

CLIENT NO.: WEP 0107-001.7

SNC NO.: \_\_\_\_\_

## DESIGN CALCULATIONS

VSC-24 CRITICALITY SAFETY ANALYSIS  
(PALISADES FUEL WITH BORATED WATER)

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### REVISION CONTROL SHEET

<u>Revision</u>	<u>Reason</u>	<u>Affected Pages</u>	<u>Preparer</u>	<u>Checker</u>	<u>Project Eng.</u>
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0	Initial Issue		HHT	MDC	
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1	Convert Byron Conc to Weight PPM	1, 3, 5-10, 14, 21, 22, 24, 25, 25, 30-38, 40, 41, 45, 48, 50-52, 54, 59-62, 64-66, 68, 71, 72, Appendix A, B, C, D, E, F, G, H, I, J, K, L, M, N, O, P, Q, R, S, T, U, V, W, X, Y, Z	MDC	JPM	JPM
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WEP 114.003.5

### SIGNATURES

<u>Title</u>	<u>Initials</u>	<u>Date</u>
Henry Hung Tran (Nuclear Engineer)	HHT	2/15/90
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John J. [unclear]	JJM	11-13-90
_____	_____	_____
_____	_____	_____
_____	_____	_____

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## 1. INTRODUCTION

This calculation is an extension of the calculation package entitled VSC-24 Criticality Safety Analysis for Palisades ISFSI (Ref. 12). Criticality analysis in this calculation package will consider natural boron dissolved in pool water as a means to control criticality rather than burnup credit of spent fuel. All loading fuel assemblies in this calculation are unirradiated (fresh fuel). Otherwise specified, all assumptions and input parameter from the previous calculation remain unchanged in this calculation.

The stainless steel in the previous KENO models of Ref. 12 is replaced with carbon steel. The atomic densities of various materials used in this calculation are given in Table 1.

TABLE ①

## Atomic Densities of Various Materials

<u>MATERIAL</u>	<u>Elements</u>	<u>Atom Densities</u> <u>[atoms/barn-cm]</u>
WATER (70F)	H	6.67E-2
	O	3.34E-2
WATER (212F)	H	6.41E-2
	O	3.20E-2
CARBON STEEL	Fe	8.28E-2
	C	2.61E-4
	Si	1.90E-4
	Mn	1.09E-3
LEAD	Pb	3.30E-2
ZIRCONIUM	Zr	4.29E-2
RX-277	H	2.77E-2
	B-11*	1.46E-3
	O	3.71E-2
	Na	2.60E-4
	Mg	2.08E-4
	Al	8.97E-3
	Si	7.67E-4
	Fe	4.89E-5
ORDINARY CONCRETE	H	1.49E-2
	C	3.81E-3
	O	4.15E-2
	Ca	1.16E-2
	Si	6.04E-3
	Mg	5.87E-4
	Fe	1.97E-4
	Al	7.35E-4
	Na	3.04E-4

\* Natural Boron

## 2. RESULTS & ANALYSIS

### 2.1 Summary of Calculated Results:

Table(2-1) is the summary of the results obtained from the k-effective calculations of the VSC cask system. From these results, many other parameters pertinent to the criticality safety of the VSC cask system can be estimated or derived. Figure(2-1) indicates the acceptable combinations of U-235 initial enrichment and boron concentration in pool water to have the system k-eff less than 0.95 and 0.98. The following subsections will give a detail description of the approach to construct this curve.

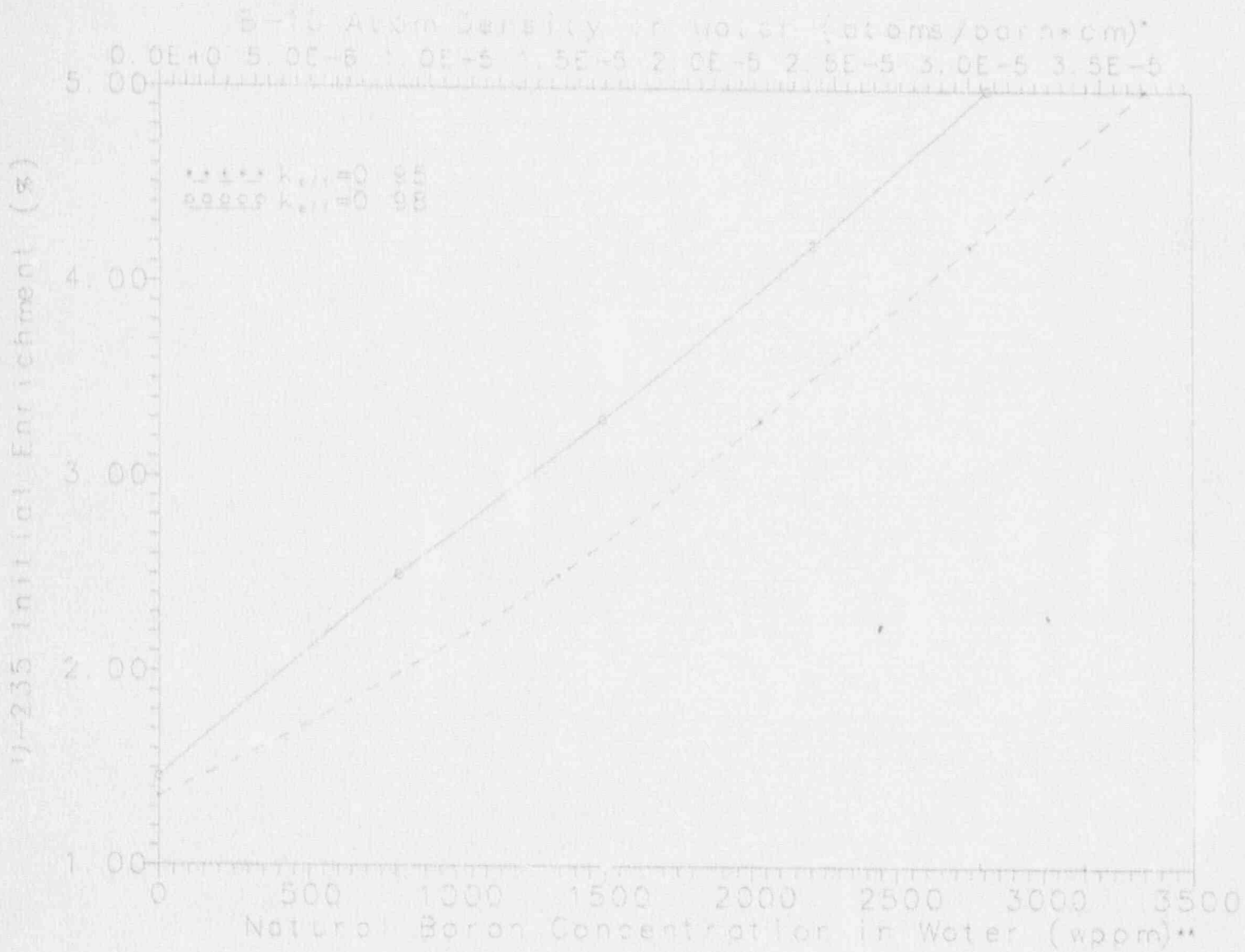
Figure (2-2) includes the  $k_{\infty}$  results from the NULIF computer analyses. The  $k_{\infty}$  as a function of Boron concentration for different fuel enrichments is presented in Figure (2-3).

TABLE 2-1

SECTION	ENRICHMENT	NAT. BORON [WPPM]	AVERAGE K-EFF	1-SIGMA	FINAL* K-EFF
4.1	3.30%	1800	0.9376	0.004	0.9586
4.2	3.30%	2040	0.9243	0.003	0.9433
4.3	2.50%	1080	0.9398	0.003	0.9588
4.4	4.20%	2760	0.9228	0.004	0.9438
4.5	5.00%	3360	Not Computed →		0.9500**

\* Includes All Uncertainties

\*\* Estimate from Figure 2-1.



\* boron -10 atoms per  $10^{-24}$  cm<sup>3</sup> in the pool water

\* grams of boron per million grams of water

~~FIGURE 11-26~~

FIGURE 2-1

ACCIDENT LOADING & EFFECTIVE CURVE



FIGURE (2-2)

EXXON 15x15 PWR (PALISADES FUEL)

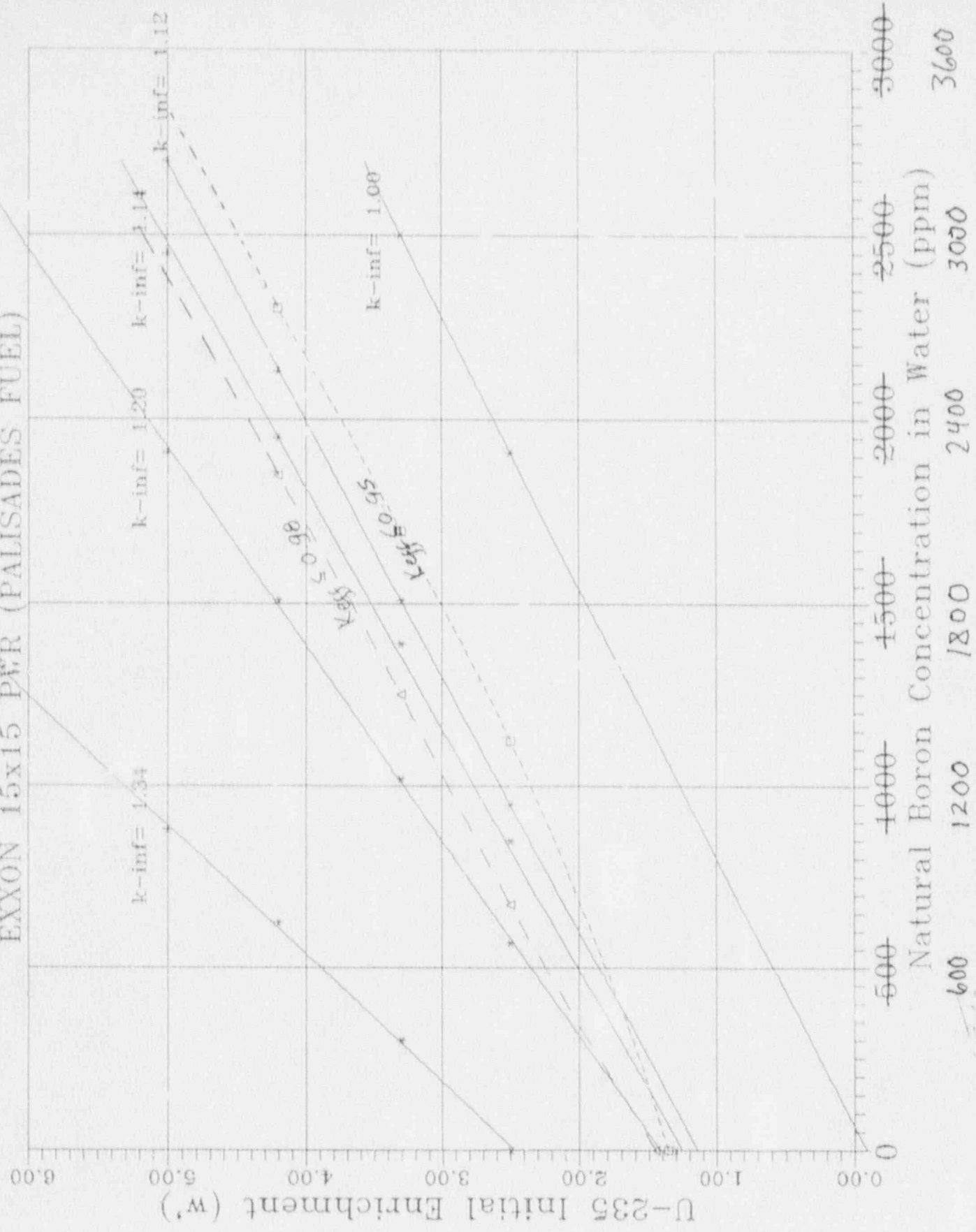
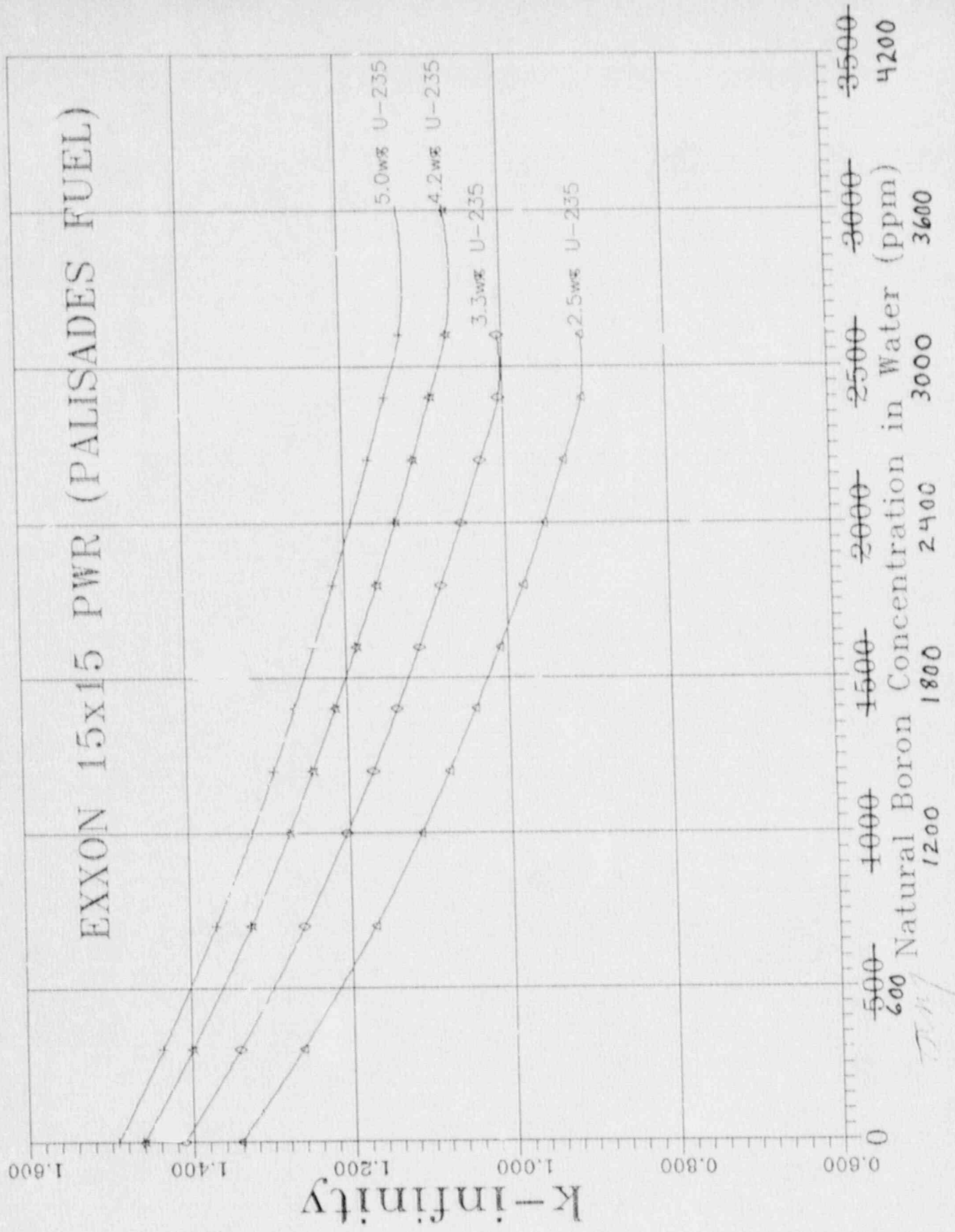


Figure (2-3)



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## 2.2 Analysis

- (a) From Ref (12), the overall uncertainty due to variation in assembly locations, water density, fuel homogenization, and KENO-IV bias is

$$\Delta K_{\text{total}} = 0.013$$

Thus, the "Final  $k$ -eff" in Table (2-1) are calculated from:

$$\text{Final } K_{\text{eff}} = \text{Average } K_{\text{eff}} + 2\sigma + \Delta K_{\text{total}}$$

Ex.)

$$\text{Section 4.1: } 0.9376 + 2 * 0.004 + 0.013 = 0.9586$$

- (b) From Ref (12), the reactivity gained per 1% of U-235 initial enrichment is:

$$\delta K_{\text{enrichment}} = 0.329$$

- (c) From Table (2-1), the reactivity reduced per 100ppm of natural Boron in water is:

$$\delta K_{\text{Boron}} = \left( \frac{0.9243 - 0.9376}{2040 - 1800} \right) (100)$$

$$\delta K_{\text{Boron}} = -0.0055417$$

④ Boron Conc. to have  $K_{eff} \approx 0.945$  ( $\leq 0.95$ )

Enrichment (%)

Natural Boron Concentration (WPPM)

1.36

∅ (From Ref ②)

2.5

$$1076 + \left[ \frac{(0.945 - 0.9588) * 100}{-0.0055417} \right] = 1325$$

3.3

2040

4.2

2760

5.0

3360

⑤ Boron Concentration to have  $K_{eff} \leq 0.98$

Enrichment (%)

Natural Boron Concentration (WPPM)

$$1.36 + \frac{0.98 - 0.95}{0.329} = 1.45$$

∅

2.5

$$1325 + \left[ \frac{(0.98 - 0.95)}{-0.0055417} \right] (100) = 784$$

3.3

$$2040 + \left[ \frac{(0.98 - 0.95)}{-0.0055417} \right] (100) = 1499$$

4.2

$$2760 + \left[ \frac{(0.98 - 0.95)}{-0.0055417} \right] (100) = 2219$$

5.0

$$3360 + \left[ \frac{(0.98 - 0.95)}{-0.0055417} \right] (100) = 2819$$

### 3.0 REFERENCES

1. W.A. Wittkopf, et al., "NULIF Neutron Spectrum Generator, Few Group Constant Calculator," BAW-426, Rev. 11, Babcock and Wilcox Co., Lynchburg, VA (1988).
2. W.A. Wittkopf, and N.M. Hassan, "NITAWL - Nordheim Integral Treatment and Working Library Production," NPGD-TM-505, Rev. 8, Babcock and Wilcox Co., Lynchburg, VA (1988).
3. W.A. Wittkopf and N.M. Hassan, "XSDRNPM - A One Dimensional Discrete Ordinates Computer Code," NPD-TM-13 [B&W version of XSDRNPM, ORNL-TM-2500 (1969)] Babcock and Wilcox Co., Lynchburg, VA (1985).
4. W.A. Wittkopf and N.M. Hassan, "KENO4 - An Improved Monte Carlo Criticality Program," NPGD-TM-5103, Rev. G, [B&W version of KENO-IV, ORNL-4938 (1975)] Babcock and Wilcox Co., Lynchburg, VA (1985).
5. R. I. Smith and G. J. Konzak, "Clean Critical Experiment Benchmarks for Plutonium Recycle in LWR's," EPRI-NP-196, Electric Power Research Institute, April 1976.
6. M.N. Baldwin et al., "Critical Experiments Supporting Close Proximity Water Storage of Pwerc Reactor Fuel," BAW-1487-7, Babcock and Wilcox Co., Lynchburg, VA (1979).

7. W.A. Wittkopf, "Summary Description of the Babcock and Wilcox Integrated Nuclear Design System," BAW-10111a, Babcock and Wilcox Co., Lynchburg, VA (1977).
8. "Characteristics of Spent Fuel, High-Level Waste, and Other Radioactive Wastes Which May Require Long-Term Isolation," Office of Civilian Radioactive Waste Management, U.S. Department of Energy, DOE/RW-0184 (1987).
9. C.O. Brown, "Palisades Nuclear Generating Station Spent Fuel Storage Pool Criticality Safety Reanalysis, Attachment A to Palisades Technical Specification Change Request for Fuel Storage May 11, 1981 Docket 50-255 (XN-NF-542 Exxon Nuclear Corporation document).
10. J.R. Lamarsh, "Introduction to Nuclear Engineering", Addison-Wesley Publishing Co., Reading MA, 1975.
11. L. J. Templin, Editor, " Reactor Physics Constants," Argonne National Laboratory, Argonne, Illinois, ANL-5800 (1963).
12. CPC-0109.001.2, "VSC-24 CRITICALITY SAFETY ANALYSIS (PALISADES ISFSI)", 1989.

# CALCULATION SHEET

## 4. K-eff CALCULATIONS

Refer to Reference (22) for the calculations of basic parameters, generalized KENO geometry, and fuel characteristics applied to this calculation package. Derivations of input parameters for NITAWL, NULIF, XSDRNP, and KENO will be presented here.

Table (4-1) gives the boron (nature) atom density in terms of [atoms/cm<sup>3</sup>]. The homogenized atomic density used in KENO code is also included.

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Table (4-1)

NAT. BORON CONCENTRATION [wppm]	NULIF & XSDRNPM B-10 ATOM [atoms/barn*cm]	KENO-IV B-10 ATOM [atoms/barn*cm]
0	0.000E+00	0.000E+00
120*	1.308E-06	7.462E-07
239	2.615E-06	1.492E-06
359	3.923E-06	2.238E-06
479	5.230E-06	2.984E-06
599	6.538E-06	3.730E-06
718	7.845E-06	4.475E-06
838	9.153E-06	5.222E-06
958	1.046E-05	5.967E-06
1078	1.177E-05	6.715E-06
1198	1.308E-05	7.462E-06
1317	1.438E-05	8.204E-06
1437	1.569E-05	8.951E-06
1557	1.700E-05	9.698E-06
1677	1.831E-05	1.045E-05
1796	1.961E-05	1.119E-05
1916	2.092E-05	1.193E-05
2036	2.223E-05	1.268E-05
2156	2.354E-05	1.343E-05
2275	2.484E-05	1.417E-05
2395	2.615E-05	1.492E-05
2515	2.746E-05	1.567E-05
2635	2.877E-05	1.641E-05
2754	3.007E-05	1.715E-05
2874	3.138E-05	1.790E-05
2994	3.269E-05	1.865E-05
3114	3.400E-05	1.940E-05
3233	3.530E-05	2.014E-05
3353	3.661E-05	2.089E-05
3473	3.792E-05	2.163E-05
3593	3.923E-05	2.238E-05
3712	4.053E-05	2.312E-05
3832	4.184E-05	2.387E-05

$$* (1.308 \times 10^{-6} \frac{B^{10}}{\text{barn} \cdot \text{cm}}) \left( 10^{24} \frac{\text{barn}}{\text{cm}^2} \right) \left( \frac{10.81 \text{ g } B^{\text{NAT}}}{6.02 \times 10^{23} B^{\text{NAT}}} \right) \left( \frac{B^{\text{NAT}}}{0.196 B^{10}} \right) \left( 10^6 \frac{\text{g } B^{\text{NAT}}}{\text{g water}} \right) = 120 \text{ PPM}$$



SUMMARY OF FUEL AND REACTOR PARAMETERS

\*\*\*\*\*

(Lxxon 15x15 PWR )

REACTOR PARAMETERS:

\*\*\*\*\*

Power Thermal Output.....: Reactor\_Power := 2650 MW

Number of Assemblies.....: Number\_Assem := 204

ASSEMBLY DESCRIPTIONS:

\*\*\*\*\*

Assembly Width .....: Assem\_Width := 8.25 in  
Assem\_Width = 20.955 cm

Array Size.....: Array := 15 15 (Rods)

Fueled Rods/Assembly.....: Number\_FuelRod := 216

Rod Pitch.....: Pitch := 0.550 in  
Pitch = 1.397 cm

Heavy Metal (Uranium).....: MTHM := 0.40724 MTU

Initial Enrichment.....: Enrichment := 3.0 %

Fuel (UO2) Density.....: Percent\_Theo := 94.0 %

FUEL ROD DESCRIPTIONS:

\*\*\*\*\*

Fuel Rod Diameter.....: Rod\_Dia := 0.415 in  
Rod\_Dia = 1.0541 cm

Active Length.....: Act\_Length := 131.80 in  
Act\_Length = 334.772 cm

Clad Thickness.....: Clad\_Thick := 0.0285 in  
Clad\_Thick = 0.0724 cm

Fuel-Clad Gap.....: Gap := 0.004 in  
Gap = 0.0102 cm

BASIC FUEL GEOMETRY CALCULATIONS:

\*\*\*\*\*

The following geometry parameters are calculated or obtained directly from the fuel parameters given in the previous summary table.

o Fuel Pellet (pin) Radius and Diameter:

$$\cdot \quad \text{Pellet\_Dia} := \text{Rod\_Dia} \cdot 2 \cdot (\text{Clad\_Thick} + \text{Gap})$$

$$\text{Pellet\_Dia} = 0.889 \cdot \text{cm}$$

$$\cdot \quad \text{Pellet\_Rad} := \frac{\text{Pellet\_Dia}}{2}$$

$$\text{Pellet\_Rad} = 0.4445 \cdot \text{cm}$$

o Inner Cladding Radius and Diameter:

$$\cdot \quad \text{InClad\_Dia} := \text{Rod\_Dia} \cdot 2 \cdot \text{Clad\_Thick}$$

$$\text{InClad\_Dia} = 0.9093 \cdot \text{cm}$$

$$\cdot \quad \text{InClad\_Rad} := \frac{\text{InClad\_Dia}}{2}$$

$$\text{InClad\_Rad} = 0.4547 \cdot \text{cm}$$

o Fuel Rod Radius and Diameter:

$$\cdot \quad \text{Rod\_Dia} = 1.0541 \cdot \text{cm}$$

$$\cdot \quad \text{Rod\_Rad} := \frac{\text{Rod\_Dia}}{2}$$

$$\text{Rod\_Rad} = 0.5271 \cdot \text{cm}$$

o Equivalent Radius of Fuel Cell (Cylindrical Model):

$$\text{Cell\_Rad} := \frac{\text{Pitch}}{\sqrt{\pi}}$$

$$\text{Cell\_Rad} = 0.7882 \cdot \text{cm}$$

Since all non-fuel rods in the fuel assembly are assumed to be water rods, the fuel cell pitch and the equivalent fuel cell radius must be modified to take these water rods into account. It is assumed that the water rods will be smeared out (homogenized) throughout the assembly volume.

$$\text{Total\_Rod} := \text{Array}$$

$$\text{Total\_Rod} = 225$$

$$\text{Mod\_Pitch} := \text{Pitch} \cdot \frac{\text{Total\_Rod}}{\sqrt{\text{Number\_FuelRod}}}$$

$$\text{Mod\_Pitch} = 1.4258 \cdot \text{cm}$$

$$\text{Mod\_Cell\_Rad} := \frac{\text{Mod\_Pitch}}{\sqrt{\pi}}$$

$$\text{Mod\_Cell\_Rad} = 0.8044 \cdot \text{cm}$$

BASIC VOLUME CALCULATIONS:

\*\*\*\*\*

o Pellet (UO2) Volume:

$$\text{Pellet\_Vol} := \text{Pellet\_Rad}^2 \cdot \pi \cdot \text{Act\_Length}$$

$$\text{Pellet\_Vol} = 207.7986 \cdot \text{cm}^3$$

o Air Gap Volume:

$$\text{Gap\_Vol} := \left[ \text{InClad\_Rad}^2 - \text{Pellet\_Rad}^2 \right] \cdot \pi \cdot \text{Act\_Length}$$

$$\text{Gap\_Vol} = 9.6079 \cdot \text{cm}^3$$

o Cladding Volume:

$$\text{Clad\_Vol} := \left[ \text{Rod\_Rad}^2 - \text{InClad\_Rad}^2 \right] \cdot \pi \cdot \text{Act\_Length}$$

$$\text{Clad\_Vol} = 74.7413 \cdot \text{cm}^3$$

o Fuel Rod Total Volume:

$$\text{Rod\_Vol} := \text{Rod\_Rad}^2 \cdot \pi \cdot \text{Act\_Length}$$

$$\text{Rod\_Vol} = 292.1478 \cdot \text{cm}^3$$

o Water Moderator Volume (based on the designed pitch):

$$\text{H2O\_Vol} := \text{Pitch}^2 \cdot \text{Act\_Length} - \text{Rod\_Vol}$$

$$\text{H2O\_Vol} = 361.1962 \cdot \text{cm}^3$$

o Water Moderator Volume (based on the modified pitch):

$$\text{Mod\_H2O\_Vol} := \text{Mod\_Pitch}^2 \cdot \text{Act\_Length} \cdot \text{Rod\_Vol}$$

$$\text{Mod\_H2O\_Vol} = 388.4189 \cdot \text{cm}^3$$

o Unit Cell Volume (based on the designed pitch):

$$\text{Cell\_Vol} := \text{Rod\_Vol} + \text{H2O\_Vol}$$

$$\text{Cell\_Vol} = 653.344 \cdot \text{cm}^3$$

o Unit Cell Volume (based on the modified pitch):

$$\text{ModCell\_Vol} := \text{Rod\_Vol} + \text{Mod\_H2O\_Vol}$$

$$\text{ModCell\_Vol} = 680.5667 \cdot \text{cm}^3$$

BASIC MASS CALCULATIONS:

=====

o Molecular weight of common material [Reference(10)]:

$$\cdot \quad MW_{U235} := 235.0 \cdot gm$$

$$\cdot \quad MW_{U238} := 238.0 \cdot gm$$

$$\cdot \quad MW_{UO2} := 270.3 \cdot gm$$

o Density of heavy metal (uranium) in the fuel rod:

$$\cdot \quad UO2\_Theo\_Density := 10.96 \cdot \frac{gm}{cm^3}$$

$$\cdot \quad Fuel\_Density := Percent\_Theo \cdot UO2\_Theo\_Density$$

$$Fuel\_Density = 10.3024 \cdot \frac{gm}{cm^3}$$

$$\cdot \quad Uranium\_Density := Fuel\_Density \cdot \frac{MW_{U238}}{MW_{UO2}}$$

$$Uranium\_Density = 9.0713 \cdot \frac{gm}{cm^3}$$

o Amount of heavy metal per assembly (calculated):

$$MHTU := Uranium\_Density \cdot Pellet\_Vol \cdot Number\_FuelRod$$

$$MHTU = 0.4072 \cdot MTU$$

# CALCULATION SHEET

4.4) Fuel at (3.3% U235, <sup>1797</sup>~~1500~~ ppm B)

Refer to Reference (12) for generalized geometry cards in the KENO input.

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NULIF INPUT PARAMETERS

\*\*\*\*\*

NULIF requires the following parameters as input: dimensions of the fuel unit cell, reactor power history, power density based on the fuel cell volume, atomic densities of the materials in the fuel cell (fuel pellet, cladding, and moderator).

The basic dimensions of the fuel unit cell are given in previous sections. The fuel cell with the designed pitch will be used for all the NULIF calculations in this criticality analysis. The reactor operating cycle is taken as 16 months at full power and 2 months of outage. Other required parameters are calculated below:

\*\* Atomic Density Calculations:

.....

The following fuel parameter will be considered in this section:

Enrichment := 3.3%

Burnup := 0.0  $\frac{\text{Gwd}}{\text{MTU}}$

Nat\_Boron\_Con := <sup>1198</sup>~~1000~~ ppm

JJM

o U-235 atomic densities based on pellet volume:

$$N_{U235} := \text{Uranium\_Density} \cdot \frac{\text{Avogadro}}{\text{MW}_{U235}} \cdot \text{Enrichment}$$

$$N_{U235} = 7.6711 \cdot 10^{-4} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

o U238 atomic densities based on pellet volume:

$$N_{U238} := \text{Uranium\_Density} \cdot \frac{\text{Avogadro}}{\text{MW}_{U238}} \cdot (1.0 - \text{Enrichment})$$



$$N_{U238} = 2.2195 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}}$$

o O16 atomic density based on pellet volume:

$$N_{O16} := 2 \cdot (N_{U238} + N_{U235})$$

$$N_{O16} = 4.5925 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}}$$

o Zirconium cladding atomic density is taken as:

$$N_{Zr40} := 4.291 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}} \quad \dots, \text{Reference}(10)$$

o H1 atomic density in water:

$$N_{H1\_70F} := 6.671 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}} \quad (\text{at } T = 70F)$$

$$N_{H1\_212F} := 6.406 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}} \quad (\text{at } T = 212F)$$

o O16 atomic density in water:

$$N_{O16\_70F} := 3.336 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}} \quad (\text{at } T = 70F)$$

$$N_{O16\_212F} := 3.203 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}} \quad (\text{at } T = 212F)$$

o Natural boron concentration in water:

~~N\_NatBoron\_70F := Net\_Boron\_Con \* N\_H1\_70F~~ *W/L*

$$N\_NatBoron\_70F = 6.671 \cdot 10^{-5} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

~~N\_NatBoron\_212F := Net\_Boron\_Con \* N\_H1\_212F~~ *W/L*

$$N\_NatBoron\_212F = 6.406 \cdot 10^{-5} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

o Operating time required to attain the desired burnup level:

$$\text{Operating\_Time} := \text{Burnup} \cdot \text{Number\_Assem} \cdot \frac{\text{MTHM}}{\text{Reactor\_Power}}$$

$$\text{Operating\_Time} = 0 \cdot \text{day}$$

NITAWL INPUT PARAMETERS

\*\*\*\*\*

The first NITAWL computer run (see Figure[ ] ) is used to format the cross sections from the 123 group cross section set contained in the AMPX master library. This NITAWL computer run also performs resonance self-shielding corrections for the following nuclides: U-236, U238, Pu-240, and Pu-242. If the loaded fuel is unirradiated (i.e., fresh fuel) then only U-238 is corrected for resonance self-shielding.

\*\* Dancoff factor:

.....

The Dancoff factor calculated by the NULIF code is given as:

Dancoff\_NULIF := ~~0.7832~~ 0.7992 HHT

However the Dancoff factor from the NULIF output is not defined in the same way as the one requested by the NITAWL computer code. The NITAWL's Dancoff factor is defined as:

Dancoff\_NITAWL := 1.0 \* Dancoff\_NULIF

Thus, for this case:

Dancoff\_NITAWL = ~~0.2168~~ 0.2008 HHT

\*\* Scattering Cross Sections Parameters

.....

The following potential scattering cross sections are obtained from Reference(11).

- $\sigma_{O16} := 3.8 \cdot \text{barn}$
- $\sigma_{U236} := 10 \cdot \text{barn}$
- $\sigma_{Pu240} := 11 \cdot \text{barn}$
- $\sigma_{U235} := 10 \cdot \text{barn}$
- $\sigma_{U238} := 9 \cdot \text{barn}$
- $\sigma_{Pu242} := 11 \cdot \text{barn}$

1). U-238 Resonance Parameter:

-----  
For fresh fuel, the atomic density of U-238 (N\_U238) previously calculated is used. For irradiated fuel, the N\_U238 must be replaced with the value obtained from the NULIF burnup calculation results.

- o First moderator (U-235) scattering cross section per absorber atom (U-238):

$$\sigma_{s1} := \frac{N_{U235}}{N_{U238}} \cdot \sigma_{U235}$$

$$\sigma_{s1} = 0.3456 \cdot \text{barn}$$

- o Second moderator (O-16) scattering cross section per absorber atom (U-238):

$$\sigma_{s2} := \frac{N_{O16}}{N_{U238}} \cdot \sigma_{O16}$$

$$\sigma_{s2} = 7.8627 \cdot \text{barn}$$

- o Effective moderator cross section per absorber atom (U-238):

$$\sigma_{m\_eff} := \sigma_{U238} + (\sigma_{s1} + \sigma_{s2}) + \frac{1}{\text{Pellet\_Dia} \cdot N_{U238}}$$

$$\sigma_{m\_eff} = 67.8885 \cdot \text{barn}$$

XSDRNPM INPUT PARAMETERS  
\*\*\*\*\*

The geometric model for the XSDRNPM code is a cylindrical fuel unit cell with radius based on the modified pitch of the square unit cell. The dimensions of the fuel unit cells are calculated in section entitled "Basic Fuel Geometry Calculations". The atomic densities used in the XSDRNPM mixing table are the same as the values calculated in the "NULIF INPUT PARAMETERS" section. The fuel-clad air gap and the cladding region is combined together to form a single Zirconium region with the atomic density calculated below:

$$N_{Zr40\_XSD} := \frac{Clad\_Vol}{Clad\_Vol + Gap\_Vol} \cdot N_{Zr40}$$
$$N_{Zr40\_XSD} = 3.8022 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

KENO INPUT PARAMETERS

\*\*\*\*\*

The geometric models of the KENO-IV computer code are discussed in Section 5.0. Unless specifically noted, all the geometry cards of the KENO input remain the same as the reference geometric model discussed in Section 5.0. This section will calculate other input parameters applied to this particular KENO run.

Since the loaded fuel assemblies in the cask are homogenized, the atomic densities in the KENO mixing table must be based on the volume of the fuel cell (with modified pitch). The homogenized atom densities of all the nuclides in the fuel cell are calculated below:

$$N_{U235\_Homo} := \frac{Pellet\_Vol}{ModCell\_Vol} \cdot N_{U235}$$

$$N_{U235\_Homo} = 2.3422 \cdot 10^{-4} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

$$N_{U238\_Homo} := \frac{Pellet\_Vol}{ModCell\_Vol} \cdot N_{U238}$$

$$N_{U238\_Homo} = 6.7769 \cdot 10^{-3} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

$$N_{Zr40\_Homo} := \frac{Clad\_Vol}{ModCell\_Vol} \cdot N_{Zr40}$$

$$N_{Zr40\_Homo} = 4.7125 \cdot 10^{-3} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

$$N_{O16\_Homo} := \frac{Pellet\_Vol}{ModCell\_Vol} \cdot N_{O16} + \frac{Mod\_H2O\_Vol}{ModCell\_Vol} \cdot N_{O16\_70F}$$

$$N_{O16\_Homo} = 3.3062 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

$$N_{H1\_Homo} := \frac{Mod\_H2O\_Vol}{ModCell\_Vol} \cdot N_{H1\_70F}$$

$$N_{H1\_Homo} = 3.8073 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

~~$$N_{NatBoron\_Homo} := \frac{N_{H1\_Homo} \cdot Nat\_Boron\_Con}{}$$~~

$$N_{NatBoron\_Homo} = 3.8073 \cdot 10^{-5} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

205  
 /MUSEP  
 MULTIF, PD, T600. HEAVY TRAM  
 USER, VXPPOK, CASX, NC.  
 CHANGE, N973001, VPC  
 TITLE: [E33NUR] EXXON PWR 15x15, 3.34 U235, BORATED WATER  
 ATTACHP(LEB1, 1, 0)  
 ATTACHP(LEB2, 1, 0)  
 ATTACHP(LEB3, 1, 0)  
 REMIND, TAPE1, TAPED, TAPED.  
 ATTACHP, MULTIF, 9, 1.  
 MULTIF(PL=777777)  
 /ECP

Note: All title Card "PPM" values  
 should be multiplied by a  
 factor of 1.198 to convert  
 value to WPPM Boron.

