

ATTACHMENT B  
ZION NUCLEAR POWER STATION  
PROPOSED CHANGES TO  
TECHNICAL SPECIFICATIONS CHANGE 91-01

PAGE(s) MODIFIED

212  
213  
214  
214a

PAGE(s) ADDED

NONE

PAGE(s) DELETED

NONE

ZOSR-6(11)

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### LIMITING CONDITIONS FOR OPERATION

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#### 3.10 CONTAINMENT STRUCTURAL INTEGRITY (per unit)

##### OBJECTIVE:

To insure that the containment structure meets its design requirements throughout plant life.

##### SPECIFICATION:

1. Containment Leakage Rate Testing
  - A. Containment Leakage Rate shall be limited to:
    1. An overall integrated leakage rate of:
      - a. Less than or equal to  $L_a$ , 0.10 percent by weight of the containment air per 24 hours at  $P_a$  (47 psig), or
      - b. Less than or equal to  $L_t$ , where  $L_t$  is as computed in 10CFR 50 Appendix J, is the maximum allowable leakage rate at pressure  $P_t$  (25 psig)
    - 2.\* A combined leakage rate of less than or equal to 0.60  $L_a$ , for all penetrations and valves subject to Type B and C tests, when pressurized to  $P_a$ .

APPLICABILITY: Modes 1, 2, 3, 4 and 7

\*Refer to note on page 214.

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### SURVEILLANCE REQUIREMENT

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#### 4.10 CONTAINMENT STRUCTURAL INTEGRITY (per unit)

##### OBJECTIVE:

To establish the testing requirements to assure containment structural integrity.

1. Containment Leakage Rate Testing
  - A. Surveillance and testing of the containment shall be performed as follows:
    1. The containment Type A leakage rate shall be determined in conformance with 10CFR50 Appendix J.
      - a. The leakage rate test shall be performed at or above the design basis accident pressure  $P_a$  (47 psig), or at or above the reduced pressure  $P_t$  (25 psig).
      - b. Deleted

Amendment Nos.

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## LIMITING CONDITIONS FOR OPERATION

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3.10.1.A (Continued)

ACTION:

- \* With either (a) the measured overall integrated containment leakage rate exceeding  $0.75 L_a$  or  $0.75 L_t$ , as applicable, or (b) with the measured combined leakage rate for all penetrations and valves subject to Type B and C tests exceeding  $0.60 L_a$ , restore the overall integrated leakage rate to less than or equal to  $0.75 L_a$  or less than or equal to  $0.75 L_t$ , as applicable, and the combined leakage rate for all penetrations subject to Type B and C tests to less than or equal to  $0.60 L_a$  prior to entering MODE 4.

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## SURVEILLANCE REQUIREMENT

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- 4.10.1.A.1. c. The maximum allowable leakage rate  $L_a$  or  $L_t$ , as applicable, shall be computed in accordance with the appropriate paragraphs of 10CFR50 Appendix J.
- 2.\* Type B and C tests (except air lock tests) shall be performed at  $P_a$  or above in accordance with the provisions of the appropriate Section of 10CFR50 Appendix J.
  3. Air locks shall be tested and demonstrated OPERABLE per Surveillance Requirement 4.10.2.
  - 4.\* Type A, B, and C leakage rate tests shall be considered to be satisfactory if the acceptance criteria delineated in 10CFR50 Appendix J are met.
  5. Leakage from containment isolation valves sealed by the Isolation Valve Seal Water system may be excluded from the combined Type B and C leakage rate.

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LIMITING CONDITIONS FOR OPERATION

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3.10.1.A (Continued)

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SURVEILLANCE REQUIREMENT

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- 4.10.1.A. 6.\* The retest schedules for Type A, B, and C tests shall be in accordance with the appropriate Section of 10CFR50 Appendix J.
7. Inspection and reporting of tests shall be in accordance with the appropriate Section of 10CFR50 Appendix J.

