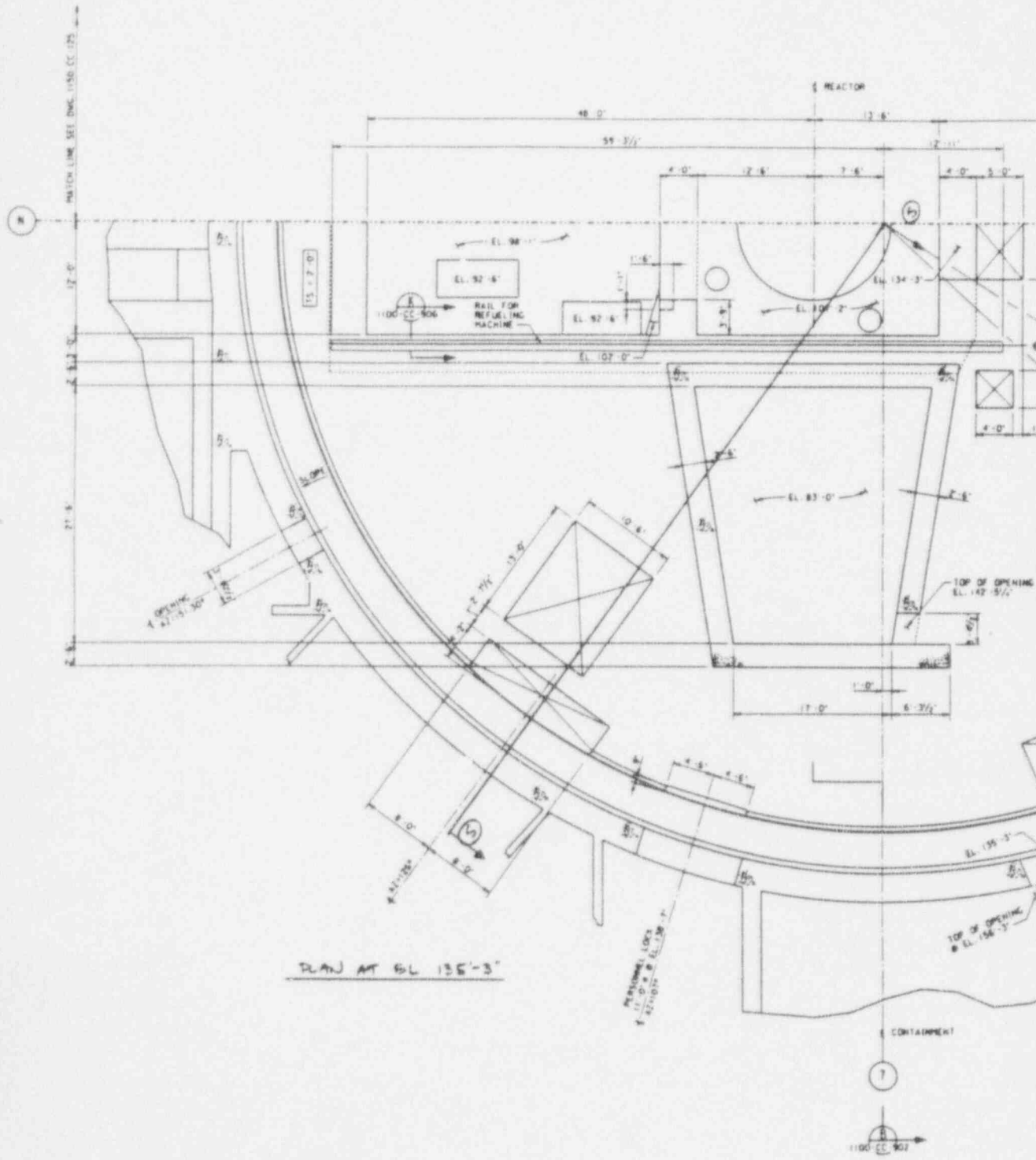








# CONTAINMENT-PASS ROOM SHIELDING-135'-3"



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## **Radiologically Controlled Areas of Auxiliary Building (RAC)**

