

ARCO

Bluewater Mill
Post Office Box 638
Grants, New Mexico 87020
Telephone 505 876 2211
Facsimile 505 876 2772

04008902 760E

40-8902
X61225

December 22, 1993

RETURN ORIGINAL TO PDR, HQ.

Mr. Ramon E. Hall
Director
United States Nuclear Regulatory Commission
Uranium Recovery Field Office
Region IV
730 Simms Street, Suite 100
Golden, Colorado 80401

RE: LICENSE #SUA-1470
DOCKET #40-8902



Dear Mr. Hall:

This letter is a request to an amendment to AP.CO's Source Material License #SUA-1470, for the following items:

1. Design modifications - Carbonate Tailings
2. Final design modifications - Main Tailings Impoundment South Toe Bench
3. Slope design modifications - Main Tailings Impoundment
4. Rock Specifications - Quarry and Scoring Criteria

Attached are the proposed modifications along with support documentation. As previously discussed with your staff the above referenced items are a result of final design investigations and discovery of unknown subsurface conditions during current reclamation activities.

Should you have any questions or wish to review this information with us please contact myself or Christopher Sanchez of my staff.

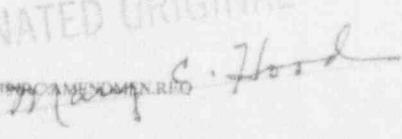
Sincerely,


R. S. Ziegler
Project Manager

Attachment

18-167

pc: CFG
SP
NP
CS

DESIGNATED ORIGINAL
Certified by 

DF02
111
94-0146

Atlantic Richfield Company
9402240057 931222
PDR ADOCK 04008902
PDR

ARCO-5011-A

40-8902

Design Modification Amendment Request

ARCO Bluewater Mill
Reclamation Plan

LICENSE NO. SUA-1470
DOCKET NO. 40-8902

December, 1993

wj lu 12/22/93
94-0146

TABLE OF CONTENTS

<u>Section</u>	<u>Page No.</u>
1.0 Design Modification - Carbonate Tailings Surface and Cover Design	1
1.1 Introduction	1
1.2 Relocation of Tailings	1
1.3 Radon Barrier Design	2
1.3.1 Disposal Area 2	2
1.3.2. Disposal Area 3	3
1.4 Erosion Protection	4
1.4.1 Hydrology	4
1.4.2 Erosion Protection	4
2.0 South Bench - Placement of Radon Barrier at Toe of South Dike of Main Tailings Impoundment.	6
2.1 Introduction	6
2.2 Radon Barrier	6
2.3 Erosion Protection	6
3.0 Slope Design Modification - North East Main Tailings Impoundment	8
3.1 Introduction	8
3.2 Slope Design	8
3.3 Construction	8
3.4 Erosion Protection	9
4.0 Rock Specification - Quarry and Scoring Criteria	10
4.1 Introduction	10
4.2 Rock Quarry	10
4.3 Specifications	10
4.4 Soil Rock Matrix Specifications	11

List of Figures

- 1.1 Carbonate Tailings - New and old boundary (also showing DA#2 and DA#3)
- 1.2 Carbonate Tailings Test Holes
- 1.3 Carbonate Tailings Final Topography
- 1.4 Profile of Disposal Area #2
- 1.5 Profile of Disposal Area #3
- 2.1 South Bench Plan View - extent of tailings
- 2.2 Design Configuration of South Bench
- 2.3 South Bench cross-section
- 3.1 Main Tailings Impoundment Area of Design Modification
- 3.2 Cross-Section of Slope Modification on Main Tailings Impoundment
- 3.3 Main Tailings Impoundment, Typical Section 75+00 to 86+00

List of Tables

- 4.1 Rock Quality
- 4.2 Erosion Protection Rock Size and Scoring

List of Appendices

Appendix A

Carbonate Tailings Log Hole Information

Hydrology

Rock Sizing

RAECOM Runs

Appendix B

South Bench Log Hole Information

RAECOM Runs

Erosion Control Calculations

1.0 DESIGN MODIFICATIONS - CARBONATE TAILINGS SURFACE AND COVER DESIGN

1.1 Introduction

ARCO proposes to make adjustments to the configuration, depth of radon cover and surface erosion protection on the Carbonate Tailings. Since approval of the reclamation plan ARCO has undertaken an exploration program to better identify the aerial extent of the Carbonate Tailings. The results of this exploration have identified the main body of Carbonate Tailings on the eastern side of the impoundment to be smaller than originally anticipated. The main body tailings has been defined as the area where tailings have significant depth. Many areas surrounding the impoundment were discovered to be shallow and uneven. Figure 1.1 illustrates the original boundary and the new boundary developed following the exploration program.

Two of the three Bluewater Mill disposal areas reside within the boundary of the Carbonate Tailings as shown in Figure 1.1. During decommissioning of the Mill these areas were filled with debris and soil. In determining the final design configuration for the Carbonate Tailings, ARCO has re-evaluated the cover requirements taking into account the layers of debris and soil. These modifications have been incorporated into the overall design of the Carbonate Tailings.

1.2 Relocation of Tailings

ARCO will relocate the existing shallow tailings outside the new Carbonate Tailings boundary into the main body of the tailings impoundment to the degree possible with conventional equipment. Tailings depths outside of the new boundary range from a few inches to approximately 3 feet. Relocation of the tailings to within the new boundary will eliminate the areas where placement of radon barrier and erosion protection would be difficult due to the irregular configuration of the tailings.

The new Carbonate Tailings boundary was established from log hole information collected along the perimeter of the impoundment. The log hole locations are shown on Figure 1.2 and profile information is attached in Appendix A. Relocated tailings will be placed in the northwest low lying areas within the new boundary prior to placement of radon barrier. The final proposed topographic surface is shown on drawing Figure 1.3. Approximately 25,000-cy of tailings will be relocated to locations within the new boundary.

The northwest area of the Carbonate Tailings are to receive radon cover to following the placement of the relocated tailings. A protocol for evaluation of the final cover over the north portion of the impoundment has been submitted in ARCO's Final Radon Barrier Design, ARCO Bluewater Mill Main Tailings Report dated December 1993. This area is to be reevaluated and the final radon cover depth placed.

1.3 Radon Barrier Design

Disposal Area #2 and Disposal Area #3 are within the boundary of the Carbonate Tailings. Each of the Disposal Areas have received a significant amount of debris and soil during the decommissioning of the Bluewater Mill. Tailings and process residues will be covered to attenuate radon to less than 20 pCi/m²/s. Cover thickness calculation were completed using the computer RAECOM model utilizing the revised parameters contained in our December 1993 Final Radon Barrier Design Report and to account for the interstitial soils placed in the debris layers. The complete analysis is included in Appendix A of this report.

1.3.1 Disposal Area #2

Disposal Area #2 in the Reclamation Plan was divided into two major sections, the Carbonate Tailings South (Asbestos Disposal Area) and the Northern Area. The asbestos disposal area is geographically distinct from the remainder of the area in that it resides in a basalt depression as shown on Figure 1.1. The remainder of the disposal area is on the surface of the former Carbonate Tailings.

Carbonate Tailings South - Asbestos Disposal Area

This area has been reclaimed in accordance with the ARCO Reclamation Plan as amended by ARCO's May 9, 1991 request for license amendment. Approximately 7-feet of asbestos contaminated debris and interstitial fill was placed, followed by 12-feet of radon barrier. A soil/rock matrix is in place on the surface with rip-rap and filter on all 5:1 slopes. Drainage out of the basin is provided by a spillway cut through the adjacent basalt.

Disposal Area #2 - Northern Area

The northern area of Disposal Area #2 received two lifts of debris and soil, with depths of 5-feet and 2-feet respectively. Each lift of debris with interstitial soil has been covered with a 2-foot layer of engineered fill.

The RAECOM model for cover thickness requirement in this area was modified to include the two lifts of soil/debris and engineered fill on the disposal area. Input for the model is derived from parameters prepared by Rogers and Associates, the Roy F. Weston Report for ARCO's Reclamation Plan and ARCO's Final Radon Barrier Design Report, December 1993. A profile of current conditions is shown on Figure 1.4. The calculated model shows that no additional cover is required in this area to meet the 20pCi/m²/s radon flux.

1.3.2 Disposal Area #3

During decommissioning Disposal Area #3 received a 5-foot lift of debris and interstitial soil. A 2-foot layer of engineered fill has been placed over the debris/soil lift.

The RAECOM model input for cover thickness requirements was modified to include the lift of soil and debris material placed on the disposal area.

Input for the model is derived from parameters prepared by Rogers and Associates and Weston for ARCO's Reclamation Plan and Decommissioning Plan. A profile of current conditions is shown on Figure 1.5. The cover requirement as calculated by the RAECOM model for Disposal Area #3 is 2.4-feet.

Drawing 1.3 shows the modified surface configuration for the Carbonate Tailings which take into account the modified cover requirements.

1.4 Erosion Protection

Erosion protection requirements for the Carbonate Tailings have been reevaluated using the new boundary and adjusted topographic surface. The erosion parameters are the same as those contained in ARCO's Reclamation Plan.

1.4.1 Hydrology

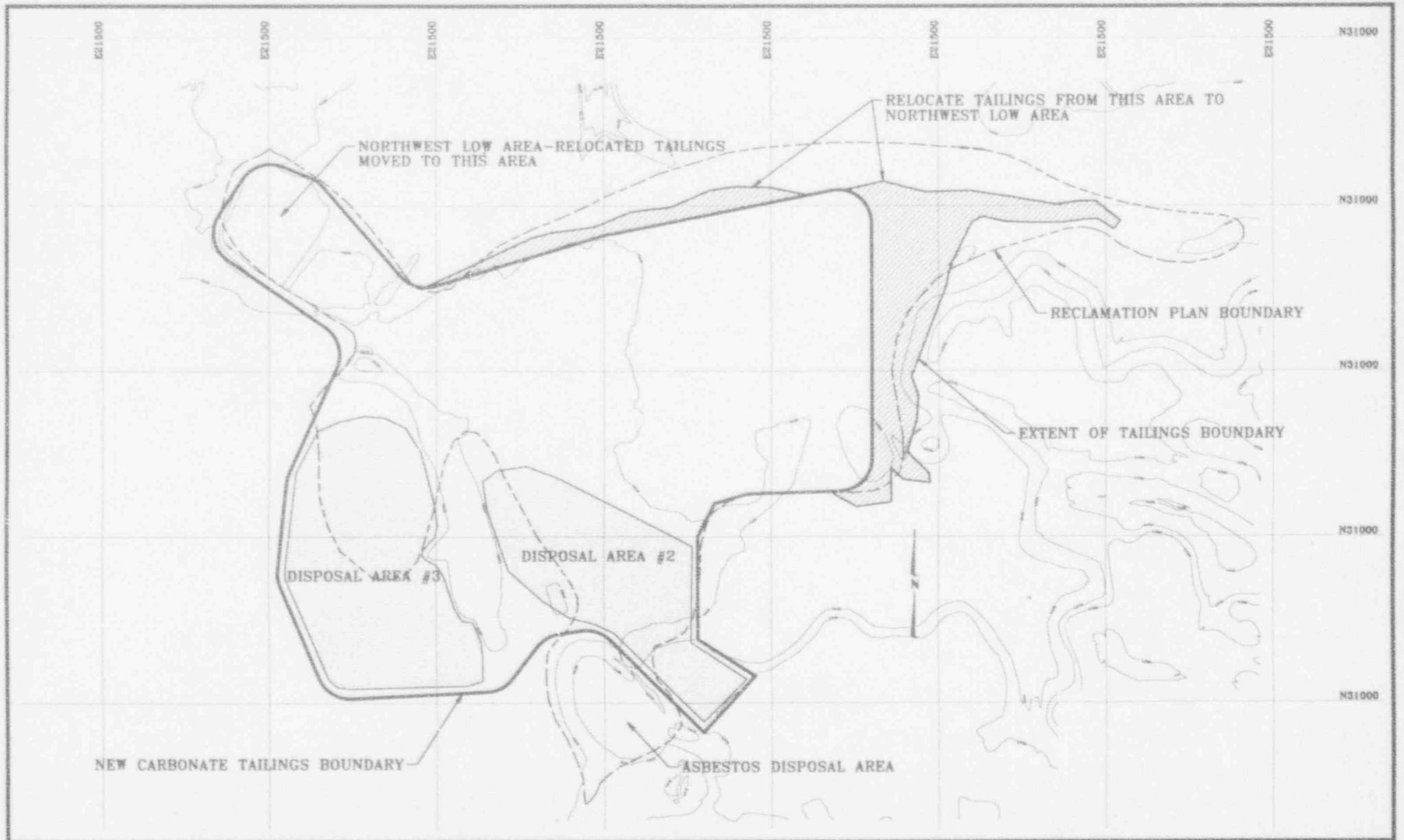
Surface configuration design of the Carbonate Tailings provides for drainage from the center of the Tailings to the exterior edges in all directions. The area defined as the northeast quadrant has the largest area relative to the hydraulic length and thus becomes the critical design area. Hydraulic modeling was completed using the Corp. of Engineers HEC-1 computer program and the natural channels computer program which employs the Manning equation. Maximum discharge was calculated using the PMF event as previously determined in ARCO's Reclamation Plan.

The calculated maximum unit discharge for the northeast quadrant is 0.57-cfs. Peak surface velocity has been calculated at 2.15-feet/second. The maximum calculated velocity on the 5:1 slope is 4.8¹ feet/second.

1.4.2 Erosion Protection

Consistent with the rock sizing methods in ARCO's Reclamation Plan, the

Corp. of Engineers Method was used to size rock covers for the newly designed surface of the Carbonate Tailings. Erosion protection will consist of a 50/50 mixture soil/rock matrix over the entire surface. A $d_{50} = 1\frac{1}{2}$ inch rock will be used in the soil/rock matrix. Slope cover protection has not required any change to the rock size and filter proposed in the 1990 Reclamation Plan. Calculations for rock selection on the top surface soil/rock matrix and verifications of the slope rock sizing are shown in Appendix A.



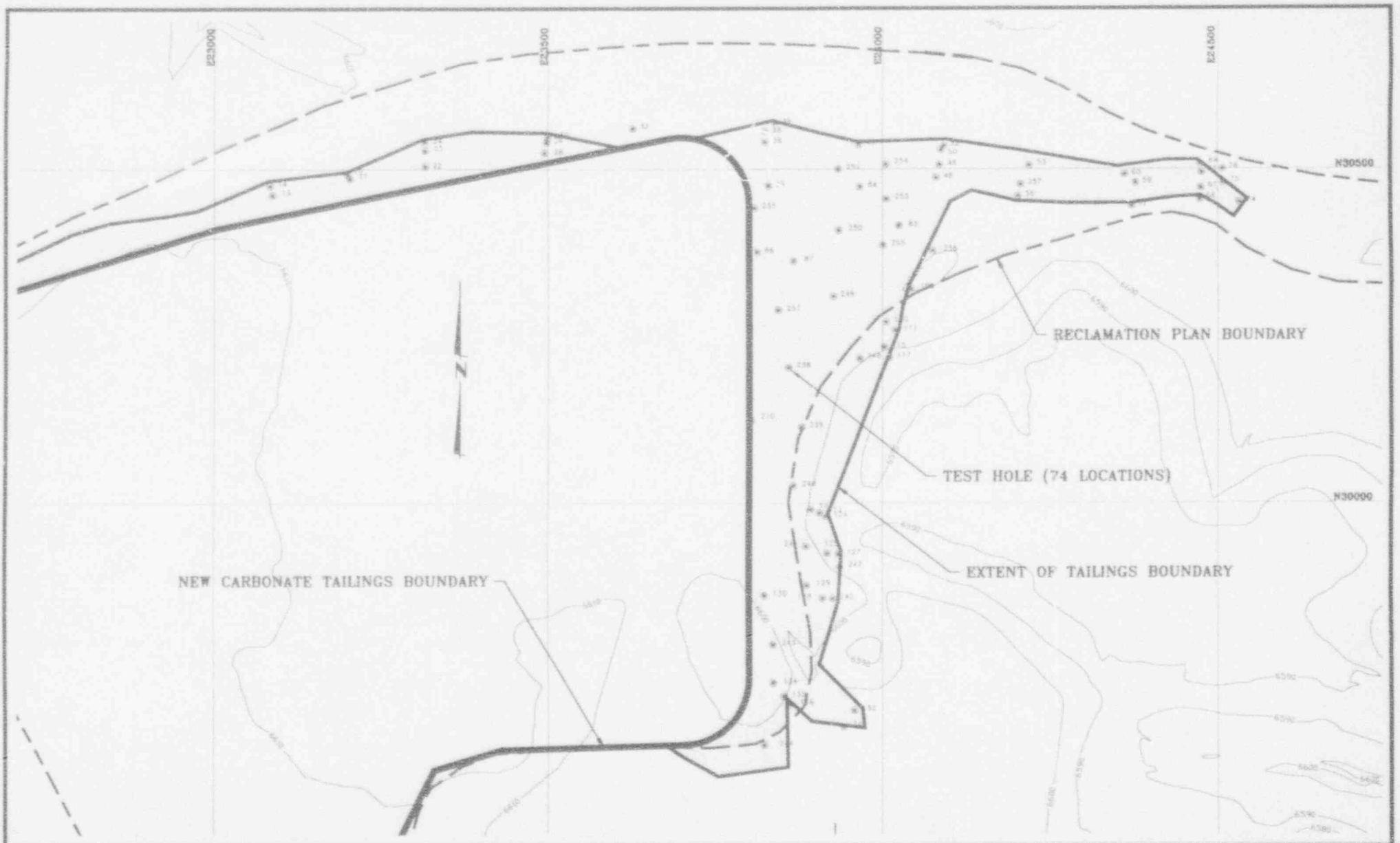
NO.	REVISION	BY	DATE


ANDERSON ENGINEERING CO., INC.
 Long Beach, California San Jose, CA Irvine, CA
 Tel: (909) 731-4888 Fax: (909) 731-7968
 CIVIL ENGINEERS CONSTRUCTION MANAGERS

FIGURE 1.1
CARBONATE TAILINGS
NEW & OLD BOUNDARY

ATLANTIC RICHFIELD COMPANY


DATE	01/87
ISSUED	02
APPROVED	03
DATE	12/21/85
SCALE	1"=500'
DRAWN BY	MA
CHECKED BY	MA
DESIGNED BY	MA



NO.	REVISION	DATE	BY	DESCRIPTION



ANDERSON ENGINEERING CO., INC.
 Long Beach, California Salt Lake City, Utah Phoenix, Arizona
 CIVIL ENGINEERS CONSTRUCTION MANAGERS

FIGURE 1.2
CARBONATE TAILINGS
TEST HOLE LOCATIONS

ATLANTIC RICEFIELD COMPANY


Drawn by:	ST
Checked by:	GA
Approved by:	ES
Date:	12/21/83
Scale:	1" = 400'
Sheet No.:	24
Project No.:	



NO.	REVISION	DATE	BY	REVISION	DATE


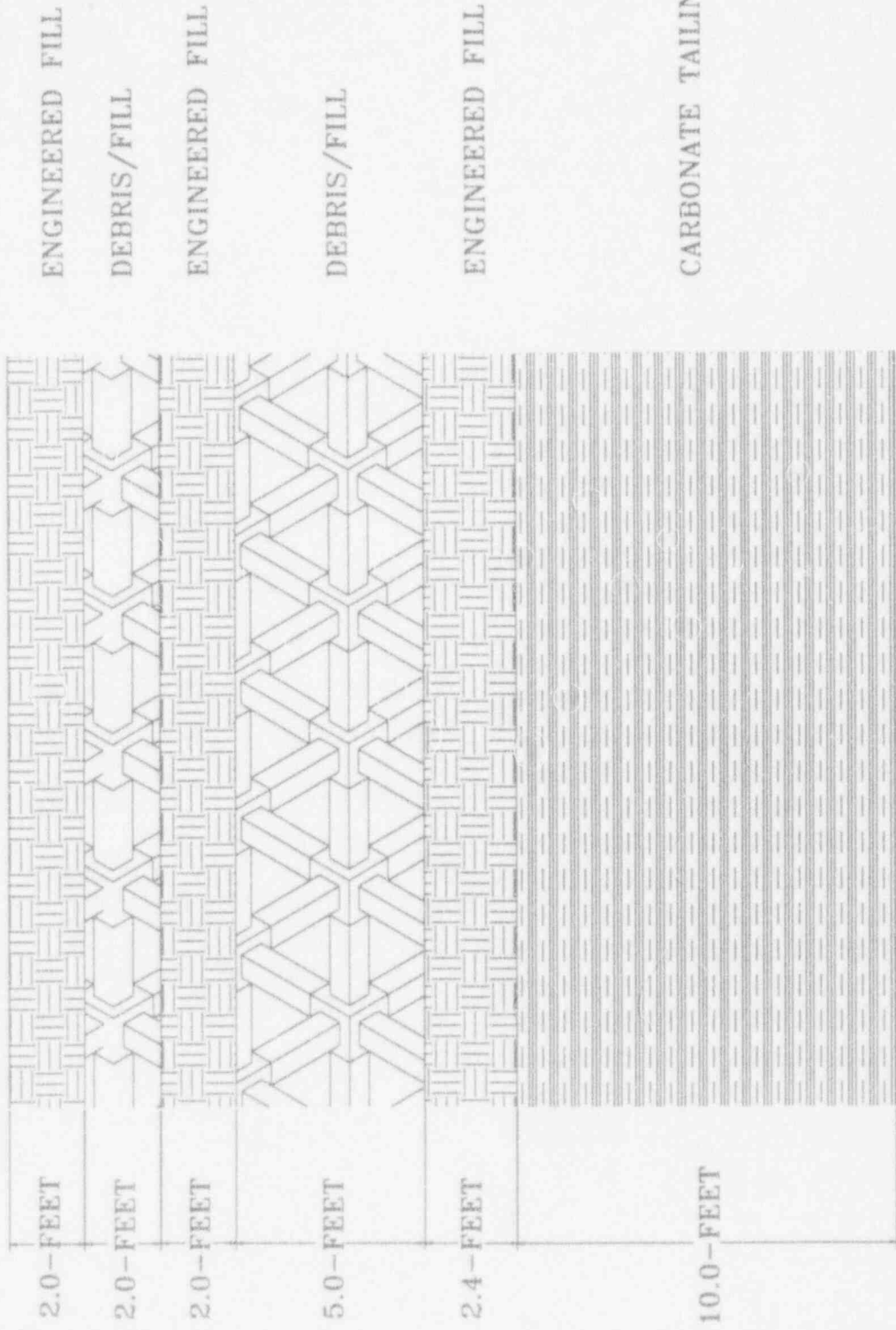

ANDERSON ENGINEERING CO., INC.
 CIVIL ENGINEERS CONSTRUCTION MANAGERS
 1000 W. 10th St. 1000 W. 10th St.
 Oklahoma City, OK 73101 Oklahoma City, OK 73101
 Phone (405) 751-8338 Fax (405) 751-1968

FIGURE 1.3
CARBONATE TAILINGS
FINAL TOPOGRAPHY


ATLANTIC PORTLAND CEMENT COMPANY
BOONVILLE MILL
 1000 W. 10th St.

