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MEMORANDUM FOR: The Files

FROM: Nancy L. Osgood, SGTB, SGTR, NMSS

SUBJECT: Meeting Summary Concerning BR-100 Spent Fuel Rail Cask

Attendees

<u>NRC</u>	<u>B&W Fuel Co.</u>	<u>EG&G Idaho</u>
Nancy Osgood	Bernie Copsey	Ken Henry
Carl Withee	Brian Butler	
Marissa Garcia	George Vames	<u>DOE HQ</u>
Bernie White	Dan Young	Alan Berusch
George Gardes	Ed McGuinn	Bill Lake
Daniel Huang	Paul Childress	
Li Yang		<u>Weston</u>
Henry W. Lee		Maraj Rahimi

Introduction

A meeting was held at the request of B&W Fuel Company at Rockville, Maryland, on December 12, 1990, to discuss the BR-100 spent fuel cask. The BR-100 is being designed by B&W Fuel Company for the Department of Energy for spent fuel shipment by rail under the Nuclear Waste Policy Act.

Discussion

The discussion followed the attached meeting handout.

Results of thermal analyses and thermal testing were reported. The current conceptual design of the impact limiters was discussed. Testing of the impact limiters will be discussed at a future meeting.

An application is expected to be submitted to the NRC spring 1992.

Nancy L. Osgood
 Transportation Branch
 Division of Safeguards and
 Transportation, NMSS

Attachment: Meeting Handout

OFC :SGTB *NLO* :SGTB *CRG*

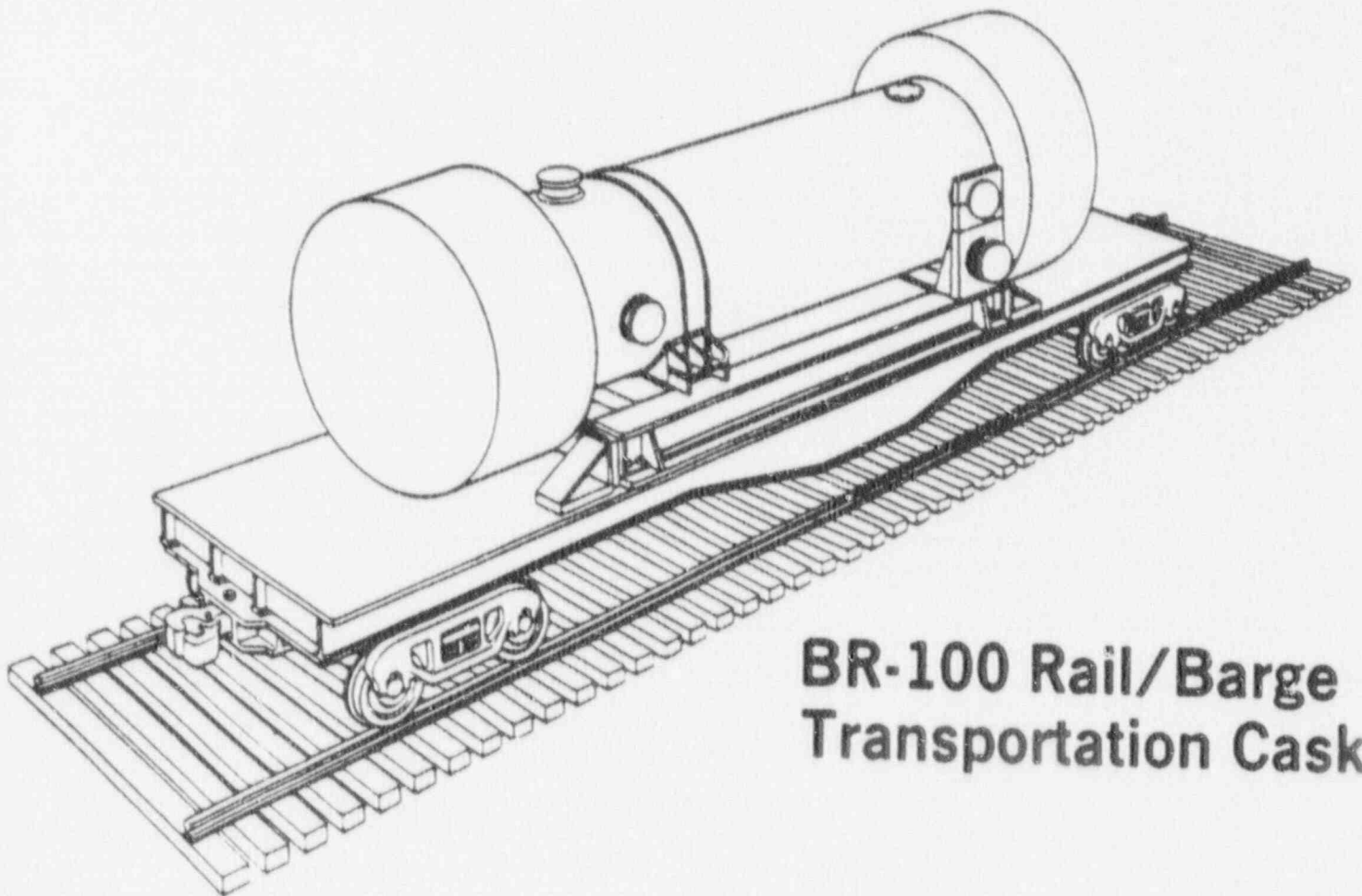
NAME:NLOsgood :CRChappell

DATE:12/13/90 :12/13/90

OFFICIAL RECORD COPY

NT03

**B&W Fuel Company
Presentation to the
NRC Transportation Branch
December 12, 1990**



**BR-100 Rail/Barge
Transportation Cask**

B&W FUEL COMPANY TEAM

GEORGE VAMES	PROJECT MANAGER
PAUL CHILDRESS	TECHNICAL CONSULTANT
DAN YOUNG	PROJECT ENGINEER
BERNIE COPSEY	THERMAL ANALYST
BRIAN BUTLER	IMPACT LIMITER DESIGNER
EDWARD MCGUINN	IMPACT LIMITER DESIGNER

***B&W FUEL
COMPANY***

NRC MEETING AGENDA
DECEMBER 12, 1990

INTRODUCTION

**G.J. VAMES /
P.C. CHILDRESS**

IMPACT LIMITER DEVELOPMENT

**E.J. McGUINN /
B.D. BUTLER**

**DESIGN CRITERIA
LIMITER DESIGN DESCRIPTION
MATERIAL PROPERTIES
DEVELOPMENT TESTING
VERIFICATION TEST PLANS**

THERMAL EVALUATION:

A.B. COPSEY

**DESIGN CRITERIA
THERMAL ANALYSIS STRATEGY
THERMAL TESTING**

WRAP-UP and QUESTIONS

G.J. VAMES

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CASK THERMAL DESIGN

O ANALYSES

- FUEL BASKET ANALYSIS
- NORMAL/ACCIDENT SCENARIOS
- "THERMAL SWITCH" CASK WALL

O THERMAL TESTING RESULTS

IMPACT LIMITER

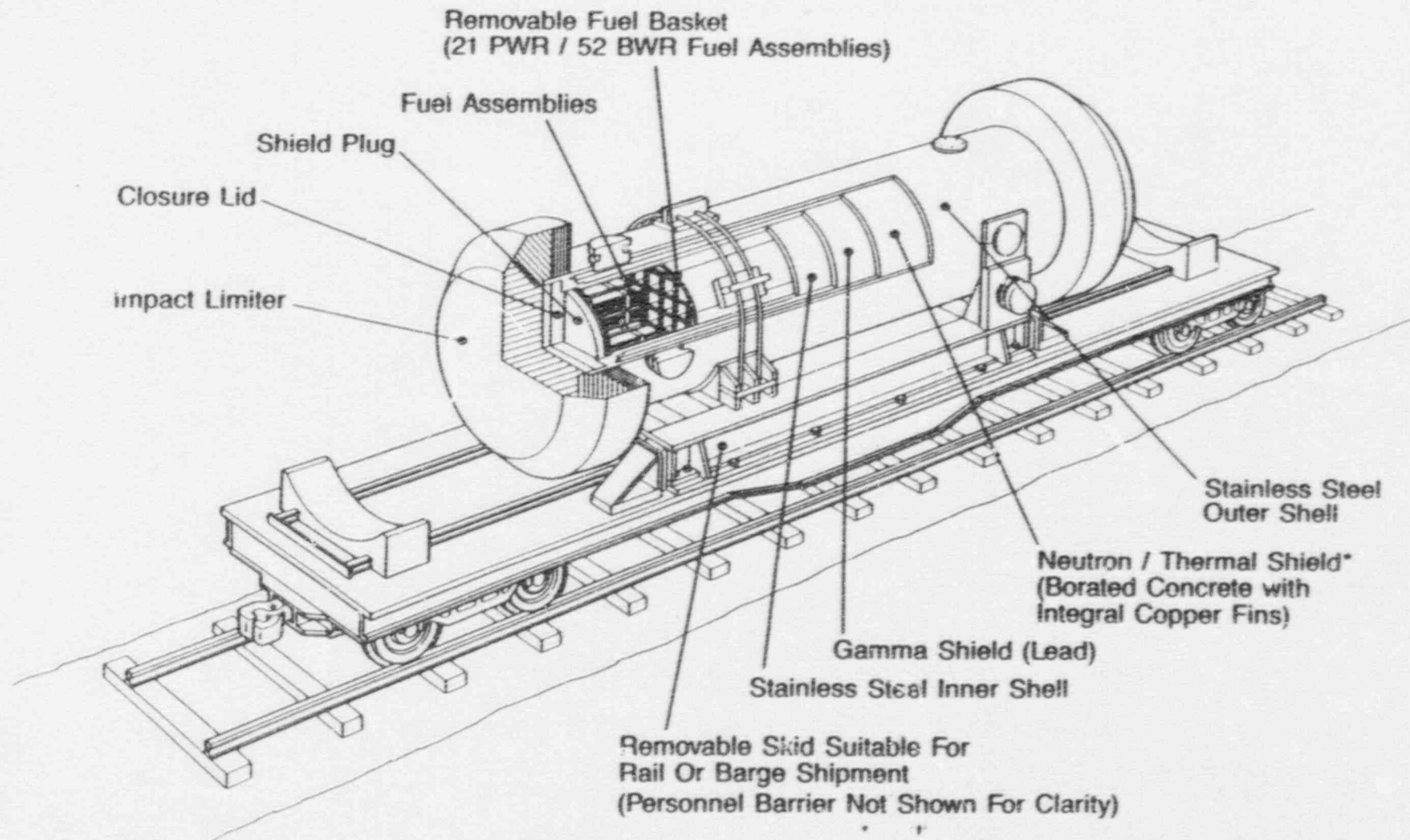
O DESIGN

- USE OF KEVLAR
- "QUICK DISCONNECT" ATTACHMENT

O TEST PROGRAM

- 1/4 SCALE VERIFICATION
- MATERIAL TESTS

BABCOCK & WILCOX BR-100 100 TON RAIL / BARGE CASK



MEETING OBJECTIVE

- PRESENTATION IS PREVIEW OF SARP MATERIAL

- WANT STAFF OPINION OF ADEQUACY OF MATERIAL

BR-100 CASK

Impact Limiter Development Program



B&W FUEL COMPANY

BR-100 IMPACT LIMITERS

- DESIGN CRITERIA
- DESIGN DESCRIPTION
- KEY MATERIAL PROPERTIES
- DEVELOPMENT TESTING
- VERIFICATION TEST PLANS

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BR-100 IMPACT LIMITERS

- IMPACT LIMITER DESIGN CRITERIA
 - LIMIT 'G' FORCES ON THE CASK BODY
 - ACCIDENT EVENT
 - LATERAL 80 G'S
 - AXIAL 60 G'S
 - NORMAL OPERATION
 - LATERAL 20 G'S
 - AXIAL 20 G'S
 - PROVIDE A LEVEL OF THERMAL PROTECTION FOR THE SEALS
 - RADIATION SHIELDING
 - NO IMPACT ON TRUNNIONS OR ATTACHMENT HARDWARE
 - MAINTAIN ATTACHMENT TO CASK BODY

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BR-100 IMPACT LIMITERS

- DESIGN CRITERIA -- ENVIRONMENTAL
 - OPERATIONAL ENVIRONMENT
 - TEMPERATURE RANGE
 - CASK SURFACE MAX. 250 F
 MIN. -20 F
 - AMBIENT MAX. 100 F
 MIN. -20 F
- OUTER ENVIRONMENT BARRIER
- SEALED SYSTEM / MOISTURE BARRIER
- CHEMICAL EXPOSURE (DURING FABRICATION)

