

H035



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September 30, 1982

Dennis M Crutchfield, Chief Operating Reactors Branch No 5 Nuclear Reactor Regulation US Nuclear Regulatory Commission Washington, DC 20555

DOCKET 50-155 - LICENSE DPR-6 -BIG ROCK POINT PLANT - SEP TOPIC III-2, WIND AND TORNADO LOADINGS

Enclosed is Consumers Power Company response to the NRC staff request for additional information regarding SEP Topic III-2, "Wind and Tornado Loadings", for the Big Rock Point Plant. The attached report replies to three (3) staff questions. Please note that the attached Appendix C, which incorporates part of question #1 response, has been revised due to results of a recent re-evaluation of the capability of the ventilation-stack to resist wind loadings, and therefore supersedes the previous Appendix C transmitted in our August 3, 1982 correspondence.

One (1) copy of a Specification and drawing for the reinforced concrete ventilation stack is also enclosed (questions #1 and 2).

It should be noted that the information requested by the staff on the cross-section of the south end of the control room wall (question #3) are shown on a security drawing which is exempt from public disclosure; therefore, the drawing is not enclosed. However, the Systematic Evaluation Program Branch staff indicated that such information can be retrieved from the NRC's office of the Nuclear Material Safety and Safeguards.

David VandeWalle

Nuclear Licensing Administrator

CC Administrator, Region III, USNRC NRC Resident Inspector-Big Rock Point

Attachment

oc0982-0017a142

9210060239 820930 PDR ADDCK 05000155 PDR Consumers Power Company Big Rock Point Plant Docket 50-155

SEP TOPIC III-2, WIND AND TORNADO LOADINGS Consumers Power Company Big Rock Point Plant Docket 50-155

SEP TOPIC III-2, WIND AND TORNADO LOADINGS

#### BIG ROCK POINT

#### SEP TOPIC III-2

## WIND AND TORNADO LOADINGS

## Request For Additional Information

 Define the thickness of the shell for the ventilation stack (concrete chimney) and identify the size and location of reinforcing steel in the stack.

#### Answer

The thickness of the 240 ft. high ventilation stack decreases with increasing height. The following table identifies the thickness profile:

Height Abo	ve Foundation	Thickness
0 f		8"
7.8 f		7 5"
16.3 f	t.	7"
56.3 f	t.	6 1/2"
116.3 f	t.	6"
236.3 f	t.	6"
240.0 f	t.	G 3 <sub>2</sub> 11

The size and location of the reinforcing steel in the stack is shown on Custouis Construction Co., Inc. Drawing No C-1-279-61 enclosed.

Subsequent to our responses to SEP Topic III-2, Wind and Tornado Loadings, dated August 3, 1982 and to a later NRC request for additional information dated August 30, 1982, we have re-evaluated the resistance of the 240 ft.

concrete chimney against wind and tornado loadings. A recently located ustouis Construction Co., Inc. drawing shows the "as built" reinforcement for the stack, whereas our original evaluation (discussed in our response dated August 3, 1982) used steel ratios found in the vendors design calculations (design ratios were 10% to 25% less than the "as built" ratios).

The results of our recent re-evaluation indicate that the 240 ft. concrete chimney has a capacity to resist the wind loading from a 200 mph tornado. This loading is greater than the one calculated in our original response due to the different steel ratios used.

Because of our re-evaluation above, you will find enclosed a revised

Appendix C for our response dated August 3, 1982. This revision reflects

the "as built" steel ratios for the concrete chimney.

 Provide a copy of Bechtel Specification No. 3159 C-21 Reinforced Concrete Chimney (Ventilation Stack).

#### Answer

Enclosed is a copy of Bechtel Specification No. 3159-C-21.

List the drawings which show the cross-section (dimensional and material data) for the south masonry wall of the control room.

#### Answer

The south wall of the control room consists of a 1/2-inch thick steel plate cover over a partition wall which contains two windows and a door. Details of this wall are shown on a drawing located in the security files of Consumers Power Company, which are confidential and not to be released for public scrutiny.