DATE	07
PROJECT	33
APPROVED	CS
DATE	12/21/82
SCALE	1"=500'
DATE	02
BY	



ENGINEERED FILL

DEBRIS/FILL

ENGINEERED FILL

DEBRIS/FILL

ENGINEERED FILL

CARBONATE TAILINGS

2.0- FEET

2.0- FEET

2.0- FEET

5.0- FEET

2.4- FEET

10.0- FEET

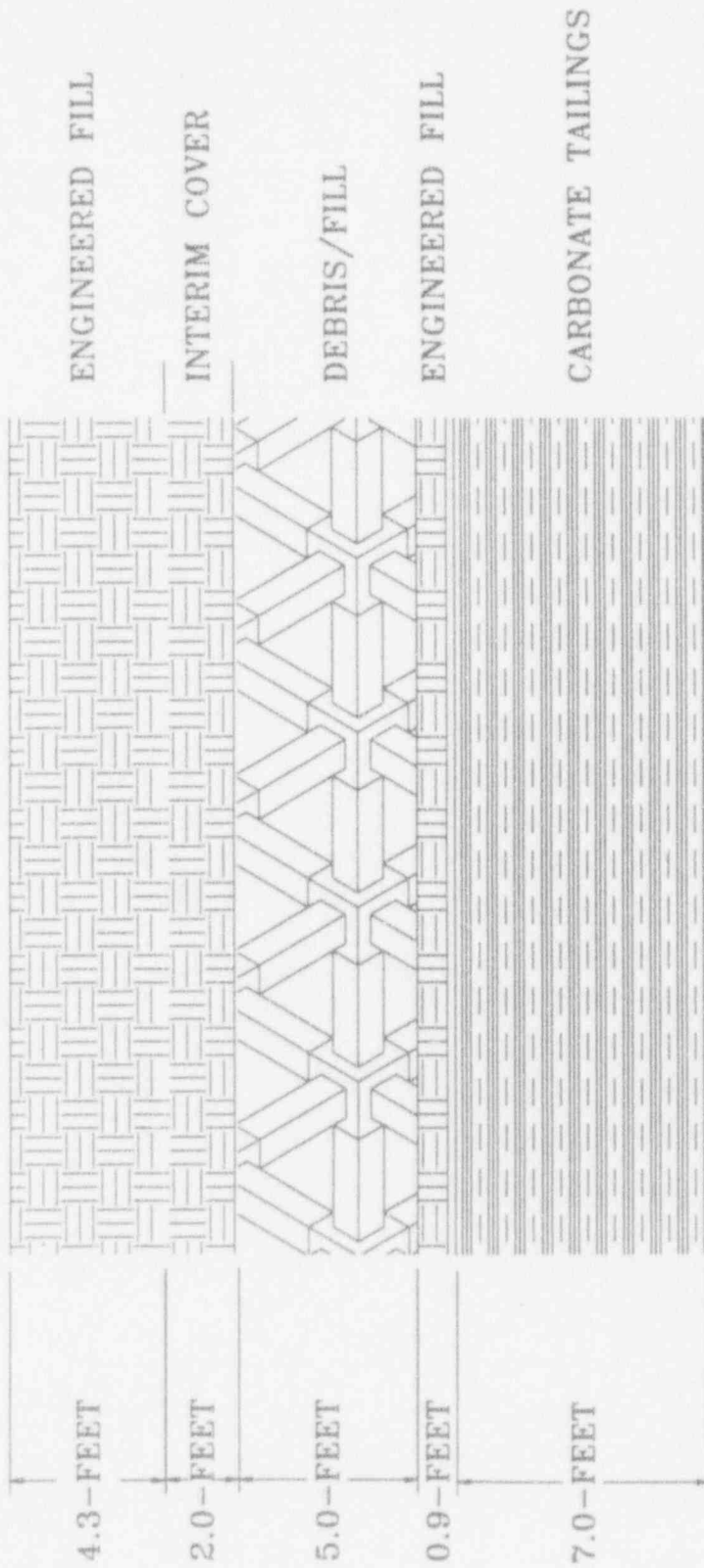
DATE	12/93
BY	NTS
CHECKED	NTS
APPROVED	
SCALE	
PROJECT NO.	



TYPICAL CROSS SECTION
DISPOSAL AREA #2
FIGURE 1.4

ANDERSON ENGINEERING CO., INC.
238 S. Main Street
Salt Lake City, Utah 84143
Telephone (801) 733-0000 Fax (801) 733-7000
CIVIL ENGINEERS CONSTRUCTION MANAGERS

NO.	DATE	REVISION



DATE: 12/20/00
 DRAWN BY: SA
 CHECKED BY: CS
 DATE: 12/20/00
 DESIGNED BY: RTJ
 SCALE: AS SHOWN



TYPICAL CROSS SECTION
 DISPOSAL AREA #3
 FIGURE 1.5

ANDERSON ENGINEERING CO., INC.
 1000 West Lake City
 Dallas, Texas 75208
 Telephone (972) 751-1000 Fax (972) 751-1000
 CIVIL ENGINEERS CONSTRUCTION MANAGERS

NO.	DATE	REVISION

2.0 SOUTH BENCH - PLACEMENT OF RADON BARRIER AT TOE OF SOUTH DIKE MAIN TAILINGS IMPOUNDMENT

2.1 Introduction

The area south of the Main Tailings Impoundment at the toe of the 5:1 slope between Station 113+00 and Station 123+00 has been determined to contain tailings materials. Figure 2.1 provides a plan view of this area showing the extent of the tailings material. The tailings material found varies in thickness from several feet to over seventeen feet in depth. ARCO proposes to cover these areas with an approximately 3.4-feet of radon barrier, a depth similar to that designed for the Main Tailings Impoundment embankments in the original 1990 Reclamation Plan.

2.2 Radon Barrier

RAECOM models indicate that 1.2-feet of cover is the maximum cover this area requires to attenuate radon levels to NRC criteria. A depth of 3.4-feet has been placed over this tailings material which is consistent with the radon cover on the adjacent Main Tailings Impoundment embankment slopes. The log hole information for the south bench area and the RAECOM calculations for this area are attached in Appendix B. Radium concentrations used in the design of the cover were determined from field samples collected at several locations within the area. The physical properties of the tailings are similar to those found in the Old Acid Tailings. In addition, early aerial photographs indicate that deposits were made during the same period as the Old Acid Tailings. RAECOM calculations use the physical characteristics of the Old Acid Tailings with the measured radium concentrations of field samples taken. Figure 2.2 shows the complete design configuration of the South Bench. A typical cross section of the proposed South Bench is shown in Figure 2.3.

2.3 Erosion Protection

The top surface of the South Bench has been designed to meet stable slope criteria. The stable slope calculation is included in Appendix B with this report. Following

final grading the surface will receive 12 inches of topsoil and be seeded with the mixture contained in the ARCO Reclamation Plan. Universal Soil Loss Equation (USLE) calculations were completed on the top surface and are also included in this report. These USLE calculations show that 2.3 inches of material will be eroded during the 1000 year design life. A 5-foot wide apron, consisting of $d_{50} = 2\frac{1}{2}$ inch rock, will be constructed at the base of the Main Tailings Impoundment embankment to dissipate hydraulic energy from slope runoff. The 5:1 slopes around the edges of the South Bench will be protected with the same 6 inch depth of $d_{50} = \frac{1}{2}$ inch filter rock and $d_{50} = 2\frac{1}{2}$ inch rock which will be placed on the Main Tailings Impoundment embankments. A 5 foot wide rock apron will be placed at the base of the 5:1 slopes to mitigate head cutting into the slope.



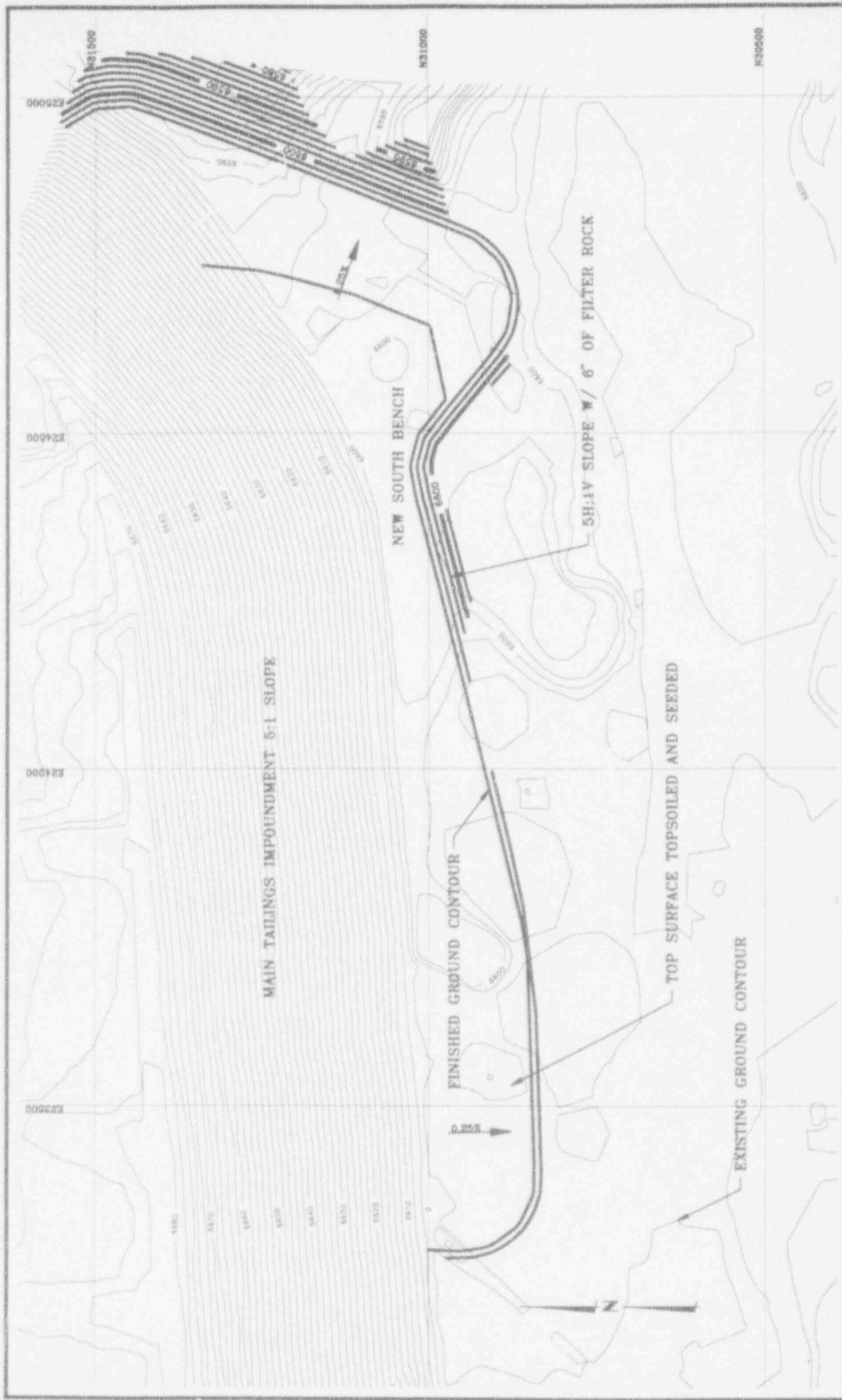
DATE	NO.	BY	REVISION



FIGURE 2.1
SOUTH BENCH
EXTENT OF TAILINGS

ANDERSON ENGINEERING CO., INC.
 1000 West 10th Street
 Oklahoma City, Oklahoma 73106
 Telephone: (405) 751-4444 Fax: (405) 751-1805
 CIVIL ENGINEERS CONSTRUCTION MANAGERS

DATE	NO.	BY	REVISION



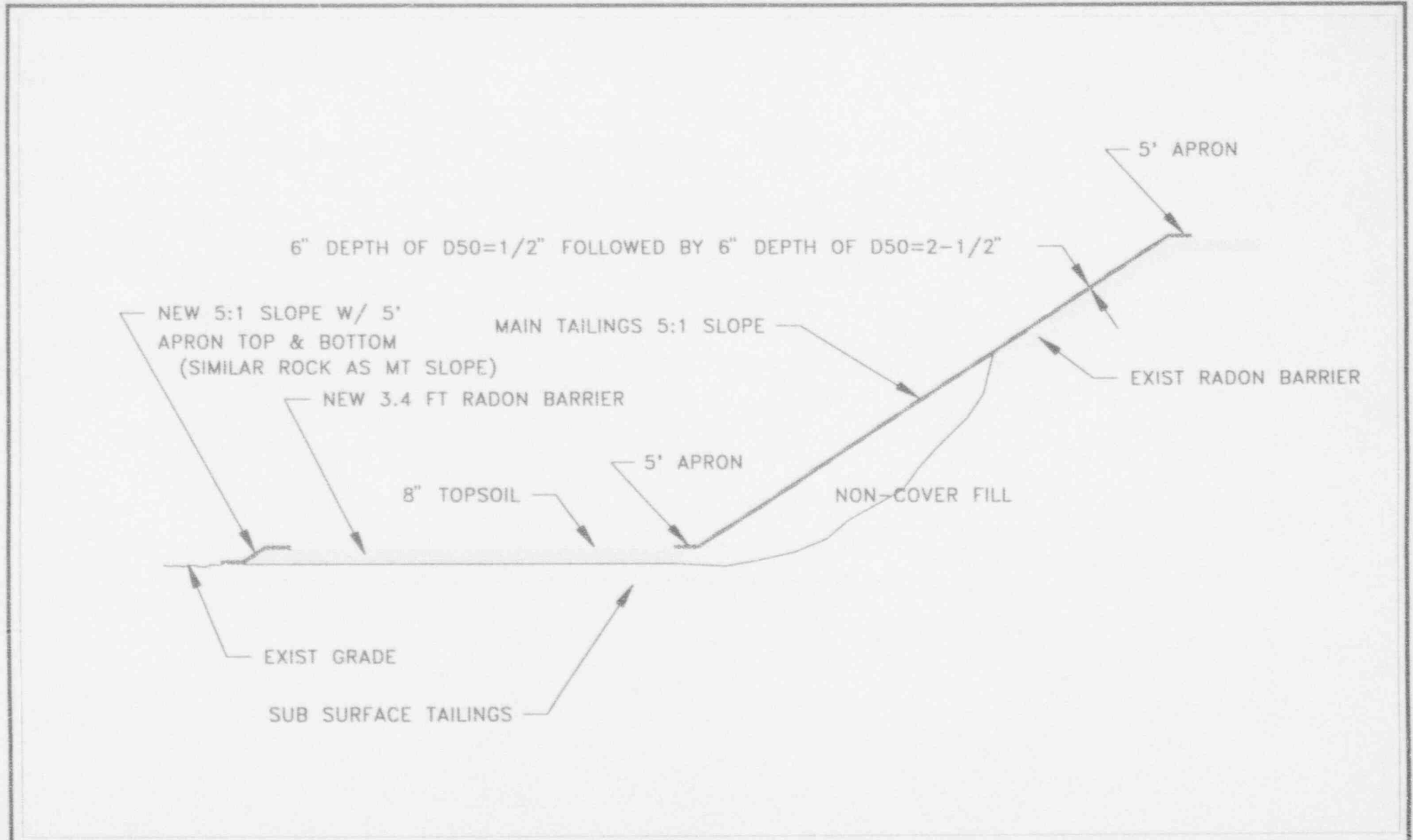
DATE	1/23/82
BY	J. J. ...
CHECKED BY	...
SCALE	AS SHOWN
PROJECT NO.	...
DRAWING NO.	...



FIGURE 2.2
DESIGN CONFIGURATION
SOUTH BENCH

ANDERSON ENGINEERING U.S., INC.
1234 Main St.
City, State, Zip
Tel: (800) 555-1234 Fax: (800) 555-1234
CIVIL ENGINEERS CONSTRUCTION MANAGERS

NO.	DATE	REVISION



6" DEPTH OF D50=1/2" FOLLOWED BY 6" DEPTH OF D50=2-1/2"

NEW 5:1 SLOPE W/ 5'
APRON TOP & BOTTOM
(SIMILAR ROCK AS MT SLOPE)

MAIN TAILINGS 5:1 SLOPE

NEW 3.4 FT RADON BARRIER

EXIST RADON BARRIER

5' APRON

8" TOPSOIL

5' APRON

NON-COVER FILL

EXIST GRADE

SUB SURFACE TAILINGS

NO.	REVISION	BY	DATE	APPROVED	DATE


ANDERSON ENGINEERING CO., INC.
 Eng. Office: 1000 N. Main St., Suite 1000, Anaheim, CA 92701
 Phone: (714) 771-0448 Fax: (714) 771-7909
 CIVIL ENGINEERS CONSTRUCTION MANAGERS

FIGURE 2.3
 TYPICAL CROSS SECTION
 SOUTH BENCH

ATLANTIC RICEFIELD COMPANY


DATE	01/01/01
PROJECT	SA
LOCATION	CS
DATE	11/03
SCALE	MTS
DATE	MTS
DATE	MTS
DATE	

3.0 SLOPE DESIGN MODIFICATION - NORTHEAST MAIN TAILINGS IMPOUNDMENT

3.1 Introduction

ARCO proposes to modify the Main Tailings Impoundment slope design contained in the 1990 Reclamation Plan between stations 75+00 and 86+00. (Figure 3.1) The 30 inch El Paso Natural Gas pipeline is to be relocated away from the present toe of the Main Tailings Impoundment at this location. The slope along the El Paso Natural Gas pipeline will be a cut and fill operation and extend over the former location of the El Paso right-of-way.

3.2 Slope Design

The slope will be modified from the 1990 Reclamation Plan to reduce the quantity of material excavated due to removal of the gas pipeline as shown on Figure 3.2. With no constraint on the slope toe from the El Paso right-of-way less cut is required to construct the reduced slope. The reclaimed slope geometry will remain 5 horizontal to 1 vertical. The slope geotechnical stability will be enhanced because of less cut into the tailings impoundment and will be similar to that of the Main Tailings slopes with cut/fill type construction. Slope geotechnical analysis of this area completed for the 1990 Reclamation Plan indicates the slope is stable under static and pseudo- static conditions.

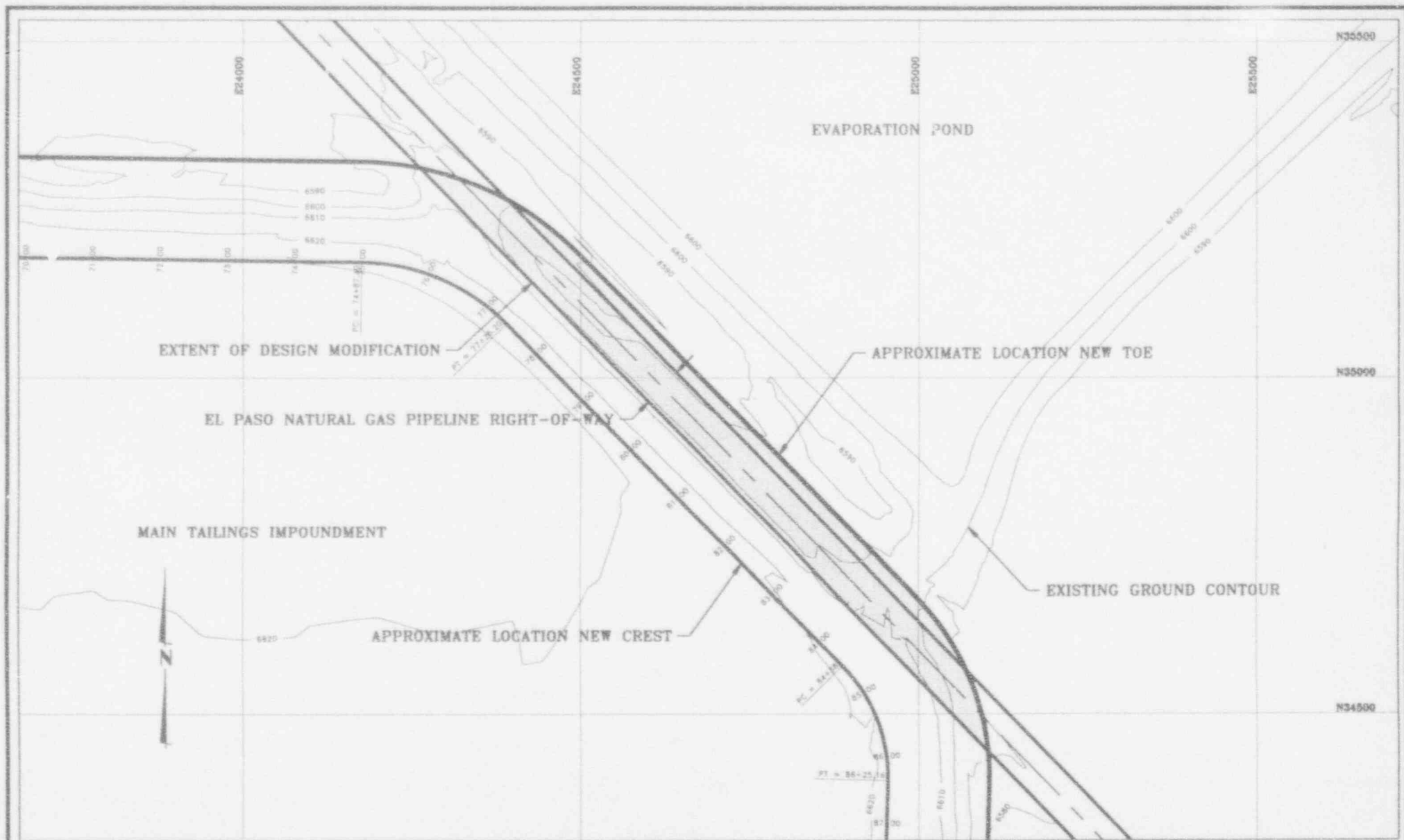
3.3 Construction

Removal of material at the upper portion of the slope will consist of sand tailings and embankment soil. This material will be excavated and placed onto the Acid Tailings Impoundment and compacted to 95% of Maximum Dry Density (MDD) in compliance with Reclamation Plan specifications. The fill material at the slope toe will be soils obtained from the borrow site or the evaporation pond dikes, and compacted to 95% MDD. Radon barrier is to be constructed over the tailings exposed by excavation. The depth of radon barrier is to be 1.4 feet which meets specifications for the sand tailings proposed in ARCO's Final Radon Barrier Design

Report - December 1993. Figure 3.2 shows detail of the slope construction.

3.4 Erosion Protection

The slope will be protected by a rock cover similar to the slope spillway areas of the Main Tailings Impoundment. A 6 inch deep filter consisting of $d_{50} = 1/2$ inch rock will be placed over the radon barrier. A 12 inch deep rip-rap cover will be constructed over the filter with $d_{50} = 5$ -inch rock. A protective apron of the same slope rock protection will be extended 10 feet at the toe of the slope and ten feet at the crest.



