

The Light company

Houston Lighting & Power South Texas Project Electric Generating Station P. O. Box 289 Wadsworth, Texas 77483

March 28, 1994
ST-HL-AE-4751
File No.: G9.18
G25
10CFR50 App A

U. S. Nuclear Regulatory Commission
Attention: Document Control Desk
Washington, DC 20555

South Texas Project
Units 1 and 2
Docket Nos. STN 50-498; STN 50-499
Additional Information Regarding Performance of
Main Cooling Reservoir and Essential Cooling Pond During and
After Filling to Elevation + 45 Feet (TAC Nos. M86279 and M86280)

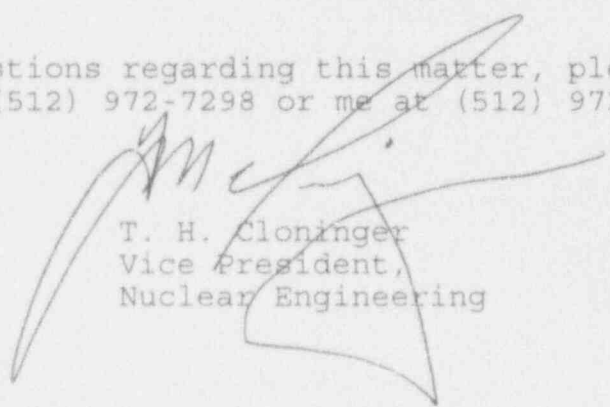
Reference: NRC Request for Addition Information Letter from Mr.
Lawrence Kokajko of the NRC Staff to Mr. William T.
Cottle dated February 10, 1994. (ST-AE-HL-93712)

Houston Lighting & Power Company (HL&P) herein submits
additional information regarding performance on Main Cooling
Reservoir (MCR) and Essential Cooling Pond (ECP) during and after
filling to elevation + 45 feet as requested by Mr. Lawrence Kokajko
of the NRC Staff in the referenced letter of February 10, 1994.

The attachment includes HL&P's response to the questions of
the referenced letter, profile cross sections of the MCR
embankment, and a plot of South Texas Project Electric Generating
Station (STPEGS) Main Cooling Reservoir "Seepage Gradient vs
Thickness of Top Clay Layer", and a table of stability
calculations.

If there are further questions regarding this matter, please
contact Mr. A. W. Harrison at (512) 972-7298 or me at (512) 972-8787.

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PDR ADOCK 05000498
P PDR


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Nuclear Engineering

HRP/eg

ADD 1

Houston Lighting & Power Company
South Texas Project Electric Generating Station

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Page 2

Attachment: Response to the NRC Request For Additional Information
letter of February 10, 1994 from Mr. Lawrence Kokajko of
the NRC Staff to Mr. William T. Cottle.

C:

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RESPONSE TO
NRC REQUEST FOR ADDITIONAL INFORMATION
LETTER DATED FEBRUARY 10, 1994

Requested information:

1. Perform necessary investigations to determine if the high water table in the Main Cooling Reservoir (MCR) embankment sand core is a temporary phenomenon. If it is not a temporary phenomenon, plot the phreatic surface across the embankment section at a few representative locations and compare them with that assumed in the original embankment stability analysis, and determine the factor of safety of the embankment against failure for the high water table condition.
2. Determine the cause for the high seepage gradients across three cross sections of the MCR embankment. Evaluate the effects of such high gradients on the stability of the embankment and take suitable measures to reduce the high seepage gradients to acceptable levels.

Response to item 1:

Attached profiles 3, 19, and 31 are cross sections of the MCR embankment at locations with relatively high water tables in the sand core. The water table in the sand core has been remarkably stable since completion of construction.

The original embankment stability analysis assumed a phreatic surface extending from the maximum design reservoir elevation of +49 feet to the top of the +35 foot berm on the down-stream side of the embankment ("Evaluation of Strength Parameters and Stability, Main Cooling Reservoir Embankment", Harza Engineering Co., September, 1984, ST-XH-YB-013). As shown on the Profiles, the assumed phreatic surface for the stability analysis is conservatively above the water level in the sand core.

Factors of safety based on assumed piezometric levels are presented on attached table 2 from the above referenced report, ST-HX-YB-060. Although the phreatic surface in the sand core is higher than expected, it remains below the design parameters selected.