$\frac{E}{W}$  = general parameters:  
 ⋮  
 300 PPM 1002, 0.0, 1, 1.0, 1

should be  
 = general parameters:  
 ⋮  
 359 PPM 1002, 0.0, 1, 1.0, 1  
 (300 x 1.198)

= [E33NUR] EXXON PWR 15x15, 3.34 U235, BORATED WATER  
 = General parameters  
 000001, 1, 0, 1-5, 1-0-20  
 000002, 300  
 000003, 1  
 100001, 1.0, 1, 1.0, 1  
 100002, 0.0, 1, 1.0, 1  
 100003, 0.0, 1, 1.0, 1  
 100004, 1.0, 1, 1.0, 1  
 100005, 0.0, 1, 1.0, 1  
 100006, 0.0, 1, 1.0, 1  
 100007, 0.0, 1, 1.0, 1  
 100008, 0.0, 1, 1.0, 1  
 100009, 0.0, 1, 1.0, 1  
 100010, 0.0, 1, 1.0, 1  
 100011, 0.0, 1, 1.0, 1  
 100012, 0.0, 1, 1.0, 0, 3  
 = Composition data  
 300100, 2, 1  
 = Cell geometry  
 310100, 1, 0.2990, 0.9090, 3.0501, 1.4050, 0  
 310101, 70.0, 70.0, 70.0, 0.0  
 = Compositions of fuel (0.34 U235 Enr.)  
 320101, U235, 7.6711-2  
 320102, U238, 3.3336-2  
 320103, O16, 4.5435-2  
 320104, P19, 4.5435-2  
 = Compositions of water coolant (T= 70 F, P=14.7 psia)  
 = EXXON PWR 15x15, 3.34 U235, 0ppm NAT. BORON  
 340101, H1, 6.671-2  
 340102, O16, 3.336-2  
 340103, B10, 1.000-20  
 /  
 = EXXON PWR 15x15, 3.34 U235, <sup>359</sup>ppm NAT. BORON  
 440101, H1, 6.671-2  
 440102, O16, 3.336-2  
 440103, B10, 3.923-6  
 /  
 = EXXON PWR 15x15, 3.34 U235, <sup>878</sup>ppm NAT. BORON  
 440101, H1, 6.671-2  
 440102, O16, 3.336-2  
 440103, B10, 4.153-6  
 /  
 = EXXON PWR 15x15, 3.34 U235, <sup>1197</sup>ppm NAT. BORON  
 440101, H1, 6.671-2  
 440102, O16, 3.336-2  
 440103, B10, 1.308-5  
 /  
 = EXXON PWR 15x15, 3.34 U235, <sup>1436</sup>ppm NAT. BORON  
 440101, H1, 6.671-2

JFM



440102, 016, 3.336-2  
440103, 810, 3.509-5

1676

= EXXON PWR 15x15, 3.31 U235, ~~100%~~ppa NAT. BORON  
440101, HI, 6.671-2  
440102, 016, 3.336-2  
440103, 810, 3.631-5

1915

= EXXON PWR 15x15, 3.31 U235, ~~100%~~ppa NAT. BORON  
440101, HI, 6.671-2  
440102, 016, 3.336-2  
440103, 810, 2.092-5

2155

= EXXON PWR 15x15, 3.31 U235, ~~100%~~ppa NAT. BORON  
440101, HI, 6.671-2  
440102, 016, 3.336-2  
440103, 810, 2.254-5

2374

= EXXON PWR 15x15, 3.31 U235, ~~100%~~ppa NAT. BORON  
440101, HI, 6.671-2  
440102, 016, 3.336-2  
440103, 810, 3.015-5

2633

= EXXON PWR 15x15, 3.31 U235, ~~100%~~ppa NAT. BORON  
440101, HI, 6.671-2  
440102, 016, 3.336-2  
440103, 810, 2.077-5

3377

= EXXON PWR 15x15, 3.31 U235, ~~100%~~ppa NAT. BORON  
440101, HI, 6.671-2  
440102, 016, 3.336-2  
440103, 810, 3.138-5

3442

= EXXON PWR 15x15, 3.31 U235, ~~100%~~ppa NAT. BORON  
440101, HI, 6.671-2  
440102, 016, 3.336-2  
440103, 810, 3.400-5

1518

1008  
 E33N18, PO, 1200 HENRY TRAN  
 USER, W, 9PBN, CASE, NC.  
 CHARGE, N973301, USC.  
 TITLE ((E33N18)) EXXON 15:15 PWR, 3.38 U235, 4500 ppm NAT-BORON)  
 ATTACHP (NITAWL, 1, 2)  
 ATTACHP (ADM127, 3, 0A)  
 REWIND, TAPE1.  
 NITAWL, PL\*777777.  
 REWIND, TAPE4.  
 REWIND, TAPE2.  
 COPYDF, TAPE4, TAPE2.  
 REWIND, TAPE8.  
 ATTACHP, XSD0NPM, 1, 0A.  
 (XSDNPM PL\*777777)  
 REWIND, TAPE2, TAPE3.  
 RETURN, TAPE3.  
 ATTACHP, NITAWL, 1, 3.  
 NITAWL, PL\*777777.  
 REWIND, TAPE4.  
 RETURN, TAPE2, TAPE3.  
 LABEL, TAPE4, W, 0\*9C, L=INSECT, MON=007421.  
 COPYDF, TA, 5, TAPE4.  
 END

148 0 41 6 0 0 3 4 3 121 0 1 0 1  
 144  
 10000 +8000 110000 120000 130000  
 140000 210000 250000 280000 290000 320000  
 320000 +35922381 +37922381 -42922381 -50922381  
 320000 +35922381 +37922381 -42922381 -50922381  
 300000 +25400000 +33400000 -42400000 -50400000  
 400000 +25400000 +33400000 -42400000 -50400000  
 500000 +25400000 +33400000 -42400000 -50400000  
 600000 +25400000 +33400000 -42400000 -50400000

912001 294.27 2 0.4445 0.2008 67.2214 1.177901-02  
 1 235.0 2.5971-1 1 15.99 7.79740 1 1.0  
 35922381 294.27 2 0.4445 0.2008 67.2214 2.227791-02  
 1 235.0 2.5971-1 1 15.99 7.79740 1 1.0  
 37922381 294.27 2 0.4445 0.2008 67.2214 1.219511-01  
 1 235.0 2.5971-1 1 15.99 7.79740 1 1.0  
 42922381 294.27 2 0.4445 0.2008 68.5378 1.199901-02  
 1 235.0 4.4406-1 1 15.99 7.93740 1 1.0  
 50922381 294.27 2 0.4445 0.2008 69.1251 2.180501-02  
 1 235.0 8.13705-1 1 15.99 8.00510 1 1.0

END  
 (E33N18) EXXON 15:15 PWR, 3.38 U235, 4500 ppm NAT-BORON  
 148 2 3 11 0 3 3 10 0 7 1 10 12 0 0 0  
 144 -2 -1 -1 E  
 148 1 0 0 0 4 0 0 0 0 0 0 1 0  
 498 -1 127 0 42 3 4 126 -1 0  
 5\*\* 1 -4 2 -4 1 0 0 0 0 1.420892 E

1388 1  
 1 1  
 1  
 2  
 2  
 3  
 3 3  
 3

32 Jm

144

0  
37922351 33922381  
3780004  
0  
33400000  
0  
3310001 3380002  
3350100

15\*\*

0.0  
7.4711-0 2.3195-2  
4.5425-0  
0.0  
3.7422-2  
0.1  
5.471-2 3.736-2  
1.941-5

16\*\*

581.0 40.0

17\*\*

410.0 110.0445 110.8271 0.0044

18\*\*

381 381 381 480

19\*\*

1 1 1 1

20\*\*

12111.0 122.0

21\*\*

0 0 10 6 3 3 4 1 10 0 0 0 0 1

22

50000 40000 110000 120000 130000  
140000 240000 250000 260000 280000 290000

50100  
37922351 42922351 50922351  
35922351 40922351 50922351  
3380004 4280004 5080004  
35400000 42400000 50400000  
3510001 4210001 5010001  
3350100 4230100 5050100  
33922351  
33922381  
3380004  
33400000  
3310001  
3350100

23\*\*



# CALCULATION SHEET

4.2) Fuel at (3.3%, <sup>2035</sup>~~1700~~ ppm B) <sup>EM</sup>

Same as section (4.2) ; Except  
ICEND input

CLIENT:	JOB NO.	REVISION:
ORIGINATOR: HENRY TRAN	DATE:	CALC. NO. :
CHECKER:	DATE:	PAGE: 351

7308  
 ANDSIO  
 E33K181, PG, T7000. HENRY TRAM  
 USER, VY9PEN, CASK, NC.  
 CHARGE, N973301, VSC.  
 TITLE (E33K181) EXXON 15x15 PWR, 3.33U235, 1000 ppm NAT-BORON  
 LABEL, TAPEA, D=0E, L=EXSICT, VSN=007421.  
 COPYBT, TAPEA, TAPE4.  
 REVIND, TAPE4.  
 RETURN, TAPEA.  
 RFL (CC=10)  
 ATTACH, XINDA, 1, 26.  
 XINDA, PI=777777.  
 CLIP

E33K181 EXXON 15x15 PWR, 3.33U235, 1000 ppm NAT-BORON  
 98.0 73 300 3 120 75 16 5 20 1  
 1 1 1 1 1 -10 1 0 2000 00 1  
 0 0 0 0 0 0 00 0 0  
 0.0 -1.0 0.0 -1.0 -1.0 -1.0  
 1 7342381 2.3422-4  
 1 37922521 6.7749-3  
 1 1380064 3.2061-2  
 1 33400000 4.7125-3  
 1 3710001 3.8973-2  
 1 3380100 1.2890-5  
 2 10001 6.6711-1 2 80004 7.156-2 3 59100 2.223-5  
 1 60002 2.6100-1 3 250005 1.0900-2  
 2 740001 8.2000-2 3 140005 1.9300-4  
 4 820000 3.2960-2  
 5 10001 2.7700-2 5 50000 1.4600-3 6 80004 3.7100-2  
 5 110500 2.6000-4 5 120005 2.0800-4 5 130000 6.9700-1  
 5 140005 7.4700-4 5 260001 4.8700-5

*generalized geometry cards*



# CALCULATION SHEET

4.3) Fuel at (2.5% U235, <sup>1077</sup>~~900~~ ppm B) <sup>300A</sup>

See section (4.1) for NITAWL input

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ORIGINATOR: HENRY TRAN	DATE:	CALC. NO. :
CHECKER:	DATE:	PAGE: 37

NULIF INPUT PARAMETERS

\*\*\*\*\*

NULIF requires the following parameters as input: dimensions of the fuel unit cell, reactor power history, power density based on the fuel cell volume, atomic densities of the materials in the fuel cell (fuel pellet, cladding, and moderator).

The basic dimensions of the fuel unit cell are given in previous sections. The fuel cell with the designed pitch will be used for all the NULIF calculations in this criticality analysis. The reactor operating cycle is taken as 16 months at full power and 2 months of outage. Other required parameters are calculated below:

\*\* Atomic Density Calculations:

.....

The following fuel parameter will be considered in this section:

Enrichment := 2.5%

Burnup := 0.0  $\frac{\text{Gwd}}{\text{MTU}}$

Nat\_Boron\_Con := ~~400~~ ppm

o U-235 atomic densities based on pellet volume:

$$N_{U235} := \text{Uranium\_Density} \cdot \frac{\text{Avogadro}}{\text{MW}_{U235}} \cdot \text{Enrichment}$$

$$N_{U235} = 5.8114 \cdot 10^{-4} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}}$$

o U238 atomic densities based on pellet volume:

$$N_{U238} := \text{Uranium\_Density} \cdot \frac{\text{Avogadro}}{\text{MW}_{U238}} \cdot (1.0 - \text{Enrichment})$$



$$N_{U238} = 2.2379 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}}$$

o O16 atomic density based on pellet volume:

$$N_{O16} := 2 \cdot (N_{U238} + N_{U235})$$

$$N_{O16} = 4.592 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}}$$

o Zirconium cladding atomic density is taken as:

$$N_{Zr40} := 4.291 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}} \quad \dots \text{Reference(10)}$$

o H1 atomic density in water:

$$N_{H1\_70F} := 6.671 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}} \quad (\text{at } T = 70F)$$

$$N_{H1\_212F} := 6.406 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}} \quad (\text{at } T = 212F)$$

o O16 atomic density in water:

$$N_{O16\_70F} := 3.336 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}} \quad (\text{at } T = 70F)$$

$$N_{O16\_212F} := 3.203 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}} \quad (\text{at } T = 212F)$$

o Natural boron concentration in water:

~~N\_NatBoron\_70F := Nat\_Boron\_Con \* N\_H1\_70F~~ *M C*

$$N\_NatBoron\_70F = 6.671 \cdot 10^{-5} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

~~N\_NatBoron\_212F := Nat\_Boron\_Con \* N\_H1\_212F~~ *M C*

$$N\_NatBoron\_212F = 6.406 \cdot 10^{-5} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

o Operating time required to attain the desired burnup level:

$$\text{Operating\_Time} := \frac{\text{Burnup} \cdot \text{Number\_Assem} \cdot \text{MTHM}}{\text{Reactor\_Power}}$$

$$\text{Operating\_Time} = 0 \cdot \text{day}$$

The NITAWL computer run (see Figure 1) is used to correct the cross sections from the 123 group cross section set contained in the AMPX master library. This NITAWL computer run also performs resonance self-shielding corrections for the following nuclides: U-236, U238, Pu-240, and Pu-242. If the loaded fuel is unirradiated (i.e., fresh fuel) then only U-238 is corrected for resonance self-shielding.

\*\* Dancoff factor:

The Dancoff factor calculated by the NULIF code is given as:

$$\text{Dancoff\_NULIF} := \cancel{0.208} \quad 0.7992 \quad \text{HHT}$$

However the Dancoff factor from the NULIF output is not defined in the same way as the one requested by the NITAWL computer code. The NITAWL's Dancoff factor is defined as:

$$\text{Dancoff\_NITAWL} := 1.0 \cdot \text{Dancoff\_NULIF}$$

Thus, for this case:

$$\text{Dancoff\_NITAWL} = \cancel{0.208} \quad 0.2008 \quad \text{HHT}$$

\*\* Scattering Cross Sections Parameters

The following potential scattering cross sections are obtained from Reference(11).

- |                                     |                                     |
|-------------------------------------|-------------------------------------|
| $\sigma_{016} := 3.8 \text{ barn}$  | $\sigma_{U235} := 10 \text{ barn}$  |
| $\sigma_{U236} := 10 \text{ barn}$  | $\sigma_{U238} := 9 \text{ barn}$   |
| $\sigma_{Pu240} := 11 \text{ barn}$ | $\sigma_{Pu242} := 11 \text{ barn}$ |

13. U-238 Resonance Parameter:

-----  
For fresh fuel, the atomic density of U-238 (N\_U238) previously calculated is used. For irradiated fuel, the N\_U238 must be replaced with the value obtained from the NULIF burnup calculation results.

- o First moderator (U-235) scattering cross section per absorber atom (U-238):

$$\sigma_{s1} := \frac{N_{U235}}{N_{U238}} \cdot \sigma_{U235}$$

$$\sigma_{s1} = 0.2597 \cdot \text{barn}$$

- o Second moderator (O-16) scattering cross section per absorber atom (U-238):

$$\sigma_{s2} := \frac{N_{O16}}{N_{U238}} \cdot \sigma_{O16}$$

$$\sigma_{s2} = 7.7974 \cdot \text{barn}$$

- o Effective moderator cross section per absorber atom (U-238):

$$\sigma_{m\_eff} := \sigma_{U238} + (\sigma_{s1} + \sigma_{s2}) + \frac{1}{\text{Pellet\_Dia} \cdot N_{U238}}$$

$$\sigma_{m\_eff} = 67.3214 \cdot \text{barn}$$

XSDRNPM INPUT PARAMETERS

XXXXXXXXXXXXXXXXXXXXXXXXXXXX

The geometric model for the XSDRNPM code is a cylindrical fuel unit cell with radius based on the modified pitch of the square unit cell. The dimensions of the fuel unit cells are calculated in section entitled "Basic Fuel Geometry Calculations". The atomic densities used in the XSDRNPM mixing table are the same as the values calculated in the "NULLIF INPUT PARAMETERS" section. The fuel-clad air gap and the cladding region is combined together to form a single Zirconium region with the atomic density calculated below:

$$N_{Zr40\_XSD} := \frac{Clad\_Vol}{Clad\_Vol + Gap\_Vol} \cdot N_{Zr40}$$

$$N_{Zr40\_XSD} = 3.8022 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

KENO INPUT PARAMETERS

\*\*\*\*\*

The geometric models of the KENO-IV computer code are discussed in Section 5.0. Unless specifically noted, all the geometry cards of the KENO input remain the same as the reference geometric model discussed in Section 5.0. This section will calculate other input parameters applied to this particular KENO run.

Since the loaded fuel assemblies in the cask are homogenized, the atomic densities in the KENO mixing table must be based on the volume of the fuel cell (with modified pitch). The homogenized atom densities of all the nuclides in the fuel cell are calculated below:

$$N_{U235\_Homo} := \frac{Pellet\_Vol}{ModCell\_Vol} \cdot N_{U235}$$

$$N_{U235\_Homo} = 1.7744 \cdot 10^{-4} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

$$N_{U238\_Homo} := \frac{Pellet\_Vol}{ModCell\_Vol} \cdot N_{U238}$$

$$N_{U238\_Homo} = 6.83^2 \cdot 10^{-3} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

$$N_{Zr40\_Homo} := \frac{Clad\_Vol}{ModCell\_Vol} \cdot N_{Zr40}$$

$$N_{Zr40\_Homo} = 4.7125 \cdot 10^{-3} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

$$N_{O16\_Homo} := \frac{Pellet\_Vol}{ModCell\_Vol} \cdot N_{O16} + \frac{Mod\_H2O\_Vol}{ModCell\_Vol} \cdot N_{O16\_70F}$$

$$N_{O16\_Homo} = 3.306 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

$$N_{H1\_Homo} := \frac{Mod\_H2O\_Vol}{ModCell\_Vol} \cdot N_{H1\_70F}$$

$$N_{H1\_Homo} = 3.8073 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

~~$$N_{NatBoron\_Homo} := N_{H1\_Homo} \cdot Nat\_Boron\_50n$$~~

$$N_{NatBoron\_Homo} = 3.8073 \cdot 10^{-5} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

*M. C.*  
*J.M.*

\*NOSED  
 NULIF,PO,3600. HENRY TRAK  
 USER,VK98DN,CASK,NC.  
 LHMPOI,N973301,VSC.  
 TITLE([E25NUR1] EXXON PWR 15x15, 2.5% U235, BORATED WATER)  
 ATTACHP(LEB1,1,0)  
 ATTACHP(LEB2,1,0)  
 ATTACHP(LEB3,1,0)  
 PLWIND,TAPE1,TAPE2,TAPE3.  
 ATTACHP,NULIF,9,1.  
 NULIF/P,=777777)  
 \*EOP

= [E25NUR1] EXXON PWR 15x15, 2.5% U235, BORATED WATER

\*General parameters:  
 000001, 1, 0, 1.0-5, 1.0-20  
 000002, 500  
 000007, 1

100001, 0.0, 1, 1.0, 1, 3  
 100002, 0.0, 1, 1.0, 1  
 100003, 0.0, 1, 1.0, 1  
 100004, 0.0, 1, 1.0, 1  
 100005, 0.0, 1, 1.0, 1  
 100006, 0.0, 1, 1.0, 1  
 100007, 0.0, 1, 1.0, 1  
 100008, 0.0, 1, 1.0, 1  
 100009, 0.0, 1, 1.0, 1  
 100010, 0.0, 1, 1.0, 1  
 100011, 0.0, 1, 1.0, 1  
 100012, 0.0, 1, 1.0, 0, 3

\*Composition data:  
 300100, 2, 1  
 \*Cell geometry  
 310100, 1, 0.8890, 0.8090, 1.0501, 1.4158, 0  
 310101, 70.0, 30.0, 70.0, 0.0  
 \*Compositions of fuel rods (2.5% U235 L-En)  
 320101, 0275, 5.8110-4  
 320102, 0275, 7.0379-2  
 320103, 015, 4.5925-0  
 330101, 124, 4.291-2  
 \*Compositions of water coolant(70 F, Pale.7 psi)  
 = EXXON PWR 15x15, 2.5% U235, Appx NAT. BORON  
 340101, H1, 6.671-2  
 340102, O15, 3.336-2  
 340103, B10, 1.009-20

= EXXON PWR 15x15, 2.5% U235, <sup>359</sup> Appx NAT. BORON  
 440101, H1, 6.671-2  
 440102, O15, 3.336-2  
 440103, B10, 3.923-4

= EXXON PWR 15x15, 2.5% U235, <sup>838</sup> Appx NAT. BORON  
 440101, H1, 6.671-2  
 440102, O15, 3.336-2  
 440103, B10, 9.153-6

= EXXON PWR 15x15, 2.5% U235, <sup>1157</sup> Appx NAT. BORON  
 440101, H1, 6.671-2  
 440102, O15, 3.336-2  
 440103, B10, 1.308-5

= EXXON PWR 15x15, 2.5% U235, <sup>1436</sup> Appx NAT. BORON  
 440101, H1, 6.671-2

46 DJM



440102, 016, 3.334-2  
440102, B10, 1.569-5

1676

= EXXON PWF 15x15, 2.5X U235, ~~2000~~ppm NAT. BORON  
440101, H1, 4.671-2  
440102, 016, 3.334-2  
440103, B10, 1.871-5

1915

= EXXON PWF 15x15, 2.5X U235, ~~2000~~ppm NAT. BORON  
440101, H1, 4.671-2  
440102, 016, 3.334-2  
440103, B10, 2.092-5

2156

= EXXON PWF 15x15, 2.5X U235, ~~2000~~ppm NAT. BORON  
440101, H1, 4.671-2  
440102, 016, 3.334-2  
440103, B10, 2.754-5

2494

= EXXON PWF 15x15, 2.5X U235, ~~2000~~ppm NAT. BORON  
440101, H1, 4.671-2  
440102, 016, 3.334-2  
440103, B10, 2.615-5

2672

= EXXON PWF 15x15, 2.5X U235, ~~2000~~ppm NAT. BORON  
440101, H1, 4.671-2  
440102, 016, 3.334-2  
440103, B10, 2.877-5

2878

= EXXON PWF 15x15, 2.5X U235, ~~2000~~ppm NAT. BORON  
440101, H1, 4.671-2  
440102, 016, 3.334-2  
440103, B10, 3.138-5

3112

= EXXON PWF 15x15, 2.5X U235, ~~2000~~ppm NAT. BORON  
440101, H1, 4.671-2  
440102, 016, 3.334-2  
440103, B10, 3.400-5

/MODE  
 [E25N]BI.P9.T200. HENRY TRAN  
 USER,VVHPSN,CASA,NC.  
 CHARGE,W973301,V61-  
 TITLE([E25N]BI) EXXON 15x15 PWR, 2.5% U235, ~~400~~ <sup>477</sup>ppm NAT.BORON  
 ATTACH([NITAW],1,2)  
 ATTACH([ATM123],1,0A)  
 REWIND,TAPE1.  
 LABEL,TAPE1,D=0E,L=KXSICT,VSN=007421.  
 COPYDF,TAPE1,TAPE2.  
 REWIND,TAPE2.  
 RETURN,TAPE1.  
 NITAW,PL=177777.  
 RETURN,TAPE2.  
 REWIND,TAPE1.  
 COPYDF,TAPE1,TAPE2.  
 REWIND,TAPE2.  
 ATTACH([XSDRNPM],1,0A).  
 XSDRNPM,PL=177777.  
 REWIND,TAPE2,TAPE3.  
 RETURN,TAPE1.  
 ATTACH([NITAW],1,2).  
 NITAW,PL=177777.  
 REWIND,TAPE4.  
 RETURN,TAPE2,TAPE3.  
 LABEL,TAPE4,M,D=0E,L=KXSICT,VSN=007421.  
 COPYDF,TAPE4,TAPE1.

-LDR  
 144 2 2 36 0 0 1 1 0 126 0 -1 0 1  
 244 1001 30004  
 50000 10001 110000 120000 130000  
 140000 150000 160000 170000 180000 190000  
 200000  
 25022351 47922351 50922351  
 25922351 47922351 50922351  
 2500004 4200004 5000004  
 25400000 42400000 50400000  
 2510001 4210001 5010001  
 2550100 4250100 5050100  
 33922751  
 33921381  
 3380064  
 33400000  
 3310001  
 3350100

[E25N]BI EXXON 15x15 PWR, 2.5% U235, ~~400~~ <sup>477</sup>ppm NAT.BORON  
 144 2 3 11 0 3 3 10 8 3 1 10 12 0 0 0  
 244 -2 -1 -1 1  
 344 1 0 0 0 4.0 0 0 0 0 0 1 0  
 444 -1 123 0 -2 3 4 126 -1 0  
 544 1.-4 2.-4 1.0 0.0 0.0 1.420892 1  
 7  
 1344 1  
 1 1  
 1  
 2  
 2  
 3 3  
 3

48 JUM

1411

0  
25922351 25922361  
2580004  
0  
23400000  
0  
2510001 2580004  
2550100

1544

0.0  
5.8114-4 2.2279-2  
6.5920-2  
0.0  
3.8622-2  
0.0  
6.4471-2 1.334-1  
1.177-

1744

581.0 40.0

1944

410.0 116.4445 310.5271 0.8064

2144

581 241 483

2344

1 2 3

2544

72

2744

12111.0 117.0

2944

0 0 0 0 1 4 3 12 0 -1 0

3144

10001 80004  
50000 40002 110000 120005 130000  
140005 240003 250005 260001 280003 820000  
50130  
41922351 50922351  
42922381 50922381  
4180004 5093304  
42400000 50400000  
4010001 5010001  
4250100 5050100  
33922351  
33922381  
3380004  
33400000  
3310001  
3350100  
25922351  
25922381  
2580004  
25400000  
2510001  
2550100

3344

FOR

/NOISE  
 EDN:1B1,F0,12000. HENRY TRAN  
 USER,VK9PSN,CASH,NC.  
 CHARGE,M973501,VSC.  
 TITLE([E25K1B1] EXXON 15x15 PWR, 2.55U235, ~~400~~ <sup>1073</sup> pps NET-BORON)  
 LABEL,TAPEA,D=0E,L=EXSECT,VEN=007421.  
 COPYRF,TAPEA,TAPEA.  
 REMIND,TAPEA.  
 RETURN,TAPEA.  
 REFL(EO=10)  
 ATTACHP,BIND0,1,24.  
 MEM04,PL=777777.  
 /LCP

([E25K1B1] EXXON 15x15 PWR, 2.55U235, ~~400~~ <sup>1073</sup> pps NET-BORON  
 99.0 73 300 3 123 75 45 5 22 0  
 1 3 1 1 -10 1 0 300 00 1  
 0 0 0 0 0 0 0 0 0 0  
 0.0 -1.0 0.0 -1.0 -1.0 -1.0  
 1 2592235 1.7744-4  
 1 2592236 6.8330-3  
 1 2592237 3.5010-2  
 1 2540000 4.7125-3  
 1 2510001 3.8073-2  
 1 2650100 8.7110-4  
 2 10501 6.4711-2 1 81004 3.7326-2 3 56100 1.1771-5  
 2 80002 2.4100-4 3 250005 1.0900-3  
 1 260001 8.1800-3 2 180003 1.9000-4  
 4 820000 3.2900-2  
 5 10001 2.7700-2 5 50000 1.4600-3 5 80034 2.7100-2  
 8 180000 2.8600-4 5 120005 2.0800-4 5 130000 2.9700-3  
 5 140005 3.4700-4 0 260001 4.0900-5

Generalized geometry cards



# CALCULATION SHEET

4.4) Fuel at (4.2% U235, <sup>2754</sup>~~2300~~ ppmB) <sup>JWV</sup>

See section (4.2) for NITAWL input

CLIENT:	JOB NO.	REVISION:
ORIGINATOR: HENRY TRAN	DATE:	CALC. NO. :
CHECKER:	DATE:	PAGE: 51

NULIF INPUT PARAMETERS  
 \*\*\*\*\*

NULIF requires the following parameters as input: dimensions of the fuel unit cell, reactor power history, power density based on the fuel cell volume, atomic densities of the materials in the fuel cell (fuel pellet, cladding, and moderator).

The basic dimensions of the fuel unit cell are given in previous sections. The fuel cell with the designed pitch will be used for all the NULIF calculations in this criticality analysis. The reactor operating cycle is taken as 16 months at full power and 2 months of outage. Other required parameters are calculated below:

\*\* Atomic Density Calculations:

.....

The following fuel parameter will be considered in this section:

$$\text{Enrichment} := 4.2\% \cdot$$

$$\text{Burnup} := 0.0 \frac{\text{GWd}}{\text{MTU}}$$

$$\text{Nat\_Boron\_Con} := 1005 \text{ ppm}$$

*1198 M Cur*

o U-235 atomic densities based on pellet volume:

$$N_{\text{U235}} := \text{Uranium\_Density} \cdot \frac{\text{Avogadro}}{\text{MW}_{\text{U235}}} \cdot \text{Enrichment}$$

$$N_{\text{U235}} = 9.7632 \cdot 10^{-4} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

o U238 atomic densities based on pellet volume:

$$N_{\text{U238}} := \text{Uranium\_Density} \cdot \frac{\text{Avogadro}}{\text{MW}_{\text{U238}}} \cdot (1.0 - \text{Enrichment})$$

$$N_{U238} = 2.1989 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

o O16 atomic density based on pellet volume:

$$N_{O16} := 2 \cdot (N_{U238} + N_{U235})$$

$$N_{O16} = 4.593 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

o Zirconium cladding atomic density is taken a

$$N_{Zr40} := 4.291 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}} \quad \dots \text{Reference(10)}$$

o H1 atomic density in water:

$$N_{H1\_70F} := 6.671 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}} \quad (\text{at } T = 70F)$$

$$N_{H1\_212F} := 6.406 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}} \quad (\text{at } T = 212F)$$

o O16 atomic density in water:

$$N_{O16\_70F} := 3.336 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}} \quad (\text{at } T = 70F)$$

$$N_{O16\_212F} := 3.203 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}} \quad (\text{at } T = 212F)$$

o Natural boron concentration in water:

~~$N_{\text{NatBoron}_70F} := \text{Nat\_Boron\_Con} \cdot N_{\text{H1}_70F}$~~

$$N_{\text{NatBoron}_70F} = 6.671 \cdot 10^{-5} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

~~$N_{\text{NatBoron}_212F} := \text{Nat\_Boron\_Con} \cdot N_{\text{H1}_212F}$~~

$$N_{\text{NatBoron}_212F} = 6.406 \cdot 10^{-5} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

o Operating time required to attain the desired burnup level:

$$\text{Operating\_Time} := \text{Burnup} \cdot \text{Number\_Assem} \cdot \frac{\text{MTHM}}{\text{Reactor\_Power}}$$

$$\text{Operating\_Time} = 0 \cdot \text{day}$$

*M. Co*  
*M. Co*

54, 2011



NITAWL INPUT PARAMETERS

\*\*\*\*\*

The first NITAWL computer run (see Figure[ ] ) is used to format the cross sections from the 123 group cross section set contained in the AMPX master library. This NITAWL computer run also performs resonance self-shielding corrections for the following nuclides: U-236, U238, Pu-240, and Pu-242. If the loaded fuel is unirradiated (i.e., fresh fuel) then only U-238 is corrected for resonance self-shielding.

\*\* Dancoff factor:

\*\*\*\*\*

The Dancoff factor calculated by the NULIF code is given as:

$$\text{Dancoff\_NULIF} := \text{~~0.7992~~} 0.7992 \quad \text{H\#J}$$

However the Dancoff factor from the NULIF output is not defined in the same way as the one requested by the NITAWL computer code. The NITAWL's Dancoff factor is defined as:

$$\text{Dancoff\_NITAWL} := 1.0 - \text{Dancoff\_NULIF}$$

Thus, for this case:

$$\text{Dancoff\_NITAWL} = \text{~~0.2008~~} 0.2008 \quad \text{H\#J}$$

\*\* Scattering Cross Sections Parameters

\*\*\*\*\*

The following potential scattering cross sections are obtained from Reference(11).

$\sigma_{016} := 3.8 \cdot \text{barn}$	$\sigma_{U235} := 10 \cdot \text{barn}$
$\sigma_{U236} := 10 \cdot \text{barn}$	$\sigma_{U238} := 9 \cdot \text{barn}$
$\sigma_{Pu240} := 11 \cdot \text{barn}$	$\sigma_{Pu242} := 11 \cdot \text{barn}$

13. U-238 Resonance Parameters:

-----  
For fresh fuel, the atomic density of U-238 (N\_U238) previously calculated is used. For irradiated fuel, the N\_U238 must be replaced with the value obtained from the NULIF burnup calculation results.

- o First moderator (U-235) scattering cross section per absorber atom (U-238):

$$\sigma_{s1} := \frac{N_{U235}}{N_{U238}} \cdot \sigma_{U235}$$

$$\sigma_{s1} = 0.444 \cdot \text{barn}$$

- o Second moderator (O-16) scattering cross section per absorber atom (U-238):

$$\sigma_{s2} := \frac{N_{O16}}{N_{U238}} \cdot \sigma_{O16}$$

$$\sigma_{s2} = 7.9374 \cdot \text{barn}$$

- o Effective moderator cross section per absorber atom (U-238):

$$\sigma_{m\_eff} := \sigma_{U238} + (\sigma_{s1} + \sigma_{s2}) + \frac{1}{\text{Pellet\_Dia} \cdot N_{U238}}$$

$$\sigma_{m\_eff} = 68.5378 \cdot \text{barn}$$

XSDRNPM INPUT PARAMETERS

\*\*\*\*\*

The geometric model for the XSDRNPM code is a cylindrical fuel unit cell with radius based on the modified pitch of the square unit cell. The dimensions of the fuel unit cells are calculated in section entitled "Basic Fuel Geometry Calculations". The atomic densities used in the XSDRNPM mixing table are the same as the values calculated in the "MULIF INPUT PARAMETERS" section. The fuel-clad air gap and the cladding region is combined together to form a single Zirconium region with the atomic density calculated below:

$$N_{Zr40\_XSD} := \frac{Clad\_Vol}{Clad\_Vol + Gap\_Vol} \cdot N_{Zr40}$$

$$N_{Zr40\_XSD} = 3.8022 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}}$$

KENO INPUT PARAMETERS

\*\*\*\*\*

The geometric models of the KENO-IV computer code are discussed in Section 5.0. Unless specifically noted, all the geometry cards of the KENO input remain the same as the reference geometric model discussed in Section 5.0. This section will calculate other input parameters applied to this particular KENO run.

Since the loaded fuel assemblies in the cask are homogenized, the atomic densities in the KENO mixing table must be based on the volume of the fuel cell (with modified pitch). The homogenized atom densities of all the nuclides in the fuel cell are calculated below:

$$N_{U235\_Homo} := \frac{Pellet\_Vol}{ModCell\_Vol} \cdot N_{U235}$$

$$N_{U235\_Homo} = 2.981 \cdot 10^{-4} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}}$$

$$N_{U238\_Homo} := \frac{Pellet\_Vol}{ModCell\_Vol} \cdot N_{U238}$$

$$N_{U238\_Homo} = 6.7138 \cdot 10^{-3} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}}$$

$$N_{Zr40\_Homo} := \frac{Clad\_Vol}{ModCell\_Vol} \cdot N_{Zr40}$$

$$N_{Zr40\_Homo} = 4.7125 \cdot 10^{-3} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}}$$

$$N_{O16\_Homo} := \frac{Pellet\_Vol}{ModCell\_Vol} \cdot N_{O16} + \frac{Mod\_H2O\_Vol}{ModCell\_Vol} \cdot N_{O16\_70F}$$

$$N_{O16\_Homo} = 3.3063 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn}\cdot\text{cm}}$$

$$N_{H1\_Homo} := \frac{Mod\_H2O\_Vol}{ModCell\_Vol} \cdot N_{H1\_70F}$$

$$N_{H1\_Homo} = 3.8073 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

~~$$N_{NatBoron\_Homo} := N_{H1\_Homo} \cdot Nat\_Boron\_Con$$~~

$$N_{NatBoron\_Homo} = 3.8073 \cdot 10^{-5} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

300  
/NOBEG  
MULTI,PO,1500, HENRY TRAN  
USER,WK9PSN,CASH,NC.  
CHANGE,0973301,VSC.  
TITLE([E42NUE1]) EXXON PWR 15x15, 4.2X U235, BOKATED WATER  
ATTACHP(LEB1,1,0)  
ATTACHP(LEB2,1,0)  
ATTACHP(LEB3,1,0)  
REWIND,TAPE1,TAPE2,TAPE3.  
ATTACHP,MULTI,9,1.  
MULTI(PL=77777)  
-EOF

=([E42NUE1]) EXXON PWR 15x15, 4.2X U235, BOKATED WATER  
\*General parameters:  
000001, 1, 0, 1.0-5, 1.0-20  
000002, 500  
000003, 1  
300001, 0.0, 1, 1.0, 1, 1  
300002, 0.0, 1, 1.0, 1  
300003, 0.0, 1, 1.0, 1  
300004, 0.0, 1, 1.0, 1  
300005, 0.0, 1, 1.0, 1  
300006, 0.0, 1, 1.0, 1  
300007, 0.0, 1, 1.0, 1  
300008, 0.0, 1, 1.0, 1  
300009, 0.0, 1, 1.0, 1  
300010, 0.0, 1, 1.0, 1  
300011, 0.0, 1, 1.0, 1  
300012, 0.0, 1, 1.0, 1  
300013, 0.0, 1, 1.0, 0, 3

\*Composition data:  
300100, 0, 1  
\*Cell geometry  
310100, 1, 0.8490, 0.8494, 1.0541, 1.0256, 0  
310101, 70.0, 70.0, 70.0, 0.0  
\*Compositions of fuel rods 15.2X U235 (1.1):  
320101, U235, 9.7673-4  
320102, U238, 1.1989-2  
320103, O16, 4.5936-2  
330101, H1, 4.671-2  
\*Compositions of water coolant(7x 70 F, Pw14.7 psi):  
= EXXON PWR 15x15, 4.2X U235, 0ppm NAT. BORON  
340101, H1, 6.671-2  
340102, O16, 3.336-2  
340103, B10, 1.000-20  
/ *300 m. Co*  
= EXXON PWR 15x15, 4.2X U235, ~~400~~ppm NAT. BORON  
400101, H1, 6.671-2  
400102, O16, 3.336-2  
400103, B10, 3.923-6  
/ *836 m. Co*  
= EXXON PWR 15x15, 4.2X U235, ~~400~~ppm NAT. BORON  
440101, H1, 6.671-2  
440102, O16, 3.336-2  
440103, B10, 9.153-6  
/ *1197 m. Co*  
= EXXON PWR 15x15, 4.2X U235, ~~400~~ppm NAT. BORON  
440101, H1, 6.671-2  
440102, O16, 3.336-2  
440103, B10, 1.308-5  
/ *1436 m. Co*  
= EXXON PWR 15x15, 4.2X U235, ~~400~~ppm NAT. BORON

60 *5/14*

440101, HI, 4-671-2  
440102, OIA, 3-336-2  
440103, B10, 1-869-5

*1676 am l*

\* EYXON FWP 15x15, 4.25 U235, ~~440101~~ NAT. BORON

440101, HI, 4-671-2  
440102, OIA, 3-336-2  
440103, B10, 1-831-5

*195 am l*

\* EYXON FWP 15x15, 4.25 U235, ~~440101~~ NAT. BORON

440101, HI, 4-671-2  
440102, OIA, 3-336-2  
440103, B10, 2-092-5

*215 am l*

\* EYXON FWP 15x15, 4.25 U235, ~~440101~~ NAT. BORON

440101, HI, 4-671-2  
440102, OIA, 3-336-2  
440103, B10, 2-754-5

*234 am l*

\* EYXON FWP 15x15, 4.25 U235, ~~440101~~ NAT. BORON

440101, HI, 4-671-2  
440102, OIA, 3-336-2  
440103, B10, 2-615-5

*2674 am l*

\* EYXON FWP 15x15, 4.25 U235, ~~440101~~ NAT. BORON

440101, HI, 4-671-2  
440102, OIA, 3-336-2  
440103, B10, 1-877-5

*2023 am l*

\* EYXON FWP 15x15, 4.25 U235, ~~440101~~ NAT. BORON

440101, HI, 4-671-2  
440102, OIA, 3-336-2  
440103, B10, 3-179-5

*2112 am l*

\* EYXON FWP 15x15, 4.25 U235, ~~440101~~ NAT. BORON

440101, HI, 4-671-2  
440102, OIA, 3-336-2  
440103, B10, 3-800-5

*351 am l*

\* EYXON FWP 15x15, 4.25 U235, ~~440101~~ NAT. BORON

440101, HI, 4-671-2  
440102, OIA, 3-336-2  
440103, B10, 3-923-5

```

#JOB
#NOSED
E42NKB1,FD,T200, HENRY TERN
USER,VKYPON,CAK,NC-
CHARGE,N973301,VSC-
TIT#F/[E42NKB1] EXXON 15x15 PWR, 4.2% U235, 2500 ppa NAT-BORON)
LABEL,TAPEA,I=OF,I=EXSECT,USN=007421.
COPYBI,TAPEA,TAPE4.
RETURN,TAPEA.
REWIND,TAPE4.
COPYBI,TAPE4,TAPE2.
REWIND,TAPE4.
ATTACHP,XSDRNPM,1,0A.
XSDRNPM(PL=777777)
REWIND,TAPE2,TAPE3.
RETURN,TAPE4.
ATTACHP,NITAWL,1,2.
NITAWL(PL=777777)
REWIND,TAPE4.
RETURN,TAPE2,TAPE3.
LABEL,TAPEA,M,DAGE,I=EXSECT,USN=007421.
COPYBI,TAPE4,TAPE4.