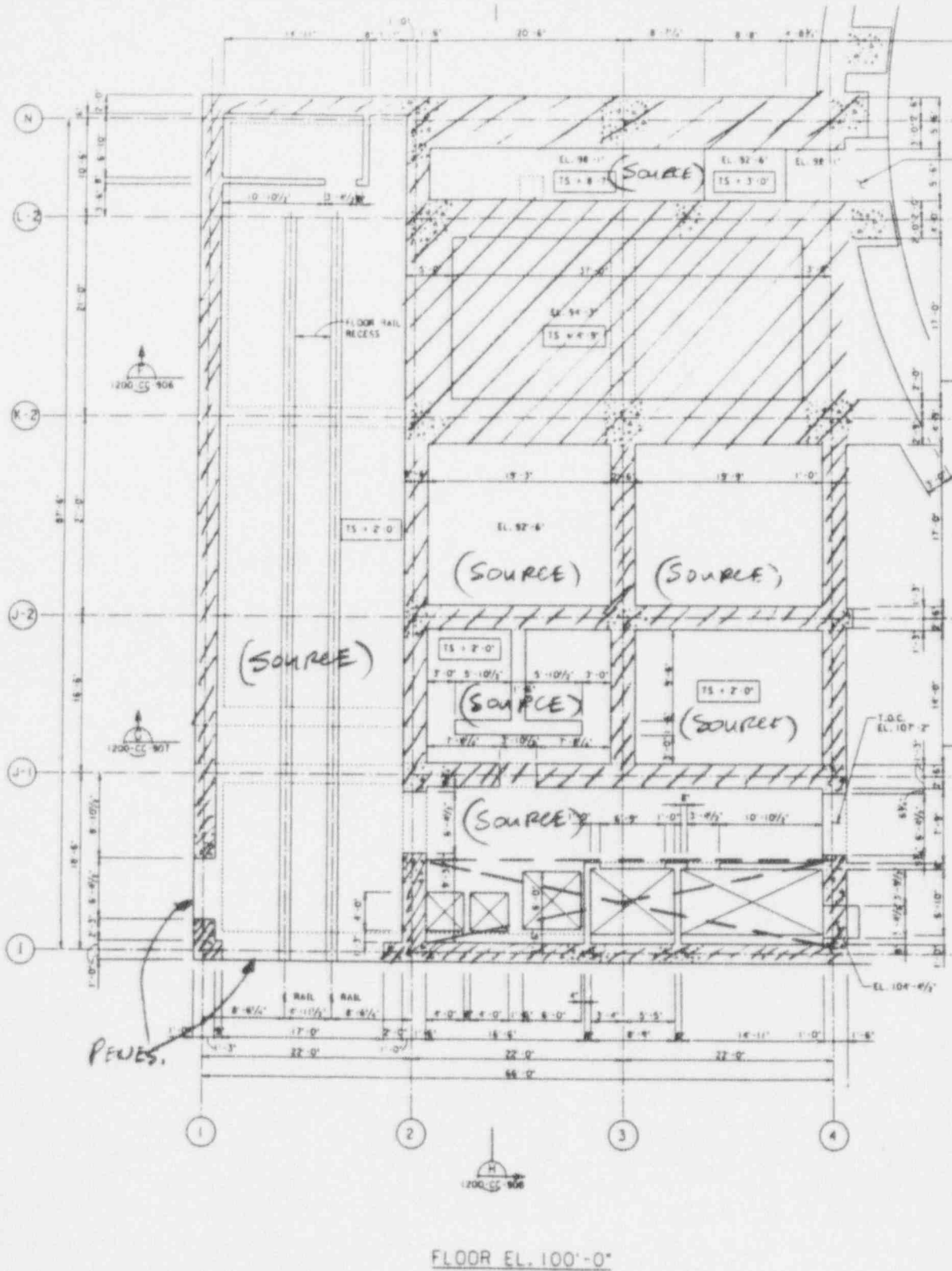
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- **Building Cloud Sources**
  - Airborne sources uniformly distributed in the entire air volumes for auxiliary buildings and each air volume for Annex building HVAC regions
  - Location of building cloud boundaries shown on SAR Figures for Post-Accident Zoning
  - Room size clouds used for access areas and routes. (Internal building structural walls and slabs around vital access areas included in model)
  
- **Dose Point Locations**
  - Representative room dose rates at center at 3' from floor
  
- **Cumulative Dose Rates**
  - Building dose rates summed where appropriate with penetrations contributions from adjacent buildings (e.g. containment penetrations to auxiliary and annex buildings)
  - Peak dose rates at any Post-Accident time are then used to determine Zoning for each area.
  
