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Common Cause Fault Rates for Valves

Estimates Based on Licensee Event Reports
at U.S. Commercial Nuclear Power Plants, 1976-1980

Prepared by J. A. Steverson, C. L. Atwood

EG&G Idaho, Inc.

Prepared for
U.S. Nuclear Regulatory
Commission

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ABSTRACT

This report presents estimates of common cause fault rates and related quantities, based on Licensee Event Reports for valves in nuclear reactors. The Licensee Event Report data base is described. For estimating rates, the binomial failure rate model is used, extended to allow for the substantial observed plant-to-plant variability, and for shocks that by their nature make all the valves in a system inoperable. Every quantity is estimated by both a point estimate and a 90% interval.

FIN No. A6283--Licensee Event Report Failure Rate Analysis Program

SUMMARY

This report presents estimates of common cause failure rates, fault rates, and related quantities, based on Licensee Event Reports of valves in nuclear reactors.

The data consist of 600 reports describing valve faults from 1976 through 1980. Coding the data is discussed; an event is coded common cause if faults were synchronized by an external shock to the system, causing several valves to fail simultaneously. Single faults are also coded common cause if the potential existed for other valves to fail simultaneously. Imperfections in the data are also discussed; the most important ones are reports with the number of failed valves not stated, inexact populations of valves, and miscoding of the data due to subjectivity.

Different types of valves, such as air-operated valves, check valves, and safety valves, are treated separately. Each type of valve has its own major failure modes. Separate rates are estimated for each of these modes. The binomial failure rate method is used to estimate the common cause rates and related quantities of interest. Every estimated quantity is estimated by both a point estimate and by a 90% interval. Many of the intervals are rather wide, reflecting the observed plant-to-plant variability.

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COMMON CAUSE FAULT RATES FOR VALVES: ESTIMATES
BASED ON LICENSEE EVENT REPORTS AT U.S. COMMERCIAL
NUCLEAR POWER PLANTS, 1976-1980

INTRODUCTION

Common cause faults are defined, for this report, as faults that are synchronized by some external shock to the system. The seriousness of having several valves simultaneously inoperable due to a single cause makes it essential to estimate the rate of valves becoming simultaneously inoperable. Therefore, this report presents estimates of common cause and individual fault rates and failure rates for valves in nuclear power plants.

The data are Licensee Event Reports. They are described and discussed in the first portion of this report. Two common cause aspects of the data are considered in detail: correctly classifying reported events as common cause events or not, and deciding which groups of valves in a plant might be susceptible to simultaneous failure due to a common cause shock.

The binomial failure rate method is used to estimate the common cause rates and related quantities of interest. Every quantity of interest is estimated both by a point estimate and by a 90% interval. Many of the intervals are rather wide, reflecting the substantial plant-to-plant variability evident in the data.

A section of the report discusses how to use binomial failure rate estimates in applications such as fault tree analyses. The basic methodology is described in the body of the report. Certain technical details not covered in the references are given in Appendix A. The required plant information, including exposure times and valve populations, is given in Appendix B. The estimates themselves are found in Appendix C. Appendix D consists of a listing of one-line summaries of the reported common cause events, and a separate listing of all the data.

THE DATA

Event Reports

The raw data are 600 Licensee Event Reports (LERs), describing valve faults in U.S. nuclear power plants. The LERs, summarized by Miller et al.,¹ describe events occurring between January 1, 1976, and December 31, 1980. They include reports from 44 pressurized water reactors (PWRs), i.e., those designed by Babcock and Wilcox, Combustion Engineering, and Westinghouse, and 22 boiling water reactors (BWRs), i.e., those designed by General Electric. Events that occurred before a plant's initial criticality date are not considered.

The pertinent information from each LER is coded into a one-line summary. These one-line summaries are grouped and listed with the respective failure rates in Appendix C. To aid in checking for possible common cause events, underscores are used to separate unrelated events. Lines not so separated describe events that occurred at the same plant on the same date. Appendix C also contains some tabular summaries of the data, giving the total numbers of various kinds of faults. In Appendix D, a list of only common cause events precedes a list of all one-line summaries.

Definitions

The definitions given here follow Reference 1. A valve is defined as the valve body and all its internal parts, the valve operator (motor, solenoid, handwheel, etc.), and any attached functional accessories, such as limit and torque switches, that are needed to make the entire assembly function. Although supply systems to the valve operator (such as electrical, air, or hydraulic) are considered outside the bounds of the component, failures involving them are included. Such failures are considered command faults to the valve assembly.

A failure is an event in which the valve itself needs repair in order to perform as designed. A command fault is an event in which the valve does not fail, but it does not function as desired due to external inputs

or lack of inputs. For example, suppose a valve is commanded to operate, but it fails to function because it receives no power due to a failure of its electrical breaker. Then the valve has not failed; it would have operated satisfactorily if power were available. A second example is when someone lines up a valve in the wrong position. The term fault is used to include both failures and command faults. Appendix C presents estimated rates based both on all faults and on failures only. To avoid needless repetition, however, the explanatory text is given just once. Because there is no convenient verb corresponding to all kinds of faults, statements are often expressed in terms of failures. Unless the context clearly rules it out, any statement about failures or faults should be understood to apply to both.

Seven failure modes identified in the data are defined here. The presence of a demand is not implied by any of the failure modes; if a valve was found to be inoperable or improperly lined up, then the event is counted as a fault, regardless of whether or not the valve was required at the time. The letter following each mode name is the code used in the one-line summaries. Failure to open (A) or failure to close (B) is reported when a valve fails to open fully or close fully when commanded to do so. Failure to close includes safety/relief valves failing to reseat. Internal leakage (C) results when there is measurable leakage past the valve seat, even though the indications show that the valve is closed. This definition assumes that the valve is repairable by cleaning and resurfacing the valve seat and disk. Reverse leakage (E) is a mode used to describe internal leakage through a check valve. It is a separate and distinct mode, applying only to check valves, and is not considered part of the internal leakage mode.

Some control valves such as pressure, level, or flow are not "open" or "close" oriented, but are designed to constantly change positions during operation. Other valves are required to open or close within rigid time constraints for systems to operate properly. Many LERs do not specifically state how a valve fails, but state only, ". . . valve failed to operate during testing." Thus, failure to operate as required (F) is used whenever (a) a valve failed to meet specific requirements such as closing or opening

times, (b) a valve lost the ability to control system parameters, or (c) the LER failed to provide sufficient information concerning the event.

The plugged (failure to remain open) (G) mode is used if any event stopped or limited flow through a normally open valve. A valve is coded plugged if, for example, a valve disk separated from the stem and fell into the closed position, or if the air supply to an air-operated valve fails, allowing the valve to drift closed.

Improper valve configuration (V) is a mode consisting entirely of events caused by human factors resulting in valves not being in the position required by applicable plant conditions. They usually involve personnel failing to close a valve or closing the wrong valve during a valve line-up procedure. All events in this mode are considered command faults, not valve failures.

Populations

As reported in Reference 1, correct valve populations are difficult to obtain. They are usually taken from plant drawings or from the text of Preliminary or Final Safety Analysis Reports, so inaccuracies may be present because the available copy of a drawing is poor, or because changes were made in a plant design and are not shown on the plan. For example, no motor-operated valves are shown in the drawing for the residual heat removal/low pressure coolant injection system at FitzPatrick; yet eight LERs report failures of such valves. In such a case, the population is counted as zero; the reported faults are shown in the one-line summaries of the data, but they are not counted in the tabular summaries of the data, and they are not used in estimates. If a drawing shows several systems as a composite system, as is common for the PWR engineered safety features systems, then Reference 1 gives only the composite population. Rates for damper valves, solenoid-operated valves and hydraulically operated valves are not estimated because their populations are unknown. Tables B-1 and B-2 of Appendix B present populations for the types of valves that were considered: air-operated, motor-operated, manually operated, check, safety, and relief valves.

Exposure Times and Estimated Demands

Except for safety and relief valves, the hours used to estimate fault rates are calendar hours. The starting date is the plant's initial criticality date or January 1, 1976, whichever came later. The ending date is December 31, 1980, except for Three Mile Island Units 1 and 2, which were both shut down following the accident of March 28, 1979. The number of calendar hours is listed for each plant in Tables B-1 and B-2 of Appendix B.

For PWR safety valves and BWR relief valves, fault rates for failure to open and failure to close are estimated using test and operational demands. These valves are required to be tested at least once every 5 years. One test demand is used in the rate estimates for the safety and relief valves in those plants that achieved initial criticality prior to January 1, 1976 and remained operational for the full 5-year period covered by this report. No test demands are assumed for plants that achieved initial criticality after January 1, 1976.

Since only one test demand is assumed for safety or relief valves, operational demands are added to the test demand to estimate failure rates for these valves. An operational demand is considered to be a plant pressure transient sufficient to raise system pressure above the setpoint of the safety or relief valve. Because it was beyond the scope of Reference 1 to obtain a 5-year pressure history for each plant, the number of operational demands was estimated for each plant. Miller et al., pp. 14-15, discuss the necessary assumptions and how estimates of the number of operational demands were obtained. Tables B-1 and B-2 of Appendix B also contain these estimates.

Imperfections in the Data

An important deficiency in the data is the imperfect population counts, as discussed in the section "Populations." Also, a detailed data analysis is impossible because the populations are only given for large systems.

Second, the LER reporting policies may vary from plant to plant. The basic concept of the LERs was to implement a systematic way of identifying risk-significant events that have occurred at U.S. commercial nuclear power plants. LERs, therefore, notify the NRC of "reportable occurrences" at the power plants, by Revision 4 of Regulatory Guide 1.16.² Three possible reasons for the reporting variations are: (a) the general wording of the reportable occurrence section of Regulatory Guide 1.16 could be misinterpreted, (b) the implementation of the Regulatory Guide may differ among plants, and (c) the importance assigned to the Regulatory Guide by the management of the individual plants may also differ. Appendix A of Reference 1 contains a detailed discussion of this LER concept and reporting variability.

A final major imperfection in the data is lack of precise detail in the LERs. The reports are often so vaguely worded that the type of valve, number of failed valves, failure mode, or failure cause is uncertain. These four cases are considered separately here.

Type of Valve

As stated in Reference 1, many LERs do not specify the valve type, but do make it clear that the valve is operated remotely. Since motor-operated valves are the most common type, Miller et al., believe that most of the failures of remotely operated valves are actually failures of motor-operated valves. In this report, LERs for remotely operated valves are pooled with those for motor-operated valves, and estimates are given on the basis of the pooled data. These estimates are upper bounds on what would be found for motor-operated valves if more complete information were available. Conversely, the estimates given for air-operated valves may be lower than estimates based on perfect classification of the data, because some of the remotely operated valves may really be air-operated.

The importance of this pooling is suggested by a scan of the one-line summaries of the data: there are 600 lines, with 313 coded motor-operated, 109 coded remotely operated, and 22 coded air-operated.

Number of Failed Valves

Some LERs contain phrases such as "many containment valves," "several isolation valves," or just the plural "valves." Therefore, in Reference 1 the following values were arbitrarily assigned as the number of failed valves, based on key words used in the LERs:

<u>Key Word</u>	<u>Code</u>	<u>Number Assigned</u>
Valves	V	2
Some	A	3
Various	B	3
Lineup wrong	L	2
Several	S	3
Other	Z	<u>>2</u>

"Other" refers to phrases that did not contain any of the above key words, phrases such as "all containment motor-operated valves" or "a series of valves." Numbers were assigned according to the information in the phrase. The codes are printed in the list of one-liners in Appendices C and D next to the assigned failure numbers when applicable.

This has a slight effect on the estimates of the rates of individual (i.e., not common cause) faults. Of the hundreds of LERs reporting individual faults, five do not state the exact number of failed valves. For these five events, numbers are assigned as described above.

For common cause faults, no arbitrarily assigned numbers of valves are used in the estimates. A common cause event involving an unknown number of valves contributes to the estimate of the rate of common cause events, but it is not used to help estimate the average number of valves per event (for details, see Appendix A). Of the 37 common cause events involving more than one valve, the exact number of valves is uncertain in 12 of the events.

Failure Mode

As mentioned in an earlier section, the mode failure to operate as required is used to include LERs that do not clearly identify the nature of the failure. This is not a serious problem for this report, because only generic fault rates are given here. For motor-operated, air-operated, and manually operated valves, the three modes failure to open, failure to close, and failure to operate as required are combined, and a single rate is estimated for such failures. For other types of valves, the failure mode can always be inferred from the LER.

Failure Cause

The cause of failure is not always clear. Sometimes the cause was unknown to the person who wrote the LER, and sometimes the cause is obscured by a vaguely written narrative. This lack of clarity introduces errors in the classification of events as common cause or not. The possible seriousness of such misclassification is discussed in the following section.

CLASSIFYING COMMON CAUSE EVENTS

To estimate common cause fault rates, it is necessary to determine which events in the data set are common cause faults and which are not. The critical question for each event is: "Was there some shock, external to the valve or valves, that caused or could have caused simultaneous failures or faults?" Synchronization of the faults is essential, because the importance of common cause faults stems from the seriousness of having several valves failing simultaneously.

Because shocks affect a random number of valves, there may be a shock causing exactly one valve to fail. When the data are examined, it is usually possible to decide whether the single valve failed on its own or from some shock that could potentially have caused other valves to fail. Correct identification of common cause shocks as the causes of these single failures helps in estimating the shock rate. If such events were ignored, then few common cause events would remain to be used, and the statistical uncertainties in the estimates would be much larger than necessary.

On February 20, 1976, for example, one discharge valve in the containment spray system at Keweenaw failed to open because the valve had been manually torqued down too tightly. And at Oconee 1, on December 4, 1978, a valve in the containment spray system failed to operate when tested because the breaker to the valve was not racked in properly. Both examples involve command faults imputed to personnel action. They are coded common cause faults, as personnel errors often are. For a personnel error affecting only one valve to be coded common cause, it must be plausible that in similar circumstances, e.g., at another time or at another plant, the person could make the same mistake, affecting more than one valve at the same time. In this report, 61 one-valve events are coded as common cause.

Faults caused by design errors are rarely coded as common cause because there usually is no mechanism to synchronize the faults. Rather, design errors normally contribute to a high individual failure rate, often leading to recurrent failures.

As can be seen, the coding of common cause events involves some judgment on the part of the coder. An inadvertent experience with diesel generator data, described by Atwood and Stevenson,³ sheds some light on the importance of the coder's judgment. After all the estimates had been calculated, Atwood and Stevenson reexamined the diesel generator data, and changed the common cause coding of eight faults, each involving one diesel generator. Two failures became common cause; five command faults became common cause command faults; and one common cause command fault became simply a command fault. So there was a net increase of six common cause faults, each involving only one diesel generator. This was in a data base of 369 LERs, with 25 events initially coded as common cause. Of the estimates that would be used in a fault tree, one of them, r_2 , changed by almost 25%. This is about 5% of the length of the interval for r_2 . The changes are smaller for the other quantities that would be used directly in fault trees. This suggests that the coder's judgment has a noticeable but not overriding effect.

It is conceivable that a person, through misunderstanding or forgetfulness, might intentionally take the same (wrong) action repeatedly, rendering all the valves of a certain type in a certain system either inoperable or incorrectly positioned. This would be an example of a lethal shock, a shock that by its nature automatically causes all the valves of a given type in a system to fail. No such events occur in the data for this report. This may be partly because most of the valves are only grouped very crudely, into major systems with large populations. However, even though no such events are observed, the model allows for their occurrence. This causes the estimated fault rates to be conservative, as described in the section "Estimating Rates Using an Extended Binomial Failure Rate Model."

EXAMINING THE DATA FOR STRUCTURE

Common Cause Systems

It is necessary to form groups of valves, or "common cause systems" such that all the valves within a group are susceptible to simultaneous failure due to a common cause. For example, valves that are serviced together and that perform similar functions and have similar mechanisms could form a common cause system. A system must not be so small that a single shock could affect valves in more than one group.

The valves of one type in a functional system of a plant form such a group. For example, air-operated valves in the engineered safety features (ESF) system all perform similar functions, and the procedures for maintaining and servicing them are normally similar. Their functions, operating environment, and maintenance procedures are different from those of, say, check valves in the auxiliary feedwater system.

Therefore, it is extremely unlikely that a single common cause shock could affect valves of different types, or valves in different systems. And, in fact, no such events occur in the LERs under consideration. On the other hand, valves of the same type in the same plant-system may fail simultaneously because of a single shock. At Rancho Seco, for example, on November 11, 1977, an operator misread the control indications of two high pressure coolant injection (HPCI) motor-operated valves, and therefore mispositioned both valves. At Yankee Rowe on February 1, 1980, three remotely operated HPCI valves were found inoperable because the time delay relays were simultaneously wired improperly when replacements were installed. At Beaver Valley 1 on May 21, 1980, remotely operated valves in the residual heat removal system failed to close because the process control signal was deenergized. And on February 1, 1980, remotely operated control valves in the auxiliary feedwater system of Joseph M. Farley 1 failed to open because contacts in a circuit breaker of the control circuit were misaligned.

Therefore, each common cause system is defined for this report as all the valves of a particular type in a particular functional system of a plant. The populations of the common cause systems are given in Tables B-1 and B-2 of Appendix B.

This grouping of valves into common cause systems is probably too coarse. In particular, there may be few or no shocks that can simultaneously affect all the valves of one type in the entire ESF system. At the very least, it would be desirable to divide the ESF system into HPCI, LPCI (low pressure coolant injection), and containment spray, since none of the reported common cause events involves more than one of these three systems. Perhaps an even finer decomposition would be useful. However, only composite populations are available at many plants, so the common cause systems used are the best that are now possible.

Variability in the Fault Rates

Whenever possible, it is desirable to pool similar data, to obtain the most precise fault rate estimates possible. Examples are pooling the data from plants of similar design, or from similar valves in different systems. Therefore, this report presents generic rates. The different types of valves are treated separately because their mechanisms and functions differ greatly. For each type of valve, fault rates are estimated for failure modes that are intended to be those of greatest interest in applications.

Thus, air-operated, manually operated, and remote/motor-operated valves have rates estimated for failure to open, close, or operate; failure to remain open, or plugged; and improper valve configuration or lineup. Rates are also estimated for internal leakage in air-operated valves, but not in remote/motor-operated or manually operated valves. Internal leakage in the two latter types of valves is considered inconsequential as far as risk to safety is concerned. For check valves, the modes failure to open and failure to remain open, or plugged, are combined, as are failure to close and reverse leakage. Rates are estimated for three failure modes in

safety valves and relief valves: failure to open, failure to close, and internal leakage. Table 1 contains a list of the valve types and their associated failure modes.

TABLE 1. TYPES OF VALVES AND ASSOCIATED FAILURE MODES

Air-Operated Valves

- Failure to open, close, or operate
- Internal leakage
- Failure to remain open (plugged)
- Improper valve configuration

Check Valves

- Failure to open or failure to remain open (plugged)
- Failure to close or reverse leakage

Remote/Motor-Operated Valves

- Failure to open, close, or operate
- Failure to remain open (plugged)
- Improper valve configuration

Manually Operated Valves

- Failure to open, close, or operate
- Failure to remain open (plugged)
- Improper valve configuration

PWR Safety Valves

- Failure to open
- Failure to close
- Internal leakage

BWR Relief Valves

- Failure to open
 - Failure to close
 - Internal leakage
-

For any of these types of valves and failure modes, the fault rates show substantial plant-to-plant variability. There are also variations in the rates among systems, but the plant-to-plant variability is dominant, as discussed below.

As a first step in estimating fault rates, the variability in the rates must be quantified. Suppose that the variability in some fault rate is to be modeled. The rate may be that of individual (i.e., not common cause) events or, if enough data are available, the rate of common cause events. The data sources are the different common cause systems at the different plants, corresponding to any one of the valve types and failure modes listed in Table 1. To model the variation among the different plants and systems, assume that the rate has a two-parameter gamma distribution. A gamma distribution is used because it is a convenient distribution covering the range $(0, \infty)$. Some other distribution, such as lognormal, might work equally well. On the basis of the observed faults, find the maximum likelihood estimates of the two unknown parameters. This gives a gamma distribution that fits the data. An interval covering 90% of the fitted distribution is an approximate 90% interval for the fault rate. That is, the probability that such an interval will include a randomly chosen new fault rate (say, from a system at a plant not yet analyzed) is approximately 90%.

Typically, most of the plants show no faults, although a few may show recurrent faults. This results in highly skewed fitted distributions, having a maximum at zero, a long flat tail to the right, and a 90% interval that is orders of magnitude wide. Although such a distribution is not what a risk analyst desires, it does reflect the great variability in the data.

ESTIMATING RATES USING AN EXTENDED BINOMIAL FAILURE RATE MODEL

The Model

Let m be the number of valves of a particular type in a system at a plant. The model assumes that there are three possible kinds of fault:

1. Each valve can fail individually, and has a constant fault rate λ .
2. A common cause shock can occur in the system, with constant occurrence rate μ . If a shock occurs, the valves in the affected system fail independently of each other, each with probability p , so the total number of failed valves is random. Vesely⁴ calls this the binomial failure rate (BFR) model, because the number of failed valves, given that a shock occurs, is a binomial(m , p) random variable. Estimators using this model are developed by Vesely⁴ and Atwood.^{5,6} These shocks are called nonlethal shocks, to distinguish them from the shocks defined below.
3. A lethal shock can occur in a system, with constant occurrence rate ω . A lethal shock, by its very nature, causes every valve in the affected system to fail. The number of failed valves is not random, but must equal m . No such events occur in the valve LERs. However, the model includes them, for reasons discussed below.

Some quantities of interest are listed below. The notations for p , λ , and μ agree with Reference 5. The quantity λ_+ is called λ'_+ in that reference. The quantities are

λ

= fault rate for an individual valve,
not counting faults due to common
cause shocks

μ	=	rate of nonlethal shock occurrences
p	=	probability that a specific valve is inoperable, given that a nonlethal shock occurs
$\lambda_+ = \mu(1 - q^m)$	=	rate of nonlethal shocks that cause at least one valve to be inoperable (rate of visible nonlethal shocks); here, $q = 1 - p$
ω	=	rate of lethal shock occurrences
$r_1 = \lambda + \mu p + \omega$	=	rate at which a specific valve becomes inoperable, either as an individual fault or due to a shock
$r_k = \mu p^k + \omega$ for $k \geq 2$	=	rate at which a specific set of k valves becomes inoperable simultaneously (due to a shock)
$\beta = [\mu p(1 - q^{m-1}) + \omega]/r_1 =$		long-term fraction of valve faults that occur in multiple faults; called the beta factor by Fleming. ⁷

The quantities r_1, r_2, \dots are the relevant rates for fault tree analysis. For, if a cut set of a fault tree involves k valves, $k \geq 1$, then the relevant rate is r_k , and the probability that the k valves all fail in a short time t is $r_k t$ plus terms of order t^2 . The use of $r_1, r_2, \text{ etc.}$, is discussed in the section "Application," and in Appendix A. The expression given for β ignores the time for discovery and repair of faults.

The basic binomial failure rate model, as defined in Reference 4, does not include lethal shocks. Lethal shocks are included here in order to put

a floor underneath the estimates of r_k , below which they cannot sink. The basic BFR method would estimate r_k as μp^k , for $k > 1$. If p is small and k is large, then μp^k can be microscopic. Using $r_k = \mu p^k + \omega$ maintains r_k at a realistic level, because the Bayes estimate of ω is always positive (even when the observed number of lethal shocks is zero). Therefore, the postulated lethal shocks act as a surrogate for other possible model inaccuracies.

Estimation

This section briefly describes the estimation procedure based on the above model. The Bayesian methods developed by Atwood^{5,6} are used, extended to allow for plant-to-plant variation and lethal shocks.

The point estimates given are Bayes means. The mean is used, rather than the mode or the median, because it is usually the largest of the three and, in fact, often the only one of the three that is not virtually zero. The median is used for β , because the computer code has not been programmed to calculate the mean. It should be realized that when the distribution has a large variance, no single point--be it median, mean, or some other point--adequately identifies the location of the distribution. The interval estimates given are Bayes 90% intervals, with a 5% probability in each tail.

The use of Bayesian methods is unavoidable, because classical non-Bayesian methods do not give confidence intervals for complicated expressions such as r_1 , or even for simple expressions such as p when the data are obtained from plants with different numbers of valves. The Bayesian distributions used are either estimated directly from the data, to reflect the apparent variability in the parameters, or are calculated in the usual way on the basis of diffuse prior distributions. Therefore, the results obtained should not differ markedly from non-Bayesian results, if the latter were obtainable.

First, a gamma distribution is fitted to the observed individual faults of the valves. This was described in the section "Variability in

the Fault Rates," and defines a distribution for the parameter λ . Similarly, if enough faults are observed, a gamma distribution is fitted to the observed nonlethal common cause events, giving a distribution for the parameter λ_+ . Only motor-operated valves have enough common cause faults to allow plant-to-plant variability to be fitted for λ_+ .

Any variability in p , from plant to plant or shock to shock, is not estimated, because a method for doing this has not been developed. Therefore, standard Bayesian methods are used to get posterior distributions for p and w , and for λ_+ when few or no common cause events occurred. For p , an approximately noninformative prior distribution is used, as described in Reference 6, pp. 16-17. For λ_+ and w , a noninformative prior distribution is used, proportional to $\lambda_+^{-1/2}$ or $w^{-1/2}$.

The quantities p , λ , λ_+ , and w are treated as fundamental. The distributions of all the other quantities are obtained from the distributions of the four fundamental quantities, using the equations relating the parameters in the preceding section. Unfortunately, these equations involve m , the number of valves in the system in question. Therefore, estimates of μ , β , and r_k , $1 \leq k \leq m$, are found separately for each value of m . Then, overall estimates that do not depend on m are given, as follows. As a point estimate, the median of the point estimates is used (if the number of point estimates is even, the larger of the two possible medians is used). As a conservative interval, the smallest lower bound and the largest upper bound are used.

DISCUSSION

Application

The uncertainty intervals for the rates should be used, not just the point estimates. Because of the great variability from one plant to another, many of the intervals are quite wide; therefore, use of the point estimate alone would be overly naive. In some cases, the lower bound is many orders of magnitude less than the point estimate. This happens when most of the plants or systems show no faults, but some of them show several faults. In such cases the distribution has a spike at zero and a very long flat tail. So the lower bound should be regarded as unknown, but essentially zero, and the point estimate should be thought of as a crude way to characterize a wide distribution.

Now consider the effect of delayed discovery of faults. Suppose that a valve becomes inoperable during a time interval t , but that the fault is not discovered until the valve is tested at the end of the time interval. Faults in the other valve(s) are also not discovered until the end of the time interval. If the interval is long enough, then a substantial portion of the simultaneous faults might not be common cause faults, but rather might be individual faults that were not discovered promptly.

In Appendix A, the section "How to Obtain Probabilities from Rates," gives the general method for using the estimated rates to estimate probabilities, for example, the probability that at least three out of four valves become inoperable during a time period t . Using the general method, approximations can be found if t is not too large, such as

$$P(1 \text{ specific valve inoperable}) = r_1 t$$

and

$$P(k \text{ specific valves inoperable}) = (xt)^k + r_k t$$

for $k \geq 2$. These approximations are accurate to at least one significant digit if, in the first case, $r_1 t < 0.1$, and in the second case, if $\lambda t < p/10$ and $r_k t < 0.1$. If t is too large for these approximations, then the more general methods of Appendix A should be used.

The formulas just given should look familiar to fault tree analysts. In particular, if $k = 2$, $r_2 t$ is used in the way that $\beta r_1 t$ is often used by analysts. The formulas given here are more general than those obtained by the beta-factor method because they recognize that systems can have more than two valves. The ratio r_k/r_1 would be a beta factor for k components, and the value given in this report as the beta factor is a compromise among these values.

The beta factor is defined as the long-term fraction of valve faults that occur in multiple faults. However, to estimate it, with uncertainty bounds, the computer program uses a formula for β that assumes immediate discovery and repair of faults. Therefore, the computed point estimates are low. The fact that medians are used rather than means may also make the point estimates low. For comparison, a simple direct estimate can be obtained by dividing the observed number of faults that occurred in multiple faults by the observed total number of faults. For failures to open, close, or operate in air-operated valves, the direct estimate is $2/18 = 0.111$, which differs little from the computed estimate of 0.165. For failures to open in BWR relief valves, the direct estimate is $12/42 = 0.286$. This differs substantially from the computed estimate of 0.095, but is still less than the computed upper bound of 0.493. In any case, this report recommends using $r_2, r_3, \text{ etc.}$, rather than β .

Diagnostic Checks

A diagnostic check on the BFR assumptions is considered. The statistical details are given in Appendix A, but the idea of the check is as follows; if the BFR assumptions are correct, then the number of valves affected by any (future) nonlethal shock is a binomial(m, p) random variable. Once p has been estimated, the observed numbers of affected valves can be compared with the numbers predicted by the BFR assumptions. If they

differ greatly, then the BFR assumptions should be questioned. The comparisons are performed by looking at the standardized residuals, defined as

(observed number - expected number)/standard deviation.

There is one residual for the number of common cause events involving exactly one valve, one residual for the common cause events involving exactly two valves, etc. If the BFR assumptions are correct for the data set, then all the residuals should be small.

The largest standardized residual obtained in this way occurs when improper lineups of remote/motor-operated valves are analyzed. For this analysis, events are considered only if the exact number of incorrect valves is reported. There are 17 such events, occurring in systems with up to 50 valves. The standardized residuals corresponding to one through ten improperly lined up valves are, respectively, -0.85, 1.79, -1.12, -0.57, -0.29, -0.14, -0.07, -0.03, -0.01, and -0.01. The standardized residuals corresponding to more than ten valves are all equal to zero, to two decimal places. The largest absolute value is approximately 1.8. This means that no observed count is more than 1.8 standard deviations from its estimated expected value. The residuals are even smaller for other kinds of valves or faults. Therefore, this investigation finds no strong evidence of departure from the binomial distribution.

In the above case, the pattern of residuals shows that there are more faults than expected involving two valves at a time, and fewer than expected involving other numbers of valves. The discrepancies are not statistically significant, but the pattern might be altered if the exact number of improper valves were reported in every case. In particular, it may be that events involving more than two valves are less likely to have the number of valves reported; this would partially account for the pattern.

THE ESTIMATES

The estimates for the 18 classes of valves and failure modes listed in Table 1 are given in Appendix C.

Depending on the application, command faults may or may not be of interest. Therefore, most of the estimated rates include both estimates based on all faults and estimates based on failures only, with command faults excluded. However, when a valve failed due to an improper lineup, the event was always coded as a command fault; the valve itself did not fail. Thus, estimates based only on command faults are presented for rates involving improper valve configuration.

Every estimate is given as a triple of numbers, showing the lower limit, the point estimate, and the upper limit. The point estimate is the mean of the Bayes posterior distribution (for the beta factor, the median rather than the mean is shown). The upper and lower limits form a 90% interval. Application of the estimates is discussed in the next section.

Appendix C also contains summaries of the data used to produce the estimates, both tabular summaries and printouts of the one-line summaries of the LERs. A few comments precede each set of estimates.

CONCLUSIONS

Estimates have been found for common cause fault rates, common cause failure rates, and related quantities. The estimates are based on Licensee Event Reports for valves from January 1, 1976, through December 31, 1980. Because the LER data base may be incomplete, the estimates should be used with care. The rates presented are per calendar hour for all systems except safety and relief valves, where estimated demands are used for failure to open and failure to close. The user must perform any conversion to other units.

Every quantity has been estimated by both a point estimate and a 90% interval. The width of the intervals reflects both statistical uncertainty, due to the random nature of the data, and also the actual substantial variability in the fault rates from plant to plant or system to system.

How to use the estimates in applications has been discussed. Diagnostic checks showed no marked departure in the data from the assumptions of the model.

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APPENDIX A
TECHNICAL DETAILS OF METHODOLOGY

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TECHNICAL DETAILS OF METHODOLOGY

Fitting a Gamma Distribution to the Data

Suppose that λ has a gamma (a, b) distribution, and that, given λ , the number of faults of a valve has a Poisson (λt) distribution. Then it is not hard to show that the unconditional distribution of the number of faults is negative binomial with parameters a and bt (see Johnson and Kotz^{A-1}). Therefore, the maximum likelihood estimates of a and bt can be found numerically, based on the exposure times and observed failures for the valves.

To illustrate this, consider the individual failures to open, close, or operate, for remote/motor-operated valves, counting failures only. There are 181 systems at the various plants, for example, the auxiliary feedwater system at Davis-Besse 1, the HPCI and LPCI systems at Crystal River 3 (combined as a single system for lack of more detailed population information), and the core spray system at Quad-Cities 2. When a gamma distribution is fitted to the 253 reported failures from these 181 plant-systems, the estimated parameters are 0.811 and 3.233E-6, the estimated mean of the distribution is 2.623E-6, and the estimated 90% interval is (7.500E-8, 8.465E-6).

A check is routinely made for outliers, but no plant-system is so far out in the tail of the fitted distribution that it should be called an outlier. The estimated mean and 90% interval given above are used in Appendix C as the mean and interval for λ .

This example is typical of all the portions of the data, except that the estimates are usually based on far fewer reported faults. If so few faults are reported that a gamma distribution cannot be estimated (that is, the estimation program finds no evidence of variability in λ), then a posterior Bayes distribution for λ is used, obtained in the usual way from a noninformative prior distribution and the reported data.

An LER may neglect to report the exact number of failed valves. If the LER reports individual faults, they are included in the data used for fitting a gamma distribution to λ , with the number of valves assigned as described in the section "Number of Failed Valves" in the main body of this report. On the other hand, if the LER describes a common cause event, then it is included in the data used for fitting a gamma distribution for λ_+ (because a shock is known to have occurred), but it is not included in the data used for estimating P (because the number of affected valves is unknown). It is not certain what effect this has on the estimates. If reports are more likely not to specify the number of valves when this number is large, then the procedure followed will tend to underestimate P. However, the procedure seems better than making up numbers whenever the counts are unknown.

How to Obtain Probabilities from Rates

When using the model of this report, the key to evaluating probabilities is to condition on the number of nonlethal shocks. Let N_S be the number of nonlethal shocks, and N_L be the number of lethal shocks. Consider any event involving the failure or survival of certain valves in some time period t. Let $P(A|B)$ denote the conditional probability of A, given B. The following decompositions hold:

$$P(\text{event}) = P(\text{event} \mid N_L > 0) P(N_L > 0) + P(\text{event} \mid N_L = 0) P(N_L = 0)$$

$$P(\text{event} \mid N_L = 0) = \sum_{n=0}^{\infty} P(\text{event} \mid N_L = 0, N_S = n) P(N_S = n).$$

Normally, only the first few terms in the sum need to be evaluated.

The model assumes independent shocks with a constant shock rate. Therefore (Reference A-1, Ch. 4.1), the number of shocks in time t is a

Poisson random variable, with parameter equal to t times the shock rate.
It follows that some of the above probabilities are easy:

$$P(N_L = 0) = e^{-\omega t}$$

$$P(N_L > 0) = 1 - e^{-\omega t}$$

$$P(N_S = n) = e^{-\mu t} (\mu t)^n / n!$$

If t is small, these expressions can be approximated by even simpler ones.

The nontrivial term to evaluate is the conditional probability of the event under consideration, given that $N_L = 0$ and $N_S = n$. As a major step toward evaluating this, let $q = 1 - p$, and note that for any specific single valve

$$P(\text{survival} \mid N_L = 0, N_S = n) = q^n e^{-\lambda t}.$$

This expression is the probability that the valve survives all n shocks (q^n), times the probability that it does not become inoperable individually ($e^{-\lambda t}$). Denote this expression by Q_n . To find $P(\text{event} \mid N_L = 0, N_S = n)$, use Q_n and the fact that, given a shock, the valves behave independently.

As an example, suppose that a system has four valves. What is the probability that at least three of the four become inoperable during some time period t ? Given that $N_L = 0$ and $N_S = n$, the conditional probability that a specific valve survives is Q_n , so the conditional probability that at least three fail to survive is

$$P(\text{exactly 3 fail} \mid N_L = 0, N_S = n) + P(\text{exactly 4 fail} \mid N_L = 0, N_S = n)$$

$$= \binom{4}{3} (1 - Q_n)^3 Q_n + (1 - Q_n)^4 = (1 - Q_n)^3 (1 + 3 Q_n).$$

Therefore, to obtain the desired probability, observe that $P(\text{event} \mid N_L > 0) = 1$, and substitute into the equation for $P(\text{event})$ at the beginning of this section. The answer is

$$(1 - e^{-\omega t}) + e^{-\omega t} \sum_n (1 - Q_n)^3 (1 + 3Q_n)e^{-\mu t} (\mu t)^n / n! .$$

Substitution of estimates for p , μ , λ , and ω yields an estimate of the desired probability. To obtain upper and lower uncertainty bounds on the probability is not so easy. Using the end points of the 90% intervals for p , μ , λ , and ω is conservative, since it is unlikely that the four parameters are all at their upper ends or all at their lower ends. In principle, a Bayes 90% interval can be found, based on the distributions of p , λ , λ_+ , and ω . This is how the intervals for β , r_1 , r_2 , etc., are found in this report. To perform this operation, however, requires numerical integration.

The point estimate obtained by substituting the Bayes means into some complicated expression is not necessarily the same as the mean of the Bayes distribution of the expression. But it is simple, and credible.

When t is not large, simple approximations can be used. Each of the approximations given here is valid if $\lambda t \ll 1$, $\mu t \ll 1$, and $\omega t \ll 1$. They follow from the Taylor series expansion for e^{-x} and are

$$e^{-\omega t} \doteq 1$$

$$1 - e^{-\omega t} \doteq \omega t$$

$$e^{-\mu t} \doteq 1$$

$$Q_n \doteq q^n$$

$$1 - Q_n \doteq (1 - q^n) + q^n \lambda t$$

$$\sum_{n=1}^{\infty} (1 - Q_n)^i Q_n^j P(N_S = n) \doteq (p + q \lambda t)^i q^j \mu t, \text{ for } i \geq 0 \text{ and } j \geq 0.$$

This leads to simple approximations of many probabilities. For each of the probabilities below, the first approximation is valid if $\lambda t \ll 1$, $\mu t \ll 1$, and $\omega t \ll 1$. The second approximation for one specific valve is valid if, in addition, $\mu \ll \lambda$ and $\omega \ll \lambda$. The second approximation is valid for k valves if the first approximation is valid and, in addition, $q\lambda t \ll p$.

$$\begin{aligned} P(1 \text{ specific valve fails}) &\doteq \lambda t + \mu t + \omega t \doteq r_1 t \\ &\doteq \lambda t \end{aligned}$$

$$\begin{aligned} P(k \text{ specific valves fail}) &\doteq (\lambda t)^k + (q\lambda t + p)^k \mu t + \omega t \\ &\doteq (\lambda t)^k + p^k \mu t + \omega t \doteq (\lambda t)^k + r_k t \quad \text{for } k \geq 2 \end{aligned}$$

$P(\text{at least } k \text{ out of } m \text{ valves fail})$

$$\begin{aligned} &\doteq \binom{m}{k} (\lambda t)^k + \mu t \sum_{i=k}^m \binom{m}{i} (q\lambda t + p)^i q^{m-i} + \omega t \\ &\doteq \binom{m}{k} (\lambda t)^k + \mu t \sum_{i=k}^m \binom{m}{i} p^i q^{m-i} + \omega t \\ &\text{for } k \geq 1. \end{aligned}$$

Diagnostic Check Based on Residuals

If the binomial failure rate (BFR) assumptions hold, then the number of valves affected by an observable shock has a binomial (m, p) distribution, truncated because zero cannot be observed. Once p has been estimated, the correctness of this distributional assumption can be studied. The sample sizes in the valve data are much too small to allow standard goodness-of-fit tests, but residuals can be used, essentially as described in Section 5 of Atwood.^{A-2}

Suppose n_+ nonlethal shocks hit the systems with m valves and cause at least one valve to become inoperable. Then define

$$z_j = \binom{m}{j} p^j q^{m-j} / (1 - q^m)$$

for $1 \leq j \leq m$, with $q = 1 - p$. Let N_j be the number of shocks that affect exactly j valves. Conditional on n_+ , N_j has mean $E_j = n_+ z_j$ and variance $V_j = n_+ z_j (1 - z_j)$. Now suppose that there are systems with various sizes m_i , and corresponding values n_{+i} , N_{ji} , E_{ji} , and V_{ji} . Then, conditional on the values of n_{+i} , $N_{j+} = \sum N_{ji}$ has mean $E_{j+} = \sum E_{ji}$ and variance $V_{j+} = \sum V_{ji}$. Here, the summations are over all i , such that $m_i \geq j$. Substitution of the estimate of p gives \hat{E}_{j+} and \hat{V}_{j+} . Then, for each j , a standardized residual can be constructed

$$U_j = \frac{(N_{j+} - \hat{E}_{j+})}{\sqrt{\hat{V}_{j+}}} .$$

Under the BFR assumptions, the U_j values have a mean and variance of approximately 0 and 1. Any large value of U_j indicates that the data do not satisfy the BFR assumptions.

Effect of Data Inaccuracies

In the main body of this report, at the end of the Classifying Common Cause Events section, there was a description of an actual experience suggesting the importance of data misclassification. Now let us investigate the effect of data inaccuracies more theoretically, by asking, "What effect does a small relative change in the data have on the estimates?" This effect can be approximated by the use of the relevant derivatives. Let θ denote a parameter to be estimated (λ , λ_+ , w , p , μ , β , or an r_k). Let x denote some quantity in the data (n_I , n_+ , n_L , or v , all defined below). Relative change means the change in the quantity, divided by the value of the quantity. Then, the rate of relative change in the estimate of θ per relative change in x is

$$C(\theta, x) = \frac{\partial \hat{\theta}}{\partial x} \cdot \frac{x}{\hat{\theta}} . \quad (A-1)$$

Approximate formulas will now be derived.

It is convenient during the derivation to work with maximum likelihood estimators rather than Bayes means. The difference between these two estimators is not important here, because the purpose is only to roughly approximate the effect of data inaccuracies. Suppose data are combined from systems with populations m_i and times t_i . Let n_{Ii} , n_{+i} , n_{Li} , and s_i denote the observed numbers of individual faults, nonlethal shocks, lethal shocks, and valves made inoperable by nonlethal shocks. Then, the maximum likelihood estimates satisfy

$$\hat{\lambda} = \frac{n_{Ii}}{m_i t_i}$$

$$\hat{\lambda}_+ = \frac{n_{+i}}{t_i}$$

$$\hat{\omega} = \frac{n_{Li}}{t_i}$$

$$\sum s_i = \hat{p} \sum \frac{m_i n_{+i}}{m_i} . \quad (A-2)$$

$$1 - \hat{q}$$

Equation (A-2) requires knowledge of each separate $m_i n_{+i}$. However, it can be approximated by

$$\sum s_i \approx \frac{p \sum m_i n_{+i}}{(1 - q^m)}$$

where m , generally not an integer, is the weighted average defined by

$$m = \frac{\sum m_i n_{+i}}{\sum n_{+i}}$$

where the sum is taken over all i such that $m_i > 1$. The terms with $m_i = 1$ are not counted because they contain no information about p .

So now, if we define $n_I = \sum n_{ij}$, $n_+ = \sum n_{+j}$, $n_L = \sum n_{Lj}$, and $v = \sum s_j / \sum m_j n_{+j}$, and if m is as just defined, then the estimates satisfy

$$\hat{\lambda} = \frac{n_I}{m_i t_i}$$

$$\hat{\lambda}_+ = \frac{n_+}{t_i}$$

$$\hat{\omega} = \frac{n_L}{t_L}$$

$$\hat{p} = v(1 - \hat{c}^m) .$$

Finally, the coefficients $C(\theta, x)$ defined by Equation (A-1), can be approximated for $\theta = \lambda$, λ_+ , ω , p , u , r_k , or β , and for $x = n_I$, n_+ , n_L , or v . Formulas are given in Table A-1, and very rough approximate values are given in Table A-2. For these approximations it is assumed that

$$\hat{r}_1 = \lambda.$$

These coefficients are used as in the following example. Suppose that information is needed about the effect on the estimate r_1 of increasing n_I and v by 10% and decreasing n_+ by 5%. The relative change is

$$\frac{\Delta \hat{r}_1}{\hat{r}_1} = C(r_1, n_I) \times (0.1) + C(r_1, n_+) \times (-0.05) + C(r_1, v) \times (0.1) .$$

Of course, the real difficulty is not in calculating derivatives, but in deciding how much inaccuracy might realistically be in the data. Inaccuracy due to misclassification of the reported events was addressed in the section "Classifying Common Cause Events," in the main body of this report. To assess the amount of missing data (unreported events or overlooked reports) is beyond the scope of this report.

TABLE A-1. FORMULAS FOR $C(\theta, x) = \frac{\partial \hat{\theta}}{\partial x} \cdot \frac{x}{\hat{\theta}}$

θ	x			v
	n_1	n_+	n_L	
λ	1	0	0	0
λ_+	0	1	0	0
ω	0	0	1	0
p	0	0	0	$\frac{1 - q^m}{1 - q^m - m p q^{m-1}}$
μ	0	1	0	$1 - C(p, v)$
r_1	$\frac{\lambda}{r_1}$	$\frac{\mu p}{r_1}$	$\frac{\omega}{r_1}$	$\frac{\mu p}{r_1}$
$r_k, k > 1$	0	$\frac{\mu p^k}{r_k}$	$\frac{\omega}{r_k}$	$\frac{\mu p^k}{r_k} [1 + (k - 1) C(p, v)]$
β	$\frac{\lambda}{r_1}$	$\frac{D}{D + \omega}$	$\frac{\mu p}{r_1}$	$\frac{D + (m - 1)\mu p^2}{D + \omega} \frac{q^{m-2} C(p, v)}{1 - C(r_1, v)}$

Notes:

1. Here, D denotes $\mu p(1 - q^{m-1})$.
2. For typographical clarity, the hat is omitted from estimated quantities.

TABLE A-2. CRUDE APPROXIMATIONS FOR $C(\theta, x)$ ^a

θ	x				v
	n_1	n_+	n_L		
λ	1	0	0		0
λ_+	0	1	0		0
ω	0	0	1		0
p	0	0	0		>1
μ	0	1	0		<0
r_1	± 1	± 0	± 0		± 0
$r_k, k > 1$	0	<1	<1		Varies
β	± -1	<1	<1		Varies

a. This table shows, for example: if n_1 increases by 10%, $\hat{\beta}$ will decrease by approximately 10%; if v increases by 5%, \hat{p} will increase by more than 5%. For unusual data, the assumptions underlying the approximations may not be true. For very small data sets, small relative changes are impossible, so the table is irrelevant.

References

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APPENDIX B
PLANT INFORMATION AND CODE DEFINITIONS

TABLE B-1. PWR PLANT DATA

Plant Name	Code	Vend	Calendar Hours	Valve Population ^a								Safety Demands	
				Auxiliary Feedwater				ESF ^b					
				Air	Check	Motor	Manual	Air	Check	Motor	Manual	Safety ^c	
Arkansas Nuclear One 1	AR1	B	43800	2	5	10	-	-	4,12, 8	2, 6,10	16,17, 6	2	10
Crystal River 3	CR3	B	34704	1	13	6	15	-	4,23	6,16	7,12	2	13
Davis-Besse 1	DB1	B	28944	-	11	2	18	-,14	2,26	4,17	6, -	2	12
Oconee 1	OE1	B	43800	3	9	0	14	-, 1, -	-, 13, 7	2,12,29	5,39,17	2	19
Oconee 2	OE2	B	43800	3	9	9	14	-, 1, -	-, 14, 7	2,12,28	5,40,18	2	9
Oconee 3	OE3	B	43800	3	9	0	14	-, 1, 4	-, 14, 7	2,12,23	5,41,15	2	11
Rancho Seco	RS1	B	43800	-	12	2	12	-	14,20	8,20	29,33	2	7
Three Mile Island 1	TI1	B	28368	3	11	4	10	-	8,19	10,17	7, 8	2	1
Three Mile Island 2	TI2	B	8736	2	10	7	9	-, 2	12,19	27, 8	18,32	2	1
Arkansas Nuclear One 2	AR2	C	18120	4	16	14	7	-, 2	13,30	13,36	21,14	3	19
Calvert Cliffs 1	CC1	C	43800	2	8	-	10	4	45	31	39	2	17
Calvert Cliffs 2	CC2	C	35784	2	8	-	10	4	45	31	39	2	8
Fort Calhoun	FC1	C	43800	5	4	1	10	32	45	5	45	2	8
Millstone 2	MI2	C	43800	2	4	3	25	4	47	30	36	2	23
Maine Yankee	MY1	C	43800	3	8	-	15	22	49	35	72	3	13
Palisades	PA1	C	43800	4	6	-	8	2	21	15	31	3	20
St. Lucie 1	SL1	C	41112	4	9	3	16	2, 1	10,30	4,30	16,27	3	14
Beaver Valley 1	BV1	W	40656	-	6	9	17	-, 3, -	4,22,14	10,15,15	-,19, 2	3	49
D. C. Cook 1	DC1	W	43800	5	12	10	32	-,25	10,34	10,43	13,46	3	17
D. C. Cook 2	DC2	W	24600	5	12	10	32	-,25	10,34	10,43	13,46	3	10
Haddam Neck	HN1	W	43800	4	8	-	19	-	27	28	46	3	10
Indian Point 2	IP2	W	43800	4	18	8	20	-	36	52	53	3	33
Indian Point 3	IP3	W	41472	4	23	8	24	4	45	58	52	3	25
Joseph M. Farley 1	JF1	W	29712	8	21	11	42	-, -, 3	5,28, 5	10,27,20	16,20,16	3	29
Keweenaw	KE1	W	43800	-	11	4	9	-	13,19	8,29	14,27	2	17
North Anna 1	NA1	W	23976	3	6	3	24	-, 3, -	5,22,14	8,25,12	6, 6, 6	3	12
North Anna 2	NA2	W	4872	3	6	3	24	-, 3, -	5,22,14	8,25,12	6, 6, 6	3	7
Prairie Island 1	PR1	W	43800	4	11	3	9	2, -	5,23	23,28	11,22	2	12
Prairie Island 2	PR2	W	43800	4	11	3	9	2, -	5,23	23,28	11,22	2	12
Point Beach 1	PT1	W	43800	3	16	11	21	2, 2	10,21	4,27	15,38	2	6
Point Beach 2	PT2	W	43800	3	16	11	21	2, 2	10,21	4,27	15,38	2	5
R. E. Ginna 1	RG1	W	43800	7	12	3	22	-	21	44	42	2	4

TABLE B-1. (continued)

Plant Name	Code	Vend	Calendar Hours	Valve Population ^a								Safety Demands
				Auxiliary Feedwater				ESF ^b				
				Air	Check	Motor	Manual	Air	Check	Motor	Manual	Safety ^c
H. B. Robinson 2	R02	W	43800	3	10	8	20	8	25	29	57	3 21
Salem 1	SA1	W	35496	14	17	-	28	-, 4	6,32	7,32	16,41	3 17
Sequoyah 1	SE1	W	4320	10	21	3	25	10,85	8,42	3,10	7,78	3 11
San Onofre 1	SO1	W	43800	7	12	3	27	-	18	23	12	2 9
Surry 1	SU1	W	43800	-	16	6	20	-, 3	7,25	10,39	9,27	3 14
Surry 2	SU2	W	43800	-	16	6	20	-, 3	7,25	10,39	9,27	3 14
Trojan	TR1	W	43800	-	15	11	26	-	6,22	10,20	13,19	3 19
Turkey Point 3	TU3	W	43800	6	7	-	17	2	34	50	40	3 21
Turkey Point 4	TU4	W	43800	6	7	-	17	2	34	50	40	3 26
Yankee Rowe	YR1	W	43800	-	4	8	10	2	17	20	26	3 8
Zion 1	ZI1	W	43800	8	7	17	8	-, 4	12,50	9,56	22,42	3 26
Zion 2	ZI2	W	43800	8	7	17	8	-, 4	12,50	9,56	22,42	3 26

a. A dash indicates that no valves of the type under consideration are shown in the available drawings.

b. Due to composite drawings, separate populations are not always available for the Containment Spray, High-Pressure Coolant Injection (HPCI), and Low-Pressure Coolant Injection (LPCI) systems. If three numbers are shown, they are the populations of the three systems, respectively. If two numbers are shown, the first is the Containment Spray population, and the second is the population of the pooled HPCI and LPCI systems. If only one number is shown, it is the total population of the three systems.

c. The populations are for safety valves that tap off the pressurizer.