```

*2753 m c*

```

-EOB
[E42NKB1] EXXON 15x15 PWR, 4.2% U235, 2500 ppa NAT-BORON
104 7 3 11 0 0 1.40 E 1 1 10 12 0 0 0
109 -2 -1 -1 E
111 1 0 0 0 0 0 0 0 0 1 0
114 -1 125 0 0 0 0 126 -1 0
117 1 -4 2 -4 1 0 0 0 0 1.420892 E

```

*2753 m c*

```

1034 1
1 1
1
1
1
1
1
1
1
1
1444
42922351 42922361
4280004
0
42400000
0
4210001 4280004
4280100
15**
0.0
9.7672-4 2.1969-2
4.5930-2
0.0
3.8022-2
0.0
6.471-2 3.336-2
3.007-5
1
33** 5R1.0 F0.0
1
35** 410.0 110.445 310.5271 0.8044
36** 5R1 2R2 4R3
39** 1 2 3
40** F3

```

*62* *8/11*



5144 12111-0 123.0

7106

144 0 0 32 4 0 3 4 6 126 0 -1 0 1

244

10001 80004

50000 60002 110000 120005 130000

140005 240003 250005 260001 280003 329000

50100

50922351

50922351

5080004

50600000

5010001

5050100

35922351

33922351

3380004

33400000

3310001

3350100

25922351

25922351

2580004

25400000

2510001

2550100

42922351

42922351

4280004

42400000

4210001

4250100

7106

1368  
 UNOSED  
 E42KEF1,PG,T2000. HENRY TRAN  
 USER,VH4PSN,CASH,NC.  
 CHARGE,N973301,VSC.  
 TITLE([E42KEB1] EXXON 15x15 PWR, 4.25U235, <sup>2753 m.c.</sup> #390 ppa NAT.BORON)  
 LABEL,TAPEA,D=GE,L=EXBECT,VSN=007421.  
 COPYBF,TAPEA,TAPE4.  
 REMIND,TAPE4.  
 RE 3, TAPE4.  
 RFL(FC=10)  
 ATTACHP,KEN04,1,3A.  
 KEN04,PL=777777.  
 /EOR

<sup>2753 m.c.</sup>  
 [E42KEB1] EXXON 15x15 PWR, 4.25U235, #390 ppa NAT.BORON  
 99.0 75 700 3 123 75 -18 8 32 4  
 1 1 1 1 -1P 3 0 2900 00 3  
 0 0 0 0 0 0 0 0 0  
 0.5 -1.0 0.0 -1.0 -1.0 -1.0  
 1 42922351 2.9910-4  
 1 42922361 6.7178-3  
 1 4280000 7.3073-2  
 1 42400000 4.7105-1  
 1 4210001 3.6073-2  
 1 4250100 1.7160-5  
 2 17001 6.671-2 2 80004 3.336-2 0 50100 3.007-5  
 3 60002 2.0100-4 3 250305 1.1700-3  
 3 260001 8.2900-2 3 140005 1.9000-4  
 4 820100 3.2960-2  
 5 10001 1.7780-2 5 30000 1.4600-3 5 80004 3.7100-2  
 5 110000 2.6000-4 5 120005 2.0800-4 5 130200 8.9700-2  
 5 140005 7.6703-4 5 260001 3.8900-5

Generalized geometry cards



64 OJM

# CALCULATION SHEET

4.5) Fuel at ( 5.0% U235, <sup>3354 Mi<sup>6</sup> GM</sup>~~2500~~ ppm B)

Only NULIF run is performed.  
Keff for this case is extrapolated  
from Figure (2-1).

CLIENT:	JOB NO.	REVISION:
ORIGINATOR: HENRY TRAN	DATE:	CALC. NO. :
CHECKER:	DATE:	PAGE: 151

## NULIF INPUT PARAMETERS

NULIF requires the following parameters as input: dimensions of the fuel unit cell, reactor power history, power density based on the fuel cell volume, atomic densities of the materials in the fuel cell (fuel pellet, cladding, and moderator).

The basic dimensions of the fuel unit cell are given in previous sections. The fuel cell with the designed pitch will be used for all the NULIF calculations in this criticality analysis. The reactor operating cycle is taken as 16 months at full power and 2 months of outage. Other required parameters are calculated below:

### \*\* Atomic Density Calculations:

-----  
The following fuel parameter will be considered in this section:

Enrichment := 5.0%

Burnup :=  $0.0 \frac{\text{Gwd}}{\text{MTU}}$

Nat\_Boron\_Con := 4000 ppm *1198 M. L. 2M*

o U-235 atomic densities based on pellet volume:

$$N_{U235} := \text{Uranium\_Density} \cdot \frac{\text{Avogadro}}{\text{MW}_{U235}} \cdot \text{Enrichment}$$

$$N_{U235} = 1.1623 \cdot 10^{-3} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

o U238 atomic densities based on pellet volume:

$$N_{U238} := \text{Uranium\_Density} \cdot \frac{\text{Avogadro}}{\text{MW}_{U238}} \cdot (1.0 - \text{Enrichment})$$

$$N_{U238} = 2.1805 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

o O16 atomic density based on pellet volume:

$$N_{O16} := 2 \cdot (N_{U238} + N_{U235})$$

$$N_{O16} = 4.5935 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

o Zirconium cladding atomic density is taken as:

$$N_{Zr40} := 4.291 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}} \quad \dots \text{Reference(10)}$$

o H1 atomic density in water:

$$N_{H1\_70F} := 6.671 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}} \quad (\text{at } T = 70F)$$

$$N_{H1\_212F} := 6.406 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}} \quad (\text{at } T = 212F)$$

o O16 atomic density in water:

$$N_{O16\_70F} := 3.336 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}} \quad (\text{at } T = 70F)$$

$$N_{O16\_212F} := 3.203 \cdot 10^{-2} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}} \quad (\text{at } T = 212F)$$

o Natural boron concentration in water:

~~$N_{\text{NatBoron}_70F} := \text{Nat\_Boron\_Con} \cdot N_{\text{H}_1\_70F}$~~  *W.C.*

$$N_{\text{NatBoron}_70F} = 6.671 \cdot 10^{-5} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

*JVM*

~~$N_{\text{NatBoron}_212F} := \text{Nat\_Boron\_Con} \cdot N_{\text{H}_1\_212F}$~~  *W.C.*

$$N_{\text{NatBoron}_212F} = 6.406 \cdot 10^{-5} \frac{\text{atoms}}{\text{barn} \cdot \text{cm}}$$

o Operating time required to attain the desired burnup level:

$$\text{Operating\_Time} := \text{Burnup} \cdot \text{Number\_Assem} \cdot \frac{\text{MTHM}}{\text{Reactor\_Power}}$$

$$\text{Operating\_Time} = 0 \cdot \text{day}$$

NITAWL INPUT PARAMETERS  
\*\*\*\*\*

The first NITAWL computer run (see Figure[ ]) is used to format the cross sections from the 123 group cross section set contained in the AMPX master library. This NITAWL computer run also performs resonance self-shielding corrections for the following nuclides: U-236, U238, Pu-240, and Pu-242. If the loaded fuel is unirradiated (i.e., fresh fuel) then only U-238 is corrected for resonance self-shielding.

\*\* Dancoff factor:  
.....

The Dancoff factor calculated by the NULIF code is given as:

$$\text{Dancoff\_NULIF} := \del{0.7832} 0.7992 \quad \text{HHT}$$

However the Dancoff factor from the NULIF output is not defined in the same way as the one requested by the NITAWL computer code. The NITAWL's Dancoff factor is defined as:

$$\text{Dancoff\_NITAWL} := 1.0 \cdot \text{Dancoff\_NULIF}$$

Thus, for this case:

$$\text{Dancoff\_NITAWL} = \del{0.2468} 0.2008 \quad \text{HHT}$$

\*\* Scattering Cross Sections Parameters  
.....

The following potential scattering cross sections are obtained from Reference(11).

$\sigma_{016} := 3.8 \cdot \text{barn}$	$\sigma_{\text{U}235} := 10 \cdot \text{barn}$
$\sigma_{\text{U}236} := 10 \cdot \text{barn}$	$\sigma_{\text{U}238} := 9 \cdot \text{barn}$
$\sigma_{\text{Pu}240} := 11 \cdot \text{barn}$	$\sigma_{\text{Pu}242} := 11 \cdot \text{barn}$

1). U-238 Resonance Parameter:

-----  
For fresh fuel, the atomic density of U-238 (N\_U238) previously calculated is used. For irradiated fuel, the N\_U238 must be replaced with the value obtained from the NU:IF burnup calculation results.

- o First moderator (U-235) scattering cross section per absorber atom (U-238):

$$\sigma_{s1} := \frac{N_{U235}}{N_{U238}} \cdot \sigma_{U235}$$

$$\sigma_{s1} = 0.533 \cdot \text{barn}$$

- o Second moderator (O-16) scattering cross section per absorber atom (U-238):

$$\sigma_{s2} := \frac{N_{O16}}{N_{U238}} \cdot \sigma_{O16}$$

$$\sigma_{s2} = 8.0051 \cdot \text{barn}$$

- o Effective moderator cross section per absorber atom (U-238):

$$\sigma_{m\_eff} := \sigma_{U238} + (\sigma_{s1} + \sigma_{s2}) + \frac{1}{\text{Pellet\_Dia} \cdot N_{U238}}$$

$$\sigma_{m\_eff} = 69.1253 \cdot \text{barn}$$



/JOB  
 /NOISE0  
 MULIF,90,7600. HENRY TRAN  
 USER,VK9PSN,CASX,NC.  
 CHARGE,N973301,VSC.  
 TITLE((E50N0B1) EXXON PWR 15x15, 5.0% U235, BORATED WATER)  
 ATTACHP(LEB1,1,0)  
 ATTACHP(LEB2,1,0)  
 ATTACHP(LEB3,1,0)  
 REWIND,TAPE1,TAPE2,TAPE3.  
 ATTACHP,MULIF,9,1.  
 MULIF(PL=777777)  
 /EOF

=(E50N0B1) EXXON PWR 15x15, 5.0% U235, BORATED WATER

=General parameters:

000001, 1, 0, 1.0-5, 1.0-20

000002, 500

000003, 1

Optm 100001,	0.0,	1,	1.0,	1,	3
300ppm 100002,	0.0,	1,	1.0,	1,	1
700ppm 100003,	0.0,	1,	1.0,	1,	1
1000ppm 100004,	0.0,	1,	1.0,	1,	1
1200ppm 100005,	0.0,	1,	1.0,	1,	1
1400ppm 100006,	0.0,	1,	1.0,	1,	1
1600ppm 100007,	0.0,	1,	1.0,	1,	1
1800ppm 100008,	0.0,	1,	1.0,	1,	1
2000ppm 100009,	0.0,	1,	1.0,	1,	1
2200ppm 100010,	0.0,	1,	1.0,	1,	1
2400ppm 100011,	0.0,	1,	1.0,	1,	1
2600ppm 100012,	0.0,	1,	1.0,	1,	1
2800ppm 100013,	0.0,	1,	1.0,	0,	3

=Composition data:

300100, 1, 1

=Cell geometry

310100, 1, 0.8290, 0.8074, 1.0541, 1.4355, 0

310101, 70.0, 70.0, 70.0, 0.0

=Compositions of fuel rod (5.0% U235 1.2%)

320101, U235, 1.1623-3

320102, U238, 2.1805-2

320103, O16, 4.8435-2

330101, ZY4, 4.291-2

=Compositions of water coolant(T= 70 F, P=14.7 psi)

= EXXON PWR 15x15, 5.0% U235, 0ppm NAT. BORON

340101, H1, 6.671-2

340102, O16, 3.336-2

340103, B10, 1.000-20

/

= EXXON PWR 15x15, 5.0% U235, <sup>259ppm</sup>ppm NAT. BORON

440101, H1, 6.671-2

440102, O16, 3.336-2

440103, B10, 3.923-6

/

= EXXON PWR 15x15, 5.0% U235, <sup>838ppm</sup>ppm NAT. BORON

440101, H1, 6.671-2

440102, O16, 3.336-2

440103, B10, 9.153-6

/

= EXXON PWR 15x15, 5.0% U235, <sup>1197ppm</sup>ppm NAT. BORON

440101, H1, 6.671-2

440102, O16, 3.336-2

440103, B10, 1.308-5

/

= EXXON PWR 15x15, 5.0% U235, <sup>1436ppm</sup>ppm NAT. BORON

71 01/19

440101, HI, 6.671-2  
440102, O16, 3.336-2  
440103, B10, 1.569-5

*1676*

= EXXON PWR 15x15, 5.04 U235, ~~4400~~ppm NAT. BORON

440101, HI, 6.671-2  
440102, O16, 3.336-2  
440103, B10, 1.831-5

*19.5*

= EXXON PWR 15x15, 5.04 U235, ~~4400~~ppm NAT. BORON

440101, HI, 6.671-2  
440102, O16, 3.336-2  
440103, B10, 2.092-5

*2155*

= EXXON PWR 15x15, 5.04 U235, ~~4400~~ppm NAT. BORON

440101, HI, 6.671-2  
440102, O16, 3.336-2  
440103, B10, 2.354-5

*2394*

= EXXON PWR 15x15, 5.04 U235, ~~4400~~ppm NAT. BORON

440101, HI, 6.671-2  
440102, O16, 3.336-2  
440103, B10, 2.615-5

*2633*

= EXXON PWR 15x15, 5.04 U235, ~~4400~~ppm NAT. BORON

440101, HI, 6.671-2  
440102, O16, 3.336-2  
440103, B10, 2.877-5

*2873*

= EXXON PWR 15x15, 5.04 U235, ~~4400~~ppm NAT. BORON

440101, HI, 6.671-2  
440102, O16, 3.336-2  
440103, B10, 3.138-5

*3112*

= EXXON PWR 15x15, 5.04 U235, ~~4400~~ppm NAT. BORON

440101, HI, 6.671-2  
440102, O16, 3.336-2  
440103, B10, 3.400-5

*3581*

= EXXON PWR 15x15, 5.04 U235, ~~4400~~ppm NAT. BORON

440101, HI, 6.671-2  
440102, O16, 3.336-2  
440103, B10, 3.923-5

EQP

72 *DM*





```

8      800000  -25400000 -13800000 -8200000 -5000000
9      10001   -2510001  -1310001  -8210001  -5010001
10     50100   -2550100  -1350100  -8250100  -5050100
11
12     922381  294.27  2  0.4445  0.2000  67.3214  2.237901-02
13     1 235.0  3.597E-1  1 15.99  7.79740  1 1.0
14     25922381 294.27  2  0.4445  0.2000  67.3214  2.237901-02
15     1 235.0  3.597E-1  1 15.99  7.79740  1 1.0
16     33922381 294.27  2  0.4445  0.2000  67.3214  2.237901-02
17     1 235.0  3.456E-1  1 15.99  7.86270  1 1.0
18     42922381 294.27  2  0.4445  0.2000  68.0376  2.192901-02
19     1 235.0  3.440E-1  1 15.99  7.90740  1 1.0
20     50922381 294.27  2  0.4445  0.2000  69.1253  2.180501-02
21     1 235.0  3.370E-1  1 15.99  8.00510  1 1.0
22

```

\*\*\*\*\* [ V D O F I R P O \* L I S T I A G \*\*\*\*\* ]

4 XRAY 10 ENTRIES READ

```

BT
FROM  NUMBER OF EXTRA CROSS SECTIONS 0
MNT  NUMBER OF NUCLIDES FROM MASTER LIBRARY 41
DNT  NUMBER OF NUCLIDES FROM 1-BEST LIBRARY 100
RNT  NUMBER OF NUCLIDES FROM 1-BEST LIBRARY 100 31
NCK  ANIS/DIF/DORSE OUTPUT TRIGGER
NIX  TOTAL CROSS SECTION POSITION 7
RE   WITHIN-GROUP SCATTERING CROSS SECTION POSITION 4
IRES NUMBER OF RESONANCE CALCULATIONS 5
TON  TABLE LENGTH FOR CROSS SECTIONS 120
JPH  TO RN OLD ANIS LIBRARY MOUNTED * (0/1 NUMBER) 0
LPA  OUTPUT OPTION TRIGGER -1
YPC  PRINT CONTROL - ANIS OUTPUT 0

```

DISK STORAGE ALLOCATED FOR THIS CASE IS 33000 WORDS

24 XRAY 41 ENTRIES READ

34 XRAY 73 ENTRIES READ

BT

GENERAL INFORMATION CONCERNING CROSS SECTION LIBRARY

```

TAPE IDENTIFICATION NUMBER 0
NUMBER OF NUCLIDES ON TAPE 208
NUMBER OF NEUTRON ENERGY GROUPS 127
FIRST THERMAL NEUTRON ENERGY GROUP 94
NUMBER OF GAMMA ENERGY GROUPS 0

```

XSDRN TAPE 0

SUPER-XSDRN LIBRARY--LAST DIGITS OF ID #'S ARE CODED AS FOLLOWS-- 5-800K, 6-800K, 7-850K, 8-750K, 9-1000K, ANYTHING ELSE IS PRACTICALLY THIN--IF THESE THERMAL TEMPERATURES ARE DESIRED, CALL C.W. DRIVEN, JR. OR N. M. GREENE---ALL THERMAL DATA IS PO (1FT0#94). ALSO J. WILSON DATA AND 3 1/2 NUCLIDES JULY, 1968 -THIS IS A CONVERTED TAPE

0 NUCLIDES FROM XSDRN TAPE

1	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	922381
2	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	25922351
3	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	33922351
4	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	42922351
5	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	50922351
6	URANIUM-238P	THERMAL TEMPERATURE = 294.6 K	922381
7	URANIUM-238P	THERMAL TEMPERATURE = 294.6 K	25922381
8	URANIUM-238P	THERMAL TEMPERATURE = 294.6 K	33922381























FOLLOWING IS A CARD IMAGE LISTING OF THE INPUT DATA  
COLUMN NUMBER

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CARD      1111111111222222222233333333334444444444555555555566666666667777777777
NUMBER 1234567890123456789012345678901234567890123456789012345678901234567890

1 1.334181] EXYON 15X15 PAR, 3.34 U35, 176PPM NAT.EGON
2 148 3 3 11 0 3 3 10 6 3 1 10 12 0 0
3 248 -2 -1 -1 .E
4 384 1 0 0 0 4.0 0 0 0 0 0 1 0
5 488 -1 123 0 -2 3 4 126 -1 0
6 5** 1 -4 2 -4 1.0 0.0 0.0 1.420642 E
7
8 1284 1
9 1
10 1
11 2
12 2
13 1
14 3 3
15 3
16 1484
17 4
18 37922354 3792235
19 3325004
20 6
21 33400090
22 8
23 3510001 351000
24 3350100
25 5**
26 0.0
27 7.6711-4 1.2155-2
28 4.3925-2
29 0.0
30 3.8022-2
31 0.0
32 4.671-2 3.335-2
33 1.961-5
34
35 77** 581.0 10.0
36
37 35** 410.0 110.1445 310.5271 0.9044
38 3644 581 282 480
39 3988 1 2 0
40 4044 63
41 5184 12111.0 123.0
42

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\*\*\*\*\* END OF INPUT LISTING \*\*\*\*\*

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XX      XX      SSSSSSSSSSSS  DDDDDDDDDDDDD  RRRRRRRRRRRR  NN      NN  PPPPPPPPPPPP  MM      MM
XX      XX      SSSSSSSSSSSSS  DDDDDDDDDDDDD  RRRRRRRRRRRR  MMN     NN  PPPPPPPPPPPP  MMM     MMM
XX      XX      SS      SS  DD      DD  RR      RR  NNNN     NN  PP      PP  MMMM     MMMM
XX      XX      SS      DD      DD  RR      RR  NN  NN     NN  PP      PP  MM  MM     MM  MM

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XX 058555555555 DD DD PRRRRRRRRRR NN NN NN PRRRRRRRRRR MM MM MM
XX 555555555555 DD DD RRRRRRRRRRR NN NN NN RRRRRRRRRRR MM MM MM
XX XX 55 DD DD RR RR NN NN NN PP MM MM
XX XX 55 DD DD RR RR NN NN NN PP MM MM
XX XX 555555555555 000000000000 RR RR NN NN PP MM MM
XX XX 555555555555 000000000000 RR RR NN NN PP MM MM

```

```

999999999999 00000000 // 00000000 // 00000000 00000000 00000000
999999999999 00000000 // 00000000 // 00000000 00000000 00000000
99 99 00 00 // 00 00 1111 // 00 00 11 11
99 99 00 00 // 00 00 11 // 00 00 11 11
99 99 00 00 // 00 00 11 // 00 00 11 11
999999999999 00 00 // 00 00 11 // 00 00 11 11
999999999999 00 00 // 00 00 11 // 00 00 11 11
99 99 00 00 // 00 00 11 // 00 00 11 11
99 99 00 00 // 00 00 11 // 00 00 11 11
999999999999 00000000 // 00000000 11111111 // 00000000 11111111
999999999999 00000000 // 00000000 11111111 // 00000000 11111111

```

```

00000000 00000000 // 11 11 // 00000000 00000000
00000000 00000000 // 11 11 // 00000000 00000000
00 00 00 00 // 11 11 // 00 00 11 11
00 00 00 00 // 11 11 // 00 00 11 11
00 00 00 00 // 11 11 // 00 00 11 11
00 00 00 00 // 11 11 // 00 00 11 11
00 00 00 00 // 11 11 // 00 00 11 11
00 00 00 00 // 11 11 // 00 00 11 11
00 00 00 00 // 11 11 // 00 00 11 11
00000000 00000000 // 11111111 11111111 // 00000000 00000000
00000000 00000000 // 11111111 11111111 // 00000000 00000000

```

[E32N16] SYNON 16X15 FWR, 3.77 UITS, <sup>776</sup> ~~PPM~~ NAT. BORO

- 1 16 ARRAY 15 ENTRIES READ
- 2 24 ARRAY 10 ENTRIES READ
- 3 14 ARRAY 12 ENTRIES READ
- 4 41 ARRAY 9 ENTRIES READ
- 5 54 ARRAY 12 ENTRIES READ

THE FOLLOWING DIRECT ACCESS SPACE IS REQUIRED  
 LOGICAL UNIT 8 HAS 153 BLOCKS OF LENGTH 1497 WORDS  
 LOGICAL UNIT 9 HAS 12 BLOCKS OF LENGTH 2047 WORDS  
 LOGICAL UNIT 10 HAS 492 BLOCKS OF LENGTH 55 WORDS

GENERAL PROBLEM DESCRIPTION DATA BLOCK  
 GENERAL PROBLEM DATA

IGE 1/2/3 = PLANE/CYLINDER/SPHERE	2	ISM QUADRATURE ORDER	8
IIM NUMBER OF ZONES	3	ISCT ORDER OF SCATTERING	3
IM NUMBER OF SPACIAL INTERVALS	11	IEVT 0/1/2/3/4/5/6=0/K/ALPHA/C/2/R/H	1
IBL 0/1/2/3 = VACUUM/REFL/PER/WHITE	0	IIM INNER ITERATION MAXIMUM	10
IBR RIGHT BOUNDARY CONDITION	3	ICM OUTER ITERATION MAXIMUM	12
MXM NUMBER OF MIXTURES	3	ICLC +1/0/N--FLAT RES/BN/ORT	0
MS MIXING TABLE LENGTH	10	ITH 0/1 = FORWARD/ADJOINT	0
IOM NUMBER OF ENERGY GROUPS	123	IFLU 0/1/2/3/4=L-S/L/S/W/L-W	0
NNG NUMBER OF NEUTRON GROUPS	123	JPRT -2/-1/0/N=MIXTURE XSEC PRINT	-2
NGG NUMBER OF GAMMA GROUPS	0	ID1 0/1/2/3=NO/PRT ND/PCH N/BOTH	-1







94	1.65910E+00	1.54980E+01	1.84660E+06	94	0	1.00000E+00
95	1.70900E+00	1.75022E+01	1.76924E+06	95	0	1.00000E+00
96	1.56660E+00	1.56692E+01	1.69258E+06	96	0	1.00000E+00
97	1.42150E+00	1.57594E+01	1.61075E+06	97	0	1.00000E+00
98	1.28490E+00	1.58674E+01	1.51951E+06	98	0	1.00000E+00
99	1.13370E+00	1.59926E+01	1.42692E+06	99	0	1.00000E+00
100	9.99190E-01	1.61189E+01	1.33974E+06	100	0	1.00000E+00
101	8.81030E-01	1.62448E+01	1.25456E+06	101	0	1.00000E+00
102	7.83530E-01	1.63816E+01	1.16906E+06	102	0	1.00000E+00
103	6.95220E-01	1.65409E+01	1.07106E+06	103	0	1.00000E+00
104	5.28800E-01	1.67181E+01	9.74241E+05	104	0	1.00000E+00
105	4.48540E-01	1.69199E+01	8.77651E+05	105	0	1.00000E+00
106	3.61840E-01	1.71388E+01	7.93277E+05	106	0	1.00000E+00
107	2.98850E-01	1.73739E+01	7.20012E+05	107	0	1.00000E+00
108	2.49380E-01	1.76270E+01	6.58317E+05	108	0	1.00000E+00
109	2.01070E-01	1.78928E+01	6.07594E+05	109	0	1.00000E+00
110	1.74240E-01	1.78338E+01	5.69506E+05	110	0	1.00000E+00
111	1.59920E-01	1.79517E+01	5.34703E+05	111	0	1.00000E+00
112	1.39810E-01	1.80954E+01	4.97557E+05	112	0	1.00000E+00
113	1.19780E-01	1.82408E+01	4.57271E+05	113	0	1.00000E+00
114	9.97500E-02	1.84233E+01	4.14734E+05	114	0	1.00000E+00
115	8.02110E-02	1.86193E+01	3.80936E+05	115	0	1.00000E+00
116	6.19950E-02	1.87977E+01	3.51816E+05	116	0	1.00000E+00
117	5.09910E-02	1.89333E+01	3.27741E+05	117	0	1.00000E+00
118	4.06190E-02	1.91165E+01	2.92906E+05	118	0	1.00000E+00
119	3.08310E-02	1.93411E+01	2.56646E+05	119	0	1.00000E+00
120	2.07800E-02	1.96310E+01	2.18933E+05	120	0	1.00000E+00
121	2.10760E-02	1.89777E+01	3.04044E+05	121	0	1.00000E+00
122	1.48910E-02	2.03251E+01	3.52137E+05	122	0	1.00000E+00
123	9.87920E-03	2.07405E+01	3.14293E+05	123	0	1.00000E+00
124	4.74190E-03	2.10694E+01		124	0	

XSDRPM VERB 1.0A 9070102 00.11.20 PAGE 10

17% ← YDRNPM VERB 1.0A 9070102 00.11.20 PAGE 10

IDENTIFIJ EXON 18115 PWP 0-31 U235, 4400 PPM NAT. BURD

MIXTURE	ORDER FILE		ACTIVITY TABLE		DIRECTIONAL CONSTANTS		
	BY ZONE	BY ZONE	MATL NO.	REACTION	WEIGHTS	DIRECTIONS	REFL DIRCC
1	1	2			0	-2.79004E-01	0
2	2	2			5.06143E-02	-1.97286E-01	0
3	3	2			5.06143E-02	1.97286E-01	2
4					0	+1.04419E-01	0
5					5.53355E-02	-5.58143E-01	8
6					5.53355E-02	-2.31301E-01	7
7					5.53355E-02	2.31301E-01	6
8					5.53355E-02	5.78410E-01	5
9					0	-8.50774E-01	15
10					5.22844E-02	-8.21784E-01	15
11					5.22844E-02	-6.01568E-01	14
12					5.22844E-02	-2.20196E-01	13
13					5.22844E-02	2.20196E-01	12
14					5.22844E-02	6.01568E-01	11
15					5.22844E-02	8.21784E-01	10
16					0	-9.83032E-01	24
17					4.53355E-02	-9.64143E-01	24
18					4.53355E-02	-8.17361E-01	23
19					4.53355E-02	-5.46143E-01	22
20					4.53355E-02	-1.91780E-01	21
21					4.53355E-02	1.91780E-01	20
22					4.53355E-02	5.46143E-01	19
23					4.53355E-02	8.17361E-01	18
24					4.53355E-02	9.64143E-01	17

CONSTANTS FOR P(3) SCATTERING

0 ANGL SET 1 SET 2 SET 3 SET 4 SET 5



























00.11.22. 6.843 CP SECONDS EXECUTION TIME.  
00.11.22.15DRNPM(PL\*777777)  
00.12.43. END 15DRNPM  
00.12.43. 245000 MAXIMUM EXECUTION FL.  
0.12.43. 109.285 CP SECONDS EXECUTION TIME.  
1.12.43. REPRIEVED NORMAL TERMINATION.  
0.12.43. JOB REPRIEVED.  
00.12.43. RPV - PREVIOUS ERROR CONDITIONS RESET.  
00.12.43.PEWIND,TAR12,TAR13.  
00.12.44.RETURN,TAR14.  
00.12.44.ATTACHP,NITAWL,1,2.  
00.12.46. STOP  
00.12.46. 355200 MAXIMUM EXECUTION FL.  
00.12.46. 0.280 CP SECONDS EXECUTION TIME.  
00.12.46.NITAWL(PL\*777777)  
00.12.51. END MNITAWL  
00.12.51. 220000 MAXIMUM EXECUTION FL.  
00.12.51. 2.831 CP SECONDS EXECUTION TIME.  
00.12.51.PEWIND,TAR14.  
00.12.51.RETURN,TAR15,TAR16.  
00.12.51.LABEL,TAR1A,W,0\*05,1\*05SIC1,VBN\*007423.  
00.12.51.NITAWL,ASHIONED TO TAR1A, VBN\*007423.  
00.14.54.COPYBE,TAR14,TAR1A.  
00.14.58. TOT 1 FILES 1 RECS 308499 WORDS  
00.14.59.UEPT, 0.106KUNB.  
00.14.59.UEMT, 3.476KUNB.  
00.14.59.UTKE, 194.773KUNB.  
00.14.59.UECP, 185.425BACS.  
00.14.59. SFU, 204.051UNTS.  
00.14.59.ROUT\*PC\*E  
00.15.00. NO FILES PROCESSED.  
00.15.00.\$DAYFILE(OUTPUT,11WD)  
00.15.00.TARG, 166E CORES (N\*OUTPUT).  
00.15.00.POWER COMPUTING\*90 ~ AOS 0.7.1.30  
00.15.00.DAT11 90/01/02.  
00.15.00.18N1 MSFN  
END OF FILE

[E3K181] EXXON 15X15 PWR, 3.3XU235, 1994 PPM NAT-BORON

99.0 73 300 3 123 75 18 5 22 6

--EOR--

12%

1  
0  
0

KK	KK	EEEEEEEEEEEE	NN	NN	0000000000
KK	KK	EEEEEEEEEEEE	NNN	NN	000000000000
KK	KK	EE	NNNN	NN	00 00
KK	KK	EE	NN NN	NN	00 00
KK	KK	EE	NN NN	NN	00 00
KKKKKK		EEEEEEEE	NN NN	NN	00 00
KKKKKK		EEEEEEEE	NN NN	NN	00 00
KK	KK	EE	NN NN NN	NN	00 00
KK	KK	EE	NN NN NN	NN	00 00
KK	KK	EEEEEEEEEEEE	NN	NNN	000000000000
KK	KK	EEEEEEEEEEEE	NN	NN	0000000000

00000000	000000	11	000000	11	000000	00000000
00000000	00000000	11	00000000	111	11	00000000
00 00	00 00	11	00 00	1111	11	00 00
00 00	00 00	11	00 00	11	11	00 00
00 00	00 00	11	00 00	11	11	00 00
00 00	00 00	11	00 00	11	11	00 00
00 00	00 00	11	00 00	11	11	00 00
00 00	00 00	11	00 00	11	11	00 00
00000000	00000000	11	00000000	11111111	11	00000000
00000000	00000000	11	00000000	11111111	11	00000000

00000000	00000000	11	00000000	11	00000000	00000000
00 00	00 00	11	00 00	1111	11	00 00
00 00	00 00	11	00 00	11	11	00 00
00 00	00 00	11	00 00	11	11	00 00
00 00	00 00	11	00 00	11	11	00 00
00 00	00 00	11	00 00	11	11	00 00
00 00	00 00	11	00 00	11	11	00 00
00 00	00 00	11	00 00	11	11	00 00
00000000	00000000	11	00000000	11111111	11	00000000
00000000	00000000	11	00000000	11111111	11	00000000

1  
0  
0

FOLLOWING IS A CARD IMAGE LISTING OF THE INPUT DATA COLUMN NUMBER

CARD NUMBER	11111111112222222222333333333344444444445555555555666666666677777777778
	12345678901234567890123456789012345678901234567890123456789012345678901234567890
1	[E3K181] EXXON 15X15 PWR, 3.3XU235, 1994 PPM NAT-BORON
2	99.0 73 300 3 123 75 18 5 22 6
3	1 1 1 1 -18 1 0 2000 00 1
4	0 0 0 0 0 00 0 0









4 20000 3.24000E-01  
 5 10001 2.77000E-01  
 5 50000 1.46000E-03  
 5 80004 3.71000E-02  
 5 110000 2.40000E-04  
 5 120005 2.00000E-04  
 5 130000 8.97000E-03  
 5 140005 7.67000E-04  
 5 260001 4.89000E-05

GROUPS SECTIONS READ FROM TAPE

NUCLIDE \* 10001 HYDROGEN--THERMO ID=1003(1-640) THERMAL TEMPERATURE= 294.6 K  
 NUCLIDE \* 80004 OXYGEN THERMAL TEMPERATURE= 294.6 K  
 NUCLIDE \* 50000 BORON NATURAL  
 NUCLIDE \* 50100 BORON-10  
 NUCLIDE \* 60002 CARBON NATURAL BROWN - DT. JOHN KERNEL TEMP. = 500.26 K  
 NUCLIDE \* 110000 SODIUM NATURAL BROWN - DT. JOHN KERNEL TEMP. = 293.5 K  
 NUCLIDE \* 120005 MAGNESIUM THERMAL TEMP = 400.0 K  
 NUCLIDE \* 130000 ALUMINUM NATURAL BROWN - DT. JOHN KERNEL TEMP. = 427.10 K  
 NUCLIDE \* 140005 SILICON THERMAL TEMP = 900.0 K  
 NUCLIDE \* 200005 MANGANESE THERMAL TEMP = 900.0 K  
 NUCLIDE \* 260001 IRON THERMAL TEMP=294.6  
 NUCLIDE \* 820000 LEAD NATURAL BROWN - DT. JOHN KERNEL TEMP. = 293.5 K  
 NUCLIDE \* 33422051 URANIUM-235 THERMAL TEMPERATURE = 294.6 K  
 NUCLIDE \* 33422052 URANIUM-238 THERMAL TEMPERATURE = 294.6 K  
 NUCLIDE \* 3310001 HYDROGEN--THERMO ID=1003(1-640) THERMAL TEMPERATURE= 294.6 K  
 NUCLIDE \* 3350100 BORON-10  
 NUCLIDE \* 3380004 OXYGEN THERMAL TEMPERATURE= 294.6 K  
 NUCLIDE \* 33400000 ZIRCONIUM NATURAL BROWN - DT. JOHN KERNEL TEMP. = 427.10 K

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GEOMETRY EXON 15X16 PWR, 3.330235, 1706 PPM NAT.BORON

GEOMETRY DESCRIPTION  
 REGION

BOX TYPE

REGION

0 1 GENERAL	1	+X = 0.	+Y = 0.	+Z = 0.	-X = 0.	-Y = 0.	-Z = 0.
0 2 GENERAL	2	+X = 0.	+Y = 0.	+Z = 0.	-X = 0.	-Y = 0.	-Z = 0.
0 3 GENERAL	3	+X = 0.	+Y = 0.	+Z = 0.	-X = 0.	-Y = 0.	-Z = 0.
0 4 GENERAL	4	+X = 0.	+Y = 0.	+Z = 0.	-X = 0.	-Y = 0.	-Z = 0.
0 5 GENERAL	5	+X = 0.	+Y = 0.	+Z = 0.	-X = 0.	-Y = 0.	-Z = 0.
0 6 CUBOID	0	+X = 1.0605E+02	+Y = -1.0000E-04	+Z = 1.0605E+02	-X = 1.0605E+02	-Y = 1.0000E-04	-Z = 1.0605E+02

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GEOMETRY EXON 15X16 PWR, 3.330235, 1706 PPM NAT.BORON

WEIGHTING FUNCTION  
 BOX TYPE

BOX TYPE	GROUP	WT LOW	WT AVG	WT HI
0 REGION 1 DEFINED BY GEOMETRY CARD	1	.167	.500	1.500
	GROUPS 2 TO 123 SAME AS ABOVE			
0 REGION 2 DEFINED BY GEOMETRY CARD	2	.167	.500	1.500
	GROUPS 2 TO 123 SAME AS ABOVE			
0 REGION 3 DEFINED BY GEOMETRY CARD	3	.167	.500	1.500
	GROUPS 2 TO 123 SAME AS ABOVE			
0 REGION 4 DEFINED BY GEOMETRY CARD	4	.167	.500	1.500
	GROUPS 2 TO 123 SAME AS ABOVE			
0 REGION 5 DEFINED BY GEOMETRY CARD	5	.167	.500	1.500
	GROUPS 2 TO 123 SAME AS ABOVE			







.10000E+01Y    +.46228E+02    4  
 .10000E+01Y    +.45570E+02    4  
 .10000E+01Y    +.24576E+02    4  
 .10000E+01Y    +.23876E+02    4  
 .10000E+01Y    +.22860E+02    4  
 .10000E+01Y    +.22162E+02    4  
 .10000E+01Y    +.12063E+01    5  
 .10000E+01Y    +.50800E+00    3  
 .10000E+01X    +.50800E+00    4  
 .10000E+01Y    +.12063E+01    4  
 .10000E+01X    +.22162E+02    4  
 .10000E+01Y    +.22860E+02    4  
 .10000E+01X    +.23876E+02    4  
 .10000E+01Y    +.24576E+02    4  
 .10000E+01X    +.45570E+02    4  
 .10000E+01Y    +.46228E+02    4  
 .10000E+01Y    +.47244E+02    4  
 .10000E+01X    +.47943E+02    4  
 .10000E+01X    +.48691E+02    4  
 .10000E+01Y    +.49441E+02    4  
 .10000E+01X    +.70104E+02    4  
 .10000E+01Y    +.41756E+02    4  
 .10000E+01Y    +.23068E+02    4

KINDIV    VER 1.2A (21/09/67) 90/01702, 01.11.14, PAGE 14

\*\*\*\*\*  
 FINAL ALLOCATION OF MEMORY HAS BEEN COMPLETED  
 \*\*\*\*\*

REQUIRED SCM FIELD LENGTH    113600 (003357048)  
 REQUIRED LCM FIELD LENGTH    36900 (002190448)  
 REQUIRED RMS FIELD LENGTH    5 (000000008)  
 REQUIRED SCM BLANK COMMON    68876 (002064148)  
 REQUIRED LCM BLANK COMMON    36900 (002190448)  
 REQUIRED RMS BLANK COMMON    0 (000000008)  
 REMAINING SCM AVAILABLE    4276 (000226788)  
 REMAINING LCM AVAILABLE    63100 (001751708)

ALLOCATION OF RELOCATABLE ARRAYS

ARRAY	NAT	LOCATION
FSP/MUBAR	1	SCM
FSP/MUBAR	2	SCM
FSP/MUBAR	3	SCM
FSP/MUBAR	4	LCM
FSP/MUBAR	5	LCM
WGT		SCM
FMABS		SCM
FMFIS		SCM

KINDIV    VER 1.2A (21/09/67) 90/01702, 01.11.14, PAGE 15

0(EDEXEPT) EXXON 15X15 PWR, 3.3&U235, <sup>1746</sup> PPM NAT.BORON

0 VOLUMES

BOX TYPE	1					
REGION DEFINED BY GEOMETRY CARD	1	VOLUME =	0.	CM..3	CUMULATIVE VOLUME =	0.
REGION DEFINED BY GEOMETRY CARD	2	VOLUME =	0.	CM..3	CUMULATIVE VOLUME =	0.
REGION DEFINED BY GEOMETRY CARD	3	VOLUME =	0.	CM..3	CUMULATIVE VOLUME =	0.
REGION DEFINED BY GEOMETRY CARD	4	VOLUME =	0.	CM..3	CUMULATIVE VOLUME =	0.

0 TOTAL VOLUMES

- 1 1.00000E+00
- 2 1.00000E+00
- 3 1.00000E+00
- 4 1.00000E+00
- 5 5.62277E+05
- 6 4.37002E+00

0 VOLUME FRACTION OF THE CORE CONTAINING FISSIONABLE MATERIAL= .417705E-05

0 START TYPE = 1

\* THE NEUTRONS WERE STARTED IN THE ARRAY WITH A COSINE DISTRIBUTION.

THE CHOSEN START TYPE MAY NOT BE ADEQUATE. TOO MANY ATTEMPTS MAY BE NEEDED TO START THE NEUTRONS

0 300 NEUTRONS WERE INITIALLY STARTED

.01450 MINUTES WERE REQUIRED FOR STARTING.

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0 (E3348F1) EXXON 17X15 PWR, 3.2XU235, 17700 PPM NAT.BORON

0 GENERATION	K-EFFECTIVE	ELAPSED TIME(MIN)	AVG. K-EFF	DEVIATION	MATRIX K-EFF
1	8.46943E+01	2.79833E+01	1.00000E+00	0.	0.
2	8.89596E+01	5.40333E+01	1.00000E+00	0.	0.
3	8.68515E+01	7.9967E+01	8.68515E-01	0.	0.
4	9.39875E+01	1.05595E+02	9.04196E-01	3.56607E-02	0.
5	9.05256E+01	1.31467E+02	9.04749E-01	2.06077E-02	0.
6	8.66711E+01	1.58317E+02	9.00139E-01	1.52835E-02	0.
7	9.06247E+01	1.85867E+02	9.01381E-01	1.19035E-02	0.
8	8.79444E+01	2.13167E+02	8.97726E-01	1.07037E-02	0.
9	9.50207E+01	2.41160E+02	9.05226E-01	1.15442E-02	0.
10	9.03611E+01	2.67367E+02	9.05024E-01	9.9965E-03	0.
11	9.08194E+01	2.89100E+02	9.05376E-01	8.82589E-03	0.
12	8.95079E+01	3.15863E+02	9.04796E-01	7.95473E-03	0.
13	8.69691E+01	3.41500E+02	9.01241E-01	7.85665E-03	0.
14	9.13717E+01	3.68017E+02	9.03281E-01	7.24707E-03	0.
15	9.16795E+01	3.93517E+02	9.03587E-01	6.75918E-03	0.
16	9.23995E+01	4.19293E+02	9.04868E-01	6.42862E-03	0.
17	9.97367E+01	4.44833E+02	9.11036E-01	6.59404E-03	0.
18	9.24607E+01	4.71167E+02	9.11884E-01	6.08350E-03	0.
19	9.59506E+01	4.97133E+02	9.14666E-01	5.89344E-03	0.
20	9.05660E+01	5.23730E+02	9.14184E-01	5.64703E-03	0.
21	9.44023E+01	5.50483E+02	9.15755E-01	5.40188E-03	0.
22	9.17302E+01	5.76008E+02	9.15842E-01	5.02254E-03	0.
23	9.42644E+01	6.02417E+02	9.17118E-01	4.80069E-03	0.
24	9.70002E+01	6.27667E+02	9.19522E-01	4.91542E-03	0.
25	9.61284E+01	6.53700E+02	9.21338E-01	4.85290E-03	0.
26	9.28723E+01	6.79567E+02	9.21446E-01	4.56836E-03	0.
27	8.98261E+01	7.06133E+02	9.20710E-01	4.36921E-03	0.
28	9.32336E+01	7.32883E+02	9.21158E-01	4.15566E-03	0.
29	9.97732E+01	7.59450E+02	9.20291E-01	3.96723E-03	0.
30	9.53864E+01	7.85783E+02	9.21491E-01	3.87385E-03	0.
31	9.95522E+01	8.11867E+02	9.24643E-01	3.71607E-03	0.
32	9.55762E+01	8.38217E+02	9.25101E-01	3.60976E-03	0.
33	9.75997E+01	8.64183E+02	9.26742E-01	3.51219E-03	0.
34	9.78066E+01	8.90833E+02	9.28346E-01	3.44069E-03	0.
35	9.13103E+01	9.15850E+02	9.27884E-01	3.46960E-03	0.
36	9.72084E+01	9.42517E+02	9.29164E-01	3.43547E-03	0.
37	9.68064E+01	9.68083E+02	9.30295E-01	3.46947E-03	0.
38	9.52932E+01	9.93883E+02	9.30924E-01	3.73865E-03	0.
39	9.45876E+01	1.02005E+03	9.31328E-01	3.59601E-03	0.
40	9.23977E+01	1.04712E+03	9.31135E-01	3.45019E-03	0.
41	8.68401E+01	1.07443E+03	9.29526E-01	3.54695E-03	0.
42	8.76402E+01	1.10137E+03	9.28198E-01	3.56724E-03	0.
43	9.49785E-01	1.12763E+03	9.28725E-01	3.45522E-03	0.

WARNING - ONLY 243 INDEPENDENT FISSION POINTS WERE GENERATED.

WARNING - ONLY 243 INDEPENDENT FISSION POINTS WERE GENERATED.

45	8.6363E-01	1.1799E+01	9.3020E-01	1.114E-03	0.
46	8.6841E-01	1.2055E+01	9.3116E-01	1.6091E-03	0.
47	9.2833E-01	1.2205E+01	9.3108E-01	5.1430E-03	0.
48	9.8803E-01	1.2558E+01	9.3223E-01	5.1801E-03	0.
49	9.9164E-01	1.2818E+01	9.3358E-01	5.2234E-03	0.
50	9.4267E-01	1.3075E+01	9.3377E-01	5.1171E-03	0.
51	9.6016E-01	1.3336E+01	9.3431E-01	5.0408E-03	0.
52	9.5934E-01	1.3595E+01	9.3481E-01	4.9639E-03	0.
53	9.2051E-01	1.3850E+01	9.3457E-01	4.8739E-03	0.
54	9.7018E-01	1.4116E+01	9.3521E-01	4.8284E-03	0.
55	9.7842E-01	1.4387E+01	9.3605E-01	4.8059E-03	0.
56	9.1782E-01	1.4642E+01	9.3569E-01	4.7281E-03	0.
57	9.6002E-01	1.4906E+01	9.3613E-01	4.6627E-03	0.
58	9.0784E-01	1.5157E+01	9.3567E-01	4.6015E-03	0.
59	9.5026E-01	1.5418E+01	9.3599E-01	4.5319E-03	0.
60	9.2058E-01	1.5676E+01	9.3526E-01	4.4808E-03	0.
61	9.4301E-01	1.5926E+01	9.3574E-01	4.3962E-03	0.
62	9.2986E-01	1.6196E+01	9.3524E-01	4.3136E-03	0.
63	9.7858E-01	1.6457E+01	9.3448E-01	4.2928E-03	0.

VER 1.2A (21/09/87) 90/01/02. 02.18.42. PAGE 17

Note

← Average Keff with 3 generations skip is calculated to be 0.9376 (see attached spreadsheet)

MEMM POWER COMPUTING/990 - NOS 2.7.1.10. NOS 2.7.1 ST-RAC: 90/01/02. 02.18.42.