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\*Prior to startup following Z1C12 and Z2C12 operating cycles:

- 1) The Type C leak rate testing requirements of this specification are not applicable to Unit 1 penetration P-80 (line 1RC158-4" AA-R), and Unit 2 penetration P-80 (line 2RC158-4" AA-R). Note 3 does not apply.
- 2) The local leak rate testing requirements of the February 29, 1980, Zion Confirmatory Order, Appendix A, Item A.3, Annex 1, Part 2, are not applicable to Unit 1 penetrations P-76 (line 1SI020-3/4" E-R) and P-80 (line 1RC158-4" AA-R), and Unit 2 penetrations P-76 (line 2SI020-3/4" E-R) and P-80 (line 2RC158-4" AA-R). Note 3 does not apply.
- 3) The Type C leak rate testing requirements of this specification and the local leak rate testing requirements of the February 29, 1980, Zion Confirmatory Order, Appendix A, Item A.3, Annex 1, Part 2, are not applicable to the untested Unit 1 and 2 containment pathways evaluated during the "Zion Containment Local Leak Rate Testing Self-Assessment" until after March 11, 1991, at 11:59 pm. This note applies only to pathways evaluated and found acceptable based on the criteria established in the technical justification provided in support of this request (Reference: February 13, 1991, letter from S. F. Stimac to T. E. Murley).

Amendment Nos.

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### LIMITING CONDITIONS FOR OPERATION

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- 3.10.2 Containment Air Locks
- A. Each containment air lock shall be OPERABLE with:
1. Both doors closed except when the air lock is being used for normal entry and exit through the containment, then at least one air lock door shall be closed, and
  - 2.\* The air lock leakage rate, when combined with other Type B and C test results, shall be less than or equal to  $0.50 L_a$  at 47 psig ( $P_a$ ).

APPLICABILITY: Modes 1, 2, 3, 4 and 7

ACTION:

- a.) With one containment air lock door inoperable:
1. Maintain at least the OPERABLE air lock door closed and either restore the inoperable air lock door to OPERABLE status within 24 hours or lock the OPERABLE air lock door closed.
  2. Operation may continue until performance of the next required overall air lock leakage test provided that the OPERABLE air lock door is verified locked closed at least once per 31 days,
  3. Otherwise be in at least MODE 3 within the next 6 hours and MODE 5 within the following 30 hours.

\* Refer to note on page 214.

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### SURVEILLANCE REQUIREMENT

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- 4.10.2. Containment Air Locks
- A. Each air lock shall be demonstrated OPERABLE:
- i. Within 72 hours following each opening (except when the air lock is being used for multiple entries, then at least once per 72 hours);
    - a. Verify that the leakage rate from the air lock door seals is less than or equal to 1.0 SCFH at a test pressure ( $F_{tr}$ ) of greater than or equal to 2.5 psig; or verify that the leakage rate from the air lock door seals is less than or equal to 4.75 SCFH at a test pressure ( $P_t$ ) of greater than or equal to 10.0 psig.
    - b. If the air lock door seal test identifies a leakage rate greater than 1.0 SCFH at a test pressure ( $P_{tr}$ ) of greater than or equal to 2.5 psig or 4.75 SCFH at a test pressure ( $P_t$ ) of greater than or equal to 10.0 psig, then an overall air lock leakage test shall be performed at a pressure ( $P_a$ ) of 47 psig or greater. The acceptance criteria shall be as stated in 3.10.2.A.2.

Amendment Nos.



ATTACHMENT C  
EVALUATION OF SIGNIFICANT HAZARDS CONSIDERATIONS

Commonwealth Edison has evaluated this proposed amendment and determined that it involves no significant hazards considerations. According to 10CFR 50.92(c), a proposed amendment to an operating license involves no significant hazards considerations if operation of the facility in accordance with the proposed amendment would not:

- 1) Involve a significant increase in the probability or consequences of an accident previously evaluated; or
- 2) Create the possibility of a new or different kind of accident from any accident previously evaluated; or
- 3) Involve a significant reduction in a margin of safety.

