

United States Department of Energy



**ANALYSIS OF COBBLY SOILS FOR  
COBBLES-TO-FINES CORRECTIONS TO  
RADIONUCLIDE CONCENTRATIONS AT  
THE NEW RIFLE, COLORADO,  
PROCESSING SITE**

May 1994



Uranium Mill Tailings Remedial Action Project

INTENDED FOR PUBLIC RELEASE

This report has been reproduced from the best available copy. Available in paper copy and microfiche.

Number of pages in this report: 294

DOE and DOE contractors can obtain copies of this report from:

Office of Scientific and Technical Information  
P.O. Box 62  
Oak Ridge, TN 37831  
(615) 576-8401

This report is publicly available from:

National Technical Information Service  
Department of Commerce  
5285 Port Royal Road  
Springfield, VA 22161  
(703) 487-4650



ANALYSIS OF COBBLY SOILS FOR COBBLES-TO-FINES CORRECTIONS TO  
RADIONUCLIDE CONCENTRATIONS AT THE NEW RIFLE, COLORADO,  
PROCESSING SITE

May 1994

Prepared for  
U.S. Department of Energy  
UMTRA Project Office  
Albuquerque, New Mexico

Prepared by  
Jacobs Engineering Group Inc.  
Albuquerque, New Mexico

## EXECUTIVE SUMMARY

A contamination depth and cobbly soil characterization study was performed in November and December 1993 at the Uranium Mill Tailings Remedial Action (UMTRA) Project's New Rifle, Colorado, processing site. This study was initiated due to a concurrence by the U.S. Nuclear Regulatory Commission (NRC) clarifying that the allowable residual contamination in soil should be averaged over the total mass of the soil volume, including cobbles and gravels (i.e., bulk concentration). The New Rifle processing site has a high percentage of cobbles and gravels underlying the pile and other contaminated areas, which preliminary excavation designs have identified for removal and disposal. The main purpose of this study was to evaluate the relative mass percentage and radionuclide concentrations of cobbles and gravels in order to determine the bulk contamination concentrations, revise the underlying excavation design depths, and improve verification methods. Another important goal of the study was to acquire more accurate contamination depth data (profile) for the subpile material. The observations from these components of the study resulted in the following conclusions:

- On average, 75 percent of the cobbly soil beneath the pile and contaminated areas is cobble and gravel having radionuclide levels below the cleanup standards. The cobbles and gravels will not require excavation, although excavation was indicated in previous designs.
- Radium-226 (Ra-226) contamination depths from past characterization studies were significantly overestimated in many areas; therefore, less excavation will be required in these areas.
- Thorium-230 (Th-230) has not migrated preferentially in suspect areas at the site in significant levels that would require excavation below the excavation depths required for Ra-226.
- The amount of excavation to be carried out below the water table has decreased significantly because 1) more accurate data on contamination depth have been compiled, and 2) cobble/gravel parameters have been used to meet the bulk concentration limits for contamination. These two factors have resulted in lower contamination levels at depth.

In summary, this recharacterization study will probably reduce the volume of material for excavation/disposal by several hundred thousand cubic yards and significantly reduce the amount of ground water expected to be pumped out of the excavation during cleanup.

TABLE OF CONTENTS

<u>Section</u>	<u>Page</u>
EXECUTIVE SUMMARY .....	ES-1
1.0 INTRODUCTION .....	1-1
1.1 Standards and criteria .....	1-1
1.2 Remedial action .....	1-3
2.0 PHYSICAL AND RADIOLOGICAL EVALUATION .....	2-1
2.1 Test pit operation and characterization results .....	2-1
2.2 Statistical parameters for cobbles-to-fines corrections .....	2-5
3.0 CHANGES TO EXCAVATION DESIGN .....	3-1
4.0 CONCLUSIONS .....	4-1
5.0 LIST OF CONTRIBUTORS .....	5-1
6.0 REFERENCES .....	6-1
APPENDIX A U.S. DEPARTMENT OF ENERGY/U.S. NUCLEAR REGULATORY COMMISSION CORRESPONDENCE	
PROCEDURE FOR BULK RADIONUCLIDE DETERMINATION, EXCAVATION CONTROL, AND SITE VERIFICATION FOR SOILS CONTAINING COBBLES	
GENERIC PROTOCOL FOR THORIUM-230 CLEANUP/VERIFICATION AT UMTRA PROJECT SITES	
APPENDIX B PHOTOGRAPHS OF TEST PITS AND OPERATIONS	
APPENDIX C TEST PIT LOGS	
APPENDIX D MASS PARTITION FUNCTIONS (COBBLES-TO-FINES RATIOS)	
APPENDIX E LABORATORY RADIOLOGICAL TEST RESULTS	

LIST OF FIGURES

<u>Figure</u>		<u>Page</u>
2.1	Test pit locations, subpile and offpile . . . . .	2-2
2.2	Test pit locations, background . . . . .	2-3

LIST OF TABLES

<u>Table</u>		<u>Page</u>
2.1	Summary of mass partition functions and radionuclide concentrations for composite soil samples retained on a #4 mesh sieve . . . . .	2-4
3.1	New Rifle, Colorado, estimated excavation depth based on cobbles-to-fines ratio and contamination profiles . . . . .	3-2

LIST OF ACRONYMS AND ABBREVIATIONS

<u>Acronym</u>	<u>Definition</u>
ALARA	as low as reasonably achievable
cm	centimeter
DOE	U.S. Department of Energy
EPA	U.S. Environmental Protection Agency
ft	foot
m	meter
m <sup>2</sup>	square meter
NRC	U.S. Nuclear Regulatory Commission
pCi/g	picocuries per gram
pCi/L	picocuries per liter
pCi/m <sup>2</sup> s	picocuries per square meter per second
pH	acidity
Ra-226	radium-226
Rn-222	radon-222
Th-230	thorium-230
UMTRA	Uranium Mill Tailings Remedial Action
UMTRCA	Uranium Mill Tailings Radiation Control Act
μR/hr	microrentgens per hour

## 1.0 INTRODUCTION

### 1.1 STANDARDS AND CRITERIA

Remedial action at the New Rifle, Colorado, processing site is being performed under the *Uranium Mill Tailings Radiation Control Act* (UMTRCA) of 1978 (42 USC §7901 *et seq.*). Under the UMTRCA, the U.S. Environmental Protection Agency (EPA) is responsible for developing appropriate and applicable standards for the cleanup of radiologically contaminated land and buildings at 24 designated sites, including the New Rifle, Colorado, inactive processing site. The UMTRCA states that the U.S. Department of Energy (DOE) shall "select and perform remedial actions at the designated processing sites and disposal sites in accordance with the general standards" prescribed by the EPA. Regulations governing the required remedial action at inactive uranium processing sites were promulgated by the EPA in 1983 and are contained in 40 CFR Part 192 (1993), *Health and Environmental Protection Standards for Uranium and Thorium Mill Tailings*.

Subpart B of 40 CFR Part 192 consists of standards for the cleanup of land and buildings. The standards applicable to land cleanup activities are as follows:

Remedial actions shall be conducted so as to provide reasonable assurance that, as a result of residual radioactive materials from any designated processing site, the concentration of radium-226 in land averaged over an area of 100 square meters ( $m^2$ ) shall not exceed the background level by more than --

- 1) Five picocuries per gram (pCi/g), averaged over the first 15 centimeters (cm) of soil below the surface, and
- 2) Fifteen pCi/g, averaged over 15-cm-thick layers of soils more than 15 cm below the surface.

In addition, 40 CFR Part 192 provides criteria for applying supplemental standards for the cleanup and stabilization of other radionuclides that present a hazard commensurate with radium-226 (Ra-226) (40 CFR §192.21 (1993)), such as thorium-230 (Th-230). The *Generic Protocol for Thorium-230 Cleanup/Verification at UMTRA Project Sites* (Appendix A) under development by the DOE UMTRA Project Office has received oral NRC approval for implementation. Fundamental provisions of the protocol are as follows:

- Th-230 concentrations exceeding Ra-226 concentrations will be remediated such that Ra-226 concentrations 1000 years in the future, including both *in situ* Ra-226 and Ra-226 produced by natural decay of Th-230 over a 1000-year period, averaged over 100  $m^2$ , will not exceed background levels



by more than 5 pCi/g in the first 15-cm surface soil layer or 15 pCi/g in successive 15-cm subsurface layers.

- For deeply buried material, excavations will be stopped when the RAECOM computer code, using site-specific parameters, calculates a radon-222 (Rn-222) flux of 3.9 picocuries per square meter per second (pCi/m<sup>2</sup>s) and expected long-term conditions are appropriate, or when construction safety or feasibility becomes a concern.
- Excavation of elevated Th-230 encountered below the water table in the saturated zone will be assessed relative to the practicality with which dewatering can be performed. An as-low-as-reasonably-achievable (ALARA) analysis using pathway techniques will be performed in cases where a major portion of the site contains Th-230 that extends into the saturated zone, and excavation into the zone is impractical.

The EPA standards were originally based on an understanding of radiologically contaminated, fine-grained, tailings-like soil. However, the NRC has concurred that the soil cleanup standards for cobbly soil should have a universal interpretation of *bulk* soil concentrations, where bulk is defined as the total activity in picocuries divided by the total sample mass in grams, independent of the radionuclide distribution as a function of soil size fraction (Appendix A). Recognizing that UMTRA Project site cleanup activities will entail the cleanup of radiologically contaminated cobbly soil, the NRC also has concurred on a procedure developed by the DOE for excavation control and verification of cobbly subsoil (Appendix A). The accepted protocol is based on establishing a representative mass partition function that is the ratio of the mass of the soil fraction retained on a #4 sieve to the mass of the soil fraction passing a #4 sieve, and the characteristic radionuclide concentration on the larger soil size fraction retained on a #4 mesh sieve. The mass partition function can be developed and applied for the entire site or for each 100-m<sup>2</sup> grid (see Appendix A). Bulk radionuclide concentration can be determined using the mass partition function, the radionuclide concentration on the larger size soil fraction, and radiometric/radiochemical measurements of only the finer soil fraction passing a #4 sieve.

The standards given above are based on *bulk* Ra-226 concentrations elevated above background level. Measurements of background radioactivity near the New Rifle, Colorado, processing site, have resulted in the following determinations (DOE, 1992):

- Background gamma exposure rates at 1 meter (m) above the earth average 15 microrentgens per hour ( $\mu$ R/hr).
- Background Ra-226 concentrations in the soil near the processing site average 1.2 pCi/g.



- Background Rn-222 concentrations in air at various locations near the processing site average approximately 0.4 picocuries per liter (pCi/L).

## 1.2 REMEDIAL ACTION

The remedial action at the processing site will be conducted to remove the tailings and contaminated materials to meet the EPA *bulk* soil cleanup standards for surface and subsurface soils. The site areas disturbed by remedial action excavation will be either contoured or backfilled with uncontaminated soil and contoured to restore the site. The final contours will produce a final surface grade that will create positive drainage from the site.

## 2.0 PHYSICAL AND RADIOLOGICAL EVALUATION

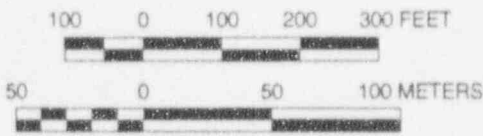
A site characterization study was conducted in November and December 1993 to determine the nature of the cobbly subsoil profile and contamination levels underlying the New Rifle, Colorado, processing site and to ascertain 1) the mass partitioning of the subpile soil relative to a #4 mesh sieve, and 2) the radiological contamination associated with the cobbly soil size fractions passing and retained on a #4 mesh sieve. The purpose of this investigation was to obtain the necessary parameters to characterize the bulk radionuclide concentrations for the site foundation soil, particularly the subpile area. With these more recent site characterization data, appropriate depths for excavating radiologically contaminated cobbly subsoil may be determined. These data also provide necessary information regarding the way in which excavation control and verification should be performed in cobbly soils.

### 2.1 TEST PIT OPERATION AND CHARACTERIZATION RESULTS

Operations consisted of excavating 22 test pits with a backhoe. Lithological logging, sampling, and photographing of the pits were also carried out. Test pit locations are shown in Figures 2.1 and 2.2, and selected photographs of pits and operations are found in Appendix B. Pits were distributed over accessible areas of the subpile (11 total), around the north, south and east sides of the pile perimeter (8 total), and in areas representing background conditions for the site (3 total). Lithological logging data for each test pit are found in Appendix C.

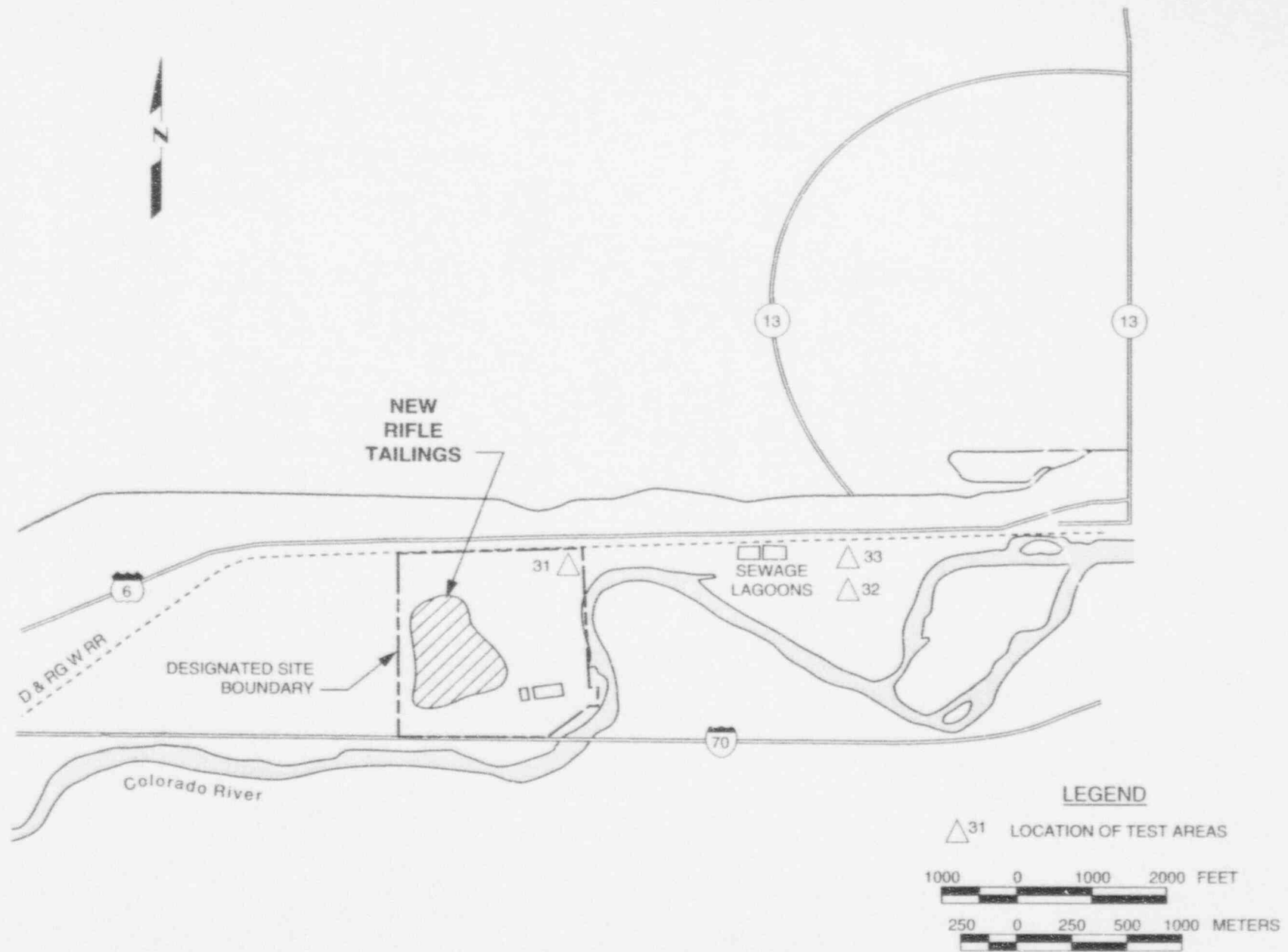
Test pits were excavated into the cobbly soil layer underlying the site and sampled in accordance with the NRC-approved protocol (Appendix A). Sampling was terminated in general at or slightly below the level that free water was encountered in the test pits. This was done because of difficulty in obtaining representative samples from below the water surface. Test pit location 4 (M-CF-04 and M-CF-04A, Appendix C) was excavated a second time to obtain additional 1-foot (ft) (0.3-m) increment samples at depths from which the initial samples may have been accidentally cross-contaminated during the first sampling. The granular material in test pit location 29 (M-CF-29) was determined to be contaminated fill material from earlier site backfill operations; therefore, its cobbles-to-fines ratio (mass partition function) and radionuclide data were not representative of the site's natural cobbly soil. These data were not used in the study.

For each pit, a representative composite sample of the cobbly soil layer was divided using appropriate gradation techniques into fractions greater and less than a #4 mesh sieve to determine mass partition functions (Appendix D). Composite samples of both soil fractions in the cobbly soil were analyzed for Ra-226 and Th-230 (Appendix E). Table 2.1 lists the individual, average, and statistical mass partition functions and cobble (> #4 mesh) radionuclide concentrations for the test pits.



**LEGEND**  
 LOCATION OF TEST AREAS

**FIGURE 2.1**  
**TEST PIT LOCATIONS, SUBPILE AND OFFPILE**



**FIGURE 2.2**  
**TEST PIT LOCATIONS, BACKGROUND**

Table 2.1 Summary of mass partition functions and radionuclide concentrations for  
composite soil samples retained on a #4 mesh sieve

Test pit ID and statistical summary	Location	Mass partition function <sup>a</sup>	Radionuclide concentration mass fraction > #4 sieve	
			Ra-226 (pCi/g)	Th-230 (pCi/g)
M-CF-01	Offpile	4.92	1.1	1.1
M-CF-02	Offpile	2.15	0.7	0.9
M-CF-03	Offpile	2.38	1.7	0.5
M-CF-04	Subpile	3.18	0.6	0.7
M-CF-05	Subpile	3.46	1.4	0.3
M-CF-06	Subpile	No data	3.3	1.6
M-CF-07	Subpile	2.72	2.0	1.7
M-CF-11	Offpile	3.24	0.8	0.4
M-CF-15	Offpile	2.88	0.9	0.8
M-CF-19	Offpile	3.22	0.8	0.7
M-CF-20	Subpile	5.41	0.5	0.8
M-CF-21	Subpile	4.49	1.6	1.2
M-CF-22	Subpile	3.83	0.9	0.9
M-CF-24	Subpile	1.84	0.9	0.7
M-CF-25	Subpile	3.65	0.8	1.3
M-CF-26	Subpile	1.90	0.7	0.5
M-CF-27	Offpile	5.67	0.8	0.8
M-CF-28	Subpile	9.42	0.8	0.5
M-CF-30	Offpile	3.85	1.2	0.6
M-CF-31	Background	3.59	0.9	0.7
M-CF-32	Background	4.21	1.8	1.1
M-CF-33	Background	4.52	1.6	0.5
Average	All	3.83	1.2	0.8
Standard deviation		1.67	0.6	0.4
95% confidence level <sup>b</sup>		3.20	1.4	0.9
Average	Background	4.11	1.4	0.8
Standard deviation		0.47	0.5	0.3
95% confidence level <sup>b</sup>		3.32	2.2	1.3
Average	Subpile	3.99	1.2	0.9
Standard deviation		2.20	0.8	0.5
95% confidence level <sup>b</sup>		2.71	1.6	1.2
Average	Offpile	3.54	1.0	0.7
Standard deviation		1.22	0.3	0.2
95% confidence level <sup>b</sup>		2.72	1.2	0.8
Average	Subpile and offpile	3.79	1.1	0.8
Standard deviation		1.80	0.7	0.4
95% confidence level <sup>b</sup>		3.05	1.4	1.0

<sup>a</sup>Mass partition function equates to cobbles-to-fines ratio,  $f = (M > \#4)/(M < \#4)$ .

<sup>b</sup>The upper 95 percent confidence level value is shown for the radionuclide concentrations, and the lower 95 percent confidence level value for the mass partition functions.

In addition to the requirements in the cobbles-to-fines protocol, an aliquot of the fine soil size fraction (< #4 mesh sieve) was obtained from each 1-ft (0.3-m) test pit depth increment (except in tailings) and separately analyzed for Ra-226 and Th-232. One to four of these increment samples for each test pit were also analyzed for Th-230 to determine the potential for significant Th-230 contamination at depth below Ra-226 contamination. Measurements of acidity (pH) in selected soil layers in subpile and offpile test pits were also taken in the field to determine whether there were acidic conditions that would enhance Th-230 mobility (see data in lithological logs of Appendix C).

## 2.2 STATISTICAL PARAMETERS FOR COBBLES-TO-FINES CORRECTIONS

The original plans developed for test pit locations had a total of approximately 30 subpile and offpile test pits. Ten of these locations were inaccessible during the study because they were underneath about 50 ft (15.3 m) of tailings. However, the data gathered from this study are considered to be sufficient for obtaining the necessary parameters to implement the statistical approach of cobbles-to-fines corrections at the site due to the following:

- Observed consistency in the mass partition functions and low radionuclide concentrations in the cobbles (Table 2.1).
- Spatial representativeness of pit locations (Figure 2.1).
- Uniformity of the geological conditions in the underlying natural cobbly soil (Appendix C).

Additionally, the protocol's method for determining conservative values for the statistical mass partition functions and cobble radionuclide concentrations was reviewed. This review revealed that using data from less than 30 test pits should actually result in more conservatism in developing the statistical values when using representative sampling plans.

The average, standard deviation and statistical values for the mass partition function and cobble radionuclide concentrations for each grouping (subpile, offpile, background, and all combined) of test pits are shown at the bottom of Table 2.1. The data from test pit M-CF-29 were not used because of its apparent unnatural contents (backfill). No mass partition function was available for test pit M-CF-06, because technical problems (cave-in) rendered the measurement nonrepresentative.

This information demonstrates the relative consistency in the physical and radiological characteristics of the cobbly soil layer in all of the test pits. In determining the correct values for calculating bulk concentrations from cobbles-to-fines corrections, the subpile and offpile combined data appear to be the most applicable because of the proximity to areas that may apply the corrections. These critical values that will be used in the correction calculations are 3.05 for the statistical mass partition function, and 1.4 and 1.0 for the



statistical Ra-226 and Th-230 cobble radionuclide concentrations, respectively. Using the statistical mass partition function and statistical Ra-226 cobble concentration for all of the pits (1.4 pCi/g, which is more appropriate than using 2.2 pCi/g from the small number of background test pits), a bulk Ra-226 background concentration of 1.4 pCi/g is established in this study.



### 3.0 CHANGES TO EXCAVATION DESIGN

From the lithological logging data (Appendix C), the thickness of the layers of relatively clean fine-grained soil (sand, silt, clay, etc.) above the cobbly soil interface in these pits ranged from 0 ft to 16 ft (0 m to 4.9 m), and averaged 5 ft (1.5 m). Cobbly soil was encountered immediately at the surface in five of the subpile test pits where the sand/silt/clay layer was previously removed with the tailings (all on the south side of the pile). At other UMTRA Project sites, Ra-226 adsorbs or precipitates within the first 1 or 2 ft (0.3 or 0.6 m) of soil below the pile or other contaminated material (DOE, 1994). This process was also apparent in many of the test pits at New Rifle. From the results for Th-230 characterization of the fines (1-ft [0.3-m] increment samples, Appendix E), it can be concluded that mobilization of Th-230 below the Ra-226 contamination was not apparent in most of the test pits (see Ra-226 and Th-230 profile data in test pit logs of Appendix C). This was somewhat expected when considering the typically neutral-to-basic pH observed in the soils. The few pits that showed Th-230 mobilization (disequilibrium with Ra-226) did not reveal levels that would require excavation beyond the Ra-226 excavation depth.

From these observations and the profiling (1-ft [0.3-m] increment samples) data on the radionuclide contamination, it is apparent that the cobbles-to-fines corrections may not be needed in most remediated areas because the contamination does not extend into the cobbly subsoil. This has resulted in a significant change in contamination depths. Original site characterization data (DOE, 1985) used in the remedial action excavation design showed the contamination in many of the test pit areas to be deeper, from 1 to 6 ft (0.3 to 1.8 m). This change in known contamination depths affects estimated excavation depths in the design, as shown in Table 3.1. The data changes are most likely due to the original study using bore hole drilling techniques, which involved drilling and sampling the subpile soil through various depths of tailings and contaminated materials. It appears that using a backhoe and not having a large (approximately 50-ft [15-m]) layer of tailings to penetrate for sampling subpile soil improved the accuracy of data for the actual contamination depth. The availability of these improved contamination depth data enables engineering and scheduling efforts to more accurately handle disposal of the actual volume of contaminated material. These data indicate that the total volume of contaminated material is less than that originally identified by an estimated several hundred thousand cubic yards, if test pit conditions are representative of the remaining site contaminated areas.

**Table 3.1 New Rifle, Colorado, estimated excavation depth based on cobbles-to-fines ratio and contamination profiles**

Area	Plan excavation depth		Excavation based on cobbles/fines profiles		Delta <sup>a</sup>	
	ft	m	ft	m	ft	m
1	6	1.8	1	0.3	(5)	(1.5)
2	5	1.5	0	0	(5)	(1.5)
3	5-6	1.5-1.8	2	0.6	(3-4)	(0.9-1.2)
4, 4A	13	4.0	9	2.7	(4)	(1.2)
5	13	4.0	11	3.4	(2)	(0.6)
6	16	4.9	13+	4.0+	--	--
			insufficient data available			
7	14	4.3	14	4.3	0	0
11	5	1.5	2	0.6	(3)	(0.9)
15	5	1.5	4	1.2	(1)	(0.3)
19	6	1.8	1	0.3	(5)	(1.5)
20	5	1.5	0	0	(5)	(1.5)
21	5	1.5	0	0	(5)	(1.5)
22	6	1.8	6	1.8	0	0
24	4	1.2	0	0	(4)	(1.2)
25	6	1.8	1	0.3	(5)	(1.5)
26	6	1.8	1	0.3	(5)	(1.5)
27	6	1.8	8	2.4	2	0.6
28	2	0.6	1	0.3	(1)	(0.3)
29	3	0.9	Insufficient data available		--	--
30	6	1.8	4	1.2	(2)	(0.6)

<sup>a</sup>Numbers within parentheses indicate amount of reduced excavation; numbers without parentheses indicate amount of increased excavation.

#### 4.0 CONCLUSIONS

Site cleanup, including the excavation control and verification, will involve the cobbles-to-fines corrections in remediated areas when applicable. Th-230 was not observed to be a significant concern in excavation design, and its residual concentrations will be further verified according to the requirements in the *Generic Protocol for Thorium-230 Cleanup/Verification at UMTRA Project Sites* (Appendix A). Whenever the application of the cobble-to-fines correction is in doubt (for example, when it appears that there is only a small percentage of cobbles), grid verification based on a representative sample will be used or grid-specific mass partition functions will be measured to demonstrate compliance with EPA soil cleanup standards.

For site verification, the *statistical cobbles radionuclide concentrations at the upper 95 percent confidence limit and the statistical mass partition function at the lower 95 percent confidence limit* are used to determine allowable fines concentrations in subpile and offpile areas (calculation JEG-RFL-03-94-09-06-00). On this basis, for cobbly subsoil to comply with the bulk cleanup standards (*total* 1000-year Ra-226 concentrations from residual Ra-226 and Th-230 not to exceed 15 pCi/g above background = 1.4 pCi/g *bulk* Ra-226 concentration), the corresponding concentrations in the finer soil size fraction (passing a #4 mesh sieve) in the subpile and offpile areas could vary as follows:

1.  $C_{<#4 Ra} = 62.2$  pCi/g Ra-226, when the Th-230 concentrations on the finer fraction,  $C_{<#4 Th}$ , are less than or equal to 63.7 pCi/g;
2.  $C_{<#4 Th} = 176.5$  pCi/g Th-230, if there is evidence that the Th-230 has differentially migrated relative to Ra-226, and the residual *bulk* Ra-226 concentration is 1.4 pCi/g ( $C_{<#4 Ra} = 1.2$  pCi/g), corresponding to average background concentrations; or
3. Th-230 concentrations (pCi/g) determined by the following relation for residual Ra-226 concentrations measured on the finer soil size fraction, ( $C_{<#4 Ra}$ ), in the range of 1.2 to 62.2 pCi/g,

$$C_{<#4 Th} = 178.8 - 1.85 \times C_{<#4 Ra}$$

### 5.0 LIST OF CONTRIBUTORS

The following individuals contributed to the preparation of this report.

---

Name	Contribution
W. James	Author
J. Lommler	Document review
M. Miller	Peer review
L. Keith	Text processing
E. Steinhoff	Graphic design
D. Thalley	Technical editing

---

## 6.0 REFERENCES

- DOE (U.S. Department of Energy), 1994. *Site-Specific Analysis of Radiological and Physical Parameters for Cobbly Soils at the Gunnison, Colorado, Processing Site, Revision 1*, DOE/AL-62350-53F, DOE UMTRA Project Office, Albuquerque Operations Office, Albuquerque, New Mexico.
- DOE (U.S. Department of Energy), 1992. *Remedial Action Plan and Site Design for Stabilization of the Inactive Uranium Mill Tailings Sites at Rifle, CO, Final, Volume II*, DOE/AL-050506.0000, DOE UMTRA Project Office, Albuquerque Operations Office, Albuquerque, New Mexico.
- DOE (U.S. Department of Energy), 1985. *Radiologic Characterization of the Rifle, Colorado, Uranium Mill Tailings Remedial Action Sites, GJ-29*, by the Bendix Field Engineering Corporation for the DOE UMTRA Project Office, Albuquerque Operations Office, Albuquerque, New Mexico.

## CODE OF FEDERAL REGULATIONS

- 40 CFR Part 192, *Health and Environmental Protection Standards for Uranium and Thorium Mill Tailings*, U S. Environmental Protection Agency (1993).

## UNITED STATES CODE

- 42 USC §7901 *et seq.*, *Uranium Mill Tailings Radiation Control Act*, November 8, 1978.

APPENDIX A

U.S. DEPARTMENT OF ENERGY/U.S. NUCLEAR  
REGULATORY COMMISSION CORRESPONDENCE

PROCEDURE FOR BULK RADIONUCLIDE  
DETERMINATION, EXCAVATION CONTROL, AND SITE  
VERIFICATION FOR SOILS CONTAINING COBBLES

GENERIC PROTOCOL FOR THORIUM-230  
CLEANUP/VERIFICATION AT UMTRA PROJECT SITES



U.S. DEPARTMENT OF ENERGY/U.S. NUCLEAR  
REGULATORY COMMISSION CORRESPONDENCE





Department of Energy

Albuquerque Operations Office  
P.O. Box 5400  
Albuquerque New Mexico 87115

SEP 0 6 1988

FEDERAL EXPRESS

Mr. John Surmeier  
Chief, Uranium Recovery Branch  
Division of Low-Level Waste  
Management & Decommissioning  
Office of Nuclear Materials Safety  
and Safeguards  
U.S. Nuclear Regulatory Commission  
Mail Stop 5-E-2  
1 White Flint North  
11555 Rockville Pike  
Rockville, MD 20852

Dear Mr. Surmeier:

Historically, the majority of Ra-226 contaminated materials being cleaned up at Uranium Mill Tailings Remedial Action (UMTRA) Project sites consisted of tailings, ore spoils, tailings intermixed with fine-grained soils (windblown and vicinity properties) and fine-grained soils under residual milling waste (tailings and raffinate ponds). However, in 1988, conditions encountered while remediating Th-230 contamination which persisted once Ra-226 had been removed at both the Riverton, Wyoming, and Durango, Colorado, sites were substantially different.

At both sites, which were located on alluvial floodplains, subsurface soils consisted of a large percentage of cobbles and gravels which were retained on a #4 sieve (4.76 mm). In addition, it was determined that approximately 95 percent of the total concentration of radioactivity was deposited on the fines (those soils passing a #4 sieve).

Based on these considerations and the fact that cleanup verification sampling routinely employed by the Remedial Action Contractors did not readily accommodate sampling and analysis of materials greater than #4 sieve, the following protocol for Th-230 cleanup/verification to a bulk subsurface concentration of 35 pCi/g was adopted and approved by the U.S. Department of Energy (DOE) and the U.S. Nuclear Regulatory Commission (NRC) in modifications to the Remedial Action Plans for those sites.

1. Determine the "fines mass fraction" by collecting several (10) representative bulk field samples, and separating fractions greater than and less than a #4 sieve:

fines mass fraction = mass fines/mass total = unitless fraction

2. Determine Ra-226 (or Th-230) concentration (passing the #4 sieve) in verification samples collected and analyzed according to standard methodology described in MK-Ferguson Company (MK-F) Procedure RAC-015, "Verification Procedures for Vicinity Properties and Tailings Sites."
3. Determine "bulk" Ra-226 (or Th-230) concentration during cleanup and verification by correcting the Ra-226 (or Th-230) concentration on fines as follows:

$$\begin{aligned} \text{bulk Ra-226 concentration} &= (\text{fines Ra-226 concentration}) \times (\text{fines mass fraction}) \text{ or,} \\ \text{bulk Th-230 concentration} &= (\text{fines Th-230 concentration}) \times (\text{fines mass fraction}) \end{aligned}$$

The DOE proposes to adopt this basic protocol, on a site specific basis, as a standard operating practice for cleanup and verification of both residual Ra-226 and Th-230 contamination at UMTRA sites yet to be remediated. The bulk concentrations of Ra-226 and Th-230 determined by the above procedure will comply with the remediation standard for Ra-226, and supplemental cleanup requirements for Th-230, as specified in 40 CFR 192. Bulk Ra-226 concentrations will not exceed 5 and 15 pCi/g for respective 15 cm deep surface and subsurface layers averaged over 100 m<sup>2</sup>. Similarly, the bulk concentration of subsurface Th-230 in 15 cm depth increments will not exceed 35 pCi/g averaged over 100 m<sup>2</sup>. The details of the protocol will be more completely described in an added section to Procedure RAC-015 which will address when the protocol would be implemented; the number of samples needed to provide the initial value for the fines mass fraction; the frequency of updating/verifying the fines mass fraction as work progresses across a site; how the fines mass fraction used will be logged on field data sheets, etc. It will also be included in future updates of the Technical Approach Document and referenced as appropriate in Remedial Action Plans for sites where it will be applied.

The sites where this protocol could be applied would likely include Grand Junction, Gunnison, Rifle, Slick Rock, and Naturita, Colorado, since they are all located on alluvial floodplains possessing characteristics similar to those described above. Therefore, the DOE requests the NRC's concurrence that such a protocol is consistent with the requirements of 40 CFR 192 and that its contractors should be directed to formally incorporate the protocol into standard operating procedures and address its potential application in site Remedial Action Plans.

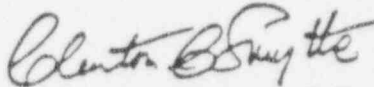
Mr. John Surmeier

- 3 -

SEP 06 1991

If you should have any further questions regarding this request, please call Mr. Don Metzler of my staff at (FIS) 845-5657.

Sincerely,



*en* Mark L. Matthews, P.E.  
Project Manager  
Uranium Mill Tailings Remedial Action  
Project Office

cc:

F. Bosiljevac, UMIRA  
S. Hill, TAC  
M. Miller, TAC  
D. Gonzales, TAC  
J. Oldham, MK-F  
D. Carlson, MK-F  
M. Madsen, CN-Geotech



UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

SEP 17 1991

Mr. Mark L. Matthews P.E.  
Project Manager  
Uranium Mill Tailings Remedial Action  
Project Office  
Department of Energy  
Albuquerque Operations Office  
P.O. Box 5400  
Albuquerque, New Mexico 87115

Dear Mr. Matthews:

Your letter of September 6, 1991, requested U.S. Nuclear Regulatory Commission (NRC) concurrence in the use of a procedure for determining and verifying radium-226 concentrations at locations with large quantities of cobbly material. Your letter states that at several Title I sites, DOE has encountered large quantities of radium-226 or thorium-230 contaminated material with a high content of cobbly material (greater than a No. 4 sieve size). Your tests show that the contained radioactivity is concentrated in the finer fraction with the coarse fraction containing negligible quantities (less than 5 percent). Procedures presently in use by your contractors for sampling and analyses are designed for relatively fine grained homogeneous soils with a minimum of larger material and are not adequate to characterize the radioactive concentrations in the heterogeneous size material being encountered. Your proposed approach would rely on measurement of the radium-226 or thorium-230 content in the finer fraction to obtain an average concentration for the entire sample.

We agree that determining an average radium-226 or thorium-230 content over an entire sample would be consistent with the Environmental Protection Agency (EPA) standards in 40 CFR 192 if the radium-226 content of the two size fractions and the percentage of each size fraction are properly factored. Part 192.12 states that the concentration of radium-226 in land can be averaged over an area of 100 square meters to meet the standards of not exceeding background level by more than 5 pCi/g averaged over the first 15 cm of soil below the surface and 15 pCi/g averaged over 15 cm thick layers of soil more than 15 cm below the surface.

You plan to address the details of the procedure in a section to be added to Procedure RAC-015 which will define when the procedure would be used, the number and distribution of samples to be taken, the determination of the radium-226 distribution and size fractions, and other appropriate details.

We agree that the proposed approach has the potential for maintaining compliance with EPA's standards while avoiding over excavation of contaminated

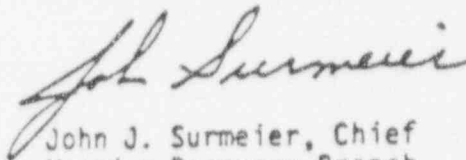


Mark Matthews

- 2 -

material. However, for final concurrence, we will have to review the details of your revised Procedure RAC-015 and the effects of its implementation on a site-specific basis. Any questions can be addressed to Allan Mullins of my staff at FTS-492-0578.

Sincerely,



John J. Surmeier, Chief  
Uranium Recovery Branch  
Division of Low-Level Waste Management  
and Decommissioning, NMSS

cc: D. Metzler, DOE, Alb.



UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

APR 4 1992

Mr. Albert R. Chernoff, Project Manager  
Uranium Mill Tailings Remedial Action  
Project Office  
U.S. Department of Energy,  
Albuquerque Operations Office  
P.O. Box 5400  
Albuquerque, New Mexico 87115

Dear Mr. Chernoff:

We have reviewed the procedure on "Bulk Radionuclide Determination, Excavation Control, and Site Verification For Cobbly Soils" sent with your letter of March 26, 1992, and supplemented by a revised Page 12 sent by facsimile on March 30, 1992. We hereby concur with its use on U.S. Department of Energy Uranium Mill Tailings Remedial Action Project sites containing a high percentage of cobbly subsoil. This procedure, designated RAC-OP-003, should be referenced in the specific Remedial Action Plans for those sites where it will be used.

One item of note concerns the section of the procedure discussing authority (Section 1.3). This section should be revised to reference this letter of concurrence rather than the September 17, 1991, letter cited, which agreed with the concept but did not concur with the procedure.

Any questions should be addressed to Allan Mullins of my staff at FTS 964-2578.

Sincerely,

A handwritten signature in cursive script, appearing to read "John J. Surmeier".

John J. Surmeier, Chief  
Uranium Recovery Branch  
Division of Low-Level Waste Management  
and Decommissioning, NMSS

cc: D. Metzler, DOE A1b  
P. Mann, DOE A1b  
D. Gonzalez, TAC

PROCEDURE FOR BULK RADIONUCLIDE  
DETERMINATION, EXCAVATION CONTROL, AND SITE  
VERIFICATION FOR SOILS CONTAINING COBBLES





INTERIM CHANGE NOTICE

(ICN)

ICN NO. SOP-OP-003-4 ICN-01/REV#0

FOR INFORMATION ONLY

Page 1 of 1

HP CONTROLLED COPY 45

PROCEDURE NUMBER: OP-003-4 REVISION NUMBER: 0

EFFECTIVE DATE  
OF ICN: 9 / 21 / 92

CHANGES REQUESTED  
BY:

Steve Hamp (DOE)

TITLE : Soil Verification Using Cobbles-to-Fines Correction

CHANGES GENERATED  
BY:

Dave Andrews

PROBLEM STATEMENT/CORRECTIVE ACTION

The DOE has requested a few changes to improve clarity and content. Improvements shall be as indicated.

ACTION

Remove pages 4 through 11, Rev. 0 and replace with new pages 4 through 11, Rev. 0 ICN-01.

APPROVAL SIGNATURES

(Please sign and date)

HP & E MANAGER: *David S. Carlson*

DATE: 10 / 1 / 92

HPP MANAGER: *[Signature]*

DATE: 10 / 1 / 92

HPO MANAGER: *Ernest M. Carl*

DATE: 9 / 29 / 92

COORDINATOR: *David Chauton*

DATE: 9 / 29 / 92

# Health Physics Standard Operating Procedures

Title: SOIL VERIFICATION USING COBBLES-TO-FINES CORRECTION

Procedure No.: OP-003-4

Rev. No.: 0

Page 1 of 15

FOR INFORMATION ONLY

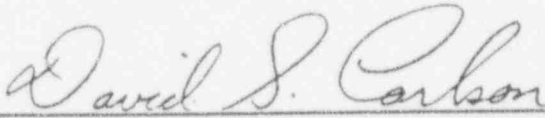
APPROVAL

HP CONTROLLED COPY 45


APPROVED:

 4-17-92  
Project Director, Remedial Actions Contractor, UMTRA Project

APPROVED:

 4/17/92  
Health Physics and Environment Manager, Remedial Actions Contractor, UMTRA Project

APPROVED:

 4/17/92  
Health Physics Programs Manager, Remedial Actions Contractor, UMTRA Project

APPROVED:

 4-17-92  
Health Physics Operations Manager, Remedial Actions Contractor, UMTRA Project

Soil Verification Using Cobbles-To-Fines Correction

1.0 SCOPE

FOR INFORMATION ONLY

1.1 Purpose

This procedure will be used for determining and verifying average bulk radionuclide concentrations for radium-226 (Ra-226), thorium-230 (Th-230), and, if necessary, thorium-232 (Th-232) at locations where the subsoil consists of a percentage of cobbles in the bulk sample sufficient to affect measurement of the total radionuclide concentration. Excavation control and verification will be based on bulk concentrations determined by this procedure.

1.2 Applicability

This procedure may be applied in areas designated for routine soil excavation and verification (see RAC-OP-003) where the subsoil media contains a high percentage of cobbles.

1.3 Authority

Letter to A.R. Chernoff, DOE/UMTRA from J.J. Surmeier, NRC dated April 4, 1992.

2.0 REFERENCES

- 2.1 RAC Health Physics Procedure RAC-RP-005 - Radiological Instrumentation.
- 2.2 RAC Health Physics Procedure RAC-OP-002 - Excavation Control Procedure
- 2.3 RAC Health Physics Procedure RAC-OP-003

3.0 DEFINITIONS

- 3.1 Cobbles - The portion of a composite soil sample which will not pass through a #4 mesh sieve.
- 3.2 Fines - The portion of a composite soil sample which will pass through a #4 mesh sieve.
- 3.3 Mass partition function,  $f$ , of a cobbly soil sample - the ratio of the dry mass of the cobbles ( $M_{cob}$ ), to the dry mass of the fines ( $M_{fine}$ ):

$$f = M_{cob}/M_{fine} \text{ (cobble to fine ratio),}$$

FOR INFORMATION ONLY

where the total dry mass of the sample,  $M_T$ , is

FOR INFORMATION ONLY

$$M_T = M_{>24} + M_{<24}$$

- 3.4 Radiological concentration (Ra-226, Th-230, or Th-232), in picocuries per gram (pCi/g), for the fines or cobbles, are designated by  $C_{<24}$  and  $C_{>24}$ , respectively.
- 3.5 Bulk radionuclide concentration (Ra-226, Th-230, or Th-232), in pCi/g, is designated by  $C_B$ , and calculated using

$$C_B = \text{Total Sample Radioactivity (pCi)} / \text{Total Dry Mass of Sample (g)}$$

$$C_B = (C_{<24} \times M_{<24} + C_{>24} \times M_{>24}) / (M_{<24} + M_{>24})$$

$$C_B = C_{<24} (1/(1+f)) + C_{>24} (f/(1+f)).$$

- 3.6 Student t distribution (t) - the mathematical quantity used to define the distribution of test statistics for small sample populations; used herein to determine the lower and upper 95 percent confidence values for mass partition function and cobble radionuclide concentrations respectively.
- 3.7 Running Average - The determination of statistical quantities based on the available data and recalculated as more data becomes available.
- 3.8 Statistical Mass Partition Function ( $f_L$ ) - The mass partition function (f), at the lower 95 percent confidence value calculated from test pit or running average data.
- 3.9 Statistical Cobble Radionuclide Concentration ( $C_{>U}$ ) - The cobble radionuclide concentration ( $C_{>24}$ ) at the upper 95 percent confidence value calculated from test pit or running average data.

#### 4.0 REQUIREMENTS

##### 4.1 Prerequisites

- 4.1.1 All instruments used under this procedure shall have valid calibration.
- 4.1.2 Backup data (correlations, etc.) must be acquired, retained on-site, and made available for audit, on all methods and analyses used for excavation control and verification measurements.

FOR INFORMATION ONLY FOR INFORMATION ONLY

4.2 Tools, Material, Equipment

4.2.1 Buckets, wheelbarrows, #4 mesh sieves or screens (4.8 millimeter), shovels or backhoe, weighing scale up to 200 lbs., drying oven, and other materials, as necessary, to obtain representative bulk soil samples. It should be noted that a 1/4 inch hardware cloth is approximately equivalent to a #4 mesh sieve, and may be used in lieu of a #4 mesh sieve.

4.3 Precautions/Limits

N/A

4.4 Acceptance Criteria

N/A

5.0 PROCEDURE

5.1 Site Evaluation

5.1.1 This guidance applies to processing sites and vicinity property areas. If the work area under consideration is less than 0.5 acre, the mass partition function (f) will be based on soil sampling from one centrally located test pit.

5.1.2 The statistical mass partition function ( $f_L$ ) and statistical cobble radionuclide concentration ( $C_{>D}$ ) may be determined by analysis of samples collected from test pits prior to construction. The purpose for developing a statistical mass partition function is only to obtain an estimate of the excavation depth required for compliance with radiological cleanup standards.

5.1.3 Approximately 30 (preferably uniformly distributed) sampling locations (test pits) should be used for the entire site. Fewer test pits may be used on small sites with prior approval from the HP & E Manager.

5.1.4 If test pit excavation activities are performed during remedial action, the statistical mass partition function ( $f_L$ ) shall be obtained by calculating a running average of the corresponding parameters obtained as test pit work progresses across the site.



FOR INFORMATION ONLY FOR INFORMATION ONLY

5.2 Test Pit Soil Sampling and Analysis

- 5.2.1 Dig each test pit to the estimated depth of contamination at the location, and record the test pit surface elevation and maximum depth of each test pit. If groundwater is encountered, the elevation of the water level at the time of test pitting shall be recorded.
- 5.2.2 Collect one composite sample from each test pit. The composite soil sample shall be comprised of all the material contained in a standard shovel from each one foot increment (no material shall be discarded). Sampling shall begin at the cobbly soil surface or tailings/cobbly soil interface and continue through a minimum of 5 feet of cobbly material or all the cobbly material (whichever is less).
- 5.2.3 Sieve the composite sample through a #4 mesh sieve, collecting the fines and cobbles in separate buckets of known weight. Weigh both fractions separately. Thoroughly mix the fine fraction and extract two (2) representative 500 gram can samples.
- 5.2.4 Determine the percent moisture content by weight of one of the can samples and calculate the adjusted dry weight of the fines. Calculate the adjusted dry weight of the cobbles assuming a moisture content of 1.5 percent. Record all pertinent information on the Cobbles to Fines Calculation Sheet (Attachment 1). Calculate the mass partition function (f) for the test pit using the adjusted dry weight of the fines and cobbles in the relation defined in Definition 3.3.
- 5.2.5 The second can shall be analyzed by the site laboratory for Ra-226 (and Th-232 if necessary) and sent to the vendor laboratory for Ra-226 and Th-230 analysis (and Th-232 if necessary). Record on-site and vendor analysis results on Attachment 1.

Note: Analysis for Th-232 shall only be performed if the site characterization indicates Th-232 is present.

- 5.2.5.1 Using the initial on-site analysis results and the vendor analysis results for all test pit or running average samples, a Ra-226 correction factor shall be established using the following equation:

$$Ra-226 \text{ C.F.} = \frac{R_1 + R_2 + \dots R_n}{n}$$



FOR INFORMATION ONLY

FOR INFORMATION ONLY

where, C.F. = correction factor,  
 $R_n$  = Vendor results (pCi/g) divided by  
 initial OCS, results (pCi/g) for the  
 $n^{\text{th}}$  sample (i.e., 1, 2, ...n), and  
 n = number of ratios.

5.2.5.2 The correction factor shall be updated using the pertinent analyses results from QA samples (section 5.10).

5.2.6 Ship the fraction retained on the #4 sieve from each test pit to the vendor laboratory, in the 5-gallon bucket. This material shall be cleaned, crushed, and analyzed for Ra-226, Th-230 and, if necessary, Th-232. Record vendor analysis results on Attachment 1.

5.2.7 Calculate the bulk radionuclide concentration ( $C_B$ ) for the test pit using the mass partition function (f) for the test pit (section 5.2.4), the vendor radiological concentration of the fines ( $C_{<\#4}$ ), and the radiological concentration of the cobbles ( $C_{>\#4}$ ) in the equation defined in Definition 3.5. Bulk radionuclide concentrations should be calculated for Ra-226, Th-230, and Th-232 (if necessary).

5.3 Establish background bulk radionuclide concentrations for Ra-226, Th-230, and, if necessary, Th-232, by the sampling and analyses detailed in steps 5.2.1 through 5.2.6 at three uncontaminated background locations containing cobbly subsoil of similar geologic deposition.