NO.	REVISION	DATE	BY	REVISION


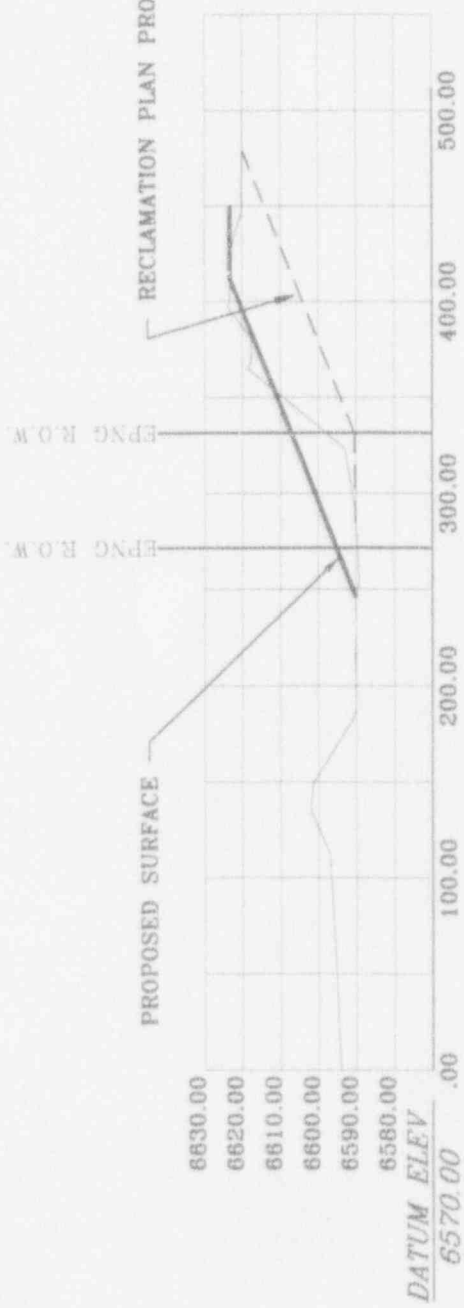

ANDERSON ENGINEERING CO., INC.
 Long Beach, California Salt Lake City, Utah Denver, New Mexico
 Telephone (801) 751-4388 Fax (801) 751-1010
 CIVIL ENGINEERS CONSTRUCTION MANAGERS

FIGURE 3.1
MAIN TAILINGS IMPOUNDMENT
DESIGN MODIFICATION

ATLANTIC REEFIELD COMPANY


DATE: 01/97
PROJECT: CA
APPRAISAL: CS
DATE: 12/20/93
NO. OF SHEETS: 11
SHEET NO.: 04
APPRAISAL:

RECLAMATION PLAN PROPOSED SURFACE



DATUM ELEV 6570.00
 GROUP M-TAILS
 SECTION NORTH

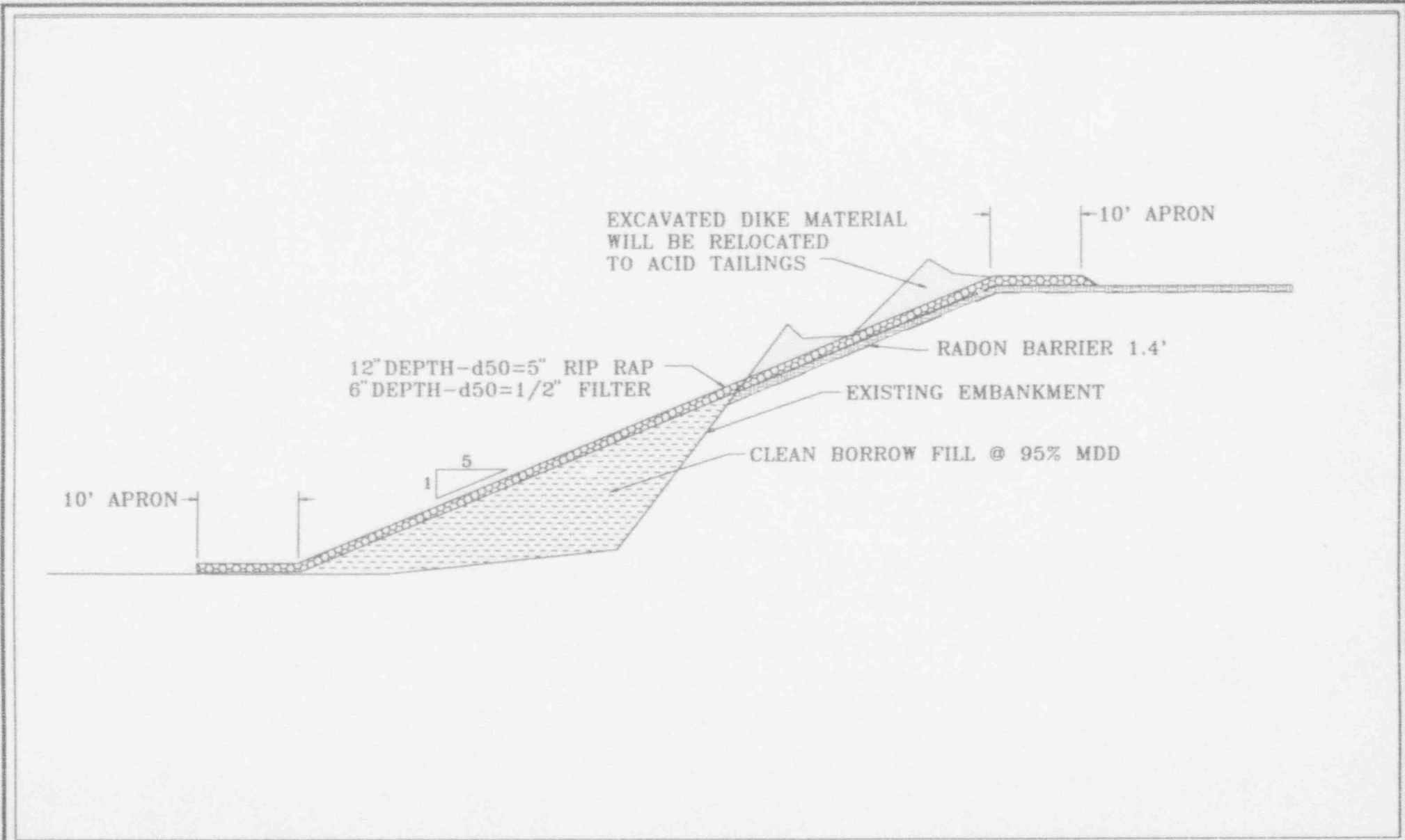
DATE	12/22/91
PROJECT	157-22-01
DRAWN BY	J. W. BIRD
CHECKED BY	T. W. BIRD



FIGURE 3-2
 MAIN TAILINGS IMPOUNDMENT
 TYPICAL SECTION

ANDERSON ENGINEERING CO., INC.
 725 Main Street
 Suite 2000 EN
 New York, NY 10002
 Telephone (212) 751-6000 Fax (212) 751-7618
 CIVIL ENGINEERS CONSULTATION SERVICES

NO.	DATE	REVISION



NO.	REVISION	BY	DATE	DESCRIPTION

ANDERSON ENGINEERING CO., INC.
 Long Beach, California Salt Lake City, Utah Omaha, Nebraska
 Telephone (801) 731-4766 Fax (801) 731-7808
 CIVIL ENGINEERS CONSTRUCTION MANAGERS

**CROSS-SECTION
SLOPE MODIFICATION
MAIN TAILINGS IMPOUNDMENT
FIGURE 3.3**

ATLANTIC RECYCLED COMPANY
 RECYCLED FILL

Drawn by	BT
Checked by	SA
Approved by	CS
Date	12/93
Scale	AS IS
Sheet No.	MTS
Project No.	

4.0 ROCK SPECIFICATIONS - QUARRY AND SCORING CRITERIA

4.1 Introduction:

The source of rock to be used for erosion protection at the Bluewater Mill has been changed from an onsite quarry to a quarry located approximately three miles east of the site on property owned by Homestake Mining Company.

ARCO is requesting that the rock material specifications be based on the Nuclear Regulatory Commission (NRC) total scoring criteria rather than individual hardness characteristic test results. This scoring criteria is to be applied to all rock products regardless of quarry location.

ARCO is also clarifying specifications for quality control of the soil/rock matrix to be used for erosion protection on the Main Tailings and the Carbonate Tailings Impoundments.

4.2 Rock Quarry

The new rock quarry is a high quality igneous rock from a local basalt flow. The preliminary in-place testing indicates the rock possesses the same properties as those of the ARCO proposed quarry as previously submitted in the Reclamation Plan. The averages for rock quality scoring from the new quarry site are shown on Table 4.1.

Rock testing from the new quarry indicates that from about 5 feet below the surface an overall score of greater than 80 can be met, which is more than adequate for the Bluewater Mill erosion protection products.

4.3 Specifications

Rock to be used for erosion protection must meet a minimum overall score of 65 for the $d_{50}=1.5$ inch, and $d_{50}=2.0$ inch products. The minimum score for the $d_{50}=5$ inch rock shall be 66 and a minimum score of 72 for the $d_{50}=2.5$ inch rock products. All

scoring will be derived in accordance with the Nuclear Regulatory Commission Final Staff Technical Position, Design of Erosion Protection Covers for Stabilization of Uranium Mill Tailings Sites, August 1990. The test series will consist of Specific Gravity, Absorption, L. A. Abrasion (100 revolutions), Na_2SO_4 Soundness and Tensile Strength to determine the scoring of the erosion protection rock.

Table 4.2 describes the erosion protection rock size and minimum scoring for the respective reclaimed areas. Rock sizing calculations and gradations for each reclaimed area are shown in Appendix B to the 1990 Reclamation Plan and subsequent amendments. The test series indicated above and gradation tests shall be performed on the material at the crusher. For each gradation specified, tests will be made at 10,000 cy intervals or at a minimum of three times during production. The initial test shall be made prior to transportation of any material from the crusher. Where the quantity of a specific size material to be produced is less than 10,000 cy, one test series shall be completed at the beginning, approximately half-way through the run and one near the end.

4.4 Soil Rock Matrix Specifications

The soil/rock matrix is to be placed onto the top surface of the Main Tailings Impoundment and the Carbonate Tailings Impoundment as described in ARCO's approved Reclamation Plan. The following criteria and sequence will be utilized to evaluate the construction of the soil rock matrix.

1. Place rock onto the radon barrier surface at about two times (2x) the rock d_{50} .
2. Rock shall be visually inspected during placement for uniformity and proper gradation. Areas which indicate segregation shall be reworked to comply with specification requirements. Random gradation tests will be conducted to verify visual appraisals.
3. Place soil over rock at approximately four to six inches in depth.

4. Mix soil and rock by use of scarification equipment (example: disc or closely spaced small rippers). The scarification is to be in three directions; one 90° to the other and the third pass is to be at 45° and bisect the first two passes. Care will be taken to prevent disruption of the underlying radon barrier.
5. Soil and rock will be roller packed with a minimum of three passes to consolidate the soil and rock bed.
6. The soil rock matrix will be field tested for depth by use of the grid described in the approved Reclamation Plan. Measurements of rock, and soil depths will be made from test holes. One depth test hole will be taken for every 200,000 square feet.
7. Revegetation of the top surface soil/rock matrix will be performed following the procedures contained in the approved 1990 Reclamation Plan.

TABLE 4.1

ROCK QUALITY SCORING
HOMESTAKE'S MALPAIS BASALT QUARRY SITE (NE 1/4, 28/T12N/R10W)

Sample Rock Type Weighting Factor (WF)/Test Value (TV) / Score for:
 Number(1 = igneous)





	Specific Gravity g/cc	Absorption %	Sulfate Soundness % Loss	LA Abrasion % Loss	Schmidt Hammer SRU	Tensile Strength psi	
Averages For All Tested Samples							
Numbers of Samples tested =	21.00	21.00	21.00	9.00	3.00	12.00	
TV =	2.65	1.84	0.93	38.40	52.40	1111.00	
Score =	8.06	3.48	9.83	0.00	6.70	8.52	
Rating =	72.51	6.97	108.16	0.00	20.20	85.20	Rock Source Composite Rating, %, Using All
Maximum possible rating (MPR) =	90.00	20.00	110.0	10.00	30.00	100.00	Rock From 0' to 30' =
Rating in % MPR =	80.56	34.83	98.33	0.00	67.21	85.20	81.4
Averages For All Samples Below Highly Vesicular Zone(0'-5')							
Numbers of Samples tested =	17.00	17.00	17.00	9.00	3.00	12.00	
TV =	2.71	1.67	0.90	38.40	52.40	1111.00	
Score =	9.28	3.87	9.82	0.00	6.70	8.52	
Rating =	83.50	7.74	107.98	0.00	20.20	85.20	Rock Source Composite Rating, %, Using Only
Maximum possible rating (MPR) =	90.00	20.00	110.00	10.00	30.00	100.00	Rock From 5' to 30' =
Rating in % MPR =	92.78	38.68	98.17	0.00	67.21	85.20	84.6

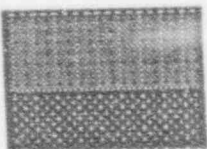
TABLE 4.2
EROSION PROTECTION ROCK SCORE

	Rock Size d_{50}		Minimum Quality Score * ²
	Minimum Design * ¹	Reclamation Plan	
Main Tailings			
Top Surface (North)	0.5"	1.5"	65
Top Surface (South)	0.5"	2.0"	65
Slopes	2.0"	2.5"	65
Spillway	4.3"	5.0"	66
Carbonate Tailings			
Top Surface	.05"	1.5"	65
Slopes	2.3"	2.5"	72
Acid Tailings			
Slopes	0.5"	1.5"	65
Stockpile			
Slopes	0.5"	1.5"	65

¹* Corp. of Engineers Method for Top Surface, Stephenson Method for Slopes




²* Minimum 65 score is required for critical areas, NRC 1990

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE #	13-2
0	0.4		COVER MATERIAL	
1	0.7		TAILINGS	
2	1.0		NATIVE SOIL	
3			MALPAIS	
4				
5				
6				
7				
8				
9				

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE #	14-2
0	1.0 	TRACE TAILINGS		
1		NATIVE SOIL		
2		MALPAIS		
3				
4				
5				
6				
7				
8				
9				

POTHOLE LOG

CARBONATE TAILINGS BOUNDARY INVESTIGATION

DEPTH	SYMBOL	DESCRIPTION	HOLE # 17-2
0	0.2		COVER MATERIAL
	0.5		TAILINGS
1		MALPAIS	
2			
3			
4			
5			
6			
7			
8			
9			

POTHOLE LOG

CARBONATE TAILINGS BOUNDARY INVESTIGATION

DEPTH	SYMBOL	DESCRIPTION	HOLE # 19-R
0	0.2		
0	0.2		
1	2.1	NATIVE SOILS	
2			
3		MALPAIS	
4			
5			
6			
7			
8			
9			

POTHOLE LOG

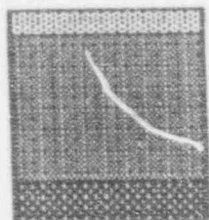
CARBONATE TAILINGS BOUNDARY INVESTIGATION

DEPTH		SYMBOL	DESCRIPTION	HOLE #
0	.04		COVER MATERIAL	22-2
1	.07		TAILINGS	
2	2.0		NATIVE SOIL	
3			MALPAIS	
4				
5				
6				
7				
8				
9				

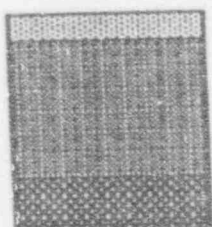
POTHOLE LOG

CARBONATE TAILINGS BOUNDARY INVESTIGATION

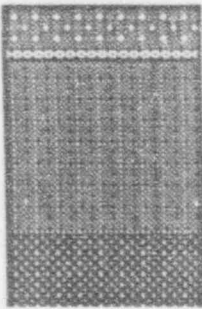
DEPTH	SYMBOL	DESCRIPTION	HOLE #
			23-2
0	0.4	TAILINGS	
1	1.5	NATIVE SOIL	
2		MALPAIS	
3			
4			
5			
6			
7			
8			
9			

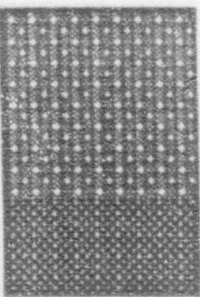


POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 24-2
0	0.4	TAILINGS	
1	1.5	NATIVE SOIL	
2		MALPAIS	
3			
4			
5			
6			
7			
8			
9			



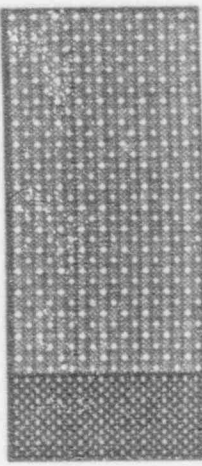
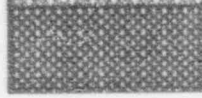
POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE #	28-2
0	0.4		COVER MATERIAL	
1	0.7		TAILINGS	
2	1.4		NATIVE SOIL	
3			MALPAIS	
4				
5				
6				
7				
8				
9				


POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE # 29-2	
0	0.4		COVER MATERIAL TRACE TAILINGS	
1	1.0		NATIVE SOIL	
2		MALPAIS		
3				
4				

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE #	30-2
0		COVER MATERIAL		
1.0				
1		MALPAIS		
2				
3				
4				

POTHOLE LOG

CARBONATE TAILINGS BOUNDARY INVESTIGATION

DEPTH	SYMBOL	DESCRIPTION	HOLE #
0		TRACE TAILINGS ON SURFACE	32-2
1 2.0		NATIVE SOIL	
2		MALPAIS	
3			
4			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE # 36-2	
0	0.4	COVER MATERIAL TAILINGS		
	0.2			
1		NATIVE SOIL		
	2.5			
2		MALPAIS		
	3			
4				

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 38-2
0	0.3	COVER MATERIAL	
	0.5	TAILINGS	
1			
	2.0	NATIVE SOIL	
2			
	3	MALPAIS	
3			
4			



POTHOLE LOG

CARBONATE TAILINGS BOUNDARY INVESTIGATION

DEPTH

SYMBOL

DESCRIPTION

HOLE # 39-2

0

0.3



COVER MATERIAL

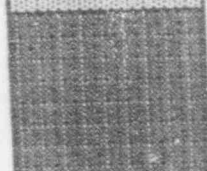
0.3



TAILINGS

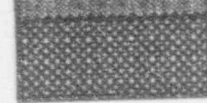
1

1.0



NATIVE SOIL

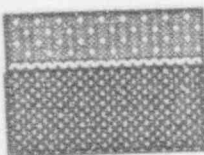
2

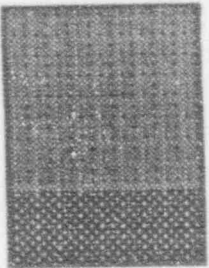


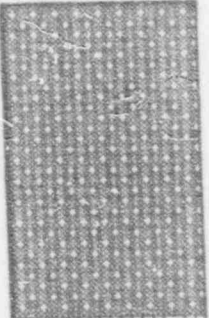

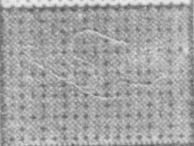

MALPAIS


3

4

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 43-2
0	0.4	 COVER MATERIAL TAILINGS - TRACE ATOP ROCK MALPAIS	
1			
2			
3			
4			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE #	45-2
0		COVER MATERIAL		
1.0				
1		MALPAIS		
2				
3				
4				

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 49-2 R
0		COVER MATERIAL	
1			
2			4.1
3			
4		TAILINGS	
5			1.1
6		NATIVE SOIL	
7			1.7
8			
9		MALPAIS	

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE #	50-2
0	0.4		HARD CLAY - BACKHOE REFUSED	
1				
2				
3				
4				

POTHOLE LOG CARBONATE TAILINGS BOUNDARY INVESTIGATION

HOLE # 52-2

DEPTH

SYMBOL

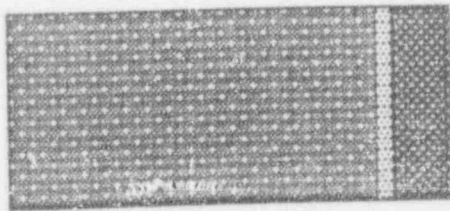
0

1 2.0

2 <0.1

3

4

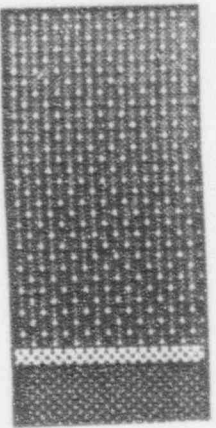


COVER MATERIAL

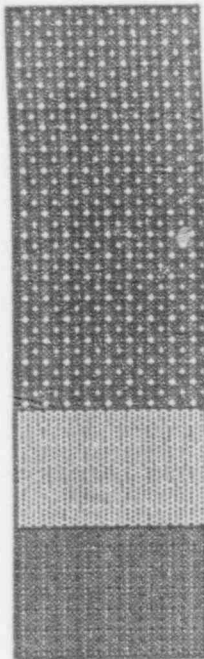
TAILINGS - THIN LENS
MALPAIS

POTHOLE LOG

CARBONATE TAILINGS BOUNDARY INVESTIGATION

DEPTH	SYMBOL	DESCRIPTION	HOLE # 54-2
0			
1			
2 4.0			COVER MATERIAL
3			
4			
5		TAILINGS MALPAIS	
6			
7			
8			
9			

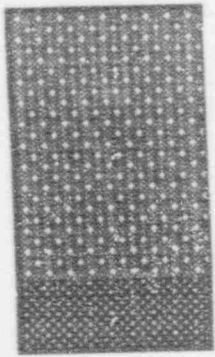
POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE #	56-2
0		COVER MATERIAL		
1				
2				
3	0.4	TAILINGS MALPAIS		
4				
5				

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE #	59-R
0		COVER MATERIAL		
1				
3.0				
2				
3				
3.9				
4				
4.9				
5				
		TAILINGS		
		NATIVE SOILS		

POTHOLE LOG

CARBONATE TAILINGS BOUNDARY INVESTIGATION

DEPTH	SYMBOL	DESCRIPTION	HOLE #
0		COVER MATERIAL	60-R
1	2.2		
2	0.4	TAILINGS	
3	0.8	NATIVE SOILS	
4		MALPAIS	
5			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 62-2
0		COVER MATERIAL	
1 2.0			
2		MALPAIS	
3			
4			
5			

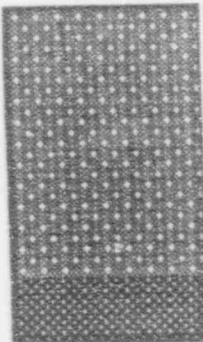
POTHOLE LOG

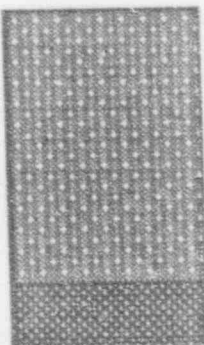
CARBONATE TAILINGS BOUNDARY INVESTIGATION

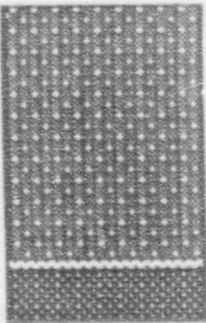

DEPTH	SYMBOL	DESCRIPTION	HOLE # 64-2
0		COVER MATERIAL	
5.0		MALPAIS	

POTHOLE LOG

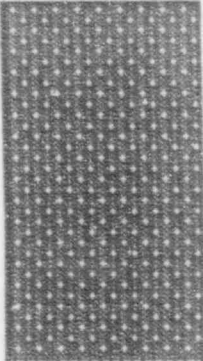
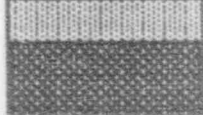

CARBONATE TAILINGS BOUNDARY INVESTIGATION

DEPTH	SYMBOL	DESCRIPTION	HOLE # 67-2
0		COVER MATERIAL	
1 2.0		MALPAIS	
2			
3			
4			
5			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE #	68-2
0		COVER MATERIAL		
1 2.0		MALPAIS		
2				
3				
4				
5				




POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 74-2
0		COVER MATERIAL	
1			
2			3.0
3		TAILINGS MALPAIS	
4			0.1
5			
6			
7			
8			
9			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 75-2
0		COVER MATERIAL	
1.0		TAILINGS	
1		NATIVE SOIL	
1.0			
2			
3			
4			
5			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 76-2
0		COVER MATERIAL	
1			
2.5		TAILINGS	
3			
0.3			
4		MALPAIS	
5			

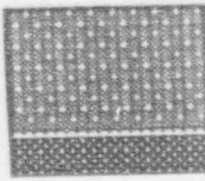

POTHOLE LOG

CARBONATE TAILINGS BOUNDARY INVESTIGATION

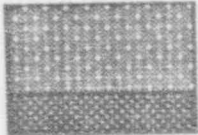
DEPTH	SYMBOL	DESCRIPTION	HOLE #	83-2
0				
1.0		COVER MATERIAL		
1				
0.2		TAILINGS		
2		MALPAIS		
3				
4				
5				
6				
7				
8				
9				

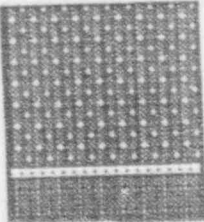
POTHOLE LOG

CARBONATE TAILINGS BOUNDARY INVESTIGATION

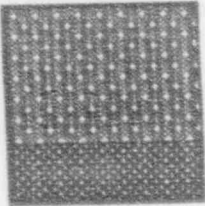
DEPTH	SYMBOL	DESCRIPTION	HOLE # 8/1-2
0		COVER MATERIAL	
1		TAILINGS (TRACE)	
2		MALPAIS	
3			
4			
5			
6			
7			
8			
9			

1.5

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 85-2
0		COVER MATERIAL	
1		MALPAIS	
2			
3			
4			
5			
6			
7			
8			
9			




POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE #	86-2
0		COVER MATERIAL		
1 2.0				
2 0.1		TAILINGS NATIVE SOIL		
3				
4				
5				
6				
7				
8				
9				

POTHOLE LOG		CARBONATE TAILS BOUNDARY INVESTIGATION INFO	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 87 -2
0	1.0	COVER MATERIAL	
1	1.0	TAILINGS	
2	1.0	NATIVE SOIL	
3	1.0	MALPAIS	
4			
5			
6			
7			
8			
9			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 109-2
0		COVER MATERIAL	
1.0		MALPAIS	
1			
2			
3			
4			
5			

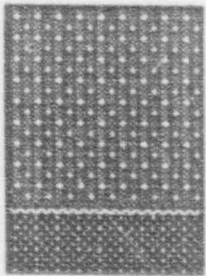
POTHOLE LOG

CARBONATE TAILS BOUNDARY INVESTIGATION INFO

DEPTH	SYMBOL	DESCRIPTION	HOLE # 110-2
0			
1.2		COVER MATERIAL	
1		TAILINGS	
0.3		MALPAIS	
2			
3			
4			
5			
6			
7			
8			
9			

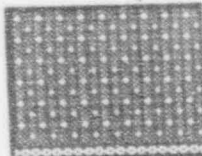
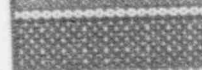
POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 111-2
0		COVER MATERIAL	
1.0		TAILINGS	
1		MALPAIS	
2			
3			
4			
5			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 115-2
0		COVER MATERIAL	
1.2		TAILINGS	
1		MALPAIS	
0.5			
2			
3			
4			
5			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE #	117-2
0		COVER MATERIAL		
1.5		TRACE TAILINGS MALPAIS		
2				
3				
4				
5				