Response to item 2:

Attached Profile 9, is a MCR embankment cross section at an area with the highest seepage gradient, 7.4% overall (measured between piezometers P38 and P40). This seepage gradient was calculated with a reservoir pool elevation of 43.5 feet. The seepage gradient at the operating reservoir level of 45 feet has been calculated at 8.3%. The drained embankment core and seepage blanket under the down-stream half of the embankment effectively reduced this gradient to a maximum calculated value of 3.8% outside the down-stream toe of the embankment, (measured between piezometers P39 and P40).

Attached is plot "STPEGS Main Cooling Reservoir, Seepage Gradient vs Thickness of Top Clay Layer" showing a very rough inverse correlation between the thickness of the surficial impermeable zone and seepage gradient. The stratigraphic information used in this plot is from information derived along the dam axis. The highly variable nature of the stratigraphy masks what should be a good inverse correlation. The 7.4% seepage gradient is probably in an area with a near surface permeable zone in the reservoir. This zone does not extend under the embankment.

With respect to embankment stability, piezometric levels used to determine stability factors of safety are higher than measured piezometric levels. Therefore, there is no reason to recalculate factors of safety based on measured piezometric levels.

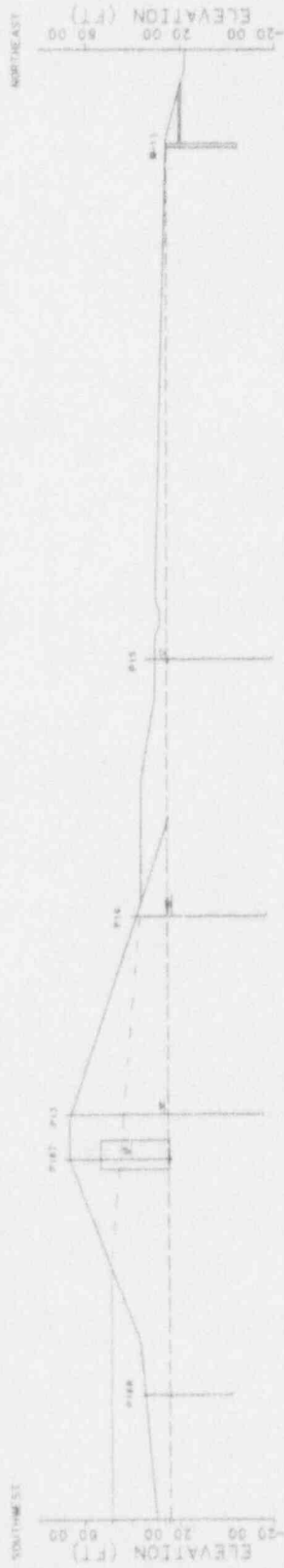
Table 2. Summary of Stability Analysis Results

<u>Section</u>	<u>Factor of Safety</u>		
	<u>Steady State</u>	<u>Drawdown from El. 49 to El. 39</u>	<u>Seismic</u>
Station 20+00			
Upstream	1.82	1.50*	1.34 * (0.1g)
Downstream	1.72	---	1.25 (0.1g)
Station 105+00			
Upstream	1.76	1.41*	1.46 * (0.05g)
Downstream	1.72	---	1.25 (0.05g)
Station 250+00			
Upstream	1.81	1.48*	1.49 (0.05g)
Downstream	1.71	---	1.42 (0.05g)
Station 365+00			
Upstream	1.89	1.54*	1.52 (0.05g)
Downstream	1.77	---	1.49 (0.05g)

* Same failure surface as critical surface using steady state conditions.