TABLE B-2. BWR PLANT DATA

Plant Name	Code	Vend	Calendar Hours	Valve Population ^a													
				Core Spray				HPCI				LPCI					
				Air	Check	Motor	Manual	Air	Check	Motor	Manual	Air	Check	Motor	Manual	Relief ^b	Relief Demands
Browns Ferry 1	BF1	G	43800	-	12	12	17	-	12	11	6	-	11	40	15	11	70
Browns Ferry 2	BF2	G	43800	-	12	12	17	-	12	11	6	-	11	40	15	11	63
Browns Ferry 3	BF3	G	38496	-	12	12	17	-	12	11	6	-	11	40	15	11	53
Brunswick 1	BR1	G	37032	-	10	10	12	-	10	13	4	4	18	49	25	9	49
Brunswick 2	BR2	G	43800	-	10	10	12	-	10	13	4	4	18	49	25	9	72
Cooper Station	CD1	G	43800	-	6	10	4	-	-	10	1	7	6	37	-	8	22
Dresden 2	DR2	G	43800	-	2	10	14	-	12	13	12	-	10	28	18	5	35
Dresden 3	DR3	G	43800	-	2	10	14	-	12	13	12	-	10	28	18	5	29
Duane Arnold	DA1	G	43800	2	2	10	4	-	3	7	2	8	16	50	28	6	29
Edwin I. Hatch 1	EN1	G	43800	2	12	10	12	1	11	13	4	10	21	45	24	9	74
Edwin I. Hatch 2	EN2	G	21816	4	6	10	9	1	12	14	4	10	12	43	30	11	20
FitzPatrick	FP1	G	43800	2	2	10	4	-	1	8	-	7	5	-	29	9	37
Millstone 1	MI1	G	43800	2	-	10	8	4	9	-	35	2	-	24	28	3	24
Monticello	MO1	G	43800	-	8	8	14	-	8	12	4	7	17	27	34	4	26
Peach Bottom 2	PB2	G	43800	-	18	14	18	3	11	12	10	2	21	32	30	11	26
Peach Bottom 3	PB3	G	43800	-	18	14	18	3	11	12	10	2	21	32	30	11	35
Pilgrim 1	PI1	G	43800	-	-	8	2	-	1	7	1	5	8	32	27	3	40
Quad-Cities 1	QC1	G	43800	-	2	10	8	5	14	15	11	1	10	32	20	5	33
Quad-Cities 2	QC2	G	43800	-	2	10	8	5	14	15	11	1	10	32	20	5	32
Vermont Yankee	YY1	G	43800	-	8	10	11	-	11	11	6	-	16	35	34	4	18
				Core Spray				ESFC ^c				Relief ^b					
Nine Mile Point 1	NM1	G	43800	1	13	12	8	4,8	10,2	4,5	12,8	6					
Oyster Creek	OC1	G	43800	-	14	14	7	-,7	6,5	10,18	-,8	4					

a. A dash indicates that no valves of the type under consideration are shown in the available drawings.

b. The populations are for relief valves that tap off the main steam header.

c. The first number is the Containment Spray population, and the second is the population of the pooled High-Pressure Coolant Injection (HPCI) and Low-Pressure Coolant Injection systems.

TABLE B-3. CODES USED IN VALVE LER ONE-LINE DESCRIPTIONS

FAILURE MODE			FAILURE CAUSE			NUMERICAL KEY WORDS			
CODE	DESCRIPTION		CODE	DESCRIPTION		NUMBER	CODE	DESCRIPTION ASSIGNED	
A - FAILED TO OPEN			00 - UNKNOWN			2	V - VALVES		
B - FAILED TO CLOSE			01 - PERSONNEL (OPERATION)			3	A - SOME		
C - INTERNAL LEAKAGE			02 - PERSONNEL (MAINTENANCE)			3	B - VARIOUS		
E - REVERSE LEAKAGE (CHECK VALVES)			03 - PERSONNEL (TESTING)			3	S - SEVERAL		
F - FAILED TO OPERATE AS REQUIRED			04 - DESIGN ERROR			>1	Z - OTHER		
G - PLUGGED (FAILS TO REMAIN OPEN)			05 - FABRICATION/CONSTRUCTION/QUALITY CONTROL				BLANK - NUMBER GIVEN	IN LER	
V - IMPROPER VALVE CONFIGURATION			06 - PROCEDURAL DISCREPANCY						
COMPONENT			07 - NORMAL WEAR				ACTIVITY RESULTING IN DISCOVERY		
CODE	DESCRIPTION		08 - EXCESSIVE WEAR				CODE	DESCRIPTION	
MV - MOTOR OPERATED VALVE (ELEC.)			09 - CORROSION				M - MAINTENANCE		
AV - PNEUMATIC OPERATED VALVE			10 - EXCESSIVE VIBRATION				N - NORMAL OPERATION		
RM - REMOTE OPERATED VALVE			11 - MECH. CONTROL/PARTS; FAILED/OUT OF ADJUST.				R - RECORDS REVIEW		
XV - MANUAL OPERATED VALVE			12 - SEAL/GASKET FAILURE/PROBLEM				T - TESTING		
CV - CHECK VALVE			13 - PACKING FAILURE/PROBLEM				U - UNKNOWN		
RV - RELIEF/SAFETY VALVE			14 - BELLOW/S/BOOT FAILURE/PROBLEM						
TYPE OF EVENT			15 - ELECTRICAL INPUT FAILURE/PROBLEM				N555 VENDOR		
CODE	COMMAND	FAULT	16 - BEARING/BUSHING FAILURE/PROBLEM				CODE	DESCRIPTION	
FAILURE			17 - WELD FAILURE				B - BABCOCK & WILCOX		
R	S	NONRECURRING, NOT COMMON CAUSE	18 - LACK OF LUBRICATION				C - COMBUSTION ENGINEERING		
C	T	RECURRING, NOT COMMON CAUSE	19 - ELECTRIC MOTOR OPERATOR FAILURE/PROBLEM				W - WESTINGHOUSE		
B	U	NONLETHAL COMMON CAUSE	20 - SOLENOID FAILURE/PROBLEM				G - GENERAL ELECTRIC		
L	V	RECURRING NONLETHAL COMMON CAUSE	21 - LEAKING/RUPTURE DIAPHRAGM						
M	W	LETHAL COMMON CAUSE	22 - TORQUE SWITCH FAILURE/PROBLEM						
	O	RECURRING LETHAL COMMON CAUSE	23 - FAILURE OF COMPONENT SUPPLY SYSTEM						
			24 - SEAT/DISC FAILURE/PROBLEM						
			25 - LIMIT SWITCH FAILURE/PROBLEM						
			26 - PILOT VALVE FAILURE/PROBLEM						
			27 -						

TABLE B-3. (continued)

SYSTEMS	
CODE	PWR
A	AUXILIARY FEED
B	CONTAINMENT ISOLATION (INCL PENETRATIONS)
CDE	CONTAINMENT SPRAY INJECTION
EFF	CHEMICAL VOLUME CONTROL (MAKE-UP & BORON)
G	HIGH PRESSURE COOLANT INJECTION
H	COMPONENT COOLING WATER
I	REACTOR COOLANT LOW PRESSURE COOLANT INJECTION (RHR)
J	LOW PRESSURE COOLANT INJECTION (LHR)
KLN	NONSAFETY-RELATED SYSTEM UNKNOWN/NOT APPLICABLE
M	CONTAINMENT FAN COOLING SYSTEM
N	SERVICE WATER
O	CONDENSATE AND FEED
PQR	CONDENSATE AND FEED
ST	CONDENSATE AND FEED
UVW	MAIN STEAM
XYZ	REACTOR PROTECTION (PPS)
Z	CONTAINMENT AIR/EFFLUENT PURIF./PURIF./SAMPLE.
	FAILED FUEL ELEMENT DETECTION

APPENDIX C
ESTIMATED FAULT RATES

APPENDIX C ESTIMATED FAULT RATES

This appendix presents estimated fault rates for each type of valve and failure mode listed in Table 1 of the main text. One-line summaries for each group of valves accompany the associated rates. To facilitate checking for possible common cause events, underscores are used to separate unrelated lines. Lines not so separated describe events that occurred at the same plant on the same date. This appendix also contains some tabular summaries of the data, giving the total numbers of various kinds of faults.

Except for the common cause coding, the letter and number codes printed in the one-line summaries here and in Appendix D all have the same meanings as in Reference 1 from the main text. The codes are briefly explained in a table in Appendix B. In the one-line summaries, the following information is given on each line:

Vendor This code tells whether the plant was designed by Babcock & Wilcox, Combustion Engineering, Westinghouse, or General Electric.

Plant This is a three-character code identifying the plant.

Control Number This is the unique six-digit identifier assigned to the LER. If a single LER refers to more than one valve or more than one date, the control number for this line has another character appended: an asterisk, or a letter A, B, C, etc.

Failure Date The month, day, and year are given.

System This code identifies the system to which the valves belong, such as containment spray, high pressure coolant injection, etc.

Component This tells whether the valves are air-operated, remote/motor-operated, or manually operated, or check, safety, or relief valves.

Failure Mode and Cause These codes classify the kind of fault. For example, the code for failure mode might mean "does not open," whereas the code for cause might mean "personnel error--maintenance."

Type This code tells whether the event is a failure or a command fault, whether it is an individual fault or caused by a common cause shock, and whether it is recurrent or not.

Failure Number This tells the number of valves that failed or, for a single valve, the number of times it failed as reported by this line.

Activity This tells when the fault was discovered, for example, during normal operation, during maintenance, etc.

Mode Description and Cause Description These are very condensed narratives from the LER.

Air-Operated Valves

There are 22 LERs involving air-operated valves. Eighteen of the events are coded failure to open, failure to close, or failure to operate. These are pooled into an estimated rate for failure to open, close, or operate. Rates are also presented for the modes internal leakage, failure to remain open (plugged), and improper valve configuration. No common cause events occurred in internal leakage or in failure to remain open, so most quantities cannot be estimated. Those that are estimated remain the same for all faults and for failures only; thus, they are presented only once. Rates are estimated for common cause command faults involving improper valve configuration; any event involving improper valve lineup is considered a common cause event and a command fault rather than a failure. One event in this failure mode was observed. Rates for each failure mode are presented first, followed by a summary table of faults in all modes and a listing of one-line descriptions of the LERs.

AIR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE
ALL FAULTS - BOTH FAILURES AND CUE LAND FAULTS

RATES ARE PER CALENDAR HOUR

TRIPLE OF NUMBERS SHOWS LOWER, IND, POINT ESTIMATE, UPPER BOUND)

LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

ESTIMATES ARE BASED ON DATA WITH N = 1, 2, 3, 4, 5, 6, 7, 8, 10, 14, 22, 25, 32, 85
THEY ARE SHOWN FOR FEWER VALUES OF N

$$P = (.002, .160, .490)$$

LAMADA = (1.9E-11, 1.3E-06, 6.5E-06)

LAMADA+ = (4.4E-08, 3.7E-07, 9.7E-07)

OMEGA = (4.9E-10, 1.2E-07, 4.8E-07)

SYSTEM SIZE M SHOCK RATE MU RATE FOR SPECIFIC COMPONENT R1

1	(2.4E-07, 2.8E-04, 1.4E-04)	(1.7E-07, 1.8E-05, 8.9E-06)	(1.003, * 165, * 503)	
2	(1.5E-07, 1.4E-04, 7.3E-05)	(1.1E-07, 1.7E-05, 8.7E-06)	(1.003, * 197, * 595)	
3	(1.1E-07, 9.2E-05, 4.8E-05)	(8.7E-08, 1.6E-05, 8.7E-06)	(1.003, * 206, * 615)	
4	(9.8E-08, 6.9E-05, 3.6E-05)	(7.3E-08, 1.6E-06, 8.7E-06)	(1.003, * 206, * 615)	
7	(7.7E-08, 4.0E-05, 2.1E-05)	(5.3E-08, 1.5E-06, 8.6E-06)	(1.002, * 196, * 694)	
8	(7.3E-08, 3.5E-05, 1.8E-05)	(5.0E-08, 1.5E-06, 8.6E-06)	(1.002, * 191, * 702)	
10	(6.8E-08, 2.8E-05, 1.5E-05)	(4.5E-08, 1.5E-06, 8.6E-06)	(1.002, * 182, * 731)	
32	(5.4E-08, 8.7E-06, 4.8E-06)	(3.4E-08, 1.5E-06, 8.6E-06)	(1.001, * 156, * 839)	
85	(4.9E-09, 3.6E-06, 2.1E-06)	(3.2E-08, 1.5E-06, 8.6E-06)	(1.001, * 151, * 853)	

OVERALL (4.9E-08, 4.0E-05, 1.4E-04) (3.2E-08, 1.5E-06, 8.9E-06) (1.001, * 191, * 863)

SYSTEM SIZE M RATE FOR SET OF K SPECIFIC COMPONENTS R4

2	(2.2E-09, 1.6E-07, 5.3E-07)	(8.0E-10, 1.3E-07, 4.9E-07)	(6.1E-10, 1.3E-07, 4.9E-07)	
3	(1.7E-09, 1.5E-07, 5.2E-07)	(7.7E-10, 1.3E-07, 4.9E-07)	(6.0E-10, 1.3E-07, 4.9E-07)	
4	(1.5E-09, 1.5E-07, 5.2E-07)	(7.3E-10, 1.3E-07, 4.9E-07)	(6.0E-10, 1.3E-07, 4.9E-07)	
7	(1.2E-09, 1.5E-07, 5.1E-07)	(7.2E-10, 1.3E-07, 4.9E-07)	(6.0E-10, 1.3E-07, 4.9E-07)	
9	(1.2E-09, 1.5E-07, 5.1E-07)	(7.2E-10, 1.3E-07, 4.9E-07)	(6.0E-10, 1.3E-07, 4.9E-07)	
10	(1.2E-09, 1.4E-07, 5.1E-07)	(7.1E-10, 1.3E-07, 4.9E-07)	(6.0E-10, 1.3E-07, 4.9E-07)	
32	(1.1E-09, 1.4E-07, 5.1E-07)	(7.1E-10, 1.3E-07, 4.9E-07)	(6.0E-10, 1.3E-07, 4.9E-07)	
85	(1.1E-09, 1.4E-07, 5.1E-07)	(7.1E-10, 1.3E-07, 4.9E-07)	(6.0E-10, 1.3E-07, 4.9E-07)	

OVERALL (1.1E-09, 1.5E-07, 5.3E-07) (7.1E-10, 1.3E-07, 4.9E-07) (6.0E-10, 1.3E-07, 4.9E-07)

AIR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE
FAILURES ONLY
RATES ARE PER CALENDAR HOUR
TRIPLE OF NUMBERS SHOWS LOWER ROUND, POINT ESTIMATE, UPPER ROUND,
LOWER AND UPPER QUINTILES FORM 90 PERCENT INTERVAL

LAMBDA = { 9.3E-12, 4.8E-07, 2.3E-06 }
LAMBDA = { 4.9E-10, 1.2E-07, 4.8E-07 }
OMEGA = { 4.0E-10, 1.2E-07, 4.8E-07 }

NO DATA WERE OBSERVED FOR ESTIMATING OTHER QUANTITIES

ALL OPERATED VALUES - INTERNAL LEAKAGE

ALL FAULTS - BOTH FAILURES AND COMMAND FAULTS

RATES ARE PER CALENDAR HOUR

TRIPLE OF NUMBERS SHOWS LOWER ROUND, POINT ESTIMATE, UPPER ROUND
LOWER AND UPPER ROUNDS FORM 90 PERCENT INTERVAL

LAMBDA = { 2.2E-13, 1.8E-07, 9.2E-07}

LAMBDA = { 4.9E-10, 1.2E-07, 4.8E-07}

OMEGA = { 4.9E-10, 1.2E-07, 4.8E-07}

NO DATA WERE RESERVED FOR ESTIMATING OTHER QUANTITIES

AIR OPERATED VALVES - FAILURE TO REMAIN OPEN (PLUGGED)

ALL FAULTS - BOTH FAILURES AND COMMAND FAULTS

RATES ARE PER CALENDAR HOUR

TRIPLE OF NUMBERS SHOWS (LOWER BOUND, POINT ESTIMATE, UPPER BOUND)

LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

LAMRDA = { 1.0E-10, 2.6E-08, 9.9E-08}

LAMBDA + = { 4.9E-10, 1.7E-07, 4.8E-07}

OMEGA = { 4.9E-10, 1.2E-07, 4.8E-07}

NO DATA WERE OBSERVED FOR ESTIMATING OTHER QUANTITIES

AIR OPERATED VALVES - IMPROPER VALVE CONFIGURATION
 COMMON CAUSE COMMAND FAULTS ONLY
 RATES ARE PER CALENDAR HOUR

TRIPLE OF NUMBERS SHOWS LOWER BOUND, POINT ESTIMATE, UPPER BOUND)

LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL
 ESTIMATES ARE BASED ON DATA WITH M = 1, 2, 3, 4, 5, 6, 7, 8, 10, 14, 22, 25, 32, 85
 THEY ARE SHOWN FOR FEWER VALUES OF M

$$P = (*157, *586, *934)$$

$$\begin{aligned} \text{LAMBDA} &= (4.4E-09, 3.7E-07, 9.7E-07) \\ \text{OMEGA} &= (4.9E-10, 1.2E-07, 4.6E-07) \end{aligned}$$

SYSTEM SIZE M	SHOCK PATH MU	RATE FOR SPECIFIC COMPONENT		BETA FACTOR
		Q1	Q2	
1	(7.3E-08, 1.0E-06, 2.9E-06)	(8.9E-08, 6.2E-07, 1.2E-06)		
2	(5.6E-08, 6.4E-07, 1.7E-06)	(6.7E-08, 5.2E-07, 9.6E-07)	(3.51, *684, *941)	
3	(5.1E-08, 5.3E-07, 1.4E-06)	(5.7E-08, 4.9E-07, 9.1E-07)	(*252, *532, *651)	
4	(4.9E-09, 4.8E-07, 1.2E-06)	(5.2E-08, 4.1E-07, 9.0E-07)	(*154, *422, *642)	
7	(4.6E-08, 4.2E-07, 1.1E-06)	(4.5E-08, 4.1E-07, 8.9E-07)	(*102, *267, *656)	
8	(4.6E-08, 4.1E-07, 1.1E-06)	(4.4E-08, 4.7E-07, 8.9E-07)	(*098, *258, *557)	
10	(4.5E-09, 4.0E-07, 1.0E-06)	(4.3E-08, 4.7E-07, 8.9E-07)	(*094, *249, *650)	
32	(4.4E-09, 3.8E-07, 9.8E-07)	(4.0E-08, 4.7E-07, 8.9E-07)	(*088, *241, *556)	
85	(4.4E-09, 3.7E-07, 9.8E-07)	(3.9E-08, 4.7E-07, 8.9E-07)	(*088, *241, *545)	
OVERALL	(4.4E-09, 4.2E-07, 2.9E-06)	(3.9E-08, 4.7E-07, 1.2E-06)	(*088, *241, *541)	

SYSTEM SIZE M	R2	RATE FOR SET OF K SPECIFIC COMPONENTS		
		Q3	Q4	
2	(2.4E-09, 2.9E-07, 7.9E-07)			
3	(2.0E-08, 2.8E-07, 7.8E-07)	(7.9E-09, 2.4E-07, 7.1E-07)		
4	(1.7E-08, 2.8E-07, 7.7E-07)	(7.3E-09, 2.4E-07, 7.0E-07)	(4.1E-09, 2.1E-07, 6.6E-07)	
7	(1.5E-08, 2.8E-07, 7.7E-07)	(6.8E-09, 2.4E-07, 7.0E-07)	(3.9E-09, 2.1E-07, 6.6E-07)	
8	(1.5E-08, 2.8E-07, 7.7E-07)	(6.7E-09, 2.4E-07, 7.0E-07)	(3.9E-09, 2.1E-07, 6.6E-07)	
10	(1.5E-08, 2.7E-07, 7.7E-07)	(6.7E-09, 2.4E-07, 7.0E-07)	(3.9E-09, 2.1E-07, 6.6E-07)	
32	(1.4E-08, 2.7E-07, 7.7E-07)	(6.6E-09, 2.4E-07, 7.0E-07)	(3.9E-09, 2.1E-07, 6.6E-07)	
85	(1.4E-08, 2.7E-07, 7.7E-07)	(6.6E-09, 2.4E-07, 7.0E-07)	(3.9E-09, 2.1E-07, 6.6E-07)	
OVERALL	(1.4E-08, 2.8E-07, 7.9E-07)	(6.6E-09, 2.4E-07, 7.1E-07)	(3.9E-09, 2.1E-07, 6.6E-07)	

AIR-OPERATED VALVES

PLANT	HOURS	POP	NUMBER OF INDIV. FAULTS /COM FLTS	VALVES AFFECTED BY NONLETHAL SHOCKS FAILERS/COM FLTS	NUMBER OF LETHAL SHOCKS FAILERS/COM FLTS	VALVES AFFECTED BY LETHAL SHOCKS FAILERS/COM FLTS	
						/	/
ARI	43800	2	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CR3	34704	1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
081	28944	14	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0
0E1	43800	4	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
0E2	43800	4	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
0E3	43800	8	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0
111	28368	3	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
T12	9736	4	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0
AR2	18120	6	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CC1	43800	6	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CC2	35784	6	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0
FC1	43800	37	0 / 0	0 / 1	0 / 1	0 / 0	0 / 0
M12	43800	6	2 / 0	0 / 0	0 / 0	0 / 0	0 / 0
HY1	43800	25	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PA1	43800	6	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0
SL1	41112	7	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BV1	40656	3	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DC1	43800	30	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DC2	24600	30	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0
HN1	43800	4	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
IP2	43800	4	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
IP3	41472	8	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
JF1	29712	11	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0
NA1	23976	6	0 / 1	0 / 1	0 / 2	0 / 0	0 / 0
NA2	4872	6	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PR1	43800	6	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PR2	43800	6	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PT1	43800	7	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PT2	43800	7	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
RG1	43800	7	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0

R02	43800	11	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SA1	35496	18	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SE1	4320	105	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SO1	43800	7	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SU1	43800	3	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0
SU2	43800	3	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TU3	43800	8	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TU4	43800	6	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
YR1	43800	2	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0
ZI1	43800	12	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0
ZI2	43800	12	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BR1	37032	4	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BR2	43800	4	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CO1	43800	7	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DA1	43800	10	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
EN1	43800	13	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
FN2	21816	15	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
FP1	43800	9	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
MI1	43800	8	0 / 4	0 / 0	0 / 0	0 / 0	0 / 0
MO1	43800	7	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
NM1	43800	13	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0
DC1	43800	7	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PB2	43800	5	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PB3	43800	5	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PI1	43800	5	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
QC1	43800	6	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0
QC2	43800	6	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
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All	2211720	587	11 / 11	0 / 2	0 / 3	0 / 0	0 / 0

AIR-OPERATED VALVES

Y E A R N T	P L A N T	C O N T R O L N U M B R	E V E N T D A T E	S Y S T E M C O M P E	C A U S E O U T P E	F A I L U T P E	A C T I V I T Y N U M B R		
								MODE DESCRIPTION	CAUSE DESCRIPTION
B ARI 020607	011378	B AV A23	0	T	VALVE CV-2667 FAILED TO OPEN REMOTELY			TORQUE SWITCH DEFECTIVE	
B DB1 030931	041080	I AV A12	1	N	DHR COOLER OUTLET VLV WOULD NOT OPEN COMPLETELY			RADIUS ARM OUT OF ADJUSTMENT	
B DE3 020064	010378	L AV F12	1	T	VALVE 3LP-14 FAILED TO CYCLE MANUALLY			MECH PARTS LOOSE+OUT OF ALIGN	
B T12 021277	040478	I AV A24 S	1	T	RHR ADV (NS-VB3G) FAILED TO OPEN DURING TEST			FAILURE OF SOLENOID OPERATED PILOT VALVE	
C CCC2 033265	111080	O AV B24 S	1	N	SI-661-CV FAILED TO CLOSE			SOLENOID AIR VLV CONTROLLING AIR FAILED	
C FC1 022469	092178	B AV A24 U	1	T	VAL YCV-1045 FAILED TO OPEN(AUX.FD.PMPSTM.INL.)			INSTRUMENT AIR SUPPLY TO VAL CLOSED	
C M12 027976*	122879	O AV F00	2	T	HPSI INJ.VLV. 2-SI-6166626 OVERTRAVELLED 3%			NO CAUSE FOUND FOR FAILURE	
C PA1 020231	010878	O AV A24 S	1	U	VALVE CV-3025 FAILED IN CLOSED POSITION			WATER IN AIR LINE TO VALVE OPERATOR	
W DC2 022838A	101078	B AV C00	1	U	PNEUMATIC TEST VALVE LEAKED THRU			UNKNOWN	
W JF1 031513	052880	L AV B12	1	T	1A RHR HEAT EXCH DISCHARGE VLV FAILED TO CLOSE			CAP SCREW CONNECT STEM AND OP CAME OUT	
W NAI 020872	031478	H AV F16 S	1	N	LET DOWN TRIP VALVE OUTSIDE ISOLATION CLOSED SPUR			SHORT IN VALVE CIRCUIT CAUSED VLV TO SHUT	
W NAI 021506	051478	B AV V06 U	2	T	AUX FEEDWATER VALS PCV-F2-159A,-159B IMP.LINEUP			CHECKOFF SHEET DOES NOT LIST NORM VAL POS	
W SAI 022422	082478	B AV A12	1	T	AUX FEED PUMP STEAM VLV (1MS132) FAILED TO OPEN			STEM WAS FOUND DISENGAGED FROM ACTUATOR	
W SUI 030321	020680	I AV B24 S	1	N	HCV-1852A DELAYED IN CLOSING WHILE RECIRC ACCUMU.			RELIEVED TO BE MOISTURE IN AIR LINES	
W YR1 033661	122780	I AV F27 R	1	N	SI-PR-59 VLV CONTROLLED PRESSURE TOO HIGH			SETPOINT DRIFT OF REGULATING PILOT	
W ZII 016047A	091676	I AV C25	1	N	NITROGEN VALVE (1HCV-SI943) LEAKED THRU			LEAKING SEAT OF AO PLUG VALVE	
G MII 014290	021276	H AV F24 T	1	N	1 OF 2 FEEDWTR.REG.VLVs LOCK-IN THE AS IS POSITION			FAILURE IN 3 WAY PRESSURE REGULATOR	
G MII 018414	071377	H AV F24 T	1	U	"B" FEEDWTR.REG.VLV EXPERIENCED CONTROL PROBLEMS			FAILURE CAUSED BY DIA.FAIL.IN SUP.SYS.VLV	
G MII 018625*	080677	H AV F24 T	2V	N	FEEDWTR.REG.VLVs. LOCKED UP "AS IS"			LOSS OF INSTRUMENT AIR PRESS.CAUSED FAIL.	
G NM1 033594	121680	I AV F24 S	1	N	#11 FEEDWATER FLOW CONTROL VLV POSITIONER UNIT HAD //EXCESS AIR VENTING FROM IT. PARTS REPL.				
G PB3 014035	010776	H AV C25	1	T	HPCI EXHAUST LINE DRAIN VLV AD-5248 -EXCESS.LEAK.			POOR MATING BETWEEN PLUG & SEATING SURF.	
G QC1 018106	041277	L AV B24 S	1	T	DRAIN VALVE FAILED TO CLOSE/COMMAND FAULT			AIR SUPPLY SV FAILED/AIR WOULDNT VENT OFF	

Check Valves

Fifty LERs involve faults of check valves. The majority of events are coded either failure to close or reverse leakage. In both modes, backflow results. If the backflow is extensive, the event is coded failed to close; otherwise, it is coded reverse leakage. It is often difficult to determine from the LER how extensive the backflow was; for this reason, and because the consequence is the same, i.e., backflow results, the two modes are combined to estimate one rate. Similarly, the modes failure to open and failure to remain open are combined. The consequence of either mode is the same: the valve is closed when it is required to be open and allowing flow.

Rates are not estimated in check valves for failure to operate or improper valve configuration. Any LERs involving these modes, however, are included in the summary table of faults and in the listing of one-line descriptions.

CHECK VALUES - FAILURE TO OPEN OR REMAIN OPEN (PLUGGED)

ALL FAULTS - BOTH FAILURES AND COMMAND FAULTS

RATES ARE PER CALENDAR HOUR

TRIPLE OF NUMBERS SHOWS LOWER BOUND, POINT ESTIMATE, UPPER BOUND

LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

ESTIMATES ARE BASED ON DATA WITH $M = \frac{1}{2}, \frac{2}{3}, \frac{3}{4}, \frac{5}{6}, \frac{7}{8}, \frac{9}{10}, \frac{11}{12}, \frac{13}{14}, \frac{15}{16}, \frac{17}{18}, \frac{19}{20}, \frac{21}{22}, \frac{23}{24}, \frac{25}{26}$

THEY ARE SHOWN FOR FEWER VALUES OF M

$$P = 1 - 0.35 \cdot e^{-203} \cdot 440$$

$$\text{LAMBDA} = \{ 5.6E-09, 2.5E-08, 5.4E-08 \}$$

$$\text{LAMBDA}_+ = \{ 2.5E-08, 2.1E-07, 5.5E-07 \}$$

$$\text{OMEGA}_+ = \{ 2.8E-10, 7.0E-08, 2.7E-07 \}$$

SYSTEM SIZE M	SHOCK RATE		RATE FOR SPECIFIC COMPONENT R_1	BEVIA FACTOR
	MU	MU		
1	1.1E-07	2.2E-06	6.9E-06	7.3E-08
2	6.7E-08	1.2E-06	3.5E-06	5.2E-08
3	5.2E-08	8.2E-07	2.4E-06	4.2E-08
4	4.4E-08	6.5E-07	1.9E-06	3.7E-08
1.8	2.8E-08	2.7E-07	7.1E-07	2.5E-08
1.9	2.7E-08	2.7E-07	7.0E-07	2.5E-08
2.6	2.6E-08	2.5E-07	6.4E-07	2.4E-08
3.4	2.6E-08	2.4E-07	6.1E-07	2.4E-08
5.0	2.5E-08	2.2E-07	5.8E-07	2.4E-08
OVERALL	{ 2.5E-08, 2.7E-07, 6.9E-06 }	{ 2.4E-08, 1.4E-07, 6.9E-07 }	{ 1.012, .337, .741 }	

SYSTEM SIZE M	RATE FOR SET OF K SPECIFIC COMPONENTS		R4
	R2	R3	
2	1.23E-09	9.5E-08	3.0E-07
3	1.16E-09	9.0E-08	3.0E-07
4	1.13E-09	8.7E-08	2.9E-07
18	1.87E-10	8.2E-08	2.9E-07
19	1.87E-10	8.2E-08	2.9E-07
26	1.85E-10	8.2E-08	2.9E-07
34	1.85E-10	8.2E-08	2.9E-07
50	1.84E-10	8.2E-08	2.9E-07
OVERALL	{ 8.4E-10, 8.2E-08, 3.0E-07 }	{ 4.3E-10, 7.4E-08, 2.8E-07 }	{ 3.4E-10, 7.2E-08, 2.7E-07 }

CHECK VALUES - FAILURE TO OPEN OR TO REMAIN OPEN (PLUGGED)

FAILURES ONLY

RATES ARE PER CALENDAR HOUR

TRIPLE OF NUMBERS SHOWS LOWER BOUND, POINT ESTIMATE, UPPER BOUND

LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

ESTIMATES ARE BASED ON DATA WITH $M = 27, 28, 30, 32, 34, 36, 42, 45, 47, 49, 50$

THEY ARE SHOWN FOR FEWER VALUES OF M

$P = (.035, .273, .440)$

LAMBDA = (5.6E-09, 2.5E-08, 5.4E-08)

LAMBDA+ = (2.5F-09, 2.1E-07, 5.5E-07)

OMEGA+ = (2.0E-10, 7.0E-08, 2.7E-07)

SYSTEM
SIZE
 M

SHOCK
RATE
MIJ

RATE FOR
SPECIFIC COMPONENT
R1

BETA FACTOR

1 (1.1E-07, 2.2E-06, 6.9E-06) (7.3E-08, 3.1E-07, 6.9E-07)

2 (6.7E-08, 1.2E-06, 3.5E-06) (5.2E-08, 2.1E-07, 4.8E-07) (0.056, .310, .525)

3 (5.2E-08, 8.2E-07, 2.4E-06) (4.2E-08, 1.0E-07, 4.3E-07) (0.074, .401, .608)

4 (4.4E-08, 6.5F-07, 1.9E-06) (3.7E-08, 1.7E-07, 4.0E-07) (0.079, .436, .637)

18 (2.8E-08, 2.7E-07, 7.1E-07) (2.5E-08, 1.4E-07, 3.6E-07) (0.019, .361, .740)

19 (2.7E-08, 2.1F-07, 7.0E-07) (2.5E-08, 1.4E-07, 3.6E-07) (0.018, .337, .741)

26 (2.6E-08, 2.5E-07, 6.4E-07) (2.4E-08, 1.4E-07, 3.6E-07) (0.015, .323, .737)

34 (2.6F-08, 2.4E-07, 6.1E-07) (2.4E-08, 1.4E-07, 3.6E-07) (0.013, .316, .731)

50 (2.5E-08, 2.2E-07, 5.8E-07) (2.4E-09, 1.4E-07, 3.6E-07) (0.012, .310, .719)

OVERALL (2.5E-08, 2.7E-07, 6.9E-06) (2.4E-08, 1.4E-07, 6.9E-07) (0.012, .337, .741)

SYSTEM
SIZE
 M

R2

RATE FOR SET OF K SPECIFIC COMPONENTS

R3

R4

RATE FOR SET OF K SPECIFIC COMPONENTS

2 (2.3E-07, 9.5F-08, 3.0E-07)	(5.3E-10, 7.6E-08, 2.9E-07)	(3.5E-10, 7.2E-09, 2.7E-07)
3 (1.6E-07, 9.0F-08, 3.0E-07)	(4.9E-10, 7.5E-08, 2.8E-07)	(3.4E-10, 7.2E-09, 2.7E-07)
4 (1.3E-07, 8.7E-08, 2.9E-07)	(4.4E-10, 7.4E-08, 2.8E-07)	(3.4E-10, 7.2E-09, 2.7E-07)
18 (8.7E-10, 8.2F-08, 2.9E-07)	(4.4E-10, 7.4E-08, 2.8E-07)	(3.4E-10, 7.2E-09, 2.7E-07)
19 (8.7E-10, 8.2E-08, 2.9E-07)	(4.4E-10, 7.4E-08, 2.8E-07)	(3.4E-10, 7.2E-09, 2.7E-07)
26 (8.5E-10, 8.2E-08, 2.9E-07)	(4.3E-10, 7.4E-08, 2.7E-07)	(3.4E-10, 7.2E-09, 2.7E-07)
34 (8.5E-10, 8.2E-08, 2.9E-07)	(4.3E-10, 7.4E-08, 2.7E-07)	(3.4E-10, 7.2E-09, 2.7E-07)
50 (8.4E-10, 8.2E-08, 2.9E-07)	(4.3E-10, 7.4E-08, 2.7E-07)	(3.4E-10, 7.2E-09, 2.7E-07)

OVERALL (8.4E-10, 8.2E-08, 3.0E-07) (4.3E-10, 7.4E-08, 2.8E-07) (3.4E-10, 7.2E-09, 2.7E-07)

CHECK VALUES - FAILURE TO CLOSE / REVERSE LEAKAGE

FAILURES ONLY

RATES ARE PER CALENDAR HOUR

TRIPLE OF NUMBERS SHOWS LOWER BOUND, POINT ESTIMATE, UPPER BOUND

LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

ESTIMATES ARE BASED ON DATA WITH $M = 27, 28, 30, 32, 34, 36, 42, 45, 47, 49, 50$

THEY ARE SHOWN FOR FEWER VALUES OF N

$P = (.002, .187, .567)$

LAMBDA = (2.6E-09, 5.5E-07, 2.1E-06)

LAMBDA+ = (2.5E-08, 2.1E-07, 5.5E-07)

OMEGA+ = (2.8E-10, 7.0E-08, 2.7E-07)

SYSTEM SIZE N	SHOCK RATE MU	RATE FOR SPECIFIC COMPONENT		BETA FACTOR
		R1	R2	
1	(1.2E-07, 1.6E-04, 7.6E-05)	(1.3E-07, 8.4E-07, 2.4E-06)		
2	(7.2E-08, 7.9E-05, 3.8E-05)	(9.1E-08, 7.4E-07, 2.3E-06)	(.003, .129, .484)	
3	(5.8E-08, 5.3E-05, 2.6E-05)	(7.5E-08, 7.1E-07, 2.3E-06)	(.004, .144, .546)	
4	(5.0E-08, 4.0E-05, 1.9E-05)	(6.6E-08, 7.0E-07, 2.3E-06)	(.004, .143, .576)	
18	(3.2E-08, 9.0E-06, 4.4E-06)	(4.4E-08, 6.7E-07, 2.2E-06)	(.001, .104, .687)	
19	(3.2E-08, 8.5E-06, 4.2E-06)	(4.4E-08, 6.7E-07, 2.2E-06)	(.001, .103, .698)	
26	(3.1E-08, 6.3E-06, 3.1E-06)	(4.2E-08, 6.7E-07, 2.2E-06)	(.001, .100, .693)	
34	(3.0E-08, 4.8E-06, 2.4E-06)	(4.2E-08, 6.7E-07, 2.2E-06)	(.001, .098, .692)	
50	(2.8E-08, 3.3E-06, 1.7E-06)	(4.1E-08, 6.7E-07, 2.2E-06)	(.001, .096, .690)	
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OVERALL	(2.8E-08, 9.0E-06, 7.6E-05)	(4.1E-08, 6.7E-07, 2.4E-06)	(.001, .104, .693)	
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SYSTEM SIZE N	RATE FOR SET OF K SPECIFIC COMPONENTS			
	R2	R3	R4	
2	(1.4E-09, 9.5F-08, 3.1F-07)			
3	(1.1E-C9, 9.0F-08, 3.0E-07)	(5.1E-10, 7.8E-08, 2.8E-07)		
4	(9.6E-10, 8.8F-08, 3.0E-07)	(4.9E-10, 7.8E-08, 2.8E-07)	(3.8E-10, 7.4E-08, 2.9E-07)	
18	(7.1E-10, 8.5F-08, 3.0E-07)	(4.5E-10, 7.7E-08, 2.8E-07)	(3.7E-10, 7.4E-08, 2.8E-07)	
19	(7.1E-10, 8.5F-08, 3.0E-07)	(4.5E-10, 7.7E-08, 2.8E-07)	(3.7E-10, 7.4E-08, 2.8E-07)	
26	(7.0E-10, 8.5F-08, 3.0E-07)	(4.5E-10, 7.7E-08, 2.8E-07)	(3.7E-10, 7.4E-08, 2.8E-07)	
34	(6.9E-10, 8.5F-08, 3.0E-07)	(4.5E-10, 7.7E-08, 2.8E-07)	(3.7E-10, 7.4E-08, 2.8E-07)	
50	(6.9E-10, 8.5F-08, 3.0E-07)	(4.5E-10, 7.7E-08, 2.8E-07)	(3.7E-10, 7.4E-08, 2.8E-07)	
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OVERALL	(6.9E-10, 8.5F-08, 3.0E-07)	(4.5E-10, 7.7E-08, 2.8E-07)	(3.7E-10, 7.4E-08, 2.8E-07)	

OVERALL (6.9E-10, 8.5F-08, 3.0E-07)

(4.5E-10, 7.7E-08, 2.8E-07) (3.7E-10, 7.4E-08, 2.8E-07)

CHECK VALVES

PLANT	HOURS	FOP	NUMBER OF INDIV. FAULTS /COM FLTS		VALVES AFFECTED BY NONLETHAL SHOCKS FAILRS/COM FLTS /		VALVES AFFECTED BY LETHAL SHOCKS FAILRS/COM FLTS /		VALVES AFFECTED BY LETHAL SHOCKS FAILRS/COM FLTS /	
			/	/	/	/	/	/	/	/
ARI	43800	29	0	0	0	0	0	0	0	0
CR3	34704	40	1	0	0	1	0	0	0	0
DR1	28944	39	3	0	0	0	0	0	0	0
DE1	43800	29	1	0	0	0	0	0	0	0
DE2	43800	30	0	0	0	0	0	0	0	0
DE3	43800	30	1	0	0	1	0	0	0	0
RS1	43800	56	0	0	0	0	0	0	0	0
T11	28369	38	0	0	0	0	0	0	0	0
T12	8736	41	0	0	0	0	0	0	0	0
AR2	18120	59	0	0	0	0	0	0	0	0
CC1	43800	53	0	0	0	0	0	0	0	0
CC2	35784	53	2	0	0	0	0	0	0	0
FC1	43800	49	0	0	1	0	0	0	0	0
M12	43800	51	3	0	0	0	0	0	0	0
NY1	43800	57	0	0	0	0	0	0	0	0
PA1	43800	27	0	0	0	0	0	0	0	0
SL1	41112	49	0	0	0	0	0	0	0	0
BV1	40656	46	3	0	0	0	0	0	0	0
DC1	43800	56	0	0	0	0	0	0	0	0
DC2	24600	56	1	0	1	0	2	0	0	0
HN1	43800	35	2	0	0	0	0	0	0	0
IP2	43800	54	1	0	0	0	0	0	0	0
IP3	41472	68	0	0	0	0	0	0	0	0
JF1	29712	59	0	0	0	0	0	0	0	0
KE1	43800	43	1	0	0	0	0	0	0	0
NA1	23976	47	0	0	0	0	0	0	0	0
NA2	4872	47	1	0	0	0	0	0	0	0
PR1	43800	39	0	0	0	0	0	0	0	0
PR2	43800	39	0	0	0	0	0	0	0	0
PT1	43800	47	0	0	0	0	0	0	0	0

PT2	43800	47	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
RG1	43800	33	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
RO2	43800	35	2 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SA1	39496	55	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SE1	43220	71	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SO1	43800	30	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SU1	43800	48	3 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SU2	43800	48	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TR1	43800	43	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TU3	43800	41	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TU4	43800	41	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
YR1	43800	21	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
ZT1	43800	69	2 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
ZT2	43800	69	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BF1	43800	35	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BF2	43800	35	3 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BF3	38496	35	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BR1	37032	38	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BR2	43800	38	2 / 0	0 / 0	0 / 1	0 / 0	0 / 0	0 / 0
CO1	43800	12	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DA1	43800	21	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DR2	43800	24	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DR3	43800	24	2 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
EN1	43800	44	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
EN2	21816	30	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
FP1	43800	8	4 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
MT1	43800	9	4 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PO1	43800	33	2 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
NM1	43800	25	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
OC1	43800	25	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
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All	2600616	2649	57 / 0	2 / 3	3 / 4	0 / 0	0 / 0	0 / 0

CHECK VALVES

V E N T	P L A N T	C O N T R O L N U M B R	E V E N T D A T E	S Y S T E M C O D E	C A U S E E E	T A Y P E E	F A I L U M N U M B R	A C T I V I T Y	MODE DESCRIPTION		CAUSE DESCRIPTION	
8	CR3	025631	032179	G CV V00 U	1	M	MAKEUP PMP 3-C DISCHG STOP CHK VLV MUV-2 IMPROPERL	POST TUNED--CAUSE UNKNOWN				
B	CR3	031894A	072880	H CV B00	1	T	CHECK VLV CFV-79 FAILED ALLOWING BACKFLOW INTO N2 SYS	CAUSE NOT GIVEN FOR FAILED CHECK VALVE				
B	D81	0209898	031678	B CV E00	2	T	CHECK VLV AF39672 LEAKED INTERNALLY	CAUSE OF REVERSE LEAKAGE NOT GIVEN				
B	D81	032832	100880	H CV E25	1	T	GROSS BACK LEAKAGE DISCOVERED THROUGH CF30	DISK DISENGAGED FROM VALVE BODY				
B	DE1	031621	061880	H CV E00	1	N	BACKLEAKAGE DISCOVERED THROUGH 'B' HPI LINE CHECK VL	NO CAUSE GIVEN				
B	DE3	016209	110176	H CV V01 U	2	M	IMP. LINEUP VALS 3HP-152 + 3HP-153 CLOSED S.B.OPEN	PERSONNEL ERROR				
B	DE3	031086	042380	L CV B00	1	N	CHECK VLV FAILED TO RESEAT AFTER TEST	NO CAUSE GIVEN FOR VLV FAILURE IN ECCS SY				
C	CC2	022246*	090778	H CV E00	2V	N	#2186228 SI.TANK OUTLET CHECK VLVs LEAKING	CAUSE OF REVERSE LEAKAGE NOT GIVEN				
C	FC1	022972	110178	B CV E05 C	1	R	AUX FEED CHECK VALVE FOUND INSTALLED WRONG	CONSTRUCTION ERROR				
C	MI2	017620	040777	H CV E00 R	1	N	INT LEAK OF CV BETW INJECT TK 4 AND PRI COOLANT	CAUSE UNKNOWN				
C	MI2	018740	072177	H CV E00 R	1	N	S.I.HEADER CHECK VLV. 2-SI-648 LEAKING INTERNALLY	NO CAUSE GIVEN				
C	MI2	018971	081677	H CV E00 R	1	N	INT LEAK OF CV BETW INJECT TK 4 AND PRI COOLANT	CAUSE UNKNOWN				
W	BV1	025486	030579	B CV F12	1	N	1C S/G STM SUP CHECK VLV INOPERABLE	NUT AND WASHER ON CHECK VLV WAS MISSING				
W	BV1	028105	091079	L CV G10	1	T	1A LHSI PUMP RECIRC CHK VLV HAD FLOW RESTRICTION	FOREIGN MATERIAL LODGED IN CHECK VLV				
W	BV1	032895	100180	H CV B12 R	1	T	SI PUMP(CH-P-2A) DISCHR CHECK DID NOT RESEAT	ANTI-ROTATION DEVICES BINDING				
W	DC2	020978	031878	B CV B00	1	N	AUX FEED SYS CHECK VALVE FROM S/G 1 STUCK OPEN	UNKNOWN (VALVE 2-FW138-1) ATWOOD & MORRILL				
W	DC2	023030*	112178	F CV A05 C	2	N	CHK.VLV.CTS-127E&W TO THE LOWER CONT.SPRAY NOZL-	-ES INSTALLED BACKWARDS//FABRICATION ERR.				
W	HNI	015218	070576	B CV E00	1	N	CHECK VALVE IN FEED LINE HAD REVERSE LEAKAGE	NO CAUSE GIVEN FOR REVERSE LEAKAGE				
W	HNI	018777	080177	B CV E00	1	T	CHECK VALVE ON AUX FEED PUMP LEAKING INTERNALY	UNKNOWN				
W	TP2	021653	052378	H CV E12	1	T	4 IN SWING CV D.S.OF PUMP 22 LEAKING INTERNALY	TWO HANGER BRACKET BOLTS MISSING				
W	KE1	031613	062480	L CV B00	1	N	RHR SUCTION CHECK VLV FAILED TO CLOSE	CYLING OF PUMPS SEATED CHECK VALVE				
W	MA2	032572	090580	G CV B09	1	T	2-SI-70(BORON INJ RECERC LINE) LEAKED EXCESSIVELY	CORROSION ALLOW SPRING TO DROP OFF PLUG				
W	RG1	018247	071377	H CV E00	1	N	SI PUMP 1A CHECK VALVE REVERSE FLOW TO RWST	UNKNOWN/ VELAN 3 INCH 1500 PSIG CHECK VAL				
W	RD2	014822	012876	H CV E00	1	N	B ACCUMULATOR CHECK VALVE 875E LEAKED THRU	REASON NOT STATED				
W	RD2	019351	081777	B CV E05	1	T	DISCH CK VAL FOR AUX FEED PUMP,C STM GEN FAILED	CK VAL HAS BURR ON HINGE JOINT,OPEN POSIT				

CHECK VALVES

PLANT NUMBER	CONTROL NUMBER	EVENT DATE	SYSTEM TEMP	C OM MON E	C AUSE E	T YPE EL	F AULT UM	ACTIVITY	MODE DESCRIPTION		CAUSE DESCRIPTION	
									MODE	DESCRIPTION	DESCRIPTION	DESCRIPTION
W SAI 033529	121480	H CV 800	1	T	VALVE 115J139 WAS FOUND TO BE COCKED OPEN						NO CAUSE GIVEN FOR LIFT CHECK VALVE FAIL	
W SE1 033789	092780	H CV 805	1	T	CHECK VLV 63-635 STUCK IN OPEN POSITION						INTERFERENCE BETWN DISC WELD AND VLV BODY	
W SU1 015522*	070276	H CV 200	2	T	TWO CHECK VLV 11-SI-128/130 LEAKED THRU						UNKNOWN	
W SU1 030005	010980	B CV 800	1	N	CHECK VLV 1-FW-89 (DISCH AUX FP) FAILED TO CLOSE						CAUSE UNKNOWN	
W SU2 019744	110877	H CV E00	1	N	CHECK VALVE 2-SI-127 LEAKING THRU						UNKNOWN	
W ZII 015162*	062376	H CV E00	2V	N	LEAKAGE THRU CHECK VALVES/ACCUMULATOR OVERFILL						UNKNOWN/DARLING 10 INCH TYPE 10-C48Z	
G BF2 021094	032578	H CV 804	1	M	CHECK VLV. 2-73-603, IN HIGH-PRESS.CI.SYS, FOUND OPEN DIMEN.ERR. IN VLV. INTERFERENCE CLEARANCE							
G BF2 032409	083080	L CV E00 R	1	T	CHECK VLV BETWEEN B&D HEAT EXCHANGERS LEAKING						NO CAUSE STATED "VALVE REPAIRED"	
G BF2 032703	091180	H CV E10	1	T	HPCI CV 2-73-609 FAILED LOCAL LEAK RATE TEST						BUILDOUP OF RESIDUAL MATERIAL COCKED DISC	
G BF3 016055	082476	H CV A00	1	T	CHECK VALVE IN HPCI TURB.EXH.LINE WAS BINDING						CAUSE OF CHECK VLV BINDING NOT STATED	
G BR1 018128	052077	H CV F04	1	T	HPCE STM.LINE EXH,CHECK VLV E41-F049 DETER.FAILED						VLV OSCIL.CAUSED DSC HINGE FAIL;IMP.DESGN	
G BR2 023033	111178	L CV B04	1	N	PHR CHECK VALVE E11-F031 WILL NOT FULLY SEAT						DESIGN ERROR/VLV.DOESN'T WORK ON LOW DP.	
G BR2 032454B	090780	H CV VO1 U	1	T	HPCE MANUAL STOP CHECK FOUND LOCKED CLOSED						PERSONNEL ERROR VLV WAS REQ OPEN	
G BR2 033238	111280	L CV E00	1	N	28 RHR PUMP DISCHRG/E CHECK VLV FAILED TO RESEAT						--FULLY,REVERSE LEAKAGE/NO DETAILS GIVEN	
G DR2 014420	032976	H CV E25	1	T	HPCI VALVE 2-2301-45 LEAKING INTERNALY						CORROSION, PITTING OF LOWER SEATING AREA	
G DR3 016163	100776	L CV E10	1	T	ISOLATION CHECK VALVE 3-1501-258 LEAKING INTERNALY						DIRT AND SMALL SCRATCHES ON VALVE SEAT	
G DR3 016454	110176	L CV E10	1	T	ISOLATION CHECK VALVE 3-205-2-7 LEAKING INTERNALY						DIRT IN SEATING AREA & ON DISK PIVOT PIN	
G EN2 033508	120980	F CV E00 R	1	T	VENT PURGE OUTLET ISO VLV 2T48-F318 LEAKED						CAUSE UNKNOWN	
G FP1 016176	101476	L CV E25	1	N	CHECK VALVE 42B LEAKING INTERNALY						NORMAL WEAR ON VALVE SEAT	
G FP1 020570	030278	L CV B00	1	N	A RHR PUMP CHECK VALVE STUCK OPEN						CAUSE UNKNOWN	
G FP1 023358	122478	L CV B00	1	N	RHR LOOP CHECK VALVE FAILED TO CLOSE						NO REASON FOUND FOR STICKING,REASSEMBLED	
G FP1 026343	063079	L CV F25	1	T	REVERSE ROTATION OF RHR PUMP WAS NOTED DURING TEST						DISCH CHECK VALVE DISC NOT ATTACHED	
G MI1 0207228	032078	U CV E00	4	T	FEED WTR.CK.(1-FW-9A,9B,10A,10B)LEAK,EXCESS OF T.S						CAUSE OF LEAKAGE NOT GIVEN	
G MI1 0304738	022080	D CV E25 R	1	N	CORE SPRAY CHECK VLV LEAKING THRU						SEAT PROBLEM	
G MD1 022808	102078	H CV E10 R	1	T	HPCI-9 TURB EXT LINE CHECK VALVE LEAKING INTERNALY						ACCUMULATED DIRT ON SEATING SURFACES	

CHECK VALVES

P V E N T	CONTROL NUMBER	EVENT DATE	S Y S T E M P	C O M P E D E	C A U S E 2	T Y P E L	F A I L M	N U M Y	A C T I V I T Y	MODE DESCRIPTION	CAUSE DESCRIPTION
G M01 030707	022380	H CV E25 R	1	T	ANCHOR 16-INCH SWING CHECK VLV LEAKING THRU TEST					LOOSE SEAT RING	
G P82 022916	102178	H CV E12	1	N	CHECK VALVE 2-23-131 LEAKING INTERNALLY, GLAND SEAL INTERNALS OF CHECK VALVE WORN OUT						
G P83 014033	010776	H CV E25	1	T	HPCI EXHAUST LINE CHECK VLV 23-65-EXCESSIVE LEAK.					POOR MATING BETWEEN FLAPPER & SEATING SUR	
G QC1 014059	010576	H CV E13	1	T	HPCI EXHAUST CHECK VLV. LEAKING INTERNALLY					DEFECT.GASKET BETWEEN VLV,SEAT AND BODY	
G QC2 020943	030578	L CV E10	1	T	REVERSE FLOW THRU CHECK VALVE 2-220-67A / TESTING					DIRT ACCUMULATED IN VALVE INTERNALS	
G YY1 032650	090480	L CV E12	1	T	D RHR-SW PUMP DISCHARGE CHECK DID NOT SEAT					DEGRADATION OF VLV INTERNALS	

Remote/Motor-Operated Valves

Motor-operated and remotely operated valves are treated as one type of valve. (The section in the main text "Imperfections in the Data" discusses this decision.) Of the 600 LERs used in this analysis, 422 events are reports of remote/motor-operated valve faults. The majority of these events, 393 LERs, are coded as failures to open, failures to close, or failures to operate. These are pooled into an estimated rate for failure to open, close, or operate. The remaining LERs are coded as failures to remain open (plugged), or improper valve configuration. Rates are given for all faults and for failures only, in the modes failure to open, close, or operate, and failure to remain open (plugged). Events involving improper valve configuration, however, are always coded as common cause events and as command faults, rather than failures. Therefore, quantities for this failure mode are presented only for common cause command faults. The estimated rates, summary tables of faults, and listings of one-line descriptions are presented separately for the three failure modes.