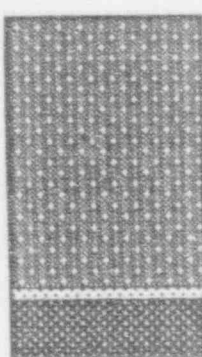
POTHOLE LOG

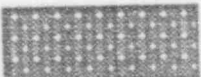

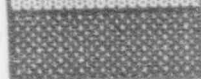
CARBONATE TAILINGS BOUNDARY INVESTIGATION

DEPTH	SYMBOL	DESCRIPTION	HOLE # 121-2
0			
1.0		COVER MATERIAL	
1		TRACE TAILINGS MALPAIS	
2			
3			
4			
5			

POTHOLE LOG

CARBONATE TAILINGS BOUNDARY INVESTIGATION

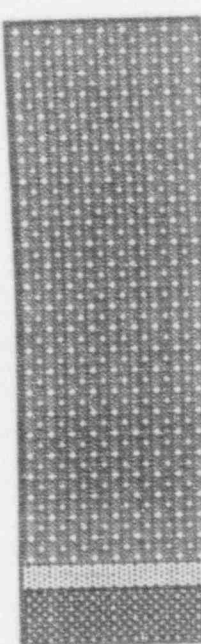
DEPTH	SYMBOL	DESCRIPTION	HOLE # 123-2
0		COVER MATERIAL	
1 2.0		TRACE TAILINGS MALPAIS	
2			
3			
4			
5			

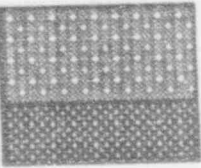
POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 124-2
0	0.5	 COVER MATERIAL	
1	0.5	 TAILINGS	
		 MALPAIS	
2			
3			
4			
5			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 125-2
0		COVER MATERIAL	
1.0		TAILINGS	
2.0		MALPAIS	
3			
4			
5			

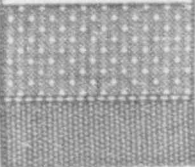
POTHOLE LOG

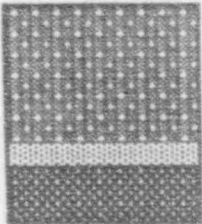
CARBONATE TAILINGS BOUNDARY INVESTIGATION

DEPTH	SYMBOL	DESCRIPTION	HOLE # 127-2
0		<p data-bbox="645 606 963 657">COVER MATERIAL</p> <p data-bbox="660 905 828 990">TAILINGS MALPAIS</p>	
1			
2 4.0			
3			
4 0.2			
5			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 128-2
0		COVER MATERIAL	
0.6		MALPAIS	
1			
2			
3			
4			
5			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 129-2
0	0.5	COVER MATERIAL TAILINGS	
	0.2		
1		MALPAIS	
2			
3			
4			
5			




POTHOLE LOG		CARBONATE TAILS BOUNDARY INVESTIGATION INFO	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 130 -2
0		COVER MATERIAL TRACE TAILINGS MALPAIS	
1			
2			
3			
4			
5			
6			
7			
8			
9			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 132-2
0		COVER MATERIAL	
1.0			
1		TAILINGS	
		MALPAIS	
2			
3			
4			
5			

POTHOLE LOG		CARBONATE TAILS BOUNDARY INVESTIGATION INFO	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 134 -2
0			
1	2.0	COVER MATERIAL	
2	1.0	TAILINGS	
3		MALPAIS	
4			
5			
6			
7			
8			
9			

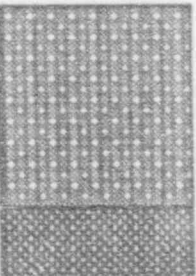
POTHOLE LOG

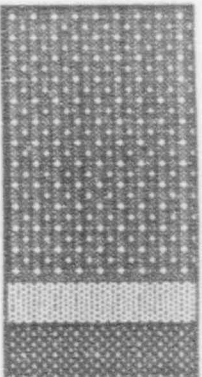
CARBONATE TAILINGS BOUNDARY INVESTIGATION

DEPTH	SYMBOL	DESCRIPTION	HOLE # 135-2
0			
1.0		COVER MATERIAL	
1		TRACE TAILINGS	
		MALPAIS	
2			
3			
4			
5			

POTHOLE LOG



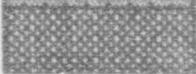

CARBONATE TAILINGS BOUNDARY INVESTIGATION

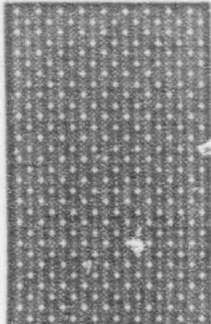

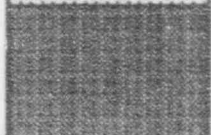
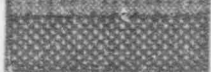
DEPTH	SYMBOL	DESCRIPTION	HOLE # 136-2
0			
1		COVER MATERIAL	
1.5			
2		MALPAIS	
3			
4			
5			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE #	210-2
0		COVER MATERIAL		
1 2.0				
2	0.4	TAILINGS MALPAIS		
3				
4				
5				

POTHOLE LOG

CARBONATE TAILINGS BOUNDARY INVESTIGATION

DEPTH	SYMBOL	DESCRIPTION	HOLE # 235
0	1.0		TRACE OF TAILINGS
1	0.5		COVER MATERIAL
2		NATIVE SOIL	
3		MALPAIS	
4			
5			
6			
7			
8			
9			

PC LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 237
0		COVER MATERIAL	
1			
2 4.0			
3			
4		TAILINGS	
5 1.0			
6 2.0		NATIVE SOIL	
7			
8		MALPAIS	
9			

POTHOLE LOG

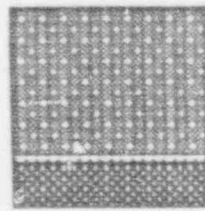
CARBONATE TAILINGS BOUNDARY INVESTIGATION

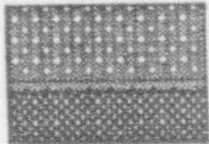
DEPTH	SYMBOL	DESCRIPTION	HOLE # 238
0			
1	1.5	COVER MATERIAL	
2		TRACE TAILINGS	
3		MALPAIS	
4			
5			
6			
7			
8			
9			

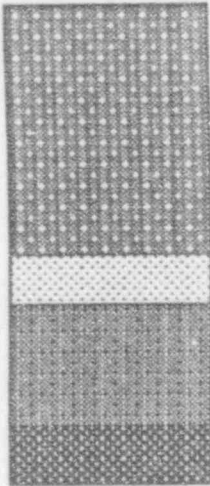
POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 239
0			
1	1.8	COVER MATERIAL TRACE TAILINGS NATIVE SOIL MALPAIS	
2	0.3		
3			
4			
5			
6			
7			
8			
9			

POTHOLE LOG

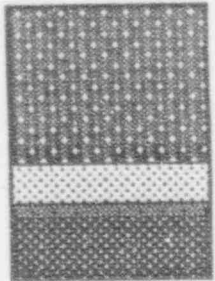
CARBONATE TAILINGS BOUNDARY INVESTIGATION

DEPTH	SYMBOL	DESCRIPTION	HOLE # 240
0		COVER MATERIAL	
1		1.8	
2		TAILINGS MALPAIS	
3			
4			
5			
6			
7			
8			
9			

POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION		
DEPTH	SYMBOL	DESCRIPTION	HOLE #	241
0	1.0		COVER MATERIAL WITH TRACE TAILINGS	
1	0.2		NATIVE SOIL MALPAIS	
2				
3				
4				
5				
6				
7				
8				
9				

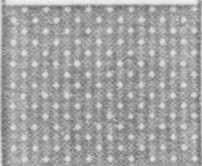




POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 242
0		COVER MATERIAL	
1			
2		3.0	
3			
4	0.7	TAILINGS	
5	1.5	NATIVE SOIL	
6		MALPAIS	
7			
8			
9			

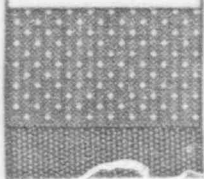
POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 243
0			
1	2.0	COVER MATERIAL	
2	0.4	TAILINGS	
3	0.2	NATIVE SOIL	
		MALPAIS	
4			
5			
6			
7			
8			
9			

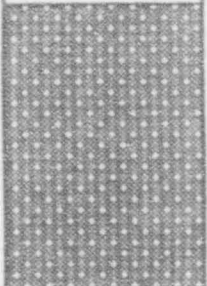




POTHOLE LOG

CARBONATE TAILS BOUNDARY INVESTIGATION INFO

DEPTH		SYMBOL	DESCRIPTION	HOLE # 244
0				
1	2.0		COVER MATERIAL	
2	0.3		CLAY	
	0.5		TAILING SANDS	
3	0.3		NATIVE SOILS	
4				
			MALPAIS	
5				
6				
7				
8				
9				





POTHOLE LOG		CARBONATE TAILS BOUNDARY INVESTIGATION INFO	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 246
0			
1		NATIVE SOILS	
2		MALPAIS	
3			
4			
5			
6			
7			
8			
9			

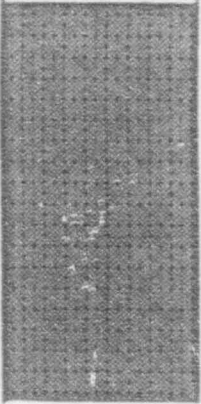
POTHOLE LOG		CARBONATE TAILS BOUNDARY INVESTIGATION INFO	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 247
0		COVER MATERIAL	
1			
2			3.5
3		TAILING SANDS	
4			0.5
5		MALPAIS	
6			
7			
8			
9			

POTHOLE LOG		CARBONATE TAILS BOUNDARY INVESTIGATION INFO		
DEPTH	SYMBOL	DESCRIPTION	HOLE # 248	
0		COVER MATERIAL		
1				
2				4.0
3				
4	0.5	TAILING SANDS		
5		MALPAIS		
6				
7				
8				
9				





POTHOLE LOG		CARBONATE TAILINGS BOUNDARY INVESTIGATION	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 249
0		COVER MATERIAL	
1 2.0			
2 0.6		TAILINGS SANDS	
3		MALPAIS	
4			
5			
6			
7			
8			
9			

POTHOLE LOG		CARBONATE TAILS BOUNDARY INVESTIGATION INFO	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 250
0			
1	1.5	COVER MATERIAL	
2	0.3	TAILING SANDS	
3	2.0	NATIVE SOILS	
4		MALPAIS	
5			
6			
7			
8			
9			

POTHOLE LOG		CARBONATE TAILS BOUNDARY INVESTIGATION INFO		
DEPTH	SYMBOL	DESCRIPTION	HOLE # 251	
0	0.6		COVER MATERIAL	
1	0.3		TAILING SANDS	
2	1.1		NATIVE SOILS	
3			MALPAIS	
4				
5				
6				
7				
8				
9				

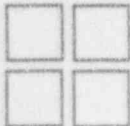
POTHOLE LOG		CARBONATE TAILS BOUNDARY INVESTIGATION INFO		
DEPTH	SYMBOL	DESCRIPTION	HOLE # 253	
0				
1				
2				
3		5.0	CLAY - STOPPED DIGGING @ 5.0' DUE TO EXTREME DENSITY	
4				
5				
6				
7				
8				
9				

POTHOLE LOG		CARBONATE TAILS BOUNDARY INVESTIGATION INFO	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 254
0			
1	2.0	COVER MATERIAL	
2			
3	1.0	NATIVE SOILS	
4		MALPAIS	
5			
6			
7			
8			
9			

POTHOLE LOG		CARBONATE TAILS BOUNDARY INVESTIGATION INFO	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 255
0			
1.0		COVER MATERIAL	
0.3		TAILING SANDS	
1.5		NATIVE SOILS	
3		MALPAIS	
4			
5			
6			
7			
8			
9			

POTHOLE LOG		CARBONATE TAILS BOUNDARY INVESTIGATION INFO	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 256
0			
1	2.0	NATIVE SOILS	
2			
3		MALPAIS	
4			
5			
6			
7			
8			
9			

POTHOLE LOG		CARBONATE TAILS BOUNDARY INVESTIGATION INFO	
DEPTH	SYMBOL	DESCRIPTION	HOLE # 257
0			
1	2.0	LOOSE COVER MATERIAL	
2		TRACE TAILINGS	
3	1.0	HARD CLAY - BACKHOE REFUSED	
4			
5			
6			
7			
8			
9			



ANDERSON Engineering Company, Inc.
4655 South 1900 West St.
Roy, Utah 84067
Telephone 801-731-4596

Southwest Office
P.O. Box 2
Grants, New Mexico 87020

Long Beach Office
231-428-9344

Engineers
Construction Managers

CALCULATION SHEET

JOB Blenkaton SHEET NO. _____ CALC JA

CK'D BY _____ DATE 12/22/93 TITLE DA#2 Source Term

Disposal Area #2
Endemic Activity Calculation

Waston 11/87 Report

$$\text{Calc P+2} \quad R_a - 224 (C_i) = 0.248 = 248(10^9) = \text{pCi}$$

$$\text{Area} \approx 260,000 \text{ ft}^2$$

$$5' \text{ debris} \quad 5(260,000) = 1,300,000 \text{ ft}^3$$

$$2' \text{ debris} \quad 2(260,000) = 520,000 \text{ ft}^3$$

$$= 1.82(10^6) \text{ ft}^3$$

$$= 1.68(42.4)(1.82(10^6)) = 190.8(10^6) \text{ lb}$$

$$= \frac{190.8(10^6) \text{ lb}(453.6 \text{ g})}{16} = 54.6(10^9) \text{ gm}$$

sp grav 1.48

$$\frac{248(10^9) \text{ pCi}}{54.6(10^9) \text{ gm}} = 2.86 \frac{\text{pCi}}{\text{gm}}$$

TABLE 6-1

SOIL AND RADON SOURCE REGIONS AND
THEIR DEFINING PARAMETERS

Region	Effective ^a Present Source Thickness (feet)	Average ^b Radium Concentration (pCi/gram)	Average Radon Emanation Fraction	Average Long-Term Moisture (% dry wt)	Average Radon Diffusion Coefficient (cm ² /s)	<i>dens.</i>
Borrow Soil	---	2.7	---	9.5	0.018	1.84
Main Tailings-Sands	40	103-409	.20	8.0	0.025	
Main Tailings-Mixed	15	242-538	.24	15.0	0.0085	
Main Tailings-Slimes	9	424-522	.20	22.0	0.0011	
Old Acid Tailings	4.7	2023-2214	.24	20.0	0.0010	1.50
East Carbonate T.	10	1030-1601	.30	20.0	0.0025	
West Carbonate T.	7	415-921				
South Carbonate T.	5	1963				
Evap. Ponds	.2-2	37-345	.17	9.5	0.0195	
Stockpile Area	1	53	.41	9.5	0.036	
Mill Area	7	22	.41	10.0	0.0164	
Windblown (W-1 & W-2)	.5-4	34	.32	9.5	0.014	
Windblown (W-3)	1	76.	.30	9.5	0.036	

Total thickness for old acid tailings, evaporation ponds, stockpile area, and windblown areas; extent of sampling for all other areas. Ranges shown for measured, non-uniform regions.

Ranges show maximum variation in averaged vertical concentration profiles.

Table B.2 Carb Tails Pit 2 Source Term

Building	Ra-226 activity (Ci)	Th-230 activity (Ci)	Volume (m ³)
Carbonate Leach	0.05	0.062	212.6
Old Yellowcake	---	---	37.3
Acid Leach	0.01	0.113	69.5
Resin Pulp	0.18	0.40	1014.4
Counter Current	0.008	0.006	6.4
New Yellowcake	---	---	0.5
TOTAL	0.248	0.581	1340.7

RAECOBPC.BAS

22 DEC 93
TA#2

OUTPUT INFORMATION : 08:56:01 12-23-1993
 BOTTOM FLUX = 0 pCi/m²/sec
 AIR CONC. = 0 pCi/l
 BARE LAYER 1 FLUX = 276.13 pCi/m²/s
 NO OPTIMIZATION APPLIED

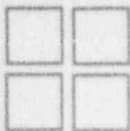
L	THICK (cm)	POR	MOIST (%)	SOURC (pCi/g)	E.F.	DENS (g/cm ³)	DIFF COEF	FLUX (pCi/m ² /s)	CONC. (pCi/cm ³)	MIC
7	50.0	.3133	9.5	1	.2	1.84	0.00753	1.94	0.0	0.587
6	61.0	.341	9.5	1	.2	1.78	0.01390	2.22	4.5	0.633
5	61.0	.37	9.5	2.86	.3	1.68	0.01900	4.52	9.3	0.681
4	61.0	.341	9.5	1	.2	1.78	0.01390	8.21	13.6	0.633
3	152.0	.37	9.5	2.86	.3	1.68	0.01900	16.63	31.1	0.681
2	73.0	.341	9.5	1	.2	1.78	0.01390	90.28	118.1	0.633
1	213.0	.411	20	921	.3	1.38	0.00250	198.77	259.8	0.503

***** TOP *****

- *- 7 -* BORROW *
-
- 6 -* BORROW *
-
- 5 -* DEBRIS *
-
- *- 4 -* BORROW *
-
- 3 -* DEBRIS *
-
- *- 2 -* BORROW *
-
- 1 -* TAILINGS *
-

***** BOTTOM *****

no cover required



ANDERSON Engineering Company, Inc.
4655 South 1900 West St.
Roy, Utah 84067
Telephone 801-731-4596

Southwest Office
P.O. Box 2
Grants, New Mexico 87020

Long Beach Office
231-428-9344

Engineers
Construction Managers

CALCULATION SHEET

JOB Plumation SHEET NO. _____ CALC EA

CK'D BY _____ DATE 12/22/93 TITLE EA#3 Source Term

Disposal Area #3

Radium Activity Calculation

Uranium Activity Calculation

Uranium 1487 Footprint

$$R_{a-226}(Ci) = 0.082 = 82(10^9) \mu Ci$$

$$\text{Area} \approx 340,000 \text{ ft}^2$$

$$5' \text{ debris } 5' (340,000 \text{ ft}^2) = 1.7(10^6) \text{ ft}^3$$

$$\text{sp grav. } 1.68 \quad 1.68(62.4) 1.7(10^6) = 178.2(10^6) \text{ ft}^3$$

$$178.2(10^6) \left(\frac{453.6 \text{ g}}{1 \text{ lb}} \right) = 80.8(10^9) \text{ g}$$

$$\frac{82(10^9) \mu Ci}{80.8(10^9) \text{ g}} = \underline{\underline{1.02 \mu Ci/g}}$$

TABLE 6-1

SOIL AND RADON SOURCE REGIONS AND
THEIR DEFINING PARAMETERS

Region	Effective ^a Present Source Thickness (feet)	Average ^b Radium Concentration (pCi/gram)	Average Radon Emanation Fraction	Average Long-Term Moisture (% dry wt)	Average Radon Diffusion Coefficient (cm ² /s)	<i>dens.</i>
Narrow Soil	---	2.7	---	9.5	0.018	1.34
Main Tailings-Sands	40	103-409	.20	8.0	0.025	
Main Tailings-Mixed	15	242-538	.24	15.0	0.0085	
Main Tailings-Slimes	9	424-522	.20	22.0	0.0011	
Old Acid Tailings	4.7	2023-2214	.24	20.0	0.0010	1.59
West Carbonate T.	10	1030-1601	.30	20.0	0.0025	
North Carbonate T.	7	415-921				
South Carbonate T.	5	1963				
Evap. Ponds	.2-2	37-345	.17	9.5	0.0195	
Stockpile Area	1	53	.41	9.5	0.036	
Hill Area	7	22	.41	10.0	0.0164	
Windblown (W-1 & W-2)	.5-4	34	.32	9.5	0.014	
Windblown (W-3)	1	76.	.30	9.5	0.036	

Total thickness for old acid tailings, evaporation ponds, stockpile area, and windblown areas; extent of sampling for all other areas. Ranges shown for measured, non-uniform regions.

Ranges show maximum variation in averaged vertical concentration profiles.

Table B.3 pH Pond Pit 3 Source Term

Building	Ra-226 activity(Ci)	Th-230 activity(Ci)	Volume (m ³)
Sand Filter	0.00014	0.009	3.5
Solvent Extraction	0.028	0.080	90.4
Storage Tanks	0.054	0.742	502.7 ^a
TOTAL	0.082	0.831	596.6

^aExcludes 924 m³ of water in the CCD storage tanks.

22 DEC 93
DA#3

OUTPUT INFORMATION : 08:48:59 12-23-1993
 BOTTOM FLUX = 0 pCi/m²/sec
 AIR CONC. = 0 pCi/l
 ARE LAYER 1 FLUX = 480.01 pCi/m²/s
 LAYER 5 ADJUSTED TO GIVE FLUX OF 20 pCi/m²/s FROM LAYER 5

L	THICK (cm)	POR	MOIST (%)	SOURC (pCi/g)	E.F.	DENS (g/cm ³)	DIFF COEF	FLUX (pCi/m ² /s)	CONC. (pCi/cm ³)	MIC
5	74.4	.3133	9.5	1	.2	1.84	0.00753	20.00	0.0	0.587
4	6.0	.341	9.5	1	.2	1.68	0.01390	36.77	88.5	0.654
3	152.4	.37	9.5	1.02	.3	1.68	0.01900	40.63	97.3	0.681
2	28.0	.375	9.5	1	.2	1.68	0.01980	273.46	382.2	0.685
1	305.0	.411	20	1501	.3	1.38	0.00250	370.06	369.2	0.503

***** TOP *****
 - 5 - * PROPOSED COVER *

 * 4 * BORROW *

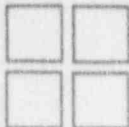
 - 3 - * DEBRIS *

 - 2 - * BORROW *

 * 1 - * TAILINGS *

 ***** BOTTOM *****

24 ft. required



ANDERSON Engineering Company, Inc.
4655 South 1900 West St.
Roy, Utah 84067
Telephone 801-731-4596

Southwest Office
P.O. Box 2
Grants, New Mexico 87020

Long Beach Office
231-428-9344

Engineers
Construction Managers

CALCULATION SHEET

JOB Blumenton SHEET NO. _____ CALC FA

CK'D BY _____ DATE 5/11/02 TITLE Coib Taila, Hydrol Calc
Surface

UNSATURATED SUBSTRAT (TYPICAL SURFACE CONDITIONS)

hydraulic length = 1200 ft.

flow is sheet flow - use unit width

$$\begin{aligned} 200(1) &= 1200 \text{ ft}^2 \\ &= 0.0275 \text{ ac} \\ &= 4.3044 (10^{-9}) \text{ mi}^2 \end{aligned}$$

use 100ft width $1200(100) = 120,000$
 $= .0043 \text{ mi}^2$

$$\text{slope} = \frac{6626 - 6610}{1200} = 1.33\%$$

$$CN = 90$$

$$\begin{aligned} S &= \frac{1000 - 10}{90} \\ &= 1.11 \end{aligned}$$

$$L = \frac{1.08 (S+1)^{0.7}}{1900 \sqrt{S}} = \frac{1200^{0.8} (1.11+1)^{0.7}}{1900 \sqrt{1.33}} = 0.22 \text{ hr}$$

initial abstraction

$$\begin{aligned} I_n &= 0.25 \\ &= 0.2(1.11) \\ &= 0.22 \end{aligned}$$

On face of Slope

Northeast Quad

```

*****
* FLOOD HYDROGRAP. PACKAGE (HEC-1) *
* FEBRUARY 1981 *
* REVISED 02 AUG 88 *
* RUN DATE 09/28/1993 TIME 15:07:56 *
*****

```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* THE HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 551-1748 *
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION. NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPJ INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM.

