



# International Agreement Report

## Assessment of RELAP5/MOD3 With the LOFT L9-1/L3-3 Experiment Simulating an Anticipated Transient With Multiple Failures

Prepared by  
Young Seok Bang, Kwang Won Seul, Hho Jung Kim

Korea Institute of Nuclear Safety  
P. O. Box 16, Daeduk-Danji  
Taejon, Korea

Office of Nuclear Regulatory Research  
U.S. Nuclear Regulatory Commission  
Washington, DC 20555-0001

February 1994

Prepared as part of  
The Agreement on Research Participation and Technical Exchange  
under the International Thermal-Hydraulic Code Assessment  
and Application Program (ICAP)

9404010254 940228  
PDR NUREG  
IA-0114 R PDR

Published by  
U.S. Nuclear Regulatory Commission

NOTICE

This report was prepared under an international cooperative agreement for the exchange of technical information. Neither the United States Government nor any agency thereof, or any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibility for any third party's use, or the results of such use, of any information, apparatus product or process disclosed in this report, or represents that its use by such third party would not infringe privately owned rights.

Available from

Superintendent of Documents  
U.S. Government Printing Office  
P.O. Box 37082  
Washington, D.C. 20013-7082

and

National Technical Information Service  
Springfield, VA 22161



## International Agreement Report

---

# Assessment of RELAP5/MOD3 With the LOFT L9-1/L3-3 Experiment Simulating an Anticipated Transient With Multiple Failures

Prepared by  
Young Seok Bang, Kwang Won Seul, Hho Jung Kim

Korea Institute of Nuclear Safety  
P. O. Box 16, Daeduk-Danji  
Taejon, Korea

Office of Nuclear Regulatory Research  
U.S. Nuclear Regulatory Commission  
Washington, DC 20555-0001

February 1994

Prepared as part of  
The Agreement on Research Participation and Technical Exchange  
under the International Thermal-Hydraulic Code Assessment  
and Application Program (ICAP)

Published by  
U.S. Nuclear Regulatory Commission

NOTICE

This report is based on work performed under the sponsorship of The Korea Advanced Energy Institute of Korea. The information in this report has been provided to the USNRC under the terms of an information exchange agreement between the United States and Korea (Agreement on Thermal-Hydraulic Research between the United States Nuclear Regulatory Commission and The Korea Advanced Energy Research Institute, May 1, 1986). Korea has consented to the publication of this report as a USNRC document in order that it may receive the widest possible circulation among the reactor safety community. Neither the United States Government nor Korea or any agency thereof, or any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibility for any third party's use, or the results of such use, or any information, apparatus, product or process disclosed in this report or represents that its use by such third party would not infringe privately owned rights.

**Assessment of RELAP5/MOD3 with the LOFT L9-1/L3-3 Experiment**  
**Simulating an Anticipated Transient with Multiple Failures**

**Abstract**

The RELAP5/MOD3 5m5 code is assessed using the L9-1/L3-3 test carried out in the LOFT facility, a 1/60-scaled experimental reactor, simulating a loss of feedwater accident with multiple failures and the sequentially-induced small break loss-of-coolant accident. The code predictability is evaluated for the four separated sub-periods with respect to the system response; initial heatup phase, spray and power operated relief valve(PORV) cycling phase, blowdown phase and recovery phase. Based on the comparisons of the results from the calculation with the experiment data, it is shown that the overall thermal-hydraulic behavior important to the scenario such as a heat removal between the primary side and the secondary side and a system depressurization can be well-predicted and that the code could be applied to the full-scale nuclear power plant for an anticipated transient with multiple failures within a reasonable accuracy. The minor discrepancies between the prediction and the experiment are identified in reactor scram time, post-scram behavior in the initial heatup phase, excessive heatup rate in the cycling phase, insufficient energy convected out the PORV under the hot leg stratified condition in the saturated blowdown phase and void distribution in secondary side in the recovery phase. This may come from the code uncertainties in predicting the spray mass flow rate, the associated condensation in pressurizer and junction fluid density under stratified condition.

## Executive Summary

This report presents the RELAP5/MOD3 code assessment calculation using the test L9-1/L3-3 conducted in the loss of fluid test(LOFT) facility. The LOFT facility was a 1/60-scaled experimental reactor. The experiment L9-1/L3-3 simulated a loss of feedwater accident(LOFA) with multiple failures and a consequentially-induced small break loss of coolant accident(LOCA).

The full period of the test was separated with four sub-periods according to the thermal-hydraulic characteristics ; the initial heatup phase, the spray and power operated relief valve(PORV) cycling phase, the blowdown phase and the recovery phase.

RELAP5/MOD3 calculation successfully simulated the complex sequence of events associated with a LOFA and a consequential LOCA. Based on the comparisons between the calculation results and the experiment data, the overall behavior such as a subcooled heatup and a depressurization in the primary coolant system, and a heat removal after the dryout in steam generator secondary side was well-predicted throughout the four sub-periods. However, the calculation results show the reactor scram earlier than the experiment, resulting in the overestimation of the post-scram cooling, which may due to a code uncertainty in the spray mass flow rate and the associated condensation in the pressurizer. Due to this difference, the predicted initiation and completion times were somewhat delayed. The excessive heatup rate was also found in the spray cycling phase, which may come from the overprediction of discharged flow rate through the PORV during the blowdown phase. And the RELAP5/MOD3 predicted an inaccurate junction fluid density under the hot leg stratified, which resulted in an insufficient energy convected out the PORV. This caused an overprediction in primary system pressure and temperature during the saturated blowdown phase. In the recovery phase, the RELAP5/MOD3 calculation yields an inaccurate void distribution in the SG secondary side. It may be ascribed to the overprediction of the pressure and temperature drop in primary coolant system.

## List of Contents

1. Introduction	1
2. Facility and Test Description	3
2.1 Facility Description	3
2.2 Test Description	4
3. Code and Modeling Description	7
3.1 Code Description	7
3.2 Input Modeling	7
3.3 Initial and Boundary Conditions	11
4. Calculation and Discussion	12
4.1 Initial Heatup Phase	13
4.2 Spray and PORV Cycling Phase	15
4.3 Blowdown Phase	16
4.4 Recovery Phase	18
5. Run Statistics	20
6. Conclusions	21
References	22
Tables	23
Figures	31
Appendix A. Input Deck for Steady State Calculation	
Appendix B. Input Deck for Transient Calculation	

## List of Tables

- Table 1. Initial conditions for L9-1/L3-3
- Table 2. Sequence of events in L9-1/L3-3
- Table 3. Summary of nodalization
- Table 4. Detailed information for heat structures
- Table 5. Summary of data channels and uncertainties in comparison plots

## List of Figures

- Fig.1 Axonometric configuration of LOFT L9-1/L3-3 test
- Fig.2 RELAP5 nodalization diagram for LOFT Experiment L9-1/L3-3
- Fig.3-a Pressurizer spray valve control trip
- Fig.3-b Pressurizer PORV control trip
- Fig.3-c Makeup feed storage boundary condition trip
- Fig.3-d MSCV Bypass valve control trip
- Fig.3-e MSCV open/close control trip
- Fig.3-f Reactor scram trip
- Fig.3-g Pressurizer heater control trip
- Fig.4 Comparison of pressure at the intact loop hot leg (short term)
- Fig.5 Comparison of coolant temperature at the intact loop hot leg (short term)
- Fig.6 Comparison of reactor power
- Fig.7 Comparison of pressure at SG steam dome (short term)
- Fig.8 Comparison of coolant temperature at SG secondary side (short term)
- Fig.9 Comparison of SG collapsed liquid level (short term)
- Fig.10 Comparison of mass flow rate through MSCV (short term)
- Fig.11 Comparison of pressure at the intact loop hot leg (long term)
- Fig.12 Comparison of coolant temperature at the intact loop hot leg (long term)
- Fig.13 Comparison of pressure at SG steam dome (long term)
- Fig.14 Comparison of coolant temperature at SG secondary side (long term)
- Fig.15 Comparison of pressurizer collapsed liquid level (long term)
- Fig.16 Comparison of mass flow rate through PORV (long term)
- Fig.17 Comparison of fluid density at intact loop hot leg (long term)
- Fig.18 Comparison of SG collapsed liquid level (long term)
- Fig.19 The required CPU time versus the advanced time
- Fig.20 Time step size of base case calculation

## ACKNOWLEDGEMENTS

This report was completed under the sponsorship of Korean Ministry of Science and Technology(MOST). Dr. Sang Hoon Lee, President of the Korea Institute of Nuclear Safety(KINS), contributed significantly to the administration of the project. Authors expressed a appreciation to Drs. Bub Dong Chung, Euy Joon Lee and Mrs Eun Kyoung Cho in KINS for installating RELAP5/MOD3 code on the CRAY-2S machine and supporting the calculation. Mrs. Eun Kyoung Cho also contributed to prepare the data plots. Authors should express their gratitude to Mr. Dick Schultz and Mr. Hershall Hardy in INEL for managing the ICAP project and for providing the related documents and test data.

## 1. Introduction

The RELAP5/MOD3 code [1] was developed by the Idaho National Engineering Laboratory (INEL) under the sponsorship of US Nuclear Regulatory Commission (NRC), and its frozen version, 5m5 was released at the end of 1990. Through the developmental assessments conducted [2], the code capability was investigated, however, the code predictability for such transients as an anticipated transient with multiple failures was not fully demonstrated. This report summarizes a code assessment using the typical experiment simulating this type of transient, the L9-1/L3-3 [3] conducted in the Loss-of-Fluid-Test (LOFT) facility [4]. The test L9-1/L3-3 composed of two sequential tests; L9-1 and L3-3, which simulated a loss of feedwater accident (LOFA) with multiple failures and a consequentially-induced small break loss of coolant accident (SBLOCA) in pressurized water reactor (PWR), respectively.

The major objective of this study was to identify the code capability of the RELAP5/MOD3 5m5 on the prediction of thermal-hydraulic (TH) behavior in primary coolant system (PCS) and secondary coolant system (SCS) during the LOFA with multiple failures and the consequentially-induced LOCA. To achieve this objective, the full period of the test L9-1/L3-3 was separated with four sub-periods with respect to the system response on the accident ; the initial heatup phase, the spray and power operated relief valve(PORV) cycling phase, the blowdown phase and the recovery phase. The programmatic objectives of this study are :

1. to provide RELAP5/MOD3 simulation of the test L9-1/L3-3 for demonstrating the code applicability to this kind of transient in full-scale PWR,
2. to evaluate the accuracy and the discrepancy of the code in predicting the following TH phenomena during the four sub-periods based on the comparison with the experiment,
  - Steam generator (SG) secondary side dry out after a LOFA
  - Post-scram PCS cooling

- PCS heatup in subcooled state and pressurizer liquid level swell
  - Pressurizer spray valve actuation and pressure control
  - Pressurizer PORV cycling and pressure control
  - PCS depressurization due to PCS mass depletion through PORV
  - Two-phase break flow through PORV and hot leg stratification
  - PCS depressurization due to the secondary side refill and secondary side feed and bleed
3. to identify reasons for the discrepancy evaluated in item 2.

The descriptions of the LOFT system and the test L9-1/L3-3 are given in Chapter 2. The code description, the input modeling and the initial and boundary conditions are given in Chapter 3. The results of the calculation are discussed in Chapter 4 and the run statistics given in Chapter 5. The conclusions obtained throughout the assessment are summarized in Chapter 6.

## 2. Facility and Test Description

### 2.1 Facility Description

The LOFT facility is an experimental 50 MWt PWR designed to simulate LOCA's and anticipated transients and to provide data on the thermal-hydraulic phenomena occurring throughout the system [4]. It is a scaled representation of a commercial PWR of Westinghouse type having 4 loops with a volume ratio of 1/60. The LOFT system consists of five major systems : reactor system, primary coolant sysstem, blowdown suppression system, emergency core cooling system and secondary coolant system, and also includes instrumentations. The lengths of the core and reactor vessel are 1.68 and 7 m, respectively. The overall configuration is shown in Fig.1.

The break location for the test L9-1/L3-3 was the experiment PORV located in the pressurizer relief line at the top of the prerssurizer. The experiment PORV was geometrically similar to the commercial PWR PORV's and was steam-scaled by  $1.32 \times 10^{-2}$  kg/s/MW. The detailed description was provided in reference [10].

## 2.2 Test Description

The experiment L9-1/L3-3 composed of two sequential tests. The test L9-1 simulated a LOFA with delayed scram and no auxiliary feedwater injection in PWR. The test L3-3 described the LOFA recovery modes initiated by tripping the PCP and depressurizing the PCS through the PORV in pressurizer. The experiment objectives were as follows [5]:

1. For L9-1:
  - a. To evaluate uncertainties in predicted primary and secondary thermal hydraulic response associated with steam generator dryout during delayed scram.
  - b. To evaluate the adequacy of PORV to provide overpressure protection in a LOFA.
2. For L3-3:
  - a. To investigate uncertainties in system response during a PORV imposed small break with loss of heat sink.
  - b. To assess the adequacy of modelling assumptions which are used in small break performance predictions such as those identified in NUREG-0623 [7].
  - c. To assess the effectiveness of steam generator refill on LOFAs following reestablishment of auxiliary feedwater availability.
  - d. To assess the relative magnitude of the change in reactor vessel mixture level as a result of primary coolant system shrink during steam generator refill.
  - e. To contribute to the NRC relief and safety valve testing program by providing experimental data on PORV performance characteristics over a range of PORV inlet fluid conditions.

Prior to the experiment, the flow rate of the primary system was  $479.1 \pm 2.6$  kg/sec under the pressure of  $14.9 \pm 0.10$  MPa. Temperatures at the hot leg and the cold leg in the intact loop were  $578.2 \pm 1.8$  K and  $558.9 \pm 1.3$  K, respectively. The important initial conditions including pressure, temperature and liquid level in the intact loop steam generator (SG) secondary side were listed in

Table 1.

Experiment L9-1 was initiated by stopping the main feedwater pump. Due to decrease in heat removal capacity of SG secondary side, the PCS pressure increased and the pressurizer spray valve was open at its setpoint (15.338 MPa), which was observed at 30.0 seconds after initiation of LOFA. As the magnitude of the primary-secondary power mismatch grew, the PCS pressurization exceeded the spray cooling, which caused a delayed scram, simulating a failure of the SG low level trip, on the high pressure of hot leg (15.745 MPa) at 65.4 seconds. Auxiliary feedwater was not activated in order to simulate nonavailability of auxiliary feedwater. The main steam control valve (MSCV) started to close on the scram signal and completed to close at 77.2 seconds. The primary system pressure was decreased on reactor scram and then increased due to the decay heat and the complete loss of heat sink in SG secondary, which caused the pressurizer spray valve open and initiate cycling at 208.9 seconds to control PCS pressure. The open/close setpoints of spray valve were 15.338 and 15.05 MPa, respectively. Spray was allowed to cycle for 900 seconds approximately, whereupon it was manually overridden, allowing PCS pressure to rise to the PORV actuation setpoint (16.20 MPa) at 1468 seconds. Thereafter, the pressurizer came into the liquid-full state. The PORV was allowed to cycle relieving single phase liquid primary coolant as the PCS volume continued to heatup and expand at 1468 seconds. The PORV cycling was ended at the time which the PCS hot leg temperature reached 597 K, 3270 seconds. At that time, the PCPs were deenergized, the PORV was held open and the test L3-3 was initiated. The sequence of important events was presented in Table 2.

As the PORV latch open for 1580 seconds from the initiation of L3-3, the PCS pressure dropped rapidly to saturation and the hot regions of the core and upper plenum flashed. ECCS actuation was inhibited. The depressurization stabilized while the upper plenum and upper head voided whereupon the hot leg stratified. As hot leg voided a higher quality fluid was convected up the surge line, and the pressurizer liquid level receded as the cooler pressurizer fluid was entrained out the PORV. A transition to higher quality PORV mass flow decreased fluid density

flowing pressurizer relief line shortly after latching open PORV. This transition resulted in a higher specific energy fluid being discharged out the PORV and resulted in increased energy removal out the break. As break energy removal exceeded decay heat addition, PCS pressure declined steadily. PCS pressure stabilized as the PORV was closed. A steam generator refill was initiated 265 seconds after the PORV-closure. PCS pressure dropped rapidly as the secondary heat sink was restored. When the normal steam generator liquid level was regained at 5746.4 seconds, the SG refill was completed and then a 966 seconds equilibration period was observed to allow the primary and secondary to reach an equilibrium. Subsequently, a secondary steam and makeup operation was initiated at 6712.2 seconds to cool down the primary and recover plant. ECCS injection was not provided throughout the experiment. The experiment was terminated as PCS pressure reached 2.15 MPa. The major sequence was summarized in Table 2.

### 3. Code and Modeling Description

#### 3.1 Code Description

RELAP5/MOD3 Cycle 5m5 version released by USNRC was used in the present assessment calculation of the test L9-1/L3-3. The changed features from the RELAP5/MOD2 were described in references [1, 2].

#### 3.2 Input Modelling

The original RELAP5/MOD1 input data for simulating the LOFT system and the sequence specific to the test L9-1/L3-3 was received from INEL at January 1991. Based on the original RELAP5/MOD1 input data, some modifications was made during the assessment work. Major changes were as follows :

1. All geometric data except the U-tube heat transfer area and separator in the intact loop SG remain unchanged.
2. Modeling options related to volume, junction, heat structure were properly modified to work with RELAP5/MOD3 [1].
3. The options, 'new transnt' were changed to 'new stdy-st' in order to re-initialize the whole plant conditions under RELAP5/MOD3 models and correlations.
4. For steady state run, three steady state control systems were added ;
  - a. PCP speed controllers for controlling a intact loop mass flow rate,
  - b. a pressurizer heater controller and a pressurizer spray controller for controlling the PCS pressure, and
  - c. a main feedwater controller for controlling the S/G secondary side liquid level.
5. For steady state run, the test specific trips were set not to be activated.
6. A new transient input data was developed with deleting steady state controllers and changing the test specific trips to be activated.
7. The moderator density feedback table in a reactor kinetics input data was appropriately changed from the original one, based on the reference [8].

In the present calculation, the LOFT system was discretized by 125 volumes, 135 junctions and 136 heat structures after implementing the items stated above. Figure 2 shows a RELAP5 nodalization diagram for simulating the test L9-1/L3-3. Table 3 summarizes the nodalization and input modelling. A steady state input deck and a transient input deck were provided in Appendix A and B.

### 3.2.1 Primary Coolant System Modelling

The PCS composed of an intact loop and a broken loop, the former included a hot leg, a crossover leg, a pump suction tee, two PCPs and a cold leg. The intact loop was modelled by 25 hydrodynamic volumes. All piping metal structures exposed to environmental atmosphere were simulated by the heat structure to consider the associated heat loss. An overall information for the all heat structures was provided in table 4. The broken loop composed of a hot leg, a SG-pump simulator, a reflood assist bypass system (RABS), a cold leg and pipings front of the quick opening blowdown valves (QOBVs). The detailed information can be found in Fig.2, table 3 and table 4. The volume and junction modelling options were set with default options.

### 3.2.2 Reactor Vessel Modeling

The LOFT reactor vessel was modelled by a downcomer annulus, a lower plenum, an active core, a core-bypass flow path, an upper plenum, an upper head and a filler gap flow path. The filler gap flow path was especially modeled for simulating an upward flow during a natural circulation phase. The active core, the downcomer and the filler gap were modeled by 3 volumes, 6 volumes and 7 volumes stacked vertically, respectively. Totally 26 volumes and 50 heat structures were used. The rod bundle interphase friction model option was selected for the active core volumes. The fuel rods were modeled by 3 heat structures representing the central fuel assembly and 3 heat structures representing the peripheral fuel assemblies of LOFT core. The axial power shape was described according to the reference[8]. The reactor kinetics was used for simulating the moderator density and doppler temperature feedback and a scram curve was provided, which was

used in the posttest calculation [8]. The ANS-79 model was used for a decay heat simulation, which was changed from ANS-73 model in the posttest calculation [8].

### 3.2.3 Pressurizer Modeling

The pressurizer system was modeled by a surgeline, a pressurizer vessel, a spray line from cold leg, a spray valve and a experiment PORV. Two volumes for the surge line, nine volumes for the vessel and one volume for the spray line were used, respectively. The spray valve and the PORV were simulated by two trip valves. The associated trip logics were prepared according to the experimental specification [6]. To consider the environmental heat loss from the pressurizer vessel wall, the vessel wall was modeled by nine heat structures.

### 3.2.4 Steam Generator Modeling

The steam generator consisted of a SG inlet plenum, U-tubes, a outlet plenum, a main feedwater tank and feed line, a auxiliary feedwater tank and feed line, a feedwater inlet annulus, a SG secondary side downcomer, a boiler section, a separator inlet annulus, a separator, a steam dome, a steimeline, a MSCV, a MSCV bypass flow path, a MSCV downstream piping and a air-cooled condenser. The numbers of volumes used for each flow path were provided in Table 3 and Fig.2. All of the SG metal wall and U-tubes were described by the proper heat structures. The detailed description can be found in Table 4. The rod bundle interphacial friction option was used for the volumes contacted with the U-tubes heat structures (Volumes 515-4, -5, -6). The separator section in SG was modeled by a branch component (Volume 520) and a SEPARATTR component (Volume 500). The separator inlet junction was connected to the bottom of the volume 520, as show in Fig.2.

The heat transfer area of U-tube heat structure in the intact loop SG generally has an impact on the initial conditions in SG secondary side. According to the previous LOFT calculations using RELAP5/MOD2 [9, 10], the predicted pressure in SG secondary side were generally underpredicted by 0.3-0.4 MPa. This discrepancy was considered as a result of underestimation of heat transfer a,

in the SG U-tube. In the present input data, an increase of heat transfer area by 110 % of the original heat transfer area [8] was made. The whole listing of steady state input data were provided in Appendix A.

### 3.2.5 Others

The emergency core cooling system (ECCS) in LOFT was also modeled, however, it is not used in the transient calculation. Table 3, Fig 2 and Appendix A provided a detailed information of it. And the containment was also modeled by time-dependent volume with a constant pressure.

### 3.3 Initial and Boundary conditions

To provide all initial conditions of the whole system prior to transient, a steady state run was carried out with three steady state controllers as stated above. The result obtained from the steady state run was compared with the measured initial conditions in Table 1. The RELAP5 calculated results generally agree with the experiment initial conditions.

Boundary conditions required to simulate the L9-1/L3-3 experiment including the pressures and temperatures at air-cooled condenser, makeup feed storage tank and reactor core power history were almost the same as those used in the posttest calculation [8]. The exact values can be found in the steady state input data.

Test specific sequence to be described are as follows: Main feedwater turned off, Reactor scran, SG MCSV closure, Pressurizer spray valve open/closure, Pressurizer PORV cycling, Pressurizer PORV latched open and closure, PCP coastdown initiation, SG secondary refill initiation/completion, and SG secondary bleed initiation/completion.

All of the sequence were as the same as the original input data [8] and were illustrated with some comments in the Figure 3-a through 3-g. The delay time in the trip logic describing the SG refill initiation (Variable trip 561) was corrected to '265 seconds' after PORV closure according to the reference [5]. The whole list of the transient input data was attached in Appendix B.

#### 4. Calculation and Discussion

A transient calculation using the input modelings, initial conditions and boundary conditions stated above was conducted by RELAP5/MOD3 5m5 code. The transient calculation was terminated at 8106 seconds due to water property failure at the SG secondary side volume 515-06. Since the calculational result up to 8100 seconds contains all of the important phenomena in the L9-1/L3-3 experiment, any additional restart transient calculation was not executed. The foregoing description was, therefore, based on the calculational result up to 8100 seconds. This chapter was devoted to address results from the transient calculation, to compare them with the corresponded measurement data and to identify the code predictability. Table 2 shows a comparison of the predicted sequence of event with the measured chronology. The detailed discussion of the comparison was provided in following sub-chapters. From the test description above, it is shown that the full period of the LOFT L9-1/L3-3 experiment can be divided into four distinguishable sub-phases according to the TH characteristics as follows;

- 1) Initial heatup phase before spray cycling,
- 2) Spray and PORV cycling phase until PORV latched open,
- 3) Blowdown phase until PORV closure, and
- 4) Recovery phase

The following discussions contain the prediction and its comparison for the important thermal-hydraulic phenomena during these four period, respectively. Table 5 summarizes the comparison plots and their data channels.

The measurement uncertainties for each parameter were also listed in this table, which were from the reference [5].

#### 4.1 Initial Heatup Phase

Figure 4 shows a comparison of the pressure at the intact loop hot leg in PCS with the measured data up to 300 seconds after the test initiation. Fig.5 shows a comparison of the coolant temperature at the intact loop hot leg with the measured data for the same period as in Fig.4. Due to LOFA the heat removal capacity in SG secondary side was degraded, the PCS pressure and temperature was increased. These figures show good agreements between the calculation and the experiment before reactor scram. The calculated reactor scram time (55.8 seconds) was earlier than the experiment (65.4 seconds). This discrepancy may come from a code uncertainty in predicting the mass flow rate through the spray valve and the associated condensation phenomena in the pressurizer. For an illustration of it, the calculation shows the PCS pressure was still increased inspite of the second spray actuation at 50 seconds approximately, while the experiment indicated the PCS pressure was slightly decreased at the almost same time and then re-increased. It can be also identified in the first activation of spray (30 seconds), in which the predicted slope of pressure decrease was slower than the predicted one. The underprediction of pressure and temperature after scram was due to the difference in scram time. Figure 6 shows a comparison of the calculated reactor power with the power measured by a neutron detector and with the decay heat reported in reference [5]. The difference in power during time period from 56 to 65 seconds lowered the PCS pressure below 14 MPa and delayed a pressure re-increase until 170 seconds, i.e., an excessive post-scram cooling. This discrepancy also delayed the spray valve activation time until 315 seconds, which was later than the experiment, 208 seconds.

Figures 7 and 8 show comparisons of the pressure and temperature in the SG steam dome and the top of the boiler section with the measured data, respectively. Before the reactor scram the predicted behavior was agreed to the measured one. Due to earlier scram in calculation, the starting time and completion time of MCV closure predicted by RELAP5/MOD3 were earlier than those in experiment as shown in Table 2. According to the experiment, just after a LOFA, the SCS pressure and temperature were both increased from saturated state until

the complete dryout, and then decreased until the MSCV began to reduce the discharging steam flow on the response to the reactor scram. This reduction yields a decrease in heat rejection from the SCS, therefore, the SCS pressure and temperature were re-increased. Afterwards, the TH behavior of the SCS was dependent on the energy balance between the heat-rejection due to the MSCV leakage flow and the heat addition from the PCS generated by core decay heat. The result from the RELAP5/MOD3 calculation generally shows these TH behavior well, however, shows an overprediction in SCS pressure and temperature after scram. It must due to a difference in the scram time. Inspite of this difference, the slope of increase in pressure after scram was almost the same as that in the experiment. Figure 9 shows a comparison of the collapsed liquid level with the measured data, which indicated a complete dryout in SG secondary side at 60 seconds after a LOFA, approximately and a good agreement between the calculation and the experiment. Figure 10 shows a comparison of the mass flow rate through MSCV. From these comparisons, it, therefore, can be stated that the consequent behavior after scram can be well-predicted if the scram time was correctly predicted.

#### 4.2 Spray and PORV Cycling Phase

Figures 11 and 12 show comparisons of the pressure and temperature at the intact loop hot leg in PCS up to 10000 seconds. The starting time of the spray valve cycling predicted was, as previously mentioned, later than the measured. The predicted duration of spray cycling was about 1055 seconds ( $= 1370 - 315$ ), which was similar to the measured duration, 1037 seconds ( $= 1246 - 209$ ). The slope of temperature increase, i.e., heatup rate was larger than the experiment, however, a saw-tooth behavior in pressure was well predicted during the spray cycling period. One of the reasons of higher heatup rate was also considered as an uncertainty in the spray mass flow rate.

The predicted starting time of PORV cycling was 1795 seconds and also later than the experiment, 1468 seconds. The duration of PORV cycling was about 1390 seconds ( $= 3185 - 1795$ ) in calculation, which was shorter than the experiment, 1802 seconds ( $= 3270 - 1468$ ). The heatup rate during the PORV cycling phase was almost same as the experiment. The cycling phase was ended at 3185 sec in calculation. During the spray and PORV cycling period the major contributor to the PCS heatup was considered as the core decay heat and the heat provided by PCP's.

Figures 13 and 14 show comparisons of the pressure and temperature at the same position as in Figures 7 and 8 up to 10000 seconds, respectively. The predicted pressure was monotonously decreased during the spray and PORV cycling phase, which was, however, higher than the experiment throughout the cycling phase. It was due to a difference in scram time, but the slope of pressure decrease was well agreed to the experiment. The secondary coolant temperature was also overpredicted as shown in Fig.14.

#### 4.3 Blowdown Phase

After the PCS hot leg temperature reached 597 K, the PORV was held open for the consequent 1580 seconds. During this period the primary coolant was discharged through the PORV, which caused a rapid depressurization until the onset time of saturation in PCS. As shown in Fig.11, the calculated pressure drop was almost same as the experiment until the PCS saturation. After the saturation, the calculation shows that the PCS pressure was almost constant until the PORV closure time (4769 seconds), which was quite different from the experiment. The difference in the pressurizer liquid level can be regarded as one reason for the pressure increase during the saturated blowdown period as shown in Fig.15. The calculated liquid level in the pressurizer was almost constant until the SG refill initiation, while the measured level was slowly decreased from the PORV open time. It is also shown that the high heatup rate during the spray cycling period yielded an overprediction in the pressurizer liquid level swell and in the PCS pressure. The over-estimated liquid level also contributed to the overprediction of mass flow rate through the PORV during the two-phase blowdown phase as shown Fig.16.

During the same period, the PCS temperature was also overpredicted, which indicated that the insufficient energy convected out the PORV. According to the reference [8], the effective flow area of PORV was correctly chosen, the reason for the insufficient energy discharged out the PORV, therefore, was a code inaccuracy in calculating the fluid density convected from the hot leg to the pressurizer surge line under the hot leg stratified. As shown in Fig.17, the measured fluid density at the intact loop hot leg was different from the calculated one from 3500 seconds, approximately. The experiment indicated that the intact loop hot leg was stratified shortly after holding open PORV, that a higher quality fluid was convected out the break as pressurizer level receded and that the hot leg fluid density significantly decreased. However, RELAP5/MOD3 predicted this phenomena inaccurately, which due to a code weakness in calculating the junction density under the stratified condition.

During the blowdown period, the SCS experienced the similar depressurization

to the previous phase as shown in Figures 13 and 14.

#### 4.4 Recovery Phase

After 265 seconds from the closure of PORV, the SG secondary side refill was initiated through the auxiliary feedwater line. The predicted hot leg pressure and temperature were rapidly decreased during the secondary refill period as shown in Figures 11 and 12. However, the magnitudes of drops in pressure and temperature were overpredicted. One of the reason for this overprediction was considered as an difference in the refill duration (1085 seconds in calculation versus 622 seconds in experiment). It is also shown in Fig.17, which presents a comparison of the SG liquid level in long term. The calculated liquid level indicated no jump which was found in the experiment and the predicted refill duration was longer than the experiment. Since the refill duration was strongly dependent on the SG secondary side liquid level, the inaccuracy of the level prediction may extend the refill duration, consequently increase the cooling effect. The major contributor to their accuracy of level prediction was a void distribution calculated by the code.

After restoring the SCS heat removal capacity, the predicted SCS pressure was increased more rapidly and the predicted peak pressure was higher than the experiment as shown in Fig.13. During the same period the predicted temperature at SG secondary side moved down as shown in Fig.14, which indicates the return from the superheated steam to the saturated state in SG secondary side at 5200 seconds, approximately. The reason for the overprediction of pressure was considered as a propagation from the previous phase. The descending behavior in pressure after saturation was almost similar to the experiment.

During the equilibration period of 966 seconds after the SG refill completion (6119 seconds in prediction), the PCS pressure and temperature were slightly increased. The calculation shows that the SG feed and bleed operation was initiated at 7085 seconds, that the PCS pressure and temperature were both decreased in stepwise manner and that the magnitudes of drops in the pressure and temperature were larger than those measured. It due to the continual feed operation from the auxiliary feedwater valve, which was different from the continuous feed operation in the experiment. Since the feed operation is also

strongly dependent on the SG secondary side liquid level, the reason for this larger drops than the experiment can be regarded as the inaccuracy of the SG secondary void distribution.

## 5. Run Statistics

The main frame computer used in the present calculation was a CRAY-2S in System Engineering Research Institute(SERI) in Taejon, Korea under UNICOS as a operating system. Figure 19 presents the plot of the required CPU time for the transient time in the calculation. And the time step size are also plotted in Fig.20. The user-specified maximum time step was 1.0 second up to 1000 seconds, 0.1 second up to 2000 seconds, 0.5 second up to 4000 seconds, 0.1 second up to 8000 seconds and 0.5 second up to 10000 seconds in real time. The grind time can be calculated as follows.

$$\text{Computer time, } \quad \text{CPU} = 7981.4 - 1.9181 = 7979.48 \text{ (sec)}$$

$$\text{Number of time step, } \quad DT = 89332 - 220 = 89112$$

$$\text{Number of volume, } \quad C = 125$$

$$\text{Transient real time, } \quad RT = 8100 \text{ (sec)}$$

$$\text{Grind time} = \text{CPU} \times 1000 / (C * DT) = 0.71635 \text{ CPU m sec/vol/step}$$

## 6. Conclusions

The RELAP5/MOD3 5m5 code was assessed using the test L9-1/L3-3 simulating a LOFA with multiple failures and the consequentially-induced LOCA. The full period of the test was divided into four sub-periods according to the thermal-hydraulic characteristics ; the initial heatup phase, the spray and PORV cycling phase, the blowdown phase and the recovery phase. The calculation results were compared with the measured data and the evaluation of the code predictability for this type of transient was conducted. The following conclusions are obtained.

- 1) RELAP5/MOD3 code calculation was successfully executed for the L9-1/L3-3 test and the code applicability to an anticipated transient with multiple failures in PWR was demonstrated.
- 2) From the fact that the result from the calculation generally shows a good agreement with the experiment data, the overall predictability of the RELAP5/MOD3 was identified and the minor discrepancies were also identified.
- 3) In the initial heatup phase, the predicted scram time was earlier than the experiment due to a code uncertainty in predicting the spray mass flow rate and the associated condensation phenomena in pressurizer, which caused an excessive heatup rate in the spray cycling phase.
- 4) In the blowdown phase, the overprediction of PORV-discharged flow was found under the over-estimated pressurizer level, which may come from the excessive heatup in the previous phase. And a code inaccuracy was found in calculating the junction fluid density at the hot leg to the pressurizer surge line under the stratified condition.
- 5) In the recovery phase, an excessive cooling was predicted both in the steam generator secondary refill phase and in the secondary feed and bleed operation phase due to a poor prediction on void distribution in the SG secondary side.