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE
ALL FAULTS - BOTH FAILURES AND COMMAND FAULTS

RATES ARE PER CALENDAR HOUR
TRIPLE OF NUMBERS FLOWER BOUND, POINT ESTIMATE, UPPER BOUND)

LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL
ESTIMATES ARE BASED ON DATA WITH N = 29, 30, 31, 32, 35, 36, 37, 39, 40, 43, 44, 45, 49, 50, 52, 56, 58, 12, 13, 14, 15, 16, 17, 18, 20, 23, 24, 25, 27, 28,
THEY ARE SHOWN FOR FEWER VALUES OF M

$$P = (1.016, \quad 0.026, \quad 0.038)$$

LAMBDA = (1.1E-07, 3.8E-06, 1.2E-05)

LAMDA+ = (1.1E-11, 6.0E-06, 3.1E-05)

OMEGA = (2.8E-10, 7.1E-08, 2.7E-07)

SYSTEM SIZE M	SHOCK RATE MU			RATE FOR SPECIFIC COMPONENT R1	RATE FOR SPECIFIC COMPONENT R2	BETA FACTOR
	1	2	3			
1	(4.5E-10, 7.5E-04, 1.3E-03)	(4.0E-07, 9.9E-06, 3.6E-05)				
2	(2.3E-10, 1.3E-04, 6.4E-04)	(3.5E-07, 7.0E-06, 2.3E-05)	(.000, .019, .043)			
3	(1.5E-10, 8.6E-05, 4.4E-04)	(3.2E-07, 6.0E-06, 1.9E-05)	(.000, .026, .074)			
4	(1.2E-10, 6.5E-05, 3.3E-04)	(3.1E-07, 5.5E-06, 1.7E-05)	(.000, .029, .101)			
24	(2.5E-11, 1.4E-05, 6.9E-05)	(2.5E-07, 4.2E-06, 1.4E-05)	(.000, .032, .332)			
25	(2.4E-11, 1.3E-05, 6.7E-05)	(2.5E-07, 4.2E-06, 1.4E-05)	(.000, .032, .336)			
30	(2.1E-11, 1.2E-05, 5.9E-05)	(2.5E-07, 4.2E-06, 1.4E-05)	(.000, .031, .349)			
44	(1.7E-11, 9.2E-06, 4.7E-05)	(2.4E-07, 4.1E-06, 1.3E-05)	(.000, .030, .353)			
58	(1.5E-11, 8.0E-06, 4.1E-05)	(2.4E-07, 4.1E-06, 1.3E-05)	(.000, .029, .335)			
OVERALL	(1.5E-11, 1.4E-05, 1.3E-03)	(2.4E-07, 4.2E-06, 3.6E-05)	(.000, .030, .353)			
SYSTEM SIZE M	RATE FOR SET OF K SPECIFIC COMPONENTS R3			RATE FOR SPECIFIC COMPONENTS R4		
	2	3	4			
2	(1.1E-09, 1.5E-07, 5.5E-07)					
3	(1.6E-09, 1.2E-07, 4.4E-07)	(3.5E-10, 7.3E-08, 2.8E-07)				
4	(1.8E-09, 1.1E-07, 3.8E-07)	(3.3E-10, 7.2E-08, 2.8E-07)	(2.8E-10, 7.1E-08, 2.7E-07)			
24	(7.7E-10, 8.0E-08, 2.9E-07)	(2.9E-10, 7.2E-09, 2.7E-07)	(2.8E-10, 7.1E-08, 2.7E-07)			
25	(7.6E-10, 8.0E-08, 2.9E-07)	(2.9E-10, 7.2E-08, 2.7E-07)	(2.8E-10, 7.1E-08, 2.7E-07)			
30	(7.0E-10, 7.9E-08, 2.9E-07)	(2.9E-10, 7.2E-08, 2.7E-07)	(2.8E-10, 7.1E-08, 2.7E-07)			
44	(6.0E-10, 7.7E-08, 2.8E-07)	(2.9E-10, 7.2E-08, 2.7E-07)	(2.8E-10, 7.1E-08, 2.7E-07)			
58	(5.6E-10, 7.7E-08, 2.8E-07)	(2.9E-10, 7.1E-08, 2.7E-07)	(2.8E-10, 7.1E-08, 2.7E-07)			
OVERALL	(5.6E-10, 8.0E-08, 5.5E-07)	(2.9E-10, 7.2E-08, 2.8E-07)	(2.8E-10, 7.1E-08, 2.7E-07)			

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE
FAILURES ONLY

RATES ARE PER CALENDAR HOUR

TRIPLE OF NUMBERS SHOWS LOWER BOUND, POINT ESTIMATE, UPPER BOUND

LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

ESTIMATES ARE BASED ON DATA WITH $N =$

THEY ARE SHOWN FOR FEWER VALUES OF N $1, 2, 3, 4, 5, 32, 35, 36, 37, 39, 40, 43, 44, 45, 49, 50, 52, 56, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100$

$P = 1.008, .019, .032$

LAMBDA = (7.5E-08, 2.6E-06, 8.5E-06)

LAMBDA, + = (4.1E-23, 3.4E-06, 2.0E-05)

OMEGA = (2.8E-10, 7.1E-08, 2.7E-07)

SYSTEM SIZE N	SHOCK RATE NU			SPECIFIC COMPONENT R1	RATE FOR K SPECIFIC COMPONENTS R2	RATE FOR SET OF K SPECIFIC COMPONENTS R3	BETA FACTOR				
	1	2	3								
1	(2.4E-21, 2.2E-04, 1.2E-03)	(1.4E-07, 6.1E-06, 2.4E-05)									
2	(1.2E-21, 1.1E-04, 6.0E-06)	(1.3E-07, 4.4E-06, 1.6E-05)									
3	(8.0E-22, 7.4E-05, 4.0E-04)	(1.3E-07, 3.9E-06, 1.3E-05)									
4	(6.0E-22, 5.6E-05, 3.0E-04)	(1.3E-07, 3.6E-06, 1.3E-05)									
24	(1.2E-22, 1.1E-05, 6.0E-05)	(1.3E-07, 2.9E-06, 1.0E-05)									
25	(1.2E-22, 1.1E-05, 5.8E-05)	(1.3E-07, 2.9E-06, 1.0E-05)									
30	(1.0E-22, 9.1E-06, 5.0E-05)	(1.3E-07, 2.8E-06, 1.0E-05)									
44	(7.8E-23, 6.9E-06, 3.9E-05)	(1.3E-07, 2.8E-06, 1.0E-05)									
58	(6.6E-23, 5.8E-06, 3.2E-05)	(1.3E-07, 2.8E-06, 9.8E-06)									
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OVERALL (6.6E-23, 1.1E-05, 1.2E-03) (1.3E-07, 2.9E-06, 2.4E-05) (.0000, .0234, .3961)											
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SYSTEM SIZE N	SHOCK RATE NU			RATE FOR SET OF K SPECIFIC COMPONENTS							
2	(1.6E-10, 1.0E-07, 4.2E-07)			R4							
3	(3.8E-10, 9.3E-08, 3.6E-07)	(3.0E-10, 7.2E-08, 2.7E-07)		R4							
4	(5.0E-10, 8.8E-08, 3.3E-07)	(3.0E-10, 7.2E-08, 2.7E-07)		R4							
24	(4.3E-10, 7.5E-08, 2.8E-07)	(2.8E-10, 7.1E-08, 2.7E-07)		R4							
25	(4.2E-10, 7.5E-08, 2.8E-07)	(2.8E-10, 7.1E-08, 2.7E-07)		R4							
30	(4.1E-10, 7.4E-08, 2.8E-07)	(2.8E-10, 7.1E-08, 2.7E-07)		R4							
44	(3.8E-10, 7.4E-08, 2.8E-07)	(2.8E-10, 7.1E-08, 2.7E-07)		R4							
58	(3.7E-10, 7.3E-08, 2.8E-07)	(2.8E-10, 7.1E-08, 2.7E-07)		R4							
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OVERALL (1.6E-10, 7.5E-08, 4.2E-07) (2.8E-10, 7.1E-08, 2.7E-07) (2.8E-10, 7.1E-08, 2.7E-07)											

REMOTE MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

PLANT	HOURS	PUP	NUMBER OF INDIV FAULTS FAILS/COM FILTS			VALVES AFFECTED BY NONLETHAL SHOCKS FAILS/COM FILTS			VALVES AFFECTED BY LETHAL SHOCKS FAILS/COM FILTS			VALVES AFFECTED BY LETHAL SHOCKS FAILS/COM FILTS
			FAILS	/	FAILS	FAILS	/	FAILS	/	FAILS	/	
AR1	43800	28	3	/	0	1	/	1	/	0	/	0
CR3	34704	28	14	/	6	0	/	0	/	0	/	0
DE1	28944	23	7	/	0	4	/	0	/	0	/	0
DE1	43800	42	1	/	0	0	/	0	/	0	/	0
DE2	43800	51	5	/	1	0	/	0	/	0	/	0
DE3	43800	46	4	/	1	0	/	0	/	0	/	0
ES1	43800	30	6	/	0	0	/	1	/	0	/	0
T11	28368	31	1	/	1	0	/	0	/	0	/	0
T12	8736	42	0	/	0	0	/	0	/	0	/	0
AR2	18120	63	4	/	6	0	/	0	/	0	/	0
CC1	43800	31	3	/	1	0	/	0	/	0	/	0
CC2	35784	31	1	/	1	0	/	0	/	0	/	0
FC1	43800	6	0	/	3	0	/	1	/	0	/	0
M12	43800	33	2	/	1	0	/	0	/	0	/	0
MV1	43800	35	4	/	0	0	/	1	/	0	/	0
PA1	43800	15	0	/	2	0	/	0	/	0	/	0
SL1	41112	37	4	/	3	0	/	0	/	0	/	0
BV1	40656	49	3	/	1	0	/	1	/	0	/	0
DC1	43800	63	3	/	3	0	/	1	/	0	/	0
DC2	24600	63	4	/	1	0	/	0	/	0	/	0
HN1	43800	28	0	/	0	0	/	0	/	0	/	0
IP2	43800	60	2	/	0	0	/	0	/	0	/	0
IP3	41472	63	0	/	0	0	/	0	/	0	/	0
JF1	29712	68	3	/	2	0	/	2	/	0	/	0
KE1	43800	41	6	/	0	2	/	0	/	0	/	0
HA1	23976	48	8	/	4	0	/	0	/	0	/	0
NA2	4872	48	0	/	0	0	/	0	/	0	/	0
PR1	43800	54	3	/	0	0	/	0	/	0	/	0
PR2	43800	54	2	/	1	0	/	0	/	0	/	0
PT1	43800	42	1	/	0	0	/	0	/	0	/	0

PY2	43800	42	3 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
RG1	43800	47	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
RD2	43800	37	7 / 2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
S41	35496	39	3 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SE1	43220	16	1 / 1	1 / 0	2 / 0	0 / 0	0 / 0	0 / 0
SD1	43800	26	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SU1	43800	55	0 / 1	1 / 0	1 / 0	0 / 0	0 / 0	0 / 0
SU2	43800	55	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TR1	43800	41	3 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TU3	43800	50	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TU4	43800	50	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
YR1	43800	28	1 / 0	0 / 1	0 / 3	0 / 0	0 / 0	0 / 0
ZI1	43800	82	3 / 4	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
ZI2	43800	82	3 / 2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BF1	43800	63	5 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BF2	43800	63	2 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BF3	38496	63	4 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BR1	37032	72	6 / 4	1 / 1	1 / 1	0 / 0	0 / 0	0 / 0
BR2	43800	72	5 / 1	0 / 1	0 / 1	0 / 0	0 / 0	0 / 0
CO1	43800	57	12 / 3	1 / 0	1 / 0	0 / 0	0 / 0	0 / 0
DA1	43800	67	5 / 0	1 / 0	1 / 0	0 / 0	0 / 0	0 / 0
DR2	43800	51	13 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DR3	43800	51	5 / 9	0 / 1	0 / 1	0 / 0	0 / 0	0 / 0
EN1	43800	66	7 / 4	1 / 1	1 / 1	0 / 0	0 / 0	0 / 0
EN2	21816	67	10 / 4	3 / 3	5 / 5	0 / 0	0 / 0	0 / 0
FP1	43800	18	14 / 1	1 / 0	1 / 0	0 / 0	0 / 0	0 / 0
MI1	43800	34	2 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
MO1	43800	47	6 / 3	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
NM1	43800	21	1 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DC1	43800	42	2 / 6	0 / 2	0 / 3	0 / 0	0 / 0	0 / 0
PB2	43800	58	9 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
P83	43800	58	7 / 2	2 / 0	2 / 0	0 / 0	0 / 0	0 / 0
P11	43800	47	6 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
QC1	43800	57	6 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
QC2	43800	57	7 / 5	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
YY1	43800	56	2 / 1	2 / 0	4 / 0	0 / 0	0 / 0	0 / 0
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All	2600616	3105	253 / 100	19 / 18	24 / 29	0 / 0	0 / 0	0 / 0

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

P E N T		CONTROL NUMBER	EVENT DATE	STATION NAME	SCADA NAME	HOUSEKEEPING	CAUSE DESCRIPTION
B	ARI	022339	072078 G RM F23	1	T	SODIUM THIOSULFATE BLOCK VLV CV-2411 FAIL.	TO OPERATE TORQUE SETTING OUT OF ADJ. DRY PACKING
B	ARI	027473	100879 F RM F16 U	1	T	CV1616 FAILED IN THE ES POSITION	CONT FUSE BLEW BECAUSE OF GROUND WIRE
B	ARI	030864	040680 B RM F02 C	1	T	EMER. FM SUPPLY VALVE FAILED TO FULLY OPEN(CV-2667 LOOSE BOLTS SECURING ACT TO VALVE BODY)	
B	ARI	030926	040780 H MV A20	1	N	CV-U227 FAILED TO OPEN ON MAN HPI (HPI VLV LOOP @ MAN ENGAGING LEVER FOUND STUCK IN ENG POS)	
B	ARI	032533	090680 G MV B23	1	N	PCS MAKE UP BLOCK VLV(CV-1234) FAILED TO FULL CLOS TORQUE SWITCH SETTING TOO LOW	
B	CR3	017168A	020377 L MV A20 R	1	H	DECAY HEAT VLV DHV-4 WOULD NOT OPEN REMOTE ACTUATOR MTR. OPERATOR WOULDN'T OVERCOME VLV. DRAE	
B	CR3	017168B	020377 L MV A20 R	1	N	DECAY HEAT VLV DHV-41 WOULD NOT OPEN REMOTE ACTUATOR MTR. OPERATOR WOULDN'T OVERCOME VLV. DRAE	
B	CR3	018561	071577 L MV A23 R	1	T	VLV DHV-41 WOULD NOT OPEN FROM CONTROL ROOM	CAUSED BY SHIFT IN TORQUE SWITCH SETTING
B	CR3	018562	071577 L MV A00 R	1	T	DECAY HEAT VLV DHV-4 WOULD NOT OPEN FROM CONT.ROOM	CAUSE OF FAILURE UNKNOWN
B	CR3	018566	072977 H MV A12	1	T	HPI VLV MUV-25 FAILED TO OPEN AUTOMATICALLY	MECH.BINDING OF THE REVERSING INTERLOCKS
B	CR3	019010	082777 L MV B23	1	N	CORE FLOOD DR.VLV FOR B CORE FL.TK.WOULDN'T CLOSE	DRIFT OF TORQUE SWITCH SETTING(GIVLV CFV-12
B	CR3	019013	083177 L RM 800	1	N	CORE FLOOD SAMP.150.VLV CFV-11 WOULDN'T CLOSE	CAUSE OF FAILURE UNKNOWN
B	CR3	021775	062178 L RM A00 R	1	N	DECAY HEAT REMOV.VLV DHV-111 WOULD NOT OPEN REMOT.	CAUSE OF EVENT IS UNDETERMINED
B	CR3	022359	090778 L RM B23	1	T	CORE FLOOD VALVE CFV-15 FAILED TO CLOSE ON TEST	FAULTY TORQUE SWITCH
B	CR3	0230958	100478 L RM F16 T	1	T	FLOW CONTROL VALVE DHV-10 FAILED TO CONTROL FLOW	NO SIGNAL FROM FLOW CONTROLLER
B	CR3	025547*	030479 L RM A00 R	2	N	DECAY HEAT REMOVAL VLV(S DHV-364 COULD NOT BE OPENED REMOTELY--CAUSE UNKNOWN)	
B	CR3	025936	040479 L RM F00 R	1	T	THROTTLE VLV HV-110 WOULD NOT CONTROL FLOW IN AUT NO CAUSE FOUND	
B	CR3	025925	042479 L RM A12 R	1	N	DECAY HEAT REMOVAL VLV DHV-4 FAILED TO OPEN REMOTE WASHER BINDING AT STEM NUT INTERFACE	
B	CR3	030369	020680 L RM F16 T	1	T	*A* DECAY HEAT PMP DISCH THROTTLE DIDN'T CONTROL IN AUTO. LOOSE WIRES ON SELECTOR SWITCH	AIR IN THE CONTROLLER SENSING LINE
B	CR3	033760	080680 L RM F24 T	1	T	DHV-110 WOULD NOT CONTROL FLOW IN AUTOMATIC	
B	CR3	032554	082780 L MV F24 T	1	T	DHV-111*B* DECAY HEAT PMP DISCH THROTTLE DID NOT // CONTROL IN AUTO. AIR IN SENSING LINES	
B	CR3	032555A	090380 L MV F20 R	1	T	DHV-110 DID NOT OPERATE AS REQUIRE (FIFTH OCCUR)	ELECTRICAL SHORT FOUND IN MOTOR
B	CR3	032555A	090580 L RM F16 S	1	I	MUV-23 FAILED TO OPERATE. NO POWER	FAILED CONTROL TRANSFORMER
B	CR3	032682	091680 L MV F16 T	1	I	DHV-111*B* DM PMP DISCHR THROTTLE DID NOT OPERATE.	HIGH ALARM SWITCH DID NOT OPERATE
B	DB1	020989A	031678 B MV A26	1	T	AUX.FOPMP.L-1 STOP VLV AF3870 FAILED TO OPEN	LIMIT SWITCH ON VLV MTR NOT ADJUSTED PRJP.

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

P L Y E N T	C O N T R O L N U M B R E R	S C H A T F I V Y C O D E P E L I N Y	M O D E D E S C R I P T I O N	C A U S E D E S C R I P T I O N
8 081 021957	071678 L MV A12	1 N	DECAY HEAT COOL 1-2 OUTLET VLV DH-14A WOULD'NT OPEN ACTUATOR ARM HAD BECOME MISALIGNED	
8 081 025402	011179 L MV B20	1 N	CORE FLOOD TANK 1-2 150 VLV CFIA WOULD NOT CLOSE LOOSE SET SCREW IN MOTOR OPERATOR	
8 081 025521	022079 B MV B23	1 T	AFW VLV AF3869 COULD NOT BE CLOSED REMOTELY FAULTY TORQUE SWITCH FN MOTOR OPERATOR	
8 081 026605	032079 L MV B10	1 T	DECAY HEAT REMOV CONT ISO VLV DH-2735 FAILED TO CL USE--BUILDUP OF BORIC ALIO ON VALVE STEM	
8 081 026597	070479 B MV F20	1 T	INTERNAL SHOT CIRCUIT IN MOTOR WINDING AFW VLV AF 3870 WOULD NOT OPERATE REMOTELY	
8 081 030872	041880 L RM B12	1 N	DH62 WAS DISCOVER OPEN REMOTE OPERATOR OUT OF ADJUSTMENT	
8 081 031898	071080 L RM F02 C	1 N	DH COOLER 1-2 DISCH CONTROL VLV OPERATED ERRATIC SFAS CH 2 DEENERGIZED FOR MAINTENANCE	
8 081 031906A	072480 L RM F02 B	1 N	PERSONNEL SHORTED FUSE CLIP IN CONTROL PC	
8 081 031906B	072480 L RM F06 B	1 N	INADEQUATE RESTORATION PROCEDURE	
8 081 031906C	08030 L RM F02 A	1 N	MAIN. SPEC. REMOVED BISTABLE	
8 081 030598	030680 L MV A26	1 T	OUT OF ADJUSTMENT LIMIT SWITCH	
8 082 016201	101476 L MV A16 S	1 T	DIRTY ELEC. CONTACT IN MOTOR CONTROL CENTER	
8 082 017541	040577 F MV B12 R	1 T	LOOSE SET SCREW ON PILOT GEAR OF MTR SF1 VALVE LP-21 FAILED TO CLOSE PERSONNEL SHOULD HAVE BEEN DOING UNIT 1-5	
8 082 027795*	120919 H MV A02	2V M	HPI SUCTION VLV FROM BWST RENDERED INOPERABLE.	
8 082 034735	062280 F MV A02 R	1 U	PREVIOUS REPAIR WORK OR VIB. AND AGE	
8 082 032690	091680 F MV A20 R	1 T	VALVE LP21 FAILED TO OPEN, SET SCREW LOOSE ON MOTOR PIN.	
8 083 014927	050476 L RM B23	1 T	LOOSE SET SCREW ON MOTOR OPERATOR PINION	
8 083 020592	020318 F MV A23	1 T	TORQUE SWITCH FAILURE	
8 083 020593	02078 F MV F12	1 T	TORQUE SWITCH FAILURE	
8 083 021047	032078 H MV A16 S	1 T	VALVE VP-24 FAILED TO OPEN DIRT ON VAL OPER CONTACTS	
8 083 027368	101379 L MV F02	1 T	MOTOR MISWIRED	
8 RSI 014306	020770 L MV A14	1 T	TIGHT PACKING /POSS STICKING HV-26106!	
8 RSI 016558*	111176 L MV A23 R	2 T	TWO DECAY HEAT MUVS FAILED TO OPEN FOR MONTH TEST	
8 RSI 019536	100177 L MV F20 R	1 N	TOURQUE SWITCHES NEEDED RESET/TESTED WEEKLY BWS ISOL VALVE FAILED TO OPERATE (SEV-25003)	
8 RSI 019798	111977 H MV F00	1 T	LIMITORQUE OPERATOR(SMS) FAILED/EXCESS OP)	
				LIMITORQUE ISOLATION VALVE FAILED TO CYCLE/TEST UNKNOWN

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REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

VENT NUMBER	CONTROL DATE	EVENT TIME	TYPE	SYNTH COM MODE	CAUSE	TYP E	F A U L T Y	ACTIVITY	MODE DESCRIPTION		CAUSE DESCRIPTION
									ACTIVITY	MODE DESCRIPTION	
B RSI 030143	010980 H RM	F16 U	1	U	POWER TO MU TANK ISO VLV SFV-23508 WAS NOT RESTORE					PERSONNEL ERROR	
B RSI 030725	032280 L MV	B20 R	1	N	SFV-25003 (BWT ISO TO DHR SUCTION) FAILED TO CLO.					FAILED CLUTCH IN MOTOR OPERATOR	
B TII 017343	030977 F MV	B23	1	T	HO SPRAY PUMP SUCTION VALVE FAILED TO CLOSE/TEST					GREASE IN SPRING PREVENTED TORQUE SW OPER	
B TII 025505	011279 H MV	A16 S	1	T	HPI DH-V-58 DID NOT OPEN FROM MID POSITION					MOTOR BREAK DID NOT RELEASE	
C AR2 023481	122078 R MV	A16 T	1	N	FLOW CONTROL VLV 2CV-1025-1 FAILED TO OPERATE					LOOSE MOTOR POWER CONNECTION	
C AR2 026245A	051479 B MV	B16 T	1	N	SUP VLV 2CV-1039-2 WOULD NOT RESPOND TO SIGNAL					BLown FUSE IN VLV CONTROL CIRCUITRY	
C AR2 026248	060379 B MV	B26 R	1	N	EMER FEED WTR CONT VLV 2CV-1036-1 WOULD NOT SHUT					LIMIT SWITCH WAS OUT OF ADJUSTMENT	
C AR2 026243A	060979 B MV	B16 T	1	N	EMER FEED WTR CONT VLV 2CV-1038-1 WOULD NOT SHUT					LOOSE WIRE ON THE HANDSWITCH	
C AR2 026543A	070679 B MV	B00 R	1	N	EMER FEED WTR CONT VLV 2CV-1038 WOULD NOT SHUT					NO REASON FOUND FOR FAILURE	
C AR2 026896	082679 H MV	A20	1	N	SAFETY INJECTION TANK MAKEUP VLV 2CV-5064 FA SHUT					SPRING TENS ON VLV OPER GATE OUT OF ADJ	
C AR2 031672	060580 B MV	A16 T	1	N	EF WTR SUP. VLV (2CV-1075) FAIL. TO OPEN ON DEMAND					LOOSE CONNECTOR AT VLV OPERATOR	
C AR2 031823	070780 B MV	A20 R	1	N	EF VALVE 2CV-1075-1 FAILED TO OPEN FROM CONTROL RM					LOOSE BRUSH CONNECTION	
C AR2 032447	081280 F MV	F16 S	1	T	CONTAINMENT SUMP RECIRC VLV 20V-5648-2 FAILED					FOREIGN MAT. IN VLV OPERATOR SW CONTACTS	
C AR2 033375	112980 H RM	B16 S	1	M	HPCI VLV 2CV-5056 FAILED TO CLOSE					BELIEVED TO BE CONTROL CIRCUIT FUSE FAIL.	
C CCC1 014465	030576 H MV	F16 S	1	N	HPSI LP,ISO,VLV 1-MOV-616 WOULD NOT OPER. REMOTELY					BLown CONTROL CIRCUIT FUSE CAUSED FAILURE	
C CCC1 016403	111776 H MV	A23 R	1	T	AUX,HI,PRESS,LP,ISO,VLV SI-617 FAILED TO OPEN					DEFECTIVE TORQUE SWITCH; BURNED CONTACTS	
C CCC1 027170	092479 H MV	A20 R	1	T	AUX HIGH PRESS LOOP ISO VLV SI-617 FAILED TO OPEN					VLV MOTOR WAS SINGLE PHASING IN OPEN DIR	
C CCC1 030214	010480 H RM	F23	1	N	12A HPSI STOP VLV WOULD NOT THROTTLE					LOOSE LEADS ON TORQUE SWITCH	
C CCC2 018881	082577 F RM	F16 S	1	N	#21 CONT,SPRAY SYS,HDR,ISO,VLV(2-SI-4150-CV) D05					VLV PLACE,OUT OF SERV.DUE TO FAIL,RESIST.	
C CCC2 019740	111577 H MV	A26	1	N	MOV-627,AUX HI PRESS HDR STP LP 11B,WOULDNT OPEN					OPEN LIMIT SWITCH CONTS. WERE DIRTY	
C FC1 014561	041476 H RM	B16 S	1	T	HCV-383-4 FAILED TO CLOSE ON TEST					BINDING CONTACT IN BREAKER TO VALVE	
C FC1 023139	112478 L RM	F16 U	1	T	PC-105B WAS NOT OPERATING					VALVE CLOSING RELAY NOT REWIRED AFT MAINT	
C FC1 025590	032179 H MV	A16 S	1	N	LOOP SAFETY INJECT. VLV HCV-311 FAILED TO OPEN					INTERLOCK SWITCH BINDING IN CONT CIRCUITRY	
C FC1 030212	011780 H RM	B16 S	1	T	CONT. SUMP RECIRC VLV HCV-383-4 FAILED TO CLOSE					AUX INTERLOCK FOUND BINDING	
C MI2 014461	030976 B RM	A16 S	1	M	AUX,FEEDPMP,STM,INLET VLV,CYCLED;WOULD NOT REOPEN					FAILURE OF VALVE OPERATING CIRCUIT	

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

PLANT NUMBER	CONTROL DATE	SYSTEM C P E E	MODE S E E	C A U T Y L M	ACTIVITY	MODE DESCRIPTION		CAUSE DESCRIPTION	
						TYPE	VALVE	DESCRIPTION	DESCRIPTION
C M12 015338	072476	B MV A20	1	N		INLET STEAM TRIVALE	WOULD NOT OPEN		VALVE OPERATOR SPINDLE FAILED
C M12 033586	121080	H MV F23	1	T		HPSI INJECTION MOV-2-SI-616	OVERTRAVELLED 1/4 INCH		OPERATOR SENSITIVE TO TORQUE SWITCH
C MY1 020758	020277	H RM F16 U	1	M		VALVE SL-P-3	FAILED TO OPERATE		WIRES DISCONNECTED (CAUSE UNKNOWN)
C MY1 025490A	030779	H MV F23	1	T	"AM TRAIN HPSI PMP SUCT.VLV	FAILED TO OPERATE		IMPROPER TORQUE SWITCH SETTING	
C MY1 025490B	030779	F MV F23	1	T	"AM TRAIN SCAT OUTLET VLV	FAILED TO OPERATE		IMPROPER TORQUE SWITCH SETTING	
C MY1 030991	040880	L MV F00 R	1	T	LPSI LOOP HEADER STOP VALVE	FAILED TO OPERATE		NO CAUSE FOUND (VLV IN LOOP #3)(LSI-M-31)	
C MY1 031389	050680	L MV F20 R	1	T	LPSI LOOP 3 HEADER STOP VLV	FAILED TO OPERATE		BROKEN WELD ON COUPLING ON LSI-M-31	
C PA1 018274	061577	H MV A16 T	1	T	MOV-3011	FAILED TO OPEN		CONTACT FOR "SEAL-IN" CKT ON RELAY FAILED	
C PA1 025184	012679	H RM F16 S	1	N	SI TANK T82D VENT VLV	OPENED WHEN PRESSURIZING TNK		SHORT BETWEEN FILL AND VNT VLV CIR(CV3051)	
C S11 015002	052176	B MV A16 T	1	N	MO AUX FEED PUMP STEAM SUPPLY VALVE	FAILED TO OPEN		NO SIGNAL TO VALVE/COMMAND FAULT/ELECT	
C S11 015507	070976	B MV A16 T	1	T	AUX FEED PUMP STEAM INLET VALVE	FAILED TO OPEN		COMMAND/H2O IN CONTROL CIRCUIT/POOR DES	
C S11 016880	120876	B MV A16 T	1	T	AUX FEED PUMP STEAM INLET VALVE	FAILED TO OPEN		COMMAND/H2O IN CONTROL CIRCUIT/DESIGN	
C S11 019504	081777	F RM A00	1	T	CONTAINMENT SPRAY VALVE	FAILED TO OPEN/TESTING		UNKNOWN/ LOCKED OPEN HANDWHEEL	
C S11 019509	092577	F RM A00	1	T	CONT.SPRAY HDR.ISO.VLV FCV-07-1B	NOT FULLY OPEN		UNKNOWN (CONT.SPRAY VLV-STICKING)	
C S11 020639	020978	B MV B20	1	T	AUX FEED PUMP VALVE (MV-09-11)	FAILED TO CLOSE		MOV MOTOR WINDING PARTIALLY SHORTED	
C S11 023141	112178	H MV A23	1	T	MOV 07-1B IN IR ECCS TRAIN	FAILED TO OPEN ON TEST		TORQUE SW FAULTY,REPLACED SWITCH	
W BVI 016356	102576	H MV B16 S	1	N	DRAIN VALVE ON ACCUMULATOR 1C	FAILED TO SHUT		NO PWR/ THERMAL OVERLOAD OF LINESTARTER	
W BVI 018725	072877	B RM A23	1	T	AUX. FEEDWATER CONT VLV	WOULD NOT OPEN ELECTRIC.		BINDING TORQUE SWITCH	
W BVI 022135	080178	L RM B10	1	T	1B LOW HEAD SAFETY INJECTION PMP.HEAD.ISO.	NOT CLOS		VLV FRIL. TO CLOSE DUE TO BORIC CRY. IN PAK	
W BVI 028146	060979	L MV F23	1	M	1B LHPSI PUMP SUCTION VLV	FOUND TO BE INOPERABLE		MTR OPERATOR TORQUE SWITCH WAS FAILED	
W BVI 031210*	052180	L RM B16 U	2V	T	RHR ISOL VLV	S FAILED TO CLOSE		DEENERGIZED PROCESS CONTROL SIGNAL	
W DC1 016367	110176	L MV F12	1	T	RHR VALVE	FAILED TO CYCLE DURING TESTING		PACKING GLAND WAS TOO TIGHT	
W DC1 020894	020878	B MV B16 S	1	N	AUX FEED MOV	FAILED TO CLOSE		COMMAND/LOOSE ELEC CONNECTION/CONTROL	
W DC1 021011*	032278	H MV F16 U	3	N	POWER FOUND OFF TO 3 ECCS VALVES			3 SPEAKERS FOUND TREPPED ON MCC	
W DC1 023114	112878	B MV B16 S	1	N	AFW THROTTLE VLV.	WOULD NOT CLOSE ELECTRICALLY		BROKEN LEAD ON MTR OPERATOR	

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

VENT PLAN NUMBER	CONTROL DATE	SYSTEM TEMP H P COM DEE ELM	C OM P U T F A N T Y	ACTIVITY	MODE DESCRIPTION		CAUSE DESCRIPTION
					M	T	
W DC1 025045B	010679	R MV 820 R	1	M	AFW VLV FMO-231 WOULD NOT CLOSE		BROKEN WIRE IN MOTOR OPERATOR
W DC1 025380	022379	B MV B16 T	1	T	AFW DISCHG VLV FMO-212 WOULD NOT CLOSE		LOOSE CONNECTION IN HOT SHUTDOWN PANEL
W DC1 025378	030379	B MV B20 R	1	N	AUX FEED VLV FMO-212 WOULD NOT SHUT FROM CONT RM		BROKEN WIRE IN VLV'S OPERATOR
W DC2 022069	071978	L MV F00	1	T	RHR PUMP SUCTION MOV FAILED TO CYCLE/TIME-WISE		UNKNOWN WHY CYCLE TIME EXCEEDED
W DC2 025045A	010679	B MV B20 R	2	M	AFW VLVS FMO-2326222 WOULD NOT CLOSE		BROKEN WIRES IN MOTOR OPERATORS
W DC2 027930	121779	F MV A23	1	N	CONTAIN SPRAY PMP DISCHG VLV IMD-220 FAILED TO OPEN FAILURE CAUSED BY TORQ SWTCH BINDING		
W DC2 030740	032580	B MV F16 S	1	T	AUX FEED VLV FMO-221 (#2 SG) DID NOT OPERATE		ARMATURE LEAD PULL OFF OF VLV OP MOTOR
W IP2 0187878	050777	F RM F23	1	T	VALVE 822B DID NOT OPERATE PROPERLY		TORQUE SWITCH MALFUNCTION
W IP2 026367	062679	B RM B00	1	T	SHUTOFF VLV PCV-1310B(STM.SUP.TO #22 AFW PMP) WOULD NOT SHUT--NO CAUSE FOUND		
W JF1 022633*	090978	B RM F16 U	3	T	CONTROL WAS LOST ON FLOW CONT.VLVS 322BA,B,EC		DEFECTIVE RELAY IN TDAPP CONTROL CIRCUIT.
W JF1 025436	012379	G MV F00	1	T	BIT INLET VLV Q1E21V016B FAILED TO OPERATE ELEC.		NO CAUSE FOUND FOR FAILURE
W JF1 030326*	020180	B RM A24 U	2	T	CONTROL VLVS FOR "A" AUX FEED TRAIN DIDN'T AUTO OP //EN. CONTACTS MISALIGNED IN CONTROL CIR		
W JF1 030614	030380	F MV A00	1	T	CS-MOV-8820B,DISCH TO CONT SP HDR,DID NOT OPEN		CAUSE UNKNOWN (AFFECTED THE B TRAIN)
W JF1 033005	102080	H MV A26	1	T	VALVE 1-CVC-MOV-115D(RWSV SUPPLY TO CHR PUMPS)AT//LED TO OPEN. LIMIT SWITCH NEEDED ADJ.		
W JF1 033572	112880	L RM F16 S	1	T	LOOP SUCTION VLV FOR "A" TRAIN RHR CLOSED		DIRTY CONTACTS IN PRESSURE TRANSMITTER
W JF1 033672	122580	L RM F16 S	1	M	RHR LOOP B SUCTION VLV WENT CLOSED WHEN REQ OPEN		IMPROPER SIGNAL TO VLV DUE TO SHORT/MAINT
W KE1 013963	010876	H MV F12	1	T	VALVE ST-2B DID NOT OPERATE		SCREW HOLDING TRIP LEVER BACKED OUT
W KE1 014240	022076	F RM A01 C	1	T	VALVE ICS-5B FAILED TO OPEN(CONT.SPRAY DISCH. VLV) VALVE MANUALLY TORQUED DOWN TOO TIGHT		
W KE1 019312	100377	F MV F02 C	1	M	MAINT.MAN DEENERGIZED 2 SW VLVS,WHEN ONLY ALLOW.T- -0 DEENER.1 VLV//PERSONNEL ERROR		
W KE1 020788	030278	H MV A00 R	1	T	CNTNMNT SUMP ISO VAL WOULD NOT FULLY OPEN		CAUSE UNKNOWN
W KE1 021077	040478	H MV A14 R	1	T	CNTNMNT SUMP ISO VAL WOULD NOT FULLY OPEN		VAL PACKING AT END OF USEFUL LIFE
W KE1 026136	053079	L RM A00	1	N	RHR LOW HEAD INJECT VLV SI-302A FAILED TO OPEN		NO CAUSE FOUND FOR FAILURE
W KE1 030654	030380	L MV A23	1	T	DURING CONT SUMP RECIRC TEST,SI-351 DID NOT OPEN		TORQUE SWITCH OUT OF ADJUSTMENT
W KE1 030693	031080	B RM B00	1	T	AUX FEED PUMP DISCH CROSSCONNECT VLV FAIL TO CLOSE NO CAUSE FOUND FOR FAILURE OF AFW 108		
W NA1 021150	042878	H RM B00	1	N	STEAM DUMP VAL 408E STUCK OPEN FOLL. TRIP		CAUSE NOT GIVEN

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

P Y E N T	L A C T U R E N U M B R E N T	S Y S T O R E E V E N T D A T E	S C H A I F T U N I T Y C O O D E P E E L U N I T	M O D E D E S C R I P T I O N	C A U S E D E S C R I P T I O N
W NAI 022269	081778 L MV A14	1 T	VALVE MOV-18608 FAILED TO OPEN DURING TEST	DRY VALVE PACKING CAUSED LIM SW TO TRIP	
W NAI 025762	030679 L RM F00	1 N	RHR DISCHG VLV MOV-17208 INADVERTANTLY OPENED	CAUSE NOT STATED	
W NAI 025862	041679 L MV B26	1 T	RHR 150-VLV MOV-1701 FAILED TO CLOSE AUTOMATICALLY MISALIGNED LIMIT SWITCH CONTACT		
W NAI 025859	043079 N RM A14	1 N	SAFETY INJECTION VLV MOV-18568 FAILED TO OPEN	VLV STUCK DUE TO DRIED PACKING	
W NAI 025974	051179 L RM A00	1 T	LOW HEAD SI PMP DISCHG, VLV MOV-1863A FAILED TO OPEN CAUSE OF EVENT UNKNOWN		
W NAI 030111	041180 F RM A16 T	1 N	MOV-RS-100A FAILED TO OPEN (COMMAND FAULT)	CLOSED SIGNAL TO VALVE (PERSONNEL ERROR)	
W NAI 030333	012980 F RM A16 T	1 N	MOV-RS-100B FAILED TO OPEN (COMMAND FAULT)	CLOSED SIGNAL TO VALVE (PERSONNEL ERROR)	
W NAI 031697	0622380 L RM A16 S	1 T	RECIRC VLV MOV-1863B FAILED TO REOPEN	DEFECTIVE ELECTRICAL SWITCH IN CON ROOM	
W NAI 0362094	122980 F MV F16 S	1 T	MOV-SW-105C FAILED TO OPERATE DURING TEST	LOOSE LEAD ON BREAKER/CONTROLLER	
W NAI 0362098	122980 F MV F10	1 T	MOV-SW-108A FAILED TO OPERATE DURING TEST	WATER IN VLV OPERATOR MOTOR	
W NAI 036209C	122980 F MV F00	1 T	MOV-RS-101A FAILED TO OPERATE DURING TEST	CAUSE UNKNOWN	
W PRI 014758	051376 L MV A23 R	1 I	MOV FAILED TO OPEN DURING TEST (MV-32065)	TORQUE SW PROBLEM/ADJUSTED ITLLIMITORQUE	
W PRI 018341	061877 B MV F20	1 N	AUX FEED PUMP DISCHARGE VALVE FAILED TO OPERATE	OPEN LEAD IN OPERATOR/LIMITORQUE SMB-COO	
W PRI 026266	041079 H MV A00	1 T	MV-32067 HPSI VLV TO RX VESSEL FAILED TO OPEN	NO CAUSE COULD BE FOUND	
W PRZ 0162844	102576 H RM B00	1 T	HOT LEG SAMPLE LOOP VLV CV-31607 FAILED TO CLOSE	UNKNOWN/RETEST WAS OK	
W PRZ 019284	100477 H MV A00	1 I	SAFETY TNJ PUMP SUPPLY VLV MV-32183 FAILED TO OPEN UNKNOWN/ STEM WAS LUBRICATED/NEXT TRY OK		
W PRZ 020125	122377 B MV A16 S	1 I	#22 TURB. DRIVEN AFN PUMP STM. SUP. VLV FAILED TO OPEN -EN/MOTOR LEAD GROUNDED TO JUNCTION RUX		
W PT1 013945	010876 B MV F20	1 T	MOV-4020 AUX FEED PUMP DISCHARGE FAILED STUCK/TEST VALVE OPERATOR RING WORN/GEAR REPLACED		
W PT2 014348	031576 F MV A03 R	1 T	CONTAINMENT SPRAY 2MOV-8608 FAILED TO OPEN / TEST PERSONNEL ERROR/TERMINAL SLIDER OPEN		
W PT2 015186	070176 B MV A23 R	1 T	MOV-2M5-2019/STEAM TO AUX FEED PUMP FAILED TO OPEN TORQUE SW SETPOINT CAUSED TIGHT CLOSING		
W PT2 017035	012777 F MV F16 T	1 N	CONT.SPRAY PMP.DISCHG, VLV 2-B6CB INOPERABLE	VALVE OPERATOR BREAKER WAS OPEN	
W PT2 021766	061678 F MV F23	1 T	CONT SPRAY VALVE(MOV) FAILED TO OPERATE FOR TEST	SMR-DO LIMITORQUE SW FAULTY/REPLACED	
W RG1 025265	020679 L MV A00	1 T	CNTMT RECIRC SUMP OUTLET MOV-851B FAILED TO OPEN	FLEX OF LONG EXIT MIGHT HAVE CAUSED OVERTC	
W R02 015570	081776 B MV A20 P	1 T	VALVE V2-16A FAILED TO OPEN	LIMITORQUE UPER FAILED TO OPEN VALVE	
W R02 017540	032677 B RM A00	1 N	VALVE V2-14A FAILED TO OPEN	INCREASE IN TENSION BETWEEN SEATING SURF.	