1

HEC-1 INPUT

PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*** FREE ***
1 ID CARBONATE TAILINGS-OPTION B-RUNOFF NORTHEAST QUAD
2 IT 3 0 0 300 0 0
3 IO 3
4 KK STG1
5 BA 0.0043
6 PH .0001 0 4.68 6.79 9.98 11.58 12.28 13.47
7 LS .22 90 0
8 UD .22
9 KK STG2
10 BA 0.0002
11 UD 0.0045

```

12 KK CM12
13 HC 2
14 ZZ

```
*****  
*  
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *  
* FEBRUARY 1981 *  
* REVISED 02 AUG 88 *  
*  
* RUN DATE 09/28/1993 TIME 15:07:56 *  
*  
*****
```

```
*****  
*  
* U.S. ARMY CORPS OF ENGINEERS *  
* THE HYDROLOGIC ENGINEERING CENTER *  
* 609 SECOND STREET *  
* DAVIS, CALIFORNIA 95616 *  
* (916) 551-1748 *  
*  
*****
```

CARBONATE TAILINGS-OPTION B-RUNOFF NORTHEAST QUAD

3 IO OUTPUT CONTROL VARIABLES

IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN 3 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 300 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 1 0 ENDING DATE
NDTIME 1457 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .05 HOURS
TOTAL TIME BASE 14.95 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

4 KK * STG1 *
 * *

SUBBASIN RUNOFF DATA

5 BA SUBBASIN CHARACTERISTICS
 TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

6 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
4.68	6.79	9.98	11.58	12.28	13.47	.00	.00	.00	.00	.00	.00

STORM AREA = .00

7 LS SCS LOSS RATE
 STRTL .22 INITIAL ABSTRACTION
 CRVNB 90.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

8 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .22 LAG

UNIT HYDROGRAPH
 24 END-OF-PERIOD ORDINATES

1.	3.	6.	8.	8.	8.	6.	4.	3.	2.
2.	1.	1.	1.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.						

HYDROGRAPH AT STATION STG1

TOTAL RAINFALL = 13.47, TOTAL LOSS = 1.25, TOTAL EXCESS = 12.22

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	14.95-HR
57.	3.25	6.	2.	2.	2.
		(INCHES) 12.224	12.225	12.225	12.225
		(AC-FT) 3.	3.	3.	3.

CUMULATIVE AREA = .00 SQ MI

 * *
 9 KK * STG2 *
 * *

SUBBASIN RUNOFF DATA

10 BA SUBBASIN CHARACTERISTICS
 TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

6 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 4.68 6.79 9.98 11.58 12.28 13.47 .00 .00 .00 .00 .00 .00
 STORM AREA = .00

7 LS SCS LOSS RATE
 STRTL .22 INITIAL ABSTRACTION
 CRVNR 90.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

11 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .00 LAG

UNIT HYDROGRAPH
 5 END-OF-PERIOD ORDINATES

2. 1. 0. 0. 0.

HYDROGRAPH AT STATION STG2

TOTAL RAINFALL = 13.47, TOTAL LOSS = 1.25, TOTAL EXCESS = 12.22

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	14.95
+ 6.	3.05	0.	0.	0.	0.
		(INCHES) 12.225	12.225	12.225	12.225
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = .00 SQ MI

 * *
 12 KK * CM12 *
 * *

13 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION CM12

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	14.95-HR
57.	3.25	6.	2.	2.	2.
		(INCHES) 12.224	12.225	12.225	12.225
		(AC-FT) 3.	3.	3.	3.

CUMULATIVE AREA = .00 SQ MI

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	STG1	57.	3.25	6.	2.	2.	.00		
HYDROGRAPH AT	STG2	6.	3.05	0.	0.	0.	.00		
2 COMBINED AT	CM12	57.	3.25	6.	2.	2.	.00		

57/100 = 0.57 cfs/ft

*** NORMAL END OF HEC-1 ***

Camb Jauls
Side Slopes
10-7-93

NATURAL CHANNELS

VARIABLES LIST:

Y - FLOW ELEVATION Q - FLOWRATE S - CHANNEL SLOPE

VARIABLE TO BE SOLVED (Y, Q OR S) ? Y Enter up to 20 cross-section points.
Enter <Return> only for distance to end.

Q (CFS) ? 57
S (FT/FT) ? .2

CROSS-SECTION POINTS

DIST	ELEV	COEFF	DIST	ELEV	COEFF
100	10	.033			
200	10	.033			

RESULTS

Y= 10.12 FT
A= 11.78 SF
P= 100.00 FT
V= 4.84 FPS
F= 2.48 SUPER-CRITICAL FLOW

<Shift> <Prt Sc> print <Return> repeat <Space Bar> back to menu

Carb Tails

9/29/93
Surface

NATURAL CHANNELS

ABLES LIST:

Y - FLOW ELEVATION Q - FLOWRATE S - CHANNEL SLOPE

VARIABLE TO BE SOLVED (Y,Q OR S) ? Y Enter up to 20 cross-section points.
Enter <Return> only for distance to end.

(CFS) ? 57
(FT/FT) ? .0133

CROSS-SECTION POINTS

DIST	ELEV	COEFF	DIST	ELEV	COEFF
0	100	.033			
100	100	.033			

RESULTS

Y= 100.27 FT
A= 26.56 SF
L= 100.00 FT
V= 2.15 FPS
F= 0.73 SUB-CRITICAL FLOW

<Shift> <Prt Sc> print <Return> repeat <Space Bar> back to menu

Carb Tails
Surface

ROCK SIZING BASED ON CORP OF ENGINEERS METHOD

REF: Hydraulic Design of Flood Control Channels
(EM1110-2-1601, 7/1970)

Description of variables used in program

29-Sep-93 02:50 PM

gamma=unit weight of stone (Saturated Surface Dry, SSD)
velocity=mean local vertical velocity (feet/second)
theta=angle of repose of rock (internally set at 40 degrees)

INPUT VARIABLES

gamma (pcf)	velocity (fps)	D(50) (nches)	depth of flow (feet)	channel slope (ft/ft)
162.24	2.15	0.5	0.27	0.0133
162.24	2.15	1	0.27	0.0133
162.24	2.15	1.5	0.27	0.0133
162.24	2.15	2	0.27	0.0133

CALCULATED QUANTITIES

local shear tau(o)	design shear tau	factor of safety (must be >1)
0.08	0.17	2.21
0.11	0.33	3.13
0.13	0.50	3.71
0.16	0.67	4.12

Carl's Tailings
Side Slope

ROCK SIZING BASED ON THE STEPHENSEN METHOD

29-Sep-93 02:37 PM

q = unit discharge
theta = surface slope (degrees)
phi = angle of repose (degrees)
n = porosity of rip rap
C = 0.22 for pebble to 0.27 for crushed granite

INPUT VARIABLES					
q	theta	phi	n	sp. grav.	C
0.57	11.3	40	0.3	2.6	0.27

OUTPUT
d(50) ft.
0.194239
= 23"



ARCO Coal Company
 Division of AtlanticRichfield Company

CONTRACT NO.

ADDITIONAL TRAILINGS - SOUTH TCE

**MAIN TRAILINGS
 IMPROVEMENT**

ANDERSON Engineering Co.
 1000 15th St. N.
 Grand Rapids, MI 49503
 Phone: (616) 454-1000
 Fax: (616) 454-1001

Drawn by: *ARCO*

LOG OF BOREHOLE

HOLE NUMBER 01

LOC. or COORDS. <u>2+00 +25' FROM TCE</u> GROUND ELEV. _____ ORIG. GROUND SURFACE _____ TOTAL DEPTH DRILLED _____ SAMPLING METHOD <u>NEVAL METER CASE</u>	DRILLING CONTRACTOR _____ RIG <u>FLORIDE - TMC</u> BIT <u>1 1/2</u> CASING <u>NA</u> FLUID <u>NA</u>	DATE <u>8/5/91</u> START <u> </u> FINISH <u> </u> TIME _____ RECORDS YES _____ HOW LEFT <u>OPEN TO B. BACKFILL</u>
---	--	---

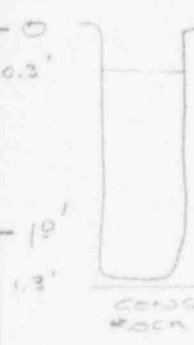
DEPTH	RET	LOSS	PENE RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
<div style="display: flex; align-items: center;"> <div style="border-left: 1px solid black; border-right: 1px solid black; padding: 5px; margin-right: 10px;"> <p>0'</p> <p>10'</p> <p>11'</p> </div> <div style="border: 1px solid black; padding: 5px; flex-grow: 1;"> <p>SANDY SOIL LIGHT BROWN</p> <p>CLAY TYPE SOIL - RED</p> <p>BASALT ROCK FRAGMENT</p> <p>CONSOLIDATED ROCK</p> </div> </div>				<p>SANDY SOIL w/ BEDDED LIMESTONE</p> <p>CLAY SOIL RED LIKE FROZEN ROCK</p> <p>BASALT ROCK BROKEN w/ INTER SOILS - TO CLAY LOAM</p> <p>< .05 m / HR ENTIRE HOLE APPEARS TO BE BKA NO CHANGE THROUGH ENTIRE DEPTH OF HOLE</p> <p>NO IDENTIFIABLE TRIMMAGE IN-THE</p>		

LOCATION _____
 LOGGED BY ES. DC

CLIENT ARCO
 JOB NO. _____

HOLE NUMBER 02

LOC. or COORDS. <u>2+00 -</u> GROUND ELEV. _____ ORIG. GROUND SURFACE _____ TOTAL DEPTH OF HOLE _____ SAMPLING METHOD <u>VEGETAL</u> <u>RAD M</u> 	DRILLING CONTRACTOR _____ <u>TMC</u> RIG <u>PACKHOE</u> BIT _____ CASING _____ FLUID _____	START FINISH DATE <u>8/5/91</u> <u>8/6/91</u> TIME _____ GEOPHYS. LOG _____ YES _____ HOW LEFT OPEN TO BE <u>BACKFILLED</u>
---	---	--

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
<div style="display: flex; align-items: center;">  <div style="margin-left: 20px;"> <p>CLAY SOIL RED ROCKEN ROCK W/ INTER SOIL CONDENSATED ROCK</p> </div> </div>						<p>VEGETATION</p> <p>CLAY LOAM SOIL - RED CLAY SOIL</p> <p>BROKEN ROCK TO BASE OF HOLE - BASALT</p> <p>BASALT ROCK W/ INTER SOIL AND CLAY CTEN</p> <p><0.05 m/hr - BKG NO CHANGE IN READING FROM 0 TO BASE OF HOLE</p> <p>No IDENTIFIABLE TAILINGS MATERIAL</p>
0						
0.3						
10'						
13'						
20'						

LOCATION B...
 LOGGED BY CLARK

CLIENT AKCO
 JOB NO. _____

LOG OF BOREHOLE

HOLE NUMBER 03

LOC. or COORDS. <u>Z+00</u> GROUND ELEV. _____ ORIG. GROUND SURFACE _____ TOTAL DEPTH _____ SAMPLING METHOD <u>USUAL / LAP UP</u>	DRILLING CONTRACTOR _____ <u>TMC</u> RIG <u>PC-140E</u> BIT _____ CASING _____ FLUID _____	DUG START _____ FINISH _____ DATE <u>8/5/61</u> <u>8/6/61</u> TIME _____ GEOPHYS. LOG _____ YES _____ HOW LEFT <u>OPEN TO AIR</u> <u>BACK FILLED</u>
---	---	---

DEPTH	RET.	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
<div style="display: flex; align-items: center;"> <div style="flex: 1; border-left: 1px solid black; border-right: 1px solid black; padding: 5px;"> <p style="font-size: 2em; margin: 0;">0</p> <p style="font-size: 2em; margin: 0;">10'</p> <p style="font-size: 2em; margin: 0;">20'</p> <p style="font-size: 2em; margin: 0;">30'</p> </div> <div style="flex: 2; padding-left: 10px;"> <p>0-0.6' SOIL CLAY</p> <p>CLAY BROKEN ROCK W/ SOIL</p> <p>CLAY BROKEN ROCK W/ SOIL</p> </div> </div>						<p><u>NEG.</u></p> <p><u>SHALLOW CLAY SOIL CAP - RED</u></p> <p><u>CLAY SOILS WITH BROKEN BRACK ROCK</u></p> <p><u>SIGNS OF Ca DEPOSITION IN SOILS</u></p> <p><u>CLAY RED -</u></p> <p><u>< 0.05 mc/hr - BKG FROM 0 - 2.4'</u></p> <p><u>NO VISABLE TAILINGS MATERIAL</u></p> <p><u>SOLID ROCK WITH SOME BROKEN</u></p> <p><u>ROCK ON TOPPED AREA</u></p>

LOCATION _____
LOGGED BY _____

CLIENT _____
JOB NO. _____

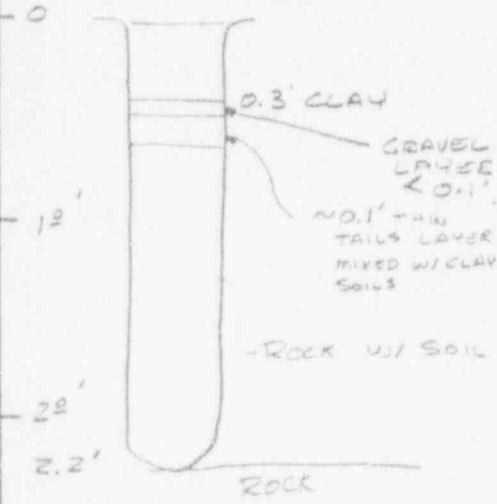
LOG OF BOREHOLE

HOLE NUMBER 04

PAGE 1 of 1

LOG. or COORDS. _____	DRILLING CONTRACTOR <u>TMC</u>	LOG START <u>7/5/91</u>	LOG FINISH <u>3/6/9</u>
GROUND ELEV. _____	RIG <u>BACKHOE</u>	DATE _____	TIME _____
ORIG. GROUND SURFACE _____	BIT _____	GEOPHYS. LOG <input type="checkbox"/> YES <input type="checkbox"/> NO	
_____ DRILLED	CASING _____	HOW LEFT <u>OPEN TO BE RECEIVED</u>	
SAMPLING METHOD <u>Visual PROXIMITY</u>	FLUID _____		

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0						VEG
						CLAY SOIL BED w/ NO ROCK
12'						TAILS 0.25 MT/HR - GRAY SANDY MATERIAL
20'						BROKEN ROCK w/ INTERSOL FINE CLAY LIGHT IN COLOR VERY LIGHT BROWN
22'						BROKEN ROCK AND SOLID ROCK FACCT
						0 - 0.3 FT 0.15 MT/HR
						0.4 TO 0.5 FT 0.7 MT/HR
						0.6 TO BASE 0.1 MT/HR
						TAILINGS IN HOLE NEAR SURFACE THIN LAYER



LOCATION 4500
 LOGGED BY SLB

CLIENT 4500
 JOB NO. _____

LOG OF BOREHOLE

HOLE NUMBER 05

LOC. or COORDS. _____	DRILLING CONTRACTOR <u>TMC</u>	LOG START <u>8/5/41</u>	LOG FINISH <u>8/12/41</u>
GROUND ELEV. _____	RIG <u>BLK-105</u>	DATE _____	TIME _____
ORIG. GROUND SURFACE _____	BIT _____	GEOPHYS LOG <u>YES</u>	
DEPTH DRILLED _____	CASING _____	HOW LEFT <u>OPEN TO AIR</u>	
SAMPLING METHOD <u>VISUAL AND METER</u>	FLUID _____	<u>BACK FILLED</u>	

DEPTH	RET	LOGS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0				CLAY <.1		VEGETATION
				BROKEN ROCK		RED CLAY - NO ROCK
0.5'				Ca LAYER CONSOLIDATED ROCK		BROKEN ROCK w/ LIGHT COLORED SOIL AND FINE TO FINE - LT BRN CLAY TO MEDIUM
						Ca LAYER OVER ROCK IN FACE OF HOLE
						< 0.05 MP HR 0 - 0.5 FT
						OUTSIDE HOLE 0.1 TO 0.2 MP HR
						THE HOLE HAS ELEVATED RAD READINGS BUT NO VISUAL TAILS

LOGGED BY CLP
 CLIENT
 JOB NO.

HOLE NUMBER 06

LOC. or COORDS. _____	DRILLING CONTRACTOR <u>TMC</u>	DATE <u>8/5/91</u>	START <u>8/5/91</u>	FINISH <u>8/6/91</u>
GROUND ELEV. _____	RIG <u>BACKHOE</u>	TIME _____	GEOPHYS. LOG <u>VEG</u>	
ORIG. GROUND SURFACE _____	BIT _____	HOW LEFT <u>OPEN TO BE</u>		
TOTAL DEPTH DRILLED _____	CASING _____	<u>PACKAGED</u>		
SAMPLING METHOD <u>VISUAL / RFD</u>	FLUID _____			

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0				0-2' CLAY		VEG
1				BROKEN ROCK, W/ LIGHT COLOR OF SANDY SOIL		RED CLAY MATERIAL
2						BROKEN BR-SACT ROCK IN LT BEDDING
3						MED TEX SOIL
4						ROCK TO BROKEN ROCK ON FACE OF LOG
5						
6						
7						
8						
9						
10						
11						
12						
13						
14						
15						
16						
17						
18						
19						
20						
21						
22						
23						
24						
25						
26						
27						
28						
29						
30						
31						
32						
33						
34						
35						
36						
37						
38						
39						
40						
41						
42						
43						
44						
45						
46						
47						
48						
49						
50						

LOCATION _____
 LOGGED BY AK
 CLIENT _____
 JOB NO. _____

LOG OF BOREHOLE

HOLE NUMBER

07

LOC. or COORDS.	DRILLING CONTRACTOR	START	FINISH
GROUND ELEV.	T.C.	DATE	8/21/91
ORIG. GROUND SURFACE	RIG	TIME	
TOTAL DEPTH DRILLED	BIT	GEOPHYS. LOG	YES
SAMPLING METHOD	WASING	HOW LEFT	YES
VISUAL RECORDS	FLUID	ACKNOWLEDG	

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0				CLAY SOIL		VEG
						CLAY SOILS W/ LITTLE TO NO ROCK CLAY MATERIAL - RED IN COLOR
0.3				BASALT		BASALT
						ROCK W/ INTERIE SOIL OF MED TEXT (TERMIN) Ca DEPOSITS IN SOIL ROCK TO BROKEN BASALT ROCK PHASE
1.5				ROCK		0.60.5 m/hr BKG 0-1.5'

LOGGED BY

JOB NO.

LOG OF BOREHOLE

HOLE NUMBER 09

LOG. OF COORDS. _____	DRILLING CONTRACTOR _____ <u>TMC</u>	DATE <u>8/5/91</u>
GROUND ELEV. _____	RIG <u>BACKHOE</u>	START <u>8/2/91</u>
ORIG. GROUND SURFACE _____	BIT _____	FINISH <u>8/6/91</u>
TOTAL DEPTH DRILLED _____	CASING _____	GEOPHYS. LOG <input type="checkbox"/> YES <input type="checkbox"/> NO
SAMPLING METHOD <u>VEGETAL METER</u>	FLUID _____	HOW LEFT <u>TO BE REPEATED</u>

DEPTH	RET	LOSS	PENE RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0				CLAY SOIL		CLAY SOIL - BED
0.4				BROKEN ROCK		LT BRN SNG MED TO HRSN TERT W/ BROKEN BASALT ROCK
1				W/ INTER SOIL - CLAY LIGHT BROWN		
2						SOLID & BROKEN ROCK HOLE BASE
2.2				SOLID / CON ROCK		at 2.2 < 0.05 MP/HR NO VISIBLE TRAILINGS

LOCATION _____
LOGGED BY _____

CLIENT _____
JOB NO. _____

LOG OF BOREHOLE

HOLE NUMBER 10

PAGE of

LOC. or COORDS. _____	DRILLING CONTRACTOR _____	DIG START <u>8/5/91</u>	FINISH <u>8/6/91</u>
GROUND ELEV. _____	RIG <u>BACKHOLE</u>	DATE _____	TIME _____
ORIG. GROUND SURFACE _____	BIT _____	GEOPHYS. LOG <input type="checkbox"/> YES <input type="checkbox"/> NO	HOW LEFT <u>SPACILL</u>
TOTAL W. IN DRILLED _____	CASING _____		
SAMPLING METHOD <u>VISUAL MP RAD</u>	FLUID _____		
<small>WETAL</small>			

DEPTH	RET	LOG	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0						BROKEN ROCK ON SURFACE - VEG
12'				CLAY SOIL RED		RED CLAY SOIL W/ LITTLE TO NO ROCK
21'				CA CEMENT WHITE		CA LAYER - T-N ABOUT 1" THICK
22'				CLAY SOIL		CLAY SOIL W/ SOME BROKEN ROCK
30'				BROKEN ROCK W/ CLAY SOIL		BROKEN BASALT ROCK W/ INTER SOIL LT BRN M TO 1+ TEXT SOLID TO BROKEN BASALT ROCK BASE OF 0-3.0' < 0.05 MP/HR DECREASED READ AS DEPTH INCREASES NO VISIBLE TAILS
				3.0 ROCK		

LOGGED BY

JOB NO.

LOG OF BOREHOLE

HOLE NUMBER 13

LOC. or COORDS. _____	DRILLING CONTRACTOR _____ <u>TMC</u>	DATE <u>2/5/91</u>	DUG START _____	SURVEY FINISH <u>2/6/91</u>
GROUND ELEV. _____	RIG <u>BACKHOE</u>	TIME _____	GEOPHYS. LOG <input type="checkbox"/> YES <input checked="" type="checkbox"/> NO	
ORIG. GROUND SURFACE _____	BIT _____	HOW LEFT <u>BACKFILL</u>		