## References

1. EG&G, *RELAP5 Input Data Requirements*, Appendix A to RELAP5/MOD3 Code Manual, January 1990.
2. W. Weaver, *Improvement to the RELAP5/MOD3 Choking Model*, EGG-EAST-8822, December 1989.
3. J. Adams, *Quick-Look-Report on LOFT Nuclear Experiment L9-1/L3-3*, EGG-LOFT-5340, April 1981.
4. D. Reeder, *LOFT System and Test Description*, NUREG/CR-0247, July 1978.
5. M.McCormick-Barger, *Experiment Data Report for LOFT Anticipated with Multiple Failures Experiment L9-1 and Small Break Experiment L3-3*, - NUREG/CR-2119, June 1981.
6. R. Beelman, *LOFT Experiment Operating Specification Anticipated Transients With Multiple Failures Test Series L9*, EGG-LOFT-5334, April 1981.
7. B. Sheron, *Generic Assessment of Delayed Reactor Coolant Pump Trip During Small Break Loss-of-Coolant Accident in Pressurized Water Reactors*, NUREG-0623, November 1979.
8. R. Beelman, *RELAP5 Reference Calculation and Posttest Analysis of Anticipated Transient with Multiple Failures Experiment L9-1/L3-3*, EGG-LOFT-5895, September 1982.
9. Y.S. Bang, et al, *Assessment of RELAP5/MOD2 Cycle 36.04 Using LOFT Large Break Experiment L2-5*, NUREG/IA-0032, April 1990.
10. E.J. Lee et al, *ICAP Assessment of RELAP5/MOD2 Cycle 36.05 Against LOFT Small Break Experiment L3-7*, NUREG/IA-0031, April 1990

Table 1. Initial conditions for L9-1/L3-3

<u>Parameter</u>	<u>Measured</u>	<u>Simulated</u>
<b>Primary Coolant System</b>		
Mass flow rate (kg/s)	$479.1 \pm 2.6$	479.34
Hot leg pressure (MPa)	$14.9 \pm 0.10$	14.8905
Cold leg temperature (K)	$558.9 \pm 1.3$	559.132
Hot leg temperature (K)	$578.2 \pm 1.8$	578.327
<b>Reactor</b>		
Power level (MW)	$49.6 \pm 0.9$	49.6
Maximum linear heat generation rate (kW/m)	$50.8 \pm 3.6$	50.8
<b>Steam Generator Secondary Side</b>		
Water level (m)	$0.14 \pm 0.08$	0.1475
Water temperature (K)	$545.0 \pm 0.8$	542.377
Pressure (MPa)	$5.67 \pm 0.08$	5.72
Mass flow rate (kg/s)	$27.0 \pm 1.0$	26.728
<b>Broken Loop</b>		
Hot leg temperature (K)	$563.3 \pm 2.6$	559.137
Cold leg temperature (K)	$557.6 \pm 2.6$	558.381
<b>Pressurizer</b>		
Steam Volume ( $m^3$ )	$0.43 \pm 0.05$	---
Liquid volume ( $m^3$ )	$0.50 \pm 0.05$	---
Water temperature (K)	$614.9 \pm 1.3$	610.4
Pressure (MPa)	$14.93 \pm 0.25$	14.901
Liquid level (m)	$0.92 \pm 0.1$	0.96

Table 2. Sequence of events in L9-1/L3-3

<u>Event</u>	<u>Description</u>	<u>Measured</u> (sec)	<u>Calculated</u> (sec)
<u>L9-1</u>			
Main feedwater pump off		0.0	0.0
Pressurizer spray activated	$P_{pzr} > 15.338^*$	$30.0 \pm 0.1$	28.94
Reactor scram (15.67 MPa) $t_{SCRAM}$	$P_{ILHL} > 15.745$ $T_{ILHL} > 583.16^*$	$65.4 \pm 0.2$	55.8
Steam generator main steam control valve closed	$t_{SCRAM} + \text{delay}^*$	$77.2 \pm 0.2$	69.0
Steam generator liquid level reached bottom of range	$L_{S/G} = 0.25 \text{ m}$	$190 \pm 20$	82.0
Pressurizer spray valve cycling initiated	$P_{pzr} > 15.338$	$208.9 \pm 0.1$	315.0
Pressurizer liquid level reached top of the range	$L_{pzr} = 1.83 \text{ m}$	$1089.7 \pm 30$	1840.0
Pressurizer spray valve cycling ended	$P_{pzr} > 16.2$	$1246.0 \pm 0.1$	1370.0
PORV cycling initiated	$P_{pzr} > 16.2$	$1467.9 \pm 0.1$	1795.0
<u>L3-3</u>			
PORV latched open ( $t_{LATCH}$ )	$T_{ILHL} > 597$	$3269.9 \pm 0.1$	3189.0
PCPs tripped off	$T_{ILHL} > 597$	$3284.8 \pm 0.2$	3189.0

(continued)

<u>Event</u>	<u>Description</u>	<u>Measured</u> (sec)	<u>Calculated</u> (sec)
PCP coastdown completed		3304.2 $\pm$ 0.8	3220.0
Upper plenum fluid reached saturation pressure		3329.4 $\pm$ 0.2	3270.0
PORV closed ( $t_{PORV-CLOSE}$ )	$t_{LATCH} + 1580$	4849.7 $\pm$ 0.1	4769.0
Steam generator secondary refill initiated	$t_{PORV-CLOSE} + 265$	5114.6 $\pm$ 0.2	5034.0
Natural circulation initiated		5205 $\pm$ 10	---
Steam generator secondary refill completed ( $t_{REF-COM}$ )	$L_{S/G} = 2.9464$	5746.4 $\pm$ 0.2	6119.0
Pressurizer liquid level reached bottom of the range	$L_{pqr} = 0.06$	5915 $\pm$ 5	5460.0
Steam generator secondary feed and bleed initiated	$t_{REF-COM} + 966$	6712.2 $\pm$ 0.2	7822.2
Experiment completed		9517.4 $\pm$ 0.2	---

Note --- : not predicted

\* : MPa in pressure, K in temperature, and m in level

Table 3. Summary of nodalization

Component	Vol	Jun	H.S
1.Reactor Vessel			
Filler Gap	7	7	14
Downcomer	6	6	18
Lower Plenum	3	5	5
Active Core	3	2	6
Core Bypass	3	2	---
Upper Plenum	3	4	5
Upper Head	1	1	2
2.Primary Coolant System (Intact Loop)			
Hot Leg (included S/G inlet plenum)	6	7	8
S/G U-tube	6	5	6
Loop Seal (included S/G outlet plenum)	4	4	3
Pump Suction Tee	5	6	5
Primary Coolant Pumps	2	4	---
Cold Leg (included pump discharge pipes)	8	12	7
3.Primary Coolant System (Broken Loop)			
Hot Leg	3	4	3
S/G-Pump Simulator	12	12	12
RABS	4	5	4
Cold Leg	5	6	5
QOBV/Line	2	2	---
4.Pressurizer System			
Surge Line/Valve	2	3	---
Pzr Vessel	9	8	10
Spray Line/Valve	1	3	---
Experiment PORV	---	1	---
Heater	---	---	1
5.Secondary Coolant System			
Feedwater Storage	2	2	---
S/G Downcomer	6	6	10
S/G Riser	5	4	12
Separator	1	3	1
Steam Dome/Line	3	2	2
MSCV/Bypass	---	2	---
6.ECCS	6	6	---
7.Others (Letdown/Charging, Containment)	3	1	---
Total	125	135	136

Table 4. Detailed information for heat structure

<u>No</u>	<u>NH</u>	<u>NA</u>	<u>Description</u>	<u>Left Bn.</u>	<u>Right Bn.</u>
60	6	8	SG U-tube	115-4:9	515-4:6
1151	2	4	SG Inlet/Outlet Plenum Wall	115-3,-10	Ambient
1152	2	20	S/G Tube Sheet Periphery Region	115-3,10	515-3
1001	12	11	Intact Loop Piping (Large Pipes)	100, 105, 110, 115-1 115-12,-13 120, 150 150, 175-1, 175-2, 180, 185	Ambient
1002	2	11	S/G Inlet-Cold Leg, Outlet-Hot Leg Connection	115-2, 11	Ambient
1003	7	11	Intact Loop Piping (0.216 m OD)	125, 130, 140, 145, 155, 160, 170	Ambient
1004	2	11	S/G Inlet/Outlet Plena	115-3,10,	Ambient
2000	1	21	Reactor Vessel Filler Block Inlet Annulus Top Volume	200	Insulated
2001	6	11	Core Support Barrel	Insulated 210-1:4	200, 205
2050	1	21	Filler Blocks Inlet Annulus Lower Volume	205-1	223-1
2100	6	21	Downcomer and Lower Plenum	210-1:4, 215, 220	223-2:7

(continued)

<u>No</u>	<u>NH</u>	<u>NA</u>	<u>Description</u>	<u>Left Bn.</u>	<u>Right Bn.</u>
2110	3	11	Reactor Vessel Wall (Mid-Part)	223-1:3	Ambient
2120	5	7	Reactor Vessel Wall (Lower-Part)	223-3:7	Ambient
2200	1	11	Reactor Vessel Bottom Wall	220	Ambient
2250	7	11	Core Flow Skirt-Core Filler Assembly	225, 230-1:3, 240, 245, 246	Insulated
2260	1	7	Lower Core Support Structure, Core Support Barrel Lips, Fuel Module Lower End Box	225	Insulated
2300	3	10	Active Core	230-1:3	Kinetics
2400	1	7	Upper Core Support Stucture	240	Insulated
2460	1	5	Fuel Module Top	245	246
2500	1	11	Core Support Barrel-Upper Plenum Lower Volume	250	Insulated
2510	2	5	Upper Plenum Internals	250	Insulated
2501	1	21	Core Support Barrel-Upper Plenum Upper part	250	Insulated
2550	1	21	Upper Head Top Plate	250	Ambient
3150	2	11	Broken Loop S/G Simulator 1	315-1:2	Ambient
3151	1	11	Broken Loop S/G Simulator 2	315-9	Ambient

(continued)

<u>No</u>	<u>NH</u>	<u>NA</u>	<u>Description</u>	<u>Left Bn.</u>	<u>Right Bn.</u>
3152	1	11	Broken Loop S/G Simulator 3	315-11	Ambient
3153	6	11	Broken Loop S/G Simulator 4	315-3:8	Ambient
3154	1	11	Broken Loop S/G Simulator 5	315-12	Ambient
3155	1	11	Broken Loop S/G Simulator 6	315-10	Ambient
3000	3	11	Broken Loop Hot Leg	300, 305 310	Ambient
2250	3	11	Broken Loop Cold Leg	335, 340, 345	Ambient
3501	1	11	Broken Loop Cold Leg	350-1	Ambient
3502	1	11	Broken Loop Cold Leg	350-2	Ambient
3700	4	11	Reflood Assist Bypass Piping	370, 375, 380, 385	Ambient
4151	1	11	Pressurizer Vessel Bottom	415-1	Ambient
4152	7	11	Pressurizer Vessel (Large Dia.)	415-2:7	Ambient
4162	1	11	Pressurizer Vessel (Small Dia.)	415-8	Ambient
4172	12	9	Pressurizer Backup Heater	415-2	Table 417/8
4201	1	11	Pressurizer Top Wall	420	Ambient
5000	3	4	S/G Shroud Upper Part	500, 505, 510-1	520, 515-8:7
5150	4	4	S/G Shroud Lower Part	510-1:4	515-7:4
5300	8	10	S/G Secondary Vessel Wall	530-1, 525 500, 505 510, 515-1:3	Ambient

Table 5. Summary of data channels and uncertainties in comparison plots

<u>Description</u>	<u>Calculation</u>	<u>Experiment</u>	<u>Uncertainty *</u>	<u>Fig. No</u>
1. Pressure at ILHL	p 100-01	PE-PC-005	0.28 MPa	4, 11
2. Coolant temperature at ILHL	tempf-100-01	TE-PC-02B	3.0 K	5, 12
3. Reactor power	rktppow-0	RE-T-77-A	2.0 MW	6
4. Pressure at SG steam dome	p 530-02	PE-SGS-01	0.12 MPa	7, 13
5. Coolant temperature at SG secondary	tempg 515-06	TE-SGS-04	3.0 K	8, 14
6. Liquid level at SG secondary	cntrlvar-1	LT-P004-08B	0.08 m	9, 18
7. Mass flow rate downstream MSCV	mflowj-550	FT-P004-012	0.8 kg/s	10
8. Liquid level at pressurizer	cntrlvar-2	LE-PdEP139-6	0.06 m	15
9. Mass flow rate through PORV	mflowj-425	FR-PC-S231	0.2 kg/s	16
10. Fluid density at the intact loop hot leg	rho-100	DE-PC-02C	0.17 Mg/m <sup>3</sup>	17

Note \* : Measurement uncertainty referred to the reference [5]

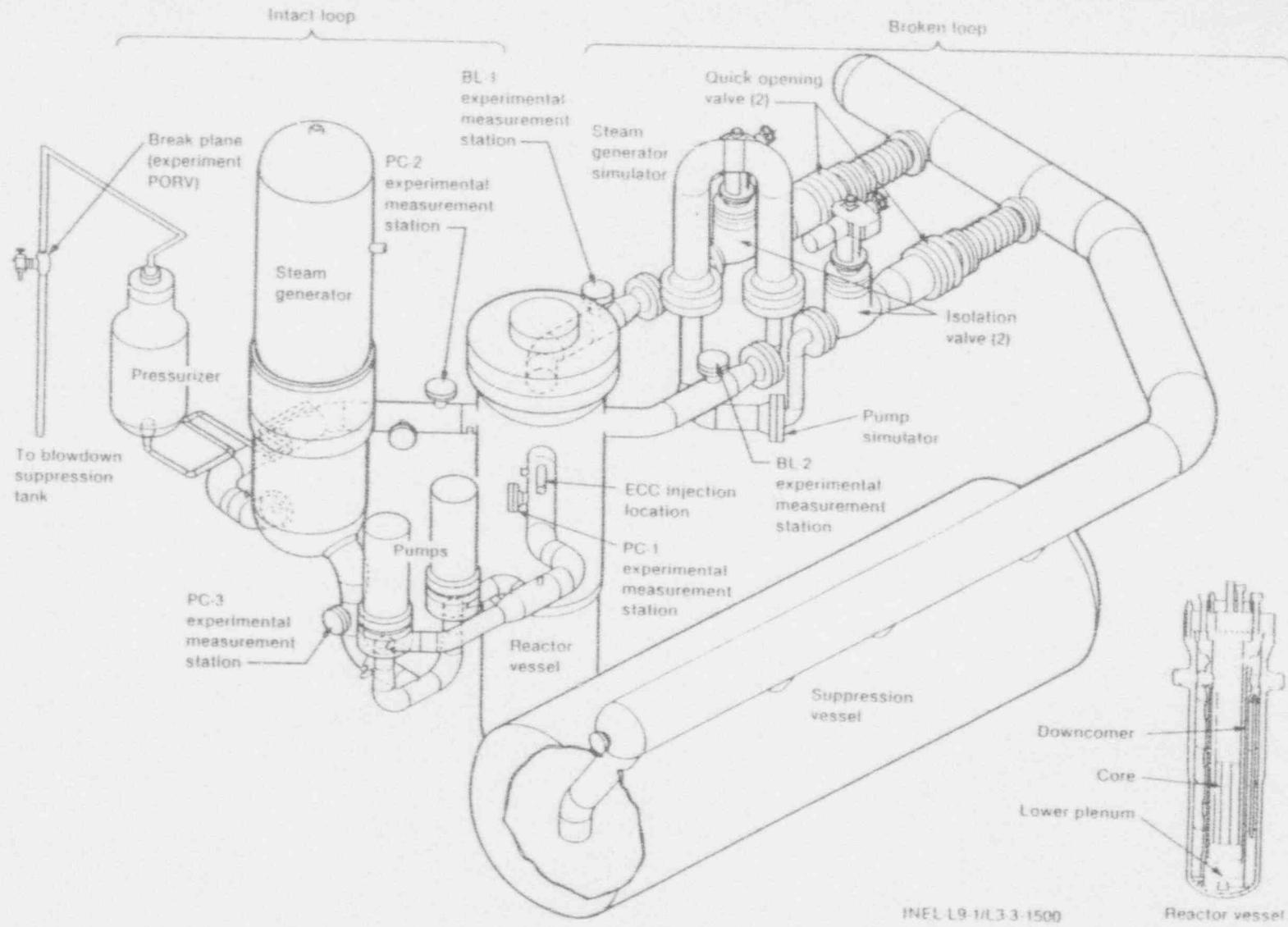


Fig.1 Axonometric configuration of LOFT L9-1/L3-3 test

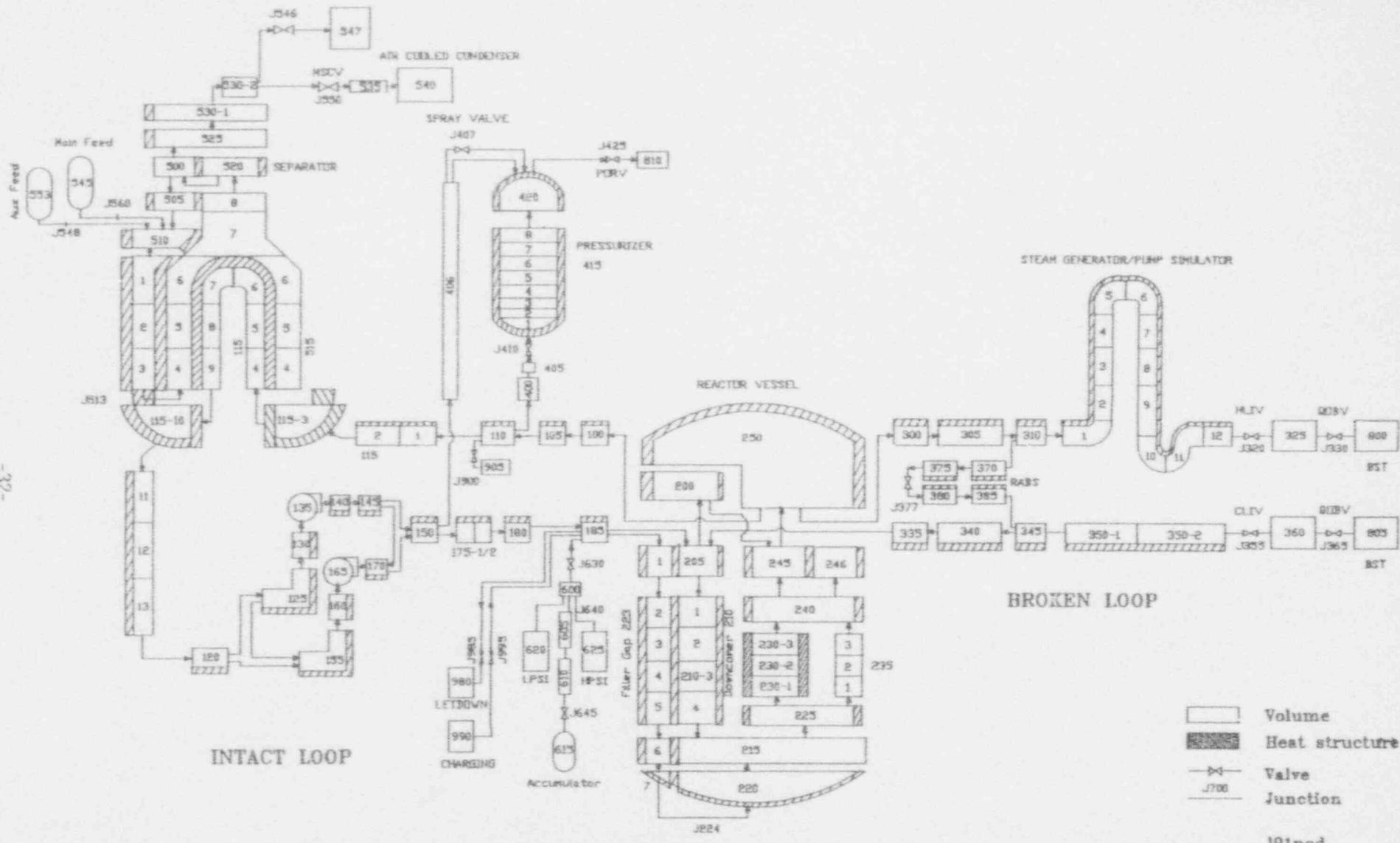


Fig. 2 RELAP5 Nodalization for LOFT Experiment L9-1/L3-3

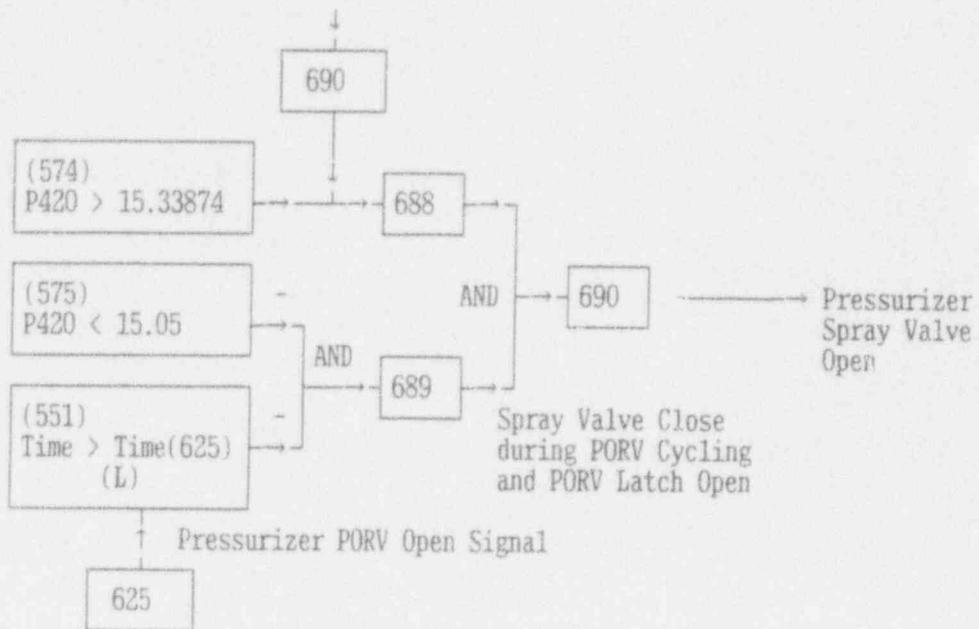


Fig.3-a. Pressurizer spray valve control trip

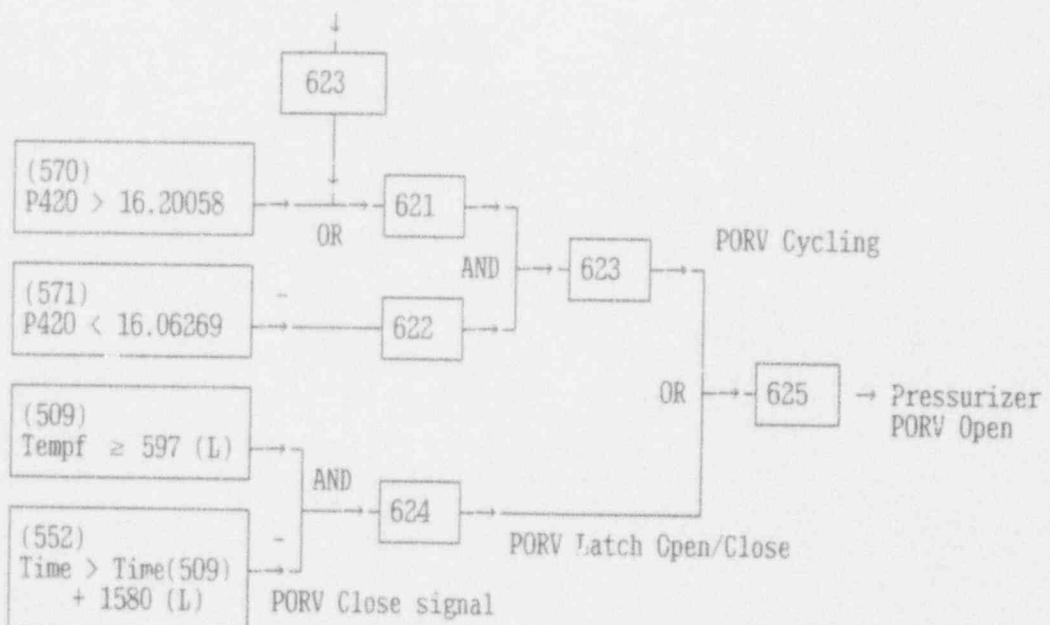


Fig.3-b. Pressurizer PORV control trip

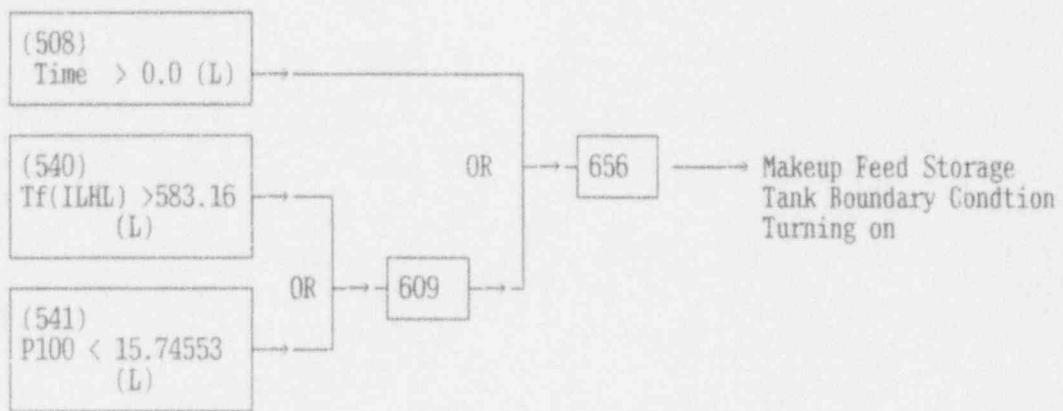


Fig.3-c. Makeup feed storage tank boundary condition trip

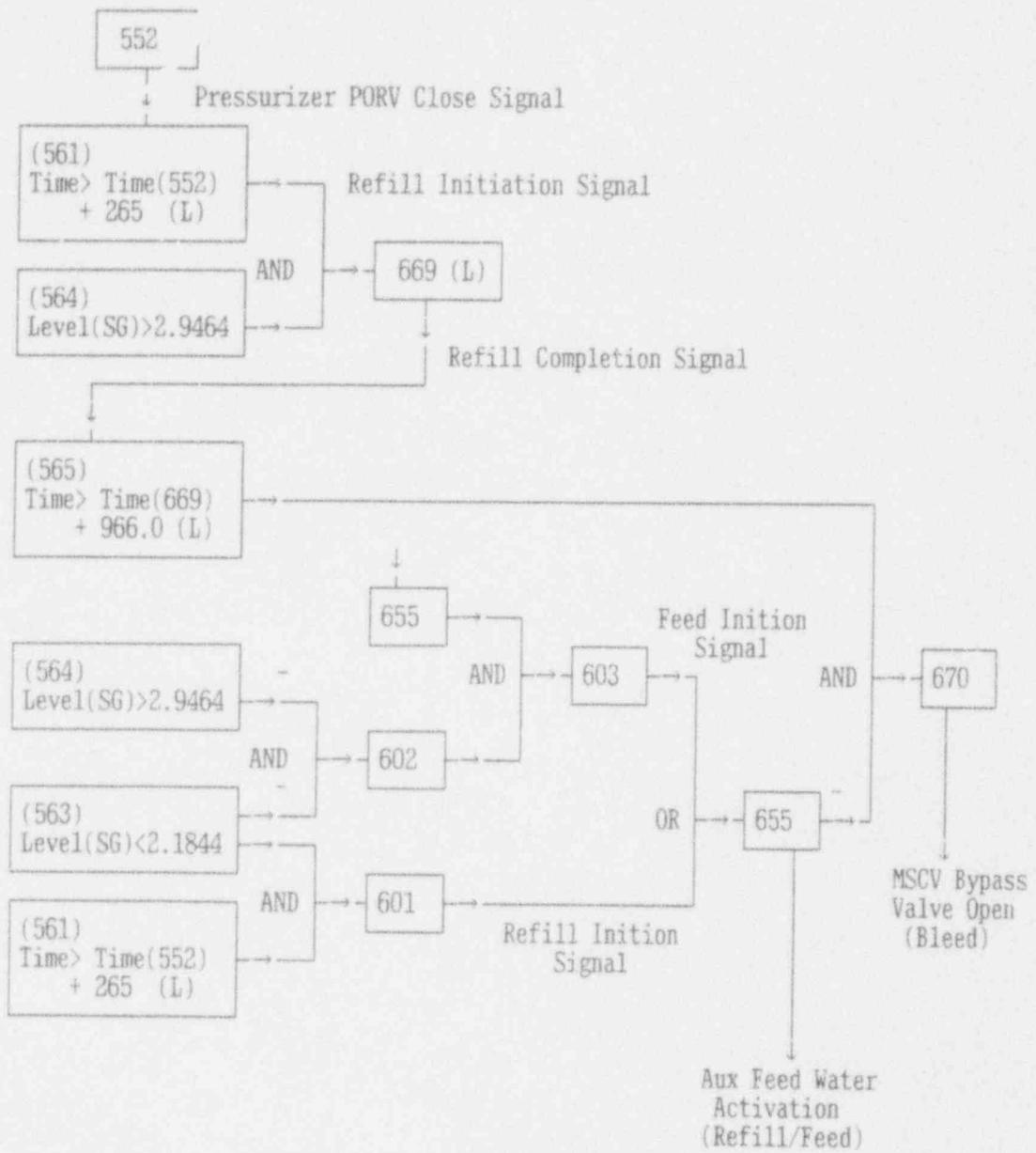


Fig.3-d MSCV bypass valve control trip

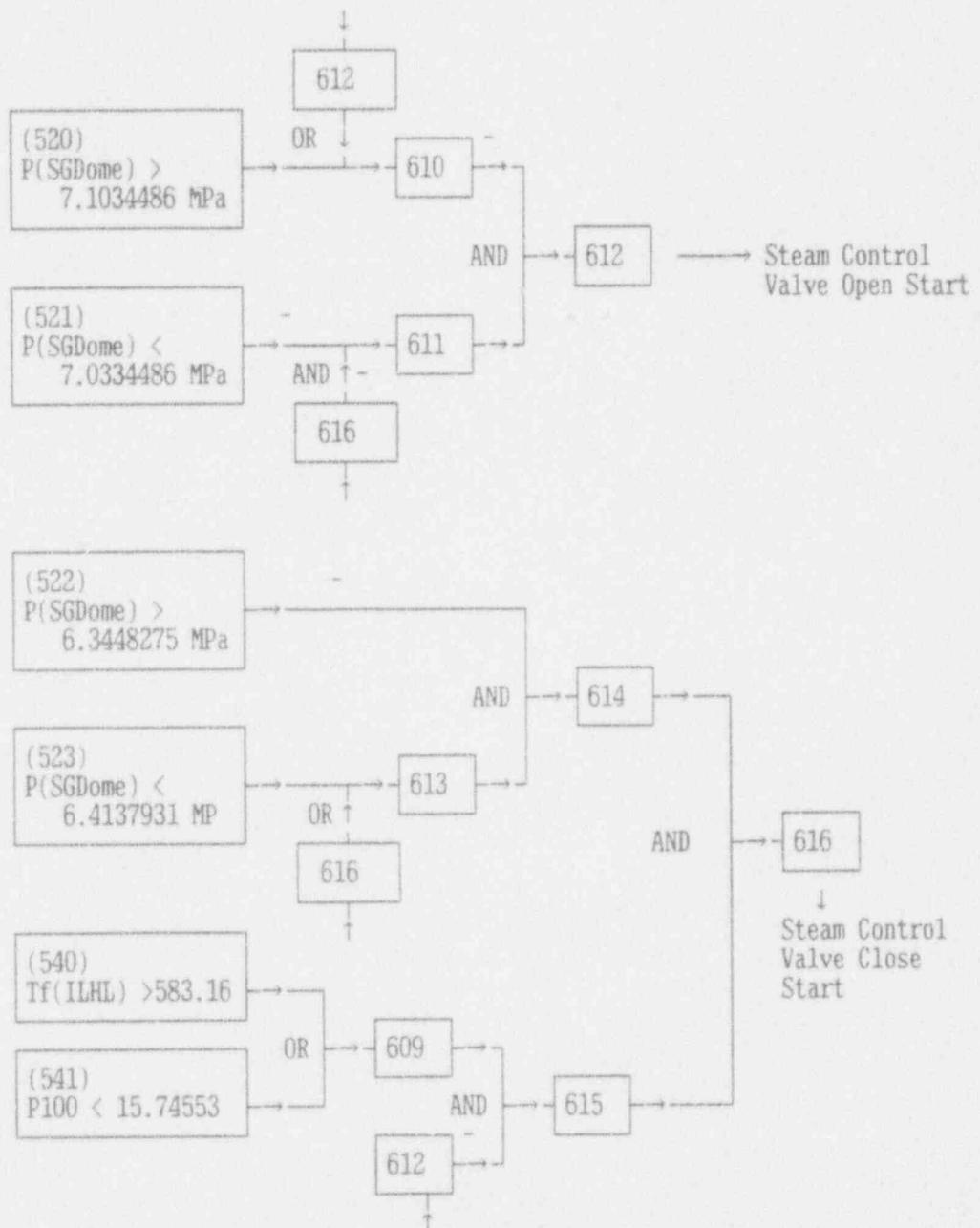


Fig.3-e MCSV open/close control trip

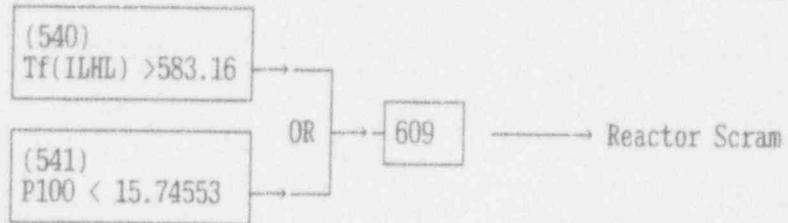


Fig.3-f Reactor scram trip

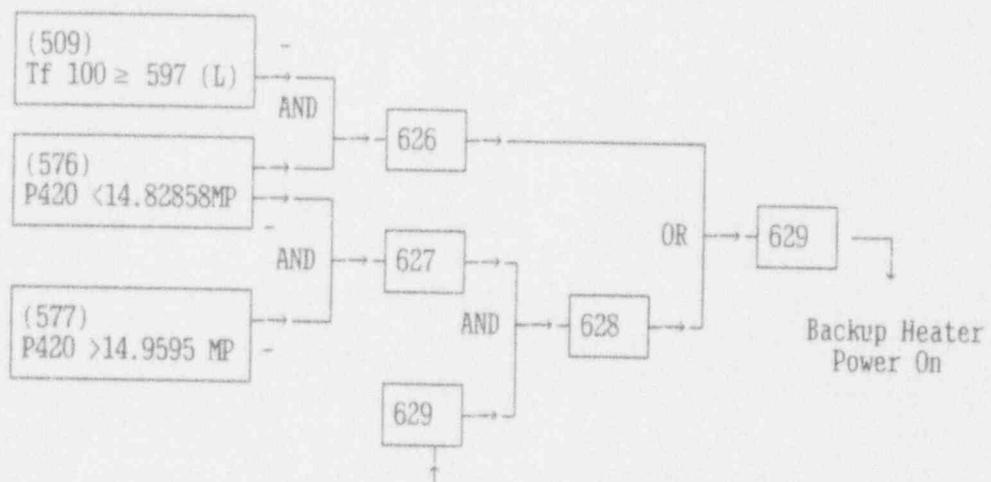
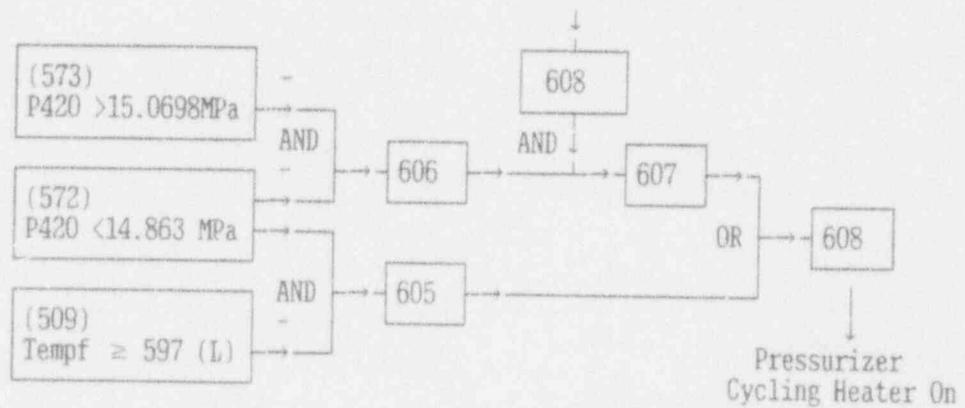