5.4 Statistical Mass Partition Function - Alternative 1 (Test Pits)

5.4.1 Upon completion of test pit sampling, pertinent data shall be compiled on the Statistical Data Sheet (Attachment 2), and the statistical mass partition function shall be calculated using the following equation:

$$f_L = \bar{f} - t(s/\sqrt{n})$$

where,  $f_L$  = statistical average mass partition function at the lower 95 percent confidence value,  
 $\bar{f}$  = mean mass partition functions of n samples,  
 s = sample standard deviation for the n samples,  
 t = t from Attachment 3, and  
 n = number of observations.

FOR INFORMATION ONLY FOR INFORMATION ONLY

5.4.2 The mean of the sample population is determined as follows:

$$\bar{f} = \frac{f_1 + f_2 + \dots + f_n}{n}$$

where,  $f_{1,2 \text{ or } n}$  = the value of f for sample 1, 2, or n; and  
 $n$  = the number of samples.

5.4.3 The standard deviation is calculated as follows:

$$S = \sqrt{\frac{\sum_{n=1}^n (f_n - \bar{f})^2}{n - 1}}$$

where, S = sample standard deviation,  
 $f_n$  = value of f for sample n,  
 $\bar{f}$  = mean of f for n samples, and  
 $n$  = number of samples.

5.4.4 The statistical cobble radionuclide concentration for Ra-226, Th-230 and Th-232 (if necessary) shall be calculated using the following equation:

$$C_{>u} = \bar{C} + t(s/\sqrt{n})$$

where,  $C_{>u}$  = The statistical cobble radionuclide concentration at the upper 95 percent confidence value,  
 $\bar{C}$  = mean radionuclide concentration of the n samples,  
 $s$  = standard deviation of the 30 samples,  
 $t$  = t from Attachment 3, and  
 $n$  = number of samples.

FOR INFORMATION ONLY

5.5 Statistical Mass Partition Function - Alternative 2 (Running Average)

5.5.1 The statistical mass partition function ( $f_L$ ) and the statistical cobble radionuclide concentration ( $C_{>u}$ ) may be obtained by calculating a running average of the corresponding parameters using the equations in sections 5.4.1 and 5.4.4 respectively. Compile data on the Statistical Data Sheet and recalculate  $f_L$  and  $C_{>u}$  as data is obtained from each new test pit.

5.6 The statistical mass partition function and statistical cobble radionuclide concentration for alternative 1 or 2, will only be used for excavation control to obtain an estimate of the final excavation depth to comply with EPA's radiological cleanup standards. Final excavation depths and verification will be determined as described in section 5.7 through 5.9.

5.6.1 By solving the equation in section 3.5 for  $C_{<#4}$  and using the statistical mass partition function ( $f_L$ ) and the statistical cobble radionuclide concentration ( $C_{>u}$ ) an estimate of the allowable fines radionuclide concentration may be obtained as follows:

$$C_{<#4} = \frac{C_B - C_{>u} [f_L / (1 + f_L)]}{[1 / (1 + f_L)]}$$

- where,  $C_{<#4}$  = The estimated fines radionuclide concentration,
- $C_B$  = the applicable limit (i.e., 5 or 15 pCi/g for Ra-226 or Th-232 or 35 pCi/g for Th-230),
- $f_L$  = statistical mass partition function, and
- $C_{>u}$  = statistical cobble radionuclide concentration.

5.7 Verification Soil Sampling & Analysis

5.7.1 Grid the entire site into squares of 100 yd<sup>2</sup> (~100 m<sup>2</sup>). Grids shall be uniformly distributed over the site so as to obtain representative data. Record location and elevation for each 100 yd<sup>2</sup> grid.

5.7.2 Further subdivide each grid where excavation control is being performed into approximately 10 x 10 foot squares (see below). Subdividing grids may normally be done visually by the technician performing the survey. Soil sample extraction will be performed at each of the nine 10 x 10 foot squares within the grid. Each soil plug should consist of all the material contained in a standard shovel. This will include soil, rock, small/large gravel and cobble. No material is to be discarded. The soil plug will be taken to a depth of 15 centimeters (cm). Sample collection shall be random (non-biased).

FOR INFORMATION ONLY  
FOR INFORMATION ONLY  
(30')

	0	0	0
(30')	0	0	0
	0	0	0

0 = sample location

5.7.3 The nine soil plugs (80-100 lbs combined weight) comprise a composite sample.

5.7.4 Sieve the composite sample through a #4 mesh sieve, collecting the fines and cobbles in separate buckets of known weight. Thoroughly mix the fine fraction.

5.8 Site Verification Alternative 1 (Grid Specific)

5.8.1 For verification alternative 1, weigh both fractions separately and record information on Attachment 1.

5.8.2 Extract two (2) 500g can samples of the fine fraction for moisture content and radiological analysis.

5.8.3 Determine the moisture content of the fines and calculate the adjusted dry weight. Calculate the adjusted dry weight of cobbles assuming a moisture content of 1.5 percent. Calculate and record the mass partition function for the grid (Attachment 1).

5.8.4 Analyze the second can sample of fines for Ra-226 and, if necessary, Th-232 with the on-site OCS. Calculate the corrected radionuclide concentration using the site Ra-226 correction factor determined in section 5.2.5.1.



FOR INFORMATION ONLY  
FOR INFORMATION ONLY

- 5.8.5 Calculate the bulk radionuclide concentration  $C_B$  for the grid using the grid specific mass partition function, radionuclide concentration of the fines (the initial corrected concentration shall be used for calculating the Ra-226 bulk radionuclide concentration) and the statistical cobbles radionuclide concentration ( $C_{>u}$ ) in the formula in section 3.5. All data shall be recorded on Form F1-OP-003-4.
- 5.8.6 Dry, seal and store the sample for 20 day on-site analysis.
- 5.8.7 After a minimum of 20 days, reanalyze the sample and calculate the final bulk radionuclide concentration ( $C_B$ ) for the grid.
- 5.9 Site Verification Alternative 2 (Statistical - Running Average)
  - 5.9.1 For each 100 m<sup>2</sup> grid, a 9-plug composite soil sample of the fines soil will be obtained following the technique outlined in Section 5.7.
  - 5.9.2 Extract a 500g can sample of the fine fraction for radiometric analysis. Discard the larger size soil fraction.
  - 5.9.3 Analyze the can sample for Ra-226 and, if necessary, Th-232 with the on-site OCS. Calculate the corrected radionuclide concentration using the site correction factor determined in section 5.2.5.1.
  - 5.9.4 Calculate the bulk radionuclide concentration for the grid using the radionuclide concentration of the fines (the initial corrected concentration shall be used for calculating the Ra-226 bulk radionuclide concentration), the statistical mass partition function ( $f_L$ ) and the statistical cobble radionuclide concentration ( $C_{>u}$ ) in the formula from section 3.5 as modified below.

$$C_B = C_{c\#4} [1/(1 + f_L)] + C_{>u} [f_L/(1 + f_L)]$$

Record the pertinent data on the Alternative 2 Bulk Concentration Data Sheet (Attachment 4).

- 5.9.5 Dry, seal and store the sample for 20 day on-site analysis.
- 5.9.6 After a minimum of 20 days, reanalyze the sample and calculate the final bulk radionuclide concentration ( $C_B$ ) for the grid.

FORM FOR INFORMATION ONLY

5.10 The verification sample from the 25th 100 m<sup>2</sup> grid of each block will be sent to an outside Vendor laboratory for independent Ra-226, Th-230, and, if necessary, Th-232 analyses in accordance with Quality Assurance requirements.

6.0 RECORDS/REPORTS/NOTIFICATIONS

6.1 All data shall be recorded on the appropriate data sheet.

7.0 ATTACHMENTS

7.1 Attachment 1 - Cobble to Fines Calculation Sheet (F1-OP-003-4)

7.2 Attachment 2 - Statistical Data Sheet (F2-OP-003-4)

7.3 Attachment 3 - Critical Values of t.

7.4 Attachment 4 - Alternative 2 Bulk Concentration Data Sheet (F4-OP-003-4)



FOR INFORMATION ONLY  
FOR INFORMATION ONLY

Attachment 1

COBBLES TO FINES CALCULATION SHEET

Site: \_\_\_\_\_ Sheet \_\_\_\_\_ of \_\_\_\_\_  
Sample/Grid I.D. \_\_\_\_\_ Date: \_\_\_\_\_

Fines	Cobbles	Moisture Content Fines
Wt. Sample & Bucket _____	Wt. Sample & Bucket _____	Wet Wt. Sample/Pan _____
Wt. Bucket _____	Wt. Bucket _____	Dry Wt. Sample/Pan _____
Wt. Sample _____	Wt. Sample _____	Tare Wt. Pan* _____
Adjusted _____	Adjusted _____	Wt. Water** _____
Dry Wt. (M <sub>&lt;sub&gt;cs&lt;/sub&gt;)* _____</sub>	Dry Wt. (M <sub>&lt;sub&gt;cs&lt;/sub&gt;)** _____</sub>	Wt. Soil*** _____
		Percent Water(*/**) _____

\* Adjusted Dry Wt. of the Fines = Wt. Sample x (1 - % water)  
\*\* Adjusted Dry Wt. of the Cobbles = Wt. Sample x (1 - .015)

Mass Partition function (f) = M<sub><sub>cs</sub>/M<sub><sub>cs</sub> = \_\_\_\_\_</sub></sub>

Radiological Analysis	<sup>226</sup> Ra (pCi/g)	<sup>230</sup> Th (pCi/g)	<sup>232</sup> Th (pCi/g)	COMMENTS
Cobbles (C <sub>&lt;sub&gt;cs&lt;/sub&gt;)</sub>				
On-Site Analysis Fines (C <sub>&lt;sub&gt;cs&lt;/sub&gt;)</sub>	* ** ***	N/A		
Vendor Analysis Fines (C <sub>&lt;sub&gt;cs&lt;/sub&gt;)</sub>				
Bulk Radionuclide Concentration (C <sub>B</sub> )	# ## ###			

\* Initial; \*\* Initial Corrected; \*\*\* 20 day (N/A for Test Pit or Running AVE.)  
# Using Vendor; ## Using Initial Corrected; ### Using 20 day (N/A for Test Pits or Running AVE.)

<sup>226</sup>Ra Correction Factor: \_\_\_\_\_

Reviewed By: \_\_\_\_\_ Date: \_\_\_\_\_

F1-DP-003-4



FOR INFORMATION ONLY FOR INFORMATION ONLY

Attachment 3

CRITICAL VALUES OF t

n-1	t <sub>.050</sub>
1	6.314
2	2.920
3	2.353
4	2.132
5	2.015
6	1.943
7	1.895
8	1.860
9	1.833
10	1.812
11	1.796
12	1.782
13	1.771
14	1.761
15	1.753
16	1.746
17	1.740
18	1.734
19	1.729
20	1.725
21	1.721
22	1.717
23	1.714
24	1.711
25	1.708
26	1.706
27	1.703
28	1.701
29	1.699
inf.	1.645



**GENERIC PROTOCOL FOR THORIUM-230  
CLEANUP/VERIFICATION AT UMTRA PROJECT SITES**



## Generic Protocol for Thorium-230 Cleanup/Verification at UMTRA Project Sites

The excavation of materials contaminated with thorium-230 ( $\text{Th}^{230}$ ) at one or more UMTRA Project sites may require extensive, deep removal of soil materials to ensure that the radium-226 ( $\text{Ra}^{226}$ ) concentrations will comply with EPA's surface and subsurface soil cleanup standards (i.e., 40 CFR 192). The following discussion presents a unified approach for the future application of standards for  $\text{Th}^{230}$  at the UMTRA Sites.

### 1. Introduction

The cleanup of radiologically contaminated soils on UMTRA Project sites provides explicit requirements for the remediation of soils contaminated with Radium-226 ( $\text{Ra}^{226}$ ), which include limits of 5 and 15 picocuries/gram (pCi/g) for the initial and successive 15 centimeter (cm) deep layers, respectively, averaged over an area of 100 m<sup>2</sup>. If other radionuclides are encountered in sufficient quantities and concentrations to constitute a significant radiological hazard, the supplemental standards provisions of 40 CFR 192.21 and 40 CFR 192.22 provide guidance for performing remedial action for these radionuclides to reduce residual radioactivity to levels that are as low as reasonable achievable.

Thorium-230 ( $\text{Th}^{230}$ ), which naturally decays, with a half-life of 77,000 years, to form  $\text{Ra}^{226}$  is also present in uranium mill tailings and contaminated soils. Therefore, it may be readily shown that for soils containing initial  $\text{Ra}^{226}$  and  $\text{Th}^{230}$  concentrations, at time  $t=0$ , of  $\text{Ra}^{226}(t=0)$  and  $\text{Th}^{230}(t=0)$ , respectively, the  $\text{Ra}^{226}$  concentration at any later time,  $t$ , is:

$$\text{Ra}^{226}(t) = \text{Ra}^{226}(t=0) e^{-\lambda t} + \text{Th}^{230}(t=0) (1 - e^{-\lambda t}),$$

where  $\lambda$  is the decay constant for  $\text{Ra}^{226}$ , or  $4.32 \times 10^{-4} \text{ yrs}^{-1}$ .

Furthermore, the geochemical behavior of  $\text{Ra}^{226}$  and  $\text{Th}^{230}$  in typical UMTRA site environments have been observed to be significantly different. Under neutral or basic soil conditions, neither  $\text{Ra}^{226}$  nor  $\text{Th}^{230}$  are preferentially mobile geochemically (i.e., both radionuclides will form chemical compounds that have similar potential for migrating into soils). However, under acidic conditions, the chemical forms taken by these radionuclides are significantly different in their potential for depth migration in soil, with  $\text{Th}^{230}$  being more mobile than  $\text{Ra}^{226}$ .

In windblown tailings areas, mill yards, and ore storage areas of UMTRA sites, it has been observed that: 1) the surface and subsurface soils are normally at neutral pH; 2) the radiological material does not contain abundant quantities of free acid; and 3) the  $\text{Ra}^{226}$  and  $\text{Th}^{230}$  concentrations are in near secular equilibrium (their activities are approximately equal). The near secular equilibrium for the radiological contamination in these areas results from the fact that most of the uranium ores processed were in near equilibrium. Therefore, the application of soil cleanup procedures for  $\text{Ra}^{226}$  according to EPA standards would also reduce the  $\text{Th}^{230}$  concentrations to acceptable levels by default, and the total  $\text{Ra}^{226}$  as a function of time will not exceed 5 or 15 pCi/g, for surface and subsurface soil respectively.

However, under acidic soil conditions that may prevail in the foundation soil under uranium mill tailings, the subpile region, or in surface and subsurface soils of raffinate or evaporation



pond, the different geochemical interactions of  $\text{Ra}^{226}$  and  $\text{Th}^{230}$  will cause these radionuclides to differentially migrate. Generally, under these conditions,  $\text{Ra}^{226}$  is adsorbed or co-precipitated on soil within a depth of one to two feet, and  $\text{Th}^{230}$  migrates deeper into the subsoil until neutralization of the transporting pore water occurs, where it is removed from solution by the formation of insoluble precipitates or co-precipitates (thorium or thoro-ferro hydroxides, for example). For example, at the Spook, Wyoming site,  $\text{Th}^{230}$  differentially migrated as deep as 20 feet below the raffinate pond before being stabilized by neutralization.

In order to be in harmony with the supplemental standards provisions to reduce  $\text{Th}^{230}$  concentrations to as low as reasonably achievable (ALARA), and to come as close to meeting otherwise applicable standards as is reasonable under the circumstances, an excavation depth less than 20 feet was selected as a viable solution for this site.

It may be concluded that the cleanup of the initial  $\text{Ra}^{226}$  contamination according to standards does not necessarily mitigate against the ultimate ingrowth of residual  $\text{Ra}^{226}$  with time due to the radioactive decay of residual  $\text{Th}^{230}$  in all areas within a site. As a consequence, residual  $\text{Ra}^{226}$  concentrations at a later date, due to ingrowth from  $\text{Th}^{230}$  contamination, may pose an undesirable health hazard. Therefore, the supplemental standards provision of 40 CFR 192 requires the development of a cleanup criterion for  $\text{Th}^{230}$ , which is health protective by reducing exposures to levels that are ALARA, keeping in consideration the measures necessary to implement the remedial actions under the circumstances that exist at the site. The following procedure establishes appropriate remedial action concentration limits for  $\text{Th}^{230}$ , and is proposed to be implemented at UMTRA Project sites after concurrence from all governing agencies involved with activities at each site agree to its implementation.

## 2. Generic Protocol

As can be seen from the equation presented in the introduction, the overall 1000-year maximum concentration of  $\text{Ra}^{226}$  in the soils will either be equal to the present  $\text{Ra}^{226}$  inventory (if  $\text{Th}^{230}$  concentrations are equal to or less than  $\text{Ra}^{226}$  concentrations), or the total  $\text{Ra}^{226}$  inventory one thousand years in the future (if  $\text{Th}^{230}$  concentrations exceed  $\text{Ra}^{226}$  concentrations). If  $\text{Ra}^{226}$  concentrations are equal to or exceed  $\text{Th}^{230}$  concentrations, the site will already meet the  $\text{Th}^{230}$  supplemental standard by default when the site is remediated to the 40 CFR 192 standards for  $\text{Ra}^{226}$ .

- (1) Therefore, the supplemental standard chosen for  $\text{Th}^{230}$  needs only to ensure that the overall  $\text{Ra}^{226}$  concentration one thousand years in the future, when averaged over 100 square-meter areas, will not exceed either 5 pCi/g in the first 15 cm layer or 15 pCi/g in successive 15 cm layers.

It should be noted that the  $\text{Ra}^{226}$  concentrations are considered to be bulk concentrations, as determined by the recently developed, NRC-approved protocol for excavation control and soil verification of cobbly subsoils.

### 2.1 Protocol for Contamination at Depth

As the depths of excavations become deeper to remove elevated  $\text{Th}^{230}$ , the thickness of overlying fill material that is eventually used to remediate the site will increase. As a result, attenuation of radon-222 ( $\text{Rn}^{222}$ ) diffusing through the overlying fill material will also increase.

Therefore, as the overlying clean fill material thickness increases, the resultant attenuation of the radon generated from the associated ingrowth of  $Ra^{226}$  will allow higher residual concentrations of  $Th^{230}$  to be left in place, while still attaining a level of protection equivalent to the intent of the  $Ra^{226}$  soil cleanup standards. To determine this concentration, the NRC model (presented in the Draft Generic Environmental Impact Statement on Uranium Milling; NUREG-0511; April 1979) can be used to determine the radon-222 ( $Rn^{222}$ ) flux that would produce 0.02 Working Levels (WL) in a hypothetical structure built on a 100 square-meter ( $m^2$ ) grid. The following equation was used:

$C = FAB/(VR * 1000)$ , where:

- C =  $Rn^{222}$  concentration (pCi/l)
- F =  $Rn^{222}$  flux (pCi/ $m^2$ -s)
- A = Area over which the flux enters ( $m^2$ )
- B = Flux reduction factor for entering structure (unitless)
- V = Volume of the structure ( $m^3$ )
- R = Effective  $Rn^{222}$  removal rate ( $s^{-1}$ )
- 1000 = conversion factor (l/ $m^3$ )

In cases where basements are feasible (based on local construction practices and deep groundwater table), it should be assumed that the thickness of fill material is eight feet less than the depth of the excavation. Using  $A = 103m^2$ ,  $B = 0.5$ ,  $V = 250m^3$ , and  $R = 1.98 \times 10^{-4} s^{-1}$ , a flux of 3.9 pCi/ $m^2$ -s would produce indoor air concentrations of approximately 4.0 pCi/l  $Rn^{222}$ . Assuming radon daughters are present at 50% equilibrium, this would correspond to 0.02 WL.

- (2) Thus, the RAECOM computer code can be used to calculate the resultant flux from higher concentrations at depth as one factor to consider in determining if further excavation is warranted. As long as the calculated flux is less than 3.9 pCi/ $m^2$ -s, it can be assumed that equivalent protection is provided as long as the backfill thickness is maintained. Therefore, the analysis will consider the potential future (at least 200 years) erosion and land use in the determination of excavation depth. The calculations shall use site-specific parameters when available. Reasonably conservative parameters that consider the expected site conditions shall be used when site-specific data are unavailable. Selection on backfill materials with superior (low) diffusion coefficients may be included in the ALARA considerations of the design. When evaluating this option for the Th-230 supplemental standard, considerations of the construction hazards to remedial action workers and the feasibility of the anticipated construction requirements should be taken into account.

## 2.2 Protocol for Contamination in the Saturated Zone

Another scenario potentially impacting excavations to remove elevated  $Th^{230}$  concentrations is when groundwater is encountered at shallow depths. Since the  $Th^{230}$  contamination has been present within the saturated zone long enough for soluble constituents to have been mobilized, it is reasonable to assume that any remaining  $Th^{230}$  that may be encountered within a saturated zone will not be appreciably mobilized by pH neutral groundwater. Furthermore, it is known that the diffusion coefficient decreases dramatically as soils approach full

saturation until it reaches values typical of water (Radon Attenuation Handbook for Uranium Mill Tailings Cover Design; NUREG/CR-3533; April 1984). It is therefore reasonable to assume that  $Rn^{222}$  generated within a saturated zone generally will not diffuse to the surface. Finally, it is very difficult to perform deep, cost effective excavations within a saturated zone.

(3) Therefore, whenever shallow groundwater is encountered, the following options will be considered:

(a) Excavation into the saturated zone will be considered when water pumping or other controls are reasonable and when high concentrations of  $Th^{230}$  extend only a short distance into the saturated zone.

(b) An ALARA analysis will be performed in cases where a major portion of the site contains Th-230 which extends into the saturated zone, and excavation into the zone is impractical. The ALARA analysis will use reasonably conservative assumptions to project future doses. If water pumping or other controls are not reasonable, excavation will halt at the level of the water table (a nominal extra foot of excavation may be considered so long as it does not require pumping/dewatering).

### 3. Verification Sampling

Under typical site conditions, verification of the  $Th^{230}$  supplemental standard is to be achieved by a three-tiered sampling approach.

(4) In areas within an UMTRA processing site that are suspected of preferentially mobilizing thorium contamination over radium contamination (e.g., under raffinate pits), based upon process knowledge or other sources such as previous sampling data, 100% of the grids are to be sampled and analyzed for  $Th^{230}$ .

(5) In subpile areas, 10% of the grids will be sampled.

(6) In areas where process knowledge and characterization data indicates no potential for preferential mobilization (e.g., windblown tailings), grids will not be sampled for  $Th^{230}$ .

An analysis of verification data from the Tuba City, Arizona, UMTRA site, which has completed remediation and used this strategy, found no instances in the area sampled at the rate of 1 out of 25 grids where  $Th^{230}$  concentrations would cause future (i.e., at  $t=1000$  years) expected  $Ra^{226}$  concentrations to exceed 40 CFR 192 standards for  $Ra^{226}$ . Furthermore, preliminary results confirm the expectation that  $Th^{230}$  concentrations are generally equal to or less than  $Ra^{226}$  concentrations in areas other than beneath the raffinate pits, and  $Ra^{226}$  concentrations are well correlated to  $Th^{230}$  concentrations in these areas.

If any verification samples exceed the  $Th^{230}$  criteria of this protocol, the surrounding eight grids will be examined to determine whether or not these grids also exceed the criteria. If sample results have not been generated for the surrounding grids already, archived samples of such grids will be analyzed. If any of the surrounding grids also exceed the  $Th^{230}$  criteria,

the surrounding eight grids around such grids will also be examined. This process will continue until no more of the surrounding grids exceed the  $\text{Th}^{230}$  criteria. All grids that exceed the criteria will undergo further remediation unless there is sufficient justification and concurring parties agreement to do otherwise.

#### 4. Conclusion

Based upon the above discussions, the following generic protocol shall be used for the excavation of  $\text{Th}^{230}$  at all future UMTRA Project sites:

- (1) Excavate bulk  $\text{Th}^{230}$  to a 1000-year corrected bulk  $\text{Ra}^{226}$  concentration of 5 or 15 pCi/g (as appropriate) in 15-cm layers;
- (2) For deeply buried material, stop excavations when the RAECOM computer code, using site-specific parameters, calculates a  $\text{Rn}^{222}$  flux of 3.9 pCi/m<sup>2</sup>-s and expected long-term conditions are appropriate or when construction safety or feasibility become a concern;
- (3) Consider the following options whenever shallow groundwater is encountered:
  - (a) Excavate into the saturated zone when water pumping or other controls are reasonable, especially when high concentrations of  $\text{Th}^{230}$  extend only a short distance into the saturated zone.
  - (b) An ALARA analysis will be performed in cases where a major portion of the site contains  $\text{Th}^{230}$  which extends into the saturated zone, and excavation into the zone is impractical. The ALARA analysis will use reasonably conservative assumptions to project future doses. Halt excavations at the level of the water table when water pumping or other controls are not reasonable (a nominal extra foot of excavation may be considered so long as it does not require pumping/dewatering).
- (4) Perform verification sampling for bulk  $\text{Th}^{230}$  in all grids underneath raffinate pits or other areas suspected of having a mechanism to preferentially mobilize  $\text{Th}^{230}$  over  $\text{Ra}^{226}$ ;
- (5) Perform verification sampling for bulk  $\text{Th}^{230}$  in 10% of the grids underneath sub-pile areas; and
- (6) Do not perform verification sampling for bulk  $\text{Th}^{230}$  in grids for which process knowledge and characterization data indicates no potential for preferential migration.
- (7) When practical, delay backfilling until verification results are obtained.



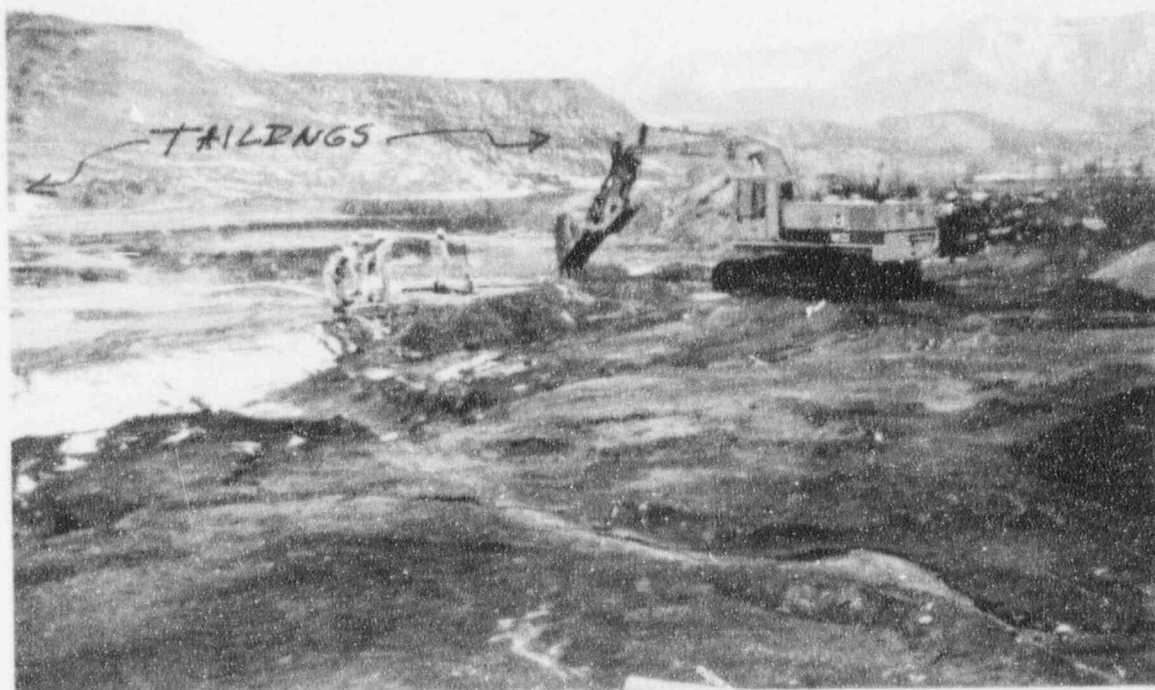
APPENDIX B

PHOTOGRAPHS OF TEST PITS AND OPERATIONS



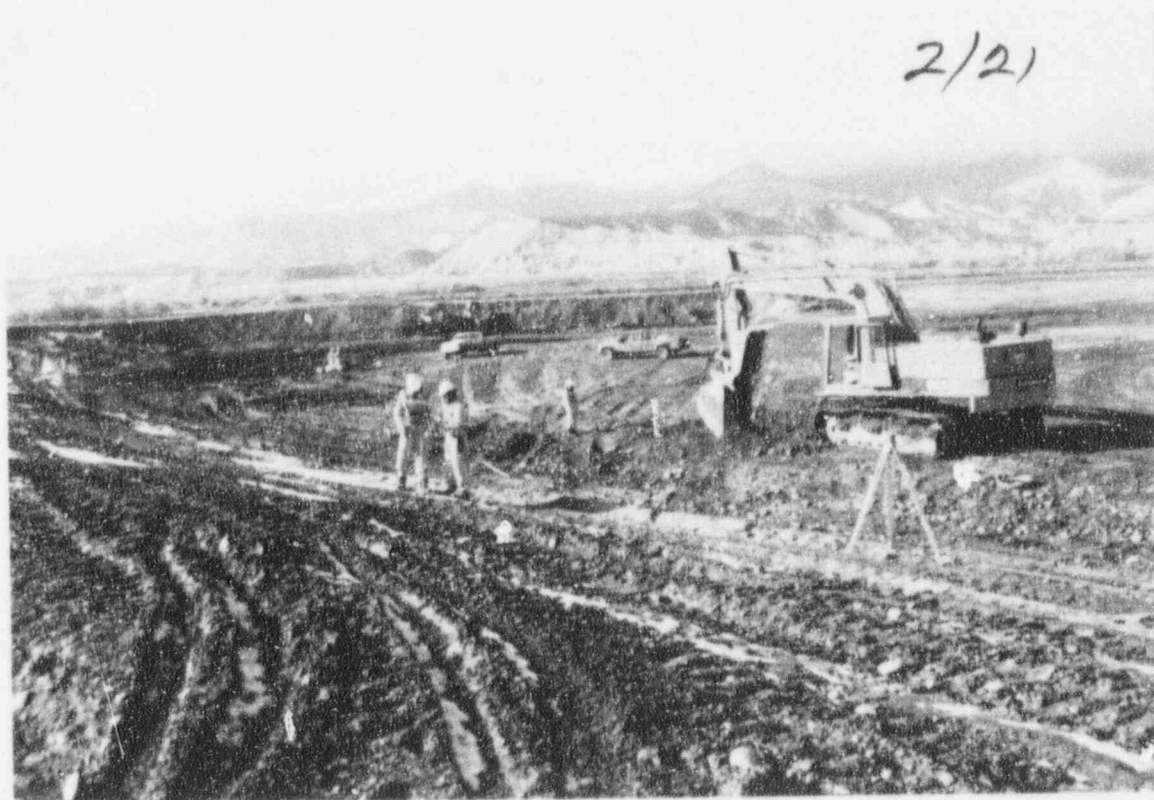
PHOTOS OF FIELD SAMPLING  
AND GRADATION DETERMINATION

3/5

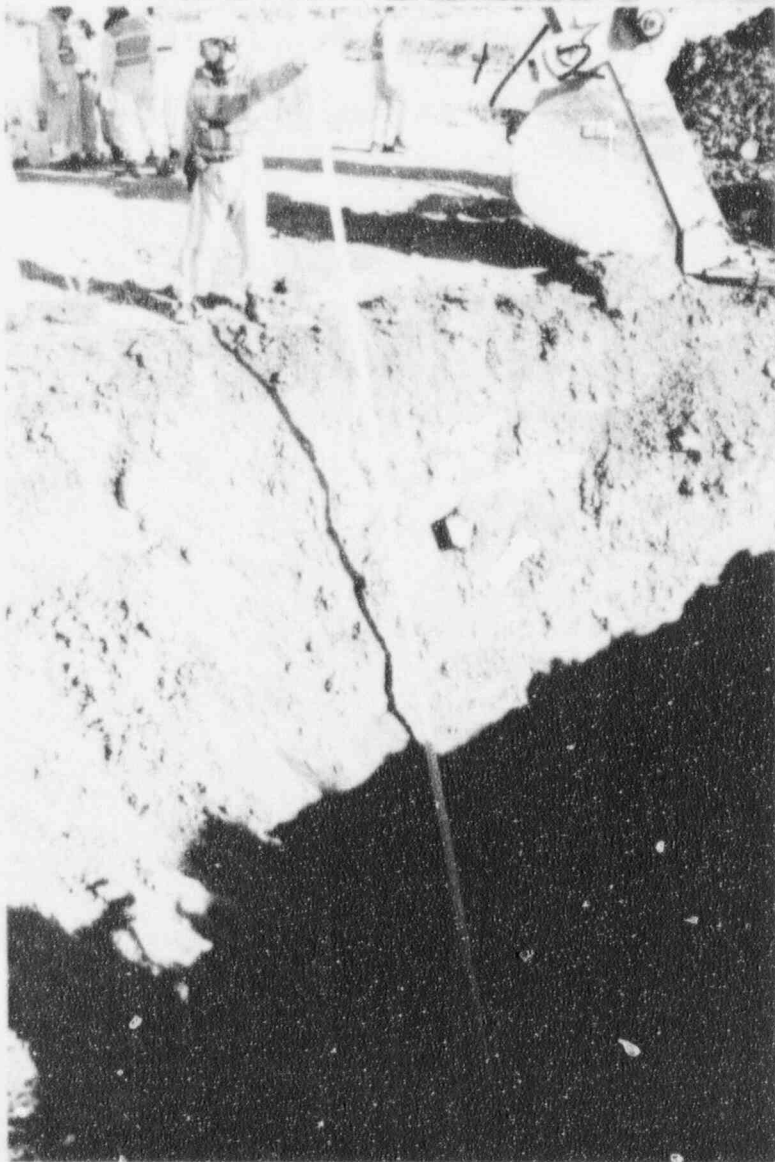


Test Pits were located around the perimeter of the tailings pile and in areas where the tailings have been removed.

2/21



Test Pit Locations



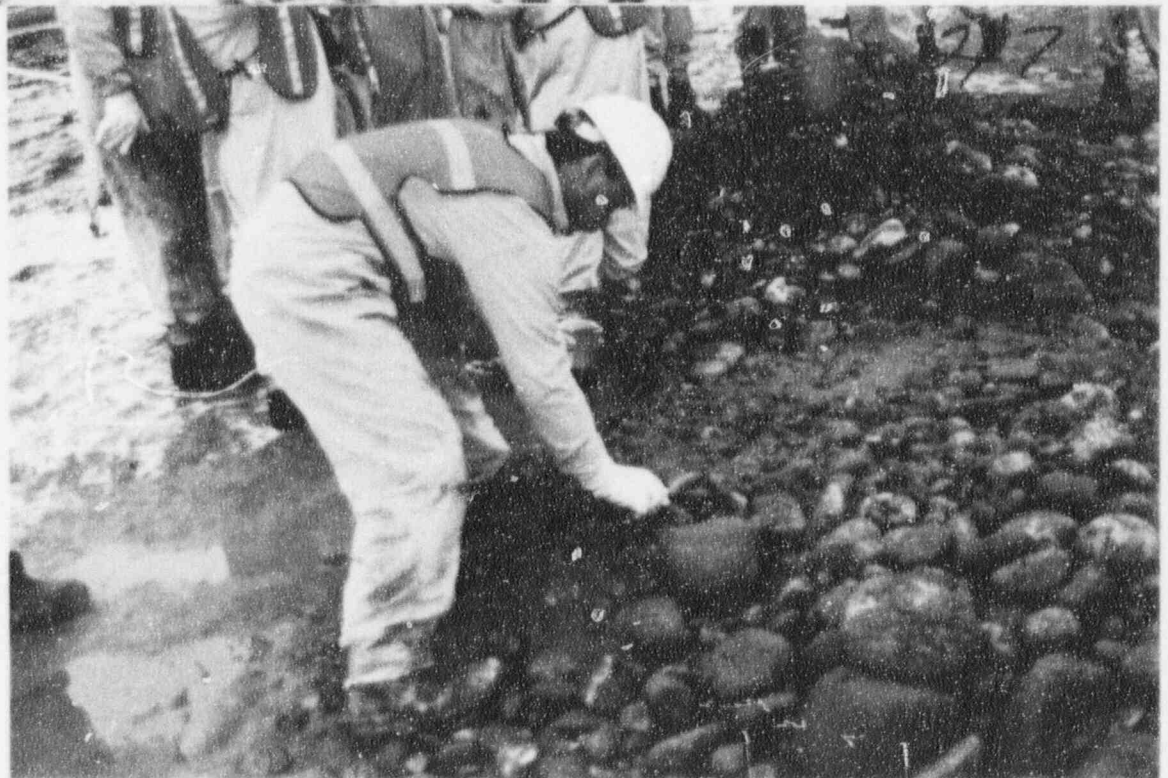
Excavation depths were measured using a survey rod.

Depth of test pit is measured upon completion of the pit.



Samples for radiological analysis were collected from test pit walls.

Samples of the gravel were taken for determination of radioactivity.







Gravel samples were collected in one-foot intervals and placed on plastic sheets in order to carry out the gradation analysis.



Sample of sand gravel and cobbles taken from the test pits.





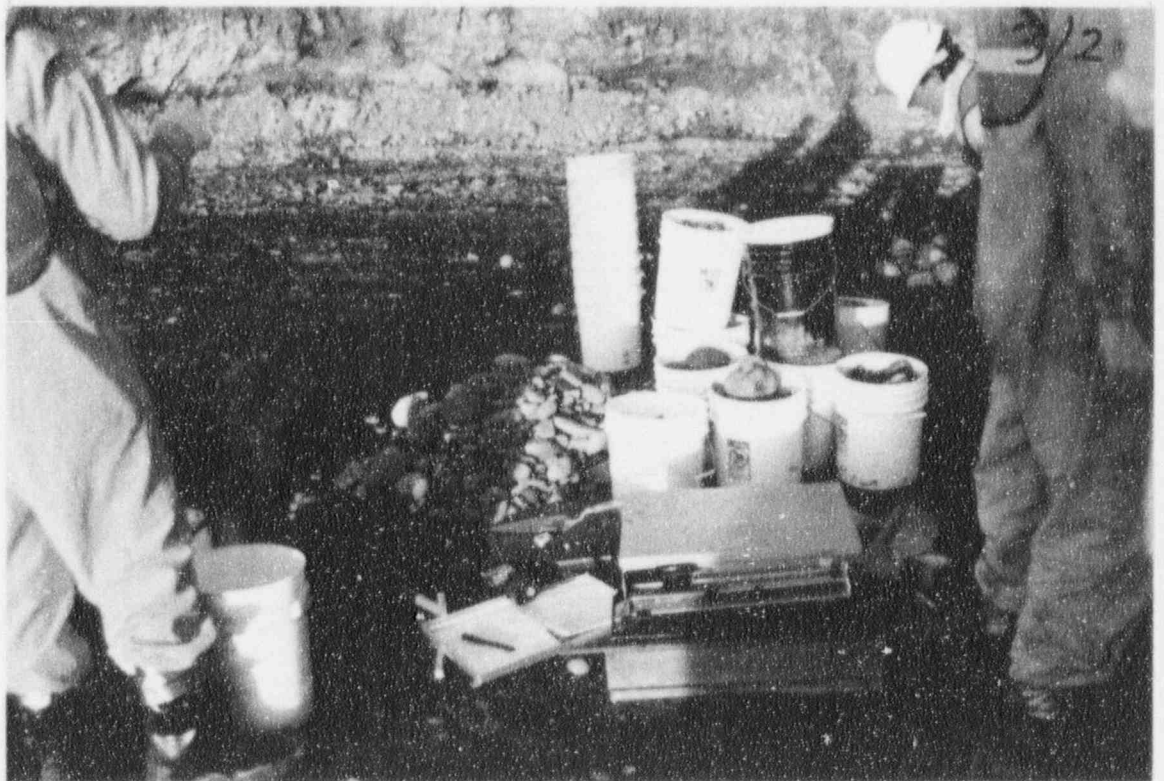
Drying and screening gravel (Cobbles and Fines) samples.



Sample too wet to screen (See photo above).

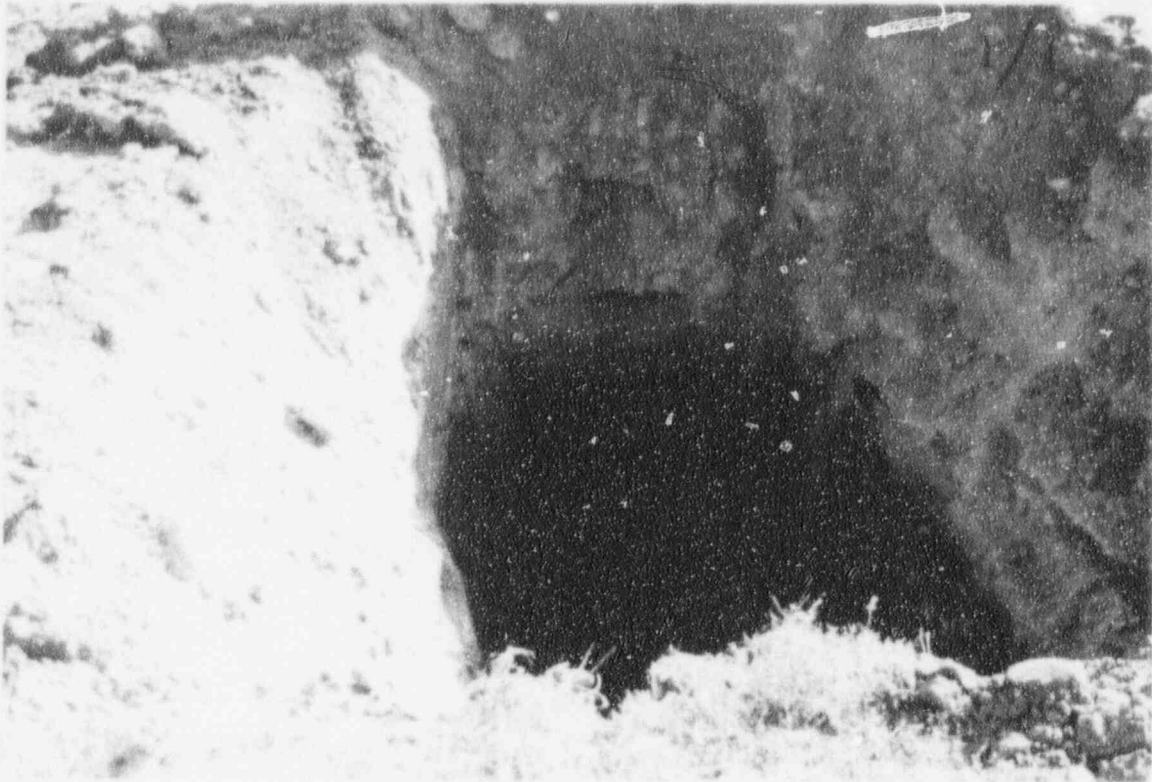


Screening semi-dry samples.



Screening and weighting gravel samples in order to determine the cobbles to fines ratio.

PHOTOS OF TEST PITS

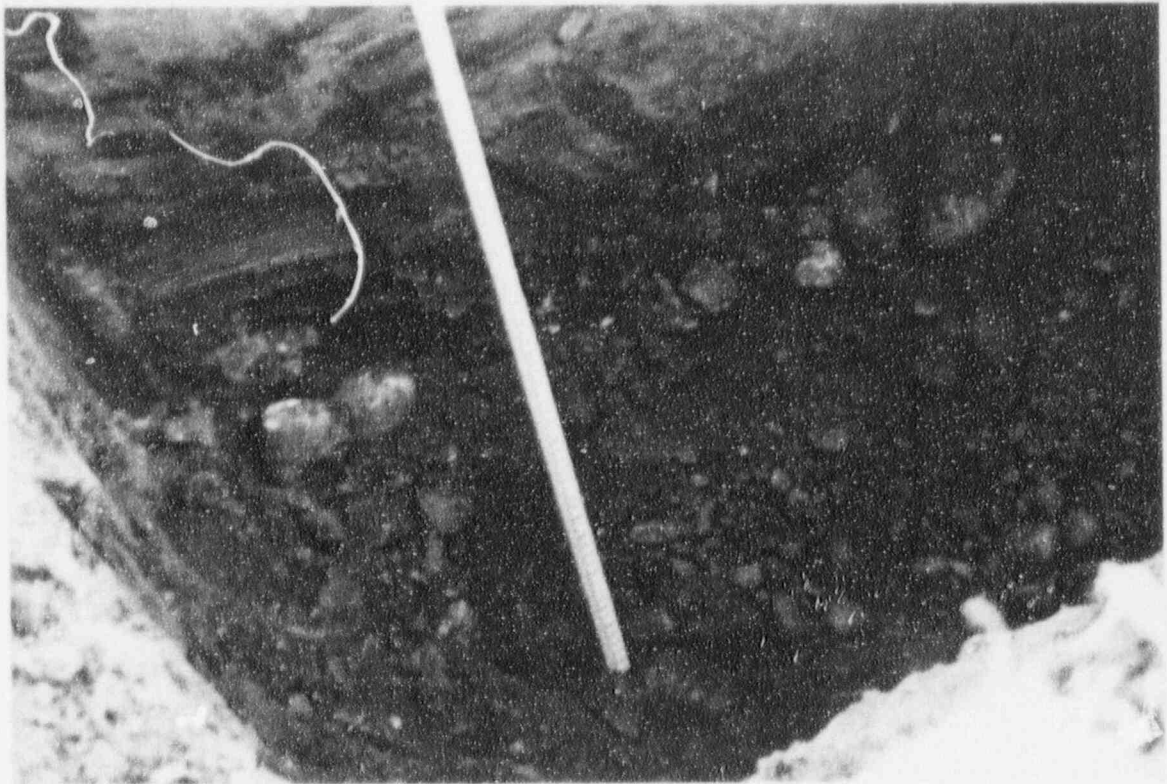


TP M-CF-01. Clay-silt soil overlying gravel deposits.



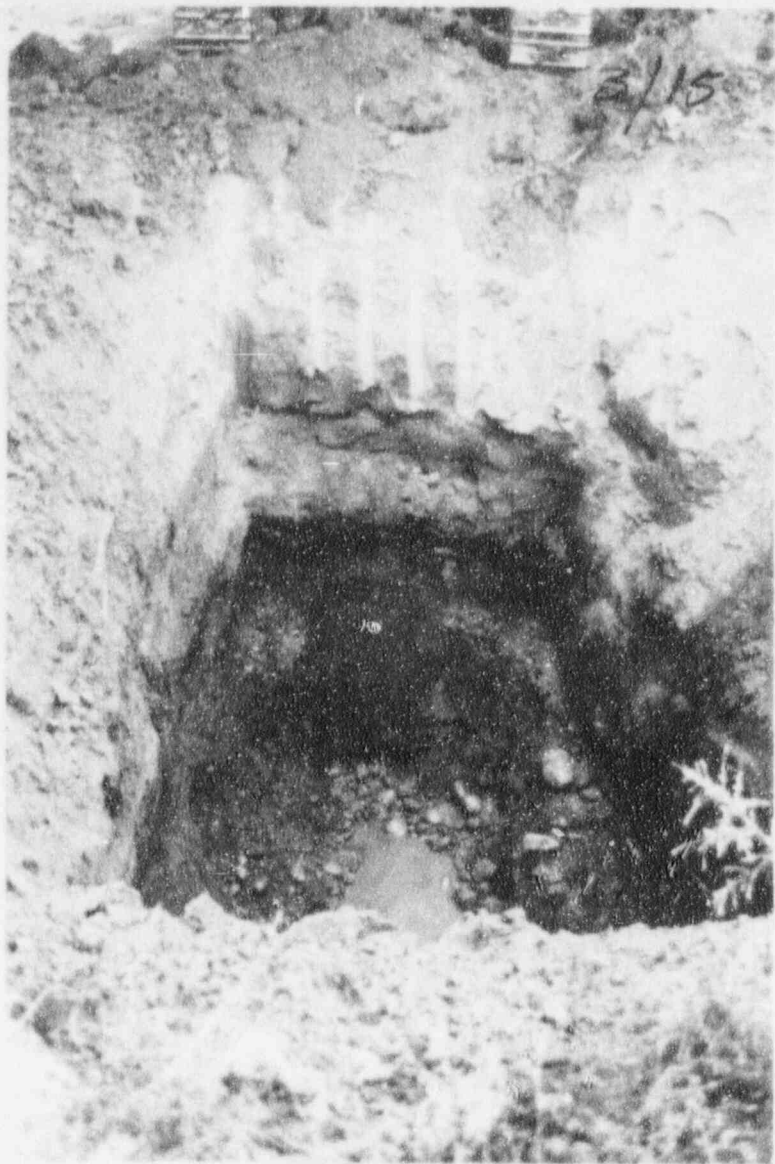
TP M-CF-01. Note organic rich clay layer above gravel deposit.





TP M-CF-01. Note sands, gravels, cobbles and boulders in the bottom of the test pit. Note the carbonaceous coating on the gravels and the film on the water surface.





TP M-CF-02. Note highly carbonaceous (peat) layer.