- **Auxiliary Building Modeled as Air Filled Box with Internal Concrete Walls and Slabs**
  - Floor and wall openings modeled as air filled bodies

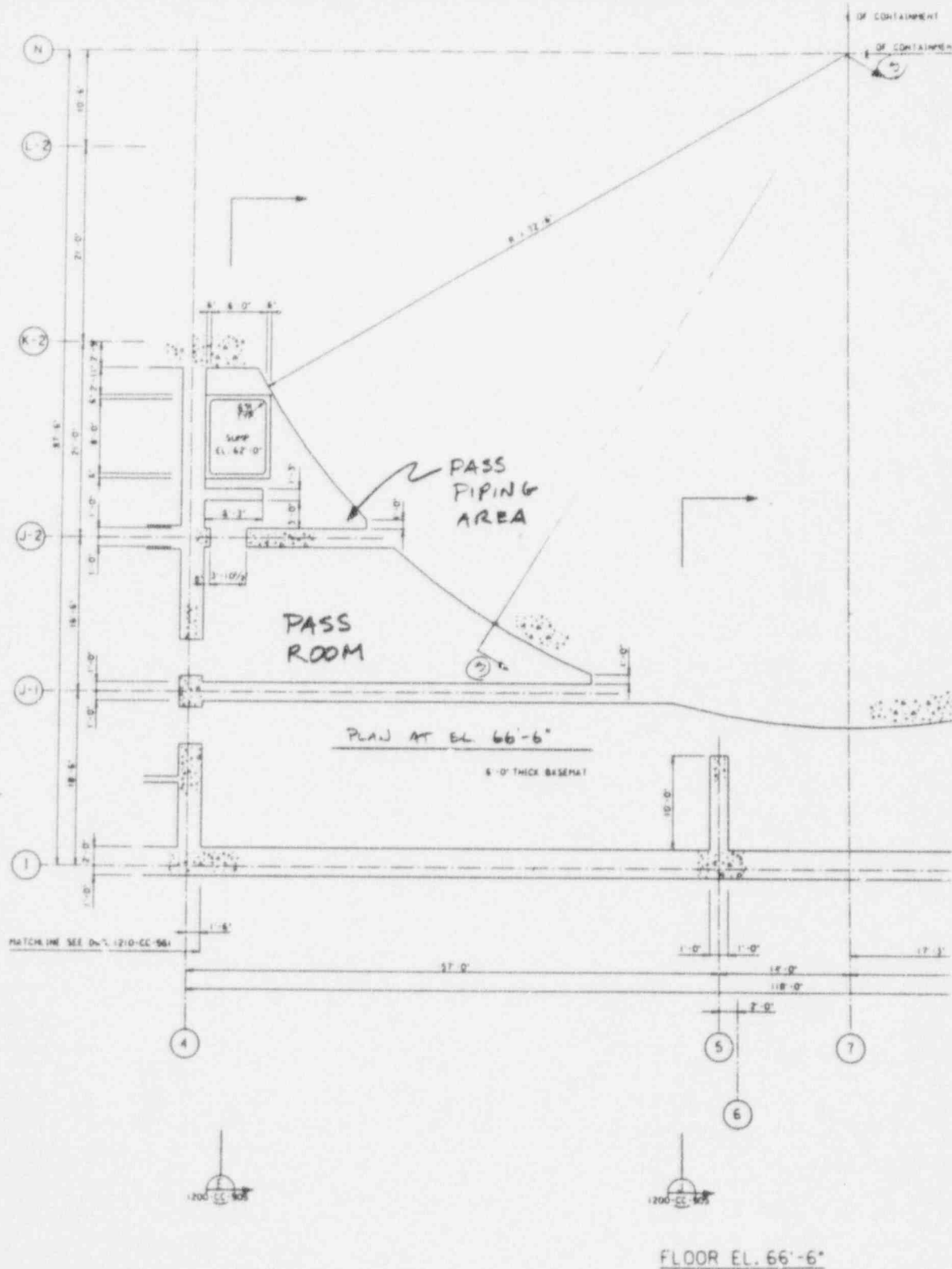




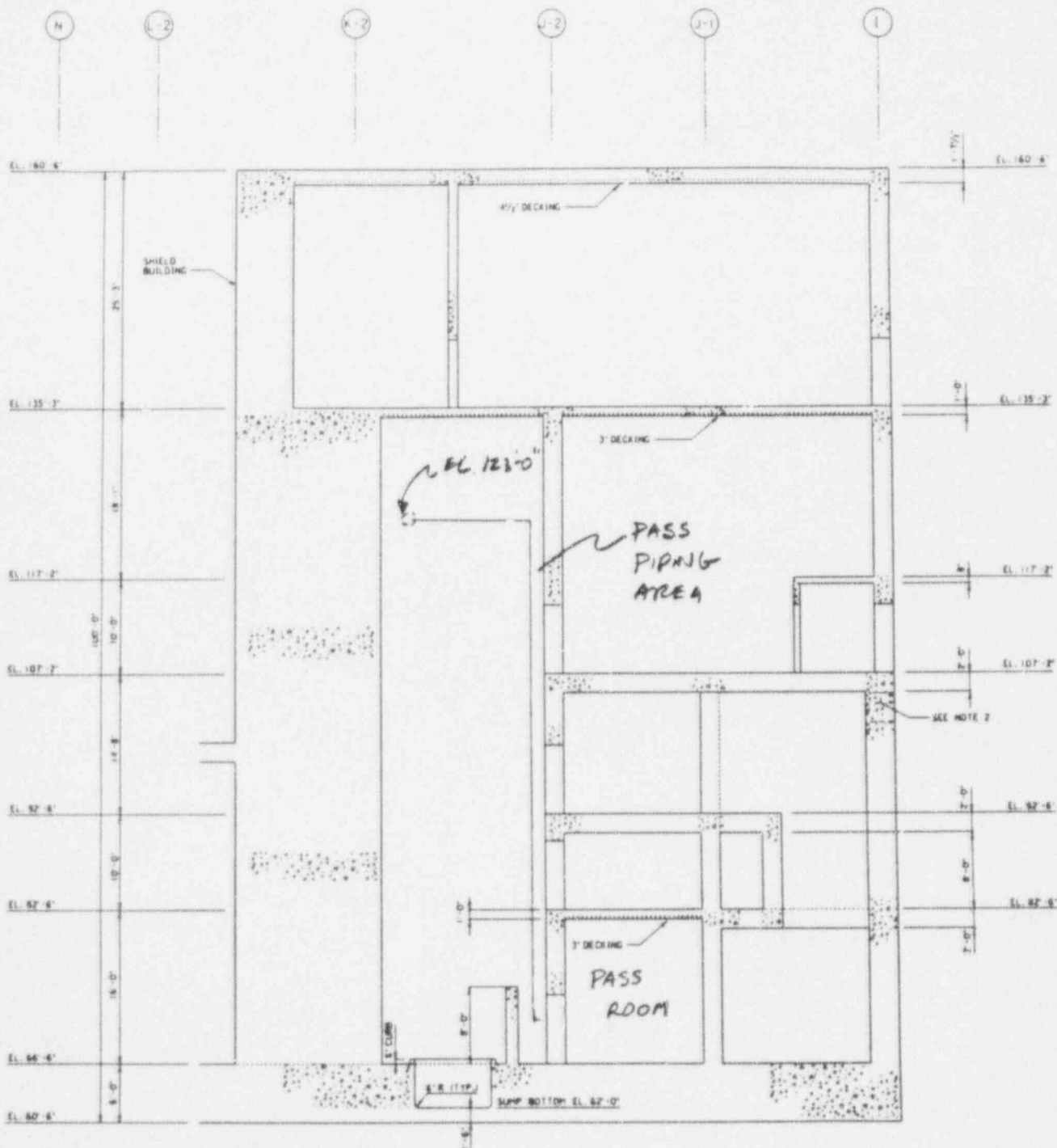
# TYPICAL RAC SOURCE-SHIELD GEOMETRY



# PASS PIPING LOCATION - PLAN 66'-6"