Fig.3-g Pressurizer heater control trip

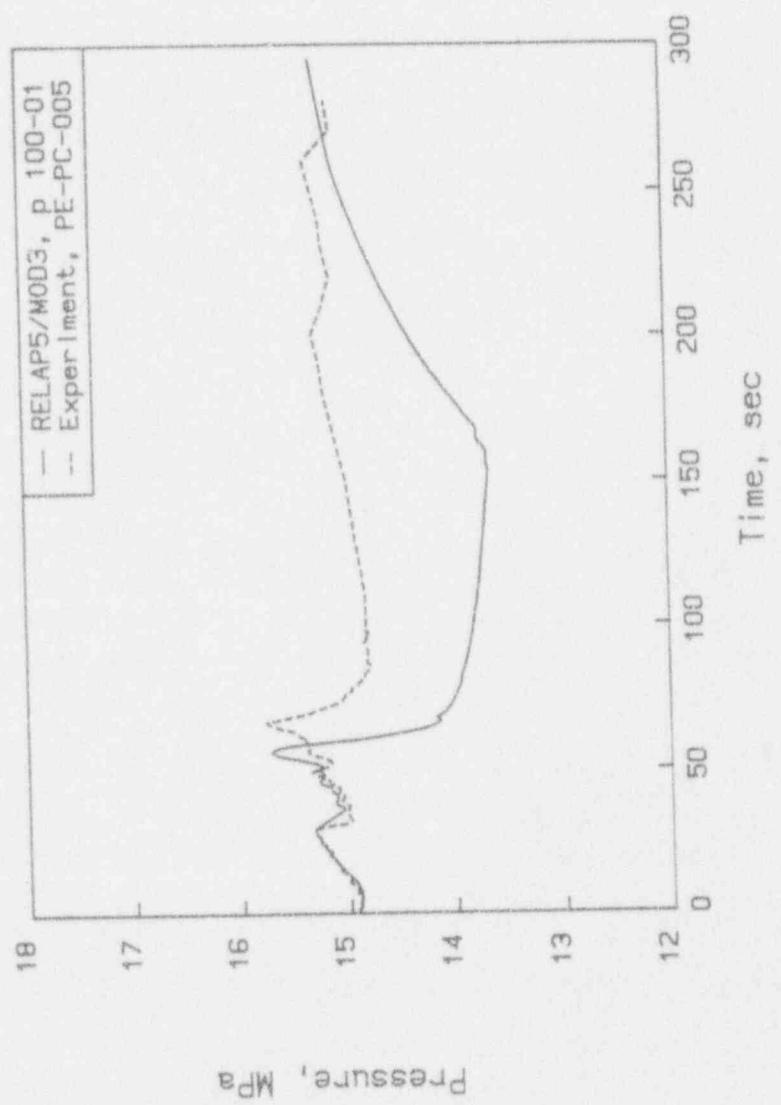


Fig.4 Comparison of pressure at the intact loop hot leg (short term)

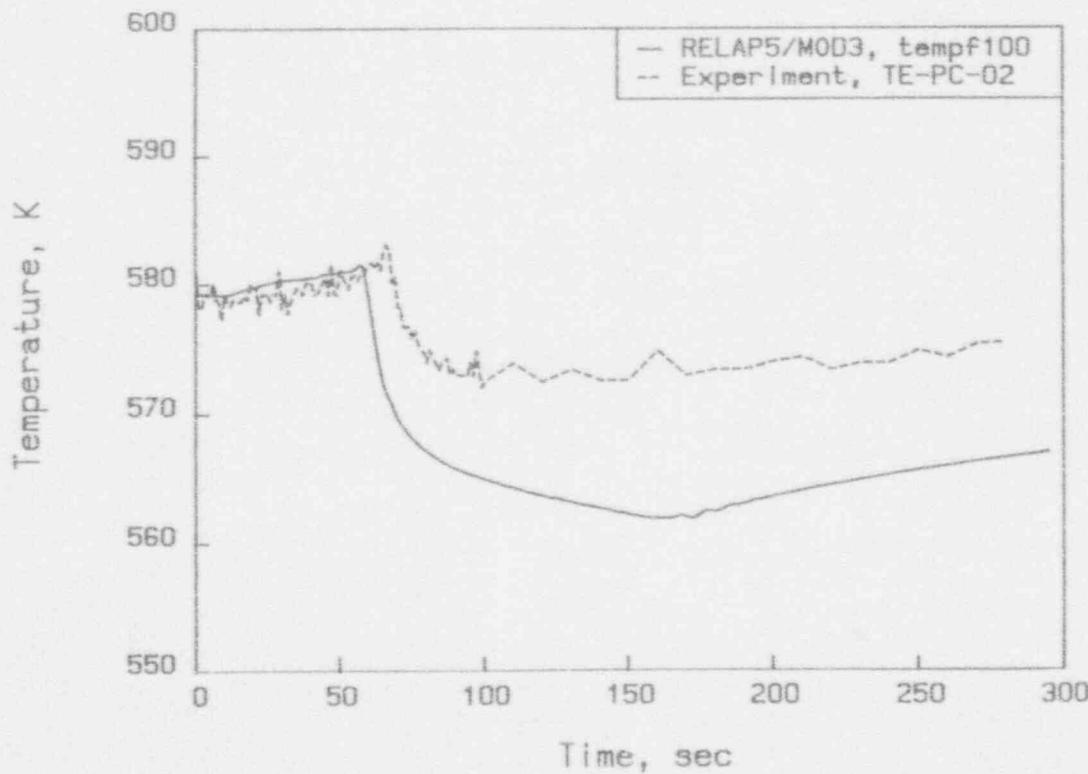


Fig.5 Comparison of coolant temperature at the intact loop hot leg (short term)

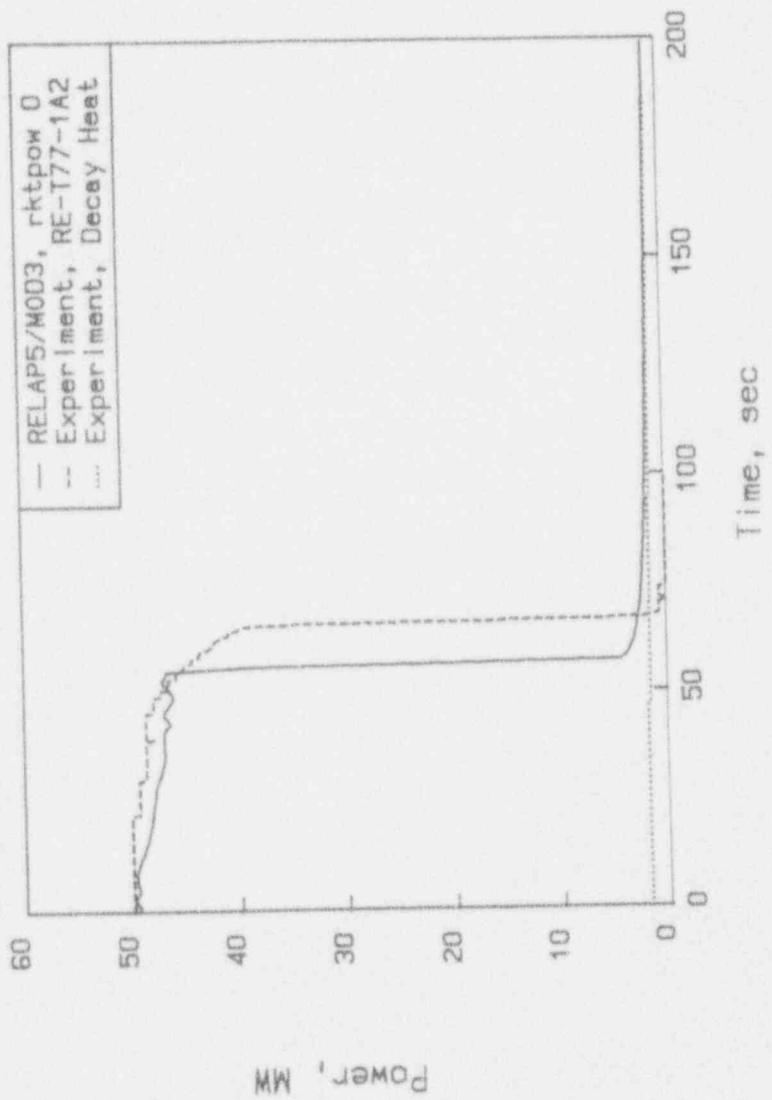


Fig.6 Comparison of reactor power

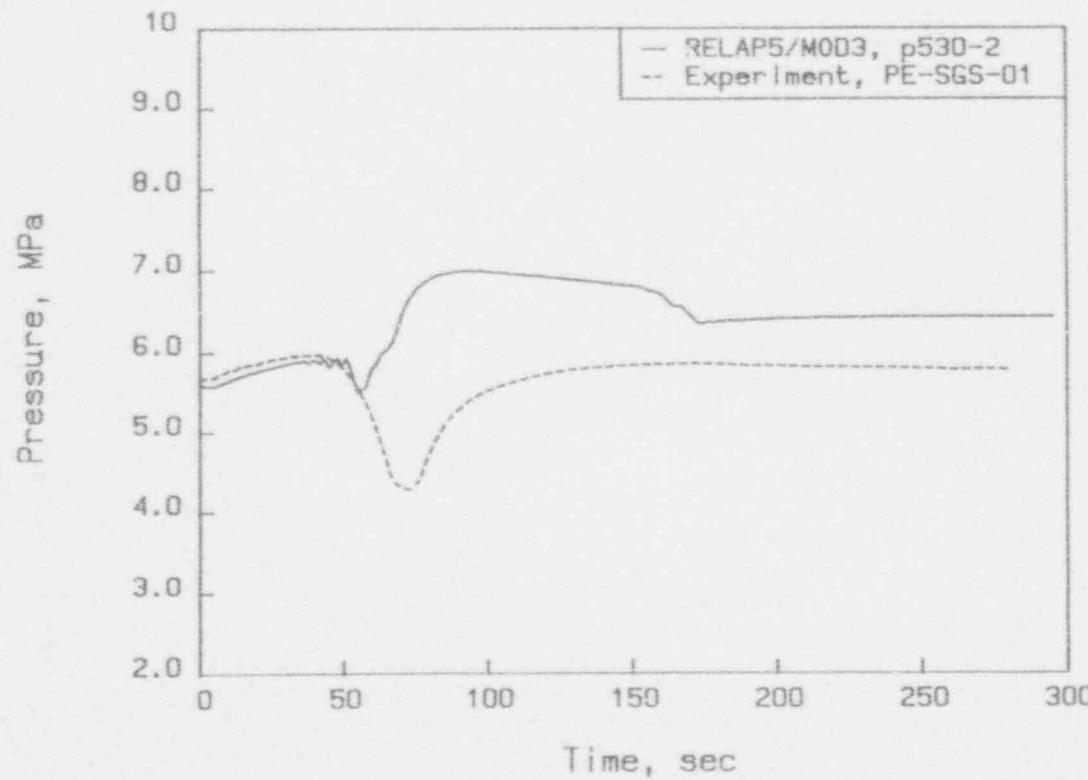


Fig.7 Comparison of pressure at SG steam dome (short term)

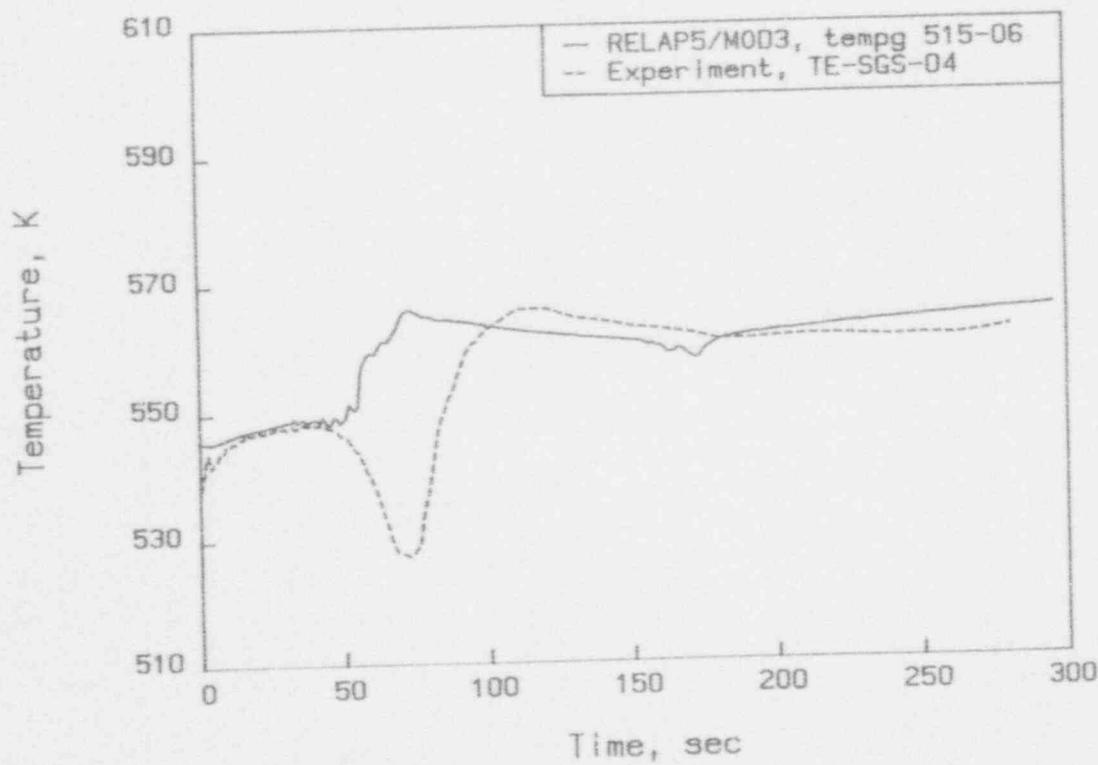


Fig.8 Comparison of coolant temperature at SG secondary side (short term)

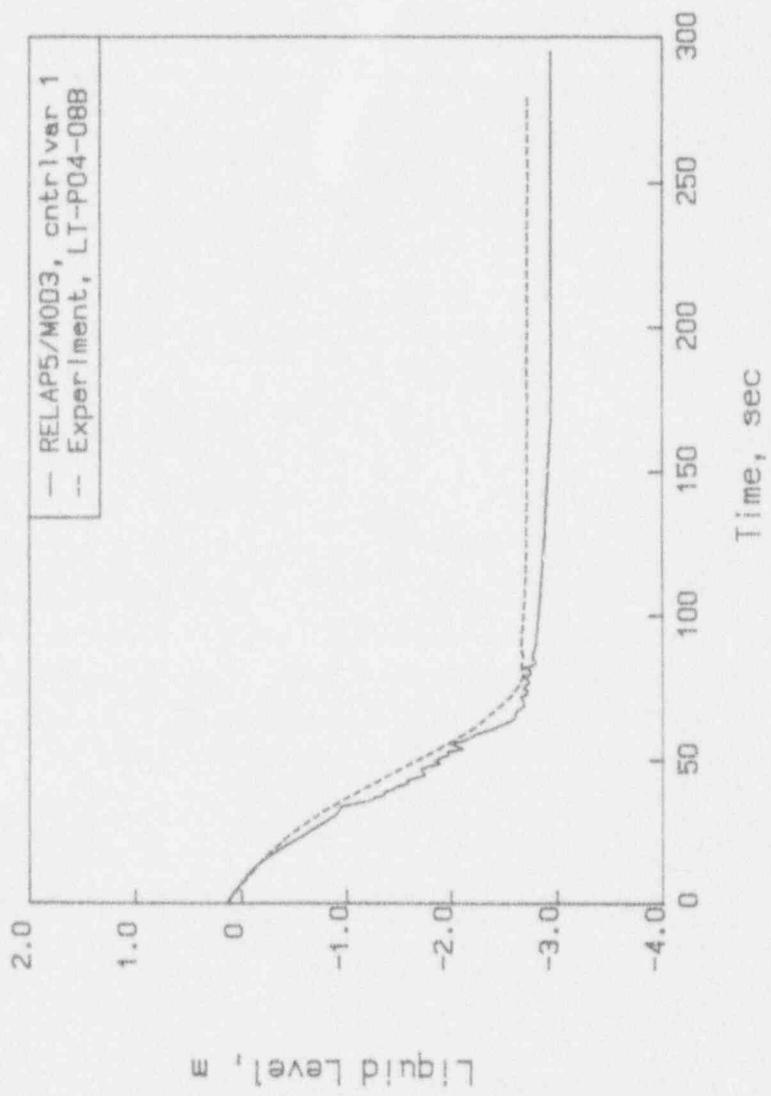


Fig.9 Comparison of SG collapsed liquid level (short term)

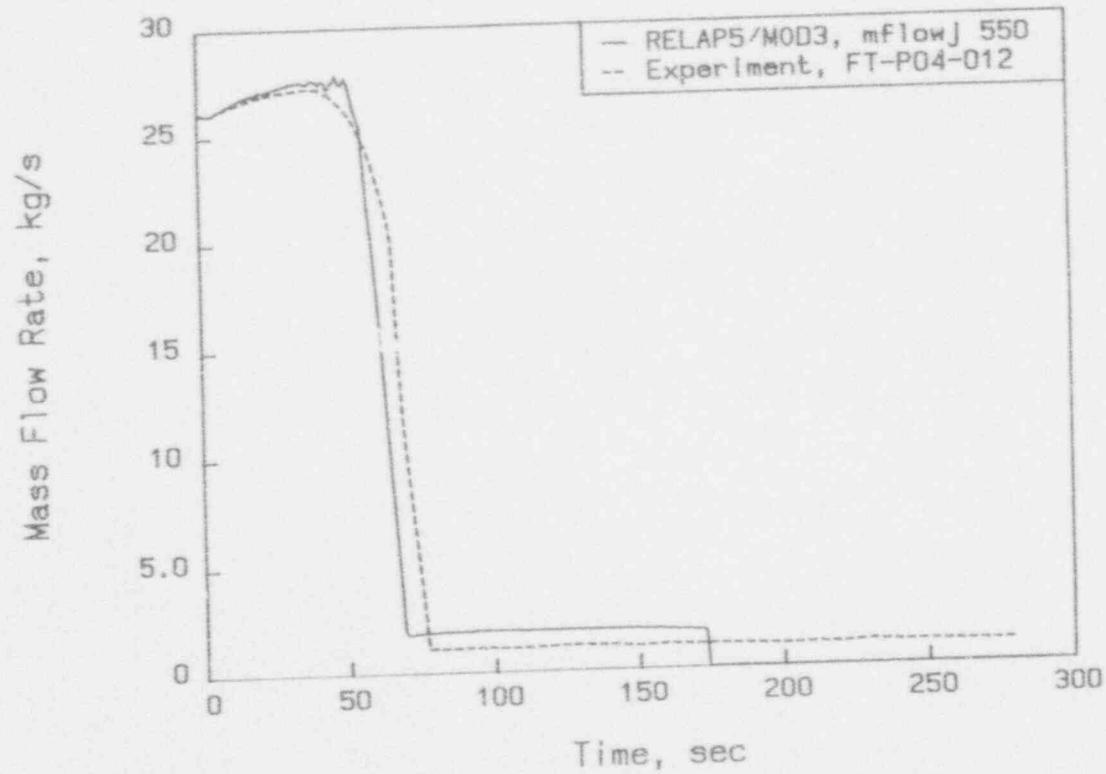


Fig.10 Comparison of mass flow rate through MCV (short term)

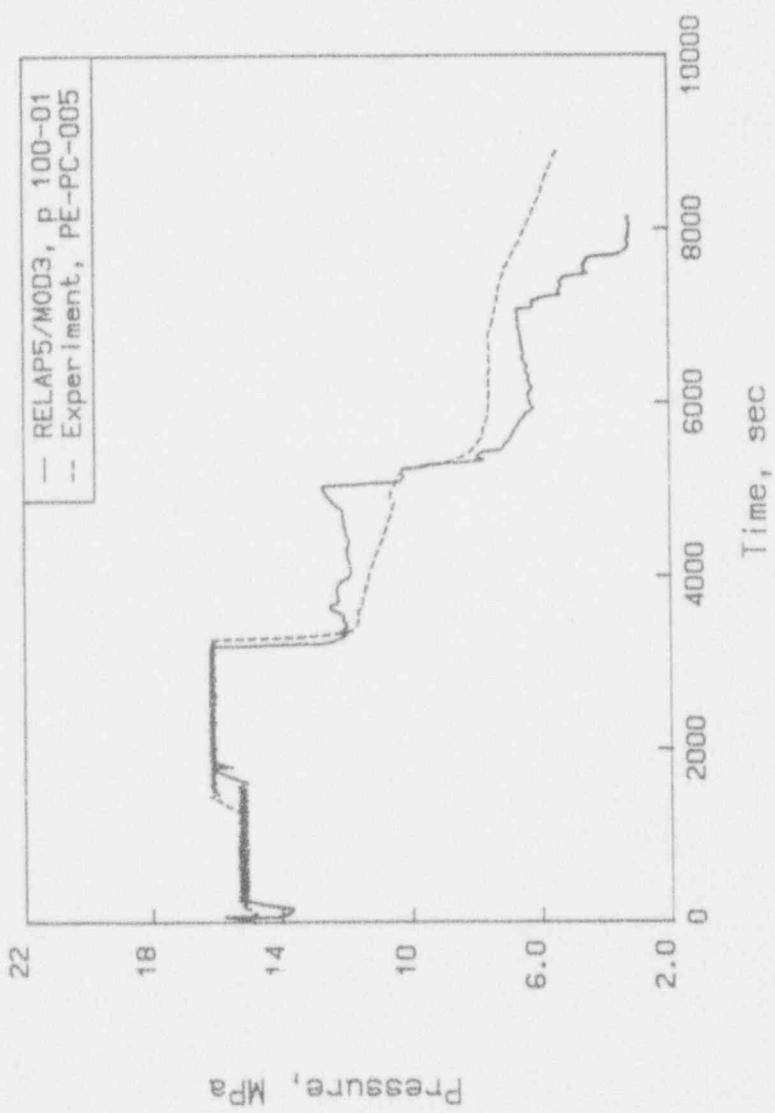


Fig.11 Comparison of pressure at the intact loop hot leg (long term)

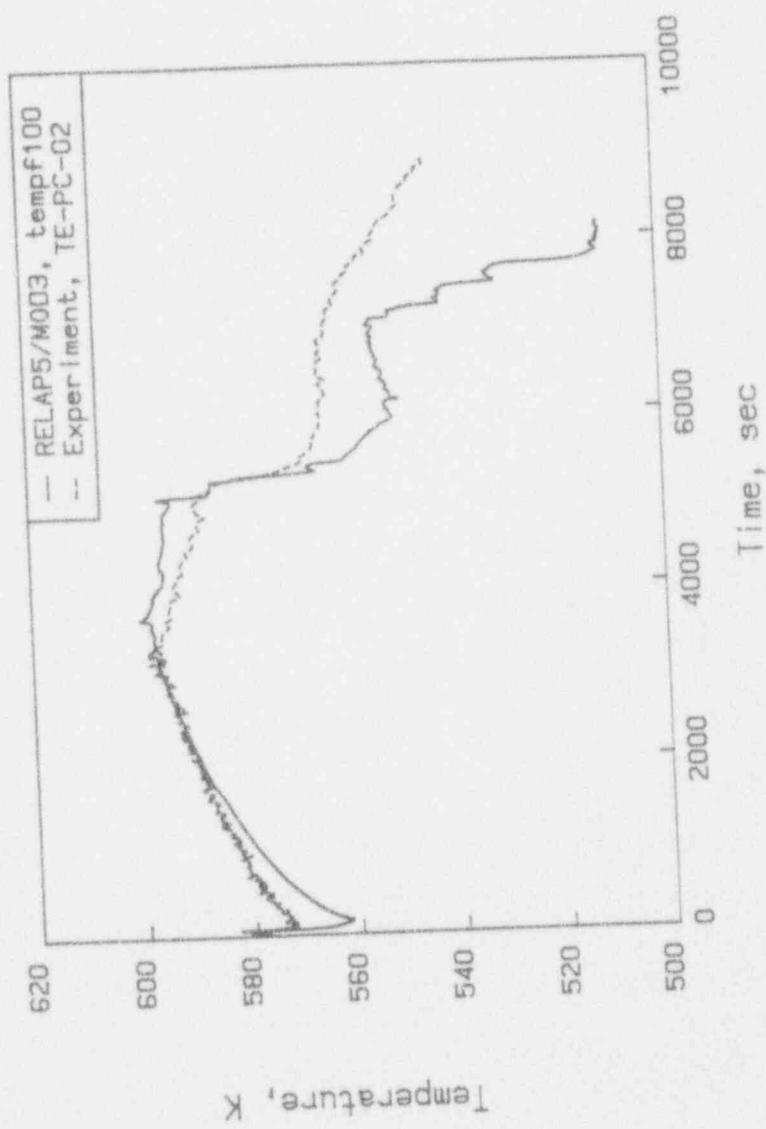


Fig. 12 Comparison of coolant temperature at the intact loop hot leg  
(long term)

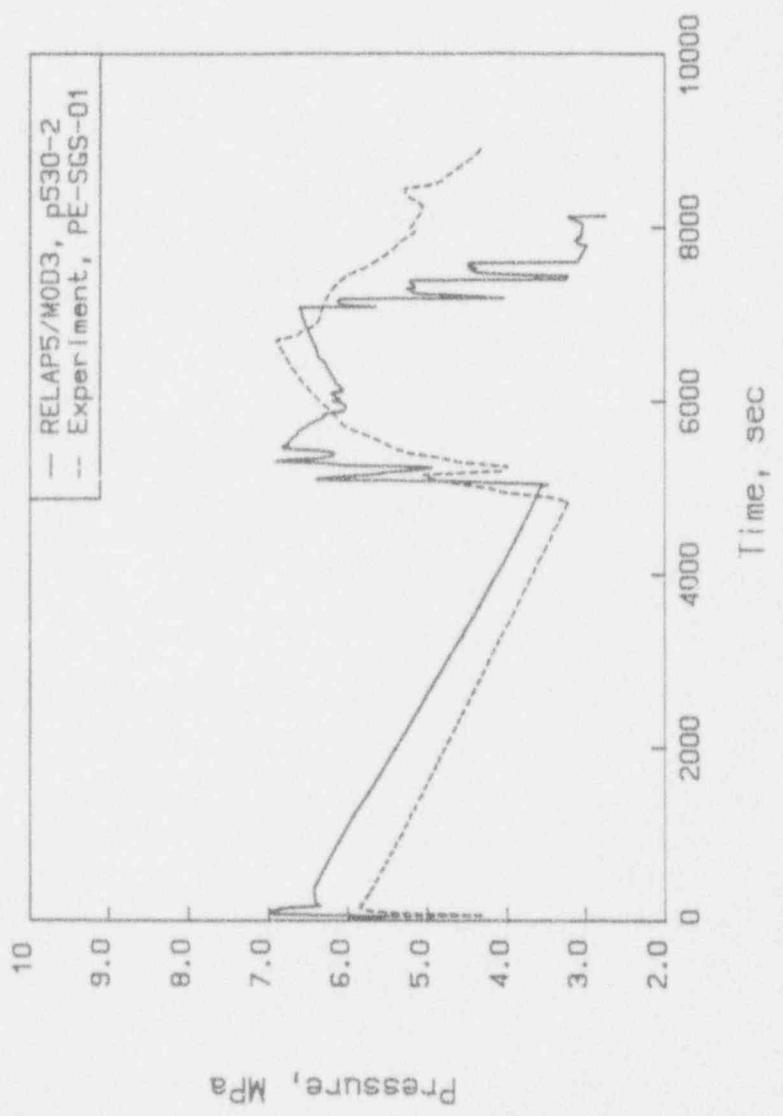


Fig.13 Comparison of pressure at S6 steam dome (long term)

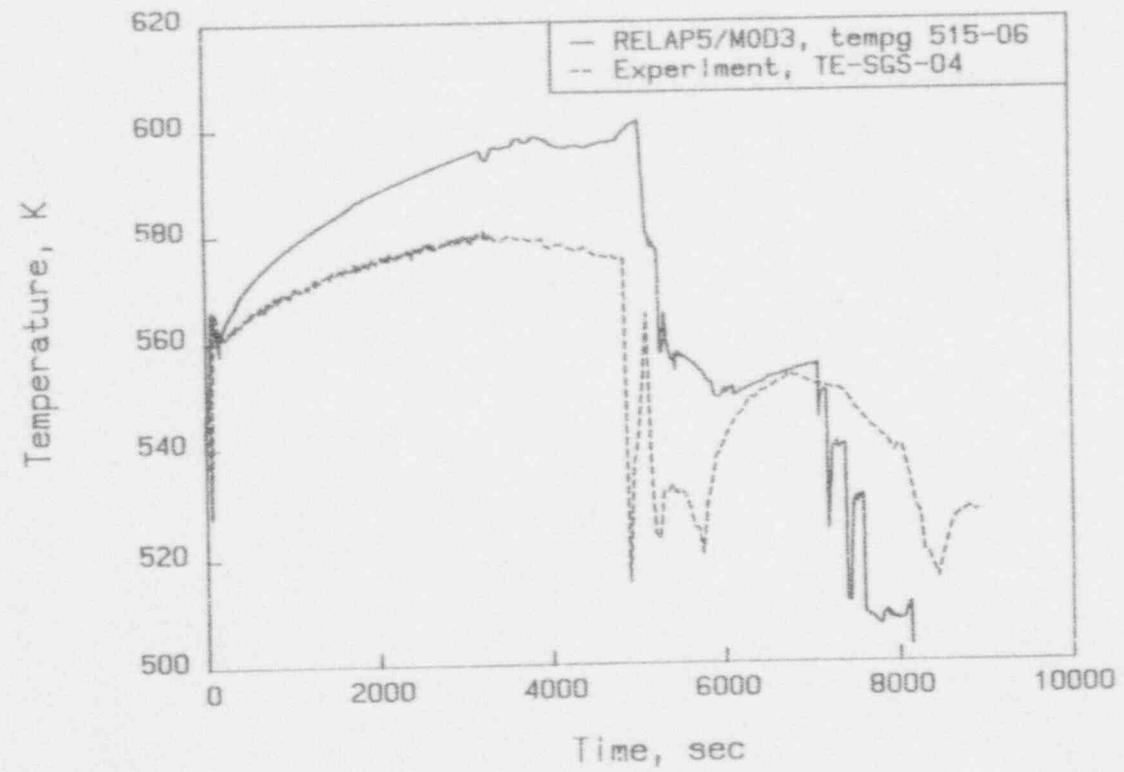


Fig.14 Comparison of coolant temperature at SG secondary side (long term)