PROF 11.F 3
 EMBANKMENT STATION 20+00
 SOUTH TEXAS PROJECT
 14926-001

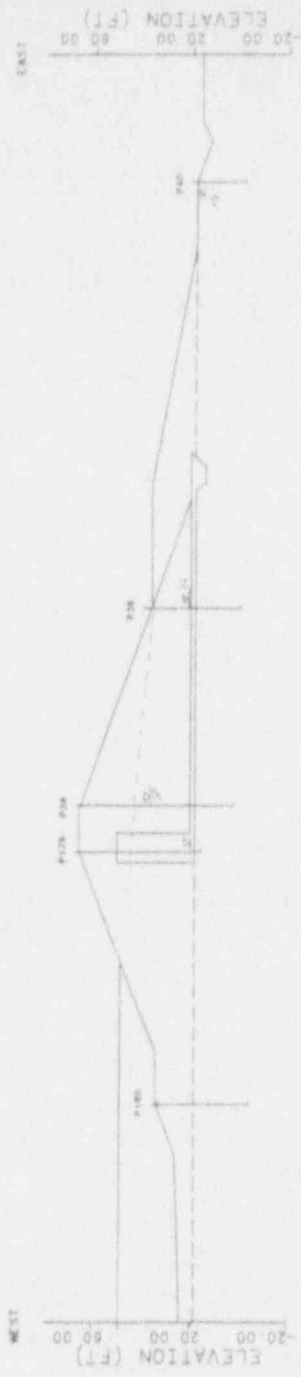
0.00 40.00 80.00 120.00
 SCALE IN FEET



0022-001
 0076-011

PROFILE 9
 EMBANKMENT STATION 160+00
 SOUTH TEXAS PROJECT
 14926-001

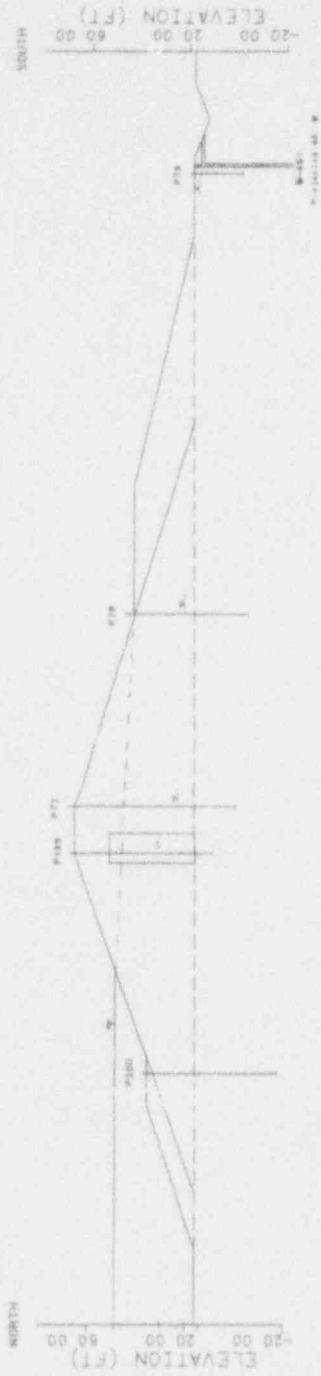
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 SCALE IN FEET