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BR-100 IMPACT LIMITERS

- DESIGN CRITERIA -- OPERATIONAL
 - OPERATION LIFE OF 25 YEARS
 - MINIMIZE WEIGHT
 - EASE OF HANDLING / REMOTE OPERATION
 - QUICK ATTACHMENT & REMOVAL FROM CASK
 - OPERATIONAL CONSIDERATIONS

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BR-100 IMPACT LIMITERS

IMPACT LIMITER DESIGN DESCRIPTION

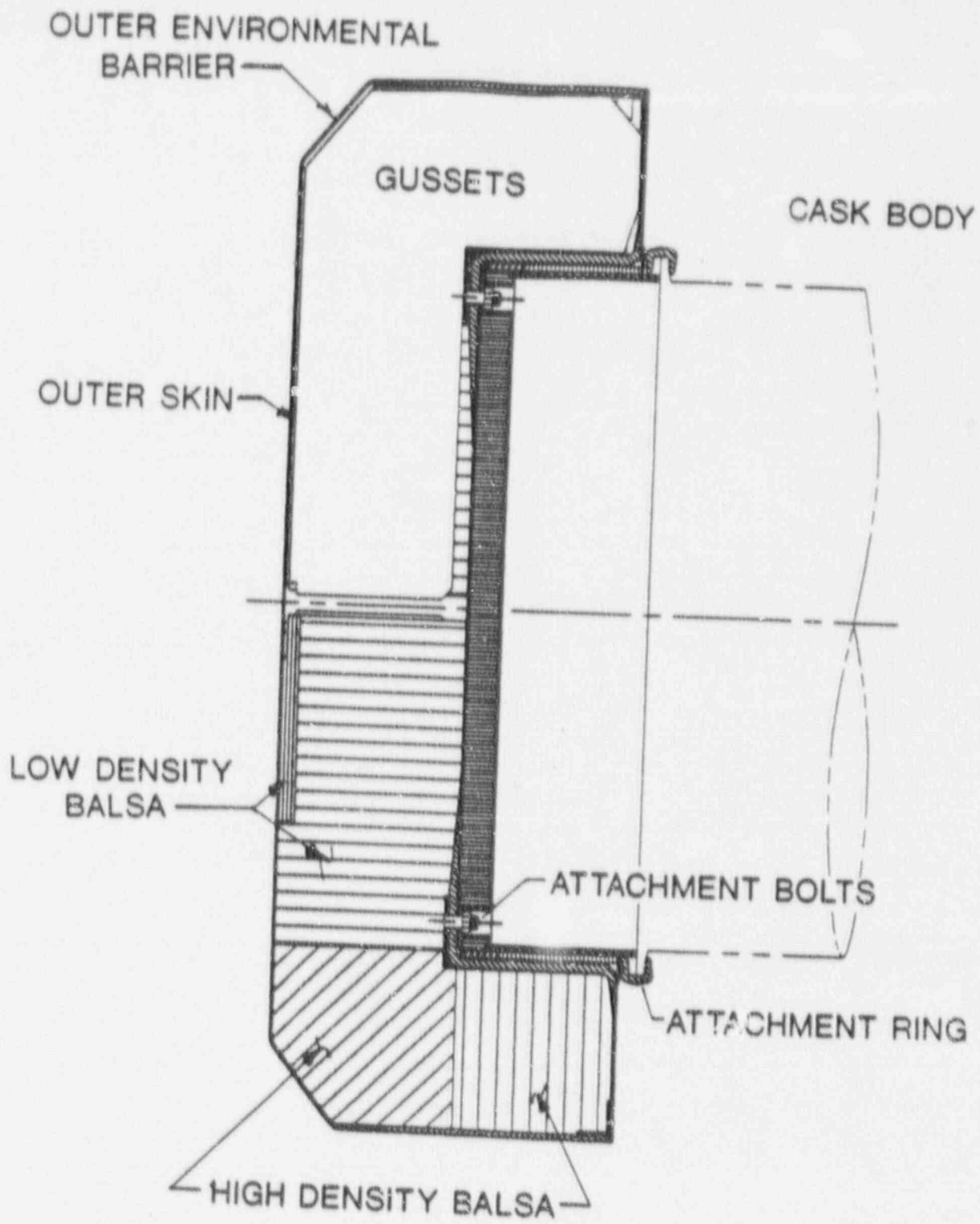
- DIMENSIONS

- MATERIALS OF CONSTRUCTION
 - KEVLAR/EPOXY COMPOSITE
 - LOW AND HIGH DENSITY Balsa
 - REDWOOD

- LIMITER DESIGN FEATURES

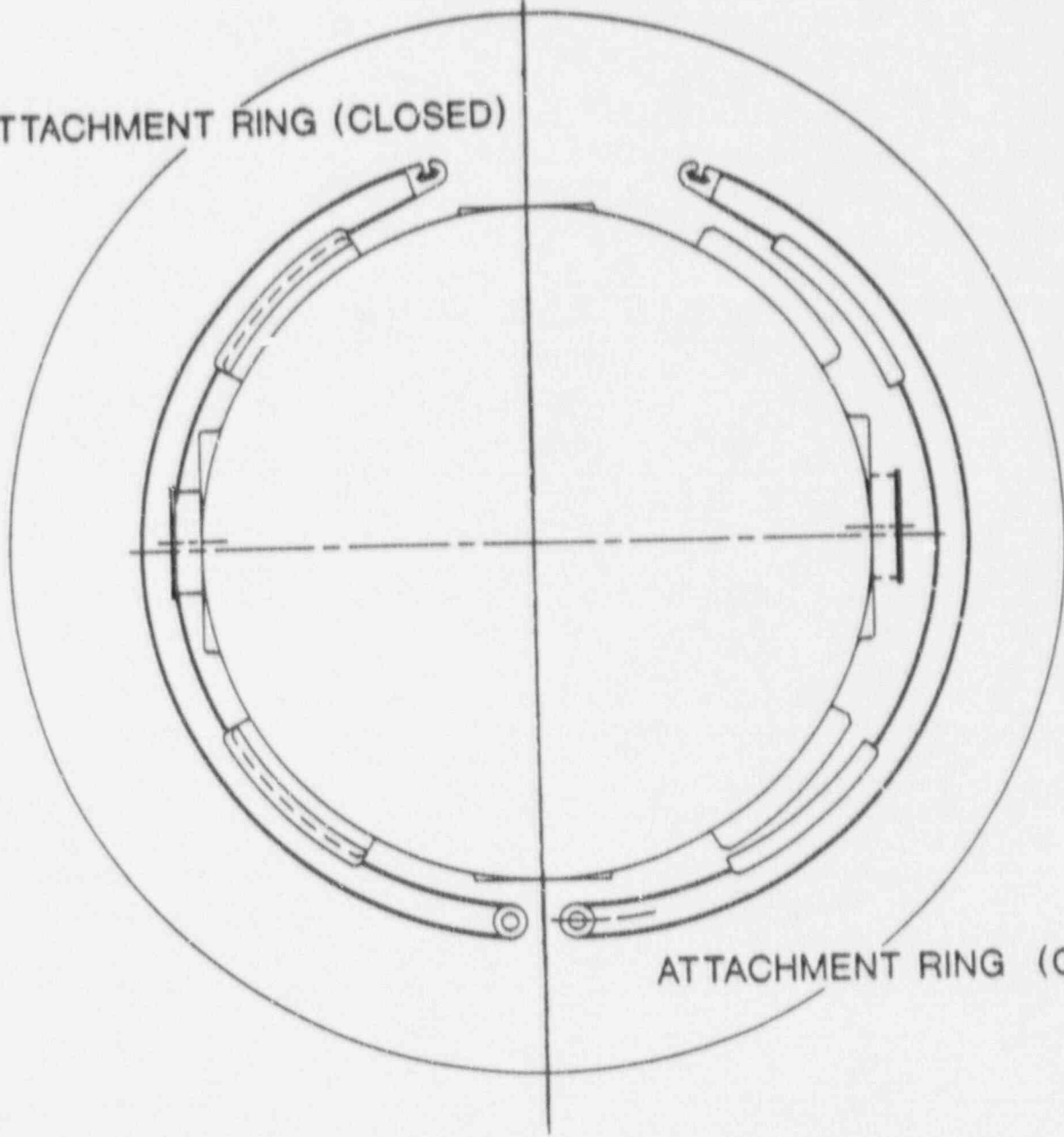
- ATTACHMENT DESIGN

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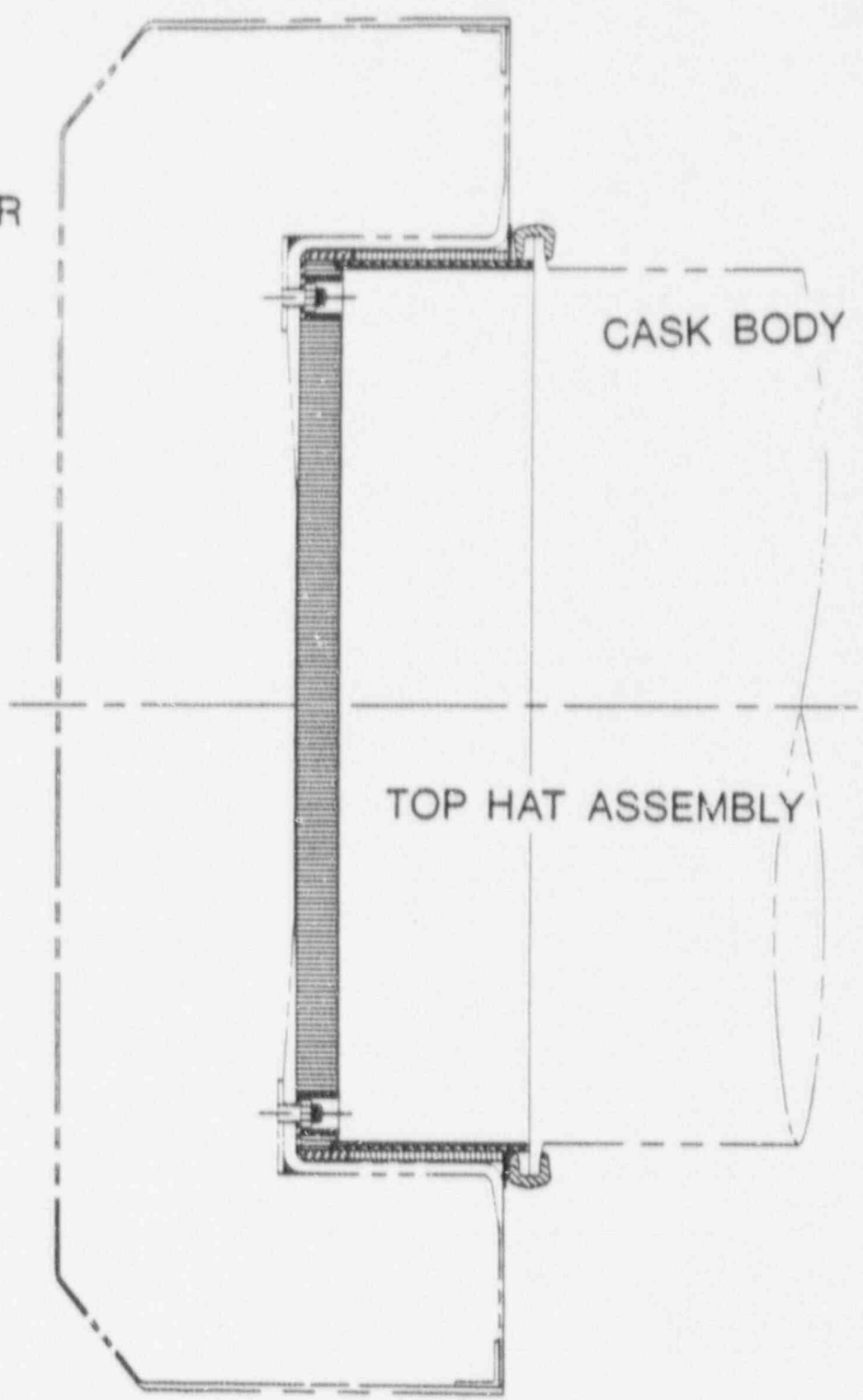
IMPACT LIMITER

ATTACHMENT RING (CLOSED)



ATTACHMENT RING (OPEN)

IMPACT LIMITER



CASK BODY

TOP HAT ASSEMBLY

BR-100 IMPACT LIMITER

MATERIAL PROPERTIES AND TESTING

- O ENERGY ABSORBER - BALSA

- O ENCASEMENT - KEVLAR/EPOXY COMPOSITE

BR-100 IMPACT LIMITER

ENERGY ABSORBING MATERIAL

BR-100 USES 7-10 AND 18-20 LB/FT³ BALSA.