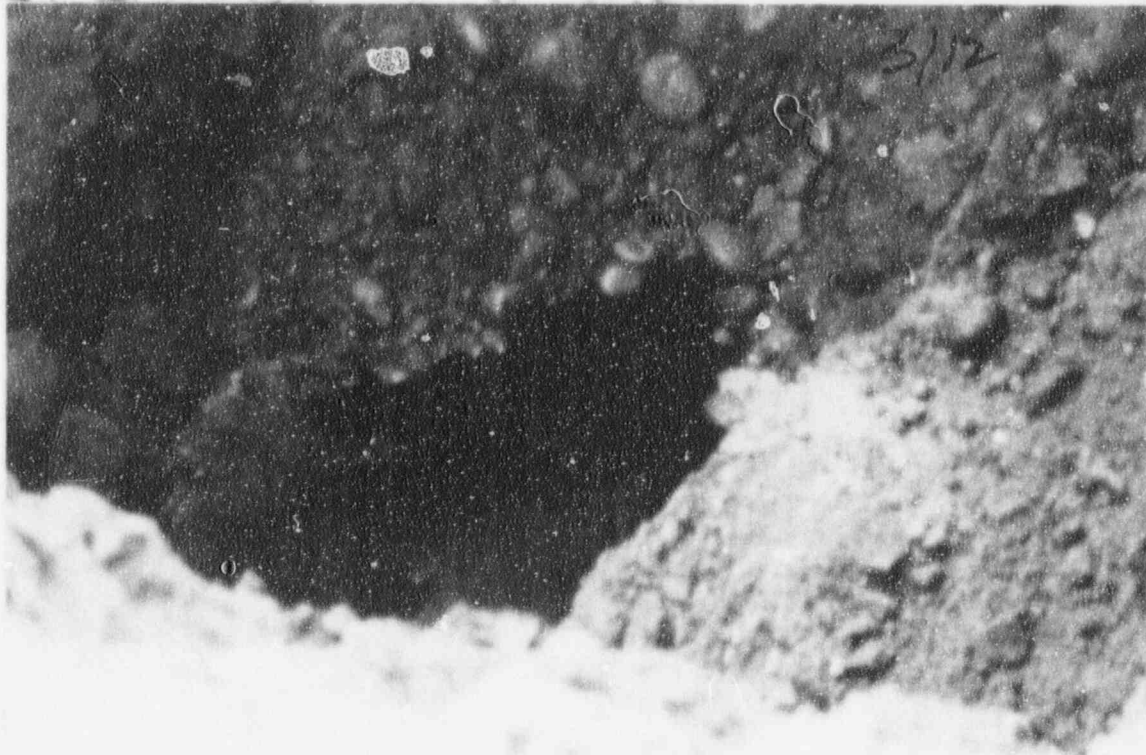
TP M-CF-02. Note film and gas bubbles on water surface in bottom of the test pit.





TP M-CF-03. Very dry soil overlying gravels. Note black carbonaceous coating on gravels.

TP M-CF-03. Bottom of test pit. Note film on surface of the ground water.



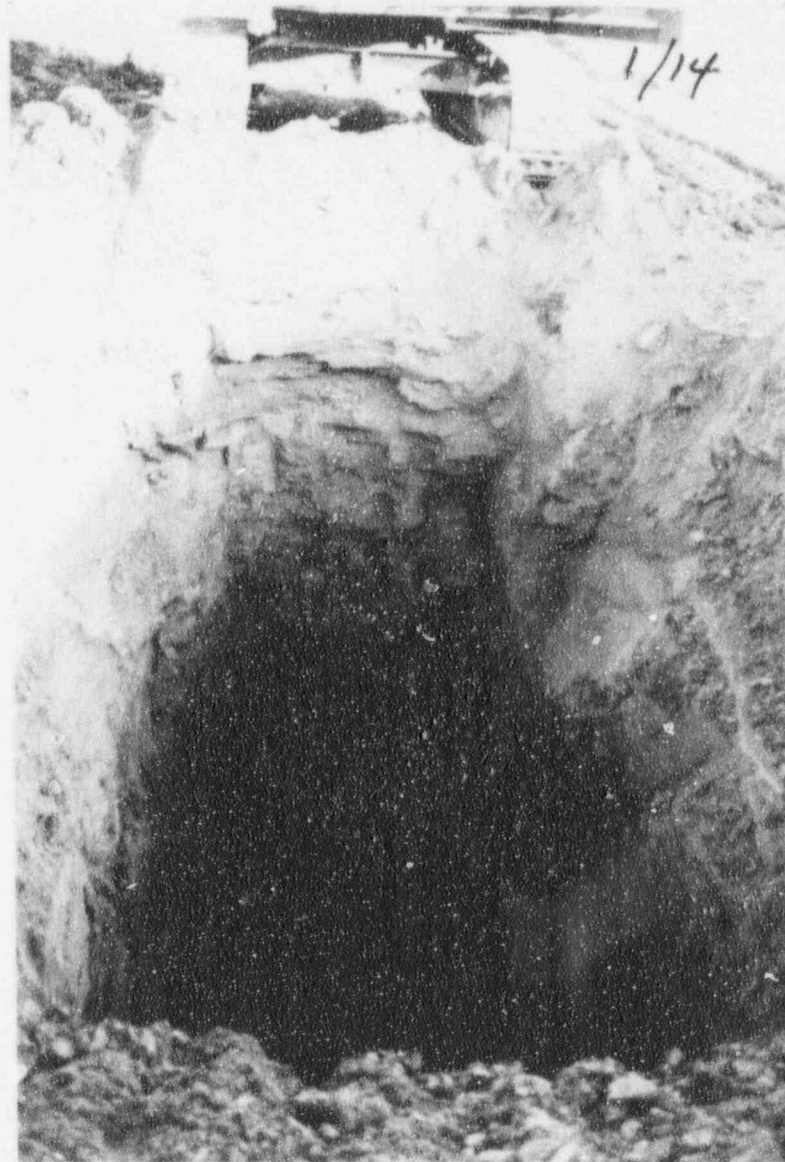


TP M-CF-04. The top five feet of the test pit is in tailings. Personnel are collecting tailings samples for radiological analysis.



TP M-CF-04. Soil profile beneath tailings with gravels in the bottom.





TP M-CF-05. Test pit profile showing lavender colored tailings on top of the original vegetated ground surface. Bottom of test pit shows gravels with a black carbonaceous coating.

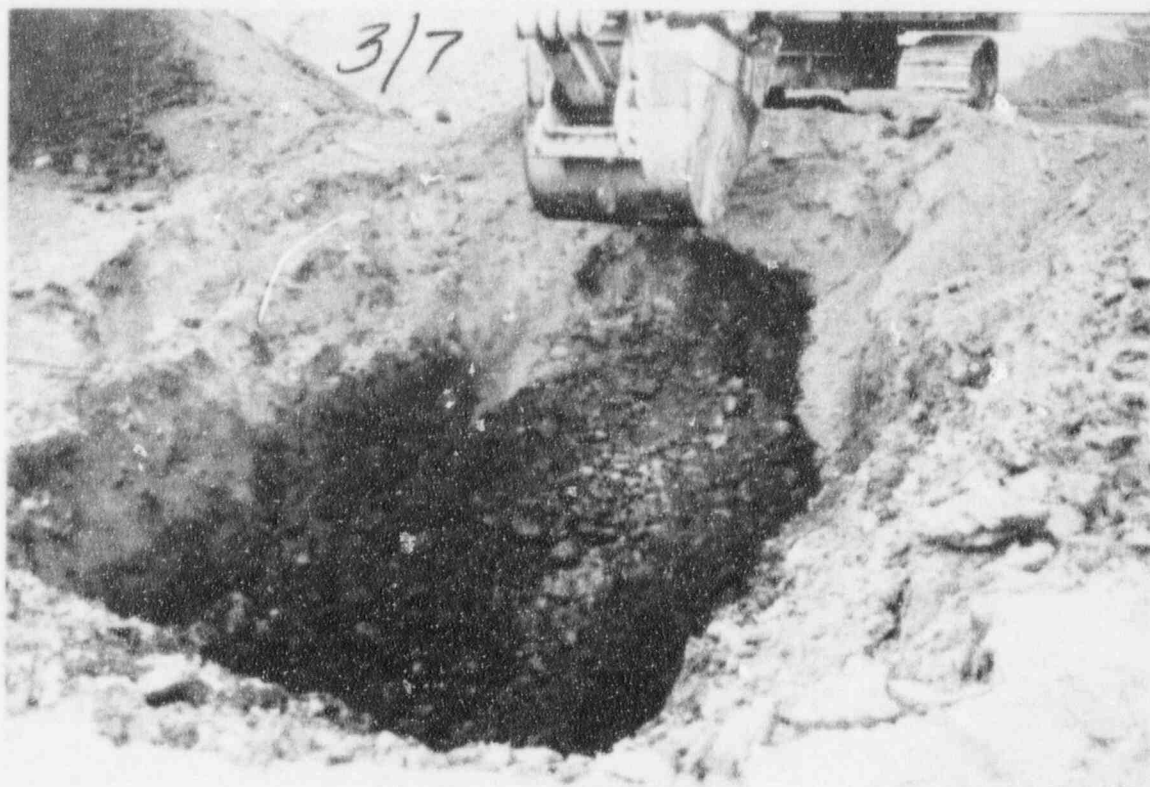


TP M-CF-06. Lavender and yellow tailings overlying clayey soil.  
Bottom of test pit shows slightly carbonaceous gravels.

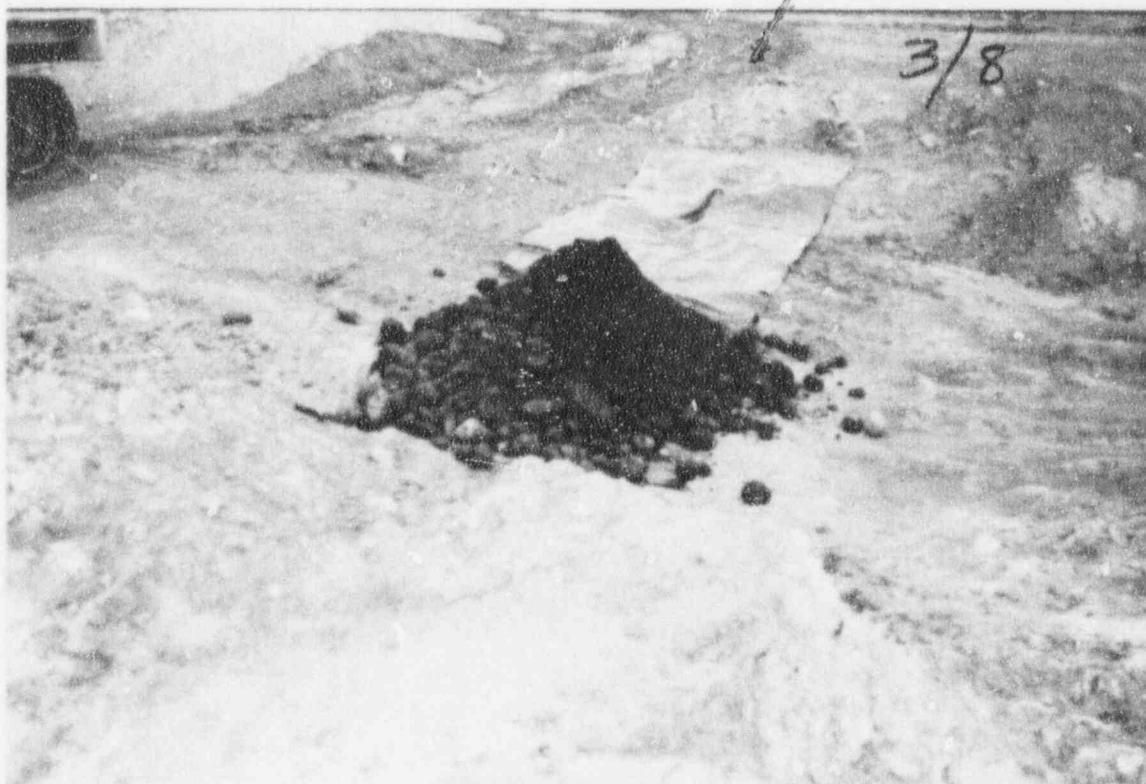




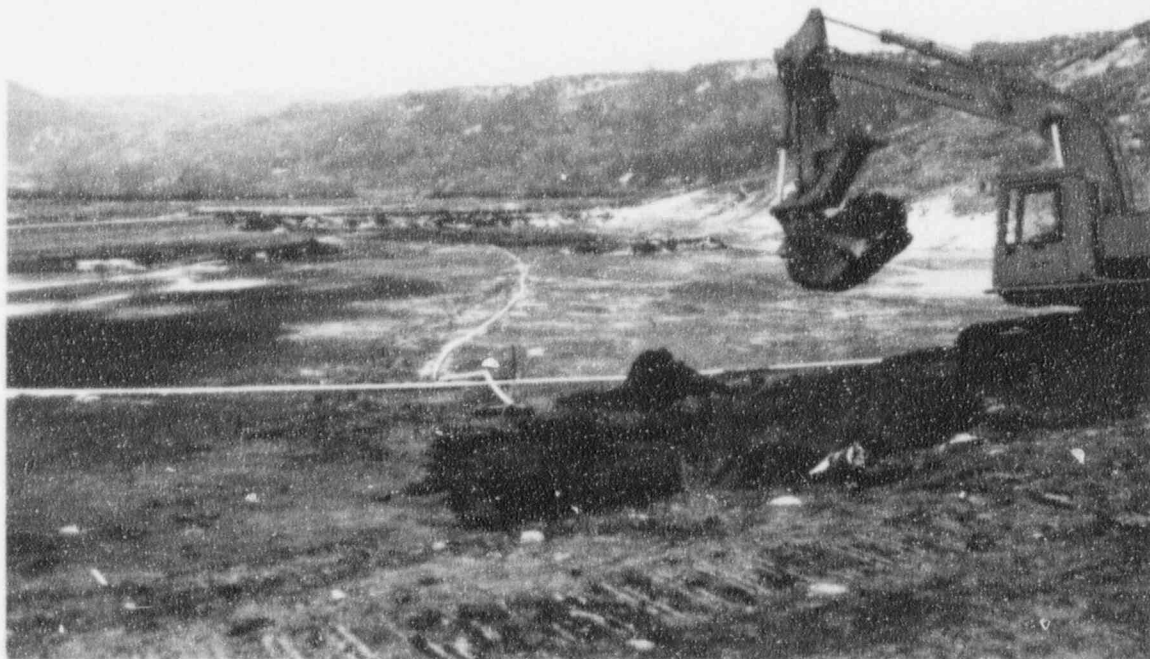
TP M-CF-07. Tailings overlying clay soil and gravels. Perched water in the tailings and equipment vibration caused severe caving of the tailings resulting in contamination of samples from the underlying material.



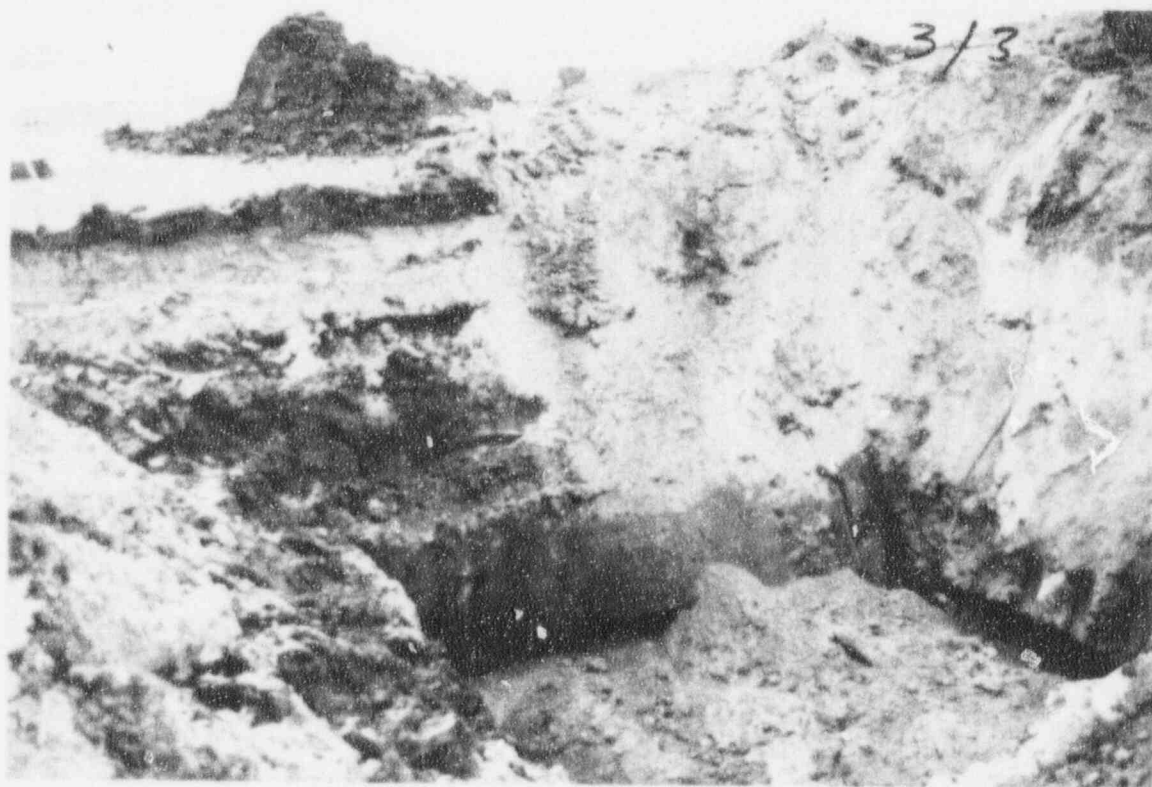
TP M-CF-11. Excavation at old collection pond. Note oxidized and acidified upper sediments (yellow pockets) of tailings. Gravels are highly organic (carbonaceous).



TP M-CF-11. Sample of highly carbonaceous gravels and cobbles.



TP M-CF-15. Excavation at North end of old acid pond.

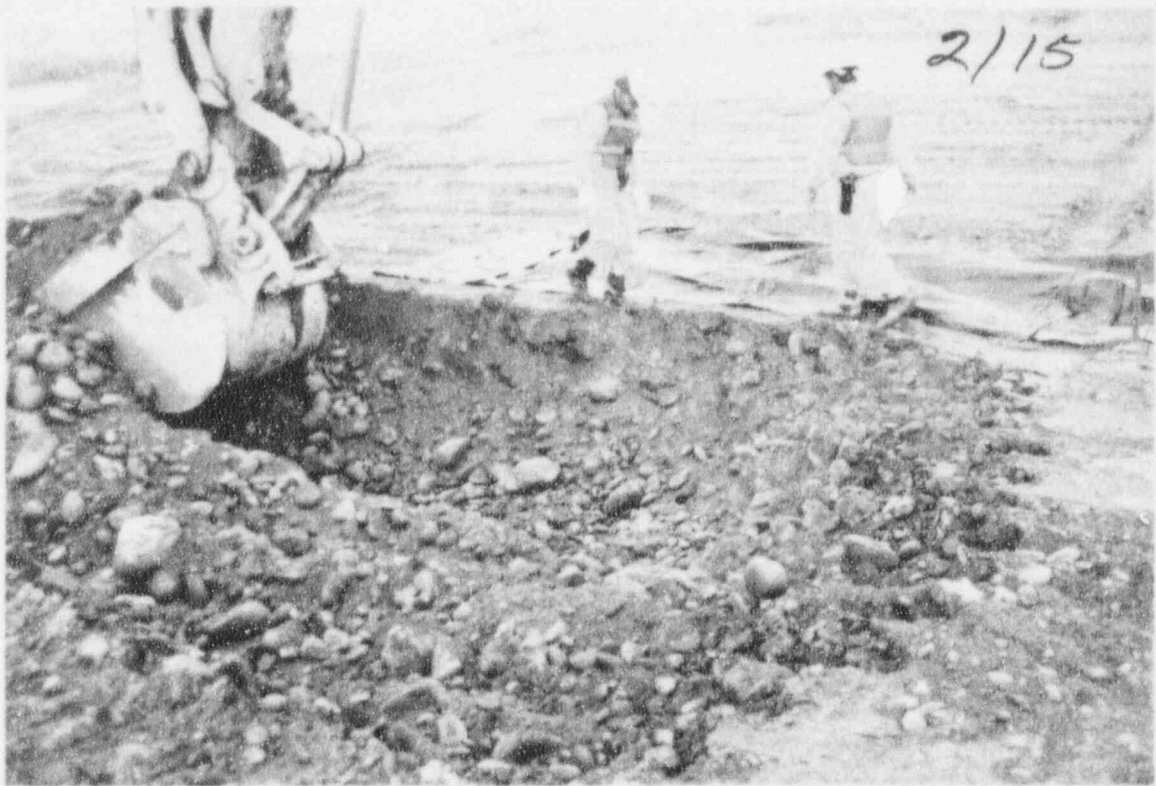


TP M-CF-15. Pond sediments overlying tailings which overlie clay soil in the bottom of the test pit.





TP M-CF-19. Below 5 feet, the backhoe bucket encountered refusal on a cemented layer of gravels and cobbles.



TP M-CF-20. Beginning excavation. Note one inch of tailings on the surface.

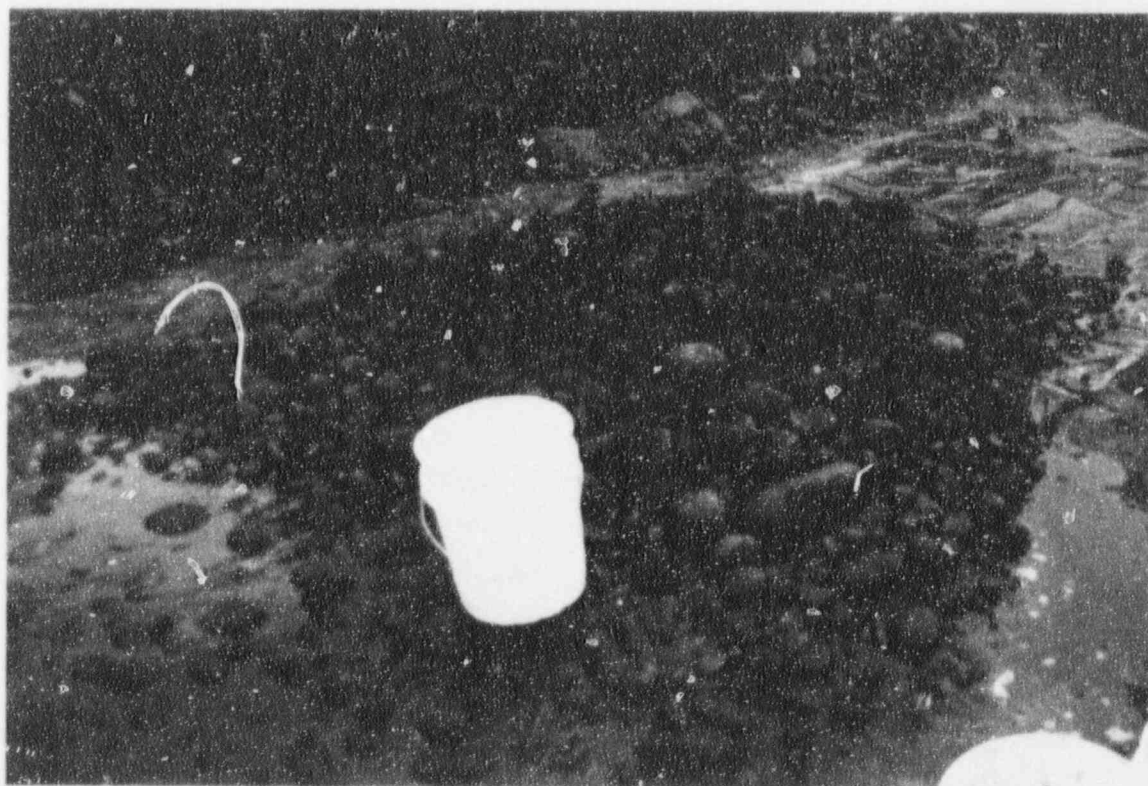


TP M-CF-20. Bottom of test pit in sand, gravel and cobbles. Ground water encountered at a shallow depth.





TP M-CF-22. About 4-feet of road fill overlying the in-situ cobbles and gravels.



TP M-CF-22. Sample of cobbles and boulders with a carbonaceous coating.



TP M-CF-25. Unsuccessful attempt to dewater the pit to allow collection of samples below the water table.

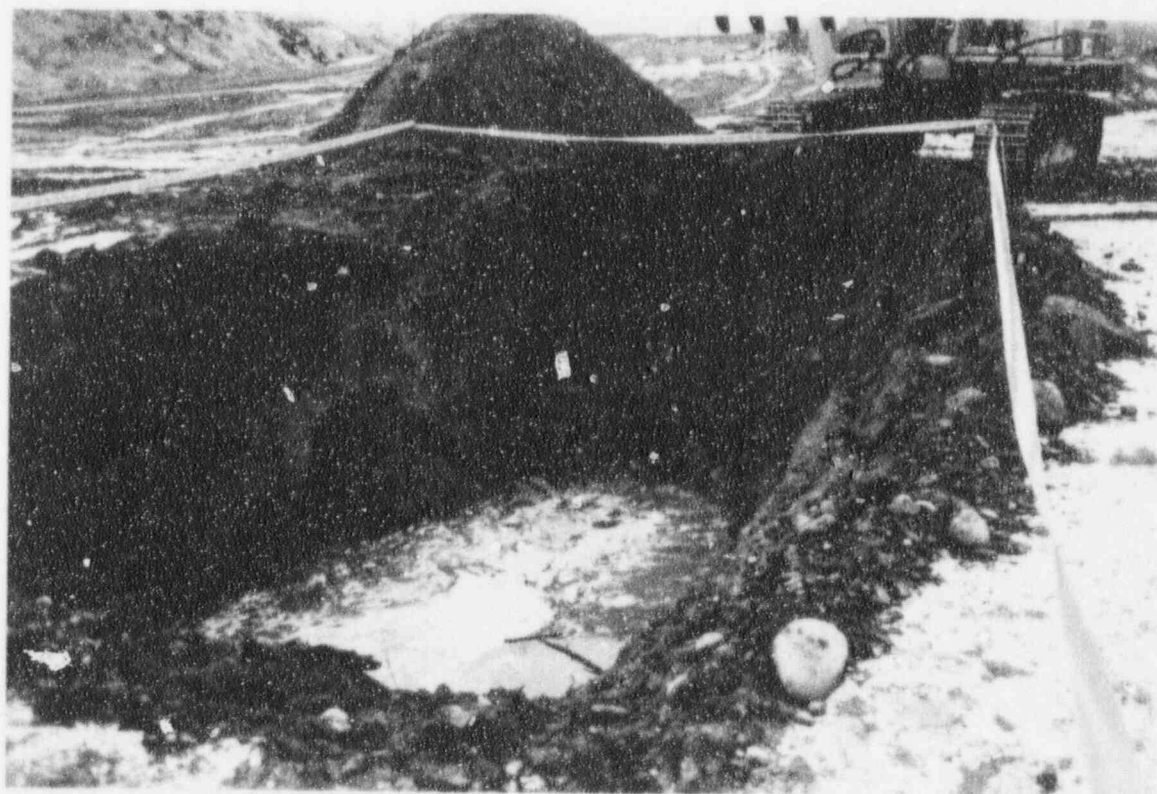


TP M-CF-25. Sample obtained from below the water table (Note how fines have been removed by the flushing action of the water when the water drains out of the sample).





TP M-CF-26. Water encountered at the interface of the soil overburden and the underlying cobbles and gravels.



TP M-CF-26. Water level two hours after excavation.



TP M-CF-27. About 4 feet of fill and wood trash overlying tailings. Bottom of the test pit is in gravels and cobbles.



TP M-CF-28. Entire test pit in gravel, cobbles, and boulders. Black organic coating at 3 feet.





TP M-CF-29. Gravels, cobbles, and boulders overlying a clay layer. Water encountered near the interface.



TP M-CF-31. Sand gravel and cobbles in a background pit.



APPENDIX C  
TEST PIT LOGS

### TEST PIT LOG

PROJECT <b>UMTRA</b>			SITE <b>RIFLE</b>		LOCATION <b>NEW RIFLE, COLORADO</b>		JOB NO. <b>3885-70</b>	TEST PIT NO. <b>M-CF-01</b>
CONTRACTOR <b>GREEN</b>		EXCAVATION METHOD <b>BACKHOE</b>	COORDINATES <b>N25130E46890</b>	BEGUN <b>11/30/93</b>	COMPLETED <b>11/30/93</b>	GROUND ELEV. <b>5275.0</b>	GROUND WATER DEPTH (FT) <b>16.5</b>	LOGGED BY: <b>J. CERCONO/G. LINDSEY</b>
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1	SS-2242		<b>SILTY CLAY, (CL)</b> , low to medium plasticity, brown, dry to moist, vertical roots.  Some calcite casts and stringers at 2 to 4 feet.	24.0	2.2			
	SS-2243			5.5	1.6			
2	SS-2244			4.3	1.8	10±1		FINES: Ra-226 (1,000 year) = 6.3 pCi/gr.
3	SS-2245			2.5	1.1			
4	SS-2246			5.9	1.4			PVC pipe at 4 feet connecting two adjacent sumps.
5	SS-2247			1.9	1.8	3.8±0.8		FINES: Ra-226 (1,000 year) = 2.6 pCi/gr.
6	SS-2248			1.4	1.8			-Plan Exc. Depth at 6.0'
7	SS-2249		1.7	1.7				
8	SS-2250		<b>CLAY-SILT, (CL-ML)</b> , low plasticity, dark gray brown, moist, becoming more clayey with depth.	1.5	2.0			Heavy odor.
9	SS-2251			1.3	1.3			
10	SS-2252			2.0	1.5			
11	SS-2253			1.6	1.5			
12	SS-2254			0.9	1.6		9.5	
13	SS-2255			1.8	1.9	4.5±0.9		FINES: Ra-226 (1,000 year) = 2.7 pCi/gr. Strong odor.
14	SS-2256		<b>GRAVELS, (GW)</b> , with cobbles to 12", well graded, approx. 30-35% fines, cobbles are	2.0	1.6		9.6	
	SS-2257			0.9	1.7			




**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

SHEET  
**1**  
OF  
**2**

TEST PIT NO.  
**M-CF-01**

### TEST PIT LOG

PROJECT <b>UMTRA</b>			SITE <b>RIFLE</b>		LOCATION <b>NEW RIFLE, COLORADO</b>		JOB NO. <b>3885-7C</b>	TEST PIT NO. <b>M-CF-01</b>	
CONTRACTOR <b>GREEN</b>		EXCAVATION METHOD <b>BACKHOE</b>	COORDINATES <b>N25130E46890</b>	BEGIN <b>11/30/93</b>	COMPLETED <b>11/30/93</b>	GROUND ELEV. <b>5275.0</b>	GROUND WATER DEPTH (FT) <b>16.5</b>	LOGGED BY: <b>J. CERcone/G. LINDSEY</b>	
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
16	SS-2258 SS-2259 SS-2260 SS-2261		coated with a black organic stain.	1.0 0.9 1.3 0.9	1.4 1.6 1.4 1.2	0.9±0.4	9.0	☹	FINES: Ra-226 (1,000 year) = 0.1 pCi/gr. Strong organic odor. Film of organic matter on top of ground water.
			BOTTOM OF TEST PIT AT 17.5'						COBBLES (Composite): Sample Depth 15' to 17'. Ra-226 Th-232 Th-230 Ra-226(1,000 yr) 1.1±0.6 1.1±0.4 FINES (Composite): Sample Depth 15' to 17'. Ra-226 Th-232 Th-230 Ra-226(1,000 yr) 4.6±1.1 3.1±0.7 +#4 sieve = 83.1% -#4 sieve = 16.9%







**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

SHEET  
**2**  
OF  
**2**

TEST PIT NO.  
**M-CF-01**

### TEST PIT LOG

PROJECT <b>UMTRA</b>			SITE <b>RIFLE</b>		LOCATION <b>NEW RIFLE, COLORADO</b>		JOB NO. <b>3885-70</b>	TEST PIT NO. <b>M-CF-02</b>
CONTRACTOR <b>GREEN</b>		EXCAVATION METHOD <b>BACKHOE</b>	COORDINATES <b>N25130 E47190</b>	BEGUN <b>12/2/93</b>	COMPLETED <b>12/2/93</b>	GROUND ELEV. <b>5274.6</b>	GROUND WATER DEPTH (FT) <b>15.0</b>	LOGGED BY <b>J. CERCONE/G. LINDSEY</b>
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226	Th-232	Th-230	pH	REMARKS PHOTOGRAPH
				pCi/gr	pCi/gr	pCi/gr		
1	SS-2492		<b>SILTY CLAY, (CL), low plasticity, med. brown, slightly moist to dry, some roots.</b>	2.2	1.3			Upper 6" frozen ground. Soil profile appears to represent several periods of deposition (Paleo Soils).  FINES: Ra-226 (1,000 year) = 1.6 pCi/gr.  -Plan Exc. Depth at 5'.
	SS-2493			1.1	1.6			
2	SS-2494			1.9	2.6	1.0±0.4		
3	SS-2495			3.0	2.2			
4	SS-2496			1.0	1.8			
5	SS-2497			1.1	1.8			
6	SS-2498		<b>SILT, (ML), low plasticity, reddish brown, moist, loose.</b>	1.3	1.5			Strong aromatic odor.
7	SS-2499			2.3	1.6	9.2		
8	SS-2500		<b>SILTY CLAY, (CL), low plasticity, gray to black, moist, abundant organic material (carbonaceous).</b>	1.5	1.6			
9	SS-2501			1.4	1.2			
10	SS-2502			0.6	1.3			
11	SS-2503			1.3	1.7			
	SS-2504			1.7	1.3			
12	SS-2505				<b>PEAT, organic material layer.</b>	1.4	1.3	9.3
	SS-2506	<b>GRAVELS, (GM), 2.5" max., poorly graded in a silty matrix.</b>	2.0			1.5		
13	SS-2507		1.2			1.4		
	SS-2508			1.8	1.5			



**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

SHEET  
**1**  
OF  
**2**

TEST PIT NO.  
**M-CF-02**



### TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.
UMTRA			RIFLE		NEW RIFLE, COLORADO		3885-70	M-CF-02
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:
GREEN		BACKHOE	N25130 E47190	12/2/93	12/2/93	5274.6	15.0	J. CERCONE/G. LINDSEY
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
15	SS-2509		GRAVELS, (GP), with cobbles to 12", poorly graded in a sandy matrix (20-50%) cobbles average 3"-6" (30-35%).	1.1	1.3			Film of organic matter on water surface (gas bubbling up to surface).  COBBLES (Composite): Sample Depth 13' to 16'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.7±0.5 0.9±0.4 FINES (Composite): Sample Depth 13' to 16'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 1.7±0.7 2.3±0.6 + #4 sieve = 68.3% - #4 sieve = 31.7%
	SS-2510			1.8	1.6			
	SS-2511			1.1	1.5			
16	SS-2512			1.4	1.3			
	SS-2513			1.0	1.8			
	SS-2514			1.4	1.9			
17	SS-2515			1.1	1.4		9.2	
	SS-2516			1.6	1.5			
18	SS-2517			1.8	1.3			
	SS-2518		BOTTOM OF TEST PIT AT 18.0'	1.7	1.3			



**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

SHEET  
2  
OF  
2

TEST PIT NO.  
**M-CF-02**

# TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.
<b>UMTRA</b>			<b>RIFLE</b>		<b>NEW RIFLE, COLORADO</b>		<b>3885-70</b>	<b>M-CF-03</b>
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:
<b>GREEN</b>		<b>BACKHOE</b>	<b>N25170 E47450</b>	<b>12/2/93</b>	<b>12/2/93</b>	<b>5278.4</b>	<b>21.0</b>	<b>J. CERCOONE/G. LINDSEY</b>
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Tl-232 pCi/gr	Tl-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1			POND SEDIMENT, silt in a CaCO3 matrix, buff colored with a surface covering of 2"-3" of yellowish silty sand.					
2	SS-2519		SILTY CLAY, (CL), low plasticity, light brown, dry, roots (trace).	1.4	1.5		5.7	
3	SS-2520			2.0	1.5	4.1+0.8		FINES: Ra-226 (1,000 year) = 2.7 pCi/gr.
4	SS-2521			2.0	1.7		8.8	
5	SS-2522		Sandy silt, light brown, dry.	9.8	1.6			Plan Exc. Depth at 5' to 6'.
6	SS-2523			1.5	1.3			
7	SS-2524		Silty-clay, low plasticity, med. brown, slightly moist.	1.1	1.5			
8	SS-2525			1.4	1.4		8.8	
9	SS-2526			1.3	1.3		8.8	
10	SS-2527			1.3	1.5			
11	SS-2528		CLAY, (CL), med. to low plasticity, brown, moist, 4" to 6" thick layers.	1.2	1.4			
12	SS-2529			1.4	1.4			
13	SS-2530		Interlayered seams of sand and silt.	0.9	1.4			
14	SS-2531			1.2	1.3			




**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

SHEET  
1  
OF  
2

TEST PIT NO.  
**M-CF-03**

### TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.
<b>UMTRA</b>			<b>RIFLE</b>		<b>NEW RIFLE, COLORADO</b>		<b>3885-70</b>	<b>M-CF-03</b>
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:
<b>GREEN</b>		<b>BACKHOE</b>	<b>N25170 E47450</b>	<b>12/2/93</b>	<b>12/2/93</b>	<b>5278.4</b>	<b>21.0</b>	<b>J. CERONE/G. LINDSEY</b>
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
16	SS-2532			1.1	1.6			
	SS-2533			1.6	1.4		9.0	
17	SS-2534			1.0	1.7			
18	SS-2535		<b>GRAVELS, (GP), with cobbles and boulders, coated with black carbonaceous material.</b>	1.7	1.3			Strong aromatic (organic) odor.
	SS-2536			0.9	0.6			
19	SS-2537			0.9	1.2			
	SS-2538			1.6	2.1			
20	SS-2539			0.9	1.0		8.2	
	SS-2540			0.9	1.2			
21								▼ Film of organic matter on water surface (Gas bubbles coming up through the water).
22								
			BOTTOM OF TEST PIT AT 22.5'					COBBLES (Composite): Sample Depth 18' to 21'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 1.7±0.7                    0.5±0.3 FINES (Composite): Sample Depth 18' to 21'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 1.9±0.7                    5.7±1.0 +#4 sieve = 70.4% -#4 sieve = 29.6%

### TEST PIT LOG

PROJECT <b>UMTRA</b>			SITE <b>RIFLE</b>		LOCATION <b>NEW RIFLE, COLORADO</b>		JOB NO. <b>3885-70</b>	TEST PIT NO. <b>M-CF-04</b>
CONTRACTOR <b>GREEN</b>		EXCAVATION METHOD <b>BACKHOE</b>	COORDINATES <b>N24890 E46900</b>	BEGUN <b>11/30/93</b>	COMPLETED <b>11/30/93</b>	GROUND ELEV. <b>5274.5</b>	GROUND WATER DEPTH (FT) <b>16.5</b>	LOGGED BY: <b>J. CERCONE/G. LINDSEY</b>
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Tn-232 pCi/gr	Tn-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1			<b>TAILINGS, (ML-SP), silty sand, gray to reddish brown, moist, yellowish-brown seam (1.0 ft thick).</b>					
2							5.45	pH Depth: 1'-4'.
3			Color changed to gray with brown spots.					
4								
5	SS-2267		<b>CLAY, (CL), low plasticity, (TOPSOIL), brown, moist to wet.</b>	85.0	3.7			Vegetation visible at interface.
6	SS-2268			92.0	4.0	32±2.0		FINES: Ra-226 (1,000 year) = 71.0 pCi/gr.
7	SS-2269			1.2				
8	SS-2270		Saturated (Perched water?).	44.0				
9	SS-2271		Gypsum stringers.	1.6	1.4			
10	SS-2272			13.0	1.9	7.6±1.1		FINES: Ra-226 (1,000 year) = 11.1 pCi/gr.
11	SS-2273			12.0	1.8			
12			<b>SILTY GRAVEL, (GM), aromatic organic odor, some organic coating.</b>				8.1	
13	SS-2274		<b>GRAVELS, (GW-GP), with cobbles and boulders to 16".</b>	2.7	1.6			-Plan Excav. Depth 13'.
14	SS-2275			2.1	1.5			
	SS-2276			* 10.0	1.8			
	SS-2277			* 14.0	1.8			










**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

SHEET  
**1**  
OF  
**2**

TEST PIT NO.  
**M-CF-04**



### TEST PIT LOG


PROJECT <b>UMTRA</b>			SITE <b>RIFLE</b>			LOCATION <b>NEW RIFLE, COLORADO</b>			JOB NO. <b>3885-70</b>	TEST PIT NO. <b>M-CF-04</b>
CONTRACTOR <b>GREEN</b>		EXCAVATION METHOD <b>BACKHOE</b>	COORDINATES <b>N24890 E46900</b>	BEGIN <b>11/30/93</b>	COMPLETED <b>11/30/93</b>	GROUND ELEV <b>5274.5</b>	GROUND WATER DEPTH (FT) <b>16.5</b>		LOGGED BY: <b>J. CERONE/G. LINDSEY</b>	
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH	
16	SS-2278			2.7	1.6			▼		
	SS-2279			3.2	1.2					
	SS-2280			* 11.0	1.3					
17	SS-2281			* 10.0	1.4					
	SS-2282			* 28.0	2.4					
	SS-2283			* 51.0	2.5					
18	SS-2284			* 15.0	1.7		7.8			
19			BOTTOM OF TEST PIT AT 19.0'							



### TEST PIT LOG

PROJECT <b>UMTRA</b>			SITE <b>RIFLE</b>		LOCATION <b>NEW RIFLE, COLORADO</b>		JOB NO. <b>3885-70</b>	TEST PIT NO. <b>M-CF-04A</b>
CONTRACTOR <b>GREEN</b>		EXCAVATION METHOD <b>BACKHOE</b>	COORDINATES <b>N24890 E46900</b>	BEGUN <b>11/30/93</b>	COMPLETED <b>11/30/93</b>	GROUND ELEV. <b>5274.5</b>	GROUND WATER DEPTH (FT) <b>16.5</b>	LOGGED BY: <b>J. CERCOONE/G. LINDSEY</b>
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-231 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1								
2								
3								
4								
5								
6								
7								
8								
9								
10								
11	SS-2463		SILTY GRAVEL, (GM), aromatic organic odor, some organic coating.	8.5	1.6			
	SS-2464			11.0	2.0	9.3±1.2		FINES: Ra-226 (1,000 year) = 10.4 pCi/gr.
12	SS-2465			17.0	2.0			
	SS-2466		GRAVELS, (GW-GP), with cobbles and boulders to 16".	17.0	1.5			
13	SS-2467			9.2	1.9		8.1	-Plan Excav. Depth 13'.
	SS-2468			11.0	1.4			
14	SS-2469			3.2	1.5			
	SS-2470			4.2	1.5			

### TEST PIT LOG

PROJECT <b>UMTRA</b>			SITE <b>RIFLE</b>		LOCATION <b>NEW RIFLE, COLORADO</b>		JOB NO. <b>3885-70</b>	TEST PIT NO. <b>M-CF-04A</b>
CONTRACTOR <b>GREEN</b>		EXCAVATION METHOD <b>BACKHOE</b>	COORDINATES <b>N24890 E46900</b>	BEGUN <b>11/30/93</b>	COMPLETED <b>11/30/93</b>	GROUND ELEV <b>5274.5</b>	GROUND WATER DEPTH (FT) <b>16.5</b>	LOGGED BY: <b>J. CERCONO/G. LINDSEY</b>
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
16	SS-2471 SS-2472 SS-2473 SS-2474			1.9 2.4 2.4 2.1	1.5 1.6 1.1 1.2			
19			BOTTOM OF TEST PIT AT 19.0'					<p>COBBLES (Composite): Sample depth 11' to 16'.  Ra-226    Th-232    Th-230    Ra-226 (1,000 yr)  0.6±0.5            0.7±0.3</p> <p>FINES (Composite): Sample depth 11' to 16'.  Ra-226    Th-232    Th-230    Ra-226 (1,000 yr)  7.4±1.4            6.6±1.0</p> <p>+ #4 sieve = 76.1%  - #4 sieve = 23.9%</p>



**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

SHEET  
**2**  
OF  
**2**

TEST PIT NO.  
**M-CF-04A**

### TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.
UMTRA			RIFLE		NEW RIFLE, COLORADO		3885-70	M-CF-05
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:
GREEN		BACKHOE	N24890 E47140	11/30/93	11/30/93	5273.7	18.0	J. CERCONO/G. LINDSEY
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1			TAILINGS, (SM), silty sand, gray, moist to saturated, with interbedded 6" to 8" thick layers of slimes.					
2							5.0	pH Depth: 1'-6".
3								
4								
5								
6			5.5'-6.0' Slime layer lavender color, saturated.					
7								
8								
9								
10			CLAY, (CL), low plasticity, brown, moist, dry vegetation and roots.				4.9	Vegetation visible at interface.
11	SS-2295			3.0	1.8			
12	SS-2296		SANDY SILT, (ML), dark brown, with some roots.	1.3	1.8	1.2±0.5	7.4	FINES: Ra-226 (1,000 year) = 1.3 pCi/gr.
13	SS-2297		CLAY, (CL), black, moist to saturated, carbonaceous.	1.8	1.6			-Plan Exc. Depth at 13'.
14	SS-2298			1.1	1.9			
15	SS-2300		Silty clay, light brown, thinly bedded.	1.1	1.6			
16	SS-2301		GRAVELS, (GP), with cobbles to 6".	1.6	1.2		7.2	COBBLES (Composite): Sample Depth 16' to 21'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 1.4±0.6 0.3±0.2
17	SS-2302			5.5	1.3			
18	SS-2304			5.7	1.3			
18	SS-2305			1.1	1.1			FINES (Composite): Sample Depth 16' to 21'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 2.5±0.8 2.3±0.6
18	SS-2306			1.3	1.1			
19	SS-2307			4.1	1.2			
19	SS-2308			3.6	1.4			
19	SS-2309			3.1	1.1			
20			BOTTOM OF TEST PIT AT 20.0'					



**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

SHEET  
1  
OF  
1

TEST PIT NO.  
**M-CF-05**



### TEST PIT LOG

PROJECT <b>UMTRA</b>			SITE <b>RIFLE</b>		LOCATION <b>NEW RIFLE, COLORADO</b>		JOB NO. <b>3885-70</b>	TEST PIT NO. <b>M-CF-06</b>
CONTRACTOR <b>GREEN</b>		EXCAVATION METHOD <b>BACKHOE</b>	COORDINATES <b>N24890 E47380</b>	BEGUN <b>11/30/93</b>	COMPLETED <b>11/30/93</b>	GROUND ELEV. <b>5276.8</b>	GROUND WATER DEPTH (FT) <b>18.8</b>	LOGGED BY: <b>J. CERCONE/G. LINDSEY</b>
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1			<b>TAILINGS, (SM), silty sand, gray, moist, loose, several seams and pockets of green slimes.</b>					
2								
3								
4							5.0	pH Depth: 1'-8'.
5								
6								
7			Becoming pale yellow.					
8								
9								
10								Tailings were caving into the pit during the excavation. Consequently, no cobbles to fines samples were taken.
11								
12							5.0	pH Depth: 8'-15'.
13			Original ground surface.					
14	SS-2310		<b>SANDY CLAY, (CL), brown, moist.</b>	2.3	1.4	1.6±0.5		FINES: Ra-226 (1,000 year) = 2.1 pCi/gr.



**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION








SHEET  
**1**  
OF  
**2**

TEST PIT NO.  
**M-CF-06**



### TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.
UMTRA			RIFLE		NEW RIFLE, COLORADO		3885-70	M-CF-06
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:
GREEN		BACKHOE	N24890 E47380	11/30/93	11/30/93	5276.8	18.8	J. CERCONE/G. LINDSEY
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
16								-Plan Exc. Depth 16'.
17			GRAVELS, (GP), with cobbles to 6", sand matrix of 30%-40% fines, average size cobble is 3" 4", max. cobble size is 8".					
18								
19								
20								
21								
22								
23								
24	SS-2313			* 85.0	3.0		6.5	
	SS-2314			* 41.0	2.5			
25				BOTTOM OF TEST PIT AT 25.0'				
								COBBLES (Composite): Sample Depth 18' to 22'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 3.3±0.9                    1.6±0.5

### TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.
UMTRA			RIFLE		NEW RIFLE, COLORADO		3885-70	M-CF-07
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:
GREEN		BACKHOE	N24850 E47500	12/2/93	12/2/93	5277.9	Not Encountered	G.LINDSEY
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1			<b>TAILINGS, (SM)</b> silty sand, fine, gray.					
2			Reddish brown color from 1'-5'.					
3								
4								
5			Turning to purple color.					
6			Clayey slimes.					
7								
8								
9								
10								
11			Very wet, possibly perched water.					
12								
13								
14	SS-2541		<b>CLAY, (CL)</b> , silty, dark gray, carbonaceous.	1.5	1.6		4.9	-Plan Exc. Depth at 14'.
15	SS-2542			3.0	1.4	1.8±0.5	4.9	FINES: Ra-226 (1,000 year) = 2.6 pCi/gr.
16	SS-2543			2.0	1.2			
17	SS-2544		<b>GRAVELS, (GP)</b> , with cobbles to 12".	5.9	1.3	4.2±0.8		FINES: Ra-226 (1,000 year) = 5.3 pCi/gr.
18	SS-2545			8.2	1.3			* Possible Cross Contamination.
19	SS-2546			* 17.0	1.5			COBBLES (Composite): Sample Depth 17'-21'
20	SS-2547			* 20.0	1.5			Ra-226 Th-232 Th-230 Ra-226 (1,000 yr)
21								2.0±0.7 1.7±0.5
								FINES (Composite): Sample Depth 17'-21'
								Ra-226 Th-232 Th-230 Ra-226 (1,000 yr)
								220±10 120±4
								+ #4 sieve = 73.1%
								- #4 sieve = 26.9%
			BOTTOM OF TEST PIT AT 21.0'					

### TEST PIT LOG

PROJECT			SITE			LOCATION			JOB NO.	TEST PIT NO.
UMTRA			RIFLE			NEW RIFLE, COLORADO			3885-70	M-CF-11
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:		
GREEN		BACKHOE	N24700 E47670	12/2/93	12/2/93	5268.0	10.0	G.LINDSEY		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH	
1			TAILINGS, (ML), silt, light gray with red brown oxidized yellow slimes.							
2			CLAY, (CL), silty, dark brown, moist.							
3	SS-2437		Silty clay, carbonaceous.	0.9	1.3	1.2±0.5	6.6		FINES: Ra-226 (1,000 year) = 1.0 pCi/gr.	
4	SS-2438			16.0	2.2		8.5			
5	SS-2439			6.5	1.5		8.2		-Plan Exc. Depth at 5'.	
6	SS-2440				GRAVELS, (GP), with cobbles to 12", black, carbonaceous.	2.4	1.7	7.7±1.1		FINES: Ra-226 (1,000 year) = 4.3 pCi/gr.
7	SS-2441			2.5	1.2					
8	SS-2442			3.2	1.3	22±2		FINES: Ra-226 (1,000 year) = 9.8 pCi/gr.		
9	SS-2443			3.6	1.0					
10	SS-2444			2.0	1.1					
11	SS-2445			2.2	1.1					
12	SS-2446			7.1	1.3	25±2	8.8	FINES: Ra-226 (1,000 year) = 16.3 pCi/gr.		
13	SS-2447			7.1	1.2					
12			Partly Cemented Conglomerate (Refusal to backhoe).							
			BOTTOM OF TEST PIT AT 12.0'						COBBLES (Composite): Sample Depth 6' to 10'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 0.8±0.5                      0.4±0.3 FINES (Composite): Sample Depth 6' to 10'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 4.2±1.1                      8.9±1.2 +#4 sieve = 76.4%. -#4 sieve = 23.6%.	