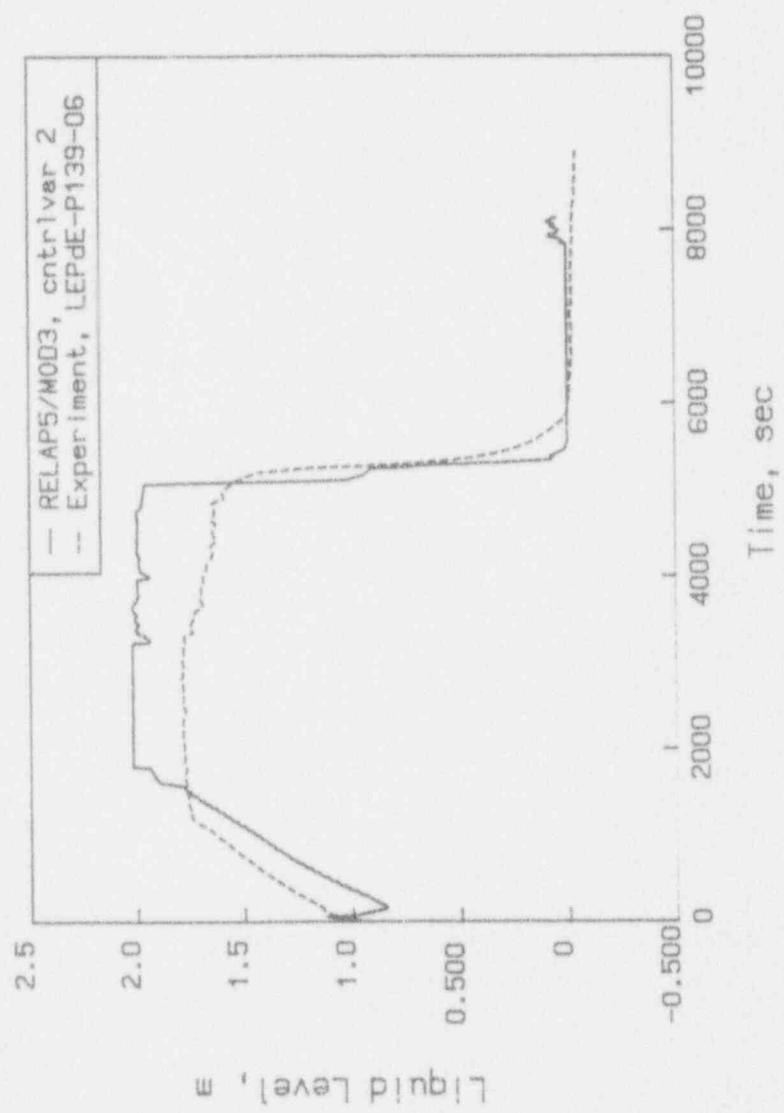


Fig.15 Comparison of pressurizer collapsed liquid level (long term)

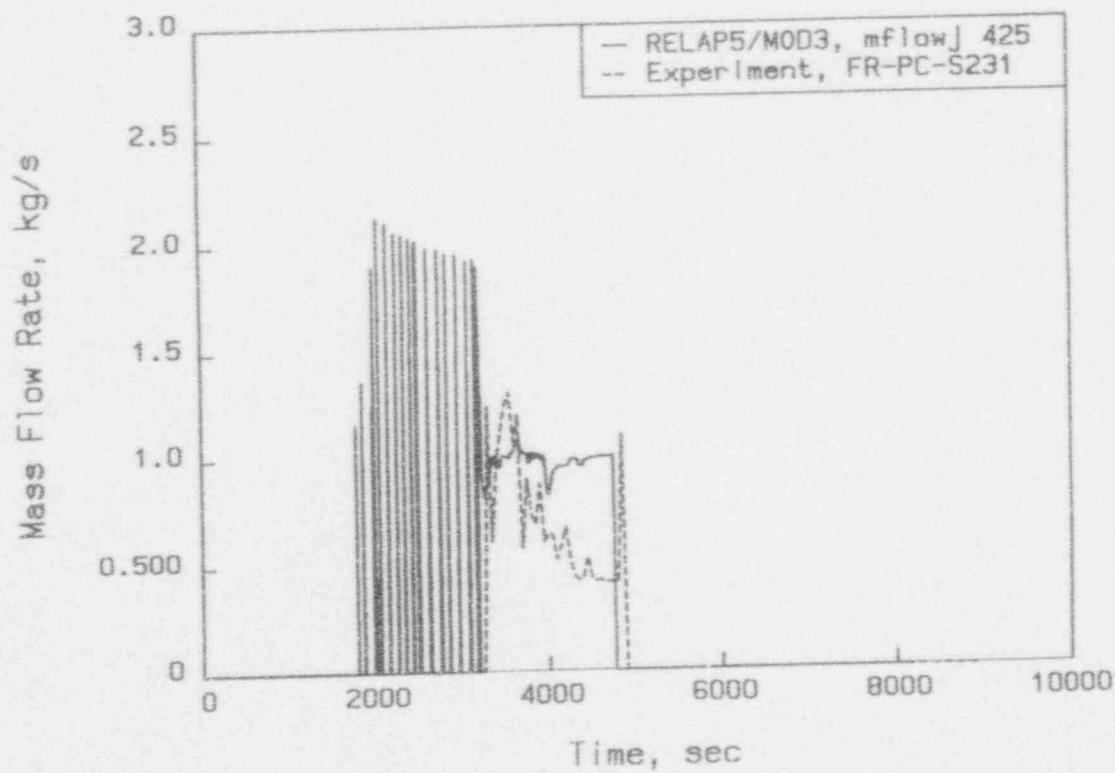


Fig.16 Comparison of mass flow rate through PORV (long term)

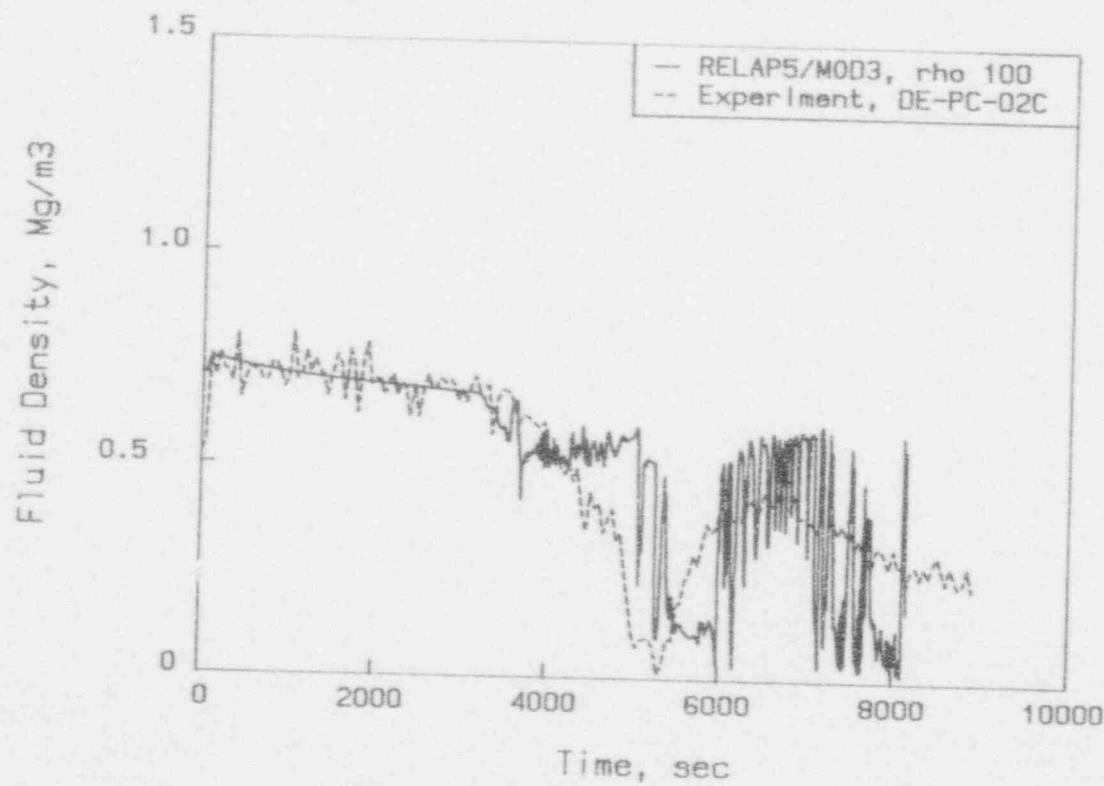


Fig.17 Comparison of fluid density at intact loop hot leg (long term)

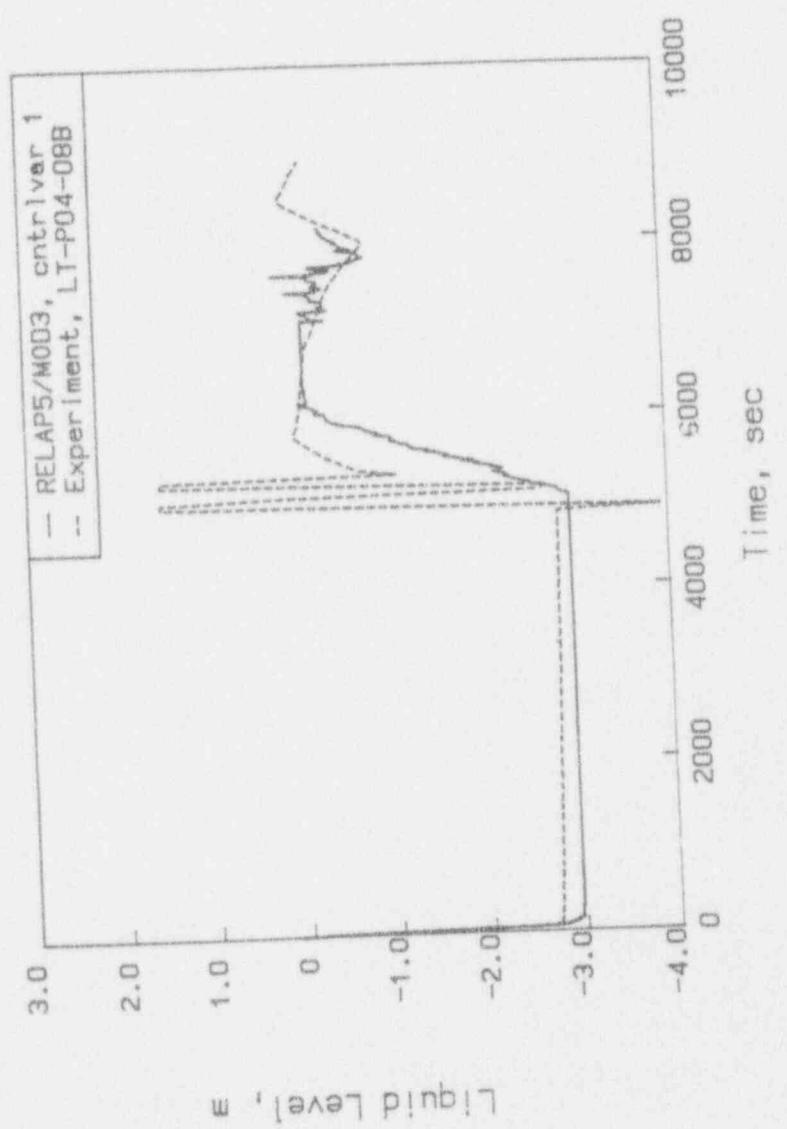


Fig.18 Comparison of SG collapsed liquid level (long term)

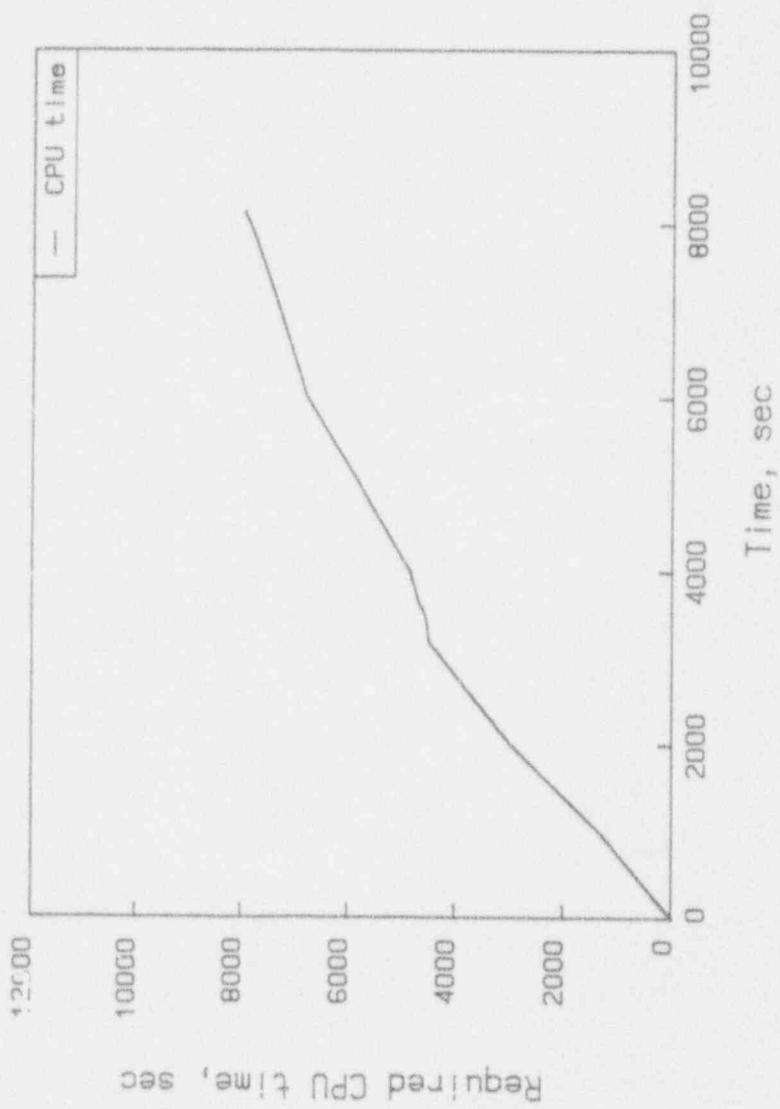


Fig.19 The required CPU time versus the advanced time

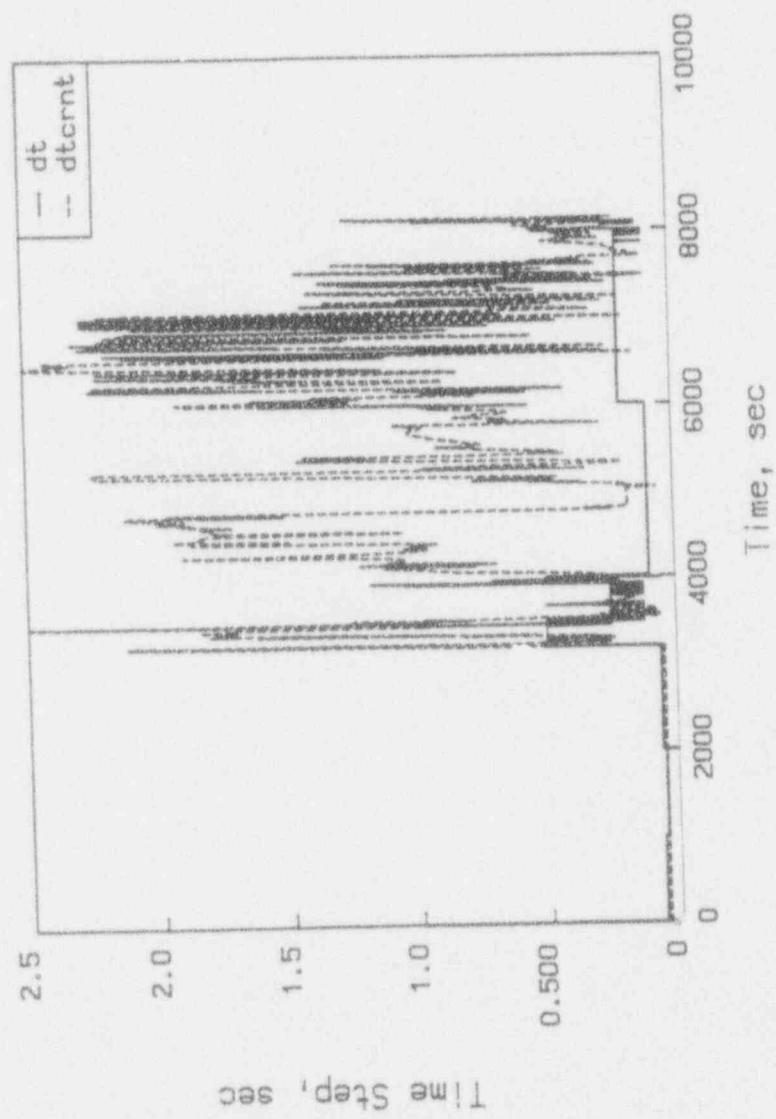


Fig. 20 Time step size of base case calculation

## **Appendix A      Input Deck for Steady State Calculation**

```

=loft 19-1 post test analysis deck
*-----|-----|-----|-----|-----|-----|
*      initial conditions
*
*      core power = 50. mw
*      pcc flow = 479.3 kg/s
*      thot = 578. k
*      teold = 559.0 k
*
*-----|-----|-----|-----|-----|-----|
0000100 new stdy-st
0000101 run
0000102 si
0000105 5. 10.
0000110 nitrogen
* time step control cards
*      end time min dt max dt optn mnr mjr rst
*0000201 5400.0 1.e-6 0.5 2 4 200 200
*
*      modification for steady state run at 91/2/8
*
0000201 1000.0 1.e-6 0.5 2 4 500 200
*-----|-----|-----|-----|-----|-----|
*
*      minor edit variables
*
*-----|-----|-----|-----|-----|-----|
* pressure
0000301 p 345010000 * pe-bl-1
0000302 p 310010000 * pe-bl-2
0000303 p 315110000 * pe-bl-3
0000304 p 350010000 * pe-bl-4
0000305 p 315090000 * pe-bl-6
0000306 p 350020000 * pe-bl-8
0000307 p 185010000 * pe-pe-1
0000308 p 100010000 * pe-pe-2
0000309 p 420010000 * porv inlet
0000310 p 110010000 * pt-139-2,3,4
0000311 p 245010000 * pe-lup-1a,1b
0000312 p 215010000 * pe-1st-1a,b/pe-2st-1a,b
0000313 p 200010000 * pe-1st-3a,3b
0000314 p 530020000 * pt-p4-10a
0000315 p 535010000 * pt-p4-85
*-----|-----|-----|-----|-----|-----|
* temperatures
0000320 tempf 406010000 * spray tempf
0000321 tempf 310010000 * te-bl-2a,2b,2c
0000322 tempf 100010000 * te-pe-2a,2b,2c
0000323 tempf 185010000 * te-pe-1
0000324 tempf 115030000 * te-sg-1
0000325 tempf 115100000 * te-sg-2
0000326 tempf 515040000 * te-sg-3
0000328 tempf 415050000 * pqr volume 5
0000329 tempf 415040000 * te-139-19
0000330 tempf 415030000 * te-139-20
0000331 tempf 315120000 * te-p138-171
0000332 tempf 350020000 * te-p138-170
0000333 tempf 205010000 * te-1st-1/te-2st-1
0000334 tempf 210010000 * te-1st-2/te-2st-2
0000335 tempf 345010000 * te-bl-1
0000336 tempf 210030000 * te-1st-14/te-2st-14
0000337 tempf 210040000 * te-3up-2
0000338 tempf 245010000 * te-1up-6
0000339 tempf 246010000 * te-2up-4
0000340 tempf 250010000 * te-1up-3
*-----|-----|-----|-----|-----|-----|
* densities
0000341 rho 345010000 * de-bl-1
0000342 rho 310010000 * de-bl-2
0000343 rho 185010000 * de-pe-1
0000344 rho 100010000 * de-pe-2
0000345 rho 115120000 * de-pe-3
0000346 voidgj 400010000 * surge line density
0000347 rho 115040000 * s/g tubes
0000348 rho 115050000 * s/g tubes
0000349 rho 115060000 * s/g tubes
0000350 rho 115070000 * s/g tubes
*-----|-----|-----|-----|-----|-----|
* velocities
0000351 voidf 100010000 * ilhl nozzle
0000352 velf 100010000 * ilhl nozzle
0000353 velf 115030000 * s/g inlet
0000354 velf 400010000 * surge line
0000355 velfj 425000000 * porv liq vel
0000356 velg 100010000 * ilhl nozzle
0000357 velg 115030000 * s/g inlet
0000358 velg 400010000 * surge line
0000359 velgj 425000000 * porv vap vel
*-----|-----|-----|-----|-----|-----|
* mass flow rates
0000360 mflowj 100010000 * ilhl nozzle
0000361 mflowj 150010000 * pump outlet
0000362 mflowj 185020000 * dtt-rake ilcl
0000363 mflowj 400010000 * pres. surge line flow
0000364 mflowj 407000000 * pqr spray flow
0000366 mflowj 425000000 * pres. relief valve flow
0000367 mflowj 550000000 * steam flow control valve
0000368 mflowj 548000000 * aux feed
0000369 mflowj 560000000 * main feed
0000370 cntrlvar 1 * s/g level
*-----|-----|-----|-----|-----|-----|
* cladding temperatures center module
0000371 httemp 230000110 * te-5h5-015
0000372 httemp 230000210 * te-5h5-034
0000373 httemp 230000310 * te-5h5-049
*-----|-----|-----|-----|-----|-----|

```

\* peak centerline temperatures

\*\*\*\*\*

0000374 httemp 230000101 \* core lower region  
 0000375 httemp 230000201 \* core middle region  
 0000376 httemp 230000301 \* core upper region

\*\*\*\*\*

\* reactor kinetic parameters

\*\*\*\*\*

0000377 rktpow 0 \* total reactor power  
 0000378 rkfpow 0 \* fission decay power  
 0000379 rkgapow 0 \* gamma decay power  
 0000380 rkreac 0 \* reactivity  
 0000381 pmphead 135 \* pep1 head  
 0000382 pmphead 165 \* pep2 head  
 0000384 cntrlvar 2 \* pwr level  
 0000385 cntrlvar 3 \* rx vessel level

\*\*\*\*\*

0000386 mflowj 185010000  
 0000387 mflowj 185030000  
 0000388 mflowj 200020000  
 0000389 pmpvel 135  
 0000390 pmpvel 165

\*\*\*\*\*

\*

\* trips

\*

\*\*\*\*\*

\* variable trips

\*\*\*\*\*

0000501 p 100010000 le null 0 14.193103e6 l  
 \* ecc check valve  
 0000502 p 600010000 ge p 185010000 20.e6 n  
 \* accumulator check valve  
 0000503 p 615010000 ge p 185010000 20.e6 n  
 \* isolation valve hot leg  
 0000504 time 0 lt null 0 0.0 l  
 \* isolation valve cold leg  
 0000505 time 0 lt null 0 0.0 l  
 \* qobv hot leg  
 0000506 time 0 lt null 0 0.0 l  
 \* qobv cold leg  
 0000507 time 0 lt null 0 0.0 l  
 \* check valve surge line pressurizer  
 0000508 time 0 ge null 0 0.0 l  
 \* pressurizer relief valve  
 0000509 tempf 100010000 ge null 0 597.0 l  
 \* steam control valve  
 0000510 time 0 lt null 0 0.0 l  
 \* boundary system valve  
 0000511 time 0 lt null 0 0.0 l  
 \* lpis trip  
 0000512 time 0 ge null 0 10000.0 l  
 \* hpis trip  
 0000513 time 0 ge null 0 10000.0 l  
 \*

0000520 p 530020000 gt null 0 7.103448e6 n  
 0000521 p 530020000 lt null 0 7.0344827e6 n

0000522 p 530020000 gt null 0 6.3448275e6 n  
 0000523 p 530020000 lt null 0 6.4137931e6 n  
 0000530 time 0 ge null 0 3600.0 n  
 0000531 p 530020000 gt p 547010000 0.0 n  
 0000536 time 0 ge null 0 10000.0 n  
 0000540 tempf 100010000 gt null 0 583.16 l  
 0000541 p 100010000 gt null 0 1.574553e7 l  
 0000550 time 0 ge null 0 10000.0 l  
 0000551 time 0 ge timeof 625 0.0 l  
 0000552 time 0 ge timeof 509 1580. l  
 0000560 p 100010000 le null 0 13.15862e6 n  
 0000561 time 0 ge timeof 552 265.0 l  
 0000562 time 0 gt null 0 5400.0 n  
 0000563 cntrlvar 1 lt null 0 2.1844 n  
 0000564 cntrlvar 1 gt null 0 2.9464 n  
 0000565 time 0 ge timeof 669 966. l  
 0000570 p 420010000 gt null 0 1.620058e7 n  
 0000571 p 420010000 lt null 0 1.606269e7 n  
 0000572 p 420010000 lt null 0 1.486300e7 n  
 0000573 p 420010000 gt null 0 1.506980e7 n  
 0000574 p 420010000 gt null 0 1.533874e7 n  
 0000575 p 420010000 lt null 0 1.505000e7 n  
 0000576 p 420010000 lt null 0 1.482853e7 n  
 0000577 p 420010000 gt null 0 1.495950e7 n

\*\*\*\*\*

\* logical trips

\*\*\*\*\*

0000600 670

0000601 563 and 561 n  
 0000602 -563 and -564 n  
 0000603 655 and 602 n  
 0000604 609 or 609 l  
 0000605 572 and -509 n  
 0000606 -572 and -573 n  
 0000607 608 and 606 n  
 0000608 605 or 607 n  
 \*0000609 540 or 541 l

\*\*\*\*\*

\* modification for steady state run at 91/2/8

\*\*\*\*\*

0000609 504 or 504 l  
 0000610 612 or 520 n  
 0000611 -521 and -616 n  
 0000612 611 and 610 n  
 0000613 616 or 523 n  
 0000614 -522 and 613 n  
 0000615 -612 and 609 n  
 0000616 615 and 614 n  
 0000617 612 or 616 n  
 0000618 605 or 607 n  
 0000621 623 or 570 n  
 0000622 -571 and -571 n  
 0000623 621 and 622 n  
 0000624 509 and -552 n  
 0000625 623 or 624 n  
 0000626 576 and -509 n

0000627	-576	and	-577	n		*****	*****	*****
0000628	629	and	627	n	1150000	sgppip	pipe	
0000629	626	or	628	n	1150001	13		
0000635	504	and	504	n	1150101	0.0	3	
0000636	509	and	-536	n	1150102	0.151	9	
0000650	-652	and	550	n	1150103	0.0	12	
0000651	650	or	652	n	1150104	0.0634	13	
0000652	-509	and	651	n	1150201	0.0	1	
0000655	601	or	603	n	1150202	0.0512	2	
0000656	508	or	609	n	1150203	0.0	9	
0000659	561	or	562	n	1150204	0.0512	10	
0000660	504	or	504	n	1150205	0.0	12	
0000669	561	and	564	l	1150301	1.4385	1	
0000670	565	and	-655	n	1150302	0.708	2	
0000680	530	or	530	n	1150303	0.63	3	
0000688	690	or	574	n	1150304	1.067	5	
0000689	-575	and	-551	n	1150305	0.45	7	
0000690	688	and	689	n	1150306	1.067	9	
*****								
*					1150307	0.63	10	
*					1150308	0.547	11	
*		intact loop			1150309	0.689	12	
*					1150310	0.559	13	
*****								
reactor vessel nozzle - intact loop hot leg					1150401	0.09	1	
*****								
1000000	rvnihl	branch			1150402	0.057	2	
1000001	2	0			1150403	0.335	3	
1000101	0.0634	1.5373	0.0	0.0	1150404	0.0	9	
1000102	4.0e-5	0.0	00000		1150405	0.335	10	
1000200	0	14901000.	1346300.0	2462060.0	1150406	0.0437	11	
1001101	250000000	100000000	0.0634	0.0	1150407	0.0462	12	
1002101	100010000	105000000	0.0	0.05	1150408	0.0	13	
1001201	10.582000	11.005000	0.0		1150501	0.0	13	
1002201	10.582000	10.625000	0.0		1150601	0.0	1	
1002201	10.582000	10.625000	0.0		1150602	90.0	6	
1002201	10.582000	10.625000	0.0		1150603	-90.0	13	
*****								
*	pressurizer connection tee reactor vessel side				1150701	0.0	1	
*****								
1050000	pzrtrvs	branch			1150702	0.246	2	
1050001	1	0			1150703	0.513	3	
1050101	0.0634	1.634	0.0	0.0	1150704	1.067	5	
1050102	4.0e-5	0.0	00000		1150705	0.2865	6	
1050200	0	1489610.	1346300.	2462190.0	1150706	-0.2865	7	
1051101	105010000	110000000	0.0	0.05	1150707	-1.067	9	
1051201	13.795000	13.974000	0.0		1150708	-0.513	10	
1051201	13.795000	13.974000	0.0		1150709	-0.498	11	
1051201	13.795000	13.974000	0.0		1150710	-0.689	12	
1051201	13.795000	13.974000	0.0		1150711	-0.356	13	
*****								
*	steam generator inlet piping				1150801	4.0e-5	0.0	2
*****								
1100000	sginlp	branch			1150802	4.0e-5	0.0102	3
1100001	1	0			1150803	1.0e-5	0.0103	9
1100101	0.0	0.623	0.0303	0.0	1150804	4.0e-5	0.0102	10
1100102	4.0e-5	0.0	00000		1150805	4.0e-5	0.0	13
1100200	0	14857200.	1346340.	24629400.0	1150901	0.15	0.15	1
1101101	110010000	115000000	0.0	0.1	1150902	0.05	0.05	2
1101201	13.801000	13.692000	0.0		1150903	0.0	0.0	4
1101201	13.801000	13.692000	0.0		1150904	0.1	0.1	5
1101201	13.801000	13.692000	0.0		1150905	0.2	0.2	6
1101201	13.801000	13.692000	0.0		1150906	0.1	0.1	7

1150907	0.0	0.0	9		1250101	0.0	1.003	0.0613	0.0	90.0	0.521	
1150908	0.05	0.05	11		1250102	4.0e-5	0.0	00000				
1150909	0.1	0.1	12		1250200	0	14600300.	1242600.	2468180.0	0.0		
1151001	00000	13			1251101	125010000	130000000	0.0	0.1	0.1	000100	
1151101	000100	3			1252101	125000000	155000000	0.0	0.0	0.0	000100	
1151102	000000	8			1251201	7.8711000	8.2528000	0.0				
1151103	000100	12			1252201	-11855000	-13539000	0.0				
1151201	0	14871600.	1346350.	2462710.0	0.0	0.001						
1151202	0	14877200.	1346350.	2462600.0	0.0	0.002						
1151203	0	14793300.	1346370.	2464340.0	0.0	0.003						
1151204	0	14770000.	1321980.	2464840.0	0.0	0.004						
1151205	0	14746400.	1301720.	2465340.0	0.0	0.005						
1151206	0	14729700.	1283950.	2465690.0	0.0	0.006						
1151207	0	14721700.	1268380.	2465870.0	0.0	0.007						
1151208	0	14715000.	1254890.	2466020.0	0.0	0.008						
1151209	0	14707300.	1242570.	2466180.0	0.0	0.009						
1151210	0	14707600.	1242600.	2466180.0	0.0	0.010						
1151211	0	14631100.	1242600.	2467720.0	0.0	0.011						
1151212	0	14621800.	1242600.	2467980.0	0.0	0.012						
1151213	0	14616700.	1242600.	2468100.0	0.0	0.013						
1151300	0											
1151301	10.728000	10.670000	0.0	01								
1151302	8.3370000	8.4284000	0.0	02								
1151303	4.4456000	4.7693000	0.0	03								
1151304	4.3865000	4.2164000	0.0	04								
1151305	4.3407000	4.6700000	0.0	05								
1151306	4.3009000	4.6296000	0.0	06								
1151307	4.2676000	4.5954000	0.0	07								
1151308	4.2398000	4.5671000	0.0	08								
1151309	4.2249000	4.5338000	0.0	09								
1151310	7.9665000	8.1922000	0.0	10								
1151311	9.4925000	9.9460000	0.0	11								
1151312	10.040000	10.505000	0.0	12								
*												
*	pump data											
*												
*	pump suction tee											
*												
1200000	pmpscrtt	branch										
1200001	3	0										
1200101	0.0634	0.76	0.0	0.0	0.0	0.0						
1200102	4.0e-5	0.0	00000									
1200200	0	14613100.	1242600.	2468180.0	0.0							
1201101	115010000	120000000	0.0	01	0.1	0.1	000000					
1202101	120010000	125000000	0.0317	0.2	0.2	0.2	000100					
1203101	120010000	155000000	0.0317	0.2	0.2	0.2	000100					
1201201	10.040000	10.505000	0.0									
1202201	5.2077000	5.2983000	0.0									
1203201	5.2071000	5.2944000	0.0									
*	pmp1 suction tee outlet											
*												
1250000	pmp1scrtt	branch										
1250001	2	0										
1250101	0.0	1.003	0.0613	0.0	90.0	0.521						
1250102	4.0e-5	0.0	00000									
1250200	0	14600300.	1242600.	2468180.0	0.0							
1251101	125010000	130000000	0.0	0.1	0.1	0.1	000100					
1252101	125000000	155000000	0.0	0.0	0.0	0.0	000100					
1251201	7.8711000	8.2528000	0.0									
1252201	-11855000	-13539000	0.0									
*****												
*	* pump 1 inlet											
*												
1300000	pmp1nlet	snglvol										
1300101	0.0	0.457	0.0189	0.0	90.0	0.457						
1300102	4.0e-5	0.0	00000									
1300200	0	14578200.	1242600.	2468900.0	0.0							
*****												
*	* primary coolant pump 1											
*												
1350000	pcpump1	pump										
1350101	0.0366	0.0	0.099	0.0	90.0	0.319						
1350102	00000											
1350108	130010000	0.0	0.0	0.0	0.0	0.000100						
1350109	140000000	0.0	0.05	0.05	0.05	0.000100						
1350200	0	14818100.	1242890.	2463900.0	0.0							
1350201	0	8.8943000	9.2942000	0.0								
1350202	0	8.8928000	8.1177000	0.0								
* 1350301	0	0	0	-1	0	509	0					
*												
*	* modification for steady state run at 91/2/8											
*												
1350301	0	0	0	-1	-1	504	0					
1350302	369.00	.90178860.	.31550	96.00	500.600	1.4310000						
1350303	613.6	0.0	207.0000	0.00400	19.598000	0.0						
1350310	0.0	0.0	0.0									
*												
*	* single phase head curves											
*												
*	* head curve no. 1											
*												
1351100	1					1						
1351101	0.000000e+00					1.403600e+00						
1351102	1.906100e-01					1.363600e+00						
1351103	3.896300e-01					1.318600e+00						
1351104	5.939600e-01					1.232800e+00						
1351105	7.902000e-01					1.133600e+00						
1351106	1.000000e+00					1.000000e+00						
*												
*	* head curve no. 2											
*												
1351200	1					2						
1351201	0 000000e+00					-6.700000e-01						
1351202	2 000000e-01					-5.000000e-01						
1351203	4 000000e-01					-2.500000e-01						
1351204	5.755400e-01					0.000000e+00						
1351205	7.443200e-01					2.583000e-01						
1351206	7.734800e-01					3.778000e-01						