The proposed change does not involve a significant increase in the probability or consequences of an accident previously evaluated. With respect to an increase in the probability of previously evaluated accidents, leakage through the containment penetrations does not alter or change initiating aspects of the events since containment leakage paths are not initiators or precursors to previously evaluated accidents. With regards to the consequences of accidents previously evaluated, the subject pathways and associated containment isolation barriers provide the necessary assurance to conclude that the overall containment leakage rates will remain within the limits assumed in the accident analysis. This conclusion can be reached, since many of the isolation barriers of the subject pathways are of seismic design; missile protected; connected to the isolation valve seal water system; and/or have demonstrated overall containment integrity under the successfully completed Containment Integrated Leak Rate Test (Type A) performed in 1988 for both units; are of similar design and exposed to similar environments as those of penetrations that are currently Type C tested. As such, the consequences of previously evaluated accidents, with respect to offsite dose considerations, would not be significantly impacted.

The proposed changes do not create the possibility of a new or different kind of accident from any previously analyzed. The proposed changes do not result in plant operations or configurations that could create a new or different type of accident. Any compensatory measures which have been/may be implemented have been/will be evaluated to ensure they do not result in any component or system being placed in an unanalyzed configuration.

The proposed changes do not represent a significant reduction in a margin of safety. As described in the Technical Specification Bases, dose calculations suggest that the public exposure would be well below the 10CFR 100 values in the event of a design basis accident.

Calculations indicate that the accident leak rate could be allowed to increase to approximately 0.148%/day before the guideline thyroid dose value given in 10CFR 100 would be exceeded. However, the 0.1%/day pre-operational test acceptance criteria provides an adequate margin of safety to assure the health and safety of the general public. Additional margin is achieved by establishing the allowable operational leakage rate at 0.075%/day. The as measured containment integrated leakage for Unit 1 during the March, 1988 Type A test was 0.0266%/day, and the as measured containment integrated leakage for Unit 2 during the October, 1988 Type A test was 0.0197%/day. Despite the lack of local leak testing, substantial barriers to fission product release are provided by the intact system piping and associated valves. These barriers provide mitigating capabilities such that the potential impact on the margin of safety is insignificant.



ATTACHMENT D  
ENVIRONMENTAL ASSESSMENT FOR PROPOSED CHANGES

The request does not involve a change in the installation or use of the facilities or components located within the restricted areas as defined in 10CFR20. Commonwealth Edison has determined that this change does not involve a significant increase in the amount, or a significant change in the types, of any effluent that may be released off-site and that there is no significant increase in individual or cumulative occupational radiation exposure. Accordingly, this change meets the eligibility criteria for categorical exclusion set forth in 10CFR Section 51.22(c)(9). Pursuant to 10CFR51.22(b), no environmental impact statement or environmental assessment need be prepared in connection with granting of the change.

ATTACHMENT E  
SUPPORTIVE DOCUMENTATION

- UFSAR page 6.6-3
- UFSAR Table 6.6.5-i sheet 5
- Penetration 76 Simplified Diagram (Unit 1)
- Penetration 76 Simplified Diagram (Unit 2)
- Penetration 80 Simplified Diagram (Unit 2)

#### 6.6.2.1.4 Class 4 - Missile Protected

Incoming and outgoing lines which penetrate the containment and are connected to closed systems inside the containment and protected from missiles throughout their length are provided with at least one manual isolation valve located outside the containment. Seal water injection is not required for this class of penetration.

#### 6.6.2.1.5 Class 5 - Normally Closed Lines Penetrating the Containment

Lines which penetrate the containment and which can be opened to containment atmosphere, but which are normally closed during reactor operation are provided with two isolation valves in series, either inside or outside the containment. In certain cases a blind flange or closed system outside the containment is utilized as the second barrier in lieu of an isolation valve.

#### 6.6.2.1.6 Class 6 - Special Service

The ventilation purge duct penetrations, the containment access opening, and the fuel transfer tube are special cases.

Each ventilation purge duct penetration is provided with two butterfly valves which are closed automatically upon a containment isolation or a containment high radiation signal. One valve is located inside and one valve is located outside the containment at each penetration.