BALSA:

CRUSH STRENGTH IS A FUNCTION OF:

DENSITY

TEMPERATURE

MOISTURE CONTENT

DEFORMATION (STRAIN) RATE

BR-100 IMPACT LIMITER

APPROACH TO GET MAX AND MIN CRUSH STRENGTH FOR HIGH DENSITY Balsa:

- O USE JPL AND BALTEK TEST DATA TO GET $f(T, \% H_2O)$ FOR 5-10 LB/FT³ Balsa.
- O CRUSH TEST HIGH DENSITY Balsa AT ROOM TEMPERATURE AND 7-10 % H₂O.
- O APPLY RELATIONSHIP IN $f(T, \%H_2O)$ TO HIGH DENSITY CRUSH TEST DATA.
- O PERFORM HIGH STRAIN RATE CRUSH TESTS

RESULT:

HIGH DENSITY Balsa CRUSH STRENGTH AS A FUNCTION OF TEMPERATURE, %H₂O DEFORMATION RATE.

BR-100 IMPACT LIMITER

ENCASEMENT MATERIAL

- BR-100 USES KEVLAR FIBERS IN A TOUGHENED EPOXY RESIN MATRIX.
- PREPREG KEVLAR/EPOXY IS PROCURED AS COMMERCIAL GRADE AND DEDICATED AS SAFETY RELATED.

BR-100 IMPACT LIMITER

COMPOSITE MATERIAL TESTS

- O CHARACTERIZATION TESTS: PERFORMED ON FIRST MATERIAL PROCURED TO GET MECHANICAL AND PHYSICAL PROPERTIES OF PREPREG AND COMPOSITE.

- O QUALIFICATION TESTS: QUALIFIES MATERIAL FOR BR-100 SERVICE.

- O CERTIFICATION TESTS: PERFORMED ON SUBSEQUENTLY PROCURED MATERIAL TO CERTIFY AS SAFETY-RELATED.

BR-100 IMPACT LIMITER

CHARACTERIZATION AND CERTIFICATION TESTS

- O MECHANICAL PROPERTIES (PERFORMED ON CURED COMPOSITE, TESTED AT ROOM TEMPERATURE).
 - TENSILE STRENGTH AND MODULUS - FIBER DEPENDENT
 - INTERLAMINAR SHEAR STRENGTH - RESIN DEPENDENT
 - COMPRESSIVE STRENGTH - DEPENDENT ON FIBER, RESIN AND INTERFACE

- O PHYSICAL PROPERTIES (PERFORMED ON PREPREG)
 - RESIN CONTENT
 - VOLATILE CONTENT
 - RESIN PERCENT FLOW

BR-100 IMPACT LIMITER

QUALIFICATION TESTS

- O MECHANICAL PROPERTIES (PERFORMED ON FULLY CURED COMPOSITE).
 - TENSILE STRENGTH AND MODULUS
(AT -20°F AND 300°F)
 - INTERLAMINAR SHEAR
(AT -20°F AND 300°F)
 - COMPRESSION STRENGTH
(AT -20°F AND 300°F)

- O ENVIRONMENTAL BEHAVIOR
 - THERMAL CYCLED PLUS MECHANICALS
 - ACCELERATED AGING PLUS MECHANICALS

CONCLUSION

- (1) Balsa min and max crush strength will be determined using JPL, Baltek and B&W test data.

- O Kevlar/epoxy composite will be characterized and qualified by a series of mechanical, physical and environmental tests.

BR-100 IMPACT LIMITERS

DEVELOPMENT TESTING

- DESIGN ANALYSIS
 - ILAN COMPUTER CODE
- "DESIGN BY TEST" APPROACH
- TESTING PROGRAMS
 - SCOPING TESTS
 - ENGINEERING TESTS
 - COMPONENT TESTING (DESIGN DEVELOPMENT)
 - STATIC FORCE-DISPLACEMENT TESTS
 - MATERIAL TESTING
- VERIFICATION TESTING (LICENSING)

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BR-100 IMPACT LIMITERS

- SCALE MODEL IMPACT LIMITER DESIGN *Later meeting*

- VERIFICATION TEST MODEL
 - QUARTER SCALE LIMITER CONFIGURATION

 - LIMITER-TO-CASK ATTACHMENT CONFIGURATION

 - SCALING CONSIDERATIONS *Later meeting*

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BR-100 IMPACT LIMITERS

- ENGINEERING TESTS
 - STATIC FORCE-DISPLACEMENT TESTS
 - SIDE LOADING
 - LOW ANGLE OBLIQUE (SLAPDOWN)
 - OBLIQUE (CG OVER CORNER)
- DATA PACKAGE
 - FORCE-DISPLACEMENT CURVE AT VARIOUS ANGLES

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BR-100 IMPACT LIMITERS

- VERIFICATION TESTING

- 30 FOOT DROP TESTS
 - SLAPDOWN @ TEMP. 240 F
 - BOTTOM END IMPACT @ AMBIENT TEMP.
 - OBLIQUE @ TEMP. -20 F

- PUNCTURE TESTS
 - CASK BODY / SIDE DROP
 - CLOSURE LID / CENTER
 - CLOSURE LID / COVER PLATE

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COMPANY*

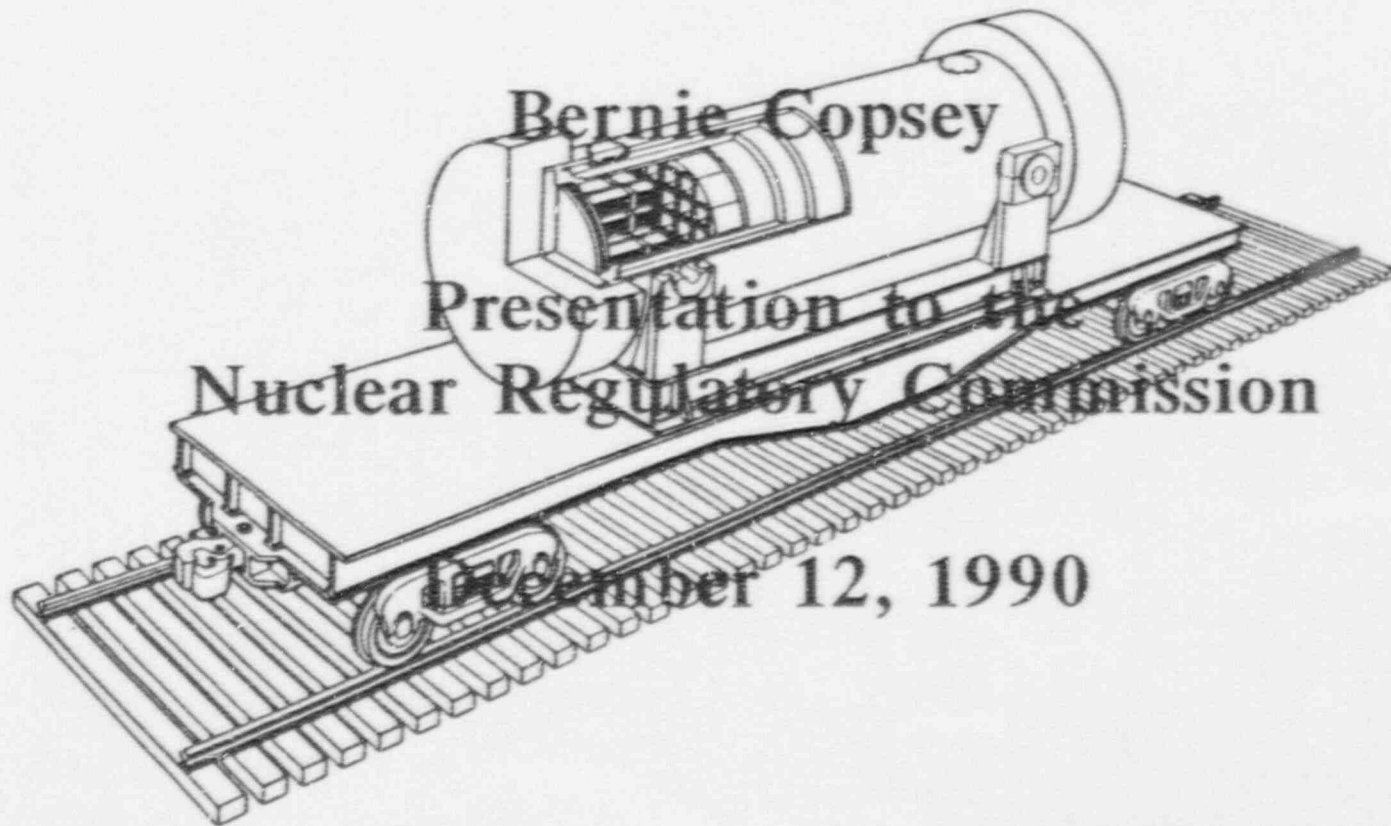
BR-100 IMPACT LIMITERS

- VERIFICATION TESTS
 - DATA PACKAGE -- REGULATORY
HYPOTHETICAL ACCIDENT TESTS
 - DEFORMATIONS
 - TEMPERATURE OF CASK SURFACE
 - CASK BODY ACCELERATION

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BR-100 CASK

Thermal Analyses



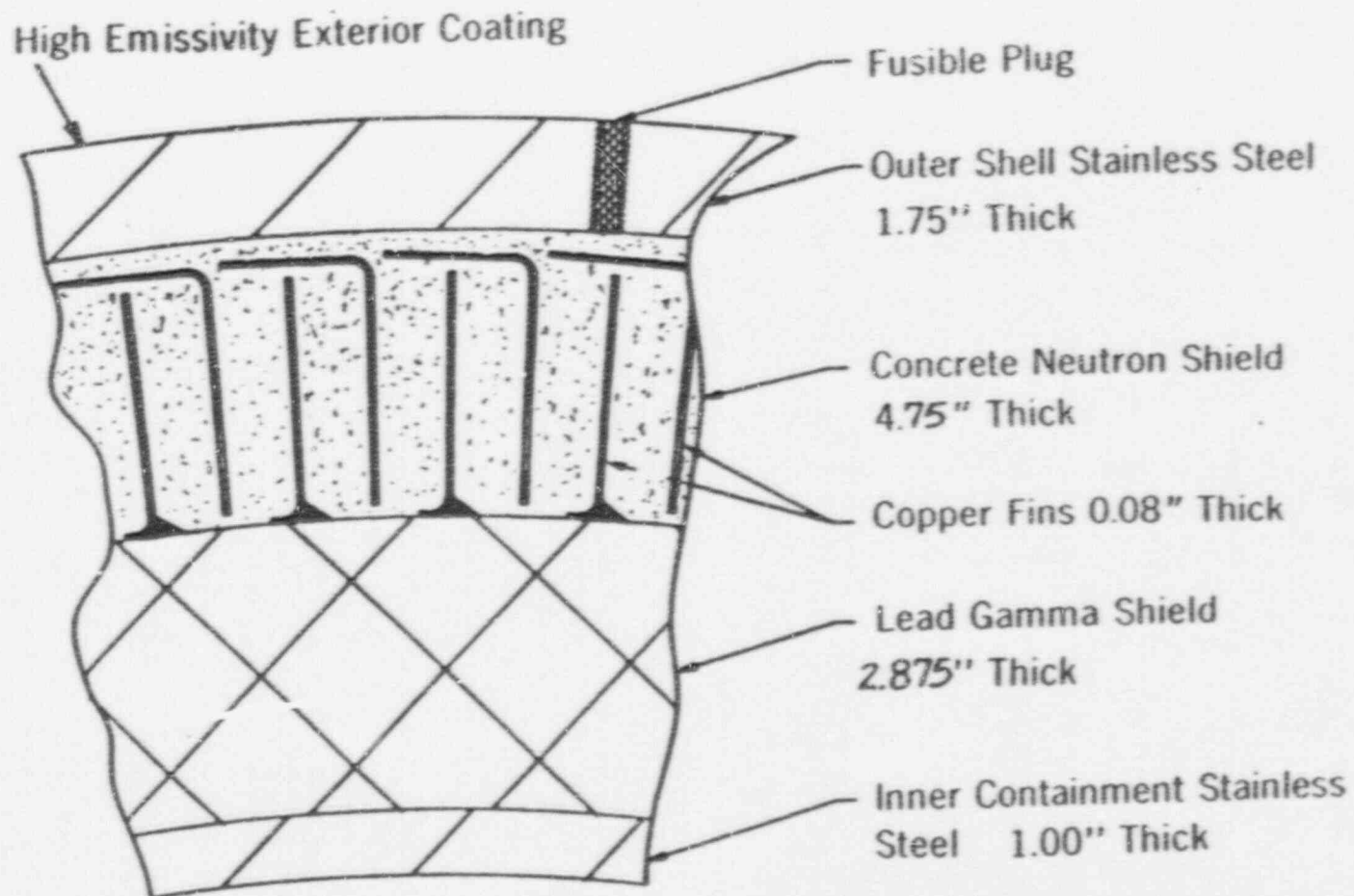
B&W Fuel Company

BR-100 Thermal Analyses

- Model Description
- Thermal Enhancements in the Design
- Normal Operation
 - Basket cross-section
 - Cask longitudinal section
- Hypothetical Accident Analyses
 - Thermal testing
 - Basket cross-section
 - Cask longitudinal section
- Conclusion