**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

SHEET  
1  
OF  
1

TEST PIT NO.  
**M-CF-11**



### TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.
UMTRA			RIFLE		NEW RIFLE, COLORADO		3885-70	M-CF-15
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:
GREEN		BACKHOE	N24410 E47825	12/1/93	12/1/93	5267.2	10.5	G. LINDSEY
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1	SS-2448		SILT, (ML), clayey, dark brown, pond sediments with oxidized seams.	167.0	3.3			
	SS-2449		(FILL) per field staff.	555.0	10.0			
2	SS-2450		TAILINGS, (ML), silt, light gray.	471.0	9.2			
3	SS-2451		CLAY, (CL), silty, med. to low plasticity, dark brown, moist.	128.0	2.5			
4	SS-2452			8.6	1.6	12±1.0		FINES: Ra-226 (1,000 year) = 9.8 pCi/gr.
5	SS-2453			3.5	1.3	5.0±4.0		FINES: Ra-226 (1,000 year) = 4.0 pCi/gr. -Plan Exc. Depth at 5'.
6	SS-2454			1.9	1.2			
7	SS-2455			1.1	1.2		8.8	
8	SS-2456		CLAY, (CL), silty, low plasticity, dark brown, moist to saturated.	16.0	1.3	23±2.0		FINES: Ra-226 (1,000 year) = 18.5 pCi/gr.
9	SS-2457			11.0	1.1			COBBLES (Composite): Sample Depth 10' to 13'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.9±0.5 0.8±0.4
10	SS-2458			2.0	1.3			FINES (Composite): Sample Depth 10' to 13'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 6.3±1.4 13±1
11	SS-2460		GRAVELS, (GW), with cobbles to 5", dark gray to black, carbonaceous.	7.9	1.2	8.8±1.2		+ #4 sieve = 74.2%. - #4 sieve = 25.8%. FINES: Ra-226 (1,000 year) = 8.2 pCi/gr.
	SS-2461			2.8	1.2			
12	SS-2459			2.2	1.0			
	SS-2462			2.6	1.2			
13			BOTTOM OF TEST PIT AT 13.0'					
Note: Pit located in the bottom of a gypsum pond.								



**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

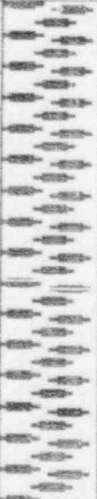
SHEET  
1  
OF  
1

TEST PIT NO.  
M-CF-15

TEST PIT LOG










PROJECT			SITE			LOCATION			JOB NO.	TEST PIT NO.
UMTRA			RIFLE			NEW RIFLE, COLORADO			3885-70	M-CF-19
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)		LOGGED BY:	
GREEN		BACKHOE	N24160 E47900	12/1/93	12/1/93	5267.1	not encountered		J. CERONE/G. LINDSEY	
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH	
1	SS-2428		SAND, (SM), silty, light brown, moist.	41.0	1.8		6.9			
1	SS-2430		ALLUVIUM	2.1	1.6	4.8±0.9	7.1		FINES Ra-226 (1,000 year) = 3.0 pCi/gr.	
2	SS-2429			2.0	1.9					
3										
4	SS-2431		GRAVELS, (GP), with cobbles in a sand matrix, iron oxide and calcite cementation.	7.3	1.5		9.2			
4	SS-2432			7.1	1.5	44±3.0		FINES Ra-226 (1,000 year) = 20 pCi/gr.		
5	SS-2433			9.5	1.5					
5	SS-2434		Hard digging with backhoe bucket below 5 feet. Cemented with CaCO <sub>3</sub> . Refusal to Backhoe.	10.0	1.9					
6	SS-2435			5.9	1.6	19±2.0		FINES Ra-226 (1,000 year) = 10.5 pCi/gr.		
6	SS-2436			6.0	1.7		9.1	-Plan Exc. Depth 6'.		
			BOTTOM OF TEST PIT AT 6.7'.						COBBLES (Composite): Sample Depth 3.5' to 5.5'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 0.8±0.5            0.7±0.3 FINES (Composite): Sample Depth 3.5' to 5.5'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 6.5±1.3            16±2 +#4 sieve = 76.3%. -#4 sieve = 23.7%.	
			Note: Pit located in the bottom of a gypsum pond.							

### TEST PIT LOG

PROJECT <b>UMTRA</b>			SITE <b>RIFLE</b>		LOCATION <b>NEW RIFLE, COLORADO</b>		JOB NO. <b>3885-70</b>	TEST PIT NO. <b>M-CF-20</b>
CONTRACTOR <b>GREEN</b>		EXCAVATION METHOD <b>BACKHOE</b>	COORDINATES <b>N23900 E46900</b>	BEGUN <b>12/1/93</b>	COMPLETED <b>12/1/93</b>	GROUND ELEV. <b>5262.0</b>	GROUND WATER DEPTH (FT) <b>4.8</b>	LOGGED BY: <b>G.LINDSEY</b>
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1	SS-2353		<b>GRAVELS</b> , (GP), with cobbles to 12", light brown.	1.3	1.3			1 inch of tailings on the surface.
2	SS-2354			2.1	1.5	2.7±0.7		FINES: Ra-226 (1,000 year) = 2.3 pCi/gr.
	SS-2355			2.7	1.2			
3	SS-2356			2.0	1.4			
	SS-2357			1.7	1.2	0.6±0.4		FINES: Ra-226 (1,000 year) = 1.3 pCi/gr.
4	SS-2358			1.6	1.1			
	SS-2359			8.6	1.4		7.4	
5	SS-2360		9.0	1.1	16±2.0		FINES: Ra-226 (1,000 year) = 11.2 pCi/gr. -Plan Exc. Depth at 5'.	
6								
7								
			<b>BOTTOM OF TEST PIT AT 7.0'</b>					COBBLES (Composite): Sample Depth 4' to 7'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 0.5±0.4                    7.8±0.4 FINES (Composite): Sample Depth 4' to 7'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 8.6±1.5                    17±2 +#4 sieve = 84.4%. -#4 sieve = 15.6%.



### TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.
UNTRA			RIFLE		NEW RIFLE, COLORADO		3885-70	M-CF-21
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:
GREEN		BACKHOE	N23900 E47180	12/1/93	12/1/93	5261.4	4.5	G. LINDSEY
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1	SS-2361		COBBLES, (GP), to 12", some sand and gravel.	4.7	1.3	5.7±0.9	8.4	FINES: Ra-226 (1,000 year) = 5.1 pCi/gr. 1 inch of tailings on the surface.
	SS-2362							
	SS-2363							
2	SS-2364							
	SS-2365							
3	SS-2366							
	SS-2367							
4	SS-2368							
	SS-2369							
6			BOTTOM OF TEST PIT AT 6.0'					FINES: Ra-226 (1,000 year) = 10.4 pCi/gr. +#4 sieve = 81.8%. -#4 sieve = 18.2%. -Plan Exc. Depth 5'.  COBBLES (Composite): Sample Depth 2' to 6'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 1.6±0.7            1.2±0.4 FINES (Composite): Sample Depth 2' to 6'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 32±3                    55±3



**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

SHEET  
1  
OF  
1

TEST PIT NO.  
**M-CF-21**






### TEST PIT LOG

PROJECT <b>UMTRA</b>			SITE <b>RIFLE</b>		LOCATION <b>NEW RIFLE, COLORADO</b>		JOB NO. <b>3885-70</b>	TEST PIT NO. <b>M-CF-22</b>
CONTRACTOR <b>GREEN</b>		EXCAVATION METHOD <b>BACKHOE</b>	COORDINATES <b>N23900 E47430</b>	BEGUN <b>12/1/93</b>	COMPLETED <b>12/1/93</b>	GROUND ELEV. <b>5262.9</b>	GROUND WATER DEPTH (FT) <b>6.0</b>	LOGGED BY: <b>J. CERCOONE/G. LINDSEY</b>
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1			FILL, gravels and cobbles in a silty sand matrix.					COBBLES (Composite): Sample Depth 4' to 8'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 0.9±0.5            0.9±0.4 FINES (Composite): Sample Depth 4' to 8'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 2.4±0.8            2.5±0.6 +#4 sieve = 79.3%. -#4 sieve = 20.7%.
2				COBBLES, (GP), with boulders, black, carbonaceous, little sand and gravel.				
3								
4								
5								
6	SS-2388			2.6	1.0	1.9±0.6	7.3	FINES: Ra-226 (1,000 year) = 2.4 pCi/gr. -Plan Exc. Depth at 6'.
7	SS-2389			3.3	1.2			
8			BOTTOM OF TEST PIT AT 8.0'					




### TEST PIT LOG

PROJECT <b>UMTRA</b>			SITE <b>RIFLE</b>		LOCATION <b>NEW RIFLE, COLORADO</b>		JOB NO. <b>3885-70</b>	TEST PIT NO. <b>M-CF-24</b>
CONTRACTOR <b>GREEN</b>		EXCAVATION METHOD <b>BACKHOE</b>	COORDINATES <b>N23700 E46915</b>	BEGIN <b>12/1/93</b>	COMPLETED <b>12/1/93</b>	GROUND ELEV. <b>5259.2</b>	GROUND WATER DEPTH (FT) <b>2.8</b>	LOGGED BY: <b>G. LINDSEY</b>
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1	SS-2390		COBBLES, to 4" with sand.	1.6	0.8			
2	SS-2391			1.1	1.6			
3	SS-2392		GRAVELS (GP), with cobbles.	1.8	1.0	1.9±0.6		FINES: Ra-226 (1,000 year) = 1.8 pCi/gr.
3	SS-2393			1.7	1.0		7.9	
3	SS-2394			2.7	1.2			
4	SS-2395			3.0	1.3			
4	SS-2396			1.8	0.8			-Plan Exc. Depth at 4'.
4	SS-2397			2.0	1.3			
5			BOTTOM OF TEST PIT AT 5.0'					COBBLES (Composite): Sample Depth 2' to 5'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 0.9±0.5            0.7±0.4 FINES (Composite): Sample Depth 2' to 5'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 2.6±0.8            3.6±0.8 +#4 sieve = 64.8%. -#4 sieve = 35.2%.

# TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.	
UMTRA			RIFLE		NEW RIFLE, COLORADO		3885-70	M-CF-25	
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:	
GREEN		BACKHOE	N23640 E47180	12/1/93	12/1/93	5263.2	8.0	J. CERONE/G. LINDSEY	
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH	
1	SS-2311		SILTY CLAY, (CL), med. plasticity, dark brown, moist to saturated.	10.0	1.6			FINES: Ra-226 (1,000 year) = 1.4 pCi/gr.  7.5	
	SS-2312			1.5	1.6	1.2±0.5			
2	SS-2315		(fill?)	1.1	1.0				
3	SS-2316		Very moist.	1.0	1.1				
4	SS-2317		Organic seam.	1.4	1.0				
5	SS-2319		CLAYEY SILT, (ML), reddish brown—probably from oxidation.	1.0	1.0			FINES: Ra-226 (1,000 year) = 6.2 pCi/gr. -Plan Exc. Depth at 6'.  Note: Attempted to dewater the pit with a 300 gpm pump. Unable to obtain a representative sample below the water table.	
6	SS-2318			6.7	1.4	5.2±0.9			
7	SS-2320		COBBLES, (GW-GP), to 12", with sand and gravel, clean material.	0.9	1.4		7.0		
	SS-2321			1.5	1.2				
8	SS-2322			0.6	1.0				
	SS-2323			1.1	1.0				
9	SS-2398			12.0	1.4				
	SS-2399		8.5	1.5					
10			BOTTOM OF TEST PIT AT 10.0'						
									COBBLES (Composite): Sample Depth 6.5' to 8.5'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 0.8±0.5            1.3±0.5 FINES (Composite): Sample Depth 6.5' to 8.5'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 5.4±1.2            4.1±0.8 +#4 sieve = 78.5%. -#4 sieve = 21.5%.

### TEST PIT LOG

PROJECT			SITE		LOCATION			JOB NO.	TEST PIT NO.
<b>UMTRA</b>			<b>RIFLE</b>		<b>NEW RIFLE, COLORADO</b>			<b>3885-70</b>	<b>M-CF-26</b>
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:	
<b>GREEN</b>		<b>BACKHOE</b>	<b>N23640 E47480</b>	<b>12/1/93</b>	<b>12/1/93</b>	<b>5263.5</b>	<b>7.5</b>	<b>J. CERCONO/G. LINDSEY</b>	
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH
1	SS-2324		FILL, dark brown, fine grained, with a lot of debris.	11.0	1.8				
	SS-2325			7.1	1.5	8.1±1.1			FINES: Ra-226 (1,000 year) = 7.5 pCi/gr. Debris and fill to 3 feet on north side of the pit.
2	SS-2326		SAND, (SP), little silt, gray to brown, med dense.	6.8	1.6		7.5		
3	SS-2327			0.9	1.5				
4	SS-2328			1.0	1.2	0.6±0.4			FINES: Ra-226 (1,000 year) = 0.9 pCi/gr.
5	SS-2329		Oxidized seam.	1.2	0.8		7.6		
6	SS-2330			1.0	0.9		7.1		
7	SS-2331			7.6	1.0	15±2.0	7.1	▼	FINES: Ra-226 (1,000 year) = 10.2 pCi/gr.
8	SS-2400		GRAVELS, (GP), with cobbles to 6".	2.0	0.8	2.6±0.7			FINES: Ra-226 (1,000 year) = 2.2 pCi/gr.
9									
			BOTTOM OF TEST PIT AT 9.5'						COBBLES (Composite): Sample Depth 8' to 9.5'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 0.7±0.5                    0.5±0.3 FINES (Composite): Sample Depth 8' to 9.5'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 1.9±0.7                    1.4±0.5 +#4 sieve = 65.5%. -#4 sieve = 34.5%.
















**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

SHEET  
1  
OF  
1





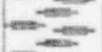

TEST PIT NO.  
**M-CF-26**



### TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.
<b>UMTRA</b>			<b>RIFLE</b>		<b>NEW RIFLE, COLORADO</b>		<b>3885-70</b>	<b>M-CF-27</b>
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:
<b>GREEN</b>		<b>BACKHOE</b>	<b>N23640 E47725</b>	<b>12/1/93</b>	<b>12/1/93</b>	<b>5267.0</b>	<b>11.0</b>	<b>J. CERCONE/G. LINDSEY</b>
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1	SS-2332		FILL, mixed soil with tailings, wood.	281.0	8.3			
	SS-2333			336.0	5.2			
2	SS-2334			370.0	7.8			
3	SS-2335		Oxidized zone at 3 to 4 feet.	349.0	7.1			
4	SS-2336		TAILINGS, (CL-ML), reddish brown with orange seams (3").	364.0	8.7		6.8	
5	SS-2337			150.0	4.5			
6	SS-2338		Slimes, gray, saturated.	1103.0	44.0			-Plan Exc. Depth at 6'.
7	SS-2339			2792.0	64.0		6.9	
8	SS-2340		SILTY CLAY, (CL), dark brown, some roots.	9.0	1.5			
9	SS-2345		GRAVELS, (GP), with cobbles to 12".	9.4	1.8	7.3±1.1	8.2	FINES: Ra-226 (1,000 year) = 8.7 pCi/gr.
10	SS-2346			10.0	1.7			
	SS-2341			2.3	1.0			
	SS-2342			2.3	1.0			
11	SS-2343		BOTTOM OF TEST PIT AT 11.0'	7.8	1.3			COBBLES (Composite): Sample Depth 9.5' to 11.0'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 0.8±0.5                    0.8±0.4 FINES (Composite): Sample Depth 9.5' to 11.0'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 3.2±0.9                    1.4±0.5 +#4 sieve = 85.0%. -#4 sieve = 15.0%.
	SS-2344			7.6	1.3			

### TEST PIT LOG

PROJECT			SITE			LOCATION			JOB NO.	TEST PIT NO.
UMTRA			RIFLE			NEW RIFLE, COLORADO			3885-70	M-CF-28
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:		
GREEN		BACKHOE	N23400 E46900	12/1/93	12/1/93	5258.0	2.0	G. LINDSEY		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	WATER DATA	REMARKS PHOTOGRAPH	
1	SS-2401		COBBLES, (GP), to 12", with black organic silt.	10.4	1.8	38±2.0	6.5	▼	FINES: Ra-226 (1,000 year) = 20.1 pCi/gr.	
	SS-2402			13.0	1.2	40±2.0			FINES: Ra-226 (1,000 year) = 22.5 pCi/gr.	
2	SS-2403			12.0	1.0				-Plan Exc. Depth at 2'.	
	SS-2404			6.9	1.1					
3	SS-2405			7.2	1.3	30±2.0			FINES: Ra-226 (1,000 year) = 15.2 pCi/gr.	
4										
			BOTTOM OF TEST PIT AT 4.5'						COBBLES (Composite): Sample Depth 0' to 4.5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 0.8±0.5 0.5±0.3 FINES (Composite): Sample Depth 0' to 4.5'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 4.2±1.0 11±1 +#4 sieve = 90.4%. -#4 sieve = 9.6%.	



**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

SHEET  
1  
OF  
1

TEST PIT NO.  
**M-CF-28**

### TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.
UMTRA			RIFLE		NEW RIFLE, COLORADO		3885-70	M-CF-29
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGIN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:
GREEN		BACKHOE	N23450 E47130	12/1/93	12/1/93	5262.2	3.8	G. LINDSEY
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1	SS-2406 SS-2407 SS-2408 SS-2409 SS-2410 SS-2411		FILL, mixed sand, gravel and cobbles to 12", dark brown.	186.0 178.0 99.0 96.0 115.0 131.0	5.4 4.5 3.0 3.1 3.7 3.4	290±10		
5			SILTY CLAY, (CL), med. plasticity, black, with carbonized roots. Med. gray seam at 4.5' - 5.0'.				6.9	
			BOTTOM OF TEST PIT AT 6.5'					
								COBBLES (Composite): Sample Depth 0' to 4'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 2.1±0.8            2.3±0.6 FINES (Composite): Sample Depth 0' to 4'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 110±10            230±10 +#4 sieve = 78.2%. -#4 sieve = 21.8%.

















**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION

SHEET  
1  
OF  
1


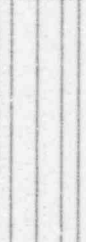


TEST PIT NO.  
**M-CF-29**

### TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.
UMTRA			RIFLE		NEW RIFLE, COLORADO		3885-70	M-CF-30
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:
GREEN		BACKHOE	N23400 E47265	12/1/93	12/1/93	5262.2	8.3	J. CERCONE
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1	SS-2412		FILL, silty gravel, poorly graded, brown, moist, low plasticity.	34.0	2.5			
	SS-2413			11.0	1.5			
2	SS-2414			236.0	4.3		7.3	
3	SS-2417			142.0	3.5			
4	SS-2418		SILTY SAND, (SM), gray, moist.	9.8	1.4			Tailings?
	SS-2419		CLAY, (CL), low to med. plasticity, black, moist to saturated, organic.	13.0	1.5	32±2.0		FINES: Ra-226 (1,000 year) = 19.7 pCi/gr.
5	SS-2420		GRAVELS, (GW), with cobbles, well graded, cobbles to 8" max., fines are med. to coarse sand.	16.0	1.4			
6	SS-2421			12.0	1.1			
	SS-2422			30.0	1.5			Plan Excavation Depth at 6'.
	SS-2423			30.0	1.5			
	SS-2424			4.4	1.2	22±2.0		FINES: Ra-226 (1,000 year) = 10.6 pCi/gr.
	SS-2425			6.0	1.1			
8	SS-2426			* 52.0	2.7			
	SS-2427			* 47.0	1.8			
9			BOTTOM OF TEST PIT AT 9.0'					
			* Possible Cross Contamination.					COBBLES (Composite): Sample Depth 4.5' to 7.5'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 1.2±0.6                    0.6±0.4 FINES (Composite): Sample Depth 4.5' to 7.5'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 3.0±0.9                    6.9±1.0 +#4 sieve = 79.4%. -#4 sieve = 20.6%.



### TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.		
<b>UMTRA</b>			<b>RIFLE</b>		<b>NEW RIFLE, COLORADO</b>		<b>3885-70</b>	<b>M-CF-31</b>		
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:		
<b>GREEN</b>		<b>BACKHOE</b>	<b>N25252 E49005</b>	<b>12/3/93</b>	<b>12/3/93</b>	<b>5272.8</b>	<b>8.5</b>	<b>J. CERCONE/G. LINDSEY</b>		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH		
1	SS-2475		CLAY, (CL), light brown, slightly moist, some roots.	1.6	1.9					
	SS-2476			1.1	2.3					
2	SS-2477			1.5	2.8					
3	SS-2478		SANDY SILT, (ML), to SILTY SAND, (SM), dark brown, moist, loose.	1.5						
4	SS-2479			1.8	2.0					
5	SS-2480			0.6	1.5					
6	SS-2481			0.8	1.5					
7	SS-2482				GRAVELS, (GP-GW), with cobbles to 4", matrix of fine sand.	0.9	1.6			
8	SS-2483					1.3	1.5			
	SS-2484	0.8	1.4							
9	SS-2485		GRAVELS, (GP-GW), with cobbles to 6", matrix of coarse sand.	1.3	1.3					
	SS-2486			0.7	1.0					
	SS-2487			0.7	1.1					
10	SS-2488			0.8	1.2					
	SS-2489			1.0	1.2					
11	SS-2490			0.6	1.2					
	SS-2491			1.0	1.1					
12			BOTTOM OF TEST PIT AT 12.0'							
			(BACKGROUND PIT LOCATED AT NORTHEAST CORNER OF NEW RIFLE SITE).							



COBBLES (Composite): Sample Depth 8.5' to 11.5'.  
 Ra-226    Th-232    Th-230    Ra-226 (1,000 yr)  
 0.9±0.5            0.7±0.4  
 FINES (Composite): Sample Depth 8.5' to 11.5'.  
 Ra-226    Th-232    Th-230    Ra-226 (1,000 yr)  
 1.8±0.8            2.2±0.6  
 +#4 sieve = 78.2%.  
 -#4 sieve = 21.8%.

### TEST PIT LOG

PROJECT			SITE		LOCATION		JOB NO.	TEST PIT NO.		
UMTRA			RIFLE		NEW RIFLE, COLORADO		3885-70	M-CF-32		
CONTRACTOR		EXCAVATION METHOD	COORDINATES	BEGUN	COMPLETED	GROUND ELEV.	GROUND WATER DEPTH (FT)	LOGGED BY:		
GREEN		BACKHOE	N24648 E51357	12/2/93	12/2/93	5271.5	3.0	J. CERONE		
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH		
1	SS-2370 SS-2371 SS-2372		GRAVELS, (GP), with cobbles to 12", poorly graded, with coarse sand, slightly moist, all gravels and cobbles appear clean and fresh.	1.3	1.0			COBBLES (Composite): Sample Depth 0'to 4.0'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 1.8±0.7 1.1±0.4 FINES (Composite): Sample Depth 0'to 4.0'. Ra-226 Th-232 Th-230 Ra-226 (1,000 yr) 1.7±0.7 0.9±0.4 +#4 sieve = 80.8%. -#4 sieve = 19.2%.		
2	SS-2374			1.5	1.1					
3	SS-2373 SS-2375			1.4	1.4					
4	SS-2376 SS-2377			1.3	1.3					
5	SS-2378			1.1	1.0					
	SS-2379			1.0	1.0					
				1.2	1.2					
				0.8	1.0					
5				BOTTOM OF TEST PIT AT 5.0'						
				(BACKGROUND PIT LOCATED IN CON SY INC. GRAVEL PIT).						



**MORRISON KNUDSEN CORPORATION**  
ENVIRONMENTAL SERVICES DIVISION



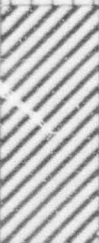






SHEET

1  
OF  
1

TEST PIT NO.

M-CF-32

## TEST PIT LOG

PROJECT <b>UMTRA</b>			SITE <b>RIFLE</b>		LOCATION <b>NEW RIFLE, COLORADO</b>		JOB NO. <b>3885-70</b>	TEST PIT NO. <b>M-CF-33</b>
CONTRACTOR <b>GREEN</b>		EXCAVATION METHOD <b>BACKHOE</b>	COORDINATES <b>N24877 E51355</b>	BEGUN <b>12/2/93</b>	COMPLETED <b>12/2/93</b>	GROUND ELEV. <b>5275.2</b>	GROUND WATER DEPTH (FT) <b>7.2</b>	LOGGED BY: <b>J. CERCONE</b>
DEPTH (FT)	SAMPLE NO.	GRAPHIC LOG	MATERIAL DESCRIPTION AND CLASSIFICATION	Ra-226 pCi/gr	Th-232 pCi/gr	Th-230 pCi/gr	pH	REMARKS PHOTOGRAPH
1			CLAY, (CL), (TOP SOIL), some roots.					
2			SILT, (ML), light brown, moist.					
3			CLAY, (CH), med. to high plasticity, black, saturated, organic.					
6	SS-2380		GRAVELS, (GW), with cobbles to 4", well graded, black to gray, organic coating.	1.3	1.1			COBBLES (Composite): Sample Depth 7.0' to 9.0'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 1.6±0.7            0.5±0.3 FINES (Composite): Sample Depth 7.0' to 9.0'. Ra-226    Th-232    Th-230    Ra-226 (1,000 yr) 1.6±0.7            1.3±0.5 +#4 sieve = 81.9%. -#4 sieve = 18.1%.
7	SS-2381			1.1	1.3			
7	SS-2382			1.0	1.2			
8	SS-2383			0.9	0.9			
8	SS-2384			0.7	0.8			
9	SS-2385			1.0	1.3			
			BOTTOM OF TEST PIT AT 9.0'.					
			(BACKGROUND PIT LOCATED IN CON SY INC. GRAVEL PIT).					



APPENDIX D

MASS PARTITION FUNCTIONS  
(COBBLES-TO-FINES RATIOS)



INTER-OFFICE CORRESPONDENCE

TO Grant Cherrington  
LOCATION San Francisco  
SUBJECT Cobbles to Fines Test Result

DATE December 13, 1993  
FROM David Farr  
LOCATION Rifle, CO 3050

As requested, we have performed particle size analyses on New Rifle site subpile material test pit samples obtained by TAC, MKES and DOE representatives during recent test pit investigations. Enclosed are the results.

As discussed during initial test pit examination, the cobble to fine analyses were performed on composite bulk samples ranging in weight from 1000 to 1500 pounds each. The larger sized samples were required due to concerns about the smaller samples originally specified being representative. To expedite this process, the bulk samples were reduced to manageable proportions in accordance with the ASTM C-136 practice of sample reduction. An explanation of this practice has been provided in the attached calculation sheet (Attachment 1).

The dry weight of the +1" and +#4 fractions was calculated using an assumed 1.5% moisture as recommended by ASTM C-136. A representative sample of the +1", including a proportionate amount of the -1" to +#4 material, was collected for radium and thorium analysis. These samples were then given to site H.P. personnel to be sent out for analysis.

It should be noted that a few of the calculation sheets do not indicate the depth of the sample as this data was not provided to us.

Should you require further information, please advise.

File: 4.15 w/ enclosure

cc: Randy Withee w/o enclosure  
QC File w/ enclosure

*Tau*

ATTACHMENT 1  
CALCULATIONS

1. A representative sample of between 1000 to 1500 pounds of material was split on the 1" sieve and weights of each fraction were obtained. The +1" fraction was corrected assuming a 1.5% moisture and the -1" fraction corrected by actual moisture content. Dry weights were calculated and added together to determine the total sample weight.
2. The -1" fraction was reduced to a manageable sized representative sample of approximately 50 pounds, split on the #4 sieve and weights were obtained for each fraction. A moisture sample was obtained from the -#4 material for correction and the +#4 fraction was corrected using an assumed moisture content of 1.5%. Dry weights were calculated. Percentages of the +#4 and -#4 were then calculated.
3. The percentages of +#4 and -#4 obtained from the reduced -1" fraction were then adjusted back to a whole sample basis by multiplying by the original dry weight of the whole -1" fraction. This weight was then added to the +1" fraction to determine the +#4 weight on a whole sample basis.
4. The weight of the +#4 and -#4 (cobble and fines) is then expressed as a percentage of the total sample weight.

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #1

DATE TESTED: 12-6-93

DEPTH: 15.0' - 17.0'

TECHNICIAN: David Miller

CHECKED BY: Steve With

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 836.28 lbs.  
 % MOIST 1.5 %  
 DRY WEIGHT 823.92 lbs.

-1" WET WEIGHT 381.92 lbs.  
 % MOIST 11.6 %  
 DRY WEIGHT 342.22 lbs.

TOTAL SAMPLE WEIGHT 1166.14 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 24.01 lbs.  
 % MOIST 1.5 %  
 DRY WEIGHT 23.66 lbs.

-#4 WET WEIGHT 35.12 lbs.  
 % MOIST 9.6 %  
 DRY WEIGHT 32.04 lbs.

REDUCED SAMPLE WEIGHT 55.70 lbs.

% + #4 IN REDUCED SAMPLE 42.5 %

% -#4 IN REDUCED SAMPLE 57.5 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 145.44 lbs.  
 + DRY WT. OF +1" IN BULK SAMPLE 823.92 lbs.  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 969.36 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION

REDUCED SAMPLE -#4

WET WEIGHT 652.6 g

488.9 g

DRY WEIGHT 585.0 g

446.0 g

WT. OF WATER 67.6 g

42.9 g

% MOISTURE 11.6 %

9.6 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 969.36 lbs.

TOTAL SAMPLE WEIGHT 1166.14 lbs.

% + #4 (COBBLES) 83.1 %

% -#4 (FINES) 16.9 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #2

DATE TESTED: 12-6-93

DEPTH: 13.0' - 16.0'

TECHNICIAN: David M. [Signature]

CHECKED BY: [Signature]

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 667.73 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 657.86 lbs

-1" WET WEIGHT 553.67 lbs  
 % MOIST 10.5 %  
 DRY WEIGHT 501.06 lbs

TOTAL SAMPLE WEIGHT 1158.92 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 12.60 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 12.41 lbs.

-#4 WET WEIGHT 37.18 lbs  
 % MOIST 9.2 %  
 DRY WEIGHT 34.05 lbs

REDUCED SAMPLE WEIGHT 46.46 lbs.

% + #4 IN REDUCED SAMPLE 26.7 %

% -#4 IN REDUCED SAMPLE 73.3 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 133.78 lbs  
 + DRY WT. OF + 1" IN BULK SAMPLE 657.86 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 791.64 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION  
 WET WEIGHT 572.9 g  
 DRY WEIGHT 518.6 g  
 WT. OF WATER 54.3 g  
 % MOISTURE 10.5 %

REDUCED SAMPLE -#4  
 WET WEIGHT 472.6 g  
 DRY WEIGHT 432.7 g  
 WT. OF WATER 39.9 g  
 % MOISTURE 9.2 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 791.64 lbs  
 TOTAL SAMPLE WEIGHT 1158.92 lbs

% + #4 (COBBLES) 68.3 %

% -#4 (FINES) 31.7 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #3

DATE TESTED: 12-7-93

DEPTH: 18.0' - 21.0'

TECHNICIAN: David M. Man

CHECKED BY: Steve With

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 706.30 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 695.86 lbs.

- 1" WET WEIGHT 561.82 lbs.  
 % MOIST 14.3 %  
 DRY WEIGHT 491.53 lbs

TOTAL SAMPLE WEIGHT 1187.39 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 15.83 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 15.60 lbs

- #4 WET WEIGHT 44.75 lbs  
 % MOIST 13.7 %  
 DRY WEIGHT 39.36 lbs

REDUCED SAMPLE WEIGHT 54.96 lbs.

% + #4 IN REDUCED SAMPLE 28.4 %

% - #4 IN REDUCED SAMPLE 71.6 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 139.59 lbs  
 + DRY WT. OF +1" IN BULK SAMPLE 695.86 lbs.  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 835.45 lbs

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT <u>497.9 g</u>	<u>523.1 g</u>
DRY WEIGHT <u>435.7 g</u>	<u>460.0 g</u>
WT. OF WATER <u>62.2 g</u>	<u>63.1 g</u>
% MOISTURE <u>14.3 %</u>	<u>13.7 %</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 835.45 lbs.  
 TOTAL SAMPLE WEIGHT 1187.39 lbs.

% + #4 (COBBLES) 70.4 %

% - #4 (FINES) 29.6 %



CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #4

DATE TESTED: 12-7-93

DEPTH: 110'-16.0'

TECHNICIAN: David Mann

CHECKED BY: Steve Witt

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 781.77 lbs.  
 % MOIST 1.5 %  
 DRY WEIGHT 770.22 lbs

- 1" WET WEIGHT 458.61 lbs  
 % MOIST 5.4 %  
 DRY WEIGHT 435.11 lbs

TOTAL SAMPLE WEIGHT 1205.33 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 21.04 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 20.73 lbs

<sup>SD 12-14-93</sup>  
 - #4 WET WEIGHT 45.4257 lbs  
 % MOIST 5.1 %  
 DRY WEIGHT 40.50 lbs

REDUCED SAMPLE WEIGHT 61.23 lbs

% + #4 IN REDUCED SAMPLE 33.9 %

% - #4 IN REDUCED SAMPLE 66.1 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 147.50 lbs  
 + DRY WT. OF + 1" IN BULK SAMPLE 770.22 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 917.72 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT <u>558.8 g</u>	<u>464.3 g</u>
DRY WEIGHT <u>530.2 g</u>	<u>441.7 g</u>
WT. OF WATER <u>28.6 g</u>	<u>22.6 g</u>
% MOISTURE <u>5.4 %</u>	<u>5.1 %</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 917.72 lbs  
 TOTAL SAMPLE WEIGHT 1205.33 lbs

% + #4 (COBBLES) 76.1 %

% - #4 (FINES) 23.9 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #5

DATE TESTED: 12-7-93

DEPTH: 16.0' - 21.0'

TECHNICIAN: David M. Jan

CHECKED BY: Steve Witt

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 692.10 lbs  
 % MOIST 1.5%  
 DRY WEIGHT 681.87 lbs

- 1" WET WEIGHT 525.88 lbs  
 % MOIST 7.2%  
 DRY WEIGHT 490.56 lbs

TOTAL SAMPLE WEIGHT 1172.43 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 24.34 lbs  
 % MOIST 1.5%  
 DRY WEIGHT 23.98 lbs

- #4 WET WEIGHT 30.99 lbs  
 % MOIST 12.0%  
 DRY WEIGHT 27.67 lbs

REDUCED SAMPLE WEIGHT 51.65 lbs.

% + #4 IN REDUCED SAMPLE 46.4%

% - #4 IN REDUCED SAMPLE 53.6%

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 227.62 lbs  
 + DRY WT. OF + 1" IN BULK SAMPLE 681.87 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 909.49 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION  
 WET WEIGHT 526.3 g  
 DRY WEIGHT 491.0 g  
 WT. OF WATER 35.3 g  
 % MOISTURE 7.2%

REDUCED SAMPLE - #4  
 WET WEIGHT 5477 g  
 DRY WEIGHT 4889 g  
 WT. OF WATER 588 g  
 % MOISTURE 12.0%

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 909.49 lbs  
 TOTAL SAMPLE WEIGHT 1172.43 lbs

% + #4 (COBBLES) 77.6%

% - #4 (FINES) 22.4%

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: # 7

DATE TESTED: 12-7-93

DEPTH: 170'-210'

TECHNICIAN: David M. Jan

CHECKED BY: Steve Witt

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 700.77 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 690.41 lbs

- 1" WET WEIGHT 501.88 lbs  
 % MOIST 11.5 %  
 DRY WEIGHT 450.12 lbs

TOTAL SAMPLE WEIGHT 1140.53 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 18.12 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 17.85 lbs

- #4 WET WEIGHT 42.51 lbs  
 % MOIST 11.2 %  
 DRY WEIGHT 38.23 lbs

REDUCED SAMPLE WEIGHT 56.08 lbs

% + #4 IN REDUCED SAMPLE 31.8 %

% - #4 IN REDUCED SAMPLE 68.2 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 143.14 lbs  
 + DRY WT. OF +1" IN BULK SAMPLE 690.41 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 833.55 lbs

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION

WET WEIGHT 530.1 g  
 DRY WEIGHT 475.5 g  
 WT. OF WATER 54.6 g  
 % MOISTURE 11.5 %

REDUCED SAMPLE -#4

531.8 g  
478.3 g  
53.5 g  
11.2 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 833.55 lbs  
 TOTAL SAMPLE WEIGHT 1140.53 lbs

% + #4 (COBBLES) 73.1 %

% - #4 (FINES) 26.9 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #11

DATE TESTED: 12-7-93

DEPTH: 60'-100'

TECHNICIAN: David M. Jan

CHECKED BY: John With

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT	<u>1031.55 lbs</u>	- 1" WET WEIGHT	<u>574.17 lbs</u>
% MOIST	<u>1.5 %</u>	% MOIST	<u>13.9 %</u>
DRY WEIGHT	<u>1016.11 lbs</u>	DRY WEIGHT	<u>504.10 lbs</u>

TOTAL SAMPLE WEIGHT 1520.21 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT	<u>15.62 lbs</u>	- #4 WET WEIGHT	<u>41.74 lbs</u>
% MOIST	<u>1.5 %</u>	% MOIST	<u>10.2 %</u>
DRY WEIGHT	<u>15.39 lbs</u>	DRY WEIGHT	<u>37.88 lbs</u>

REDUCED SAMPLE WEIGHT 53.27 lbs

% + #4 IN REDUCED SAMPLE ~~145.68~~ 28.9 %

% - #4 IN REDUCED SAMPLE 71.1 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE	<u>145.68 lbs</u>
+ DRY WT. OF + 1" IN BULK SAMPLE	<u>1016.11 lbs</u>
= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE	<u>1161.79 lbs.</u>

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT <u>526.0 g</u>	<u>459.1 g</u>
DRY WEIGHT <u>461.8 g</u>	<u>416.5 g</u>
WT. OF WATER <u>64.2 g</u>	<u>42.6 g</u>
% MOISTURE <u>13.9 %</u>	<u>10.2 %</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4	<u>1161.79 lbs</u>
TOTAL SAMPLE WEIGHT	<u>1520.21 lbs</u>

% + #4 (COBBLES) 76.4 %

% - #4 (FINES) 23.6 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #15

DATE TESTED: 12/6/93

DEPTH: 10.0' - 13.0'

TECHNICIAN: David Moran

CHECKED BY: Steve Witt

BULK SAMPLE WEIGHTS

+1" WET WEIGHT 650.45 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 640.84 lbs

-1" WET WEIGHT 586.97 lbs  
 % MOIST 11.2 %  
 DRY WEIGHT 527.85 lbs

TOTAL SAMPLE WEIGHT 1168.69 lbs

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 22.30 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 21.97 lbs

-#4 WET WEIGHT 31.60 lbs  
 % MOIST 8.2 %  
 DRY WEIGHT 29.21 lbs

REDUCED SAMPLE WEIGHT 51.18 lbs

% + #4 IN REDUCED SAMPLE 42.9 %

% - #4 IN REDUCED SAMPLE 57.1 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 226.45  
 + DRY WT. OF +1" IN BULK SAMPLE 640.84  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 867.29 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION

WET WEIGHT 603.4 g  
 DRY WEIGHT 542.6 g  
 WT. OF WATER 60.8 g  
 % MOISTURE 11.2 %

REDUCED SAMPLE -#4

568.6 g  
525.3 g  
43.3 g  
8.2 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 867.29 lbs  
 TOTAL SAMPLE WEIGHT 1168.69 lbs

% + #4 (COBBLES) 74.2 %

% - #4 (FINES) 25.8 %



CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #19

DATE TESTED: 12.3.93

DEPTH: 3.5' - 5.5'

TECHNICIAN: David Mann

CHECKED BY: Jim With

BULK SAMPLE WEIGHTS

+1" WET WEIGHT 717.17 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 706.57 lbs

-1" WET WEIGHT 480.03 lbs  
 % MOIST 7.3 %  
 DRY WEIGHT 447.37 lbs

TOTAL SAMPLE WEIGHT 1153.94 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 19.02 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 18.74 lbs

- #4 WET WEIGHT 31.94 lbs  
 % MOIST 7.9 %  
 DRY WEIGHT 29.60 lbs

REDUCED SAMPLE WEIGHT 48.34 lbs.

% + #4 IN REDUCED SAMPLE 38.8 %

% - #4 IN REDUCED SAMPLE 61.2 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 173.58 lbs  
 + DRY WT. OF +1" IN BULK SAMPLE 706.57 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 880.15 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION  
 WET WEIGHT 600.0 g  
 DRY WEIGHT 559.1 g  
 WT. OF WATER 40.9 g  
 % MOISTURE 7.3 %

REDUCED SAMPLE -#4  
 WET WEIGHT 492.1 g  
 DRY WEIGHT 455.9 g  
 WT. OF WATER 36.2 g  
 % MOISTURE 7.9 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 880.15 lbs  
 TOTAL SAMPLE WEIGHT 1153.94 lbs

% + #4 (COBBLES) 76.3 %

% - #4 (FINES) 23.7 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #20

DATE TESTED: 12.3-93

DEPTH: 4 E + 07

TECHNICIAN: David M. Jan

CHECKED BY: Jim Webb

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 845.63 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 833.13 lbs

-1" WET WEIGHT 348.28 lbs  
 % MOIST 7.2 %  
 DRY WEIGHT 324.89 lbs

TOTAL SAMPLE WEIGHT 1158.02 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 28.43 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 28.01 lbs

-#4 WET WEIGHT 37.41 lbs  
 % MOIST 7.2 %  
 DRY WEIGHT 34.90 lbs

REDUCED SAMPLE WEIGHT 62.91 lbs.

% + #4 IN REDUCED SAMPLE 44.5 %

% -#4 IN REDUCED SAMPLE 55.5 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 144.58 lbs  
 + DRY WT. OF + 1" IN BULK SAMPLE 833.13 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 977.71 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION  
 WET WEIGHT 693.8 g  
 DRY WEIGHT 647.4 g  
 WT. OF WATER 46.4 g  
 % MOISTURE 7.2 %

REDUCED SAMPLE -#4  
 WET WEIGHT 536.1 g  
 DRY WEIGHT 500.2 g  
 WT. OF WATER 35.9 g  
 % MOISTURE 7.2 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 977.71 lbs  
 TOTAL SAMPLE WEIGHT 1158.02 lbs

% + #4 (COBBLES) 84.4 %

% -#4 (FINES) 15.6 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #21

DATE TESTED: 12-3-93

DEPTH: 2'-6"

TECHNICIAN: David M. [Signature]

CHECKED BY: [Signature]

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 833.19 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 820.88 lbs

- 1" WET WEIGHT 402.59 lbs  
 % MOIST 9.9 %  
 DRY WEIGHT 366.32 lbs

TOTAL SAMPLE WEIGHT 1187.20 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 19.88 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 19.59 lbs

- #4 WET WEIGHT 30.68 lbs  
 % MOIST 8.7 %  
 DRY WEIGHT 28.22 lbs

REDUCED SAMPLE WEIGHT 47.81 lbs.

% + #4 IN REDUCED SAMPLE 41.0 %

% - #4 IN REDUCED SAMPLE 59.0 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 150.19 lbs  
 + DRY WT. OF + 1" IN BULK SAMPLE 820.88 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 971.07 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION	REDUCED SAMPLE -#4
WET WEIGHT <u>711.0 g</u>	<u>495.1 g</u>
DRY WEIGHT <u>647.0 g</u>	<u>455.3 g</u>
WT. OF WATER <u>64.0 g</u>	<u>39.8 g</u>
% MOISTURE <u>9.9 %</u>	<u>8.7 %</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 971.07 lbs  
 TOTAL SAMPLE WEIGHT 1187.20 lbs

% + #4 (COBBLES) 81.8 %

% - #4 (FINES) 18.2 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #22

DATE TESTED: 12-1-93

DEPTH: -3 - 6'

TECHNICIAN: David M. Lee

CHECKED BY: Steve Wilts

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 847.35 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 834.83 lbs

- 1" WET WEIGHT 471.52 lbs  
 % MOIST 13.4 %  
 DRY WEIGHT 415.80 lbs

TOTAL SAMPLE WEIGHT 1250.63 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 20.68 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 20.37 lbs

- #4 WET WEIGHT 38.41 lbs  
 % MOIST 13.8 %  
 DRY WEIGHT 33.75 lbs

REDUCED SAMPLE WEIGHT 54.12 lbs

% + #4 IN REDUCED SAMPLE 37.6 %

% - #4 IN REDUCED SAMPLE 62.4 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 156.34 lbs  
 + DRY WT. OF +1" IN BULK SAMPLE 834.83 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 991.17 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION  
 WET WEIGHT 734.2 g  
 DRY WEIGHT 647.3 g  
 WT. OF WATER 86.9 g  
 % MOISTURE 13.4 %

REDUCED SAMPLE -#4  
 WET WEIGHT 661.6 g  
 DRY WEIGHT 581.5 g  
 WT. OF WATER 80.1 g  
 % MOISTURE 13.8 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 991.17 lbs  
 TOTAL SAMPLE WEIGHT 1250.63 lbs

% + #4 (COBBLES) 79.3 %

% - #4 (FINES) 20.7 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #24

DATE TESTED: 12-2-93

DEPTH: 2-5'

TECHNICIAN: David M. Lane

CHECKED BY: Spa. With

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 617.88 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 608.75 lbs

- 1" WET WEIGHT 600.51 lbs  
 % MOIST 15.0 %  
 DRY WEIGHT 522.18 lbs

TOTAL SAMPLE WEIGHT 1130.93 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 12.92 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 12.73 lbs

- #4 WET WEIGHT 44.87 lbs  
 % MOIST 9.2 %  
 DRY WEIGHT 41.09 lbs

REDUCED SAMPLE WEIGHT 53.82 lbs

% + #4 IN REDUCED SAMPLE 23.7 %

% - #4 IN REDUCED SAMPLE 76.3 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 123.76 lbs  
 + DRY WT. OF +1" IN BULK SAMPLE 608.75 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 732.51 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION  
 WET WEIGHT 698.0 g  
 DRY WEIGHT 607.1 g  
 WT. OF WATER 90.9 g  
 % MOISTURE 15.0 %

REDUCED SAMPLE -#4  
 WET WEIGHT 539.9 g  
 DRY WEIGHT 494.6 g  
 WT. OF WATER 45.3 g  
 % MOISTURE 9.2 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 732.51 lbs  
 TOTAL SAMPLE WEIGHT 1130.93 lbs

% + #4 (COBBLES) 64.8 %

% - #4 (FINES) 35.2 %



CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #25

DATE TESTED: 12/1-93

DEPTH: 6.5'-8.5'

TECHNICIAN: David M. [unclear]

CHECKED BY: Steve [unclear]

BULK SAMPLE WEIGHTS

+1" WET WEIGHT 739.64 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 728.71 lbs

-1" WET WEIGHT 576.66 lbs  
 % MOIST 10.8 %  
 DRY WEIGHT 466.30 lbs

TOTAL SAMPLE WEIGHT 1195.01 lbs

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 34.01 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 33.51 lbs

-#4 WET WEIGHT 45.98 lbs  
 % MOIST 11.4 %  
 DRY WEIGHT 41.27 lbs

REDUCED SAMPLE WEIGHT 74.78 lbs

% + #4 IN REDUCED SAMPLE 44.8 %

% -#4 IN REDUCED SAMPLE 55.2 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 208.90 lbs  
 + DRY WT. OF +1" IN BULK SAMPLE 728.71 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 937.61 lbs

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION

WET WEIGHT 855.5 g  
 DRY WEIGHT 771.8 g  
 WT. OF WATER 83.7 g  
 % MOISTURE 10.8 %

REDUCED SAMPLE -#4

648.9 g  
582.4 g  
66.5 g  
11.4 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 937.61 lbs  
 TOTAL SAMPLE WEIGHT 1195.01 lbs

% + #4 (COBBLES) 78.5 %

% -#4 (FINES) 21.5 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #26

DATE TESTED: 12-6-93

DEPTH: 0.0'-9.5'

TECHNICIAN: [Signature]

CHECKED BY: [Signature]

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 675.65 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 665.67 lbs

- 1" WET WEIGHT 624.43 lbs  
 % MOIST 6.4 %  
 DRY WEIGHT 586.87 lbs

TOTAL SAMPLE WEIGHT 1252.54 lbs

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 14.66 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 14.44 lbs

- #4 WET WEIGHT 42.90 lbs  
 % MOIST 6.0 %  
 DRY WEIGHT 40.77 lbs

REDUCED SAMPLE WEIGHT 54.91 lbs

% + #4 IN REDUCED SAMPLE 26.3 %

% - #4 IN REDUCED SAMPLE 73.7 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 154.35 lbs  
 + DRY WT. OF +1" IN BULK SAMPLE 665.67 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 820.02 lbs

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION  
 WET WEIGHT 551.0 g  
 DRY WEIGHT 518.1 g  
 WT. OF WATER 32.9 g  
 % MOISTURE 6.4 %

REDUCED SAMPLE -#4  
 WET WEIGHT 557.1 g  
 DRY WEIGHT 525.5 g  
 WT. OF WATER 31.6 g  
 % MOISTURE 6.0 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 820.02 lbs  
 TOTAL SAMPLE WEIGHT 1252.54 lbs

% + #4 (COBBLES) 65.5 %

% - #4 (FINES) 34.5 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #27

DATE TESTED: 12-3-93

DEPTH: 9.5'-11.0'

TECHNICIAN: David A. Fry

CHECKED BY: Steve Mills

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 900.36 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 887.05 lbs

-1" WET WEIGHT 319.62 lbs  
 % MOIST 11.0 %  
 DRY WEIGHT 287.95 lbs

TOTAL SAMPLE WEIGHT 1175.00 lbs

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 21.64 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 21.32 lbs

-#4 WET WEIGHT 37.10 lbs  
 % MOIST 11.0 %  
 DRY WEIGHT 33.42 lbs

REDUCED SAMPLE WEIGHT 54.74 lbs

% + #4 IN REDUCED SAMPLE 38.9 %

% -#4 IN REDUCED SAMPLE 61.1 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 112.01 lbs  
 + DRY WT. OF +1" IN BULK SAMPLE 887.05 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 999.06 lbs

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION

WET WEIGHT 705.3 g  
 DRY WEIGHT 635.5 g  
 WT. OF WATER 69.8 g  
 % MOISTURE 11.0 %

REDUCED SAMPLE -#4

646.8 g  
582.5 g  
64.3 g  
11.0 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 999.06 lbs  
 TOTAL SAMPLE WEIGHT 1175.00 lbs

% + #4 (COBBLES) 85.0 %

% -#4 (FINES) 15.0 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #28

DATE TESTED: 12-3-93

DEPTH: 00'-4.5'

TECHNICIAN: David M. Fair

CHECKED BY: Ann Witt

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 938.47 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 924.60 lbs

- 1" WET WEIGHT 161.34 lbs  
 % MOIST 21.5 %  
 DRY WEIGHT 132.79 lbs

TOTAL SAMPLE WEIGHT 1057.39 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 13.87 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 13.67 lbs

- #4 WET WEIGHT 48.77 lbs  
 % MOIST 9.5 %  
 DRY WEIGHT 44.54 lbs

REDUCED SAMPLE WEIGHT 58.21 lbs.