# PASS PIPING LOCATION - PIPEWAY SECTION





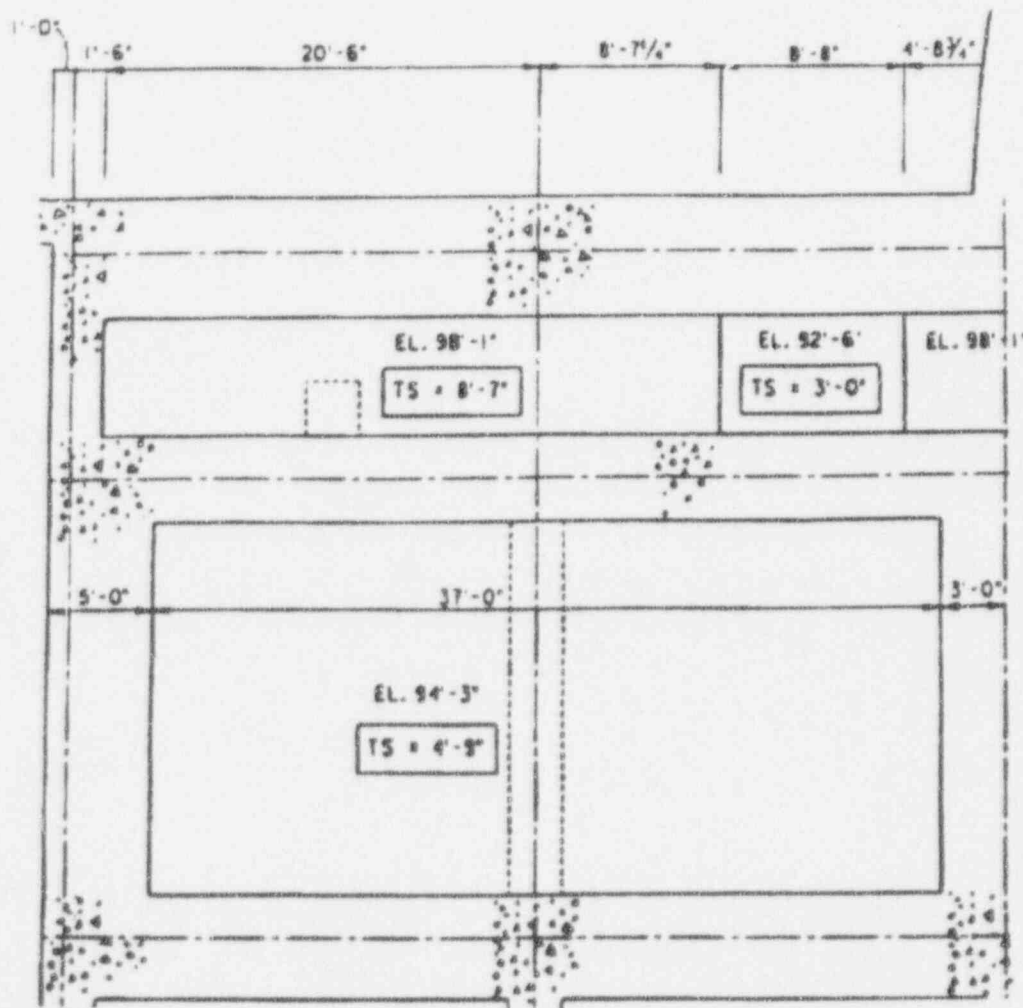
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## *AP600*

