

***** MRC OPERATING STATUS REPORT COMPLETED BY REACTOR ENGINEERING *****

1. DOCKET.....50-423
 2. REPORTING PERIOD...JANUARY 1991
 3. UTILITY CONTACT.....A. L. ELMS 203-644-5388
 4. LICENSED THERMAL POWER..... 3411
 5. NAMEPLATE RATING (GROSS MWE)..... 1,253 MW
 6. DESIGN ELECTRICAL RATING (NET MWE)..... 1,153.6
 7. MAXIMUM DESIGNABLE CAPACITY (GROSS MWE)..... 1,184.2
 8. MAXIMUM DESIGNABLE CAPACITY (NET MWE)..... 1,137.0
 9. IF CHANGES LISTED ABOVE SINCE LAST REPORT, REASONS ARE.....
 N/A
 10. POWER LEVEL TO WHICH RESTRICTED, IF ANY (NET MWE).....N/A
 11. REASON FOR RESTRICTION, IF ANY....N/A

 * MILLSTONE *
 * UNIT 3 *

	MONTH	YEAR TO DATE	CUMULATIVE TO DATE
	*****	*****	*****
12. HOURS IN REPORTING PERIOD	744.0	744.0	41,880.0
13. NUMBER OF HOURS THE REACTOR WAS CRITICAL	574.6	574.6	34,159.7
14. REACTOR RESERVE SHUTDOWN HOURS	169.4	169.4	1,698.3
15. HOURS GENERATOR ONLINE	554.9	554.9	33,520.4
16. UNIT RESERVE SHUTDOWN HOURS	0.0	0.0	0.0
17. GROSS THERMAL ENERGY GENERATED (MWH)	1,384,282.0	1,384,282.0	109449094.0
18. GROSS ELECTRICAL ENERGY GENERATED (MWH)	456,486.0	456,486.0	37,765,462.5
19. NET ELECTRICAL ENERGY GENERATED (MWH)	426,453.0	426,453.0	36,000,062.5
20. UNIT SERVICE FACTOR	74.6	74.6	80.0
21. UNIT AVAILABILITY FACTOR	74.6	74.6	80.0
22. UNIT CAPACITY FACTOR (USING MDC NET)	50.4	50.4	75.4
23. UNIT CAPACITY FACTOR (USING DER NET)	49.7	49.7	74.5
24. UNIT FORCED OUTAGE RATE	25.4	25.4	10.1
25. UNIT FORCED OUTAGE HOURS	189.1	189.1	3,767.6

SHUTDOWNS SCHEDULED OVER NEXT SIX MONTHS (TYPE, DATE, AND DURATION OF EACH).....
 N/A

IF CURRENTLY SHUTDOWN, ESTIMATED STARTUP DATE.....March 21, 1991

9102150141 910211
 FDR ADÖCK 05000423
 R FDR

UNIT SHUTDOWNS AND POWER REDUCTIONS

DOCKET NO. 50-423
 UNIT NAME MILLSTONE 3
 DATE 2-7-91
 COMPLETED BY A. ELMS
 TELEPHONE (203) 444-5388

No.	Date	Type (1)	Duration Hours	Reason (2)	Method of Shut down Reactor(3)	Licensee Event Rept No.	System Code	Component Code	Cause and Corrective Action to Prevent Recurrence
90-13	12-31-90	F	189.1	A	2	90-030-00	SB	LCV	Manually tripped reactor due to two ruptured moisture separator reheater drain tank pipes. The cause of the break was single phase erosion/corrosion. Corrective action included removing the pipes from service by capping, adding the pipe to the erosion/corrosion program and investigating why the pipes were not already included in the program.

1: F: Forced
 S: Scheduled

2: Reasons:
 A-Equipment Failure (Explain)
 B-Maintenance or Test
 C-Refueling
 D-Regulatory Restriction
 E-Operator Training & License Exam
 F-Administrative
 G-Operational Error (Explain)
 H-Other

3: Method
 1-Manual
 2-Manual Scram
 3-Automatic Scram
 4-Continued from previous month
 5-Power Reduction (Duration = 0)
 9-Other (Explain)

4: Exhibit G - Instructions for Preparation of Data Entry Sheets for Licensee Event Report (LER) File (NUREG-0161)
 5: Exhibit 1 - Same Source

REFUELING INFORMATION REQUEST

January 1991

1. Name of facility: Millstone 3.
2. Scheduled date for next refueling shutdown: February 1, 1991 (currently in refuel).
3. Scheduled date for restart following refueling: March 21, 1991
4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendments?

As a result of the new fuel design, Technical Specifications changes to the Axial Flux Difference, Heat Flux Hot Channel Factor, and Refueling Water Storage Tank sections will be required. Furthermore, the Fuel Storage section of Design Features will be changed to allow continued regionalized storage of spent fuel in the spent fuel pool. Also, the Instrumentation section will be changed to reflect a new High Flux at Shutdown setpoint.

5. Scheduled date for submitting licensing action and supporting information.

All Technical Specification changes submitted.

6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design of performance analysis methods, significant changes in fuel design, new operating procedures:

Cycle 4 fuel assemblies will be of the Westinghouse Vantage 5H design. This design includes debris filter bottom nozzles, intermediate flow mixing grids, integral fuel rod burnable absorbers, and axial blankets.

7. The number of fuel assemblies (a) in the core and (b) in the spent fuel storage pool:

(a): 193 (b): 248

8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned, in number of fuel assemblies:

Present size - 756.

No increase requested.

9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity:

End of cycle 5.