1351207 8.631300e-01 6.326000e-01  
 1351208 1.000000e+00 1.000000e+00  
 \*-----|-----|-----|-----|-----|-----|  
 \* head curve no. 3  
 \*-----|-----|-----|-----|-----|-----|  
 1351300 1 3  
 1351301 -1.000000e+00 2.472200e+00  
 1351302 -8.057400e-01 2.047400e+00  
 1351303 -6.069000e-01 1.831000e+00  
 1351304 -4.068300e-01 1.624000e+00  
 1351305 -2.001710e-01 1.470500e+00  
 1351306 0.000000e+00 1.403600e+00  
 \*-----|-----|-----|-----|-----|-----|  
 \* head curve no. 4  
 \*-----|-----|-----|-----|-----|-----|  
 1351400 1 4  
 1351401 -1.000000e+00 2.472200e+00  
 1351402 -8.229700e-01 1.996800e+00  
 1351403 -6.333200e-01 1.589700e+00  
 1351404 -4.553400e-01 1.327900e+00  
 1351405 -2.710900e-01 1.194900e+00  
 1351406 -1.771600e-01 1.060500e+00  
 1351407 -9.073000e-02 1.015600e+00  
 1351408 0.000000e+00 9.342790e-01  
 \*-----|-----|-----|-----|-----|-----|  
 \* head curve no. 5  
 \*-----|-----|-----|-----|-----|-----|  
 1351500 1 5  
 1351501 0.000000e+00 2.500000e-01  
 1351502 2.000000e-01 2.800000e-01  
 1351503 4.000000e-01 3.400000e-01  
 1351504 4.118000e-01 2.768000e-01  
 1351505 5.976300e-01 4.584000e-01  
 1351506 7.934670e-01 6.992000e-01  
 1351507 1.000000e+00 1.000000e+00  
 \*-----|-----|-----|-----|-----|-----|  
 \* head curve no. 6  
 \*-----|-----|-----|-----|-----|-----|  
 1351600 1 6  
 1351601 0.000000e+00 9.342790e-01  
 1351602 9.109900e-02 9.229000e-01  
 1351603 1.865090e-01 8.963000e-01  
 1351604 2.717620e-01 8.750000e-01  
 1351605 4.558720e-01 8.433000e-01  
 1351606 5.744060e-01 8.355000e-01  
 1351607 7.405760e-01 8.466000e-01  
 1351608 7.666190e-01 8.469000e-01  
 1351609 8.714710e-01 8.838000e-01  
 1351610 1.000000e+00 1.000000e+00  
 \*-----|-----|-----|-----|-----|-----|  
 \* head curve no. 7  
 \*-----|-----|-----|-----|-----|-----|  
 1351700 1 7  
 1351701 -1.000000e+00 -1.000000e+00  
 1351702 -8.000000e-01 -6.300000e-01  
 1351703 -6.000000e-01 -3.000000e-01  
 1351704 -4.000000e-01 -5.000000e-02  
 1351705 -2.000000e-01 1.500000e-01  
 1351706 0.000000e+00 2.500000e-01  
 \*-----|-----|-----|-----|-----|-----|  
 \* head curve no. 8  
 \*-----|-----|-----|-----|-----|-----|  
 1351800 1 8  
 1351801 -1.000000e+00 -1.000000e+00  
 1351802 -8.000000e-01 -9.700000e-01  
 1351803 -6.000000e-01 -9.500000e-01  
 1351804 -4.000000e-01 -8.800000e-01  
 1351805 -2.000000e-01 -8.000000e-01  
 1351806 0.000000e+00 -6.700000e-01  
 \*\*\*\*\*  
 single phase torque data  
 \*\*\*\*\*  
 \* torque curve no. 1  
 \*-----|-----|-----|-----|-----|-----|  
 1351900 2 1  
 1351901 0.000000e+00 6.032000e-01  
 1351902 1.930000e-01 6.325000e-01  
 1351903 3.930000e-01 7.369000e-01  
 1351904 5.955200e-01 8.331000e-01  
 1351905 7.978200e-01 9.229000e-01  
 1351906 1.000000e+00 1.000000e+00  
 \*-----|-----|-----|-----|-----|-----|  
 \* torque curve no. 2  
 \*-----|-----|-----|-----|-----|-----|  
 1352000 2 2  
 1352001 0.000000e+00 -6.700000e-01  
 1352002 4.000000e-01 -2.500000e-01  
 1352003 5.000000e-01 1.500000e-01  
 1352004 7.372550e-01 5.265860e-01  
 1352005 7.680490e-01 6.065940e-01  
 1352006 8.672300e-01 7.436600e-01  
 1352007 1.000000e+00 1.000000e+00  
 \*-----|-----|-----|-----|-----|-----|  
 \* torque curve no. 3  
 \*-----|-----|-----|-----|-----|-----|  
 1352100 2 3  
 1352101 -1.000000e+00 1.984300e+00  
 1352102 -8.009600e-01 1.394000e+00  
 1352103 -6.063800e-01 1.097500e+00  
 1352104 -4.068600e-01 8.220000e-01  
 1352105 -1.992800e-01 6.648000e-01  
 1352106 0.000000e+00 6.032000e-01  
 \*-----|-----|-----|-----|-----|-----|  
 \* torque curve no. 4  
 \*-----|-----|-----|-----|-----|-----|  
 1352200 2 4  
 1352201 -1.000000e+00 1.984300e+00  
 1352202 -8.223400e-01 1.830800e+00  
 1352203 -6.337100e-01 1.682400e+00  
 1352204 -4.585300e-01 1.557000e+00  
 1352205 -2.670230e-01 1.436200e+00  
 1352206 -1.761070e-01 1.387900e+00

1352207	-8.931000e-02	1.348100e+00
1352208	0.000000e+00	1.233610e+00
* torque curve no. 5		
1352300	2	5
1352301	0.000000e+00	-4.500000e-01
1352302	4.000000e-01	-2.500000e-01
1352303	5.000000e-01	0.000000e+00
1352304	1.000000e+00	3.569000e-01
* torque curve no. 6		
1352400	2	6
1352401	0.000000e+00	1.233610e+00
1352402	9.064300e-02	1.196500e+00
1352403	1.885690e-01	1.109600e+00
1352404	2.734700e-01	1.041600e+00
1352405	4.586690e-01	8.958000e-01
1352406	5.744800e-01	7.807000e-01
1352407	7.381600e-01	6.134000e-01
1352408	7.685200e-01	5.849000e-01
1352409	8.700570e-01	4.877000e-01
1352410	1.000000e+00	3.569000e-01
* torque curve no. 7		
1352500	2	7
1352501	-1.000000e+00	-1.000000e+00
1352502	-3.000000e-01	-9.000000e-01
1352503	-1.000000e-01	-5.000000e-01
1352504	0.000000e+00	-4.500000e-01
* torque curve no. 8		
1352600	2	8
1352601	-1.000000e+00	-1.000000e+00
1352602	-2.500000e-01	-9.000000e-01
1352603	-8.000000e-02	-8.000000e-01
1352604	0.000000e+00	-6.700000e-01

two - phase multiplier data from 19-1 test data

\* head curve

1353000	0	
1353001	0.000000e+00	0.000000e+00
1353002	2.000000e-02	2.000000e-02
1353003	6.000000e-02	5.000000e-02
1353004	1.000000e-01	1.000000e-01
1353005	2.000000e-01	4.600000e-01
1353006	2.400000e-01	8.000000e-01
1353007	3.000000e-01	9.600000e-01
1353008	4.000000e-01	9.800000e-01
1353009	6.000000e-01	9.700000e-01
1353010	8.000000e-01	9.000000e-01

1353011	9.000000e-01	8.000000e-01
1353012	9.600000e-01	5.000000e-01
1353013	1.000000e+00	0.000000e+00
* torque curve		
1353100	0	
1353101	0.000000e+00	0.000000e+00
1353102	1.250000e-01	7.000000e-02
1353103	1.650000e-01	1.250000e-01
1353104	2.400000e-01	5.600000e-01
1353105	8.000000e-01	5.600000e-01
1353106	9.600000e-01	4.500000e-01
1353107	1.000000e+00	0.000000e+00
*****		
pump 2-phase difference data		
*****		
* head curve no. 1		
1354100	1	1
1354101	0.000000e+00	0.000000e+00
1354102	1.000000e-01	8.300000e-01
1354103	2.000000e-01	1.090000e+00
1354104	5.000000e-01	1.020000e+00
1354105	7.000000e-01	1.010000e+00
1354106	9.000000e-01	9.400000e-01
1354107	1.000000e+00	1.000000e+00
* head curve no. 2		
1354200	1	2
1354201	0.000000e+00	0.000000e+00
1354202	1.000000e-01	-4.000000e-02
1354203	2.000000e-01	0.000000e+00
1354204	3.000000e-01	1.000000e-01
1354205	4.000000e-01	2.100000e-01
1354206	8.000000e-01	6.700000e-01
1354207	9.000000e-01	8.000000e-01
1354208	1.000000e+00	1.000000e+00
* head curve no. 3		
1354300	1	3
1354301	-1.000000e+00	-1.160000e+00
1354302	-9.000000e-01	-1.240000e+00
1354303	-8.000000e-01	-1.770000e+00
1354304	-7.000000e-01	-2.360000e+00
1354305	-6.000000e-01	-2.790000e+00
1354306	-5.000000e-01	-2.910000e+00
1354307	-4.000000e-01	-2.670000e+00
1354308	-2.500000e-01	-1.690000e+00
1354309	-1.000000e-01	-5.000000e-01
1354310	0.000000e+00	0.000000e+00
* head curve no. 4		
1354400	1	4

1354400	1	4
1354401	-1.000000e+00	-1.160000e+00
1354402	-9.000000e-01	-7.800000e-01
1354403	-8.000000e-01	-5.000000e-01
1354404	-7.000000e-01	-3.100000e-01
1354405	-6.000000e-01	-1.700000e-01
1354406	-5.000000e-01	-8.000000e-02
1354407	-3.500000e-01	0.000000e+00
1354408	-2.000000e-01	5.000000e-02
1354409	-1.000000e-01	8.000000e-02
1354410	0.000000e+00	1.100000e-01
* head curve no. 5		
1354500	1	5
1354501	0.000000e+00	0.000000e+00
1354502	2.000000e-01	-3.400000e-01
1354503	4.000000e-01	-6.500000e-01
1354504	6.000000e-01	-9.300000e-01
1354505	8.000000e-01	-1.190000e+00
1354506	1.000000e+00	-1.470000e+00
* head curve no. 6		
1354600	1	6
1354601	0.000000e+00	1.100000e-01
1354602	1.000000e-01	1.300000e-01
1354603	2.500000e-01	1.500000e-01
1354604	4.000000e-01	1.300000e-01
1354605	5.000000e-01	7.000000e-02
1354606	6.000000e-01	-4.000000e-02
1354607	7.000000e-01	-2.300000e-01
1354608	8.000000e-01	-5.100000e-01
1354609	9.000000e-01	-9.100000e-01
1354610	1.000000e+00	-1.470000e+00
* head curve no. 7		
1354700	1	7
1354701	-1.000000e+00	0.000000e+00
1354702	0.000000e+00	0.000000e+00
* head curve no. 8		
1354800	1	8
1354801	-1.000000e+00	0.000000e+00
1354802	0.000000e+00	0.000000e+00
* torque curve no. 1		
1354900	2	1
1354901	0.000000e+00	6.032000e-01
1354902	1.930000e-01	6.325000e-01
1354903	3.930000e-01	7.369000e-01
1354904	5.955200e-01	8.331000e-01
1354905	7.978200e-01	9.229000e-01

1354906	1.000000e+00	1.000000e+00
* torque curve no. 2		
1355000	2	2
1355001	0.000000e+00	-6.700000e-01
1355002	4.000000e-01	-2.500000e-01
1355003	5.000000e-01	1.500000e-01
1355004	7.372550e-01	5.265860e-01
1355005	7.680490e-01	6.065940e-01
1355006	8.672300e-01	7.436600e-01
1355007	1.000000e+00	1.000000e+00
* torque curve no. 3		
1355100	2	3
1355101	-1.000000e+00	1.984300e+00
1355102	-8.009600e-01	1.394000e+00
1355103	-6.063800e-01	1.097500e+00
1355104	-4.068600e-01	8.220000e-01
1355105	-1.992800e-01	6.648000e-01
1355106	0.000000e+00	6.032000e-01
* torque curve no. 4		
1355200	2	4
1355201	-1.000000e+00	1.984300e+00
1355202	-8.223400e-01	1.830800e+00
1355203	-6.337100e-01	1.682400e+00
1355204	-4.585300e-01	1.557000e+00
1355205	-2.670230e-01	1.436200e+00
1355206	-1.761070e-01	1.387900e+00
1355207	-8.931000e-02	1.348100e+00
1355208	0.000000e+00	1.233610e+00
* torque curve no. 5		
1355300	2	5
1355301	0.000000e+00	-4.500000e-01
1355302	4.000000e-01	-2.500000e-01
1355303	5.000000e-01	0.000000e+00
1355304	1.000000e+00	3.569000e-01
* torque curve no. 6		
1355400	2	6
1355401	0.000000e+00	1.233610e+00
1355402	9.064300e-02	1.196500e+00
1355403	1.885690e-01	1.109600e+00
1355404	2.734700e-01	1.041600e+00
1355405	4.586690e-01	8.958000e-01
1355406	5.744800e-01	7.807000e-01
1355407	7.381600e-01	6.134000e-01
1355408	7.685200e-01	5.849000e-01
1355409	8.700570e-01	4.877000e-01
1355410	1.000000e+00	3.569000e-01

\*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* torque curve no. 7  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 1355500 2 7  
 1355501 -1.000000e+00 -1.000000e+00  
 1355502 -3.000000e-01 -9.000000e-01  
 1355503 -1.000000e-01 -5.000000e-01  
 1355504 0.000000e+00 -4.500000e-01  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* torque curve no. 8  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 1355600 2 8  
 1355601 -1.000000e+00 -1.000000e+00  
 1355602 -2.500000e-01 -9.000000e-01  
 1355603 -8.000000e-02 -8.000000e-01  
 1355604 0.000000e+00 -6.700000e-01  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* pep1 pump velocity table  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* modification for steady state run at 91/2/8  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \*1356100 536  
 \*1356101 0.0 0.0  
 \*1356102 1.0 220.  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 pump 1 outlet pump side  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 1400000 pmp1outp snglvol  
 1400101 0.0366 0.502 0.0 0.0 0.0 0.0  
 1400102 4.0e-5 0.0 00000  
 1400200 0 15165000. 1242900. 2458470. 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* pump1 outlet pipe tee side  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 1450000 pmp1outt branch  
 1450001 2 0  
 1450101 0.0 1.4084 0.0633 0.0 0.0 0.0  
 1450102 4.0e-5 0.0 00000  
 1450200 0 15069300. 1242900. 2458230.0 0.0  
 1451101 140010000 145000000 0.0 0.1 0.1 000100  
 1452101 145010000 150000000 0.0 0.0 0.0 000100  
 1451201 8.8901000 8.6110000 0.0  
 1452201 10.611000 10.694000 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* pump outlet tee  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 1500000 pmpoutt branch  
 1500001 3 0  
 1500101 0.0634 0.4966 0.0 0.0 0.0 0.0  
 1500102 4.0e-5 0.0 00000  
 1500200 0 15048800. 1242900. 2458680.0 0.0  
 1501101 170010000 150000000 0.0183 0.2 0.2 000100  
 1502101 150010000 175000000 0.0 0.1 0.1 000100  
 1503101 150010000 406000000 0.0 0.0 0.0 000100  
 1501201 4.3528000 5.2611000 0.0  
 1502201 10.035000 10.103000 0.0  
 1503201 .08890000 .02735000 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* pump 2 suction tee outlet  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 1550000 pmp2scrt branch  
 1550001 1 0  
 1550101 0.0 1.003 0.0613 0.0 90.0 0.521  
 1550102 4.0e-5 0.0 00000  
 1550200 0 14601200. 1242600. 2468430.0 0.0  
 1551101 155010000 160000000 0.0 0.1 0.1 000100  
 1551201 7.5199000 7.8923000 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* pump 2 inlet pipe  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 1600000 pmp2inet snglvol  
 1600101 0.0 0.457 0.0189 0.0 90.0 0.457  
 1600102 4.0e-5 0.0 00000  
 1600200 0 14580700. 1242600. 2468050.0 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* primary coolant pump 2  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 1650000 pcpump2 pump  
 1650101 0.0366 0.0 0.099 0.0 90.0 0.319  
 1650102 00000  
 1650108 160010000 0.0 0.0 0.0 000100  
 1650109 170000000 0.0 0.1 0.1 000100  
 1650200 0 14832700. 1242890. 2463590.0 0.0  
 1650201 0 8.4974000 8.8872000 0.0  
 1650202 0 8.4959000 6.6507000 0.0  
 \*1650301 135 135 135 -1 135 509 0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* modification for steady state run at 91/2/8  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 1650301 135 135 135 -1 -1 504 0  
 1650302 369.00 .89699187 .31550 96.00 500.60000 1.431  
 1650303 613.6 0.0 207.433 0.004 19.5980 0.0  
 1650310 0.0 0.0 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* pump 2 outlet  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 1700000 pmp2outt branch  
 1700001 1 0  
 1700101 0.0366 0.514 0.0 0.0 0.0 0.0  
 1700102 4.0e-5 0.0 00000  
 1700200 0 15089900. 1242900. 2457860.0 0.0  
 1701101 145010000 170010000 0.0183 0.2 0.2 000100  
 1701201 -4.140400 -4.242200 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* cold leg pipe to ecc connection tee  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 1750000 ilelpipe pipe  
 1750001 2  
 1750101 0.0634 2  
 1750201 0.0 1



2230001 7  
 2230101 2.9110-2 7  
 2230201 0.0 6  
 2230301 0.424 1  
 2230302 0.958 5  
 2230303 0.36 6  
 2230304 0.37 7  
 2230401 0.0 7  
 2230501 0.0 7  
 2230601 -90.0 7  
 2230801 4.0e-5 0.0 7  
 2230901 0.0 0.0 6  
 2231001 00000 7  
 2231101 000000 6  
 2231201 0 15023600. 1242730. 2459340.0 0.0 0.0 01  
 2231202 0 15028700. 1242320. 2459220.0 0.0 0.0 02  
 2231203 0 15035700. 1241930. 2459050.0 0.0 0.0 03  
 2231204 0 15042700. 1241540. 2458880.0 0.0 0.0 04  
 2231205 0 15049700. 1241160. 2458710.0 0.0 0.0 05  
 2231206 0 15054500. 1241010. 2458600.0 0.0 0.0 06  
 2231207 0 15057200. 1240860. 2458530.0 0.0 0.0 07  
 2231300 0  
 2231301 1.6569000 1.81115000 0.0 01  
 2231302 1.6565000 1.81111000 0.0 02  
 2231303 1.6561000 1.81070000 0.0 03  
 2231304 1.6558000 1.81030000 0.0 04  
 2231305 1.6554000 1.80990000 0.0 05  
 2231306 1.6553000 1.80970000 0.0 06  
 \* junction from filler gap to lower plenum  
 \* lower core support structure  
 2240000 flrgapp sngljun  
 2240101 223010000 220010000 0.0 10. 10. 000100  
 2240201 0 1.6552000 1.7051000 0.0  
 \* active core  
 2300000 core pipe  
 2300001 3  
 2300101 0.1705 3  
 2300201 0.1440 2  
 2300301 0.559 2  
 2300302 0.657 3  
 2300401 0.0 3  
 2300501 0.0 3  
 2300601 90.0 3  
 2300801 4.0e-5 0.012 3  
 2300901 0.5 0.5 2  
 2301001 00100 3  
 2301101 000100 2  
 2301201 0 15009300. 1289110. 2459680. 0.0 0.0 01  
 2301202 0 14996400. 1339030. 2459990. 0.0 0.0 02  
 2301203 0 14982500. 1354980. 2460310. 0.0 0.0 03  
 2301300 0  
 2301301 3.5187000 3.5227000 0.0 01  
 2301302 3.6127000 3.6166000 0.0 02  
 \* core bypass volume  
 2350000 corebyps pipe  
 2350001 3  
 2350101 0.015 3  
 2350201 0.0 2  
 2350301 0.559 2  
 2350302 0.657 3  
 2350401 0.0 3  
 2350501 0.0 3  
 2350601 90.0 3  
 2350801 4.0e-5 0.003 3  
 2350901 0.0 0.0 2  
 2351001 00000 3  
 2351101 000000 2  
 2351201 0 15021500. 1242940. 2459390.0 0.0 0.0 01  
 2351202 0 15002400. 1242980. 2459850.0 0.0 0.0 02  
 2351203 0 14981700. 1243020. 2460330.0 0.0 0.0 03  
 2351300 0  
 2351301 2.2307000 2.3978000 0.0 01  
 2351302 2.2307000 2.3980000 0.0 02  
 \* upper core support structure  
 2400000 ucoss1 branch  
 2400001 2 0  
 2400101 0.297 1.118 0.0 0.0 90.0 1.118  
 2400102 4.0e-5 0.145 00000  
 2400200 0 14966500. 1348980. 2460680.0 0.0  
 2401101 230010000 240000000 0.12 0.3 0.3 0.3 000100  
 2402101 235010000 240000000 0.0 0.0 0.0 0.0 000100  
 2401201 3.6456000 3.6509000 0.0  
 2402201 2.3080000 2.3981000 0.0  
 \* upper flow skirt region  
 2450000 ufsre branch  
 2450001 1 0  
 2450101 0.114 0.843 0.0 0.0 90.0 0.843  
 2450102 4.0e-5 0.131 00000  
 2450200 0 14945200. 1347660. 2461140.0 0.0  
 2451101 240010000 245000000 0.0 0.0 0.0 0.0 000100  
 2451201 5.7436 6.0742 0.0





3501201 0 15018600. 1067100. 2459470.0 0.0 0.0 01  
 3501202 0 15018600. 1173730. 2459470.0 0.0 0.0 02  
 3501300 0  
 3501301 .0 .0 .0 .0 01  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* isolation valve cold leg  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 3550000 isvel valve  
 3550101 350010000 3600000000 0.0 0.0 0.0 000100  
 3550201 1 0.0 0.0 0.0  
 3550300 trpvlv  
 3550301 505  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* pipe section between isolation valve and qobv cold leg  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 3600000 vvoicl snglvol  
 3600101 0.0525 0.813 0.0 0.0 0.0 0.0  
 3600102 4.0e-5 0.0 00000  
 3600200 3 14.74e6 558.  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* quick opening blowdown cold leg  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 3650000 qobvel valve  
 3650101 360010000 805000000 0.0466 0.0 0.0 000100  
 3650201 1 0.0 0.0 0.0  
 3650300 trpvlv  
 3650301 507  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* reflood assist bypass piping - cold leg side  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 3700000 rabsphl branch  
 3700001 1 0  
 3700101 0.0388 2.203 0.0 0.0 90.0 0.653  
 3700102 4.0e-5 0.0 00000  
 3700200 0 14755500. 1239680.0 2460930.0 0.0  
 3701101 375010000 370000000 0.0 0.0 0.0 000100  
 3701201 .21294000. 24585000 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* reflood assist bypass parrel pipes hot leg side  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 3750000 rabphl snglvol  
 3750101 0.0776 0.0 0.0858 0.0 0.0 0.0  
 3750102 4.0e-5 0.0 00000  
 3750200 0 14957900. 1239760.0 2460880.0 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* reflood assist bypass valves  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 3770000 rabsvlv sngljun  
 3770101 380010000 375000000 0.0 1.4e+4 1.4e+4 000000  
 3770201 0 .106460 .25646 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* reflood assist bypass parrel pipes cold leg side  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 3800000 rabppcl snglvol  
 3800101 0.0776 0.0 0.0855 0.0 0.0 0.0  
 3800102 4.0e-5 0.0 00000

4100000 s1valv valve  
 4100101 405010000 415000000 0.0 0.93 0.93 000100  
 4100201 0 -17704000 -1770400 0.0  
 4100300 trpviv  
 4100301 508  
 \*-----|-----|-----|-----|-----|-----|-----|  
 \* pressurizer vessel  
 \*-----|-----|-----|-----|-----|-----|-----|  
 4150000 pzrve pipe  
 4150001 8  
 4150101 0.362 1  
 4150102 0.565 5  
 4150103 0.466 7  
 4150104 0.13 8  
 4150201 0.0 7  
 4150301 0.224 1  
 4150302 0.403 3  
 4150303 0.207 5  
 4150304 0.1705 7  
 4150305 0.118 8  
 4150401 0.0 8  
 4150501 0.0 8  
 4150601 90.0 8  
 4150801 4.0e-5 0.0 8  
 4151001 00000 8  
 4151101 000000 7  
 4151201 0 14917400. 1511010. 2461750.0 .0 0.0 01  
 4151202 0 14915500. 1568180. 2461790.0 .1839e-3 0.0 02  
 4151203 0 14913200. 1558810. 2463620.0 .15145 0.0 03  
 4151204 0 14912100. 1582630. 2461930.0 .9996500 0.0 04  
 4151205 0 14911900. 1582620. 2461840.0 .9996400 0.0 05  
 4151206 0 14911700. 1582560. 2461840.0 .9996000 0.0 06  
 4151207 0 14911500. 1582300. 2461840.0 .9995300 0.0 07  
 4151208 0 14911400. 1575760. 2461840.0 1.0 0.0 08  
 4151300 0  
 4151301 -.716473e-3 .05388 0.0 01  
 4151302 -.62376e-3 .3445 0.0 02  
 4151303 -.27965 .12293e-2 0.0 03  
 4151304 -.27030 .17636e-3 0.0 04  
 4151305 -.30526 .20283e-3 0.0 05  
 4151306 -.28127 .19339e-3 0.0 06  
 4151307 -.58439 .64379e-3 0.0 07  
 \*-----|-----|-----|-----|-----|-----|-----|  
 \* pressurizer top hat and relief connection  
 \*-----|-----|-----|-----|-----|-----|-----|  
 4200000 toppre branch  
 4200001 1 0  
 4200101 0.13 0.118 0.0 0.0 90.0 0.118  
 4200102 4.0e-5 0.0 00000  
 4200200 0 14911300. 1541380. 2461830.0 .99907000  
 4201101 415010000 420000000 0.0 0.0 0.0 000000  
 4201201 -.38729 5.44472e-4 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|  
 \* porv  
 \*-----|-----|-----|-----|-----|-----|-----|  
 4250000 porv valve  
 4250101 420010000 810000000 2.4784-5 0.0 0.0 000100  
 4250201 0 .000000 .00000 0.0  
 4250300 trpvlv  
 4250301 625  
 \*-----|-----|-----|-----|-----|-----|-----|  
 \* steam generator secondary side  
 \*-----|-----|-----|-----|-----|-----|-----|  
 \* primary separator  
 \*-----|-----|-----|-----|-----|-----|-----|  
 5000000 sepaout separair  
 5000001 3 0  
 5000101 1.273 0.718 0.0 0.0 +90.0 +0.718  
 5000102 4.e-5 0.7874 00010  
 5000200 0 5670640.0 1444230. 3000000.0 .19415000  
 5001101 500010000 525000000 1.272800 0.0 0.0 001100 0.5  
 5002101 500000000 505000000 0.000000 0.0 0.0 001100 +  
 + 0.15  
 5003101 520000000 500000000 0.19600 0.4 0.4 001100  
 5001201 -.4175 .75723 0.0  
 5002201 0.8006 -9.39768e-2 0.0  
 5003201 1.9086 4.4093 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|  
 \* separator outlet region  
 \*-----|-----|-----|-----|-----|-----|-----|  
 5050000 lwrsep branch  
 5050001 1  
 5050101 1.273 0.718 0.0 0.0 -90.0 -0.718  
 5050102 4.e-5 0.7874 00000  
 5050200 0 5672780.0 1183350. 2400000.0 .01138160  
 5051101 505010000 510000000 0.0 0.0 0.0 0.0 000100  
 5051201 0.21828 -.30041 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|  
 \* feed inlet volume  
 \*-----|-----|-----|-----|-----|-----|-----|  
 5100000 feedinl branch  
 5100001 1 0  
 5100101 0.7525 0.518 0.0 0.0 -90.0 -0.518  
 5100102 4.e-5 0.10796 00000  
 5100200 0 5676840.0 1109810. 2400000.0 .408589e-5  
 5101101 510010000 515000000 0.0 0.0 0.0 0.0 000100  
 5101201 0.6323700 0.632870 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|  
 \* steam generator downcomer  
 \*-----|-----|-----|-----|-----|-----|-----|  
 5150000 dwncmr annulus  
 5150001 8  
 5150101 0.23226 3  
 5150102 0.27871 8  
 5150201 0.0 7  
 5150301 0.7102 3  
 5150302 1.85075 7  
 5150303 0.718 8  
 5150401 0.0 8  
 5150601 -.90.0 3



\*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* air cooled condenser  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 5470000 condensers tmdpvol  
 5470101 0.21677 17.67 0.0 0.0 0.0 0.0  
 5470102 4.e-5 0.0 00000  
 5470200 1 680  
 5470201 0.0 559.15 0.999  
 \*5470202 18000. 334.15 0.999  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* modification for steady state run at 91/2/8  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* aux feed water  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 5480000 auxfeed tmdpjun  
 5480101 553000000 510000000 0.10  
 5480200 1 655  
 5480201 -1.0 0.0 0.0 0.0  
 5480202 0.0 0.0 0.0 0.0  
 \*5480203 0.0 2.5207 0.0 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* modification for steady state run at 91/2/8  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* steam flow control valve  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 5500000 cv-p4-1 valve  
 5500101 530010000 535000000 0.0043266 0.0 0.0 000100  
 5500201 v 19.758 22.082 0.0  
 5500300 mtrvlv  
 5500301 612 616 0.05 0.67 550  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* makeup feed tank  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 5530000 demin tmdpvol  
 5530101 3.0 10.0 0.0 0.0 0.0 0.0  
 5530102 3.33e-5 1.0 00011  
 5530200 1  
 5530201 0.0 366.5 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* flow path to the air cooled condenser  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 5550000 coacco sngljun  
 5550101 535010000 540000000 0.0 0.0 0.0 0.0 000100  
 5550201 0 13.171 36.498 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* main feed water valve  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 5600000 mafeed tmdpjun  
 5600101 545000000 510000000 0.05  
 5600200 1 656  
 5600201 0.0 26.533 26.533 0.0  
 \*5600202 0.0 0.0 0.0 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* modification for steady state run at 91/2/8

\*-----|-----|-----|-----|-----|-----|-----|-----|  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* ecc system  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* piping pcs hpis injection point  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 6000000 ppchp branch  
 6000001 0 1  
 6000101 0.009099 8.8776 0.0 0.0 -90.0 -3.2  
 6000102 4.0e-5 0.0 00000  
 6000200 0 14081300. 128835.00 2400000.0 .000000  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* piping accumulator  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 6050000 piac1 branch  
 6050001 2 0  
 6050101 0.014582 9.4891 0.0 0.0 0.0 0.0  
 6050102 4.0e-5 0.0 00000  
 6050200 0 14065600. 131740.00 260000.0 .000000  
 6051101 605010000 600000000 0.0 0.8 0.8 000100  
 6052101 610010000 605000000 0.0 0.7 0.7 000100  
 6051201 .98481-14 .98481-14 0.0  
 6052201 -.1251-13 -.1251-13 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* accumulator pipe  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 6100000 piac2 snglvol  
 6100101 0.018638 7.55998 0.0 0.0 0.0 0.0  
 6100102 4.0-5 0.0 00000  
 6100200 0 14065600. 131744. 2600000.0 0.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* accumulator vessel  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 6150000 accumlr accum  
 6150101 1.254 2.33 0.0 0.0 90.0 2.33  
 6150102 4.0-5 0.0 00000  
 6150200 4.37+6 304.7 0.0  
 6151101 610000000 0.016817 24.6 24.6 000000  
 6152200 1.97 0.0 75.13 0.0 0.04445 0 0 0 0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* bwst lpis  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 6200000 bwstlps tmdpvol  
 6200101 20.44 5.0 0.0 0.0 90.0 5.0  
 6200102 4.0e-5 0.0 00000  
 6200200 3  
 6200201 0.0 1.0e+5 305.0  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 \* bwst hpis  
 \*-----|-----|-----|-----|-----|-----|-----|-----|  
 6250000 bwstbps tmdpvol  
 6250101 20.44 5.0 0.0 0.0 90.0 5.0  
 6250102 4.0e-5 0.0 00000  
 6250200 3

6250201	0.0	1.0e+5	305.0		8000101	0.0	1.0	0.1	0.0	0.0	0.0
* ecc check valve				8000102	0.0	0.0	0.00000				
* eccvlv valve				8000200	2						
6300000	eccvlv	valve			8000201	0.0	0.0	0.107e6	1.0		
6300101	600010000	1850000000	0.0	0.0	8000202	10000.0	0.0	0.107e6	1.0		
6300201	0	.00000000	.00000000	0.0	* containment broken loop cold leg						
6300300	trpvlv				* containment power operated relief valve						
6300301	502				8050000	c805	tmdpvol				
* low pressure injection system				8050101	0.0	1.0	0.1	0.0	0.0	0.0	
* containment broken loop cold leg				8050102	0.0	0.0	0.00000				
6350000	lpis	tmdpjun			8050200	2					
6350101	620000000	600000000	0.0		8050201	0.0	1.0e+5	1.0			
6350200	1	635	p	205010000	8050202	10000.0	1.0e+5	1.0			
6350201	-1.0	0.0	0.0	0.0	* boundary valve intact loop hot leg						
6350202	8.483+4	7.045	0.0	0.0	8100000	cporv	tmdpvol				
6350203	4.297+5	6.091	0.0	0.0	8100101	0.0	1.0	0.1	0.0	0.0	0.0
6350204	7.745+5	5.045	0.0	0.0	8100102	0.0	0.0	0.00000			
6350205	9.448+5	4.313	0.0	0.0	8100200	2					
6350206	1.119+6	3.454	0.0	0.0	8100201	0.0	0.0	0.107e+6	1.0		
6350207	1.186+6	3.173	0.0	0.0	8100201	10000.0	0.0	0.107e+6	1.0		
6350208	1.257+6	2.673	0.0	0.0	* steam generator heat structures						
6350209	1.326+6	2.159	0.0	0.0	9000000	bvalv	valve				
6350210	1.395+6	1.536	0.0	0.0	9000101	110010000	905000000	0.0	0.0	0.0	0.000100
6350211	1.464+6	0.7182	0.0	0.0	9000201	0	0.0	0.0	0.0		
6350212	1.517+6	0.0	0.0	0.0	9000300	trpvlv					
* high pressure injection system				9000301	511						
* accumulator valve				*****							
6400000	hpis	tmdpjun			9050000	bvolum	tmdpvol				
6400101	625000000	600000000	0.0		9050101	0.0	1.0	0.1	0.0	0.0	0.0
6400200	1	660	p	100010000	9050102	0.0	0.0	0.00000			
6400201	-1.0	0.0	0.0	0.0	9050200	3					
6400202	0.0	0.0	0.0	0.0	9050201	0.0	0.0	14.9664e6	577.86		
6400203	0.0	.75687272	0.0	0.0	9050202	10000.0	0.0	14.9664e6	577.86		
6400204	.7725144+6	.75687272	0.0	0.0	* steam generator tubing						
6400205	8.3597+6	.31536281	0.0	0.0	*****	*****	*****	*****	*****	*****	*****
6400206	17.2436+6	.31536281	0.0	0.0							
* containment											
* containment broken loop hot leg											
8000000	cbihl	tmdpvol			10060000	6	8	2	1	0.0051054	
					10060100	0	1				
					10060101	7					
					10060201	6	7				
					10060301	0.0	7				