```

02.08.49.ETDIERI,PO,TI000. HENRY TRAN
01.02.49.USFE,VERPDR,,MC.
02.10.49.489C, D.
03.08.49. YOUR PASSWORD EXPIRES AT 00:00:00 ON 90/02/08.
02.08.49.CHEPDI,N973301,USI.
02.03.50. CHARGE = N973301, PROJECT = VER.
02.08.51.2722101.
02.09.51.PROCL. SYSTEM PROLOGUE
02.08.51.COMMINT. SYSTEM PROLOG.
01.08.51.NEWS(A).
02.08.52.CHEKEXP.
02.08.55. INDUSTRY COMPLETE.
02.08.55.REVERT.
02.06.53.TITLE (IICDIERI) EXON 15X11 PMP, S.3RUSTS, 1.0 FM NAT.SOKOM)
02.08.53.LABEL,TAPE4,D=0R,C=11SECT,USM=007421.
02.11.08.NTI08, ASSIGNED TO TAPE4, USM=007421.
02.11.06.COPYDF,TAPE4,TAPE4.
02.11.11. COPY 1 FILES 1 RECS 747442 WORDS
02.11.11.REWIND,TAPE4.
02.11.11.RETURN,TAPE4.
02.11.11.RFL(FC=10)
02.11.11.ATTACHP,KENOW,1.2A.
02.11.13. STOP
02.11.13. 035200 MAXIMUM EXECUTION FL.
02.11.13. 0.209 CP SECONDS EXECUTION TIME.
02.11.13.KEND4,PL=777777.
02.18.42. TIME LIMIT.
02.18.42.UERF, 0.133KUNS.
02.18.42.UEMT, 2.723KUNS.
02.18.42.UEMS, 33.728KUNS.
02.18.42.UECP, 1001.8548SECS.
02.18.42.SRU, 1990.957UNTS.
02.18.42.#OUT(*70P=E)
02.18.42. NO FILES PROCESSED.
02.18.42.#DAYFILE(OUTPUT,JT=D)
02.18.42.IABG, 52B SDBS FN=OUTPUT.
02.18.42.POWER COMPUTING/990 - NOS 2.7.1.10
02.18.42.DATE: 90/01/02.

```

1	0.88959	0.88959	0.00000
2	0.868515	0.868515	0.00000
3	0.939876	0.904196	0.035680
4	0.905856	0.904749	0.020607
5	0.836311	0.900139	0.013283
6	0.906347	0.901381	0.011903
7	0.879449	0.897726	0.010383
8	0.950227	0.905226	0.011544
9	0.903611	0.905024	0.009999
10	0.908194	0.905376	0.008825
11	0.895575	0.904376	0.009954
12	0.869691	0.901241	0.007956
13	0.913717	0.902291	0.007247
14	0.916795	0.903397	0.006759
15	0.923995	0.904868	0.006428
16	0.897387	0.911036	0.005594
17	0.924607	0.911824	0.005083
18	0.959506	0.914636	0.005093
19	0.90566	0.914104	0.007647
20	0.944023	0.915755	0.007401
21	0.917502	0.915842	0.007022
22	0.942649	0.917118	0.006800
23	0.970002	0.919522	0.006915
24	0.961289	0.921338	0.006852
25	0.928723	0.921646	0.004768
26	0.898261	0.92071	0.006349
27	0.932336	0.921138	0.006128
28	0.897772	0.920291	0.005987
29	0.953864	0.921491	0.005673
30	0.995522	0.924043	0.006216
31	0.955762	0.925101	0.006097
32	0.975997	0.926742	0.006121
33	0.976066	0.928346	0.006140
34	0.913103	0.937984	0.005969
35	0.972084	0.939184	0.005935
36	0.968064	0.930295	0.005849
37	0.952932	0.930924	0.005738
38	0.945876	0.931328	0.005596
39	0.923977	0.931135	0.005450
40	0.868401	0.929526	0.005516
41	0.876402	0.928196	0.005607
42	0.949785	0.928725	0.005455
43	0.960724	0.929485	0.005377
44	0.963636	0.930281	0.005311
45	0.968414	0.931147	0.005260
46	0.928333	0.931085	0.005143
47	0.988038	0.932323	0.005180
48	0.99164	0.933585	0.005223
49	0.942873	0.933773	0.005117
50	0.960164	0.934317	0.005040
51	0.959346	0.934817	0.004963
52	0.920312	0.934533	0.004873
53	0.970189	0.935219	0.004828
54	0.978425	0.936034	0.004805
55	0.917824	0.935697	0.004728
56	0.96002	0.936139	0.004662
57	0.907847	0.935634	0.004606
58	0.950268	0.93589	0.004531
59	0.92058	0.935626	0.004460
60	0.943818	0.935765	0.004386
61	0.939863	0.935834	0.004313
62	0.97558	0.936485	0.004292

1796 mm  
3.3%, 4500

=====

AVERAGE: 0.937618      0.00429 (SKIP 3)

[E33K1B1] EXXON 15X15 PWR, 3.3XU235, 1700 PPM NAT.BORON

-10F--

2035

KA	KA	EEEEEEEEEEEE	NN	NN	0000000000
KK	KK	EEEEEEEEEEEE	NNN	NA	000000000000
KL	KL	EE	NNNN	NN	00 00
KM	KM	EE	NN NN	NN	00 00
KN	KN	EE	NN NN	NN	00 00
KO	KO	EEEEEEEEEE	NN NN	NA	00 00
KP	KP	EEEEEEEEEE	NN NN	NA	00 00
KQ	KQ	EE	NN NN	NN	00 00
KR	KR	EE	NN NN	NN	00 00
KS	KS	EE	NN NN	NN	00 00
KT	KT	EE	NN NN	NN	00 00
KU	KU	EEEEEEEEEEEE	NN	NNN	00 00
KV	KV	EEEEEEEEEEEE	NN	NNN	00 00

9999999999	00000000	99	00000000	11	00000000	0000000000
9999999999	00000000	99	00000000	11	00000000	0000000000
99	00	00	99	00	00	00
99	00	00	99	00	00	00
9999999999	00000000	99	00000000	11	00000000	0000000000
9999999999	00000000	99	00000000	11	00000000	0000000000
99	00	00	99	00	00	00
99	00	00	99	00	00	00
9999999999	00000000	99	00000000	11	00000000	0000000000
9999999999	00000000	99	00000000	11	00000000	0000000000

00000000	2222222222	3333333333	6666666666	11	9999999999
0000000000	2222222222	3333333333	6666666666	11	9999999999
00	00	22	33	66	99
00	00	22	33	66	99
00	00	22	33	66	99
00	00	22	33	66	99
00	00	22	33	66	99
00	00	22	33	66	99
00	00	22	33	66	99
00	00	22	33	66	99
00000000	2222222222	3333333333	6666666666	11111111	9999999999
00000000	2222222222	3333333333	6666666666	11111111	9999999999

FOLLOWING IS A CARD IMAGE LISTING OF THE INPUT DATA COLUMN NUMBER

CARD NUMBER	11111111112222222222333333333344444444445555555555666666666677777777778
	1234567890123456789012345678901234567890123456789012345678901234567890

1	[E33K1B1] EXXON 15X15 PWR, 3.3XU235, 1700 PPM NAT.BORON
2	99.0 73 300 3 123 75 18 5 22 6
3	1 1 1 1 -1P 1 0 2000 00 1
4	0 0 0 0 0 00 0 0









177	1.0X	-0.5080	3
178	1.0X	-1.2065	3
179	1.0X	-22.1615	3
180	1.0Y		
181			
182	1.0X	-24.5745	3
183	1.0Y		
184	1.0X	-46.2280	3
185	1.0X	-47.24	3
186	1.0X	-47.9425	3
187	1.0Y	-68.8975	3
188	1.0Y	-69.5960	3
189	1.0X	-70.1040	3
190	1.0Y	-46.7360	3
191	1.0Y	-23.3680	3
192		END CASE	
193		END KENO	

\*\*\*\*\* E N D O F I N P U T L I S T I N G \*\*\*\*\*

KENOIV VER 1.2A (21/09/87) 90/01/02, 02.36.19, PAGE 7

0[033161] EXXON 15115 PWR, 3.340235, <sup>2035</sup> PPM NAT. BORON

NUMBER OF GENERATIONS	73	START TYPE	1
NUMBER PER GENERATION	300	GENERATIONS BETWEEN CHECKPOINTS	0
NUMBER OF GENERATIONS TO BE SKIPPED	3	LIST INPUT X-SECTIONS READ FROM TAPE	NO
NUMBER OF ENERGY GROUPS	127	LIST 1-D MIXTURE X-SECTIONS	NO
MAX. NUMBER OF ENERGY TRANSFERS	75	LIST 2-D MIXTURE X-SECTIONS	NO
NUMBER OF INPUT NUCLIDES	18	LIST FISS. AND ABS. BY REGION	NO
NUMBER OF MIXTURES	5	USE X-SECTIONS FROM PREVIOUS CASE	NO
NUMBER OF MIXING TABLE ENTRIES	22	USE GEOMETRY FROM PREVIOUS CASE	NO
NUMBER OF GEOMETRY CARDS	6	USE VELOCITIES FROM PREVIOUS CASE	NO
NUMBER OF BOX TYPES	1	COMPUTE MATRIX K-EFFECTIVE BY UNIT	NO
NUMBER OF UNITS IN X DIRECTION	1	COMPUTE MATRIX K-EFFECTIVE BY BOX TYPE	NO
NUMBER OF UNITS IN Y DIRECTION	1	LIST FISS. PROB. MATRIX BY UNIT	NO
NUMBER OF UNITS IN Z DIRECTION	1	ADJOINT CALCULATION	NO
NUMBER OF NUCLIDES READ FROM TAPE	-18	USE EXPONENTIAL TRANSFORM	NO
ALBEDO TYPE	1	CALCULATE FLUX	YES
SEARCH TYPE	0	CALCULATE FISSION DENSITIES	YES

THIS PROBLEM WILL BE RUN WITH SPECULARLY REFLECTING BOUNDARY CONDITION  
 OTHE ALBEDOS ARE X1 = C, X2 = 1.00000E+00, X3 = 0, X4 = 1.00000E+00, X5 = 0, X6 = 1.00000E+00  
 MAXIMUM TIME = 99.0000 MINUTES  
 STORAGE LOCATIONS REQUIRED FOR THIS JOB = 34306  
 REMAINING AVAILABLE LOCATIONS = 45595  
 REQUIRED LCM STORAGE LOCATIONS = 33380 (001014548)  
 REMAINING LCM AVAILABLE = 66420 (002015648)

KENOIV VER 1.2A (21/09/87) 90/01/02, 02.36.19, PAGE 8

0[033161] EXXON 15115 PWR, 3.340235, <sup>2035</sup> PPM NAT. BORON

MIXTURE	NUCLIDE	DENSITY
1	33922351	2.34220E-04
1	33922381	6.77690E-03
1	3380004	3.30620E-02
1	33400000	4.71250E+03
1	3310001	3.80730E-02
1	3350100	1.26900E-05
2	10061	6.67100E-02
2	80004	3.33600E-02
2	50100	2.22300E-05
3	60002	2.61000E-04
3	250005	1.09000E-03











0 60	0.		4.1790E-03	4.8603E-04
0 61	0.		1.54515E-03	5.54655E-04
0 62	0.		1.69179E-03	6.09316E-04
0 63	0.		1.68231E-03	6.35909E-04
0 64	0.		1.62420E-03	7.12416E-04
0 65	0.		1.72745E-03	7.77148E-04
0 66	0.		1.85173E-03	9.31229E-04
0 67	0.		2.00901E-03	1.02116E-03
0 68	0.		2.41302E-03	1.08155E-03
0 69	0.		2.65659E-03	1.14511E-03
0 70	0.		3.05429E-03	1.57151E-03
0 71	0.		2.99552E-03	1.62827E-03
0 72	0.		3.20073E-03	1.76362E-03
0 73	0.		6.38051E-03	2.03709E-03
0 74	4.20681E-05		3.99548E-03	3.04451E-03
0 75	0.		4.90496E-03	2.41673E-03
0 76	0.		4.05501E-03	2.83155E-03
0 77	0.		7.20836E-03	2.21288E-03
0 78	4.50183E-05		4.97983E-03	6.67797E-03
0 79	0.		7.14969E-03	2.58033E-03
0 80	0.		4.52894E-03	6.87057E-03
0 81	0.		5.81176E-03	4.11082E-03

KENPIL VEP 1.2A (21/09/87) 90/01/02 02.36.19. PAGE 20

1  
 0[E33K1B1] EXXON 15X15 PWR, 204 PPM NAT.BORON  
 000000 REGION LEAKAGE ABSORPTIONS FISSIONS WITH 3 GENERATIONS SKIPPED

0 82	0.		1.38840E-03	4.84271E-03
0 83	0.		4.94384E-03	3.17523E-03
0 84	0.		1.89922E-03	5.68236E-03
0 85	0.		3.66378E-03	3.63778E-03
0 86	0.		6.30428E-03	5.13484E-03
0 87	0.		7.07805E-03	1.02346E-03
0 88	0.		1.08866E-02	1.07589E-03
0 89	0.		1.28425E-02	2.37008E-03
0 90	0.		3.65126E-03	4.61698E-04
0 91	0.		4.09879E-03	1.89089E-03
0 92	0.		3.35168E-03	1.29812E-03
0 93	0.		3.85023E-03	1.39607E-03
0 94	0.		1.68002E-03	4.84898E-04
0 95	0.		1.32954E-03	5.72787E-04
0 96	0.		1.38873E-03	5.98011E-04
0 97	0.		1.43005E-03	6.57711E-04
0 98	0.		3.48265E-03	3.22096E-03
0 99	0.		3.89255E-03	4.40169E-03
0100	0.		3.55804E-03	3.29166E-03
0101	0.		3.42426E-03	2.84768E-03
0102	0.		5.17637E-03	4.24831E-03
0103	0.		5.62140E-03	4.95484E-03
0104	1.48e08E-05		7.68821E-03	7.14505E-03
0105	0.		1.17650E-02	1.22929E-03
0106	0.		9.55439E-03	1.09265E-03
0107	0.		1.24268E-02	1.41842E-03
0108	0.		1.58229E-02	1.65e08E-02

KENPIL VEP 1.2A (21/09/87) 90/01/02 02.36.19. PAGE 21

1  
 0[E33K1B1] EXXON 15X15 PWR, 3.35U235, 770 PPM NAT.BORON  
 000000 REGION LEAKAGE ABSORPTIONS FISSIONS WITH 3 GENERATIONS SKIPPED

0109	0.		8.54017E-03	8.71523E-03
0110	0.		1.05328E-02	1.06789E-02
0111	0.		1.48465E-02	1.49080E-02
0112	0.		2.09017E-02	2.11193E-02
0113	0.		3.18264E-02	3.16472E-02
0114	0.		4.95574E-02	4.97569E-02
0115	0.		3.60758E-02	3.62887E-02













8	2580004	4280004	5080004
9	25900000	42900000	50900000
10	2510001	4210001	5010001
11	2550100	4250100	5050100
12	33922351		
13	33922381		
14	3380004		
15	33400000		
16	3310001		
17	3250000		
18			

\*\*\*\*\* [ N D O F I N P U T L I S T I N G ] \*\*\*\*\*

MTM1 VERS 1.2 90/01/02 02-01-51 PAGE 3

16 ARRAY 12 ENTRIES READ  
07

MSM	NUMBER OF EXTRA CROSS SECTIONS	0
MNT	NUMBER OF NUCLIDES FROM MASTER LIBRARY	2
MWT	NUMBER OF NUCLIDES FROM X-SECT LIBRARY (LOW ST)	34
MXT	NUMBER OF NUCLIDES FROM X-SECT LIBRARY (LOI)	0
MCR	ANIS/DOT/MORSE OUTPUT TRIGGER	3
MCE	TOTAL CROSS SECTION POSITION	3
MS	WITHIN-GROUP SCATTERING CROSS SECTION POSITION	4
RES	NUMBER OF RESONANCE CALCULATIONS	0
LOM	TABLE LENGTH FOR CROSS SECTIONS	104
IPM	IS AN OLD ANIS LIBRARY MOUNTED ? (Y/N) NO/YES	Y
IPR	OUTPUT OPTION TRIGGER	+1
IFS	PRINT CONTROL - ANIS OUTPUT	0

OTHER STORAGE ALLOCATED FOR THIS CASE IS 33000 WORDS

24 ARRAY 39 ENTRIES READ  
07

GENERAL INFORMATION CONCERNING CROSS SECTION LIBRARY

TAPE IDENTIFICATION NUMBER	34
NUMBER OF NUCLIDES ON TAPE	34
NUMBER OF NEUTRON ENERGY GROUPS	123
FIRST THERMAL NEUTRON ENERGY GROUP	94
NUMBER OF GAMMA ENERGY GROUPS	0

XSDRN TAPE 0

SUPER-XSDRN LIBRARY--LAST DIGITS OF ID #'S ARE CODED AS FOLLOWS-- 5-900K, 6-800K, 7-850K, 8-750K, 9-1000K, ANYTHING ELSE IS PRECISELY THAT--IF THESE THERMAL TEMPERATURES ARE DESIRED, CALL OWI CRAVEN, IA, OR K. M. GREENE--ALL THERMAL DATA IS P1 (1FT6+94), ALSO J. WILSON DATA AND 3 17% NUCLIDES JULY, 1966  
-THIS IS A CONVERTED TAPE

WORK TAPE 145

THIS XSDRN WORKING TAPE WAS CREATED 90/01/02

THE TITLE OF THE PARENT CASE IS AS FOLLOWS

XSDRN WEIGHTED TAPE--PARENT CASE ENTITLED-- [E33N1B1] EXXON 15X15 PWR, 3.3% U235, 1500 PPM NAT. BORO

NUCLIDES FROM XSDRN TAPE

1	HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	10001
2	OXYGEN	THERMAL TEMPERATURE= 294.6 K	80004

NUCLIDES FROM WORK TAPE

3	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	25922351
4	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	42922351
5	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	50922351
6	URANIUM-238F	THERMAL TEMPERATURE = 294.6 K	25922381











1	0	0	1	2550004	4.59200E-02
2	0	0	2	0	0
3	0	0	2	25400000	3.80220E-02
4	0	0	3	0	0
5	0	0	3	2510001	6.47100E-02
6	0	0	3	2500004	3.33600E-02
7	0	0	3	2550100	1.17700E-05
8	0	0			
9	0	0			
10	0	0			
11	0	0			
12	0	0			
13	0	0			
14	0	0			
15	0	0			
16	0	0			
17	0	0			
18	0	0			
19	0	0			
20	0	0			
21	0	0			
22	0	0			
23	0	0			
24	0	0			
25	0	0			
26	0	0			
27	0	0			
28	0	0			
29	0	0			
30	0	0			
31	0	0			
32	0	0			
33	0	0			
34	0	0			
35	0	0			
36	0	0			
37	0	0			
38	0	0			

TIME OF DAY 02:02:14.

YIDATI=0 REQUIRES 74688 LOCATIONS. THIS VERSION OF IBDRN ALLOWS A MAXIMUM OF 13000

> CROSS SECTIONS WILL BE STORED EXTERNALLY

> 32248 LOCATIONS WILL BE USED

RD EXECUTING FIRST TIME

0 33\* ARRAY 1753 ENTRIES READ

0 0T

0 35\* ARRAY 12 ENTRIES READ

0 36\* ARRAY 11 ENTRIES READ

IBDRNPM VERS. 1.0A 90/01/02. 02:02:08. PAGE 6

0 39\* ARRAY 3 ENTRIES READ

0 40\* ARRAY 3 ENTRIES READ

0 51\* ARRAY 123 ENTRIES READ

0 0T

IBDRNPM VERS. 1.0A 90/01/02. 02:02:08. PAGE 7

[E25M3B1] EYXON 19X18 PWR, 2.5A U235, 900 PPM NAT.BORON

NEUTRON GROUP PARAMETERS

GP	ENERGY	LETHARGY	MID PT	BROAD GP	CALC	RIGHT	LEFT
	BOUNDARIES	BOUNDARIES	VELOCITIES	NUMBERS	TYPE	ALBEDO	ALBEDO
1	1.49180E+07	-3.99983E-01	5.21033E+09	1	0	1.00000E+00	
2	1.34990E+07	-3.00031E-01	4.95624E+09	2	0	1.00000E+00	
3	1.22140E+07	-1.99998E-01	4.71452E+09	3	0	1.00000E+00	
4	1.10520E+07	-1.00026E-01	4.48459E+09	4	0	1.00000E+00	
5	1.00000E+07	0	4.26585E+09	5	0	1.00000E+00	
6	9.04840E+06	9.99971E-02	4.05780E+09	6	0	1.00000E+00	
7	8.19730E+06	2.00001E-01	3.85990E+09	7	0	1.00000E+00	
8	7.40820E+06	2.99998E-01	3.67165E+09	8	0	1.00000E+00	







2	1952	1.0000000E+00	1.0081169E+00	1.1200013E+00	1.063240E+00	1.7698934E+00	0145
3	2623	1.0000000E+00	1.0005733E+00	1.1384404E+00	1.0039222E+00	1.0126260E+00	0191
4	2880	1.0000000E+00	9.9999992E-01	1.1388094E+00	1.0000586E+00	1.0007408E+00	0224
5	3053	1.0000000E+00	1.0000049E+00	1.1388415E+00	1.0000702E+00	1.0000292E+00	0225

GRP.	1	REQUIRED	1	ITERATIONS, MFD OF	5.44677E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	2	REQUIRED	1	ITERATIONS, MFD OF	5.46517E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	3	REQUIRED	1	ITERATIONS, MFD OF	5.54414E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	4	REQUIRED	1	ITERATIONS, MFD OF	6.07551E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	5	REQUIRED	1	ITERATIONS, MFD OF	6.57367E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	6	REQUIRED	1	ITERATIONS, MFD OF	6.90854E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	7	REQUIRED	1	ITERATIONS, MFD OF	6.39294E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	8	REQUIRED	1	ITERATIONS, MFD OF	6.15872E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	9	REQUIRED	1	ITERATIONS, MFD OF	6.59629E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	10	REQUIRED	1	ITERATIONS, MFD OF	6.82161E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	11	REQUIRED	1	ITERATIONS, MFD OF	6.14057E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	12	REQUIRED	1	ITERATIONS, MFD OF	5.56822E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	13	REQUIRED	1	ITERATIONS, MFD OF	6.85163E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	14	REQUIRED	1	ITERATIONS, MFD OF	6.99461E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	15	REQUIRED	1	ITERATIONS, MFD OF	6.06618E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	16	REQUIRED	1	ITERATIONS, MFD OF	5.36002E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	17	REQUIRED	1	ITERATIONS, MFD OF	6.32125E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	18	REQUIRED	1	ITERATIONS, MFD OF	6.29786E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	19	REQUIRED	1	ITERATIONS, MFD OF	6.67909E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	20	REQUIRED	1	ITERATIONS, MFD OF	6.15645E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	21	REQUIRED	1	ITERATIONS, MFD OF	6.34978E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	22	REQUIRED	1	ITERATIONS, MFD OF	6.53414E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	23	REQUIRED	1	ITERATIONS, MFD OF	4.76480E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	24	REQUIRED	1	ITERATIONS, MFD OF	5.67762E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	25	REQUIRED	1	ITERATIONS, MFD OF	5.02459E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	26	REQUIRED	1	ITERATIONS, MFD OF	5.01213E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	27	REQUIRED	1	ITERATIONS, MFD OF	4.65199E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	28	REQUIRED	1	ITERATIONS, MFD OF	4.61297E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	29	REQUIRED	1	ITERATIONS, MFD OF	5.18179E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	30	REQUIRED	1	ITERATIONS, MFD OF	5.25366E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	31	REQUIRED	1	ITERATIONS, MFD OF	5.22769E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	32	REQUIRED	1	ITERATIONS, MFD OF	5.11466E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	33	REQUIRED	1	ITERATIONS, MFD OF	4.98770E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	34	REQUIRED	1	ITERATIONS, MFD OF	4.61374E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	35	REQUIRED	1	ITERATIONS, MFD OF	4.49173E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	36	REQUIRED	1	ITERATIONS, MFD OF	4.21347E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	37	REQUIRED	1	ITERATIONS, MFD OF	4.56174E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	38	REQUIRED	1	ITERATIONS, MFD OF	4.85169E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	39	REQUIRED	1	ITERATIONS, MFD OF	5.12302E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	40	REQUIRED	1	ITERATIONS, MFD OF	3.24725E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	41	REQUIRED	1	ITERATIONS, MFD OF	5.26849E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	42	REQUIRED	1	ITERATIONS, MFD OF	5.26756E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	43	REQUIRED	1	ITERATIONS, MFD OF	5.24637E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	44	REQUIRED	1	ITERATIONS, MFD OF	5.21745E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	45	REQUIRED	1	ITERATIONS, MFD OF	5.17820E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP.	46	REQUIRED	1	ITERATIONS, MFD OF	5.13318E-05	OCCURRED IN INT.	10	COARSE MESH=	1
GRP.	47	REQUIRED	1	ITERATIONS, MFD OF	5.10040E-05	OCCURRED IN INT.	10	COARSE MESH=	1
GRP.	48	REQUIRED	1	ITERATIONS, MFD OF	5.04999E-05	OCCURRED IN INT.	10	COARSE MESH=	1
GRP.	49	REQUIRED	1	ITERATIONS, MFD OF	5.00254E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP.	50	REQUIRED	1	ITERATIONS, MFD OF	4.32882E-05	OCCURRED IN INT.	10	COARSE MESH=	1
GRP.	51	REQUIRED	1	ITERATIONS, MFD OF	4.27279E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP.	52	REQUIRED	1	ITERATIONS, MFD OF	4.20304E-05	OCCURRED IN INT.	9	COARSE MESH=	1

1 XSDRPM VERS. 1.0A 90/01/02, 02.02.09, PAGE 13

0	GRP.	53	REQUIRED	1	ITERATIONS, MFD OF	4.10147E-05	OCCURRED IN INT.	9	COARSE MESH=	1
	GRP.	54	REQUIRED	1	ITERATIONS, MFD OF	4.01856E-05	OCCURRED IN INT.	9	COARSE MESH=	1
	GRP.	55	REQUIRED	1	ITERATIONS, MFD OF	3.91968E-05	OCCURRED IN INT.	9	COARSE MESH=	1
	GRP.	56	REQUIRED	1	ITERATIONS, MFD OF	3.77981E-05	OCCURRED IN INT.	9	COARSE MESH=	1
	GRP.	57	REQUIRED	1	ITERATIONS, MFD OF	3.64348E-05	OCCURRED IN INT.	9	COARSE MESH=	1





GRP. 121 REQUIRED 4 ITERATIONS. MFD OF 4.66540E+05 OCCURRED IN INT. 10 COARSE MESH= 2  
 GRP. 122 REQUIRED 4 ITERATIONS. MFD OF 3.93031E+05 OCCURRED IN INT. 11 COARSE MESH= 2  
 GRP. 123 REQUIRED 4 ITERATIONS. MFD OF 6.31202E+06 OCCURRED IN INT. 11 COARSE MESH= 2

6 3236 1.0000000E+00 1.0000041E+00 3.1388703E+00 1.0000249E+00 1.0000365E+00 .0283  
 FINAL MINITOR LAMBDA 1.1273898E+00 ANGULAR FLUX ON 16

TIME OF DAY 02:07:02.

1 1077 XSDRNPH VERS. 1.04 90/01/02. 02-02-08. PAGE 15

0 (LEGNRBT) 6x 15X15 PWR, 2.5% U235, 400 PPM NAT. BORON

INT.	ZONE	NO	DEF	RADIUS	INT. MIDPOINT	AREA	VOLUME	PROD DENSITY
1	1	1	0	0	4.44500E-02	0	2.48267E-02	3.52918E-02
2	1	1	8.89000E-02	1.33350E-01	5.59575E-01	7.44860E-02	1.36303E-01	
3	1	1	1.77800E-01	2.22250E-01	1.117.5E+00	1.24143E-01	2.20180E+01	
4	1	1	2.66700E-01	3.11150E-01	1.67573E+00	1.73801E-01	3.20973E-01	
5	1	1	3.55600E-01	4.00050E-01	2.23430E+00	2.23450E-01	4.24642E-01	
6	2	2	4.44500E-01	4.88150E-01	2.79298E+00	1.20704E-01	0	
7	2	2	4.85800E-01	5.06450E-01	3.05227E+00	1.31422E-01	0	
8	3	3	5.27100E-01	5.61763E+01	3.31187E+00	2.44694E-01	0	
9	3	3	5.66325E-01	6.31088E-01	3.74745E+00	2.74890E-01	0	
10	2	2	6.65750E-01	7.00413E-01	4.18303E+00	3.05087E-01	0	
11	3	3	7.35075E-01	7.69738E-01	4.61861E+00	3.35264E-01	0	
12	2	2	8.04400E-01		5.05419E+00			

TIME OF DAY 02:03:02.

TIME OF DAY 02:43:03.

XSDRNPH VERS. 1.04 90/01/02. 02-02-08. PAGE 11

STRANGROBY CROSS SECTION WEIGHING FUNCTION

ZONE	GRP. 1	GRP. 2	GRP. 3	GRP. 4	GRP. 5	GRP. 6	GRP. 7	GRP. 8
1	6.56195E-06	1.80727E-05	4.54832E-05	1.02041E-04	3.08824E-04	3.64733E-04	4.47743E-04	1.09319E-03
2	1.27729E-06	2.03456E-05	5.04175E-05	1.12956E-04	2.30506E-04	4.29866E-04	7.42963E-04	1.20492E-03
3	2.59997E-06	7.37240E-06	1.80317E-05	4.07210E-05	8.27312E-05	1.54366E-04	2.66515E-04	4.32773E-04
4	4.38958E-06	1.22832E-05	3.04308E-05	6.81264E-05	1.29335E-04	2.58855E-04	4.48091E-04	7.27347E-04
5	1.63099E-03	2.25150E-03	3.01667E-03	3.96094E-03	4.73889E-03	5.34091E-03	6.32002E-03	7.72665E-03
6	1.82348E-03	2.57979E-03	3.50380E-03	4.57498E-03	5.57902E-03	6.48987E-03	7.61480E-03	9.11028E-03
7	6.59463E-04	9.38786E-04	1.27921E-03	1.67283E-03	2.05875E-03	2.41122E-03	2.84362E-03	3.39081E-03
8	1.10111E-03	1.54316E-03	2.09192E-03	2.73148E-03	3.32758E-03	3.60746E-03	4.49440E-03	5.42414E-03
9	8.75215E-03	9.37099E-03	9.76380E-03	9.15493E-03	8.45596E-03	9.54199E-03	9.15991E-03	9.73706E-03
10	1.02825E-02	1.10853E-02	1.16772E-02	1.12350E-02	1.07816E-02	1.17563E-02	1.14053E-02	1.20189E-02
11	3.84736E-03	4.16089E-03	4.48639E-03	4.35023E-03	4.19978E-03	4.57226E-03	4.47945E-03	4.72714E-03
12	6.14040E-03	6.60814E-03	6.97364E-03	6.67129E-03	6.37681E-03	6.90081E-03	6.76743E-03	7.15781E-03
13	6.68583E-03	6.37924E-03	7.33617E-03	7.64366E-03	6.98941E-03	1.06581E-02	9.23913E-03	8.54772E-03
14	1.06902E-02	1.16110E-02	9.75053E-03	9.69124E-03	1.23794E-02	1.31727E-02	1.18026E-02	1.06130E-02
15	4.13206E-03	4.60465E-03	5.77769E-03	5.89237E-03	4.91193E-03	5.24759E-03	4.63039E-03	4.27248E-03
16	6.47309E-03	6.93157E-03	5.35584E-03	5.75700E-03	7.38852E-03	7.67562E-03	6.89965E-03	6.36634E-03
17	7.71918E-03	6.69538E-03	4.06323E-03	3.46657E-03	6.02342E-03	7.34184E-03	6.50672E-03	4.41464E-03
18	9.52312E-03	8.22280E-03	4.99759E-03	4.13578E-03	7.21315E-03	8.93390E-03	6.80320E-03	5.21376E-03
19	3.83475E-03	3.32583E-03	2.10668E-03	1.72443E-03	2.85591E-03	3.54851E-03	2.76615E-03	2.12301E-03
20	5.72639E-03	4.96209E-03	3.06267E-03	2.55547E-03	4.36354E-03	5.27473E-03	4.13423E-03	3.20610E-03
21	3.77319E-03	3.36637E-03	2.90657E-03	2.57072E-03	2.29333E-03	2.05203E-03	1.88418E-03	1.68204E-03
22	4.35369E-03	3.74047E-03	3.21842E-03	2.77236E-03	2.40509E-03	2.04330E-03	1.89553E-03	1.63360E-03
23	1.77089E-03	1.52303E-03	1.31203E-03	1.13272E-03	9.83986E-04	8.21958E-04	7.77523E-04	6.69791E-04
24	2.70264E-03	2.34260E-03	2.03512E-03	1.77518E-03	1.56005E-03	1.34904E-03	1.25411E-03	1.09842E-03
25	1.48410E-03	3.09209E-03	2.49530E-03	1.98492E-03	1.85081E-03	1.21273E-03	9.92496E-04	8.74673E-04
26	1.38417E-03	2.69198E-03	1.97944E-03	1.36004E-03	8.06579E-04	4.47992E-04	1.87170E-04	4.77960E-05
27	5.70954E-04	1.11468E-03	8.29548E-04	5.77019E-04	3.42578E-04	2.16709E-04	1.06050E-04	8.86462E-05
28	9.50645E-04	1.91412E-03	1.48081E-03	1.10404E-03	7.69062E-04	5.49530E-04	3.86785E-04	2.78069E-04
29	9.52483E-04	1.06032E-03	1.08172E-03	1.14024E-03	1.15217E-03	1.19328E-03	1.14160E-03	1.16002E-03









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00000000 22212222222 00000000 333333333333 111 000000000
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00 00 22 .... 00 / 33 ..... 11 00 00
00 00 22 ..... 00 w 33 ..... 11 00 00
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FOLLOWING IS A CARD IMAGE LISTING OF THE INPUT DATA  
COLUMN NUMBER

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CARD 11111111222222222277777 333344444444455555555556666666677777777788
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2 244
3 10001 80014
4 50000 60007 110000 121007 130400
5 140005 240001 250008 340001 290007 301000
6 50100
7 41922381 50922381
8 42922381 50922381
9 4200004 5080004
10 42400000 50400000
11 4210001 5010001
12 4250100 5050100
13 33922381
14 33922381
15 3380004
16 33400000
17 3310001
18 3350100
19 25922381
20 25922381
21 2580004
22 25400000
23 2510001
24 2550100
25

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\*\*\*\*\* END INPUT LISTING \*\*\*\*\*