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

P E N T	C O N T R O L N U M B E R	E V E N T D A T E	S Y S T E M C A T E R I V I T Y H U S T A N T I S P U L H Y	M O D E D E S C R I P T I O N	C A U S E D E S C R I P T I O N
					A C
W R02 019350	081677	B MV A20 R	I	N VALVE V2-16B FAILED TO OPEN AS REQUIRED	LIMIT TORQUE VALVE OPERATOR FAILED
W R02 019352	081777	B MV A20 R	I	N VALVE V2-15A FAILED TO OPEN	LIMIT TORQUE VALVE OPERATOR FAILED
W R02 019667	102677	L MV A20	I	N RHR VALVE 759B FAILED TO OPEN	MOTOR WINDINGS WERE SHORTED
W R02 020053	120377	L MV A16 S	I	T RHR VALVE 744B FAILED TO OPEN	CIRCUIT THERMAL OVERLOAD DEVICE TRIPPED
W R02 022626	122177	B MV A12 R	I	T AUX FEED PUMP DISCH V6, V2-16A FAILED TO OPEN	EXCESS SEATING PRESSURE CAUSED BY OVERHEAT
W R02 020322	011178	L MV F20	I	T VALVE RHR-744B FAILED TO FUNCTION PROPERLY	OIL LEAKED INTO MOTOR (GASKET FAILED)
W R02 027067	090579	B MV A16 T	I	N AFW ISO+VLV AFN-V2-16A FAILED TO OPEN	OPERATOR POWER SUPPLY BREAKER WAS TRIPPED
W SAI 016939*	011077	H MV F20	I	N MFR.BRKS. TO VLVS 15J1&2 TRIPPED WHEN VLVS WERE OPENED//BOTH MFR.OPERATORS HAD FAILED	PENMED//BOTH MFR.OPERATORS HAD FAILED
W SAI 021910	052378	H MV A20	I	T MOV 15J1 (PHISI) FAILED TO OPEN DURING TEST	WINDING FAILED/INCORRECT MOTOR SIZE/PERSA
W SFI 033818A	092280	L MV F26	I	U 1-FCV-70-156 FAILED TO OPERATE	LIMIT SW REQUIRED ADJUSTMENT
W SFI 032973*	100580	B RM F01 C	I	T AUX FEEDWATER VLVS LCV-3-174E173 WOULD NOT HAVE OPENED IN AUTO. PRESS SWITCH LEFT ISOLATE	INTER LIMIT SW ON FCV7421 FAILED ICV72-2
W SFI 033298	111980	F MV A16 S	I	T CMNT SUMP VLV TO CMNT SPRAY PMP DID NOT OPEN	UNKNOWN/POSSIBLE LUBRICATION PROBLEM
W SFI 020609	013078	F RM B00	I	T CONT SPRAY VLV (CV-517) FAILED TO CLOSE FOR TEST	SHAFT DISTORTED/PROB DUE TO EXCESS TORQUE
W SFI 021207	041878	H MV F12	I	T MOV-850C FAILED TO OPEN IN REQUIRED TIME / TESTING	-OPEN/TIMING RELAY FAILURE
W SFI 014871	031876	B MV A16 S	I	N AUX.FEEDWTR.PUMP DISC.VLV.MOV-FW-151A FAILED TO OPEN	MAIN ERROR/SYSTEM WAS NOT ENGAGED TO DISC
W SFI 021802	062278	L MV A02 C	I	T MOV-RH-100 FAILED TO OPEN	INTERNAL OVERLOAD DUE TO VALVE PLUG BIND
W SU2 015526	061576	L MV F12	I	T LPIS MOV-28628 FAILED TO OPERATE FROM CONSOLE	TORQUE SW SET TOO LOW/WAL WOULDNT UNSEAT
W TRI 016250A	102676	H MV A23	I	N RWST SUCTION VALVE(MO-112) FAILED TO OPEN/DEMAND	MOTOR OPER FAILED/WATER CAME THRU GASKET
W TRI 016250B	102676	H MV A16 S	I	N RWST SUCTION VALVE (MO-112) FAILED TO OPEN/DEMAND BREAKER SUPPLYING POWER FAILED/COMMAND	VALVE STEM LACKED LUBRICATION
W TRI 020325	112777	B MV F20	I	N AUX FEED VLV (CV-300482) FAILED TO OPERATE	UNKNOWN / SETPOINT DRIFT / ADJUSTED VLV
W TRI 020516	010478	H MV A19	I	T MOV-88807A FAILED TO OPEN DURING TESTING	IMPROPER WIRING OF TIME DELAY RELAYS
W YRI 019495	102477	H RM F00	I	N REGULATOR VALVE FAILED TO OPERATE (CONTROL PRESSURE)	STEM STICKING DUE TO LUBRICATION PROBLEM
W YRI 030161*	020180	H RM F16 U	I	T SI ACCUMULATOR N2 VLV SI-TV-604,605,606 DIDN'T OP.	COMMAND/AUX CONTACTS IN CONTL CKT STUCK
W ZII 017154	012177	F MV A19	I	T CONTAINMENT SPRAY 1MOV-C50002 FAILED TO OPEN	PAGE
W ZII 017040	012677	H MV A16 T	I	T VALVE 1MOV-S160RA FAILED TO OPEN	7

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

PLANT VENT	CONTROL NUMBER	EVENT DATE	SYSTEM COMP. E	C ODE E	M ODE E	A TYP E	F LIM I	N UM H	ACT IV TY		
										MODE DESCRIPTION	
W ZII 017223	012877	H MV A16 T	1	T	VALVE 1MOV-SI880BB FAILED TO OPEN					COMMAND/AUX CONTACTS, CONTROL CKT, STUCK	
W ZII 017251	012877	H MV A16 T	1	T	VALVE 1MOV-SI8800C FAILED TO OPEN/COMMAND					AUX CONTACTS IN CONTROL CIRCUIT STUCK	
W ZII 021337	042178	L MV A00	1	T	RHR 1MOV-8700B FAILED TO OPEN DURING TESTING					UNKNOWN/SOMETHING CAUSED THERMALS TO OPER	
W ZII 021397	050378	F MV A19	1	T	CONTAINMENT SPRAY VALVE 1MOV-CS0002 FAILED TO OPEN LACK OF LUBRICATION						
W ZII 033533	121580	L RM B16 S	1	T	RHR MINI FLOW VLV(1FIC-610A) WOULD NOT HAVE CLOSED FAILED MICRO SWITCH						
W ZII 014253	021376	H MV A16 T	1	T	2B SE PMP. SUC. VLV 2MOV-SI8923B FAILED TO OPEN					DIRTY CONT.ON CKT.BRKER.TO MTR.OPERATOR	
W ZII 017861	051977	H MV A20	1	N	VALVE 2MOV-SI8800D FAILED TO OPEN					LIMIT TORQUE MOTOR OPERATOR FAILURE	
W ZII 018212	060477	L MV A16 S	1	T	RHR VALVE(2MOV-RH8700B) FAILED TO OPEN DURING TEST					COMMAND/AUX CONTACTS STUCK IN MCC	
W ZII 026750	071879	L MV A26	1	T	2MOV-SI8801A FAILED TO STROKE OPEN(RECIRC FROM SU/ IMP TO RHR SUCTION). LIMIT SWITCH FAILURE						
W ZII 031245	042980	F MV A23	1	T	2B CONT SPRAY PUMP STOP VLV FAILED TO OPEN					FAILED TORQUE SWITCH	
G BF1 017594A	032177	L MV B08	1	T	VLV FCV 74-52 WOULD NOT GO COMPLETELY CLOSED					WORN BRNG.ASS,LOCKNUT,YOKEENUT,GASKETS	
G BF1 017594B	032177	L MV B20	1	T	VLV FCV 74-52 WOULD NOT CLOSE:MTR TRIP, THERMAL O.E					MOTOR SHAFT WAS BENT	
G BF1 018126	050977	H MV A20	1	T	HPCI TURB. STM. SUP. ISO. VLV. FCV 1-73-16 FAIL TO OPEN BROKEN TEETH ON MTR PINION/CLUTCH GEAR						
G RF1 027620	101779	H MV A26	1	T	FCV-73-27 WOULD NOT OPEN-HPCI INOPERABLE					DIRTY CONTACTS ON OPER. LIMIT SWITCH	
G BF1 030712	031380	L MV B16 S	1	T	RHR INJECT VLV 74-67 FAILED TO CLOSE DURING TEST					LMT SW IN ISOLATION LOGIC FAILED	
G BF1 032742	092480	L MV F20	1	N	RHR TORUS VLV FCV-74-71 FOUND TO BE INOPERABLE					GROUNDED MOTOR(3.9HP,SMBZ,LIMIT TORQUE)	
G BF2 016807	111676	H MV A23 R	1	T	HPCI TURB. STM. SUP. VLV 2-FCV-73-16 FAILED TO OPEN					TOR.SWT.GEAR ASS.PIN FOR VLV OPER.SHEARED	
G BF2 025015	011379	H MV A26 R	1	T	HPCI INOPERABLE-FCV-73-16 FAILED TO OPEN					MECH FAILURE OF OPERATOR LIMIT SWITCH	
G BF3 018637	070577	H MV A23 R	1	T	HPCI TURB. STM. SUP. 3-FCV-73-16 FAILED TO OPEN					TOR.SWTH.GEAR ASS.SHEARED;CAUS.DVLD ON MT	
G BF3 020524	021378	L MV F12 R	1	T	VLV FCV.3-74-52 WAS FOUND INOPERABLE					UPPER BRNG.LOCKNUT STRIPPED FROM NOR. POS	
G BF3 021245	042878	L MV F12 R	1	T	VLV FCV 3-74-52 WAS FOUND INOPERABLE					UP.BRNG.LOCKNUT STRIPPED FROM NOR.POSITIN	
G BF3 030363	020580	L MV F26 R	1	T	RHR VLV FCV 74-73 FAILED TO OPERATE DURING TEST					LIMIT SW IN ACTUATOR ASSEMBLY FAILED	
G BRI 016402	111976	L MV F16 U	1	N	RHR INJECTION VALVE(E11-F015A) FAILED TO OPERATE					UNDERSIZED BKR/DESIGN PROBLEM(ROOT)	
G BRI 016861	112176	H MV A20 R	1	T	E41-F001(HPCI STM.SUP.VLV) WOULD NOT OPEN					BRUSHES ON VLV MOTOR WERE STICKIN	
G BRI 017081	011977	H MV B20 R	1	T	HPCI STM.SUP.VLV E41-F003 WOULD NOT CLOSE					DIRTY COMMUTATOR IN VLV OPERATOR	

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

P L Y E N	A C T U A L C O D E	C O N T R O L N U M B R	E V E N T T I M E	S Y S T E M N A M E	M A T E R I A L U N I T	M O D E	D E S C R I P T I O N	C A U S E D S C R I P T I O N
G BRI 017600	021077 D	MV A16 S	1 N	CORE SPRAY VALVE	FAILED TO OPEN AT REQUIRED PRESS	SETPOINT ON CONTROLLING INST DRIFTED HI		
G BRI 017290	030177 H	MV B12	1 T	HPC1 MIN. FLOW VLV E41-F012	FAILED TO CLOSE	ANTI-ROT. KEY SET SCREW HAD UNSCREWED		
G BRI 017330	030677 L	MV A00	1 T	RHR PMP 10 TORUS SUC.VLV E11-F0040	WOULD NOT OPEN	CAUSE OF FAILURE UNKNOWN		
G BRI 019677	110577 L	MV A02 C	1 N	RHR VALVE E11-F004A	FAILED TO OPEN	MOTOR PROBLEM	PERSONNEL ERROR/COVER LEFT LOOSE/WATER LEAK	
G BRI 019824	120377 L	MV B20	1 U	VALVE E11-F0040	FAILED IN OPEN POSITION		MOTOR FOUND TO BE OPEN(UNDETERMINED WHY)	
G BRI 022C928	072878 L	MV A16 T	1 U	VALVE F06BB	FAILED TO OPEN		BLOWN FUSE	
G BRI 022092A	080278 L	MV A16 T	1 U	VALVE F06BB	FAILED TO OPEN		BLOWN FUSE/FOUND GND WIRE IN LOGIC CKT	
G BRI 022218	080878 H	MV A00	1 N	HPLA FEED INJ VALVE E41-F006	FAILED TO OPEN AUTO		UNKNOWN/TESTING COULDNT DUPLICATE FAILURE	
G BRI 030638	031480 H	RM B16 S	1 T	HPC1 TORUS SUCTION VLV E41-F041	FAILED TO CLOSE		RTGR CONTROL SW FAILED	
G BR2 014618	031076 H	RM A26	1 T	VALVE 2-E41-PV-12190	FAILED TO OPEN DURING TEST		LIMIT SW WAS OUT OF ADJUSTMENT	
G BR2 020240	010478 H	MV F26	1 T	CLOSING TIME ON E41-F002	EXCEED. IS LIMIT (HPC1)		LIMIT SWITCH(OPEN) OUT OF ADJUSTMENT	
G BR2 020913	040378 L	M A20	1 N	SHUTDOWN COOL-DUTY.SUF.VLV E11-F008	WOULDN'T OPEN		ELECTRO-MECHANICAL BRAKE ON VLV.OP.FAILED	
G BR2 021663	060378 L	MV A00	1 N	RHR VLV E11-F009	WOULD NOT OPEN FROM CONTROL ROOM		CAUSE OF VLV NOT OPENING, NOT GIVEN	
G BR2 023034	111278 L	MV A16 U	1 N	RHR VLV E11-F008	WOULD NOT OPEN AT REQ. SETPOINT		FAIL. OF RX-STM.DOME HIGH PRESS.SWITCH	
G BR2 026521	072179 H	MV F20	1 T	HPC1 STEAM ISOLATION VALVE ECO1	INOPERABLE		PINION GEAR INSTALLED BACKWARD ON OP SHAFT	
G BR2 030412	021490 L	RM A16 S	1 N	VALVE E11-F049 FROM PHR TO RAOWASTE	FAILED TO OPEN		COMMAND FAULT,RELAY FAILED IN LOGIC CKT	
G C01 014359	012476 L	MV F20 R	1 N	VLV RHR-MU-34A	WOULD NOT OPERATE BY MTR.OPERATOR		SNARfed WOODRUFF KEY.IN MTR.OPERATOR	
G C01 015717	081076 D	MV F20	1 T	VALVE CS-MD-12B	WOULD NOT OPERATE		TRIPPER PIN IN OPERATOR DISLODGED	
G C01 016008	090776 D	MV A20	1 T	VALVE CNS-MV-12B	FAILED TO OPEN		THE REPAIR CLUTCH AND COMPONENTS FAILED	
G C01 016658	102876 L	RM A16 S	1 T	VALVE RHR MO-17	FAILED TO OPEN		BRKEN RELAY COIL KEEPER LODGED IN CONT.	
G C01 017301	021977 L	MV B12 R	1 N	MOTOR OPERATED VALVE RHR-MD-34	WOULD NOT CLOSE		SHREADED KEY BETWEEN VALVE AND OPERATOR	
G C01 018004	042077 D	MV F20	1 T	CORE SPRAY PUMP VALVE	INOPERATIVE,MOTOR RUNS		MOTOR GEAR SET SCREW ON VAL OPER LOOSE	
G C01 020343	011378 L	MV B16 S	1 T	RHR INJ BLOCK VALVE	FAILED TO CLOSE DURING TEST		DIRTY CONTACTS ON RELAY&WIRING ERROR	
G C01 0208068	020778 H	RM B16 T	1 T	HPC1 VALVE	FAILED TO CLOSE DURING TEST		NO SIGNAL FROM OP SWITCH	
G C01 023049	091678 L	MV A20	1 N	VALVE RHR-MD-668	FAILED TO OPEN		SET SCREW ON VALVE OPERATOR LOOSSTENED	

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

P L A Y E N T	C O N T R O L N U M B E R	S Y S T E M C A T I V E H A U Y A N T I D U S P L A Y E L W Y	E V E N T E M P U R E D E L M Y	MODE DESCRIPTION		CAUSE DESCRIPTION
				DATE		
G C01 0226068	032179 0 MV A20	I	I	C5-M0-11A CORE SPRAY VALVE FAILED TO OPEN		WORN SET CLUTCH COLLAR ON OPERATOR
G C01 0227749	110979 0 MV A20 R	I	I	C5 VALVE C5-MU-12A WOULD NOT OPEN		WORN WORM SET CLUTCH COLLAR ON OPERATOR
G C01 031544	051680 L RM F26 C	I	I	R&R VLV M0-57 FAIL TO CLOSE IN REQUIRED TIME		LIMIT SW SET WRONG(PERSONNEL ERROR)
G C01 0321114	062980 L MV B12	I	N	RHR-M0-57 FAILED TO CLOSE		STEM RACKED OUT OF DISC JAMMING VLV
G C01 0322111	081380 L MV F20 R	I	I	RHR-M0-34B FAILED TO OPERATE		KEY BETWEEN MOTOR SHAFT AND PINION FAILED
G C01 033825	111780 L MV F05 R	I	N	RHR-M0-34A WOULD NOT OPERATE--KEY CONNECTING MOTOR		PINION GEAR AND SHAFT MADE OF WRONG MATERIAL
G C01 033709	121680 L RM A23	I	Y	RHR-M0-25B WOULD NOT OPEN		CLOSING TORQ-SWITCH. SET TOO CLOSE TO REQ.
G DAI 017043	021177 0 MV F05	I	I	CLUTCH HOUSING FOR MOV 2115 FRACTURED DUR. TEST		MATERIAL TOO BRITTLE
G DAI 017312	021977 H RM F03 C	I	N	CONTACT BLOCK FOUND INSTALLED IN VALVE CIRCUIT		PERSONNEL ERROR,FAILED TO REMOVE AFTER TEST
G DAI 019963	112377 H MV A00	I	I	HPCI INJECTION VALVE MOV 2312 FAILED TO CLOSE		CAUSE UNKNOWN
G DAI 019967	121577 L MV A20	I	N	RHR CROSS-TIE VALVE FAILED TO OPEN		FRACUTRED TEETH ON WORM AND WORM GEAR
G DAI 027096	091879 L HV A20	I	T	RHR MINIMUM FLOW VALVE WOULD NOT OPEN		OPERATOR WORM GEAR WAS STRIPPED
G DAI 028004	091979 0 MV F02	I	N	WAM CORE SPRAY MINIMUM FLOW VALVE WOULD NOT CLOSE		LEVER ON OPERATOR MOVED TO NEUTRAL POSITION
G DR2 014330	031376 H RM A16 S	I	I	HPCI STEAM SUPPLY VALVE 2-2301-4 FAILED TO OPEN		DIRTY CONTACTS IN BREAKER SUPPLYING VALVE
G DR2 015748	061076 D RM B19 R	I	I	VALVE M02-1402-4B FAILED TO CLOSE AGAINST PUMP HED		INADEQUATE LUBRICATION OF VALVE STEM
G DR2 015378	071176 0 MV F26	I	I	CORE SPRAY INJECTION VAL M02-1402-24B FAILED		BROKEN LIMIT SWITCH CONTACT BLOCK
G DR2 016453	111376 H HV F12 R	I	I	HPCI INJECTION VALVE M02-2301-B FAILED		VALVE STEM SHEARED
G DR2 017182	021777 L MV A26	I	I	LPCI CROSS-TIE VALVE M02-1501-32B FAILED TO OPEN		LIMIT SWITCH OPENED BEFORE VALVE OFF SEAT
G DR2 018508	080277 H HV A23 R	I	I	HPCI VALVE 2-2301-B FAILED TO OPEN		SUSPECT PROBLEM WITH TORQUE SWITCH
G DR2 018934	081577 L MV A00	I	I	SUCTION VALVE MO-2-1501-5A FAILED TO OPEN		CAUSE UNKNOWN
G DR2 018985	091077 H HV A06	I	I	HPCI VALVE 2-2301-B FAILED TO OPEN, VAL DAMAGED		OVER SIZED HIR OPERATORS OVERSTRESS SYSTEM
G DR2 022776	101378 0 PM B19 R	I	I	THE 2-1402-4B FLOW TEST VALVE FAILED TO CLOSE		VALVE STEM NOT ADEQUATELY LUBRICATED
G DR2 022775	101878 L RM B19	I	I	LPCI SUCTION VALVE M0-1501-5C FAILED TO CLOSE		VALVE STEM NOT ADEQUATELY LUBRICATED
G DR2 025246	011179 L MV B20	I	I	LPCI FLOW TEST VALVE FAILED TO CLOSE WHEN ACTUATED		OPENED PINION GEAR ON OP MOTOR SHAFT
G DR2 025248	012579 L MV B00	I	I	LPCI MIN FLOW VALVE FAILED TO CLOSE COMPLETELY		CAUSE UNKNOWN

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

P E N T A N C O N T R O L N U M B R E H P E E D S P E L H Y	S Y S C O N T R O L F A U T O M A T I C V A L V E R Y	E V E N T D A T E	M O D E D E S C R I P T I O N	C A U S E D E S C R I P T I O N
				A C T I V E D E S P E L H Y
G DR2 031264 051280 H RM B14 1 N	HPC1 ISOL VLV FAILED TO CLOSE			STEAM CAUSED PACKING TO SWELL (PERSONNEL)
G DR2 032749 101180 H MV A23 R 1 N	HPC1 STEAM SUPPLY VLV FAILED TO OPEN			TORQUE SW CONTACTS STUCK OPEN REPLACED
G DR3 014750 051076 0 MV B16 U 1 T	MO 3-1402-258 TRIPPED WHILE BEING CLOSED			WRONG SIZE OVERLOAD HEATER
G DR3 016695 101276 L MV A16 S 1 T	VALVE 3-1501-27A FAILED TO OPEN ELECTRICALLY			LOOSE TERMINAL IN VALVE CONTROL CIRCUIT
G DR3 016474* 111976 H MV F16 S 2V U	HPC1 VLV FAILED TO OPERATE (CYCLING)			DESIGN ERROR IN LOGIC CIRCUIT
G DR3 018936 081177 L MV A19 1 N	VALVE MU-3-1501-208 FAILED TO OPEN			VALVE STEM NOT ADEQUATELY LUBRICATED
G DR3 019996 121677 L MV A00 R 1 N	LPCI HX DISCH VALVE MO3-1501-3A FAILED TO OPEN			CAUSE UNKNOWN
G DR3 020602 020778 L MV A00 R 1 T	VALVE MO-3-1501-5C FAILED TO OPEN			CAUSE UNKNOWN
G DR3 021679 060678 F MV F23 1 N	VALVE MO3-1501-6B FAILED WHILE BEING CYCLED			INFFECTIVE SHAFT PIN ON TORQUE SWITCH
G DR3 0222561 092278 L MV B16 S 1 T	LPCI VALVE 3-1501-20A FAILED TO CLOSE ON TESTING			STUCK CONTACTOR IN MCC
G DR3 022591 092278 L MV F00 1 N	LPCI HX VALVE MO3-1501-3A FAILED TO OPERATE			CAUSE UNKNOWN
G DR3 027260 092379 L MV A16 S 1 T	LPCI MOV 3-1501-3A WOULD NOT OPEN REMOTELY			SIDEWIRE ON POSITION CONTROLLER GOT OFF
G DR3 030246 012280 L MV B16 S 1 T	LPCI VLV MO-3-1501-11B FAILED TO CLOSE			PROBLEMS WITH VLV SUPPLY BREAKER
G DR3 030528 030680 L MV A16 S 1 T	LPCI VLV MO-3-1501-22A FAILED TO OPEN DURING TEST			LOOSE WIRE IN MCC SUPPLYING PWR TO VLV
G DR3 033668 121980 F MV B16 S 1 N	DRYFELL SPRAY HEADER ISD-VLV WOULD NOT CLOSE			STUCK PLUNG.ON CLOS.COIL OF VLV MOTOR (RM
G DR3 033713 122380 L RM B16 S 1 T	SHUTDOWN COOL.SYS.INBOARD ISO.VLV DID NOT CLOSE			PROBLEMS IN VLV CONTROL CIRCUITRY
G EN1 014785 040776 L MV F20 1 M	VALVE E11-F047A FAILED TO OPERATE ELECTRICALLY			A MOTOR WINDING FAILURE OCCURRED
G EN1 014792 050176 H MV A26 R 1 N	HPC1 DISCHARGE VALVE E41-F006 FAILED TO OPEN			FAILURE OF A SNAP LOCK LIMIT SWITCH
G EN1 015555 061576 H MV A00 R 1 N	HPC1 VALVE E41-F006 DID NOT FULLY OPEN			CAUSE UNKNOWN
G EN1 018191 060477 L RM F02 C 1 T	LPCI VALVE E11-F017B CYCLE TIME OUTSIDE T.S.			VALVE STEM PACKED TOO TIGHTLY/PERSONNEL
G EN1 022113 070278 L MV A16 S 1 T	RHR MOV E11-F024A FAILED TO OPEN			DIRT IN INTERLOCK ON BREAKER CAUSED BIND
G EN1 025019 011979 H MV F20 1 T	HPC1 INJECTION VALVE FAILED TO OPERATE			MOTOR BURNED UP
G EN1 026631 072679 L MV F16 U 1 M	RHR OUTBOARD ISOLATION VALVE MADE INOPERABLE			NO PWR AVAILABLE TO VLV (PERSON.ERROR)
G EN1 030031 010580 L MV F00 R 1 T	RHR VLV 1E11-F004 FAILED TO OPER IN REQ TIME			CAUSE UNKNOWN AT PRESENT
G EN1 031143 042980 L MV A20 R 1 T	MOV 1E11-F016A FAILED TO OPEN DURING TEST			KEY BETWEEN MOTOR SHAFT AND PINION FAILED

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

P E N T N A L	C O N T R O L N U M B E R	E V E N T D A T E	S C H A F T O D U S P E L H	M O D E D E S C R I P T I O N	C A U S E D E S C R I P T I O N	
					1	2
G EN1 031281	052580 L MV A16 S	1	RHR VALVE 1E11-F006B FAILED TO OPEN	FAULTY AUX CONTACT BLOCK (COMMAND FAULT)		
G EN1 0317698	071180 L MV F16 S	1	LPCI INJECTION VLV LOST POWER (INVERTER OVERHEATED)	LOSS OF POWER (PERSONNEL SEE 31760A)		
G FN1 032190	080680 L MV A20	1	RHR VLV 1E11-F015A FAILED TO OPEN ON TEST	MOTOR HOLDINGS AND ROTOR FOUND BURNED		
G EN1 032667	091980 L RM B16 S	1	HPC1 MIN FLOW VLV 1E41-F012 FAILED TO CLOSE (TEST)	NO PWR TO VLV, CONTACTOR WAS BINDING		
G EN2 022024*	071778 L MV F16 U	2V N	RHR VALVES HAD POWER LOST TO THEM	BREAKER TRIPPED DUE TO BLOWN FUSES		
G EN2 022500*	091078 L RM B04	2	N RHR VALVES 2E11-F003A, F047A FAILED TO CLOSE	VALVE GATES SAG+BIND IN FULL OPEN POSITION		
G EN2 022486*	092678 L RM F12	2	RESTRICTED FLOW THROUGH RHR SYSTEM CONTROL VALVFS	DAMAGED CAVITROL TRIMS IN VALVES		
G FN2 022675	102778 H HV F20	1	HPC1 VALVE 2E41-F001 FAILED TO OPERATE	FAILURE OF MOTOR SHUNT FIELD INSULATION		
G EN2 022753*	110678 H HM F16 U	2V T	HPC1 CONTROL VALVES FAILED TO OPERATE	WIRE LEFT OFF BY MAINT PERSONNEL		
G EN2 026148	060379 H HV F20	1	HPC1 SUCTION VALVE EXCEEDED OPERATING TIME	LOOSE CONNECTION IN SHUNT FIELD CIRCUIT		
G EN2 026422	070779 H HV F16 S	1	HPC1 STEAM SUPPLY ISOLATION VALVE FAILED TO OPERATE	MOTOR OPERATED 12 TIMES IN 5 HRS		
G EN2 026639	073079 H HV B20 R	1	HPC1 SUCTION FROM SUPP CHAMBER FAILED TO CLOSE	TURNED MOTOR-PINION KEY HAD SLIPPED ON SP		
G EN2 027321	101579 H HV A20 R	1	HPC1 SUCTION FROM SUPP CHAMBER FAILED TO OPEN	MOTOR WINDING FAILURE		
G EN2 030178	013080 H RM B16 T	1	HPC1 MIN FLOW VLV 2E41-F012 FAILED TO CLOSE	FAILED FCW SW CONTROLLING VLV		
G EN2 030975	042180 H RM F16 T	1	MIN FLOW CONT VLV 2E41-F012 FAILED TO OPER	FLOW SW PROVIDING SIGNAL TO VLV FAILED		
G EN2 033764	050780 L MV B20 C	1	2E41-F006 INBOARD ISO. VLV FAILED TO CLOSE	WATER SHORTED OUT MOTOR OPERATOR WINDINGS		
G EN2 031318*	051480 L MV F26 C	2	N RHR VLV 2E11-F004 & F006 FAILED TO OPERATE	LOOSE & BROKEN LIMIT SWITCHES		
G EN2 031431A	053080 L MV A20 B	2	TORUS SUCTION VLV 2E41-F041642 FAILED TO OPEN	VALVE MOTORS SHORTED OUT(STREAM LEAK)		
G EN2 031555	060480 H RM A16 S	1	N HPC1 VLV 2E41-F003 COULD NOT BE OPENED	LOGIC CKT FAILED TO RESET		
G EN2 031842	071180 H MV A20 R	1	N HPC1 INJ VLV 2E41-F006 FAILED TO OPEN	MOTOR WINDING FAILURE, POSS. EXCEED. DUTY CY		
G EN2 032135	072480 H RM F16 U	1	N HPC1 VLV 2E41-F002 CLOSED WHEN REQUIRED OPEN	INAUDIBLE SIGNAL, OPERATOR BUMPED RELAY		
G EN2 033210A	110480 L RM B23	1	2E11-F007A/RHR MINIMUM FLOW VLV LEAKED DUE TO NOT SHARING CLOSED.	TORQUE SWITCHES ADJUSTED		
G FP1 015058	042076 H MV A20	1	T HPC1 TOPUS SUCTION VALVE FAILED TO OPEN	SHORT IN-OPERATOR MOTOR		
G FP1 015237	070376 L MV A20	1	RHR VALVE 10 MOV 25A FAILED TO OPEN	SUSPECT OPEN CIRCUIT IN MOTOR WINDINGS		
G FP1 016269	102676 L MV A20	1	RHR SYSTEM VALVE 10-MOV-25A WOULD NOT OPEN	VALVE MOTOR OPERATOR BURNED OUT		

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

P L Y E N T	A C T U A T I O N S	C O N T R O L N U M B E R	E V E N T D A T E	S C H O O T U P E P I N T H E L N Y	M O D E D E S C R I P T I O N	C A U S E D E S C R I P T I O N
G FPI 016497	111976 H MV A20	I	N	HPCI VALVE 23-MOV-57 FAILED TO OPEN	FATUE OF VALVE MOTOR WINDINGS	
G FPI 017956	061177 H MV A00	I	T	VALVE 23 MOV 58 FAILED TO OPEN ON TEST SIGNAL	CAUSE UNKNOWN	
G FPI 021142	100477 L MV A23	I	T	LPCI MOV 25A FAILED TO OPEN ON TEST	LOW TORQUE SWITCH SETTING	
G FPI 019310	100877 H MV A23	I	T	HPCI STEAM ISOL VALVE FAILED TO CLOSE ELECTRICALLY	TORQUE SWITCH NEEDED ADJUSTMENT	
G FPI 021022	040678 L MV A16 S	I	N	RHR ISOLATION VALVE 10MOV14 INOPERABLE (CLOSED)	CONTROLLER AUXILIARY CONTACT FAILURE	
G FPI 021023	040878 H MV F12	I	T	VALVE 23MOV14 SEPERATED FROM OPERATOR	FAILURE OF MECHANICAL FASTENERS	
G FPI 021225	042978 H MV A23	I	N	HPCI 23-MOV-15 WOULD NOT OPEN	TORQUE SWITCH WAS RESET	
G FPI 021227	050878 D MV F02 C	I	H	POWER REMOVED FROM CORE SPRAY VALVE MOTOR	PERSONNEL ERROR	
G FPI 021712	062978 H MV B16 S	I	T	HPCI VALVE 23-MOV-15 FAILED TO CLOSE	DEFECTIVE TEMP SWITCHING SIGNAL TO CLOSE	
G FPI 021924	072278 D MV B20	I	T	OUTBOARD INJECTION VALVE 14-MOV-18 FAILED TO CLOS	OPERATOR SHAFT KEY SHEARED	
G FPI 022329	090378 D MV A04	I	T	CORE SPRAY INJECTION VALVE 14-MOV-12B FAIL TO OPEN	DESIGN ERROR, DIFFERENTIAL PRESS.TOO HIGH	
G FPI 026344	062779 L MV A23	I	T	B LOOP LPC1 INJECTION VALVE DID NOT OPEN	TORQUE SWITCH FAILURE	
G FPI 027006	090679 H MV A20	I	T	HPCI CONDENSATE STOPPAGE TANK SUCTION VALVE FAILED	MOTOR FAILURE	
G FPI 027872	122179 D MV A20	I	T	CS ISOLATION VALVE WOULD NOT REOPEN AFTER CLOSURE	MOTOR PINION GEAR LOOSE ON SHAFT	
G FPI 030081	010880 D MV F00	I	R	CORE SPRAY INJ VLV FAILED TO OPERATE PROPERLY	CAUSE NOT KNOWN	
G FPI 033793	010980 D MV A02	I	T	CORE SPRAY INJ VLV 14-MOV-12B FAILED TO OPEN	PERSONNEL ERROR IN ADJ LIMIT & TORQUE SW	
G FPI 030974	041080 H MV B20	I	T	HPCI MIN FLOW VLV FAILED TO CLOSE	CRICKED CRUSH HOLDER ON DRIVE MOTOR	
G FPI 031016	041580 L MV A26	I	N	RHR VLV 10-MOV-67 FAILED TO OPEN	TORQUE BYPASS LIMIT SW SET IMPROPERLY	
G FPI 032007	041880 L MV B07	I	T	RHR VLV 10-MOV-67 FAILED TO FULLY CLOSE	NORMAL WEAR & TEAR, SEAT,DISC,PACKING	
G FPI 032919	101180 L MV B02	I	N	CONT ISUL VLV 10-MOV-57 FAILED TO CLOSE	PERSONNEL ACCIDENTALLY DISENGAGED CLUTCH	
G FPI 033410	120880 H MV F23	I	T	HPCI STEAM SUPPLY VALVE FAILED TO OPERATE	TORQUE SW SET FAILURE	
G MII 016689	121876 L MV B23	I	T	CONDENSATE RETURN VAL 1-IC-4 FAILED TO CLOSE	TORQUE SW SET INCORRECTLY	
G MII 019326	101277 F RM A00	I	N	TORUS SPRAY VLV FAILED TO OPEN ON SIGNAL	CAUSE OF OCCURRENCE IS UNKNOWN	
G MII 027674	111579 L MV F16 S	I	T	LPCI INBOARD ISOLATION VALVE INOPERABLE	ELECTRICAL FAILURE IN MOTOR CONTROLLER	
G M01 015026	060376 H MV B23	I	T	HPCI STM LINE 130 VAL FAILED TO CLOSE	TORQUE SW SETTING DRIFTED TOO LOW	

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

P L Y E N	A C T U A T I O N N U M B R E A T D A T E H P E E S U P L I Y	S C H A T F I V E T O O U P Y A N I D E S U P L I Y	M O D E D E S C R I P T I O N	C A U S E D S C R I P T I O N D E S C R I P T I O N
G M01 015708	090276 F MV B12 R	I N	VALVE MU-2008 FAILED TO OPEN	STEM CLAMP SET SCREWS SHEARED
G M01 018C94	053077 L MV A16 T	I T	"8" RHR INJECTION VALVE FAILED TO OPEN (MO-2013)	CONTACTOR IN CONT.CIRCUITRY DID NOT CLOSE
G M01 018955	0R2R77 L MV A16 T	I T	"BH" RHR INJECTION VALVE FAILED TO OPEN (MO-2013)	CONTACTOR IN CONT.CIRCUITRY DID NOT CLOSE
G M01 019050	090977 F MV FC4 R	I N	VALVE MU 2009 FAILED TO OPERATE PROPERLY	SET CLAMP SCREWS UNDERSIZED
G M01 019158	092377 F MV F12 R	I N	VALVE MO-2008 FOUND FAILED DURING MAINTENANCE	SEAT RING THREADS STRIPPED
G M01 023389	112178 L MV F16 S	I N	MO-2014 LPC1 W/A ADMISSION VALVE INOPERABLE	BLOWN FUSE IN CONTROL POWER CIRCUIT
G M01 026492	070879 L MV A26	I N	TORUS COOLING INJECTION VLV MOTOR OPERATOR FAILED	LIMIT SWITCH DID NOT DEENERGIZE MOTOR
G M01 032221	372980 H MV F20	I I	HPC1 STEAM SUPPLY VLV FAILED TO OPERATE	FAILED MOTOR WINDINGS
G NM1 014656	051576 L MV A20	I M	SHUTDOWN COOL SYST 150 VALVE 38-02 FAIL TO OPEN	OPEN MOTOR WINDINGS
G NM1 018299	063077 H RM F16 S	I T	NO.12 INLET INSIDE IV-8640-01 FAIL TO OPERATE	FAILURE OF ELECT CONTACTOR (CLOSING)
G OCI 014413	040176 F MV A16 S	I T	TORUS SPRAY VLV V-21-15 FAILED TO OPEN ON AUTO.SIG	EFFECT SWITCH IN VLV.MOTOR CONTROL
G OCI 015375	0R2076 F MV A16 S	I T	VLV V-21-18 FAILED TO OPEN ON AUTO START SIGNAL	CAUSE UNKNOWN / VLV OPENED HARD MANUALLY
G OCI 016486	111176 F RM A00	I T	VALVE V-21-5 FAILED TO OPEN/CKT BRKR TRIPPED	INTERMIT.GRD.SHRT.IN VLV.MTR.OPER.PWR.FL
G OCI 016479	120176 D MV A16 T	I T	CORE SPRAY ISU.VLV V-20-15 FAILED TO OPEN ON SIGNAL	VLV.MTR. OPERATOR BREAKER TRIPPED
G OCI 017472	032377 D MV B16 T	I T	CORE SPRAY ISU.VLV V-20-15 INOPERABLE IN OPEN POS.	-ULLY OPEN/IMP.CKT.BRKR.OVERLOAD SETTING
G OCI 018623*	072777 D MV A16 V	2 T	CORE SPRAY ISU.VLV V-20-40 S V-20-15 FAILED TO F-	DEFECTIVE CKT.BRKR. TO MOTOR
G OCI 019080	090877 O MV B16 T	I T	CORE SPRAY ISU.VLV V-20-15 FAILED TO CLOSE	SET SCREW ON TORQUE SW LOOSENESS, SET DRFT
G OCI 022576	091478 L MV A23	I T	VALVE V-14-37 SHOULD NOT OPEN, BRKR TRIPPED	BREAKER TO VALVE NOT RACKED IN PROPERLY
G OCI 023144	120478 F MV A16 U	I T	CONT SPRAY VALVE V-21-78 FAILED TO OPEN ON TESTING	INADVERTENT VALVE CLOSE SIGNAL DURING OP
G OCI 026709	080779 D MV F16 T	I T	CORE SPRAY ISOLATION VALVE V-20-15 INOPERABLE	MOTOR ON VLV OVERHEATED AND DAMAGED WHEN ONE
G PB2 013902	010776 L MV A20	I T	MO-10-25B RHR INJECTION VLV FAILED TO OPEN	MTR SHAFT TO PINION GEAR KEY SHEARED
G PB2 013900	011576 L MV A20	I T	RHR INJECTION VALVE MO-10-25A FAILED TO OPEN	
G PB2 015142	061876 L MV F12	I T	RHR SO COOL SUCT 150 VAL MO-2-10-18 FAIL TO STROKE	VALVE STEM BENT
G PB2 016390	110976 D MV B20	I T	CORE SPRAY VALVE MO-26A FAILED TO CLOSE	MTR OPER GEAR TRAIN FAILED
G PB2 019C94	091377 H MV F16 S	I T	HPC1 TURB EXHAUST VAL MTR DAMAGED	SHORT IN VAL CONTROL CIRCUIT

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

V E N T	P L A N T	C O N T R O L N U M B R	E V E N T D A T E	S Y S T E M C O M P E	M O D E S E	C A U S E P E	T Y P E F L	A N I M U L	A C T I V I T Y Y	MODE DESCRIPTION		CAUSE DESCRIPTION		
G	PB2	026944	090579	L	RM	F02	1	N	BKR FOR "A" RHR LOOP INJ VLV(MO-25A) OPENED	SWITCH HIT BY SCAFFOLDING/PERSONNEL ERROR				
G	PR3	014032	010576	D	MV	A16	S	1	N	MO-3-14-12B(B CORE SPR.LP.INJ.VLV) FAILED TO OPEN	PROBLEM WITH MAGNET/TRIP DEVICE MTR. BRKF			
G	PR3	014475	021776	L	MV	A16	S	1	U	RHR INJ. VLV.MO-10-25A FAILED TO FULLY OPEN	BROKEN WIRE TO OPENING TORQUE SWITCH			
G	PR3	014471	030176	L	MV	B12	R	1	N	B RHR OUTBOARD INJECTION VLV MO-154B FAIL.TO CLOSE	VLV DISC SEPARATED FROM VLV STEM			
G	PR3	016476	112376	D	MV	B23	1	T	CORE SPR.B FULL FL.YST.RET.VLV FAILED TO CLOSE	TORQUE SWITCH SETTING WAS TOO LOW				
G	PR3	018884	090277	H	MV	A09	1	T	HPCI SYS.VLV MO-3-23-41 FAILED TO FULLY OPEN	CORRODED VLV STEM DUE TO VLV PACKING LEAK				
G	PR3	023062	111678	L	MV	A20	R	1	T	RHR VALVE MO154B FAILED TO OPEN ON TESTING	MOTOR & SEVERAL OPERATOR PARTS REPLACED			
G	PR3	026763	010879	L	MV	F00	1	N	VALVE OPERATOR FAILURE ON MO16A CAUSED LOSS OF RHR	NO CAUSE GIVEN. RELEASE RATE EXCEEDED				
G	PR3	031104	042180	L	MV	A05	R	1	T	LPCI VLV MO-3-10-25B FAILED TO OPEN ON TEST	WALWORTH 23-INCH IMPROPER INTERNAL CLEAR?			
G	PR3	031740	060880	F	MV	B05	C	1	T	CONT SPRAY VLV MO-3-10-26B FAILED TO CLOSE	STEM LOCKING NUT NOT STAKED BACKED OUT			
G	PR3	032270	080680	L	MV	A17	1	T	LPCI VLV MO-3-10-25A FAILED TO OPEN DURING TEST	THRUST BEARING IN LIMITORQUE OPER FAILED				
G	PR3	033292	112480	H	RM	F23	1	T	HPCI VLV MO-3-23-1 /EPT DRIVING CLOSED ONCE AND //	FAILED TO CLOSE ANOTHER TIME. TORQUE SW.				
G	PII	018325	062077	L	MV	B12	R	1	N	VALVE MO-1001-36A FAILED TO CLOSE,RHR PUMP OPERAT	KEY WHICH PREVENTS STEM ROTATION SHEARED			
G	PII	019669	110477	L	MV	F20	1	N	MTR OPER FOR VAL MO-1001-18B OVERLOADED,BURNED OUT	WORN GEARS ALLOWED MTR TO RUN AFT VLV CL				
G	PII	026427	062779	L	MV	F00	R	1	T	RHR VALVE 1001-36A INOPERABLE	CAUSE UNKNOWN			
G	PII	026760	072579	L	MV	A12	R	1	N	RHR VALVE MOV-1001-36B INOPERABLE	VALVE STEM GUIDE KEY SHEARED			
G	PII	027177	091979	L	MV	F12	R	1	T	RHR MOV-1001-36B FAILED TO OPERATE	ALLEN SCREW LOOSEND, STEM GUIDE SLIPPED			
G	PII	031177	051380	D	RM	A16	S	1	T	CORE SPRAY VLV 1400-24B FAILED TO OPEN	DIRTY CONTACT IN LOGIC CIRCUIT			
G	PII	032578	082580	D	RM	A09	1	T	MO 1400-24A FAILED TO OPEN(CORE SPRAY SYSTEM)	VLV LUBRICATED AND SUCCESSFULLY OPERATED				
G	QCI	015257	070176	F	MV	F12	1	U	LOOP SPRAY VALVE FAILED TO OPERATE(MO-1-1001-23-B)	LOOSE BOLTS HOLDING OPERATOR TO VALVE				
G	QCI	026162	090276	F	MV	B20	1	T	MOV FAILED TO CLOSE DURING TESTING(MO-1-1001-26-A)	EXCESS GREASE/COMPACTATION/HYDRAULIC LOCK				
G	QCI	019489	093077	D	MV	F05	1	T	CORE SPRAY VALVE 1-1402-25B FAILED TO OPERATE	CRACKED YOKE/PROB SINCE INSTALLATION				
G	QCI	020264	111877	H	MV	A23	1	T	HPCI MOV 1-2301-4 FAILED TO OPEN DURING TESTING	MOV HAD DEFECTIVE TORQUE SWITCH				
G	QCI	021436	050478	H	MV	B23	1	T	HPCI PMP SUCTION VLV MO-1-2301-6 WOULD NOT CLOSE	VLV.TORQUE SWITCH WAS WORN OUT				
G	QCI	030440	020680	L	MV	F16	S	1	T	LPCI VLV MO-1-1001-36A FAILED TO OPERATE	POWER TRANSFORMER BURNED OUT(COMMAND)			

REMOTE/MOTOR OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE

P L A N T	C O N T R O L N U M B E R	E V E N T D A T E	S Y S T E M C O D E	C A U S E L	T Y P E E	F I L M	A C T I V I T Y	MODE DESCRIPTION	CAUSE DESCRIPTION
G QC1 030965	041080	L MV A23	1 T	LPCI MD-1-1001-36B	FAILED TO OPEN ON TESTING				TORQUE SWITCH NEEDED ADJUSTMENT
G QC2 019759	111477	D MV A08	1 T	CORE SPRAY MOV 2-1402-24B	FAILED TO OPEN / TEST				STEM AND BONNET BADLY GALLED
G QC2 02L128	040478	L RM F16 S	1 N	VLV FOR FILL WTR TO LPCI DISCHARGE PIPE	FAILED				NO POWER TO VLV, FUSE FAILED
G QC2 025429	021179	L MV B16 S	1 T	RHR SUCTION ISOLATION VALVE	FAILED TO CLOSE				STICKING CONTACTS IN CIRCUIT BREAKER
G QC2 026557	071279	L MV A16 S	1 T	LPCI MOV THERMAL OVERLOAD	TRIPPED				PROBABLE CAUSE-LOOSE CONNECTORS AT BREAKER
G QC2 027100	090579	L MV F12	1 T	DRYWELL SPRAY VALVE	TRIPPED BREAKER WHEN OPERATED				BROKEN BOLT IN VALVE MOTOR OPERATOR
G QC2 027551	102679	L RM F00	1 T	2 C RHR PUMP SUCTION VLV	MD2-100-7C BKR TRIPPED				NO APPARENT CAUSE FOUND
G QC2 031189	042880	L MV B16 S	1 T	LPCI MOV 2-1001-36A	FAILED TO CLOSE DURING TEST				PROBLEM IN CKT BKR SUPPLYING PWR TO VLV
G QC2 032779	091480	D MV A23	1 T	MD-2-1402-3A	WOULD NOT OPEN (CORE SPRAY)				TEMPORARY STICKING OF TORQUE SWITCH
G QC2 032967	101080	F MV A23	1 T	MD-2-1001-29A	FAILED TO OPEN INITIALLY				DISC TO TIGHT, TORQUE SWITCH ADJUSTED
G QC2 032968	101080	L MV A26	1 T	MD-2-1001-34A	FAILED TO OPEN FULLY				LIMIT SWITCHES OUT OF ADJUSTMENT
G QC2 033451	120380	H MV F20	1 N	HPCI INJECTION VLV	MD-2-2301-8 FOUND INOPERABLE				SHORT IN MOTOR OPERATOR
G QC2 033744	123080	L MV A16 S	1 N	RHR VLV MD-2-1001-34A	FAILED TO OPEN				CORRODED CONTACTS IN AUX CONTACTOR
G VY1 014230*	021776	L MV F01 C	2 N	RHR VLVS. 25A&B	WOULD NOT STROKE ELECTRICALLY				PERSON, ERROR(MUST STRO.VLVS.MANUALLY 1ST)
G VY1 014584*	051076	L MV A14 C	2 T	TWO 24 INCH MOV'S (RHR-27A/B)	FAILED TO OPEN / TEST				PACKING MAINTENANCE PROBLEM
G VY1 015855	092076	L MV A00	1 T	LPCI MOV (RHR-25B)	FAILED TO OPEN DURING TESTING				UNKNOWN/WALWORTH AND LIMITORQUE INVESTIG.
G VY1 030837	040180	L MV A20	1 T	LPCI VLV 2-53B	WOULDN'T FULLY OPEN DURING TEST				LOOSE PINION GEAR ON LIMITORQUE OPERATOR
G VY1 032649	093080	H RM F16 S	1 N	V23-19 HPCI PUMP DISCHARGE VLV	LOST CONTROL POWER				OVERLOAD RELAY HAD TRIPPED NO CAUSE

REMOTE/MOTOR OPERATED VALVES - FAILURE TO REMAIN OPEN (PLUGGED)
 ALL FAULTS = BOTH FAILURES AND COMMAND FAULTS
 RATES ARE PER CALENDAR HOUR

TRIPLE OF NUMBERS SHOWS LOWER BOUND, POINT ESTIMATE, UPPER BOUND
 LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

ESTIMATES ARE BASED ON DATA WITH $N = 29, 30, 31, 32, 35, 36, 37, 38, 40, 43, 44, 45, 46, 47, 48, 49, 50, 52, 56$,
 THEY ARE SHOWN FOR FEWER VALUES OF N
 $P = 1.000, .050, .169$

LAMBDA = { 3.6E-21, 5.3E-08, 3.1E-07}

LAMBDA = { 8.2E-08, 3.6E-07, 7.9E-07}

OMEGA = { 2.8E-10, 7.1E-08, 2.7E-07}

SYSTEM SIZE N	SHOCK RATE MU	RATE FOR SPECIFIC COMPONENT	BETA FACTOR
1	{ 1.2E-05, 1.3E-03, 6.6E-04}	{ 1.5E-07, 4.8E-07, 1.4E-06}	
2	{ 6.2E-07, 6.4E-04, 3.3E-04}	{ 8.4E-08, 3.1E-07, 1.0E-06}	{ .028, .219, .330}
3	{ 4.4E-07, 4.2E-04, 2.2E-04}	{ 5.3E-08, 2.5E-07, 8.9E-07}	{ .035, .301, .452}
4	{ 3.5E-07, 3.2E-04, 1.6E-04}	{ 4.3E-08, 2.2E-07, 8.3E-07}	{ .038, .366, .530}
24	{ 1.3E-07, 5.3E-05, 2.8E-05}	{ 7.8E-09, 1.5E-07, 7.2E-07}	{ .034, .668, .828}
25	{ 1.3E-07, 5.1E-05, 2.7E-05}	{ 7.6E-09, 1.5E-07, 7.1E-07}	{ .034, .670, .832}
30	{ 1.3E-07, 4.3E-05, 2.2E-05}	{ 8.9E-09, 1.5E-07, 7.1E-07}	{ .032, .676, .853}
44	{ 1.1E-07, 2.9E-05, 1.5E-05}	{ 5.8E-09, 1.5E-07, 7.1E-07}	{ .028, .675, .890}
58	{ 1.1E-07, 2.2E-05, 1.2E-05}	{ 5.1E-09, 1.4E-07, 7.1E-07}	{ .026, .669, .912}
OVERALL	{ 1.1E-07, 5.3E-05, 6.6E-04}	{ 5.1E-09, 1.5E-07, 1.4E-06}	{ .026, .669, .912}

SYSTEM SIZE N

R2

R3

R4

SYSTEM SIZE N	RATE FOR SET OF K SPECIFIC COMPONENTS
2	{ 7.1E-10, 8.1E-09, 2.9E-07}
3	{ 5.8E-10, 7.8E-09, 2.8E-07}
4	{ 5.2E-10, 7.7E-08, 2.8E-07}
24	{ 3.7E-10, 7.4E-08, 2.8E-07}
25	{ 3.7E-10, 7.4E-08, 2.8E-07}
30	{ 3.6E-10, 7.4E-08, 2.8E-07}
44	{ 3.6E-10, 7.3E-08, 2.8E-07}
58	{ 3.6E-10, 7.3E-08, 2.8E-07}
OVERALL	{ 3.6E-10, 7.4E-08, 2.9E-07}

REMOTE/MOTOR OPERATED VALVES - FAILURE TO REMAIN OPEN (PLUGGED)
FAILURES ONLY
RATES ARE PER CALENDAR HOUR
TRIPLE OF NUMBERS SHOWS (LOWER ROUND, POINT ESTIMATE, UPPER ROUND)
LOWER AND UPPER ROUNDS FORM 90 PERCENT INTERVAL

LAMBDA = (3.8E-10, 8.4E-09, 4.8E-08)
LAMBDA_+ = (2.8E-10, 7.1E-08, 2.7E-07)
OMEGA_+ = (2.8E-10, 7.1E-08, 2.7E-07)

NO DATA WERE OBTAINED FOR ESTIMATING OTHER QUANTITIES

REMOTE/HOT OPERATED VALVES - PLUGGED (FAILED TO REMAIN OPEN)

PLANT	HURTS	PIP	NUMBER OF INDIVIDUAL FAULTS FAILURES/COM FLTS		NUMBER OF NONLETHAL SHOCKS FAILURES/CUM FLTS		NUMBER OF AFFECTED BY NONLETHAL SHOCKS FAILURES/CUM FLTS		VALVES AFFECTED BY LETHAL SHOCKS FAILURES/CUM FLTS		VALVES AFFECTED BY LETHAL SHOCKS FAILURES/CUM FLTS
			0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	
AP1	43800	28	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CR2	34704	29	1 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PA1	24944	22	0 / 0	0 / 0	0 / 1	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
UE1	43800	52	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
UF2	43900	51	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
OF3	43800	46	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PS1	43800	30	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TI1	28368	31	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TI2	8736	47	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BP2	19120	63	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CC1	43800	31	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CC2	35784	31	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
FC1	43800	6	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
FL2	43800	33	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
HY1	43800	35	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PA1	43800	15	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SL1	41112	37	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PV1	40656	49	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TC1	43800	63	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DC2	24600	63	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
HN1	43800	28	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TP2	43800	60	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TP3	41472	66	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
JF1	23712	68	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
KF1	43800	41	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
NA1	23976	48	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
NA2	4872	48	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PV1	43800	54	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PP2	43800	54	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PT1	43800	47	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0

PT?	41800	42	0 / 0	0 / 0	3 / 0	0 / 0
PT?	43800	47	0 / 0	0 / 0	0 / 0	0 / 0
PT?	43800	37	0 / 0	0 / 0	0 / 0	0 / 0
SA1	35496	39	0 / 0	0 / 0	0 / 0	0 / 0
SE1	4320	16	0 / 0	0 / 0	0 / 0	0 / 0
SI1	43800	26	0 / 0	0 / 0	0 / 0	0 / 0
SU1	43800	58	0 / 0	0 / 0	0 / 0	0 / 0
SV1	43800	58	0 / 0	0 / 0	0 / 0	0 / 0
TQ1	43800	41	0 / 1	0 / 1	0 / 0	0 / 0
TY1	43800	50	0 / 0	0 / 0	0 / 0	0 / 0
TI1	43800	50	0 / 0	0 / 0	0 / 0	0 / 0
YR1	43800	28	0 / 0	0 / 0	0 / 0	0 / 0
ZT1	41800	82	0 / 0	0 / 0	0 / 0	0 / 0
ZT2	43800	82	0 / 0	0 / 0	0 / 0	0 / 0
PR1	43920	62	0 / 0	0 / 0	0 / 0	0 / 0
RF?	43800	63	0 / 0	0 / 0	0 / 0	0 / 0
RF3	39496	63	0 / 0	0 / 0	0 / 0	0 / 0
RR1	37032	72	0 / 0	0 / 0	0 / 0	0 / 0
RR2	43800	72	0 / 0	0 / 0	0 / 0	0 / 0
CO1	41800	57	0 / 0	0 / 0	0 / 0	0 / 0
DA1	43800	67	0 / 0	0 / 0	0 / 0	0 / 0
DE?	43800	51	0 / 0	0 / 0	0 / 0	0 / 0
DR1	43800	51	0 / 0	0 / 0	0 / 0	0 / 0
EN1	43800	68	0 / 1	0 / 0	0 / 0	0 / 0
EN?	21816	67	0 / 0	0 / 0	0 / 0	0 / 0
EP1	43800	18	0 / 0	0 / 0	0 / 0	0 / 0
MII	43800	34	0 / 0	0 / 0	0 / 0	0 / 0
MN1	43800	47	0 / 0	0 / 0	0 / 0	0 / 0
ME1	43800	21	0 / 0	0 / 0	0 / 0	0 / 0
UC1	43800	42	0 / 0	0 / 0	0 / 0	0 / 0
PA2	43800	58	0 / 0	0 / 0	3 / 0	0 / 0
PA3	43800	58	0 / 0	0 / 0	0 / 0	0 / 0
PT1	43800	47	0 / 0	0 / 0	0 / 0	0 / 0
OC1	43800	57	0 / 1	0 / 0	0 / 0	0 / 0
QC?	43800	57	0 / 0	0 / 0	0 / 0	0 / 0
YY1	43800	56	0 / 0	0 / 0	0 / 0	0 / 0
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AL?	2602616	3104	1 / 5	0 / 2	0 / 3	0 / 0