% + #4 IN REDUCED SAMPLE 23.5 %

% - #4 IN REDUCED SAMPLE 76.5 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 31.21 lbs  
 + DRY WT. OF + 1" IN BULK SAMPLE 924.60 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 955.81 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION  
 WET WEIGHT 876.5 g  
 DRY WEIGHT 721.2 g  
 WT. OF WATER 155.3 g  
 % MOISTURE 21.5 %

REDUCED SAMPLE -#4  
 WET WEIGHT 515.5 g  
 DRY WEIGHT 470.7 g  
 WT. OF WATER 44.8 g  
 % MOISTURE 9.5 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 955.81 lbs  
 TOTAL SAMPLE WEIGHT 1057.39 lbs

% + #4 (COBBLES) 90.4 %

% - #4 (FINES) 9.6 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #30

DATE TESTED: 12-6-93

DEPTH: 4.5'-7.5'

TECHNICIAN: David M. Jones

CHECKED BY: John White

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 874.78 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 861.85 lbs

- 1" WET WEIGHT 502.99 lbs  
 % MOIST 6.6 %  
 DRY WEIGHT 471.85 lbs

TOTAL SAMPLE WEIGHT 1333.70 lbs

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 21.41 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 21.09 lbs

- #4 WET WEIGHT 30.74 lbs  
 % MOIST 4.3 %  
 DRY WEIGHT 29.47 lbs

REDUCED SAMPLE WEIGHT 50.56 lbs.

% + #4 IN REDUCED SAMPLE 41.7 %

% - #4 IN REDUCED SAMPLE 58.3 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 196.76 lbs

+ DRY WT. OF +1" IN BULK SAMPLE 861.85 lbs

= TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 1058.61 lbs.

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION

WET WEIGHT 649.0 g  
 DRY WEIGHT 609.0 g  
 WT. OF WATER 40.0 g  
 % MOISTURE 6.6 %

REDUCED SAMPLE -#4

528.9 g  
507.0 g  
21.9 g  
4.3 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 1058.61 lbs

TOTAL SAMPLE WEIGHT 1333.70 lbs

% + #4 (COBBLES) 79.4 %

% - #4 (FINES) 20.6 %



CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: BACKGROUND PIT (ON-SITE) #31

DATE TESTED: 12-7-93

DEPTH: 35-11.5

TECHNICIAN: David M. [Signature]

CHECKED BY: [Signature]

BULK SAMPLE WEIGHTS

+1" WET WEIGHT 786.00 lbs.  
 % MOIST 1.5 %  
 DRY WEIGHT 774.38 lbs

-1" WET WEIGHT 454.95 lbs  
 % MOIST 10.7 %  
 DRY WEIGHT 410.98 lbs

TOTAL SAMPLE WEIGHT 1185.36 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 20.31 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 20.01 lbs

-#4 WET WEIGHT 37.92 lbs  
 % MOIST 11.2 %  
 DRY WEIGHT 34.10 lbs

REDUCED SAMPLE WEIGHT 54.11 lbs.

% + #4 IN REDUCED SAMPLE 37.0 %

% - #4 IN REDUCED SAMPLE 63.0 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 152.06 lbs  
 + DRY WT. OF +1" IN BULK SAMPLE 774.38 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 926.44 lbs

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION

REDUCED SAMPLE -#4

WET WEIGHT 639.4 g

515.6 g

DRY WEIGHT 577.8 g

463.8 g

WT. OF WATER 61.6 g

57.8 g

% MOISTURE 10.7 %

11.2 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 926.44 lbs

926.44 lbs

TOTAL SAMPLE WEIGHT 1185.36 lbs

1185.36 lbs

% + #4 (COBBLES) 78.2 %

% - #4 (FINES) 21.8 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #32

DATE TESTED: 12-8-93

DEPTH: 0.0' - 4.0'

TECHNICIAN: David M. Jones

CHECKED BY: Jim With

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 909.88 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 896.43 lbs

-1" WET WEIGHT 492.38 lbs  
 % MOIST 3.7 %  
 DRY WEIGHT 474.81 lbs

TOTAL SAMPLE WEIGHT 1371.24 lbs

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 33.73 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 33.23 lbs

-#4 WET WEIGHT 42.64 lbs  
 % MOIST 3.1 %  
 DRY WEIGHT 41.36 lbs

REDUCED SAMPLE WEIGHT 74.59 lbs

% + #4 IN REDUCED SAMPLE 44.6 %

% -#4 IN REDUCED SAMPLE 55.4 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 211.77 lbs  
 + DRY WT. OF + 1" IN BULK SAMPLE 896.43 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 1108.20 lbs

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION      REDUCED SAMPLE -#4

WET WEIGHT	<u>655.9 g</u>	<u>413.5 g</u>
DRY WEIGHT	<u>632.5 g</u>	<u>401.2 g</u>
WT. OF WATER	<u>23.4 g</u>	<u>12.3 g</u>
% MOISTURE	<u>3.7 %</u>	<u>3.1 %</u>

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 1108.20 lbs  
 TOTAL SAMPLE WEIGHT 1371.24 lbs

% + #4 (COBBLES) 80.8 %

% -#4 (FINES) 19.2 %

CALCULATIONS FOR COBBLES TO FINES RATIO

TEST PIT: #33

DATE TESTED: 12.8-93

DEPTH: 7.0' - 9.0'

TECHNICIAN: David M. Jones

CHECKED BY: Steve Witt

BULK SAMPLE WEIGHTS

+ 1" WET WEIGHT 923.26 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 909.62 lbs

-1" WET WEIGHT 413.68 lbs  
 % MOIST 9.0 %  
 DRY WEIGHT 379.52 lbs

TOTAL SAMPLE WEIGHT 1289.14 lbs.

REDUCED SAMPLE WEIGHTS (-1" FRACTION)

+ #4 WET WEIGHT 26.16 lbs  
 % MOIST 1.5 %  
 DRY WEIGHT 25.77 lbs

-#4 WET WEIGHT 44.09 lbs  
 % MOIST 6.9 %  
 DRY WEIGHT 41.24 lbs

REDUCED SAMPLE WEIGHT 67.02 lbs.

% + #4 IN REDUCED SAMPLE 38.5 %

% -#4 IN REDUCED SAMPLE 61.5 %

CONVERSION OF REDUCED SAMPLE PERCENTAGES TO WHOLE SAMPLE WEIGHTS

% + #4 IN REDUCED SAMPLE X DRY WT. OF -1" IN BULK SAMPLE 146.12 lbs  
 + DRY WT. OF + 1" IN BULK SAMPLE 909.62 lbs  
 = TOTAL DRY WEIGHT OF + #4 IN BULK SAMPLE 1055.74 lbs

MOISTURE CORRECTIONS

BULK SAMPLE -1" FRACTION  
 WET WEIGHT 535.1 g  
 DRY WEIGHT 491.1 g  
 WT. OF WATER 44.0 g  
 % MOISTURE 9.0 %

REDUCED SAMPLE -#4  
 WET WEIGHT 525.2 g  
 DRY WEIGHT 491.4 g  
 WT. OF WATER 33.8 g  
 % MOISTURE 6.9 %

COBBLES TO FINES RATIO

TOTAL DRY WEIGHT OF + #4 1055.74 lbs  
 TOTAL SAMPLE WEIGHT 1289.14 lbs

% + #4 (COBBLES) 81.9 %

% -#4 (FINES) 18.1 %

APPENDIX E

LABORATORY RADIOLOGICAL TEST RESULTS

VENDOR LABORATORY RADIOLOGICAL  
MEASUREMENTS: COMPOSITE SOIL SAMPLES >#4  
MESH SIEVE



FOR INFORMATION ONLY

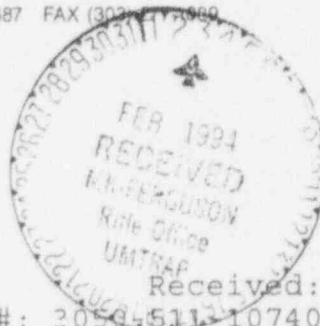


# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1999

31-Jan-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650



Attn:  
Project: Rifle

Received: 21-Dec-93 11:38  
PO #: 20504511-10740 #338

Job: 939351E

Status: Final

## ANALYTICAL REPORT PACKAGE

CASE NARRATIVE.....i  
 ANALYTICAL RESULTS.....R-1  
 QUALITY CONTROL REPORT.....Q-1

Init	Dist.	Info	Actn.	Exp.
<input checked="" type="checkbox"/>	F. WHITE	<input checked="" type="checkbox"/>		
<input checked="" type="checkbox"/>	E. SIMONSON	<input checked="" type="checkbox"/>		
<input checked="" type="checkbox"/>	E. STINE	<input checked="" type="checkbox"/>		
<input checked="" type="checkbox"/>	M. WENY	<input checked="" type="checkbox"/>		
<input type="checkbox"/>	B. W. LEE	<input type="checkbox"/>		
<input type="checkbox"/>	J. ROBERTS	<input type="checkbox"/>		
FILE				
M-FILE				

*copy was forwarded to Grant Channing*



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

31-Jan-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

Page: 1  
Copy: 1 of 1

Attn:  
Project: Rifle

Received: 21-Dec-93 11:38  
PO #: 3050-511-10740 #338

Job: 939351E

Status: Final

## CASE NARRATIVE

A total of 23 Soil samples were received on 21-Dec-93. All were properly preserved and in good condition. As stated in the chain of custody, the samples were run for the following analyses: Ra-226 and Th-230. Our procedures are summarized on the Quality Control Data Sheet. All samples were extracted and analyzed within the proper holding times.

Quality control standards for organic and inorganic analyses followed the appropriate SW-846 or EPA methodology. For radiochemistry, the acceptance criteria for spikes and laboratory control standards is fifteen percent, plus the counting error. Duplicates will pass if the Replicate Error Ratio (RER) is 1.00 or less. The RER is defined as follows:

$$RER = \frac{ABS(R2 - R1)}{SQRT(ERROR1^2 + ERROR2^2)}$$

where: R1/R2 = original/duplicate sample result  
ERROR1/ERROR2 = total 2 sigma uncertainty of R1/R2

All QC checks, including duplicates, spikes, and blanks, passed.

Signed:

*Steven L. Sincoff*  
.....  
Steven L. Sincoff, Ph.D.  
Director of Operations



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

31-Jan-94

Page: R-1

Copy: 1 of 3

Status: Final

## MK-FERGUSON (Rifle)

Analyte: Ra-226  
Fraction: Total  
Method: SM-705  
Units: pCi/g

Project: Rifle  
Date Analyzed: 01/25-01/31  
LLD: 0.3

Lab Id	Date Sampled	Matrix	Sample Id	Concentration ± 2σ
939351-1	30-Nov-93	Soil	RFL-SS-2649-01-CTF	1.1±0.6
939351-2	6-Dec-93	Soil	RFL-SS-2650-02-CTF	0.7±0.5
939351-3	7-Dec-93	Soil	RFL-SS-2651-03-CTF	1.7±0.7
939351-4	7-Dec-93	Soil	RFL-SS-2652-04-CTF	0.6±0.5
939351-5	7-Dec-93	Soil	RFL-SS-2653-05-CTF	1.4±0.6
939351-6	30-Nov-93	Soil	RFL-SS-2654-06-CTF	3.3±0.9
939351-7	7-Dec-93	Soil	RFL-SS-2655-07-CTF	2.0±0.7
939351-8	7-Dec-93	Soil	RFL-SS-2656-11-CTF	0.8±0.5
939351-9	6-Dec-93	Soil	RFL-SS-2657-15-CTF	0.9±0.5
939351-10	3-Dec-93	Soil	RFL-SS-2658-19-CTF	0.8±0.5
939351-11	2-Dec-93	Soil	RFL-SS-2659-20-CTF	0.5±0.4
939351-12	2-Dec-93	Soil	RFL-SS-2660-21-CTF	1.6±0.7
939351-13	10-Dec-93	Soil	RFL-SS-2661-22-CTF	0.9±0.5
939351-14	2-Dec-93	Soil	RFL-SS-2662-24-CTF	0.9±0.5
939351-15	1-Dec-93	Soil	RFL-SS-2663-25-CTF	0.8±0.5
939351-16	6-Dec-93	Soil	RFL-SS-2664-26-CTF	0.7±0.5
939351-17	6-Dec-93	Soil	RFL-SS-2665-27-CTF	0.8±0.5
939351-18	3-Dec-93	Soil	RFL-SS-2666-28-CTF	0.8±0.5
939351-19	3-Dec-93	Soil	RFL-SS-2667-29-CTF	2.1±0.8
939351-20	6-Dec-93	Soil	RFL-SS-2668-30-CTF	1.2±0.6
939351-21	7-Dec-93	Soil	RFL-SS-2669-31-CTF	0.9±0.5
939351-22	9-Dec-93	Soil	RFL-SS-2670-32-CTF	1.8±0.7
939351-23	9-Dec-93	Soil	RFL-SS-2671-33-CTF	1.6±0.7



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

31-Jan-94

Page: R-2

Copy: 1 of 3

Status: Final

MK-FERGUSON (Rifle)

Analyte: Th-230  
Fraction: Total  
Method: USAEC  
Units: pCi/g

Project: Rifle  
Date Analyzed: 01/20-01/26  
LLD: 0.4

Lab Id	Date Sampled	Matrix	Sample Id	Concentration+ 2σ
939351-1	30-Nov-93	Soil	RFL-SS-2649-01-CTF	1.1±0.4
939351-2	6-Dec-93	Soil	RFL-SS-2650-02-CTF	0.9±0.4
939351-3	7-Dec-93	Soil	RFL-SS-2651-03-CTF	0.5±0.3
939351-4	7-Dec-93	Soil	RFL-SS-2652-04-CTF	0.7±0.3
939351-5	7-Dec-93	Soil	RFL-SS-2653-05-CTF	0.3±0.2
939351-6	30-Nov-93	Soil	RFL-SS-2654-06-CTF	1.6±0.5
939351-7	7-Dec-93	Soil	RFL-SS-2655-07-CTF	1.7±0.5
939351-8	7-Dec-93	Soil	RFL-SS-2656-11-CTF	0.4±0.3
939351-9	6-Dec-93	Soil	RFL-SS-2657-15-CTF	0.8±0.4
939351-10	3-Dec-93	Soil	RFL-SS-2658-19-CTF	0.7±0.3
939351-11	2-Dec-93	Soil	RFL-SS-2659-20-CTF	0.8±0.4
939351-12	2-Dec-93	Soil	RFL-SS-2660-21-CTF	1.2±0.4
939351-13	10-Dec-93	Soil	RFL-SS-2661-22-CTF	0.9±0.4
939351-14	2-Dec-93	Soil	RFL-SS-2662-24-CTF	0.7±0.4
939351-15	1-Dec-93	Soil	RFL-SS-2663-25-CTF	1.3±0.5
939351-16	6-Dec-93	Soil	RFL-SS-2664-26-CTF	0.5±0.3
939351-17	6-Dec-93	Soil	RFL-SS-2665-27-CTF	0.8±0.4
939351-18	3-Dec-93	Soil	RFL-SS-2666-28-CTF	0.5±0.3
939351-19	3-Dec-93	Soil	RFL-SS-2667-29-CTF	2.3±0.6
939351-20	6-Dec-93	Soil	RFL-SS-2668-30-CTF	0.6±0.4
939351-21	7-Dec-93	Soil	RFL-SS-2669-31-CTF	0.7±0.4
939351-22	9-Dec-93	Soil	RFL-SS-2670-32-CTF	1.1±0.4
939351-23	9-Dec-93	Soil	RFL-SS-2671-33-CTF	0.5±0.3



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

31-Jan-94

Page: Q-1

Copy: 1 of 3

Status: Final

## MK-FERGUSON (Rifle)

### QUALITY CONTROL REPORT

Sample Id	Ra-226		Th-230	
	Total pCi/g	+ 2σ	Total pCi/g	+ 2σ
Duplicate	3.8	±1.0	0.7	±0.4
Duplicate	4.2	±1.0	0.4	±0.3
RER	0.18		0.46	
Std (found value)	80	±6	101	±7
Std (true value)	99		97	
Std % rec.	81		104	
Blank	0.0	±0.1	0.0	±0.1
Spike % rec.	96		77	





**BARRINGER LABORATORIES INC.**

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

31-Jan-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

Page: Q-2  
Copy: 1 of 3

Attn:  
Project: Rifle

Received: 21-Dec-93 11:38  
PO #: 3050-511-10740 #338

Job: 939351E

Status: Final

Abbreviations:

Parameters:

Ra-226 : Radium-226  
Th-230 : Thorium-230

Units:

pCi/g : picoCuries per gram



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

31-Jan-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

Page: Q-3  
Copy: 1 of 3

Attn:  
Project: Rifle

Received: 21-Dec-93 11:38  
PO #: 3050-511-10740 #338

Job: 939351E

Status: Final

## QUALITY CONTROL DATA SHEET

Received by: rc

Via: Client

Sample Container Type: 5gal bucket  
Additional Lab Preparation: None

Parameter	Method	Preservative	Analyst	Analysis Dates
Ra-226	SM-705	None	Lowrey	01/25-01/31
Th-230	USAEC	None	Kyle	01/20-01/26



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

31-Jan-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

Page: Q-4  
Copy: 1 of 3

Attn:  
Project: Rifle

Received: 21-Dec-93 11:38  
PO #: 3050-511-10740 #338

Job: 939351E

Status: Final

Signed:

*Helene Langlois*  
.....  
Radiochemistry Manager

Barringer Laboratories, Inc. will return or dispose of your samples 30 days from the date your final report is mailed, unless otherwise specified by contract. Barringer Laboratories, Inc. reserves the right to return samples prior to the 30 days if radioactive levels exceed our license.

cc: Helene Langlois, MK-FERGUSON (Rifle)

FOR INFORMATION ONLY 9351  
LABORATORY SERVICES AUTHORIZATION FORM

Page 1 of 2

Robert Fencil  
Requisitioner  
12/20/93  
Date

24 am 12/17/93  
12/21/94  
Need Date  
Priority X Standard

Rifle, CO  
Location  
3050-511-10740  
P.O. Number

338  
Request No.

ATTENTION LABORATORY:  
All reports and invoices must  
Reference PO and Request Nos

Type of Sample: \_\_\_\_\_ Water  Soil \_\_\_\_\_ Environmental Air Sample  
Occupational Air Sample \_\_\_\_\_ Vegetation

Type of Analysis:  Ra-226  Th-230 \_\_\_\_\_ Nat U. \_\_\_\_\_ Gross Alp  
Gross Beta \_\_\_\_\_ Solubility \_\_\_\_\_  
Other (Specify under special instructions)

Special Instructions/Comments: \_\_\_\_\_

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
RFL-SS-2649-01-CTF	11/30/93	~62 lbs	Test Pit #1 Cobbles
RFL-SS-2650-02-CTF	12/6/93		Test Pit #2 Cobbles
RFL-SS-2651-03-CTF	12/7/93		Test Pit #3 Cobbles
RFL-SS-2652-04-CTF	12/7/93		Test Pit #4 Cobbles
RFL-SS-2653-05-CTF	12/7/93		Test Pit #5 Cobbles
RFL-SS-2654-06-CTF	11/30/93		Test Pit #6 Cobbles
RFL-SS-2655-07-CTF	12/7/93		Test Pit #7 Cobbles
RFL-SS-2656-11-CTF	12/7/93		Test Pit #11 Cobbles
RFL-SS-2657-15-CTF	12/6/93		Test Pit #15 Cobbles
RFL-SS-2658-19-CTF	12/3/93		Test Pit #19 Cobbles

CHAIN-OF-CUSTODY

Relinquished by (Site Representative Signature): <i>James Stadelman</i>	Date/Time 12-21-93 0700
Carrier: <i>Daniel Frank</i>	Date/Time 12-21-93 0700
Received at Lab by (Lab Representative Signature):* <i>David R. Spivey</i>	Date/Time 12-21-93 1138

\*Barringer Chain-of-Custody as per contract will be attached

MK-F CWMFES USE ONLY:

*R. Lyman*  
MK-F Site Manager

*Robert L. Jamel*  
Health Physics Site Manager

Technical Review: \_\_\_\_\_ Date: \_\_\_\_\_

Ship to: Approved Vendor  
For Radioanalytical Services

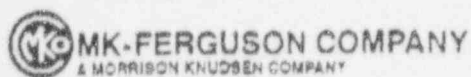
Copy to: HPP Manager

LABORATORY SERVICES AUTHORIZATION FORM  
(CONTINUATION PAGE)

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
BFL-SS-2659-20-CTF	12/2/93	~68 lbs	Test Pit # 20 Cobble
BFL-SS-2660-21-CTF	12/2/93		Test Pit # 21 Cobble
BFL-SS-2661-22-CTF	12/10/93		Test Pit # 22 Cobbles
BFL-SS-2662-24-CTF	12/2/93		Test Pit # 24 Cobbles
BFL-SS-2663-25-CTF	12/1/93		Test Pit # 25 Cobble
BFL-SS-2664-26-CTF	12/6/93		Test Pit # 26 Cobbles
BFL-SS-2665-27-CTF	12/6/93		Test Pit # 27 Cobble
BFL-SS-2666-28-CTF	12/3/93		Test Pit # 28 Cobble
BFL-SS-2667-29-CTF	12/3/93		Test Pit # 29 Cobbles
BFL-SS-2668-30-CTF	12/6/93		Test Pit # 30 Cobble
BFL-SS-2669-31-CTF	12/7/93		Test Pit # 31 Cobble
BFL-SS-2670-32-CTF	12/9/93		Test Pit # 32 Cobble
BFL-SS-2671-33-CTF	12/9/93	✓	Test Pit # 33 Cobble
N A			



ENGINEERS  
AND  
CONSTRUCTORS



HEADQUARTERS OFFICE  
ONE BRIEVING PLAZA  
CLEVELAND, OHIO U.S.A. 44114  
PHONE (216) 523-1600 TELEX 985542

FOR INFORMATION ONLY

\*Rich C -  
Please file in folder  
Thanks  
June

REPLY TO: MK-FERGUSON COMPANY  
REMEDIAL ACTIONS  
CONTRACTOR/UMTRA PROJECT  
P.O. BOX 8130  
ALBUQUERQUE, NEW MEXICO U.S.A. 87110

January 5, 1994

Barringer Laboratories  
15000 West 6th Avenue, Suite 300  
Golden, Colorado 80401  
Attn: June Brennan

Subject: Job No. 9351 - Rifle Site

Dear Ms. Brennan:

As per discussions today with Jim Turner, Barringer Laboratories is authorized to subcontract sample preparation work for samples containing large stone and cobbles for the subject Job Number.

Please contact Jim Turner at (505) 845-5868, if you have any questions.

Sincerely,

MK-Ferguson Company

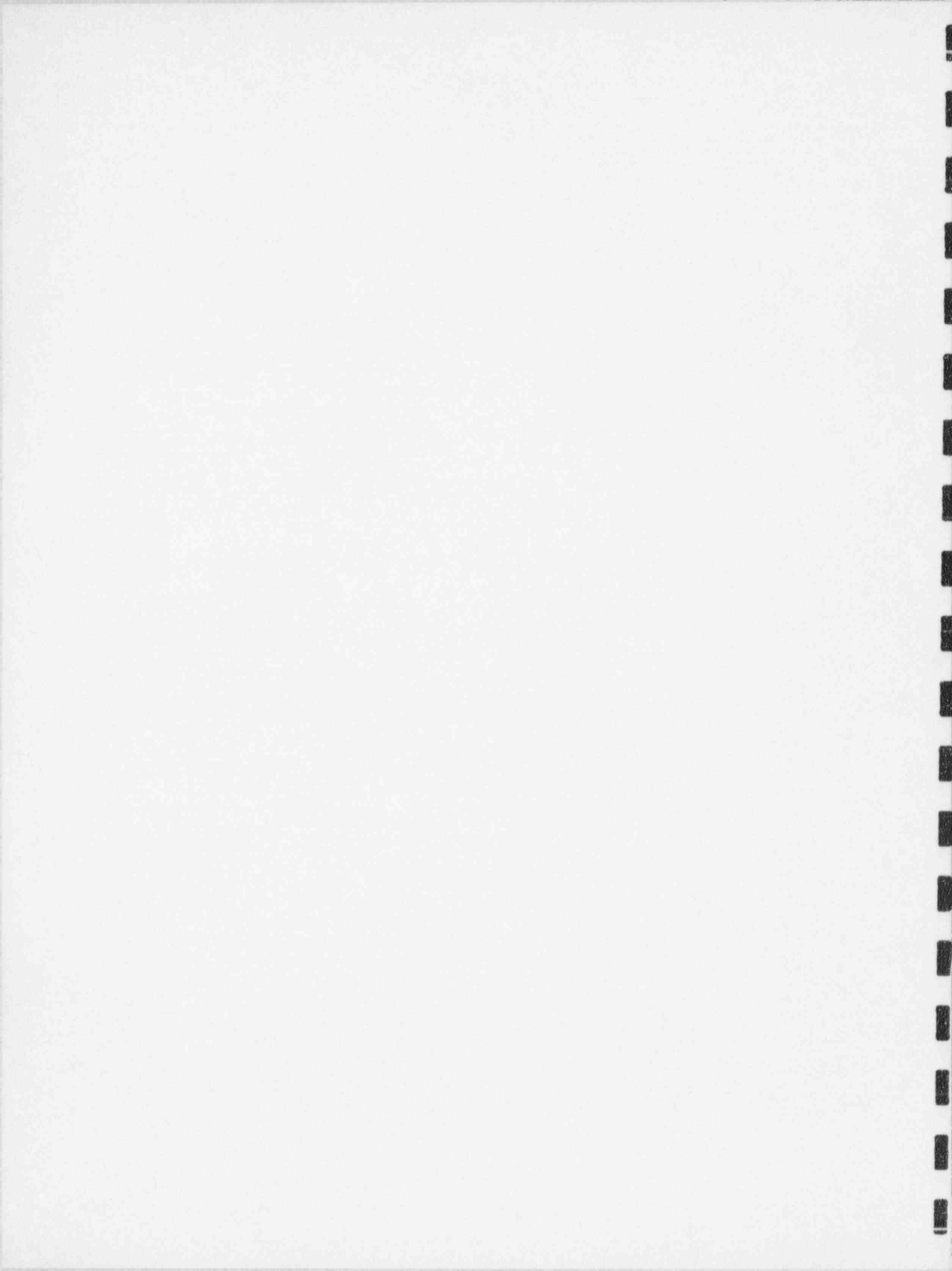
*Don L. Blasdel*

Don L. Blasdel  
Procurement Manager

DLB/JBT/jmg

Fax: 94-35  
Date: 1-5-94 4:19 p.m.  
Delivered to June

Received by Vera  
BARRINGER LABORATORIES, INC.



\*Subbed to SKYLINE for prep - Girson

BARRINGER LABORATORIES, INC.

15000 West 6th Ave. Suite #300, Golden, Colorado 80401  
 (303) 277-1687 Toll Free 1-800-654-0506 FAX (303) 277-1689

Chain-of-Custody Record

Client Barringer Labs Contact June Brennan  
 Address 15000 W 6th Ave Suite 300  
Golden CO 80401  
 Phone (303) 277-1687 Fax ( )

Project ID / Description \_\_\_\_\_  
 P.O. Number \_\_\_\_\_

STANDARD TAT  RUSH TAT (specify TAT): 3 day

ANALYSES REQUIRED

Indicate Parameters / Methods / Volumes / Preservatives

Vol																				
Pres																				

FOR INFORMATION ONLY

Crush, pulverize to 120-150 mesh

FOR BLI USE ONLY

- BLI # \_\_\_\_\_
- SAMPLES WERE (circle)
- Shipped / Hand delivered
  - Ambient / Chilled
  - In good condition Y N
  - Properly preserved Y N
  - Within holding times Y N
- COC TAPE WAS (circle)
- Present on outer pkg Y N
  - Unbroken on outer pkg Y N
  - Present on sample Y N
  - Unbroken on sample Y N
  - Sample labels/COC record in agreement? Y N
- IF the answer to any of the above qu is NO, please see attached Call Report

BLI ID #	Date Collected	Time Collected	Client Sample Identification	Matrix	No of Bottles	Filtered	Unfiltered
			9351-1, 2, 3, 4, 5, 6	rock	23		
			-7, 8, 9, 10, 11, 12				
			-13, 14, 15, 16, 17				
			-18, 19, 20, 21, 22, 23				

Comments

Comments / Special Instructions

\* please call JUNE Brennan when Ready \*

\* this is Logged

Relinquished by	Date/Time	Received by	Date/Time
<u>June Brennan</u>	<u>1-11-94 15:13</u>	<u>Paul Vester</u>	<u>1-6-94 0900</u>
Relinquished by	Date/Time	Received by	Date/Time
<u>Paul Vester</u>	<u>1-11-94 15:13</u>	<u>Paul Vester</u>	<u>1-11-94 1513</u>
Relinquished by	Date/Time	Received by	Date/Time
Relinquished by	Date/Time	Received by	Date/Time

PM Lab Order CHAIN

DEC63 PM LabData11 CUSTODY

BLI Job #93 9351

Rec'd Date 12-21-93

(circle one) Disposal / Return / Empty

Date

Sign-off

Date

PREPPED DRY

PREPPED COLD

Type SOIL Analyst

Type Analyst

Start 12/21/93 Complete 1/11/94

Start Complete

Comments Prepped by Skyline rec'd 1/11/94

Comments

BULK DRY

BULK COLD

Sample Type SOIL

Sample Type

Comments

Comments

Sample #'s 23

Sample #'s FOR INFORMATION ONLY

Location Buckets on Floor

Location

Sample #'s 1-23

Sample #'s

Location Soil Prep Shelf

Location

Date Time Out Time In Samp #s Initials

Date Time Out Time In Samp #s Initials

Date Time Out Time In Samp #s Initials

Date Time Out Time In Samp #s Initials

1/20 0920 1230 1-23 DM  
1/24/94 0910 1000 1,2 BB  
1/25/94 0207 0333 3-23 HGT

VENDOR LABORATORY RADIOLOGICAL  
MEASUREMENTS: COMPOSITE SOIL SAMPLES <#4  
MESH SIEVE



FOR INFORMATION ONLY

Recd. 3/14/94



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

9-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

Attn:  
Project: Rifle

Received: 28-Feb-94 09:20  
PO #: 3050-511-10740 #356

Job: 941417E

Status: Final

## ANALYTICAL REPORT PACKAGE

CASE NARRATIVE..... i  
ANALYTICAL RESULTS..... R-1  
QUALITY CONTROL REPORT..... Q-1

Init.	Dist.	Info	Actn	Comp
<input checked="" type="checkbox"/>	RWITKEE		<input checked="" type="checkbox"/>	
	C.SIMONSON			
	B.FENCIL		<input checked="" type="checkbox"/>	
	S.SUMMEY			
	S.YALJE			
	J.ROEGER			
FILE				
X-FILE				

FOR INFORMATION ONLY



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

9-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

Page: 1  
Copy: 1 of 3

Attn:  
Project: Rifle

Received: 28-Feb-94 09:20  
PO #: 3050-511-10740 #356

Job: 941417E

Status: Final

## CASE NARRATIVE

A total of 22 Soil samples were received on 28-Feb-94. All were properly preserved and in good condition. As stated in the chain of custody, the samples were run for the following analyses: Ra-226 and Th-230. Our procedures are summarized on the Quality Control Data Sheet. All samples were extracted and analyzed within the proper holding times.

Quality control standards for organic and inorganic analyses followed the appropriate SW-846 or EPA methodology. For radiochemistry, the acceptance criteria for spikes and laboratory control standards is fifteen percent, plus the counting error. Duplicates will pass if the Replicate Error Ratio (RER) is 1.00 or less. The RER is defined as follows:

$$\text{RER} = \frac{\text{ABS}(R2 - R1)}{\text{SQRT}(\text{ERROR1}^2 + \text{ERROR2}^2)}$$

where: R1/R2 = original/duplicate sample result  
ERROR1/ERROR2 = total 2 sigma uncertainty of R1/R2

All QC checks, including duplicates, spikes, and blanks, passed.

Signed:

..... *Steven L. Sincoff* .....  
Steven L. Sincoff, Ph.D.  
Director of Operations



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

9-Mar-94

Page: R-1

Copy: 1 of 3

Status: Final

MK-FERGUSON (Rifle)

Analyte: Ra-226  
Fraction: Total  
Method: SM-705  
Units: pCi/g

Project: Rifle  
Date Analyzed: 03/04-03/08  
LID: 0.3

Lab Id	Date Sampled	Matrix	Sample Id	Concentration	2σ
941417-1	6-Dec-93	Soil	RFL-SS-2596-TP-1-CTF	4.6	±1.1
941417-2	6-Dec-93	Soil	RFL-SS-2598-TP-2-CTF	1.7	±0.7
941417-3	7-Dec-93	Soil	RFL-SS-2600-TP-3-CTF	1.9	±0.7
941417-4	7-Dec-93	Soil	RFL-SS-2602-TP-4-CTF	7.4	±1.4
941417-5	7-Dec-93	Soil	RFL-SS-2604-TP-5-CTF	2.5	±0.8
941417-6	7-Dec-93	Soil	RFL-SS-2606-TP-7-CTF	220	±10
941417-7	7-Dec-93	Soil	RFL-SS-2608-TP-11-CTF	4.2	±1.1
941417-8	6-Dec-93	Soil	RFL-SS-2610-TP-15-CTF	6.3	±1.4
941417-9	2-Dec-93	Soil	RFL-SS-2612-TP-19-CTF	6.5	±1.3
941417-10	2-Dec-93	Soil	RFL-SS-2614-TP-20-CTF	8.6	±1.5
941417-11	6-Dec-93	Soil	RFL-SS-2616-TP-21-CTF	32	±3
941417-12	6-Dec-93	Soil	RFL-SS-2618-TP-22-CTF	2.4	±0.8
941417-13	1-Dec-93	Soil	RFL-SS-2620-TP-24-CTF	2.6	±0.8
941417-14	1-Dec-93	Soil	RFL-SS-2622-TP-25-CTF	5.4	±1.2
941417-15	6-Dec-93	Soil	RFL-SS-2624-TP-26-CTF	1.9	±0.7
941417-16	3-Dec-93	Soil	RFL-SS-2626-TP-27-CTF	3.2	±0.9
941417-17	9-Dec-93	Soil	RFL-SS-2628-TP-28-CTF	4.2	±1.0
941417-18	6-Dec-93	Soil	RFL-SS-2630-TP-29-CTF	110	±10
941417-19	6-Dec-93	Soil	RFL-SS-2632-TP-30-CTF	3.0	±0.9
941417-20	9-Dec-93	Soil	RFL-SS-2634-TP-32-CTF	1.7	±0.7
941417-21	9-Dec-93	Soil	RFL-SS-2636-TP-33-CTF	1.6	±0.7
941417-22	7-Dec-93	Soil	RFL-SS-2638-TP-BKG-CTF	1.8	±0.8



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

9-Mar-94

Page: R-2

Copy: 1 of 3

Status: Final

## MK-FERGUSON (Rifle)

Analyte: Th-230  
Fraction: Total  
Method: USAEC  
Units: pCi/g

Project: Rifle  
Date Analyzed: 03/03-03/08  
LLD: 0.4

Lab Id	Date Sampled	Matrix	Sample Id	Concentration+ 2σ
941417-1	6-Dec-93	Soil	RFL-SS-2596-TP-1-CTF	3.1±0.7
941417-2	6-Dec-93	Soil	RFL-SS-2598-TP-2-CTF	2.3±0.6
941417-3	7-Dec-93	Soil	RFL-SS-2600-TP-3-CTF	5.7±1.0
941417-4	7-Dec-93	Soil	RFL-SS-2602-TP-4-CTF	6.6±1.0
941417-5	7-Dec-93	Soil	RFL-SS-2604-TP-5-CTF	2.3±0.6
941417-6	7-Dec-93	Soil	RFL-SS-2606-TP-7-CTF	120±4
941417-7	7-Dec-93	Soil	RFL-SS-2608-TP-11-CTF	8.9±1.2
941417-8	6-Dec-93	Soil	RFL-SS-2610-TP-15-CTF	13±1
941417-9	2-Dec-93	Soil	RFL-SS-2612-TP-19-CTF	16±2
941417-10	2-Dec-93	Soil	RFL-SS-2614-TP-20-CTF	17±2
941417-11	6-Dec-93	Soil	RFL-SS-2616-TP-21-CTF	55±3
941417-12	6-Dec-93	Soil	RFL-SS-2618-TP-22-CTF	2.5±0.6
941417-13	1-Dec-93	Soil	RFL-SS-2620-TP-24-CTF	3.6±0.8
941417-14	1-Dec-93	Soil	RFL-SS-2622-TP-25-CTF	4.1±0.8
941417-15	6-Dec-93	Soil	RFL-SS-2624-TP-26-CTF	1.4±0.5
941417-16	3-Dec-93	Soil	RFL-SS-2626-TP-27-CTF	1.4±0.5
941417-17	9-Dec-93	Soil	RFL-SS-2628-TP-28-CTF	11±1
941417-18	6-Dec-93	Soil	RFL-SS-2630-TP-29-CTF	230±10
941417-19	6-Dec-93	Soil	RFL-SS-2632-TP-30-CTF	6.9±1.0
941417-20	9-Dec-93	Soil	RFL-SS-2634-TP-32-CTF	0.9±0.4
941417-21	9-Dec-93	Soil	RFL-SS-2636-TP-33-CTF	1.3±0.5
941417-22	7-Dec-93	Soil	RFL-SS-2638-TP-BKG-CTF	2.2±0.6



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

9-Mar-94

Page: Q-1

Copy: 1 of 3

Status: Final

## MK-FERGUSON (Rifle)

### QUALITY CONTROL REPORT

Sample Id	Ra-226		Th-230	
	Total pCi/g	+ 2σ	Total pCi/g	+ 2σ
Duplicate	0.0	±0.2	16	±2
Duplicate	0.3	±0.4	16	±2
RER	0.58		0.00	
Std (found value)	91	±6	311	±12
Std (true value)	99		305	
Std % rec.	91		102	
Blank	0.0	±0.1	0.2	±0.2
Spike % rec.	92		94	





# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

9-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

Page: Q-2  
Copy: 1 of 3

Attn:  
Project: Rifle

Received: 28-Feb-94 09:20  
PO #: 3050-511-10740 #356

Job: 941417E

Status: Final

Abbreviations:

Parameters:

Ra-226 : Radium-226  
Th-230 : Thorium-230

Units:

pCi/g : picoCuries per gram



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

9-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

Page: Q-3  
Copy: 1 of 3

Attn: Project: Rifle

Received: 28-Feb-94 09:20  
PO #: 3050-511-10740 #356

Job: 941417E

Status: Final

## QUALITY CONTROL DATA SHEET

Received by: rc

Via: UPS

Sample Container Type: 500g can  
Additional Lab Preparation: 100 mesh

Parameter	Method	Preservative	Analyst	Analysis Dates
Ra-226	SM-705	None	Lowrey	03/04-03/08
Th-230	USAEC	None	Melcher	03/03-03/08



**BARRINGER LABORATORIES INC.** FOR INFORMATION ONLY

15000 W. 8TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

9-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

Page: Q-4  
Copy: 1 of 3

Attn: Project: Rifle

Received: 28-Feb-94 09:20  
PO #: 3050-511-10740 #356

Job: 941417E

Status: Final

Signed: *Bill Vitorel*  
.....  
Radiochemistry Manager

Barringer Laboratories, Inc. will return or dispose of your samples 30 days from the date your final report is mailed, unless otherwise specified by contract. Barringer Laboratories, Inc. reserves the right to return samples prior to the 30 days if radioactive levels exceed our license.

cc: Helene Langlois, MK-FERGUSON (Rifle)



LABORATORY SERVICES AUTHORIZATION FORM

Jeff Fencil  
Requisitioner

2/25/94  
Date

3/14/94		FOR INFORMATION ONLY	
Need Date	Priority	Urgent	Standard
<input checked="" type="checkbox"/>			

Rifle, CO  
Location

3050-511-10740  
P.O. Number

356  
Request No.

ATTENTION LABORATORY:  
All reports and invoices must  
Reference PO and Request Nos.

Type of Sample: Water  Soil  Environmental Air Sample   
Occupational Air Sample  Vegetation

Type of Analysis:  Ra-226  Th-230  Nat U.  Gross Alpha  
 Gross Beta  Solubility  
 Other (Specify under special instructions)

Special Instructions/Comments: Final, composite

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
FL-SS-2596-TP-1-CTF	12/6/93	453g	TP-1 15-17'
FL-SS-2598-TP-2-CTF	12/6/93	473g	TP-2 13-16'
FL-SS-2600-TP-3-CTF	12/7/93	450g	TP-3 18-21'
FL-SS-2602-TP-4-CTF	12/7/93	453g	TP-4 11-16'
FL-SS-2604-TP-5-CTF	12/7/93	452g	TP-5 16-21'
FL-SS-2606-TP-7-CTF	12/7/93	432g	TP-7 11-21' 30/90
FL-SS-2608-TP-11-CTF	12/7/93	423g	TP-11 6-10'
FL-SS-2610-TP-15-CTF	12/6/93	460g	TP-15 10-13'
FL-SS-2612-TP-19-CTF	12/2/93	450g	TP-19 3.5-5.5'
FL-SS-2614-TP-20-CTF	12/2/93	520g	TP-20 1-5'

CHAIN-OF-CUSTODY

Relinquished by (Site Representative Signature): <u>Bobbie V. Hickey</u>	Date/Time: <u>2/25/94 @ 1047</u>
Carrier: <u>UPS PICKUP Record # 272 076 087</u>	Date/Time:
Received at Lab by (Lab Representative Signature): <u>R. Cantor</u>	Date/Time: <u>02/28/94 0920</u>

\*Barringer Chain-of-Custody as per contract will be attached

MK-F/CWMFES USE ONLY:

Scott B MK-F Site Manager Robert Fencil Health Physics Site Manager

Technical Review: \_\_\_\_\_ Date: \_\_\_\_\_

Copy to: Approved Vendor:  
For Radioanalytical Services

Copy to: HPP Manager





941417

LABORATORY SERVICES AUTHORIZATION FORM  
(CONTINUATION PAGE)

FOR INFORMATION ONLY

Page 2 of 2

3050-511-10740  
P.O. Number/Request Number

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
FEL-SS-2616-TP-21-CTF	12/6/93	502 g	TP-21 1-5'
FEL-SS-2618-TP-22-CTF	12/6/93	634 g	TP-22 4-7'
FEL-SS-2620-TP-24-CTF	12/1/93	509 g	TP-24 2.5-5'
FEL-SS-2622-TP-25-CTF	12/1/93	487 g	TP-25 6.5-8.5'
FEL-SS-2624-TP-26-CTF	12/6/93	508 g	TP-26 8-9.5'
FEL-SS-2626-TP-27-CTF	12/3/93	520 g	TP-27 9.5-11'
FEL-SS-2628-TP-28-CTF	12/9/93	510 g	TP-28 0-15'
FEL-SS-2630-TP-29-CTF	12/6/93	458 g	TP-29 0-3' 350/65
FEL-SS-2632-TP-30-CTF	12/6/93	518 g	TP-30 4.5-7.5'
FEL-SS-2634-TP-32-CTF	12/9/93	469 g	TP-32 0-4'
FEL-SS-2636-TP-33-CTF	12/9/93	454 g	TP-33 0-4'
FEL-SS-2638-TP-BK9-CTF	12/7/93	471 g	TP-BK9 7-12'

N





Internal Chain-of-Custody Record 00417

DEC93 PM LabData11.CUSTODY

BLI Job #94 1417

Rec'd by *[Signature]*  
 Rec'd date 2-28-94

How Disposed (circle one) Return / Waste / Sewer

Sign-off \_\_\_\_\_ Date \_\_\_\_\_

PREPPED DRY				PREPPED COLD			
Type	Soil	Analyst	SW	Type		Analyst	
Start	3/1/94	Complete	3/2/94	Start		Complete	
Comments				Comments			
Sample #'s 1-22				Sample #'s			
Location Soil Prep Shelf Y6				Location			

BULK DRY						BULK COLD					
Sample Type Soil						Sample Type					
Comments						Comments					
Sample #'s 22						Sample #'s					
Location Safe						Location					

Date	Samp #s	Time Out	Initials	Time In	Initials	Date	Samp #s	Time Out	Initials	Time In	Initials	Date	Samp #s	Time Out	Initials	Time In	Initials	Date	Samp #s	Time Out	Initials	Time In	Initials	
3/1/94	6	0750	BS	0920	BS							3/3	2710	1-22	DM	2350	DM							
3/1/94	1-22	3:30	QW	12:30	QW							3/4	0312	1/2	0345	1/2								
												3/7	1622	0028	1/2	0057	1/2							

VENDOR LABORATORY TH-230 MEASUREMENTS OF  
1-FT DEPTH INCREMENT SOIL SAMPLES <#4 MESH



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

1-Feb-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650



FOR INFORMATION ONLY

Attn:  
Project: Rifle

Received: 30-Dec-93 09:30  
PO #: 3050-511-10740 #341

Job: 939420E

Status: Final

## ANALYTICAL REPORT PACKAGE

CASE NARRATIVE.....i

ANALYTICAL RESULTS.....R-1

QUALITY CONTROL REPORT.....Q-1

*OK*  
*LB*

Int.	Det.	Info	Notes
<input checked="" type="checkbox"/>	RWTR	<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>	CSMKT	<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>	BFE	<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>	SM	<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>	LC	<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	
<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	

1-Feb-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

FOR INFORMATION ONLY

Page: i  
Copy: 1 of 3

Attn:  
Project: Rifle

Received: 30-Dec-93 09:30  
PO #: 3050-511-10740 #341

Job: 939420E

Status: Final

**CASE NARRATIVE**

A total of 30 Soil samples were received on 30-Dec-93. All were properly preserved and in good condition. As stated in the chain of custody, the samples were run for the following analysis: Th-230. Our procedures are summarized on the Quality Control Data Sheet. All samples were extracted and analyzed within the proper holding times.


Quality control standards for organic and inorganic analyses followed the appropriate SW-846 or EPA methodology. For radiochemistry, the acceptance criteria for spikes and laboratory control standards is fifteen percent, plus the counting error. Duplicates will pass if the Replicate Error Ratio (RER) is 1.00 or less. The RER is defined as follows:

$$RER = \frac{ABS(R2 - R1)}{SQRT(ERROR1^2 + ERROR2^2)}$$

where: R1/R2 = original/duplicate sample result  
ERROR1/ERROR2 = total 2 sigma uncertainty of R1/R2

All QC checks, including duplicates, spikes, and blanks, passed.