```

0 14 ARRAY 12 ENTRIES READ
0 01
0 HSCN NUMBER OF EXTRA CROSS SECTIONS 0
MM1 NUMBER OF NUCLIDES FROM MASTER LIBRARY 0
MWT NUMBER OF NUCLIDES FROM X-SECT LIBRARY (LOO 2) 32
MXT NUMBER OF NUCLIDES FROM X-SECT LIBRARY (LOO 3) 6
MCR ANISN/DOT/MORSE OUTPUT TRIGGER 0
MYT TOTAL CROSS SECTION POSITION 3
MS WITHIN-GROUP SCATTERING CROSS SECTION POSITION 4

```

1PM TABLE LENGTH FOR CROSS SECTIONS 125  
 1PM IS AN OLD ANION LIBRARY MOUNTED 5 (0/1 50/YES) 0  
 1PM OUTPUT OPTION TRIGGER -1  
 1PG PRINT CONTROL - FINISH OUTPUT 0

OTHER STORAGE ALLOCATED FOR THIS CASE IS 33000 WORDS

0 24 ARRAY 38 ENTRIES READ  
 0 0T

0 GENERAL INFORMATION CONCERNING CROSS SECTION LIBRARY

TAPE IDENTIFICATION NUMBER 162  
 NUMBER OF NUCLIDES ON TAPE 6  
 NUMBER OF NEUTRON ENERGY GROUPS 125  
 FIRST THERMAL NEUTRON ENERGY GROUP 94  
 NUMBER OF GAMMA ENERGY GROUPS 3

- WORK TAPE 165  
0 THIS XDRN WORKING TAPE WAS CREATED 90/01/02

THE TITLE OF THE PARENT CASE IS AS FOLLOWS

THIS XDRN WORKING TAPE WAS CREATED 90/01/02

THE TITLE OF THE PARENT CASE IS AS FOLLOWS

XDRN WEIGHTED TAPE--PARENT CASE ENTITLED-- (202581) TYPON 15X15 PWR, 3.2% U235

- WTD. TAPE 162

0 162X WEIGHTED TAPE--PARENT CASE ENTITLED-- (202581) TYPON 15X15 PWR, 3.2% U235

, 444--PRM NAT BORON

0 NUCLIDES FROM WORK TAPE

1	HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	10000
2	OXYGEN	THERMAL TEMPERATURE= 294.6 K	80904
3	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	82922351
4	URANIUM-238	THERMAL TEMPERATURE = 294.6 K	50922381
5	URANIUM-238R	THERMAL TEMPERATURE = 294.6 K	42922381
6	URANIUM-238R	THERMAL TEMPERATURE = 294.6 K	50922381
7	HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	4210001
8	HYDROGEN--THERMOS ID=1807(X-640)	THERMAL TEMPERATURE= 294.6 K	5010001
9	BORON NATURAL		55000
10	BORON-10		50100
11	BORON-10		4250100

RITANL VERB. 1.2 90/01/02, 01/03/10 PAGE 6

12	BORON-10		5050100
13	CARBON NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 809.26 K	40000
14	OXYGEN	THERMAL TEMPERATURE= 294.6 K	8260064
15	OXYGEN	THERMAL TEMPERATURE= 294.6 K	5080064
16	SODIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 293.6 K	110000
17	MAGNESIUM	THERMAL TEMP = 900.0 K	120005
18	ALUMINIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	130000
19	SILICON	THERMAL TEMP = 900.0 K	140005
20	CHROMIUM	THERMAL TEMP=294.6	240003
21	MANGANESE	THERMAL TEMP = 900.0 K	250005
22	IRON	THERMAL TEMP=294.6	260001
23	NICKEL	THERMAL TEMP=294.6	260003
24	ZIRCONIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	42400000
25	ZIRCONIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	50400000
26	LEAD NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 293.6 K	820000
27	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	33922351
28	URANIUM-238R	THERMAL TEMPERATURE = 294.6 K	33922381
29	HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	3310001
30	BORON-10		3350100
31	OXYGEN	THERMAL TEMPERATURE= 294.6 K	3380004
32	ZIRCONIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	33400000

0 NUCLIDES FROM WTD. TAPE

33	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	25922351
34	URANIUM-238R	THERMAL TEMPERATURE = 294.6 K	25922381

34 BORON-10 2550100  
 37 OXYGEN THERMAL TEMPERATURE= 294.6 K 2560004  
 38 ZIRCONIUM NATURAL BROWN - ST. JOHN KERNEL TEMP. = 627.13 K 25400000

TIME OF DAY 02-03-12

NITAWL VERS. 1.2 90-01-02 02-05-12 1991 5

THIS XDRN WORKING TAPE WAS CREATED 90/01/02  
 THE TITLE OF THE PARENT CASE IS AS FOLLOWS  
 XDRN WEIGHTED TAPE--PARENT CASE ENTITLED-- [E25NIB1] CAYON 15715 PWR, 2-28 U335  
 400 PPM NAT.BORON  
 IDTT

TAPE ID	327	NUMBER OF NUCLIDES	38
NUMBER OF NEUTRON GROUPS	123	NUMBER OF GAMMA GROUPS	0
FIRST THERMAL GROUP	94		

TABLE OF CONTENTS

HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	ID	10001
OXYGEN	THERMAL TEMPERATURE= 294.6 K	ID	20004
URANIUM-235	THERMAL TEMPERATURE = 294.6 K	ID	42922351
URANIUM-235	THERMAL TEMPERATURE = 294.6 K	ID	51922351
URANIUM-238F	THERMAL TEMPERATURE = 294.6 K	ID	42912381
URANIUM-238F	THERMAL TEMPERATURE = 294.6 K	ID	50922381
HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	ID	6210001
HYDROGEN--THERMOS ID=1803(Y-640)	THERMAL TEMPERATURE= 294.6 K	ID	5910001
BORON NATURAL		ID	30000
BORON-10		ID	50301
BORON-10		ID	4250101
BORON-10		ID	5150101
CARBON NATURAL BROWN - ST. JOHN KERNEL TEMP. = 589.26 K		ID	40002
OXYGEN	THERMAL TEMPERATURE= 294.6 K	ID	4280004
OXYGEN	THERMAL TEMPERATURE= 294.6 K	ID	5060004
SODIUM NATURAL BROWN - ST. JOHN KERNEL TEMP. = 297.6 K		ID	110000
MAGNESIUM	THERMAL TEMP = 900.0 K	ID	120005
ALUMINUM NATURAL BROWN - ST. JOHN KERNEL TEMP. = 627.13 K		ID	130000
SILICON	THERMAL TEMP = 900.0 K	ID	140005
CHROMIUM THERMAL TEMP=294.6		ID	240005
MANGANESE THERMAL TEMP = 900.0 K		ID	250005
IRON THERMAL TEMP=294.6		ID	260001
NICKEL THERMAL TEMP=294.6		ID	280003
ZIRCONIUM NATURAL BROWN - ST. JOHN KERNEL TEMP. = 627.13 K		ID	4240000
ZIRCONIUM NATURAL BROWN - ST. JOHN KERNEL TEMP. = 627.13 K		ID	5040000
LEAD NATURAL BROWN - ST. JOHN KERNEL TEMP. = 292.6 K		ID	810000
URANIUM-235 THERMAL TEMPERATURE = 294.6 K		ID	33922351
URANIUM-238F THERMAL TEMPERATURE = 294.6 K		ID	33922381
HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	ID	3310001
BORON-10		ID	3350100
OXYGEN THERMAL TEMPERATURE= 294.6 K		ID	3780004
ZIRCONIUM NATURAL BROWN - ST. JOHN KERNEL TEMP. = 627.13 K		ID	33400000
URANIUM-235 THERMAL TEMPERATURE = 294.6 K		ID	25922351
URANIUM-238F THERMAL TEMPERATURE = 294.6 K		ID	25922381
HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	ID	2510001
BORON-10		ID	2550100
OXYGEN THERMAL TEMPERATURE= 294.6 K		ID	2560004
ZIRCONIUM NATURAL BROWN - ST. JOHN KERNEL TEMP. = 627.13 K		ID	25400000

--EOR--

1 NBLE POWER COMPUTING/990 - NOS 2.7.1.10. NOS 2.7.1 ST=MAC. 90/01/02. 02.05.42.







[E25K1B1] MIWO MASSEY JOHN OC1 90/01/03, 04.04.05, MID = MAC = NS2

[E25K1B1] EXYON 15X15 PWR, 2.5XU235, 250 PPM NAT.BORON

10F

1077

KK	KK	EEEEEEEEEEEE	NN	NN	0000000000
KK	KK	EEEEEEEEEEEE	NNN	NN	000000000000
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KK	KK	EE	NN NN	NN	00 00
KK	KK	EE	NN NN	NN	00 00
KKKKKKK		EEEEEEEEE	NN NN	NN	00 00
KKKKKKK		EEEEEEEEE	NN NN	NN	00 00
KK	KK	EE	NN NN	NN	00 00
KK	KK	EE	NN NN	NN	00 00
KK	KK	EE	NN	NNNN	00 00
KK	KK	EEEEEEEEEEEE	NN	NNN	000000000000
KK	KK	EEEEEEEEEEEE	NN	NN	0000000000

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99 99	00 00	99	00 00	11	99	00 00	00 00
99 99	00 00	99	00 00	11	99	00 00	00 00
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999999999999	00000000	99	00000000	11111111	99	00000000	000000000000

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00 00	44 44	11	44 44	00 00	8888888888
00 00	444444444444	11	444444444444	00 00	88 88
00 00	444444444444	11	444444444444	00 00	88 88
00 00	44 44	11	44 44	00 00	88 88
000000000	44	11111111	44	000000000	888888888888
0000000	44	11111111	44	0000000	8888888888

FOLLOWING IS A CARD IMAGE LISTING OF THE INPUT DATA COLUMN NUMBER

CARD NUMBER	11111111112222222222333333333344444444445555555555666666666677777777778
	12345678901234567890123456789012345678901234567890123456789012345678901234567890
1	[E25K1B1] EXYON 15X15 PWR, 2.5XU235, 250 PPM NAT.BORON
2	99.0 73 300 3 123 75 18 5 22 6
3	1 1 1 1 -18 1 0 2000 00 1
4	0 0 0 0 0 00 0 0



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88 0 1 -1
89 SECTOR 0 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 0 0 -1
90 0 0 0
91 SECTOR 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0
92 1 -1 0
93 SECTOR 0 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 0 0
94 0 0 1
95 SECTOR 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0
96 1 -1 0
97 SECTOR 0 0 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 0
98 1 -1 0
99 SECTOR 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0
100 0 0 1
101 SECTOR 0 0 0 0 0 0 0 0 0 0 -1 0 0 1 0 0 0 0 0 0 0 0
102 1 -1 0
103 SECTOR 0 0 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 0
104 1 -1 0
105 SECTOR 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0
106 0 0 -1
107 SECTOR 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0
108 0 0 -1
109 SECTOR 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0
110 1 -1 0
111 SECTOR 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0
112 1 -1 0
113 SECTOR 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0
114 0 0 -1
115 SECTOR 0 0 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 0
116 0 0 1
117 SECTOR 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0
118 0 0 -1

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BLOCK 2 1 1
MEDIA 3, 5, 3, 4, 3, 2, 3, 2, 3, 2,

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XINDIV VER 1-24 (21/09/87) 40/01/03, 04, 14, 04, PAGE 5

THE FOLLOWING IS A CARD IMAGE LISTING OF THE INPUT DATA COLUMN NUMBER

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CARD NUMBER 111111111222222222233333333334 44444445555555555666666667777777777
1234567890123456789012345678901234567890123456789012345678901234567890
103 2, 2, 3, 1, 3, 2, 3, 2, 2, 2, 1, 2,
104 3, 1000
105 SURFACES 1, 2, 3, 4, 5, 6, 7, 8, 14, 15,
106 16, 17, 18, 19, 20, 21, 24, 27, 28, 29, 35
107 SECTOR -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
108 SECTOR 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
109 SECTOR 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
110 SECTOR 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
111 SECTOR 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
112 SECTOR 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
113 SECTOR 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0
114 SECTOR 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1
115 SECTOR 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 1 0 0 -1 -1
116 SECTOR 0 0 0 0 0 0 0 0 -1 0 0 1 0 0 0 0 0 1 -1 0 0 0
117 SECTOR 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 1 -1 0 0
118 SECTOR 0 0 0 0 0 0 0 0 -1 0 0 1 0 0 0 0 0 0 0 1 -1 0

```





3	140005	1.90000E-01
4	820000	3.29600E-02
5	10001	2.77000E-02
5	50000	1.46000E-03
5	90004	3.71000E-02
5	110000	2.60000E-04
5	120005	2.08000E-04
5	130000	8.97000E-03
5	140005	7.67000E-04
5	240001	4.89000E-05

ACROSS SECTIONS READ FROM TAPE

NUCLIDE *	10001	HYDROGEN--THERMOS ID=1203(1-140)	THERMAL TEMPERATURE= 294.6 K
NUCLIDE *	80004	OXYGEN	THERMAL TEMPERATURE= 294.6 K
NUCLIDE *	50000	BORON NATURAL	
NUCLIDE *	50100	BORON-10	
NUCLIDE *	60002	CARBON NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 589.26 K
NUCLIDE *	110000	SODIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 293.6 K
NUCLIDE *	120005	MAGNESIUM	THERMAL TEMP = 900.0 K
NUCLIDE *	130000	ALUMINUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K
NUCLIDE *	140005	SILICON	THERMAL TEMP = 900.0 K
NUCLIDE *	250005	MANGANESE	THERMAL TEMP = 900.0 K
NUCLIDE *	260001	IRON	THERMAL TEMP=294.6
NUCLIDE *	620000	LEAD NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 293.6 K
NUCLIDE *	25922351	URANIUM-235	THERMAL TEMPERATURE = 294.6 K
NUCLIDE *	25922351	URANIUM-238	THERMAL TEMPERATURE = 294.6 K
NUCLIDE *	2510001	HYDROGEN--THERMOS ID=1203(1-140)	THERMAL TEMPERATURE= 294.6 K
NUCLIDE *	2550100	BORON-10	
NUCLIDE *	2580004	OXYGEN	THERMAL TEMPERATURE = 294.6 K
NUCLIDE *	25400000	ZIRCONIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K

1 KENOIV VER 1-24 (21/09/87) 9/01/03. 04.14.08. PAGE 5

0(125x181) LYON 15X15 PWR, 2.5XU235, <sup>100%</sup> PPH NAT.BORON

GEOMETRY DESCRIPTION  
OREGION

OREGION  
OBY TYPE

0 2 GENERAL	1	+X = 0.	-X = 0.	+Y = 0.	-Y = 0.	+Z = 0.	-Z = 0.
0 2 GENERAL	2	+X = 0.	-X = 0.	+Y = 0.	-Y = 0.	+Z = 0.	-Z = 0.
0 3 GENERAL	3	+X = 0.	-X = 0.	+Y = 0.	-Y = 0.	+Z = 0.	-Z = 0.
0 4 GENERAL	4	+X = 0.	-X = 0.	+Y = 0.	-Y = 0.	+Z = 0.	-Z = 0.
0 5 GENERAL	5	+X = 0.	-X = 0.	+Y = 0.	-Y = 0.	+Z = 0.	-Z = 0.
0 6 CUBOID	0	+X = 1.0605E+02	-X = -1.0000E-04	+Y = 1.0605E+02	-Y = -1.0000E-04	+Z = 5.0000E+01	-Z = -1.0000E-04

1 KENOIV VER 1-24 (21/09/87) 9/01/03. 04.14.08. PAGE 10

0(125x181) LYON 15X15 PWR, 2.5XU235, <sup>100%</sup> PPH NAT.BORON

WEIGHTING FUNCTION  
OBY TYPE

GROUP	WTLOW	WT AVG	WT HI
0 REGION 1 DEFINED BY GEOMETRY CARD 1			
1	.167	.500	1.500
GROUPS 2 TO 123 SAME AS ABOVE			
0 REGION 2 DEFINED BY GEOMETRY CARD 2			
1	.167	.500	1.500
GROUPS 2 TO 123 SAME AS ABOVE			
0 REGION 3 DEFINED BY GEOMETRY CARD 3			
1	.167	.500	1.500
GROUPS 2 TO 123 SAME AS ABOVE			
0 REGION 4 DEFINED BY GEOMETRY CARD 4			
1	.167	.500	1.500
GROUPS 2 TO 123 SAME AS ABOVE			
0 REGION 5 DEFINED BY GEOMETRY CARD 5			
1	.167	.500	1.500
GROUPS 2 TO 123 SAME AS ABOVE			











46	8.87925E-01	1.37145E+01	9.38146E-01	4.81055E-03	0.
47	9.32022E-01	1.40120E+01	9.38028E-01	4.70637E-03	0.
48	9.10556E-01	1.40112E+01	9.37430E-01	4.64150E-03	0.
49	9.75509E-01	1.46137E+01	9.38241E-01	4.61337E-03	0.
50	9.64669E-01	1.49073E+01	9.39208E-01	4.61966E-03	0.
51	9.53022E-01	1.52125E+01	9.39490E-01	4.53219E-03	0.
52	9.46687E-01	1.55197E+01	9.39630E-01	4.44283E-03	0.
53	9.36377E-01	1.58238E+01	9.39565E-01	4.35572E-03	0.
54	9.28891E-01	1.61227E+01	9.39360E-01	4.27568E-03	0.

KENDIV VER 1.2A (21/09/87) 90/01/03 04.14.08 PAGE 17

55	9.47115E-01	1.64117E+01	9.39506E-01	4.19678E-03	0.
56	9.22128E-01	1.67167E+01	9.39184E-01	4.17088E-03	0.
57	9.46209E-01	1.70145E+01	9.39312E-01	4.05709E-03	0.
58	9.29797E-01	1.73267E+01	9.39142E-01	3.98760E-03	0.
59	9.31222E-01	1.76338E+01	9.39007E-01	3.91949E-03	0.
60	9.46138E-01	1.79569E+01	9.39126E-01	3.85326E-03	0.
61	9.41974E-01	1.82877E+01	9.39174E-01	3.78771E-03	0.
62	9.48727E-01	1.86342E+01	9.39334E-01	3.7245E-03	0.
63	9.17328E-01	1.89829E+01	9.39475E-01	3.66354E-03	0.
64	9.24214E-01	1.93402E+01	9.39738E-01	3.6049E-03	0.
65	9.44633E-01	1.97049E+01	9.39529E-01	3.5485E-03	0.
66	9.30460E-01	1.99735E+01	9.39698E-01	3.49407E-03	0.
67	9.14573E-01	2.00252E+01	9.39327E-01	3.44193E-03	0.
68	9.65085E-01	2.03250E+01	9.38732E-01	3.45656E-03	0.
69	9.00968E-01	2.06177E+01	9.38144E-01	3.45092E-03	0.
70	9.74241E-01	2.09175E+01	9.38694E-01	3.44093E-03	0.
71	9.38813E-01	2.12092E+01	9.38701E-01	3.39070E-03	0.
72	9.82074E-01	2.15128E+01	9.39316E-01	3.39991E-03	0.
73	9.18613E-01	2.18240E+01	9.39041E-01	3.36566E-03	0.

WAVE MATRIX  $\lambda_{-1}$  IS THE LARGEST EIGENVALUE OF THE MATRIX OF FISSION PROBABILITIES BY UNIT.  
 THREE ARE NDMAX, NDMYX, NDBMX UNITS IN AN ARRAY.

KENDIV VER 1.2A (21/09/87) 90/01/03 04.14.08 PAGE 18

G[E25K1B1] EXXON 15X15 PWR, 2.5XU235, 900 PPM NAT.BORON

ELFTIME = 3.70524E-05 + 0E - 2.80899E-07 GENERATION TIME = 2.71122E-05 + 0E - 1.86427E-07

NO. OF INITIAL

GENERATIONS	AVG K		47 PER CENT		49 PER CENT		49 PER CENT		NUMBER OF HISTORIES
	SKIPPED	K-EFFECTIVE	DEVIATION	CONFIDENCE INTERVAL	CONFIDENCE INTERVAL	CONFIDENCE INTERVAL	CONFIDENCE INTERVAL		
0	0	.93902	+ 0E - .00301	.93651 TO .94312	.93220 TO .94645	.92995 TO .94976	.92995 TO .94976	21000	
1	4	.94084	+ 0E - .00326	.93739 TO .94390	.93413 TO .94715	.93088 TO .95041	.93088 TO .95041	20700	
2	5	.94265	+ 0E - .00330	.93924 TO .94595	.93606 TO .94925	.93274 TO .95066	.93274 TO .95066	20400	
3	6	.94058	+ 0E - .00335	.93722 TO .94393	.93387 TO .94728	.93052 TO .95063	.93052 TO .95063	20100	
4	7	.94062	+ 0E - .00340	.93721 TO .94403	.93382 TO .94745	.93041 TO .95083	.93041 TO .95083	19800	
5	8	.94135	+ 0E - .00338	.93798 TO .94473	.93460 TO .94810	.93123 TO .95148	.93123 TO .95148	19500	
6	9	.94211	+ 0E - .00334	.93876 TO .94545	.93542 TO .94879	.93208 TO .95213	.93208 TO .95213	19200	
7	10	.94174	+ 0E - .00333	.93940 TO .94607	.93607 TO .94941	.93273 TO .95274	.93273 TO .95274	18900	
8	11	.94310	+ 0E - .00337	.93972 TO .94644	.93636 TO .94963	.93294 TO .95320	.93294 TO .95320	18600	
9	12	.94321	+ 0E - .00342	.93979 TO .94664	.93637 TO .95006	.93294 TO .95348	.93294 TO .95348	18300	
10	17	.94171	+ 0E - .00334	.93837 TO .94506	.93503 TO .94840	.93166 TO .95175	.93166 TO .95175	18000	
11	22	.93985	+ 0E - .00349	.93636 TO .94334	.93288 TO .94683	.92939 TO .95032	.92939 TO .95032	17500	
12	27	.94177	+ 0E - .00372	.93805 TO .94548	.93434 TO .94920	.93062 TO .95291	.93062 TO .95291	17000	
13	32	.94171	+ 0E - .00410	.93761 TO .94581	.93351 TO .94991	.92940 TO .95402	.92940 TO .95402	16500	
14	37	.94021	+ 0E - .00429	.93573 TO .94450	.93165 TO .94878	.92737 TO .95306	.92737 TO .95306	16000	
15	42	.94009	+ 0E - .00416	.93597 TO .94425	.93176 TO .94842	.92760 TO .95258	.92760 TO .95258	15500	
16	47	.94064	+ 0E - .00435	.93634 TO .94505	.93198 TO .94940	.92763 TO .95376	.92763 TO .95376	15000	
17	52	.93751	+ 0E - .00433	.93318 TO .94184	.92885 TO .94617	.92452 TO .95050	.92452 TO .95050	14500	
18	57	.93794	+ 0E - .00555	.93239 TO .94349	.92685 TO .94904	.92130 TO .95459	.92130 TO .95459	14000	
19	62	.93720	+ 0E - .00802	.92918 TO .94522	.92117 TO .95324	.91315 TO .96126	.91315 TO .96126	13500	
20	67	.94634	+ 0E - .01341	.93293 TO .95975	.91951 TO .97316	.90610 TO .98657	.90610 TO .98657	12000	

KENDIV VER 1.2A (21/09/87) 90/01/03 04.14.08 PAGE 19

G[E25K1B1] EXXON 15X15 PWR, 2.5XU235, 900 PPM NAT.BORON

GROUP REGION LEAKAGE ABSORPTIONS FISSIONS WITH 3 GENERATIONS SKIPPED

C 1	0.	9.02643E-06	1.33379E-05
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[[42N1E] MESS RASSLY JOHN 001 90/01/03, 02.37.04, MID = MAC = MS2  
[[42N1E] EXXON 15X15 PWR, 4.2% U235, ~~230~~ PPM NAT.BORON  
--EOP--

FOLLOWING IS A CARD IMAGE LISTING OF THE INPUT DATA  
COLUMN NUMBER

CARD NUMBER	11111111112222222222333333333344444444445555555555666666666677777777778	1234567890123456789012345678901234567890123456789012345678901234567890
1	[[42N1E] EXXON 15X15 PWR, 4.2% U235, <del>230</del> PPM NAT.BORON	
2	14# 2 3 11 0 5 2 10 0 3 1 10 12 0 0 0	
3	24# -2 -1 -1 1	
4	34# 1 0 0 0 4.0 0 0 0 0 0 1 0	
5	44# -1 123 0 -2 3 4 124 -1 0	
6	54# 1.4 2.4 1.0 0.0 0.0 1.420992 1	
7	7	
8	134# 1	
9	1	
10	1	
11	2	
12	2	
13	3	
14	7 2	
15	3	
16	144#	
17	0	
18	42#12351 42#21201	
19	4200004	
20	0	
21	42400000	
22	0	
23	4240001 42#0004	
24	4250100	
25	15#	
26	0.0	
27	9.7433-4 2.1469-2	
28	4.5930-2	
29	0.0	
30	3.8022-2	
31	0.0	
32	6.671-2 3.336-4	
33	3.007-3	
34	7	
35	33# 581.0 10.0	
36	7	
37	35# 410.0 110.4445 310.3271 0.8344	
38	36# 581 262 487	
39	39# 1 2 3	
40	40# 77	
41	51# 12111.0 123.0	
42	7	

\*\*\*\*\* END OF INPUT LISTING \*\*\*\*\*







25 0  
 26 0  
 27 0  
 28 0  
 29 0  
 30 0  
 31 0  
 32 0  
 33 0  
 34 0  
 35 0  
 36 0  
 37 v  
 38 0

TIME OF DAY 02.39.51.

01DAT=0 REQUIRES 74638 LOCATIONS. THIS VERSION OF ASDRN ALLOWS A MAXIMUM OF 33000

0 CROSS SECTIONS WILL BE STORED EXTERNALLY

0 22248 LOCATIONS WILL BE USED

RD EXECUTING FIRST TIME

0 004 ARRAY 1250 ENTRIES READ

0 01

0 004 ARRAY 12 ENTRIES READ

0 004 ARRAY 11 ENTRIES READ

ASDRNPM VERS. 1.0A 00/01/05. 02.39.56. PAGE 4

0 004 ARRAY 3 ENTRIES READ

0 004 ARRAY 3 ENTRIES READ

0 004 ARRAY 123 ENTRIES READ

0 01

ASDRNPM VERS. 1.0A 00/01/05. 02.39.56. PAGE 7

[E42NIB] EXXON 15X15 FWR, 4.21 U335, 1000 PPM NAT.BORON

NEUTRON GROUP PARAMETERS

GROUP	ENERGY BOUNDARIES	LETHARGY BOUNDARIES	MID PT VELOCITIES	BROAD GRP NUMBERS	CALC TYPE	RIGHT ALBEDO	LEFT ALBEDO
1	1.49180E+07	-3.99983E-01	5.21033E+09	1	0	1.00000E+00	
2	1.34990E+07	-3.00031E-01	4.95624E+09	2	0	1.00000E+00	
3	1.22140E+07	-1.99992E-01	4.71452E+09	3	0	1.00000E+00	
4	1.10520E+07	1.00026E-01	4.48459E+09	4	0	1.00000E+00	
5	1.00000E+07	0	4.26585E+09	5	0	1.00000E+00	
6	9.04840E+06	9.99971E-01	4.05780E+09	6	0	1.00000E+00	
7	8.19730E+06	2.00001E-01	3.85190E+09	7	0	1.00000E+00	
8	7.40820E+06	2.99998E-01	3.67165E+09	8	0	1.00000E+00	
9	6.70320E+06	4.00000E-01	3.49259E+09	9	0	1.00000E+00	
10	6.06530E+06	5.00001E-01	3.32224E+09	10	0	1.00000E+00	
11	5.48810E+06	6.00003E-01	3.16020E+09	11	0	1.00000E+00	
12	4.96580E+06	7.00011E-01	3.00609E+09	12	0	1.00000E+00	
13	4.49330E+06	7.99998E-01	2.85948E+09	13	0	1.00000E+00	
14	4.06570E+06	8.99999E-01	2.72002E+09	14	0	1.00000E+00	
15	3.67890E+06	9.99998E-01	2.58736E+09	15	0	1.00000E+00	
16	3.32070E+06	1.10000E+00	2.46117E+09	16	0	1.00000E+00	
17	3.01190E+06	1.20001E+00	2.34113E+09	17	0	1.00000E+00	
18	2.72530E+06	1.30001E+00	2.22697E+09	18	0	1.00000E+00	
19	2.46600E+06	1.39999E+00	2.11836E+09	19	0	1.00000E+00	
20	2.23130E+06	1.50000E+00	2.01505E+09	20	0	1.00000E+00	
21	2.01900E+06	1.59998E+00	1.91677E+09	21	0	1.00000E+00	
22	1.82680E+06	1.70002E+00	1.82328E+09	22	0	1.00000E+00	
23	1.65300E+06	1.79999E+00	1.73437E+09	23	0	1.00000E+00	
24	1.49570E+06	1.89999E+00	1.64976E+09	24	0	1.00000E+00	
25	1.35330E+06	2.00004E+00	1.56931E+09	25	0	1.00000E+00	
26	1.22460E+06	2.09997E+00	1.49278E+09	26	0	1.00000E+00	
27	1.10800E+06	2.20003E+00	1.41997E+09	27	0	1.00000E+00	
28	1.00260E+06	2.29999E+00	1.35073E+09	28	0	1.00000E+00	
29	9.07180E+05	2.40000E+00	1.28485E+09	29	0	1.00000E+00	







GRP. 18	REQUIRED	1 ITERATIONS, MFD OF	6.29896E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 19	REQUIRED	1 ITERATIONS, MFD OF	5.68034E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 20	REQUIRED	1 ITERATIONS, MFD OF	5.19920E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 21	REQUIRED	1 ITERATIONS, MFD OF	5.35419E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 22	REQUIRED	1 ITERATIONS, MFD OF	5.53890E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 23	REQUIRED	1 ITERATIONS, MFD OF	4.76833E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 24	REQUIRED	1 ITERATIONS, MFD OF	5.57814E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 25	REQUIRED	1 ITERATIONS, MFD OF	5.02817E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 26	REQUIRED	1 ITERATIONS, MFD OF	5.02270E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 27	REQUIRED	1 ITERATIONS, MFD OF	4.65812E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 28	REQUIRED	1 ITERATIONS, MFD OF	4.51642E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 29	REQUIRED	1 ITERATIONS, MFD OF	5.18698E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 30	REQUIRED	1 ITERATIONS, MFD OF	5.25841E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 31	REQUIRED	1 ITERATIONS, MFD OF	5.23278E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 32	REQUIRED	1 ITERATIONS, MFD OF	5.11940E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 33	REQUIRED	1 ITERATIONS, MFD OF	4.95207E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 34	REQUIRED	1 ITERATIONS, MFD OF	4.61732E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 35	REQUIRED	1 ITERATIONS, MFD OF	4.48398E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 36	REQUIRED	1 ITERATIONS, MFD OF	4.26497E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 37	REQUIRED	1 ITERATIONS, MFD OF	4.56370E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 38	REQUIRED	1 ITERATIONS, MFD OF	4.65408E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 39	REQUIRED	1 ITERATIONS, MFD OF	5.12580E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 40	REQUIRED	1 ITERATIONS, MFD OF	5.25024E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 41	REQUIRED	1 ITERATIONS, MFD OF	5.37141E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 42	REQUIRED	1 ITERATIONS, MFD OF	5.27028E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 43	REQUIRED	1 ITERATIONS, MFD OF	5.24581E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 44	REQUIRED	1 ITERATIONS, MFD OF	5.21970E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 45	REQUIRED	1 ITERATIONS, MFD OF	5.18635E-05	OCCURRED IN INT.	11	COARSE MESH=	1
GRP. 46	REQUIRED	1 ITERATIONS, MFD OF	5.13528E-05	OCCURRED IN INT.	10	COARSE MESH=	1
GRP. 47	REQUIRED	1 ITERATIONS, MFD OF	5.19247E-05	OCCURRED IN INT.	10	COARSE MESH=	1
GRP. 48	REQUIRED	1 ITERATIONS, MFD OF	5.05211E-05	OCCURRED IN INT.	10	COARSE MESH=	1
GRP. 49	REQUIRED	1 ITERATIONS, MFD OF	5.00469E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 50	REQUIRED	1 ITERATIONS, MFD OF	4.73109E-05	OCCURRED IN INT.	10	COARSE MESH=	1
GRP. 51	REQUIRED	1 ITERATIONS, MFD OF	4.27569E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 52	REQUIRED	1 ITERATIONS, MFD OF	4.20543E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 53	REQUIRED	1 ITERATIONS, MFD OF	4.10395E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 54	REQUIRED	1 ITERATIONS, MFD OF	4.02116E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 55	REQUIRED	1 ITERATIONS, MFD OF	3.92241E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 56	REQUIRED	1 ITERATIONS, MFD OF	3.78274E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 57	REQUIRED	1 ITERATIONS, MFD OF	3.64655E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 58	REQUIRED	1 ITERATIONS, MFD OF	3.53517E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 59	REQUIRED	1 ITERATIONS, MFD OF	3.40506E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 60	REQUIRED	1 ITERATIONS, MFD OF	3.24691E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 61	REQUIRED	1 ITERATIONS, MFD OF	3.10807E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 62	REQUIRED	1 ITERATIONS, MFD OF	2.95351E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 63	REQUIRED	1 ITERATIONS, MFD OF	2.83251E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 64	REQUIRED	1 ITERATIONS, MFD OF	2.72245E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 65	REQUIRED	1 ITERATIONS, MFD OF	2.56872E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 66	REQUIRED	1 ITERATIONS, MFD OF	2.40054E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 67	REQUIRED	1 ITERATIONS, MFD OF	2.32183E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 68	REQUIRED	1 ITERATIONS, MFD OF	2.18269E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 69	REQUIRED	1 ITERATIONS, MFD OF	2.08501E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 70	REQUIRED	1 ITERATIONS, MFD OF	1.98753E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 71	REQUIRED	1 ITERATIONS, MFD OF	1.95051E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 72	REQUIRED	1 ITERATIONS, MFD OF	1.90082E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 73	REQUIRED	1 ITERATIONS, MFD OF	1.73349E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 74	REQUIRED	1 ITERATIONS, MFD OF	1.68282E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 75	REQUIRED	1 ITERATIONS, MFD OF	1.49572E-05	OCCURRED IN INT.	9	COARSE MESH=	2
GRP. 76	REQUIRED	1 ITERATIONS, MFD OF	1.63045E-05	OCCURRED IN INT.	9	COARSE MESH=	1
GRP. 77	REQUIRED	1 ITERATIONS, MFD OF	1.37023E-05	OCCURRED IN INT.	9	COARSE MESH=	2
GRP. 78	REQUIRED	1 ITERATIONS, MFD OF	1.55288E-05	OCCURRED IN INT.	9	COARSE MESH=	1