REMOTE/MOTOR-OPERATED VALVES - FAILURE TO REMAIN OPEN (PLUGGED)

PLANT VENT	CONTROL NUMBER	EVENT DATE	S Y S T E M P C O M P E E S P E L	C A U S E E E L Y	F A I L U N Y	ACT IV I T Y		
							MODE DESCRIPTION	CAUSE DESCRIPTION
B CR3 022361	081978	L RM G16 T	1 N	DHV-3 WEP	CLOSED WHEN REQUIRED TO REMAIN OPEN		LOSS OF 120 VOLT AC VITAL BUS (INVERTER)	
B CR3 030667	030680	L RM G00	1 N	DECAY HEAT SUCTION ISO VLV DHV-3	CLOSED INADVERTEN //TLY.	NO CAUSE COULD BE FOUND		
B DB1 032122	081380	L RM G16 V	1 N	DECAY HEAT ISO VLV DH-11	BEGAN CLOSING, STOPPED PMP	PERSONNEL FAILED TO BLOCK AUTO CLOS. SIGNAL		
C PA1 020230	122377	H MV G16 T	1 T	MOV-3011(HPCI ISO.VLV)	FAILED TO REMAIN OPEN		BAD SWITCH CAUSED CLOSING CONT. TO STICK	
W TRI 014504	022176	L MV G16 S	1 N	RHR VLV	CLOSED WHEN IT WAS REQUIRED TO REMAIN OPEN	VOLT. FLUC. ON INSTRUMENT AC BUS		
W TRI 021068*	032078	L MV G16 U	2V T	DEENERGIZING PROTECTION SYS	CAUSED RHR VALVES TO-- --CLOSE//	PROCEDURAL DEFICIENCY		
G EN1 015564	072076	L RM G16 S	1 T	RHR FLOW VALVE E11-F007B	FAILED TO STAY OPEN		DEFECTIVE SWITCH SUPPLYING SIGNAL TO VALV	
G QC1 018459	061177	H RM G16 S	1 T	HPCI PUMP INLET VALVE	WOULD NOT STAY OPEN/TESTING		MALFUNCTION IN LOCAL VALVE CONT STAT CIRC	

REMOTE/MOTOR OPERATED VALVES - IMPROPER VALVE CONFIGURATION

COMMON CAUSE COMMAND FAULTS ONLY

RATES ARE PER CALENDAR HOUR

TRIPLE OF NUMBERS SHOWS (LOWER BOUND, POINT ESTIMATE, UPPER BOUND)

LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

ESTIMATES ARE BASED ON DATA WITH M = 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 20, 23, 24, 25, 27, 28,
THEY ARE SHOWN FOR FEWER VALUES OF M

P = (.019, .037, .058)

LAMBDA = (1.8E-09, 3.1E-08, 1.3E-05)

OMEGA = (2.8E-10, 7.1E-08, 2.7E-07)

SYSTEM SIZE M	SHOCK RATE MU	RATE FOR SPECIFIC COMPONENT R1	BETA FACTOR
1	{ 5.1E-08, 9.6E-05, 4.1E-04}	{ 3.4E-09, 3.3E-06, 1.3E-05}	
2	{ 2.6E-08, 4.9E-05, 2.1E-04}	{ 2.6E-09, 1.7E-06, 6.9E-06}	{ .039, .061, .085}
3	{ 1.8E-08, 3.3E-05, 1.4E-04}	{ 2.4E-09, 1.2E-06, 4.7E-06}	{ .067, .103, .145}
4	{ 1.3E-08, 2.5E-05, 1.1E-04}	{ 2.3E-09, 9.5E-07, 3.6E-06}	{ .093, .142, .197}
24	{ 3.2E-09, 5.7E-06, 2.5E-05}	{ 3.1E-09, 3.4E-07, 9.4E-07}	{ .378, .464, .516}
25	{ 3.1E-09, 5.6E-06, 2.4E-05}	{ 3.2E-09, 3.3E-07, 9.2E-07}	{ .382, .467, .520}
30	{ 2.8E-09, 5.0E-06, 2.1E-05}	{ 3.1E-09, 3.1E-07, 8.4E-07}	{ .380, .478, .540}
44	{ 2.3E-09, 4.1E-06, 1.8E-05}	{ 3.8E-09, 2.9E-07, 7.3E-07}	{ .310, .470, .572}
58	{ 2.1E-09, 3.7E-06, 1.6E-05}	{ 4.0E-09, 2.7E-07, 6.8E-07}	{ .244, .434, .584}
<hr/>			
OVERALL { 2.1E-09, 5.7E-06, 4.1E-04} { 2.3E-09, 3.4E-07, 1.3E-05} { .039, .464, .584}			

SYSTEM SIZE M	RATE FOR SET OF K SPECIFIC COMPONENTS		
	R2	R3	R4
2	{ 4.1E-09, 1.3E-07, 4.1E-07}		
3	{ 3.3E-09, 1.1E-07, 3.6E-07}	{ 3.6E-10, 7.3E-08, 2.8E-07}	
4	{ 2.6E-09, 1.0E-07, 3.3E-07}	{ 3.4E-10, 7.3E-08, 2.8E-07}	{ 2.8E-10, 7.1E-08, 2.7E-07}
24	{ 7.1E-10, 7.9E-08, 2.8E-07}	{ 2.9E-10, 7.2E-08, 2.7E-07}	{ 2.8E-10, 7.1E-08, 2.7E-07}
25	{ 6.9E-10, 7.9E-08, 2.8E-07}	{ 2.9E-10, 7.2E-08, 2.7E-07}	{ 2.8E-10, 7.1E-08, 2.7E-07}
30	{ 6.5E-10, 7.8E-08, 2.7E-07}	{ 2.9E-10, 7.2E-08, 2.7E-07}	{ 2.8E-10, 7.1E-08, 2.7E-07}
44	{ 5.8E-10, 7.7E-08, 2.8E-07}	{ 2.9E-10, 7.2E-08, 2.7E-07}	{ 2.8E-10, 7.1E-08, 2.7E-07}
58	{ 5.5E-10, 7.6E-08, 2.8E-07}	{ 2.9E-10, 7.2E-08, 2.7E-07}	{ 2.8E-10, 7.1E-08, 2.7E-07}
<hr/>			
OVERALL { 5.5E-10, 7.9E-08, 4.1E-07} { 2.9E-10, 7.2E-08, 2.8E-07} { 2.8E-10, 7.1E-08, 2.7E-07}			

REMOTE/MOTOR OPERATED VALVES - IMPROPER VALVE CONFIGURATION

VALVE NUMBER	HOLDING TIME	POP	NUMBER OF INDIV. FAULTS FAILS/COM FILTS	NUMBER OF NONLETHAL SHOCKS FAILS/COM FILTS	NUMBER OF AFFECTED BY NONLETHAL SHOCKS FAILS/COM FILTS	VALVES AFFECTED BY LETHAL SHOCKS FAILS/COM FILTS	
						LETHAL SHOCKS FAILS/COM FILTS	LETHAL SHOCKS FAILS/COM FILTS
AIR1	43800	.7R	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
C93	34704	.2R	C / 0	0 / 3	0 / 6	0 / 0	0 / 0
D81	28944	.22	0 / 0	0 / 1	0 / 2	0 / 0	0 / 0
DE1	43800	.52	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DE2	43800	.51	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DE3	43800	.46	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PS1	43800	.30	0 / 0	0 / 1	0 / 2	0 / 0	0 / 0
T11	29368	.31	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
T12	9736	.42	0 / 0	0 / 1	0 / 2	0 / 0	0 / 0
AP2	19120	.63	0 / 0	0 / 1	0 / 1	0 / 0	0 / 0
CC1	43800	.31	0 / 0	0 / 2	0 / 3	0 / 0	0 / 0
CC2	35704	.31	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
FC1	43800	.6	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
ME2	43800	.33	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
HY1	43800	.35	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PA1	43820	.15	0 / 0	0 / 1	0 / 1	0 / 0	0 / 0
SL1	41112	.37	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
AV1	40636	.49	0 / 0	0 / 1	0 / 1	0 / 0	0 / 0
DC1	43800	.63	0 / 0	0 / 1	0 / 1	0 / 0	0 / 0
DC2	24639	.63	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
HNL	43800	.28	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
IP2	43800	.60	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
IP3	41472	.66	0 / 0	0 / 1	0 / 2	0 / 0	0 / 0
JF1	23712	.68	0 / 0	0 / 2	0 / 3	0 / 0	0 / 0
KF1	43800	.41	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
N81	23976	.48	0 / 0	0 / 1	0 / 1	0 / 0	0 / 0
NA2	4872	.48	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PP1	43800	.54	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PP2	43800	.54	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PT1	43900	.47	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0

PT2	43800	47	0 / 0	0 / 1	0 / 1	0 / 0	0 / 0
RC1	43800	47	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
RT2	43800	37	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SAT	35496	39	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SE1	4370	16	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SO1	43800	26	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SU1	43800	55	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SU2	43800	55	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TG1	43800	41	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TH1	43800	50	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TO4	43800	50	0 / 0	0 / 1	0 / 2	0 / 0	0 / 0
Y91	43800	28	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
ZI1	43800	82	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
ZI2	43800	82	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BF1	43800	63	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BF2	43800	63	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
RF3	38496	63	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
RQ1	37C32	72	0 / 0	0 / 1	0 / 1	0 / 0	0 / 0
RQ2	43800	72	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CO1	43800	57	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DA1	43800	67	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DR2	43800	51	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DR3	43800	51	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
EN1	43800	68	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
EN2	21816	67	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
FP1	43800	18	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PT1	43800	34	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
M11	43800	47	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
NM1	43800	21	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
OC1	43800	42	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PA2	43800	58	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PA3	43800	58	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PT1	43800	47	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
QC1	43800	57	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
QC2	43800	57	0 / 0	0 / 1	0 / 1	0 / 0	0 / 0
VR1	43800	56	0 / 0	0 / 1	3 / 2	0 / 0	0 / 0
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All	2600616	3104	0 / 0	0 / 21	0 / 32	0 / 0	0 / 0

REMOTE/MOTOR OPERATED VALVES - IMPROPER VALVE CONFIGURATION

P L A N E N T	V N T	C O N T R O L	S Y S T E M	C O M P U T E	M A T H E F E L Y	A C T I V I T Y	MODE DESCRIPTION	CAUSE DESCRIPTION
B CR3 0173228	030777	H RM	V01	U	2L	M	"B" LOOP OF RPI SYS. ISOLATED TO T.S. FOR MAINTENANCE PERSONNEL ERROR	
B CR3 017658	042177	G RM	V01	V	2	N	SUCT. VLV S CAV-38846 FROM BORIC ACID STOR.TANK. SHIFT T.S.VTO./PERSONNEL ERROR/IMP.VLV LINEUP	
B CR3 023237	103078	G RM	V01	V	2	N	CONC.BORIC ACID TK.DISC.VLV S.CAV38843 CLOSED/ITS VT PERSONNEL ERROR;IMPROPER VALVE LINEUP	
B DB1 025520	030679	H RM	V01	U	2	N	BORATED WTR STOR TANK ISO VLV DH7A678 CLOSED WHEN REQUIRED OPEN--PERSONNEL ERROR	
B RSI 019666	111177	H MV	V04	U	2	T	VALVE LINE-UP INCORRECT//NEW VALVES WERE INSTALLED --WITH OPEN/CLOSE INDICATION ATYPICAL	
B TIZ 027456A	032879	B RM	V00	U	2L	N	AUX FEEDWATER BLOCK VLV DISCOVERED CLOSED	NO CONCLUSIVE CAUSE COULD BE FOUND
C AR2 031374	040830	F RM	V03	V	4	T	*A* TRAIN CONT. SPRAY ACCIDENTALLY INITIATED	PERSONNEL ERROR DURING TESTING
C CC1 025619	041179	H MV	V06	U	1	T	SI HDR ISO VLV SI-856 SHUT WHEN REQUIRED OPEN	DEFECTIVE PROCEDURES
C CC1 0267P5	082879	L MV	V01	U	2	T	SI-4145-MOV OPEN REQ SHUT, SI-4143-MOV SHUT REQ OPEN OPERATIONS PERSONNEL ERROR	
C PA1 032224	091980	H RM	V03	U	1	N	CV-3031 WAS CLOSED AND THEN IMMEDIATELY OPENED	OPERATOR FAILED TO RELATE TEST REQUIRE.
W BVI 027663	112779	H MV	V01	U	1	M	HHSI PMP SUC VLV CH-1150 ISO FOR MAINT WHEN REQ DP PERSONNEL ERROR--2ND VLV ALSO SHUT	
W DC1 016648	121776	F MV	V01	U	1	T	CONTAINMENT SPRAY PUMP SUCTION VALVE FOUND CLOSED	PERSONNEL LEFT VALVE SHUT AFTER A TEST
W IP3 014604	042976	F PM	V03	U	2L	T	INCRT.VLV LINUP FOR TEST,CNTMNT SPRY ACCID.TURN ON PERSONNEL ERROR	
W JF1 020993	032578	B MV	V02	U	2	N	MDA FP & TDAFP RECIRC BYPASS ISO VLVS OPEN	PERSONNEL ERROR
W JF1 022629	091878	L RM	V06	U	1	T	RHR PUMP SUCTION VLV 8701A CLOSED WHEN REQ. OPEN	INADEQUATE PROCEDURES
W NAI 027593	110679	L RM	V02	U	1	N	RHR INLET VLV MDV-1701 SHUT WHEN REQ. OPEN	MAINTENANCE PERSONNEL ERROR
W PT2 018572	072877	H MV	V01	U	1	N	MDV FOUND IN INTERMEDIATE POSITION/SINCE PREV TEST PERSONNEL FAILED TO ASSURE FULLY OPEN	
W TU4 019421	091377	L RM	V01	U	2	T	TWO VALVES INADVERTANTLY OPENED/RWST LEVEL DECREAS PERSONNEL ERROR/POSSIBLE PROCEDURE PROBL	
G BP1 029036	121979	L MV	V01	U	1	N	RHR THURS SUCTION VALVE FOUND SHUT	OPERATOR ERROR-FORGOT TO OPEN VALVE
G QC2 021561	052178	D RM	V01	U	1	N	ZA CORE SPRAY SUC.VLV. NO 2-1402-3A CLOSED WHEN RE- REQUIRED TO BE OPEN//PERSONNEL ERROR	
G VY1 016997	011877	L RM	V03	U	2L	T	"B" RHR PMP DISCH.VLV. SHIFT WHEN REQ. TO BE OPEN PERSONNEL ERROR	

Manually Operated Valves

Rates are estimated for three failure modes in manually operated valves: failure to open, close, or operate; failure to remain open (plugged); and improper valve configuration. Twenty-six LERs involve manually operated valves. Of these, 22 are reports of faults due to improper valve lineup and 4 are reports of failures to open, close, or operate. Any LER involving improper valve configuration is coded as a common cause event and as a command fault, rather than a failure. Therefore, the rates estimated in this mode are for common cause command faults. No LERs involve faults due to plugged valves or valves unable to remain open, so most quantities cannot be estimated for this mode. Summary tables of all the faults and brief one-line descriptions of the LERs follow the estimated rates.

MANUALLY OPERATED VALVES - FAILURE TO OPEN, CLOSE, OR OPERATE
ALL FAULTS - BOTH FAILURES AND COMMAND FAULTS
RATES ARE PER CALENDAR HOUR
TRIPLET OF NUMBERS SHOWS LOWER BOUND, POINT ESTIMATE, UPPER BOUND
LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

LAMBDA = { 1.7E-08, 3.3E-08, 6.1E-08}
LAMBDA+ = { 2.7E-10, 7.0E-08, 2.7E-07}
OMEGA = { 2.7E-10, 7.0E-08, 2.7E-07}

NO DATA WAS OBSERVED FOR ESTIMATING OTHER QUANTITIES

MANUALLY OPERATED VALVES - FAILURE TO REMAIN OPEN (PLUGGED)
ALL FAULTS - BOTH FAILURES AND COMMAND FAULTS

RATES ARE PER CALENDAR HOUR
TRIPLE OF NUMBERS SHOWS LOWER BOUND, POINT ESTIMATE, UPPER BOUND
LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

LAMRDA = { 1.4E-11, 3.6E-09, 1.4E-08 }

LAMRDA+ = { 2.7E-10, 7.0E-08, 2.7E-07 }

OMEGA = { 2.7E-10, 7.0E-08, 2.7E-07 }

NO DATA WERE OBSERVED FOR ESTIMATING OTHER QUANTITIES

MANUALLY OPERATED VALVES - IMPROPER VALVE CONFIGURATION

COMMON CAUSE COMMAND FAULTS ONLY

RATES ARE PER CALENDAR HOUR

TRIPLE OF NUMBERS SHOWS (LOWER BOUND, POINT ESTIMATE, UPPER BOUND)

LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

ESTIMATES ARE BASED ON DATA WITH M = { 1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 24, 25, 26,
27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 38, 39, 40, 41, 42, 43, 45, 46, 52, 53, 57, 72, 78 }

P = { .005, .016, .031 }

LAMBDA = { 4.5E-11, 3.1E-06, 1.5E-05 }

OMEGA = { 2.7E-10, 7.0E-08, 2.7E-07 }

SYSTEM SIZE M	SHOCK RATE MU	RATE FOR SPECIFIC COMPONENT R1	BETA FACTOR
1	{ 3.1E-07, 2.5E-04, 1.2E-03 }	{ 1.5E-10, 3.2E-06, 1.5E-05 }	
2	{ 1.6E-09, 1.3E-04, 6.0E-04 }	{ 1.3E-10, 1.7E-06, 7.7E-06 }	{ .024, .041, .050 }
4	{ 7.9E-10, 6.5E-05, 3.1E-04 }	{ 1.4E-10, 9.2E-07, 4.0E-06 }	{ .053, .090, .136 }
25	{ 1.5E-10, 1.2E-05, 5.6E-05 }	{ 9.4E-10, 2.9E-07, 8.5E-07 }	{ .266, .404, .475 }
26	{ 1.5E-10, 1.1E-05, 5.4E-05 }	{ 9.8E-10, 2.8E-07, 8.3E-07 }	{ .274, .413, .502 }
36	{ 1.1E-10, 8.7E-06, 4.1E-05 }	{ 1.3E-09, 2.5E-07, 6.8E-07 }	{ .337, .477, .556 }
46	{ 9.6E-11, 7.2E-06, 3.4E-05 }	{ 1.5E-09, 2.3E-07, 6.0E-07 }	{ .377, .514, .593 }
78	{ 7.0E-11, 5.1E-06, 2.4E-05 }	{ 2.0E-09, 2.1E-07, 4.9E-07 }	{ .365, .563, .668 }
<hr/>			
OVERALL	{ 7.0E-11, 1.2E-05, 1.2E-03 }	{ 1.3E-10, 2.9E-07, 1.5E-05 }	{ .024, .413, .668 }

SYSTEM SIZE M	R2	R3	R4
2	{ 1.6E-09, 9.5E-09, 3.2E-07 }		
4	{ 1.0E-09, 8.2E-08, 2.9E-07 }	{ 2.9E-10, 7.0E-08, 2.7E-07 }	{ 2.7E-10, 7.0E-08, 2.7E-07 }
25	{ 4.0E-10, 7.2E-09, 2.7E-07 }	{ 2.8E-10, 7.0E-08, 2.7E-07 }	{ 2.7E-10, 7.0E-08, 2.7E-07 }
26	{ 3.9E-10, 7.2E-08, 2.7E-07 }	{ 2.8E-10, 7.0E-08, 2.7E-07 }	{ 2.7E-10, 7.0E-08, 2.7E-07 }
36	{ 3.7E-10, 7.2E-08, 2.7E-07 }	{ 2.8E-10, 7.0E-08, 2.7E-07 }	{ 2.7E-10, 7.0E-08, 2.7E-07 }
46	{ 3.5E-10, 7.1E-08, 2.7E-07 }	{ 2.8E-10, 7.0E-08, 2.7E-07 }	{ 2.7E-10, 7.0E-08, 2.7E-07 }
78	{ 3.3E-10, 7.1E-08, 2.7E-07 }	{ 2.7E-10, 7.0E-08, 2.7E-07 }	{ 2.7E-10, 7.0E-08, 2.7E-07 }
<hr/>			
OVERALL	{ 3.3E-10, 7.2E-08, 3.2E-07 }	{ 2.7E-10, 7.0E-08, 2.7E-07 }	{ 2.7E-10, 7.0E-08, 2.7E-07 }

MANUALLY OPERATED VALVES

PLANT	HOURS	POP	VALVES BY NUMBER OF INDIV. FAULTS			VALVES BY NUMBER OF NONLETHAL SHOCKS			VALVES BY NUMBER OF LETHAL SHOCKS			VALVES BY NUMBER OF FAILS/COM FLTS		
			FAILS/COM FLTS	FAILS/COM FLTS	FAILS/COM FLTS	FAILS/COM FLTS	FAILS/COM FLTS	FAILS/COM FLTS	FAILS/COM FLTS	FAILS/COM FLTS	FAILS/COM FLTS	FAILS/COM FLTS	FAILS/COM FLTS	FAILS/COM FLTS
API	43800	39	0 / 0	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CR3	34704	34	0 / 0	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
OBL	28944	24	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
OF1	43800	75	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
OF2	43800	77	0 / 0	0 / 0	0 / 1	0 / 1	0 / 1	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
OE3	43800	75	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
R51	43800	74	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
T11	28368	25	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
T12	8736	59	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
AR2	18120	42	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CC1	43800	49	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CC2	35784	49	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
FC1	43600	55	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
M12	43800	61	0 / 0	0 / 0	0 / 1	0 / 1	0 / 1	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
MY1	43800	87	1 / 0	0 / 0	0 / 2	0 / 2	0 / 4	0 / 4	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PA1	43800	39	0 / 0	0 / 0	0 / 1	0 / 1	0 / 1	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SL1	41112	59	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BV1	40656	38	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DC1	43800	91	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DC2	24600	91	0 / 0	0 / 0	0 / 2	0 / 2	0 / 2	0 / 2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
HNI	43800	65	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
IP2	43800	73	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
IP3	41472	76	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
JF1	29712	94	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
KE1	43800	50	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
NA1	23976	42	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
HA2	4872	42	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PR1	43800	42	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PR2	43800	42	0 / 0	0 / 0	0 / 1	0 / 1	0 / 1	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PT1	43800	74	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0

PT2	43800	74	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
RG1	43800	64	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
RO2	43800	77	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SAL	35496	85	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SE1	4320	110	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SO1	43800	39	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SU1	43800	56	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SU2	43800	56	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TR1	43800	58	0 / 0	0 / 0	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1
TU3	43800	57	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
TU4	43800	57	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
YR1	43800	26	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
ZI1	43800	72	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
ZI2	43800	72	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BF1	43800	38	0 / 0	0 / 0	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1
BF2	43800	38	0 / 0	0 / 0	0 / 2	0 / 2	0 / 2	0 / 2	0 / 2	0 / 2	0 / 2
BF3	38496	38	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BD1	37032	41	0 / 0	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1
BR2	43800	41	0 / 0	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1
CD1	43800	5	0 / 0	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1	0 / 1
DA1	43800	34	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DR2	43800	44	0 / 0	0 / 1	0 / 1	0 / 2	0 / 2	0 / 2	0 / 2	0 / 2	0 / 2
DR3	43800	44	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
EN1	43800	40	0 / 0	0 / 4	0 / 4	0 / 7	0 / 7	0 / 7	0 / 7	0 / 7	0 / 7
EN2	21816	43	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
FP1	43800	33	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
M11	43800	71	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
M01	43800	52	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
NM1	43800	28	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DC1	43800	15	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
P82	43800	58	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
P83	43800	58	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
P11	43800	30	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
QC1	43800	39	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
QC2	43800	39	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
YY1	43800	51	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
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ALL	2600516	3536	6 / 0	0 / 22	0 / 28	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0

MANUALLY OPERATED VALVES

V E N T	P L A N T	C O N T R O L N U M B R E H	E V E N T D A T E	S Y S T E M C O M P E E L H	C A T O D E S P E L H	F A N U M B R E H	A C T I V I T Y	MODE DESCRIPTION		CAUSE DESCRIPTION
								M	A	
B ARI 015207	061276	H XV V06 U	1 N	VALVE SF-22 WAS NOT CLOSED/DIA SPILL RESULTED						PROCEDURES WERE INADEQUATE
B CR3 023095A	100478	I XV V03 U	1 T	ISOL VALVE TO FLOW CONTROLLER SHUT(SEE 023095)						PERSONNEL ERROR/VALVE REQUIRED TO BE OPEN
B DE1 014808	041376	H XV F12	1 N	FLOOD TANK 1A NITROGEN ADD VLV FAILED OPEN						VAL STEM SEPERATED FROM DISK
B DE2 019970	120877	F XV V01 U	1 N	ISO.VLV. TO CHAN.3 RB PRESS.TRANS.SHUT BY MISTAKE						PERSONNEL ERROR
C MIZ 031945	070380	O XV V06 U	1 T	HPSI PUMP MINIMUM FLOW VLV WAS SHUT						DEFECTIVE PROCEDURES CAUSED PUMP SEIZURE
C MY1 026274	060779	O XV A12	1 N	CS-14 PB TRAIN SPRAY HEADER ISO.VLV WOULD NOT OPN						REMOTE LINKAGE DISCONNECT FROM HANDWHEEL
C MY1 030804	031980	O XV V01 U	2 N	RHR VLVS RH-8 AND RH-10 FOUND OPENED AND UNLOCKED						PERSONNEL ERROR
C MY1 031390	050780	O XV V03 U	2L U	COOLING WATER IMPROP LINED UP TO S-CHARGING PUMP						PERSONNEL ERROR (SEPARATION NOT MAINTAIN)
C PA1 032156	071980	O XV V03 U	1 N	INST. EQ. VLV NOT CLOSE AFTER CALIBRATION						PERSONNEL ERROR WHEN CAL. HPSI FLOW IND.
W DC2 021079	041678	I XV V01 U	1 N	HANDWHEEL CAME OFF RHR VALVE POSITIONING IT WRONG						PERSONNEL FAILED TO REPOSITION THE VALVE
W DC2 022838M	101078	B XV V01 U	1 T	AUX FEED VALVE FOUND UNLOCKED & OPEN/WRONG LINE-UP						PERSONNEL ERROR
W IP3 030696	031580	O XV A08	1 T	VC ISO VLV 8698(ISO SPRAY PUMP FROM CONT SPRAY HDR DIDN'T OPEN,KEY FAILURE IN YOKE NUT BUSH.						
W PR2 017889	051977	B XV V06 U	1 U	PUMP INLET VALVE FOUND NEARLY SHUT/AUX FEED INLET						POSITION REQUIREMENT WILL GO ON CHECKLIST
W TR1 019580	101677	I XV V01 U	1 N	RHR DISCHARGE VLV (87288) FOUND LOCKED CLOSED						PERSONNEL ERROR/IMPROPER VALVE LINEUP
G BF1 016053	092376	D XV V02 U	1 U	VALVE FOUND CLOSED TO PRESSURE SWITCH						PERSONNEL ERROR
G BF2 016199	100776	H XV V03 U	1 T	EQUALIZER VALVE ON FLOW INSTRUMENT FOUND OPEN						PERSONNEL ERROR
G BF2 021782	062778	H XV V01 U	1 T	VALVE LEFT SHUT IN LUB OIL LINE TO HPCI PUMP						PERSONNEL ERROR IN VALVE LINE UP
G BR1 030407	021480	H XV V01 V	1 T	MANUAL ISOL VLV LOW SIDE OF 1E41LS15A FOUND CLOSED						PERSONNEL ERROR (WHEN UNDETERMINED)
G BR2 014647	020576	L XV V03 U	1 N	PRESS SW FOUND ISOLATED AFTER TESTING						PERSONNEL ERROR
G CO1 020806A	020778	H XV V03 V	1 T	ISOLATION VALVE TO DPIS-76 FOUND CLOSED(SEE020806)						PERSONNEL ERROR
G DA1 015991	092876	H XV COO	1 T	HPCI TURB STM LINE HI FLO EQUALIZING VALVE LEAKS						CAUSE UNKNOWN
G DR2 021158	042878	L XV V01 U	2L N	VALVES IN LPCI & CORE SPRAY LINED UP IMPROPERLY						OPERATING PERSONNEL ERROR
G EN1 017096	011777	L XV V03 U	1 U	PRESS SW FOUND VALVED OUT WHEN REQUIRED OPEN						PERSONNEL ERROR
G EN1 031157	051080	L XV V03 U	2 N	TWO COOLING WTR VLVS TO PUMPS A & B FOUND CLOSED						PERSONNEL ERROR
G EN1 031521	062280	L XV V01 U	2 T	RHR MIN FLOW VLVS E11-F0188 & D FOUND CLOSED						PERSONNEL ERROR

MANUALLY OPERATED VALVES

PLANT NUMBER	CONTROL NUMBER	EVENT DATE	SYSTEM TEMP	COM- MODE	CAUSE CODE	TYPE ELM	VALVE NUM	ACTIVITY	MODE DESCRIPTION		CAUSE DESCRIPTION	
G EN1 0317694	071180	L XV V01 U	2L N	COOLING WATER VLV SECURED WHEN REQUIRED OPEN					PERSONNEL ERROR			
G MO1 023390	112478	S XV C25	1 N	HPC1 DRAIN VALVE CV-2043 LEAKING THRU INTERNALLY					INTERNAL PARTS NEED REPLACEMENT			
G VY1 019854	110177	D XV F08	1 T	MANIFOLD BYPASS VALVE FAILED TO OPERATE					GALLED THREADS/STEM SEIZED			

PWR Safety and BWR Relief Valves

There are 9 LERs on PWR safety valves and 71 LERs on BWR relief valves. For both types of valves, rates are estimated for failure to open, failure to close, and internal leakage. No common cause events were reported for safety valves or for failures to close in relief valves, so most quantities cannot be estimated in these cases. Although rates are not estimated for failure to operate or improper valve lineup, events involving these modes are included in the summary tables of faults and in the one-line descriptions.

PWR SAFETY VALVES - FAILURE TO OPEN
ALL FAULTS - 90TH FAILURES AND COMMAND FAULTS
RATES ARE PER ESTIMATED DEMAND
TRIPLET OF NUMBERS SHOWS LOWER BOUND, POINT ESTIMATE, UPPER BOUND
LAMDA AND UPPR ROUNDS FORM 90 PERCENT INTERVAL

LAMDA = { 1.1E-05, 4.4E-03, 1.8E-02 }
LAMDA = { 3.0E-05, 7.5E-04, 2.9E-03 }
OMEGA = { 3.0E-06, 7.5E-04, 2.9E-03 }

NO DATA WERE OBSERVED FOR ESTIMATING OTHER QUANTITIES

PWR SAFETY VALVES - FAILURE TO CLOSE
ALL FAULTS - BOTH FAILURES AND COMMAND FAULTS
RATES ARE PER ESTIMATED DEMAND
TRIPLE OF NUMBERS SHOWS (LOWER ROUND, POINT ESTIMATE, UPPER ROUND)
LOWER AND UPPER ROUNDS FORM 90 PERCENT INTERVAL

LAMBDA = { 1.1E-06, 2.8E-06, 1.1E-03 }
LAMBDA+ = { 3.0E-06, 7.5E-06, 2.9E-03 }
OMEGA+ = { 3.0E-06, 7.5E-06, 2.9E-03 }

NO DATA WERE OBSERVED FOR ESTIMATING OTHER QUANTITIES

PWP SAFETY VALVES - INTERNAL LEAKAGE
ALL FAULTS - 90TH FAILURES AND COMMAND FAULTS
RATES ARE PER CALENDAR HOUR
TRIPLE OF NUMBERS SHOWS LOWER ROUND, POINT ESTIMATE, UPPER ROUND
LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

LAMBDA = { 1.2E-20, 1.2E-06, 7.0E-06}
LAMBDA+ = { 1.2E-09, 3.0E-07, 1.1E-06}
OMEGA+ = { 1.2E-09, 3.0E-07, 1.1E-06}

NO DATA WERE OBSERVED FOR ESTIMATING OTHER QUANTITIES

PWR SAFETY VALVES

PLANT	HOURS	POP	VALVES AFFECTED BY INOVY FAULTS/COM FLTS			VALVES AFFECTED BY NONLETHAL SHOCKS FAILRS/COM FLTS			VALVES AFFECTED BY LETHAL SHOCKS FAILRS/COM FLTS			VALVES AFFECTED BY LETHAL SHOCKS FAILRS/COM FLTS
			/	/	/	/	/	/	/	/	/	
ARI	43800	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CR3	34704	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DB1	28944	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DE1	43800	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DE2	43800	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
DE3	43800	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
RS1	43800	2	3 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
T11	28368	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
T12	8736	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
AR2	16120	3	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CC1	43800	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
CC2	3574	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
FC1	43800	2	1 / 0	0 / 1	0 / 1	0 / 2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
HL2	43800	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
HY1	43800	3	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PA1	43800	3	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
SL1	41112	3	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
BV1	40656	3	2 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
OC1	43800	3	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
OC2	24000	3	0 / 0	0 / 0	0 / 1	0 / 1	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
HN1	43800	3	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
IP2	43800	3	2 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
IP3	41452	3	1 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
JF1	23712	3	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
RF1	43800	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
NA1	23976	3	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
NA2	4872	3	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PR1	43800	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PR2	43800	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0
PT1	43800	2	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0	0 / 0

9T2	43800	2	0 / 0	0 / 0	0 / 0
RG1	43800	2	0 / 0	0 / 0	0 / 0
RD2	43800	3	0 / 0	0 / 0	0 / 0
SA1	35496	3	0 / 0	0 / 0	0 / 0
SF1	4320	3	0 / 0	0 / 0	0 / 0
SD1	43800	2	0 / 0	0 / 0	0 / 0
SU1	43800	3	1 / 0	0 / 0	0 / 0
SU2	43800	3	0 / 0	0 / 0	0 / 0
TR1	43800	3	0 / 0	0 / 0	0 / 0
TU3	43800	3	0 / 0	0 / 0	0 / 0
TU4	43800	3	0 / 0	0 / 0	0 / 0
YR1	43800	2	2 / 0	0 / 0	0 / 0
ZI1	43800	3	0 / 0	0 / 0	0 / 0
ZI2	43800	3	0 / 0	0 / 1	0 / 0
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All	1671072	111	14 / 0	0 / 3	0 / 5

PWR SAFETY VALVES

PLAN	CONTROL NUMBER	EVENT DATE	SYNOPSIS	MODE DESCRIPTION		CAUSE DESCRIPTION
				ACT	ACT	
B RSI	021746B	061178 K RV COO	3 T 2 SAFETY, 1 ELECTRO RV LEAKING THRU DURING TESTING	UNKNOWN/2 REPLACED, 1 REBUILT		
C FC1	019551	102677 K RV AOO R	1 M VALVE RC-142 RELIEF PRESSURE OUT SPEC HIGH	COULD NOT BE DETERMINED		
C FC1	023171	122078 K RV V06 U	2 M TWO PRESS OP RELIEF VALVES OPENED WHEN REQ CLOSED	TECH PULLED FUSES, DEFECTIVE PROCEDURES		
C MY1	022141	081578 K RV AOO	1 M PRESSURIZER RV PPS-13 SETPOINT OUT OF SPEC	CAUSE UNKNOWN, SETPOINT ADJUSTED		
C PAL	0273658	101279 K RV A12	1 T RV1039(PZR RELIEF V.V) SET PRESSURE FOUND HIGH	ALIGNMENT PIN FOUND MISPOSITION		
W BVI	033542*	121880 K RV F00 R	2Y U PLANT DOWN TO REPAIR PZR SAFETY VLVS	CAUSE NOT GIVEN		
W OC2	0222581	092278 K RV V01 U	1 T PRESSURIZER RV OPENED WHEN REQUIRED TO BE CLOSED	PERSONNEL ERROR		
W IP2	018788A	051377 K RV AOO R	1 T RV PCV-468 DID NOT OPEN AT SETPOINT PRESSURE	SET POINT DRIFT		
W IP2	0187888	051377 K RV C25	1 T INTERNAL LEAKAGE PAST VALVE PCV-466	EXCESSIVE VALVE SEAT WEAR		
W IP3	033011A	101780 K RV C25	1 T PCV-466 WOULD NOT RELEASE AT SET PRESSURE & LEAKED VALVE SEAT AND DISK HAD GROOVES			
W SUI	0168828	111376 K RV AOO R	1 T PRESS SAFETY VLV (SV15518) OPENED AT HI PRESS	UNKNOWN/ SETPOINT DRIFT™ UP		
W YRI	018419*	062777 K RV AOO	2 T PRESSURIZER SAFETY VALVES (1017182) FAILED TO OPEN UNKNOWN/ SETPOINT DRIFTED HIGH/DRESSER INC			
# Z12	031625	061880 K RV V06 U	2 N IMPROPER VLV LINE UP MADE PVRVS INOPERABLE	PROCEDURE CHANGED TO BLOCK THE VLV'S OPEN		

BWR RELIEF VALVES - FAILURE TO OPEN
 ALL FAULTS - 30TH FAILURES AND COMMAND FAULTS

RATES ARE PER ESTIMATED DEMAND

TRIPLE OF NUMBERS SHOWS LOWER BOUND, POINT ESTIMATE, UPPER BOUND
 LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

P = { .079, .256, .471 }
 LAMBDA = { 1.8E-05, 1.9E-02, 7.7E-02 }
 LAMBDA = { 1.1E-06, 4.8E-03, 2.1E-02 }
 OMEGA = { 2.4E-06, 6.1E-04, 2.4E-03 }

SYSTEM SIZE	SHOCK RATE	RATE FOR SPECIFIC COMPONENT	BETA FACTOR
M	H	R1	
3	{ 2.0E-06, 1.1E-02, 4.6E-02 }	{ 5.1E-04, 2.1E-02, 8.2E-02 }	{ .002, .095, .493 }
4	{ 1.7E-06, 8.7E-03, 3.8E-02 }	{ 5.0E-04, 2.1E-02, 8.1E-02 }	{ .002, .095, .501 }
5	{ 1.5E-06, 7.6E-03, 3.3E-02 }	{ 5.0E-04, 2.1E-02, 8.1E-02 }	{ .002, .091, .500 }
6	{ 1.4E-06, 7.0E-03, 3.0E-02 }	{ 5.0E-04, 2.1E-02, 8.1E-02 }	{ .002, .085, .496 }
8	{ 1.3E-06, 6.2E-03, 2.7E-02 }	{ 5.0E-04, 2.1E-02, 8.1E-02 }	{ .002, .071, .471 }
9	{ 1.2E-06, 5.9E-03, 2.6E-02 }	{ 4.9E-04, 2.1E-02, 8.1E-02 }	{ .002, .066, .471 }
11	{ 1.2E-06, 5.6E-03, 7.5E-02 }	{ 4.9E-04, 2.0E-02, 8.1E-02 }	{ .001, .056, .446 }
OVERALL	{ 1.2E-06, 7.0E-03, 4.6E-02 }	{ 4.9E-04, 2.1E-02, 8.2E-02 }	{ .001, .085, .501 }

OVERALL { 1.2E-06, 7.0E-03, 4.6E-02 } { 4.9E-04, 2.1E-02, 8.2E-02 } { .001, .085, .501 }

SYSTEM SIZE	SHOCK RATE	RATE FOR SET OF K SPECIFIC COMPONENTS	R4
M	H	R3	
3	{ 2.5E-05, 1.2E-03, 4.0E-03 }	{ 9.9E-06, 8.0E-04, 2.8E-03 }	
4	{ 2.3E-05, 1.1E-03, 3.8E-03 }	{ 8.9E-06, 7.8E-04, 2.7E-03 }	{ 4.6E-06, 6.8E-04, 2.5E-03 }
5	{ 2.2E-05, 1.1E-03, 3.6E-03 }	{ 8.3E-06, 7.7E-04, 2.7E-03 }	{ 4.4E-06, 6.7E-04, 2.5E-03 }
6	{ 2.1E-05, 1.0E-03, 3.6E-03 }	{ 8.0E-06, 7.6E-04, 2.7E-03 }	{ 4.3E-06, 6.7E-04, 2.5E-03 }
8	{ 1.9E-05, 1.0E-03, 3.5E-03 }	{ 7.6E-06, 7.6E-04, 2.7E-03 }	{ 4.2E-06, 6.7E-04, 2.5E-03 }
9	{ 1.9E-05, 1.0E-03, 3.5E-03 }	{ 7.4E-06, 7.5E-04, 2.7E-03 }	{ 4.2E-06, 6.7E-04, 2.5E-03 }
11	{ 1.8E-05, 1.0E-03, 3.4E-03 }	{ 7.3E-06, 7.5E-04, 2.7E-03 }	{ 4.2E-06, 6.7E-04, 2.5E-03 }
OVERALL	{ 1.8E-05, 1.0E-03, 4.0E-03 }	{ 7.3E-06, 7.6E-04, 2.8E-03 }	{ 4.2E-06, 6.7E-04, 2.5E-03 }

AWD RELIEF VALUES - FAILURE TO OPEN
FAILURES ONLY

RATES ARE PER ESTIMATED DEMAND
TRIPLE OF NUMBERS SHOWS LOWER ROUND, POINT ESTIMATE, UPPER ROUND
LOWER AND UPPER ROUNDS FORM 90 PERCENT INTERVAL

P = (.079, .256, .471)
LAMDA = (3.2E-06, 1.4E-02, 6.4E-02)
LAMDA+ = (1.3E-03, 4.3E-03, 8.6E-03)
OMEGA+ = (2.4E-06, 6.1E-04, 2.4E-03)

SYSTEM SIZE	SHOCK RATE (NU)	RATE FOR SPECIFIC COMPONENT R1	BETA FACTOR
3	(2.2E-03, 9.5E-03, 2.3E-02)	(1.4E-03, 1.7E-02, 7.0E-02)	(.008, .158, .520)
4	(1.9E-03, 7.9E-03, 1.9E-02)	(1.2E-03, 1.7E-02, 7.0E-02)	(.008, .158, .529)
5	(1.8E-03, 6.9E-03, 1.6E-02)	(1.1E-03, 1.6E-02, 7.0E-02)	(.007, .147, .532)
6	(1.7E-03, 6.3E-03, 1.4E-02)	(1.0E-03, 1.6E-02, 7.0E-02)	(.006, .133, .534)
8	(1.5E-03, 5.5E-03, 1.2E-02)	(9.5E-04, 1.6E-02, 7.0E-02)	(.006, .108, .528)
9	(1.5E-03, 5.3E-03, 1.1E-02)	(9.2E-04, 1.6E-02, 7.0E-02)	(.003, .098, .522)
11	(1.5E-03, 5.0E-03, 1.1E-02)	(8.8E-04, 1.6E-02, 7.0E-02)	(.002, .083, .504)
OVERALL	(1.5E-03, 6.3E-03, 2.3E-02)	(8.0E-04, 1.6E-02, 7.0E-02)	(.002, .133, .534)

SYSTEM SIZE	R2	R3	R4
3	(7.6E-05, 1.1E-03, 3.1E-03)	(1.2E-05, 7.8E-04, 2.6E-03)	
4	(5.8E-05, 1.1E-03, 3.0E-03)	(1.0E-05, 7.6E-04, 2.6E-03)	(4.7E-06, 6.7E-04, 2.4E-03)
5	(4.8E-05, 1.0E-03, 2.9E-03)	(9.4E-06, 7.5E-04, 2.5E-03)	(4.5E-06, 6.7E-04, 2.4E-03)
6	(4.3E-05, 1.0E-03, 2.9E-03)	(8.3E-06, 7.5E-04, 2.5E-03)	(4.4E-06, 6.7E-04, 2.4E-03)
8	(3.7E-05, 9.8E-04, 2.9E-03)	(8.4E-06, 7.4E-04, 2.5E-03)	(4.3E-06, 6.6E-04, 2.4E-03)
9	(3.5E-05, 9.8E-04, 2.9E-03)	(8.2E-06, 7.4E-04, 2.5E-03)	(4.3E-06, 6.6E-04, 2.4E-03)
11	(3.2E-05, 9.7E-04, 2.9E-03)	(8.0E-06, 7.4E-04, 2.5E-03)	(4.2E-06, 6.6E-04, 2.4E-03)
OVERALL	(3.2E-05, 1.0E-03, 3.1E-03)	(8.0E-06, 7.5E-04, 2.6E-03)	(4.2E-06, 6.7E-04, 2.4E-03)

BWR RELIEF VALVES - FAILURE TO CLOSE
ALL FAULTS - 90TH FAILURES AND COMMAND FAULTS
RATES ARE PER ESTIMATED DEMAND
TRIPLE OF NUMBERS SHOWS LOWER ROUND, POINT ESTIMATE, UPPER ROUND,
LOWER AND UPPER ROUNDS FORM 90 PERCENT INTERVAL