The equipment access closure is a bolted, gasketed closure which is sealed during reactor operation. The personnel air locks consist of two doors in series with mechanical interlocks to assure that one door is closed at all times. Each air lock door and the equipment closure are provided with double gaskets to permit pressurization between the gaskets by the Penetration Pressurization System.

The fuel transfer tube penetration inside the containment is designed to present a missile protected and pressurized double barrier between the containment atmosphere and the atmosphere outside the containment. The penetration closure is treated in a manner similar to the equipment access hatch. A positive pressure is maintained between these gaskets to complete the double barrier between the containment atmosphere and the inside of the fuel transfer tube. The interior of the fuel transfer tube is not pressurized. Seal water injection is not required for this penetration.

#### 6.6.2.1.7 Class 7 - Lines Required for Post-Accident Service

Lines which are required for post-accident service have power operated valves which are either normally open and must remain open during an accident or are normally closed and must be opened should an accident occur. For such lines a minimum one valve outside the containment is provided for containment isolation when the system is no longer required.

TABLE 6.6.5-1 (Cont'd)

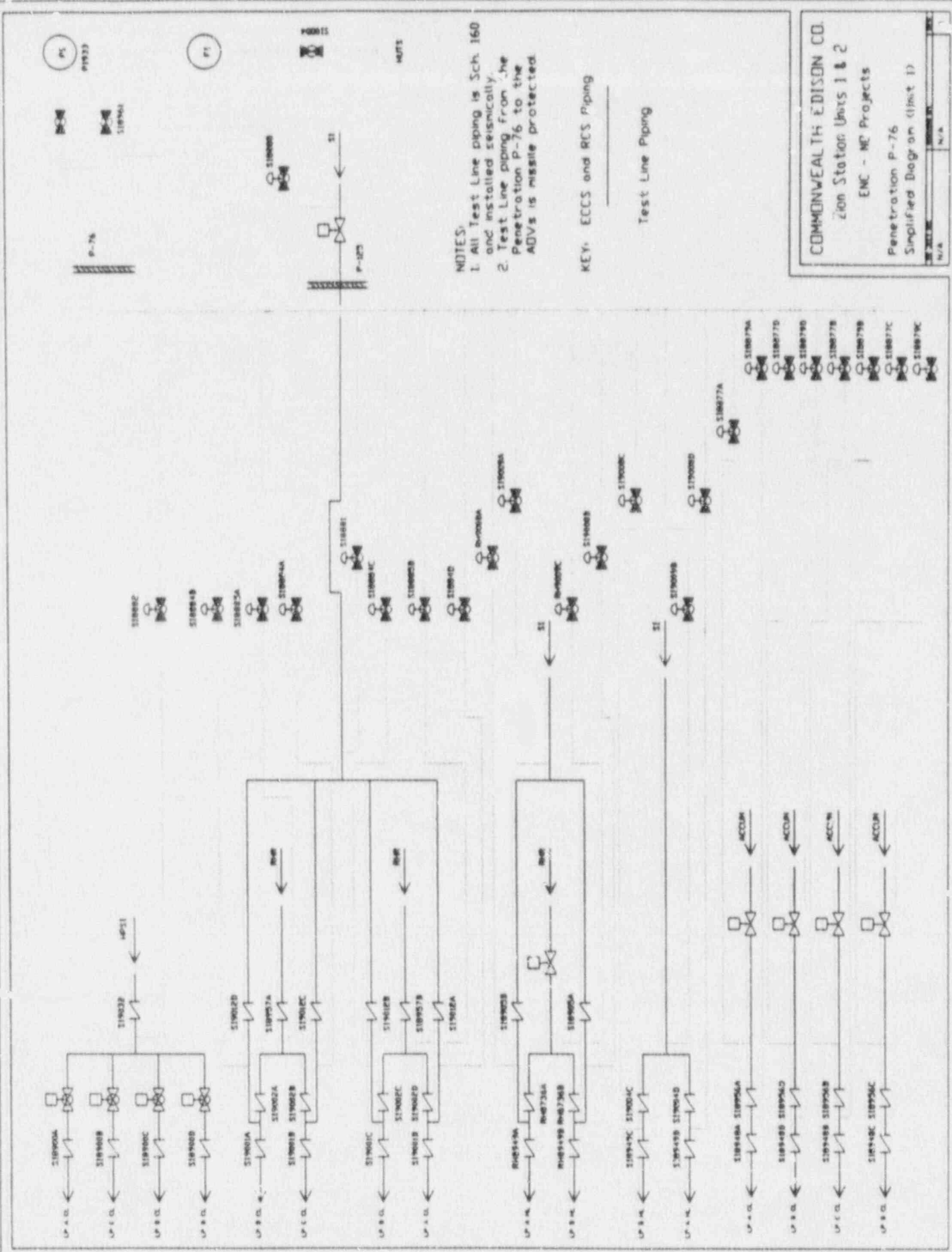
Sheet 5 of 6

CONTAINMENT ISOLATION AND ISOLATION VALVE SEAL WATER

<u>Penetration</u>	<u>Line Size</u>	<u>INSIDE</u>		<u>OUTSIDE</u>		<u>Penetration Class</u>	<u>IVSW+</u>
		<u>Barrier(s)</u>	<u>Isolation Signal</u>	<u>Barrier(s)</u>	<u>Isolation Signal</u>		
Aux FW Pump Steam Line Drain	2"			2 AOV	T	2	A
Heating Water Supply	2"			2 AOV	T	5	A
Heating Water Return	2"			2 AOV	T	5	A
Purification Pump from Refueling Cavity	3"			2 NC Manual valves		5	A
Primary Water to Pressurizer Relief Tank	3"			2 AOV	T	4	A
Steam to Auxiliary Feedwater Pump (3)	6"	Missile Protected		MOV		7	None
Cold Leg Safety Injection	3"	Check Valve		MOV		7	None
Steam Generator Blowdown Sample (3)	3/4"	Missile Protected		AOV	T	4	None
Accumulator Tank Sample	3/8"			2 AOV	T	2	A
Accumulator Nitrogen Supply	1"	Missile Protected & Check Valve		AOV	T	4	None
Loop Fill Header	2"	Check Valve		2 NC Manual valves		5	A
Accumulator Test Line	3/4"	Missile Protected		NC Manual Valve		4	None

Rev. 1  
December 31, 1982





NOTES:  
1. All Test Line piping is Sch. 160 and installed seismically.  
2. Test Line piping from the Penetration P-76 to the ADVs is missile protected.

KEY: ECCS and RCS Piping  
Test Line Piping

COMMONWEALTH EDISON CO  
zion Station Units 1 & 2  
ENC - NE Projects  
Penetration P-76  
Simplified Diagram (Sheet 1)