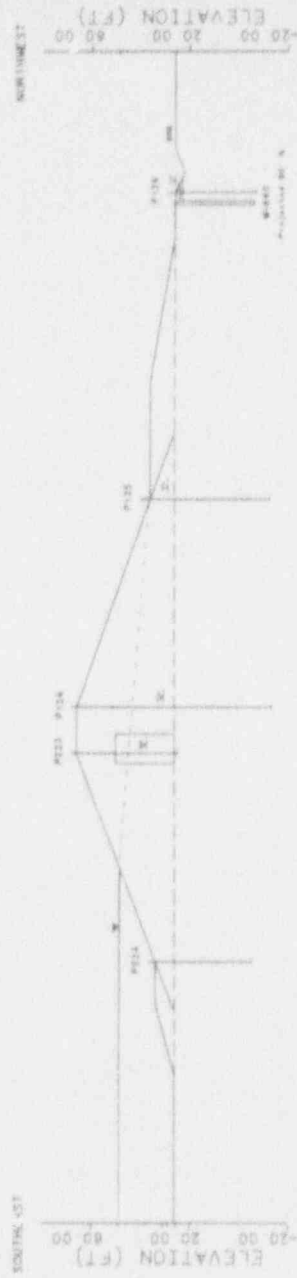
14926-001
 10/17/12

PROFILE 19
 EMBANKMENT STATION 359+60
 SOUTH TEXAS PROJECT
 14925-001

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 SCALE IN FEET



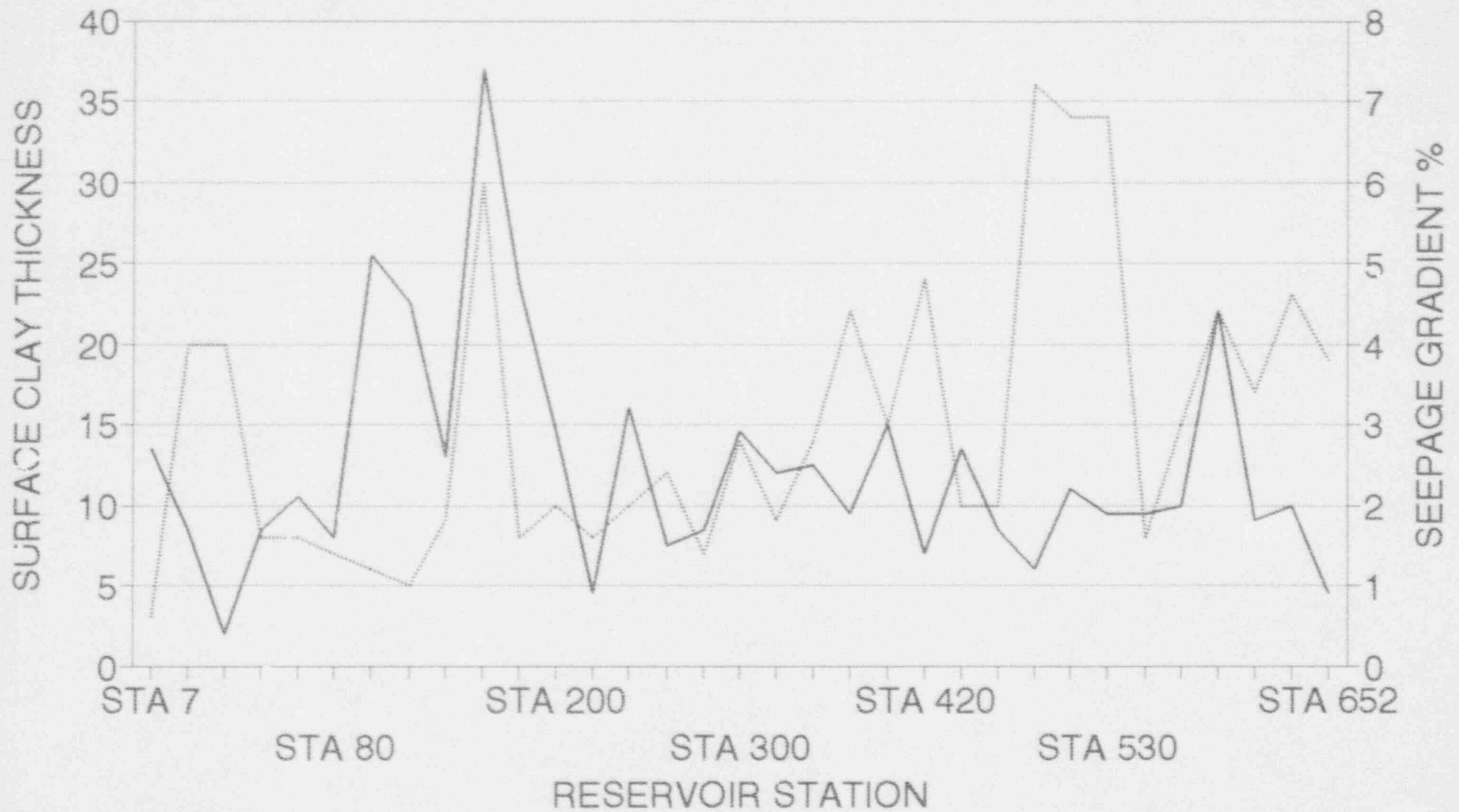
PROFILE 31
 EMBANKMENT STATION 610+00
 SOUTH TEXAS PROJECT
 14826-001



CROSS 305
 03/25/13

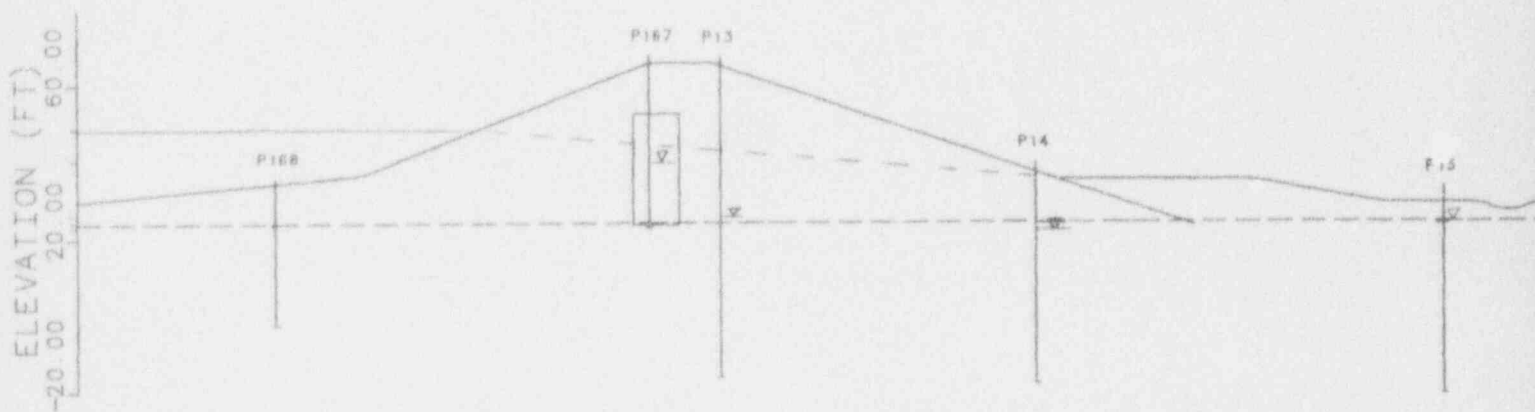