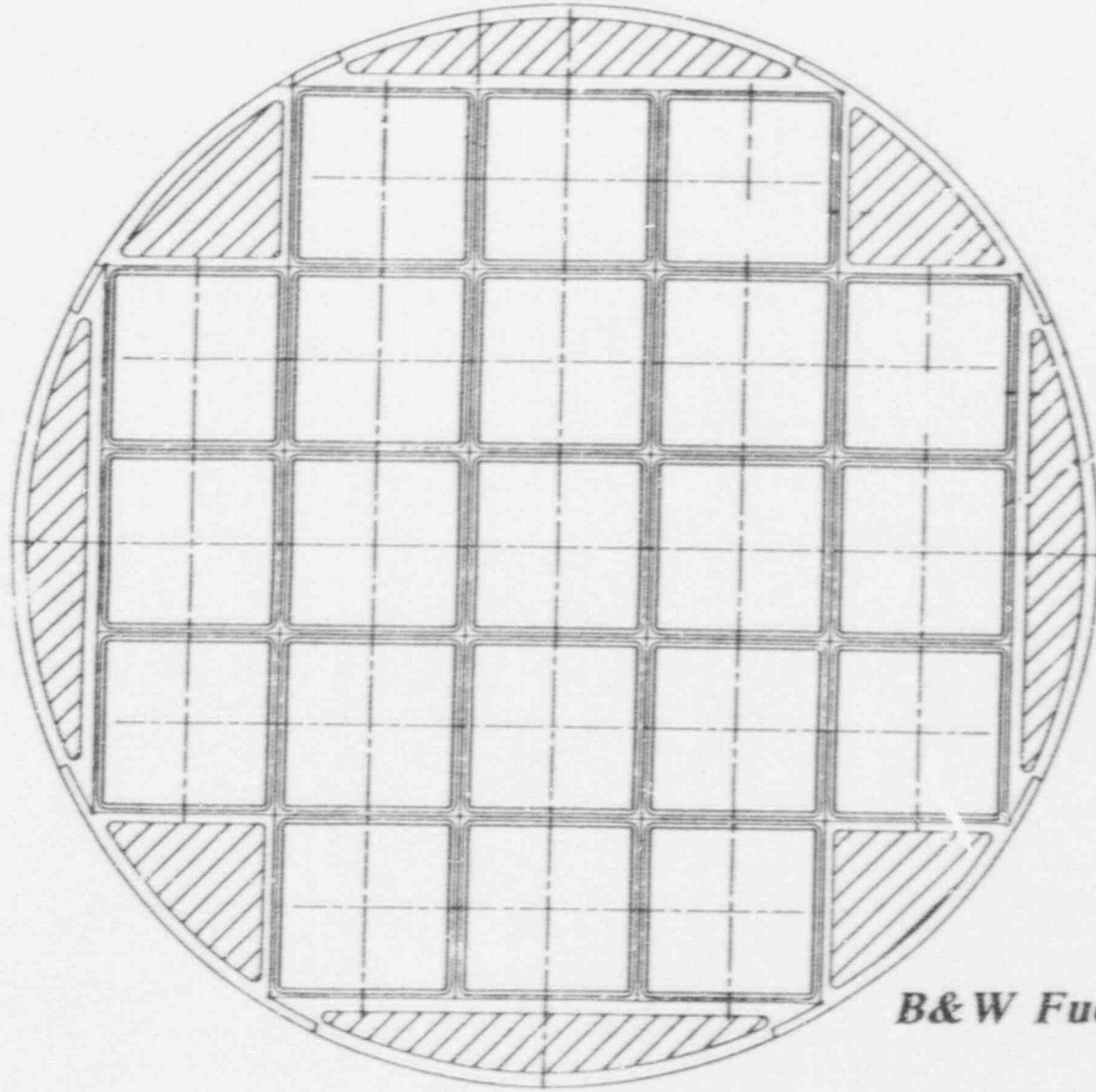
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BR-100 Multi-layer Cask Wall



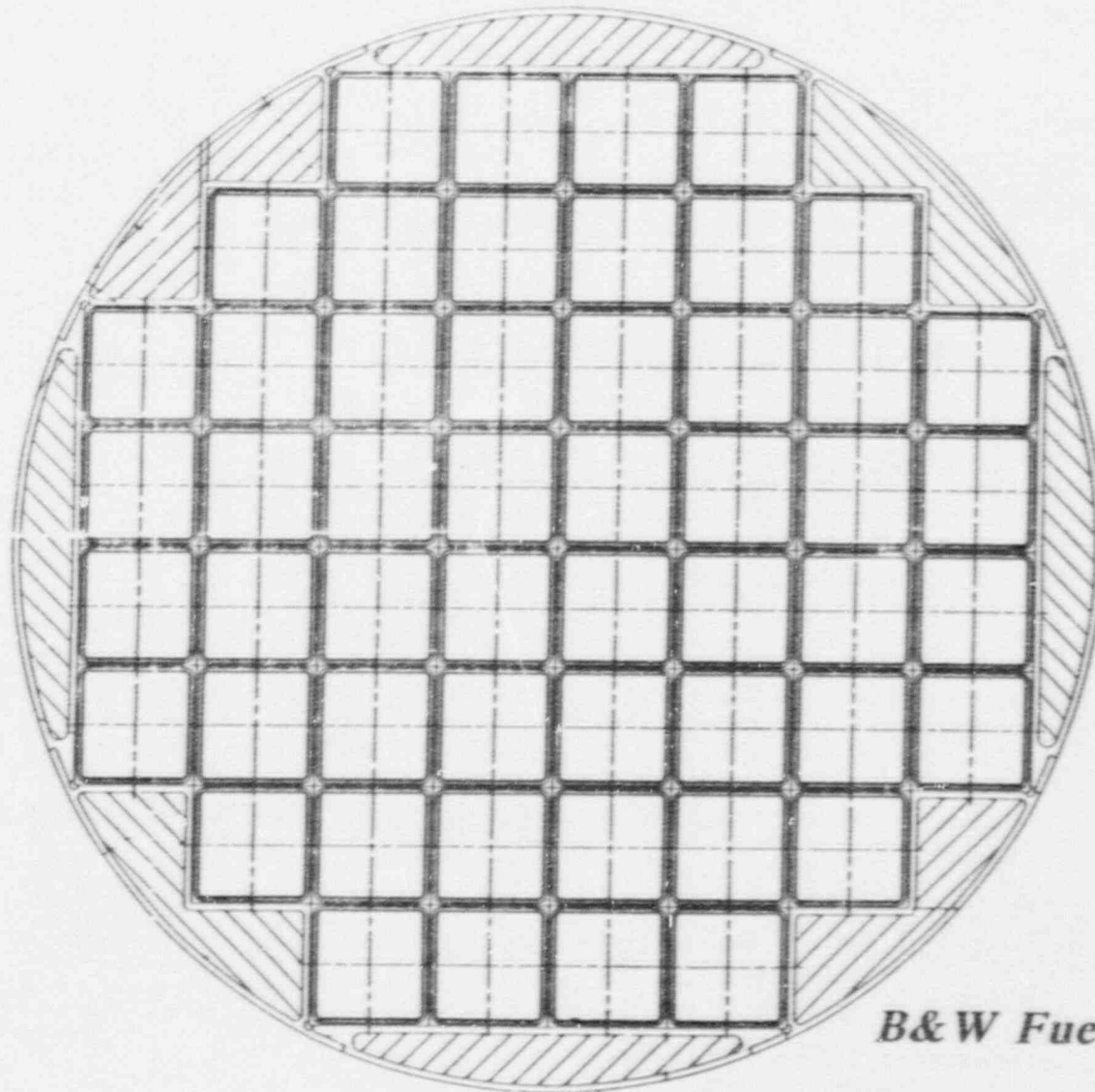
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BR-100 Cask Basket PWR Configuration



B&W Fuel Company

BR-100 Cask Basket BWR Configuration



B&W Fuel Company

BR-100 Thermal Enhancements in the Design

- White paint exterior coating
- Robatel concrete-copper fin thermal/neutron shield
- Helium fill gas
- Copper/stainless steel laminate in basket

B&W Fuel Company

Thermal Analyses Assumptions

- Maximum temperatures occur near the axial midpoint
- Cask wall heat transfer is primarily one-dimensional
- Basket heat transfer is two-dimensional
- Cladding temperature calculated using Wooten-Epstein equation
- Cask inner wall-to-former gap is 100 mils

Cask Exterior Paint

- Clean white paint
 - Solar band $\alpha = 0.16$
 - Infrared band $\epsilon = 0.89$
- Dirty white paint
 - Solar band $\alpha = 0.30$
 - Infrared band $\epsilon = 0.89$
- There is little data on the effect of:
dirt, scratches, nicks, corrosion, weathering

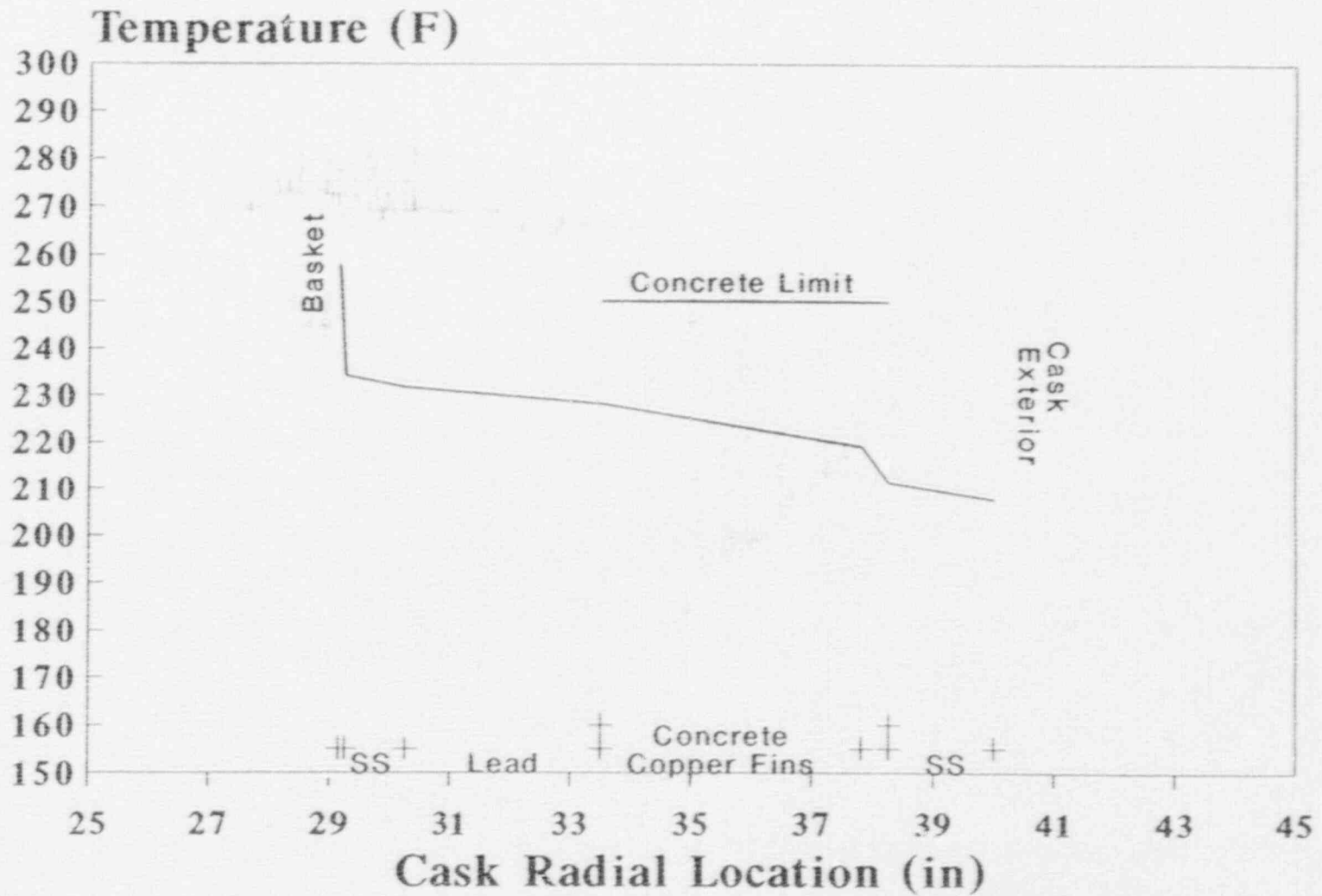
Personnel Barrier

- All of the thermal analyses assumed no personnel barrier
- The current personnel barrier will shade the cask and allow adequate ventilation
- Sensitivity studies indicate the personnel barrier will improve thermal performance
- The maximum personnel barrier temperature is less than 170 F