DATE	NO.	BY

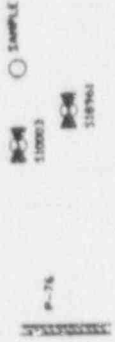
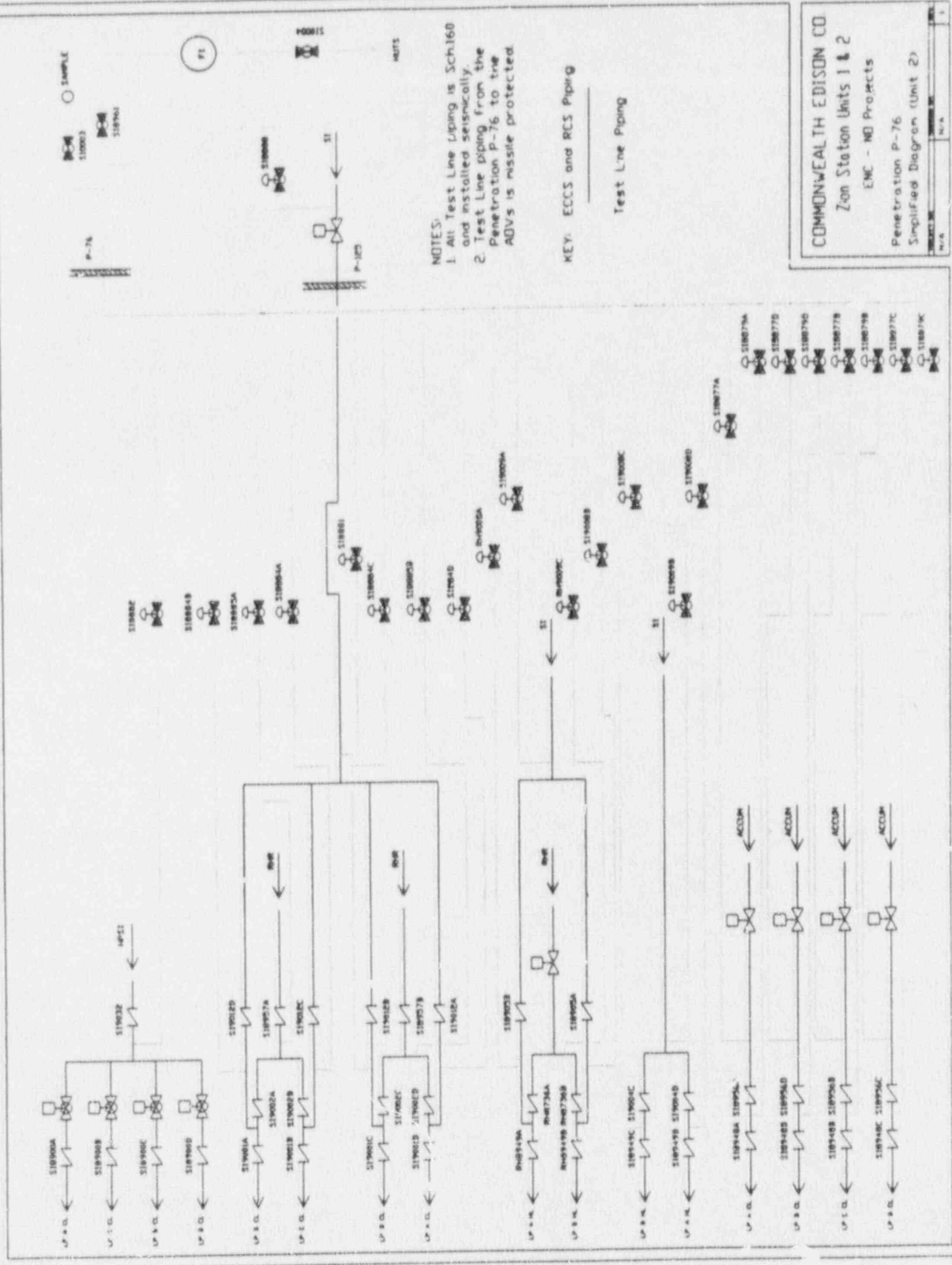
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PT

400 II

400 II

- S180076A
- S180077D
- S180079D
- S180077B
- S180079B
- S180077C
- S180079C
- S180077A
- S180080D
- S180080C
- S180080B
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- S180092F
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- S180092H
- S180092I
- S180092J
- S180092K
- S180092L
- S180092M
- S180092N
- S180092O
- S180092P
- S180092Q
- S180092R
- S180092S
- S180092T
- S180092U
- S180092V
- S180092W
- S180092X
- S180092Y
- S180092Z



F1

FOOTING

VALVES

NOTES:  
 1. All Test Line Piping is Sch.160 and installed seismically.  
 2. Test Line piping from the Penetration P-76 to the ADVs is missile protected

KEY: ECCS and RCS Piping

Test Line Piping

COMMONWEALTH EDISON CO  
 Zion Station Units 1 & 2  
 ENC - NO Projects  
 Penetration P-76  
 Simplified Diagram (Unit 2)

DATE	NO.	BY	CHK