STPEGS MAIN COOLING RESERVOIR

SEEPAGE GRADIENT VS THICKNESS OF TOP CLAY LAYER



— SEEPAGE GRADIENT CLAY THICKNESS

SOUTHWEST



PROFILE 3
EMBANKMENT STATION 20+00
SOUTH TEXAS PROJECT
14926-001

**ANSTEC
APERTURE
CARD**

Also Available on
Aperture Card

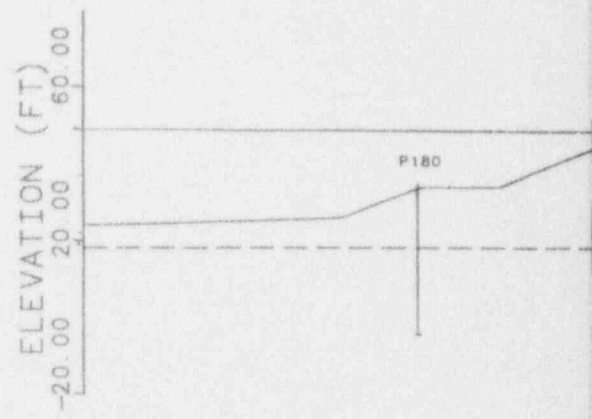


NORTHEAST



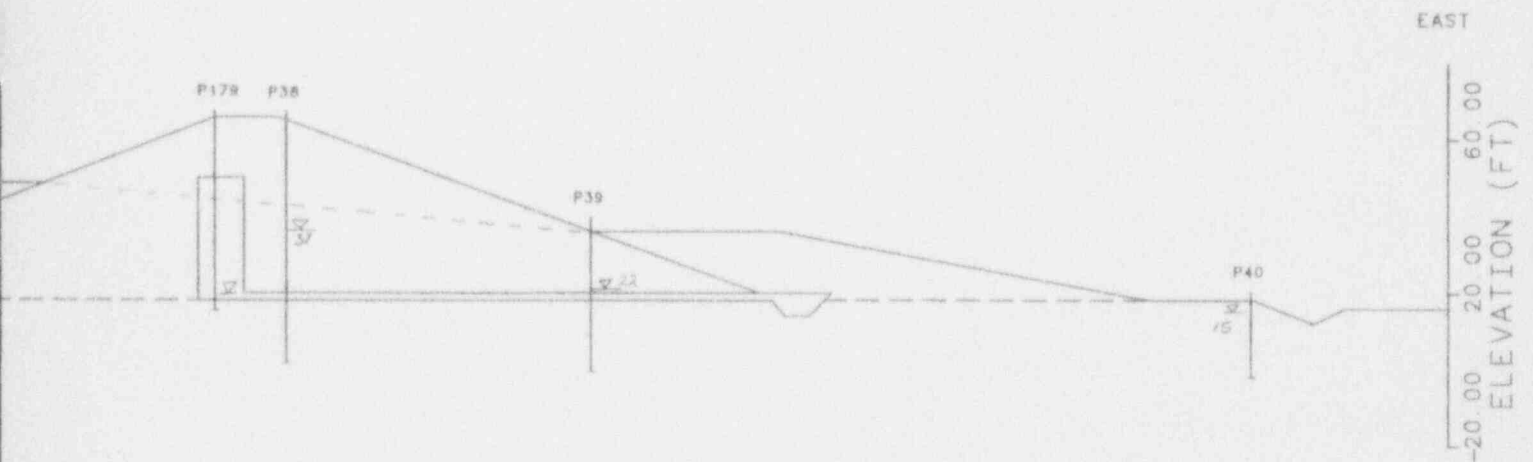