LAMBDA = { 2.2E-03, 3.3E-03, 4.5E-03 }
LAMBDA+ = { 2.4E-06, 6.1E-06, 2.4E-03 }
OMEGA = { 2.4E-05, 6.1E-05, 2.4E-03 }

NO DATA WERE MAINTAINED OR ESTIMATING OTHER QUANTITIES

BWR RELIEF VALVES - FAILURE TO CLOSE

FAILURES ONLY

RATES ARE PER ESTIMATED DEMAND

TRIPLE OF NUMBERS SHOWS LOWER BOUND, POINT ESTIMATE, UPPER BOUND
LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

```
LAMBDA = { 2.1E-03, 3.1E-03, 4.4E-03 }
LAMBDA = { 2.4E-06, 6.1E-04, 2.4E-03 }
OMEGA = { 2.4E-06, 6.1E-04, 2.4E-03 }
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NO DATA WERE OBSERVED FOR ESTIMATING OTHER QUANTITIES

BWR RELIEF VALVES - INTERNAL LEAKAGE
 ALL FAULTS - BOTH FAILURES AND COMMAND FAULTS
 RATES ARE PER CALNDAR HOUR

TRIPLE OF NUMBERS SHOWS LOWER BOUND, POINT ESTIMATE, UPPER BOUND
 LOWER AND UPPER BOUNDS FORM 90 PERCENT INTERVAL

$\varphi = \{ .002, .159, .498 \}$
 $\text{LAMBDA} = \{ 7.1E-20, 2.7E-06, 1.5E-05 \}$
 $\text{LAMBDA}_+ = \{ 1.9E-07, 1.6E-06, 4.2E-06 \}$
 $\text{OMEGA} = \{ 2.1E-09, 5.4E-07, 2.1E-06 \}$

SYSTEM SIZE	SHOCK RATE μH	RATE FOR SPECIFIC COMPONENT q_1	BETA FACTOR
3	{ 4.9E-07, 4.2E-04, 2.2E-04 }	{ 2.3E-07, 3.3E-06, 2.0E-05 }	{ *010, *416, *532 }
4	{ 4.2E-07, 3.1E-04, 1.6E-04 }	{ 2.4E-07, 3.4E-06, 2.0E-05 }	{ *010, *471, *652 }
5	{ 3.8E-07, 2.5E-04, 1.3E-04 }	{ 2.3E-07, 3.7E-06, 2.0E-05 }	{ *009, *497, *677 }
6	{ 3.5E-07, 2.1E-04, 1.1E-04 }	{ 1.8E-07, 3.6E-06, 2.0E-05 }	{ *009, *508, *701 }
8	{ 3.2E-07, 1.6E-04, 8.2E-05 }	{ 1.5E-07, 3.6E-06, 2.0E-05 }	{ *008, *508, *742 }
9	{ 3.1E-07, 1.4E-04, 7.3E-05 }	{ 1.4E-07, 3.6E-06, 2.0E-05 }	{ *007, *502, *757 }
11	{ 2.9E-07, 1.1E-04, 6.0E-05 }	{ 1.2E-07, 3.6E-06, 2.0E-05 }	{ *006, *490, *784 }
OVERALL	{ 2.9E-07, 2.1E-04, 2.2E-04 }	{ 1.2E-07, 3.6E-06, 2.0E-05 }	{ *006, *497, *784 }

SYSTEM SIZE	R2	R3	R4
3	{ 7.3E-09, 6.6E-07, 2.3E-06 }	{ 3.4E-09, 5.9E-07, 2.1E-06 }	
4	{ 6.4E-09, 6.5E-07, 2.2E-06 }	{ 3.3E-09, 5.8E-07, 2.1E-06 }	{ 2.6E-09, 5.6E-07, 2.1E-06 }
5	{ 5.9E-09, 6.4E-07, 2.2E-06 }	{ 3.2E-09, 5.8E-07, 2.1E-06 }	{ 2.6E-09, 5.6E-07, 2.1E-06 }
6	{ 5.6E-09, 6.3E-07, 2.2E-06 }	{ 3.2E-09, 5.7E-07, 2.1E-06 }	{ 2.6E-09, 5.6E-07, 2.1E-06 }
8	{ 5.2E-09, 6.3E-07, 2.2E-06 }	{ 3.1E-09, 5.7E-07, 2.1E-06 }	{ 2.6E-09, 5.6E-07, 2.1E-06 }
9	{ 5.1E-09, 6.3E-07, 2.2E-06 }	{ 3.1E-09, 5.7E-07, 2.1E-06 }	{ 2.6E-09, 5.5E-07, 2.1E-06 }
11	{ 4.9E-09, 6.2E-07, 2.2E-06 }	{ 3.1E-09, 5.7E-07, 2.1E-06 }	{ 2.6E-09, 5.5E-07, 2.1E-06 }
OVERALL	{ 4.9E-09, 6.3E-07, 2.3E-06 }	{ 3.1E-09, 5.7E-07, 2.1E-06 }	{ 2.6E-09, 5.6E-07, 2.1E-06 }

BWR RELIEF VALVES - INTERNAL LEAKAGE

FAILURES ONLY

RATES ARE PER CALENDAR HOUR

TRIPLE OF NUMBERS SHOWS (LOWER ROUND, POINT ESTIMATE, UPPER ROUND)

LOWER AND UPPER ROUNDS FORM 90 PERCENT INTERVAL

$$P = (.002, .159, .488)$$

$$\text{LAMBDA} = (7.1E-20, 2.7E-06, 1.6E-05)$$

$$\text{LAMBDA}_+ = (1.9E-07, 1.6E-06, 4.2E-06)$$

$$\text{OMEGA} = (2.1E-03, 5.4E-07, 2.1E-06)$$

SYSTEM SIZE	SHOCK RATE MU	RATE FOR SPECIFIC COMPONENT R1	BETA FACTOR
3	(4.9E-07, 4.2E-04, 2.2E-04)	(2.7E-07, 3.9E-06, 2.0E-05)	(.010, .416, .632)
4	(4.2E-07, 3.1E-04, 1.6E-04)	(2.1E-07, 3.8E-06, 2.0E-05)	(.010, .471, .652)
5	(3.8E-07, 2.5E-04, 1.3E-04)	(1.9E-07, 3.7E-06, 2.0E-05)	(.009, .497, .677)
6	(3.5E-07, 2.1E-04, 1.1E-04)	(1.6E-07, 3.6E-06, 2.0E-05)	(.009, .508, .701)
8	(3.2E-07, 1.6E-04, 8.2E-05)	(1.3E-07, 3.6E-06, 2.0E-05)	(.008, .508, .741)
9	(3.1E-07, 1.4E-04, 7.3E-05)	(1.2E-07, 3.6E-06, 2.0E-05)	(.007, .502, .757)
11	(2.9E-07, 1.1E-04, 6.0E-05)	(1.1E-07, 3.6E-06, 2.0E-05)	(.006, .490, .784)
OVERALL	(2.9E-07, 2.1E-04, 2.2E-04)	(1.1E-07, 3.6E-06, 2.0E-05)	(.006, .497, .794)

SYSTEM SIZE	R2	R3	R4
3	(7.3E-09, 6.6E-07, 2.3E-06)	(3.4E-09, 5.6E-07, 2.1E-06)	
4	(6.4E-09, 6.5E-07, 2.2E-06)	(3.3E-09, 5.8E-07, 2.1E-06)	(2.6E-09, 5.6E-07, 2.1E-06)
5	(5.9E-09, 6.4E-07, 2.2E-06)	(3.2E-09, 5.8E-07, 2.1E-06)	(2.6E-09, 5.6E-07, 2.1E-06)
6	(5.6E-09, 6.3E-07, 2.2E-06)	(3.2E-09, 5.7E-07, 2.1E-06)	(2.6E-09, 5.6E-07, 2.1E-06)
8	(5.2E-09, 6.3E-07, 2.2E-06)	(3.1E-09, 5.7E-07, 2.1E-06)	(2.6E-09, 5.5E-07, 2.1E-06)
9	(5.1E-09, 6.3E-07, 2.2E-06)	(3.1E-09, 5.7E-07, 2.1E-06)	(2.6E-09, 5.5E-07, 2.1E-06)
11	(4.9E-09, 6.2E-07, 2.2E-06)	(3.1E-09, 5.7E-07, 2.1E-06)	(2.6E-09, 5.5E-07, 2.1E-06)
OVERALL	(4.9E-09, 6.3E-07, 2.3E-06)	(3.1E-09, 5.7E-07, 2.1E-06)	(2.6E-09, 5.6E-07, 2.1E-06)

BWR RELIEF VALVES

PLANT	HOURS	POP	NUMBER OF INDIV. FAULTS		VALVES AFFECTED BY NONLETHAL SHOCKS		VALVES AFFECTED BY LETHAL SHOCKS		NUMBER OF LETHAL SHOCKS FAILS/COM FLTS	NUMBER OF LETHAL SHOCKS FAILS/COM FLTS
			FAILS	COM FLTS	FAILS	COM FLTS	FAILS	COM FLTS		
BF1	43800	11	1 / 0		0 / 0		0 / 0		0 / 0	0 / 0
BF2	43800	11	7 / 0		0 / 0		0 / 0		0 / 0	0 / 0
BF3	39496	11	10 / 0		0 / 0		0 / 0		0 / 0	0 / 0
BR1	37032	9	1 / 0		0 / 0		0 / 0		0 / 0	0 / 0
BR2	43800	9	3 / 2		0 / 3		0 / 0		0 / 0	0 / 0
CO1	43800	8	1 / 0		1 / 1		1 / 0		0 / 0	0 / 0
DA1	43800	6	20 / 0		0 / 0		0 / 0		0 / 0	0 / 0
DR2	43800	5	3 / 0		0 / 0		0 / 0		0 / 0	0 / 0
DR3	43800	5	7 / 0		1 / 0		1 / 0		0 / 0	0 / 0
EN1	43800	9	10 / 0		0 / 1		0 / 0		0 / 0	0 / 0
FN2	21816	11	17 / 0		1 / 0		3 / 0		0 / 0	0 / 0
FP1	43800	9	0 / 0		0 / 0		0 / 0		0 / 0	0 / 0
ML1	43800	3	3 / 0		0 / 0		0 / 0		0 / 0	0 / 0
MO1	43800	4	1 / 1		0 / 0		0 / 0		0 / 0	0 / 0
NM1	43800	6	0 / 3		0 / 0		0 / 0		0 / 0	0 / 0
OC1	43800	4	2 / 1		1 / 0		1 / 0		0 / 0	0 / 0
PS2	43800	11	3 / 0		0 / 0		0 / 0		0 / 0	0 / 0
PS3	43800	11	2 / 1		0 / 0		0 / 0		0 / 0	0 / 0
PI1	43800	3	6 / 2		0 / 0		0 / 0		0 / 0	0 / 0
QC1	43800	9	5 / 3		0 / 0		0 / 0		0 / 0	0 / 0
QC2	43800	5	8 / 2		0 / 0		0 / 0		0 / 0	0 / 0
YY1	43800	4	3 / 0		1 / 0		3 / 0		0 / 0	0 / 0
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ALL	922944	160	113 / 15		5 / 0		9 / 0		0 / 0	0 / 0

BWR RELIEF VALVES

P V E N T	PLAN NUMBER	CONTROL DATE	S Y S T E M P E M P E	C O M P R E S T E	M O D U L E S P E C I L U M N U M Y	A C T I V I T Y	MODE DESCRIPTION	CAUSE DESCRIPTION
G	BF1 017525	042177	K RV B27 R	1	N	MN STM SAFE RELIEF V.V. FAILED TO RESEAT		SEVERE STM CUTS ON PILOT DISC
G	BF2 020380	020578	K RV 800 R	1	N	RELIEF VALVE 2-1-41 OPENED AND FAILED TO RESEAT		CAUSE OF MALFUNCTION UNKNOWN
G	BF2 020469	021378	K RV 800 R	1	N	RELIEF VALVE 2-1-5 OPENED AND FAILED TO RESEAT		CAUSE OF MALFUNCTION UNKNOWN
G	BF2 032705*	092980	K RV FOO R	5	T	5 MS RELIEF VLVS FAILED TO ACTUATE AT PROPER PRESS	NO CAUSE STATED SET PRESS WAS RESET	
G	BF3 020923	041578	K RV 800 R	1	N	RELIEF 3-1-31 FAILED TO RESEAT AT PROPER PRESSURE		CAUSE OF MALFUNCTION IS NOT KNOWN
G	BF3 022126A	081778	K RV 800 R	1	N	A MAIN STM RELIEF VLV DID NOT CLOSE AFTER LIFTING		CAUSE OF FAILURE NOT GIVEN
G	BF3 033640*	121080	K RV FOO R	8	T	8 MS RVS FAILED TO ACTUATE AT REQUIRED PRESS(TEST)	CAUSE NOT PRECISELY KNOWN(RESET ADJUSTMT)	
G	BR1 020771	031378	K RV B27 R	1	N	RELIEF VLV B21-F013F FAILED TO RESEAT AT REQ.PRESS DEFECTIVE PILOT VLV/PILOT REPLACED		
G	BR2 018697	071577	K RV B16 S	1	N	SAFETY REL.VLV B21-F013B STUCK OPEN;AFTER MAN.OPEN GRMD. DM SOLENOID ASS. FOR REMOTE ACTUATOR		
G	BR2 025638A	032079	K RV A27 R	2	T	2B21-F013H&013B SET POINTS FOUND DRIFTED HIGH		SETPOINT DRIFT OF PILOT VALVES
G	BR2 026626	071779	K RV F27	1	N	SAFETY RELIEF VALVE F013E LIFTED & RESET-SPURIOUS		EXCESSIVE PILOT VALVE ASSEMBLY LEAKAGE
G	BR2 032662	091080	K RV A16 S	1	T	ADS RV 2-B21-F013E FAILED TO ACTUATE AS REQUIRED		BROKEN WIRE IN SOLENOID COIL(COMMAND FLT)
G	CD1 014936	051476	K RV A27	1	M	MAIN STEAM SAFETY RELIEF VALVE MALFUNCTIONING		CRACK IN BELLows TO BASE WELD
G	CD1 015873	081376	K RV A02 C	1	R	SETPOINT OF HS-RV-71E ADJUSTED INCORRECTLY		INCORRECT MAINTENANCE PROCEDURE
G	DA1 014445*	033175	K RV C27	6	T	SIX RELIEF VALVES LEAKING INTERNALLY		EXCESS STEAM CUTTING ON PILOT VALVE SEAT
G	DA1 017631*	032877	K RV A27	6	T	6 MAIN STEAM RV DID NOT LIFT AT PROPER PRESSURE		FAILURE OF PILOT VALVE TO OPERATE
G	DA1 021169*	040378	K RV A00	4	T	SETPOINTS OUT OF SPEC ON 1 SAFTEY#3 RELIEF VALVES	CAUSE UNKNOWN	
G	DA1 030530*	031080	K RV FOO R	3	T	3 TARGET ROCK RELIEF VLVS FOUND WITH BAD SETPOINTS	CAUSE UNKNOWN	
G	DA1 033106	111080	K RV B27	1	N	RELIEF VLV PSV-4405 FAILED TO CLOSE/SCRAMMED PLANT PILOT VLV PROBLEM OF UNKNOWN NATURE		
G	DR2 014747	052576	K RV B27	1	T	DURING BLOWDOWN TEST VALVE 203-3A REMAINED OPEN		EXCESS LEAKAGE ON PILOT STAGE OF VALVE
G	DR2 019985	120977	K RV A00 R	1	T	ELECTROMATIC RELIEF VALVE 3B FAILED TO OPEN		CAUSE UNKNOWN
G	DR2 033323	112480	K RV FOO	1	N	2A SAFETY RV VLV NOT OPERABLE IN SAFETY MODE		CAUSE UNKNOWN AT THIS TIME
G	DR3 018378A	061177	K RV C02 B	1	N	ELECTROMATIC RELIEF VALVE 203-3D LEAKING INTERNALY PILOT PIN ADJUSTED INCORRECTLY		
G	DR3 018378B	061177	K RV C10 R	1	N	ELECTROMATIC RELIEF VALVE 203-3E LEAKING INTERNALY DIRT UNDER VALVE SEAT		
G	DR3 018377	061277	K RV C27 R	1	T	ELECTROMATIC RELIEF VALVE 203-3D LEAKING INTERNALY DEFECTIVE PILOT VALVE STEM		

BWR RELIEF VALVES

PLANT VEN	CONTROL NUMBER	EVENT DATE	SYSTEM COMP	MODE	CAUSE	TYPE	FAIL NUM	ACTIVITY	MODE DESCRIPTION		CAUSE DESCRIPTION	
G DR3 018376	061377	K RV A20 R	1	T	SOLENOID OPERATING LEVER FOR 203-3C STICKING				RUST BUILDUP ON GUIDE PINS			
G DR3 030967A	042580	K RV A12 R	1	N	3A TARGET ROCK ADS RELIEF FAILED TO OPEN				AIR ACTUATOR IMPROPERLY BOLTED TO VLV			
G DR3 030967B	042580	K RV A27 R	3	N	3B, 2C, 3E ADS ELECTROMATIC RELIEFS FAILED TO OPEN				VARIOUS PILOT VALVE PROBLEMS			
G EN1 016841	120976	K RV 800 R	1	T	RELIEF VALVE WOULD NOT RESEAT				CAUSE UNKNOWN			
G EN1 017110	010977	K RV B27 R	1	N	RELIEF VALVE B21-F013G OPENED AND STUCK OPEN				GROSS LEAKAGE OF PILOT+2ND STAGE ASSEMBLY			
G EN1 017189	020177	K RV 800 R	1	N	RELIEF VALVE B21-F013G OPENED AND STUCK OPEN				CAUSE UNKNOWN, VALVE TO BE TESTED			
G EN1 018649	080977	K RV A00	1	N	SAFETY RV 1C FAILED TO OPEN AT HIGH REACTOR PRESS.				CAUSE UNKNOWN			
G EN1 020019*	100677	K RV A00 R	4	N	FOUR RELIEF VALVES FAILED TO OPEN FOLLOWING SCRAM				CAUSE UNKNOWN, VALVES BEING EXAMINED			
G EN1 021723*	060978	K RV A12 R	2	T	TWO RELIEF VALVES FAILED BENCH CHECK				PROBLEMS WITH PLUNGERS AND SPRINGS			
G EN2 025467*	021479	K RV A27	2	R	2 SAFETY RELIEF VALVES FAILED TO OPEN AS REQUIRED				SCUFFING OF PILOT DISCS AND SEATS			
G EN2 025875*	050879	K RV F05 C	3	M	AIR OPERATORS FOR THREE SRV'S IMPROPERLY INSTALLED				IMPROPERLY INSTALLED BY WYLE LAB			
G EN2 033426A	112680	K RV F27 R	8	T	OUT OF THE VLVS 2821-5013A-M, 8 VLVS FAILED				PILOT SEAT LEAKAGE			
G EN2 033426B	112680	K RV A00 R	7	T	OUT OF THE VLVS 2821-5013A-M, 7 VLVS SET PRESSURE WAS TOO HIGH// CAUSE UNKNOWN							
G MI1 018156	061877	K RV C27	1	N	RV DISCH TEMP HIGH/VLV LEAKING STM INTERNALLY				COLLAPSED FILTER, STR CUTTING OF PTY SEATS			
G MI1 020698B	031078	K RV C27 R	1	T	RELIEF VALVE LEAKING THROUGH				LEAKAGE IN PILOT VALVE // STEAM CUT			
G MI1 025313	022679	K RV B27 R	1	N	SRV LIFTED PREMATURELY & FAILED TO RESEAT				PILOT DISC STEAM CUT			
G M01 015100	061476	K RV A24 S	1	T	SAFETY RELIEF VLV 2-71A FAILED TO ACTUATE				AIR LEAK IN AIR SUPPLY SYSTEM			
G M01 025804	031579	K RV F06	1	T	OPENING DELAY TIME OF "A" SRV IN EXCESS OF ASSUMED				PROCEDURE DID NOT HAVE INSULATION INSPEC			
G NM1 017401*	030977	K RV A16 S	3	N	3 OUT OF 6 ADS RELIEF VLVS WOULD NOT HAVE OPERATE-				-0 IF NEEDED//RESET SWITCH FAILURE			
G DC1 018671	080277	K RV A12	1	T	ELECTROMATIC RV C FAILED TO OPEN				ACTUATOR PLATE BOUND AGAINST A RIVET			
G DC1 027195	091779	K RV A16 S	1	T	ELECTROMATIC RV WOULD NOT HAVE OPENED				HIGH PRESSURE MICROSWITCH WAS DEFECTIVE			
G DC1 030047A	010580	K RV A05 C	1	T	ELECTROMATIC RV"D" FAILED TO OPEN DURING TEST				RETAINER RING BACKED OUT, GRUB SCREW GONE			
G DC1 032048	071680	K RV A06	1	T	ELECTROMATIC RV"D" FAILED TO OPEN DURING TEST				PROCEDURES FAILED TO DESCRIBE ADJUSTMENT			
G PB2 015085	062976	K RV B27 R	1	N	MAIN STEAM RV FAILED IN OPEN POSITION				PILOT VALVE SEAT LEAKAGE			
G PB2 016333	111476	K RV B10 R	1	N	MAIN STM RV 71F FAILED IN OPEN POSITION				DIRT UNDER PILOT DISK AND SEAT			

BWR RELIEF VALVES

P V E N T	L A N C O N T R O L N U M B R	S E N T D A T E	S Y S T E M P M O D E	C O D E	A U S T E L	T Y P E	F A I L U M Y	A C T I V I T Y	MODE DESCRIPTION	CAUSE DESCRIPTION
G PB2	016676A	010677	K RV	B27	R	1	N		MAIN STM RV 71E FAILED OPEN	EXCESSIVE PILOT SEAT LEAKAGE
G PB3	015153	071276	K RV	B27	R	1	N		71B MAIN STEAM RELIEF VALVE FAILED OPEN	FAILURE DUE TO PILOT VLV SEAT LEAKAGE
G PB3	015228	072076	K RV	B27	R	1	N		MAEN STEAM RELIEF VLV 71G FAILED OPEN	FAILURE DUE TO PILOT VLV SEAT LEAKAGE
G PB3	025311	022579	K RV	F16	S	1	N		RELIEF VALVE RV-71L FAILED TO OPERATE	FUSES BLOWN, SHORT TO GROUND
G PII	017674	051077	K RV	A24	S	1	N		RV 203-3C DID NOT OPEN FROM REMOTE CONTROL SWITCH	DETET OF THE REMOTE AIR ACTUATOR DIAPH
G PII	019736	111477	K RV	A24	S	1	T		RELIEF/SAFETY VALVE 203-3B COULD NOT BE MAN OPENED	FAIL OF 3-WAY SOLENOID VAL TO PORT PROPER
G PII	019859	111577	K RV	C27	R	1	N		RELIEF VALVE 203-3B DETERMINED TO BE LEAKING	FIRST+SECOND STAGE OF PILOT VALVE LEAKING
G PII	019756	111777	K RV	C27	R	1	N		RELIEF VALVE 203-3D DETERMINED TO BE LEAKING	FIRST STAGE OF PILOT VLV SEAT LEAKING
G PII	022757	100978	K RV	B27	R	1	N		RV-203-3C FAILED TO RESEAT AT PROPER PRESSURE	EXCESSIVE PILOT SEAT LEAKAGE
G PII	031759	072580	K RV	A21	R	1	T		RV 203-3D FAILED TO OPEN DURING TEST/LOCKTITE IN	THE VLVS SOLENOID ASSEMBLY REPLACED SAME
G PII	032273	080180	K RV	A00	R	1	U		RV 203-3D DID NOT OPEN GIVEN MANUAL OPEN SIGNAL	NO CAUSE COULD BE DISCOVERED BY FACT REP
G PII	032812	100180	K RV	B12		1	N		*D* RELIEF VLV STUCK OPEN DURING SHUTDOWN	MAIN PISTON SCORED
G QC1	016472*	110176	K RV	A13		2	T		ELECTROMATIC RELIEF VALVES FAILED TO OPEN/TESTNG	EXCESSIVE INTERNAL STEAM LEAKAGE
G QC1	020532	032077	K RV	A12		1	T		MAIN STEAM ELECTROMATIC RELIEF FAILED TO OPEN/TEST	INTERNAL PARTS FOUND LOOSE AND MISSING
G QC1	020425	111677	K RV	A16	S	1	N		RELIEF VALVE 1-203-3B FAILED TO OPEN ON DEMAND	COMMAND/WIRE TIE IN ELECT CONTACTOR
G QC1	020636	020678	K RV	A12		1	T		ELECTROMATIC RELIEF 1-203-3E FAILED TO OPEN / TEST	WORN INTERNAL PARTS/VALVE WAS REPLACED
G QC1	021408	042478	K RV	A18		1	T		ELECTROMATIC RV 1-203-3C FAILED TO OPERATE / TEST	WELD FAILURE BETWEEN BODY AND CAGE/VIBRAT
G QC1	026560	071779	K RV	F16	S	1	T		RELIEF VALVE FAILED TO OPERATE	PRESSURE SWITCH WIRE NOT CONNECTED
G QC1	031359	051180	K RV	A16	S	1	T		RV 1-203-3B FAILED TO OPEN DURING TEST	DIRT ON CONTACTS OF HOLD-IN COIL SWITCH
G QC2	016473*	110176	K RV	A09	R	2	T		TWO ELECTROMATIC RELIEFS FAILED TO OPEN ON TESTING	INTERNAL BINDING DUE TO CORROSION PROBLE
G QC2	020533	032377	K RV	A12	R	1	T		ELECTROMATIC RELIEF FAILED TO OPEN DURING TESTING	LOOSE INTERNAL PARTS BOUND/EXCESS VIBRAT
G QC2	019223	092377	K RV	A12	R	1	T		ELECTROMATIC RELIEF FAILED TO OPEN DURING TESTING	RINGS CUT GROOVES IN DISC GUIDE/STEAM CUT
G QC2	019745	110677	K RV	B27		1	N		RELIEF VALVE 2-203-3B FAILED TO RESEAT	PILOT VALVE WAS STEAM CUT AND ERODED
G QC2	020245	011478	K RV	F16	S	1	T		RELIEF VALVE FAILED TO OPERATE AS REQUIRED	PRESSURE CONTROL SWITCH SETPOINT DRIFT
G QC2	022815	092978	K RV	A24	S	1	T		RV 2-203-3A FAILED TO OPEN(MANUAL) / COMMAND	AIRLINE TO MANUAL AIR OPERATOR BROKE

BWR RELIEF VALVES

PLANT NUMBER	CONTROL NUMBER	EVENT DATE	SYSTEM COMP.	MODE	CAUSE TYPE	FAIL NUM	ACTIVITY	MODE DESCRIPTION		CAUSE DESCRIPTION	
G OC2 031100	042080	K RV A27 R	I T	RV 2-203-3C FAILED TO OPERATE DURING TEST				EXCESS CLEARANCE,PLUNGER TO PILOT VL STEP			
G OC2 033138	101780	K RV A25 R	I U	RELIEF VLV 2-203-3C FAILED TO OPEN				LEAKAGE BETWEEN MAIN DISC AND DISC GUIDE			
G OC2 033525	120380	K RV A12 R	I N	ELECTROMATIC RELIEF 2-203-3D FAILED TO OPEN				STEAM LEAKAGE RETAINER PLUG TO MAIN DISK			
G VY1 015184*	070676	K RV A22 C	3 T	3 TARGET ROCK RVS FAILED TO OPERATE(SIGNAL/MANUAL)				DIAPHRAGM IN AIR OPERATORS FAILED/HEAT			
G VY1 020910	041278	K RV A00	I R	RV {67HH13} SET TOO HIGH				SETPOINT DRIFT/RESET TO LOWER LIFT PRESS			
G VY1 025152	012379	K RV A00 R	I T	STEAM VLV SAFETY FOUND TO HAVE TOO HIGH SETPOINT				SETPOINT DRIFT			
G VY1 032985	100780	K RV A00 R	I T	MAIN-STEAM RELIEF VLV S/N67HH12 SET POINT 3# TO HI SETPOINT DRIFT							

APPENDIX D
ONE-LINE DESCRIPTIONS OF ALL RELEVANT VALVE LERS

COMMON CAUSE EVENTS

COMMON CAUSE EVENTS

P L Y E N T	A C T I V E Y	S Y S T E M C O N T R O L N U M B R	E V E N T T E M P D A T E	M O D E D E S C R I P T U R Y	C A U S E D E S C R I P T U R Y
C FCI 023171	122078 K RV V06 U	2 M TWO PRESS UP RELIEF VALVES OPENED WHEN REQ CLOSED	TECH PULLED FUSES, DEFECTIVE PROCEDURES		
C M12 031945	070380 H XV V06 U	1 T HPSI PUMP MINIMUM FLOW VLV WAS SHUT	DEFECTIVE PROCEDURES, CAUSED PUMP SEIZURE		
C MYL 020758	020277 H RM F16 U	1 M VALVE SL-P-3 FAILED TO OPERATE	WIRE DISCONNECTED (CAUSE UNKNOWN)		
C MYL 030804	031980 L XV VOL U	2 N RHR VLV RH-R AND RH-10 FOUND OPENED AND UNLOCKED	PERSONNEL ERROR		
C MYL 031360	050780 H XV V03 U	2 L U COOLING WATER IMPROP LINED UP TO S-CHARGING PUMP	PERSONNEL ERROR (SEPARATION NOT MAINTAIN)		
C PAI 032156	071980 H XV V03 U	1 N INST. EQ. VLV NOT CLOSE AFTER CALIBRATION	PERSONNEL ERROR WHEN CAL. HPSI FLOW IND.		
C PAI 032224	081980 H RM V03 U	1 N CV-3031 WAS CLOSED AND THEN IMMEDIATELY OPENED	OPERATOR FAILED TO RELATE TEST REQUIRE.		
W BVI 027663	112779 H MV VOL U	1 M HPSI PMP SUC VLV CH-1150 ISO FOR MAINT WHEN REQ OP	PERSONNEL ERROR--2ND VLV ALSO SHUT		
W BVI 031210*	057180 L RM 816 U	2 V T RHR 150L VLV FAILED TO CLOSE	DEENERGIZED PROCESS CONTROL SIGNAL		
W DC1 016648	121776 F MV VOL U	1 T CONTAINMENT SPRAY PUMP SUCTION VALVE FOUND CLOSED	PERSONNEL LEFT VALVE SHUT AFTER A TEST		
W DC1 021011*	032278 H MV F16 U	3 N POWER FOUND OFF TO 3 ECCS VLVES	3 BREAKERS FOUND TRIPPED ON MCC		
W DC2 021079	041678 L XV VOL U	1 N HANDWHEEL CAME OFF RHR VALVE POSITIONING IT WRONG	PERSONNEL FAILED TO REPOSITION THE VALVE		
W DC2 0222581	092278 K RV VOL U	1 T PRESSURIZER RV OPENED WHEN REQUIRED TO BE CLOSED	PERSONNEL ERROR		
W DC2 0228388	101078 B XV VOL U	1 T AUX FEED VALVE FOUND UNLOCKED & OPEN/WRON LINE-UP	PERSONNEL ERROR		
W DC2 023030*	112178 F CV A05 C	2 N CHK-VLV.C15-127EW TO THE LOWER CONT.SPRAY NOZZL-	-ES INSTALLED BACKWARDS//FABRICATION ERR.		
W IP3 014604	042976 F RM V03 U	2 L T INCR.VLV LINUP FOR TEST,CNTRNT SPRY ACCIO.TURN ON PERSONNEL ERROR	PERSONNEL ERROR		
W JF1 020993	032578 B MV V02 U	2 N MDAPP & TDAPP RECIRC BYPASS ISO VLV'S OPEN	DEFECTIVE RELAY IN TDAPP CONTROL CIRCUIT.		
W JF1 022633*	090978 B RM F16 U	3 T CONTROL WAS LOST ON FLOW CONT.VLV'S 3228A, 8+6C	INADEQUATE PROCEDURES		
W JF1 022629	091878 L RM V06 U	1 T RHR PUMP SUCTION VLV 6701A CLOSED WHEN REQ. OPEN	INADEQUATE PROCEDURES		
W JF1 030326*	020180 B RM A24 U	2 V T CONTROL VLV'S FOR "A" AUX FEED TRAIN DIDN'T AUTO OP	CONTACTS MISALIGNED IN CONTROL CIR		
W KE1 014240	022076 F RM A01 C	1 T VALVE IC5-5R FAILED TO OPEN/CONT.SPRAY DISCH. VLV	VALVE MANUALLY TORQUED DOWN TOO TIGHT		
W KE1 019312	100377 F MV F02 C	1 M MAINT.MAN DEENERGIZED 2 SW VLV'S,OPEN ONLY ALLV.H.T-	-O DEFENDER.1 VLV/PERSONNEL ERROR		
W MAI 021506	051476 B AV V06 U	2 T AUX FEEDWATER VALS PCV-F2-159A,-159B IMP.LINEUP	CHECKOFF SHEET DOES NOT LIST NORM VAL POS		
W MAI 027593	110679 L RM V02 U	1 N RHR INLET VLV MOV-1701 SHUT WHEN REQ. OPEN	MAINTENANCE PERSONNEL ERROR		
W PR2 017889	051977 B XV V06 U	1 U PUMP INLET VALVE FOUND NEARLY SHUT/AUX FEED INLET	POSITION REQUIREMENT WILL GO ON CHECKLIST		

COMMON CAUSE EVENTS

P L Y E N T	A C T U N T	S Y C O M A T F A N T I V I U N T H O U S P I A U R H E P E L H	S Y C O M A T F A N T I V I U N T H O U S P I A U R H E P E L H	M O D E D E S C R I P T I O N	C A U S E D E S C R I P T I O N
W PT2 018572	072877 H MV V01 U	1 N	MOV FOUND IN INTERMEDIATE POSITION/SINCE PREV TEST PERSONNEL FAILED TO ASSURE FULLY OPEN		
W SE1 032973*	100580 N PH F01 C	2 T	AUX FEEDWATER VLV LCV-3-1746173 WOULD NOT HAVE OPEN IN AUTO. PRESS SWITCH LEFT ISOLATED		
W SU1 071802	062278 L MV A02 C	1 T	MOV-RH-100 FAILED TO OPEN	Maint. ERROR/SYSTEM WAS NOT ENGAGED TO DISC	
W TR1 019580	101677 L XV V01 U	1 N	RHR DISCHARGE VLV 1872081 FOUND LOCKED CLOSED	PERSONNEL ERROR/IMPROPER VALVE LINEUP	
W TR1 021068*	032078 L MV C16 U	2 V	T DEENERGIZING PROTECTION SYS CAUSED RHR VALVES TO--	--CLOSED//PROCEDURAL DEFICIENCY	
W TU4 019421	091377 L RM V01 U	2 T	TWO VALVES INADVERTANTLY OPENED//WEST LEVEL DECREASES PERSONNEL ERROR/POSSIBLE PROCEDURE PROBL/P		
W YR1 030441*	020180 H RM F16 U	3 T	SI ACCUMULATOR N2 VLV SI-TV-604x605x606 DIDN'T OP.	IMPROPER WIRING OF TIME DELAY RELAYS	
W Z12 031625	061880 K RV V06 U	2 N	IMPROPER VLV LINE UP MADE PUPS UNOPERABLE	PROCEDURE CHANGED TO BLOCK THE VLV'S OPEN	
G AF1 016253	092376 D XV V02 U	1 U	VALVE FOUND CLOSED TO PRESSURE SWITCH	PERSONNEL ERROR	
G BF2 016199	100776 H XV V03 U	1 T	EQUALIZER VALVE ON FLOW INSTRUMENT FOUND OPEN	PERSONNEL ERROR	
G BF2 021782	062778 H XV V01 U	1 T	VALVE LEFT SHUT IN LUB OIL LINE TO HPC 1 PUMP	PERSONNEL ERROR IN VALVE LINE UP	
G BR1 016402	111976 L MV F16 U	1 N	RHR INJECTION VALVE(E11-F05A) FAILED TO OPERATE	UNDERSIZED BKR/DESIGN PROBLEM(ROTI)	
G BR1 012677	110577 L MV A02 C	1 N	RHR VALVE E11-F00A FAILED TO OPEN/MOTOR PROBLEM	PERSONNEL ERROR/COVER LEFT LOOSE/WATER LK	
G BR1 028434	121979 L MV V01 U	1 N	RHR TORUS SUCTION VALVE FOUND SHUT	OPERATOR ERROR-FORGOT TO OPEN VALVE	
G BR1 030407	021480 H XV V01 V	1 T	MANUAL ISOL VLV LOW SIDE OF 1E41151A FOUND CLOSED	PERSONNEL ERROR (WHEN UNDETERMINED)	
G BR2 014647	020576 L XV V03 U	1 N	FRESS SW FOUND ISOLATED AFTER TESTING	PERSONNEL ERROR	
G BR2 023034	111278 L MV A16 U	1 N	RHR VLV E11-F00B WOULD NOT OPEN AT REQ. SETPOINT	FAIL. OF RX-STW, DOME HIGH PRESS-SWITCH	
G BR2 0324548	090780 H CV V01 U	1 T	HPC1 MANUAL STOP CHECK FOUND LOCKED CLOSED	PERSONNEL ERROR VLV WAS REQ OPEN	
G CO1 015873	081376 W RV A02 C	1 R	SETPOINT OF MS-RV-TIE ADJUSTED INCORRECTLY	INCORRECT MAINTENANCE PROCEDURE	
G CO1 020806A	020778 H XV V03 V	1 T	ISOLATION VALVE TO OPS-76 FOUND CLOSED(SEE020806)	PERSONNEL ERROR	
G CO1 031544	051680 L RM F26 C	1 Y	RHR VLV HO-57 FAIL TO CLOSE IN REQUIRED TIME	LIMIT SW SET WRONG(PERSONNEL ERROR)	
G DA1 017312	021977 H RM F03 C	1 N	CONTACT BLOCK FOUND INSTALLED IN VALVE CIRCUIT	PERSONNEL ERROR, FAILED TO REMOVE AFTER TS	
G DR2 021158	042878 L XV V01 U	2L N	VALVES IN LPC1 & CORE SPRAY LINED UP IMPROPERLY	OPERATING PERSONNEL ERROR	
G DR3 014750	051076 D MV B16 U	1 Y	MO 3-1402-258 TRIPPED WHILE BEING CLOSED	WRONG SIZE OVERLOAD HEATER	
G DR3 018378A	061177 W RV C02 B	1 N	ELECTROMATIC RELIEF VALVE 203-10 LEAKING INTERNALLY PILOT PIN ADJUSTED INCORRECTLY		

COMMON CAUSE EVENTS

P E N T	A C T I V I T Y	S Y S T E M C O N T R O L N U M B R E A K E L N	E V E N T D A T E	M O D E D E S C R I P T I O N	C A U S E D E S C R I P T I O N
G EN1 017096	011777 L XV V03 U 1 U	PRESS SW FOUND VALVED OUT WHEN REQUIRED OPEN	PERSONNEL ERROR		
G EN1 018191	060477 L RM F02 C 1 T	LPCI VALVE ELL-F0178 CYCLE TIME OUTSIDE T.S.	VALVE STEM PACKED TOO TIGHTLY/PERSONNEL		
G EN1 026631	072679 L MV F16 U 1 M	RHR OUTBOARD ISOLATION VALVE MADE INOPERABLE	NO PWR AVAILABLE TO VLV (PERSONNEL ERROR)		
G EN1 031157	051080 L XV V03 U 2 N	TWO COOLING WTR VLVS TO PUMPS A & B FOUND CLOSED	PERSONNEL ERROR		
G EN1 031521	062280 L XV VOL U 2 T	RHR MIN FLOW VLV F11-F0188 & D FOUND CLOSED	PERSONNEL ERROR		
G EN1 031789A	071180 L XV VOL U 2L N	COOLING WATER VLV SECURED WHEN REQUIRED OPEN	PERSONNEL ERROR		
G EN2 022024*	0711778 L MV F16 U 2V N	RHR VALVES HAD POWER LOST TO THEM	BREAKER TRIPPED DUE TO BLOWN FUSES		
G EN2 022753*	1106778 H RM F16 U 2Y T	HPC1 CONTROL VALVES FAILED TO OPERATE	WIRE LEFT OFF BY MAINT PERSONNEL		
G EN2 025872*	050872 W RV F05 C 3 M	AIR OPERATORS FOR THREE SRV'S IMPROPERLY INSTALLED	IMPROPERLY INSTALLED BY WYLE LAB		
G EN2 033764	050780 L MV 820 C 1 T	2E41-F006 INBOARD ISO.VLV FAILED TO CLOSE	WATER SHORTED OUT MOTOR OPERATOR WINDINGS		
G EN2 031318*	051480 L MV F26 C 2 N	RHR VLV 2E11-F004D E F006 FAILED TO OPERATE	LOOSE & BROKEN LIMIT SWITCHES		
G EN2 031431A	053080 L MV A20 B 2 T	TORUS SUCTION VLV 2E41-F041642 FAILED TO OPEN	VALVE MOTORS SHORTED OUT(STEAM LEAK)		
G EN2 032135	072480 H RM F16 U 1 N	HPC1 VLV 2E41-F002 CLOSED WHEN REQUIRED OPEN	IMADYFRANT SIGNAL, OPERATOR BUMPED RELAY		
G FP1 021227	050878 D MV F02 C 1 M	POWER REMOVED FROM CORE SPRAY VALVE MOTOR	PERSONNEL ERROR		
G OC1 018623*	072777 D MV A16 V 2 T	CORE SPRAY ISO.VLV V-20-40 6 V-20-15 FAILED TO F-	FULLY OPEN/IMP.CK'S, SRK&.OVERLOAD SETTING		
G OC1 023144	120478 F MV A16 U 1 T	CONT SPRAY VALVE V-21-78 FAILED TO OPEN ON TESTING	VALVE NOT RACKED IN PROPERLY		
G OC1 030047A	010580 W RV A05 C 1 T	ELECTROMATIC RV-UW FAILED TO OPEN DURING TEST	RETAINER RING BACKED OUT, GRUB SCREW GONE		
G P83 031104	042180 L MV A05 B 1 T	LPCI VLV MO-10-258 FAILED TO OPEN ON TEST	WALWORTH 23-INCH IMPROPER INTERNAL CLEARANCE		
G P83 031740	060880 F MV B05 C 1 T	CONT SPRAY VLV MO-3-10-268 FAILED TO CLOSE	STEM LOCKING MUT NOT STAKED BACKED OUT		
G QC2 021561	052178 D RM VOL U 1 N	2A CORE SPRAY SUC.VLV. MO 2-1602-3A CLOSED WHEN R-	REQUIRED TO BE OPEN/PERSONNEL ERROR		
G VY1 014230*	021776 L MV F01 C 2 N	RHR VLV. 25A6B WOULD NOT STROKE ELECTRICALLY	PERSONNEL ERROR/MUST STRO.VLV'S, MANUALLY 1ST !		
G VY1 014584*	051076 L MV A14 C 2 T	TWO 24 INCH MOVS (RHR-27AB) FAILED TO OPEN / TEST PACKING MAINTENANCE PROBLEM			
G VY1 015184*	070676 A RV A22 C 3 T	3 TARGET ROCK RVS FAILED TO OPERATE(SIGNAL,MANUAL) DIAPHRAGM IN AIR OPERATORS FAILED/HEAT			
G VY1 016997	011877 L RM V03 U 2L T	"8" RHR PMP DISCH.VLV'S. SHUT WHEN REQ. TO BE OPEN	PERSONNEL ERROR		

ALL VALVE LERS USED

PLANT	CONTROL NUMBER	EVENT DATE	SYS	CMP	MODE	CAUSE	TYPE	FAM	MUMY	ACTIVITY	MODE DESCRIPTION	CAUSE DESCRIPTION
B ARI 015207	061276	G XV V06 U	I	N	VALVE SF-22 WAS NOT CLOSED;IA SPILL RESULTED						PROCEDURES WERE INADEQUATE	
B ARI 020607	011378	B AV A23	I	T	VALVE CV-2667 FAILED TO OPEN REMOTELY						TORQUE SWITCH DEFECTIVE	
B ARI 022339	072078	G RM F23	I	T	SODIUM THIOSULFATE BLOCK VLV CV-2411 FAIL.	TO OPER					TORQUE SETTING OUT OF ADJ; DRY PACKING	
B ARI 027473	100879	F RM F16 U	I	T	CV1616 FAILED IN THE ES POSITION						CONT FUSE BLEW BECAUSE OF GROUND WIRE	
B ARI 030864	040680	B RM F02 C	I	T	EMER. FW SUPPLY VALVE FAILED TO FULLY OPEN(CV-2667)	LOOSE BOLTS SECURING ACT TO VALVE BODY						
B ARI 030926	040780	H MV A20	I	N	CV-U227 FAILED TO OPEN ON MAN HPI (HPI VLV LOOP B)	MAN ENGAGING LEVER FOUND STUCK IN ENG POS						
B ARI 032533	090680	G MV B23	I	N	RCS MAKE UP BLOCK VLV(CV-1234) FAILED TO FULL CLOS	TORQUE SWITCH SETTING TOO LOW						
B CR3 017168A	020377	L MV A20 R	I	N	DECAY HEAT VLV DHV-4 WOULD NOT OPEN	REMOTE ACTUATOR MTR. OPERATOR WOULDN'T OVERCOME VLV. DRAG						
B CR3 017168B	020377	L MV A20 R	I	N	DECAY HEAT VLV DHV-41 WOULD NOT OPEN	REMOTE ACTUATOR MTR. OPERATOR WOULDN'T OVERCOME VLV. DRAG						
B CR3 017322B	030777	H RM V01 U	ZL	M	"B" LOOP OF HPI SYS. ISOL.CONT.TO T.S.FOR MAINTENANCE PERSONNEL ERROR							
B CR3 017658	042177	G RM V01 V	Z	N	SUCT.VLV CAV-38646 FROM BORIC ACID STOR.TANK.SHUT T.S.VTO./PERSONNEL ERROR/IMP.VLV LINEUP							
B CR3 018561	071577	L MV A23 R	I	T	VLV DHV-41 WOULD NOT OPEN FROM CONTROL ROOM						CAUSED BY SHIFT IN TORQUE SWITCH SETTING	
B CR3 018562	071577	L MV A00 R	I	T	DECAY HEAT VLV DHV-4 WOULD NOT OPEN FROM CONT.ROOM	CAUSE OF FAILURE UNKNOWN						
B CR3 018566	072977	H MV A12	I	T	HPI VLV MUW-25 FAILED TO OPEN AUTOMATICALLY						MECH.BENDING OF THE REVERSING INTERLOCKS	
B CR3 019010	082777	L MV B23	I	N	CORE FLOOD DR.VLV FOR B CORE FL.TK.WOULDN'T CLOSE	DRIFT OF TORQUE SWTCH SETTING;VLV CFV-12						
B CR3 019013	083177	L RM 800	I	N	CORE FLOOD SAMP.ISO.VLV CFV-11 WOULDN'T CLOSE	CAUSE OF FAILURE UNKNOWN						
B CR3 021775	082178	L RM A00 R	I	N	DECAY HEAT REMOV.VLV DHV-111 WOULD NOT OPEN REMOT.	CAUSE OF EVENT IS UNDETERMINED						
B CR3 022361	081978	L RF G16 T	I	W	DHV-3 WENT CLOSED WHEN REQUIRED TO REMAIN OPEN	LOSS OF 120 VOLT AC VITAL BUS(INVERTER)						
B CR3 022359	090778	L RM 823	I	T	CORE FLOOD VALVE CFV-15 FAILED TO CLOSE ON TEST	FAULTY TORQUE SWITCH						
B CR3 023095A	100478	L XV V03 U	I	T	ISOL VALVE TO FLOW CONTROLLER SHUT(SEE 023095)	PERSONNEL ERROR/VALVE REQUIRED TO BE OPEN						
B CR3 023095B	100478	L RM F16 T	I	T	FLOW CONTROL VALVE DHV-110 FAILED TO CONTROL FLOW	NO SIGNAL FROM FLOW CONTROLLER						
B CR3 023237	103018	G RM V01 V	Z	N	CONC.BORIC ACID TK.DISC.VLVS.CAV38643 CLOSED;ITS VI PERSONNEL ERROR;IMPROPER VALVE LINEUP							
B CR3 0255479	072479	L RM A00 R	Z	N	DECAY HEAT REMOVAL VLVS DHV-3&4 COULD NOT BE OPENED & REMOTELY--CAUSE UNKNOWN							
B CR3 025631	032179	G CV V00 U	I	M	MAKEUP PMP 3-C DISCHG STOP CHG VLV MUW-2 IMPROPERLY POSITIONED--CAUSE UNKNOWN							
B CR3 025936	040479	L RM F00 R	I	T	THROTTLE VLV HDV-110 WOULD NOT CONTROL FLOW IN AUT NO CAUSE FOUND							

ALL VALVE LERS USED

PLANT VENT	CONTROL NUMBER	EVENT DATE	TEMP HMP	SYSE MODE	CAUSE SEE	FF SEL	F IUM	ACTIVITY	MODE DESCRIPTION		CAUSE DESCRIPTION	
B CR3 025925	042479	L RM A12 R	1	N	DECAY HEAT REMOVAL VLV DHV-4 FAILED TO OPEN REMOTE WASHER BINDING AT STEM NUT INTERFACE							
B CR3 030369	020680	L RM F16 T	1	T	*A* DECAY HEAT PMP DISCH THROTTLE DIDN'T CONTROL				IN AUTO. LOOSE WIRES ON SELECTOR SWITCH			
B CR3 030667	030680	L RM G00	1	N	DECAY HEAT SUCTION ISO VLV DHV-3 CLOSED INADVERTEN //TLY. NO CAUSE COULD BE FOUND							
B CR3 031894A	072880	H CV B00	1	T	CK VLV CFV-79 FAILED ALLOWING BACKFLOW INTO N2 SYS				CAUSE NOT GIVEN FOR FAILED CHECK VALVE			
B CR3 033760	080680	L RM F24 T	1	T	DHV-110 WOULD NOT CONTROL FLOW IN AUTOMATIC				AIR IN THE CONTROLLER SENSING LINE			
B CR3 032554	082780	L MV F24 T	1	T	DHV-111(*B* DECAY HEAT PMP DISCH THROTTLE) DID NOT // CONTROL IN AUTO. MTR IN SENSING LINES							
B CR3 032555A	090380	L MV F20 R	1	T	DHV-110 DID NOT OPERATE AS REQUIRE (FIFTH OCCUR)				ELECTRICAL SHORT FOUND IN MOTOR			
B CR3 032555B	090580	L RM F16 S	1	T	MUV-23 FAILED TO OPERATE, NO POWER				FAILED CONTROL TRANSFORMER			
B CR3 032682	091680	L MV F16 T	1	T	DHV-111(*B* DH PMP DISCHR THROTTLE) DID NOT OPER.				HIGH ALARM SWITCH DID NOT OPERATE			
B DB1 020989A	031678	B MV A26	1	T	AUX.FDPMP.1-1 STOP VLV AF3870 FAILED TO OPEN				LIMIT SWTCH ON VLV MTR NOT ADJUSTED PROP.			
B DB1 020989B	031678	B CV E00	2	T	CHECK VLVS AF38672 LEAKED INTERNALLY				CAUSE OF REVERSE LEAKAGE NOT GIVEN			
B DB1 021957	071678	L MV A12	1	N	DECAY HEAT COOL.1-2 OUTLET VLV DH-14A WOULDN'T OPEN				ACTUATOR ARM HAD BECOME MISALIGNED			
B DB1 025402	011779	L MV B20	1	N	CORE FLOOD TANK 1-2 ISO VLV CFIA WOULD NOT CLOSE				LOOSE SET SCREW IN MOTOR OPERATOR			
B DB1 025521	022079	B MV B23	1	T	AFW VLV AF3869 COULD NOT BE CLOSED REMOTELY				FAULTY TORQUE SWITCH IN MOTOR OPERATOR			
B DB1 025520	030679	H RM VOL U	2	N	BORATED WTR STOR TANK ISO VLVS DH7A&7B CLOSED WHEN REQUIRED OPEN--PERSONNEL ERROR							
B DB1 026602	032079	L MV B10	1	T	DECAY HEAT REMOV CONT ISO VLV DH 2735 FAILED TO CL				OSE--BUILDUP OF BORIC ACID ON VALVE STEM			
B DB1 026597	070479	B MV F20	1	T	AFW VLV AF 3870 WOULD NOT OPERATE REMOTELY				INTERNAL SHORT CIRCUIT IN MOTOR WINDING			
B DB1 030931	041080	L AV A12	1	N	DHR COOLER OUTLET VLV WOULD NOT OPEN COMPLETELY				RADIUS ARM OUT OF ADJUSTMENT			
B DB1 030872	041880	L RM B12	1	N	DH62 WAS DISCOVER OPEN				REMOTE OPERATOR OUT OF ADJUSTMENT			
B DB1 031898	071080	L RM F02 C	1	N	DH COOLER 1-2 DISCH CONTROL VLV OPERATED ERRATIC				SFAS CH 2 DEENERGIZED FOR MAINTENANCE			
B DB1 031906A	072480	L RM F02 B	1	N	DH 12 CLOSED				PERSONNEL SHORTED FUSE CLIP IN CONTROL PC			
B DB1 031906B	072480	L RM F06 B	1	N	DH 11 CLOSED				INADEQUATE RESTORATION PROCEDURE			
B DB1 031906C	080380	L RM F02 B	1	N	DH 11 CLOSED				MAIN. SPEC. REMOVED BISTABLE			
B DB1 032122	081380	L RM G16 V	1	N	DECAY HEAT ISO VLV DH-11 BEGAN CLOSING STOPPED PMP				PERSONNEL FAILED TO BLOCK AUTO CLOS.SIGNAL			
B DB1 032832	100880	H CV E25	1	T	GROSS BACK LEAKAGE DISCOVERED THROUGH CF30				DISK DISENGAGED FROM VALVE BODY			

ALL VALVE LEADS USED

ACT	S Y N C O N T R O L N U M B E R -	EVENT DATE	S C M C A T F A N U T Y D O U S E L E -	MODE DESCRIPTION	CAUSE DESCRIPTION	
					P	L
B	DE1 014808	041376	H XV F12	1 N FLOOD TANK 1A NITROGEN ADD VLV FAILED OPEN	VAL STEM SEPERATED FROM DISK	
B	DE1 030598	030680	L MV A26	1 T DHR COOLER 1B OUTLET VLV 1LP-14 FAILED TO OPEN	OUT OF ADJUSTMENT LIMIT SWITCH	
B	DE1 031621	061880	H CV E00	1 N BACKLEAKAGE DISCOVERED THROUGH "B" HPI LINE CHECK VLV NO CAUSE GIVEN	DIRRY ELEC CONTACT IN MOTOR CONTROL CENTER	
B	DE2 016201	101476	L MV A16 S	1 T VLV LPW-5 COULD NOT BE OPENED REMOTELY	LOOSE SET SCREW ON PINION GEAR OF MTR SFT	
B	DE2 017541	040577	F MV B12 R	1 T VALVE 2LP-21 FAILED TO CLOSE	PERSONNEL ERROR	
B	DE2 019970	120877	F XV V01 U	1 N ISO-VLV TO CHAN 3 RB PRESS TRANS SHUT BY MISTAKE	PERSONNEL SHOULD HAVE BEEN DOING UNIT 1'S	
B	DE2 027792*	120979	H MV A02	2V M HPI SUCTION VLV FROM AWST RENDERED INOPERABLE	PREVIOUS REPAIR WORK OR VIB. AND AGE	
B	DE2 031735	062580	F MV A02 R	1 U 2LP21 FAILED TO OPEN, SET SCREW LOOSE ON MOTOR PIN.	LOOSE SET SCREW ON MOTOR OPERATOR PINION	