Temperature Design Limits For Normal Operation

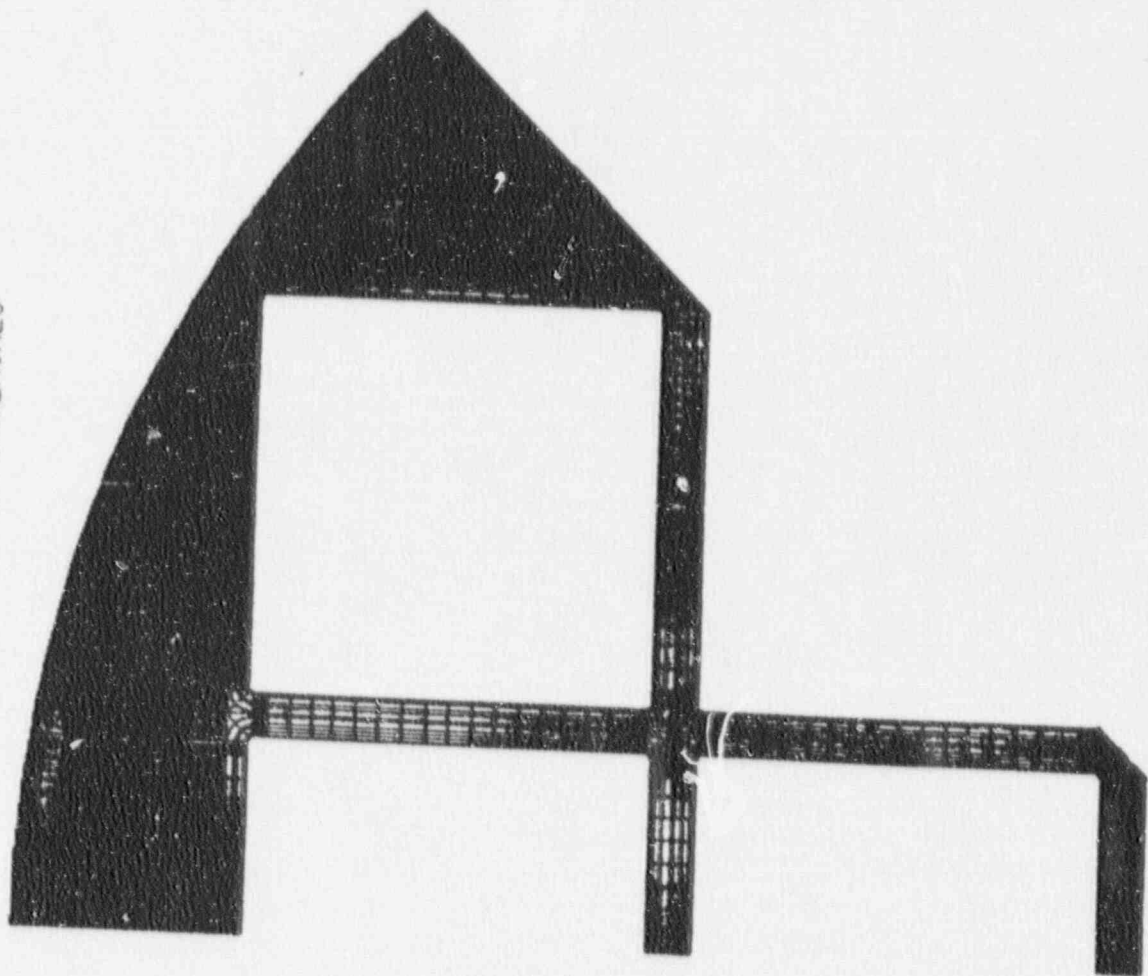
• Personnel Barrier	180 F
• Concrete	250
• Kevlar/Epoxy	250
• Closure Lid Seal	300
• Lead	621
• Fuel Cladding	680