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WEST



PROFILE 9
EMBANKMENT STATION 160+00
SOUTH TEXAS PROJECT
14926-001

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SCALE IN FEET



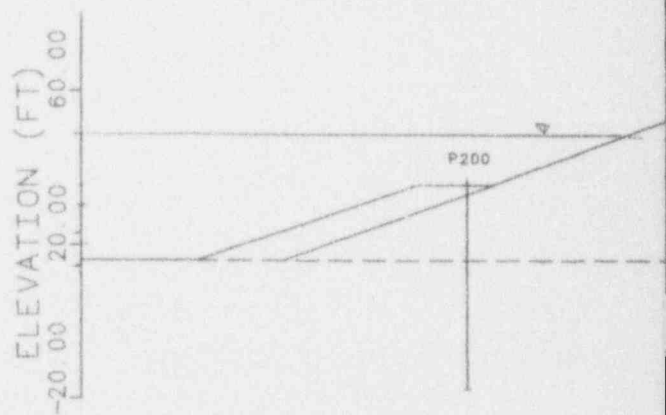
**ANSTEC
APERTURE
CARD**

Also Available on
Aperture Card

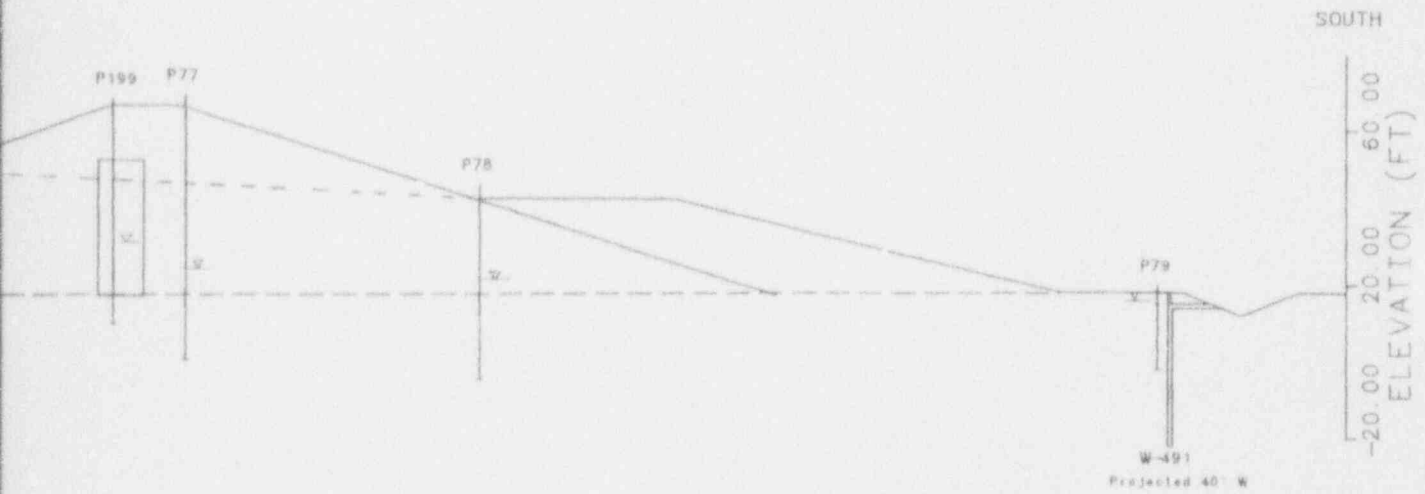
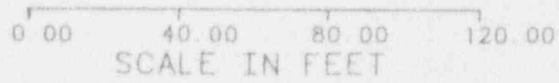
CO227.001
CO227.C11