TRANSPORT CROSS SECTION WEIGHTING FUNCTION

ZONE	GRP. 1	GRP. 2	GRP. 3	GRP. 4	GRP. 5	GRP. 6	GRP. 7	GRP. 8	
0	1	6.49066E-06	1.81788E-05	4.50061E-05	1.01025E-04	2.06705E-04	3.80852E-04	6.61262E-04	1.07285E-03
0	2	7.28039E-06	2.02540E-05	5.04337E-05	1.12995E-04	2.30554E-04	4.29760E-04	7.42816E-04	1.20530E-03
0	3	2.66108E-06	7.27540E-06	1.80375E-05	4.63310E-05	8.23480E-05	1.54401E-04	2.66605E-04	4.32911E-04
0	4	4.36914E-06	1.22269E-05	3.02905E-05	6.78752E-05	1.38702E-04	2.57791E-04	4.46184E-04	7.24117E-04
ZONE	GRP. 9	GRP. 10	GRP. 11	GRP. 12	GRP. 13	GRP. 14	GRP. 15	GRP. 16	
0	1	1.61861E-03	2.23985E-03	3.06797E-03	3.92436E-03	4.89405E-03	5.28795E-03	6.25935E-03	7.65966E-03
0	2	1.82905E-03	2.59054E-03	3.50518E-03	4.57660E-03	5.56122E-03	6.46277E-03	7.61779E-03	9.11393E-03
0	3	6.59666E-04	9.39055E-04	1.27960E-03	1.67349E-03	2.05955E-03	2.41212E-03	2.84470E-03	3.39216E-03
0	4	1.09660E-03	1.53679E-03	2.08344E-03	2.72099E-03	3.30078E-03	3.79261E-03	4.47937E-03	5.40473E-03
ZONE	GRP. 17	GRP. 18	GRP. 19	GRP. 20	GRP. 21	GRP. 22	GRP. 23	GRP. 24	
0	1	6.67965E-03	9.29230E-03	1.26009E-02	1.66862E-02	2.14905E-02	2.45339E-02	2.97033E-02	3.60240E-02
0	2	1.02863E-02	1.40680E-02	1.86776E-02	2.42333E-02	3.07785E-02	3.17563E-02	3.13959E-02	1.20080E-02
0	3	3.84475E-03	4.16190E-03	4.45053E-03	4.74947E-03	4.98566E-03	4.56984E-03	4.47602E-03	4.71893E-03
0	4	6.11972E-03	6.58503E-03	6.94931E-03	7.24426E-03	7.4919E-03	6.95161E-03	6.73717E-03	7.12754E-03
ZONE	GRP. 25	GRP. 26	GRP. 27	GRP. 28	GRP. 29	GRP. 30	GRP. 31	GRP. 32	
0	1	6.60533E-03	9.30172E-03	1.26708E-02	1.66854E-02	2.14903E-02	1.05556E-02	9.16655E-03	8.48067E-03
0	2	1.08820E-02	1.46015E-02	1.94275E-02	2.47152E-02	3.0496E-02	1.31347E-02	1.14739E-02	1.05803E-02
0	3	4.32544E-03	4.60095E-03	4.77332E-03	4.88461E-03	4.90040E-03	5.23362E-03	4.61719E-03	4.26473E-03
0	4	6.64563E-03	6.90461E-03	7.12964E-03	7.32756E-03	7.50402E-03	7.03290E-03	6.65477E-03	6.33258E-03
ZONE	GRP. 33	GRP. 34	GRP. 35	GRP. 36	GRP. 37	GRP. 38	GRP. 39	GRP. 40	
0	1	7.65649E-03	8.63652E-03	1.01723E-02	1.22547E-02	1.49761E-02	1.20949E-02	8.55979E-03	4.77052E-03
0	2	9.49077E-03	1.19374E-02	1.49753E-02	1.81691E-02	2.18392E-02	1.69450E-02	1.17644E-02	5.15074E-03
0	3	3.82212E-03	3.91407E-03	3.99910E-03	4.07169E-03	4.1459E-03	3.53322E-03	2.75136E-03	2.11008E-03
0	4	5.69600E-03	6.07429E-03	6.44105E-03	6.83637E-03	7.23910E-03	6.04521E-03	4.10714E-03	3.18197E-03
ZONE	GRP. 41	GRP. 42	GRP. 43	GRP. 44	GRP. 45	GRP. 46	GRP. 47	GRP. 48	
0	1	3.73828E-03	3.27136E-03	2.87179E-03	2.54130E-03	2.26619E-03	2.02608E-03	1.86094E-03	1.66071E-03
0	2	4.30320E-03	3.71148E-03	3.18940E-03	2.74694E-03	2.39106E-03	2.02054E-03	1.87399E-03	1.61352E-03
0	3	1.75596E-03	1.51169E-03	1.30145E-03	1.12277E-03	9.74573E-04	8.13083E-04	7.69074E-04	6.61915E-04
0	4	2.68047E-03	2.32184E-03	2.01597E-03	1.75737E-03	1.54341E-03	1.37345E-03	1.23953E-03	1.09492E-03
ZONE	GRP. 49	GRP. 50	GRP. 51	GRP. 52	GRP. 53	GRP. 54	GRP. 55	GRP. 56	
0	1	1.46462E-03	1.04767E-03	7.45520E-04	5.94828E-04	4.51732E-04	3.19199E-04	2.61204E-04	1.99675E-04
0	2	1.36560E-03	2.44775E-03	1.93715E-03	1.31969E-03	7.68661E-04	4.11091E-04	1.49829E-04	8.64625E-05
0	3	5.63660E-04	1.09733E-03	8.12959E-04	5.61201E-04	3.27744E-04	2.02207E-04	9.14096E-05	1.85510E-05
0	4	4.38234E-04	1.88516E-03	1.45385E-03	1.07832E-03	7.45669E-04	5.07016E-04	3.64243E-04	2.96070E-04
ZONE	GRP. 57	GRP. 58	GRP. 59	GRP. 60	GRP. 61	GRP. 62	GRP. 63	GRP. 64	
0	1	9.78539E-04	1.08624E-03	1.11115E-03	1.17147E-03	1.18799E-03	1.23150E-03	1.18542E-03	1.21003E-03
0	2	2.25584E-04	3.70868E-04	4.79405E-04	5.82692E-04	6.04055E-04	6.74918E-04	6.37620E-04	6.62045E-04
0	3	7.37821E-05	1.17582E-04	1.65204E-04	2.22590E-04	2.28242E-04	2.56131E-04	2.50664E-04	2.57885E-04
0	4	3.68854E-04	4.44777E-04	4.90416E-04	5.56995E-04	5.67913E-04	6.05892E-04	5.83590E-04	5.98912E-04
ZONE	GRP. 65	GRP. 66	GRP. 67	GRP. 68	GRP. 69	GRP. 70	GRP. 71	GRP. 72	
0	1	1.29186E-03	1.32796E-03	1.20434E-03	1.46934E-03	1.45294E-03	1.52255E-03	1.50948E-03	1.55019E-03
0	2	7.79105E-04	8.38253E-04	8.92221E-04	1.06438E-03	1.04936E-03	1.14309E-03	1.13586E-03	1.21461E-03
0	3	2.99248E-04	3.21961E-04	2.79748E-04	4.10350E-04	4.08699E-04	5.09413E-04	4.43205E-04	4.77675E-04
0	4	6.61860E-04	6.93179E-04	6.13231E-04	8.14831E-04	8.07019E-04	9.67825E-04	8.54704E-04	8.96750E-04
ZONE	GRP. 73	GRP. 74	GRP. 75	GRP. 76	GRP. 77	GRP. 78	GRP. 79	GRP. 80	
0	1	1.68458E-03	1.99565E-03	2.74303E-03	1.04284E-03	3.61391E-03	1.07583E-03	3.04320E-03	1.56487E-03
ZONE	GRP. 81	GRP. 82	GRP. 83	GRP. 84	GRP. 85	GRP. 86	GRP. 87	GRP. 88	
0	1	2.31764E-03	5.17335E-03	7.34541E-04	5.77876E-03	1.21057E-03	2.33568E-03	2.73017E-03	6.45213E-03
0	2	2.42257E-03	7.31709E-03	1.06968E-04	7.97982E-03	7.74153E-04	2.51820E-03	3.11251E-03	9.01161E-03
0	3	9.44282E-04	2.80457E-03	3.36456E-05	3.05066E-03	3.64698E-04	9.96615E-04	1.21765E-03	3.44522E-03
0	4	1.54694E-03	4.08757E-03	2.56759E-04	4.49505E-03	6.73770E-04	1.59308E-03	1.91451E-03	5.05378E-03
ZONE	GRP. 89	GRP. 90	GRP. 91	GRP. 92	GRP. 93	GRP. 94	GRP. 95	GRP. 96	
0	1	3.80996E-03	1.39154E-03	1.36274E-03	1.00881E-03	1.08212E-03	1.96846E-04	2.74379E-04	4.13901E-04



3	1.96348E-03	5.39709E-04	5.10534E-04	3.09044E-04	3.81317E-04	6.35413E-04	5.10179E-05	1.32162E-04
4	2.81452E-03	8.83191E-04	8.54957E-04	5.68939E-04	6.24160E-04	6.53038E-05	1.26149E-04	2.41177E-04
0 ZONE	GRP. 97	GRP. 98	GRP. 99	GRP. 100	GRP. 101	GRP. 102	GRP. 103	GRP. 104
1	4.86283E-04	8.83330E-04	1.07720E-03	8.65342E-04	8.88672E-04	1.13423E-03	1.28949E-03	1.70497E-03
2	3.20884E-04	8.51943E-04	1.17620E-03	8.21606E-04	8.56852E-04	1.04730E-03	1.29023E-03	1.77780E-03
3	1.23671E-04	3.31287E-04	4.57657E-04	3.21894E-04	3.34491E-04	4.06847E-04	5.04738E-04	6.85066E-04
4	2.58855E-04	5.64437E-04	7.35957E-04	5.49815E-04	5.68499E-04	7.08390E-04	8.41253E-04	1.13202E-03
0 ZONE	GRP. 105	GRP. 106	GRP. 107	GRP. 108	GRP. 109	GRP. 110	GRP. 111	GRP. 112
1	2.62694E-03	2.27507E-03	2.90653E-03	3.40871E-03	1.74915E-03	2.12927E-03	2.77611E-03	3.72881E-03
2	3.00196E-03	2.80405E-03	3.62734E-03	4.19728E-03	2.15197E-03	2.62942E-03	3.45988E-03	4.68629E-03
3	1.18967E-03	1.07785E-03	1.58575E-03	1.62094E-03	8.34899E-04	1.02704E-03	1.35896E-03	1.85124E-03
4	1.83620E-03	1.65752E-03	2.12814E-03	2.48638E-03	1.27742E-03	1.56222E-03	2.05245E-03	2.77618E-03
0 ZONE	GRP. 113	GRP. 114	GRP. 115	GRP. 116	GRP. 117	GRP. 118	GRP. 119	GRP. 120
1	5.37901E-03	8.61746E-03	5.62051E-03	7.09041E-03	8.68104E-03	1.03370E-02	1.18217E-02	1.27920E-02
2	6.85789E-03	1.03807E-02	7.39324E-03	9.29985E-03	1.16764E-02	1.40695E-02	1.6.1.9E-02	1.80104E-02
3	2.72418E-03	4.15260E-03	2.96524E-03	3.72447E-03	4.68679E-03	5.59373E-03	6.47935E-03	7.07872E-03
4	4.04866E-03	6.10520E-03	4.32523E-03	5.41636E-03	6.75623E-03	8.09330E-03	9.33303E-03	1.01791E-02
0 ZONE	GRP. 121	GRP. 122	GRP. 123	GRP. 124				
1	6.29988E-03	5.71386E-03	4.45144E-03	4.49603E-03				
2	9.05076E-03	8.36819E-03	6.74969E-03	5.33278E-03				
3	3.81194E-03	3.20699E-03	2.54872E-03	2.09865E-03				
4	5.05022E-03	4.41280E-03	3.65727E-03	3.23183E-03				

TIME OF DAY 02:40:46.

ISDRMFM VERS. 1.04 90701/03 02:39:26. F00E 16

EXON 15415 RWR, 4.25 U216, 7752 PPM NAT. BORDO  
 CELL AVERAGED FLUXES

0 ZONE	GRP. 1	GRP. 2	GRP. 3	GRP. 4	GRP. 5	GRP. 6	GRP. 7	GRP. 8
1	2.32906E-04	6.55389E-04	1.61870E-03	3.61201E-03	7.45164E-03	1.32819E-02	2.33798E-02	3.77091E-02
2	1.25279E-04	6.34253E-04	1.56195E-03	3.48338E-03	7.21057E-03	1.28312E-02	2.25625E-02	3.64474E-02
3	2.20525E-04	6.20974E-04	1.52679E-03	3.41933E-03	7.05962E-03	1.25446E-02	2.20712E-02	3.56094E-02
4	2.24904E-04	6.33167E-04	1.55912E-03	3.48747E-03	7.19804E-03	1.28046E-02	2.25195E-02	3.63773E-02
0 ZONE	GRP. 9	GRP. 10	GRP. 11	GRP. 12	GRP. 13	GRP. 14	GRP. 15	GRP. 16
1	5.34436E-02	7.14754E-02	9.40643E-02	1.22278E-01	1.38211E-01	1.42451E-01	1.71378E-01	2.27827E-01
2	5.35092E-02	6.87498E-02	9.07524E-02	1.17429E-01	1.32264E-01	1.35515E-01	1.62181E-01	2.18204E-01
3	5.23095E-02	6.69995E-02	8.79585E-02	1.14209E-01	1.28359E-01	1.30882E-01	1.57706E-01	2.11697E-01
4	5.34178E-02	6.89873E-02	9.01198E-02	1.17118E-01	1.31951E-01	1.34999E-01	1.62566E-01	2.17430E-01
0 ZONE	GRP. 17	GRP. 18	GRP. 19	GRP. 20	GRP. 21	GRP. 22	GRP. 23	GRP. 24
1	2.66043E-01	2.84724E-01	2.97106E-01	2.63823E-01	2.39637E-01	2.71460E-01	2.59410E-01	2.83683E-01
2	2.53377E-01	2.73344E-01	2.85531E-01	2.52745E-01	2.28991E-01	2.59859E-01	2.48291E-01	2.71919E-01
3	2.47930E-01	2.65231E-01	2.76755E-01	2.44062E-01	2.20534E-01	2.50651E-01	2.39112E-01	2.62242E-01
4	2.54394E-01	2.72189E-01	2.84056E-01	2.51173E-01	2.27421E-01	2.58147E-01	2.46447E-01	2.69905E-01
0 ZONE	GRP. 25	GRP. 26	GRP. 27	GRP. 28	GRP. 29	GRP. 30	GRP. 31	GRP. 32
1	2.51029E-01	2.78577E-01	2.13268E-01	2.17013E-01	2.83735E-01	3.03580E-01	2.70393E-01	2.54426E-01
2	2.40395E-01	2.67459E-01	2.04214E-01	2.07481E-01	2.71399E-01	2.90505E-01	2.59349E-01	2.44274E-01
3	2.31791E-01	2.57956E-01	1.96170E-01	1.99208E-01	2.60977E-01	2.79241E-01	2.49426E-01	2.35124E-01
4	2.38504E-01	2.65431E-01	2.02789E-01	2.05671E-01	2.69219E-01	2.89070E-01	2.57040E-01	2.42152E-01
0 ZONE	GRP. 33	GRP. 34	GRP. 35	GRP. 36	GRP. 37	GRP. 38	GRP. 39	GRP. 40
1	2.17582E-01	2.15858E-01	1.60301E-01	1.46813E-01	1.97716E-01	2.22214E-01	1.89891E-01	1.67817E-01
2	2.28502E-01	2.08087E-01	1.56002E-01	1.43189E-01	1.90597E-01	2.13271E-01	1.83553E-01	1.63125E-01
3	2.20294E-01	2.00945E-01	1.51415E-01	1.39524E-01	1.84547E-01	2.05565E-01	1.77566E-01	1.58620E-01
4	2.26591E-01	2.06385E-01	1.54697E-01	1.42206E-01	1.89319E-01	2.11605E-01	1.82072E-01	1.61987E-01
0 ZONE	GRP. 41	GRP. 42	GRP. 43	GRP. 44	GRP. 45	GRP. 46	GRP. 47	GRP. 48
1	1.55857E-01	1.46446E-01	1.38328E-01	1.31777E-01	1.26325E-01	1.21831E-01	1.14570E-01	1.09249E-01
2	1.52021E-01	1.43238E-01	1.35658E-01	1.29563E-01	1.24487E-01	1.20285E-01	1.13231E-01	1.08211E-01
3	1.48299E-01	1.40059E-01	1.32941E-01	1.27239E-01	1.22487E-01	1.18663E-01	1.11650E-01	1.06868E-01
4	1.51069E-01	1.42403E-01	1.34923E-01	1.28913E-01	1.23907E-01	1.19832E-01	1.12738E-01	1.07777E-01
0 ZONE	GRP. 49	GRP. 50	GRP. 51	GRP. 52	GRP. 53	GRP. 54	GRP. 55	GRP. 56
1	1.04482E-01	2.42987E-01	2.23668E-01	2.06757E-01	1.92723E-01	1.82352E-01	1.73385E-01	1.66872E-01
2	1.03653E-01	2.41675E-01	2.23075E-01	2.06762E-01	1.93218E-01	1.83315E-01	1.74576E-01	1.68223E-01
3	1.02522E-01	2.39513E-01	2.21491E-01	2.05704E-01	1.92671E-01	1.82966E-01	1.74449E-01	1.68343E-01
4	1.03260E-01	2.40842E-01	2.22352E-01	2.06157E-01	1.92755E-01	1.82822E-01	1.74140E-01	1.67879E-01







2	10001 00004
3	
4	50000 60002 110000 120005 170000
5	140005 240003 250005 260001 280003 320000
6	50100
7	50922351
8	50922381
9	5080004
10	50400000
11	5010001
12	F 400
13	33922351
14	33922381
15	3380004
16	33400000
17	3310001
18	3350100
19	25922351
20	25922381
21	2580004
22	25400000
23	2510001
24	2550100
25	42922351
26	42922381
27	4280004
28	42400000
29	4210001
30	4250100
31	

\*\*\*\*\* END OF INPUT LISTING \*\*\*\*\*

14 ARRAY 12 ENTRIES READ  
07

MSCM	NUMBER OF EXTRA CROSS SECTIONS	0
MNT	NUMBER OF NUCLIDES FROM MASTER LIBRARY	0
PWT	NUMBER OF NUCLIDES FROM X-SECT LIBRARY (LOG 2)	32
NXT	NUMBER OF NUCLIDES FROM X-SECT LIBRARY (LOG 3)	6
MCR	ANISN/DOT/MORSE OUTPUT TRIGGER	0
M/J	TOTAL CROSS SECTION POSITION	1
MS	WITHIN-GROUP SCATTERING CROSS SECTION POSITION	4
IRCS	NUMBER OF RESONANCE CALCULATIONS	0
IMM	TABLE LENGTH FOR CROSS SECTIONS	126
IPM	IS AN OLD ANISN LIBRARY MOUNTED ? (071 NO/YES)	0
IPP	OUTPUT OPTION TRIGGER	-1
IFG	PRINT CONTROL - ANISN OUTPUT	0

OTHER STORAGE ALLOCATED FOR THIS CASE IS 33000 WORDS

24 ARRAY 38 ENTRIES READ  
07

GENERAL INFORMATION CONCERNING CROSS SECTION LIBRARY

TAPE IDENTIFICATION NUMBER	162
NUMBER OF NUCLIDES ON TAPE	6
NUMBER OF NEUTRON ENERGY GROUPS	123
FIRST THERMAL NEUTRON ENERGY GROUP	94
NUMBER OF GAMMA ENERGY GROUPS	0

WORK TAPE 327

THE TITLE OF THE PARENT CASE IS AS FOLLOWS  
 XSDRN WEIGHTED TAPE--PARENT CASE ENTITLED-- [E25NXB1] EXXON 15X15 PWR, 2.5% U235  
 , 900 PPM NAT.BORON

- WTD. TAPE 162

0 XSDRN WEIGHTED TAPE--PARENT CASE ENTITLED-- [E42NXB1] EXXON 15X15 PWR, 4.2% U235  
 , 2300 PPM NAT.BORON

0 NUCLIDES FROM WORK TAPE

1	HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	10001
2	OXYGEN	THERMAL TEMPERATURE= 294.6 K	80004
3	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	50922351
4	URANIUM-238P	THERMAL TEMPERATURE = 294.6 K	50922381
5	HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	5010001
6	BORON NATURAL		50000
7	BORON-10		50100
8	BORON-10		5050100
9	CARBON NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 509.26 K	60002
10	OXYGEN	THERMAL TEMPERATURE= 294.6 K	5090004
11	SODIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 293.6 K	110000

NITAWL VERS. 1.2 90/01/03. 02:40:49. PAGE 4

12	MAGNESIUM	THERMAL TEMP = 900.0 K	120005
13	ALUMINIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	130000
14	SILICON	THERMAL TEMP = 900.0 K	140005
15	CHROMIUM	THERMAL TEMP=294.6	240003
16	MANGANESE	THERMAL TEMP = 900.0 K	210005
17	IRON	THERMAL TEMP=294.6	210001
18	NICKEL	THERMAL TEMP=294.6	280003
19	ZIRCONIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	5040000
20	LEAD NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 293.6 K	620000
21	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	33422351
22	URANIUM-238P	THERMAL TEMPERATURE = 294.6 K	33422381
23	HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	3310001
24	BORON-10		3350100
25	OXYGEN	THERMAL TEMPERATURE= 294.6 K	3390004
26	ZIRCONIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	3340000
27	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	25922351
28	URANIUM-238P	THERMAL TEMPERATURE = 294.6 K	25922381
29	HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	2510001
30	BORON-10		2550100
31	OXYGEN	THERMAL TEMPERATURE= 294.6 K	2590004
32	ZIRCONIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	2540000

0 NUCLIDES FROM WTD. TAPE

33	URANIUM-235	THERMAL TEMPERATURE = 294.6 K	42922351
34	URANIUM-238P	THERMAL TEMPERATURE = 294.6 K	42922381
35	HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	4210001
36	BORON-10		4250100
37	OXYGEN	THERMAL TEMPERATURE= 294.6 K	4290004
38	ZIRCONIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	4240000

TIME OF DAY 02:40:51.

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1 THIS XSDRN WORKING TAPE WAS CREATED 90/01/03  
 THE TITLE OF THE PARENT CASE IS AS FOLLOWS  
 XSDRN WEIGHTED TAPE--PARENT CASE ENTITLED-- [E42NXB1] EXXON 15X15 PWR, 4.2% U235  
 , 2300 PPM NAT.BORON

2753

TAPE ID	489	NUMBER OF NUCLIDES	38
NUMBER OF NEUTRON GROUPS	123	NUMBER OF GAMMA GROUPS	0

TABLE OF CONTENTS

HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	ID	10001
OXYGEN	THERMAL TEMPERATURE= 294.6 K	ID	80004
URANIUM-235	THERMAL TEMPERATURE = 294.6 K	ID	50922351
URANIUM-238R	THERMAL TEMPERATURE = 294.6 K	ID	50922381
HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	ID	5010001
BORON NATURAL		ID	50000
BORON-10		ID	50100
BORON-10		ID	5050100
CARBON NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 589.26 K	ID	60002
OXYGEN	THERMAL TEMPERATURE= 294.6 K	ID	5080004
SODIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 293.6 K	ID	110000
MAGNESIUM	THERMAL TEMP = 900.0 K	ID	120005
ALUMINIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	ID	130000
SILICON	THERMAL TEMP = 900.0 K	ID	140005
CHROMIUM	THERMAL TEMP=294.6	ID	243003
MANGANESE	THERMAL TEMP = 900.0 K	ID	250005
IRON	THERMAL TEMP=294.6	ID	260001
NICKEL	THERMAL TEMP=294.6	ID	260003
ZIRCONIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	ID	50400000
LEAD NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 293.6 K	ID	8200.0
URANIUM-235	THERMAL TEMPERATURE = 294.6 K	ID	33922351
URANIUM-238R	THERMAL TEMPERATURE = 294.6 K	ID	33922381
HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	ID	3510001
BORON-10		ID	3750100
OXYGEN	THERMAL TEMPERATURE= 294.6 K	ID	3750004
ZIRCONIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	ID	30400500
URANIUM-235	THERMAL TEMPERATURE = 294.6 K	ID	25922351
URANIUM-238R	THERMAL TEMPERATURE = 294.6 K	ID	25922381
HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	ID	2510001
BORON-10		ID	2550100
OXYGEN	THERMAL TEMPERATURE= 294.6 K	ID	2580004
ZIRCONIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	ID	25400000
URANIUM-235	THERMAL TEMPERATURE = 294.6 K	ID	41922351
URANIUM-238R	THERMAL TEMPERATURE = 294.6 K	ID	41922381
HYDROGEN--THERMOS ID=1803(X-640)	THERMAL TEMPERATURE= 294.6 K	ID	4110001
BORON-10		ID	4250100
OXYGEN	THERMAL TEMPERATURE= 294.6 K	ID	4280004
ZIRCONIUM NATURAL	BROWN - ST. JOHN KERNEL TEMP. = 627.13 K	ID	42400000

--EOR--

1 MESS POWER COMPUTING/990 - NOS 2.7.1.10. NOS 2.7.1 ST=MAC. 90/01/03. 02.42.14.

02.37.00.E42NXBI,PO,T200. HENRY TRAN  
 02.37.00.USER,VX99SN,,NC.  
 02.37.00.ABSC, O.  
 02.37.00. YOUR PASSWORD EXPIRES AT 00.00.00 ON 90/02/08.  
 02.37.00.CHARGE,N973301,VSC.  
 02.37.01. CHARGE = N973301, PROJECT = VSC.  
 02.37.01.Z111201.  
 02.37.02.PROC1. SYSTEM PROLOGUE  
 02.37.02.COMMENT. SYSTEM PROLOG  
 02.37.02.NEWS(A).  
 02.37.03.CHEKEXP.  
 02.37.04. INQUIRY COMPLETE.  
 02.37.04.REVERT.  
 02.37.04.TITLE([E42NXBI] EXXON 15X15 PWR, 4.2% U235, ~~2500~~ PPM NAT.BORON)  
 02.37.04.LABEL,TAPEA,D=GE,L=EXSECT,VSN=007421.  
 02.39.37.NT101, ASSIGNED TO TAPEA, VSN=007421.

*2753 m/c*





E42KEB1 MEVT MABSEY JOHN 001 90/01/03, 03.30.14, MID = MAC = NS2

[E42KEB1] EXXON 15X15 PWR, 4.2XU235, ~~2300~~ PPM NAT.BORON

--EOP--

*2753*

KK	KK	EEEEEEEEEEEE	NN	NN	0000000000
KK	KK	EEEEEEEEEEEE	NNN	NN	000000000000
KK	KK	EE	NNNN	NN	00 00
KK	KK	EE	NN NN	NN	00 00
KK	KK	EE	NN NN	NN	00 00
KKKKKKK		EEEEEEEEE	NN NN	NN	00 00
KKKKKKK		EEEEEEEEE	NN NN	NN	00 00
KK	KK	EE	NN NN	NN	00 00
KK	KK	EE	NN NN	NN	00 00
KK	KK	EE	NN	NNNN	00 00
KK	KK	EEEEEEEEEEEE	NN	NNN	000000000000
KK	KK	EEEEEEEEEEEE	NN	NN	0000000000

9999999999	00000000	//	00000000	//	00000000	3333333333
9999999999	00000000	//	00000000	//	00000000	3333333333
99	99	00	00	//	00	00
99	99	00	00	//	00	00
9999999999	00	00	00	//	00	00
9999999999	00	00	00	//	00	00
99	00	00	00	//	00	00
99	00	00	00	//	00	00
99	00	00	00	//	00	00
9999999999	00000000	//	00000000	//	00000000	3333333333
9999999999	00000000	//	00000000	//	00000000	3333333333

00000000	3333333333	3333333333	//	3333333333	00000000
00000000	3333333333	3333333333	//	3333333333	00000000
00	00	33	33	33	00
00	00	33	33	33	00
00	00	33	33	33	00
00	00	333	333	333	00
00	00	333	333	333	00
00	00	33	33	33	00
00	00	33	33	33	00
00	00	33	33	33	00
00000000	3333333333	3333333333	//	3333333333	00000000
00000000	3333333333	3333333333	//	3333333333	00000000

FOLLOWING IS A CARD IMAGE LISTING OF THE INPUT DATA COLUMN NUMBER

CARD NUMBER	11111111112222222222333333333344444444445555555555666666666677777777778
	1234567890123456789012345678901234567890123456789012345678901234567890
1	[E42KEB1] EXXON 15X15 PWR, 4.2XU235, <del>2300</del> PPM NAT.BORON
2	99.0 73 300 3 123 75 18 5 22 6
3	1 1 1 1 -18 1 0 2000 00 1
4	0 0 0 0 0 00 0 0

*2753*





```

120 SECTOR 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 1 -1 0 0
121 SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 -1
122 SECTOR 0 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 1 -1 0 0
123 SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 1 0 0 -1 0
124 SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 0 -1 0 0 1 1 -1 0 0 0
125 SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 1 -1 0 0
126 SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 0 -1 0 0 1 0 0 1 -1 0
127 SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 1 -1 0 0
128 SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -1 1 0 1 -1 0 0
129 SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 -1 0
130 SECTOR 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
131 BLOCK 3 1 1
132 MEDIA 1, 5, 3, 4, 3, 2, 3, 2, 3,
133 2, 1, 2, 3, 2, 3, 3, 2, 1000
134 SURFACES 1, 2, 7, 4, 5, 6, 7, 8, 16, 19,
135 20, 21, 30, 31, 32, 33, 34, 36
136 SECTOR -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
137 SECTOR 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
138 SECTOR 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
139 SECTOR 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
140 SECTOR 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
141 SECTOR 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0
142 SECTOR 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0
143 SECTOR 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 0 0 1
144 SECTOR 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 1 -1
145 SECTOR 0 0 0 0 0 0 0 0 0 1 0 0 0 0 1 0 0 -1 0 -1
146 SECTOR 0 0 0 0 0 0 0 0 -1 0 0 1 1 -1 0 0 0 0
147 SECTOR 0 0 0 0 0 0 0 0 0 -1 1 0 0 1 -1 0 0 0
148 SECTOR 0 0 0 0 0 0 0 0 -1 0 0 1 0 1 1 -1 0 0
149 SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 -1 0 0 0 0 -1
150 SECTOR 0 0 0 0 0 0 0 0 0 0 -1 1 0 1 -1 0 0 0
151 SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 -1 -1
152 SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 -1 0 0
153 SECTOR 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 1 -1 0 0 0

```

KENDIV VER 1.2A (21/04/87) 80701-90. 03.01.88. PAGE 8

FOLLOWING IS A CAPD IMAGE LISTING OF THE INPUT DATA COLUMN NUMBER

CARD NUMBER 11111111122222222223333333333444444444555555555566666666677777777778  
12345678901234567890123456789012345678901234567890123456789012345678901234567890

```

154 SECTOR 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
155 36 QUADRATIC SURFACES IN THE SYSTEM
156 1.0YS0 1.0XS0 -11245.542 $
157 1.0YS0 1.0XS0 -10713.285 $
158 1.0YS0 1.0XS0 -8713.2890 $
159 1.0YS0 1.0XS0 -8595.1441 $
160 1.0YS0 1.0XS0 -6814.5025 $
161 1.0YS0 1.0XS0 -6401.6001 $
162 1.0YS0 1.0XS0 -6199.9276 $
163 1.0YS0 1.0XS0 -5903.6172 $
164 1.0Y -70.1040 $
165 1.0Y -69.5960 $
166 1.0Y -68.8975 $
167 1.0Y -47.9425 $
168 1.0Y -47.2440 $
169 1.0Y -46.2280 $
170 1.0Y -45.5295 $
171 1.0Y -24.5745 $
172 1.0Y -23.8760 $
173 1.0Y -22.8600 $
174 1.0Y -22.1615 $
175 1.0Y -1.2075 $

```



3 140005 1.40000E-04  
 4 820000 3.29600E-02  
 5 10901 2.77000E-02  
 5 50000 1.46000E-03  
 5 80004 3.71000E-02  
 5 110000 2.60000E-04  
 5 120005 2.00000E-04  
 5 130000 8.47000E-03  
 5 140005 7.67000E-04  
 5 260001 4.89000E-05

CROSS SECTIONS READ FROM TAPE

NUCLIDE = 10001 HYDROGEN--THERMOS ID=1803(LX-640) THERMAL TEMPERATURE= 294.6 K  
 NUCLIDE = 80004 OXYGEN THERMAL TEMPERATURE= 294.6 K  
 NUCLIDE = 50000 BORON NATURAL  
 NUCLIDE = 50100 BORON-10  
 NUCLIDE = 60002 CARBON NATURAL BROWN - ST. JOHN KERNEL TEMP. = 509.26 K  
 NUCLIDE = 110000 SODIUM NATURAL BROWN - ST. JOHN KERNEL TEMP. = 293.6 K  
 NUCLIDE = 120005 MAGNESIUM THERMAL TEMP = 900.0 K  
 NUCLIDE = 130000 ALUMINUM NATURAL BROWN - ST. JOHN KERNEL TEMP. = 627.13 K  
 NUCLIDE = 140005 SILICON THERMAL TEMP = 900.0 K  
 NUCLIDE = 260001 IRON THERMAL TEMP=294.6  
 NUCLIDE = 820000 LEAD NATURAL BROWN - ST. JOHN KERNEL TEMP. = 293.6 K  
 NUCLIDE = 42922351 URANIUM-235 THERMAL TEMPERATURE = 294.6 K  
 NUCLIDE = 42922381 URANIUM-238 THERMAL TEMPERATURE = 294.6 K  
 NUCLIDE = 4010001 HYDROGEN--THERMOS ID=1803(LX-640) THERMAL TEMPERATURE= 294.6 K  
 NUCLIDE = 4250100 BORON-10  
 NUCLIDE = 4280004 OXYGEN THERMAL TEMPERATURE= 294.6 K  
 NUCLIDE = 42900000 ZIRCONIUM NATURAL BROWN - ST. JOHN KERNEL TEMP. = 627.13 K

KENDIV VER 1.2A (21/09/87) 90/01/03, 03.01.30, PAGE 9

Q[E429E61] EXXON 15X15 PWR, 4.21U235, <sup>nat 11-</sup> 2300 PPM NAT.BORON

GEOMETRY DESCRIPTION  
 REGION

BOX TYPE 1  
 REGION

0 1 GENERAL 1	+X = 0.	-X = 0.	+Y = 0.	-Y = 0.	+Z = 0.	-Z = 0.
0 2 GENERAL 2	+X = 0.	-X = 0.	+Y = 0.	-Y = 0.	+Z = 0.	-Z = 0.
0 3 GENERAL 3	+X = 0.	-X = 0.	+Y = 0.	-Y = 0.	+Z = 0.	-Z = 0.
0 4 GENERAL 4	+X = 0.	-X = 0.	+Y = 0.	-Y = 0.	+Z = 0.	-Z = 0.
0 5 GENERAL 5	+X = 0.	-X = 0.	+Y = 0.	-Y = 0.	+Z = 0.	-Z = 0.
0 6 CUBOID 6	+X = 1.0605E+02	-X = -1.0000E-04	+Y = 1.0605E+02	-Y = -1.0000E-04	+Z = 5.0000E+01	-Z = -1.0000E-04

KENDIV VER 1.2A (21/09/87) 90/01/03, 03.01.30, PAGE 10

Q[E429E61] EXXON 15X15 PWR, 4.21U235, <sup>nat 11-</sup> 2300 PPM NAT.BORON

WEIGHTING FUNCTION

BOX TYPE	1	GROUP	WTLOW	WT AVG	WT HI
0 REGION 1	DEFINED BY GEOMETRY CARD 1	1	.167	.500	1.500
		GROUPS 2 TO 123 SAME AS ABOVE			
0 REGION 2	DEFINED BY GEOMETRY CARD 2	1	.167	.500	1.500
		GROUPS 2 TO 123 SAME AS ABOVE			
0 REGION 3	DEFINED BY GEOMETRY CARD 3	1	.167	.500	1.500
		GROUPS 2 TO 123 SAME AS ABOVE			
0 REGION 4	DEFINED BY GEOMETRY CARD 4	1	.167	.500	1.500
		GROUPS 2 TO 123 SAME AS ABOVE			
0 REGION 5	DEFINED BY GEOMETRY CARD 5	1	.167	.500	1.500
		GROUPS 2 TO 123 SAME AS ABOVE			

0 REGION 6 DEFINED BY GEOMETRY CARD  
 1 .167 .500 1.500  
 GROUPS 2 TO 123 SAME AS ABOVE

1 KENOIV VER 1.2A (21/09/87) 90/01/03. 03.31.30. PAGE 11

0 2 REALIZE GEOMET

DEAR IT

WITH THE DEEPEST REGRET I MUST INFORM YOU THAT A DREADFUL MISFORTUNE HAS OCCURRED.  
 YOU HAVE FAILED TO MENTION YOUR SEX AND MARITAL STATUS.