Signed:

  
.....  
Steven L. Sincoff, Ph.D.  
Director of Operations

**MK-FERGUSON (Rifle)**  
 FOR INFORMATION ONLY

Analyte: Th-230  
 Fraction: Total  
 Method: USAEC  
 Units: pCi/g

Project: Rifle  
 Date Analyzed: 01/28-01/02  
 LLD: 0.4

Lab Id	Date Sampled	Matrix	Sample Id	Concentration+ 2σ
939420-1	1-Dec-93	Soil	RFL-SS-2360✓	16±2
939420-2	1-Dec-93	Soil	RFL-SS-2354✓	2.7±0.7
939420-3	1-Dec-93	Soil	RFL-SS-2312✓	1.2±0.5
939420-4	1-Dec-93	Soil	RFL-SS-2392✓	1.9±0.6
939420-5	1-Dec-93	Soil	RFL-SS-2419✓	32±2
939420-6	1-Dec-93	Soil	RFL-SS-2402✓	40±2
939420-7	1-Dec-93	Soil	RFL-SS-2331✓	15±2
939420-8	1-Dec-93	Soil	RFL-SS-2345✓	7.3±1.1
939420-9	1-Dec-93	Soil	RFL-SS-2388✓	1.9±0.6
939420-10	3-Dec-93	Soil	RFL-SS-2464✓	9.3±1.2
939420-11	2-Dec-93	Soil	RFL-SS-2452✓	12±1
939420-12	2-Dec-93	Soil	RFL-SS-2460✓	8.8±1.2
939420-13	2-Dec-93	Soil	RFL-SS-2437✓	1.2±0.5
939420-14	2-Dec-93	Soil	RFL-SS-2494✓	1.0±0.4
939420-15	30-Nov-93	Soil	RFL-SS-2268✓	32±2
939420-16	30-Nov-93	Soil	RFL-SS-2247✓	3.8±0.8
939420-17	30-Nov-93	Soil	RFL-SS-2258✓	0.9±0.4
939420-18	30-Nov-93	Soil	RFL-SS-2244✓	10±1
939420-19	30-Nov-93	Soil	RFL-SS-2255✓	4.5±0.9
939420-20	2-Dec-93	Soil	RFL-SS-2520✓	4.1±0.8
939420-21	1-Dec-93	Soil	RFL-SS-2435✓	19±2
939420-22	1-Dec-93	Soil	RFL-SS-2361✓	5.7±0.9
939420-23	2-Dec-93	Soil	RFL-SS-2542✓	1.8±0.5
939420-24	2-Dec-93	Soil	RFL-SS-2440✓	7.7±1.1
939420-25	2-Dec-93	Soil	RFL-SS-2544✓	4.2±0.8
939420-26	30-Nov-93	Soil	RFL-SS-2310✓	1.6±0.5
939420-27	30-Nov-93	Soil	RFL-SS-2296✓	1.2±0.5
939420-28	1-Dec-93	Soil	RFL-SS-2325✓	8.1±1.1
939420-29	1-Dec-93	Soil	RFL-SS-2369✓	12±1
939420-30	1-Dec-93	Soil	RFL-SS-2318✓	5.2±0.9





# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

1-Feb-94  
Page: Q-1  
Copy: 1 of 3  
Status: Final

## MK-FERGUSON (Rifle)

### QUALITY CONTROL REPORT

FOR INFORMATION ONLY

Sample Id	Th-230	
	Total	
	pCi/g	+ 2σ
Duplicate	5.2	±0.9
Duplicate	4.6	±0.9
RER	0.24	
Std (found value)	292	±12
Std (true value)	305	
Std % rec.	96	
Blank	0.1	±0.2
Spike % rec.	101	



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

1-Feb-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

FOR INFORMATION ONLY

Page: Q-2  
Copy: 1 of 3

Attn:  
Project: Rifle

Received: 30-Dec-93 09:30  
PO #: 3050-511-10740 #341

Job: 939420E

Status: Final

Abbreviations:

Parameters:

Th-230 : Thorium-230

Units:

pCi/g : picoCuries per gram



**BARRINGER LABORATORIES INC.**

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

1-Feb-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

FOR INFORMATION ONLY

Page: Q-3  
Copy: 1 of 3

Attn: Project: Rifle

Received: 30-Dec-93 09:30  
PO #: 3050-511-10740 #341

Job: 939420E

Status: Final

QUALITY CONTROL REPORT

QUALITY CONTROL DATA SHEET

Received by: rc

Via: UPS

Sample Container Type: 500g can  
Additional Lab Preparation: 100 mesh

Parameter	Method	Preservative	Analyst	Analysis Dates
Th-230	USAEC	None	Ortiz	01/28-02/01



**LABORATORY SERVICES AUTHORIZATION FORM**

Robert Fencil  
Requisitioner

12 / 29 / 93  
Date

4 pm 12/29/93  
211193 Need Date  
Priority X Standard

Rifle, CO  
Location

3050-511-10740  
P.O. Number

341  
Request No.

**ATTENTION LABORATORY:**  
All reports and invoices must  
Reference PO and Request Nos.

FOR INFORMATION ONLY

Type of Sample: Water  Soil  Environmental Air Sample   
Occupational Air Sample  Vegetation

Type of Analysis: Ra-226  Th-230  Nat U.  Gross Al;  
Gross Beta  Solubility   
Other (Specify under special instructions)

Special Instructions/Comments: \_\_\_\_\_

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
RFL-SS-2360	12-1-93	696 gm	TP # 20 DUP
RFL-SS-2354	12-1-93	567 gm	TP # 20 DUP
L-SS-2312	12-1-93	419 gm	TP # 25
RFL-SS-2392	12-1-93	664 gm	TP # 24
RFL-SS-2419	12-1-93	510 gm	TP # 30
RFL-SS-2402	12-1-93	607 gm	TP # 28
RFL-SS-2331	12-1-93	592 gm	TP # 26
RFL-SS-2345	12-1-93	669 gm	TP # 27
RFL-SS-2388	12-1-93	632 gm	TP # 22
RFL-SS-2464	12-3-93	636 gm	TP # 4A DUP

CHAIN-OF-CUSTODY

Relinquished by (Site Representative Signature): Bonnie J. McCard Date/Time: 12/29/93 1000  
Carrier: UPS Pickup Record # 27076058 Date/Time: \_\_\_\_\_  
Received at Lab by (Lab Representative Signature): R.C. [Signature] Date/Time: 12/30/93 0930

\*Barringer Chain-of-Custody as per contract will be attached

**MK-F/CWM/FES USE ONLY:**  
MK-F Site Manager: [Signature]  
Health Physics Site Manager: Robert Fencil  
Date: \_\_\_\_\_

Ship to: Approved Vendor  
For Radioanalytical Services

Copy to: HPP Manager

9420

LABORATORY SERVICES AUTHORIZATION FORM  
(CONTINUATION PAGE)

Page 2 of 2

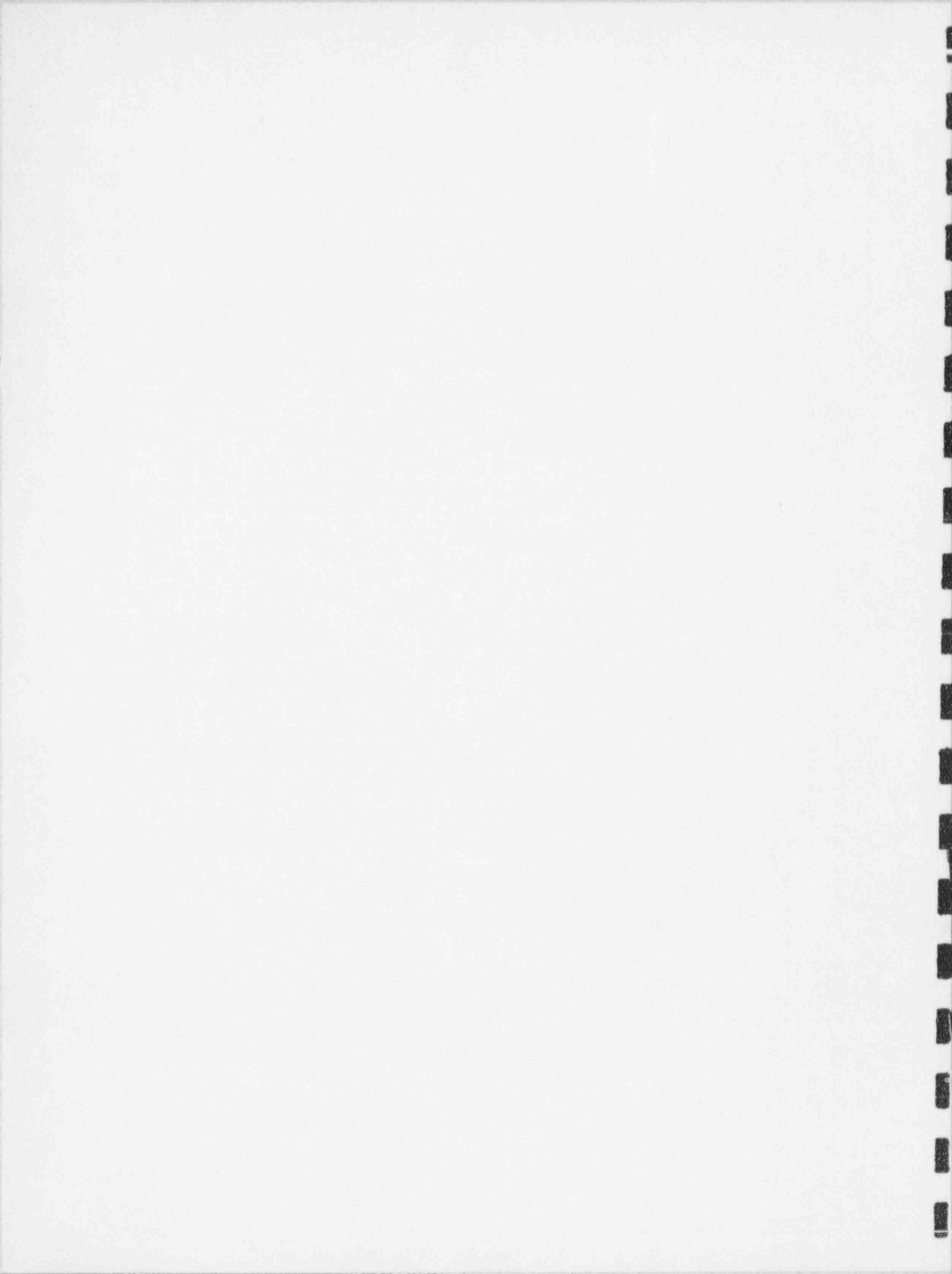
FOR INFORMATION ONLY

3050-511-10740/ 341  
P.O. Number/Request Number

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
RFL-SS-2452	12-2-93	513 gm	TP # 15
RFL-SS-2460	12-2-93	675 gm	TP # 15
RFL-SS-2437	12-2-93	468 gm	TP # 11
RFL-SS-2494	12-2-93	378 gm	TP # 2
RFL-SS-2268 490/160	11-30-93	487 gm	TP # 4
RFL-SS-2247	11-30-93	460 gm	TP # 1
RFL-SS-2258	11-30-93	653 gm	TP # 1
RFL-SS-2241	11-30-93	472 gm	TP # 1
RFL-SS-2255	11-30-93	550 gm	TP # 1
20 RFL-SS-2520	12-2-93	401 gm	TP # 3
RFL-SS-2435	12-1-93	581 gm	TP # 19
RFL-SS-2361	12-1-93	525 gm	TP # 21
RFL-SS-2542	12-2-93	449 gm	TP # 7
RFL-SS-2440	12-2-93	644 gm	TP # 11
RFL-SS-2544	12-2-93	617 gm	TP # 7
RFL-SS-2310	11-30-93	517 gm	TP # 6
RFL-SS-2296	11-30-93	612 gm	TP # 5
RFL-SS-2325	12-1-93	487 gm	TP # 26
RFL-SS-2369	12-1-93	600 gm	TP # 21
RFL-SS-2318	12-1-93	502 gm	TP # 25
N A			









# BARRINGER LABORATORIES INC

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689



9-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

Attn:  
Project: Rifle

Received: 15-Feb-94 09:30  
PO #: 3050-511-10740 #353

Job: 941337E \_\_\_\_\_ Status: Final \_\_\_\_\_

## ANALYTICAL REPORT PACKAGE

CASE NARRATIVE.....i  
ANALYTICAL RESULTS.....R-1  
QUALITY CONTROL REPORT.....Q-1





# BARRINGER LABORATORIES INC.

FOR INFORMATION ONLY

15000 W 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

9-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

Page: 1  
Copy: 1 of 3

Attn:  
Project: Rifle

Received: 15-Feb-94 09:30  
PO #: 3050-511-10740 #353

Job: 941337E

Status: Final

## CASE NARRATIVE

A total of 5 Soil samples were received on 15-Feb-94. All were properly preserved and in good condition. As stated in the chain of custody, the samples were run for the following analysis: Th-230. Our procedures are summarized on the Quality Control Data Sheet. All samples were extracted and analyzed within the proper holding times.

Quality control standards for organic and inorganic analyses followed the appropriate SW-846 or EPA methodology. For radiochemistry, the acceptance criteria for spikes and laboratory control standards is fifteen percent, plus the counting error. Duplicates will pass if the Replicate Error Ratio (RER) is 1.00 or less. The RER is defined as follows:

$$RER = \frac{ABS(R2 - R1)}{SQRT(ERROR1^2 + ERROR2^2)}$$

where: R1/R2 = original/duplicate sample result  
ERROR1/ERROR2 = total 2 sigma uncertainty of R1/R2

All QC checks, including duplicates, spikes, and blanks, passed.

Signed:

*Steven L. Sincoff*  
.....  
Steven L. Sincoff, Ph.D.  
Director of Operations



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION ONLY

9-Mar-94

Page: R-1

Copy: 1 of 3

Status: Final

MK-FERGUSON (Rifle)

Analyte: Th-230  
Fraction: Total  
Method: USAEC  
Units: pCi/g

Project: Rifle  
Date Analyzed: 03/07-03/09  
LLD: 0.4

Lab Id	Date Sampled	Matrix	Sample Id	Concentration+ 2σ
941337-1	1-Dec-93	Soil	RFL-SS-2405-TP28-CTF	30±2
941337-2	1-Dec-93	Soil	RFL-SS-2410-TP29-CTF	290±10
941337-3	1-Dec-93	Soil	RFL-SS-2424-TP30-CTF	22±2
941337-4	2-Dec-93	Soil	RFL-SS-2442-TP11-CTF	22±2
941337-5	2-Dec-93	Soil	RFL-SS-2446-TP11-CTF	25±2





# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

9-Mar-94

Page: Q-1

Copy: 1 of 3

Status: Final

FOR INFORMATION

MK-FERGUSON (Rifle)

## QUALITY CONTROL REPORT

Sample Id	Th-230	
	Total	
	pCi/g	+ 2 $\sigma$
Duplicate	25	$\pm 2$
Duplicate	28	$\pm 2$
RER	0.35	
Std (found value)	103	$\pm 8$
Std (true value)	97	
Std % rec.	106	
Blank	0.1	$\pm 0.3$
Spike % rec.	121	



9-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

FOR INFORMATION ONLY Page: Q-2  
Copy: 1 of 3

Attn:  
Project: Rifle

Received: 15-Feb-94 09:30  
PO #: 3050-511-10740 #353

Job: 941337E

Status: Final

Abbreviations:

Parameters:

Th-230 : Thorium-230

Units:

pCi/g : picoCuries per gram



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

FOR INFORMATION 9-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

Page: Q-3  
Copy: 1 of 3

Attn: Project: Rifle

Received: 15-Feb-94 09:30  
PO #: 3050-511-10740 #353

Job: 941337E Status: Final

## QUALITY CONTROL DATA SHEET

Received by: rc Via: UPS

Sample Container Type: 500g can  
Additional Lab Preparation: 100 mesh

Parameter	Method	Preservative	Analyst	Analysis Dates
Th-230	USAEC	None	Ortiz	03/07-03/09



**BARRINGER LABORATORIES INC.**

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

9-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

FOR INFORMATION ONLY

Page: Q-4  
Copy: 1 of 3

Attn: Project: Rifle

Received: 15-Feb-94 09:30  
PO #: 3050-511-10740 #353

Job: 941337E

Status: Final

Signed:

.....  
Radiochemistry Manager

Barringer Laboratories, Inc. will return or dispose of your samples 30 days from the date your final report is mailed, unless otherwise specified by contract. Barringer Laboratories, Inc. reserves the right to return samples prior to the 30 days if radioactive levels exceed our license.

cc: Helene Langlois, MK-FERGUSON (Rifle)

LABORATORY SERVICES AUTHORIZATION FORM

Page 1 of 1

Health Physics Requisitioner

21 111 94  
Date

31 161 94  
Need Date

Priority

Urgent

Standard

Rifle, CO  
Location

3050-511-10740  
P.O. Number

353

Request No.

ATTENTION LABORATORY:  
All reports and invoices must  
Reference PO and Request Nos.

Type of Sample: Water  Soil  Environmental Air Sample   
Occupational Air Sample  Vegetation

Type of Analysis: Ra-226  Th-230  Nat U.  Gross Alpha   
Gross Beta  Solubility   
Other (Specify under special instructions)

Special Instructions/Comments:

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
EL-SS-2405-TP28-CTF	12/1/93	608 g	TP# 28 2-3'
EL-SS-2410-TP29-CTF	12/1/93	651 g	TP# 29 2-3' 240 @ 120
EL-SS-2424-TP30-CTF	12/1/93	602 g	TP# 30 7-8'
EL-SS-2442-TP11-CTF	12/2/93	624 g	TP# 11 7-8'
EL-SS-2446-TP11-CTF	12/2/93	669 g	TP# 11 9-10'
		N	
		A	

CHAIN-OF-CUSTODY

Relinquished by (Site Representative Signature): <i>Bobbie V. Hickley</i>	Date/Time: 2/11/94 @ 1600
Carrier: UPS Pickup Record # 272076082	Date/Time: 2/14/94
Received at Lab by (Lab Representative Signature): <i>R. C. Intagli</i>	Date/Time: 02/15/94 0530

Barringer Chain-of-Custody as per contract will be attached

MK-F/CWMFES USE ONLY

*Ruby W. ...*  
MK-F Site Manager

*John H. Fencil*  
Health Physics Site Manager

Technical Review: \_\_\_\_\_ Date: \_\_\_\_\_

Ship to: Approved Vendor  
For Radioanalytical Services

Copy to: HPP Manager





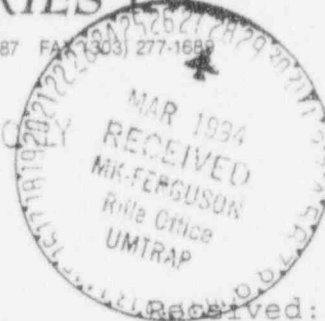
# BARRINGER LABORATORIES INC

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1688

24-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

FOR INFORMATION ONLY



Attn:  
Project: Rifle

Received: 16-Mar-94 09:25  
PO #: 3050-511-10740 #360

Job: 941524E

Status: Final

## ANALYTICAL REPORT PACKAGE

CASE NARRATIVE.....	i
ANALYTICAL RESULTS.....	R-1
QUALITY CONTROL REPORT.....	Q-1

Unit	DML	Info	Actn	Dist
P	FLM/KEE	/		
	COM/NDON	/		
	OFF/NDR			
	SR/ANDY			
	EXT/VE			
	SU/CP			
FILE				
X FILE				

*specials New Rifle CTF  
OK RF 3-29-94*



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

24-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

FOR INFORMATION ONLY

Page: 1  
Copy: 1 of 3

Attn: Project: Rifle

Received: 16-Mar-94 09:25  
PO #: 3050-511-10740 #360

Job: 941524E

Status: Final

## CASE NARRATIVE

A total of 9 Soil samples were received on 16-Mar-94. All were properly preserved and in good condition. As stated in the chain of custody, the samples were run for the following analysis: Th-230. Our procedures are summarized on the Quality Control Data Sheet. All samples were extracted and analyzed within the proper holding times.

Quality control standards for organic and inorganic analyses followed the appropriate SW-846 or EPA methodology. For radiochemistry, the acceptance criteria for spikes and laboratory control standards is fifteen percent, plus the counting error. Duplicates will pass if the Replicate Error Ratio (RER) is 1.00 or less. The RER is defined as follows:

$$RER = \frac{ABS(R2 - R1)}{SQRT(ERROR1^2 + ERROR2^2)}$$

where: R1/R2 = original/duplicate sample result  
ERROR1/ERROR2 = total 2 sigma uncertainty of R1/R2

All QC checks, including duplicates, spikes, and blanks, passed.

Signed:

..... *Steven L. Sincoff* .....  
Steven L. Sincoff, Ph.D.  
Director of Operations



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

24-Mar-94

Page: R-1

Copy: 1 of 3

Status: Final

MK-FERGUSON (Rifle)

FOR INFORMATION ONLY

Analyte: Th-230  
Fraction: Total  
Method: USAEC  
Units: pCi/g

Project: Rifle  
Date Analyzed: 03/21-03/22  
LLD: 0.4

Lab Id	Date Sampled	Matrix	Sample Id	Concentration+ 2σ
941524-1	30-Nov-93	Soil	RFL-SS-2272-CTF	7.6±1.1
941524-2	1-Dec-93	Soil	RFL-SS-2328-CTF	0.6±0.4
941524-3	1-Dec-93	Soil	RFL-SS-2357-CTF	0.6±0.4
941524-4	1-Dec-93	Soil	RFL-SS-2400-CTF	2.6±0.7
941524-5	1-Dec-93	Soil	RFL-SS-2401-CTF	38±2
941524-6	1-Dec-93	Soil	RFL-SS-2430-CTF	4.8±0.9
941524-7	1-Dec-93	Soil	RFL-SS-2432-CTF	44±3
941524-8	2-Dec-93	Soil	RFL-SS-2453-CTF	5.0±0.9
941524-9	2-Dec-93	Soil	RFL-SS-2456-CTF	23±2



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

24-Mar-94  
Page: Q-1  
Copy: 1 of 3  
Status: Final

MK-FERGUSON (Rifle)

## QUALITY CONTROL REPORT FOR INFORMATION ONLY

Sample Id	Th-230	
	Total	
	pCi/g	+ 2 $\sigma$
Duplicate	23	$\pm 2$
Duplicate	21	$\pm 2$
RER	0.28	
Std (found value)	327	$\pm 13$
Std (true value)	305	
Std % rec.	107	
Blank	0.0	$\pm 0.2$
Spike % rec.	90	



# BARRINGER LABORATORIES INC.

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

FOR INFORMATION ONLY

24-Mar-94

Page: Q-2  
Copy: 1 of 3

Attn:  
Project: Rifle

Received: 16-Mar-94 09:25  
PO #: 3050-511-10740 #360

Job: 941524E

Status: Final

Abbreviations:

Parameters:

Th-230 : Thorium-230

Units:

pCi/g : picoCuries per gram





# BARRINGER LABORATORIES INC.

15000 W 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

24-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

FOR INFORMATION ONLY

Page: Q-3  
Copy: 1 of 3

Attn:  
Project: Rifle

Received: 16-Mar-94 09:25  
PO #: 3050-511-10740 #360

Job: 941524E

Status: Final

## QUALITY CONTROL DATA SHEET

Received by: cs

Via: UPS

Sample Container Type: 500g can  
Additional Lab Preparation: 100 mesh

Parameter	Method	Preservative	Analyst	Analysis Dates
Th-230	USAEC	None	Ortiz	03/21-03/22



**BARRINGER LABORATORIES INC.**

15000 W. 6TH AVE., SUITE 300 GOLDEN, CO 80401 (303) 277-1687 FAX (303) 277-1689

24-Mar-94

ATTN: Site Manager  
MK-FERGUSON (Rifle)  
P.O. Box 151  
Rifle, CO 81650

FOR INFORMATION ONLY

Page: Q-4  
Copy: 1 of 3

Attn:  
Project: Rifle

Received: 16-Mar-94 09:25  
PO #: 3050-511-10740 #360

Job: 941524E

Status: Final

Signed:

.....  
Radiochemistry Manager

Barringer Laboratories, Inc. will return or dispose of your samples 30 days from the date your final report is mailed, unless otherwise specified by contract. Barringer Laboratories, Inc. reserves the right to return samples prior to the 30 days if radioactive levels exceed our license.

cc: Helene Langlois, MK-FERGUSON (Rifle)

**LABORATORY SERVICES AUTHORIZATION FORM**

Requester Robert Fencil  
Requisitioner 3114194  
Date

4118194  
Need Date  
 Priority  
 Urgent  
 Standard

Location Rifle, CO  
P.O. Number 3050-511-10740  
Request No. 360

**ATTENTION LABORATORY:**  
All reports and invoices MUST  
Reference PO and Request Nos.

Type of Sample:  Water  Soil  Environmental Air Sample  
 Occupational Air Sample  Vegetation

Type of Analysis:  Ra-226  Th-230  Nat U.  Gross Alpha  
 Gross Beta  Solubility  
 Other (Specify under special instructions)

Special Instructions/Comments: \_\_\_\_\_

I.D. NO	DATE COLLECTED	VOLUME	DESCRIPTION
FL-SS-2272-CTF	11-30-93	627	TP # 4
FL-SS-2328-CTF	12-01-93	517	TP # 26
FL-SS-2357-CTF	12-01-93	582	TP # 20
FL-SS-2400-CTF	12-01-93	648	TP # 26
FL-SS-2401-CTF	12-01-93	610	TP # 28
FL-SS-2430-CTF	12-01-93	531	TP # 19
FL-SS-2432-CTF	12-01-93	534	TP # 19
FL-SS-2453-CTF	12-02-93	537	TP # 15
FL-SS-2456-CTF	12-02-93	531	TP # 15

**CHAIN-OF-CUSTODY**

Relinquished by (Site Representative Signature): <u>Bobbie Hickey</u>	Date/Time <u>3/14/94 1605</u>
Carrier: <u>UPS Pickup Record # 272 076 097</u>	Date/Time <u>3/15/94</u>
Received at Lab by (Lab Representative Signature):* <u>Stephenson</u>	Date/Time <u>3-16-94/925</u>

Shipping Chain-of-Custody as per contract will be attached

**MK-F/CWM/FES USE ONLY:**

[Signature] F Site Manager  
[Signature] Health Physics Site Manager

Technical Review: \_\_\_\_\_ Date: \_\_\_\_\_

# Internal Chain-of-Custody Record

DEC93 FM LabData11 CUSTODY

**BLI Job #94** 1524

Rec'd by *JH*  
 Rec'd date 3-16-94

How Disposed, (circle one) Return / Waste / Sewer  
 Sign-off *JH* Date 3-25-94

PREPPED DRY		PREPPED COLD	
Type Soil	Analyst JW	Type	Analyst
Start 3/16/94	Complete 3/17/94	Start	Complete
Comments		Comments	
Sample #'s 1-9		Sample #'s	
Location Soil Prep Shelf		Location	

BULK DRY	BULK COLD
Sample Type soil	Sample Type
Comments	Comments
Sample #'s 9	Sample #'s
Location E3 Out	Location

Date	Samp #'s	Time Out	Initials	Time In	Initials	Date	Samp #'s	Time Out	Initials	Time In	Initials	Date	Samp #'s	Time Out	Initials	Time In	Initials
3/16/94	1-9	3:00	JW	3:10	JW	3/21/94	1-9	0332	JW	0352	JW						

INFORMATION ONLY

ON-SITE RADIOLOGICAL MEASUREMENTS OF 1-FT  
DEPTH INCREMENT SOIL SAMPLES <#4 MESH SIEVE





JSC ENVIRONMENTAL SERVICES, INC.  
A MORRIS ANDRUEN COMPANY

CWM Federal Environmental Services, Inc.

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	BI-214 pCi INITIAL 20 DAY	TI-208 pCi INITIAL 20 DAY	MASS (grams) WEL THY	Rn-220 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
11-20-93	RFL-SS-2237	11-19-93	11-22-93	400	512.1	853.3	406	1.3	2.1	✓	YU	@ Surface
12-10-93	-001			546	502.1	537.0	363	1.4	1.5		B	Main. Yard @ E.G. 601 cptm
11-20-93	RFL-SS-2238	11-19-93	11-22-93	500	274.7	795.9	401	0.69	2.0	✓	YU	@ Surface
12-13-93	-002			468	459.2	722.7	350	1.3	2.1		B	Main. Yard @ E.G. 573 cptm
11-20-93	RFL-SS-2239	11-19-93	11-22-93	402	636.3	522.4	336	1.9	1.6	✓	YU	@ Surface
12-13-93	-003			568	550.1	709.6	291	1.9	2.4		B	Main. Yard @ E.G. 546 cptm
11-22-93	RFL-SS-2240	11-20-93	11-23-93	510	345.9	1132	522	0.66	2.2	✓	YU	@ 18"
12-14-93	493			412	10283	888.2	568	18.	1.6	✓	B	10+65, 6+20 Lt.
11-22-93	RFL-SS-2241	11-20-93	11-23-93	548	14439	1419	515	28	2.8	✓	B	@ 4'
12-14-93	493			496	5374	1141	519	10.4	2.2	✓	B	10+65, 4+80 Lt.
11/30/93	RFL-SS-2242	11/30/93	12/1/93	430	11559	1115	482	2.4	2.3	✓	B	TP#1
12/21/93	TP#1			430	11559	1115	482	2.4	2.3	✓	B	0-1'
11/30/93	RFL-SS-2243	11/30/93	12/1/93	526	1737	882.2	550	3.2	1.6	✓	B	TP#1
12/21/93	TP#1			528	2841	1189	513	5.5	2.3	✓	B	1-2'
11/30/93	RFL-SS-2244	11/30/93	12/1/93	428	1187	896.9	503	2.4	1.8	✓	B	TP#1
12/21/93	TP#1			530	2011	1132	472	4.3	2.4	✓	B	2-3'
11/30/93	RFL-SS-2245	11/30/93	12/1/93	528	949.6	516.6	497	1.9	1.1	✓	B	TP#1
12/21/93	TP#1			434	1118	1001	456	2.5	2.2	✓	B	3-4'
11/30/93	RFL-SS-2246	11/30/93	12/1/93	432	1896	819.5	608	3.1	1.4	✓	B	TP#1
12/21/93	TP#1			532	3070	1247	523	5.9	2.4	✓	B	4-5'

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY:

*John R. Fernald*  
Site HP Manager



MK-FE  
A MORRIS  
JASON COMPANY  
A MUDSEN COMPANY



CWM Federal Environmental Services, Inc.

FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID DATE & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 POC INITIAL 20 DAY	TL-208 POC INITIAL 20 DAY	MASS (g) WET DRY	Hs-226 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
11/30/93	RFL-SS-22477	11/30/93	12-1-93	532	803	613.7	509	1.6	1.7		B	TP#1
12-21-93	TP #1			532	885	1084	460	1.9	2.4	✓	B	5-6'
11/30/93	RFL-SS-22478	11/30/93	12-1-93	434	527.7	896.9	495	1.1	1.8	✓	B	TP#1
12/21/93	TP #1			534	613	1132	450	1.4	2.5	✓	B	6-7'
11/30/93	RFL-SS-22479	11/30/93	12-1-93	534	815.8	816.5	507	1.7	1.7	✓	B	TP#1
12/21/93	TP #1			436	806	984	467	1.7	2.1	✓	B	7-8'
11/30/93	RFL-SS-22480	11/30/93	12-1-93	436	50.3	110.6	56.6	0.99	2.0	✓	B	TP#1
12/22/93	TP #1			440	781.7	1001	57.6	1.5	1.9	✓	B	8-9'
11/30/93	RFL-SS-22481	11/30/93	12-1-93	536	588.6	738.4	55.3	1.1	1.3	✓	B	TP#1
12/21/93	TP #1			438	685	975	50.8	1.3	1.9	✓	B	9-10'
11/30/93	RFL-SS-22482	11/30/93	12-1-93	438	709.8	870.7	59.9	1.2	1.5	✓	B	TP#1
12/22/93	TP #1			540	1055	863.0	53.5	2.0	1.6	✓	B	10-11'
11/30/93	RFL-SS-22483	11/30/93	12-1-93	538	1130	805.5	54.8	2.1	1.5	✓	B	TP#1
12/21/93	TP #1			536	802	1141	50.6	1.6	2.3	✓	B	11-12'
11/30/93	RFL-SS-22484	11-30-93	12-1-93	440	763.4	914.3	58.5	1.3	1.6	✓	PU	TP#1
12/21/93	TP #1			538	491	969	54.1	.91	1.8	✓	B	12'-13'
11/30/93	RFL-SS-22485	11-30-93	12-1-93	540	607.7	1151	60.7	1.0	1.9	✓	PU	TP#1
12/21/93	TP #1			440	986	1028	55.0	1.8	1.9	✓	B	13'-14'
11-30-93	RFL-SS-22486	11-30-93	12-1-93	442	740.2	1045	64.9	1.1	1.6	✓	PU	TP#1
12/21/93	TP #1			552	1193	873	60.2	2.0	1.5	✓	B	14'-15' Screened #4

REVIEWED BY: *[Signature]*  
Site HP Manager

Site Correction Factor = 1.8  
VP Correction Factor (if applicable) = 2.0  
Count Time = 500 sec, unless otherwise noted

RIFLE, CO. FOR INFORMATION ONLY  
**OCS SAMPLE LOG**

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	B-214 PGM INITIAL 20 DAY	Tl-208 PGM INITIAL 20 DAY	MASS (grams) MET DRY	Ra-226 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
11-30-93	RFL-SS-2257	11-30-93	12-2-93	542	750.2	1123	679	1.1	1.7		YU	TP#1
12-28-93	TP#1-DUP	11-30-93	12-2-93	454	541.5	914.3	537	0.92	1.6	✓	DEC	14'-15' Screened #4
11-30-93	RFL-SS-2258	11-30-93	12-1-93	444	481.5	966.5	696	0.69	1.4		YU	TP#1
12-21-93	TP#1	11-30-93	12-1-93	454	679	1176	653	1.0	1.8	✓	DEC	15'-16' Screened #4
11-30-93	RFL-SS-2259	11-30-93	12-2-93	544	652.1	1074	668	0.98	1.6		YU	TP#1
12-28-93	TP#1-DUP	11-30-93	12-2-93	452	543.1	1036	592	0.92	1.3	✓	DEC	15'-16' Screened #4
11-30-93	RFL-SS-2260	11-30-93	12-2-93	446	528.7	1010	732	0.72	1.4		YU	TP#1
12/22/93	TP#1	11-30-93	12/2/93	442	798.4	1062	601	1.3	1.8	✓	DEC	16'-17' Screened #4
11-30-93	RFL-SS-2261	11-30-93	12-2-93	546	906.8	911.0	770	1.2	1.2		YU	TP#1
12-28-93	TP#1-DUP	11-30-93	12-2-93	453	522	809.8	611	0.85	1.3	✓	DEC	16'-17' Screened #4
11-30-93	RFL-SS-2262	11-30-93	12-1-93	454	261040	8890	550	475	16.2		YU	TP#4
12-21-93	TP#4	11-30-93	12-1-93	554	382540	17635	505	758	35	✓	DEC	0-1'
11-30-93	RFL-SS-2263	11-30-93	12-1-93	554	266640	11824	573	465	21		YU	TP#4
12-21-93	TP#4	11-30-93	12-1-93	456	349720	11990	527	664	23	✓	DEC	1'-2'
11-30-93	RFL-SS-2264	11-30-93	12-1-93	456	282280	10736	581	486	18		YU	TP#4
12-21-93	TP#4	11-30-93	12-1-93	556	414310	20857	514	8.6	41	✓	DEC	2'-3'
11-30-93	RFL-SS-2265	11-30-93	12/2/93	556	881530	46594	650	1556	72		YU	TP#4
12/22/93	TP#4	11-30-93	12/2/93	572	919900	6697	495	1980	125	✓	DEC	3'-4'
11-30-93	RFL-SS-2266	11-30-93	12/2/93	458	858970	29892	604	1419	49		YU	TP#4
12-27-93	TP#4	11-30-93	12/2/93	400	957760	3292	453	2119	72	✓	DEC	4'-5'

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 scc. unless otherwise noted  
 REVIEWED BY: *John R. Thomas* Site HP Manager





MK-FEI  
A MORRIS  
ISON COMPANY  
MUDSEN COMPANY



CWM Federal Environmental Services, Inc.

SITE NAME  
RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 µCi INITIAL 20 DAY	T-208 µCi INITIAL 20 DAY	MASS (gross) REL DRY	Ra-226 µCi INITIAL 20 DAY	Th-232 µCi INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
11-30-93	RFL-SS-2267	11-30-93	12/1/93	558	34629	2129	580	60	3.7		PU	TP#4
12-21-93	TP#4	11-30-93	12/1/93	458	44658	2595	525	85	4.9	✓	PU	5'-6'
11-30-93	RFL-SS-2268	11-30-93	12/1/93	460	35265	2133	534	66	4.0	✓	PU	TP#4
12-21-93	TP#4	11-30-93	12/1/93	558	44725	2503	487	92	5.1	✓	PU	6'-7'
11-30-93	RFL-SS-2269	11-30-93	12/1/93	560	750.3	767.1	553	1.4	1.4		PU	TP#4
12-21-93	TP#4	11-30-93	12/1/93	460	601	949	499	1.2	1.9	✓	PU	7'-8'
11-30-93	RFL-SS-2270	11-30-93	12/1/93	462	18151	1289	595	31	2.2	✓	PU	TP#4
12-21-93	TP#4	11-30-93	12/1/93	560	23625	1812	539	44	3.4	✓	PU	8'-9'
11-30-93	RFL-SS-2271	11-30-93	12/1/93	562	677.1	757.6	541	1.3	1.4	✓	PU	TP#4
12-21-93	TP#4	11-30-93	12/1/93	462	832	801	516	1.6	1.6	✓	PU	9'-10'
11-30-93	RFL-SS-2272	11-30-93	12/1/93	464	6445	1324	701	9.2	1.9		PU	TP#4
12-21-93	TP#4	11-30-93	12/1/93	562	8585	1237	627	13	2.0	✓	PU	10'-11' Screened 4
11-30-93	RFL-SS-2273	11-30-93	12-2-93	564	5435	1208	690	7.9	1.8	✓	PU	TP#4
12-28-93	TP#4-DUP	11-30-93	12-2-93	546	6570	1266	556	12	2.3	✓	DRC	10'-11' Screened 4
11-30-93	RFL-SS-2274	11-30-93	12/1/93	466	1337	1062	645	2.1	1.6		PU	TP#4
12-21-93	TP#4	11-30-93	12/1/93	464	1614	1132	601	2.7	1.9	✓	PU	13'-14' Screened 4
11-30-93	RFL-SS-2275	11-30-93	12/1/93	566	1121	958.9	639	1.8	1.5		PU	TP#4
12-28-93	TP#4-DUP	11-30-93	12/2/93	552	1195	1160	572	2.1	2.0	✓	DRC	13'-14' Screened 4
11-30-93	RFL-SS-2276	11-30-93	12/1/93	472	5091	1080	586	8.7	1.8	✓	PU	TP#4
12-21-93	TP#4	11-30-93	12/1/93	466	5615	853	552	10	1.5	✓	PU	14'-15' Screened 4

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec., unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager

SITE NAME  
RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SCALED	OCS # INITIAL 20 DAY	BI-214 PCI INITIAL 20 DAY	TI-208 PCI INITIAL 20 DAY	MASS (gross) WET DRY	BI-228 PCB/g INITIAL/CORB 20 DAY	Th-232 Bq/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
11-30-93	RFL-SS-2277	11-30-93	12-2-93	573	6129	1103	620	9.9	1.8		PU	TP#4
12-28-93	TP#4-DUP	11-30-93	12-2-93	554	8020	1117	572	14	1.9	✓	DRC	14'-15' Screened 4
11-30-93	RFL-SS-2278	11-30-93	12-1-93	474	1255	1167	734	1.7	1.6		PU	TP#4
12-21-93	TP#4	11-30-93	12-1-93	564	1550	988	572	2.7	1.7	✓	PU	15'-16' Screened 4
11-30-93	RFL-SS-2279	11-30-93	12-2-93	575	1797	901.4	768	2.3	1.2		PU	TP#4
12-28-93	TP#4-DUP	11-30-93	12-2-93	550	2166	1170	671	3.2	1.7	✓	DRC	15'-16' Screened 4
12/1/93	RFL-SS-2280	11/30/93	12/2/93	400	6602	1115	877	7.5	1.3		PU	TP#4
12/27/93	TP#4	11/30/93	12/2/93	402	8611	1202	776	11	1.5	✓	DRC	16-17' Screened 4
12/1/93	RFL-SS-2281	11/30/93	12/2/93	500	6524	1180	824	7.7	1.4		PU	TP#4
12/28/93	TP#4-DUP	11/30/93	12/2/93	460	7105	1054	709	10	1.5	✓	DRC	16-17' Screened 4
12-1-93	RFL-SS-2282	11-30-93	12-2-93	502	15940	1889	798	20	2.4		PU	TP#4
12-27-93	TP#4	11-30-93	12-2-93	406	19325	1411	697	28	2.0	✓	DRC	17'-18' Screened 4
12-1-93	RFL-SS-2283	11-30-93	12-2-93	402	25979	1959	790	33	2.5		PU	TP#4
12-28-93	TP#4-DUP	11-30-93	12-2-93	556	34033	1927	664	51	2.9	✓	DRC	17'-18' Screened 4
12-1-93	RFL-SS-2284	11-30-93	12-2-93	504	8549	1295	775	11	1.7		PU	TP#4
12-27-93	TP#4	11-30-93	12-2-93	404	10678	1010	702	15	1.4	✓	DRC	18'-19'
12-1-93	RFL-SS-2285	11-30-93	12-2-93	404	28700	11067	559	514	20		PU	TP#5
12/22/93	TP#5	11-30-93	12/2/93	512	42470	22276	561	848	44	✓	PU	0'-1'
12-1-93	RFL-SS-2286	11-30-93	12/2/93	506	31590	15084	554	570	27		PU	TP#5
12/22/93	TP#5	11-30-93	12/2/93	414	435830	15430	494	882	31	✓	PU	1-2'

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec. unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager





MK-FE  
A MORRIS  
IRON COMPANY  
MUSSEN COMPANY



CWM Federal Environmental Services, Inc.

FOR INFORMATION ONLY

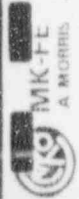
OCS SAMPLE LOG

SITE NAME RIFLE, CO.

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	BI-214 pCi INITIAL 20 DAY	TI-20B pCi INITIAL 20 DAY	MASS (grams) RET. IRY	He-220 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH: <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-1-93	RFL-SS-2237	11-30-93	12/2/93	406	33860	10745	608	482	18	✓	PU	TP#5
12/22/93	TP#5	11-30-93	12/2/93	514	42550	2250	540	788	42	✓	✓	2'-3'
12-1-93	RFL-SS-2238	11-30-93	12/2/93	508	37650	18450	601	626	31	✓	PU	TP#5
12/22/93	TP#5	11-30-93	12/2/93	416	46950	15177	528	889	29	✓	✓	3'-4'
12-1-93	RFL-SS-2239	11-30-93	12/2/93	408	50400	18782	538	938	35	✓	PU	TP#5
12/22/93	TP#5	11-30-93	12/2/93	516	704490	39076	467	1518	84	✓	✓	4'-5'
12-1-93	RFL-SS-2290	11-30-93	12/2/93	510	620950	33745	639	972	53	✓	PU	TP#5
12/22/93	TP#5	11-30-93	12/2/93	418	253690	23527	552	1329	43	✓	✓	5'-6'
12/1/93	RFL-SS-2291	11/30/93	12/2/93	440	67220	22667	653	958	36	✓	✓	TP#5
12/22/93	TP#5	11/30/93	12/2/93	518	82430	51379	574	1502	90	✓	✓	7'-8' 6-7'
12/1/93	RFL-SS-2292	11/30/93	12/2/93	512	54650	3129	533	1026	57	✓	✓	TP#5
12/22/93	TP#5	11/30/93	12/2/93	420	223750	24137	467	1550	52	✓	✓	7'-8'
12/1/93	RFL-SS-2293	11/30/93	12/2/93	472	47930	12005	612	783	30	✓	✓	TP#5
12/22/93	TP#5	11/30/93	12/2/93	520	688400	39661	539	1277	74	✓	✓	9-10'
12/1/93	RFL-SS-2294	11/30/93	12/2/93	514	67950	3766	540	1166	67	✓	✓	TP#5
12/22/93	TP#5	11/30/93	12/2/93	422	756020	24812	472	1559	53	✓	✓	10-11'
12/1/93	RFL-SS-2295	11/30/93	12/2/93	414	1391	992.6	540	3.5	1.8	✓	✓	TP#5
12/22/93	TP#5	11/30/93	12/2/93	522	1443	180	482	3.0	2.4	✓	✓	11-12'
12/1/93	RFL-SS-2296	11/30/93	12/2/93	516	2581	1285	716	3.6	1.8	✓	✓	TP#5
12/22/93	TP#5	11/30/93	12/2/93	424	776.7	8272	612	1.3	1.4	✓	✓	12-13'

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 SEC., unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site H/P Manager



**MK-TE**  
A MORRIS  
A KRUDSEN COMPANY



**CWM Federal Environmental S...**

FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	DCS # INITIAL 20 DAY	B6-214 pCi INITIAL 20 DAY	T1-208 pCi INITIAL 20 DAY	MASS (g) WET DRY	18-228 pCi/g INITIAL 20 DAY	TS-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12/1/93	RFL-SS-2297	11/30/93	12/2/93	416	668.8	1019	618	1.1	1.6		B	TP#5
12/22/93	TP#5	11/30/93	12/2/93	524	985.7	901.4	550	1.8	1.6	✓	B	13-14'
12/1/93	RFL-SS-2298	11/30/93	12/2/93	518	613.7	1314	707	0.87	1.9	✓	B	TP#5
12/22/93	TP#5	11/30/93	12/2/93	486	723.1	783.7	636	1.1	1.2	✓	B	14-15'
12/1/93	RFL-SS-2299	11/30/93	12/2/93	418	4890.0	1817.2	501	976.2	36.3		B	TP#5
12/22/93	TP#5	11/30/93	12/2/93	526	7082.6	4480.1	410	172.7	10.9	✓	B	8-9'
12/1/93	RFL-SS-2300	11/30/93	12/2/93	520	712.6	1132	720	1.1	1.6	✓	B	TP#5
12/22/93	TP#5	11/30/93	12/2/93	428	726.4	1028	639	1.1	1.6	✓	B	15-16'
12/1/93	RFL-SS-2301	11/30/93	12/2/93	420	1880	827.2	697	2.7	1.2		B	TP#5
12/22/93	TP#5	11/30/93	12/2/93	528	931.4	1036	599	1.6	1.7	✓	B	16-17'
12/1/93	RFL-SS-2302	11/30/93	12/2/93	522	3241	1026	771	4.2	1.3		B	TP#5
12/22/93	TP#5	11/30/93	12/2/93	430	3731	1028	675	5.5	1.5	✓	B	16-17' SCREENED 4
12/1/93	RFL-SS-2303	12/1/93	12/2/93	422	4408	914.3	722	6.1	1.3		B	TP#25
12/22/93	TP#25	12/1/93	12/2/93	530	4667	930.2	595	7.8	1.6	✓	B	10'
12/1/93	RFL-SS-2304	11/30/93	12/2/93	524	3575	1045	809	4.4	1.3		B	TP#5
12/28/93	TP#5-DUP	12/1/93	12/2/93	462	3672	1239	649	5.7	2.0	✓	DEC	16-17' SCREENED 4
12/1/93	RFL-SS-2305	11/30/93	12/2/93	424	683.8	951.8	837	0.82	1.1		B	TP#5
12/28/93	TP#5	11/30/93	12/2/93	530	773.0	931.2	692	1.1	1.3	✓	DEC	17-18' SCREENED 4
12/1/93	RFL-SS-2306	11/30/93	12/2/93	526	683.3	824.3	786	0.87	1.1		B	TP#5
12/28/93	TP#5-DUP	11/30/93	12/2/93	543	862.3	815.1	637	1.3	1.3	✓	DEC	17-18' SCREENED 4

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 SEC., unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager



MK-FE JSON COMPANY  
A MORRISON KNUDSEN COMPANY



CWME Federal Environmental Services, Inc.

SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	DCS # INITIAL 20 DAY	BI-214 pCi INITIAL 20 DAY	TI-208 pCi INITIAL 20 DAY	MASS (gross) WET DRY	Be-228 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12/1/93	RFL-SS-2307	11/30/93	12/2/93	496	1794	870.7	757	2.4	7.2	TP#5	B	TP#5
12/22/93	TP#5	11/30/93	12/2/93	432	2743	1036	661	4.1	1.6	18-19' screened	B	TP#5
12/1/93	RFL-SS-2308	11/30/93	12/2/93	528	1552	1093	760	2.0	1.4	TP#5	B	TP#5
12/28/93	TP#5-DUP	11/30/93	12/2/93	456	2296	835.9	636	3.6	1.3	18-19' screened	ORC	TP#5
12/1/93	RFL-SS-2309	11/30/93	12/3/93	428	2231	810.7	789	2.8	1.1	TP#5	B	TP#5
12-28-93	TP#5	11/30/93	12/3/93	526	2450	755.4	670	3.7	1.1	19-20'	ORC	TP#5
12/1/93	RFL-SS-2310	11/30/93	12/2/93	530	8750	786.3	576	1.5	1.4	TP#6	B	TP#6
12/22/93	TP#6	11/30/93	12/2/93	532	1190	652.1	517	2.3	1.3	14-15'	B	TP#6
12/1/93	RFL-SS-2311	11/30/93	12/2/93	430	2804	801.1	501	5.6	1.6	TP#25	B	TP#25
12/22/93	TP#25	11/30/93	12/2/93	434	4692	792.4	465	10.0	1.7	0-1'	B	TP#25
12/1/93	RFL-SS-2312	11/30/93	12/2/93	582	820.9	834.3	531	1.5	1.6	TP#25	B	TP#25
12/27/93	TP#25	11/30/93	12/2/93	510	6430	872.6	419	1.5	2.1	1-2'	ORC	TP#25
12/1/93	RFL-SS-2313	11/30/93	12-3-93	432	5131	2651	837	61.0	3.0	TP#6	B	TP#6
12-28-93	TP#6	11/30/93	12-3-93	536	6233	2656	759	95	3.6	24-25'	ORC	TP#6
12/1/93	RFL-SS-2314	11/30/93	12/2/93	534	2896	2206	883	3.2	2.5	TP#6	B	TP#6
12/22/93	TP#6	11/30/93	12/2/93	534	3353	2254	826	4.1	2.7	24-25'	B	TP#6
12/1/93	RFL-SS-2315	11/30/93	12/3/93	431	752.6	653.1	648	1.2	1.0	TP#25	B	TP#25
12/23/93	TP#25	11/30/93	12/3/93	439	534.3	801.1	517	1.1	1.5	2-3'	ORC	TP#25
12/1/93	RFL-SS-2316	11/30/93	12/3/93	536	757.8	680.8	631	1.2	1.1	TP#25	B	TP#25
12-28-93	TP#25	11/30/93	12/3/93	534	526.1	949.3	503	1.0	1.9	3-4'	ORC	TP#25

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec, unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager





MK-FE  
A MORRISON KNUDSEN COMPANY



CWM Federal Environmental Services, Inc.