#### APPENDIX C

# EVALUATION OF THE 240-FOOT-HIGH STACK

The analysis of the 240-foot-high stack was performed using ACI 307-69 and ASCE paper 3269 with the following exception: in lieu of using the allowable stresses identified in the ACI code for normal wind loading, the values for the extreme tornado wind loading were:

Maximum concrete stress = 0.8f'<sub>c</sub> = 2,800 psi Maximum reinforcing steel stress = 0.9f<sub>y</sub> = 36,000 psi

These values are consistent with the values used by D'Appolonia in analyzing the 240-foot stack under extreme earthquake loading. (C-1)

The critical sections of the stack were determined by reviewing the original calculation and were found to be 56'-4" above the base for maximum reinforcing steel stresses and at the base for maximum concrete stresses.

The following outlines the method used in analyzing the stack when subjected to a 200 mph wind:

$$P = qC_D = .00256 (200)^2 (.55)$$
  
= 56.3 lbs/ft<sup>2</sup>

In determining the stresses at 56'-4" above the base, the following information was used:

Stress at mean diameter of chimney shell:

$$f'_{cw} = \frac{W(1-\cos \alpha)}{2rt \left[ (1-\rho) (\sin \alpha - \alpha \cos \alpha) - \rho n \pi \cos \alpha \right]}$$
= 120.8 k/ft<sup>2</sup> = 840 psi < 2,800 psi

Stress at outside diameter of chimney shell:

$$f_{cw} = f'_{cw} \left[ 1 + \frac{t}{2r (1-\cos \alpha)} \right]$$
  
= 921 psi < 2,800 psi

Maximum stress in vertical reinforcement

$$f_{sw} = nf'_{cw} \left[ \frac{1 + \cos \alpha}{1 - \cos \alpha} \right]$$

= 24,800 psi < 36,000 psi

In determining the stresses at the base, the following information was used:

Stress at mean diameter of chimney shell:

$$f_{cw}' = \frac{W (\cos \beta - \cos \alpha)}{[2rt (1-\rho)(\sin \alpha - \alpha \cos \alpha) - (1-\rho+\rho n)(\sin \beta - \beta \cos \alpha) - \rho n \pi \cos \alpha]}$$
  
= 235k/ft<sup>2</sup> = 1,632 psi < 2,800 psi

Stress at outside diameter of chimney shell:

$$f_{cw} = f_{cw}' \left[ 1 + \frac{t}{2r \cos \beta (\cos \beta - \cos \alpha)} \right]$$

= 1,766 psi < 2,800 psi

Maximum stress in vertical reinforcement:

$$f_{sw} = nf'_{cw} \left[ \frac{1 + \cos \alpha}{\cos \beta - \cos \alpha} \right]$$

= 35,500 psi < 36,000 psi

The foundation was checked for 200 mph wind as follows:

Total load on the soil (including stack, foundation, soil, and buoyancy) = 1,970 kips

Moment at the bottom of the foundation = 15,557 ft-kips

Since  $\frac{M}{W} = \frac{15,557}{1,970} = 7.9$  ft is larger than 1/6 of the base, dimension (5.72 ft) full surface contact does not exist.

Maximum soil pressure is determined by:

(C-2)

$$P = {\frac{2W}{3a (b/2-e)}} = 5.84 k/ft^2$$

Where

p = soil pressure

W = weight = 1,970 kips

a = width

b = length

e = M/W

The maximum allowable soil pressure for loadings including wind or seismic, in accordance with the original design criteria (C-3) is  $5 \text{ k/ft}^2 \times 1.33 = 6.65 \text{ k/ft}^2$ , which is greater than the calculated maximum soil pressure.

Factor of safety (FS) against overturning:

$$FS = \left\{ \frac{1,970 (24.27/2)}{15,557} \right\} = 1.54 < 1.5$$

## APPENDIX C

# References

- C-1 D'Appolonia Report Volume IV Appendix E "Seismic Safety Margin Evaluation, Reinforced Concrete Stack"
- C-2 F.S. Merritt, Standard Handbook for Civil Engineers, 2nd edition
- C-3 Design Criteria, Big Rock Point Plant Consumers Power Company, Job 3159 (Civil, Structural, Architectural)

# REQUISITION

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1	<b>*</b>	directions oct forth in Westruction Harking and Lighting
3		issued by Ci.11 terenauties definistration. The painting
	4	on 11 consist of geven bands of intermetional orange and
		white. Each bind shall be 20 ft. in height. The top end
E		Lotton band shall be international orting.
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		The presence of objectionable alkalinity in the concrete
3	ali.	shall to checked by using pink litrus paper or by phonolphtic lein
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