12100604	223050000 0		1	1	0.958	4	12200000	1	11	1	1	0.0	
12100605	223060000 0		1	1	0.36	5	12200100	0	1				
12100606	223070000 0		1	1	0.37	6	12200101	10	0.092				
12100701	0	0.0	0.0	0.0	6		12200201	5	10				
12100801	0.0	11.0	11.0	0.0	0.0	0.0	1.0	4	*	mod	3		
12100802	0.0	11.0	11.0	0.0	0.0	0.0	1.0	5	*	mod	3		
12100803	0.0	11.0	11.0	0.0	0.0	0.0	1.0	6	*	mod	3		
12100901	0.0	11.0	11.0	0.0	0.0	0.0	1.0	4	*	mod	3		
12100902	0.0	11.0	11.0	0.0	0.0	0.0	1.0	5	*	mod	3		
12100903	0.0	11.0	11.0	0.0	0.0	0.0	1.0	6	*	mod	3		
*****													
* reactor vessel wall above station 178 - 5.50 inches thick													
* station 178 to 258 rv not modelled above bottom of nozzles													
*****													
12110000	3	11	2	1	0.7328		12250000	7	11	2	1	0.3	
12110100	0	1					12250100	0	1				
12110101	10	0.8725					12250101	10	0.38				
12110201	5	10					12250201	4	10				
12110301	0.0	10					12250301	0.0	10				
12110401	558.0	11					12250401	558.0	11				
12110501	223010000 0		1	1	0.424	1	12250501	225010000 0		1	1	0.52	
12110502	223020000 0		1	1	0.958	2	12250502	230010000 0		1	1	0.559	
12110503	223030000 0		1	1	0.6500	3	12250503	230020000 0		1	1	0.559	
12110601	-939	0	3949	1	0.424	1	12250504	230030000 0		1	1	0.657	
12110602	-939	0	3949	1	0.958	2	12250505	240010000 0		1	1	1.118	
12110603	-939	0	3949	1	0.6500	3	12250506	245010000 0		1	1	0.42	
12110701	0	0.0	0.0	0.0	3		12250507	246010000 0		1	1	0.35	
12110801	0.0	11.0	11.0	0.0	0.0	0.0	1.0	1	*	mod	3		
12110802	0.0	11.0	11.0	0.0	0.0	0.0	1.0	2	*	mod	3		
12110803	0.0	11.0	11.0	0.0	0.0	0.0	1.0	3	*	mod	3		
*****													
* reactor vessel wall bellow station 178 - 3.62 inches thick													
* station 67.7 to 178													
*****													
12120000	5	7	2	1	0.7328		12250701	0	0.0	0.0	0.0	7	
12120100	0	1					12250801	0.0	11.0	11.0	0.0	0.0	
12120101	6	0.8247					12250802	0.0	11.0	11.0	0.0	0.0	
12120201	5	6					12250803	0.0	11.0	11.0	0.0	0.0	
12120301	0.0	6					12250804	0.0	11.0	11.0	0.0	0.0	
12120401	558.0	7					12250805	0.0	11.0	11.0	0.0	0.0	
12120501	223030000 0		1	1	0.308	1	12250806	0.0	11.0	11.0	0.0	0.0	
12120502	223040000 10000		1	1	0.958	3	*****						
12120503	223060000 0		1	1	0.3600	4	* lower core support structure station 96.44 to 116.91						
12120504	223070000 0		1	1	0.37	5	* includes core support barrel lip , lower core support						
12120601	-939	0	3949	1	0.308	1	* structure , and fuel module lower end boxes						
12120602	-939	0	3949	1	0.958	3	*****						
12120603	-939	0	3949	1	0.36	4	12260000	1	7	2	1	0.282	
12120604	-939	0	3949	1	0.37	5	12260100	0	1				
12120701	0	0.0	0.0	0.0	5		12260101	6	0.3				
12120801	0.0	11.0	11.0	0.0	0.0	0.0	1.0	1	*	mod	3		
12120802	0.0	11.0	11.0	0.0	0.0	0.0	1.0	3	*	mod	3		
12120803	0.0	11.0	11.0	0.0	0.0	0.0	1.0	4	*	mod	3		
12120804	0.0	11.0	11.0	0.0	0.0	0.0	1.0	5	*	mod	3		
*****													
* reactor vessel bottom station 67.7													
*****													
12200000	1	11	1	1	1	0.0	12260501	225010000 0		1	1	0.52	
12200100	0	1					12260601	0	0	0	1	1	
12200101	10	0.092					12260701	0	0.0	0.0	0.0	1	
12200201	5	10					12260801	0.0	11.0	11.0	0.0	0.0	

*****						
* active core station 116.91 to 182.94						
*****						
12300000	3	10	2	1	0.0	
12300100	0	1				
12300101	5	4.647e-3				
12300102	1	4.742e-3				
12300103	3	5.359e-3				
12300201	1	5				
12300202	2	6				
12300203	3	9				
12300301	1.0	5				
12300302	0.0	9				
12300401	558.0	10				
12300501	0	0	0	1	725.1	3
12300601	230010000	0	1	1	725.1	1
12300602	230020000	0	1	1	725.1	2
12300603	230030000	0	1	1	725.1	3
12300701	1000	0.41209	0.0	0.0	1	
12300702	1000	0.44565	0.0	0.0	2	
12300703	1000	0.14226	0.0	0.0	3	
12300901	0.0124	11.0	11.0	0.0	0.0	1.0 3 *mod 3
*****						
* upper core support structure station 190.5 to 234.5						
*****						
12400000	1	7	2	1	0.282	
12400100	0	1				
12400101	6	0.31				
12400201	4	6				
12400301	0.0	6				
12400401	558.0	7				
12400501	240010000	0	1	1	1.118	1
12400601	0	0	0	1	1.118	1
12400701	0	0.0	0.0	0.0	1	
12400801	0.0	11.0	11.0	0.0	0.0	0.0 1.0 1 * mod 3
*****						
* fuel modules station 187.6 to 258.4						
*****						
12460000	1	5	1	1	0.0	
12460100	0	1				
12460101	4	0.01				
12460201	4	4				
12460301	0.0	4				
12460401	558.0	5				
12460501	245010000	0	1	1	1.8	1
12460601	246010000	0	1	1	1.8	1
12460701	0	0.0	0.0	1.8	1	
12460801	0.0	11.0	11.0	0.0	0.0	0.0 1.0 1 * mod 3
12460901	0.0	11.0	11.0	0.0	0.0	0.0 1.0 1 * mod 3
*****						
* core support barrel - upper plenum lower volume						
* station 264 to 297.6						
* reactor vessel not modelled above bottom of nozzles						
* the vessel to filler gap is assumed to insulate the vessel						
* from the fillers, the vessel to filler gap is not modelled						
* at this elevation						
12500000	1	11	2	1	0.381	
12500100	0	1				
12500101	10	0.419				
12500201	5	10				
12500301	0.0	10				
12500401	558.0	11				
12500501	250010000	0	1	1	0.854	1
12500601	0	0	0	1	0.854	1
12500701	0	0.0	0.0	0.0	1	
12500801	0.0	11.0	11.0	0.0	0.0	0.0 1.0 1 * mod 3
*****						
* internals upper plenum						
*****						
12510000	2	5	1	1	0.0	
12510100	0	1				
12510101	4	0.005				
12510201	4	4				
12510301	0.0	4				
12510401	558.0	5				
12510501	250010000	0	1	1	1.0	1
12510502	250010000	0	1	1	1.0	2
12510601	0	0	0	1	1.0	2
12510701	0	0.0	0.0	0.0	2	
12510801	0.0	11.0	11.0	0.0	0.0	0.0 1.0 2 * mod 3
*****						
* core support barrel - upper plenum top volume						
* station 297.6 to 325						
* reactor vessel not modelled above bottom of nozzles						
* the vessel to filler gap is assumed to insulate the vessel						
* from the fillers, the vessel to filler gap is not modelled						
* at this elevation.						
*****						
12501000	1	21	2	1	0.381	
12501100	0	1				
12501101	20	0.728				
12501201	5	20				
12501301	0.0	20				
12501401	558.0	21				
12501501	250010000	0	1	1	0.712	1
12501601	0	0	0	1	0.712	1
12501701	0	0.0	0.0	0.0	1	
12501801	0.0	11.0	11.0	0.0	0.0	0.0 1.0 1 * mod 3
*****						
* upper head top plate station 325						
*****						
12550000	1	21	1	1	0.0	
12550100	0	1				
12550101	20	0.474				
12550201	5	20				
12550301	0.0	20				
12550401	558.0	21				
12550501	250010000	0	1	1	0.712	1
12550601	-939	0	3949	1	0.712	1
12550701	0	0.0	0.0	0.0	1	

12550801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3
*****										
* broken loop hot leg piping heat structures										
*****										
13150000	2	11	2	1	0.0515					
13150100	0	1								
13150101	10	0.0705								
13150201	4	10								
13150301	0.0	10								
13150401	540.0	11								
13150501	3150100000	0	1	1	0.4054 1					
13150502	3150200000	0	1	1	0.5265 2					
13150601	-939	0	3979	1	0.4054 1					
13150602	-939	0	3979	1	0.5265 2					
13150701	0	0	0	0	2					
13150801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3
13150802	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	2	* mod 3
*****										
13151000	1	11	2	1						
0.0550										
13151100	0	1								
13151101	10	0.0705								
13151201	4	10								
13151301	0.0	10								
13151401	540.0	11								
13151501	3150900000	0	1	1	0.0120357 1					
13151601	-939	0	3979	1	0.0120357 1					
13151701	0	0	0	0	1					
13151801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3
*****										
13152000	1	11	2	1	0.0660					
13152100	0	1								
13152101	10	0.0840								
13152201	4	10								
13152301	0.0	10								
13152401	540.0	11								
13152501	3151100000	0	1	1	0.00836 1					
13152601	-939	0	3979	1	0.00836 1					
13152701	0	0	0	0	1					
13152801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3
*****										
13153000	6	11	2	1	0.1835					
13153100	0	1								
13153101	10	0.2285								
13153201	4	10								
13153301	0.0	10								
13153401	540.0	11								
13153501	3150300000	10000	1	1	0.108 6					
13153601	-939	0	3979	1	0.108 6					
13153701	0	0	0	0	6					
13153801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	6	* mod 3
*****										
13154000	1	11	2	1	0.1285					
13154100	0	1								
13154101	10	0.1620								
13154201	4	10								
13154301	0.0	10								
13154401	540.0	11								
13154501	3151200000	0	1	1	0.0525 1					
13154601	-939	0	3979	1	0.0525 1					
13154701	0	0	0	0	1					
13154801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3
*****										
13155000	1	11	2	1	0.1420					
13155100	0	1								
13155101	10	0.1780								
13155201	4	10								
13155301	0.0	10								
13155401	540.0	11								
13155501	3151000000	0	1	1	0.0489057 1					
13155601	-939	0	3979	1	0.0489057 1					
13155701	0	0	0	0	1					
13155801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3
*****										
* nozzle piping										
*****										
13000000	3	11	2	1	0.1420					
13000100	0	1								
13000101	10	0.1780								
13000201	4	10								
13000301	0.0	10								
13000401	540.0	11								
13000501	3000100000	0	1	1	0.876 1					
13000502	3050100000	0	1	1	0.698 2					
13000503	3100100000	0	1	1	1.424 3					
13000601	-939	0	3979	1	0.876 1					
13000602	-939	0	3979	1	0.698 2					
13000603	-939	0	3979	1	1.424 3					
13000701	0	0	0	0	3					
13000801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3
13000802	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	2	* mod 3
13000803	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	3	* mod 3
*****										
* broken loop cold leg										
*****										
* nozzle piping										
*****										
13350000	3	11	2	1	0.1420					
13350100	0	1								
13350101	10	0.1780								
13350201	4	10								
13350301	0.0	10								
13350401	540.0	11								
13350501	3350100000	0	1	1	0.7495 1					
13350502	3400100000	0	1	1	0.698 2					
13350503	3450100000	0	1	1	0.974 3					
13350601	-939	0	3949	1	0.7495 1					
13350602	-939	0	3949	1	0.698 2					
13350603	-939	0	3949	1	0.974 3					
13350701	0	0	0	0	3					
13350801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3
13350802	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	2	* mod 3
13350803	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	3	* mod 3

\*\*\*\*\*

13501000	1	11	2	1	0.0550
13501100	0	1			
13501101	10	0.1780			
13501201	4	10			
13501301	0.0	10			
13501401	540.0	11			
13501501	350010000	0	1	1	0.488 1
13501601	-939	0	3949	1	0.488 1
13501701	0	0	0	0	1
13501801	0.0	11.0	11.0	0.0	0.0 0.0 0.0 1.0 1 * mod 3

\*\*\*\*\*

13502000	1	11	2	1	0.0865
13502100	0	1			
13502101	10	0.1095			
13502201	4	10			
13502301	0.0	10			
13502401	540.0	11			
13502501	350020000	0	1	1	1.6085 1
13502601	-939	0	3949	1	1.6085 1
13502701	0	0	0	0	1
13502801	0.0	11.0	11.0	0.0	0.0 0.0 0.0 1.0 1 * mod 3

\*\*\*\*\*

\* reflood assist piping and valves [rabvs]

\*\*\*\*\*

13700000	4	11	2	1	0.111
13700100	0	1			
13700101	10	0.1365			
13700201	4	10			
13700301	0.0	10			
13700401	540.0	11			
13700501	370010000	0	1	1	2.00 1
13700502	375010000	0	1	1	1.10567 2
13700503	380010000	0	1	1	1.101804 3
13700504	385010000	0	1	1	3.04201 4
13700601	-939	0	3979	1	2.00 1
13700602	-939	0	3979	1	1.10567 2
13700603	-939	0	3949	1	1.101804 3
13700604	-939	0	3949	1	3.04201 4
13700701	0	0	0	0	4
13700801	0.0	11.0	11.0	0.0	0.0 0.0 0.0 1.0 1 * mod 3
13700802	0.0	11.0	11.0	0.0	0.0 0.0 0.0 1.0 2 * mod 3
13700803	0.0	11.0	11.0	0.0	0.0 0.0 0.0 1.0 3 * mod 3
13700804	0.0	11.0	11.0	0.0	0.0 0.0 0.0 1.0 4 * mod 3

\*\*\*\*\*

\* pressurizer heat structures

\*\*\*\*\*

\* vessel bottom

\*\*\*\*\*

14151000	1	11	1	1	0.0
14151100	0	1			
14151101	10	0.0762			
14151201	5	10			
14151301	0.0	10			
14151401	617.0	11			
14151501	415010000	0	1	1	0.362 1

14151601	-939	0	3969	1	0.362 1
14151701	0	0	0	0	1
14151801	0.0	11.0	11.0	0.0	0.0 0.0 0.0 1.0 1 * mod 3

\* vessel sides - large diameter section

\*\*\*\*\*

14152000	7	11	2	1	0.42291
14152100	0	1			
14152101	10	0.49911			
14152201	5	10			
14152301	0.0	10			
14152401	617.0	11			
14152501	415010000	0	1	1	0.224 1
14152502	415020000	10000	1	1	0.403 3
14152503	415040000	10000	1	1	0.207 5
14152504	415060000	10000	1	1	0.1705 7
14152601	-939	0	3969	1	0.224 1
14152602	-939	0	3969	1	0.403 3
14152603	-939	0	3969	1	0.207 5
14152604	-939	0	3969	1	0.1705 7
14152701	0	0	0	0	7
14152801	0.0	11.0	11.0	0.0	0.0 0.0 0.0 1.0 1 * mod 3

\*\*\*\*\*

\* vessel sides - small diameter section

\*\*\*\*\*

14162000	1	11	2	1	0.2032
14162100	0	1			
14162101	10	0.3683			
14162201	5	10			
14162301	0.0	10			
14162401	617.0	11			
14162501	415080000	0	1	1	0.118 1
14162601	-939	0	3969	1	0.118 1
14162701	0	0	0	0	1
14162801	0.0	11.0	11.0	0.0	0.0 0.0 0.0 1.0 1 * mod 3

\*\*\*\*\*

\* pressurizer heaters

\*\*\*\*\*

14172000	12	9	2	1	0.0
14172100	0	1			
14172101	3	4.0132e-3			
14172102	2	4.3942e-3			
14172103	1	5.6642e-3			
14172104	2	8.3820e-3			
14172201	7	3			
14172202	8	5			
14172203	7	6			
14172204	4	8			
14172301	0.0	3			
14172302	1.0	5			
14172303	0.0	8			
14172401	617.6	9			
14172501	0	0	0	1	0.6096 12
14172601	415020000	0	1	1	0.6096 12
14172701	417	1.0	0.0	0.0	9 *cycli
14172702	418	1.0	0.0	0.0	12 *backu

14172901	1.6764e-2	11.	11.	0.	0.	0.	0.	1.	12	* mod 3
*****										
* pressurizer cycling heaters										
*****										
* pressurizer backup heaters										
*****										
14201000	1	11	2	1	0.2032					
14201100	0	1								
14201101	10	0.3683								
14201201	5	10								
14201301	0.0	10								
14201401	617.	11								
14201501	4200100000	0	1	1	0.118	1				
14201601	-939	0	3969	1	0.118	1				
14201701	0	0	0	0	1					
14201801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3
14202000	1	11	1	1	0.0					
14202100	0	1								
14202101	10	0.18415								
14202201	5	10								
14202301	0.0	10								
14202401	617.	11								
14202501	4200100000	0	1	1	0.13	1				
14202601	-939	0	3969	1	0.13	1				
14202701	0	0	0	0	1					
14202801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	1	* mod 3
*****										
* steam generator heat structures										
*****										
* shroud secondary side steam generator -upper section										
*****										
15000000	3	4	2	1	0.3048					
15000100	0	1								
15000101	3	0.314325								
15000201	5	3								
15000301	0.0	3								
15000401	540.0	4								
15000501	5000100000	0	1	1	0.7725	1				
15000502	5050100000	0	1	1	0.7725	2				
15000503	5100100000	0	1	1	0.152	3				
15000601	5200100000	0	1	1	0.7725	1				
15000602	5150800000	0	1	1	0.7725	2				
15000603	5150700000	0	1	1	0.152	3				
15000701	0	0.0	0.0	0.0	3					
15000801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	3	* mod 3
15000901	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	3	* mod 3
*****										
* shroud - lower section										
*****										
15150000	4	4	2	1	0.6445					
15150100	0	1								
15150101	3	0.6572								
15150201	5	3								
15150301	0.0	3								
15150401	540.0	4								
15150501	5100100000	0	1	1	0.152	1				
15150502	5150100000	0	1	1	0.000	1	1	1	1	0.7113 4
15150601	5150700000	0	1	1	0.152	1				
15150602	5150600000	-10000	1	1	0.7113	4				
15150701	0	0	0	0	4					
15150801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	4	* mod 3
15150901	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	4	* mod 3
*****										
* vessel wall										
*****										
15300000	8	10	2	1	0.7112					
15300100	0	1								
15300101	9	0.765165								
15300201	5	9								
15300301	0.0	9								
15300401	530.0	10								
15300501	5300100000	0	1	1	0.762	1				
15300502	5250100000	0	1	1	0.762	2				
15300503	5000100000	0	1	1	0.718	3				
15300504	5050100000	0	1	1	0.718	4				
15300505	5100100000	0	1	1	0.518	5				
15300506	5150100000	10000	1	1	0.7102	8				
15300601	-939	0	3959	1	0.762	2				
15300602	-939	0	3959	1	0.718	4				
15300603	-939	0	3959	1	0.518	5				
15300604	-939	0	3959	1	0.7102	8				
15300701	0	0.0	0.0	0.0	8					
15300801	0.0	11.0	11.0	0.0	0.0	0.0	0.0	1.0	8	* mod 3
*****										
* heat structure thermal property data										
*****										
20100100	tbl/fctn	1	1	* uo2						
20100200	tbl/fctn	1	1	* gap						
20100300	tbl/fctn	1	1	* zr						
20100400	tbl/fctn	1	1	* s-steel						
20100500	c-steel									
20100600	tbl/fctn	1	1	* inconel 600						
20100700	tbl/fctn	1	1	* mgo						
20100800	tbl/fctn	1	1	* nicr						
*****										
* uo2 - thermal conductivity										
*****										
20100101	2.7315e2	8.44								
20100102	4.1667e2	6.46								
20100103	5.3315e2	5.782385								
20100104	6.99817e2	4.633177								
20100105	8.66483e2	3.880307								
20100106	1.03315e3	3.357625								
20100107	1.08871e3	3.155129								
20100108	1.19982e3	2.983787								
20100109	1.28315e3	2.836674								
20100110	1.36648e3	2.713792								
20100111	1.53315e3	2.521680								
20100112	1.61648e3	2.448990								

20100113	1.69982e3	2.391875	
20100114	1.97759e3	2.289762	
20100115	2.25537e3	2.307069	
20100116	2.53315e3	2.433413	
20100117	2.81093e3	2.661870	
20100118	3.08871e3	2.994171	
*-----	-----	-----	-----
* gap - thermal conductivity			
*-----	-----	-----	-----
20100201	273.15	0.14	
20100202	590.0	0.24	
20100203	810.0	0.29	
20100204	1090.0	0.36	
20100205	1370.0	0.42	
20100206	3260.0	0.75	
*-----	-----	-----	-----
* zircaloy-4 - thermal conductivity from matpro			
*-----	-----	-----	-----
20100301	380.4	13.6	
20100302	469.3	14.6	
20100303	577.6	15.8	
20100304	685.9	17.3	
20100305	774.8	18.4	
20100306	872.0	19.8	
20100307	973.2	21.8	
20100308	1073.2	23.2	
20100309	1123.2	25.4	
20100310	1152.3	24.2	
20100311	1232.2	25.5	
20100312	1331.2	26.6	
20100313	1404.2	28.2	
20100314	1576.2	33.0	
20100315	1625.2	36.7	
20100316	1755.2	41.2	
20100317	2273.2	55.0	
*-----	-----	-----	-----
* s-steel - thermal conductivity			
*-----	-----	-----	-----
20100401	273.15	12.98	
20100402	1199.82	25.1	
*-----	-----	-----	-----
* inconel-600 - thermal conductivity			
*-----	-----	-----	-----
20100601	366.5	13.85	
20100602	477.6	15.92	
20100603	588.7	18.17	
20100604	700.0	20.42	
20100605	810.9	22.50	
20100606	922.0	24.92	
20100607	1033.2	26.83	
20100608	1144.3	29.42	
20100609	1477.6	36.06	
*-----	-----	-----	-----
* uo2 - volumetric heat capacity			
*-----	-----	-----	-----
20100151	2.73150e2	2.310427e6	
20100152	3.23150e2	2.571985e6	
20100153	3.73150e2	2.746357e6	
20100154	6.7315e2	3.138694e6	
20100155	1.37315e3	3.443844e6	
20100156	1.77315e3	3.531030e6	
20100157	1.97315e3	3.792588e6	
20100158	2.17315e3	4.228518e6	
20100159	2.37315e3	4.882412e6	
20100160	2.67315e3	6.015829e6	
20100161	2.77315e3	6.320980e6	
20100162	2.87315e3	6.582538e6	
20100163	2.97315e3	6.713317e6	
20100164	3.11315e3	6.800503e6	
20100165	4.69982e3	6.800503e6	
*-----	-----	-----	-----
* gap - volumetric heat capacity			
*-----	-----	-----	-----
20100251	273.15	5.4	
20100252	3260.0	5.4	
*-----	-----	-----	-----
* zircaloy-4 - volumetric heat capacity from matpro			
*-----	-----	-----	-----
20100351	255.4	1.904e6	
20100352	1077.6	2.312e6	
20100353	1185.9	5.712e6	
20100354	1248.4	2.311e6	
20100355	2199.8	2.312e6	
*-----	-----	-----	-----
* s-steel - volumetric heat capacity			
*-----	-----	-----	-----
20100451	273.15	3.83e6	
20100452	366.5	3.83e6	
20100453	1366.5	5.376e6	
*-----	-----	-----	-----
* inconel-600 - volumetric heat capacity			
*-----	-----	-----	-----
20100651	366.5	3.908e6	
20100652	477.6	4.084e6	
20100653	588.7	4.260e6	
20100654	700.0	4.436e6	
20100656	810.9	4.665e6	
20100657	922.0	4.929e6	
20100658	1033.2	5.105e6	
20100659	1477.6	5.727e6	
*-----	-----	-----	-----
* magnesium oxide - thermal conductivity			
*-----	-----	-----	-----
20100701	373.15	0.2451	
20100702	422.04	0.2405	
20100703	477.59	0.2352	
20100704	533.15	0.2300	
20100705	588.71	0.2249	
20100706	644.26	0.2196	
20100707	699.82	0.2143	
20100708	755.37	0.2091	
20100709	810.93	0.2039	

20100710	866.48	0.1987	*----- ----- ----- ----- ----- ----- ----- -----
20100711	922.04	0.1934	20100801 373.15 1.1163
20100712	977.59	0.1882	20100802 1922.04 1.1163
20100713	1033.15	0.1830	20100803 5000.00 1.1163
20100714	1088.71	0.1777	*----- ----- ----- ----- ----- ----- ----- -----
20100715	1144.26	0.1725	* nichrome - volumetric heat capacity
20100716	1199.82	0.1673	*----- ----- ----- ----- ----- ----- ----- -----
20100717	1255.37	0.1621	20100851 373.15 2180.80
20100718	1310.93	0.1568	20100852 1922.04 2180.80
20100719	1366.48	0.1516	20100853 5000.00 2180.80
20100720	1422.04	0.1464	*----- ----- ----- ----- ----- ----- ----- -----
20100721	1477.59	0.1412	* pressurizer cycling heaters
20100722	1533.15	0.1359	*----- ----- ----- ----- ----- ----- ----- -----
20100723	1588.71	0.1307	20241700 power 608
20100724	1644.26	0.1255	20241701 0.0 0.0
20100725	1699.82	0.1203	20241702 60. 4.e3
20100726	1755.37	0.1150	*----- ----- ----- ----- ----- ----- ----- -----
20100727	1810.93	0.1098	* pressurizer backup heaters
20100728	1866.48	0.1046	*----- ----- ----- ----- ----- ----- ----- -----
20100729	1922.04	0.0993	20241800 power 629
20100730	5000.00	0.0993	20241801 0.0 0.0
*----- ----- ----- ----- ----- ----- ----- -----	20241802 60. 4.e3		
* magnesium oxide - volumetric heat capacity			*----- ----- ----- ----- ----- ----- ----- -----
*----- ----- ----- ----- ----- ----- ----- -----	* scram reactivity data		
20100751	373.15	2033.52	*----- ----- ----- ----- ----- ----- ----- -----
20100752	422.04	2004.59	20260900 *reac-t 609
20100753	477.59	1917.74	20260901 0.0 0.0
20100754	533.15	1938.87	20260902 0.5 -0.5
20100755	588.71	1906.01	20260903 0.59 -3.13
20100756	644.26	1873.15	20260904 0.65 -3.95
20100757	699.82	1840.29	20260905 0.75 -6.27
20100758	755.37	1807.43	20260906 0.83 -8.72
20100759	810.93	1774.56	20260907 0.90 -12.00
20100760	866.48	1741.70	20260908 0.97 -17.12
20100761	922.04	1708.84	20260909 1.125 -20.67
20100762	977.59	1675.96	20260910 1.213 -22.10
20100763	1033.15	1643.11	20260911 1.3 -22.78
20100764	1088.71	1610.25	20260912 1.4 -23.17
20100765	1144.26	1577.39	20260913 1.6 -23.32
20100766	1199.82	1544.53	20260914 60.0 -23.32
20100767	1255.37	1511.67	*----- ----- ----- ----- ----- ----- ----- -----
20100768	1310.93	1478.80	* reactor power table
20100769	1366.48	1445.94	*----- ----- ----- ----- ----- ----- ----- -----
20100770	1422.04	1413.08	20290000 power
20100771	1477.59	1380.22	20290001 0.0 48.9e6
20100772	1533.15	1347.35	*----- ----- ----- ----- ----- ----- ----- -----
20100773	1588.71	1314.49	* environmental heat loss boundary temperature
20100774	1644.26	1281.63	*----- ----- ----- ----- ----- ----- ----- -----
20100775	1699.82	1248.77	20293900 temp
20100776	1755.37	1215.90	20293901 0.0 311.0
20100777	1810.93	1183.04	*----- ----- ----- ----- ----- ----- ----- -----
20100778	1866.48	1150.18	* reactor vessel environmental loss h at xfer coefficient
20100779	1922.04	1117.32	*----- ----- ----- ----- ----- ----- ----- -----
20100780	5000.00	1117.32	20294900 htc-t
*----- ----- ----- ----- ----- ----- ----- -----	20294901 0.0 13.450		
* nichrome - thermal conductivity			*----- ----- ----- ----- ----- ----- ----- -----

\* steam generator environmental loss heat xfer coefficient  
 \*-----1-----1-----1-----1-----1-----  
 20295900 htc-t  
 20295901 0.0 3.385  
 \*-----1-----1-----1-----1-----1-----  
 \* pressurizer generator environmental loss heat xfer coefficient  
 \*-----1-----1-----1-----1-----1-----  
 20296900 htc-t  
 20296901 0.0 3.019  
 \*-----1-----1-----1-----1-----1-----  
 \* bhl environmental loss heat xfer coefficient  
 \*-----1-----1-----1-----1-----1-----  
 20297900 htc-t 509  
 20297901 -1.0 0.0  
 20297902 0.0 13.450  
 \*\*\*\* core collapsed liquid level \*\*\*\*  
 20255000 normarea 0 1.0 1.0  
 20255001 0.0 9.25e-4  
 20255002 9.25e-4 9.25e-4  
 20255003 1.0 1.0  
 20290000 power 609  
 20290001 0.0 48.9e+6  
 20290002 0.15 43.032e6  
 20290003 0.3 37.164e6  
 20290004 0.6 28.362e6  
 20290005 0.85 8.6064e6  
 20290006 1.0 5.99538e6  
 20290007 1.3 4.89e6  
 20290008 2.0 4.274e6  
 20290009 4.0 3.7060332e6  
 20290010 7.0 3.1296e6  
 20290011 10.0 2.93458e6  
 20290012 25.0 2.28548e6  
 20290013 65.0 1.7115e6  
 20290014 100.0 1.5425994e6  
 20290015 250.0 1.232769e6  
 20290016 650.0 0.91932e6  
 20290017 1000.0 0.80196e6  
 20290018 1500.0 0.6846e6  
 20290019 3000.0 0.5379e6  
 20290020 5000.0 0.44988e6  
 \*\*\*\* reactor kinetics data \*\*\*\*  
 \*-----1-----1-----1-----1-----1-----  
 30000000 point  
 30000001 gamma-ac 49.6e+6 0.0 348.43 1.0  
 0.556  
 30000002 ans79-1  
 \*-----1-----1-----1-----1-----1-----  
 \* shoud not be changed for transient  
 \*-----1-----1-----1-----1-----1-----  
 \* delayed neutron constants  
 \*-----1-----1-----1-----1-----1-----  
 30000101 0.0349 0.01275  
 30000102 0.2035 0.03177  
 30000103 0.1848 0.1181  
 30000104 0.4046 0.3160  
 30000105 0.1401 1.402  
 30000106 0.0321 3.914  
 \*\*\*\* power history \*\*\*\*  
 30000401 4.96e+7 70. hr  
 \*-----1-----1-----1-----1-----1-----  
 \* reactivity curve numbers  
 \*-----1-----1-----1-----1-----1-----  
 30000011 609  
 \*\*\*\* moderator density reactivity table \*\*\*\*  
 \*-----1-----1-----1-----1-----1-----  
 30000501 0.818 -4.428  
 30000502 0.905 -2.249  
 30000503 0.955 -1.032  
 30000504 1.000 0.000  
 30000505 1.044 0.926  
 30000506 1.095 1.853  
 30000507 1.139 2.589  
 30000508 1.213 3.689  
 30000509 1.270 4.489  
 30000510 1.316 5.212  
 \*\*\*\* doppler reactivity table \*\*\*\*  
 \*-----1-----1-----1-----1-----1-----  
 30000601 293.16 1.375  
 30000602 338.72 1.125  
 30000603 422.05 0.682  
 30000604 477.60 0.419  
 30000605 505.38 0.274  
 30000606 570.72 0.000  
 30000607 588.72 -0.075  
 30000608 695.83 -0.526  
 30000609 922.05 -1.386  
 30000610 1310.94 -2.543  
 30000611 1810.94 -3.865  
 30000612 2088.72 -4.502  
 30000613 2499.83 -5.392  
 30000614 3027.60 -6.417  
 \*\*\*\* moderator density reactivity table \*\*\*\*  
 \*-----1-----1-----1-----1-----1-----  
 30000501 0.818 0.0  
 30000502 0.905 0.0  
 30000503 0.955 0.0  
 30000504 1.000 0.0  
 30000505 1.044 0.0  
 30000506 1.095 0.0  
 30000507 1.139 0.0  
 30000508 1.213 0.0  
 30000509 1.270 0.0