9404040105-02

NORTH



PROFILE 19
EMBANKMENT STATION 359+60
SOUTH TEXAS PROJECT
14926-001



**ANSTEC
APERTURE
CARD**

Also Available on
Aperture Card

CO22R-001
T022R-011

9404040105-03

SOUTHEAST

ELEVATION (FT)
60.00
20.00
-20.00

PROPOSED GRADE

EXISTING GRADE

PROPOSED GRADE

EXISTING GRADE

PROPOSED GRADE

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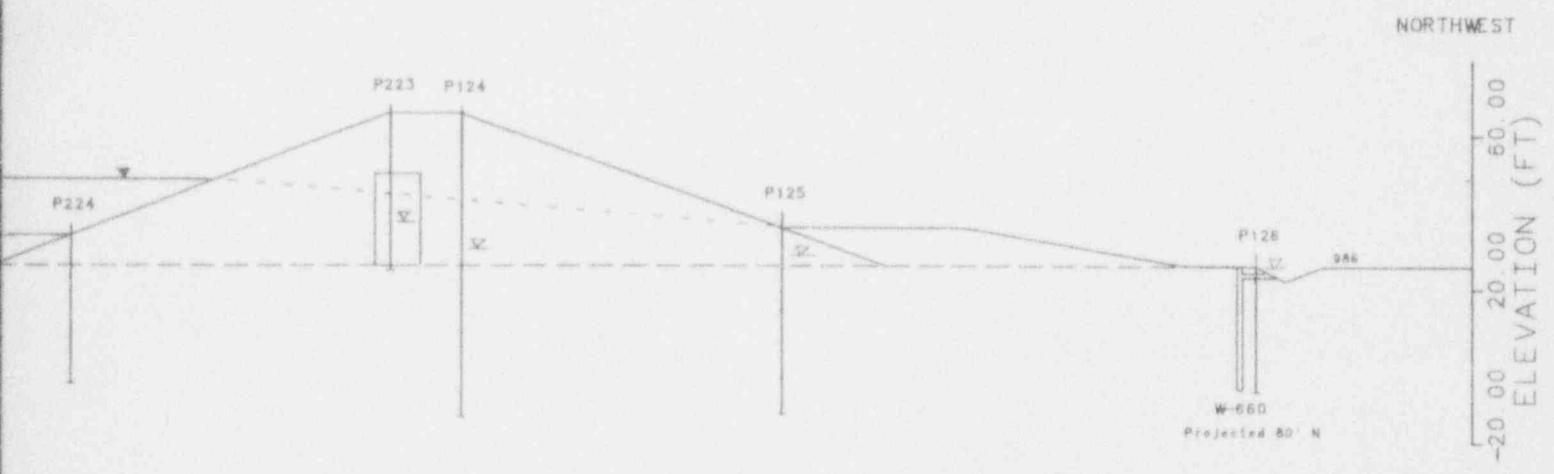
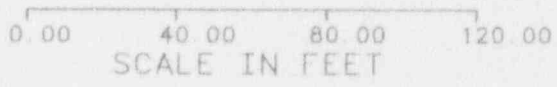
PROPOSED GRADE

EXISTING GRADE

PROPOSED GRADE

EXISTING GRADE

PROFILE 31
EMBANKMENT STATION 610+00
SOUTH TEXAS PROJECT
14926-001



ANSTEC
APERTURE
CARD

Also Available on
Aperture Card

C0226-001
C0225-C11

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