PWR Cask Temperature Distribution

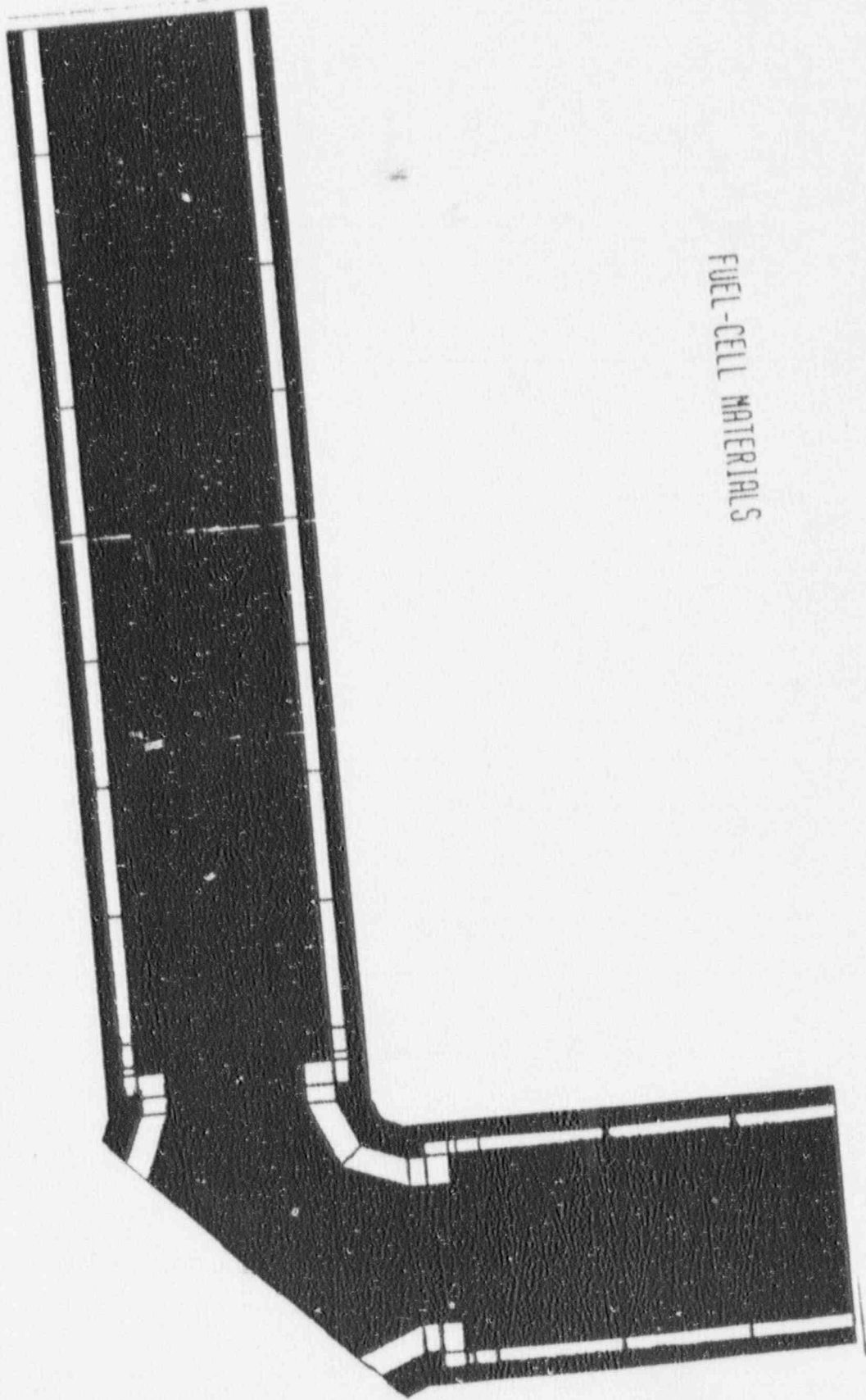


B&W Fuel Company

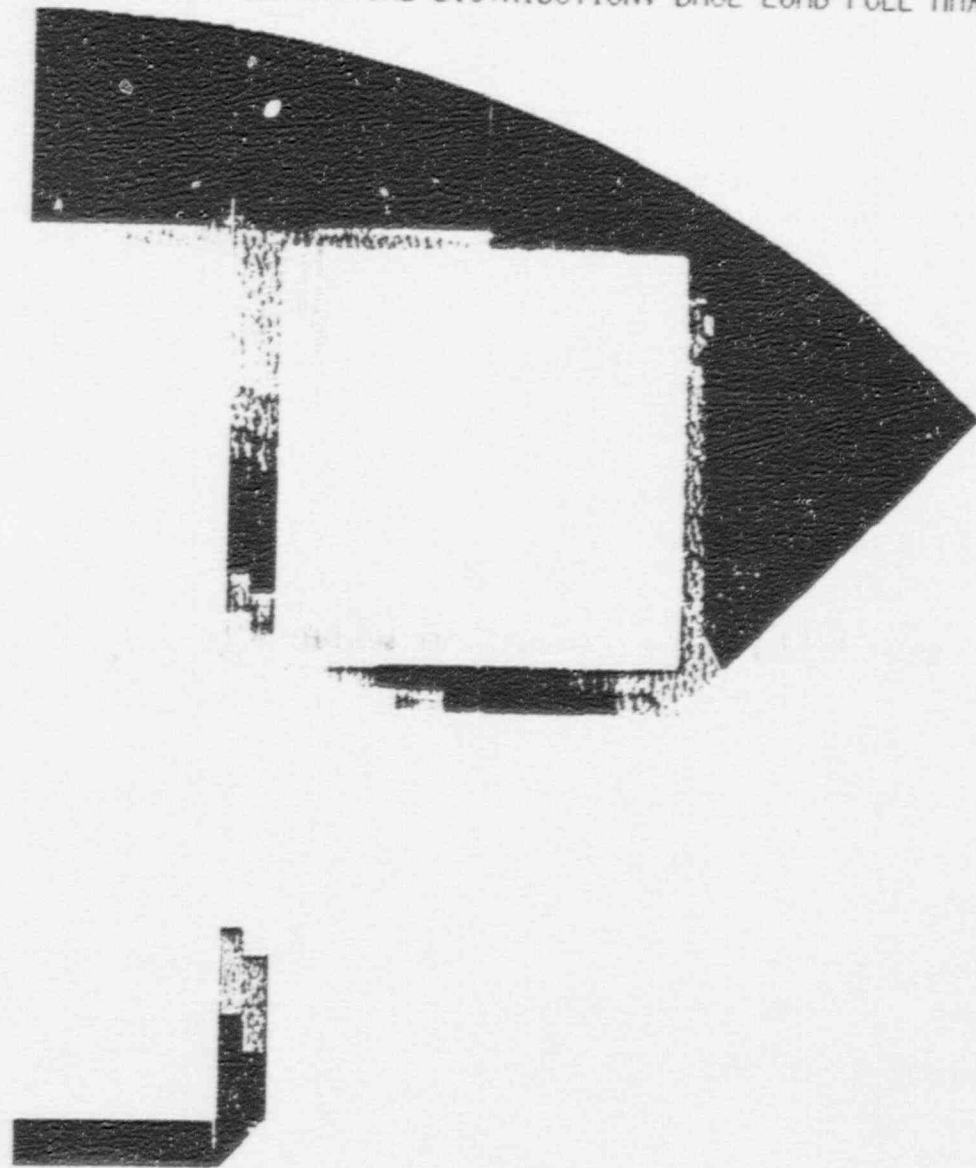
BASKET CROSS-SECTION MATERIALS



FUEL-CELL MATERIALS

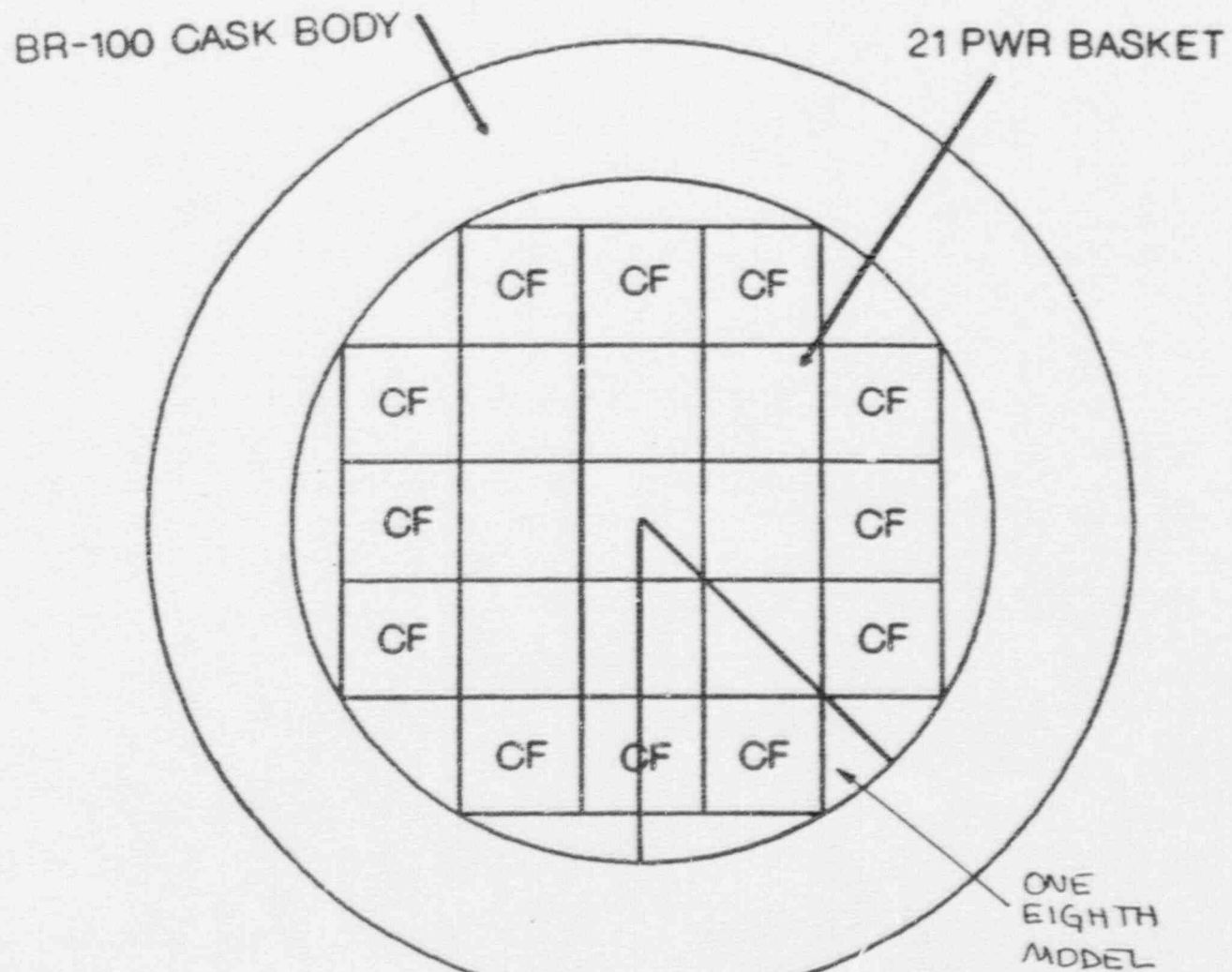


BASKET CROSS-SECTION TEMPERATURE DISTRIBUTION, BASE-LOAD FUEL MAX TEMP



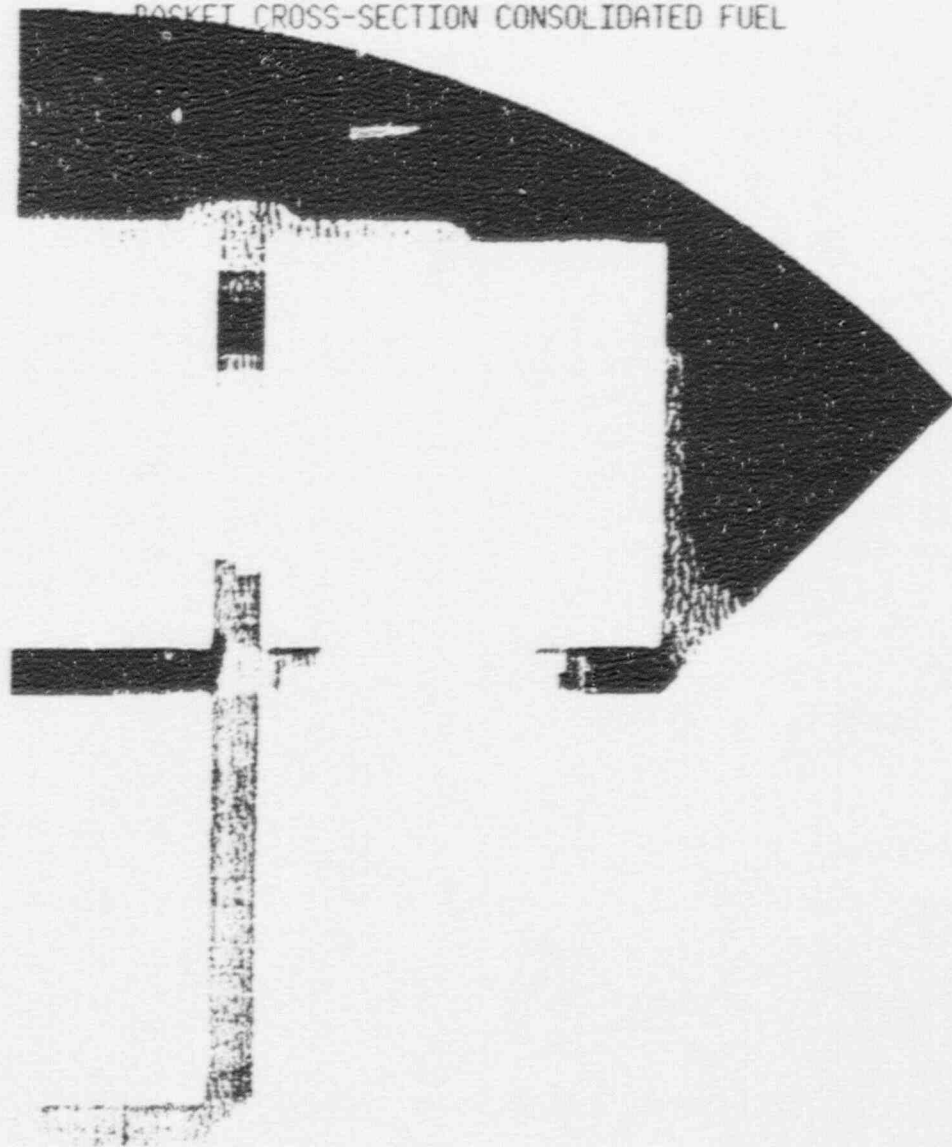
356.5
350.9
345.3
339.7
334.2
328.6
323.0
317.5
311.9
306.3
300.8
295.2
289.6
284.1
278.5
272.9

Consolidated Fuel Model



B&W Fuel Company

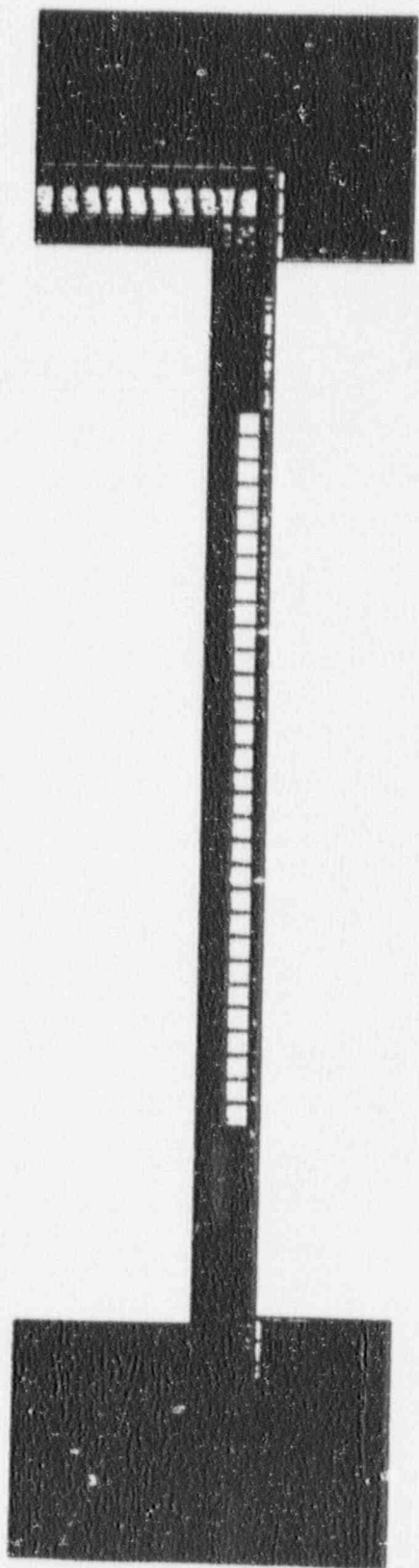
BASKET CROSS-SECTION CONSOLIDATED FUEL



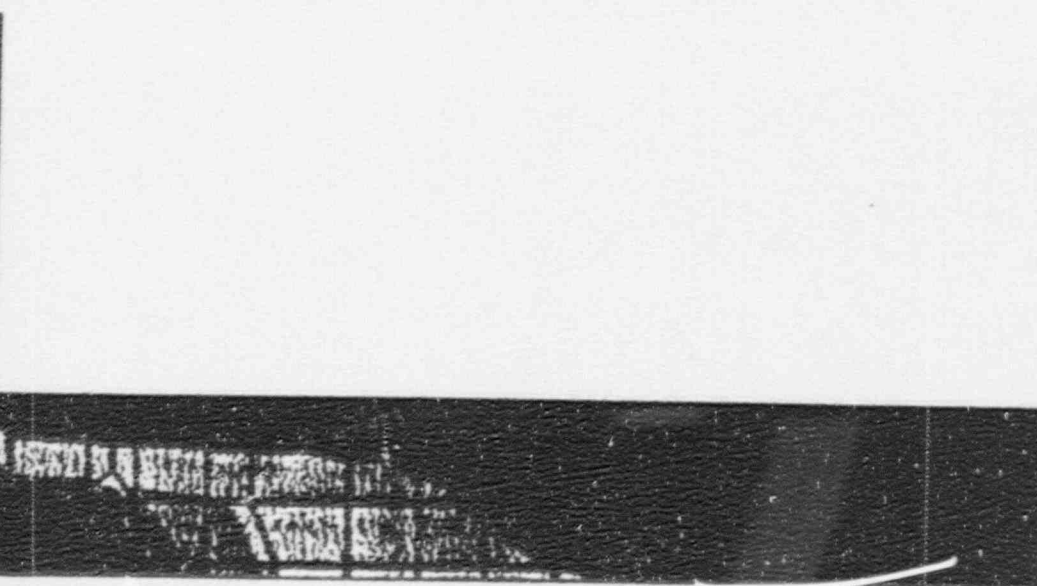
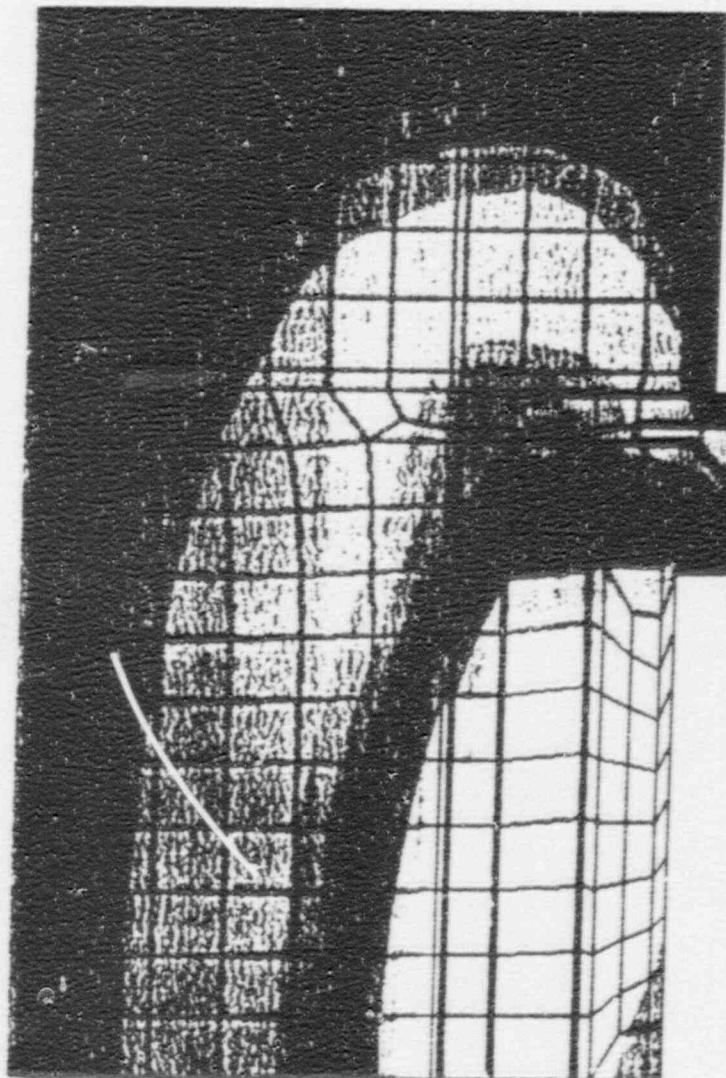
330.168
327.462
324.757
322.052
319.347
316.642
313.937
311.231
308.526
305.821
303.116
300.411
297.705
295.000
292.295
289.590