30000510	1.316	0.0						
*****								
* doppler reactivity table								
*****								
30000601	293.16	0.0						
30000602	338.72	0.0						
30000603	422.05	0.0						
30000604	477.60	0.0						
30000605	505.38	0.0						
30000606	570.72	0.0						
30000607	588.72	0.0						
30000608	695.83	0.0						
30000609	922.05	0.0						
30000610	1310.94	0.0						
30000611	1810.94	0.0						
30000612	2088.72	0.0						
30000613	2499.83	0.0						
30000614	3027.60	0.0						
* ----- no reactivity feedback for steady state run								
* ----- should be replaced by original one for transient								
*****								
* volume weighting factors								
*****								
* moderator temperature feedback								
*****								
30000701	230010000	0	0.31493	0.0				
30000702	230020000	0	0.31493	0.0				
30000703	230030000	0	0.37014	0.0				
*****								
doppler feedback								
*****								
30000801	2300001	0	0.43153	0.0				
30000802	2300002	0	0.51686	0.0				
30000803	2300003	0	0.05161	0.0				
*****								
*								
* control variables								
*								
*****								
* steam generator downcomer collapsed liquid level								
*****								
20500100	sglvl	sum	1.0	0.0	1			
20500101	0.0	0.718	voidf	500010000				
20500102	0.718	voidf	505010000					
20500103	0.518	voidf	510010000					
20500104	0.7102	voidf	515010000					
20500105	0.7102	voidf	515020000					
20500106	0.7102	voidf	515030000					
*****								
* pressurizer collapsed liquid level								
*****								
20500200	pzrlvl	sum	1.0	0.0	1			
20500201	0.0	0.224	voidf	415010000				
20500202	0.403	voidf	415020000					
20500203	0.403	voidf	415030000					
20500204	0.207	voidf	415040000					
*****								
20500205			0.207	voidf	415050000			
20500206			0.1705	voidf	415060000			
20500207			0.1705	voidf	415070000			
20500208			0.118	voidf	415080000			
20500209			0.118	voidf	420010000			
*****								
* core collapsed liquid level								
*****								
20500300	rvlvl	sum	1.0	0.0	1			
20500301	0.0	0.712	voidf	250010000				
20500302			0.854	voidf	250010000			
20500303			0.843	voidf	245010000			
20500304			1.118	voidf	240010000			
20500305			0.657	voidf	230030000			
20500306			0.559	voidf	230020000			
20500307			0.559	voidf	230010000			
20500308			0.520	voidf	225010000			
20500309			0.360	voidf	215010000			
20500310			0.370	voidf	220010000			
*****								
* hot leg intact loop								
*****								
20504100	pcsvol1	sum	1.0	0.0	1			
20504101	0.0	0.09746482	rho	100010000				
20504102			0.1035956	rho	105010000			
20504103			3.0300e-2	rho	110010000			
20504104			9.0000e-2	rho	115010000			
20504105			5.7000e-2	rho	115020000			
*****								
* steam generator								
*****								
20504200	pcsvol2	sum	1.0	0.0	1			
20504201	0.0	0.3350000	rho	115030000				
20504202			0.1611170	rho	115040000			
20504203			0.1611170	rho	115050000			
20504204			6.7950e-2	rho	115060000			
20504205			6.7950e-2	rho	115070000			
20504206			1.61117-1	rho	115080000			
20504207			1.61117-1	rho	115090000			
20504208			3.3500e-1	rho	115100000			
*****								
* sg-pump piping								
*****								
20504300	pcsvol3	sum	1.0	0.0	1			
20504301	0.0	4.37000-2	rho	115110000				
20504302			4.62000-2	rho	115120000			
20504303			3.54406-2	rho	115130000			
20504304			4.81840-2	rho	120010000			
20504305			6.13000-2	rho	125010000			
20504306			1.89000-2	rho	130010000			
20504307			6.13000-2	rho	155010000			
20504308			1.89000-2	rho	160010000			
*****								
* cold leg intact loop								
*****								
20500400	pcsvol4	sum	1.0	0.0	1			

20500401	0.0	9.90000-2 rho	135010000	20500704	5.41000-3 rho	350010000
20500402		1.83732-2 rho	140010000	20500705	8.55000-2 rho	380010000
20500403		6.33000-2 rho	145010000	20500706	1.18030-1 rho	385010000
20500404		3.14844-2 rho	150010000	*	*	*
20500405		9.90000-2 rho	165010000	*	pressurizer	*
20500406		1.88124-2 rho	170010000	*	*	*
20500407		3.54406-2 rho	175010000	20500800	pcsvol8 sum 1.0	0.0 1
20500408		3.88642-2 rho	175020000	20500801	0.0 5.00250-3 rho	400010000
20500409		4.44434-2 rho	180010000	20500802	5.00250-3 rho	405010000
20500410		9.26274-2 rho	185010000	20500803	8.10880-2 rho	415010000
*	*	*	*	20500804	2.27695-1 rho	415020000
*	reactor	*	*	20500805	2.27695-1 rho	415030000
*	*	*	*	20500806	1.16955-1 rho	415040000
20500500	pcsvol5	sum 1.0	0.0 1	20500807	1.16955-1 rho	415050000
20500501	0.0	2.66400-1 rho	215010000	20500808	7.94530-2 rho	415060000
20500502		2.92300-1 rho	220010000	20500809	7.94530-2 rho	415070000
20500503		1.30000-1 rho	225010000	20500810	1.53400-2 rho	415080000
20500504		9.53095-2 rho	230010000	*	*	*
20500505		9.53095-2 rho	230020000	*	reactor vessel downcomer mass	*
20500506		0.1120185 rho	230030000	*	*	*
20500507		8.38500-3 rho	235010000	20500900	dwnrms sum 1.0	0.0 1
20500508		8.38500-3 rho	235020000	20500901	0.0 8.55000-2 rho	200010000
20500509		9.35500-3 rho	235030000	20500902	1.10000-1 rho	205010000
20500510		3.32046-1 rho	240010000	20500903	1.36036-1 rho	210010600
20500511		9.61020-2 rho	245010000	20500904	1.36036-1 rho	210020000
20500512		1.28100-1 rho	246010000	20500905	1.36036-1 rho	210030000
20500513		2.45952-1 rho	250010000	20500906	1.36036-1 rho	210040000
20500514		1.73728-1 rho	250010000	20500907	1.23426-2 rho	223010000
*	*	*	*	20500908	2.78874-2 rho	223020000
*	hot leg broken loop	*	*	20500909	2.78874-2 rho	223030000
*	*	*	*	20500910	2.78874-2 rho	223040000
20500600	pcsvol6	sum 1.0	0.0 1	20500911	2.78874-2 rho	223050000
20500601	0.0	5.55384-2 rho	300010000	20500912	1.04796-2 rho	223060000
20500602		4.42532-2 rho	305010000	20500913	1.04796-2 rho	223070000
20500603		6.68000-2 rho	310010000	*	*	*
20500604		3.38914-3 rho	315010000	*	pcs mass	*
20500605		4.40154-3 rho	315020000	*	*	*
20500606		3.90960-2 rho	315030000	20501000	pcsmass sum 1.0	0.0 1
20500607		1.82736-1 rho	315040000	20501001	0.0 1.0 cntrivar 41	
20500608		9.17460-2 rho	315050000	20501002	1.0 cntrivar 42	
20500609		9.17460-2 rho	315060000	20501003	1.0 cntrivar 43	
20500610		1.82736-1 rho	315070000	20501004	1.0 cntrivar 4	
20500611		3.90960-2 rho	315080000	20501005	1.0 cntrivar 5	
20500612		1.62000-2 rho	315090000	20501006	1.0 cntrivar 6	
20500613		6.48000-2 rho	315100000	20501007	1.0 cntrivar 7	
20500614		.01539912 rho	315110000	20501008	1.0 cntrivar 8	
20500615		3.50175-2 rho	315120000	20501009	1.0 cntrivar 9	
20500616		8.54764-2 rho	370010000	*	*	*
20500617		8.58000-2 rho	375010000	*	break energy computer	*
*	*	*	*	20542500	pvfstm div 1.0	0.0 1
*	cold leg broken loop	*	*	20542501	rhof 420010000 p	420010000
*	*	*	*	*	*	*
20500700	pcsvol7	sum 1.0	0.0 1	20542600	hfstm sum 1.0	0.0 1
20500701	0.0	4.75183-2 rho	335010000	20542601	0.0 1.0 uf 420010000	
20500702		4.42532-2 rho	340010000	20542602	1.0 cntrivar 425	
20500703		6.17516-2 rho	345010000			

20542700	pvgstm	div	1.0	0.0	i	20511307	1.86543	htnr	212000401		
20542701	rhog	420010000 p		420010000		20511308	1.91724	htnr	212000501		
*						20511309	1.68000	htnr	220000101		
20542800	hgstm	sum	1.0	0.0	1	20511310	0.71200	htnr	255000101		
20542801	0.0	1.0	ug	420010000		*	1	1	1		
20542802		1.0	cntrivar	427		*	1	1	1		
*						20511400	przheat	sum	1.0	0.0	1
20542900	xhgstm	mult	1.0	0.0	1	20511401	0.0	0.362	htnr	415100101	
20542901	quals	420010000 cntrivar	428			20511402		0.702464	htnr	415200101	
*						20511403		1.26381	htnr	415200201	
20543000	xhfstm	mult	1.0	0.0	1	20511404		1.26381	htnr	415200301	
20543001	quals	420010000 cntrivar	426			20511405		0.649152	htnr	415200401	
*						20511406		0.649152	htnr	415200501	
20543100	yhfstm	sum	1.0	0.0	1	20511407		0.534688	htnr	415200601	
20543101	0.0	1.0	cntrivar	426		20511408		0.534688	htnr	415200701	
20543102		-1.0	cntrivar	430		20511409		0.273063	htnr	416200101	
*						20511410		0.130000	htnr	420100101	
20543200	hsteam	sum	1.0	0.0	1	20511411		0.273063	htnr	420200101	
20543201	0.0	1.0	cntrivar	429		*	1	1	1		
20543202		1.0	cntrivar	431		*	heat loss from s/g				
*						*	1	1	1		
20543300	brkpwr	mult	1.0	0.0	1	20511500	sgheat	sum	1.0	0.0	1
20543301	mflowj	425000000 cntrivar	432			20511501	0.0	3.5343	htnr	530000101	
*						20511502		3.5343	htnr	530000201	
20543400	brkflow	integral	1.0	0.0	1	20511503		3.33022	htnr	530000301	
20543401	mflowj	425000000				20511504		3.33022	htnr	530000401	
*						20511505		2.40258	htnr	530000501	
*	011 - 031 heat transfer rate calculator					20511506		3.29404	htnr	530000601	
*						20511507		3.29404	htnr	530000701	
*	heat added to pcs from core					20511508		3.29404	htnr	530000801	
*						*	1	1	1		
20511100	corhitr	sum	1.0	0.0	1	*	toal heat loss from major components				
20511101	0.0	24.374	htnr	230000101		*	1	1	1		
20511102		24.374	htnr	230000201		20511600	toheat	sum	1.0	0.0	1
20511103		24.374	htnr	230000301		20511601	0.0	1.0	cntrivar	113	
*						20511602		1.0	cntrivar	114	
*	heat removed from pcs at to s/g tubes					20511603		1.0	cntrivar	115	
*						*	1	1	1	1	
20511200	sghttr	sum	1.0	0.0	1	*	heat loss from broken loop hot leg				
20511201	0.0	44.824	htnr	006000100		*	1	1	1		
20511202		44.824	htnr	006000200		20511700	bliheat	sum	1.0	0.0	1
20511203		44.824	htnr	006000300		20511701	0.0	0.97972	htnr	300000101	
20511204		44.824	htnr	006000400		20511702		0.78065	htnr	300000201	
20511205		44.824	htnr	006000500		20511703		1.59260	htnr	300000301	
20511206		44.824	htnr	006000600		*	1	1	1	1	
*						*	heat loss from broken loop cold leg				
*	heat loss from reactor vessel					*	1	1	1		
*						20511800	bclheat	sum	1.0	0.0	1
20511300	rvheat	sum	1.0	0.0	1	20511801	0.0	0.83825	htnr	335000101	
20511301	0.0	2.3244	htnr	211000101		20511802		0.78065	htnr	335000201	
20511302		5.25183	htnr	211000201		20511803		1.0893	htnr	335000301	
20511303		3.56335	htnr	211000301		*	1	1	1	1	
20511304		1.59598	htnr	212000101		*	heat loss from rabs piping				
20511305		4.96411	htnr	212000201		*	1	1	1		
20511306		4.96411	htnr	212000301		20511900	rabheat	sum	1.0	0.0	1

20511901	0.0	1.7153	htnr	3700060101	20512308	0.453056	htnr	415200700		
20511902	0.94828	htnr	370000201	20512309	0.150656	htnr	416200100			
20511903	0.94497	htnr	370000301	20512310	0.13000	htnr	420100100			
20511904	2.6090	htnr	370000401	20512311	0.150656	htnr	420200100			
* heat loss from intact loop hot leg										
* metal heating in reactor vessel (1st part)										
20512000	ilclheat sum	1.0	0.0	1	20525100	rv1	sum	1.0	0.0	1
20512001	0.0	1.7193	htnr	100100101	20525101	0.0	1.05331	htnr	200000100	
20512002	1.8275	htnr	100100201	20525102	0.79000	htnr	200100101			
20512003	0.69677	htnr	100100301	20525103	1.01501	htnr	200100201			
20512004	1.6088	htnr	100100401	20525104	2.29335	htnr	200100301			
20512005	0.90304	htnr	100200101	20525105	2.29335	htnr	200100401			
20512006	1.8855	htnr	100400101	20525106	2.29335	htnr	200100501			
* heat loss from intact loop cold leg										
20512100	ilclheat sum	1.0	0.0	1	20525107	2.29335	htnr	200100601		
20512101	0.0	0.77058	htnr	100100501	20525108	1.33475	htnr	205000100		
20512102	0.62519	htnr	100100601	20525109	1.93518	htnr	205000101			
20512103	0.84999	htnr	100100701	20525110	2.82907	htnr	210000100			
20512104	0.55540	htnr	100100801	20525111	2.82907	htnr	210000200			
20512105	0.62519	htnr	100100901	20525112	2.82907	htnr	210000300			
20512106	0.68558	htnr	100101001	20525113	2.82907	htnr	210000400			
20512107	0.78400	htnr	100101101	20525114	1.06311	htnr	210000500			
20512108	1.6340	htnr	100101201	20525115	1.09265	htnr	210000600			
20512109	0.69769	htnr	100200201	20525116	4.37241	htnr	210000101			
20512110	0.85765	htnr	100300101	20525117	4.37241	htnr	210000201			
20512111	0.39195	htnr	100300201	20525118	4.37241	htnr	210000301			
20512112	0.43054	htnr	100300301	20525119	4.37241	htnr	210000401			
20512113	1.2079	btrnr	100300401	20525120	1.64308	htnr	210000501			
20512114	0.86023	htnr	100300501	*						
20512115	0.39195	htnr	100300601	20525200	rv2	sum	1.0	0.0	1	
20512116	0.44083	htnr	100300701	20525201	0.0	1.68872	htnr	210000601		
20512117	1.8855	htnr	100400201	20525202	1.95223	htnr	211000100			
* total heat loss to environment										
20512200	sumhtls sum	1.0	0.0	1	20525203	4.41094	htnr	211000200		
20512201	0.0	1.0	cntrivar	116	20525204	2.99281	htnr	211000300		
20512202	1.0	cntrivar	117	20525205	1.41813	htnr	212000100			
20512203	1.0	cntrivar	118	20525206	4.41094	htnr	212000200			
20512204	1.0	cntrivar	119	20525207	4.41094	htnr	212000300			
20512205	1.0	cntrivar	120	20525208	1.65755	htnr	212000400			
20512206	1.0	cntrivar	121	20525209	1.70360	htnr	212000500			
* metal heating in pzs										
20512300	pzrmtht sum	1.0	0.0	1	20525210	1.6800	htnr	220000100		
20512301	0.0	0.3620	htnr	415100100	*					
20512302	0.59522	htnr	415200100	20525300	rv3	sum	1.0	0.0	1	
20512303	1.07086	htnr	415200200	20525301	0.0	0.695734	htnr	225000700		
20512304	1.07086	htnr	415200300	20525302	0.921366	htnr	226000100			
20512305	0.550045	htnr	415200400	20525303	1.98094	htnr	240000100			
20512306	0.550045	htnr	415200500	20525304	1.80000	htnr	246000100			
20512307	0.453056	htnr	415200600	20525305	1.80000	htnr	246000101			
				20525306	2.04439	htnr	250000100			
				20525307	1.00000	htnr	251000100			
				20525308	1.00000	htnr	251000200			
				20525309	1.70445	htnr	250100100			
				20525310	0.71200	htnr	255000100			
				20525311	1.68000	htnr	220000101			
				20525312	0.980177	htnr	225000100			
				20525313	1.05369	htnr	225000200			
				20525314	1.05369	htnr	225000300			

20525315	1.23842	htnr	225000400	
20525316	2.10738	htnr	225000500	
20525317	0.791681	htnr	225000600	
20525318	1.0	cntrvar	251	
20525319	1.0	cntrvar	252	
*-----1-----1-----1-----1-----1-----1-----				
* metal heating in broken loop (1st part)				
*-----1-----1-----1-----1-----1-----1-----				
20512600	bklpmht	sum	1.0 0.0 1	
20512601	0.0	0.157878	htnr	300000100
20512602		0.622764	htnr	300000200
20512603		1.27051	htnr	300000300
20512616		0.668713	htnr	335000100
20512617		0.622764	htnr	335000200
20512618		0.869015	htnr	335000300
*-----1-----1-----1-----1-----1-----1-----				
* metal heating in broken loop				
*-----1-----1-----1-----1-----1-----1-----				
20512700	bklpmht	sum	1.0 0.0 1	
20512701	0.0	1.39487	htnr	370000100
20512702		0.771131	htnr	370000200
20512703		0.768435	htnr	370000300
20512704		2.12160	htnr	370000400
20512705		1.0	cntrvar	126
*-----1-----1-----1-----1-----1-----1-----				
* metal heating in intact loop hot leg				
*-----1-----1-----1-----1-----1-----1-----				
20512800	ilhlmht	sum	1.0 0.0 1	
20512801	0.0	1.3716	htnr	100100100
20512802		1.45787	htnr	100100200
20512803		0.55548	htnr	100100300
20512804		1.28345	htnr	100100400
20512805		0.72288	htnr	100200100
20512806		1.4772	htnr	100400100
*-----1-----1-----1-----1-----1-----1-----				
* metal heating in intact loop cold leg				
*-----1-----1-----1-----1-----1-----1-----				
20512900	ilclmht	sum	1.0 0.0 1	
20512901	0.0	0.614734	htnr	100100500
20512902		0.498747	htnr	100100600
20512903		0.678081	htnr	100100700
20512904		0.443073	htnr	100100800
20512905		0.498747	htnr	100100900
20512906		0.546926	htnr	100101000
20512907		0.625441	htnr	100101100
20512908		1.30352	htnr	100101200
20512909		0.558497	htnr	100200200
20512910		0.678584	htnr	100300100
20512911		0.310113	htnr	100300200
20512912		0.340649	htnr	100300300
20512913		0.955718	htnr	100300400
20512914		0.680620	htnr	100300500
20512915		0.310113	htnr	100300600
20512916		0.348792	htnr	100300700
20512917		1.4772	htnr	100400200
*-----1-----1-----1-----1-----1-----1-----				

* metal heating in broken loop simulators						
*-----1-----1-----1-----1-----1-----1-----						
20513000	blhlsim	sum	1.0 0.0 1			
20513001	0.0	0.1312	htnr	315000100		
20513002		0.1703	htnr	315000200		
20513003		0.0042	htnr	315100100		
20513004		0.00347	htnr	315200100		
20513005		0.12452	htnr	315300100		
20513006		0.12452	htnr	315300200		
20513007		0.12452	htnr	315300300		
20513008		0.12452	htnr	315300400		
20513009		0.12452	htnr	315300500		
20513010		0.12452	htnr	315300600		
20513011		0.04239	htnr	315400100		
20513012		0.04363	htnr	315500100		
*-----1-----1-----1-----1-----1-----1-----						
* metal heating in steam generator						
*-----1-----1-----1-----1-----1-----1-----						
20555100	sgmth1	sum	1.0 0.0 1			
20555101	0.0	1.47943	htnr	500000100		
20555102		1.47943	htnr	500000200		
20555103		0.291097	htnr	500000300		
20555104		1.52566	htnr	500000101		
20555105		1.52566	htnr	500000201		
20555106		0.300194	htnr	500000301		
20555107		0.615526	htnr	515000100		
20555108		2.88042	htnr	515000200		
20555109		2.88042	htnr	515000300		
20555110		2.88042	htnr	515000400		
20555111		0.627655	htnr	515000101		
20555112		2.93718	htnr	515000201		
20555113		2.93718	htnr	515000301		
20555114		2.93718	htnr	515000401		
*-----1-----1-----1-----1-----1-----1-----						
20555200	sgmth2	sum	1.0 0.0 1			
20555201	0.0	3.40507	htnr	530000100		
20555202		3.40507	htnr	530000200		
20555203		3.20846	htnr	530000300		
20555204		3.30846	htnr	530000400		
20555205		2.31474	htnr	530000500		
20555206		3.17360	htnr	530000600		
20555207		3.17360	htnr	530000700		
20555208		3.17360	htnr	530000800		
*-----1-----1-----1-----1-----1-----1-----						
* pcs-tubesheet heat transfer						
*-----1-----1-----1-----1-----1-----1-----						
20513200	pcstub	sum	1.0 0.0 1			
20513201	0.0	56.4226	htnr	115100100		
20513202		56.4226	htnr	115100200		
20513203		0.157962	htnr	115200100		
20513204		0.157962	htnr	115200200		
*-----1-----1-----1-----1-----1-----1-----						
* tubesheet-scs heat transfer						
*-----1-----1-----1-----1-----1-----1-----						
20513300	tushscs	sum	1.0 0.0 1			
20513301	0.0	0.157962	htnr	115200101		

```

20513302      0.157962 htrnr  115200201
*****1-----1-----1-----1-----1-----1-----
* metal hx in tabs
*****1-----1-----1-----1-----1-----1-----
20517000 tabs sum 1.0 0.0 1
20517001 0.0 1.39487 htrnr 370000100
20517002 0.77113 htrnr 370000200
20517003 0.77278 htrnr 370000300
20517004 2.12160 htrnr 370000400
*****
bi total metal hx
*****
20517100 qbltotal sum 1.0 0.0 1
20517101 0.0 1.0 cntrivar 127
*20517102 1.0 cntrivar 170
20517103 1.0 cntrivar 130 * only for simula
*****
* pcs stored energy excluding pressurizer
*****
20557000 pcsgre sum 1.0 0.0 1
20557001 0.0 1.0 cntrivar 253 * rv metal heat
20557002 1.0 cntrivar 113 * rv ambloss
20557003 1.0 cntrivar 171 * only for simula
20557004 1.0 cntrivar 117 * blhl ambloss
20557005 1.0 cntrivar 118 * blcl ambloss
20557006 1.0 cntrivar 119 * rabv ambloss
20557007 1.0 cntrivar 128 * ilhi heat
20557008 1.0 cntrivar 120 * ilhi ambloss
20557009 1.0 cntrivar 129 * ilcl heat
20557010 1.0 cntrivar 121 * ilcl ambloss
20557011 1.0 cntrivar 132 * pcs-tubesheet
20557012 1.0 cntrivar 133 * tubesheet-scs
*****
ses stored energy
*****
20557300 scsqse sum 1.0 0.0 1
20557301 0.0 1.0 cntrivar 552 * sg heat
20557302 1.0 cntrivar 115 * sg ambloss
*****
* heat flow calculations
*****
ecc energy flow
*****
20515300 pvecc div 1.0 0.0 1
20515301 rhofj 630000000 p 600010000
20515400 hecc sum 1.0 0.0 1
20515401 0.0 1.0 uff 630000000
20515402 1.0 cntrivar 153
20515500 mdothecc mult 1.0 0.0 1
20515501 mflowj 630000000
20515502 cntrivar 154
20515600 qecc/v mult 0.126646 0.0 1
20515601 cntrivar 155
20515700 mdotev mult 0.126646 0.0 1
20515701 mflowj 630000000
*****

```

```

sg hx per unit pcs volume
*****
20516000 qsg/v mult 0.126646 0.0 1
20516001 cntrivar 112
*****
* core hx per unit pcs volume
*****
20516100 qcove/v mult 0.126646 0.0 1
20516101 cntrivar 111
*****
pump power
*****
20516200 pledotv mult 0.04136 0.0 1
20516201 voidgj 135020000
20516202 velgj 135020000
20516203 pmphd 135
20516300 pledot mult 0.04136 0.0 1
20516301 voidfj 135020000
20516302 vslfj 135020000
20516303 pmphd 135
20516400 p2edotv mult 0.04136 0.0 1
20516401 voidgj 165020000
20516402 velgj 165020000
20516403 pmphd 165
20516500 p2edotl mult 0.04136 0.0 1
20516501 voidfj 165020000
20516502 vslfj 165020000
20516503 pmphd 165
20516600 qpmp sum 1.0 0.0 1
20516601 0.0 1.0 cntrivar 162
20516602 1.0 cntrivar 163
20516603 1.0 cntrivar 164
20516604 1.0 cntrivar 165
20516700 qpmp/v mult 0.126646 0.0 1
20516701 cntrivar 166
*****
energy to fluid in vessel from structures
*****
20562000 rvhx sum 6.2832 0.0 1
20562001 0.0 0.3080 htrnr 205000101
20562002 0.6959 htrnr 210000101
20562003 0.6959 htrnr 210000201
20562004 0.6959 htrnr 210000301
20562005 0.6959 htrnr 210000401
20562006 0.2615 htrnr 210000501
20562007 0.2688 htrnr 210000601
20562008 0.3107 htrnr 211000100
20562009 0.7020 htrnr 211000200
20562010 0.7020 htrnr 212000100
20562011 0.7020 htrnr 212000200
20562012 0.7030 htrnr 212000300
20562013 0.6 htrnr 212000400
20562014 0.2 htrnr 212000500
20562015 1.0 cntrivar 253
*****
* total vessel hx/v
*****
```

```

*-----|-----|-----|-----|-----|-----|-----|-----|
20562100 rvhx/v mult 1.0 0.0 1
20562101 cntrivar 620
***** total massless energy flows from pcs excluding qcore and qsg *****
*****-----|-----|-----|-----|-----|-----|-----|-----|
20562200 qstruc sum 1.0 0.0 1
20562201 0.0 1.0 cntrivar 123 * przr
20562202 1.0 cntrivar 620 * rv
20562203 1.0 cntrivar 171 * bl
20562204 1.0 cntrivar 128 * ilhl
20562205 1.0 cntrivar 129 * ilcl
20562300 qstruc/v mult 0.126646 0.0 1
20562301 cntrivar 622
*****-----|-----|-----|-----|-----|-----|-----|-----|
* sum of all massless energy flows from pcs
*****-----|-----|-----|-----|-----|-----|-----|-----|
20562400 de/dt sum 1.0 0.0 1
20562401 0.0 1.0 cntrivar 111 * core
20562402 1.0 cntrivar 112 * sg
20562403 1.0 cntrivar 622 * structure
20562404 1.0 cntrivar 166 * pumps
20562500 de/dt/vv mult 0.126646 0.0 1
20562501 cntrivar 624
*****-----|-----|-----|-----|-----|-----|-----|-----|
* sum of mass flow energy flows and massless energy flows
*****-----|-----|-----|-----|-----|-----|-----|-----|
20562600 dtqflo sum 1.0 0.0 1
20562601 0.0 1.0 cntrivar 624 * de/dt
20562602 -1.0 cntrivar 433 * porv
20562700 dtqf/v mult 0.126646 0.0 1
20562701 cntrivar 626
*****-----|-----|-----|-----|-----|-----|-----|-----|
*-----|-----|-----|-----|-----|-----|-----|-----|
* primary coolant pump speed controllers
*****-----|-----|-----|-----|-----|-----|-----|-----|
* calculate mass flow error
*****-----|-----|-----|-----|-----|-----|-----|-----|
20590100 msserr sum 1.0 0.0 1
20590101 479.30 -1.0 mflowj 100010000
*****-----|-----|-----|-----|-----|-----|-----|-----|
* pump 1 speed
*****-----|-----|-----|-----|-----|-----|-----|-----|
20590200 pcp1spd integral 0.34482 333.7236 1
20590201 cntrivar 901
*****-----|-----|-----|-----|-----|-----|-----|-----|
* pcp1 pump velocity table
*****-----|-----|-----|-----|-----|-----|-----|-----|
1356100 508 cntrivar 902
1356101 0.0 0.0
1356102 369.0 369.0
*****-----|-----|-----|-----|-----|-----|-----|-----|
* modify pcp1 pump data
*****-----|-----|-----|-----|-----|-----|-----|-----|
1350301 0 0 0 -1 0 504 0
*****-----|-----|-----|-----|-----|-----|-----|-----|
*-----|-----|-----|-----|-----|-----|-----|-----|
* pump 2 speed
*****-----|-----|-----|-----|-----|-----|-----|-----|
20590300 pcp2spd integral 0.34482 331.9524 1
20590301 cntrivar 901
*****-----|-----|-----|-----|-----|-----|-----|-----|
* pcp2 pump velocity table
*****-----|-----|-----|-----|-----|-----|-----|-----|
1656100 508 cntrivar 903
1656101 0.0 0.0
1656102 369.0 369.0
*****-----|-----|-----|-----|-----|-----|-----|-----|
* modify pcp2 pump data
*****-----|-----|-----|-----|-----|-----|-----|-----|
1650301 135 135 135 -1 0 504 0
*****-----|-----|-----|-----|-----|-----|-----|-----|
* pressurizer spray valve controller
*****-----|-----|-----|-----|-----|-----|-----|-----|
* spray valve
*****-----|-----|-----|-----|-----|-----|-----|-----|
4070000 sprv1 valve
4070101 406010000 420010000 3.3451e-4 1.5432e01
1.5432e01 000100
4070201 0 .00000000 .00000000 0.0
4070300 srvv1v
4070301 904 999
*****-----|-----|-----|-----|-----|-----|-----|-----|
* spray valve position calculator
*****-----|-----|-----|-----|-----|-----|-----|-----|
20590400 sprv2 sum -1.0 0.0 1 * contin
+ 3 0.0 1.0
20590401 14.93+6 -1.0 p 420010000
*****-----|-----|-----|-----|-----|-----|-----|-----|
* position vs area table
*****-----|-----|-----|-----|-----|-----|-----|-----|
20299900 normarea
20299901 0.0 0.0
20299902 0.0001 0.0
20299903 1.0 1.0
*****-----|-----|-----|-----|-----|-----|-----|-----|
* pressurizer level control using charging and letdown components
*****-----|-----|-----|-----|-----|-----|-----|-----|
* charging reservoir
*****-----|-----|-----|-----|-----|-----|-----|-----|
*6%00000 chrg tmdpyol
*9800101 1.0 1.0 0.0 0.0 0.0 0.0
*9800102 4.0-5 0.0 00000
*9800200 3
*9800201 0.0 2.07+07 558.9
*****-----|-----|-----|-----|-----|-----|-----|-----|
* charging valve
*****-----|-----|-----|-----|-----|-----|-----|-----|
*9850000 chrg valve
*9850101 980000000 185000000 3.8e-05 0.0 0.0
000100

```

```

*9850201 0      .00000000 .00000000 0.0      *20290802 -0.25  -0.25
*9850300 srvvlv
*9850301 905    999
*      1      1      1
* charging valve position calculator
*      1      1      1
*20590500 charge sum   7.7   0.0   1  *contin
*+   3     0.0   1.0
*20590501 0.92  -1.0  cntrlvar 2
*      1      1      1
* letdown sink
*      1      1      1
*9900000 ltdwn   tmdpvol
*9900101 1.0    1.0   0.0   0.0   0.0   0.0      *20591000 tcontrol sum   1.0   0.645229 0  *conti
*9900102 4.0-5  0.0    00000
*9900200 3
*9900201 0.0    1.4+7  558.9
*      1      1      1
* letdown valve
*      1      1      1
*9950000 ltdwn   valve
*9950101 185000000 990000000 2.5-5  0.0   0.0      20591100 sglvler sum   1.0   0.0   1
000100
*9950201 0      .00000000 .00000000 0.0      20591101 3.09  -1.0  cntrlvar 001
*9950300 srvvlv
*9950301 906    999
*      1      1      1
* letdown valve position calculator
*      1      1      1
*20590600 letdown sum   -7.7   0.0   1  *contin      20591200 feedflow sum   1.0   0.0   1
*+   3     0.0   1.0
*20590601 1.10  -1.0  cntrlvar 2
*      1      1      1
* steam valve controller
*      1      1      1
* changes to steam valve
*      1      1      1
*5500201 0      19.758  22.082  0.0
*5500300 srvvlv
*5500301 910    540
*20254000 normarea
*20254001 0.0    0.0
*20254002 0.0001  0.0
*20254003 1.0    1.0
*      1      1      1
* compute delta t error
*      1      1      1
*20590700 delta sum   1.0   0.0   1
*20590701 559.0  -1.    tempf   185010000
*      1      1      1
* filter delta t thru deadband
*      1      1      1
*20590800 deadband function 1.0    0.0   1
*20590801 cntrlvar 907    908
*20290800 reac-
*20290801 -100.  -100.

```

**Appendix B      Input Deck for Transient Calculation**

=loft 19-1 post test analysis deck

\* initial conditions

\* pcp pressure = 14.901 mpa

\* core power = 50. mw

\* pcc flow = 479.3 kg/s

\* thot = 578. k

\* tcold = 559.0 k

0000100 restart transm

0000101 run

0000102 si

\* 0000103 16006

0000103 6934

0000105 5. 10.