SITE NAME  
RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Re-226 pCi/g INITIAL 20 DAY	Pb-210 pCi/g INITIAL 20 DAY	DEPTH < 15cm > 15cm	TECH INITIAL 20 DAY	COMMENTS
12-1-93	RFL-SS-2317	12-1-93	12-3-93	436	1054	705.3	725	1.5	0.97	✓	PU	TP#25
12-28-93	TP#25	12-1-93	12-3-93	432	845.2	905.6	586	1.4	1.5	✓	DRC	4'-5'
12-1-93	RFL-SS-2318	12-1-93	12-3-93	538	1875	882.2	615	3.0	1.4	✓	PU	TP#25
12-27-93	TP#25	12-1-93	12-3-93	457	3358	958.3	502	6.7	1.7	✓	DRC	6'-7'
12-1-93	RFL-SS-2319	12-1-93	12-2-93	488	8418	655.1	732	1.2	0.90	✓	PU	TP#25
12/22/93	TP#25	12-1-93	12-3-93	76	588.9	766.3	618	0.95	1.2	✓	B	5'-6'
12-1-93	RFL-SS-2320	12-1-93	12-3-93	540	318.2	1064.8	769	4.2	1.4	✓	PU	TP#25
12-28-93	TP#25	12-1-93	12-3-93	510	542.3	1232	609	0.89	2.0	✓	DRC	7'-8' SOLID
12-1-93	RFL-SS-2321	12-1-93	12-3-93	442	730.9	846.9	712	0.95	1.2	✓	PU	TP#25
12-28-93	TP#25-Dup	12-1-93	12-3-93	506	914.9	920.6	622	1.5	1.5	✓	DRC	7'-8' SOLID
12-1-93	RFL-SS-2322	12-1-93	12-3-93	542	6015	446.8	765	0.79	1.0	✓	PU	TP#25
12-28-93	TP#25	12-1-93	12-3-93	525	322.1	901.4	634	0.57	1.9	✓	DRC	8'-9' SOLID
12-1-93	RFL-SS-2323	12-1-93	12-3-93	442	66.9	801.1	792	0.83	1.0	✓	PU	TP#25
12-28-93	TP 25-Dup	12-1-93	12-3-93	518	703.0	719.2	657	1.1	1.1	✓	DRC	8'-9' SOLID
12-1-93	RFL-SS-2324	12-1-93	12-2-93	544	3305	930.2	524	6.3	1.8	✓	PU	TP#25
12/22/93	TP 26	12-1-93	12-2-93	536	5072	1285	475	11	2.7	✓	B	0'-1'
12-1-93	RFL-SS-2325	12-1-93	12-1-93	444	2144	801.1	529	4.1	1.5	✓	PU	TP#26
12/22/93	TP#26	12-1-93	12-2-93	438	3457	1010	487	7.1	2.1	✓	B	1'-2'
12-1-93	RFL-SS-2326	12-1-93	12-2-93	546	1805	911.2	582	3.1	1.6	✓	PU	TP#26
12/22/93	TP#26	12-1-93	12-2-93	538	3517	1064	529	6.8	2.0	✓	B	2'-3'

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 SEC, unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager



MK-FC JSON COMPANY  
A MORRISON-KRUDSEN COMPANY



CWM Federal Environmental Services, Inc.

OCS SAMPLE LOG

FOR INFORMATION ONLY

RIFLE, CO.

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	BI-214 pCi INITIAL 20 DAY	TI-208 pCi INITIAL 20 DAY	MASS (gross) WGT. DRYS	Ba-220 pCi/g INITIAL (CORR.) 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-1-93	RFL-SS-2327 TF #26	12-1-93	12-3-93	446 442	7443 5027	9143 1271	608 559	1.2 .91	1.5 2.8	✓	PU DRC	TF#26 3'-4'
12-28-93	RFL-SS-2328 TF #26	12-1-93	12/3/93	548 408	3940 5018	6329 7224	547 517	.73 .97	4.2 1.5	✓	PU B	TF#26 4'-5'
12-1-93	RFL-SS-2329 TF #26	12-1-93	12/3/93	448 410	5458 7018	5921 7485	759 600	.72 1.2	.78 1.2	✓	PU B	TF#26 5'-6'
12-1-93	RFL-SS-2330 TF #26	12-1-93	12/3/93	550 408	5897 6353	6017 7053	757 632	.78 1.0	.87 1.1	✓	PU B	TF#26 6'-7'
12-1-93	RFL-SS-2331 TF #26	12-1-93	12-3-93	450 400	2612 4491	6879 8620	715 592	3.7 7.6	.96 1.5	✓	PU DRC	TF #26 7'-8'
12-28-93	RFL-SS-2332 TF #27	12-1-93	12-2-93	552 560	8557 14060	4612 5154	554 501	16 281	8.3 11	✓	PU DRC	TF #27 0'-1'
12-1-93	RFL-SS-2333 TF #27	12-1-93	12-2-93	452 460	87813 179200	3039 6452	557 534	115 350	5.2 12	✓	PU DRC	TF #27 1'-2'
12-1-93	RFL-SS-2334 TF #27	12-1-93	12/3/93	551 510	93640 197460	4881 8554	629 539	115 370	7.8 16	✓	PU B	TF #27 2'-3'
12-1-93	RFL-SS-2335 TF #27	12-1-93	12-2-93	451 404	96750 180900	4197 6519	589 535	164 349	7.1 12	✓	PU DRC	TF #27 3'-4'
12-1-93	RFL-SS-2336 TF #27	12-1-93	12-2-93	550 553	100050 179730	4852 6895	550 491	180 364	8.7 14	✓	PU DRC	TF #27 4'-5'

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 300 sec., unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager





SITE NAME: RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	BI-214 pCi INITIAL 20 DAY	TI-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	IR-220 pCi/g INITIAL 20 DAY	TR-232 pCi/g INITIAL 20 DAY	DEPTH < 15cm > 15cm	TECH INITIAL 20 DAY	COMMENTS
12-1-93	RFL-SS-2337	12-1-93	12-2-93	456	5624	2665	589	99	4.5	✓	PU	TP#27
12-28-93	TP#27			468	81416	3596	545	150	6.7	✓	DEC	5'-6'
12-1-93	RFL-SS-2338	12-1-93	12-2-93	558	47823	24922	564	840	4.4		PU	TP#27
12-28-93	TP#27			562	56460	25766	512	1103	5.0	✓	DEC	6'-7'
12-1-93	RFL-SS-2339	12-1-93	12-5-93	458	104980	37668	556	1753	6.4		PU	TP#27
12-27-93	TP#27			459	104980	34231	572	2792	8.7	✓	DEC	7'-8'
12-1-93	RFL-SS-2340	12-1-93	12/3/93	565	4668	853.4	556	8.4	1.5		PU	TP#27
12/29/93	TP#27			412	3996	809.8	442	9.0	1.8	✓	B	8'-9'
12-1-93	RFL-SS-2341	12-1-93	12-3-93	466	1099	818.5	790	1.4	1.0		PU	TP#27
12-28-93	TP#27			436	1437	745.3	634	2.3	1.2	✓	DEC	10'-11' SCREENS
12-1-93	RFL-SS-2342	12-1-93	12-3-93	562	1414	843.9	821	1.8	1.0		PU	TP#27
12-28-93	TP#27-DUP			412	1533	862.0	674	2.3	1.3	✓	DEC	10'-11' SCREENS
12-1-93	RFL-SS-2343	12-1-93	12-2-93	470	3707	1045	790	4.7	1.3		PU	TP#27
12-28-93	TP#27			470	5068	914.3	696	7.8	1.4	✓	DEC	11'-12' SCREENS
12-1-93	RFL-SS-2344	12-1-93	12-2-93	564	3892	1017	769	5.1	1.3		PU	TP#27
12-28-93	TP#27-DUP			563	4861	911.6	637	7.6	1.4	✓	DEC	11'-12' SCREENS
12-1-93	RFL-SS-2345	12-1-93	12-3-93	464	4699	1480	819	5.7	1.8		PU	TP#27
12-28-93	TP#27			500	6267	1912	669	9.4	2.7	✓	DEC	9'-10' SCREENS
12-1-93	RFL-SS-2346	12-1-93	12/3/93	566	5932	1381	839	7.2	1.7		PU	TP#27
12/29/93	TP#27-DUP			506	6822	1256	684	10.	1.8	✓	B	9'-10' SCREENS

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 SEC. unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager



MK-FL USON COMPANY  
A MORRISON KNUDSEN COMPANY



CWM Federal Environmental Services, Inc.

FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 (pCi) INITIAL 20 DAY	Tl-208 (pCi) INITIAL 20 DAY	MASS (micrograms) WEL DRY	Ba-220 (pCi/g) INITIAL 20 DAY	Th-232 (pCi/g) INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-2-93	RFL-SS-2347	12-1-93	12/3/93	400	768.6	896.9	576	1.3	1.6		YU	TP#19 (compare to 12-2-93-1)
1/11/94	TP#19	12-1-93	12/3/93	426	781.7	1001	557	1.4	1.8	✓	YU	5.5' - 6.5'
12-2-93	RFL-SS-2348	11-30-93	12/2/93	500	387.5	1026	407.9	0.95	2.5	✓	YU	TP#1 (compare to 12-2-93)
2-11-94	TP#1	11-30-93	12/2/93	508	402.2	939.6	407.9	0.99	2.3	✓	WUW	14' - 17'
12-2-93	RFL-SS-2349	11-30-93	12/2/93	502	1226	911.0	489.4	2.5	1.9	✓	YU	TP#4 (compare to 12-2-93)
2-11-94	TP#4	11-30-93	12/2/93	502	1027	1055	489.4	2.1	2.2	✓	WUW	15' - 16.5'
12-2-93	RFL-SS-2350	11-30-93	12/2/93	402	3512	775.0	375.2	9.4	2.1	✓	YU	TP#4 (compare to 12-2-93)
2-11-94	TP#4	11-30-93	12/2/93	500	4637	1007	375.2	12.4	2.7	✓	WUW	11.5' - 15.0'
12-2-93	RFL-SS-2351	11-30-93	12/2/93	504	979.5	824.7	398.4	2.5	2.1	✓	YU	TP#5 (compare to 12-2-93)
2-11-94	TP#5	11-30-93	12/2/93	504	804.7	901.4	398.4	2.0	2.3	✓	WUW	16.5' - 18.0'
12-2-93	RFL-SS-2352	11-30-93	12/2/93	404	2645	1001	406.1	6.5	2.5	✓	YU	TP#5 (compare to 12-2-93)
2/11/94	TP#5	11-30-93	12/2/93	402	3881	801.1	406.1	9.6	2.0	✓	WUW	18' - 19'
12-2-93	RFL-SS-2353	12-1-93	12-3-93	506	891.8	815.1	608	1.5	1.3	✓	YU	TP#20
12-2-93	TP#20	12-1-93	12-3-93	506	748.3	920.6	517	1.3	1.6	✓	DEC	1' - 2'
12-2-93	RFL-SS-2354	12-1-93	12-3-93	406	1131	914.3	603	1.9	1.5	✓	YU	TP#20
12-2-93	TP#20-DUP	12-1-93	12-3-93	504	1197	505.8	507	2.1	1.0	✓	DEC	1' - 2'
12-2-93	RFL-SS-2355	12-1-93	12-3-93	508	1156	767.1	645	1.8	1.2	✓	YU	TP#20
12-2-93	TP#20	12-1-93	12-3-93	471	1633	731.4	601	2.7	1.2	✓	DEC	2' - 3'
12-2-93	RFL-SS-2356	12-1-93	12/3/93	408	1367	844.6	622	2.2	1.4	✓	YU	TP#20
12/29/93	TP#20-DUP	12-1-93	12/3/93	406	1136	705.3	580	2.0	1.2	✓	YU	2' - 3'

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 s.c.c., unless otherwise noted

REVIEWED BY: *[Signature]*  
Site H<sup>2</sup> Manager



RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 PC INITIAL 20 DAY	T-208 PC INITIAL 20 DAY	MA-55 (g/100ml) WET WEIGHT	Ba-226 pCi/g (INITIAL/CORR) 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-2-93	RFL-SS-2357	12-1-93	12-3-93	510	772.0	767.1	618	1.2	1.2	✓	PO	TP#20
12-27-93	TP#20	12-1-93	12-3-93	457	1007	170.5	582	1.7	1.2	✓	SEC	3'-4'
12-2-93	RFL-SS-2358	12-1-93	12-3-93	410	6885	600.8	547	1.3	1.1	✓	PO	TP#20
12-28-93	TP#20-DUP	12-1-93	12-3-93	520	796.9	805.5	509	1.6	1.6	✓	SEC	3'-4'
12-2-93	RFL-SS-2359	12-1-93	12-3-93	512	3170	872.6	627	5.1	1.4	✓	PO	TP#20
12-28-93	TP#20	12-1-93	12-3-93	446	4580	519.5	534	5.6	1.5	✓	SEC	4'-5'
12-2-93	RFL-SS-2360	12-1-93	12-3-93	412	3817	879.5	798	4.8	1.1	✓	PO	TP#20
12-27-93	TP#20-DUP	12-1-93	12-3-93	453	6385	1019	1910	9.0	1.5	✓	SEC	4'-5'
12-2-93	RFL-SS-2361	12-1-93	12-3-93	514	1976	700.0	551	3.6	1.3	✓	PO	TP#21
12-27-93	TP#21	12-1-93	12-3-93	415	2444	731.4	525	4.7	1.4	✓	SEC	0'-1'
12/2/93	RFL-SS-2362	12/1/93	12-3-93	414	6076	827.2	597	10.2	1.4	✓	PO	TP#21
12/27/93	TP#21	12/1/93	12-3-93	558	9385	1151	507	17	3.0	✓	SEC	1-2' Screened
12/2/93	RFL-SS-2363	12/1/93	12-3-93	516	5997	901.4	601	10.0	1.5	✓	PO	TP#21
12-28-93	TP#21-DUP	12/1/93	12-3-93	474	9144	1306	572	16	2.3	✓	SEC	1-2' Screened
12/2/93	RFL-SS-2364	12/1/93	12/3/93	416	4476	1080	648	6.9	1.7	✓	PO	TP#21
12/27/93	TP#21	12/1/93	12/3/93	419	7371	949.1	610	12	1.6	✓	SEC	2-3' Screened
12/2/93	RFL-SS-2365	12/1/93	12/3/93	518	3696	1103	566	6.5	1.9	✓	PO	TP#21
12-28-93	TP#21	12/1/93	12/3/93	566	6808	901.4	530	13	1.7	✓	SEC	2-3' Screened
12/2/93	RFL-SS-2366	12/1/93	12/3/93	418	8513	1158	673	13.7	1.7	✓	PO	TP#21
12/27/93	TP#21	12/1/93	12/3/93	456	15866	1184	622	25	1.9	✓	SEC	3-4' Screened

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec. unless otherwise noted

REVIEWED BY: *John M. Fernald*  
Site HP Manager





MK-FE JSON COMPANY  
A MORRISON KNUDSEN COMPANY



CWM Federal Environmental Services, Inc.

FOR INFORMATION ONLY

OCS SAMPLE LOG

SITE NAME RIFLE, CO.

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 pCi INITIAL 20 DAY	Tl-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH < 15cm > 15cm	TECH INITIAL 20 DAY	COMMENTS
12/2/93	RFL-SS-2367	12/1/93	12/3/93	520	8476	930.2	542	16 15-6	1.7	✓	B	TP#21
12-28-93	TP #21-Dup	12/1/93	12/3/93	564	13712	1199	497	23	2.4	✓	ARC	3-4' Screened
12/2/93	RFL-SS-2368	12/1/93	12/3/93	420	2809	696.6	604	4.7	1.2	✓	B	TP#21
12/27/93	TP #21	12/1/93	12/3/93	441	5751	883.2	535	11	1.7	✓	ARC	4-5' Screened
12/2/93	RFL-SS-2369	12/1/93	12/3/93	522	3129	865.5	671	4.7	1.2	✓	B	TP#21
12/27/93	TP #21-Dup	12/1/93	12/3/93	562	5112	872.6	600	9.5	1.5	✓	ARC	4-5' Screened
12/2/93	RFL-SS-2370	12/2/93	12/3/93	422	4444	618.2	616	0.67	1.0	✓	B	TP#32 Bkg
12/27/93	TP #32	12/2/93	12/3/93	417	745.7	635.6	579	1.3	1.1	✓	ARC	0-1' Screened
12/2/93	RFL-SS-2371	12/2/93	12/3/93	524	2311	853.4	655	1.0	1.3	✓	B	TP#32 Bkg
12/27/93	TP #32	12/2/93	12/3/93	408	701	636	609	1.2	1.0	✓	ARC	0-1' Screened
12/2/93	RFL-SS-2372	12/2/93	12/3/93	424	388.8	635.6	689	0.60	0.99	✓	B	TP#32 Bkg
12/27/93	TP #32	12/2/93	12/3/93	414	562	653	595	0.94	1.10	✓	ARC	1-2' Screened
12/2/93	RFL-SS-2373	12/2/93	12/3/93	526	465.9	920.6	761	0.70	1.4	✓	B	TP#32 Bkg
12/27/93	TP #32	12/2/93	12/3/93	429	861.5	761.3	596	1.4	1.3	✓	ARC	2-3' Screened
12/2/93	RFL-SS-2374	12/2/93	12/3/93	426	432.2	696.6	631	0.68	1.1	✓	B	TP#32 Bkg
12/27/93	TP #32	12/2/93	12/3/93	425	814.4	714.0	541	1.5	1.2	✓	ARC	1-2' Screened
12/2/93	RFL-SS-2375	12/2/93	12/6/93	528	649.5	863.0	644.9	1.0	1.3	✓	B	TP#32 Bkg
12/30/93	TP #32	12/2/93	12/6/93	400	773.9	687.9	579	1.3	1.2	✓	B	2-3' Screened
12/2/93	RFL-SS-2376	12/2/93	12/3/93	428	420.1	705.3	709	0.59	0.99	✓	B	TP#32 Bkg
12/27/93	TP #32	12/2/93	12/3/93	429	666.0	879.5	607	1.1	1.4	✓	ARC	3-4' Screened

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec. unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager



MK-FE  
A MORRISON KRUSDEN COMPANY



CWM Federal Environmental Services, Inc.

SITE NAME  
RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	BI-214 pCi INITIAL 20 DAY	TI-208 pCi INITIAL 20 DAY	MASS (gross) WET DRY	Ra-226 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12/2/93	RFL-SS-2377	12/2/93	12/3/93	530	757.8	680.8	762	1.1	0.97		B	TP #32 Bkg
12/27/93	TP #32	12/2/93	12/3/93	412	538	557	598	.98	.93	✓	DRC	3-4' Screened
12/2/93	RFL-SS-2378	12/2/93	12/3/93	430	197.5	888.2	759	0.26	1.2	✓	B	TP #32 Bkg
12/27/93	TP #32	12/2/93	12/3/93	531	77.5	611.3	659	1.2	1.0	✓	DRC	4-5' Screened
12/2/93	RFL-SS-2379	12/2/93	12/3/93	532	720.6	757.6	800	0.90	0.95	✓	B	TP #32 Bkg
12/27/93	TP #32	12/2/93	12/3/93	410	564	766	703	.80	1.1	✓	DRC	4-5' Screened
12/2/93	RFL-SS-2380	12/2/93	12/3/93	432	197.0	783.4	687	0.29	1.1	✓	B	TP #33 Bkg
12/27/93	TP #32	12/2/93	12/3/93	423	777.6	661.8	602	1.3	1.1	✓	DRC	6-7' Screened
12/2/93	RFL-SS-2381	12/2/93	12/3/93	534	462.5	968.5	754	0.61	1.3	✓	B	TP #33 Bkg
12/27/93	TP #32	12/2/93	12/3/93	421	695.5	744.8	647	1.1	1.2	✓	DRC	6-7' Screened
12-2-93	RFL-SS-2382	12-2-93	12-3-93	434	721.3	853.3	716	1.0	1.2		PU	TP #33 Bkg
12-28-93	TP #33	12-2-93	12-3-93	534	615.8	305.5	607	1.0	1.3	✓	DRC	7'-8' Screened
12-2-93	RFL-SS-2383	12-2-93	12-3-93	536	435.8	728.8	774	0.56	0.94		PU	TP #33 Bkg
12-27-93	TP #33	12-2-93	12-3-93	437	557.1	862.0	652	0.85	1.3	✓	DRC	7'-8' Screened
12-2-93	RFL-SS-2384	12-2-93	12-3-93	436	546.4	600.8	748	0.73	0.80		PU	TP #33 Bkg
12-27-93	TP #33	12-2-93	12-3-93	435	433.9	992.6	613	0.72	1.6	✓	DRC	8'-9' Screened
12-2-93	RFL-SS-2385	12-2-93	12-3-93	538	307.3	930.3	728	0.42	1.3		PU	TP #33 Bkg
12-27-93	TP #33	12-2-93	12-3-93	444	615.8	833.2	628	0.98	1.4	✓	DRC	8'-9' Screened
12-2-93	RFL-SS-2386	12-2-93	12-3-93	438	386.5	1238	695	5.6	1.8	✓	PU	S.W. Corner
12-28-93	493	12-2-93	12-3-93	450	553.7	1010	632	9.8	1.6	✓	DRC	

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec. unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager





MK-FE JSON COMPANY  
A MORRISON KNUDSEN COMPANY



CWM Federal Environmental Services, Inc.

FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID DATE & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	BI-214 pCi INITIAL 20 DAY	TI-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	BI-220 pCi/g INITIAL/CORR 20 DAY	TR-232 pCi/g INITIAL 20 DAY	DEPTH < 15cm > 15cm	TECH INITIAL 20 DAY	COMMENTS
12-28-93	RFL-SS-2387	12-2-93	12-3-93	540	6878	1045	769	8.9	1.4		YU	SW Corner
12-28-93	-493	12-2-93	12-3-93	448	11324	1106	605	17	1.7	✓	DRS	
12-28-93	RFL-SS-2388	12-1-93	12-6-93	440	1501	748.8	754	2.0	0.99		YU	TP#22
12-28-93	TP#22	12-1-93	12-6-93	408	1612	705.3	632	2.6	1.1	✓	DRS	6'-7' Screened
12-28-93	RFL-SS-2389	12-1-93	12-3-93	542	1004	949.3	798	1.3	1.2		YU	TP#22
12-28-93	TP#22-DUP	12-1-93	12-3-93	544	2253	719.2	679	3.3	1.1	✓	DRS	6'-7' Screened
12-28-93	RFL-SS-2390	12-1-93	12-3-93	442	985.1	522.4	685	1.4	1.76		YU	TP#22
12-28-93	TP#24	12-1-93	12-3-93	542	1014	891.8	654	1.6	1.04	✓	DRS	TP#24 C-1
12-28-93	RFL-SS-2391	12-1-93	12-3-93	544	415.5	1103	689	.60	1.6		YU	TP#24
12-28-93	TP#24	12-1-93	12-3-93	434	706.6	226.9	631	1.1	.99	✓	DRS	1-2'
12-28-93	RFL-SS-2392	12-1-93	12-3-93	444	867.2	757.5	779	1.1	.97		YU	TP#24
12-28-93	TP#24	12-1-93	12-3-93	400	1189	827.2	664	1.8	1.2	✓	DRS	2-3' Screened
12-28-93	RFL-SS-2393	12-1-93	12-3-93	546	744.6	786.3	787	.95	1.0		YU	TP#24
12-28-93	TP#24 DUP	12-1-93	12-3-93	410	1177	644.4	680	1.7	0.95	✓	DRS	2-3' Screened
12-28-93	RFL-SS-2394	12-1-93	12-3-93	446	1649	975.2	794	2.1	1.2		YU	TP#24
12-28-93	TP#24	12-1-93	12-3-93	440	1835	827.2	687	2.7	1.2	✓	DRS	3-4' Screened
12-28-93	RFL-SS-2395	12-1-93	12-3-93	548	1506	1064	809	1.9	1.3		YU	TP#24
12/29/93	TP#24 DUP	12-1-93	12/3/93	401	2065	855.3	696	3.0	1.2	✓	DRS	3-4' Screened
12-28-93	RFL-SS-2396	12-1-93	12-3-93	448	1560	626.9	778	1.7	.81		YU	TP#24
12-28-93	TP#24	12-1-93	12-3-93	538	1172	1141	655	1.8	1.7	✓	DRS	4-5' Screened

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec. unless otherwise noted

REVIEWED BY:

*[Signature]*  
Site HP Manager



SITE NAME RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 PCI INITIAL 20 DAY	T-208 PCI INITIAL 20 DAY	MASS (grams) WET DRY	IN-220 PC/G INITIAL 20 DAY	IN-232 PC/G INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-2-93	RFL-SS-2397	12-1-93	12/5/93	550	1249	1017	741	1.6	1.3		YU	TP#24 Screened
12/29/93	TP#24			502	1309	1202	605	2.0	1.8	✓	YU	4-5 Dup
12-2-93	RFL-SS-2398	12-1-93	12-3-93	450	5661	975.2	681	8.3	1.4	✓	YU	TP#25
12-28-93	TP#25			441	6798	1010	575	12	1.2		DRC	9-10 Screened
12-2-93	RFL-SS-2399	12-1-93	12-3-93	552	4659	1151	759	6.1	1.5		YU	TP#25 Screened
12-28-93	TP#25			472	5952	975.2	638	8.5	1.5	✓	DRC	9-10 Dup
12-2-93	RFL-SS-2400	12-1-93	12-8-93	452	1700	600.8	776	2.2	1.7		YU	TP#26
2-11-94	TP#26		12/2/94	506	1288	786.3	648	2.0	1.2	✓	WLV	8-9.5
12-2-93	RFL-SS-2401	12-1-93	10/3/93	554	3698	1218	665	5.6	1.8		YU	TP#28
12/29/93	TP#28			512	6348	959.8	610	10.4	1.5	✓	YU	0-1
12-2-93	RFL-SS-2402	12-1-93	12/3/93	556	5404	911.1	732	7.4	1.2		YU	TP#28
12-28-93	TP#28			404	7855	975.2	607	13	1.6	✓	DRC	1-2' Screened
12-2-93	RFL-SS-2403	12-1-93	12-3-93	454	4606	731.4	735	6.3	1.0		YU	TP#28 Dup
12-25-93	TP#28 Dup			476	7042	1149	611	12	1.9	✓	DRC	1-2' Screened
12-2-93	RFL-SS-2404	12-1-93	12/3/93	558	2553	1160	728	3.6	1.6		YU	TP#28
12/29/93	TP#28			414	4077	983.9	592	6.9	1.7	✓	YU	2-3' Screened
12-2-93	RFL-SS-2405	12-1-93	12/3/93	456	2415	966.5	740	3.3	1.3		YU	TP#28 Dup
12/29/93	TP#28			500	4348	930.2	608	7.2	1.5	✓	YU	2-3' Screened
12-2-93	RFL-SS-2406	12-1-93	12/3/93	560	60753	3347	618	9.8	5.4		YU	TP#29
12/29/93	TP#29			508	103280	4229	555	186	7.6	✓	YU	0-1' Screened

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec. unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager



MK-FE  
A MORRISON KNUDSEN COMPANY



CWM Federal Environmental Services, Inc.

SITE NAME  
RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 PCI INITIAL 20 DAY	TI-208 PCI INITIAL 20 DAY	MASS (grams) WET 1HR	Rn-220 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-2-93	RFL-SS-2407	12-1-93	12/3/93	458	6786	3344	740	91	4.5	✓	YU	TP 29 DUP
12/29/93	TP 29 DUP			482	114990	4787	673	178	7.4	✓	SE	0-1' SCREENED
12-2-93	RFL-SS-2408	12-1-93	12/3/93	562	35225	2100	690	51	3.0	✓	YU	TP 29
12/29/93	TP 29			514	60950	3174	618	99	5.1	✓	SE	1-2' SCREENED
12-2-93	RFL-SS-2409	12-1-93	12/3/93	460	32065	2064	662	48	3.1	✓	YU	TP 29 DUP
12/29/93	TP 29			504	57491	2327	596	96	4.0	✓	SE	1-2' SCREENED
12-2-93	RFL-SS-2410	12-1-93	12/3/93	564	41989	2608	705	60	3.7	✓	YU	TP 29
12/29/93	TP 29			416	74697	3344	651	115	5.1	✓	SE	2-3' SCREENED
12-2-93	RFL-SS-2411	12-1-93	12/3/93	462	47500	2438	721	60	3.4	✓	YU	TP 29 DUP
12/29/93	TP 29			516	82609	3519	639	131	5.5	✓	SE	2-3' SCREENED
12-2-93	RFL-SS-2412	12-1-93	12-3-93	566	9650	1410	557	17	2.5	✓	YU	TP 30
12-27-93	TP 30			455	17034	1132	516	34	2.2	✓	ORC	0-1'
12-2-93	RFL-SS-2413	12-1-93	12-3-93	464	2586	8207	567	4.6	1.5	✓	YU	TP 30
12-27-93	TP 30			568	6150	1130	543	11	2.2	✓	ORC	1-2'
12-2-93	RFL-SS-2414	12-1-93	12-3-93	568	34583	2014	468	74	4.3	✓	YU	TP 30
12-27-93	TP 30			560	65412	2603	292	290	8.9	✓	ORC	2-3'
12-2-93	RFL-SS-2415	12-1-93		466	518.5	8533	390	1.3	3.2	✓	YU	TP 25, COMPOSITE
12-2-93	RFL-SS-2416	12-1-93	12-2-93	570	2615	8151	419	6.2	1.9	✓	YU	TP 27 Composite
2-11-14	TP 27			400	2114	7140	419	9.3	1.7	✓	WW	9-12'

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 3.0  
 Count Time = 500 sec. unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager





MK-FE  
A MORRISON KNUDSEN COMPANY



CWM Federal Environmental Services, Inc.

RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	B-214 pCi INITIAL 20 DAY	TI-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Re-220 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS-2417	12-1-93	12/6/93	400	31580	2020	572	55	3.5		PU	TP#30
12/30/93	TP #30			500	54683	2417	384	142	6.3	✓	PU	3-4'
12-3-93	RFL-SS-2418	12-1-93	12/6/93	300	2244	795.4	565	4.0	1.4		PU	TP#30
12/30/93	TP #30			400	4714	992.6	501	9.8	2.0	✓	PU	4-5' Screened
12-3-93	RFL-SS-2419	12-1-93	12-6-93	402	2878	870.1	574	5.0	1.5		PU	TP#30 Dup.
12-28-93	TP #30			407	6879	696.6	510	13	1.4	✓	ORC	4-5' Screened
12-3-93	RFL-SS-2420	12-1-93	12/6/93	502	2829	863.0	626	4.5	1.4		PU	TP#30
12/30/93	TP #30			503	8360	834.3	533	16.0	1.6	✓	PU	5-6' Screened
12-3-93	RFL-SS-2421	12-1-93	12-6-93	404	2400	731.4	651	3.7	1.1		PU	TP#30
12/28/93	TP #30			418	6679	730.4	558	12	1.3	✓	ORC	5-6' Dup Screened
12-3-93	RFL-SS-2422	12-1-93	12-6-93	524	7290	1056	686	11	1.5		PU	TP#30
12/30/93	TP #30			407	17045	1628	564	30	2.9	✓	PU	6-7' Screened
12-3-93	RFL-SS-2423	12-1-93	12-6-93	406	6232	953.4	647	9.6	1.5		PU	TP#30
12-28-93	TP #30			524	16710	1247	542	30	2.3	✓	ORC	6-7' Dup Screened
12-3-93	RFL-SS-2424	12-1-93	12/6/93	506	2129	991.8	729	2.9	1.2		PU	TP#30
12/30/93	TP #30			504	2440	853.4	602	4.4	1.4	✓	PU	7-8' Screened
12-3-93	RFL-SS-2425	12-1-93	12-6-93	408	2244	757.5	687	3.3	1.1		PU	TP#30 Screen
12-28-93	TP #30			420	3430	674.2	509	6.0	1.2	✓	ORC	7-8' Dup
12-3-93	RFL-SS-2426	12-1-93	12/6/93	508	17004	1793	676	25	2.7		PU	8-9' Screened
12/30/93	TP #30			406	26641	1715	513	52	3.3	✓	PU	8-9' Screened

Site Correction Factor = 1.3  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec., unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager



MK-FL JSON COMPANY  
A MORRISON KNUDSEN COMPANY



CWM Federal Environmental Services, Inc.

FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	BI-214 pCi INITIAL 20 DAY	TI-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS-2427	12-1-93	12-6-93	410	16055	1223	681	24	1.8		PU	TP #30 Screened
12-23-93	TP #30			510	24590	1477	521	47	2.3	✓	ORC	8'-9' Dup.
12-3-93	RFL-SS-2428	12-1-93	12/6/93	510	7341	1045	580	13	1.8		PU	TP #19
12/30/93	TP #19			506	19013	1467	460	41	3.2	✓	ORC	0'-1'
12-3-93	RFL-SS-2429	12-1-93	12/6/93	412	5321	1158	606	.88	1.9		PU	TP #19 *
12/30/93	TP #19			408	1087	1106	549	2.0	2.0	✓	ORC	2'-3'
12-3-93	RFL-SS-2430	12-1-93	12/6/93	512	6590	851	509	1.4	1.6		PU	TP #19
12/30/93	TP #19			508	1126	661.7	531	2.1	1.2	✓	ORC	1'-2'
12-3-93	RFL-SS-2431	12-1-93	12/6/93	414	2174	9578	643	3.4	1.5		PU	TP #19
12/30/93	TP #19			410	4017	1132	550	7.3	2.1	✓	ORC	3 1/2 - 4 1/2
12-3-93	RFL-SS-2432	12-1-93	12-6-93	514	1550	9493	630	3.0	1.5		PU	TP #19
12-28-93	TP #19			430	3758	1019	534	7.1	1.9	✓	ORC	3 1/2 - 4 1/2 Dup
12-3-93	RFL-SS-2433	12-1-93	12/6/93	416	2604	8446	572	4.6	1.5		PU	TP #19
12/30/93	TP #19			510	4870	843.9	513	9.5	1.6	✓	ORC	4 1/2 - 5 1/2
12-3-93	RFL-SS-2434	12-1-93	12-6-93	516	2459	1036	553	4.4	1.9		PU	TP #19
12-28-93	TP #19			522	4554	6327	493	10	1.3	✓	ORC	4 1/2 - 5 1/2 Dup
12-3-93	RFL-SS-2435	12-1-93	12-6-93	418	1602	1036	658	2.4	1.6		PU	TP #19
12-27-93	TP #19			445	3471	1123	581	5.9	1.9	✓	ORC	5 1/2 - 6 1/2
12-3-93	RFL-SS-2436	12-1-93	12-6-93	518	1915	1112	661	2.9	1.7		PU	TP #19
12-28-93	TP #19			428	3525	8557	592	6.0	1.4	✓	ORC	5 1/2 - 6 1/2 Dup

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 SEC, unless otherwise noted

REVIEWED BY:

*[Signature]*

Site HP Manager





**MIK-FE**  
A MORRIS KNUDSEN COMPANY



**CWM Federal Environmental Services, Inc.**

RIFLE, CO.

**OCS SAMPLE LOG**

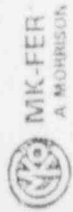
INFORMATION ONLY

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	Bi-214 PCI INITIAL 20 DAY	Ti-208 PCI INITIAL 20 DAY	MASS (grams) WET DRY	Re-220 pCi/g INITIAL 20 DAY	Tn-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS-2437	12-2-93	12-6-93	420	719.7	731.4	55.3	1.3	1.3	✓	PU	TP # 11
12-27-93	TP # 11			443	435.3	1086	408	0.93	2.2	✓	ORC	3'-4'
12-3-93	RFL-SS-2438	12-2-93	12-6-93	520	492.2	1486	666	7.4	2.2	✓	PU	TP # 11
12/30/93	TP # 11			412	858.4	1176	535	16.0	2.2	✓	B	4'-5'
12-3-93	RFL-SS-2439	12-2-93	12-6-93	422	185.6	949.1	650	2.9	1.5	✓	PU	TP # 11
12/30/93	TP # 11			512	330.9	882.2	507	6.5	1.7	✓	B	5'-6'
12-3-93	RFL-SS-2440	12-2-93	12-6-93	522	925.8	1323	782	1.2	1.7	✓	PU	TP # 11 screened
12-27-93	TP # 11			447	152.7	1350	644	2.4	2.1	✓	ORC	6'-7'
12-3-93	RFL-SS-2441	12-2-93	12-6-93	424	128.3	905.6	753	1.7	1.2	✓	PU	TP # 11 screened
12-28-93	TP # 11			422	171.5	1025	644	2.5	1.7	✓	ORC	6'-7' Dup
12-3-93	RFL-SS-2442	12-2-93	12-6-93	524	1030	991.3	761	1.4	1.3	✓	PU	TP # 11 screened
12/30/93	TP # 11			414	1980	1297	624	3.2	2.1	✓	B	7'-8'
12-3-93	RFL-SS-2443	12-2-93	12-6-93	426	1735	792.4	762	2.3	1.0	✓	PU	TP # 11 Screen
12/30/93	TP # 11			514	2233	1017	621	3.6	1.6	✓	B	7'-5' Dup
12-3-93	RFL-SS-2444	12-2-93	12-6-93	526	733.6	911.0	830	1.88	1.1	✓	PU	TP # 11 Screen
12/30/93	TP # 11			416	1408	1080	692	2.0	1.6	✓	B	8'-9'
12-3-93	RFL-SS-2445	12-2-93	12-6-93	428	1141	870.7	812	1.4	1.1	✓	PU	TP # 11 Screen
12-28-93	TP # 11			514	1951	621.2	617	2.6	1.3	✓	ORC	8'-9' Dup
12-3-93	RFL-SS-2446	12-2-93	12-6-93	528	3010	1036	795	3.8	1.3	✓	PU	TP # 11 screened
12/30/93	TP # 11			516	4737	815.1	669	7.1	1.2	✓	B	9-10

Site Correction Factor = 1.9  
 VP Correction Factor (if applicable) = 2.1  
 Count Time = 5.00 sec., unless otherwise noted

REVIEWED BY: [Signature]  
 Site HP Manager



MK-FER  
A MORRISON  
IRON COMPANY  
JOHNSON COMPANY



CWEM Federal Environmental Services, Inc.

SITE NAME RIFLE, CO.

GCS SAMPLE LOG

FOR INFORMATION ONLY

COMB # DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	Ru-214 pCi/g INITIAL 20 DAY	Tl-208 pCi/g INITIAL 20 DAY	MASS (gms) WET DRY	Pu-238 pCi/g INITIAL/COMB 20 DAY	Pu-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS-2447	12-2-93	12-6-93	430	25933	555.2	727	3.5	1.2		PU	TP # 11 Screened
12-28-93	TP # 11			572	4350	949.3	613	7.1	1.5	✓	DEC	9-10' Dup
12-3-93	RFL-SS-2448	12-2-93	12/6/93	530	37026	2215	666	56	3.3	✓	PU	TP # 15
12/30/93	TP # 15			418	83688	4049	500	167	8.1		B	0-1'
12-3-93	RFL-SS-2449	12-2-93	12/6/93	432	132832	6017	589	236	10		PU	TP # 15
12/30/93	TP # 15			518	268600	11191	484	555	23	✓	B	1-2'
12-3-93	RFL-SS-2450	12-2-93	12/6/93	532	120090	5399	587	205	9.2	✓	PU	TP # 15
12/30/93	TP # 15			420	232430	9659	494	471	20	✓	B	2-3'
12-3-93	RFL-SS-2451	12-2-93	12/6/93	434	27267	1395	565	48	2.5		PU	TP 15
12/30/93	TP 15			520	59645	2791	467	128	6.0	✓	B	3-4'
12-3-93	RFL-SS-2452	12-2-93	12-6-93	519	1484	1064	661	2.2	1.6		PU	TP 15
12-27-93	TP 15			518	4133	815.1	513	8.6	1.6	✓	DEC	4-5'
12-3-93	RFL-SS-2453	12-2-93	12/6/93	436	1441	896.9	708	2.0	1.3		PU	TP 15
12/30/93	TP 15			422	1900	940.4	537	3.5	1.8	✓	B	5-6'
12-3-93	RFL-SS-2454	12-2-93	12/6/93	536	666.3	871.8	763	.87	1.2		PU	TP 15
12/30/93	TP 15			522	1114	786.3	583	1.9	1.3	✓	B	6-7'
12-3-93	RFL-SS-2455	12-2-93	12/6/93	438	4920	535.9	698	.72	1.2		PU	TP 15
12/30/93	TP 15			424	581.4	775.0	516	1.1	1.5	✓	B	7-8'
12-3-93	RFL-SS-2456	12-2-93	12/6/93	538	4458	853.4	651	7.3	1.3		PU	TP 15
12/30/93	TP 15			524	8433	843.9	531	16	1.6	✓	B	8-9'

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec. unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager



Mik-Pel  
A MORRISON  
SUN COMPANY  
A JUDSEN COMPANY



CWEM Federal Environmental Services, Inc.

FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	BI-214 PCl INITIAL 20 DAY	TI-208 PCl INITIAL 20 DAY	MASS (g) WET DRY	He-220 pCi/g INITIAL (CORR) 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS-2457	12-2-93		440	4037	553.3	747	5.4	1.1		YU	TP15
12/30/93	TP15		12/6/93	426	6650	1263	612	11	2.1	✓	B	9-10'
12-3-93	RFL-SS-2458	12-2-93		340	731.1	952.2	623	1.1	1.3		YU	TP15
12/30/93	TP15		12/6/93	526	1061	989.8	533	2.0	1.8	✓	B	10-11'
12-3-93	RFL-SS-2459	12-2-93		442	972.4	809.8	799	1.2	1.0		YU	TP#15
12/30/93	TP#15		12/6/93	428	1452	1071	674	2.2	1.6	✓	B	12'-13' Screened #4
12-3-93	RFL-SS-2460	12-2-93		512	3050	997.3	831	3.7	1.2		YU	TP#15
12-27-93	TP#15	12-2-93		546	5323	811.8	675	7.9	1.3	✓	ORC	11'-12' Screened #4
12-3-93	RFL-SS-2461	12-2-93		444	796.2	931.7	767	1.0	1.2		YU	TP#15
12-28-93	TP#15-DUP	12-2-93		520	1726	1007	623	2.8	1.6	✓	ORC	12'-13' Screened #4
12-3-93	RFL-SS-2462	12-2-93		544	1474	939.8	808	1.8	1.2		YU	TP#15
12-28-93	TP#15-DUP	12-2-93	12-6-93	426	1796	705.3	633	2.1	1.0	✓	ORC	12'-13' Screened #4
12-3-93	RFL-SS-2463A	12-3-93		446	4372	1228	775	5.6	1.6		YU	TP#4
12/29/93	TP#4	12-3-93	12/6/93	418	5420	819.5	635	8.5	1.4	✓	B	11'-12' Screened
12-3-93	RFL-SS-2464	12-3-93		546	5027	1534	771	6.5	2.0		YU	TP#4
12-28-93	TP#4-DUP	12-3-93		502	6977	1199	636	11	1.9	✓	ORC	11'-12' Screened
12-3-93	RFL-SS-2465A	12-3-93		448	8482	1358	694	12	2.0		YU	TP#4
12/29/93	TP#4	12-3-93	12/6/93	518	10823	1122	619	17	1.8	✓	B	12'-13' Screened
12-3-93	RFL-SS-2466A	12-3-93		548	8563	1026	673	13	1.5		YU	TP#4
12-28-93	TP#4-DUP	12-3-93	12-6-93	424	10088	1010	600	17	1.7	✓	ORC	12'-13' Screened

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec., unless otherwise noted

REVIEWED BY: *John R. [Signature]*  
 Site HP Manager





MK-FEI  
A MORRIS  
SON COMPANY  
A HUBBARD COMPANY



CWM Federal Environmental Services, Inc.

TE NAME RIFLE, CO.

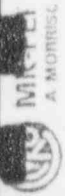
GCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	DCS # INITIAL 20 DAY	BI-214 pCi INITIAL 20 DAY	TI-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Re-220 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS					
													450 INITIAL 20 DAY	550 INITIAL 20 DAY	414 INITIAL 20 DAY	452 INITIAL 20 DAY	520 INITIAL 20 DAY
2-3-93	RFL-SS-2467A			450	3259	1219	654	6.1	1.9		YU	TP#4					
2/29/93	TP#4	12-3-93	12/6/93	420	5882	896.9	574	9.2	1.6	✓	B	13'-14' Screened					
2-3-93	RFL-SS-2468A			550	5132	1036	731	7.0	1.4		YU	TP#4					
2-28-93	TP#4-DUP	12-3-93	12-6-93	414	7671	923.0	642	1.1	1.4	✓	ORC	13'-14' Screened					
2-3-93	RFL-SS-2469A			452	1143	905.6	611	1.9	1.5		YU	TP#4					
2/29/93	TP#4	12-3-93	12/6/93	520	1815	767.1	565	3.2	1.4	✓	B	14'-15' Screened					
2-3-93	RFL-SS-2470A			552	1651	1064	729	2.3	1.5		YU	TP#4					
2-28-93	TP#4-DUP	12-3-93	12-6-93	416	2466	775.0	581	4.2	1.3	✓	ORC	14'-15' Screened					
2-3-93	RFL-SS-2471A			454	923.1	1045	718	1.3	1.5		YU	TP#4					
2/29/93	TP#4	12-3-93	12/6/93	422	1264	722.7	651	1.9	1.1	✓	B	15'-16' Screened					
2-3-93	RFL-SS-2472A			554	1071	1055	669	1.6	1.6		YU	TP#4					
12-28-93	TP#4-DUP	12-3-93	12-6-93	516	1500	1343	133	2.4	2.1	✓	ORC	15'-16' Screened					
12-3-93	RFL-SS-2473A			456	979.5	923.0	823	1.2	1.1		YU	TP#4					
2/29/93	TP#4	12-3-93	12/6/93	522	1668	798.4	697	2.4	1.1	✓	B	16-17' Screened					
12-3-93	RFL-SS-2474A			556	968.4	1045	854	1.1	1.2		YU	TP#4					
12-28-93	TP#4-DUP	12-3-93	12-6-93	508	1519	960.0	719	2.1	1.3	✓	ORC	16-17' Screened					
12-3-93	RFL-SS-2475			458	653.6	966.5	519	1.2	1.9		YU	TP#31 Background					
2/30/93	TP#31	12-3-93	12/6/93	528	707.9	690.4	456	1.6	1.5	✓	B	0-1'					
12-3-93	RFL-SS-2476			558	514.5	1074	471	1.1	2.3		YU	TP#31 Background					
12/30/93	TP#31	12-3-93	12/6/93	430	445.7	1097	409	1.1	2.7	✓	B	1-2'					

Site Correction Factor = 1.8  
 P Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec., unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager



SON COMPANY  
A MORRIS COMPANY



CWM Federal Environmental Services, Inc.

FOR INFORMATION ONLY

CCS SAMPLE LOG

RIFLE, CO.

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	H <sub>2</sub> 214 pCi/g INITIAL 20 DAY	Tl-208 pCi/g INITIAL 20 DAY	MASS (g) WET DRY	Hw-220 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS-2477	12-3-93	12/6/93	460	117.6	116.7	421	.42	2.9		PU	TP#31
12/30/93	TP #31			580	515.8	911.0	353	1.5	2.6	✓	B	2-3 Background
12-3-93	RFL-SS-2478	12-3-93	12/6/93	560	244.4	102.6	450	.65	2.3		PU	TP#31
12/30/93	TP #31			432	606.7	844.6	392	1.5	2.2	✓	B	3-4 Background
12-3-93	RFL-SS-2479	12-3-93	12/6/93	462	352.0	102.2	541	.70	2.0		PU	TP#31
12/30/93	TP #31			532	841.8	719.2	481	1.8	1.5	✓	B	4-5 Background
12-3-93	RFL-SS-2480	12-3-93	12/6/93	562	675.6	100.7	681	.99	1.5		PU	TP#31
12/30/93	TP #31			434	377.2	101.9	617	1.2	1.7	✓	B	5-6 Background
12-3-93	RFL-SS-2481	12-3-93	12/6/93	464	301.2	923.0	605	.50	1.5		PU	TP#31
12/30/93	TP #31			534	423.8	876.8	544	0.76	1.6	✓	B	6-7 Background
12-3-93	RFL-SS-2482	12-3-93	12/6/93	564	635.9	114.1	716	.89	1.6		PU	TP#31
12/30/93	TP #31			436	604.1	109.7	667	0.91	1.6	✓	B	7-8 Background
12-3-93	RFL-SS-2483	12-3-93	12/6/93	466	562.1	103.6	685	.82	1.5		PU	TP#31
12/29/93	TP #31-Dup			436	832.8	618.2	636	1.3	0.97	✓	B	7-8 Background
12-3-93	RFL-SS-2484	12-3-93	10/6/93	566	512.0	113.2	806	.64	1.4	✓	PU	TP#31
12/30/93	TP #31			536	556.7	968.5	727	0.77	1.3	✓	B	8-9 Background
12-3-93	RFL-SS-2485	12-3-93	12/6/93	468	626.1	104.5	829	.75	1.3		PU	TP#31
2-11-94	TP #31-Dup			404	981.2	949.1	750	1.3	1.3	✓	W/W	8-9 Background
12-3-93	RFL-SS-2486	12-3-93	12/6/93	568	744.6	786.3	780	.95	1.0		PU	TP#31
12/30/93	TP #31-Dup			438	385.4	853.2	593	0.65	1.4	✓	W/W	8-9 Background

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 3.0

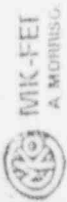
Count Time = 5.00 sec, unless otherwise noted

REVIEWED BY:

*[Signature]*

Site HP Manager





SON COMPANY  
A. MORRISSEY COMPANY



CWMI Federal Environmental Services, Inc.