Longitudinal Section Model

- Peak component temperatures
 - Seals
 - Lead
 - Kevlar/Epoxy
- Thermal stress
 - Shield plug
 - Closure lid
 - Cask wall



TEMPERATURE DISTRIBUTION UPPER CASK LONGITUDINAL SECTION NORMAL OPERATION



265.
260.
255.
250.
245.
240.
235.
230.
225.
220.
215.
210.
205.
200.
195.
189.

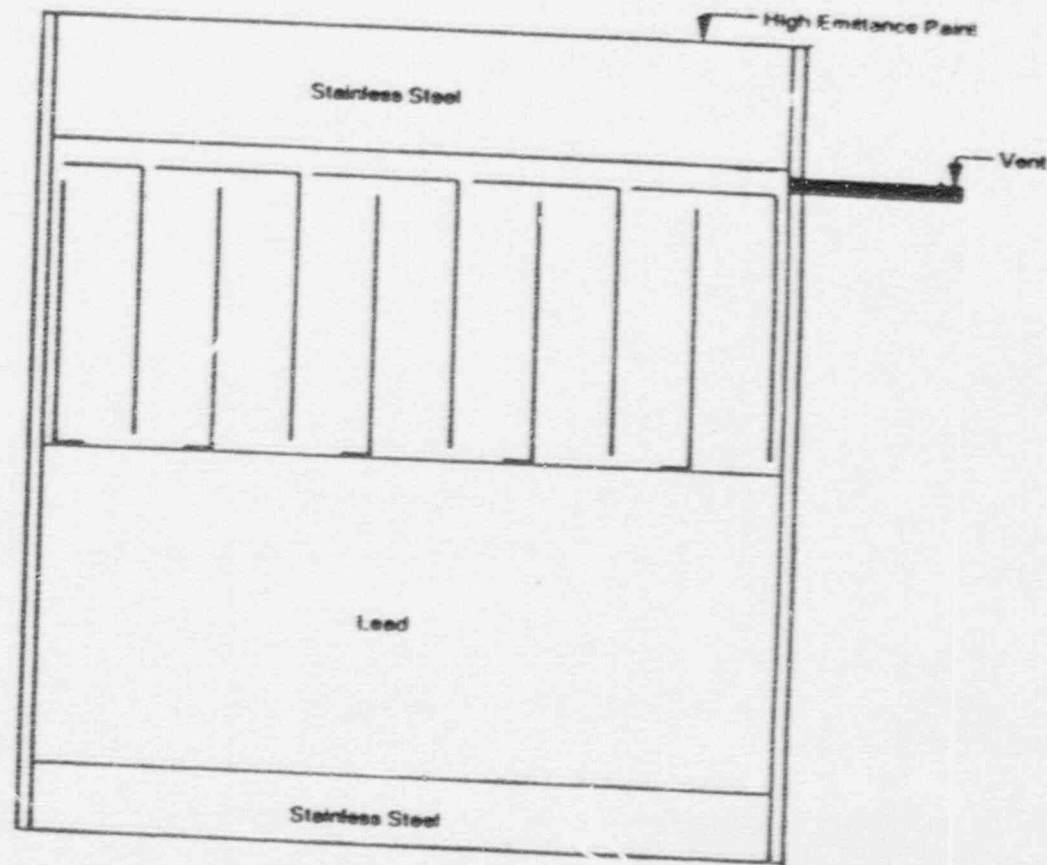


Thermal Transient Testing

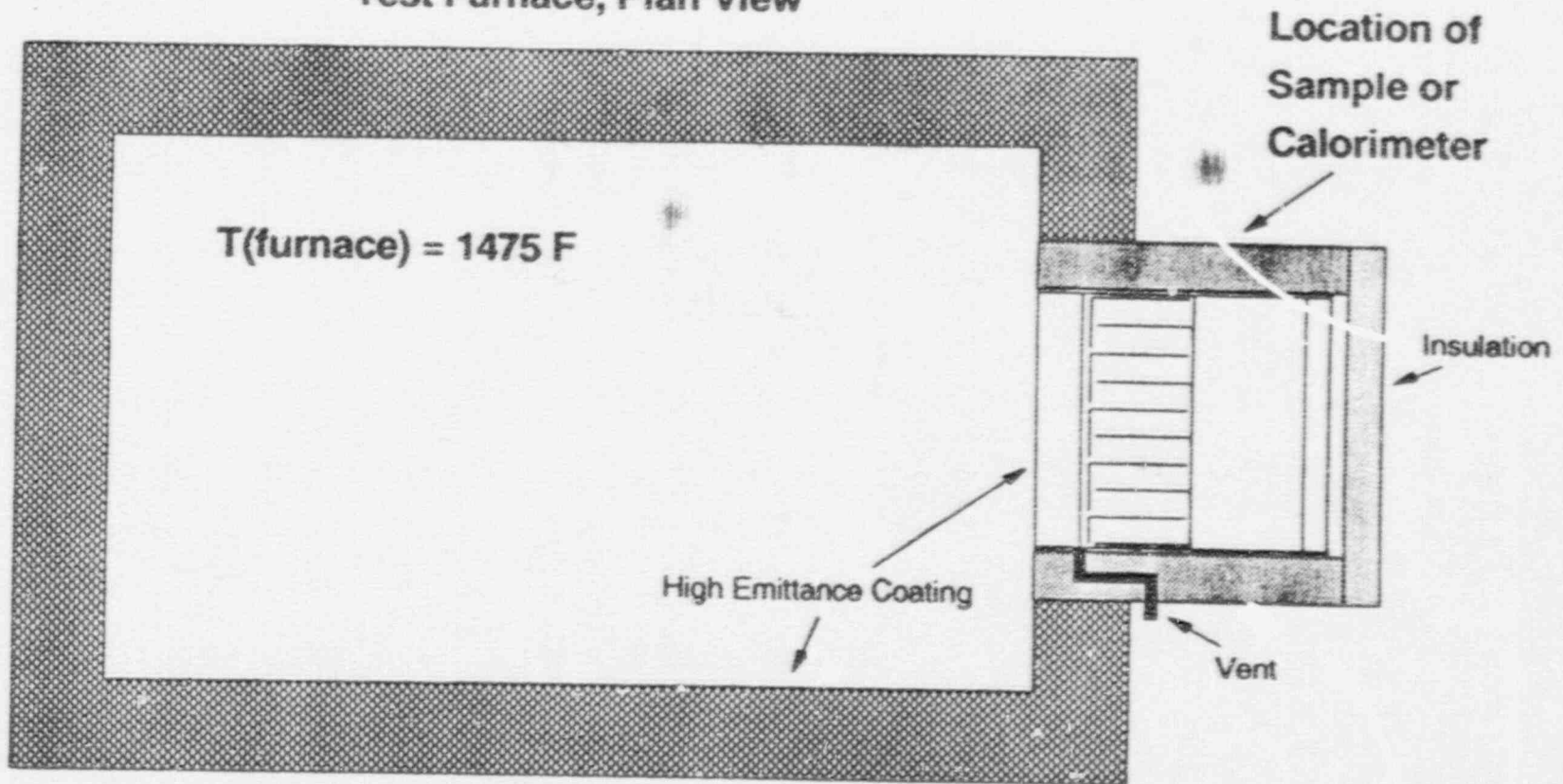
- Pre-test thermal conductivity measurement
- Establish realistic thermal gradient
- Exposure to 1475 F heat flux for 30 minutes
- Controlled cooldown
- Post-cooldown steady-state thermal conductivity measurement
- Post-cooldown destructive analysis

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Hypothetical Accident Thermal Test Section