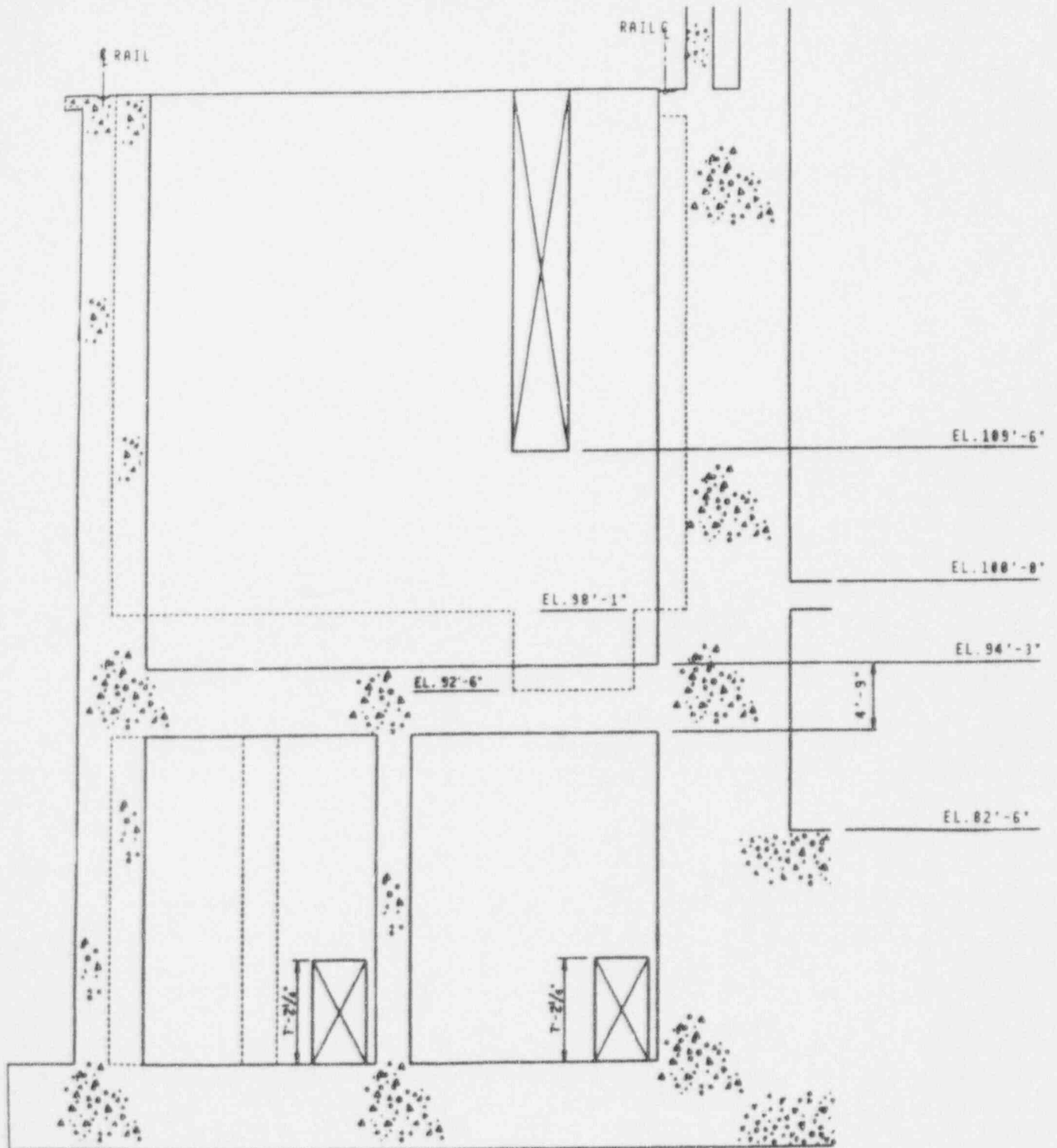
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- Fuel Transfer Canal Upender Shielding

# FUEL UPENDER AREA LAYOUT - PLAN



# FUEL UPENDER AREA LAYOUT - SECTION





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## FUEL UPENDER SHIELDING PROVISIONS

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- **Shielding Provisions For Upender Pit**
  - Concrete slab
    - 8'-7" thick at Elev. 98'-1"
    - 3'-0" below upender pit at Elev. 92'-6"
  - In horizontal fuel position, (fuel carriage Elev. 100'-5 3/4")
    - Water  $\approx$ 7'-4" at 1.0 g/cc
  - In vertical fuel position, active fuel region  $\approx$ 22.9" from top of upender pit slab
    - Fuel plenum 9.7" at 1.8 g/cc
    - Bottom nozzle 3.2" at 2.7 g/cc
    - Water 10" at 1.0 g/cc





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## FUEL UPENDER SHIELDING EVALUATION

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- WLS Pump room at Elev 82'-6" below upender pit is designated Zone V (< 1000 mR/hr) due to normal WLS piping sources
- 3'-0" concrete slab in upender pit reduces spent fuel radiation levels at roof elevation to 90-100 mR/hr with two fuel assemblies in vertical position
- Zoning drawings annotated to indicate WLS pump room has Zone IV (< 100 mR/hr) contribution from spent fuel in vertical position in upender above
- WLS Pump room access control provisions include a barricade (e.g. rope, chain, etc.)