B	DE2 032690	091680	F MV A20 R	1 T 2LP21 FAILED TO OPEN	TORQUE SWITCH FAILURE	
B	DE3 014927	050476	L RM P23	1 T VALVE 3CS-5 WOULD NOT CLOSE REMOTELY	PERSONNEL ERROR	
B	DE3 016209	110176	H CV V01 U	2 M IMP-LINEUP VALS 3HP-152 + 3HP-153 CLOSED S+8.OPEN	MECH PARTS LOOSE+OUT OF ALIGN	
B	DE3 020064	010378	L AV F12	1 T VALVE 3LP-14 FAILED TO CYCLE MANUALLY	TORQUE SWITCH FAILURE	
B	DE3 020592	020378	F MV A23	1 T VALVE BS-3 FAILED TO OPEN	VALVE STEM FAILURE	
B	DE3 020593	020770	F MV F12	1 T VALVE BS-2 FAILED IN INTERMEDIATE POSITION	DIRT ON VAL OPER CONTACTS	
B	DE3 021047	032078	H MV A16 S	1 T VALVE HP-24 FAILED TO OPEN	MOTOR MISWIRED	
B	DE3 027368	101979	L MV F02	1 T LPI VLV 3HP-10 OPENED FULL WHEN ATTEMPTING CLOSE	NO CAUSE GIVEN FOR VLV FAILURE IN ECCS SY	
B	DE3 031086	042380	L CV 800	1 N CHECK VLV FAILED TO RESEAT AFTER TEST	TIGHT PACKING /POSS STICKING SEAT	
B	RS1 014306	020776	L MV A14	1 T RHR M0V FAILED TO OPEN DURING TESTING (HV-261061)	TOURGE SWITCHS NEEDED RESET/TESTED WEEKLY	
B	RS1 016598*	111176	L MV A23 R	2 T TWO DECAY HEAT MOVS FAILED TO OPEN FOR MONTH TEST	LIMITORQUE OPERATOR ISMBI FAILED/EXCESS O/P	
B	RS1 019536	100177	L MV F20 R	1 N BWS ISOL VALVE FAILED TO OPERATE (SEV-2003)	UNKNWN/2 REPLACED, 1 REBUILD	
B	RS1 019666	111177	H MV V04 U	2 T VALVE LINE-UP INCORRECT/NEW VALVES WERE INSTALLED --WITH OPEN/CLOSE INDICATION ATYPICAL	UNKNOWN	
B	RS1 019793	111977	H MV F00	1 T HPI INJECTION ISOLATION VALVE FAILED TO CYCLE/TEST UNKNOWN		
B	RS1 0217468	061178	K RV C00	3 T 2 SAFETY, 1 ELECTRO RV LEAKING THRU DURING TESTING		
B	RS1 030143	010980	H RM F16 U	1 U POWER TO MU TANK ISO VLV SFV-23508 WAS NOT RESTORE PERSONNEL ERROR		
B	RS1 030725	032280	L MV B20 R	1 N SFV-25003 48WST ISO TO DHR SUCTION) FAILED TO CLO. FAILED CLUTCH IN MOTOR OPERATOR		

ALL VALVE LERS USED

P/N	VALVE NUMBER	CONTROL EVENT DATE	SYSTEM CONN	CAT FCTV	HOUSING LINE	MODE DESCRIPTION	CAUSE DESCRIPTION	
							A	C
B T11 017343	030977 F MV B23	1 T	NO SPRAY PUMP SUCTION VALVE FAILED TO CLOSE/TEST	GREASE IN SPRING PREVENTED TORQUE SW OPER				
B T11 075505	011279 H MV A16 S	1 T	HPI OH-V-5B DID NOT OPEN FROM MID POSITION	MOTOR BREAK DID NOT RELEASE				
B T12 021277	040478 L AV A24 S	1 T	RHR ADV (NS-V838) FAILED TO OPEN DURING TEST	FAILURE OF SOLENOID OPERATED PILOT VALVE				
B T12 027456A	032879 B RM V00 U	2L N	AUX FEEDWATER BLOCK VALVS DISCOVERED CLOSED	NO CONCLUSIVE CAUSE COULD BE FOUND				
C AR2 023481	122078 B MV A16 T	1 N	FLOW CONTROL VLV 2CV-1025-1 FAILED TO OPERATE	LOOSE MOTOR POWER CONNECTION				
C AR2 026243A	051679 B MV B16 T	1 N	SUP VLV 2CV-1039-2 WOULD NOT RESPOND TO SIGNAL	BLOWN FUSE IN VLV CONTROL CIRCUITRY				
C AR2 026248	060379 B MV B26 R	1 N	EMER FEED MTR CONT VLV 2CV-1036-1 WOULD NOT SHUT	LIMIT SWITCH WAS OUT OF ADJUSTMENT				
C AR2 026243A	060979 B MV B16 T	1 N	EMER FEED MTR CONT VLV 2CV-1038-1 WOULD NOT SHUT	LOOSE WIRE ON THE HANDSWITCH				
C AR2 026543A	070679 B MV B00 R	1 N	EMER FEED MTR CONT VLV 2CV-1036 WOULD NOT SHUT	NO REASON FOUND FOR FAILURE				
C AR2 026896	082679 H MV A20	1 N	SAFETY INJECTION TANK MAKEUP VLV 2CV-5064 FA SHUT	SPRING TENS ON VLV OPER GATE OUT OF ADJ				
C AR2 031374	040880 F RM V03 V	1 T	*A* TRAIN CONT. SPRAY ACCIDENTALLY INITIATED	PERSONNEL ERROR DURING TESTING				
C AR2 031672	060580 B MV A16 T	1 N	EF WTR SUP. VLV 12CV-10751 FAIL. TO OPEN ON DEMAND LOOSE CONNECTOR AT VLV OPERATOR					
C AR2 031823	070780 B MV A20 R	1 N	EF VALVE 2CV-1075-1 FAILED TO OPEN FROM CONTROL RM LOOSE BRUSH CONNECTION					
C AR2 032447	081280 F MV F16 S	1 T	CONTAINMENT SUMP RECIRC VLV 20V-2648-2 FAILED	FOREIGN MAT. IN VLV OPERATOR SW CONTACTS				
C AR2 033375	112980 H RM B16 S	1 M	HPCI VLV 2CV-5056 FAILED TO CLOSE	ACHIEVED TO BE CONTROL CIRCUIT FUSE FAIL.				
C CCI 014465	030576 H MV F16 S	1 N	HP51 LP-150-VLV 1-MOV-616 WOULD NOT OPER. REMOTELY	BLOWN CONTROL CIRCUIT FUSE CAUSED FAILURE				
C CCI 016403	111776 H MV A23 R	1 T	AUX.HI.PRESS.LP.ISO.VLV SI-617 FAILED TO OPEN	DEFECTIVE TORQUE SWITCH BURNED CONTACTS				
C CCI 025619	041179 H MV V06 U	1 T	SI HOR ISO VLV SI-696 SHUT WHEN REQUIRED OPEN	DEFECTIVE PROCEDURES				
C CCI 026785	082879 L MV V01 U	2 T	SI-4145-MOV OPEN REQ SHUT, SI-643-MOV SHUT REQ OPN	OPERATIONS PERSONNEL ERROR				
C CCI 027170	092479 H MV A20 R	1 T	AUX HIGH PRESS LOOP ISO VLV SI-617 FAILED TO OPEN	VLV MOTOR WAS SINGLE PHASING IN OPEN DIR				
C CCI 030214	010480 H RM F23	1 N	12A HPSI STOP VLV WOULD NOT THROTTLE	LOOSE LEADS ON TORQUE SWITCH				
C CCI 018881	082577 F RM F16 S	1 N	#21 CONI.SPRAY SYS.HOR+150.VLV2-SI-4150-CVI 005	VLV PLACE+OUT OF SERV.DUE TO FAIL+RESIST.				
C CCI 019740	111577 H MV A26	1 N	MOV-627,AUX HI PRESS HOR STP LP 118,WOULDNT OPEN	OPEN LIMIT SWITCH CONTS. WERE DIRTY				
C CCI 022246*	090778 H CV E00	2Y N	#21886228 SI-TANK OUTLET CHECK VLVs LEAKING	CAUSE OF REVERSE LEAKAGE NOT GIVEN				
C CCI 033265	111080 H AV B24 S	1 N	SOLENOID AIR NLV CONTROLLING AIR FAILED	SOLENOID AIR NLV CONTROLLING AIR FAILED				

ALL VALVE LERS USED

Y E N T	PLA NT	CONTR OL NUMBER	EVENT DATE	S Y ST EM	C O M P	M O D E	C A U S E	T A Y P E	F A I L U M Y	ACTIV ITY	MODE DESCRIPTION		CAUSE DESCRIPTION	
C	FC1	014561	041476	H	RM	B16	S	1	T	HCV-383-4 FAILED TO CLOSE ON TEST			BINDING CONTACT IN BREAKER TO VALVE	
C	FC1	019551	102677	K	RV	A00	R	1	M	VALVE PC-142 RELIEF PRESSURE OUT SPEC HIGH			COULD NOT BE DETERMINED	
C	FC1	022469	092178	B	AV	A24	U	1	T	VAL YCV-1045 FAILED TO OPEN/AUX.FD.PMP.STM.INL.1			INSTRUMENT AIR SUPPLY TO VAL CLOSED	
C	FC1	022972	110178	B	CV	E05	C	1	R	AUX FEED CHECK VALVE FOUND INSTALLED WRONG			CONSTRUCTION ERROR	
C	FC1	023139	112478	L	RM	F16	U	1	T	PC-105B WAS NOT OPERATING			VALVE CLOSING RELAY NOT REWIRED AFT MAINT	
C	FC1	023171	122078	K	RV	V06	U	2	M	TWO PRESS OP RELIEF VALVES OPENED WHEN REQ CLOSED			TECH FULLED FUSES,DEFECTIVE PROCEDURES	
C	FC1	025590	032179	H	MV	A16	S	1	N	LOOP SAFETY INJECT. VLV HCV-311 FAILED TO OPEN			INTERLOCK SWTCH BINDING IN CONT CERCUTRY	
C	FC1	030212	011780	H	RM	B16	S	1	T	CONT.' SUMP RECIRC VLV HCV-383-4 FAILED TO CLOSE			AUX INTERLOCK FOUND BINDING	
C	M12	014461	030976	B	RM	A16	S	1	M	AUX.FEEDPMP,STM,INLET VLV,CYCLED;WOULD NOT REOPEN			FAILURE OF VALVE OPERATING CIRCUIT	
C	M12	015338	072476	B	MV	A20		1	N	INLET STEAM TRIVALEVE WOULD NOT OPEN			VALVE OPERATOR SPINDLE FAILED	
C	M12	017620	040777	H	CV	E00	R	1	N	INT LEAK OF CV BETW INJECT TK 4 AND PRI COOLANT			CAUSE UNKNOWN	
C	M12	018740	072177	H	CV	E00	R	1	N	S.I.HEADER CHECK VLV. 2-SI-648 LEAKING INTERNALLY			NO CAUSE GIVEN	
C	M12	018971	081677	H	CV	E00	R	1	N	INT LEAK OF CV BETW INJECT TK 4 AND PRI COOLANT			CAUSE UNKNOWN	
C	M12	027976*	122879	H	AV	F00		2	T	HPSI INJ.VLVS. 2-SI-616&626 OVERTRAVELED 3%			NO CAUSE FOUND FOR FAILURE	
C	M12	028075*	122879	H	RM	C00	R	2	N	SI TANK #1 FILL VLV AND/OR DRAIN VLV LEAKING INTER NALLY--NO CAUSE FOR LEAKAGE GIVEN				
C	M12	031945	070380	H	XV	V06	U	1	T	HPSI PUMP MINIMUM FLOW VLV WAS SHUT			DEFECTIVE PROCEDURES, CAUSED PUMP SEIZURE	
C	M12	033586	121080	H	MV	F23		1	T	HPSI INJECTION MOV-2-SI-616 OVERTRAVELED 1/4 INCH OPERATOR SENSITIVE TO TORQUE SWITCH			DEFECTIVE PROCEDURES (CAUSE UNKNOWN)	
C	MY1	020758	020277	H	RM	F16	U	1	M	VALVE SL-P-3 FAILED TO OPERATE			WIRES DISCONNECTED (CAUSE UNKNOWN)	
C	MY1	022141	081578	K	RV	A00		1	M	PRESSURIZER RV PR-S-13 SETPOINT OUT OF SPEC			CAUSE UNKNOWN, SETPOINT ADJUSTED	
C	MY1	025490A	030779	H	MV	F23		1	T	"A" TRAIN HPSI PMP SUCT.VLV FAILED TO OPERATE			IMPROPER TORQUE SWITCH SETTING	
C	MY1	025490B	030779	F	MV	F23		1	T	"A" TRAIN SCAT OUTLET VLV FAILED TO OPERATE			IMPROPER TORQUE SWITCH SETTING	
C	MY1	026274	060779	F	XV	A12		1	N	CS-14 "B" TRAIN SPRAY HEADER ISO.VLV WOULD NOT OPN REMOTE LINKAGE DISCONNECT FROM HANDWHEEL				
C	MY1	030804	031980	L	XV	V01	U	2	N	RHR VLVS RH-8 AND RH-10 FOUND OPENED AND UNLOCKED			PERSONNEL ERROR	
C	MY1	030991	040880	L	MV	F00	R	1	T	LPSI LOOP HEADER STOP VALVE FAILED TO OPERATE			NO CAUSE FOUND (VLV IN LOOP #3)(LSI-M-31)	
C	MY1	031389	050680	L	MV	F20	R	1	T	LPSI LOOP 3 HEADER STOP VLV FAILED TO OPERATE			BROKEN WELD ON COUPLING ON LSI-M-31	

ALL VALVE LERS USED

P N Y E N T	A C T U A L C O N T R O L N U M B R E A T H E D A T E	S Y C H A T F I V I T U S T C H O D S E L H P E E L H	C O N T R O L N U M B R E A T H E D A T E	A C T U A L C O N T R O L N U M B R 	MODE DESCRIPTION		CAUSE DESCRIPTION
					S Y C H A T F I V I T U S T C H O D S E L H P E E L H	A C T U A L C O N T R O L N U M B R 	
C MY1 031390	050780 H XV V03 U	2L U	C OOLING WATER IMPROP LINED UP TO S-CHARGING PUMP	P	PERSONNEL ERROR (SEPARATION NOT MAINTAIN)		
C PA1 018274	061577 H MV A16 T	1 T	M0V-3011(HPC) ISO-VLV FAILED TO OPEN	P	CONTACT FOR "SEAL-IN" CKT ON RELAY FAILED		
C PA1 020230	122377 H MV G16 Y	1 T	BAD SWITCH CAUSED CLOSING CONT. TO STICK	P			
C PA1 020231	010878 L AV A24 S	1 U	WATER IN AIR LINE TO VALVE OPERATOR	P			
C PA1 025184	012679 H RM F16 S	1 N	SI TANK F1620 VENT VLV OPENED WHEN PRESSURIZING TNK	P	SHORT BETWEEN FILL AND VNT VLV CIR(CV305)		
C PA1 0273658	101279 K RV A12	1 T	RV1039(PZR) RELIEF VLV SET PRESSURE FOUND HIGH	P	ALIGNMENT PIN FOUND MISPOSITION		
C PA1 032156	071980 H XV V03 U	1 N	INST. EO. VLV NOT CLOSE AFTER CALIBRATION	P	PERSONNEL ERROR WHEN CAL. HPSI FLOW IND.		
C PA1 032224	081980 H RM V03 U	1 N	CV-3031 WAS CLOSED AND THEN IMMEDIATELY OPENED	P	OPERATOR FAILED TO RELATE TEST REQUIRE.		
C SL1 015002	052176 8 MV A16 Y	1 N	NO AUX FEED PUMP STEAM SUPPLY VALVE FAILED TO OPEN	P	NO SIGNAL TO VALVE/COMMAND FAULT(F1620)		
C SL1 015507	070976 8 MV A16 T	1 T	AUX FEED PUMP STEAM INLET VALVE FAILED TO OPEN	P	COMMAND(H20) IN CONTROL CIRCUIT/POR DES		
C SL1 016880	120876 8 MV A16 T	1 T	AUX FEED PUMP STEAM INLET VALVE FAILED TO OPEN	P	COMMAND(H20) IN CONTROL CIRCUIT/DESIGN		
C SL1 019504	081777 F RM A00	1 T	CONTAINMENT SPRAY VALVE FAILED TO OPEN/TESTING	P	UNKNOWN/ LOCKED OPEN HANDWHEEL		
C SL1 019509	092577 F RM A00	1 T	CONT.SPRAY HOR. ISO-VLV FCV-07-18 NOT FULLY OPEN	P	UNKNOWN (CONT.SPRAY VLV. STICKING)		
C SL1 020639	020978 8 MV 820	1 T	AUX FEED PUMP VALVE (MV-09-11) FAILED TO CLOSE	P	MOV MOTOR WINDING PARTIALLY SHORTED		
C SL1 023141	112178 H MV A23	1 T	MOV 07-18 IN 18 ECCS TRAIN FAILED TO OPEN ON TEST	P	TORQUE SW FAULTY.REPLACED SWITCH		
W BVI 016356	102576 H MV B16 S	1 N	DRAIN VALVE ON ACCUMULATOR IC FAILED TO SHUT	P	NO PWR/TERMAL OVERLOAD OF LINESTARTER		
W BVI 018725	072677 8 RM A23	1 T	AUX. FEEDWATER CONT VLV WOULD NOT OPEN ELECTRIC.	P	BINDING TORQUE SWITCH		
W BVI 022135	080178 L RM 810	1 T	18 LOW HEAD SAFETY INJECTION PMP+HEAD.150.NOT CLOS VLV FAIL.10 CLOSE DUE TO BORIC CRY. IN PAK	P			
W BVI 025486	030579 8 CV F12	1 N	1C 5/G STM SUP CHECK VLV INOPERABLE	P	NUT AND WASHER ON CHECK VLV WAS MISSING		
W BVI 028146	060979 L MV F23	1 M	18 LH51 PUMP SUCTION VLV FOUND TO BE INOPERABLE	P	MTR OPERATOR TORQUE SWITCH WAS FAILED		
W BVI 028105	091079 L CV G10	1 T	1A LH51 PUMP RECIRC CHM VLV HAD FLOW RESTRICTION	P	FOREIGN MATERIAL LODGED IN CHECK VLV		
W BVI 027663	112779 H MV V01 U	1 M	HHS1 PMP SUC VLV CH-1150 150 FOR MAINT WHEN RFQ OP	P	PERSONNEL ERROR--2ND VLV ALSO SHUT		
W BVI 031210*	052180 L RM B16 U	2V T	RHR 150 VLV FAILED TO CLOSE	P	DEENERGIZED PROCESS CONTROL SIGNAL		
W BVI 032895	100160 H CV 812 R	1 T	SI PUMP(CH-P-2A) DISCHR CHECK DID NOT RESEAT	P	ANTI-ROTATION DEVICES BINDING		
W BVI 033542*	121680 K RV F00 R	2V U	PLANT SHUT DOWN TO REPAIR PZR SAFETY VLVs	P	CAUSE NOT GIVEN		

ALL VALVE LERS USED

P L A N T	V E N T	C O N T R O L	E V E N T	S Y S T E M	C O M P R E S S	M O D E	C A U S E	T Y P E	F A L L	H U M I T Y	A C T I V I T Y	MODE DESCRIPTION	CAUSE DESCRIPTION	
W DC1 016367	110176	L MV F12	1	T	RHR VALVE FAILED TO CYCLE DURING TESTING								PACKING GLAND WAS TOO TIGHT	
W DC1 016648	121776	F MV VOL U	1	T	CONTAINMENT SPRAY PUMP SUCTION VALVE FOUND CLOSED								PERSONNEL LEFT VALVE SHUT AFTER A TEST	
W DC1 020694	020878	B MV B16 S	1	N	AUX FEED MOV FAILED TO CLOSE								COMMAND/LOOSE ELEC CONNECTION/CONTROL	
W DC1 021011*	032278	H MV F16 U	3	N	POWER FOUND OFF TO 3 ECCS VALVES								3 BREAKERS FOUND TRIPPED ON MCC	
W DC1 023114	112878	B MV B16 S	1	N	AFW THROTTLE VLV. WOULD NOT CLOSE ELECTRICALLY								BROKEN LEAD ON MTR OPERATOR	
W DC1 025045B	010679	B MV B20 R	1	M	AFW VLV FMO-231 WOULD NOT CLOSE								BROKEN WIRE IN MOTOR OPERATOR	
W DC1 025380	022379	B MV B16 T	1	T	AFW DISCHG VLV FMO-212 WOULD NOT CLOSE								LOOSE CONNECTION IN HOT SHUTDOWN PANEL	
W DC1 025378	030379	B MV B20 R	1	N	AUX FEED VLV FMO-212 WOULD NOT SHUT FROM CONT RM								BROKEN WIRE IN VLV'S OPERATOR	
W DC2 020978	031878	B CV B00	1	N	AUX FEED SYS CHECK VALVE FROM S/G 1 STUCK OPEN								UNKNOWN (VALVE Z-FW138-11)ATWOOD & MORRILL	
W DC2 021079	041678	L XV VOL U	1	N	HANDWHEEL CAME OFF RHR VALVE POSITIONING IT WRONG								PERSONNEL FAILED TO REPOSITION THE VALVE	
W DC2 022069	071978	L MV F00	1	T	RHR PUMP SUCTION MOV FAILED TO CYCLE/TIME-WISE								UNKNOWN WHY CYCLE TIME EXCEEDED	
W DC2 022581	092278	K RV VOL U	1	T	PRESSURIZER RV OPENED WHEN REQUIRED TO BE CLOSED								PERSONNEL ERROR	
W DC2 022838A	101078	B AV COO	1	U	PNEUMATIC TEST VALVE LEAKED THRU								UNKNOWN	
W DC2 022838B	101078	B XV VOL U	1	T	AUX FEED VALVE FOUND UNLOCKED & OPEN/WRONGB LINE-UP								PERSONNEL ERROR	
W DC2 023030*	112178	F CV A05 C	2	N	CHK.VLV.S-CTS-127EGW TO THE LOWER CONT.SPRAY NOZZLE-								-ES INSTALLED BACKWARDS//FABRICATION ERR.	
W DC2 025045A	010679	B MV B20 R	2	M	AFW VLV FMO-232&222 WOULD NOT CLOSE								BROKEN WIRES IN MOTOR OPERATORS	
W DC2 027930	121779	F MV A23	1	N	CONTAIN SPRAY PMP DISCHG VLV FMO-220 FAILED TO OPN								FAILURE CAUSED BY TORQ SWTCH BENDING	
W DC2 030740	032580	B MV F16 S	1	T	AUX FEED VLV FMO-221 (#2 SGF DID NOT OPERATE								ARMATURE LEAD PULL OFF OF VLV OP MOTOR	
W DC2 031630	061380	B RM COO	1	M	FRV-225 LEAKED ENOUGH TO HINDER WELDING DOWNSTREAM								NO CAUSE GIVEN. MINOR LEAKAGE	
W HN1 015218	070576	B CV E00	1	N	CHECK VALVE IN FEED LINE HAD REVERSE LEAKAGE								NO CAUSE GIVEN FOR REVERSE LEAKAGE	
W HN1 018777	080177	B CV E00	1	T	CHECK VALVE ON AUX FEED PUMP LEAKING INTERNALY								UNKNOWN	
W IP2 0187878	050777	F RM F23	1	T	VALVE 822B DID NOT OPERATE PROPERLY								TORQUE SWITCH MALFUNCTION	
W IP2 018788A	051377	K RV A00 R	1	T	RV PCV-468 DID NOT OPEN AT SETPOINT PRESSURE								SET POINT DRIFT	
W IP2 018788B	051377	K RV C25	1	T	INTERNAL LEAKAGE PAST VALVE PCV-466								EXCESSIVE VALVE SEAT WEAR	
W IP2 021653	052378	H CV E12	1	T	4 IN SWING CV D.S.OF PUMP 22 LEAKING INTERNALY								TWO HANGER BRACKET BOLTS MISSING	

ALL VALVE LERS USED

PLANT NUMBER	CONTROL EVENT DATE	SYSTEM TEMP	COMP MODE	CAUSE	TYPE	ELM	ACTIVITY	NUM Y	MODE DESCRIPTION		CAUSE DESCRIPTION	
									MODE	ELM	Y	MODE
W IP2 026367	062679	B RM 800	1	T	SHUTOFF VLV PCV-1310B1STM.SUP. TO #22 AFW PMP1 WOULD NOT SHUT--NO CAUSE FOUND							
W IP3 014604	042976	F RM V03 U	2L	T	INCRT.VLV LINUP FOR TEST,CNTNMNT SPRY ACCID.TURN ON PERSONNEL ERROR							
W IP3 030696	031580	F XV A08	1	T	VC ISO VLV 869B(ESO SPRAY PUMP FROM CONT SPRAY HDR DIDN'T OPEN.KEY FAILURE IN YOKE NUT BUSH.							
W IP3 033011A	101780	X RV C25	1	T	PCV-466 WOULD NOT RELEASE AT SET PRESSURE & LEAKED VALVE SEAT AND DISK HAD GROOVES							
W JF1 020993	032578	B MV V02 U	2	N	MDAFFF & TDAFFF RECIRC BYPASS ISO VLVS OPEN						PERSONNEL ERROR	
W JF1 022633*	090978	B RM F16 U	3	T	CONTROL WAS LOST ON FLOW CONY.VLV 3228A,B,EC						DEFECTIVE RELAY IN TDAFFF CONTROL CIRCUIT.	
W JF1 022629	091878	L RM V06 U	1	T	RHR PUMP SUCTION VLV 8701A CLOSED WHEN REQ. OPEN						INADEQUATE PROCEDURES	
W JF1 025436	012379	G MV F00	1	T	BIT INLET VLV Q1E21V016B FAILED TO OPERATE ELEC.						NO CAUSE FOUND FOR FAILURE	
W JF1 030326*	020180	B RM A24 U	2V	T	CONTROL VLVS FOR "A" AUX FEED TRAIN DIDN'T AUTO OP //EN. CONTACTS MISALIGNED IN CONTROL CIR							
W JF1 030614	030380	F MV A00	1	T	CS-MOV-88208,DISCH TO CONT SP HDR,DID NOT OPEN						CAUSE UNKNOWN (AFFECTED THE B TRAIN)	
W JF1 031513	052880	L AV B12	1	T	1A RHR HEAT EXCH DISCHARGE VLV FAILED TO CLOSE						CAP SCREW CONNECT STEM AND OP CAME OUT	
W JF1 033005	102080	H MV A26	1	T	VALVE 1-CVC-MOV-115D(RWST SUPPLY TO CHR PUMPS)FAT/ LED TO OPEN. LIMIT SWITCH NEEDED ADJ.							
W JF1 033572	112880	L RM F16 S	1	T	LOOP SUCTION VLV FOR "A" TRAIN RHR CLOSED						DIRTY CONTACTS IN PRESSURE TRANSMITTER	
W JF1 033672	122580	L RM F16 S	1	M	RHR LOOP B SUCTION VLV WENT CLOSED WHEN REQ OPEN						IMPROPER SIGNAL TO VLV DUE TO SHORT/MAINT	
W KE1 013963	010876	H MV F12	1	T	VALVE SI-2B DID NOT OPERATE						SCREW HOLDING TRIP LEVER BACKED OUT	
W KE1 014240	022076	F RM A01 C	1	T	VALVE ICS-5B FAILED TO OPEN(CONT-SPRAY DISCH. VLV)						VALVE MANUALLY TORQUED DOWN TOO TIGHT	
W KE1 019312	100377	F MV F02 C	1	M	MAINT.MAN DEENERGIZED 2 SW VLVS,WHEN ONLY ALLOW.T- -O DEFNER.1 VLV//PERSONNEL ERROR							
W KE1 020788	030278	H MV A00 R	1	T	CNTNMNT SUMP ISO VAL WOULD NOT FULLY OPEN						CAUSE UNKNOWN	
W KE1 021077	040478	H MV A14 R	1	T	CNTNMNT SUMP ISO VAL WOULD NOT FULLY OPEN						VAL PACKING AT END OF USEFULL LIFE	
W KE1 026136	053079	L RM A00	1	N	RHR LOW HEAD INJECT VLV SI-302A FAILED TO OPEN						NO CAUSE FOUND FOR FAILURE	
W KE1 030654	030380	L MV A23	1	T	DURING CONT SUMP RECIRC TEST,SI-351 DID NOT OPEN						TORQUE SWITCH OUT OF ADJUSTMENT	
W KE1 030693	031080	B RM 800	1	T	AUX FEED PUMP DISCH CROSSCONNECT VLV FAIL TO CLOSE						NO CAUSE FOUND FOR FAILURE OF AFW 10B	
W KE1 031613	062480	L CV 800	1	N	RHR SUCTION CHECK VLV FAILED TO CLOSE						CYCLING OF PUMPS SEATED CHECK VALVE	
W MA1 020872	031478	G AV F16 S	1	N	LET DOWN TRIP VALVE OUTSIDE ISOLATION CLOSED SPUR						SHORT IN VALVE CIRCUIT CAUSED VLV TO SHUT	
W MA1 021150	042878	H RM 800	1	N	STEAM DUMP VAL 408E STUCK OPEN FULL. TRIP						CAUSE NOT GIVEN	

ALL VALVE LERS USED

P L A N T N U M B R E H C O N T R O L E	S Y S T E M C O M M D E U S E P E E L M Y	C A U T F A I L N U M B R	A C T I V I T Y	MODE DESCRIPTION		CAUSE DESCRIPTION
				DATE	MODE	
W NA1 021506	051478	R AV V06	U	2	T	AUX FEEDWATER VALS PCV-F2-159A,-159B IMP.LINEUP
W NA1 022269	081778	L MV A14		1	T	VALVE MOV-1860B FAILED TO OPEN DURING TEST
W NA1 025767	030679	L RM F00		1	N	RHR DISCHG VLV MOV-1720B INADVERTANTLY OPENED
W NA1 025862	041679	L MV B26		1	T	RHR ISO.VLV MOV-1701 FAILED TO CLOSE AUTOMATICALLY
W NA1 025859	043079	H RM A14		1	N	SAFETY INJECTION VLV MOV-1856B FAILED TO OPEN
W NA1 025974	051179	L RM A00		1	T	LOW HEAD SI PMP DISCHG.VLV.MOV-1863A FAILED TO OPN
W NA1 027593	110679	L RM V02	U	1	N	RHR INLET VLV MOV-1701 SHUT WHEN REQ. OPEN
W NA1 030111	011880	F RM A16	T	1	N	MOV-RS-100A FAILED TO OPEN (COMMAND FAULT)
W NA1 030333	012980	F RM A16	T	1	N	MOV-RS-100B FAILED TO OPEN (COMMAND FAULT)
W NA1 031697	062380	L RM A16	S	1	T	RECIRC VLV MOV-1863B FAILED TO REOPEN
W NA1 036209A	122980	F MV F16	S	1	T	MOV-SW-105C FAILED TO OPERATE DURING TEST
W NA1 036209B	122980	F MV F10		1	T	MOV-SW-108A FAILED TO OPERATE DURING TEST
W NA1 036209C	122980	F MV F00		1	T	MOV-RS-101A FAILED TO OPERATE DURING TEST
W NA2 032572	090580	G CV B09		1	T	Z-SI-70(BORON INJ RECIRC LINE) LEAKED EXCESSIVELY
W PR1 014758	051376	L MV A23	R	1	T	MOV FAILED TO OPEN DURING TEST (MV-32065)
W PR1 018341	061877	B MV F20		1	N	AUX FEED PUMP DISCHARGE VALVE FAILED TO OPERATE
W PR1 026266	041079	H MV A00		1	T	MV-32067 HPSI VLV TO RX VESSEL FAILED TO OPEN
W PR2 016284A	102576	H RM B00		1	T	HOT LEG SAMPLE LOOP VLV CV-31807 FAILED TO CLOSE
W PR2 017889	051977	B XV V06	U	1	U	PUMP INLET VALVE FOUND NEARLY SHUT/AUX FEED INLET
W PR2 019284	100477	H MV A00		1	T	SAFETY INJ PUMP SUPPLY VLV MV-32183 FAILED TO OPEN
W PR2 020125	122377	B MV A16	S	1	T	#22 TURB.DRIVEN AFW PUMP STM.SUP.VLV FAILED TO OP-
W PT1 013945	010876	B MV F20		1	T	-EN//MOTOR LEAD GROUNDED TO JUNCTION BOX
W PT2 014348	031576	F MV A03	R	1	T	MOV-4020 AUX FEED PUMP DISCHARGE FAILED STUCK/TEST VALVE OPERATOR RING WORN/GEAR REPLACED
W PT2 015186	070176	B MV A23	R	1	T	CONTAINMENT SPRAY 2MOV-860B FAILED TO OPEN / TEST PERSONNEL ERROR/TERMINAL SLIDER OPEN
W PT2 017035	012777	F MV F16	T	1	N	MOV-2MS-2019/STEAM TO AUX FEED PUMP FAILED TO OPEN TORQUE SW SETPOINT CAUSED TIGHT CLOSING
		CONT.SPRAY PMP.DISCHG.VLV.2-860B INOPERABLE				VALVE OPERATOR BREAKER WAS OPEN

ALL VALVE LERS USED

PLANT NUMBER	CONTROL NUMBER	EVENT DATE	SYSTEM COMP	MODE	CAUSE EELM	TYPE FILM	ACTIVITY NUMY	MODE DESCRIPTION		CAUSE DESCRIPTION	
W PT2	018572	072877	H MV	VOL U	1	N	MOV FOUND IN INTERMEDIATE POSITION/SINCE PREV TEST			PERSONNEL FAILED TO ASSURE FULLY OPEN	
W PT2	021766	061678	F MV	F23	1	T	CONT SPRAY VALVE(MOV) FAILED TO OPERATE FOR TEST			SMB-00 LIMITORQUE SW FAULTY/REPLACED	
W RG1	018247	071377	H CV	E00	1	N	SI PUMP 1A CHECK VALVE REVERSE FLOW TO RWST			UNKNOWN/H VELAN 3 INCH 1500 PSIG CHECK VAL	
W RG1	025265	020679	L MV	A00	1	T	CNTMT RECIRC SUMP OUTLET MOV-851B FAILED TO OPEN			FLEX OF LONG EXT MIGHT HAVE CAUSED OVERTO	
W RD2	014822	012876	H CV	E00	1	N	B ACCUMULATOR CHECK VALVE 879E LEAKED THRU			REASON NOT STATED	
W RD2	019570	081776	B MV	A20 R	1	T	VALVE V2-16A FAILED TO OPEN			LIMITORQUE OPER FAILED TO OPEN VALVE	
W RD2	017540	032677	B RM	A00	1	N	VALVE V2-14A FAILED TO OPEN			INCREASE IN TENSION BETWEEN SEATING SURF.	
W RD2	019350	081677	B MV	A20 R	1	N	VALVE V2-16B FAILED TO OPEN AS REQUIRED			LIMITORQUE VALVE OPERATOR FAILED	
W RD2	019351	081777	B CV	E05	1	T	DISCH CK VAL FOR AUX FEED PUMP,C STM GEN FAILED			CK VAL HAS BURR ON HINGE JOINT,OPEN POSIT	
W RD2	019352	081777	B MV	A20 R	1	N	VALVE V2-16A FAILED TO OPEN			LIMITORQUE VALVE OPERATOR FAILED	
W RD2	019667	102677	L MV	A20	1	N	RHR VALVE 759B FAILED TO OPEN			MOTOR WINDINGS WERE SHORTED	
W RD2	020053	120377	L MV	A16 S	1	T	RHR VALVE 744B FAILED TO OPEN			CIRCUIT THERMAL OVERLOAD DEVICE TRIPPED	
W RD2	022626	122177	B MV	A12 R	1	T	AUX FEED PUMP DISCH VAL,V2-16A FAILED TO OPEN			EXCESS SEATING PRESS CAUSED BY OVERHEAT	
W RD2	020181	122277	B RM	C19	1	N	VALVE V2-14C LEAKING INTERNALLY / NOT SHUT FULLY			INSUFFICIENT VALVE STEM LUBRICATION	
W RD2	020322	011178	L MV	F20	1	T	VALVE RHR-744B FAILED TO FUNCTION PROPERLY			OIL LEAKED INTO MOTOR {GASKET FAILED}	
W RD2	027067	090579	B MV	A16 T	1	N	AFW ISO.VLV AFW-V2-16A FAILED TO OPEN			OPERATOR POWER SUPPLY BREAKER WAS TRIPPED	
W SA1	016939*	011077	H MV	F20	2	N	MTR.BRKRS.TD VLVS 15J162 TRIPPED WHEN VLVS WERE OPENED//BOTH MTR.OPERATORS HAD FAILED				
W SA1	021910	052378	H MV	A20	1	T	MOV 15J1 (HP15) FAILED TO OPEN DURING TEST			WINDING FAILED/INCORRECT MOTOR SIZE/PERSN	
W SA1	022422	082478	B AV	A12	1	T	AUX FEED PUMP STEAM VLV (1MS132) FAILED TO OPEN			STEM WAS FOUND DISENGAGED FROM ACTUATOR	
W SA1	033529	121480	H CV	B00	1	T	VALVE 11SJ139 WAS FOUND TO BE COCKED OPEN			NO CAUSE GIVEN FOR LIFT CHECK VALVE FAIL	
W SE1	033818A	092280	L MV	F26	1	U	1-FCV-70-156 FAILED TO OPERATE			LIMIT SW REQUIRED ADJUSTMENT	
W SE1	033789	092780	H CV	B05	1	T	CHECK VLV 63-635 STUCK IN OPEN POSITION			INTERFERENCE BETWN DISC WELD AND VLV BODY	
W SE1	032973*	100580	B RM	F01 C	2	T	AUX FEEDWATER VLVS LCV-3-1746173 WOULD NOT HAVE OP //ER IN AUTO. PRESS SWITCH LEFT ISOLATED				
W SE1	033298	111980	F MV	A16 S	1	T	CNTMT SUMP VLV TO CNTMNT SPRAY PMP DID NOT OPEN			INTER LIMIT SW ON FCV7421 FAILED ICV72-2C	
W SD1	020609	013078	F RM	B00	1	T	CONT SPRAY VLV (CV-517) FAILED TO CLOSE FOR TEST			UNKNOWN/POSSIBLE LUBRICATION PROBLEM	

ALL VALVE LERS USED

P L Y E N T	A N T C O N T R O L N U M B R	S C H A T F A N S C H O U S P I L H	C A U T H Y Y E V E N T E E P D A T E H P E M	M O D E D E S C R I P T I O N	C A U S E D D E S C R I P T I O N
					CAUSE DESCRIPTION
					MOV-850C FAILED TO OPEN IN REQUIRED TIME / TESTING SHAFT DISTORTED/PROB DUE TO EXCESS TORQUE
					AUX.FEEDWTR.PUMP DISC.VLV.MOV-FW-151A FAILED TO OPEN -PENITIMING RELAY FAILURE
					UNKNOWN
					MOV-850C FAILED TO OPEN AT HI PRESS UNKNOWN / SETPOINT DRIFTN UP
					MAINT ERROR/STEM WAS NOT ENGAGED TO DISC
					UNKNOWN
					MOV-RH-100 FAILED TO OPEN CAUSE UNKNOWN
					MOV-1-FW-89 40ISCH AUX FP) FAILED TO CLOSE CAUSE UNKNOWN
					MOV-1852A DELAYED IN CLOSING WHILE RECIRC ACCUMULATED BELIEVED TO BE MOISTURE IN AIR LINES
					MOV-2862B FAILED TO OPERATE FROM CONSOLE THERMAL OVERLOAD DUE TO VALVE PLUG BIND
					UNKNOWN
					MOV-2-51-127 LEAKING THRU UNKNOWN
					RHR VLV CLOSED WHEN IT WAS REQUIRED TO REMAIN OPEN VOLT.FLUC.ON INSTRUMENT AC BUS
					RWST SUCTION VALVE FRO-112 IF FAILED TO OPEN/DEMAND TORQUE SW SET TO LOW/VAL WOULDNT UNSEAT
					RWST SUCTION VALVE (MO-112D) FAILED TO OPEN/DEMAND BREAKER SUPPLYING POWER FAILED/COMMAND
					RHR DISCHARGE VLV (8728B) FOUND LOCKED CLOSED PERSONNEL ERROR/IMPROPER VALVE LINING
					MOTOR OPER FAILED/WATER CAME THRU GASKET
					VALVF STEM LACKED LUBRICATION
					--CLOSE//PROCEDURAL DEFICIENCY
					MOV-85016 010478 H MV A19 1 T DEENERGIZING PROTECTION SYS CAUSED RHR VALVES TO CLOSE//PROCEDURAL DEFICIENCY
					MOV-88807A FAILED TO OPEN DURING TESTING
					TWO VALVES INADVERTANTLY OPENED/RMST LEVEL DECREASES PERSONNEL ERROR/POSSIBLE PROCEDURE PROBL
					YRI 018419* 062777 K RV A00 2 T PRESSURIZER SAFETY VALVES (181/182) FAILED TO OPEN UNKNOWN/SETPOINT DRIFTED HIGH/DRESSER INC
					YRI 019495 102477 H RM F00 1 N REGULATOR VALVE FAILED TO OPERATE CONTROL PRESSURE UNKNOWN / SETPOINT DRIFT / ADJUSTED VLV
					YRI 030141* 020180 H RM F16 U 3 T SI ACCUMULATOR N2 VLV SI-TV-604,605,606 DIDN'T OP. IMPROPER WIRING OF TIME DELAY RELAYS
					SI-PR59 VLV CONTROLLED PRESSURE TOO HIGH SETPOINT DRIFT OF REGULATING PILOT
					ZII 015162* 062376 H CV E00 2V N LEAKAGE THRU CHECK VALVES/ACCUMULATOR OVERFILL UNKNOWN/DARLING 10 INCH TYPE 10-C48Z
					ZII 016047A 091676 H AV C25 1 N NITROGEN VALVE (LHCV-S1943) LEAKED THRU LEAKING SEAT OF AD PLUG VALVE
					ZII 017154 012177 F MV A19 1 T CONTAINMENT SPRAY 1MOV-C50002 FAILED TO OPEN STEM STICKING DUE TO LUBRICATION PROBLEM
					COMMAND/AUX CONTACTS IN CTL CKT STUCK

ALL VALVE LERS USED

P Y E N T	L A C O N T R O L N U M B R E D A T E R H P E N T	C S C H A I F T O N D O U S P I L H U T Y	M O D E D E S C R I P T I O N	C A U S E D E S C R I P T I O N
W Z11 017223	012877 H MV A16 T	1 T	VALVE 1MOV-S188088 FAILED TO OPEN	COMMAND/AUX CONTACTS, CONTROL CKT, STUCK
W Z11 017251	012877 H MV A16 T	1 T	VALVE 1MOV-S18800C FAILED TO OPEN/COMMAND	AUX CONTACTS IN CONTROL CIRCUIT STUCK
W Z11 021337	042178 L MV A00	1 T	RHR 1MOV-87008 FAILED TO OPEN DURING TESTING	UNKNOWN/SOMETHING CAUSED THERMALS TO OPERATE
W Z11 021397	050378 F MV A19	1 T	CONTAINMENT SPRAY VALVE 1MOV-C50002 FAILED TO OPEN LACK OF LUBRICATION	
W Z11 031533	121580 L RM B16 S	1 T	RHR MINI FLOW VLVIFC-610A) WOULD NOT HAVE CLOSED FAILED MICRO SWITCH	
W Z12 014253	021376 H MV A16 T	1 T	28 SI PMP-SUC-VLV 2MOV-S18923B FAILED TO OPEN	DIRECT CONT.ON CKT,APKR,TO MTR,OPERATOR
W Z12 017661	051977 H MV A20	1 N	VALVE 2MOV-S188000 FAILED TO OPEN	LIMIT TORQUE MOTOR OPERATOR FAILURE
W Z12 018212	060477 L NV A16 S	1 T	RHR VALVE(2MOV-RH87008) FAILED TO OPEN DURING TEST COMMAND/AUX CONTACTS STUCK IN MCC	
W Z12 026750	071879 L MV A26	1 T	2MOV-S188011A FAILED TO STROKE OPEN/RECIRC FROM SUP TO RHR SUCTION). LIMIT SWITCH FAILURE	
W Z12 031245	042980 F MV A23	1 T	2A CONT SPRAY PUMP STOP VLV FAILED TO OPEN	FAILED TORQUE SWITCH
W Z12 031625	061880 X RV V06 U	2 N	IMPROPER VLV LINE UP MADE PURVS INOPERABLE	PROCEDURE CHANGED TO BLOCK THE VLV'S OPEN
G BF1 016053	092376 D RV V02 U	1 U	VALVE FOUND CLOSED TO PRESSURE SWITCH	PERSONNEL ERROR
G BF1 0175944	032177 L MV B08	1 T	VLV FCV 74-52 WOULD NOT GO COMPLETELY CLOSED	WORN BRNG,ASS,LOCKNUT,YOKEGNUT,GASKETS
G BF1 0175948	032177 L MV B20	1 I	VLV FCV 74-52 WOULD NOT CLOSE,MTR TRIP, THERMAL N.L. MOTOR SHAFT WAS BENT	
G BF1 017525	042177 W RV 827 R	1 N	MN-STM,SAFE+RELIEF VLV. FAILED TO RESEAT	SEVERE STM,CUTS ON PILOT DISC
G BF1 018126	050977 H MV A20	1 T	HPC1 TURB,STM,SUP,ISO,VLV. FCV 1-73-16 FAIL,T0 O/P BROKEN TEETH ON MTR PINION&CLUTCH GEAR	
G RF1 027620	101779 H MV A26	1 T	FCV-73-27 WOULD NOT OPEN-HPC1 INOPERABLE	DIRECT CONTACTS ON OPER. LIMIT SWITCH
G BF1 030712	031380 L MV B16 S	1 T	RHR INJECT VLV 74-67 FAILED TO CLOSE DURING TEST	LIMIT SH IN ISOLATION LOGIC FAILED
G BF1 032742	092480 L MV F20	1 N	RHR TORUS VLV FCV-74-71 FOUND TO BE INOPERABLE GROUNDED MOTOR(3.9HP,SMBZ,LIMIT TORQUE)	
G BF2 016199	100776 H XV V03 U	1 T	EQUALIZER VALVE ON FLOW INSTRUMENT FOUND OPEN	PERSONNEL ERROR
G BF2 016907	111676 H MV A23 R	1 T	HPC1 TURB,STM,SUP+ VLV 2-FCV-73-16 FAILED TO OPEN	TUR,SWT,GEAR ASS,PIN FOR VLV OPER,SHARER C
G BF2 020380	020578 W RV B00 R	1 N	RELIEF VALVE 2-1-41 OPENED AND FAILED TO RESEAT	CAUSE OF MALFUNCTION UNKNOWN
G BF2 020469	021378 W RV B00 R	1 N	RELIEF VALVE 2-1-5 OPENED AND FAILED TO RESEAT	CAUSE OF MALFUNCTION UNKNOWN
G BF2 021094	032578 H CY B04	1 M	CHECK VLV 2-73-603, IN HIGH-PRESS.CI, SYS, FOUND OPEN DIMEN. ERR. IN VLV. INTERFERENCE CLEARANCE	
G BF2 021782	062778 H XV V01 U	1 T	VALVE LEFT SHUT IN LUB OIL LINE TO HPCI PUMP	PERSONNEL ERROR IN VALVE LINE UP

ALL VALVE LERS USED

PLANT VENT	CONTROL NUMBER	EVENT DATE	SYSTEM COMP	MODE E	CAUSE C USE	TYPE T	FAIL EL	NUM M	ACTIVITY	MODE DESCRIPTION		CAUSE DESCRIPTION	
G BF2 025015	011379	H MV A26 R	1	T	HPCI INOPERABLE-FCV-73-16 FAILED TO OPEN							MECH FAILURE OF OPERATOR LIMIT SWITCH	
G BF2 032409	083080	L CV E00 R	1	T	CHECK VLV BETWEEN B&D HEAT EXCHANGERS LEAKING							NO CAUSE STATED "VALVE REPAIRED"	
G BF2 032703	09L180	H CV E10	1	T	HPCI CV 2-73-609 FAILED LOCAL LEAK RATE TEST							BUILDDUP OF RESIDUAL MATERIAL COCKED DISC	
G BF2 032705*	092980	W RV F00 R	5	T	5 MS RELIEF VLV'S FAILED TO ACTUATE AT PROPER PRESS							NO CAUSE STATED SET PRESS WAS RESET	
G BF3 016055	082476	H CV A00	1	T	CHECK VALVE IN HPCI TURB.EXH.LINE WAS BINDING							CAUSE OF CHECK VLV BINDING NOT STATED	
G BF3 018637	070577	H MV A23 R	1	T	HPCI TURB.STM.SUP. 3-FCV-73-16 FAILED TO OPEN							TOR.SWTH.GEAR ASS.SHEARED/CAUS.BVLD ON MT	
G BF3 020524	021378	L MV F12 R	1	T	VLV FCV 3-74-52 WAS FOUND INOPERABLE							UP.BRNG.LOCKNUT STRIPPED FROM NOR.POS	
G BF3 020923	041578	W RV B00 R	1	N	RELIEF 3-1-31 FAILED TO RESEAT AT PROPER PRESSURE							CAUSE OF MALFUNCTION IS NOT KNOWN	
G BF3 021245	042878	L MV F12 R	1	T	VLV FCV 3-74-52 WAS FOUND INOPERABLE							UP.BRNG.LOCKNUT STRIPPED FROM NOR.POSITIN	
G BF3 022126A	081778	W RV B00 R	1	N	A MAIN STM RELIEF VLV DID NOT CLOSE AFTER LIFTING							CAUSE OF FAILURE NOT GIVEN	
G BF3 030363	020580	L MV F26 R	1	T	RHR VLV FCV 74-73 FAILED TO OPERATE DURING TEST							LIMIT SW IN ACTUATOR ASSEMBLY FAILED	
G BF3 033640*	121080	W RV F00 R	8	T	8 MS RVS FAILED TO ACTUATE AT REQUIRED PRESS(TEST)							CAUSE NOT PRECISELY KNOWN(RESET ADJUSTMT)	
G BR1 016402	111976	L MV F16 U	1	N	RHR INJECTION VALVE(E11-F015A) FAILED TO OPERATE							UNDERSIZED BKR/DESIGN PROBLEM(ROOT)	
G BR1 016861	112176	H MV A20 R	1	T	E41-F001(HPCI STM.SUP.VLV) WOULD NOT OPEN							BRUSHES ON VLV MOTOR WERE STICKIN	
G BR1 017081	011977	H MV B20 R	1	T	HPCI STM.SUP.VLV E41-F003 WOULD NOT CLOSE							DIRTY COMMUTATOR IN VLV OPERATOR	
G BR1 017600	021077	D MV A16 S	1	N	CORE SPRAY VALVE FAILED TO OPEN AT REQUIRED PRESS							SETPOINT ON CONTROLLING INST DRIFTED HI	
G BR1 017290	030177	H MV B12	1	T	HPCI MIN. FLOW VLV E41-F012 FAILED TO CLOSE							ANTI-ROT. KEY SET SCREW HAD UNSCREWED	
G BR1 017330	030677	L MV A00	1	T	RHR PMP IN TORUS SUC.VLV E11-F004D WOULD NOT OPEN							CAUSE OF FAILURE UNKNOWN	
G BR1 018128	052077	H CV F04	1	T	HPCI STM.LIME EXH.CHECK VLV E41-F049 DETER.FAILED							VLV OSCIL.CAUSED DSC HINGE FAIL;IMP.DESGN	
G BR1 019387	102577	D MV C20	1	N	B CORE SPRAY LOOP FULL FLOW TST.VLV E21-F015B LEAK							VLV OPER. HAD STRIPPED OPERATING GARS	
G BR1 019677	110577	L MV A02 C	1	N	RHR VALVE E11-F004A FAILED TO OPEN(MOTOR PROBLEM)							PERSONNEL ERROR/COVER LEFT LOOSE/WATER LK	
G BR1 019824	120377	L MV B20	1	U	VALVE E11-F040 FAILED IN OPEN POSITION							MOTOR FOUND TO BE OPEN(UNDETERMINED WHY)	
G BR1 020771	031378	W RV B27 R	1	N	RELIEF VLV B21-F013F FAILED TO RESEAT AT REQ.PRESS							DEFECTIVE PILOT VLV/PILOT REPLACED	
G BR1 0220928	072878	L MV A16 T	1	U	VALVE F06BB FAILED TO OPEN							BLOWN FUSE	
G BR1 022092A	080278	L MV A16 T	1	U	VALVE F06BB FAILED TO OPEN							BLOWN FUSE/FOUND GRND WIRE IN LOGIC CKT	

ALL VALVE LERS USED

P L A N T	C O N T R O L E	S Y S T E M C O N D I P E	M O D E S U P P L I C E	C A U S T E R Y	F A U L T U R Y	H U M I T Y	A C T I V I T Y
MODE DESCRIPTION							
G BR1 022218	080878	H MV A00	1	N	HPCI FEED INJ VALVE E41-F006 FAILED TO OPEN AUTO		
G BR1 028036	121979	L MV V01 U	1	N	RHR TORUS SUCTION VALVE FOUND SHUT		UNKNOWN/TESTING COULDNT DUPLICATE FAILURE
G BR1 030407	021480	H XV V01 V	1	T	MANUAL ISOL VLV LOW SIDE OF 1E41LS15A FOUND CLOSED		OPERATOR ERROR-FORGOT TO OPEN VALVE
G BR1 030638	031480	H RM B16 S	1	T	HPCI TORUS SUCTION VLV E41-F041 FAILED TO CLOSE		PERSONNEL ERROR (WHEN UNDETERMINED)
G BR2 014647	020576	L XV V03 U	1	N	PRESS SW FOUND ISOLATED AFTER TESTING		RTGB CONTROL SW FAILED