DEPTH DRILLED _____	CASING _____			
SAMPLING METHOD <u>USUAL METER</u>	FLUID _____			

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0						VEG.
0.4'				LIGHT COLORED MED TEXTURED SOIL - 5CM W/ BROKEN LIME STONE (GRAVEL)		LT BRN MIED TEX SOIL LIMESTONE - FLAKY BRKCS TO 1.6 GRAVEL IS MIXED INTO MED TEXT SOIL 0.4 - 1.6
1.0			1.2 m/hr			RED CLAY SOIL
1.6				RED CLAY SOIL 2		GRAY TAILS MIXED W/ SOIL
2.0						
2.4			0.8 m/hr			
2.8				TAILS LAYER GRAY W/ SOIL	2.5	
3.2				RED CLAY LAYER		
3.6						
4.0				BROKEN ROCK W/ SOIL 1		
4.2'				RED CLAY ON BOTTOM		
				TOTAL DEPTH NO ROCK		
5.0						

LOCATION _____
 LOGGED BY _____
 CLIENT _____
 JOB NO. _____

LOG OF BOREHOLE

HOLE NUMBER 16

PAGE of

LOC. or COORDS. <u>124 +00 -25'</u> GROUND ELEV. _____ ORIG. GROUND SURFACE _____ TOTAL DEPTH DRILLED _____ SAMPLING METHOD _____	DRILLING CONTRACTOR _____ RIG _____ BIT _____ CASING _____ FLUID _____	START _____ DATE _____ TIME _____ GEOPHY. LOG _____ HOW LEFT _____
---	--	--

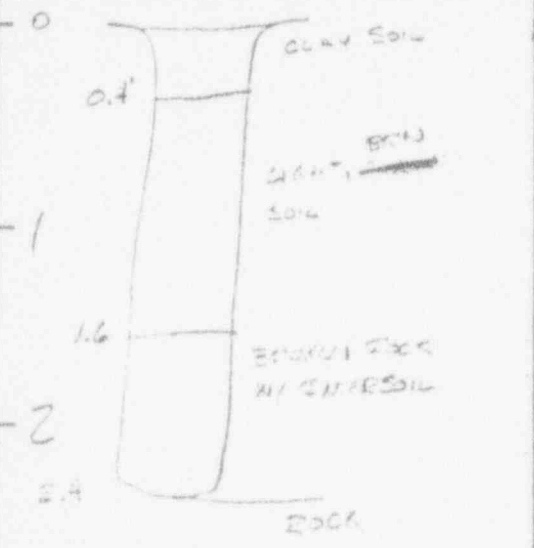
DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0				CLAY DARK BDN		
10				CLAY SOIL RED		GRAY LAUER
20				BRDN GRAY LOCK w/ INTER SOIL		
30						BK 0.08 SURFACE LO.05 m/hr DECREASES w/ DEPTH GRAY LAUER 0.12

LOCATION
LOGGED BY

CLIENT
JOB NO.

LOC. or COORDS. _____ _____ GROUND ELEV. _____ ORIG. GROUND SURFACE _____ TOTAL DEPTH DRILLED _____ SAMPLING METHOD _____	DRILLING CONTRACTOR _____ _____ RIG _____ BIT _____ CASING _____ FLUID _____	START _____ FINISH _____ DATE _____ TIME _____ GEOPHYS. LOG YES _____ N _____ HOW LEFT _____ _____
--	---	---

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
-------	-----	------	------------	-----------	---------	-------------



0 - 2.4' 0.05 m/hr

LOGGED BY _____

JOB NO. _____

CLIENT _____

HOLE NUMBER 18

LOC. or COORDS. _____ _____ GROUND ELEV. _____ ORIG. GROUND SURFACE _____ TOTAL DEPTH DRILLED _____ SAMPLING METHOD _____	DRILLING CONTRACTOR _____ _____ RIG _____ BIT _____ CASING _____ FLUID _____	START _____ FINISH _____ DATE _____ TIME _____ GEOPHYS. LOG _____ YES _____ HOW LEFT _____ _____
--	---	--

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0			0.3	RED CLAY SOIL		
1				LT BGN SOIL		
1.6				MIXED w/ FROZEN ROCK		
2				ROCK		0-1.6' < 0.05 ml/H
3						

LOGGED BY

JOB NO.

LOCATION

CLIENT

HOLE NUMBER

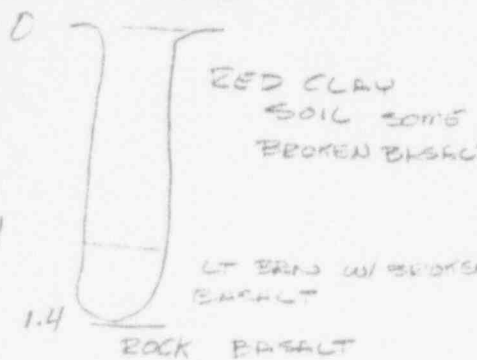
21 - 33

LOG OF BOREHOLE

PAGE ____ of ____

LOC. or COORDS. _____	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	
ORIG. GROUND SURFACE _____	BIT _____	TIME _____	
DEPTH DRILLED _____	CASING _____	GEOPHYS. LOG _____	YES _____
SAMPLING METHOD _____	FLUID _____	HOW LEFT _____	

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
-------	-----	------	------------	-----------	---------	-------------



0-1.4' 20.05 ml-R
 NO TAILS VISIBLE

LOCATION
 LOGGED BY
 CLIENT
 JOB NO.

HOLE NUMBER

22

LOG OF BOREHOLE

PAGE ___ of ___

LOC. or COORDS. _____
 GROUND ELEV. _____
 ORIG. GROUND SURFACE _____
 TOTAL L. DRILLED _____
 SAMPLING METHOD _____

DRILLING CONTRACTOR _____
 RIG _____
 BIT _____
 CASING _____
 FLUID _____

START FINISH
 DATE _____
 TIME _____
 GEOPHYS. LOG YES ___
 HOW LEFT _____

DEPTH	RET.	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL
-------	------	------	------------	-----------	---------

DESCRIPTION

0			0.2	RED SOIL	
1			1.0	RED & LBEN W/ BROKEN ROCK	
				↑	
				ROCK	

0 - 1.0 20.05 m/hr
 NO TAILS VISIBLE

LOGGED BY

JOB NO.

LOG. or COORDS. _____	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	
ORIG. GROUND SURFACE _____	BIT _____	TIME _____	
TOTAL DEPTH DRILLED _____	CASING _____	GEOPHYS. LOG _____	YES _____ N _____
SAMPLING METHOD _____	FLUID _____	HOW LEFT _____	

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
-------	-----	------	------------	-----------	---------	-------------



0-1.5' @ 0.05 m/min
NO TAILS VISIBLE

LOGGED BY

JOB NO.

HOLE NUMBER

24

LOG OF BOREHOLE

PAGE ___ of ___

LOC. or COORDS. <u>170+00 -25</u>	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	
ORIG. GROUND SURFACE _____	BIT _____	TIME _____	
TOTAL DEPTH DRILLED _____	CASING _____	GEOPHYS. LOG <input type="checkbox"/> YES <input type="checkbox"/> NO	
SAMPLING METHOD _____	FLUID _____	HOW LEFT _____	

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0				RED CLAY		
0.5				CA LAYER		
1.2				RED CLAY W/ LT BRN SOIL SOME BROKEN ROCK		
1.1				ROCK & BROKEN ROCK INTER SOLS		
2.0				NOT TO ROCK		
						0-1.1 < 0.1 ml/hr
						BOTTOM OF HOLE 0.12
						NOT SURE RE TRAIL CONTENT

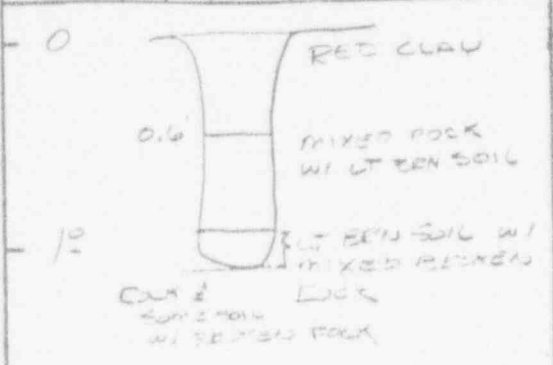
LOGGED BY

JOB NO.

HOLE NUMBER 27

LOC. or COORDS. _____ GROUND ELEV. _____ ORIG. GROUND SURFACE _____ TOTAL DEPTH DRILLED _____ SAMPLING METHOD _____	DRILLING CONTRACTOR _____ RIG _____ BIT _____ CASING _____ FLUID _____	START DATE _____ FINISH DATE _____ GEOPHYS. LOG <input type="checkbox"/> YES <input type="checkbox"/> NO HOW LEFT _____
---	--	--

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
-------	-----	------	------------	-----------	---------	-------------



0.10' < 0.05 m/hr

No change in...

LOCATION LOGGED BY

CLIENT JOB NO.

LOG OF BOREHOLE

HOLE NUMBER 28

LDC. or COORDS. <u>113-30-25</u>	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	
ORIG. GROUND SURFACE _____	BIT _____	TIME _____	
TOTAL DEPTH DRILLED _____	CASING _____	GEOPHYS. LOG _____	
SAMPLING METHOD _____	FLUID _____	HOW LEFT _____	

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0						VEG
			0.4	RED CLAY		RED CLAY SOIL NO ROCK
				SANDY SOIL		RED / GRAY SOIL MED TEXT
10'			1.0	RED CLAY		NO ROCK
20'			1.8			LT BROWN MED. TEXT SOIL NO ROCK
			2.5	LT SAND		LT BROWN MED TO SANDY SOIL
30'			2.9	GRAY TAILS		NO ROCK
40'			3.9			SURFACE 40.05 MP/HR
						PERFICIE INCREASES W/ DEPTH
						GRAY 2.9-3.9' 1.2 MP/HR
						TAILS 1" THICK AT 6-7' DEPTH

LOGGED BY

CLIENT JOB NO.

LOG OF BOREHOLE

HOLE NUMBER 29

PAGE of

LOG. or COORDS. <u>TOE - 125</u>	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	
ORIG. GROUND SURFACE _____	RIT _____	TIME _____	
TOTAL DEPTH DRILLED _____	CASING _____	GEOPHYS LOG _____	
SAMPLING METHOD _____	FLUID _____	HOW LEFT _____	

DEPTH	RET	LOSS	PENE RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
-------	-----	------	-----------	-----------	---------	-------------



REG

RED CLAY SOIL

LT BEN SOIL w/ BROKEN BASALT ROCK

GRAY LAYER @ 0.1' THICK

RED SOIL w/ BROKEN BASALT

0 - 0.7 0.9 m/hr

0.7 - 0.8' 0.15 m/hr GRAY LAYERS

BOTTOM 0.15 m/hr

TAILS @ 0.7 TO 0.8

LOCATION Blue Springs, MO
LOGGED BY _____

CLIENT
JOB NO. _____

LOG OF BOREHOLE

HOLE NUMBER 30

PAGE of

LDC. or COORDS. _____	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	TIME _____
ORIG. GROUND SURFACE _____	BIT _____	GEOPHYS. LOG <input type="checkbox"/> YES <input type="checkbox"/> NO	
TOTAL DEPTH DRILLED _____	CASING _____	HOW LEFT _____	
SAMPLING METHOD _____	FLUID _____		

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0				LT BROWN FINE SOIL		LT BROWN FINE TEXTURE
2.5				CA LAYER		CA DEPOSIT OVER 2" THICK
10'				LT BROWN SOIL W/ NO ROOTS		LT BROWN SOIL w/ NO BROKEN TO A TAN - SANDY TEXTURE
1.5				RED CLAY w/ BROCK 1.3		RED CLAY w/ SOME BROKEN ROCK
20'						EASE BROKEN BRKLT ROCK
						0 TO 0.5 0.15 MP/HR
						0.5 TO 1.5 0.40 MP/HR
						1.5' TO 1.8 0.15 MP/HR
						APP APPENDS TO TAILS

LOCATION
LOGGED BY

CLIENT
JOB NO.

HOLE NUMBER

31

LOG OF BOREHOLE

PAGE ____ of ____

LOG. or COORDS. _____	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	
ORIG. GROUND SURFACE _____	BIT _____	TIME _____	
TOTAL DEPTH DRILLED _____	CASING _____	GEOPHYS. LOG <input type="checkbox"/> YES <input type="checkbox"/> NO	
SAMPLING METHOD _____	FLUID _____	HOW LEFT _____	

DEPTH	RET	LOG	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0				RED CLAY		RED CLAY W/ BROKEN LIMESTONE
1.2				BROKEN LIMESTONE		0.50 - 3 - 4"
1.6				LT BRN SOIL		LT BRN KIE - TEST SOIL W/ LITTLE TO 1/2 ROCK
2.5				RED CLAY		RED CLAY SOIL
3.9						NO TO ROCK RISE
						3.9 < 0.05 MP/HR
						NO VISIBL TRACS

LOGGED BY

CLIENT JOB NO.

LOG OF BOREHOLE

PAGE ____ of ____

HOLE NUMBER 32

LDC. or COORDS. <u>116 + 00 - 25'</u>	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	
ORIG. GROUND SURFACE _____	RIT _____	TIME _____	
TOTAL DEPTH DRILLED _____	CASING _____	GEO. PHYS. LOG <input checked="" type="checkbox"/> YES	
SAMPLING METHOD _____	FLUID _____	HOW LEFT _____	

DEPTH	RET. LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0					VEG.
12			RED CLAY		RED CLAY SOIL NO ROCK
22					
32			GRAY MATERIAL		GRAY TAILINGS MATERIAL NO ROCK
40					HOLE NOT COMPLETED TO BOTTOM
40					NOT TO GO
50					0-2' 0.1 MP/HK. INCREASE DEPTH
					2'-4' 0.9 MP/HK. GRAY TAIL

LOCATION _____
LOGGED BY _____

CLIENT _____
JOB NO. _____

HOLE NUMBER 33

LOG. of COORDS. _____	DRILLING CONTRACTOR <u>TMC</u>	START _____	FINISH <u>8-8-91</u>
GROUND ELEV. _____	RIG <u>RACHNE</u>	DATE _____	TIME _____
ORIG. GROUND SURFACE _____	BIT _____	GEOPHYS. LOG <u>YES</u>	HOW LEFT <u>OPEN</u>
TOTAL DEPTH DRILLED _____	CASING _____		
SAMPLING METHOD _____	FLUID _____		

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0'						VEGETATION SPACES & GRASSES
2'-10'						LT GRAY SANDS, THIN RED CLAY LAYERS, VERT THIN, MED. LOSS
10'						10'-15'; RED CLAY AND LT GRAY SAND LAYERS, VERT THIN, STRATIFIED, COARSE
15'						1.5'-2.1' LT GRAY SANDS, STRATIFIED WITH DARK DECOMPOSED ORGANICS, FINE
20'						2.1'-3.8' / 1.25 m. VERT LT BROWN BROWN SAND, SOFT, MED. FINE, VERT GRAY
30'						
38'						

LOGGED BY _____
 JOB NO. _____

LOG. or COORDS. <u>LOW REEF</u>		DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____		RIG _____	DATE _____	_____
ORIG. GROUND SURFACE _____		BIT _____	TIME _____	_____
TOTAL DEPTH DRILLED _____		CASING _____	GEOPHYS ID# _____	YES _____
SAMPLING METHOD _____		FLUID _____	HOW LEFT _____	_____

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0				RED CLAY SOIL		
10				LIGHT COLORED SOIL W/ BECKEN LIMESTONE ROCK RED TEXTURE		
20				SUB GABY		
30				CLAY SOIL RED		
40						BKG 0.1 m/hr 0-2' 0.1 TO 1.0 m/hr .1 ON SURFACE 2-2.5' 1.9 m/hr 2.5-6.1 0.6 m/hr DECREASE IN RESISTANCE AWAY FROM TAILS
50						
60				SOME BEDDED BASALT ROCK		
				BROKEN ROCK BASALT		

LOGGED BY _____

CLIENT JOB NO. _____

LOC. or COORDS. _____	DRILLING CONTRACTOR <u>TMC</u>	START _____	FINISH _____
GROUND ELEV. _____	RIG <u>ROCKHOG</u>	DATE _____	<u>8-8-60</u>
ORIG. GROUND SURFACE _____	SIT _____	TIME _____	_____
TOTAL DEPTH DRILLED _____	CASING _____	GEOPHYS. 'OG _____	YES _____
SAMPLING METHOD _____	FLUID _____	HOW LEFT <u>OPEN</u>	_____

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0						LIGHT VEGETATION
0.2						0'-0.2' BROWN SAND WITH WATER
0.5						0.2'-1.2' VERT LT TAN SILTY SAND STRATIFIED IN TOP 0.5', LOWER PORTION NOT STRATIFIED, CONTAINING CALCAREOUS GRAINLS AND POCKETS OF DARK BROWN SH CLAY CONT. LORMS.
1.0						
1.2						1.2' - 3.6' LIGHT TAN SILTY SAND, APPEAR TO BE ALLUVIAL FILL, STRATIFIED, TOP FINE SUBANGULAR GRAVEL
2.0						
3.0						3.6' BOTTOM: FINE GRAY SAND WITH LT. BROWN CLAY LAMINAE, APPEAR TO BE ALLUVIAL MATERIAL IN SAND
3.6						

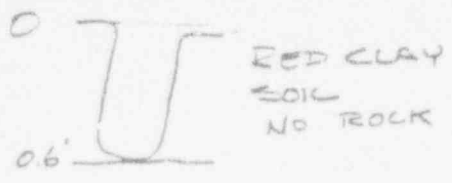
LOGGED BY MAR/ACF
 LOCATION M

JOB NO. _____

HOLE NUMBER 38

LOC. or COORDS. _____ GROUND ELEV. _____ ORIG. GROUND SURFACE _____ TOTAL DEPTH DRILLED _____ SAMPLING METHOD _____	DRILLING CONTRACTOR _____ RIG _____ BIT _____ CASING _____ FLUID _____	START _____ FINISH _____ DATE _____ TIME _____ GEOPHYS. LOG _____ YES _____ HOW LEFT _____
---	--	---

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
-------	-----	------	------------	-----------	---------	-------------



0-0.6' < 0.05 m/hr
NO TAILS

LOCATION LOGGED BY

CLIENT JOB NO.

HOLE NUMBER

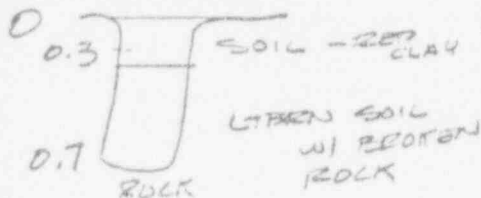
40

LOG OF BOREHOLE

PAGE _____ of _____

LDC. or COORDS. _____	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	
ORIG. GROUND SURFACE _____	BIT _____	TIME _____	
TOTAL DEPTH DRILLED _____	CASING _____	GEOPHYS. LOG <input checked="" type="checkbox"/> YES	
SAMPLING METHOD _____	FLUID _____	HOW LEFT _____	

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
-------	-----	------	------------	-----------	---------	-------------



0-0.7' 40.05 m/hr
 No visible tails

LOGGED BY _____

JOB NO. _____

LOC. or COORDS. _____	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	_____
ORIG. GROUND SURFACE _____	BIT _____	TIME _____	_____
_____	CASING _____	GEOPHYS. LOG <input type="checkbox"/> YES <input type="checkbox"/> NO	_____
SAMPLING METHOD _____	FLUID _____	HOW LEFT _____	_____

DEPTH	RET	LOSS	PENE RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
-------	-----	------	-----------	-----------	---------	-------------



0-1.7 < 0.05 m/hr

NO TAILS VISIBLE

LOGGED BY

JOB NO.

HOLE NUMBER

45

LOG OF BOREHOLE

PAGE ___ of ___

LOG. or COORDS. _____	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	_____
ORIG. GROUND SURFACE _____	BIT _____	TIME _____	_____
TOTAL DEPTH DRILLED _____	CASING _____	GEOPHYS. LOG _____	YES _____
SAMPLING METHOD _____	FLUID _____	HOW LEFT _____	_____

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0						VEG
				RED CLAY		RED CLAY
				CA LAYER		CA LAYER
10				LT BROWN fine grained rock		LT BROWN FINE TEXTURE SAND W/ BROKEN FLINT
				1.2'		
				Rock is broken at base		
20						0-1.2 60.05 MP/Hr NO TAILS

LOGGED BY

JOB NO.

HOLE NUMBER

46

LOG OF BOREHOLE

PAGE _____ of _____

LDC. or COORDS. _____	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	
ORIG. GROUND SURFACE _____	BIT _____	TIME _____	
TOTAL DEPTH DP" LED _____	CASING _____	GEOPHYS LOG <input type="checkbox"/> YES <input type="checkbox"/> NO	
SAMPLING METHOD _____	FLUID _____	HOW LEFT _____	

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0				RED CLAY		VEG RED CLAY SOIL
10			0.4	LT BRN RED TCK SOIL W/ BROKEN ROCK		LT BRN RED TCK SOIL W/ BROKEN ROCK FALLT BROKEN ROCK
20			0.6	ROCK		SOIL & BROKEN BASALT FET
						D-0.6' < 0.05' MP NO SAMPLE TAKEN

LOCATION LOGGED BY

JOB NO.

HOLE NUMBER 47

LOG OF BOREHOLE

PAGE of

LOC. or COORDS. _____	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	
ORIG. GROUND SURFACE _____	BIT _____	TIME _____	
TOTAL DEPTH DRILLED _____	CASING _____	GLDPR. & WDG _____	YES _____
SAMPLING METHOD _____	FLUID _____	HOW LEFT _____	

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0				RED CLAY		RED CLAY SOME BROKEN ROCK
1.2			0.6	ROCK W/ INTER. SOIL		ROCK AND SOME BROKEN FRAGMENTS W/ INTER SOIL LT PLN COURSE SOIL MED TEN
2.0						0-0.6 20.05 MP/HR NO VISIBLE TRAILS

CAT...
LOGGED BY

JOB NO.

LDC. or COORDS.	DRILLING CONTRACTOR	START	FINISH
GROUND ELEV.	RIG	DATE	
ORIG. GROUND SURFACE	BIT	TIME	
TOTAL DEPTH DRILLED	CASING	GEOPH. LOG	YES
SAMPLING METHOD	FLUID	HOW LEFT	

DEPTH	RET LOSS	PENE RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