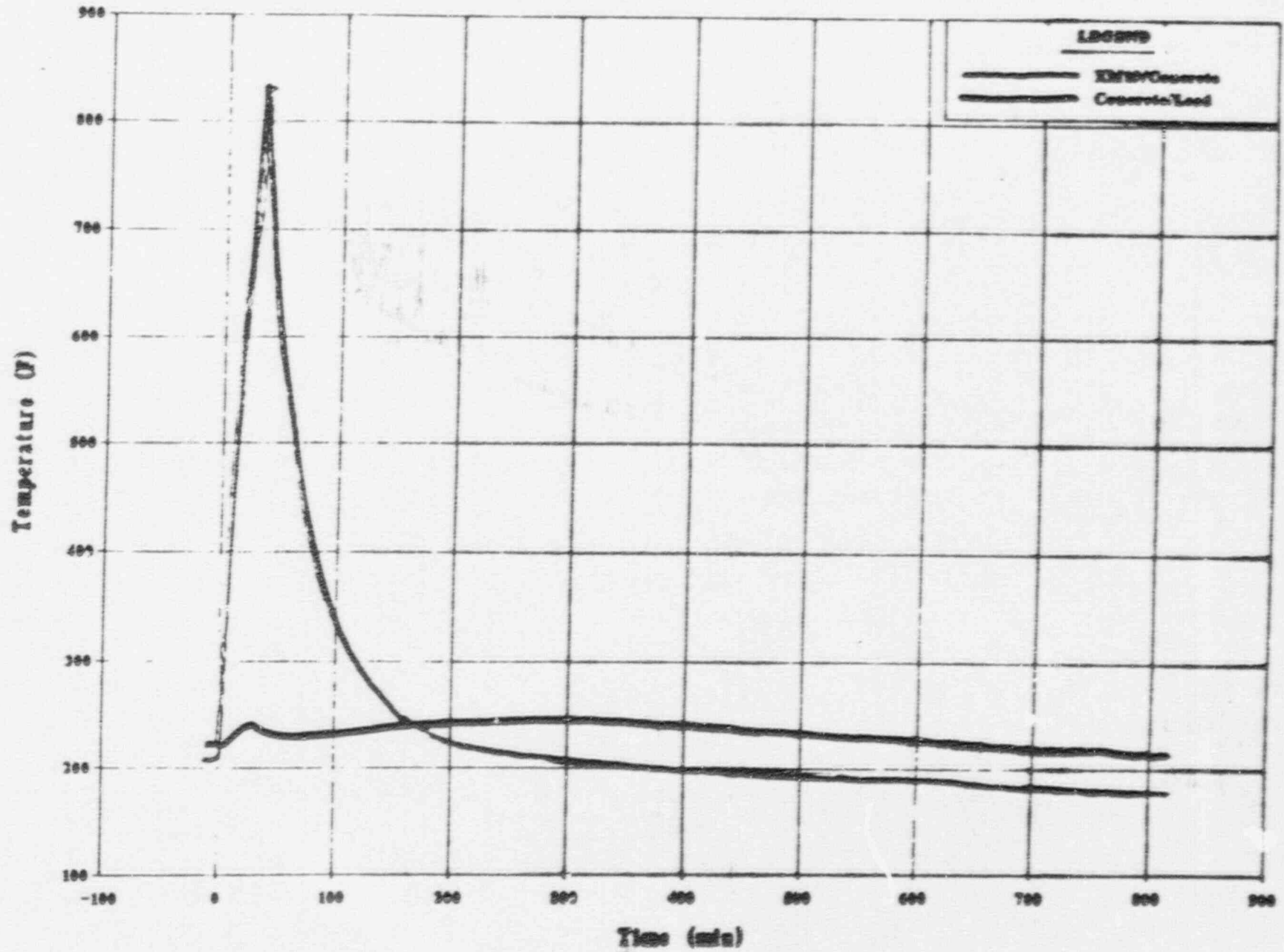
Test Furnace, Plan View



-91-

Figure 4. HAT Test Configuration

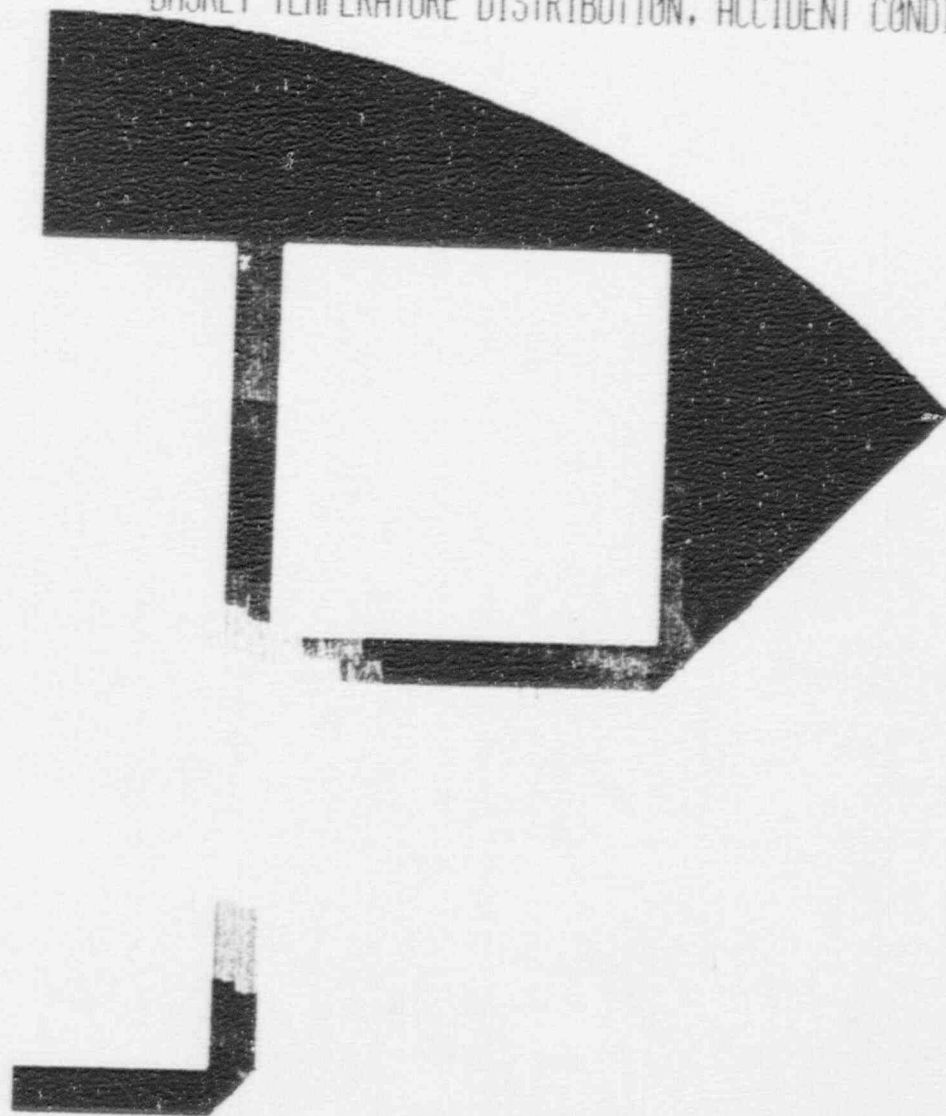
ARC Fire Test Temperature Response Channel 70 and 64



Thermal Design Limits for the Hypothetical Fire Accident

- Cladding temperature limit of 680 F
- Lead temperature limit of 621 F
- Closure lid seal temperature limit of 300 F
- Acceptable thermal stress and temperatures for structural analyses

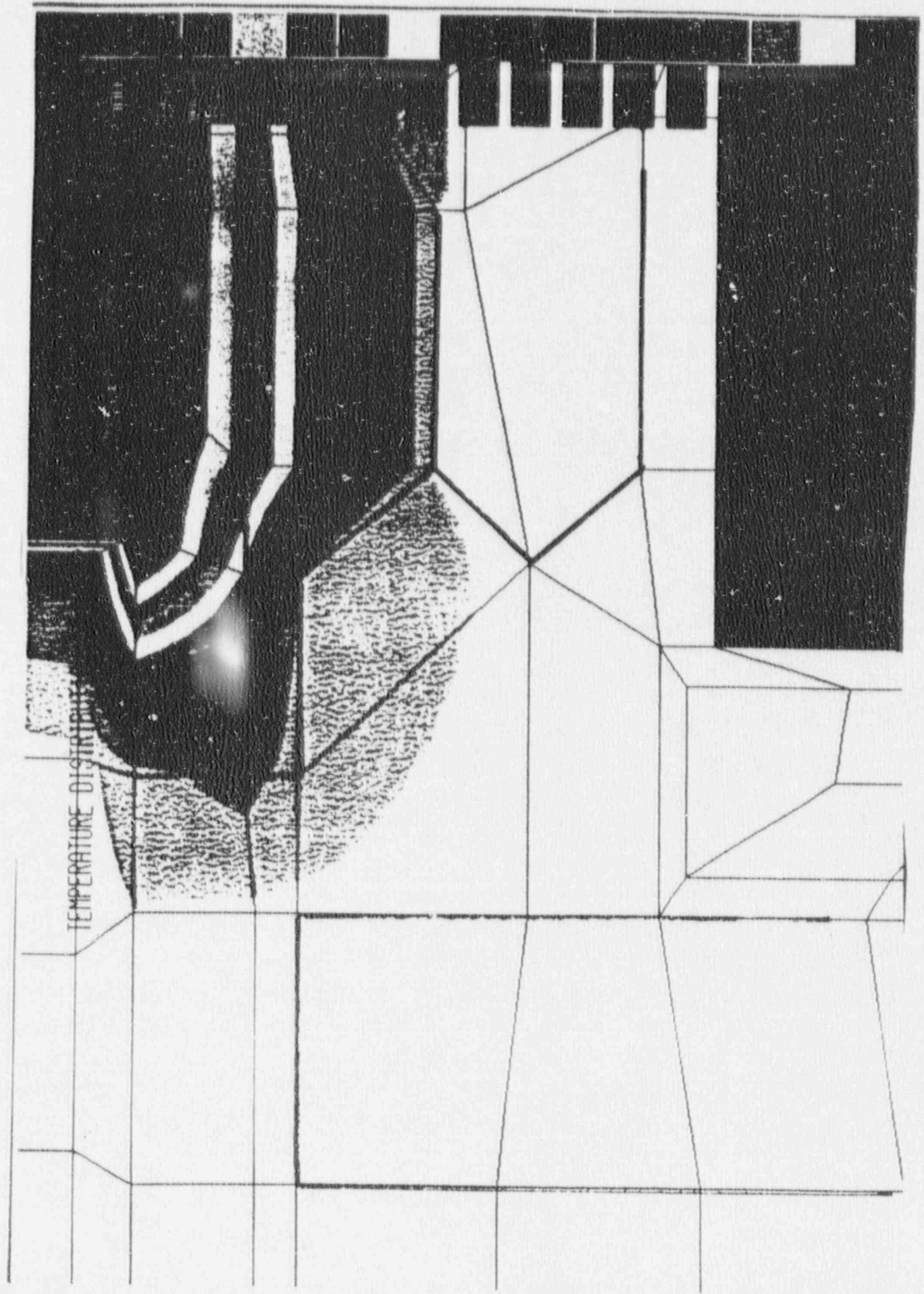
BASKET TEMPERATURE DISTRIBUTION, ACCIDENT CONDITIONS



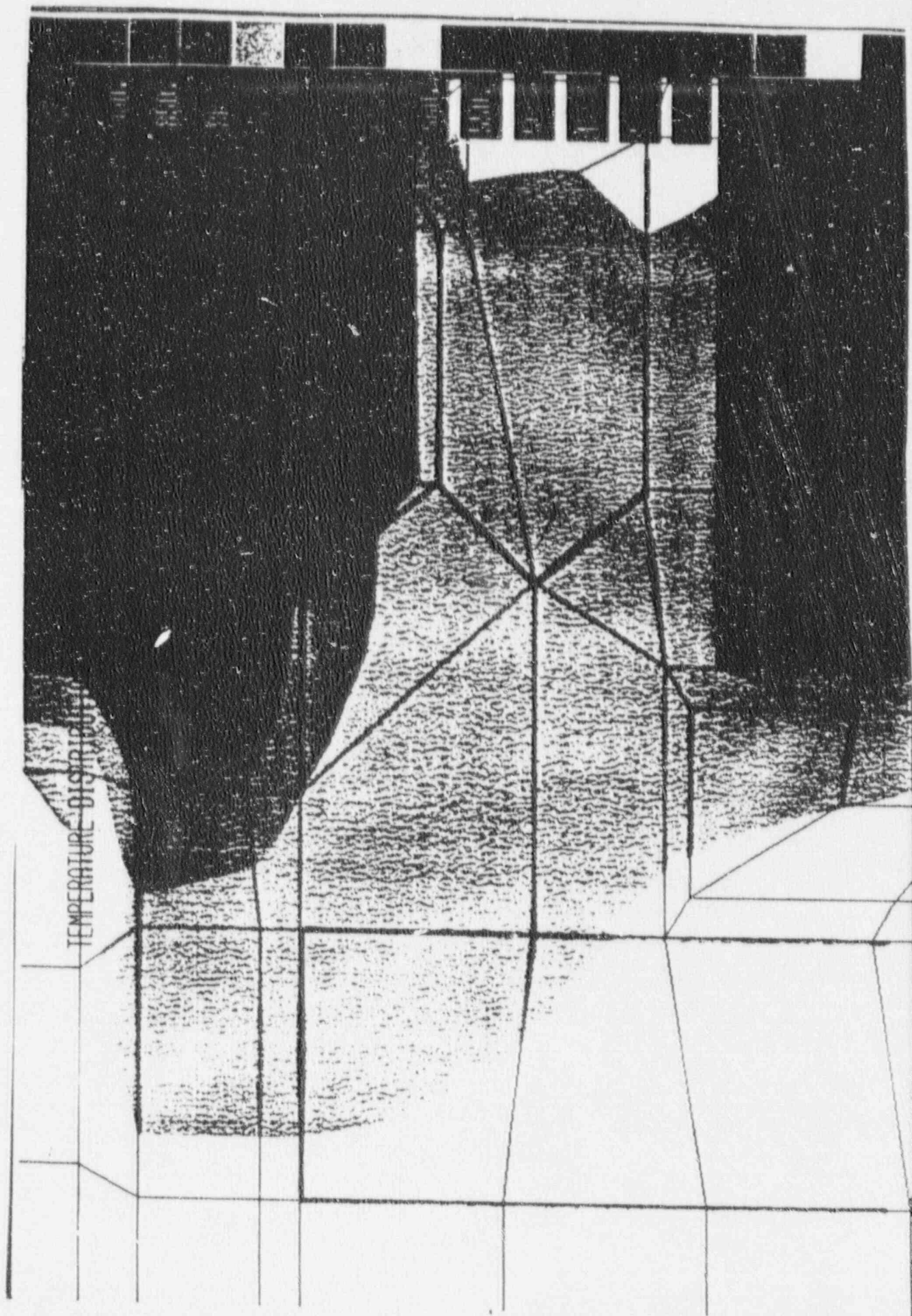
365.584
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355.242
350.071
344.900
339.729
334.558
329.387
324.216
319.045
313.874
308.703
303.532
298.361
293.190
288.019

Longitudinal Section Model

- Impact limiter crushed by 80%
- Boundary conditions
 - All external temperatures from hypothetical accident thermal test
 - Concrete/lead interface temperature is from the HAT test
- Initial temperatures from the time zero results



TEMPERATURE DISTRIBUTION



Conclusions

- The temperatures in the basket and cask are less than the temperature limits for
 - PWR normal operation
 - PWR hypothetical accident
 - BWR normal operation
 - BWR hypothetical accident
- The thermal analyses have been completed with documentation and QA remaining