G BR2 014618	031076	H RM A26	1	T	VALVE 2-E41-PV-1219D FAILED TO OPEN DURING TEST		PERSONNEL ERROR
G BR2 018697	071577	W RV B16 S	1	N	SAFETY REL.VLV B21-F0133 STUCK OPEN;AFTER MAN.OPEN GRND. ON SOLENOID ASS. FOR REMOTE ACTUATOR		LIMIT SW WAS OUT OF ADJUSTMENT
G BR2 019023*	090677	L MV C00	2	N	RHR TORUS COOL.RETRN.LN.ISOS.E11-F024B&2BB LEAKING VLV'S FAILED TO SEAT PROPERLY/UNKNOWN		CAUSE OF VLV NOT OPENING, NOT GIVEN
G BR2 020240	010478	H MV F26	1	T	CLOSING TIME ON E41-F002 EXCEED. TS LIMIT (HPCI)		DESIGN ERROR/VLV.DNEESN'T WORK ON LOW DP.
G BR2 020913	040378	L MV A20	1	N	SHUTDOWN COOL.DUTB.SUC.VLV E11-F008 WOULDNT OPEN		EXCESSIVE PILOT VALVE ASSEMBLY LEAKAGE
G BR2 021663	060378	L MV A00	1	N	RHR VLV E11-F009 WOULD NOT OPEN FROM CONTROL ROOM		PINION GEAR INSTALLED BACKWARD ON OP SHAFT
G BR2 023033	111178	L CV B04	1	N	RHR CHECK VALVE E11-F031 WILL NOT FULLY SEAT		COMMAND FAULT,RELAY FAILED IN LOGIC CKT
G BR2 023034	111278	L MV A16 U	1	N	RHR VLV E11-F008 WOULD NOT OPEN AT REQ. SETPOINT		PERSONNEL ERROR VLV WAS REQ OPEN
G BR2 025638A	032079	W RV A27 R	2	T	2B21-F013H6013B SET POINTS FOUND DRIFTED HIGH		BROKEN WIRE IN SOLENOID COIL(COMMAND FLT)
G BR2 026626	071779	W RV F27	1	N	SAFETY RELIEF VALVE F013E LIFTED & RESET-SPURIOUS		--FULLY,REVERSE LEAKAGE/NO DETAILS GIVEN
G BR2 026521	072179	H MV F20	1	T	HPCI STEAM ISOLATION VALVE F001 INOPERABLE		SHEARED WOODRUFF KEY.IN MTR.OPERATOR
G BR2 030412	021480	L RM A16 S	1	N	VLV E11-F049 FROM RHR TO RADWASTE FAILED TO OPEN		CRACK IN BELLows TO BASE WELD
G BR2 0324548	090780	H CV V01 U	1	T	HPCI MANUAL STOP CHECK FOUND LOCKED CLOSED		TRIPPER PIN IN OPERATOR DISLODGED
G BR2 032662	091080	A RV A16 S	1	T	ADS RV 2-B21-F013E FAILED TO ACTUATE AS REQUIRED		INCORRECT MAINTENANCE PROCEDURE
G BR2 033238	111280	L CV E00	1	N	2B RHR PUMP DISCHRG CHECK VLV FAILED TO RESEAT		THE REPAIR CLUTCH AND COMPONENTS FAILED
G CO1 014359	012476	L MV F20 R	1	N	VLV RHR-MD-34A WOULD NOT OPERATE BY MTR.OPERATOR		
G CO1 014936	051476	W RV A27	1	M	MAIN STEAM SAFETY RELIEF VALVE MALFUNCTIONING		
G CO1 015717	081076	D MV F20	1	T	VALVE CS-MD-12B WOULD NOT OPERATE		
G CO1 015873	081376	W RV A02 C	1	R	SETPOINT OF MS-RV-71E ADJUSTED INCORRECTLY		
G CO1 016008	090776	D MV A20	1	T	VALVE CNS-MV-12B FAILED TO OPEN		

ALL VALVE LERS USED

ALL VALVE LEVERS USED

P E N T C O N T R O L N U M B R A H E V E N T D A T E		S Y S T E M C O N T R O L N U M B R A H E V E N T D A T E		C A T A G I F A U T I M Y D E S P I L H W Y		M O D E D E S C R I P T I O N		C A U S E D E S C R I P T I O N		C A U S E D E S C R I P T I O N	
										C A U S E D E S C R I P T I O N	
G	DAI 033106	111080 A	RV 827	1	N	RELIEF VLV PSV-4405 FAILED TO CLOSE/SCRAMMED PLANT	PILOT VLV PROBLEM OF UNKNOWN NATURE				
G	DRZ 014330	031376 H	RM A16 S	1	T	HPCI STEAM SUPPLY VALVE 2-2301-4 FAILED TO OPEN	DIRTY CONTACTS IN BREAKER SUPPLYING VALVE				
G	DRZ 014420	032976 H	CV E25	1	T	HPCI VALVE 2-2301-45 LEAKING INTERNALLY	CORROSION, PITTING OF LOWER SEATING AREA				
G	DRZ 014747	052576 A	RV 827	1	T	DURING BLOWDOWN TEST VALVE 203-3A REMAINED OPEN	EXCESS LEAKAGE ON PILOT STAGE OF VALVE				
G	DRZ 015168	061076 D	RM B19 R	1	T	VALVE M02-1402-4D FAILED TO CLOSE AGAINST PUMP HED	INADQUATE LUBRICATION OF VALVE STEM				
G	DRZ 015378	071176 D	MV F26	1	T	CORE SPRAY INJECTION VAL M02-1402-24B FAILED	BROKEN LIMIT SWITCH CONTACT BLOCK				
G	DRZ 016153	111376 H	MV F12 R	1	T	HPCI INJECTION VALVE M02-2301-8 FAILED	VALVE STEM SHEARED				
G	DRZ 017182	021777 L	MV A26	1	T	LPCI CROSS-TIE VALVE M02-1501-32B FAILED TO OPEN	LIMIT SWITCH OPENED BEFORE VALVE OFF SEAT				
G	DRZ 018508	080277 H	MV A23 R	1	T	HPCI VALVE 2-2301-8 FAILED TO OPEN	SUSPECT PROBLEM WITH TORQUE SWITCH				
G	DRZ 018934	081577 L	MV A00	1	T	SUCTION VALVE M0-2-1501-5A FAILED TO OPEN	CAUSE UNKNOWN				
G	DRZ 018935	091677 H	MV A04	1	T	HPCI VALVE 2-2301-8 FAILED TO OPEN, VAL DAMAGED	OVER SIZED MTR OPERATORS OVERSTRESS STEM				
G	DRZ 019945	120977 W	RV A00 R	1	T	ELECTROMATIC RELIEF VALVE 3B FAILED TO OPEN	CAUSE UNKNOWN				
G	DRZ 021158	042878 L	XV VOL U	2	N	VALVES IN LPC1 & CORE SPRAY LINED UP IMPROPERLY	OPERATING PERSONNEL ERROR				
G	DRZ 022776	101378 D	RM B19 R	1	T	THE 2-1402-48 FLOW TEST VALVE FAILED TO CLOSE	VALVE STEM NOT ADEQUATELY LUBRICATED				
G	DRZ 022775	101878 L	RM B19	1	T	LPCI SUCTION VALVE M0-1501-9C FAILED TO CLOSE	VALVE STEM NOT ADEQUATELY LUBRICATED				
G	DRZ 025246	011179 L	MV B20	1	T	LPCI FLOW TEST VALVE FAILED TO CLOSE WHEN ACTUATED	BROKEN PINION GEAR ON UP MOTOR SHAFT				
G	DRZ 025248	012679 L	MV B00	1	T	LPCI MIN FLOW VALVE FAILED TO CLOSE COMPLETELY	CAUSE UNKNOWN				
G	DRZ 031264	051280 H	RM B14	1	N	HPCI ISOL VLV FAILED TO CLOSE	STEAM CAUSED PACKING TO SWELL (PERSONNEL P)				
G	DRZ 032749	101180 H	MV A23 R	1	N	HPCI STEAM SUPPLY VLV FAILED TO OPEN	TORQUE SW CONTACTS STUCK OPEN REPLACED				
G	DRZ 033323	112480 A	RV F00	1	N	2A SAFETY RV VLV NOT OPERABLE IN SAFETY MODE	CAUSE UNKNOWN AT THIS TIME				
G	DRZ 016550	051076 D	MV B16 U	1	T	M0 3-1402-25B TRIPPED WHILE BEING CLOSED	WRONG SIZE OVERLOAD HEATER				
G	DRZ 016163	100776 L	CV E10	1	T	ISOLATION CHECK VALVE 3-1501-25B LEAKING INTERNALLY	DIRT AND SMALL SCRATCHES ON VALVE SEAT				
G	DRZ 016695	101276 L	MV A16 S	1	T	VALVE 3-1501-2A FAILED TO OPEN ELECTRICALLY	LOOSE TERMINAL IN VALVE CONTROL CIRCUIT				
G	DRZ 016454	110176 L	CV E10	1	T	ISOLATION CHECK VALVE 3-205-2-7 LEAKING INTERNALLY	DIRT IN SEATING AREA & ON DISK PIVOT PIN				
G	DRZ 016474	111976 H	MV F16 S	2	V	HPCI VLV FAILED TO OPERATE (CYCLING)	DESIGN ERROR IN LOGIC CIRCUIT				

ALL VALVE LERS USED

P L A N T	V E N T	C O N T R O L U M B E R	E V E N T D A T E	S Y S T E M	C O M P E E	M O D E	T Y P E	F A I L U M Y	A C T I V I T Y	MODE DESCRIPTION	CAUSE DESCRIPTION
G DR3	018378A	061177	W RV C02	B	1	N	ELECTROMATIC RELIEF VALVE	203-3D	LEAKING INTERNALY	PILOT PIN ADJUSTED INCORRECTLY	
G DR3	018378B	061177	W RV C10	R	1	N	ELECTROMATIC RELIEF VALVE	203-3E	LEAKING INTERNALY	DIRT UNDER VALVE SEAT	
G DR3	018377	061277	W RV C27	X	1	T	ELECTROMATIC RELIEF VALVE	203-3D	LEAKING INTERNALY	DEFECTIVE PILOT VALVE STEM	
G DR3	018376	061377	W RV A10	R	1	T	SOLENOID OPERATING LEVER FOR	203-3C	STICKING	RUST BUILDUP ON GUIDE PINS	
G DR3	018936	081177	L MV A19		1	N	VALVE MO-3-1501-208	FAILED TO OPEN		VALVE STEM NOT ADEQUATELY LUBRICATED	
G DR3	019996	121677	L MV A00	R	1	N	LPCI HX DISCH VALVE	MO3-1501-3A	FAILED TO OPEN	CAUSE UNKNOWN	
G DR3	020602	020778	L MV A00	R	1	T	VALVE MO-3-1501-5C	FAILED TO OPEN		CAUSE UNKNOWN	
G DR3	021679	060678	F MV F23		1	N	VALVE MO3-1501-288	FAILED WHILE BEING CYCLED		DEFECTIVE SHAFT PIN ON TORQUE SWITCH	
G DR3	022561	092278	L MV B16	S	1	T	LPCI VALVE	3-1501-20A	FAILED TO CLOSE ON TESTING	STUCK CONTACTOR IN MCC	
G DR3	022591	092278	L MV F00		1	N	LPCI HX VALVE	MO3-1501-3A	FAILED TO OPERATE	CAUSE UNKNOWN	
G DR3	027260	092379	L MV A16	S	1	T	LPCI MOV	3-1501-3A	WOULD NOT OPEN REMOTELY	SLIDEWIRE ON POSITION CONTROLLER GOT OFF	
G DR3	030246	012280	L MV B16	S	1	T	LPCI VLV	MO-3-1501-11B	FAILED TO CLOSE	PROBLEMS WITH VLVS SUPPLY BREAKER	
G DR3	030528	030680	L MH A16	S	1	T	LPCI VLV	MO-3-1501-22A	FAILED TO OPEN DURING TEST	LOOSE WIRE IN MCC SUPPLYING PWR TO VLV	
G DR3	030878	040280	H MV C25		1	T	HPCI SUCTION VLV	MO-3-2301-35	FOUND LEAKING THRU	NORMAL SEAT DISC DETERIORATION	
G DR3	030967A	042580	A RV A12	R	1	N	3A TARGET ROCK ADS RELIEF	FAILED TO OPEN		AIR ACTUATOR IMPROPERLY BOLTED TO VLV	
G DR3	030967B	042580	A RV A27	R	3	N	3B,3C,3E ADS ELECTROMATIC RELIEFS	FAILED TO OPEN		VARIOUS PILOT VALVE PROBLEMS	
G DR3	033668	121980	F MV B16	S	1	N	DRYWELL SPRAY HEADER ISO.VLV	WOULD NOT CLOSE		STUCK PLUNG.ON CLOS.COIL OF VLV MOTOR BRK	
G DR3	033713	122380	L RM B16	S	1	T	SHUTDOWN COOL.SYS.INBOARD ISO.VLV	DID NOT CLOSE		PROBLEMS IN VLV CONTROL CIRCUITRY	
G EN1	014785	040776	L MV F20		1	M	VALVE E11-F047A	FAILED TO OPERATE ELECTRICALLY		A MOTOR WINDING FAILURE OCCURRED	
G EN1	014792	050176	H MV A26	R	1	N	HPCI DISCHARGE VALVE	E41-F006	FAILED TO OPEN	FAILURE OF A SNAP LOCK LIMIT SWITCH	
G EN1	015555	061576	H MV A00	R	1	N	HPCI VALVE	E41-F006	DID NOT FULLY OPEN	CAUSE UNKNOWN	
G EN1	015564	072076	L RM G16	S	1	T	RHR FLOW VALVE	E11-F007B	FAILED TO STAY OPEN	DEFECTIVE SWITCH SUPPLYING SIGNAL TO VALV	
G EN1	016841	120976	A RV B00	R	1	T	RELIEF VALVE	WOULD NOT RESEAT		CAUSE UNKNOWN	
G EN1	017110	010977	A RV B27	R	1	N	RELIEF VALVE	B21-F013G	OPENED AND STUCK OPEN	GROSS LEAKAGE OF PILOT+2ND STAGE ASSEMBLY	
G EN1	017096	011777	L XV V03	U	1	U	PRESS SW	FOUND VALVED OUT WHEN REQUIRED OPEN		PERSONNEL ERROR	

ALL VALVE LERS USED

PLANT EVENT NUMBER	CONTROL NUMBER	EVENT DATE	S Y S T E M P	C O M M O D E	C A U S E	T Y P E	F A I L U R Y	ACTIVITY	MODE DESCRIPTION		CAUSE DESCRIPTION	
G EN1 017189	020177	A RV 800 F	1	N	RELIEF VALVE B21-F013G OPENED AND STUCK OPEN				CAUSE UNKNOWN,VALVE TO BE TESTED			
G EN1 018191	060477	L RM F02 C	1	T	LPCI VALVE E11-F017B CYCLE TIME OUTSIDE T.S.				VALVE STEM PACKED TOO TIGHTLY/PERSONNEL			
G EN1 018649	080977	W RV A00	1	N	SAFETY RV 1C FAILED TO OPEN AT HIGH REACTOR PRESS.				CAUSE UNKNOWN			
G EN1 020019*	100677	A RV A00 R	4	N	FOUR RELIEF VALVES FAILED TO OPEN FOLLOWING SCRAM				CAUSE UNKNOWN,VALVES BEING EXAMINED			
G EN1 021723*	060978	A RV A12 R	2	T	TWO RELIEF VALVES FAILED BENCH CHECK				PROBLEMS WITH PLUNGERS AND SPRINGS			
G EN1 022113	070278	L MV A16 S	1	T	RHR MOV E11-F024A FAILED TO OPEN				DIRT IN INTERLOCK OM BREAKER CAUSED BIND			
G EN1 025019	011979	H MV F20	1	T	HPCI INJECTION VALVE FAILED TO OPERATE				MOTOR BURNED UP			
G EN1 026631	072679	L MV F16 U	1	M	RHR OUTBOARD ISOLATION VALVE MADE INOPERABLE				NO PWR AVAILABLE TO VLV (PERSONNEL ERROR)			
G EN1 030031	010580	L MV F00 R	1	T	RHR VLV 1E11-F008 FAILED TO OPERATE IN REQ TIME				CAUSE UNKNOWN AT PRESENT			
G EN1 030954	042580	L MV C00 R	1	T	MOV E11-F015A STARTED LEAKING THRU AFTER TESTING				NO CAUSE STATED			
G EN1 031143	042980	L MV A20 R	1	T	MOV 1E11-F016A FAILED TO OPEN DURING TEST				KEY BETWEEN MOTOR SHAFT AND PINION FAILED			
G EN1 031157	051080	L XV V03 U	2	N	TWO COOLING WTR VLV'S TO PUMPS A & B FOUND CLOSED				PERSONNEL ERROR			
G EN1 031267	052480	L MV C00	1	R	RHR INJECTION VLV LEAKING THRU				NO CAUSE STATED			
G EN1 031281	052580	L MV A16 S	1	T	RHR VALVE 1E11-F006B FAILED TO OPEN				FAULTY AUX CONTACT BLOCK (COMMAND FAULT)			
G EN1 031521	062280	L XV V01 U	2	T	RHR MIN FLOW VLV E11-F018B & D FOUND CLOSED				PERSONNEL ERROR			
G EN1 031769A	071180	L XV V01 U	2L	N	COOLING WATER VLV SECURED WHEN REQUIRED OPEN				PERSONNEL ERROR			
G EN1 031769B	071180	L MV F16 S	1	N	LPCI INJECTION VLV LOST POWER (INVERTER OVERHEATED)				LOSS OF POWER(PERSONNEL SEE 31769A)			
G EN1 032190	080880	L MV A20	1	T	RHR VLV 1E11-F015A FAILED TO OPEN ON TEST				MOTOR WINDINGS AND ROTOR FOUND BURNED			
G EN1 032667	091980	H RM B16 S	1	T	HPCI MIN FLOW VLV 1E41-F012 FAILED TO CLOSE (TEST)				NO PWR TO VLV. CONTACTOR WAS BINDING			
G EN1 033579	121280	L RM C25 R	1	N	RHR VLV 1E11-F0158 LEAKING THRU				SEAT GALLED,DISC CRACKED			
G EN2 022024*	071778	L MV F16 U	2V	N	RHR VALVES HAD POWER LOST TO THEM				BREAKER TRIPPED DUE TO BLOWN FUSES			
G EN2 022500*	091078	L RM B04	2	N	RHR VALVES 2E11-F003A,F047A FAILED TO CLOSE				VALVE GATES SAG+BIND IN FULL OPEN POSIT			
G EN2 022486*	092678	L RM F12	2	T	RESTRICTED FLOW THROUGH RHR SYSTEM CONTROL VALVES				DAMAGED CAVITROL TRIMS IN VALVES			
G EN2 022675	102778	H MV F20	1	T	HPCI VALVE 2E41-F001 FAILED TO OPERATE				FAILURE OF MOTOR SHUNT FIELD INSULATION			
G EN2 022753*	110678	H RM F16 U	2V	T	HPCI CONTROL VALVES FAILED TO OPERATE				WIRE LEFT OFF BY MAINT PERSONNEL			

ALL VALVE LEWS USED

P L Y E N T	A C T U A T I V E	S Y C H A U F T H O O D S P I A N T H P E E S E L H	C O N T R O L N U M B R E	E V E N T D A T E	M O D E D E S C R I P T I O N	C A U S E D E S C R I P T I O N
G EN2 025467*	021479	W RV A27	2 R	2 SAFETY RELIEF VALVES FAILED TO OPEN AS REQUIRED	SCUFFING OF PILOT DISCS AND SEATS	
G EN2 025875*	050879	W RV F05 C	3 M	AIR OPERATORS FOR THREE SRV'S IMPROPERLY INSTALLED	IMPROPERLY INSTALLED BY WYLE LAB	
G EN2 026148	060979	H MV F20	1 T	HPCI SUCTION VALVE EXCEEDED OPERATING TIME	LOOSE CONNECTION IN SHUNT FIELD CIRCUIT	
G EN2 026422	070779	H MV F16 S	1 T	HPCI STEAM SUPPLY ISOLATION VALVE FAILED TO OPERATE	MOTOR OPERATED 12 TIMES IN 5 HRS	
G EN2 026639	073079	H MV B20 R	1 N	HPCI SUCT FROM SUPP CHAMBER FAILED TO CLOSE	BURNED MOTOR-PINION KEY HAD SLIPPED ON SW	
G EN2 027321	101579	H MV A20 R	1 T	HPCI SUCT FROM SUPP CHAMBER FAILED TO OPEN	MOTOR WINDING FAILURE	
G EN2 030178	013080	H RM B16 T	1 T	HPCI MIN FLOW VLV 2E41-F012 FAILED TO CLOSE	FAILED FLOW SW CONTROLLING VLV	
G EN2 030975	042180	H RM F16 T	1 T	MIN FLOW CONT VLV 2E41-F012 FAILED TO OPERATE	FLOW SW PROVIDING SIGNAL TO VLV FAILED	
G EN2 033764	050780	L MV B20 C	1 T	2E41-F006 INBOARD ISO-VLV FAILED TO CLOSE	WATER SHORTED OUT MOTOR OPERATOR WINDINGS	
G EN2 031318*	051480	L MV F26 C	2 N	RHR VLV 2E11-F0040 & F0060 FAILED TO OPERATE	LOOSE & BROKEN LIMIT SWITCHES	
G EN2 031431A	053080	L MV A20 S	2 T	TORUS SUCTION VLV 2E41-F01642 FAILED TO OPEN	VALVE MOTORS SHORTED OUT (STEAM LEAK)	
G EN2 031555	060480	H RM A16 S	1 N	HPCI VLV 2E41-F003 COULD NOT BE OPENED	LOGIC CKT FAILED TO RESET	
G EN2 031842	071180	H MV A20 R	1 N	HPCI INJ VLV 2E41-F006 FAILED TO OPEN	MOTOR WINDING FAILURE, POSS. EXCEED-DUTY CY	
G EN2 032135	072480	H RM F16 U	1 N	HPCI VLV 2E41-F002 CLOSED WHEN REQUIRED OPEN	INADEQUATE SIGNAL, OPERATOR BUMPED RELAY	
G EN2 033210A	110480	L RM B23	1 T	2E11-F007A(RHR MINIMUM FLOW VLV) LEAKED DUE TO NOT BREING CLOSED.	TORQUE SWITCHES ADJUSTED	
G EN2 033426A	12680	A RV F27 R	0 T	OUT OF THE VLVS 2821-5013A-M, 8 VLVs FAILED	PILOT SEAT LEAKAGE	
G EN2 033426R	112680	A RV A00 R	7 T	OUT OF THE VLVS 2821-5013A-M, 7 VLVs SET PRESSURE W AS TOO HIGH/ CAUSE UNKNOWN	CAUSE UNKNOWN	
G EN2 033508	120980	F CV E00 R	1 T	VENT PURGE OUTLET ISO VLV 2T48-F318 LEAKED	SHORT IN OPERATOR MOTOR	
G FPI 015058	042076	H MV A20	1 T	HPCI TORUS SUCTION VALVE FAILED TO OPEN	SUSPECT OPEN CIRCUIT IN MOTOR WINDINGS	
G FPI 015237	070376	L MV A20	1 T	RHR VALVE 10 MOV 25A FAILED TO OPEN	"NORMAL WEAR ON VALVE SEAT	
G FPI 046176	101476	L CV E25	1 N	CHECK VALVE 42B LEAKING INTERNALLY	VALVE MOTOR OPERATOR BURNED OUT	
G FPI 0166269	102676	L MV A20	1 T	RHR SYSTEM VALVE 10-MOV-2A WOULD NOT OPEN	FAILURE OF VALVE MOTOR WINDINGS	
G FPI 016497	111976	H MV A20	1 N	HPCI VALVE 23-MOV-57 FAILED TO OPEN	CAUSE UNKNOWN	
G FPI 017956	061177	H MV A00	1 T	VALVE 23 MOV 58 FAILED TO OPEN ON TEST SIGNAL	LOW TORQUE SWITCH SETTING	
G FPI 021142	100477	L MV A23	1 T	L PCI MOV 25A FAILED TO OPEN ON TEST		

ALL VALVE LERS USED

P V E N T	PLAN NUMBER	CONTROL EVENT DATE	S Y S T E M P M O D E E S S U P L I Y	C C A U S E F A I L H U I T Y	A C T T W I T H	MODE DESCRIPTION	CAUSE DESCRIPTION
G FPI 019310	100877 H MV B23	1	T	HPCI STEAM ISOL VALVE FAILED TO CLOSE ELECTRICALLY	TORQUE SWITCH NEEDED ADJUSTMENT		
G FPI 020570	030278 L CV 800	1	N	A RHR PUMP CHECK VALVE STUCK OPEN	CAUSE UNKNOWN		
G FPI 021022	040678 L MV A16 S	1	N	RHR ISOLATION VALVE 10MOV18 INOPERABLE (CLOSED)	CONTROLLER AUXILIARY CONTACT FAILURE		
G FPI 021023	040878 H MV F12	1	T	VALVE 23MOV14 SEPERATED FROM OPERATOR	FAILURE OF MECHANICAL FASTENERS		
G FPI 021225	042978 H MV A23	1	N	HPCI 23-MOV-15 WOULD NOT OPEN	TORQUE SWITCH WAS RESET		
G FPI 021227	050878 D MV F02 C	1	M	POWER REMOVED FROM CORE SPRAY VALVE MOTOR	PERSONNEL ERROR		
G FPI 021712	062978 H MV B16 S	1	T	HPCI VALVE 23-MOV-15 FAILED TO CLOSE	DEFECTIVE TEMP SWITCH(NO SIGNAL TO CLOSE)		
G FPI 021924	072278 D MV B20	1	T	OUTBOARD INJECTION VALVE 14-MOV-11B FAILED TO CLOS	OPERATOR SHAFT KEY SHEARED		
G FPI 022329	090378 D MV A04	1	T	CORE SPRAY INJECTION VALVE 14-MOV-12B FAIL TO OPEN	DESIGN ERROR, DIFFERENTIAL PRESS.TOO HIGH		
G FPI 023358	122478 L CV 800	1	N	RHR LOOP CHECK VALVE FAILED TO CLOSE	NO REASON FOUND FOR STICKING,REASSEMBLED		
G FPI 026344	062779 L MV A23	1	T	B LOOP LPCI INJECTION VALVE DID NOT OPEN	TORQUE SWITCH FAILURE		
G FPI 026343	063079 L CV F25	1	T	REVERSE ROTATION OF RHR PUMP WAS NOTED DURING TEST	DISCH CHECK VALVE DISC NOT ATTACHED		
G FPI 027006	090679 H MV A20	1	T	HPCI CONDENSATE STORAGE TANK SUCTION VALVE FAILED	MOTOR FAILURE		
G FPI 027872	122179 D MV A20	1	T	CS ISOLATION VALVE WOULD NOT REOPEN AFTER CLOSURE	MOTOR PINION GEAR LOOSE ON SHAFT		
G FPI 030081	010880 D MV F00	1	R	CORE SPRAY INJ VLV FAILED TO OPERATE PROPERLY	CAUSE NOT KNOWN		
G FPI 033799	010980 D MV A02	1	T	CORE SPRAY INJ VLV 14-MOV-12B FAILED TO OPEN	PERSONNEL ERROR IN ADJ LIMIT & TORQUE SW		
G FPI 030974	041080 H MV B20	1	T	HPCI MIN FLOW VLV FAILED TO CLOSE	COCKED BRUSH HOLDER ON DRIVE MOTOR		
G FPI 031016	041580 L MV A26	1	N	RHR VLV 10-MOV-67 FAILED TO OPEN	TORQUE BYPASS LIMIT SW SET IMPROPERLY		
G FPI 032007	041880 L MV B07	1	T	RHR VLV 10-MOV-67 FAILED TO FULLY CLOSE	"NORMAL WEAR & TEAR",SEAT,DISC,PACKING		
G FPI 032919	101180 L MV B02	1	N	CONT ISOL VLV 10-MOV-57 FAILED TO CLOSE	PERSONNEL ACCIDENTALLY DISENGAGED CLUTCH		
G FPI 033415	120880 H MV F23	1	T	HPCI STEAM SUPPLY VALVE FAILED TO OPERATE	TORQUE SWITCH FAILURE		
G MII 014290	021276 U AV F24 T	1	N	1 OF 2 FEEDWTR.REG.VLVs LOCK IN THE AS IS POSITION	FAILURE IN 3 WAY PRESSURE REGULATOR		
G MII 016689	121876 L MV B23	1	T	CONDENSATE RETURN VAL 1-IC-4 FAILED TO CLOSE	TORQUE SW SET INCORRECTLY		
G MII 018156	061877 W RV C27	1	N	RV DISCH TEMP HIGH/VLV LEAKING STM INTERNALLY	COLLAPSED FILTER,STM CUTTING OF PLT SEATS		
G MII 018414	071377 U AV F24 T	1	U	"B" FEEDWTR.REG.VLV EXPERIENCED CONTROL PROBLEMS	FAILURE CAUSED BY DIA.FAIL.IN SUP.SYS.VLV		

ALL VALVE LERS USED

P L A N T	C O N T R O L N U M B E R	E V E N T D A T E	S Y S T E M C O M P E E R	C A U G E E E L	T Y P E I P L	F A N U N I T Y	A C T I V I T Y	MODE DESCRIPTION	CAUSE DESCRIPTION
G MII 018625*	080677 U AV F24 T	2V N	FEEDWTR.REG.VLV5.	LOCKED UP WAS ISM				LOSS OF INSTRUMENT AIR PRESS.CAUSED FAIL.	
G MII 019326	101277 F RM A00	1 N	TORUS SPRAY VLV FAILED TO OPEN ON SIGNAL					CAUSE OF OCCURRENCE IS UNKNOWN	
G MII 0206988	031078 K RV C27 R	1 T	RELIEF VALVE LEAKING THROUGH					LEAKAGE IN PILOT VALVE / STEAM CUT	
G MII 0207228	032078 U CV E00	4 T	FEED WTR.CK.(1-FW-9A,9B,10A,10B)LEAK,EXCESS OF T.S					CAUSE OF LEAKAGE NOT GIVEN	
G MII 025313	022679 W RV B27 R	1 N	SRV LIFTED PREMATURELY & FAILED TO RESEAT					PILOT DISC STEAM CUT	
G MII 027674	111579 L MV F16 S	1 T	LPCI INBOARD ISOLATION VALVE INOPERABLE					ELECTRICAL FAILURE IN MOTOR CONTROLLER	
G MII 030473A	022080 D RM C25 R	1 N	CORE SPRAY INJ VALVE LEAKING THRU					SEAT PROBLEM	
G MII 030473B	022080 D CV E25 R	1 N	CORE SPRAY CHECK VLV LEAKING THRU					SEAT PROBLEM	
G MO1 015026	060376 H MV B23	1 T	HPCI STM LINE ISO VAL FAILED TO CLOSE					TORQUE SW SETTING DRIFTED TOO LOW	
G MO1 015100	061476 K RV A24 S	1 T	SAFETY RELIEF VLV Z-71A FAILED TO ACTUATE					AIR LEAK IN AIR SUPPLY SYSTEM	
G MO1 015708	090276 F MV B12 R	1 N	VALVE MO-2008 FAILED TO OPEN					STEM CLAMP SET SCREWS SHEARED	
G MO1 018094	053077 L MV A16 T	1 T	"B" RHR INJECTION VALVE FAILED TO OPEN (MO-2013)					CONTACTOR IN CONT.CIRCUITRY DID NOT CLOSE	
G MO1 018955	082877 L MV A16 T	1 T	"B" RHR INJECTION VALVE FAILED TO OPEN (MO-2013)					CONTACTOR IN CONT.CIRCUITRY DID NOT CLOSE	
G MO1 019050	090977 F MV F04 R	1 N	VALVE MO 2009 FAILED TO OPERATE PROPERLY					SET CLAMP SCREWS UNDERSIZED	
G MO1 019158	092377 F MV F12 R	1 M	VALVE MO-2008 FOUND FAILED DURING MAINTENANCE					SEAT RING THREADS STRIPPED	
G MO1 022808	102078 H CV E10 R	1 T	HPCI-9 TURB EXT LINE CHECK VALVE LEAKING INTERNALLY					ACCUMULATED DIRT ON SEATING SURFACES	
G MO1 023389	112178 L MV F16 S	1 N	MO-2014 LPCI "A" ADMISSION VALVE INOPERABLE					BLOWN FUSE IN CONTROL POWER CIRCUIT	
G MO1 023390	112478 H XV C25	1 N	HPCI DRAIN VALVE CV-2043 LEAKING THRU INTERNALLY					INTERNAL PARTS NEED REPLACEMENT	
G MO1 025804	031579 W RV F08	1 T	OPENING DELAY TIME OF "A" SRV IN EXCESS OF ASSUMED					PROCEDURE DID NOT HAVE INSULATION INSPEC	
G MO1 026492	070879 L MV A26	1 N	TORUS COOLING INJECTION VLV MOTOR OPERATOR FAILED					LIMIT SWITCH DID NOT DEENERGIZE MOTOR	
G MO1 030707	022380 H CV E25 R	1 T	ANCHOR 16-INCH SWING CHECK VLV LEAKING THRU(TEST)					LOOSE SEAT RING	
G MO1 032221	072980 H MV F20	1 T	HPCI STEAM SUPPLY VLV FAILED TO OPERATE					FAILED MOTOR WINDINGS	
G HM1 014666	051576 L MV A20	1 M	SHUTDOWN COOL SYST ISO VALVE 38-02 FAIL TO OPEN					OPEN MOTOR WINDINGS	
G HM1 017401*	030977 A RV A16 S	3 N	3 OUT OF 6 ADS RELIEF VLV'S WOULD NOT HAVE OPERATE-					-0 IF NEEDED//RESET SWITCH FAILURE	
G HM1 018299	063077 H RM F16 S	1 T	NO.12 INLET INSIDE IV-B(40-01)FAIL TO OPERATE					FAILURE OF ELECT CONTACTOR (CLOSING)	

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ALL VALUE IS USED

ALL VALVE LENS USED

P V E N T	PLAN CONTROL NUMBER	EVENT DATE	S Y S T E M C O M P E E S U P E L I M U N I T	C A U S T F A N I V I T Y	MODE DESCRIPTION	CAUSE DESCRIPTION
G PB3 014032	010576	D MV A16 S	1 N	MD-3-14-12B18 CORE SPR,LP,INJ,VLV	FAILED TO OPEN	PROBLEM WITH MAGNET,TRIP DEVICE MTR, BRKR
G PB3 014033	010776	H CV E25	1 T	HPCI EXHAUST LINE CHECK VLV 23-65-EXCESSIVE LEAK.	LEAK.	POOR MATING BETWEEN FLAPPER & SEATING SUR
G PB3 014035	010776	H AV C25	1 T	HPCI EXHAUST LINE DRAIN VLV AD-5248	-EXCESS.LEAK.	POOR MATING BETWEEN PLUG & SEATING SURF.
G PB3 014475	021776	L MV A16 S	1 U	RHR INJ. VLV MO-10-25A	FAILED TO FULLY OPEN	BROKEN WIRE TO OPENING TORQUE SWITCH
G PB3 014471	030176	L MV B12 R	1 N	B RHR OUTBOARD INJECTION VLV MO-1548	FAIL TO CLOSE	VLV DISC SEPARATED FROM VLV STEM
G PB3 015153	071276	W RV B27 R	1 N	718 MAIN STEAM RELIEF VALVE	FAILED OPEN	FAILURE DUE TO PILOT VLV SEAT LEAKAGE
G PB3 015228	072076	W RV B27 R	1 N	MAIN STEAM RELIEF VLV 71G	FAILED OPEN	FAILURE DUE TO PILOT VLV SEAT LEAKAGE
G PB3 016476	112376	D MV B23	1 T	CORE SPR,B FULL FL,TST,RET,VLV	FAILED TO CLOSE	TORQUE SWITCH SETTING WAS TOO LOW
G PB3 018884	090277	H MV A09	1 T	HPCI SYS.VLV MO-3-23-41	FAILED TO FULLY OPEN	CORRODED VLV STEM DUE TO VLV PACKING LEAK
G PB3 023062	111678	L MV A20 R	1 T	RHR VALVE MO1548	FAILED TO OPEN ON TESTING	MOTOR & SEVERAL OPERATOR PARTS REPLACED
G PB3 026763	010879	L MV F00	1 N	VALVE OPERATOR FAILURE ON MO16A	CAUSED LOSS OF RHR NO CAUSE GIVEN, RELEASE RATE EXCEEDED	
G PB3 025311	022579	W RV F16 S	1 N	RELIEF VALVE RV-71L	FAILED TO OPERATE	FUSES BLOWN, SHORT TO GROUND
G PB3 031104	042180	L MV A05 B	1 T	LPCI VLV MO-3-10-25B	FAILED TO OPEN ON TEST	VALWORTH 23-INCH IMPROPER INTERNAL CLEARK
G PB3 031740	060880	F MV B05 C	1 T	CONT SPRAY VLV MO-3-10-26B	FAILED TO CLOSE	STEM LOCKING HUY NOT STAKED BACKED OUT
G PB3 032270	080680	L MV A17	1 T	LPCI VLV MO-3-10-25A	FAILED TO OPEN DURING TEST	THRUST BEARING IN LIMITORQUE OPER FAILED
G PB3 033292	112480	H RM F23	1 T	HPCI VLV MO-3-23-1	KEPT DRIVING CLOSED ONCE AND //	FAILED TO CLOSE ANOTHER TIME. TORQUE SW.
G PII 017674	051077	W RV A24 S	1 N	RV 203-3C	DID NOT OPEN FROM REMOTE CONTROL SWITCH	DETERI OF THE REMOTE AIR ACTUATOR DIAPH
G PII 018325	062077	L MV B12 R	1 N	VALVE MO-1001-36A	FAILED TO CLOSE,RHR PUMP OPERAT	KEY WHICH PREVENTS STEM ROTATION SHEARED
G PII 019669	110477	L MV F20	1 N	MTR OPER FOR VAL MO-1001-18B	OVERLOADED,BURNED OUT	WORN GEARS ALLOWED MTR TO RUN AFT VLV CLS
G PII 019736	111477	W RV A24 S	1 T	RELIEF/SAFETY VALVE 203-3B	COULD NOT BE MAN OPENED	FAIL OF 3-WAY SOLENOID VAL TO PORT PROPER
G PII 019859	111577	W RV C27 R	1 N	RELIEF VALVE 203-3B	DETERMINED TO BE LEAKING	FIRST+SECOND STAGE OF PILOT VALVE LEAKING
G PII 019756	111777	W RV C27 R	1 N	RELIEF VALVE 203-3D	DETERMINED TO BE LEAKING	FIRST STAGE OF PILOT VLV SEAT LEAKING
G PII 022757	100978	W RV B27 R	1 N	RV-203-3C	FAILED TO RESEAT AT PROPER PRESSURE	EXCESSIVE PILOT SEAT LEAKAGE
G PII 026427	062779	L MV F00 R	1 T	RHR VALVE 1001-36A	INOPERABLE	CAUSE UNKNOWN
G PII 026760	072579	L MV A12 R	1 N	RHR VALVE MOV-1001-36B	INOPERABLE	VALVE STEM GUIDE KEY SHEARED

ALL VALVE LERS USED

P V E N T	PLAN NUMBER	CONTROL EVENT DATE	S Y S T E M C O M P R E	M O D E C A U S T	F A I L U M Y	A C T I V I T Y	MODE DESCRIPTION	CAUSE DESCRIPTION
G PII 027177	091979	L MV F12 R	1 T	RHR MOV-1001-36B FAILED TO OPERATE				ALLEN SCREW LOOSENEO, STEM GUIDE SLIPPED
G PII 031177	051380	D RM A16 S	1 T	CORE SPRAY VLV 1400-24B FAILED TO OPEN				DIRTY CONTACT IN LOGIC CIRCUIT
G PII 0-1759	072580	A RV A21 R	1 T	RV 203-30 FAILED TO OPEN DURING TEST/LOCKTITE IN				THE VLV'S SOLENOID ASSEMBLY REPLACED SAME
G PII 032273	080180	A RV A00 R	1 U	RV 203-30 DID NOT OPEN GIVEN MANUAL OPEN SIGNAL				NO CAUSE COULD BE DISCOVERED BY FACT REP
G PII 032578	082580	D RM A19	1 T	MO 1400-24A FAILED TO OPEN(CORE SPRAY SYSTEM)				VLV LUBRICATED AND SUCCESSFULLY OPERATED
G PII 032812	100180	A RV B12	1 N	*D* RELIEF VLV STUCK OPEN DURING SHUTDOWN				MAIN PISTON SCORED
G QC1 014059	010576	H CV E13	1 T	HPCI EXHAUST CHECK VLV. LEAKING INTERNALLY				DEFECT.GASKET BETWEEN VLV.SEAT AND BODY
G QC1 014057	011476	L MV C23 R	1 T	VALVE MO-1-1001-37A FAILED LEAKRATE TEST				TORQUE SW OUT OF ADJUSTMENT/LIMIT TORQUE
G QC1 015257	070176	F MV F12	1 U	LOOP SPRAY VALVE FAILED TO OPERATE(MO-1-1001-23-B)				LOOSE BOLTS HOLDING OPERATOR TO VALVE
G QC1 016162	090276	F MV B20	1 T	MOV FAILED TO CLOSE DURING TESTING(MO-1-1001-26-A)				EXCESS GREASE/COMPACTATION/HYDRAULIC LOCK
G QC1 016472*	110176	A RV A13	2 T	ELECTROMATIC RELIEF VALVES FAILED TO OPEN/TESTING				EXCESSIVE INTERNAL STEAM LEAKAGE
G QC1 0205318	032077	F MV C25	2M T	EXCESS LEAKAGE THRU SPRAY VALVES DURING TEST				IMPROPER SEATING OF VALVE
G QC1 020532	032077	A RV A12	3 T	MAIN STEAM ELECTROMATIC RELIEF FAILED TO OPEN/TEST				INTERNAL PARTS FOUND LOOSE AND MISSING
G QC1 018106	041277	F AV B24 S	1 T	DRAIN VALVE FAILED TO CLOSE/COMMAND FAULT				AIR SUPPLY SV FAILED/AIR WOULDNT VENT OFF
G QC1 018459	061177	H RM G16 S	1 T	HPCI PUMP INLET VALVE WOULD NOT STAY OPEN/TESTING				HALFUNCTION IN LOCAL VALVE CONT STAT CIRC
G QC1 019489	093077	D MV F05	1 T	CORE SPRAY VALVE 1-1402-25B FAILED TO OPERATE				CRACKED YOKE/PROB SINCE INSTALLATION
G QC1 020425	111677	A RV A16 S	1 N	RELIEF VALVE 1-203-3B FAILED TO OPEN ON DEMAND				COMMAND/WIRE TIE IN ELECT CONTACTOR
G QC1 020264	111877	H MV A23	1 T	HPCI MOV 1-2301-4 FAILED TO OPEN DURING TESTING				MOV HAD DEFECTIVE TORQUE SWITCH
G QC1 020636	020678	A RV A12	1 T	ELECTROMATIC RELIEF 1-203-3E FAILED TO OPEN / TEST				WORN INTERNAL PARTS/VALVE WAS REPLACED
G QC1 021408	042478	A RV A18	1 T	ELECTROMATIC RV 1-203-3C FAILED TO OPERATE / TEST				WELD FAILURE BETWEEN BODY AND CAGE/VIBRAT
G QC1 021436	050478	H MV B23	1 T	HPCI PMP SUCTION VLV MO-1-2301-6 WOULD NOT CLOSE				VLV.TORQUE SWITCH WAS WORN OUT
G QC1 026560	071779	W RV F16 S	1 T	RELIEF VALVE FAILED TO OPERATE				PRESSURE SWITCH WERE NOT CONNECTED
G QC1 030440	020680	L MV F16 S	1 T	LPCI VLV MO-1-1001-36A FAILED TO OPERATE				POWER TRANSFORMER BURNED OUT(COMMAND)
G QC1 030965	041080	L MV A23	1 T	LPCI MO-1-1001-36B FAILED TO OPEN ON TESTING				TORQUE SWITC' NEEDED ADJUSTMENT
G QC1 031359	051180	A RV A16 S	1 T	RV 1-203-3B FAILED TO OPEN DURING TEST				DIRT ON CONTACTS OF HOLD-IN COIL SWITCH

ALL VALVE LERS USED

PLANT NUMBER	CONTROL DATE	SYNTHETIC TEMP	COMPRESSOR MODE	CAUSE	TYPE	FUNCTION	ACTIVITY	MODE DESCRIPTION		CAUSE DESCRIPTION	
								RELIEF	VALVE	MOV	VALVE
G QC2 016473*	110176	A RV A09	R	2	T	TWO ELECTROMATIC RELIEFS FAILED TO OPEN ON TESTING					INTERNAL BINDING DUE TO CORROSION PROBLEM
G QC2 020533	032377	A RV A12	R	1	T	ELECTROMATIC RELIEF FAILED TO OPEN DURING TESTING					LOOSE INTERNAL PARTS BOUND//EXCESS VIBRAT
G QC2 019223	092377	A RV A12	R	1	T	ELECTROMATIC RELIEF FAILED TO OPEN DURING TESTING					RINGS CUT GROOVES IN DISC GUIDE/STEAM CUT
G QC2 019745	110677	W RV B27		1	M	RELIEF VALVE 2-203-3B FAILED TO RESEAT					PILOT VALVE WAS STEAM CUT AND ERODED
G QC2 019759	111477	D MV A08		1	T	CORE SPRAY MOV 2-1402-24B FAILED TO OPEN / TEST					STEM AND BONNET BADLY GALLED
G QC2 020245	011478	W RV F16	S	1	T	RELIEF VALVE FAILED TO OPERATE AS REQUIRED					PRESSURE CONTROL SWITCH SETPOINT DRIFT
G QC2 020943	030578	L CV E10		1	T	REVERSE FLOW THRU CHECK VALVE 2-220-67A / TESTING					DIRT ACCUMULATED IN VALVE INTERNALS
G QC2 021128	040478	L RM F16	S	1	N	VLV FOR FILL WTR TO LPCI DISCHARGE PIPE FAILED					NO POWER TO VLV/FUSE FAILED
G QC2 021561	052178	D RM V01	U	1	N	2A CORE SPRAY SUC.VLV. MO 2-1402-3A CLOSED WHEN R-					-EQUIRED TO BE OPEN//PERSONNEL ERROR
G QC2 022815	092978	W RV A24	S	1	T	RV 2-203-3A FAILED TO OPEN(MANUAL) / COMMAND					AIRLINE TO MANUAL AIR OPERATOR BROKE
G QC2 025429	021179	L MV B16	S	1	T	RHR SUCTION ISOLATION VALVE FAILED TO CLOSE					STICKING CONTACTS IN CIRCUIT BREAKER
G QC2 026557	071279	L MV A16	S	1	T	LPCI MOV THERMAL OVERLOAD TRIPPED					PROBABLE CAUSE-LOOSE CONNECTORS AT BREAKER
G QC2 027100	090579	L MV F12		1	T	DRYWELL SPRAY VALVE TRIPPED BREAKER WHEN OPERATED					BREAKER BOLT IN VALVE MOTOR OPERATOR
G QC2 027551	102679	L RM F00		1	T	2 C RHR PUMP SUCTION VLV MO2-100-7C BKR TRIPPED					NO APPARENT CAUSE FOUND
G QC2 028115	020480	L MV C25		1	T	LEAKAGE THRU MO-2-1001-36B DURING TEST					VARIOUS SEAT/DISC PROBLEMS;WARP,CORROSION
G QC2 031100	042080	A RV A27	R	1	T	RV 2-203-3C FAILED TO OPERATE DURING TEST					EXCESS CLEARANCE:PLUNGER TO PILOT VL STEP
G QC2 031189	042880	L MV B16	S	1	T	LPCI MOV 2-1001-36A FAILED TO CLOSE DURING TEST					PROBLEM IN CKT BKR SUPPLYING PWR TO VLV
G QC2 032779	091480	D MV A23		1	T	MO-2-1402-3A WOULD NOT OPEN (CORE SPRAY)					TEMPORARY STICKING OF TORQUE SWITCH
G QC2 032967	101080	F MV A23		1	T	MO-2-1001-29A FAILED TO OPEN INITIALLY					DISC TO TIGHT,TORQUE SWITCH ADJUSTED
G QC2 032968	101080	L MV A26		1	T	MO-2-1001-34A FAILED TO OPEN FULLY					LIMIT SWITCHES OUT OF ADJUSTMENT
G QC2 033138	101780	A RV A25	R	1	U	RELIEF VLV 2-203-3C FAILED TO OPEN					LEAKAGE BETWEEN MAIN DISC AND DISC GUIDE
G QC2 033451	120380	H MV F20		1	N	HPCI INJECTION VLV MO-2-2301-8 FOUND INOPERABLE					SHORT IN MOTOR OPERATOR
G QC2 033525	120380	A RV A12	R	1	N	ELECTROMATIC RELIEF 2-203-3D FAILED TO OPEN					STEAM LEAKAGE RETAINER PLUG TO MAIN DISK
G QC2 033744	123080	L MV A16	S	1	N	RHR VLV MO-2-1001-34A FAILED TO OPEN					CORRODED CONTACTS IN AUX CONTACTOR
G VY1 014230*	021776	L MV F01	C	2	N	RHR VLVS. 25A&B WOULD NOT STROKE ELECTRICALLY					PERSON,ERRORMUST STRO.VLVS.MANUALLY 1ST

ALL VALVE LERS USED

P L Y E N T	C O N T R O L N U M B R E H E R D A T E	E V E N T E N T R I C I T Y	S Y S T E M C O N D O U S P A N T H I G H T E L E V E R Y	C A U S E D E S C R I P T I O N	
				M O D E D E S C R I P T I O N	M O D E D E S C R I P T I O N
G VYI 016584*	051076 L MV A14 C	2 T	TWO 24 INCH MOVS (RHR-27A/B) FAILED TO OPEN / TEST PACKING MAINTENANCE PROBLEM		
G VYI 015184*	070676 A RV A22 C	3 T	3 TARGET ROCK RVS FAILED TO OPERATE(SIGNAL/MANUAL) DIAPHRAGM IN AIR OPERATORS FAILED/HEAT		
G VYI 015859	092076 L MV A00	1 T	LPC1 MOV (RHR-25B) FAILED TO OPEN DURING TESTING UNKNOWN/WALWORTH AND LIMITORQUE INVESTIG.		
G VYI 016997	011877 L RM V03 U	2L T	#B# RHR PMP DSCH.VLV. SHUT WHEN REQ. TO BE OPEN PERSONNEL ERROR		
G VYI 019854	110177 D XV F08	1 T	MANIFOLD BYPASS VALVE FAILED TO OPERATE GALLED THREADS/STEM SEIZED		
G VYI 020910	041278 K RV A00	1 R	RV (67HH13) SET TOO HIGH SETPOINT DRIFT/RESET TO LOWER LIFT PRESS		
G VYI 025152	012379 W RV A00 R	1 T	STEAM VLV SAFETY FOUND TO HAVE TOO HIGH SETPOINT SETPOINT DRIFT		
G VYI 030837	040180 L MV A20	1 T	LPC1 VLV 2-53B WOULDNT FULLY OPEN DURING TEST LOOSE PINION GEAR ON LIMITORQUE OPERATOR		
G VYI 032650	090180 L CV E12	1 T	O RHR-SW PUMP DISCHARGE CHECK DID NOT SEAT DEGRADATION OF VLV INTERNALS		
G VYI 032649	093080 H RM F16 S	1 N	723-19 HPCT PUMP DISCHARGE VLV LOST CONTROL POWER OVERLOAD RELAY HAD TRIPPED NO CAUSE		
G VYI 032985	100780 W RV A00 R	1 T	MAIN-STEAM RELIEF VLV S/N67HH12 SET POINT 3# TO HI SETPOINT DRIFT		

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16. ABSTRACT (200 words or less)

This report presents estimates of common cause fault rates and related quantities, based on Licensee Event Reports for valves in nuclear reactors. The Licensee Event Report data base is described. For estimating rates, the binomial failure rate model is used, extended to allow for the substantial observed plant-to-plant variability, and for shocks that by their nature make all the valves in a system inoperable. Every quantity is estimated by both a point estimate and a 90 percent interval.

17. KEY WORDS AND DOCUMENT ANALYSIS

17a. DESCRIPTORS

Common Cause
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Licensee Event Report (LER)
Valves
Binomial Failure Rate Model

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Shocks
Bayesian Methods
Plant-to-Plant Variation
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Gamma Distribution
Point and Interval Estimates

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