-------	----------	-----------	-----------	---------	-------------

0

10'

20'

RED CLAY / SOME BROKEN BASALT

0.6'

ROCK

LOGGED BY

JOB NO.

RED CLAY SOIL W/ SOME BROKEN BASALT

SOLID AND BROKEN BASALT ROCK W/ SOME INTER SOIL - MINE - LT BRN W/ RED CLAY

0 - 0.6 < 0.05 AIR / MIN
NO VISIBLE TAILS

HOLE NUMBER 49

LOG OF BOREHOLE PAGE of

LOC. or COORDS. _____	DRILLING CONTRACTOR _____	START _____	FINISH _____
GROUND ELEV. _____	RIG _____	DATE _____	_____
ORIG. GROUND SURFACE _____	BIT _____	TIME _____	_____
TOTAL DEPTH DRILLED _____	CASING _____	GEOPHYS. LOG _____	_____
SAMPLING METHOD _____	FLUID _____	HOW LEFT _____	_____

DEPTH	RET	LOSS	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
0				RED CLAY		RED CLAY SOIL
10'			0.3	RED CLAY MIXED W/ LIGHT SOIL SMALL BROKEN LIMESTONE SOME BROKEN		RED CLAY W/ LT FEN SOIL - COURSE TEL MIXED W/ SMALL FROKEN LIMESTONE AND FROKEN FRAGM
20'			1.2'	BRK AND SHAL		BROKE BRUSACT AND OVER ROCKS SOLID ROCK
						Q - 1.2' @ 0.05 MP/HR NO TAILS VISABLE

LOCATION _____
LOGGED BY _____

JOB NO. _____

HOLE NUMBER 51

LOC. or COORDS. _____
GROUND ELEV. _____
ORIG. GROUND SURFACE _____
TOTAL DEPTH DRILLED _____
SAMPLING METHOD _____

DRILLING CONTRACTOR _____
RIG _____
BIT _____
FLUID _____

START _____ FINISH _____
DATE _____
TIME _____
GEOPHYS LOG _____ YES
HOW LEFT _____

DEPTH	RET	LOG	PENE. RATE	ROCK TYPE	SYM-BOL	DESCRIPTION
-------	-----	-----	------------	-----------	---------	-------------

0
1²
2⁰
2.3
3⁰
4⁰

RED SOIL
W/ SOME
BROKEN
ROCK

ON SOIL &
MIXED
ROCK

APPEARS UNDISTURBED - NO
FILL

0 - 2.3' < 0.05"
NO VISIBLE FRILLS

LOGGED BY
JOB NO.

HOLE NUMBER

CUT

LOG OF BOREHOLE

PAGE ___ of ___

119+00 -

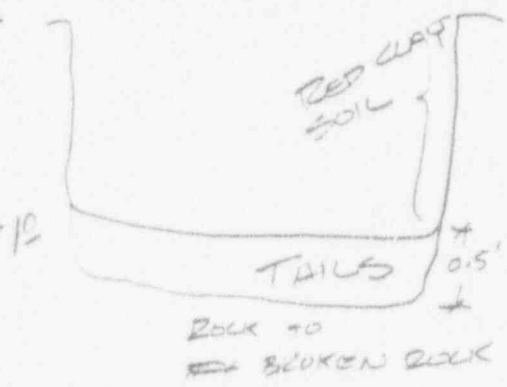
LOC. or COORDS. 119+00 + 20'
 GROUND ELEV. _____
 ORIG. GROUND SURFACE _____
 TOTAL DEPTH DRILLED _____
 SAMPLING METHOD _____

DRILLING CONTRACTOR _____
 RIG _____
 BIT _____
 CASING _____
 FLUID _____

START _____ FINISH _____
 DATE _____
 TIME _____
 GEOPHYS. LOG Yes No
 HOW LEFT _____

DEPTH	RET	LOG	PENE. RATE	ROCK TYPE	SYM-BOL
-------	-----	-----	------------	-----------	---------

DESCRIPTION



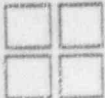
0-12' ~~0.2 m/hr~~ 0.09 m/hr

TAILS 0.3 m/hr
GRAY SAND TAILS

NOTE TAILS IN CUT @ 119+00

LOGGED BY

JOB NO.



ANDERSON Engineering Company
 4656 South 1900 West St.
 Roy, Utah 84067
 Telephone 801-731-4596

ARCO COAL COMPANY
 BLUEWATER MILL
 BORROW MATERIAL

BORING NO. Pit 28 S2A

SHEET / OF 2

DATE STARTED: 7-10-71

DATE COMPLETE:

TOTAL DEPTH: 15

SURFACE ELEV:

X: Y:

SAMPLING METHOD:

Hand Driven Auger

LOGGED BY:

J. H. STINEBAUGH

SAMPLE NO.	SAMPLE DEPTH (ft)	DEPTH (ft)	SYMBOL	USC	DESCRIPTION
1	0-2			SC	Yellowish sandy clay soil
2				SC	GRAY TAILINGS SAND - COMPACT - MGD
3				SC	Sandy clay - light gray-brown color
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22					
23					
24					
25					
26					
27					
28					
29					
30					
31					
32					
33					
34					
35					
36					
37					
38					
39					
40					
41					
42					
43					
44					
45					
46					
47					
48					
49					
50					
51					
52					
53					
54					
55					
56					
57					
58					
59					
60					
61					
62					
63					
64					
65					
66					
67					
68					
69					
70					
71					
72					
73					
74					
75					
76					
77					
78					
79					
80					
81					
82					
83					
84					
85					
86					
87					
88					
89					
90					
91					
92					
93					
94					
95					
96					
97					
98					
99					
100					

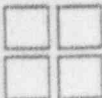
GRAY TAILINGS SAND - almost green

5-10' Tailings SAND - Light gray, coarse texture
 Partly consolidated -

all rest almost (not green color)
 due to presence of sand

NO ROCKS

Partly consolidated (not green color) from sand



ANDERSON Engineering Company
 4655 South 1900 West St.
 Roy, Utah 84067
 Telephone 801-731-4596

ARCO COAL COMPANY
 BLUEWATER MILL
 BORROW MATERIAL

BORING NO. 32-4

SHEET 2 OF

DATE STARTED: 9-12-91

DATE COMPLETE:

TOTAL DEPTH:

SURFACE ELEV:

X: Y:

SAMPLING METHOD: *Hand-drawn
 AUGER CORE
 Core 200*

LOGGED BY: *J. R. N. N. N.*

DESCRIPTION

SAMPLE NO.
 SAMPLE DEPTH (ft)
 DEPTH (ft)
 SYMBOL
 USC

12-12

12

12-14

13

14

15

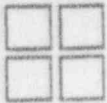
12-15

2

NO. 100
TAILINGS SAND
*Partly cemented - some clay on the top
 by limonite.*

COARSE SAND
COARSE SAND

4-5" SAND
COARSE SAND



ANDERSON Engineering Company
 4855 South 1900 West St.
 Roy, Utah 84067
 Telephone 801-731-4596

ARCO COAL COMPANY
 BLUEWATER MILL
 BORROW MATERIAL

BORING NO. 20 A

SHEET / OF 1

DATE STARTED: 7-10-91

DATE COMPLETE: 9-10-91

TOTAL DEPTH: 8 FT

SURFACE ELEV:

X: Y:

Sta 113+00 To 18 LF

SAMPLING METHOD: Hollow Stem
 Auger - Core

LOGGED BY: J. MONTANALE

SAMPLE NO.	SAMPLE DEPTH (ft)	DEPTH (ft)	SYMBOL	USC	DESCRIPTION
		0			
	2-2	1		SC	
		2		SW	SANDY LOAM - 1/2" to 1" particles
				SC-CL	Reddish clay + sand
	2-4	2		SP	
					NO RE-DUGS
					TILLING SAND
	6-8	7		SP	
					NO RE-DUGS - TILLING SAND
					Partial ...
					...
				CL	...

ARCO BY WATER MILL
SOIL SAMPLE ROUTING LOG

Sample ID #	Description	Date Sampled	Tech	Date Sealed	Tech	1st Cnt Date	Tech	28 Day Count	Tech	QA/QC
91-262 S	28 I S Toe 0-2' ↓	9-10-91	RV	9-25-91	JT	10-1-91	SF	10-23-91 SF	SF	
91-263 S	32 I ↓	↓	RV	↓	JT	↓	↓	10-24-91 ↓	↓	

A
N

Comments: Core Composite Samples from the South Toe (1st set - I - taken)
13.5 Source Item Samples

Reviewed By: _____

ARCO RSO: _____

Date: _____

ARCO BLUEWATER MILL
SOIL SAMPLE ROUTING LOG

20155

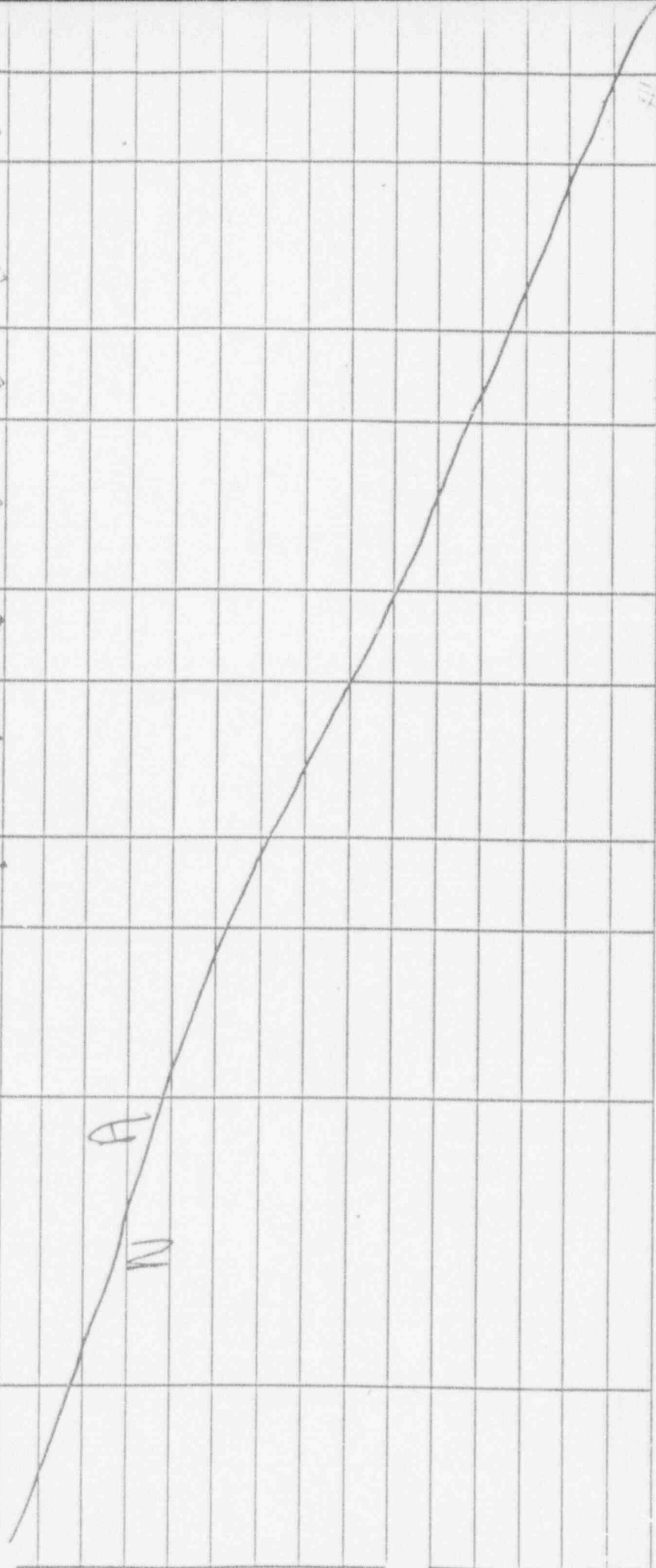
Sample ID #	Description	Date Sampled	Tech	Date Sealed	Tech	1st Cnt Date	Tech	28 Day Count	Tech	QA/QC
91-227S	S. Toe #24 Down to Malpais	8-20-91	RL/KS	9-19-91	RL/JT	9-21-91	SF	10-17-91	KS	
91-228S	#29 Above Tails				RL					
91-229S	#12 to Malpais				RL					
91-230S	#36 Tails				RL					
91-231S	#37 Down to Malpais			9-20-91	RL/JT			10-18-91	KS	
91-232S	#28 Tails									
91-233S	#29 Tails									
91-234S	#13 Above Tails					SF NA				

A
N

Comments: * QA/QC Sample - South Toe Composites

ARCO B. WATER HILL
SOIL SAMPLE ROUTING LOG

Sample ID #	Description	Date Sampled	Tech	Date Sealed	Tech	1st Cnt Date	Tech	28 Day Count	Tech	QA/QC
91-2355	S. Toe #13 TAILS	8-20-91	KS/RL	9-20-91	J/RL	9-23-91	KS	10-18-91	KS	
91-2365	#34 Below Tails									
91-2375	#36 Below Tails									
91-2385	#34 Above Tails									
91-2395	#28 Above Tails									
91-2405	#36 Above Tails									



Comments: * QA/QC Sample - South Toe Composites

Reviewed By: _____

ARCO-RSO: _____

Date: _____

**ARCO B. WATER MILL
SOIL SAMPLE ROUTING LOG**

Sample ID #	Description	Date Sampled	Tech	Date Sealed	Tech	1st Cnt Date	Tech	28 Day Count	Tech	QA/QC
91-241-S	#13 S. TOE Tails Comp	8-20-91	RL/KS	9-20-91	JT/RL	9-23-91	KS	10-18-91	KS	
91-242-S	#13 S. TOE 2' below Tails	8-20-91	RL/KS	9-20-91	JT/RL	↓	↓	↓	↓	
91-243-S	#30 S. TOE 0.2' To Malpais	8-20-91	RL/KS	9-20-91	JT/RL	↓	↓	↓	↓	
91-244-S	#35 S. TOE Tails comp tails	8-20-91	RL/KS	9-20-91	JT/RL	↓	↓	↓	↓	
91-245-S	#35 S. TOE 0.2' above tails	8-20-91	RL/KS	9-20-91	JT/RL	9-24-91	SE			
91-246-S	S. Toe #13, 28, 32 ^{TOP} Comp	8-21-91	RL/JS	9-20-91	JT/RL	↓	↓	↓	↓	
11-247-S	S. Toe #23 0-2' To Malpais	8-21-91	RL/JS	9-20-91	JT/RL	↓	↓	↓	↓	
91-248-S	S. Toe #20 0-10" No Tails	8-21-91	RL/JS	9-20-91	JT/RL	↓	↓	↓	↓	

A
N

Comments: South Toe Composites

Reviewed By: _____

ARCO RSO: _____

Date: _____

W. J. [Signature]

9/14/90
13, 28 + 32 TOP

ARCO BLK. WATER MILL
SOIL SAMPLE ROUTING LOG

Sample ID #	Description	Date Sampled	Tech	Date Sealed	Tech	ay Count	Tech	QA/QC
91-251 S	#4 0-2' No Tails	8-21-91	JSTRL	9-23-91	JT			
* 91-250 SX	#5 0-1 1/2' No Tails							
91-249 SX	#8 0-6" Tails mixed							
91-248 SX	#20 0-16" No Tails	9-20-91	JT/RL					
91-247 SX	#23 0-2' TO MIXED							
	#13 TOP COMPOSITE		RL+K					
	#28 TOP COMPOSITE							
	#32 TOP COMPOSITE							

COMPOSITE MIX
EQUAL AMOUNTS
TOGETHER AS ONE SAMPLE

N A

Comments: Samples are from South toe of tail.
* QA/QC Sample

Bulk Sample

ARCO BLUEWATER MILL
SOIL SAMPLE ROUTING LOG

Sample ID #	Description	Date Sampled	Tech	Date Sealed	Tech	1st Cnt Date	Tech	28 Day Count	Tech	QA/QC
91-252 S	37 II 0 2-1	9/16/91	VV	9-23-91	JT	9-30-91	KS	10-21-91	SF	
91-253 S	" 4-6			9-24-91	RL/JT			10-22-91	SF	
91-254 S	" 10-8			9-23-91	JT			10-21-91	SF	
91-255 S	" 5-6			9-23-91	JT			↓	↓	
* 91-256 S	" 10-12			9-24-91	RL/JT			10-22-91	SF	*
91-257 S	" 12-14			9-23-91	JT			10-21-91	SF	
91-258 S	" 14-16			9-24-91	RL/JT			10-22-91	SF	
91-259 S	" 16-18 (Composite Sample)			9-23-91	JT			10-21-91	SF	
* 91-260 S	23 II 3-5			9-24-91	RL/JT			10-22-91	SF	*
91-261 S	" 5-7 (Composite Sample)			9-24-91	RL/JT	✓	✓	10-22-91	SF	

Comments: Core Composite Samples (Source Term Samples) - South Toe
* QA/QC Samples (from 2nd set - II - taken)

Reviewed By: _____ ARCO RSO: _____ Date: _____

MCA RA-226 Analy on Soil Samples

#	Sample ID #	Sample Description	Std. Wt. gms.	Samp. Wt. gms.	Count Date	Std. Cnt. Time	Samp. Count Time	BKG. COUNTS			R226 (pCi/gm)			Lab Tech			
								Area	%Error	Std. Counts	Area	%Error	Conc.				
29	91-2275	Main Tails, Main Tails Toe Misc. Samples South Toe #24 0-2' Down to Malpais (Composite)	1200	1200	9-19-91	30	30	434	73	119960	100.0	23538	5	19.3	0.9	0.63	KS
30	91-2285	Main Tails, Main Tails Toe Misc. Samples South Toe #29 0-2' Above Tails to Malpais (Composite)	1200	1200	9-19-91	30	30	434	73	119960	100.0	13636	7	11.0	0.8	0.63	KS
31	91-2295	Main Tails, Main Tails Toe Misc. Samples South Toe #12 0-2' to Malpais	1200	1200	9-19-91	30	30	434	73	119960	100.0	169152	2	141.2	2.4	0.63	KS
32	91-2305	Main Tails, Main Tails Toe Misc. Samples South Toe #36 Tails Composite	1200	1200	9-19-91	30	30	454	73	119960	100.0	332233	1	277.6	3.3	0.63	KS
33	91-2315	Main Tails, Main Tails Toe Misc. Samples South Toe #37 0-2' Down to Malpais	1200	1200	9-20-91	20	20	35	784	80056	100.0	43689	3	54.6	1.9	0.82	KS
34	91-2325	Main Tails, Main Tails Toe Misc. Samples South Toe #28 Tails Composite	1200	1200	9-20-91	20	20	35	784	80056	100.0	424364	1	530.3	5.7	0.82	KS
35	91-2335	Main Tails, Main Tails Toe Misc. Samples South Toe #29 Tails Composite to Malpais	1200	1200	9-20-91	20	20	35	784	80056	100.0	173927	2	217.3	3.6	0.82	KS
36	91-2345	Main Tails, Main Tails Toe Misc. Samples South Toe #13 Above Tails 0-2'	1200	1200	9-20-91	20	20	35	784	80056	100.0	26649	4	33.3	1.5	0.82	KS
37	91-2355	Main Tails, Main Tails Toe Misc. Samples South Toe #13 Tails Composite	1200	1200	9-20-91	20	20	35	784	80056	100.0	516054	1	644.9	6.3	0.82	KS
38	91-2365	Main Tails, Main Tails Toe Misc. Samples South Toe #34 Below Tails	1200	1200	9-20-91	20	20	35	784	80056	100.0	15925	6	19.9	1.3	0.82	KS
39	91-2375	Main Tails, Main Tails Toe Misc. Samples South Toe #36 Below Tails	1200	1200	9-20-91	20	20	35	784	80056	100.0	108138	2	135.1	2.8	0.82	KS
40	91-2385	Main Tails, Main Tails Toe Misc. Samples South Toe #34 Above Tails	1200	1200	9-20-91	20	20	35	784	80056	100.0	12684	7	15.8	1.2	0.82	KS
41	91-2395	Main Tails, Main Tails Toe Misc. Samples South Toe #28 Above Tails	1200	1200	9-20-91	20	20	35	784	80056	100.0	27673	4	34.5	1.5	0.82	KS
42	91-2405	Main Tails, Main Tails Toe Misc. Samples South Toe #36 Above Tails	1200	1200	9-20-91	20	20	35	784	80056	100.0	6524	9	8.1	0.6	0.82	KS
43	91-2415	Main Tails, Main Tails Toe Misc. Samples South Toe #34 Tails Composite	1200	1200	9-20-91	20	20	35	784	80056	100.0	1072792	1	1340.6	9.4	0.82	KS

MCA Ra-226 Analy. on Soil Samples

#	Sample ID#	Sample Description	Sample Date	Field Tech	Seal Date	Std Wt gms	Samp Wt gms	Count Initial	Count Date	Std. Count	ROI#1, BI-214 609 kev	Std. pC/gm	Area	%Error	Conc	Error	LLD	Tech		
44	91-242S	Main Tails/Main Tails Toe Misc Samples South Toe #13 2' Composite Below Tails	8-20-91	RL/KS	9-20-91	1200	1200	10-18-91	20	35	794	80056	100.0	23545	5	29.4	1.5	0.82	KS	
45	91-243S	Main Tails/Main Tails Toe Misc Samples South Toe #30 0-2' to Melpas	8-20-91	RL/KS	9-20-91	1200	1200	10-18-91	20	35	784	80056	100.0	130729	2	163.3	3.1	0.82	KS	
46	91-244S	Main Tails/Main Tails Toe Misc Samples South Toe #35 Tails Composite to Melpas	8-20-91	RL/KS	9-20-91	1200	1200	10-18-91	20	35	784	80056	100.0	354398	1	480.3	5.3	0.82	KS	
47	91-245S	Main Tails/Main Tails Toe Misc Samples South Toe #35 0-2' Above Tails	8-20-91	RL/KS	9-20-91	1200	1200	10-18-91	20	35	784	80056	100.0	6760	10	8.4	0.9	0.82	KS	
48	91-246S	Main Tails/Main Tails Toe Misc Samples South Toe #13, 28, 32 Top Composite Equal Weight of Each	8-21-91	RL/JS	9-20-91	1200	1200	10-18-91	20	35	784	80056	100.0	23064	5	28.8	1.4	0.82	KS	
49	91-247S	Main Tails/Main Tails Toe Misc Samples South Toe #23 0-2' to Melpas	8-21-91	RL/JS	9-20-91	1200	1200	10-18-91	20	35	784	80056	100.0	3322	17	4.1	0.8	0.82	KS	
50	91-248S	Main Tails/Main Tails Toe Misc Samples South Toe #20 0-10' No Tails	8-21-91	RL/JS	9-20-91	1200	1200	10-18-91	20	35	784	80056	100.0	29788	4	37.2	1.6	0.82	KS	
51	91-249S	Main Tails/Main Tails Toe Misc Samples South Toe #8 0-6' Tails Mix Soil	8-21-91	JS/RL	9-23-91	1200	1200	10-21-91	30	30	881	122206	100.0	135577	2	111.8	2.1	-0.67	SF	
52	91-250S	Main Tails/Main Tails Toe Misc Samples South Toe #5 0-1.5' No Tails	8-21-91	JS/RL	9-23-91	1200	1200	10-21-91	30	30	881	122206	100.0	45870	3	37.6	1.3	-0.67	SF	
53	91-251S	Main Tails/Main Tails Toe Misc Samples South Toe #4 0-2' No Tails	8-21-91	JS/RL	9-23-91	1200	1200	10-21-91	30	30	881	122206	100.0	72780	3	59.6	1.6	-0.67	SF	
54	91-252S	Main Tails/Main Tails Toe Misc Samples South Toe #32 2-4' Source Term	9-10-91	RV	9-23-91	1200	1200	10-21-91	30	30	881	122206	100.0	192116	2	157.2	2.5	-0.67	SF	
55	91-253S	Main Tails/Main Tails Toe Misc Samples South Toe #32 4-6' Source Term	9-10-91	RV	9-24-91	1200	1200	10-22-91	30	30	404	72	121964	100.0	389516	1	320.1	3.6	0.57	SF
56	91-254S	Main Tails/Main Tails Toe Misc Samples South Toe #32 6-8' Source Term	9-10-91	RV	9-23-91	1200	1200	10-21-91	30	30	881	122206	100.0	424263	1	347.1	3.7	-0.67	SF	
57	91-255S	Main Tails/Main Tails Toe Misc Samples South Toe #32 8-10' Source Term	9-10-91	RV	9-23-91	1200	1200	10-21-91	30	30	881	122206	100.0	305694	1	250.1	3.1	-0.67	SF	
58	91-256S	Main Tails/Main Tails Toe Misc Samples South Toe #32 10-12' Source Term Run on 12-19-91, 91-3885	9-10-91	RV	9-24-91	1200	1200	10-22-91	30	30	404	72	121964	100.0	299509	1	246.1	3.1	0.57	SF

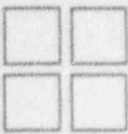
MCA Ra-226 Analy... on Soil Samples

#	Sample ID#	Sample Description	Sample Date	Field Tech	Seed Date	Std Wt. gms.	Samp. Wt. gms.	Count Date	Std. Cnt. Time	Samp. Count	ROA#1, BI-214 609 Key		BKG. COUNTS		SAMPLE COUNTS		Ra226 (pCi/gm)		Lab Tech	
											Initial/28-Day	%Error	Area	%Error	Area	%Error	Conc.	Error*		LLD
59	91-257S	Main Tails; Main Tails Toe Misc. Samples South Toe #32 12-14' Source Term	9-10-91	RV	9-23-91	1200	1200	10-21-91	30	30	-59	881	122206	100.0	268368	1	219.6	2.9	-0.67	SF