SITE NAME

RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	BI-214 (pg) INITIAL 20 DAY	TI-208 (pg) INITIAL 20 DAY	MASS (grams) WET DRY	Pa-220 (pg) INITIAL 20 DAY	Th-232 (pg) INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS-2457	12-3-93		470	533.4	858.2	828	0.64	1.1		B	TP # 31 screened
12/29/93	TP # 31 - Dup	12-3-93	12/6/93	424	501.3	687.9	708	0.71	0.97	✓	B	9'-10' Background
12-3-93	RFL-SS-2458	12-3-93		570	771.8	853.4	701	1.1	1.2	✓	B	TP # 31 screened
12/30/93	TP # 31	12-3-93	12/6/93	538	489.6	767.1	598	0.82	1.3	✓	B	10'-11' Background
12-3-93	RFL-SS-2459	12-3-93		472	758.8	844.6	691	1.1	1.2		B	TP # 31 screened
12/30/93	TP # 31 - Dup	12-3-93	12/6/93	440	599.8	993	605	0.98	1.5	✓	B	10'-11' Background
12-3-93	RFL-SS-2490	12-3-93		572	474.7	939.8	800	0.59	1.2	✓	B	TP # 31 screened
12/30/93	TP # 31 - Dup	12-3-93	12/6/93	540	410.1	104.5	688	0.61	1.5	✓	B	11'-12' Background
12-3-93	RFL-SS-2491	12-3-93		474	940.9	318.5	777	1.2	1.1		B	TP # 31 screened
12/30/93	TP # 31 - Dup	12-3-93	12/6/93	442	684.9	975.2	683	1.0	1.4	✓	B	11'-12' Background
12-3-93	RFL-SS-2492	12-3-93		574	802.2	604.1	450	1.8	1.3		B	TP # 2 screened
12/29/93	TP # 2	12-3-93	12/6/93	524	935.6	527.4	423	2.2	1.2	✓	B	0'-1' Background
12-3-93	RFL-SS-2493	12-2-93		476	773.1	966.5	605	1.3	1.6		B	TP # 2 screened
12/29/93	TP # 2	12-2-93	12/6/93	426	634.9	888.2	563	1.1	1.6	✓	B	1'-2' Background
12-5-93	RFL-SS-2494	12-2-93		576	910.3	1132	415	2.2	2.7		B	TP # 2 screened
12-27-93	TP # 2	12-2-93	12-6-93	433	707.4	931.7	375	1.9	2.5	✓	ORC	2'-3' Background
12-3-93	RFL-SS-2495	12-2-93		478	555.4	835.9	383	1.5	2.2		B	TP # 2 screened
12/29/93	TP # 2	12-2-93	12/6/93	526	1056	700.0	353	3.0	2.0	✓	B	3'-4' Background
12-3-93	RFL-SS-2496	12-2-93		578	549.1	786.3	439	1.3	1.8		B	TP # 2 screened
12/20/93	TP # 2	12-2-93	12/6/93	542	594.6	888.2	412	0.97	2.2	✓	B	4'-5' Background

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 5.00 sec., unless otherwise noted

REVIEWED BY: *[Signature]*  
Site HP Manager

FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 pCi INITIAL 20 DAY	TL-208 pCi INITIAL 20 DAY	MASS (gross) (net) (dry)	Ra-226 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-3-93	RFL-SS-2497	12-2-93	12/6/93	480	466.6	931.7	521	.90	1.8	✓	B	TP#2-5'-6'
12/30/97	TP #2			444	529.7	931.7	462	1.1	2.0		B	
12-3-93	RFL-SS-2498	12-2-93	12/6/93	580	315.3	939.8	616	.51	1.5	✓	B	TP#2-6'-7'
12/29/93	TP #2			488	546.3	696.6	555	0.98	1.3		B	
12-3-93	RFL-SS-2499	12-2-93	12/6/93	588	463.7	893.2	556	.83	1.6	✓	B	TP#2-7'-8'
12/29/93	TP #2			588	1139	556.2	505	2.3	1.1		B	
12-3-93	RFL-SS-2500	12-2-93	12/6/93	582	665.5	882.2	556	1.2	1.6	✓	B	TP#2-8'-9'
12/29/93	TP #2			480	745.1	781.4	507	1.5	1.4		B	
12-3-93	RFL-SS-2501	12-2-93	12/6/93	484	618.7	819.5	708	.96	1.2	✓	B	TP#2-9'-10'
12/29/93	TP #2			580	818.5	652.1	637	1.4	1.0		B	
12-3-93	RFL-SS-2502	12-2-93	12/6/93	584	583.8	767.1	586	1.0	1.3	✓	B	TP#2-10'-11'
12/30/93	TP #2			584	385.5	920.6	564	0.59	1.6		B	
12-3-93	RFL-SS-2503	12-2-93	12/6/93	486	696.7	1158	693	1.0	1.7	✓	B	TP#2-11'-12' screened
12/29/93	TP #2			432	831.7	905.6	644	1.3	1.4		B	
12-3-93	RFL-SS-2504	12-2-93	12/6/93	586	532.3	353.4	648	.82	1.3	✓	B	TP#2-11-12' Screened
2-11-94	TP #2-Dup			406	1039	966.5	604	1.7	1.6		WAW	
12-6-93	RFL-SS-2505	12-2-93	12/6/93	400	520.3	783.7	608	.86	1.3	✓	PU	TP#2-12'-13' Screened
12/29/93	TP#2			536	806.2	920.6	574	1.4	1.6		B	
12-6-93	RFL-SS-2506	12-2-93	12/7/93	500	620.3	949.3	613	1.0	1.5	✓	PU	TP#2-12'-13' Screened
12/29/93	TP#2-DUP			534	1132	938.4	577	2.0	1.3		B	

REVIEWED BY: *[Signature]*  
Site HP Manager

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec. unless otherwise noted



MK-FEY  
A MORRISO  
SON COMPANY  
ADDER COMPANY



CWM Federal Environmental Services, Inc.

SITE NAME

RIFLE, CO.

OCS SAMPLE LOG

FORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS INITIAL 20 DAY	B-214 pCi INITIAL 20 DAY	TI-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 nCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH < 15cm > 15cm	TECH INITIAL 20 DAY	COMMENTS
12-6-93	RFL-SS-2507	12-2-93	12/17/93	402	803.7	949.1	673	1.2	1.4		PU	TP#2
12/29/93	TP#2	12-2-93	12/17/93	438	747.8	870.7	619	1.2	1.4	✓	B	13'-14' Screened
12-6-93	RFL-SS-2508	12-2-93	12/17/93	502	571.7	1064	691	0.83	1.5		PU	TP#2
12/29/93	TP#2-DUP	12-2-93	12/17/93	458	113.2	834.3	642	1.8	1.3	✓	B	13'-14' Screened
12-6-93	RFL-SS-2509	12-2-93	12/17/93	404	844.6	896.9	673	1.3	1.3		PU	TP#2
12/29/93	TP#2	12-2-93	12/17/93	440	707.3	112.3	618	1.1	1.8	✓	B	14'-15' Screened
12-6-93	RFL-SS-2510	12-2-93	12/17/93	504	744.9	968.5	607	1.2	1.6		PU	TP#2
12/29/93	TP#2-DUP	12-2-93	12/17/93	540	971.9	911.0	553	1.8	1.6	✓	B	14'-15' Screened
12-6-93	RFL-SS-2511	12-2-93	12/17/93	406	716.6	975.2	631	1.1	1.5		PU	TP#2
12/29/93	TP#2	12-2-93	12/17/93	442	641.2	888.2	573	1.1	1.6	✓	B	15'-16' Screened
12-6-93	RFL-SS-2512	12-2-93	12/17/93	506	845.0	863.2	672	1.3	1.3		PU	TP#2
12/29/93	TP#2-DUP	12-2-93	12/17/93	542	867.4	1227	616	1.4	2.0	✓	B	15'-16' Screened
12-6-93	RFL-SS-2513	12-2-93	12/17/93	408	581.7	1045	597	1.0	1.8		RUC	TP#2
12/29/93	TP#2	12-2-93	12/17/93	444	571.9	818.5	523	1.0	1.6	✓	B	16'-17' Screened
12-6-93	RFL-SS-2514	12-2-93	12/17/93	508	521.5	891.8	468	1.1	1.9		RUC	TP#2
12/29/93	TP#2-DUP	12-2-93	12/17/93	544	561.0	843.9	410	1.4	2.1	✓	B	16'-17' Screened
12-6-93	RFL-SS-2515	12-2-93	12/17/93	410	726.9	1036	730	1.0	1.4		RUC	TP#2
12/29/93	TP#2	12-2-93	12/17/93	446	732.1	1115	647	1.1	1.7	✓	B	17'-18' Screened
12-6-93	RFL-SS-2516	12-2-93	12/17/93	570	428.6	997.3	660	0.5	1.5		RUC	TP#2
12/29/93	TP#2-DUP	12-2-93	12/17/93	546	919.7	891.8	582	1.6	1.5	✓	B	17'-18' Screened

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

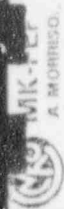
Count Time = 500 sec, unless otherwise noted

REVIEWED BY:

*[Signature]*  
Site HP Manager

00000000





SON COMPANY  
A MORRISO, JUDSEN COMPANY

CWM Federal Environmental Services, Inc.

SITE NAME  
RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE S/DALED	OCS # INITIAL 20 DAY	B-214 pCi INITIAL 20 DAY	Ti-208 pCi INITIAL 20 DAY	MASS (g) WET DRY	Pa-229 pCi/g INITIAL 20 DAY	Pb-214 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-6-93	RFL-SS-2517			412	678.7	879.5	740	9.2		1.2		RUC	TP#2
12/29/93	TP#2	12-2-93	12/7/93	448	1092	992.6	601	1.8		1.7	✓	B	18'-19' screened
12-6-93	RFL-SS-2518			512	438.9	767.1	586	7.5		1.3		RUC	TP#2
12/29/93	TP#2 - DUP	12-2-93	12/7/93	548	760.4	896.8	457	1.7		2.0	✓	B	18'-19' screened
12-6-93	RFL-SS-2519			414	701.3	740.1	500	1.4		1.5		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	450	606.6	766.3	444	1.4		1.7	✓	B	2'-3'
12-6-93	RFL-SS-2520			514	750.5	680.8	465	1.6		1.5		RUC	TP#3
12/27/93	TP#3 DUP	12-2-93	12-7-93	427	314.4	531.2	401	2.6		1.3	✓	B	3'-4'
12-6-93	RFL-SS-2521			416	859.7	740.1	438	2.0		1.7		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	550	791.1	824.7	393	2.0		2.1	✓	B	3'-4'
12-6-93	RFL-SS-2522			516	1944	805.5	506	3.8		1.6		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	452	4532	766.2	463	9.8		1.7	✓	B	5'-6'
12-6-93	RFL-SS-2523			418	433.9	222.7	492	8.8		1.5		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	552	656.5	949.3	445	1.5		2.1	✓	B	7'-8'
12-6-93	RFL-SS-2524			578	722.0	767.1	601	1.3		1.3		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	454	615.6	853.3	547	1.1		1.6	✓	B	6'-7'
12-6-93	RFL-SS-2525			420	629.7	905.6	651	9.7		1.4		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	554	831.5	786.3	593	1.4		1.3	✓	B	RUC 12-6-93 7'-8'-8'-9'
12-6-93	RFL-SS-2526			520	871.6	834.3	636	1.4		1.3		RUC	TP#3
12/27/93	TP#3	12-2-93	12/7/93	615k	766.3	865.0	570	1.3		1.5	✓	B	RUC 12-6-93 6'-9'-9'-10'

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 SEC. unless otherwise noted

REVIEWED BY: *John H. Fernald*  
 Site HP Manager



MK-FE SON COMPANY  
A MORRISON, HUDSEN COMPANY



CWM Federal Environmental Services, Inc.

FOR INFORMATION ONLY

OCS SAMPLE LOG

RITILE, CO.

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 PCI INITIAL 20 DAY	TI-208 PCI INITIAL 20 DAY	MASS (g/min) MET ID#	16-220 (g/g) INITIAL 20 DAY	TR-232 (g/g) INITIAL 20 DAY	DEPTH Δ15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-6-93	RFL-SS-2527			422	608.4	983.9	647	.97	1.5		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	556	681.2	719.2	576	1.02	1.2	✓	RUC	10'-11'
12-6-93	RFL-SS-2528			522	535.7	978.1	685	.78	1.4		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	458	723.7	799.4	592	1.2	1.3	✓	RUC	11'-12'
12-6-93	RFL-SS-2529			424	659.1	820.7	619	1.1	1.4		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	558	783.2	815.1	543	1.4	1.5	✓	RUC	12'-13'
12-6-93	RFL-SS-2530			524	695.5	805.5	586	1.2	1.4		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	460	431.2	116.7	507	0.85	2.3	✓	RUC	13'-14'
12-6-93	RFL-SS-2531			426	643.6	827.2	663	.97	1.3		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	560	719.3	920.6	598	1.2	1.5	✓	RUC	14'-15'
12-6-93	RFL-SS-2532			526	507.3	1074	664	.76	1.6		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	462	647	870.7	549	1.1	1.6	✓	RUC	15'-16'
12-6-93	RFL-SS-2533			428	682.0	1028	724	.94	1.4		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	562	1029	779.2	642	1.6	1.1	✓	RUC	16'-17'
12-6-93	RFL-SS-2534			528	608.1	978.1	591	1.0	1.7		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	464	505.2	844.6	527	0.96	1.6	✓	RUC	17'-18'
12-6-93	RFL-SS-2535			430	539.4	888.2	661	.82	1.3		RUC	TP#3
12/29/93	TP#3	12-2-93	12/7/93	564	1012	872.6	592	1.7	1.5	✓	RUC	18'-19' screened
12-6-93	RFL-SS-2536			530	529.2	382.7	697	.76	.56		RUC	TP#3
12/29/93	TP#3 DUP	12-2-93	12/7/93	434	534.7	809.8	624	0.86	1.3	✓	RUC	19'-19' screened

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 300 sec. unless otherwise noted

REVIEWED BY: *[Signature]*  
Site HP Manager



FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

SITE NAME

DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 pCi INITIAL 20 DAY	Ti-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Re-220 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH ≤ 15cm > 15cm	TECH INITIAL 20 DAY	COMMENTS
12-6-93	RFL-SS-2537	12-2-93	12/7/93	432	224.7	100.1	820	0.88	1.2		RUC	TP#3
12/29/93	TP#3			466	690.1	957.8	746	0.93	1.3	✓	RUC	19'-20' screened
12-6-93	RFL-SS-2538	12-2-93	12/6/93	532	474.9	1208	870	0.55	1.4	✓	RUC	TP#3 DUP screened
12/29/93	TP#3 DUP			532	1910	263	795	1.6	1.1	✓	RUC	19'-20' screened
12-6-93	RFL-SS-2539	12-2-93	12/7/93	434	548.6	731.4	754	0.73	0.97		RUC	TP#3
12/29/93	TP#3			467	690.1	957.8	746	0.93	1.3	✓	RUC	20'-21' screened
12-6-93	RFL-SS-2540	12-2-93	12/7/93	534	636.5	882.2	731	0.87	1.2	✓	RUC	TP#3 DUP
12/29/93	TP#3 DUP			468	534.0	896.9	616	0.87	1.5	✓	RUC	20'-21' screened
12-6-93	RFL-SS-2541	12-2-93	12/7/93	436	324.4	696.6	440	2.0	1.6	✓	RUC	TP#7
12/30/93	TP#7			446	546.8	801.1	353	1.5	2.3	✓	RUC	14'-15'
12-6-93	RFL-SS-2542	12-2-93	12-7-93	536	860.8	815.1	577	1.5	1.4	✓	RUC	TP#7
12/27/93	TP#7			536	1344	934.8	449	3.0	2.1	✓	RUC	15'-16' screened
12-6-93	RFL-SS-2543	12-2-93	12/7/93	438	670.1	748.8	618	1.1	1.2		RUC	TP#7
12/29/93	TP#7 DUP			568	943.5	938.4	481	2.0	1.5	✓	RUC	DUP 15'-16' screened
12-6-93	RFL-SS-2544	12-2-93	12-7-93	538	3378	930.2	735	4.6	1.3	✓	RUC	TP#7
12/27/93	TP#7			552	3667	743.0	617	5.9	1.2	✓	RUC	16'-17' screened
12-6-93	RFL-SS-2545	12-2-93	12/7/93	440	3893	975.2	756	5.1	1.3		RUC	TP#7
12/29/93	TP#7 DUP			470	5222	1237	638	8.2	1.9	✓	RUC	DUP 16'-17' screened
12-6-93	RFL-SS-2546	12-2-93	12/1/93	540	9549	1218	801	12	1.5	✓	RUC	TP#7
12/30/93	TP#7			546	11601	1160	686	17	1.7	✓	RUC	17'-18' screened

Site Correction Factor = 1.8  
 P Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec., unless otherwise noted

REVIEWED BY: *John R. Jensen*  
 Site HP Manager



MK-FEE  
A MORRISON  
SON COMPANY  
LUDSEN COMPANY



CWM Federal Environmental Services, Inc.

SITE NAME

RIFLE, CO.

OCS SAMPLE LOG

FOR INFORMATION ONLY

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 pCi INITIAL 20 DAY	TI-208 pCi INITIAL 20 DAY	MASS (grams) WET DRY	Ra-226 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12-6-93	RFL-SS-2547			442	11579	1280	809	14	1.6		B	TP#7 screened
12/29/93	TP#7 DUP	12-2-93	12/7/93	570	14105	1112	693	20	1.6		B	17-18' DUP
12-6-93	RFL-SS-2548			448	73263	3030	465	158	6.5		B	TP#6 Composite
	TP#6	11/30/93										20-25'
12-6-93	RFL-SS-2549			548	1001	1084	559	1.8	1.9		B	TP#19 Composite
	TP#19	12/3/93										3.5'-5.5'
12-6-93	RFL-SS-2550			450	1957	653.1	648	3.0	1.0		B	TP#20 Composite
	TP#20	12-3-93										
12-6-93	RFL-SS-2551			550	2243	863.0	561	4.0	1.5		B	TP#20 Composite
	12-6-93 Kc TP#20 20	12-1-93										1'-5'
12-6-93	RFL-SS-2552			452	980.4	548.6	637	1.5	0.86		B	TP#21 Composite
	TP#21	12-1-93										
12-6-93	RFL-SS-2553			562	12270	1458	698	19	2.3		B	TP#21 Composite
	TP#21	12-3-93										
12-6-93	RFL-SS-2554			454	452.8	818.5	648	0.70	1.3		B	TP#22 Composite
	TP#22	12/3/93										
12-6-93	RFL-SS-2555			554	929.3	920.6	608	1.5	1.5		B	TP#24 Composite
	TP#24	12/3/93										
12-6-93	RFL-SS-2556			456	787.9	1193	772	1.0	1.5		B	TP#25 Composite
	TP#25	12/3/93										6.5'-8.5'

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec., unless otherwise noted

REVIEWED BY:

*Richard M. Smith*  
Site HP Manager

FORM 001 (SN-0)



FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

TEST NAME

DATE INITIAL 20 DAY	COUNT	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 pCi INITIAL 20 DAY	TI-208 pCi INITIAL 20 DAY	MASS (g) WET DRY	Pa-228 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH 0-15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
2-6-93		RFL-SS-2557			586	810.7	1064	534	1.5	2.0		R	TP#25 Composite
2-6-93		TP#25	12-1-93		458	1234	8446	538	2.3	1.6	✓	R	7.5'-8.5' TP#25 Composite
2-6-93		TP#25	12-1-93		558	1229	958.9	635	1.9	1.5	✓	R	9'-10' TP#27 Composite
2-6-93		RFL-SS-2559	12-3-93		460	9576	879.5	678	1.4	1.3	✓	R	9.5'-11' TP#28 Composite
2-6-93		TP#27	12-3-93		560	9785	2014	410	92.1	4.9		R	TP#29 Composite
2-6-93		RFL-SS-2560	12-3-93		572	14255	1112	732	19	1.5		R	
2-6-93		TP#28	12-6-93	12/7/93	448	20784	1811	676	31	2.7	✓	R	
2-6-93		RFL-SS-2563	12-6-93		464	2247	9056	519	0.53	1.2		RAC	TP#2
2-6-93		TP#2	12-6-93		564	4504	9973	586	0.77	1.7	✓	RAC	13'-16' Composite TP#1
2-6-93		RFL-SS-2564	12-6-93		466	628.4	783.9	543	1.2	1.8		RAC	15'-17' Composite TP#15
2-6-93		TP#1	12-6-93		566	3272	228.8	519	0.63	1.4		RAC	Composite TP#26
2-6-93		RFL-SS-2565	12-6-93										Composite
2-6-93		TP#15	12-6-93										Composite
2-6-93		RFL-SS-2566	12-6-93										Composite
2-6-93		TP#26	12-6-93										Composite

Count Time = 500 sec., unless otherwise noted  
 P Correction Factor (if applicable) = 2.0  
 RFL Correction Factor = 1.8

REVIEWED BY: *John P. Fernald*  
 Site HP Manager





MK-FER  
A MORRISON JOSEN COMPANY



CWM Federal Environmental Services, Inc.

FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 PC INITIAL 20 DAY	T-208 PC INITIAL 20 DAY	MASS (g) WET DRY	H <sub>2</sub> O-220 pC/g INITIAL 20 DAY	TN-232 pC/g INITIAL 20 DAY	DEPTH < 15cm > 15cm	TECH INITIAL 20 DAY	COMMENTS
12-7-93	RFL-SS-2567			408	1922	809.8	60Y	3.0	1.3		RUC	TP#30
12-8-93	TP#30	12-6-93		424	489.7	801.1	578.3	0.85	1.4	✓	RUC	4.5'-7.5' Composite composite BK6 Pit
12-8-93	BK6 Pit	12-7-93		524	926.9	623.3	530.7	1.8	1.2	-	RUC	TP#4 Composite
12-8-93	RFL-SS-2569	12-7-93		426	555.1	539.9	436.2	1.3	1.2	-	RUC	TP#3 Composite
12-8-93	TP#3	12-7-93		526	309.3	776.7	491.3	0.63	1.6	-	RUC	TP#5 Composite
12-8-93	RFL-SS-2570	12-7-93		428	579.2	668.2	462.0	1.3	1.3	-	RUC	TP#11 Composite
12-8-93	TP#5	12-7-93		528	2597.1	343.3	476.0	1.60	7.2	-	RUC	TP#7 Composite
12-8-93	RFL-SS-2575	12-7-93		400	1372	626.9	446	3.1	1.4		✓	TP#1 -4 MOIST Composite
12/9/93	TP#7	12/6/93	12/9/93	450	1528	870.7	446	3.4	2.0	✓	✓	15-17' Composite
12/30/93	RFL-SS-2574	12/6/93	12/9/93	500	521.2	918.1	433	1.2	2.3		✓	TP#2 -4 MOIST Composite
12/9/93	TP#1	12/6/93	12/9/93	550	42.8	891.8	433	0.95	2.1	✓	✓	13-16' Composite
12/30/93	RFL-SS-2515	12/6/93	12/9/93	402	921.0	609.5	460	2.0	1.3		✓	TP#3 18-21' -4 MOIST Composite
12/9/93	TP#2	12/7/93	12/9/93	500	624.7	1093	460	1.4	2.4	✓	✓	Composite
1-3-94	RFL-SS-2576	12/7/93	12/9/93									
1-3-94	TP#3	12/7/93	12/9/93									

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec, unless otherwise noted

REVIEWED BY:

*Robert H. Fernald*  
Site HP Manager

FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS #	BI-214 PGI INITIAL 20 DAY	TI-208 PGI INITIAL 20 DAY	MASS (grams) WET DRY	Mo-220 PGM INITIAL 20 DAY	Th-232 PGM INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
3/9/93	RFL-SS-2577	12/7/93	12/9/93	502	2339	805.6	442	5.3	1.8		B	TP#4 -4 Moist
1/3/94	RFL-SS-2578 TP#4	12/7/93	12/9/93	518	2949	1074	442	6.7	2.4	✓	B	11-16' Composite
2/9/93	RFL-SS-2578 TP#5	12/7/93	12/9/93	404	885.8	653.1	427	2.1	1.5	✓	B	TP#5 16-21' Composite
1-3-94	RFL-SS-2579 TP#7	12/7/93	12/9/93	400	1172	757.5	427	2.7	1.8	✓	B	TP#7 -4 Moist
2/9/93	RFL-SS-2580 TP#11	12/7/93	12/9/93	504	7389	5360	479	154.3	6.8	✓	B	11-21' Composite
1/3/94	RFL-SS-2581 TP#15	12/7/93	12/9/93	406	10030	4476	479	209.4	9.3	✓	B	TP#11 6-10' -4 Moist Composite
2/9/93	RFL-SS-2582 TP#19	12/7/93	12/9/93	502	1061	809.8	417	2.5	1.9	✓	B	TP#15 10-13' Composite
1/3/94	RFL-SS-2585 TP#20	12/6/93	12/9/93	506	1563	786.3	525	3.0	1.5	✓	B	TP#19 -4 Moist
12/9/93	RFL-SS-2584 TP#21	12/2/93	12/9/93	408	2978	911.0	525	5.7	1.7	✓	B	3.5'-5.5' Composite
1/3/94	RFL-SS-2585 TP#22	12/2/93	12/9/93	404	1698	757.5	456	3.7	1.7	✓	B	TP#20 -4 Moist Composite
12/9/93	RFL-SS-2586 TP#24	12/2/93	12/9/93	508	2612	949.1	456	7.9	2.1	✓	B	TP#21 -4 Moist Composite
1/3/94	RFL-SS-2586 TP#24	12/6/93	12/9/93	506	2774	949.5	500	5.9	1.9	✓	B	TP#22 -4 Moist Composite
12/9/93	RFL-SS-2586 TP#24	12/6/93	12/9/93	410	10557	940.4	456	2.3	2.1	✓	B	TP#24 -4 Moist Composite
1/3/94	RFL-SS-2586 TP#24	12/6/93	12/9/93	406	18350	1724	456	40	3.8	✓	B	TP#24 -4 Moist Composite
12/9/93	RFL-SS-2586 TP#24	12/6/93	12/9/93	510	838.3	958.9	582	1.4	1.6	✓	B	TP#24 -4 Moist Composite
1/3/94	RFL-SS-2586 TP#24	12/6/93	12/9/93	508	1020	872.6	582	1.8	1.5	✓	B	TP#24 -4 Moist Composite
12/9/93	RFL-SS-2586 TP#24	12/6/93	12/9/93	412	565.3	696.7	495	1.1	1.4	✓	B	TP#24 -4 Moist Composite
1/3/94	RFL-SS-2586 TP#24	12/1/93	12/9/93	408	1214	1115	495	2.5	2.3	✓	B	TP#24 -4 Moist Composite

Site Correction Factor = 1.8  
 P Correction Factor (if applicable) = 2.0  
 Count Time = 500 s.c.c., unless otherwise noted

REVIEWED BY: *[Signature]*  
 Site HP Manager





MK-FER  
A MORRISON JOHNSON COMPANY



CWM Federal Environmental Services, Inc.  
FOR INFORMATION ONLY

OCS SAMPLE LOG

SITE NAME RIFLE, CO.

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	HW-214 PCL INITIAL 20 DAY	TI-208 PCL INITIAL 20 DAY	MASS (g-raw) MET HWY	Pa-228 PClg INITIAL 20 DAY	Th-232 PClg INITIAL 20 DAY	DEPTH <15cm >15cm	TECH INITIAL 20 DAY	COMMENTS
12/9/93	RFL-SS-2587	12/1/93	12/9/93	512	1218	997.3	553	2.2	1.8		B	TP#25 - 4 MOIST Composite
1/3/94	TP#25			410	2232	975.2	553	4.0	1.8	✓	B	
12/9/93	RFL-SS-2588	12/6/93	12/9/93	444	199.3	687.9	526	1.5	1.3	✓	B	TP#26 - 4 MOIST Composite
1/3/94	TP#26			510	1106	863.0	526	2.1	1.6	✓	B	
12/9/93	RFL-SS-2589	12/6/93	12/9/93	514	658.5	795.9	583	1.1	1.4	✓	B	TP#27 - 4 MOIST Composite
1/3/94	TP#27			512	899.6	911.0	583	1.5	1.6	✓	B	
12/9/93	RFL-SS-2590	12/6/93	12/9/93	416	34566	2020	417	83.	4.8	✓	B	TP#29 - 4 MOIST Composite
1/3/94	TP#29			412	62066	3100	417	149	7.4	✓	B	
12/9/93	RFL-SS-2591	12/6/93	12/9/93	516	730.1	786.3	507	1.4	1.6	✓	B	TP#30 - 4 MOIST Composite
1/3/94	TP#30			514	1117	1007	507	2.2	2.0	✓	B	
12/9/93	RFL-SS-2592	12/8/93	12/9/93	418	859.7	740.1	633	1.4	1.2	✓	B	TP#32 Composite
1/3/94	TP#32			414	819.3	896.9	633	1.3	1.4	✓	B	
12/9/93	RFL-SS-2593	12/8/93	12/9/93	518	559.1	622.5	492	1.1	1.3	✓	B	TP#33 Composite
1/3/94	TP#33			516	511.3	767.1	492	1.0	1.6	✓	B	
12/9/93	RFL-SS-2594	12/7/93	12/9/93	420	794.6	809.8	464	1.7	1.7	✓	B	TP# BK9 - 4 MOIST Composite
1/3/94	TP# BK9			416	790.7	1237	464	1.7	2.7	✓	B	
12/9/93	RFL-SS-2595	12/6/93	12/13/93	426	1237	783.7	490	2.5	1.6	✓	B	TP#1 10f2
1/3/94	TP#1			418	2096	1228	448	4.7	2.7	✓	B	15-17' Rust Comp.
12/9/93	RFL-SS-2596	12/6/93	12/13/93	526	1416	853.4	494	2.9	1.7	✓	B	TP#1 20f2
1/3/94	TP#1			420	2077	748.8	453	4.6	1.7	✓	B	15-17' Rust Comp.

Site Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec, unless otherwise noted

REVIEWED BY: *John H. Farnell* Site HP Manager

FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

WTE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	OCS # INITIAL 20 DAY	B-214 pCi INITIAL 20 DAY	T-208 pCi INITIAL 20 DAY	MASS (grams) WLE THY	Hs-238 pCi/g INITIAL 20 DAY	Th-232 pCi/g INITIAL 20 DAY	DEPTH <15cm X 15cm	TECH INITIAL 20 DAY	COMMENTS
9/9/93	RFL-SS-2597	12/6/93	12/13/93	428	503.0	809.8	495	1.0	1.6		B	TP#2 1 of 2
1/3/94	TP#2			520	566.5	911.0	452	1.3	2.0	✓	B	13-16' Rust Comp.
12/9/93	RFL-SS-2598	12/6/93	12/13/93	528	583.7	767.1	515	1.1	1.5	✓	B	TP#2 2 of 2
1/3/94	TP#2			524	789.1	707.6	473	1.7	1.5		B	13-16' Rust Comp.
12/9/93	RFL-SS-2599	12/7/93	12/13/93	430	965.2	801.1	488	2.0	1.6	✓	B	TP#3 1 of 2
1/3/94	TP#3			424	1036	714.0	432	2.4	1.7	✓	B	18-21' Rust Comp.
12/9/93	RFL-SS-2600	12/7/93	12/13/93	531	698.8	752.6	511	1.4	1.5	✓	B	TP#3 2 of 2
1/3/94	TP#3			426	1285	748.8	450	2.9	1.7	✓	B	18-21' Rust Comp.
12/9/93	RFL-SS-2601	12/7/93	12/13/93	432	2593	975.2	484	5.45	2.0	✓	B	TP#4 1 of 2
1/3/94	TP#4			526	4244	537.0	463	9.2	1.2	✓	B	11-16' Rust Comp.
12/9/93	RFL-SS-2602	12/7/93	12/13/93	532	3101	642.5	479	6.5	1.3	✓	B	TP#4 2 of 2
1/3/94	TP#4			428	4287	809.8	453	9.5	1.8	✓	B	11-16' Rust Comp.
12-9-93	RFL-SS-2603	12-7-93	12/13/93	438	747.2	957.8	528	1.4	1.8	✓	YU	TP#5 1 of 2
1/3/94	TP#5			528	869.3	805.5	476	1.8	1.7	✓	YU	16-21' Rust Comp.
12-9-93	RFL-SS-2604	12-7-93	12/13/93	538	1990	671.3	503	1.4	1.3	✓	YU	TP#5 2 of 2
1/3/94	TP#5			430	1238	705.3	452	2.7	1.6	✓	B	16-21' Rust Comp.
12-9-93	RFL-SS-2605	12-7-93	12/13/93	440	73019	4658	539	135	7.5	✓	YU	TP#7 1 of 2
1/3/94	TP#7			530	100520	4306	485	207	8.9	✓	B	17-21' Rust Comp.
12-9-93	RFL-SS-2606	12-7-93	12/13/93	540	73183	3280	527	139	6.2	✓	YU	TP#7 2 of 2
1/3/94	TP#7			432	99635	3527	474	210	7.4	✓	B	17-21' Rust Comp.

REVIEWED BY: *[Signature]*  
Site HP Manager

Site Correction Factor = 1.8  
 HP Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec., unless otherwise noted



M&K-TEF  
A MORRISON JOHNSON COMPANY



CWMA Federal Environmental Services, Inc.

FOR INFORMATION ONLY

GCS SAMPLE LOG

SITE NAME

RIFLE, CO.

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SCALED	GCS # INITIAL 20 DAY	SS-214 PCL INITIAL 20 DAY	Ts-208 PCL INITIAL 20 DAY	MASS (PPM) SEEL DRV	Ts-225 PCL INITIAL 20 DAY	Ts-232 PCL INITIAL 20 DAY	DEPTH (FEET) 2-1500	TECH INITIAL 20 DAY	REMARKS
12-9-93	RFL-SS-2607			412	9981	222.7	486	2.1	1.5		RWC	TP#11 1 of 2
1/3/94	TP#11	12-7-93	12/13/93	532	1227	930.2	443	2.8	2.1	✓	B	6'-10' Rust Comp
12-9-93	RFL-SS-2608			542	1084	776.7	465	2.3	1.7		RWC	TP#11 2 of 2
1/3/94	TP#11	12-7-93	12/13/93	434	1401	975.2	423	3.3	2.3	✓	B	6'-10' Rust Comp
12-9-93	RFL-SS-2609			444	1440	792.4	553	2.6	1.4		RWC	TP#15 1 of 2
1/3/94	TP#15	12-6-93	12/13/93	534	2753	901.4	507	5.4	1.8	✓	B	10'-13' Rust Comp
12-9-93	RFL-SS-2610			544	1706	671.3	501	3.4	1.3		RWC	TP#15 2 of 2
1/3/94	TP#15	12-6-93	12/13/93	436	2880	714.0	460	6.3	1.6	✓	B	10'-13' Rust Comp
12-9-93	RFL-SS-2611			446	2054	544.6	493	4.2	1.7		RWC	TP#19 1 of 2
1/3/94	TP#19	12-2-93	12/13/93	536	3158	815.1	459	6.9	1.8	✓	B	3.5'-5.5' Rust Comp
12-9-93	RFL-SS-2612			546	1945	834.3	483	4.1	1.7		RWC	TP#19 2 of 2
1/3/94	TP#19	12-2-93	12/13/93	542	2698	939.8	450	6.0	2.1	✓	B	3.5'-5.5' Rust Comp
12-9-93	RFL-SS-2613			448	3779	592.1	522	7.2	1.1		RWC	TP#20 1 of 2
1/3/94	TP#20	12-2-93	12/13/93	544	4898	1007	489	10.0	2.1	✓	B	1'-5' Rust Comp
12-9-93	RFL-SS-2614			548	3957	748.0	557	7.1	1.3		RWC	TP#20 2 of 2
1/3/94	TP#20	12-2-93	12/13/93	444	4875	870.7	520	9.4	1.7	✓	B	1'-5' Rust Comp
12-9-93	RFL-SS-2615			450	11532	1280	540	2.1	2.4		RWC	TP#21 1 of 2
1/3/94	TP#21	12-6-93	12/13/93	446	19101	1376	498	38	2.8	✓	B	1'-5' Rust Comp
12-9-93	RFL-SS-2616			550	12200	1017	511	23	1.9		RWC	TP#21 2 of 2
1/3/94	TP#21	12-6-93	12/13/93	546	19679	1381	502	39	2.8	✓	B	1'-5' Rust Comp

Sita Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec, unless otherwise noted

REVIEWED BY:

*John R. Fernald*  
Site EIP Manager



FOR INFORMATION ONLY

COG SAMPLE LOG

RIFLE, CO.

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	QCS# 1 INITIAL 20 DAY	QCS# 2 INITIAL 20 DAY	TH-203 POC INITIAL 20 DAY	TH-204 POC INITIAL 20 DAY	TH-205 POC INITIAL 20 DAY	TH-206 POC INITIAL 20 DAY	TH-207 POC INITIAL 20 DAY	DEPTH 2.15m ± 0.05m	TECH INITIAL 20 DAY	COMMENTS
12-9-93	RFL-SS-2617			452	936.3	844.6	623	1.5	1.4	1.4		RUC	TP#22 1 of 2
12-9-93	TP#22	12-6-93	12-13-93	448	1066	801.1	548	1.9	1.5	1.5	✓	B	4'-7' Rust Comp
12-9-93	RFL-SS-2618			552	1330	680.8	719	1.8	9.5	9.5	✓	RUC	TP#22 2 of 2
12-9-93	TP#22	12-6-93	12-13-93	548	1382	786.3	634	2.2	1.2	1.2	✓	B	4'-7' Rust Comp
12-9-93	RFL-SS-2619			454	1131	626.9	548	2.1	1.1	1.1		RUC	TP#24 1 of 2
12-9-93	TP#24	12-1-93	12-13-93	450	1454	819.5	505	2.9	1.6	1.6	✓	B	2.5'-5' Rust Comp
12-9-93	RFL-SS-2620			554	1007	632.9	554	1.8	1.1	1.1		RUC	TP#24 2 of 2
12-9-93	TP#24	12-1-93	12-13-93	550	1384	632.9	509	2.7	1.2	1.2	✓	B	2.5'-5' Rust Comp
12-9-93	RFL-SS-2621			456	1430	731.4	634	2.3	1.2	1.2		RUC	TP#25 1 of 2
12-9-93	TP#25	12-1-93	12-13-93	552	2160	738.4	571	3.8	1.3	1.3	✓	B	6.5'-8.5' Rust Comp
12-9-93	RFL-SS-2622			556	938.7	1036	539	1.7	1.9	1.9		RUC	TP#25 2 of 2
12-9-93	TP#25	12-1-93	12-13-93	452	2110	862.0	487	4.3	1.8	1.8	✓	B	6.5'-8.5' Rust Comp
12-9-93	RFL-SS-2623			458	618.4	635.6	544	1.1	1.2	1.2		RUC	TP#26 1 of 2
12-9-93	TP#26	12-6-93	12-13-93	554	1086	704.6	514	2.1	1.4	1.4	✓	B	8'-9.5' Rust Comp
12-9-93	RFL-SS-2624			558	902.6	680.8	537	1.7	1.3	1.3		RUC	TP#26 2 of 2
12-9-93	TP#26	12-6-93	12-13-93	454	1086	896.9	508	2.1	1.8	1.8	✓	B	8'-9.5' Rust Comp
12-9-93	RFL-SS-2625			460	1008	679.2	637	1.6	1.1	1.1		RUC	TP#27 1 of 2
12-9-93	TP#27	12-3-93	12-13-93	556	1122	795.9	572	2.0	1.4	1.4	✓	B	9.5'-11' Rust Comp
12-9-93	RFL-SS-2626			560	627.5	949.3	579	1.1	1.6	1.6		RUC	TP#27 2 of 2
12-9-93	TP#27	12-3-93	12-13-93	456	198.5	870.7	520	1.5	1.7	1.7	✓	B	9.5'-11' Rust Comp

Date Correction Factor = 1.8

VP Correction Factor (if applicable) = 2.0

Count Time = 500 sec, unless otherwise noted

REVIEWED BY: *John R. Jensen*  
Site HP Manager





MK-FE  
A MORRISON JOSEPH COMPANY



DWM Federal Environmental Services, Inc.  
FOR INFORMATION ONLY

KIFLE, CO.

OC3 SAMPLE LOG

SITE NAME

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE RECAL	OC3 INITIAL 20 DAY	TC203 PC INITIAL 20 DAY	AIR55 INITIAL 20 DAY	TC203 INITIAL 20 DAY	TC203 INITIAL 20 DAY	DEPTH	FISH	COMMENTS
12-9-93	RFL-SS-2627	12-9-93	12/13/93	462	1285	482	2.7	1.6	✓	RUC	TP#28 10/2
1/3/94	TP#28	12-9-93	12/13/93	558	2269	442	5.1	1.9	✓	✓	0'-4.5' Rust Con
12-9-93	RFL-SS-2628	12-9-93	12/13/93	562	1962	557	3.5	1.8	✓	RUC	TP#28 20/2
1/3/94	TP#28	12-9-93	12/13/93	458	2189	510	4.3	2.4	✓	✓	0'-4.5' Rust Con
12-9-93	RFL-SS-2629	12-6-93	12/13/93	464	3035	498	7.7	4.1	✓	RUC	TP#29 10/2
1/3/94	TP#29	12-6-93	12/13/93	470	6469	460	14.1	5.9	✓	✓	0'-3' Rust Con
12-9-93	RFL-SS-2630	12-6-93	12/13/93	564	4095	493	8.3	3.7	✓	RUC	TP#29 20/2
1/3/94	TP#29	12-6-93	12/13/93	570	6784	458	14.8	6.6	✓	✓	0'-3' Rust Con
12-9-93	RFL-SS-2631	12-6-93	12/13/93	466	1209	590	2.1	.93	✓	RUC	TAN30 10/2
1/3/94	TP#30	12-6-93	12/13/93	572	1238	566	2.2	1.4	✓	✓	4.5'-7.5' Rust Con
12-9-93	RFL-SS-2632	12-6-93	12/13/93	566	992.2	540	1.8	1.2	✓	RUC	TP#3 20/2
1/3/94	TP#30	12-6-93	12/13/93	472	1491	518	2.9	1.7	✓	✓	4.5'-7.5' Rust Con
12-9-93	RFL-SS-2633	12-9-93	12/13/93	469	667.9	473	1.4	1.5	✓	RUC	TP#32 10/2
1/3/94	TP#32	12-9-93	12/13/93	574	536.9	460	1.2	1.2	✓	✓	0'-1' Rust Con
12-9-93	RFL-SS-2634	12-9-93	12/13/93	568	3021	482	.62	1.6	✓	RUC	TP#32 20/2
1/3/94	TP#32	12-9-93	12/13/93	474	510.4	469	1.1	1.8	✓	✓	0'-4' Rust Con
12-9-93	RFL-SS-2635	12-9-93	12/13/93	470	530.7	521	1.0	1.4	✓	RUC	TP#33 10/2
1/3/94	TP#33	12-9-93	12/13/93	576	631.0	488	1.3	1.1	✓	✓	7'-9' Rust Con
12-9-93	RFL-SS-2636	12-9-93	12/13/93	570	470.4	486	.97	1.5	✓	RUC	0'-7.5' Rust Con
1/3/94	TP#33	12-9-93	12/13/93	476	421.3	454	0.93	1.4	✓	✓	17'-9' Rust Con

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count time = 5.00 sec. unless otherwise noted

REVIEWED BY: *Richard K. Howard*  
 Site Mgr. Manager

FOR INFORMATION ONLY

OCS SAMPLE LOG

RIFLE, CO.

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SCALED	QCS # INITIAL 20 DAY	B-214 GC BETALS 20 DAY	T-200 #C INITIAL 20 DAY	SIASS (gross) (net) (skt)	14-220 #C/B INITIAL 20 DAY	T-232 #C/B INITIAL 20 DAY	DEPTH $\frac{1}{2}$ 15 min > 15 min	TECH INITIAL 20 DAY	COMMENTS
12-9-93	RFL-SS-2637			422	5612	8222	483	1.2	1.7		RMC	TP# BKG 1 of 2
1/3/94	TP# BKG	12-7-93	93 12-13-94	578	7061	7576	436	1.6	1.7	✓	B	7-12' Rust Con
12-9-93	RFL-SS-2638			522	8626	9014	522	1.7	1.7		RMC	TP# BKG 2 of 2
1/3/94	TP# BKG	12-7-93		478	1039	8620	471	2.2	1.8	✓	B	7-12' Rust Con
12/10/93	RFL-SS-2639			406	34978	2055	505	6.8	4.1		B	TP# 29 0-1'
1/10/94	TP# 29	12/1/93		554	56401	2532	505	11.2	5.0	✓	B	TAC sample
12/10/93	RFL-SS-2640			506	11247	1074	561	20.0	1.9		B	TP# 29 1-2'
1/10/94	TP# 29	12/1/93		454	20115	1768	561	36	3.2	✓	B	TAC sample
12/10/93	RFL-SS-2641			408	32618	1698	554	59.0	3.1		B	TP# 29 2-3'
1/10/94	TP# 29	12/1/93		558	55305	2503	554	100	4.5	✓	B	TAC sample
12/10/93	RFL-SS-2642			422	1672	8446	471	3.5	1.8		B	TP# 28 0-15'
1/3/94	TP# 28	12/9/93		480	2434	7663	471	5.4	1.6	✓	B	Composite
12/10/93	RFL-SS-2643			522	4345	6233	401	1.1	1.6		B	TP# 32
1/3/94	TP# 32	12/9/93		580	710.9	460.3	401	1.8	1.1	✓	B	comsy Ampcol
12/10/93	RFL-SS-2644			424	451.1	7924	491	0.92	1.6		B	TP# 33
1/3/94	TP# 33	12/9/93		582	593.2	527.4	491	1.2	1.1	✓	B	comsy Ampcol
12/15/93	RFL-SS-2645			400	1909	1315	803	34.0	1.6		B	TP# 4
1/5/94	TP# 4	12/15/93		446	26094	1881	803	32.8	2.3	✓	B	17-18' TAC
12/15/93	RFL-SS-2646			500	190510	8534	805	337.0	10.6		B	TP# 6
1/5/94	TP# 6	12/15/93		448	218120	7480	805	271	9.3	✓	B	24-25' TAC

Site Correction Factor = 1.18  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec, unless otherwise noted

REVIEWED BY: *John H. ...*  
 Site Mgr. Manager



WICK-FEE  
A MORRISON COMPANY



CWMA Federal Environmental Services, Inc.  
FOR INFORMATION ONLY

SITE NAME  
RIFLE, CO.

CCS SAMPLE LOG

COUNT DATE INITIAL 20 DAY	SAMPLE ID & LOCATION	DATE SAMPLED	DATE SEALED	DCS # INITIAL 20 DAY	B-214 P/C INITIAL 20 DAY	TI-408 P/C INITIAL 20 DAY	MASS (g) WGT. DATE	U-235 P/C/g INITIAL 20 DAY	U-238 P/C/g INITIAL 20 DAY	DEPTH < 15cm > 15cm	TECH INITIAL 20 DAY	COMMENTS
12/15/93	RFL-SS-2647	12/15/93	12/16/93	402	6780	827.2	755	9.0	1.1	✓	B	17-13' TAC
1/5/94	TP # 1	12/15/93	12/16/93	546	9534	937.8	755	13	1.2	✓	B	TP # 7 TAC
12/15/93	RFL-SS-2648	12/15/93	12/16/93	503	17120	1611	809	51.2	2.0	✓	B	8-9' TP # 30 TAC
1/5/94	TP # 30	12/15/93	12/16/93	548	45157	2206	809	56	2.7	✓	B	TP # 30 TAC
12-16-93	RFL-SS-2649A	12-15-93	12/17/93	400	1767	853.3	498	3.5	1.7	✓	PV	A-914 CPTM
1/6/94	RFL-SS-2650A	12-15-93	12/17/93	514	3664	1064	466	7.9	2.3	✓	B	B-N.W.
12-16-93	RFL-SS-2651A	12-15-93	12/17/93	500	883.0	7959	522	1.7	1.5	✓	PV	A 1040 CPTM
1/6/94	RFL-SS-2652A	12-15-93	12/17/93	508	697.4	1007	480	1.5	2.1	✓	B	Area B-Fence Line
12-16-93	RFL-SS-2653A	12-15-93	12/17/93	402	1656	801.1	430	3.9	1.9	✓	DRC	B-N.W.
1/6/94	RFL-SS-2654A	12-15-93	12/17/93	408	4240	661.8	363	12	1.8	✓	B	A 1350 CPTM
12-16-93	RFL-SS-2655A	12-15-93	12/17/93	502	587.4	901.4	498	1.2	1.8	✓	DRC	B-N.W.
1-10-94	RFL-SS-2656A	12-15-93	12/16/93	510	715.9	700.0	464	1.5	1.5	✓	B	A 412 CPTM
12-16-93	RFL-SS-2657A	12-15-93	12/16/93	404	2631	879.5	452	5.8	1.9	✓	DRC	B-N.W.
1/6/94	RFL-SS-2658A	12-15-93	12/16/93	458	4819	983.9	452	11	2.2	✓	B	A-1610 CPTM
12-16-93	RFL-SS-2659A	12-15-93	12/17/93	504	773.9	968.5	517	1.5	1.9	✓	DRC	B-N.W. FENCE
1/6/94	RFL-SS-2660A	12-15-93	12/17/93	410	970.6	496.3	459	2.1	1.1	✓	B	A-1040 CPTM
12-16-93	RFL-SS-2661A	12-15-93	12/17/93	406	639.6	766.3	575	1.1	1.3	✓	DRC	B-N.W.
1/6/94	RFL-SS-2662A	12-15-93	12/17/93	512	352.6	863.0	573	0.62	1.5	✓	B	A 550 CPTM
12-16-93	RFL-SS-2663A	12-15-93	12/17/93	506	717.0	1084	493	1.5	2.2	✓	DRC	B-N.W.
1/6/94	RFL-SS-2664A	12-15-93	12/17/93	412	423.5	757.5	463	0.91	1.6	✓	B	A-712 CPTM

Site Correction Factor = 1.8  
 VP Correction Factor (if applicable) = 2.0  
 Count Time = 500 sec., unless otherwise noted

REVIEWED BY: *John H. ...*  
 Site HP Manager

\*The "A" was added to the sample ID # for 2649 - 2656 to avoid confusion with duplicate sample ID numbers assigned