RESPECTFULLY YOURS,  
 GEOM

```

X ZONE BDRY 0.           ,   .10605E+03
Y ZONE BDRY 0.           ,   .20405E+03
Z ZONE BDRY 0.           ,   .50000E+02
OZONE   1   1   1
X BLOC BDRY 0.           ,   .23369E+02,   .46736E+02,   .10605E+03
Y BLOC BDRY 0.           ,   .10605E+03
Z BLOC BDRY 0.           ,   .50000E+02
OBLOCK  1   1   1
MEDIA          3,    5,    7,    4,    3,    2,    3,    2,    3,    2,
              1,    2,    3,    1,    3,    2,    3,    2,    2,    2,    1,    2,
              3,    2,    2,    2,    1,    2,    3, 1000
SURFACES          1,    2,    3,    4,    5,    6,    7,    8,    9,   10,
              11,   12,   13,   14,   15,   16,   17,   18,   19,   20,   21,   22,
              23,   24,   25
SECTOR -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SECTOR 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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OBLOCK  2   1   1
MEDIA          3,    5,    3,    4,    3,    2,    3,    2,    3,    2,
              2,    2,    3,    1,    3,    2,    3,    2,    2,    2,    1,    2,
SURFACES          1,    2,    3,    4,    5,    6,    7,    8,   14,   15,
    
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.10000E+01Y    -.45530E+02    1  
 .10000E+01Y    -.24575E+02    1  
 .10000E+01Y    -.23876E+02    1  
 .10000E+01Y    -.22860E+02    1  
 .10000E+01Y    -.22162E+02    1  
 .10000E+01Y    -.12045E+01    1  
 .10000E+01Y    -.50800E+00    1  
 .10000E+01X    -.50800E+00    1  
 .10000E+01X    -.12045E+01    1  
 .10000E+01X    -.22162E+02    1  
 .10000E+01X    -.22860E+02    1  
 .10000E+01Y    -.23876E+02    1  
 .10000E+01X    -.24575E+02    1  
 .10000E+01Y    -.45530E+02    1  
 .10000E+01X    -.46228E+02    1  
 .10000E+01X    -.47244E+02    1  
 .10000E+01X    -.47943E+02    1  
 .10000E+01X    -.68898E+02    1  
 .10000E+01X    -.68596E+02    1  
 .10000E+01X    -.70104E+02    1  
 .10000E+01Y    -.46738E+02    1  
 .10000E+01Y    -.23368E+02    1

.....  
 FINAL ALLOCATION OF MEMORY HAS BEEN COMPLETED  
 .....  
 REQUIRED SCM FIELD LENGTH 117604 (00335704B)  
 REQUIRED LCM FIELD LENGTH 36900 (00110044B)  
 REQUIRED RMS FIELD LENGTH 0 (00000000B)  
 REQUIRED SCM BLANK COMMON 68676 (00206414E)  
 REQUIRED LCM BLANK COMMON 36900 (00110044B)  
 REQUIRED RMS BLANK COMMON 0 (00000000B)  
 REMAINING SCM AVAILABLE 9276 (00022074E)  
 REMAINING LCM AVAILABLE 63100 (00173174E)  
 .....

LOCATION OF RELOCATABLE ARRAYS

ARRAY	MAT	LOCATION
FSP/MUBAR	1	SCM
FSP/MUBAR	2	SCM
FSP/MUBAR	3	SCM
FSP/MUBAR	4	LCM
FSP/MUBAR	5	LCM
WGT		SCM
FMABS		SCM
FMFIS		SCM

1  
 0[E42KEB] EXXON 15X15 PWR, 4.2XU235, 2300 PPM NAT.BORON  
 0 VOLUMES  
 0 BOX TYPE 1

REGION DEFINED BY GEOMETRY CARD		VOLUME =		CM..3	CUMULATIVE VOLUME =		CM..3
REGION DEFINED BY GEOMETRY CARD	1	VOLUME =	0.	CM..3	CUMULATIVE VOLUME =	0.	CM..3
REGION DEFINED BY GEOMETRY CARD	2	VOLUME =	0.	CM..3	CUMULATIVE VOLUME =	0.	CM..3
REGION DEFINED BY GEOMETRY CARD	3	VOLUME =	0.	CM..3	CUMULATIVE VOLUME =	0.	CM..3
REGION DEFINED BY GEOMETRY CARD	4	VOLUME =	0.	CM..3	CUMULATIVE VOLUME =	0.	CM..3



46	9.01275E-01	1.07955E+01	9.18010E-01	4.10457E-03	0.
47	9.21751E-01	1.10238E+01	9.18101E-01	4.50185E-03	0.
48	8.93824E-01	1.12550E+01	9.17573E-01	4.43441E-03	0.
49	9.43036E-01	1.14890E+01	9.18115E-01	4.07273E-03	0.
50	9.09215E-01	1.17168E+01	9.17930E-01	4.29467E-03	0.
51	9.52076E-01	1.1958E+01	9.18626E-01	4.25279E-03	0.
52	9.15943E-01	1.21630E+01	9.18573E-01	4.16819E-03	0.
53	9.84964E-01	1.24163E+01	9.19875E-01	4.28802E-03	0.
54	9.00331E-01	1.26527E+01	9.19499E-01	4.22152E-03	0.

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55	9.06004E-01	1.28807E+01	9.20754E-01	4.02704E-03	0.
56	9.56957E-01	1.31148E+01	9.21424E-01	4.29876E-03	0.
57	9.04917E-01	1.33468E+01	9.21124E-01	4.03053E-03	0.
58	9.41475E-01	1.35842E+01	9.21487E-01	4.17017E-03	0.
59	9.29049E-01	1.38223E+01	9.21550E-01	4.09680E-03	0.
60	9.46913E-01	1.40505E+01	9.21967E-01	4.06426E-03	0.
61	9.19629E-01	1.42803E+01	9.21947E-01	3.98023E-03	0.
62	9.05179E-01	1.45189E+01	9.21668E-01	3.92330E-03	0.
63	8.95950E-01	1.47492E+01	9.21246E-01	3.88141E-03	0.
64	9.31128E-01	1.49792E+01	9.21405E-01	3.82162E-03	0.
65	9.37493E-01	1.52147E+01	9.21669E-01	3.76968E-03	0.
66	9.19427E-01	1.54483E+01	9.21634E-01	3.71047E-03	0.
67	9.26373E-01	1.56815E+01	9.21707E-01	3.65367E-03	0.
68	9.17107E-01	1.59153E+01	9.21627E-01	3.59856E-03	0.
69	9.80201E-01	1.61482E+01	9.22511E-01	3.65063E-03	0.
70	9.41705E-01	1.63827E+01	9.23087E-01	3.64244E-03	0.
71	9.42003E-01	1.66200E+01	9.23362E-01	3.59972E-03	0.
72	9.04729E-01	1.68495E+01	9.23095E-01	3.55789E-03	0.
73	8.97274E-01	1.70820E+01	9.23732E-01	3.51630E-03	0.

OTHER MATRIX EIGENVALUE IS THE LARGEST EIGENVALUE OF THE MATRIX OF FISSION PROBABILITIES BY UNIT.  
 THERE ARE NRXMAX, NBYMAX, NDBMAX UNITS IN AN ARRAY.

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[E42KEB] EXXON 15X15 PWR, 4.2XU235, 2000 PPM NAT.BORON  
 OLIFETIME = 1.22676E+05 + OR - 1.67928E+07  
 % OF INITIAL

01	ATIONS	AVERAGE	67 PER CENT	95 PER CENT	99 PER CENT	NUMBER OF
SKIPPED	K-EFFECTIVE	DEVIATION	CONFIDENCE INTERVAL	CONFIDENCE INTERVAL	CONFIDENCE INTERVAL	HISTORIES
0	3	.92284 + OR - .00358	.915 TO .92641	.91569 TO .92499	.91211 TO .93356	21000
0	4	.92319 + OR - .00361	.91958 TO .92680	.91597 TO .93041	.91236 TO .93402	20700
0	5	.91368 + OR - .00363	.92005 TO .92731	.91642 TO .93094	.912 TO .93457	20400
0	6	.92443 + OR - .00360	.92083 TO .92804	.91722 TO .93164	.91362 TO .93524	20100
0	7	.92426 + OR - .00365	.92060 TO .92791	.91695 TO .93156	.91329 TO .93522	19800
0	8	.92481 + OR - .00367	.92114 TO .92848	.91747 TO .93215	.91380 TO .93581	19500
0	9	.92426 + OR - .00368	.92058 TO .92794	.91689 TO .93163	.91321 TO .93531	19200
0	10	.92399 + OR - .00372	.92016 TO .92761	.91644 TO .93133	.91271 TO .93506	18900
0	11	.92394 + OR - .00378	.92015 TO .92772	.91637 TO .93151	.91259 TO .93529	18600
0	13	.92407 + OR - .00384	.92022 TO .92791	.91638 TO .93175	.91253 TO .93560	18300
0	17	.92738 + OR - .00383	.92356 TO .93121	.91973 TO .93504	.91590 TO .93886	16800
0	22	.92946 + OR - .00389	.92558 TO .93334	.92170 TO .93721	.91782 TO .94109	15300
0	27	.93031 + OR - .00410	.92621 TO .93441	.92212 TO .93851	.91802 TO .94261	13800
0	32	.92929 + OR - .00433	.92496 TO .93362	.92063 TO .93795	.91630 TO .94228	12300
0	37	.92893 + OR - .00470	.92423 TO .93363	.91954 TO .93832	.91484 TO .94302	10800
0	42	.92983 + OR - .00484	.92498 TO .93467	.92014 TO .93952	.91530 TO .94436	9300
0	47	.93075 + OR - .00541	.92533 TO .93616	.91992 TO .94157	.91451 TO .94698	7800
0	52	.93263 + OR - .00623	.92640 TO .93887	.92017 TO .94510	.91394 TO .95133	6300
0	57	.92826 + OR - .00578	.92248 TO .93404	.91670 TO .93981	.91092 TO .94559	4800
0	62	.92854 + OR - .00790	.92063 TO .93644	.91273 TO .94434	.90482 TO .95225	3300
0	67	.93384 + OR - .01349	.92035 TO .94732	.90686 TO .96081	.89338 TO .97430	1800

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[E42KEB] EXXON 15X15 PWR, 4.2XU235, 2000 PPM NAT.BORON

GROUP REGION LEAKAGE ABSORPTIONS FISSIONS WITH 3 GENERATIONS SKIPPED  
 0 1 0. 1.25282E-05 1.35254E-05

0 4	0.	7.95562E-05	9.10481E-05
0 5	0.	2.04727E-04	3.15454E-04
0 6	0.	3.72912E-04	5.61943E-04
0 7	0.	4.83367E-04	9.31153E-04
0 8	0.	7.94664E-04	1.36185E-03
0 9	0.	9.15436E-04	1.50762E-03
0 10	0.	6.38216E-04	1.53809E-03
0 11	0.	9.97590E-04	1.88529E-03
0 12	4.08201E-05	1.27153E-03	2.45354E-03
0 13	0.	1.48085E-03	2.87800E-03
0 14	0.	1.24813E-03	2.77563E-03
0 15	0.	1.12726E-03	3.09097E-03
0 16	0.	1.64254E-03	4.41535E-03
0 17	0.	1.82472E-03	4.79079E-03
0 18	0.	2.02567E-03	5.21424E-03
0 19	0.	2.08778E-03	5.25532E-03
0 20	0.	1.99576E-03	4.90520E-03
0 21	0.	1.73003E-03	4.13218E-03
0 22	0.	1.16903E-03	3.02020E-03
0 23	0.	9.71386E-04	1.88484E-03
0 24	0.	7.08511E-04	1.03994E-03
0 25	0.	5.78605E-04	6.41894E-04
0 26	0.	6.46480E-04	5.90972E-04
0 27	0.	5.17250E-04	4.11054E-04

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[E42KEB] EXXON 15X15 PWR, 4.25U235, 2753 PPM NAT.BORON

GROUP	REGION	LEAKAGE	ABSORPTIONS	FISIONS	WITH 3 GENERATIONS SKIPPED
0 28	0.	5.38281E-04	3.78773E-04		
0 29	0.	6.95883E-04	4.40155E-04		
0 30	0.	7.45346E-04	4.59131E-04		
0 31	0.	6.31250E-04	3.87319E-04		
0 32	4.75901E-05	5.63450E-04	3.52701E-04		
0 33	0.	5.32160E-04	3.35621E-04		
0 34	0.	4.74391E-04	3.07406E-04		
0 35	0.	3.57110E-04	2.35442E-04		
0 36	0.	3.28070E-04	2.19300E-04		
0 37	0.	4.37778E-04	2.93938E-04		
0 38	0.	5.14955E-04	3.45643E-04		
0 39	0.	4.66519E-04	3.08138E-04		
0 40	0.	4.41374E-04	2.81978E-04		
0 41	0.	4.04319E-04	2.48081E-04		
0 42	0.	4.21016E-04	2.50604E-04		
0 43	0.	4.12952E-04	2.37420E-04		
0 44	0.	4.10935E-04	2.26067E-04		
0 45	0.	4.33849E-04	2.28890E-04		
0 46	0.	4.33037E-04	2.22664E-04		
0 47	0.	4.29409E-04	2.14990E-04		
0 48	0.	4.01043E-04	1.93914E-04		
0 49	0.	3.98607E-04	1.88657E-04		
0 50	4.68507E-05	1.00545E-03	4.69395E-04		
0 51	0.	1.02482E-03	4.58641E-04		
0 52	0.	1.04877E-03	4.57808E-04		
0 53	0.	1.08896E-03	4.64701E-04		
0 54	0.	1.08778E-03	4.59809E-04		

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[E42KEB] EXXON 15X15 PWR, 4.25U235, 2753 PPM NAT.BORON

GROUP	REGION	LEAKAGE	ABSORPTIONS	FISIONS	WITH 3 GENERATIONS SKIPPED
0 55	0.	4.64623E-05	1.13717E-03	4.76219E-04	
0 56	0.	1.15843E-03	4.89027E-04		
0 57	0.	1.25963E-03	5.24824E-04		
0 58	4.57519E-05	1.35689E-03	5.48362E-04		

0 60	0.	1.53406E-03	6.37015E-04
0 61	0.	1.62375E-03	7.01647E-04
0 62	0.	1.70787E-03	7.36755E-04
0 63	0.	1.79105E-03	8.10463E-04
0 64	0.	1.71349E-03	8.90144E-04
0 65	0.	1.86415E-03	9.90320E-04
0 66	0.	1.91164E-03	1.12937E-03
0 67	0.	2.15683E-03	1.27714E-03
0 68	9.19258E-05	2.62387E-03	1.37417E-03
0 69	0.	2.92425E-03	1.48162E-03
0 70	0.	3.99755E-03	1.92616E-03
0 71	0.	3.29991E-03	2.31530E-03
0 72	0.	3.37303E-03	2.13009E-03
0 73	0.	6.54326E-03	2.50181E-03
0 74	0.	4.68847E-03	4.00094E-03
0 75	0.	5.19742E-03	2.96359E-03
0 76	0.	4.49100E-03	3.49443E-03
0 77	0.	7.72250E-03	2.84106E-03
0 78	0.	5.41880E-03	3.30657E-03
0 79	0.	7.32457E-03	3.13695E-03
0 80	0.	5.37150E-03	8.25656E-03
0 81	4.39882E-05	6.62411E-03	5.22521E-03

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0[E42KEB] EXXON 15X15 PWR, 4.28U235, <sup>2753</sup>PPM NAT.BORON

GROUP	REGION	LEAKAGE	ABSORPTIONS	FISSIONS
0 82	0.	1.33021E-02	5.90228E-07	
0 83	3.71004E-05	5.81883E-03	6.41437E-03	
0 84	7.84433E-05	1.93186E-02	6.95140E-03	
0 85	0.	4.42367E-02	4.49652E-03	
0 86	0.	7.69478E-03	6.26557E-03	
0 87	0.	9.17285E-03	1.30957E-02	
0 88	0.	2.40844E-02	1.35836E-03	
0 89	2.96966E-05	1.38240E-02	2.99377E-03	
0 90	0.	4.17457E-03	5.72179E-04	
0 91	0.	4.85707E-02	3.63991E-07	
0 92	0.	3.85865E-02	1.60914E-03	
0 93	0.	4.44544E-03	1.66556E-03	
0 94	0.	1.48090E-02	6.36851E-04	
0 95	0.	1.56003E-03	6.94579E-04	
0 96	0.	1.63234E-03	7.54337E-04	
0 97	0.	2.23340E-03	1.17380E-03	
0 98	0.	4.35488E-03	4.09040E-03	
0 99	0.	4.60063E-03	5.32411E-03	
0100	0.	4.14923E-03	3.96437E-03	
0101	0.	4.03710E-03	3.47210E-03	
0102	0.	5.95459E-03	5.13149E-03	
0103	0.	6.59930E-03	6.02588E-03	
0104	0.	9.19000E-03	8.86992E-03	
0105	0.	1.36975E-02	1.44271E-02	
0106	0.	1.10656E-02	1.29051E-02	
0107	0.	1.43343E-02	1.66300E-02	
0108	0.	1.81408E-02	1.93859E-02	

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0[E42KEB] EXXON 15X15 PWR, 4.28U235, <sup>2753</sup>PPM NAT.BORON

GROUP	REGION	LEAKAGE	ABSORPTIONS	FISSIONS
0109	0.	9.42668E-03	9.70728E-03	
0110	0.	1.16557E-02	1.19986E-02	
0111	0.	1.59913E-02	1.64562E-02	
0112	0.	2.17423E-02	2.24562E-02	
0113	0.	3.21061E-02	3.26538E-02	
0114	0.	4.96598E-02	5.04749E-02	
0115	0.	3.51007E-02	3.59257E-02	

WITH 3 GENERATIONS SKIPPED

0117	0.	4.3030E-02	5.44392E-02
0118	0.	6.83793E-02	6.87700E-02
0119	0.	8.07404E-02	8.06920E-02
0120	0.	9.19095E-02	9.09242E-02
0121	0.	4.75622E-02	4.41041E-02
0122	0.	4.49704E-02	4.26661E-02
0123	0.	3.04530E-02	3.52681E-02
TOTAL	5.34625E-04	9.97890E-01	9.22839E-01

ELAPSED TIME 17.00200MINUTES

1  
 D[E42HZD1] EXXON 15X15 PWR, 4.25U235, <sup>2.63</sup> ~~4.00~~ PPM NAT.BORON  
 0... FISSION DENSITIES ...

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ORIG TYPE	REGION	FISSION DENSITY	PERCENT DEVIATION	TOTAL FISSIONS
1	1	9.228E-01	.39	9.228E-01
	2	0.	0.00	0.
	3	0.	0.00	0.
	4	0.	0.00	0.
	5	0.	0.00	0.
	6	0.	0.00	0.

0..... WARNING ..... WARNING .....

THE FISSION DENSITY AND FLUX WERE SO DETERMINED USING ARBITRARY VOLUMES (LISTED UNDER - TOTAL VOLUMES -) IN THE REGIONS DESCRIBED BY GENERALIZED GEOM. THEY MUST BE MULTIPLIED BY THE TRUE VOLUME OVER THE ARBITRARY VOLUME TO OBTAIN THE CORRECT VALUES.

1  
 D[E42HZD1] EXXON 15X15 PWR, 4.25U235, <sup>2.753</sup> ~~4.00~~ PPM NAT.BORON  
 0... FISSION DENSITIES ...

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ORIG TYPE	REGION 1		REGION 2		REGION 3		REGION 4		REGION 5		REGION 6	
	FLUX	PERCENT DEVIATION	FLUX	PERCENT DEVIATION	FLUX	PERCENT DEVIATION	FLUX	PERCENT DEVIATION	FLUX	PERCENT DEVIATION	FLUX	PERCENT DEVIATION
1	3.968E-04	100.00	1.925E-05	100.00	0.	0.00	0.	0.00	0.	0.00	0.	0.00
2	1.277E-03	83.98	7.695E-04	86.14	4.111E-04	82.02	0.	0.00	0.	0.00	2.110E-09	100.00
3	1.987E-03	54.56	4.855E-04	70.44	1.315E-04	100.00	0.	0.00	0.	0.00	1.106E-06	59.89
4	2.304E-03	42.57	1.490E-03	60.69	4.558E-04	53.50	0.	0.00	0.	0.00	3.850E-09	100.00
5	1.142E-02	28.18	9.657E-04	41.88	6.359E-04	46.41	0.	0.00	0.	0.00	2.567E-08	54.96
6	1.961E-02	17.95	2.464E-03	27.26	1.167E-03	29.32	0.	0.00	0.	0.00	3.640E-09	34.19
7	3.237E-02	15.00	5.664E-03	27.93	3.046E-03	26.10	1.172E-08	100.00	0.	0.00	6.796E-09	34.54
8	5.848E-02	5.05	6.417E-03	17.93	4.230E-03	14.50	3.169E-04	100.00	0.	0.00	1.158E-07	19.71
9	9.205E-02	9.91	1.315E-02	16.00	6.803E-03	14.50	0.	0.00	0.	0.00	1.767E-07	26.52
10	1.019E-01	7.91	1.208E-02	15.06	6.226E-03	14.96	2.111E-04	100.00	0.	0.00	1.544E-07	20.14
11	1.339E-01	6.64	1.888E-02	12.15	1.117E-02	11.07	6.830E-05	100.00	0.	0.00	3.325E-07	25.94
12	1.945E-01	5.49	3.099E-02	9.90	1.530E-02	8.94	5.119E-04	100.00	7.921E-10	100.00	3.285E-07	14.85
13	1.953E-01	4.96	3.057E-02	11.63	1.713E-02	11.10	3.124E-03	51.36	0.	0.00	4.282E-07	12.64
14	2.277E-01	4.79	3.111E-02	11.96	1.752E-02	9.21	0.	0.00	0.	0.00	4.651E-07	11.85
15	2.982E-01	4.32	3.255E-02	7.55	1.870E-02	7.45	6.926E-04	100.00	1.001E-09	100.00	4.740E-07	11.87
16	5.736E-01	3.86	4.513E-02	6.62	2.683E-02	7.19	5.049E-04	100.00	6.061E-10	100.00	8.433E-07	10.20
17	3.967E-01	3.78	5.124E-02	6.81	3.069E-02	6.66	1.227E-03	78.73	2.944E-11	100.00	9.188E-07	8.61
18	4.358E-01	3.67	6.102E-02	5.72	3.473E-02	5.39	2.161E-03	79.72	7.242E-10	72.76	9.860E-07	9.70
19	4.452E-01	3.50	7.102E-02	5.84	4.032E-02	5.60	3.976E-03	56.67	1.452E-09	55.79	1.085E-06	9.76
20	4.237E-01	3.89	5.846E-02	5.52	3.197E-02	5.30	1.892E-03	59.79	6.667E-10	62.73	9.713E-07	7.76
21	3.896E-01	3.57	5.153E-02	6.62	2.813E-02	7.42	0.	0.00	3.320E-10	100.00	7.805E-07	11.06
22	4.320E-01	3.10	5.635E-02	6.15	3.970E-02	6.34	7.350E-04	94.32	7.197E-10	82.59	1.094E-06	10.50
23	4.072E-01	3.04	5.570E-02	5.89	3.188E-02	7.03	2.802E-03	60.45	2.254E-09	62.53	9.600E-07	15.90
24	4.359E-01	2.84	5.807E-02	6.35	3.583E-02	6.11	1.850E-03	79.77	6.456E-11	100.00	8.868E-07	7.71
25	3.912E-01	2.74	5.334E-02	5.49	3.368E-02	5.99	1.451E-03	70.75	1.312E-09	98.23	8.584E-07	9.54
26	4.436E-01	2.62	6.261E-02	4.95	3.855E-02	6.52	1.578E-03	57.83	1.590E-09	66.53	1.212E-06	13.08
27	3.401E-01	2.78	4.79E-02	5.35	3.192E-02	8.62	7.509E-04	89.05	4.758E-11	100.00	1.057E-06	19.82
28	3.445E-01	3.12	4.461E-02	5.31	2.783E-02	7.40	3.161E-03	57.33	1.656E-09	59.30	7.347E-07	10.13

30	4.275E-01	2.89	5.153E-02	4.54	4.182E-02	4.25	1.00E-03	73.98	4.945E-10	52.60	1.056E-06	7.68
31	4.396E-01	2.80	5.930E-02	4.66	3.961E-02	4.66	5.526E-03	65.98	6.511E-10	70.64	9.848E-07	8.62
32	3.661E-01	2.62	5.059E-02	5.30	3.847E-02	7.07	6.997E-03	59.44	1.260E-09	69.75	1.013E-06	10.45
33	3.800E-01	2.75	5.235E-02	5.16	3.743E-02	7.30	4.381E-03	66.60	9.472E-10	76.71	1.033E-06	11.15
34	3.503E-01	2.77	4.806E-02	4.73	2.949E-02	5.81	2.918E-03	66.08	1.859E-09	68.09	6.563E-07	10.12
35	2.605E-01	2.51	3.570E-02	4.78	2.236E-02	6.46	3.799E-03	46.51	1.438E-09	47.17	6.975E-07	12.59
36	2.584E-01	2.71	5.308E-02	4.93	2.221E-02	6.90	1.516E-03	57.15	1.366E-09	40.08	4.964E-07	12.20
37	3.174E-01	2.77	4.584E-02	5.80	3.126E-02	7.99	8.086E-03	42.43	1.584E-09	41.59	8.549E-07	10.94
38	3.605E-01	2.38	5.000E-02	4.96	3.227E-02	7.00	4.554E-03	49.94	5.087E-09	46.24	7.863E-07	7.99
39	3.086E-01	2.57	4.034E-02	5.02	2.763E-02	7.89	4.502E-03	47.24	1.604E-09	53.84	6.801E-07	10.51
40	2.632E-01	2.62	3.895E-02	5.74	2.502E-02	7.48	3.575E-03	45.17	1.503E-09	66.79	7.125E-07	10.09
41	2.410E-01	2.07	3.487E-02	4.60	2.116E-02	7.67	2.733E-03	51.64	1.557E-09	53.80	6.328E-07	10.37
42	2.407E-01	2.54	3.056E-02	5.62	1.831E-02	10.86	4.500E-03	59.31	1.090E-09	77.44	4.776E-07	13.57
43	2.247E-01	2.46	3.328E-02	5.61	2.012E-02	10.05	9.952E-03	73.88	4.201E-10	60.25	5.590E-07	14.52
44	2.148E-01	2.95	3.027E-02	5.64	2.004E-02	9.12	1.457E-03	33.15	1.624E-09	58.07	4.962E-07	12.34
45	2.082E-01	2.82	2.127E-02	7.49	2.125E-02	9.74	1.789E-03	62.65	1.566E-09	32.90	5.014E-07	12.25
46	2.040E-01	2.99	2.728E-02	5.07	1.622E-02	8.93	1.837E-03	71.16	1.492E-09	57.44	4.234E-07	11.81
47	1.887E-01	2.40	2.630E-02	5.31	1.578E-02	9.23	2.976E-04	100.00	9.200E-10	51.80	4.058E-07	14.95
48	1.721E-01	2.10	2.545E-02	5.68	1.728E-02	9.10	1.438E-03	90.35	1.728E-09	39.55	4.461E-07	12.18
49	1.673E-01	2.28	2.485E-02	5.62	1.870E-02	10.59	8.429E-03	77.59	1.194E-09	42.26	4.154E-07	13.87
50	3.898E-01	2.71	5.386E-02	3.53	3.276E-02	6.19	1.347E-03	94.54	2.003E-09	39.55	1.156E-06	20.64
51	3.591E-01	1.99	5.172E-02	3.42	1.534E-02	6.97	3.403E-03	59.14	2.45E-09	26.61	9.218E-07	9.44

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52	3.345E-01	1.89	4.697E-02	3.67	2.884E-02	2.37	1.100E-03	78.23	1.780E-09	42.33	7.545E-07	10.92		
53	3.242E-01	1.89	4.822E-02	4.42	3.166E-02	6.04	0.	0.00	1.817E-09	37.69	7.990E-07	11.02		
54	2.915E-01	2.02	4.282E-02	7.61	2.416E-02	7.64	0.	0.00	1.479E-09	43.49	6.759E-07	11.42		
55	1.817E-01	1.96	4.473E-02	4.09	2.664E-02	9.30	2.415E-03	100.00	1.817E-09	46.92	7.151E-07	11.62		
56	2.669E-01	2.26	4.071E-02	4.18	2.705E-02	8.19	1.116E-03	99.90	4.999E-10	47.09	7.932E-07	10.25		
57	2.715E-01	2.19	4.216E-02	4.23	2.376E-02	9.24	1.027E-03	73.60	1.515E-09	95.76	6.096E-07	10.44		
58	2.644E-01	1.71	3.904E-02	3.80	2.085E-02	6.75	7.425E-04	100.00	2.950E-09	42.45	6.089E-07	10.65		
59	2.500E-01	2.20	3.847E-02	4.32	2.467E-02	7.88	3.639E-03	62.87	5.210E-10	40.05	9.580E-07	26.60		
60	2.51E-01	1.68	3.716E-02	3.85	2.202E-02	7.40	3.054E-03	73.90	1.664E-09	32.61	5.481E-07	15.17		
61	2.459E-01	1.92	3.740E-02	4.06	2.255E-02	8.19	1.052E-03	100.00	2.463E-09	43.24	6.665E-07	14.78		
62	2.378E-01	1.89	3.925E-02	3.88	2.420E-02	7.21	0.	0.00	2.664E-09	42.59	6.828E-07	11.26		
63	2.391E-01	2.07	3.939E-02	3.81	2.213E-02	6.90	1.958E-04	100.00	1.858E-09	35.54	4.905E-07	9.62		
64	2.325E-01	1.81	3.805E-02	3.62	2.127E-02	8.59	1.776E-03	76.90	1.937E-09	38.40	5.764E-07	9.67		
65	2.333E-01	1.88	3.864E-02	3.79	2.140E-02	8.93	4.408E-04	100.00	3.588E-10	57.29	5.054E-07	10.10		
66	2.254E-01	2.02	3.674E-02	4.34	2.269E-02	8.29	6.948E-04	100.00	1.511E-09	34.34	5.950E-07	19.40		
67	2.317E-01	2.30	3.846E-02	3.94	2.303E-02	6.62	0.	0.00	7.920E-10	70.01	5.709E-07	13.08		
68	2.271E-01	2.07	3.829E-02	3.71	2.344E-02	7.35	0.	0.00	9.315E-10	52.44	6.284E-07	13.58		
69	2.276E-01	2.17	3.790E-02	3.79	2.268E-02	7.24	2.571E-03	60.34	1.079E-09	41.51	5.699E-07	10.04		
70	2.310E-01	1.75	3.879E-02	3.64	2.041E-02	7.81	3.829E-03	75.26	2.755E-09	39.05	5.597E-07	9.41		
71	2.349E-01	2.22	3.690E-02	3.08	2.327E-02	7.94	1.173E-03	81.38	1.040E-09	43.89	6.210E-07	15.80		
72	2.132E-01	1.89	3.813E-02	4.00	1.961E-02	6.67	1.107E-03	90.24	1.311E-09	46.45	5.045E-07	13.33		
73	2.081E-01	2.27	3.817E-02	4.28	2.285E-02	6.14	8.023E-04	100.00	1.405E-09	40.73	8.543E-07	40.58		
74	2.202E-01	1.40	3.645E-02	4.37	2.244E-02	7.03	0.	0.00	7.324E-10	41.40	7.370E-07	15.55		
75	2.041E-01	2.26	3.445E-02	4.24	2.150E-02	7.95	6.77E-04	91.26	1.151E-09	40.87	5.515E-07	11.51		
76	2.238E-01	1.83	3.824E-02	4.47	2.503E-02	6.75	3.282E-03	94.22	7.746E-10	54.83	5.972E-07	14.27		
77	1.997E-01	1.77	3.421E-02	3.62	2.225E-02	7.38	8.819E-04	100.00	1.225E-09	37.91	5.937E-07	15.56		
78	2.103E-01	2.19	3.714E-02	3.34	2.208E-02	7.42	8.707E-04	74.05	1.108E-09	42.30	5.104E-07	12.63		
79	1.902E-01	2.78	3.612E-02	3.47	2.010E-02	8.25	0.	0.00	1.496E-09	34.07	4.593E-07	14.48		
80	2.063E-01	2.16	3.597E-02	4.42	1.844E-02	8.17	5.696E-03	62.73	2.410E-09	75.23	5.110E-07	11.62		
81	2.049E-01	2.23	3.562E-02	4.21	2.200E-02	7.52	3.995E-03	88.82	9.654E-10	37.39	5.713E-07	13.39		
82	1.723E-01	1.99	3.506E-02	4.65	2.128E-02	7.68	2.684E-03	87.84	1.539E-09	34.30	5.160E-07	13.57		
83	2.063E-01	1.66	3.601E-02	4.05	1.910E-02	7.75	9.746E-08	100.00	1.342E-09	40.98	5.036E-07	12.55		
84	1.680E-01	2.34	3.402E-02	4.56	2.037E-02	7.76	1.188E-03	76.62	1.076E-09	48.18	5.108E-07	13.17		
85	1.951E-01	1.84	3.733E-02	3.51	2.531E-02	7.14	2.440E-03	71.73	7.539E-10	38.96	5.150E-07	13.65		
86	1.868E-01	2.13	3.361E-02	3.94	1.791E-02	5.85	4.174E-03	92.57	1.522E-09	30.50	6.015E-07	13.15		
87	1.860E-01	1.80	3.354E-02	3.73	2.007E-02	7.12	8.363E-04	70.21	6.465E-10	46.93	4.510E-07	13.31		
88	1.500E-01	1.92	3.200E-02	4.21	1.826E-02	6.91	1.992E-03	100.00	1.007E-09	44.28	3.974E-07	13.61		
89	1.628E-01	2.30	3.083E-02	4.00	1.657E-02	8.01	5.549E-04	100.00	6.992E-10	39.82	3.692E-07	12.41		
90	1.739E-01	2.06	3.280E-02	3.34	1.845E-02	8.21	9.751E-04	100.00	1.090E-09	40.98	4.120E-07	10.76		

92	1.689E-01	1.90	3.26E-02	4.03	1.597E-02	7.66	1.22E-03	86.87	6.53E-10	21.25	5.79E-07	18.25
93	1.678E-01	2.11	3.26E-02	4.26	1.828E-02	7.53	1.05E-03	87.00	8.02E-10	32.47	6.10E-07	12.50
94	6.325E-02	3.77	1.20E-02	5.31	6.178E-03	10.39	5.22E-04	100.00	2.749E-10	61.05	1.492E-07	22.00
95	6.362E-02	5.71	1.262E-02	6.56	6.944E-03	11.70	0.	0.00	2.306E-10	69.87	1.271E-07	25.51
96	6.442E-02	3.06	1.227E-02	6.40	6.88E-03	10.71	6.102E-04	86.39	6.593E-10	56.14	1.359E-07	22.00
97	6.312E-02	3.49	1.425E-02	5.49	7.924E-03	9.26	0.	0.00	1.028E-10	64.72	2.722E-07	33.27
98	9.360E-02	2.70	1.753E-02	6.34	9.439E-03	12.60	0.	0.00	1.636E-10	51.75	4.232E-07	36.61
99	8.279E-02	2.93	1.609E-02	6.66	8.890E-03	9.73	0.	0.00	2.501E-11	87.77	1.942E-07	17.59
100	9.400E-02	2.94	1.663E-02	5.11	9.404E-03	10.63	0.	0.00	4.354E-10	42.29	2.138E-07	16.63
101	6.971E-02	2.88	1.814E-02	5.18	1.071E-02	10.14	0.	0.00	9.881E-11	71.26	2.400E-07	23.73
102	1.253E-01	2.47	2.417E-02	4.29	1.466E-02	8.77	0.	0.00	4.611E-11	68.21	2.924E-07	17.50
103	1.314E-01	2.82	2.451E-02	4.51	1.187E-02	7.63	0.	0.00	9.137E-11	69.99	3.107E-07	31.13
104	1.535E-01	2.19	1.997E-02	5.66	1.513E-02	7.84	0.	0.00	1.473E-10	47.94	4.038E-07	15.06
105	1.740E-01	1.89	3.403E-02	3.44	1.854E-02	7.12	0.	0.00	6.245E-10	31.77	6.856E-07	11.73
106	1.110E-01	2.36	2.149E-02	4.59	1.145E-02	6.40	0.	0.00	4.841E-10	44.15	3.128E-07	15.19
107	3.247E-01	2.20	2.640E-02	4.34	1.309E-02	6.85	0.	0.00	1.650E-10	48.96	3.429E-07	13.46
108	1.615E-01	1.92	3.847E-02	3.58	1.958E-02	6.45	4.180E-04	100.00	2.891E-10	48.88	3.757E-07	12.06
109	8.142E-02	2.40	1.793E-02	4.19	6.875E-03	5.73	0.	0.00	2.927E-10	54.04	3.119E-07	21.99

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110	9.958E-02	1.40	2.103E-02	4.28	9.684E-03	6.24	7.166E-04	94.69	3.534E-11	71.13	2.318E-07	15.07
111	1.237E-01	2.05	2.987E-02	3.25	1.352E-02	7.41	6.442E-04	100.00	5.535E-12	71.33	4.107E-07	16.45
112	1.588E-01	1.41	3.976E-02	3.34	1.605E-02	5.11	4.557E-04	100.00	1.211E-10	66.13	3.441E-07	14.49
113	2.117E-01	1.32	5.593E-02	3.02	2.292E-02	4.92	1.972E-04	100.00	2.528E-10	38.77	7.114E-07	14.91
114	2.880E-01	1.15	6.526E-02	2.57	3.023E-02	3.75	1.280E-04	75.42	2.414E-10	39.91	7.147E-07	7.45
115	1.879E-01	1.43	5.420E-02	2.57	1.977E-02	6.30	5.573E-04	75.54	2.036E-10	43.54	4.369E-07	9.12
116	2.155E-01	1.09	7.175E-02	2.62	2.439E-02	3.80	2.953E-04	72.54	1.801E-10	54.66	5.627E-07	4.11
117	2.449E-01	1.17	6.443E-02	2.25	2.950E-02	3.68	0.	0.00	1.727E-10	51.52	6.040E-07	6.63
118	2.684E-01	.96	9.352E-02	2.49	3.103E-02	3.54	2.128E-04	72.76	3.891E-11	68.54	7.661E-07	6.11
119	2.769E-01	.96	1.031E-01	2.54	3.100E-02	6.04	1.645E-04	95.05	2.432E-10	50.49	8.335E-07	1.00
120	2.410E-01	1.00	1.026E-01	2.25	3.025E-02	3.94	0.	0.00	1.206E-10	45.23	1.702E-07	8.14
121	1.145E-01	1.29	4.824E-02	1.59	1.224E-02	5.27	0.	0.00	1.541E-11	69.12	2.632E-07	12.09
122	9.248E-02	1.37	3.876E-02	2.55	9.271E-03	6.27	0.	0.00	0.	0.00	2.031E-07	9.72
123	6.310E-02	1.94	2.888E-02	1.27	5.367E-03	7.47	0.	0.00	3.873E-11	76.14	1.331E-07	12.14

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0142HERI) EXXON 15X15 PWR, 4.28U235, 2506 PPM NAT.BORON

0 FREQUENCY FOR GENERATIONS 4 TO 73

- .8470 TO .8481 \*\*
- .8651 TO .8882 \*\*\*\*
- .8882 TO .9113 \*\*\*\*\*
- .9113 TO .9344 \*\*\*\*\*
- .9344 TO .9575 \*\*\*\*\*
- .9575 TO .9806 \*\*\*\*\*
- .9806 TO 1.0037 \*\*

0 FREQUENCY FOR GENERATIONS 22 TO 73

- .8420 TO .8651 \*
- .8651 TO .8882 \*
- .8882 TO .9113 \*\*\*\*\*
- .9113 TO .9344 \*\*\*\*\*
- .9344 TO .9575 \*\*\*\*\*
- .9575 TO .9806 \*\*\*\*\*
- .9806 TO 1.0037 \*\*

0 FREQUENCY FOR GENERATIONS 39 TO 73

- .8420 TO .8651 \*
- .8651 TO .8882 \*
- .8882 TO .9113 \*\*\*\*\*
- .9113 TO .9344 \*\*\*\*\*
- .9344 TO .9575 \*\*\*\*\*
- .9575 TO .9806 \*\*\*
- .9806 TO 1.0037 \*\*

0 FREQUENCY FOR GENERATIONS 56 TO 73

- .8420 TO .8651 \*
- .8651 TO .8882 \*



0.12 TO .934 \*\*\*\*\*  
.934 TO .9575 \*\*\*\*\*  
.9575 TO .9806 \*\*  
.9806 TO 1.0037

--EOF--

1 MEVT POWER COMPUTING/990 - NOS 2.7.1.10. NOS 2.7.1 ET\*MAC. 90/01/03. 03.40.15.

03.30.06.E42KEB1,P0,T2000. HENRY TRAN  
03.30.06.UBER,VK4PSN,NC.  
03.30.06.ABSC, 0.  
03.30.06.YOUR PASSWORD EXPIRES AT 00.00.00 ON 90/02/08.  
03.30.06.CHARGE,N973301,V3C.  
03.30.08.CHARGE = N973301, PROJECT = V3C.  
03.30.09.2221101.  
03.30.09.PF0C). SYSTEM PROLOGUE  
03.30.09.COMMENT. SYSTEN PROLOG  
03.30.09.NWB(A).  
03.30.11.CHEKEXP.  
03.30.13. INQUIRY COMPLETE.  
03.30.13.REVERT.  
03.30.14.TITLE([E42KEB1]) EXTON 15x15 AWP, 4-280235-0300 PRK NAT-BORON)  
03.30.14.LABEL,TAPEA,D=0F,L=EXSECT,VBN#007421.  
03.31.23.HT1U7, ASSIGNED TO TAPEA, VBN#007421.  
03.31.24.COPYBF,TAPEA,TAPEA.  
03.31.27. COPY 1 FILES 1 RECS 350426 WORDS  
03.31.27.REWIND,TAPEA.  
03.31.27.RETURN,TAPEA.  
03.31.28.RF:(IC=10)  
03.31.28.ATTACH,KEND4,1,2K.  
03.31.29. STOP  
03.31.29. 035200 MAXIMUM EXECUTION FL.  
03.31.29. 0.238 CF SECONDS EXECUTION TIME.  
03.31.29.KEND4,FL=777777.  
03.40.14. STOP  
03.40.14. 372700 MAXIMUM EXECUTION FL.  
03.40.14. 1030.453 CF SECONDS EXECUTION TIME.  
03.40.15.UFPT, 0.129KUN.  
03.40.15.UFMT, 2.747KUN.  
03.40.15.UFMS, 35.165KUN.  
03.40.15.UFCF, 1031.723SECS.  
03.40.15. BRU, 2050.561UNTS.  
03.40.15.#OUT(\*OF=5)  
03.40.15. NO FILE: PROCESSED.  
03.40.15.#DAYFILE(OUTPUT,JI=0)  
03.40.15.JABO, 105E SDBS FN=OUTPUT.  
03.40.15.POWER COMPUTING/990 - NOS 2.7.1.10  
03.40.15.DATE# 90/01/03.  
03.40.15.JSN# MEVT

END OF FILE

22

04.14.34.USER,VK9PSN,,NC.  
04.14.34.ABSC, 0.  
04.14.34.YOUR PASSWORD EXPIRES AT 00-00-00 ON 90/02/08.  
04.14.34.CHARGE,N973301,VSC.  
04.14.35.CHARGE \* N973301, PROJECT \* VSC.  
04.14.36.ZZZZZG1.  
04.14.36.PROC1: SYSTEM PROLOGUE  
04.14.36.COMMENT: SYSTEM PROLOG  
04.14.36.NEWS(A).  
04.14.37.CHEKEXP.  
04.14.38. INQUIRY COMPLETE.  
04.14.39.REVERT.  
04.14.39.TITLE([ISONUB]) EXYON PWR 15X15, 5-04 U235, BORATED WATER)  
04.14.39.ATTACHP(LER1,1,0)  
04.14.40. STOP  
04.14.40. 035200 MAXIMUM EXECUTION FL.  
04.14.40. 0.243 CP SECONDS EXECUTION TIME.  
04.14.40.ATTACHP(LER2,1,0)  
04.14.41. STOP  
04.14.41. 035200 MAXIMUM EXECUTION FL.  
04.14.41. 0.244 CP SECONDS EXECUTION TIME.  
04.14.42.ATTACHP(LER3,1,0)  
04.14.43. STOP  
04.14.43. 035200 MAXIMUM EXECUTION FL.  
04.14.43. 0.244 CP SECONDS EXECUTION TIME.  
04.14.43.REWIND,TAPE1,TAPE2,TAPE3.  
04.14.43.ATTACHP(NULLIF,4,1).  
04.14.45. STOP  
04.14.45. 035200 MAXIMUM EXECUTION FL.  
04.14.45. 0.241 CP SECONDS EXECUTION TIME.  
04.14.45.NULLIF(PL=777777)  
04.14.53.TIME = 000, KEFF = 1.49151  
04.14.55.TIME = 000, KEFF = 1.43527  
04.15.00.TIME = 000, KEFF = 1.34746  
04.15.07.TIME = 000, KEFF = 1.32145  
04.15.11.TIME = 000, KEFF = 1.29269  
04.15.15.TIME = 000, KEFF = 1.26525  
04.15.20.TIME = 000, KEFF = 1.23424  
04.15.24.TIME = 000, KEFF = 1.21435  
04.15.28.TIME = 000, KEFF = 1.19069  
04.15.32.TIME = 000, KEFF = 1.16902  
04.15.37.TIME = 000, KEFF = 1.14441  
04.15.42.TIME = 000, KEFF = 1.12566  
04.15.47.TIME = 000, KEFF = 1.12566  
04.15.47. STOP 222  
04.15.47. 230100 MAXIMUM EXECUTION FL.  
04.15.47. 66.182 CP SECONDS EXECUTION TIME.  
04.15.48.UEPF, 0.116KUNS.  
04.15.48.UEMS, 110.300KUNS.  
04.15.48.UECP, 67.321SECS.  
04.15.48.SRU, 143.711UNTS.  
04.15.48.#OUT(\*OP=E)  
04.15.48. NO FILES PROCESSED.  
04.15.48.#DAYFILE(OUTPUT,JT=D)  
04.15.48.IABO, 517B SDBS FN=OUTPUT.  
04.15.48.POWER COMPUTING/990 - NOS 2.7.1.10  
04.15.48.DATE: 89/12/29.  
04.15.48.JSN: MHKO  
END OF FILE

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# CALCULATION SHEET

TABLE (2-1)

SECTION	ENPL/Ch.	NAT. P [ppm]	AVERAGE K-EFF	1 SIGMA	FINAL * K-EFF
3.1	3.50%	1500	0.9376	0.002	0.9381
3.2	3.30%	1700	0.9343	0.003	0.9351
3.3	2.80%	900	0.9799	0.005	0.9829
3.4	4.20%	2700	0.9299	0.008	0.9400
3.5	3.20%	1700	0.9376	0.002	0.9381 **

\* Include all uncertainties

\*\* Estimate from Figure (2-1)

CLIENT:	JOB NO.	REVISION:
ORIGINATOR: HENRY TRAN	DATE:	CALC. NO. :
CHECKER:	DATE:	PAGE: 1

Figure (2-1)



# CALCULATION SHEET

## 2.2 Analysis

- (a) From Ref (12), the overall uncertainty due to variation in assembly locations, water density, fuel homogenization, and KENO-IV bias is

$$\Delta k_{\text{total}} = 0.013$$

Thus, the "Final  $k_{\text{eff}}$ " in Table (2-1) are calculated from:

$$\text{Final } k_{\text{eff}} = \text{Average } k_{\text{eff}} + 2\sigma + \Delta k_{\text{total}}$$

Ex

Section 4.1:  $0.9376 + 2 * 0.004 + 0.013 = 0.9586$

- (b) From Ref (12), the reactivity gained per 1% of U-235 initial enrichment is:

$$\Delta k_{\text{enrichment}} = 0.329$$

- (c) From Table (2-1), the reactivity reduced per 100 ppm of natural boron in water is:

$$\Delta k_{\text{boron}} = \frac{0.9243 - 0.9376}{(1700 - 1500)} = -0.0067$$

CLIENT:	JOB NO.	REVISION:
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CHECKER:	DATE:	PAGE: 1

# CALCULATION SHEET

d) Boron Contractions to have  $k_{eff} \approx 0.945$  ( $\leq 0.95$ )

Enrichment (%)	Nat. Boron Concentration [ppm]
1.36	$\emptyset$ (From Ref 22)
2.5	$300 + \frac{0.945 - 0.9588 * 100}{-0.0067} = 1125$
3.3	1700 (From Table 2-1)
4.2	2300 (From Table 2-1)
5. $\emptyset$	2800 (From Figure 2-1)

e) Boron concentration to have  $k_{eff} \leq 0.98$

Enrichment (%)	Nat. Boron Concentration [ppm]
$1.36 + \frac{0.98 - 0.95}{0.329} = 1.45$	$\emptyset$
2.5	$1125 + \frac{(.98 - .95) * 100}{-0.0067} = 675$
3.3	$1700 + \frac{(.98 - .95) * 100}{-0.0067} = 125\emptyset$
4.2	$2300 + \quad \quad \quad = 185\emptyset$
5. $\emptyset$	$2800 + \quad \quad \quad = 235\emptyset$

CLIENT:	JOB NO.	REVISION:
ORIGINATOR: HENRY TRAN	DATE:	CALC. NO. :
CHECKER:	DATE:	PAGE: 1

FIGURE (2-2)

EXXON 15x15 PWR (PALISADES FUEL)

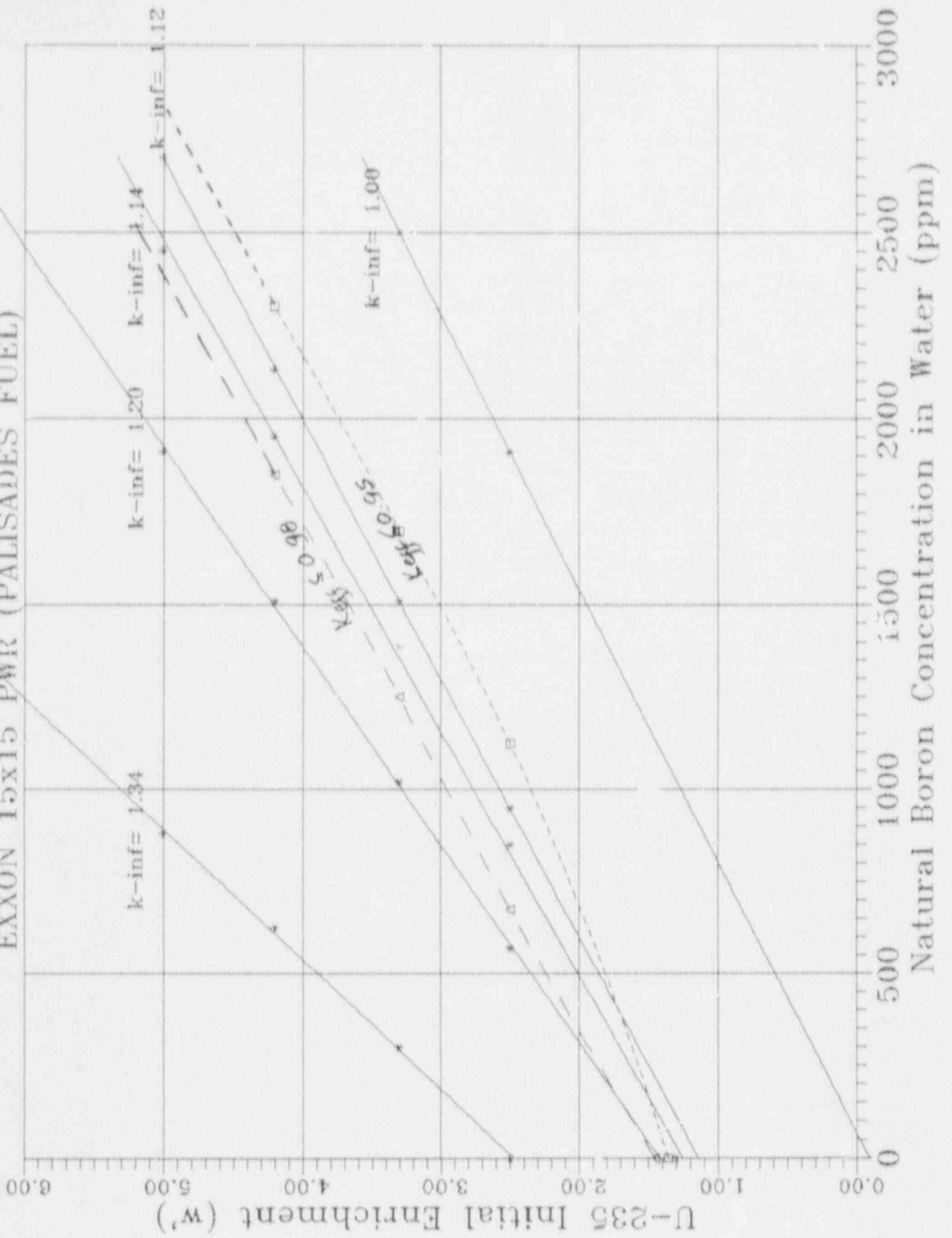




Figure (2-3)

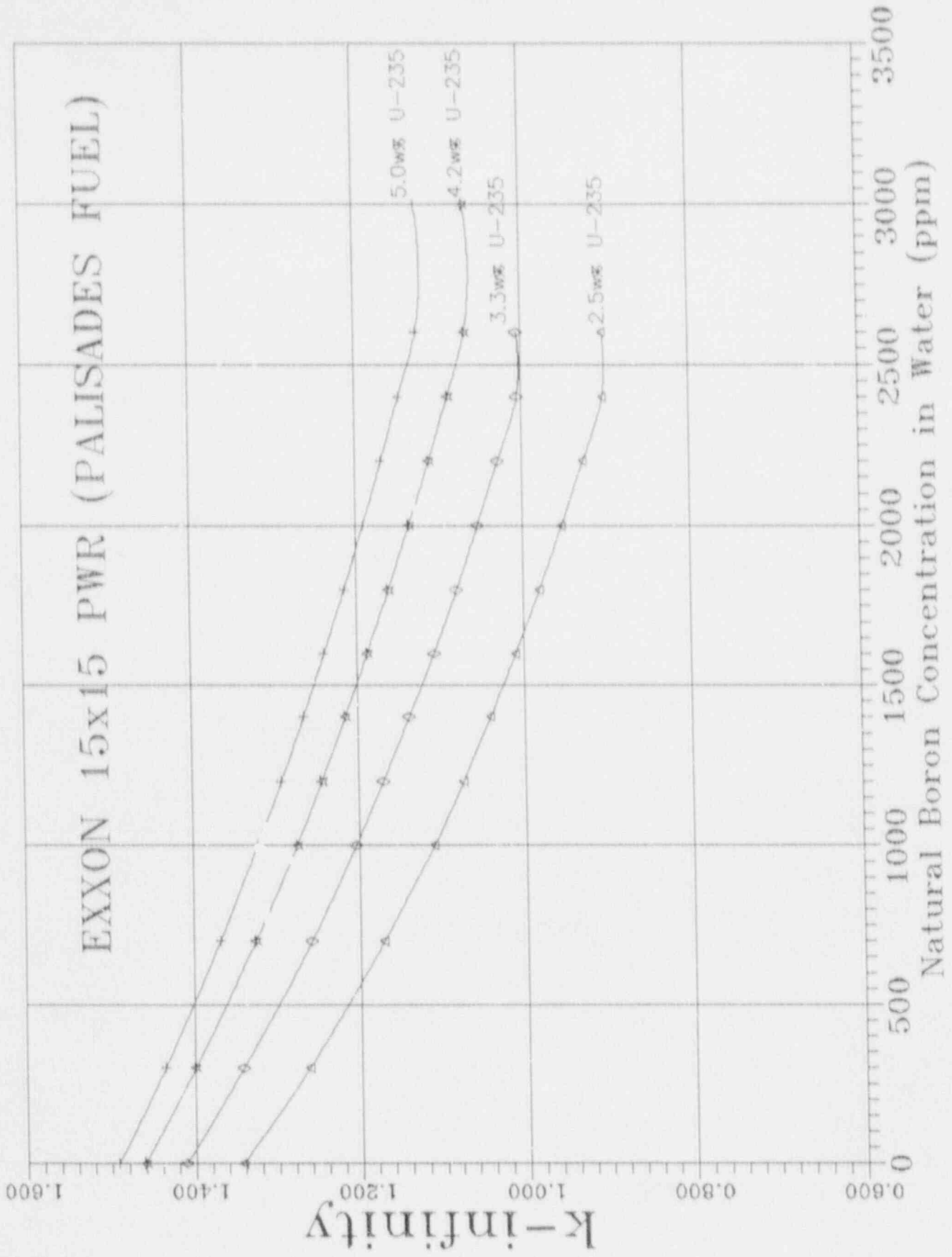


Table (4-2)

H (in water) : 6.671E-02 [atoms/barn.cm]  
 H (homo. fuel): 3.807E-02 [atoms/barn.cm]

NAT. BORON CONCENTRATION [ ppm ]	NULIF & XSDRNPM B-10 ATOM [atoms/barn.cm]	KENO-IV B-10 ATOM [atoms/barn.cm]
0	0.000E+00	0.000E+00
100	1.308E-06 (*)	7.462E-07 (**)
200	2.615E-06	1.492E-06
300	3.923E-06	2.239E-06
400	5.230E-06	2.985E-06
500	6.538E-06	3.731E-06
600	7.845E-06	4.477E-06
700	9.153E-06	5.224E-06
800	1.046E-05	5.970E-06
900	1.177E-05	6.716E-06
1000	1.308E-05	7.462E-06
1100	1.438E-05	8.209E-06
1200	1.569E-05	8.955E-06
1300	1.700E-05	9.701E-06
1400	1.831E-05	1.045E-05
1500	1.961E-05	1.119E-05
1600	2.092E-05	1.194E-05
1700	2.223E-05	1.269E-05
1800	2.354E-05	1.343E-05
1900	2.484E-05	1.418E-05
2000	2.615E-05	1.492E-05
2100	2.746E-05	1.567E-05
2200	2.877E-05	1.642E-05
2300	3.007E-05	1.716E-05
2400	3.138E-05	1.791E-05
2500	3.269E-05	1.866E-05
2600	3.400E-05	1.940E-05
2700	3.530E-05	2.015E-05
2800	3.661E-05	2.089E-05
2900	3.792E-05	2.164E-05
3000	3.923E-05	2.239E-05
3100	4.053E-05	2.313E-05
3200	4.184E-05	2.388E-05

5034

2811

$$(*) \quad 100 \text{ ppm} \times \frac{10^{-6}}{\text{ppm}} \times 6.671 \times 10^{-2} \frac{\text{atoms H}}{\text{barn cm}} \times 0.196 \frac{B_{10}}{B_{\text{nat}}} = 1.308 \times 10^{-6} \frac{\text{atoms B-10}}{\text{barn cm}}$$

$$(**) \quad 100 \text{ ppm} \times \frac{10^{-6}}{\text{ppm}} \times 3.807 \times 10^{-2} \frac{\text{atoms H}}{\text{barn cm}} \times 0.196 \frac{B_{10}}{B_{\text{nat}}} = 7.462 \times 10^{-7} \frac{\text{atoms B-10}}{\text{barn cm}}$$





\*\*\*\*\*  
VSC-2415.DENRICH:2820 WPMB,70F  
\*\*\*\*\*

\*\*\*\*\* LOGICAL PARAMETERS \*\*\*\*\*  
RUN EXECUTE PROGRAM AFTER CHECKING DATA YES PLOT PLOT PICTURE MAP(S) NO  
FLX COMPUTE FLUX NO FDN COMPUTE FISSION DENSITIES NO  
SMU COMPUTE AVG UNIT SELF-MULTIPLICATION NO NUB COMPUTE NU-BAR & AVG FISSION GROUP NO  
MKU COMPUTE MATRIX K-EFF BY UNIT NUMBER NO MKP COMPUTE MATRIX K-EFF BY UNIT LOCATION NO  
DKU COMPUTE COFACTOR K-EFF BY UNIT NUMBER NO DKP COMPUTE COFACTOR K-EFF BY UNIT LOCATION NO  
FMU PRINT FISSION PROD MATRIX BY UNIT NUMBER NO FMP PRINT FISSION PROD MATRIX BY UNIT LOCATION NO  
MKH COMPUTE MATRIX K-EFF BY HOLE NUMBER NO MHA COMPUTE MATRIX K-EFF BY ARRAY NUMBER NO  
DKH COMPUTE COFACTOR K-EFF BY HOLE NUMBER NO DKA COMPUTE COFACTOR K-EFF BY ARRAY NUMBER NO  
FMH PRINT FISSION PROD MATRIX BY HOLE NUMBER NO FHA PRINT FISSION PROD MATRIX BY ARRAY NUMBER NO  
IML COLLECT MATRIX BY HIGHEST HOLE LEVEL NO IML COLLECT MATRIX BY HIGHEST ARRAY LEVEL NO  
IMY PRINT ALL MIXTURE CROSS SECTIONS NO IAR PRINT PDS AND ARS BY REGION NO  
XSI PRINT 1-D MIXTURE X-SECTIONS NO XAY PRINT XSEC-ALIGNED CORRELATION TABLE NO  
XSD PRINT 2-D MIXTURE X-SECTIONS NO XAT PRINT WEIGHT AVERAGE ARRAY NO  
XAD PRINT MIXTURE PROBABILITIES NO XAM PRINT INPUT GEOMETRY NO  
XAD PRINT MIXTURE PROBABILITIES NO XAD PRINT MIXTURE PROBABILITIES NO  
XAD PRINT MIXTURE PROBABILITIES NO XAD PRINT MIXTURE PROBABILITIES NO  
XAD PRINT MIXTURE PROBABILITIES NO XAD PRINT MIXTURE PROBABILITIES NO  
XAD PRINT MIXTURE PROBABILITIES NO XAD PRINT MIXTURE PROBABILITIES NO

PARAMETER INPUT COMPLETED

0 TO'S WERE USED READING THE PARAMETER DATA  
\*\*\*\*\* DATA READING COMPLETED \*\*\*\*\*

\*\*\*\*\*  
VSC-2415.DENRICH:2820 WPMB,70F  
\*\*\*\*\*

UNIT VOLUME UNIT FUNCTION  
NUMBER NAME  
DATA SET NAME