60	91-258S	Main Tails; Main Tails Toe Misc. Samples South Toe #32 14-16' Source Term	9-10-91	RV	9-24-91	1200	1200	10-22-91	30	20	404	72	121964	100.0	171400	2	211.4	3.7	0.85	SF
61	91-259S	Main Tails; Main Tails Toe Misc. Samples South Toe #32 16-18' Source Term	9-10-91	RV	9-23-91	1200	1200	10-21-91	30	30	-39	881	122206	100.0	315334	1	258.0	3.2	-0.67	SF
62	91-260S	Main Tails; Main Tails Toe Misc. Samples South Toe #286 3-5' Source Term	9-10-91	RV	9-24-91	1200	1200	10-22-91	30	30	404	72	121964	100.0	337648	1	277.4	3.3	0.57	SF
63	91-261S	Main Tails; Main Tails Toe Misc. Samples South Toe #286 5-7'	9-10-91	RV	9-24-91	1200	1200	10-22-91	30	30	404	72	121964	100.0	595861	1	489.8	4.4	0.57	SF
64	91-262S	Main Tails; Main Tails Toe Misc. Samples South Toe #288 0-2'	9-10-91	RV	9-25-91	1200	1200	10-24-91	30	30	339	86	119780	100.0	29890	4	24.7	1.1	0.58	SF
65	91-263S	Main Tails; Main Tails Toe Misc. Samples South Toe #328 0-2'	9-10-91	RV	9-25-91	1200	1200	10-24-91	30	30	339	86	119780	100.0	1734	31	1.2	0.5	0.58	SF

Engineering Comp:
105 South 1900 West
Provo, Utah 84067
Phone 801-731-XXXX

C

center



ANDERSON Engineering Company, Inc.
4655 South 1900 West St.
Roy, Utah 84067
Telephone 801-731-4596

Southwest Office
P.O. Box 2
Grants, New Mexico 87020

Long Beach Office
231-428-9344

Engineers
Construction Managers

CALCULATION SHEET

JOB Bluewater SHEET NO. _____ CALC JA

CK'D BY _____ DATE 7/26/93 TITLE _____

South Beach

In-place Density

Avg Prc $116.8 \frac{\text{lb}}{\text{ft}^3}$

Avg. Opt 12.2%

3/2/93 40

Avg Sand Conc $115.0 \text{ lb/ft}^3 = 1.84 \text{ gr/cm}^3$

Avg Opt. 12.0%

EVAN
VOR
LW

TABLE 6-1

SOIL AND RADON SOURCE REGIONS AND
THEIR DEFINING PARAMETERS

Region	Effective ^a Present Source Thickness (feet)	Average ^b Radium Concentration (pCi/gram)	Average Radon Emanation Fraction	Average Long-Term Moisture (% dry wt)	Average Radon Diffusion Coefficient (cm ² /s)	
Borrow Soil	---	2.7	---	9.5	0.018	1.34
Main Tailings-Sands	40	103-409	.20	8.0	0.025	
Main Tailings-Mixed	15	242-538	.24	15.0	0.0085	
Main Tailings-Slimes	9	424-522	.20	22.0	0.0011	
Old Acid Tailings	4.7	2023-2214	.24	20.0	0.0010	1.59
East Carbonate T.	10	1030-1601	.30	20.0	0.0025	
North Carbonate T.	7	415-921				
South Carbonate T.	5	1963				
Evap. Ponds	.2-2	37-345	.17	9.5	0.0195	
Stockpile Area	1	53	.41	9.5	0.036	
Fill Area	7	22	.41	10.0	0.0164	
Windblown (W-1 & W-2)	.5-4	34	.32	9.5	0.014	
Windblown (W-3)	1	76.	.30	9.5	0.036	

Total thickness for old acid tailings, evaporation ponds, stockpile area, and windblown areas; extent of sampling for all other areas. Ranges shown for measured, non-uniform regions.

Ranges show maximum variation in averaged vertical concentration profiles.

Disposal Area #2

Test No.	in-place wt	in-place rd	proc wt	proc rd	Asbestos Pb
7	110.8	11.0	114.7	15.4	
8	115.4	10.3	114.7	15.4	
9	112.4	10.5	114.7	15.4	
10	112.2	10.8	114.7	15.4	
11	114.7	12.1	114.7	15.4	
12	114.8	14.7	114.7	15.4	
13	111.8	10.8	114.7	15.4	
14	113.9	13.3	114.7	15.4	
15	112.3	15.4	114.7	15.4	
16	119.5	10.8	114.7	15.4	
17	110.7	13.4	114.7	15.4	
18	118.8	9.8	114.7	15.4	
42	116.2	12.4	114.7	15.4	
56	118.2	12.2	121	11.7	
60	117.5	12.1	121	11.7	
61	123.1	10.3	121	11.7	
62	119.5	9.9	121	11.7	
67	124.8	9	121	12.2	
68	121.9	6.7	120	12.2	
69	116.7	11.4	120	12.2	
90	122	11	120	12.2	Average
94	121.7	11.7	120	12.2	
102	121.9	10.2	122.2	10.5	
104	122.4	10.6	122.2	10.5	
105	120.7	9.5	122.2	10.5	
106	118.9	8.2	122.2	10.5	
107	121	9.9	122.2	10.5	
108	119.1	8.4	122.2	10.5	
111	121	10	122.2	10.5	
112	121	9.1	122.2	10.5	
115	121	8.1	122.2	10.5	
114	111.8	12.8	118.9	14	
116	115.2	12.8	118.9	14	
118	114.3	13.9	118.9	14	
117	112.5	13.1	118.9	14	
118	115.3	13.8	118.9	14	
119	115.1	12	118.9	14	
120	113.8	12.2	118.9	14	
121	114.3	13.3	118.9	14	
122	118.6	13.6	118.9	14	
123	113.8	13.1	118.9	14	
124	114.7	13.2	118.9	14	
125	112.8	12.4	118.9	14	
126	115.5	13.6	118.9	14	
127	118.3	15.5	118.9	14	
154	118.7	13.2	118.8	12.4	
155	119.5	13.1	118.8	12.4	
158	114.4	14.1	118.8	12.4	
157	110.7	12.2	118.8	12.4	
156	117.5	11.8	118.8	12.4	
158	116.9	12.7	118.8	12.4	
160	116.1	12.1	118.8	12.6	
161	119.8	12.2	118.8	12.6	
162	118.9	12.8	118.8	12.6	
163	119.5	12.6	118.8	12.6	
164	117.2	13.1	118.8	12.6	
168	117.8	12.1	118.8	12.6	
166	120	10.8	121.5	11.5	
167	120.2	11.8	121.5	11.5	
168	119	12.3	121.5	11.5	
195	117	11.7	119.1	12.3	
196	120.4	12.5	119.1	12.3	
214	122.7	11.2	119.3	12.5	
215	118.9	13.8	119.3	12.5	
216	119.9	11.5	119.3	12.5	
217	119.5	12.7	119.3	12.5	
230	119.7	11.6	120	13	
231	119.4	11.1	120	13	
233	114.7	12.2	119.1	12.3	
234	119.3	11.3	118.5	12.1	
235	116.7	12.7	118.4	12.7	
236	118.1	12.8	118.5	12.7	
237	112.7	12.4	120.6	12.4	
238	113.3	11.5	120.6	12.4	
239	119.1	11.9	120.6	12.4	
241	111.2	16.4	120.6	12.4	
242	115.9	13.1	120.6	12.4	
Average	117.1	12.3	118.8	12.6	

Test No.	in-place wt	in-place rd	proc wt	proc rd	Disposal Area #2
228	112.1	12.3	118.7	12.3	
229	113.9	12.1	118.7	12.3	
230	119	13.2	118.7	12.3	
231	112.1	12.7	118.7	12.3	
232	118.8	13.2	122.8	10.8	
233	119.5	12.7	123.8	10.8	
234	116.1	13.2	123.8	10.8	
242	118.1	11.8	123.8	10.8	
243	117.9	10.9	123.8	10.8	
250	121.2	12	123.8	10.8	
261	119.7	12.3	123.8	10.8	
174	117.8	10.9	120.1	12.5	
175	114.8	14.8	120.1	12.5	
176	118.7	14.3	120.1	12.5	
177	119.5	10.9	120.1	12.5	
178	118	11.9	120.1	12.5	
179	117.9	15	120.1	12.5	
180	118.5	12.4	120.1	12.5	
181	115.1	13.4	120.1	12.5	
182	113.2	14.5	120.1	12.5	
Average	118.5	12.8	120.8	11.8	

Test No.	in-place wt	in-place rd	proc wt	proc rd	Disposal Area #2
92	112.3	14.9	118.2	14.4	
93	116.9	13.4	118.2	14.4	
94	112.7	15.2	118.2	14.4	
95	118.8	15.9	118.2	14.4	
96	112.4	14	118.2	14.4	
97	109.9	14.5	118.2	14.4	
98	116.2	14	118.2	14.4	
99	116.1	13.8	118.2	14.4	
100	118.3	9.4	122.2	10.5	
101	120.1	9.7	122.2	10.5	
102	118	8.2	122.2	10.5	
218	120.8	11.3	118.4	12.5	
219	119	11	118.4	12.5	
220	117.7	10.7	118.4	12.5	
221	119.6	10.8	118.4	12.5	
222	117.9	12.4	118.4	12.5	
223	118.9	11.4	118.4	12.5	
224	111.8	11.5	121.1	12.1	
225	118.1	11.2	121.1	12.1	
226	114.6	13.1	121.1	12.1	
227	114.6	12.1	121.1	12.1	
228	120.3	10.7	121.1	12.1	
229	121.8	13.2	121.1	12.1	
243	116.3	13.4	118.1	12.9	
244	117.7	11.3	119.1	12.8	
245	115	12.9	119.1	12.8	
246	118.1	12.9	119.1	12.8	
247	116.9	13	119.1	12.8	
248	117.2	12.9	119.1	12.8	
249	119	12.9	119.1	12.8	
250	123.4	11.8	119.1	12.8	
251	118.8	14.5	119.1	12.8	
252	121.1	10.8	119.1	12.8	
253	116.1	11.8	119.1	12.8	
254	123.5	12.8	119.2	12.5	
255	116	12.8	119.2	12.5	
256	120.6	12.8	119.2	12.5	
257	117.7	10.6	119.2	12.5	
258	119.4	12	119.2	12.5	
259	119.9	12.8	119.2	12.5	
260	122.8	12.5	119.2	12.5	
261	115.8	13.9	119.6	13	
262	120.8	9.4	119.9	13	
Average	117.4	12.3	119.1	12.8	

47202

RAECOB/C.BAS

UT INFORMATION : 07:35:55 12-09-1994

BOTTOM FLUX = 0 pCi/m²/sec

AIR CONC. = 0 pCi/l

BARE LAYER 1 FLUX = 4.75 pCi/m²/s

NO OPTIMIZATION APPLIED

L	THICK (cm)	POR	MOIST (%)	SOURC (pCi/g)	E.F.	DENS (g/cm ³)	DIFF COEF	FLUX (pCi/m ² /s)	CONC. (pCi/cm ³)	MIC
2	0.0	.3133	9.5	1	.2	1.84	0.00753	4.75	0.0	0.587
1	20.3	.411	20	37.2	.24	1.59	0.00100	4.75	0.0	0.427

***** TOP *****

- 2 - COVER *

- 1 - SO BENCH TAILINGS *

***** BOTTOM *****

No COVER REQUIRED

ST253

RAECOBPC.BAS

OUTPUT INFORMATION : 17:09:03 12-09-1994

OM FLUX = 0 pCi/m²/sec

AIR CONC. = 0 pCi/l

ARE LAYER 1 FLUX = 85.16 pCi/m²/s

NO OPTIMIZATION APPLIED

L	THICK (cm)	POR	MOIST (%)	SOURC (pCi/g)	E.F.	DENS (g/cm ³)	DIFF COEF	FLUX (pCi/m ² /s)	CONC. (pCi/cm ³)	MIC
3	61.0	.411	20	24.1	.24	1.59	0.00100	1.58	0.0	0.427
2	91.4	.411	20	317.1						
					.24	1.59	0.00100	25.83	159.6	0.427
1	61.0	.411	20	490.9						
					.24	1.59	0.00100	15.52	372.7	0.427

***** TOP *****

- 3 -* 0-2 TAILINGS *

- 2 - 2-5' TAILINGS *

- 1 -* 5-7' TAILINGS *

***** BOTTOM *****

No COVER REQUIRED

ST 29 P3

RAECOBPC.BAS

PUT INFORMATION : 11:57:24 12-09-1994

OM FLUX = 0 pCi/m²/sec

IR CONC. = 0 pCi/l

ARE LAYER 1 FLUX = 22.87 pCi/m²/s

NO OPTIMIZATION APPLIED

L	THICK (cm)	POR	MOIST (%)	SOURC (pCi/g)	E.F.	DENS (g/cm ³)	DIFF COEF	FLUX (pCi/m ² /s)	CONC. (pCi/cm ³)	MIC
3	50.0	.3133	9.5	1	.2	1.842	0.00753	9.00	0.0	0.587
2	15.2	.411	20	11	.24	1.59	0.00100	11.89	15.3	0.427
1	15.2	.411	20	217.4						
					.24	1.59	0.00100	15.61	64.1	0.427

***** TOP *****

- 3 -* COVER *

- 2 -* 0-0.5' TAILINGS *

- 1 -* 0.5-1' TAILINGS *

***** BOTTOM *****

No Cover Required

ST 30B

RAECORPC.BAS

UT INFORMATION : 10:02:36 12-09-1994

BOTTOM FLUX = 0 pCi/m²/sec

AIR CONC. = 0 pCi/l

BARE LAYER 1 FLUX = 28.19 pCi/m²/s

LAYER 2 ADJUSTED TO GIVE FLUX OF 20 pCi/m²/s FROM LAYER 2

L	THICK (cm)	POR	MOIST (%)	SOURC (pCi/g)	E.F.	DENS (g/cm ³)	DIPP COEF	FLUX (pCi/m ² /s)	CONC. (pCi/cm ³)	MIC
2	37.2	.3133	9.5	1	.2	1.842	0.00753	20.00	0.0	0.587
1	54.9	.411	20	163.4	.24	1.59	0.00100	23.67	24.3	0.427

***** TOP *****

- 2 -* COVER *

- 1 -* 0-1.8' TAILINGS *

***** BOTTOM *****

$$\frac{37.2 \text{ cm}}{2.54 \text{ cm}} \left(\frac{\text{cm}}{12 \text{ in}} \right) = 1.2 \text{ ft.}$$

ST32B

RAECOBPC.BAS

INPUT INFORMATION : 11:50:32 12-09-1994

GM FLUX = 0 pCi/m²/sec

AIR CONC. = 0 pCi/l

ARE LAYER 1 FLUX = 48.12 pCi/m²/s

NO OPTIMIZATION APPLIED

L	THICK (cm)	POR	MOIST (%)	SOURC (pCi/g)	E.F.	DENS (g/cm ³)	DIFF COEF	FLUX (pCi/m ² /s)	CONC. (pCi/cm ³)	MIC
7	20.0	.3113	9.5	1	.2	1.842	0.00753	1.83	0.0	0.587
6	61.0	.411	20	1.2	.24	1.59	0.00100	0.89	5.8	0.427
5	61.0	.411	20	157.3	.24	1.59	0.00100	0.88	150.7	0.427
4	61.0	.411	20	320.5	.24	1.59	0.00100	0.11	298.2	0.427
3	61.0	.411	20	347.6	.24	1.59	0.00100	-0.51	320.0	0.427
2	61.0	.411	20	250.3	.24	1.59	0.00100	-8.38	278.4	0.427
1	213.4	.411	20	275.3	.24	1.59	0.00100	1.66	246.8	0.427

***** TOP *****
- 7 -* COVER *

- 6 -* 0-2' TAILINGS *

- 5 -* 2'-4' TAILINGS *

- 4 -* 4'-6' TAILINGS *

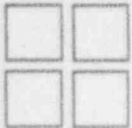
- 3 -* 6'-8' TAILINGS *

- 2 -* 8'-10' TAILINGS *

- 1 -* 10'-17' TAILINGS * ASSUMED DEPTH BASED ON TOPOG *

***** BOTTOM *****

No COVER REQUIRED



ANDERSON Engineering Company, Inc.
4655 South 1900 West St.
Roy, Utah 84067
Telephone 801-731-4596

Southwest Office
P.O. Box 2
Grants, New Mexico 87020

Long Beach Office
231-428-9344

Engineers
Construction Managers

CALCULATION SHEET

JOB Blankets SHEET NO. _____ CALC SA

CK'D BY _____ DATE 10 Dec 93 TITLE Erosion -

NOTE Calculations for South Branch

$R = 40$ Table 5.1 NUREG 4620

Assume topsoil similar to Composite #9 in ARLO Rec. Plan

% silt and very fine particle (0.002 mm - 0.1 mm) = 13%

% sand (0.1 mm - 2 mm) = 68%

% organic = assume 1%

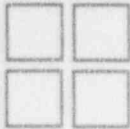
$K = 0.08$ from Fig 5.1 NUREG 4620

$$LS = \frac{650 + 450s + 65s^2}{10,000 + s^2} \quad \frac{L}{72.6} \text{ m}$$

$L = 500 \text{ ft.}$ $m = 0.2$ (NUREG 4620, Table 5.2)

$s = 0.25\%$

$$LS = \frac{650 + 450(.25) + 65(.25)^2}{10,000 + 0.25^2} \left(\frac{500}{72.6} \right)^{1.5} = 110 (10^{-3})$$



ANDERSON Engineering Company, Inc.
4655 South 1900 West St.
Roy, Utah 84067
Telephone 801-731-4596

Southwest Office
P.O. Box 2
Grants, New Mexico 87020

Long Beach Office
231-428-9344

Engineers
Construction Managers

CALCULATION SHEET

JOB Blumentown SHEET NO. 2/2 CALC FA

CK'D BY _____ DATE 10 Dec 93 TITLE _____

assume disked topsoil VM-1

$$\begin{aligned} A &= \text{FIELDS}(VM) \\ &= 40(0.08)(110(10^{-3})) \\ &= 350(10^{-3}) \frac{\text{tons-yr}}{\text{acre}} \end{aligned}$$

$$= 0.35 \frac{\text{tons}}{\text{acre-yr}} \left(\frac{2000 \text{ lb}}{\text{ton}} \right) \frac{\text{acre-yr}}{\text{acre-yr}} \quad \text{assume loose condition}$$

$$= 700 \frac{\text{lb}}{\text{yr-acre}} \left(\frac{\text{ft}^3}{83.5 \text{ lb}} \right) \left(\frac{\text{acre}}{43560 \text{ ft}^2} \right)$$

$$= 190(10^{-6}) \text{ ft/yr} \quad \text{assume 1000 yr. design}$$

$$= 1000 \text{ yr} \left(190(10^{-6}) \text{ ft/yr} \right) = 190(10^{-3}) \text{ ft} = 2.3 \text{ in}$$

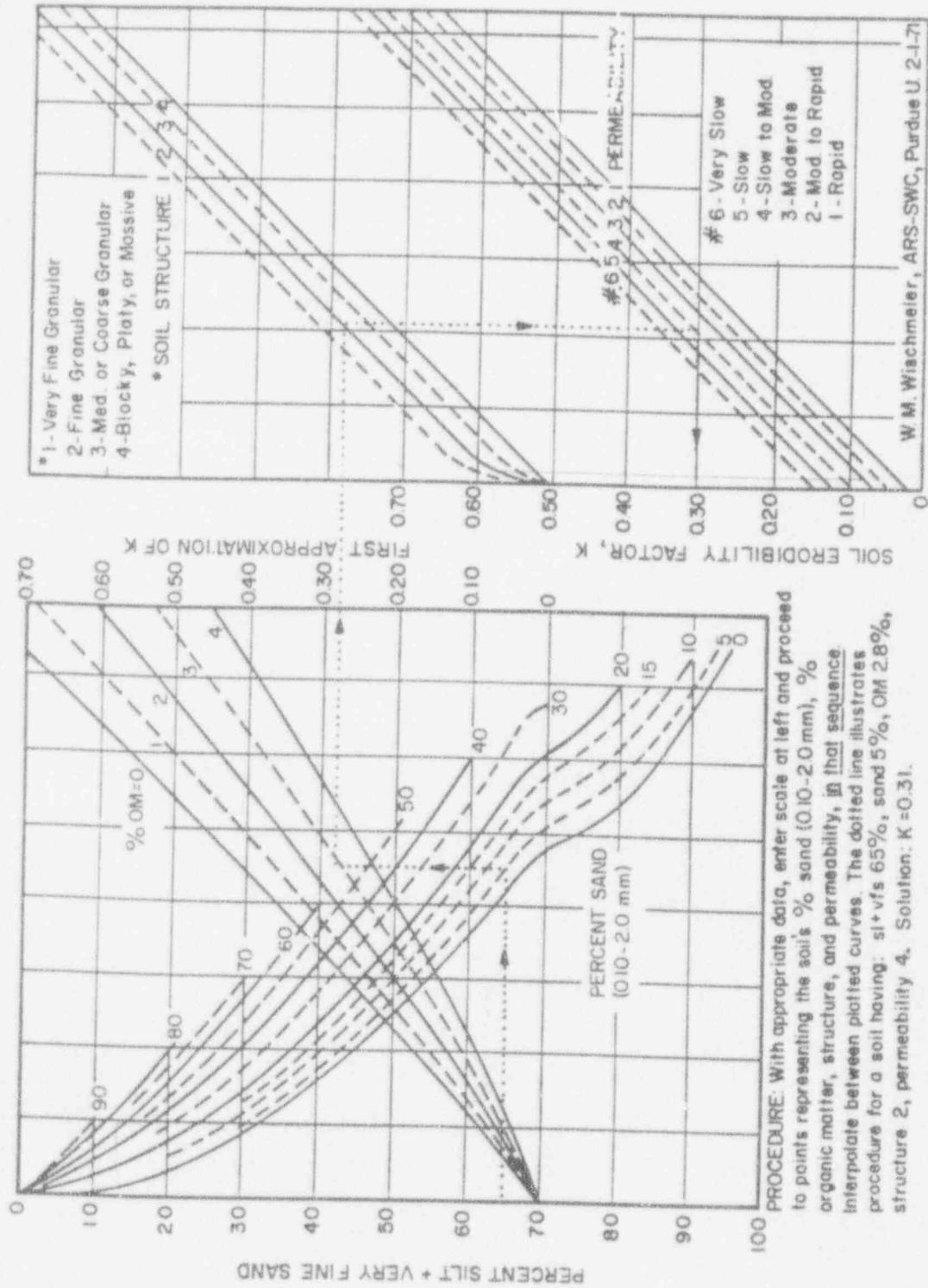
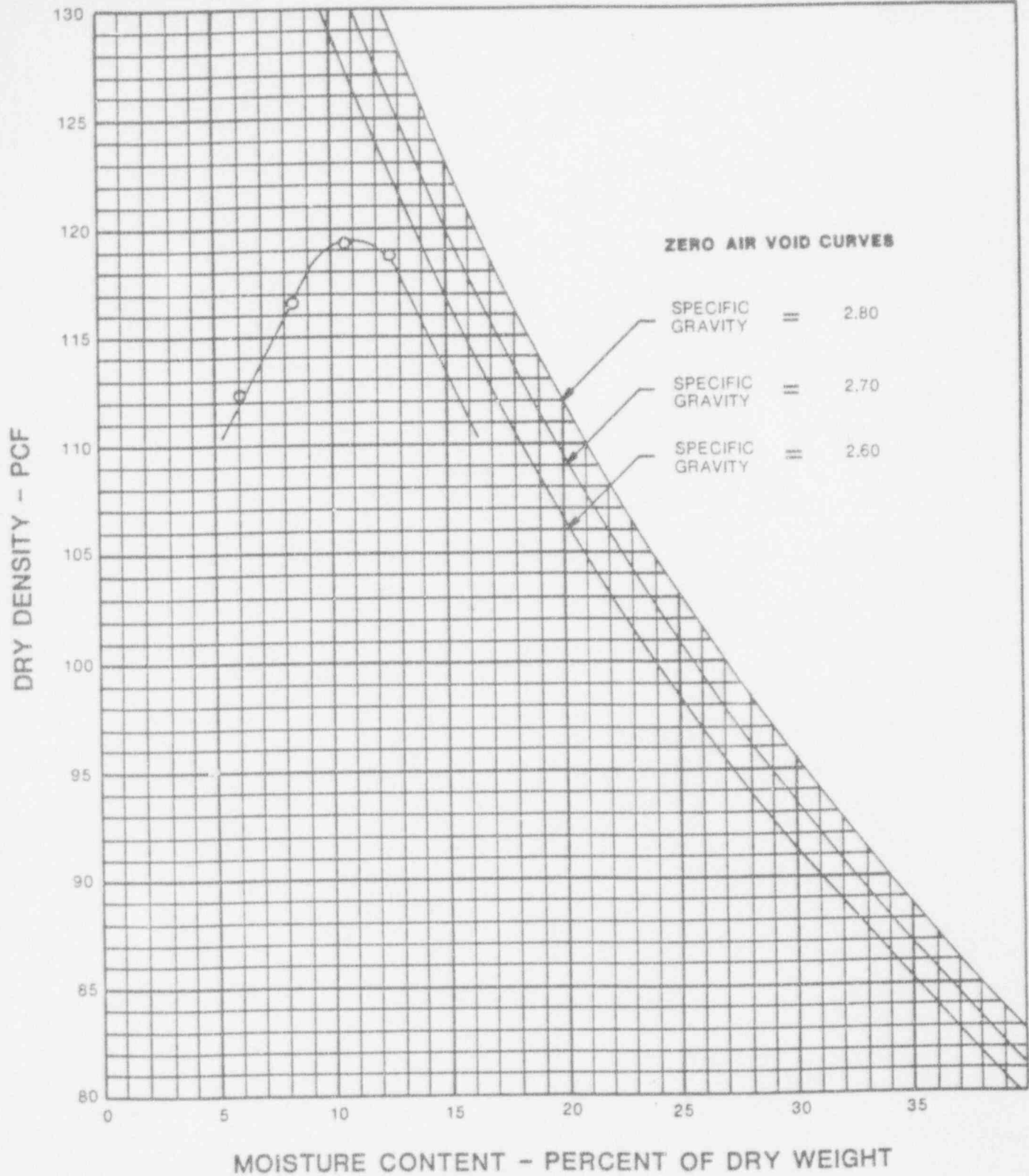


Fig. 5.1. Nomograph for determining soil erodibility factor K. Source: after Wischmeier et al., 1971.



LOCATION: Composite #9	MOISTURE-DENSITY RELATIONSHIPS	
HOLE NO.: DEPTH: SAMPLE NO.: B-17		
SOIL DESCRIPTION: Silty sand	Chen & Associates	
MAX. DRY DENSITY: 119.3 PCF	OPT. MOIST. CONTENT: 11.0 %	PROCEDURE: ASTM D 698-78 Method A
LIQUID LIMIT: _____	PLASTICITY INDEX: Nonplastic	JOB NO.: 1 633 87
GRAVEL: 0 % SAND: 78 % SILT AND CLAY (-200): 20 %	DATE: August 5, 1987	FIG. NO. 15

5.1.2.1 The Rainfall and Runoff Factor (R)

As noted by previous research at Los Alamos National Laboratory (Nyhan and Lane, 1983), the R factor as used in the MUSLE is often misinterpreted only as a rainfall factor. In reality, it must quantify both the raindrop impact and provide information on the amount and rate of runoff likely to be associated with the rain. More specifically, the R factor is described in terms of a rainfall storm energy (E) and the maximum 30-minute rainfall intensity (I_{30}). Generalized R factors applicable to the interior western United States are given in Table 5.1. For R factors in specific areas of the United States, it is recommended that erosion index distribution curves be obtained from local SCS offices.

Table 5.1. Generalized Rainfall and Runoff (R) Values.

State	Eastern Third	Central Third	Western Third
N. Dakota	50 - 75		
S. Dakota	75 - 100	40 - 50	40
Montana	30 - 40	50	40
Wyoming	30 - 50	20	20 - 50
Colorado	75 - 100	15 - 30	15 - 25
Utah	20 - 30	40 - 50	20 - 40
New Mexico	75 - 100	20 - 50	15 - 40
Arizona	20 - 50	40 - 50	20 - 40
		20 - 50	25 - 40

5.1.2.2 The Soil Erodibility Factor (K)

The soil erodibility factor (K) recognized the fact that the erodibility potential of a given soil is dependent on its compositional makeup, which in turn reflects the grain size distribution of the soil. To predict soil erodibility, five soil characteristics that include the percent silt and fine sand, percent sand greater than 0.1 mm, percent organic material, general soil structure and general permeability are determined. The K factor is then found by using the Wischmeier nomograph presented in Figure 5.1.

The makeup of the various soil fractions presented in Figure 5.1 is based on separating sand and silt at the 0.1 mm size. This differs from the Unified Soil Classification System which uses the No. 200 sieve size (0.075 mm) for the separation between sand and silt. The value to enter Figure 5.1 with should be the percentage of material finer than 0.1 mm in size, not the percentage passing the No. 200 sieve. Also, the determination of the Soil Erodibility Factor (K) as shown on Figure 5.1 does not specifically reference the percentage of clay (finer than 0.002 mm) contained in the material. The percentage of silt plus very fine sand to be used for Figure 5.1, therefore, is the percentage of material contained between 0.002 mm and 0.1 mm.