```

0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0 1 1 1 2 2 2 2 2 2 2 2 1 1 1 1
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

```

```

0 ----- UNIT ORIENTATION DESCRIPTION FOR ARRAY 2 -----
07 LAYER 1, X COLUMN 1 TO 4 LEFT TO RIGHT Y ROW 1 TO 4 BOTTOM TO TOP
0 3 3 3 0
0 3 3 3 0
0 0 0 3 0
0 3 3 3 0

```

```

0 ----- UNIT ORIENTATION DESCRIPTION FOR ARRAY 3 -----
07 LAYER 1, X COLUMN 1 TO 2 LEFT TO RIGHT Y ROW 1 TO 1 BOTTOM TO TOP
0 1 0

```

USE=243,ORIENT=000000000000000000

```

0 ----- UNIT ORIENTATION DESCRIPTION FOR ARRAY 4 -----
07 LAYER 1, X COLUMN 1 TO 1 LEFT TO RIGHT Y ROW 1 TO 2 BOTTOM TO TOP
0 1
0 1

```

```

0 ----- UNIT ORIENTATION DESCRIPTION FOR ARRAY 5 -----
07 LAYER 1, X COLUMN 1 TO 1 LEFT TO RIGHT Y ROW 1 TO 1 BOTTOM TO TOP
0 1

```

USE=243,ORIENT=000000000000000000  
VOLUMES FOR THOSE UNITS PLACED ON THIS PROBLEM

UNIT	REGION	REGION	VOLUME	CUMULATIVE VOLUME
0	1	1	0.10050E+01 CMKK3	0.10050E+01 CMKK3
0	2	2	1.14071E+00 CMKK3	1.24768E+01 CMKK3
0	3	3	1.12540E+01 CMKK3	2.37308E+01 CMKK3
0	4	4	0.39202E+01 CMKK3	2.76510E+01 CMKK3
0	5	5	0.75004E+01 CMKK3	3.51514E+01 CMKK3
0	SURROUNDING GEOMETRY VOLUMES - GEOMETRY REGION		6 IS AN ARRAY PLACEMENT BOUNDARY REGION	
0	7	6	2.19556E+04 CMKK3	5.71070E+01 CMKK3
0	8	7	3.02459E+03 CMKK3	6.03529E+01 CMKK3
0	9	8	0.32004E+03 CMKK3	6.35533E+01 CMKK3
0	SURROUNDING GEOMETRY VOLUMES - GEOMETRY REGION		9 IS AN ARRAY PLACEMENT BOUNDARY REGION	
0	4	9	5.46017E+04 CMKK3	1.18155E+02 CMKK3
0	SURROUNDING GEOMETRY VOLUMES - GEOMETRY REGION		10 IS AN ARRAY PLACEMENT BOUNDARY REGION	
0	5	10	5.46017E+04 CMKK3	1.72757E+02 CMKK3
0	SURROUNDING GEOMETRY VOLUMES - GEOMETRY REGION		11 IS AN ARRAY PLACEMENT BOUNDARY REGION	
0	6	11	4.36913E+05 CMKK3	1.96810E+02 CMKK3
0	7	12	2.72188E+05 CMKK3	2.68998E+02 CMKK3
0	8	13	4.65538E+04 CMKK3	3.15552E+02 CMKK3
0	4	14	0.16698E+04 CMKK3	3.32250E+02 CMKK3
0	5	15	6.49586E+04 CMKK3	3.97208E+02 CMKK3
0	6	16	2.92481E+05 CMKK3	6.89689E+02 CMKK3

UNIT	USES	REGION	MIXTURE	TOTAL VOLUME
0	1	5194	1	1.60890E+05 CMKK3
0			2	7.44862E+03 CMKK3
0			3	5.78824E+04 CMKK3
0			4	2.79616E+05 CMKK3

0	2	216	1	3	2.10774E+04 CMKK3
0	3	24	2	3	7.25998E+04 CMKK3
			3	4	5.56658E+04 CMKK3
0	4	2	1		1.09208E+05 CMKK3
0	5	2	1		1.09208E+05 CMKK3
0	6	1	1		4.36813E+05 CMKK3
			2	9	2.72118E+05 CMKK3
			3	4	4.65538E+04 CMKK3
			4	0	2.16693E+04 CMKK3
			5	4	6.48586E+04 CMKK3
			6	0	2.92401E+05 CMKK3

TOTAL MIXTURE VOLUMES

MIXTURE	TOTAL VOLUME
0	2.99930E+05 CMKK3
1	1.20870E+05 CMKK3
2	5.70824E+04 CMKK3
3	6.77081E+05 CMKK3
4	1.67090E+05 CMKK3

\*\*\*\*\*  
 XXX  
 XXX  
 XXX  
 XXX  
 A DEFAULT WEIGHT OF 0.500 WILL BE USED FOR ALL OTHER JOBS.  
 XXX  
 \*\*\*\*\*

0.70'S WERE USED IN KEND-V BEFORE TRACKING  
 0.95000MINUTES WERE USED PROCESSING DATA.  
 VOLUME FRACTION OF FISSIONABLE MATERIAL IN THE CORE = 0.11008E+00  
 DETAYR TYPE 0 WAS USED  
 OTHER NEUTRONS WERE STARTED WITH A FLAT DISTRIBUTION IN A CUBOID DEFINED BY:  
 X= 1.65100E+07 Y= 0.00000E+00 Z= 1.65100E+07 X= 0.00000E+00 Y= 1.00000E+01 Z= 0.00000E+00  
 01 00000 MINUTES WERE REQUIRED FOR STARTING. TOTAL CHARGED TIME IS 1.95000 MINUTES.

WGT. 3415.020812112876 WPMU.70F

GENERATION	K EFFECTIVE	ELAPSED TIME MINUTES	AVERAGE K EFFECTIVE	AVERAGE DIVISION	MIXTURE FRACTION	REACTIVITY
1	9.18400E-01	1.00000E+00	1.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
2	9.98940E-01	1.06667E+01	1.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
3	9.97487E-01	1.47833E+01	9.97487E-01	0.00000E+00	0.00000E+00	0.00000E+00
4	9.92050E-01	1.90833E+01	9.94723E-01	7.71843E-02	0.00000E+00	0.00000E+00
5	9.74319E-01	2.34500E+01	9.71298E-01	2.85278E-02	0.00000E+00	0.00000E+00
6	9.89811E-01	2.78167E+01	9.75926E-01	1.72600E-02	0.00000E+00	0.00000E+00
7	1.00240E+00	3.20000E+01	9.81022E-01	1.43874E-02	0.00000E+00	0.00000E+00
8	9.98160E-01	3.65000E+01	9.74049E-01	1.03762E-02	0.00000E+00	0.00000E+00
9	9.80521E-01	4.08500E+01	9.74970E-01	8.14706E-03	0.00000E+00	0.00000E+00
10	9.61086E-01	4.52000E+01	9.73308E-01	1.02385E-02	0.00000E+00	0.00000E+00
11	9.74886E-01	4.94500E+01	9.67954E-01	1.05129E-02	0.00000E+00	0.00000E+00
12	1.03800E+00	5.38000E+01	9.74959E-01	1.17254E-02	0.00000E+00	0.00000E+00
13	9.90440E-01	5.84000E+01	9.71584E-01	1.12572E-02	0.00000E+00	0.00000E+00
14	9.89353E-01	6.28000E+01	9.72190E-01	1.03266E-02	0.00000E+00	0.00000E+00
15	9.66007E-01	6.68000E+01	9.70938E-01	9.58047E-03	0.00000E+00	0.00000E+00
16	9.85149E-01	7.11000E+01	9.71880E-01	8.92990E-03	0.00000E+00	0.00000E+00
17	9.86866E-01	7.59167E+01	9.72900E-01	8.07201E-03	0.00000E+00	0.00000E+00
18	9.47180E-01	7.97000E+01	9.71348E-01	7.99550E-03	0.00000E+00	0.00000E+00
19	9.86029E-01	8.40477E+01	9.72930E-01	7.55955E-03	0.00000E+00	0.00000E+00
20	9.93609E-01	8.85667E+01	9.73418E-01	7.22577E-03	0.00000E+00	0.00000E+00
21	9.64099E-01	9.24000E+01	9.72940E-01	6.85147E-03	0.00000E+00	0.00000E+00
22	9.94179E-01	9.68000E+01	9.74105E-01	6.60269E-03	0.00000E+00	0.00000E+00
23	1.09579E+00	1.01000E+02	9.77039E-01	6.93208E-03	0.00000E+00	0.00000E+00
24	1.00000E+00	1.00000E+02	9.77039E-01	6.93208E-03	0.00000E+00	0.00000E+00

26	1.03533E+00	1.13533E+00	9.79154E-01	6.40463E-03	0.00000E+00	0.00000E+00
27	1.01654E+00	1.17667E+02	9.80655E-01	6.32237E-03	0.00000E+00	0.00000E+00
28	9.39468E-01	1.22133E+02	9.79068E-01	6.27730E-03	0.00000E+00	0.00000E+00
29	9.43297E-01	1.26433E+02	9.77743E-01	6.18418E-03	0.00000E+00	0.00000E+00
30	1.00020E+00	1.30650E+02	9.78545E-01	6.01315E-03	0.00000E+00	0.00000E+00
31	1.00578E+00	1.34817E+02	9.79484E-01	5.87742E-03	0.00000E+00	0.00000E+00
32	1.01466E+00	1.38983E+02	9.80656E-01	5.79807E-03	0.00000E+00	0.00000E+00
33	1.02529E+00	1.43138E+02	9.82096E-01	5.79013E-03	0.00000E+00	0.00000E+00
34	9.51019E-01	1.47350E+02	9.81125E-01	5.68973E-03	0.00000E+00	0.00000E+00
35	9.17388E-01	1.51750E+02	9.79194E-01	5.84333E-03	0.00000E+00	0.00000E+00
36	9.50760E-01	1.55950E+02	9.78357E-01	5.73009E-03	0.00000E+00	0.00000E+00
37	9.62414E-01	1.60267E+02	9.77902E-01	5.58251E-03	0.00000E+00	0.00000E+00
38	9.99667E-01	1.64817E+02	9.78507E-01	5.45872E-03	0.00000E+00	0.00000E+00
39	1.04866E+00	1.69183E+02	9.80403E-01	5.63702E-03	0.00000E+00	0.00000E+00
40	9.82686E-01	1.73583E+02	9.80463E-01	5.48754E-03	0.00000E+00	0.00000E+00
41	1.01811E+00	1.77950E+02	9.81454E-01	5.43004E-03	0.00000E+00	0.00000E+00
42	9.82103E-01	1.82400E+02	9.79495E-01	5.44996E-03	0.00000E+00	0.00000E+00
43	9.18667E-01	1.86817E+02	9.78011E-01	5.70540E-03	0.00000E+00	0.00000E+00
44	9.73475E-01	1.90950E+02	9.77903E-01	5.56900E-03	0.00000E+00	0.00000E+00
45	9.76084E-01	1.95249E+02	9.77015E-01	5.50548E-03	0.00000E+00	0.00000E+00
46	9.78744E-01	1.99550E+02	9.77600E-01	5.39071E-03	0.00000E+00	0.00000E+00
47	1.02110E+00	2.00070E+02	9.78074E-01	5.25840E-03	0.00000E+00	0.00000E+00
48	9.99744E-01	2.00183E+02	9.78817E-01	5.25999E-03	0.00000E+00	0.00000E+00
49	9.66821E-01	2.10567E+02	9.78271E-01	5.13496E-03	0.00000E+00	0.00000E+00
50	9.87413E-01	2.16817E+02	9.78915E-01	5.04173E-03	0.00000E+00	0.00000E+00
51	9.99761E-01	2.21100E+02	9.78922E-01	4.95726E-03	0.00000E+00	0.00000E+00
52	1.07037E+00	2.25567E+02	9.80760E-01	5.18911E-03	0.00000E+00	0.00000E+00
53	1.00136E+00	2.29750E+02	9.81751E-01	5.18740E-03	0.00000E+00	0.00000E+00
54	1.00721E+00	2.34100E+02	9.82810E-01	5.17248E-03	0.00000E+00	0.00000E+00
55	9.68003E-01	2.38183E+02	9.82599E-01	5.16139E-03	0.00000E+00	0.00000E+00
56	9.33084E-01	2.42400E+02	9.81619E-01	5.08985E-03	0.00000E+00	0.00000E+00
57	9.39261E-01	2.46683E+02	9.80643E-01	5.08086E-03	0.00000E+00	0.00000E+00
58	9.81870E-01	2.50950E+02	9.80863E-01	4.99915E-03	0.00000E+00	0.00000E+00
59	1.00001E+00	2.55300E+02	9.81199E-01	4.92728E-03	0.00000E+00	0.00000E+00
60	1.00874E+00	2.59717E+02	9.81571E-01	4.85104E-03	0.00000E+00	0.00000E+00
61	1.00027E+00	2.64000E+02	9.81884E-01	4.77840E-03	0.00000E+00	0.00000E+00
62	9.81314E-01	2.68183E+02	9.81308E-01	4.70775E-03	0.00000E+00	0.00000E+00
63	9.40197E-01	2.72417E+02	9.81041E-01	4.64020E-03	0.00000E+00	0.00000E+00
64	9.45900E-01	2.76833E+02	9.80477E-01	4.57174E-03	0.00000E+00	0.00000E+00
65	9.66204E-01	2.80950E+02	9.80767E-01	4.50180E-03	0.00000E+00	0.00000E+00
66	9.84870E-01	2.85333E+02	9.80519E-01	4.43177E-03	0.00000E+00	0.00000E+00
67	1.00187E+00	2.89471E+02	9.81199E-01	4.36075E-03	0.00000E+00	0.00000E+00
68	1.00263E+00	2.93800E+02	9.81524E-01	4.28922E-03	0.00000E+00	0.00000E+00
69	9.90687E-01	2.98150E+02	9.81705E-01	4.21979E-03	0.00000E+00	0.00000E+00
70	9.90110E-01	3.02367E+02	9.81985E-01	4.15097E-03	0.00000E+00	0.00000E+00

END MESSAGE NUMBER K5-123 EXECUTION TERMINATED DUE TO COMPLETION OF THE SPECIFIED NUMBER OF GENERATIONS.

MSD-2415 GENRICH/2800 WPMO, 70F

START TIME = 1.41155E-05 OR 1.92407E-07 GENERATION TIME = 1.28095E-05 + OR - 7.5610E-06

NO. OF INITIAL CONCENTRATIONS SKIPPED	AVERAGE K EFFECTIVE	DEVIATION	67 PER CENT CONFIDENCE INTERVAL		95 PER CENT CONFIDENCE INTERVAL		99 PER CENT CONFIDENCE INTERVAL		NUMBER OF HISTORIES
			CONFIDENCE	INTERVAL	CONFIDENCE	INTERVAL	CONFIDENCE	INTERVAL	
0	0.98104	+ OR - 0.00486	0.97660	TO 0.98541	0.97292	TO 0.98977	0.96795	TO 0.99414	20100
0	0.98088	+ OR - 0.00413	0.97645	TO 0.98530	0.97300	TO 0.98973	0.96759	TO 0.99416	17800
0	0.98125	+ OR - 0.00411	0.97704	TO 0.98618	0.97290	TO 0.99056	0.96852	TO 0.99497	19500
0	0.98163	+ OR - 0.00448	0.97714	TO 0.98610	0.97267	TO 0.99057	0.96819	TO 0.99505	19200
0	0.98129	+ OR - 0.00454	0.97675	TO 0.98580	0.97222	TO 0.99036	0.96768	TO 0.99490	18900
0	0.98199	+ OR - 0.00455	0.97743	TO 0.98654	0.97288	TO 0.99109	0.96832	TO 0.99565	18600
0	0.98201	+ OR - 0.00463	0.97738	TO 0.98666	0.97275	TO 0.99127	0.96812	TO 0.99599	18300
0	0.98234	+ OR - 0.00470	0.97765	TO 0.98704	0.97296	TO 0.99170	0.96826	TO 0.99643	18000
0	0.98232	+ OR - 0.00467	0.97765	TO 0.98799	0.97308	TO 0.99266	0.96780	TO 0.99733	17700
0	0.98238	+ OR - 0.00465	0.97772	TO 0.98703	0.97307	TO 0.99169	0.96841	TO 0.99634	17400
0	0.98264	+ OR - 0.00498	0.97865	TO 0.98863	0.97367	TO 0.99360	0.96869	TO 0.99858	15900

0	22	0.9828	+ DR - 0.00543	0.97885 TO 0.98970	0.97342 TO 0.99513	0.98800 TO 1.00058	12400
0	27	0.98165	+ DR - 0.00579	0.97587 TO 0.98744	0.97006 TO 0.99329	0.96429 TO 0.99701	12900
0	32	0.98178	+ DR - 0.00627	0.97552 TO 0.98805	0.96925 TO 0.99431	0.96298 TO 1.00058	11400
0	37	0.98487	+ DR - 0.00664	0.97823 TO 0.99151	0.97159 TO 0.99816	0.96495 TO 1.00480	9900
0	42	0.98384	+ DR - 0.00674	0.97710 TO 0.99059	0.97035 TO 0.99733	0.96361 TO 1.00408	8400
0	47	0.98698	+ DR - 0.00724	0.97974 TO 0.99422	0.97251 TO 1.00146	0.96527 TO 1.00867	6900
0	52	0.98275	+ DR - 0.00776	0.97498 TO 0.99051	0.96722 TO 0.99827	0.95945 TO 1.00604	5400
0	57	0.98392	+ DR - 0.00694	0.97698 TO 0.99086	0.97004 TO 0.99779	0.96010 TO 1.00473	3900
0	62	0.98111	+ DR - 0.00961	0.97150 TO 0.99072	0.96190 TO 1.00033	0.95229 TO 1.00994	2400
0	67	0.98315	+ DR - 0.01524	0.96791 TO 0.99839	0.95267 TO 1.01363	0.93749 TO 1.02887	900

VSC-24;5.0XENRICH;2820 WPPMB,70F

PLOT OF AVERAGE K-EFFECTIVE BY GENERATION RUN.

THE LINE REPRESENTS K-EFF = 0.9810 + DR - 0.0044 WHICH OCCURS FOR 70 GENERATIONS RUN.

0 0.9582 0.9751 0.9921



60  
65  
70  
75  
80  
85  
90  
95  
45

USC-2415 OXENRICH1283J WPNB, 70F

PLOT OF AVERAGE K-EFFECTIVE BY GENERATION SKIPPED

THE LINE REPRESENTS K-EFF = 0.9810 + 00 -- 0.0044 WHICH OCCURS FOR 0 GENERATIONS SKIPPED.

0.9734

0.9836

0.9889



50 +  
55 +  
60 +  
65 +



USC-2415 OXENRICH:2820 WPMU,70F

GROUP	FRACTION	UNIT	REGION	POSITIONS	PERCENT DEFIATION	Absorptions	PERCENT DEFIATION	LEAKAGE	SKIPPING PERCENT DEFIATION	GENERATIONS
0 1	0.0246			2.10945E-02	2.5054	1.07270E-02	2.0070	1.92250E-04	50.8771	
0 2	0.0308			2.27091E-02	2.7027	1.20167E-02	1.2757	7.82000E-04	50.0146	
0 3	0.0027			9.58296E-03	2.0484	3.03468E-03	9.608	2.42048E-04	52.1813	
0 4	0.0024			1.32946E-02	1.0055	4.04088E-03	1.7107	6.24710E-04	29.0180	
0 5	0.0041			4.02784E-03	1.5586	5.90097E-03	1.4398	7.19105E-04	24.6189	
0 6	0.0048			4.70071E-03	1.7026	8.44328E-03	1.6568	6.05691E-04	27.7475	
0 7	0.0064			6.23425E-03	1.9253	1.18482E-02	1.8068	3.38995E-04	41.4630	
0 8	0.0105			1.07066E-02	2.2147	1.38774E-02	2.0587	1.91247E-04	40.9100	
0 9	0.0248			2.37037E-02	1.6922	2.92987E-02	1.5024	1.91607E-04	49.0674	
0 10	0.0304			2.98066E-02	2.0574	4.56098E-02	1.7816	1.82484E-04	48.8570	
0 11	0.0249			1.88132E-02	2.0758	3.25879E-02	2.0211	4.87848E-05	100.0000	
0 12	0.0190			1.86648E-02	2.4293	6.42741E-02	2.0379	1.24481E-04	73.8771	
0 13	0.0195			1.91503E-02	2.6311	2.42230E-02	1.4320	0.00000E+00	0.0000	
0 14	0.0043			2.55842E-02	2.7664	3.46210E-02	1.5626	0.00000E+00	0.0000	
0 15	0.1871			1.89571E-01	1.3779	1.63061E-01	0.9506	1.05744E-04	59.3088	
0 16	0.5650			5.54016E-01	0.7406	5.43239E-01	0.4266	1.28044E-04	47.5431	
SYSTEM TOTAL =				2.81043E-01	0.4448	9.94609E-01	0.1899	4.19404E-03	10.6025	
DELAGED TIME 002.48000 MINUTES										
RANDOM NUMBER= 3F000000000000										

USC-2415 OXENRICH:2820 WPMU,70F

0	FREQUENCY FOR GENERATIONS	4 TO 70
0.8926 TO 0.9157	X	
0.9157 TO 0.9388	XXXXXX	
0.9388 TO 0.9619	XXXXXXXXXX	
0.9619 TO 0.9849	XXXXXXXXXXXXXX	
0.9849 TO 1.0080	XXXXXXXXXXXXXXXXXXXX	
1.0080 TO 1.0311	XXXXXX	
1.0311 TO 1.0542	XXXXX	
1.0542 TO 1.0773	X	
0	FREQUENCY FOR GENERATIONS	71 TO 70
0.8926 TO 0.9157	X	
0.9157 TO 0.9388	XXXX	
0.9388 TO 0.9619	XXXXXXXX	
0.9619 TO 0.9849	XXXXXXXXXX	
0.9849 TO 1.0080	XXXXXXXXXXXXXXXX	
1.0080 TO 1.0311	XXXXXX	