\* time step control cards

	end time	min dt	max dt	optn	mnr	mjr	rst
0000201	200.00	1.e-5	1.0	2	1	30	100
0000202	1000.0	1.e-6	1.0	2	5	300	500
0000203	2000.0	1.e-6	0.1	2	50	3000	5000
0000204	4000.0	1.e-6	0.5	2	10	1000	2000
0000205	8000.0	1.e-6	0.1	2	50	4000	5000
0000206	10000.	1.e-6	0.5	2	10	2000	2000

\* minor edit variables

\* pressure

	p	345010000	* pe-bl-1
0000301	p	310010000	* pe-bl-2
*0000303	p	315110000	* pe-bl-3
*0000304	p	350010000	* pe-bl-4
*0000305	p	315090000	* pe-bl-6
*0000306	p	350020000	* pe-bl-8
0000302	p	185010000	* pe-pc-1
0000303	p	100010000	* pe-pc-2
0000304	p	420010000	* porv inlet
*0000310	p	110010000	* pt-139-2,3,4
0000305	p	245010000	* pe-lup-1a,1b
0000306	p	215010000	* pe-1st-1a,b/pe-2st-1a,b
*0000313	p	200010000	* pe-1st-3a,3b
0000307	p	530010000	* pe-sgs-01
0000308	p	535010000	* pt-p-4-85

\* temperatures

	tempf	406010000	* spray tempf
0000309	tempf	310010000	* te-bl-2a,2b,2c
0000311	tempf	100010000	* te-pc-2a,2b,2c
0000312	tempf	185010000	* te-pc-1
0000313	tempf	115030000	* te-sg-1
0000314	tempf	115100000	* te-sg-2
0000315	tempf	515070000	* te-sg-4

\*0000328 tempf 415050000 \* pqr volume 5

\*0000316 tempf 415040000 \* te-139-19

\*0000330 tempf 415030000 \* te-139-20

\*0000331 tempf 315120000 \* te-p138-171

\*0000332 tempf 350020000 \* te-p138-170

\*0000333 tempf 205010000 \* te-1st-1/te-2st-1

0000317 tempf 210010000 \* te-1st-2/te-2st-2

\*0000335 tempf 345010000 \* te-bl-1

\*0000336 tempf 210030000 \* te-1st-14/te-2st-14

\*0000337 tempf 210040000 \* te-3up-2

\*0000338 tempf 245010000 \* te-1up-6

\*0000339 tempf 246010000 \* te-2up-4

\*0000340 tempf 250010000 \* te-1up-3

\*\*\*\*\*

\* densities

\*\*\*\*\*

\* velocities

\*\*\*\*\*

	voidf	100010000	* ilhl nozzle
*0000351	voidf	100010000	* ilhl nozzle
*0000352	velf	100010000	* ilhl nozzle
*0000353	velf	115030000	* s/g inlet
*0000354	velf	400010000	* surge line
*0000355	velj	425000000	* porv liq vel
*0000356	velg	100010000	* ilhl nozzle
*0000357	velg	115030000	* s/g inlet
*0000358	velg	400010000	* surge line
*0000359	velgj	425000000	* porv vap vel

\* mass flow rates

	mflowj	100010000	* ilhl nozzle
0000322	mflowj	100010000	* ilhl nozzle
*0000361	mflowj	150010000	* pump outlet
*0000362	mflowj	185020000	* dtt-rake ilcl
0000323	mflowj	400010000	* pres. surge line flow
0000324	mflowj	407000000	* pqr spray flow
0000325	mflowj	425000000	* pres. relief valve flow
0000326	mflowj	550000000	* steam flow control valve
0000327	mflowj	548000000	* aux feed
*0000369	mflowj	560000000	* main feed

\* cladding temperatures center module

	httemp	230000110	* te-5h5-015
*0000371	httemp	230000210	* te-5h5-034

*0000373	htemp	230000310	* te-5h5-049	0000365	cntrlvar	128					
*****				0000366	cntrlvar	129					
* peak centerline temperatures				0000367	cntrlvar	130					
*****				0000368	cntrlvar	551					
*0000374	htemp	230000101	* core lower region	0000369	cntrlvar	552					
*0000375	htemp	230000201	* core middle region	0000370	cntrlvar	132					
*0000376	htemp	230000301	* core upper region	0000371	cntrlvar	133					
*****				0000372	cntrlvar	170					
* reactor kinetic parameters				0000373	cntrlvar	171					
*****				0000374	cntrlvar	570					
0000328	rktppow	0	* total reactor power	0000375	cntrlvar	573					
*0000378	rkfipow	0	* fission decay power	0000376	cntrlvar	153					
*0000379	rkgapow	0	* gamma decay power	0000377	cntrlvar	154					
*0000380	rkreac	0	* reactivity	0000378	cntrlvar	155					
*0000381	pmphead	135	* pcp1 head	0000379	cntrlvar	156					
*0000382	pmphead	165	* pcp2 head	0000380	cntrlvar	157					
0000329	mflowj	185010000		0000381	cntrlvar	160					
0000330	mflowj	185030000		0000382	cntrlvar	161					
*0000388	mflowj	200020000		0000383	cntrlvar	166					
0000331	pmpvel	135		0000384	cntrlvar	167					
*****				0000385	cntrlvar	620					
* control variable requests				0000386	cntrlvar	621					
*****				0000387	cntrlvar	622					
0000332	cntrlvar	001		0000388	cntrlvar	623					
0000333	cntrlvar	002		0000389	cntrlvar	624					
0000334	cntrlvar	003		0000390	cntrlvar	625					
0000335	cntrlvar	041		0000391	cntrlvar	626					
0000336	cntrlvar	042		0000392	cntrlvar	627					
0000337	cntrlvar	043		0000393	tempg	515070000					
0000338	cntrlvar	004		0000394	rho	420010000					
0000339	cntrlvar	005		0000395	cputime	0					
0000340	cntrlvar	006		20800095	dt	0					
0000341	cntrlvar	007		20800096	dternt	0					
0000342	cntrlvar	008		*****							
0000343	cntrlvar	009		*							
0000344	cntrlvar	010		*							
0000345	cntrlvar	433		*							
0000346	cntrlvar	434		*							
0000347	cntrlvar	111		*****							
0000348	cntrlvar	112		*							
0000349	cntrlvar	113		*							
0000350	cntrlvar	114		0000501	p	100010000	le	null	0	14.193103e6	1
0000351	cntrlvar	115		*							
0000352	cntrlvar	116		0000502	p	600010000	ge	p		185010000	20.e6
0000353	cntrlvar	117		*							
0000354	cntrlvar	118		0000503	p	615010000	ge	p		185010000	20.e6
0000355	cntrlvar	119		*							
0000356	cntrlvar	120		0000504	time	0	lt	null	0	0.0	1
0000357	cntrlvar	121		*							
0000358	cntrlvar	122		0000505	time	0	lt	null	0	0.0	1
0000359	cntrlvar	123		*							
0000360	cntrlvar	251		0000506	time	0	lt	null	0	0.0	1
0000361	cntrlvar	252		*							
0000362	cntrlvar	253		0000507	time	0	lt	null	0	0.0	1
0000363	cntrlvar	126		*							
0000364	cntrlvar	127		0000508	time	0	ge	null	0	0.0	1

\* pressurizer relief valve  
 0000509 tempf 100010000 ge null 0 597.0 1 0000615 -612 and 609 n  
 \* steam control valve  
 0000510 time 0 lt null 0 0.0 1 0000616 615 and 614 n  
 0000511 boundary system valve  
 0000511 time 0 lt null 0 0.0 1 0000617 612 or 616 n  
 0000511 time 0 lt null 0 0.0 1 0000618 605 or 607 n  
 0000511 time 0 lt null 0 0.0 1 0000621 623 or 570 n  
 0000511 time 0 lt null 0 0.0 1 0000622 -571 and -571 n  
 \* lpis trip  
 0000512 time 0 ge null 0 10000.0 1 0000623 621 and 622 n  
 \* hpis trip  
 0000513 time 0 ge null 0 10000.0 1 0000624 509 and -552 n  
 0000513 time 0 ge null 0 10000.0 1 0000625 623 or 624 n  
 0000513 time 0 ge null 0 10000.0 1 0000626 576 and -509 n  
 \* 0000513 time 0 ge null 0 10000.0 1 0000627 -576 and -577 n  
 0000520 p 530020000 gt null 0 7.103448e6 n 0000628 629 and 627 n  
 0000521 p 530020000 lt null 0 7.0344827e6 n 0000629 626 or 628 n  
 0000522 p 530020000 gt null 0 6.3448275e6 n 0000635 504 and 504 n  
 0000523 p 530020000 lt null 0 6.4137931e6 n 0000636 509 and -536 n  
 0000530 time 0 ge null 0 3600.0 n 0000650 -652 and 550 n  
 0000531 p 530020000 gt p 547010000 0.0 n 0000651 650 or 652 n  
 0000536 time 0 ge null 0 10000.0 n 0000652 -509 and 651 n  
 0000540 tempf 100010000 gt null 0 583.16 1 0000655 601 or 603 n  
 0000541 p 100010000 gt null 0 1.574553e7 1 0000656 508 or 609 n  
 0000550 time 0 ge null 0 10000.0 1 0000659 561 or 562 n  
 0000551 time 0 ge timeof 625 0.0 1 0000660 504 or 504 n  
 0000552 time 0 ge timeof 509 1580. 1 0000669 561 and 564 1  
 0000560 p 100010000 le null 0 13.15862e6 n 0000670 565 and -655 n  
 0000561 time 0 ge timeof 552 265.0 1 0000680 530 or 530 n  
 0000562 time 0 gt null 0 5400.0 n 0000688 690 or 574 n  
 0000563 cntrlvar 1 lt null 0 2.1844 n 0000689 -575 and -551 n  
 0000564 cntrlvar 1 gt null 0 2.9464 n 0000690 688 and 689 n  
 0000565 time 0 ge timeof 669 966. 1 \*\*\*\* pqr heater delete  
 0000570 p 420010000 gt null 0 1.620058e7 n 14201000 delete  
 0000571 p 420010000 lt null 0 1.606269e7 n 14202000 delete  
 0000572 p 420010000 lt null 0 1.486300e7 n \*-----1-----1-----1  
 0000573 p 420010000 gt null 0 1.506980e7 n \* control variable 114 re-define  
 0000574 p 420010000 gt null 0 1.533874e7 n \*-----1-----1-----1  
 0000575 p 420010000 lt null 0 1.505000e7 n 20511400 pqrheat sum 1.0 0.0 1  
 0000576 p 420010000 lt null 0 1.482853e7 n 20511401 0.0 0.362 htrnr 415100101  
 0000577 p 420010000 gt null 0 1.495950e7 n 20511402 0.702464 htrnr 415200101  
 \*\*\*\*\*  
 \* logical trips  
 \*\*\*\*\*  
 0000600 536  
 \* modify from 670 in original input  
 0000601 563 and 561 n 20511403 1.26381 htrnr 415200201  
 0000602 -563 and -564 n 20511404 1.26381 htrnr 415200301  
 0000603 655 and 602 n 20511405 0.649152 htrnr 415200401  
 0000604 609 or 609 1 20511406 0.649152 htrnr 415200501  
 0000605 572 and -509 n 20511407 0.534688 htrnr 415200601  
 0000606 -572 and -573 n 20511408 0.534688 htrnr 415200701  
 0000607 608 and 606 n 20511409 0.273063 htrnr 416200101  
 \*-----1-----1-----1  
 0000608 605 or 607 n  
 0000609 540 or 541 1  
 0000610 612 or 520 n  
 0000611 -521 and -616 n  
 0000612 611 and 610 n  
 0000613 616 or 523 n  
 0000614 -522 and 613 n  
 20512300 pqr sum 1.0 0. 1  
 20512301 0.0 0.362 htrnr 415100100  
 20512302 0.59522 htrnr 415200100  
 20512303 1.07086 htrnr 415200200  
 20512304 1.07086 htrnr 415200300  
 20512305 0.550045 htrnr 415200400  
 20512306 0.550045 htrnr 415200500  
 20512307 0.453056 htrnr 415200600  
 20512308 0.453056 htrnr 415200700

20512309	0.150656	htnnr	416200100				1351402	-8.229700e-01	1.996800e+00	
*****							1351403	-6.333200e-01	1.589700e+00	
* primary coolant pump 1							1351404	-4.553400e-01	1.327900e+00	
*****							1351405	-2.710900e-01	1.194900e+00	
1350000	pcpump1	pump					1351406	-1.771600e-01	1.060500e+00	
1350101	0.0366	0.0	0.099	0.0	90.0	0.319	1351407	-9.073000e-02	1.015600e+00	
1350102	00000						1351408	0.000000e+00	9.342790e-01	
1350108	130010000	0.0	0.0	0.0	000100		*****			
1350109	140000000	0.0	0.05	0.05	000100		* head curve no. 5			
1350200	0	14818100.	1242890.	2463900.	0.0	0.0		*****		
1350201	0	8.8943000	9.2942000	0.0			1351500	1	5	
1350202	0	8.8928000	8.1177000	0.0			1351501	0.000000e+00	2.500000e-01	
1350301	0	0	0	-1	0	509	0			
1350302	369.00	.90178860	.31550	96.00	500.60	1.4310	1351503	4.000000e-01	3.400000e-01	
1350303	613.6	0.0	207.0000	0.0040000	19.598000	0.0	1351504	4.118000e-01	2.768000e-01	
1350310	0.0	0.0	0.0				1351505	5.976300e-01	4.584000e-01	
*							1351506	7.934670e-01	6.992000e-01	
*****							1351507	1.000000e+00	1.000000e+00	
* single phase head curves							*****			
*****							* head curve no. 6			
* head curve no. 1							*****			
*****							1351600	1	6	
1351100	1		1				1351601	0.000000e+00	9.342790e-01	
1351101	0.000000e+00		1.403600e+00				1351602	9.109900e-02	9.229000e-01	
1351102	1.906100e-01		1.363600e+00				1351603	1.865090e-01	8.963000e-01	
1351103	3.896300e-01		1.318600e+00				1351604	2.717620e-01	8.750000e-01	
1351104	5.939600e-01		1.232800e+00				1351605	4.558720e-01	8.433000e-01	
1351105	7.902000e-01		1.133600e+00				1351606	5.744060e-01	8.355000e-01	
1351106	1.000000e+00		1.000000e+00				1351607	7.405760e-01	8.466000e-01	
*							1351608	7.666190e-01	8.469000e-01	
* head curve no. 2							1351609	8.714710e-01	8.838000e-01	
*****							1351610	1.000000e+00	1.000000e+00	
1351200	1		2				*****			
1351201	0.000000e+00		-6.700000e-01				* head curve no. 7			
1351202	2.000000e-01		-5.000000e-01				*****			
1351203	4.000000e-01		-2.500000e-01				1351700	1	7	
1351204	5.755400e-01		0.000000e+00				1351701	-1.000000e-00	-1.000000e+00	
1351205	7.443200e-01		2.583000e-01				1351702	-8.000000e-01	-6.300000e-01	
1351206	7.734800e-01		3.778000e-01				1351703	-6.000000e-01	-3.000000e-01	
1351207	8.631300e-01		6.326000e-01				1351704	-4.000000e-01	-5.000000e-02	
1351208	1.000000e+00		1.000000e+00				1351705	-2.000000e-01	1.500000e-01	
*							1351706	0.000000e+00	2.500000e-01	
* head curve no. 3							*****			
*****							* head curve no. 8			
1351300	1		3				1351800	1	8	
1351301	-1.000000e+00		2.472200e+00				1351801	-1.000000e+00	-1.000000e+00	
1351302	-8.057400e-01		2.047400e+00				1351802	-8.000000e-01	-9.700000e-01	
1351303	-6.069000e-01		1.831000e+00				1351803	-6.000000e-01	-9.500000e-01	
1351304	-4.068300e-01		1.624000e+00				1351804	-4.000000e-01	-8.800000e-01	
1351305	-2.001710e-01		1.470500e+00				1351805	-2.000000e-01	-8.000000e-01	
1351306	0.000000e+00		1.403600e+00				1351806	0.000000e+00	-6.700000e-01	
*							*****			
* head curve no. 4							* single phase torque data			
*****							*****			
1351400	1		4				* torque curve no. 1			
1351401	-1.000000e+00		2.472200e+00							

1351900	2	1						
1351901	0.000000e+00	6.032000e-01						
1351902	1.930000e-01	6.325000e-01						
1351903	3.930000e-01	7.369000e-01						
1351904	5.955200e-01	8.331000e-01						
1351905	7.978200e-01	9.229000e-01						
1351906	1.000000e+00	1.000000e+00						
* torque curve no. 2								
1352000	2	2						
1352001	0.000000e+00	-6.700000e-01						
1352002	4.000000e-01	-2.500000e-01						
1352003	5.000000e-01	1.500000e-01						
1352004	7.372550e-01	5.265860e-01						
1352005	7.680490e-01	6.065940e-01						
1352006	8.672300e-01	7.436600e-01						
1352007	1.000000e+00	1.000000e+00						
* torque curve no. 3								
1352100	2	3						
1352101	-1.000000e+00	1.984300e+00						
1352102	-8.009600e-01	1.394000e+00						
1352103	-6.063800e-01	1.097500e+00						
1352104	-4.068600e-01	8.220000e-01						
1352105	-1.992800e-01	6.648000e-01						
1352106	0.000000e+00	6.032000e-01						
* torque curve no. 4								
1352200	2	4						
1352201	-1.000000e+00	1.984300e+00						
1352202	-8.223400e-01	1.830800e+00						
1352203	-6.337100e-01	1.682400e+00						
1352204	-4.585300e-01	1.557000e+00						
1352205	-2.670230e-01	1.436200e+00						
1352206	-1.761070e-01	1.387900e+00						
1352207	-8.931000e-02	1.348100e+00						
1352208	0.000000e+00	1.233610e+00						
* torque curve no. 5								
1352300	2	5						
1352301	0.000000e+00	-4.500000e-01						
1352302	4.000000e-01	-2.500000e-01						
1352303	5.000000e-01	0.000000e+00						
1352304	1.000000e+00	3.569000e-01						
* torque curve no. 6								
1352400	2	6						
1352401	0.000000e+00	1.233610e+00						
1352402	9.064300e-02	1.196500e+00						
1352403	1.885690e-01	1.109600e+00						
1352404	2.734700e-01	1.041600e+00						
1352405	4.586690e-01	8.958000e-01						
1352406	5.744800e-01	7.807000e-01						
1352407	7.381600e-01	6.134000e-01						
1352408	7.685200e-01	5.849000e-01						
1352409	8.700570e-01	4.877000e-01						
1352410	1.000000e+00	3.569000e-01						
* torque curve no. 7								
1352500	2	7						
1352501	-1.000000e+00	-1.000000e+00						
1352502	-3.000000e-01	-9.000000e-01						
1352503	-1.000000e-01	-5.000000e-01						
1352504	0.000000e+00	-4.500000e-01						
* torque curve no. 8								
1352600	2	8						
1352601	-1.000000e+00	-1.000000e+00						
1352602	-2.500000e-01	-9.000000e-01						
1352603	-8.000000e-02	-8.000000e-01						
1352604	0.000000e+00	-6.700000e-01						
***** two - phase multiplier data from 19-1 test data *****								
***** head curve *****								
1353000	0							
1353001	0.000000e+00	0.000000e+00						
1353002	2.000000e-02	2.000000e-02						
1353003	6.000000e-02	5.000000e-02						
1353004	1.000000e-01	1.000000e-01						
1353005	2.000000e-01	4.600000e-01						
1353006	2.400000e-01	8.000000e-01						
1353007	3.000000e-01	9.600000e-01						
1353008	4.000000e-01	9.800000e-01						
1353009	6.000000e-01	9.700000e-01						
1353010	8.000000e-01	9.000000e-01						
1353011	9.000000e-01	8.000000e-01						
1353012	9.600000e-01	5.000000e-01						
1353013	1.000000e+00	0.000000e+00						
* torque curve								
1353100	0							
1353101	0.000000e+00	0.000000e+00						
1353102	1.250000e-01	7.000000e-02						
1353103	1.650000e-01	1.250000e-01						
1353104	2.400000e-01	5.600000e-01						
1353105	8.000000e-01	5.600000e-01						
1353106	9.600000e-01	4.500000e-01						
1353107	1.000000e+00	0.000000e+00						
***** pump 2-phase difference data *****								

```

* head curve no. 1
*-----|-----|-----|-----|-----|-----|
1354100 1 1
1354101 0.000000e+00 0.000000e+00
1354102 1.000000e-01 8.300000e-01
1354103 2.000000e-01 1.090000e+00
1354104 5.000000e-01 1.020000e+00
1354105 7.000000e-01 1.010000e+00
1354106 9.000000e-01 9.400000e-01
1354107 1.000000e+00 1.000000e+00
*-----|-----|-----|-----|-----|-----|
* head curve no. 2
*-----|-----|-----|-----|-----|-----|
1354200 1 2
1354201 0.000000e+00 0.000000e+00
1354202 1.000000e-01 -4.000000e-02
1354203 2.000000e-01 0.000000e+00
1354204 3.000000e-01 1.000000e-01
1354205 4.000000e-01 2.100000e-01
1354206 8.000000e-01 6.700000e-01
1354207 9.000000e-01 8.000000e-01
1354208 1.000000e+00 1.000000e+00
*-----|-----|-----|-----|-----|-----|
* head curve no. 3
*-----|-----|-----|-----|-----|-----|
1354300 1 3
1354301 -1.000000e+00 -1.160000e+00
1354302 -9.000000e-01 -1.240000e+00
1354303 -8.000000e-01 -1.770000e+00
1354304 -7.000000e-01 -2.360000e+00
1354305 -6.000000e-01 -2.790000e+00
1354306 -5.000000e-01 -2.910000e+00
1354307 -4.000000e-01 -2.670000e+00
1354308 -2.500000e-01 -1.690000e+00
1354309 -1.000000e-01 -5.000000e-01
1354310 0.000000e+00 0.000000e+00
*-----|-----|-----|-----|-----|-----|
* head curve no. 4
*-----|-----|-----|-----|-----|-----|
1354400 1 4
1354401 -1.000000e+00 -1.160000e+00
1354402 -9.000000e-01 -7.800000e-01
1354403 -8.000000e-01 -5.000000e-01
1354404 -7.000000e-01 -3.100000e-01
1354405 -6.000000e-01 -1.700000e-01
1354406 -5.000000e-01 -8.000000e-02
1354407 -3.500000e-01 0.000000e+00
1354408 -2.000000e-01 5.000000e-02
1354409 -1.000000e-01 8.000000e-02
1354410 0.000000e+00 1.100000e-01
*-----|-----|-----|-----|-----|-----|
* head curve no. 5
*-----|-----|-----|-----|-----|-----|
1354500 1 5
1354501 0.000000e+00 0.000000e+00
1354502 2.000000e-01 -3.400000e-01
1354503 4.000000e-01 -6.500000e-01
1354504 6.000000e-01 -9.300000e-01
1354505 8.000000e-01 -1.190000e+00
1354506 1.000000e+00 -1.470000e+00
*-----|-----|-----|-----|-----|-----|
* head curve no. 6
*-----|-----|-----|-----|-----|-----|
1354600 1 6
1354601 0.000000e+00 1.100000e-01
1354602 1.000000e-01 1.300000e-01
1354603 2.500000e-01 1.500000e-01
1354604 4.000000e-01 1.300000e-01
1354605 5.000000e-01 7.000000e-02
1354606 6.000000e-01 -4.000000e-02
1354607 7.000000e-01 -2.300000e-01
1354608 8.000000e-01 -5.100000e-01
1354609 9.000000e-01 -9.100000e-01
1354610 1.000000e+00 -1.470000e+00
*-----|-----|-----|-----|-----|-----|
* head curve no. 7
*-----|-----|-----|-----|-----|-----|
1354700 1 7
1354701 -1.000000e+00 0.000000e+00
1354702 0.000000e+00 0.000000e+00
*-----|-----|-----|-----|-----|-----|
* head curve no. 8
*-----|-----|-----|-----|-----|-----|
1354800 1 8
1354801 -1.000000e+00 0.000000e+00
1354802 0.000000e+00 0.000000e+00
*-----|-----|-----|-----|-----|-----|
* torque curve no. 1
*-----|-----|-----|-----|-----|-----|
1354900 2 1
1354901 0.000000e+00 6.032000e-01
1354902 1.930000e-01 6.325000e-01
1354903 3.930000e-01 7.369000e-01
1354904 5.955200e-01 8.331000e-01
1354905 7.978200e-01 9.229000e-01
1354906 1.000000e+00 1.000000e+00
*-----|-----|-----|-----|-----|-----|
* torque curve no. 2
*-----|-----|-----|-----|-----|-----|
1355000 2 2
1355001 0.000000e+00 -6.700000e-01
1355002 4.000000e-01 -2.500000e-01
1355003 5.000000e-01 1.500000e-01
1355004 7.372550e-01 5.265860e-01
1355005 7.680490e-01 6.065940e-01
1355006 8.672300e-01 7.436600e-01
1355007 1.000000e+00 1.000000e+00
*-----|-----|-----|-----|-----|-----|
* torque curve no. 3
*-----|-----|-----|-----|-----|-----|
1355100 2 3
1355101 -1.000000e+00 1.984300e+00

```

1355102	-8.009600e-01	1.394000e+00
1355103	-6.063800e-01	1.097500e+00
1355104	-4.068600e-01	8.220000e-01
1355105	-1.992800e-01	6.648000e-01
1355106	0.000000e+00	6.032000e-01
*****		
* torque curve no. 4		
*****		
1355200	2	4
1355201	-1.000000e+00	1.984300e+00
1355202	-8.223400e-01	1.830800e+00
1355203	-6.337100e-01	1.682400e+00
1355204	-4.585300e-01	1.557000e+00
1355205	-2.670230e-01	1.436200e+00
1355206	-1.761070e-01	1.387900e+00
1355207	-8.931000e-02	1.348100e+00
1355208	0.000000e+00	1.233610e+00
*****		
* torque curve no. 5		
*****		
1355300	2	5
1355301	0.000000e+00	-4.500000e-01
1355302	4.000000e-01	-2.500000e-01
1355303	5.000000e-01	0.000000e+00
1355304	1.000000e+00	3.569000e-01
*****		
* torque curve no. 6		
*****		
1355400	2	6
1355401	0.000000e+00	1.233610e+00
1355402	9.064300e-02	1.196500e+00
1355403	1.885690e-01	1.109600e+00
1355404	2.734700e-01	1.041600e+00
1355405	4.586690e-01	8.958000e-01
1355406	5.744800e-01	7.807000e-01
1355407	7.381600e-01	6.134000e-01
1355408	7.685200e-01	5.849000e-01
1355409	8.700570e-01	4.877000e-01
1355410	1.000000e+00	3.569000e-01
*****		
* torque curve no. 7		
*****		
1355500	2	7
1355501	-1.000000e+00	-1.000000e+00
1355502	-3.000000e-01	-9.000000e-01
1355503	-1.000000e-01	-5.000000e-01
1355504	0.000000e+00	-4.500000e-01
*****		
* torque curve no. 8		
*****		
1355600	2	8
1355601	-1.000000e+00	-1.000600e+00
1355602	-2.500000e-01	-9.000000e-01
1355603	-8.000000e-02	-8.000000e-01
1355604	0.000000e+00	-6.700000e-01
*****		

* pcp1 pump velocity table							
*****							
1356100	536						
1356101	0.0	0.0					
1356102	1.0	220.					
*****							
* primary coolant pump 2							
*****							
1650000	pepump2	pump					
1650101	0.0366	0.0	0.099	0.0	90.0	0.319	
1650102	00000						
1650108	160010000	0.0	0.0	0.0	000100		
1650109	170000000	0.0	0.1	0.1	000100		
1650200	0	14832700.	1242890.	2463590.0	0.0		
1650201	0	8.4974000	8.8872000	0.0			
1650202	0	8.4959000	6.6507000	0.0			
1650301	135	135	135	-1	135	509	0
1650302	369.0	.89699187	.31550	96.000	500.60000	1.431	
1650303	613.6	0.0	207.433	0.004	19.5980	0.0	
1650310	0.0	0.0	0.0				
*****							
* spray valve							
*****							
4070000	sprvly	valve					
4070101	406010000	420010000	3.3451e-4	15.432	15.432		
000100							
4070201	0	.000000	.000000	0.0			
4070300	trpvly						
4070301	690						
*****							
* air cooled condenser							
*****							
5470000	conders	tmdpvol					
5470101	0.21677	17.67	0.0	0.0	0.0	0.0	
5470102	4.e-5	0.0	00000				
5470200	1	680					
5470201	0.0	559.15	0.999				
5470202	18000.	334.15	0.999				
*****							
* aux feed water							
*****							
5480000	auxfeed	tmdpjun					
5480101	553000000	510000000	0.10				
5480200	1	655					
5480201	-1.0	0.0	0.0	0.0			
5480202	0.0	0.0	0.0	0.0			
5480203	0.0	2.5207	0.0	0.0			
*****							
* steam flow control valve							
*****							
*5500000	cv-p4-1	valve					
*5500101	530010000	535000000	0.0043266	0.0	0.0	000100	
*5500201	0	18.276	20.246	0.0			
* initial velocity modified from 21.268, 21.599 in original one							
*5500300 mtrvly							

\*5500301 612 616 0.05 0.7279808 550 \* doppler reactivity table  
 \* initial valve position modified from 0.67 in original one \*\*\*\*  
 \* main feed water valve  
 \* mnfeed tmdpjun  
 5600000 5600101 545000000 510000000 0.05 30000601 293.16 1.375  
 5600200 1 656 30000602 338.72 1.125  
 5600201 0.0 26.533 26.533 0.0 30000603 422.05 0.682  
 5600202 0.0 0.0 0.0 0.0 30000604 477.60 0.419  
 \*\*\*\*\* 30000605 505.38 0.274  
 \* core collapsed liquid level 30000606 570.72 0.000  
 \*\*\*\*\* 30000607 588.72 -0.075  
 \*20255000 normarea 0 1.0 1.0 30000608 695.83 -0.526  
 \*20255001 0.0 9.25e-3 30000609 922.05 -1.386  
 \*20255002 9.25e-3 9.25e-3 30000610 1310.94 -2.543  
 \*20255003 1.0 1.0 30000611 1810.94 -3.865  
 \*\*\*\*\* 30000612 2088.72 -4.502  
 \* volume weighting factors 30000613 2499.83 -5.392  
 \* moderator temperature feedback 30000614 3027.60 -6.417  
 \*\*\*\*\*  
 \* reactor kinetics data  
 \*  
 30000000 point separabl 30000701 230010000 0 0.31493 0.0  
 30000001 gamma-ac 49.6e+6 0.0 348.43 1.0 0.556 30000702 230020000 0 0.31493 0.0  
 30000002 ans79-1 30000703 230030000 0 0.37014 0.0  
 \* delayed neutron constants 30000801 2300001 0 0.43153 0.0  
 30000101 0.0349 0.01275 30000802 2300002 0 0.51686 0.0  
 30000102 0.2035 0.03177 30000803 2300003 0 0.05161 0.0  
 30000103 0.1848 0.1181  
 30000104 0.4046 0.3160  
 30000105 0.1401 1.402  
 30000106 0.0321 3.914  
 \*\*\*\*\*  
 \* power history  
 \*  
 30000401 4.89e+7 70. hr 20260900 \*react \* 609  
 \*\*\*\*\*  
 \* reactivity curve numbers 20260901 0.0 0.0  
 30000011 609 20260902 0.5 -0.5  
 \* moderator density reactivity table 20260903 0.59 -3.13  
 \*\*\*\*\* 20260904 0.65 -3.95  
 30000501 0.62626e+3 -4.4769 20260905 0.75 -6.27  
 30000502 0.66396e+3 -3.2923 20260906 0.83 -8.72  
 30000503 0.71617e+3 -1.5692 20260907 0.90 -12.00  
 30000504 0.76112e+3 -0.1692 20260908 0.97 -17.12  
 30000505 0.76837e+3 0.04615 20260909 1.125 -20.67  
 30000506 0.79157e+3 0.6923 20260910 1.213 -22.10  
 30000507 0.81188e+3 1.2398 20260911 1.3 -22.78  
 30000508 0.86263e+3 2.2415 20260912 1.4 -23.17  
 30000509 0.93804e+3 3.9231 20260913 1.6 -23.32  
 30000510 0.99749e+3 5.1077 20260914 60.0 -23.32  
 \*\*\*\*

BIBLIOGRAPHIC DATA SHEET

*(See instructions on the reverse)*

2. TITLE AND SUBTITLE

Assessment of RELAP5/MOD3 with the LOFT L9-1/L3-3 Experiment  
Simulating an Anticipated Transient with Multiple Failures

5. AUTHOR(S)

Young Seok Bang, Kwang Won Seul and Hho Jung Kim

1. REPORT NUMBER  
(Assigned by NRC, Add Vol., Supp., Rev.,  
and Addendum Numbers, if any.)

NUREG/IA-0114

ICAP00196

3. DATE REPORT PUBLISHED

MONTH YEAR

February 1994

4. FIN OR GRANT NUMBER

L2245

6. TYPE OF REPORT

Technical Report

7. PERIOD COVERED (inclusive Dates)

8. PERFORMING ORGANIZATION – NAME AND ADDRESS (If NRC, provide Division, Office or Region, U.S. Nuclear Regulatory Commission, and mailing address; if contractor, provide name and mailing address.)

Korea Institute of Nuclear Safety

P.O. Box 16, Daeduk-Danji, Daejon, Korea 305-353

9. SPONSORING ORGANIZATION – NAME AND ADDRESS (If NRC, type "Same as above"; if contractor, provide NRC Division, Office or Region, U.S. Nuclear Regulatory Commission, and mailing address.)

Office of Nuclear Regulatory Research  
U.S. Nuclear Regulatory Commission  
Washington, D.C. 20555

10. SUPPLEMENTARY NOTES

11. ABSTRACT (200 words or less)

The RELAP5/MOD3 5m5 code was assessed using the L9-1/L3-3 test carried out in the LOFT facility, a 1/60-scaled experimental reactor, simulating a loss of feedwater accident with multiple failures and the sequentially-induced small break loss-of-coolant accident. The code predictability was evaluated for the four separated sub-periods with respect to the system response; initial heatup phase, spray and PORV cycling phase, blowdown phase and recovery phase. Based on the comparisons of the results from the calculation with the experiment data, it is shown that the overall thermal-hydraulic behavior important to the scenario such as a heat removal between the primary side and the secondary side and a system depressurization was well-predicted and that the code could be applied to the full-scale nuclear power plant for an anticipated transient with multiple failures within a reasonable accuracy. The minor discrepancies between the prediction and the experiment were identified in reactor scram time, post-scram behavior in the initial heatup phase, excessive heatup rate in the cycling phase, insufficient energy convected out the PORV under the hot leg stratified condition in the saturated blowdown phase and void distribution in secondary side in the recovery phase. This may come from the code uncertainties in predicting the spray mass flow rate, the associated condensation in pressurizer and junction fluid density under stratified condition.

12. KEY WORDS/DESCRIPTORS (List words or phrases that will assist researchers in locating the report.)

ICAP Program  
RELAPS/MOD3  
Anticipated Transient Loft

13. AVAILABILITY STATEMENT

Unlimited

14. SECURITY CLASSIFICATION

*(This Page)*

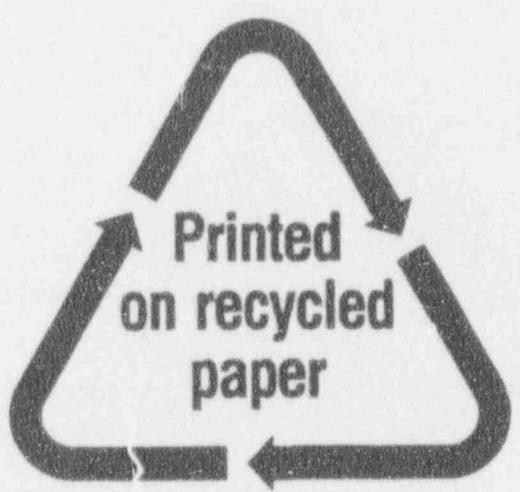
Unclassified

*(This Report)*

Unclassified

15. NUMBER OF PAGES

16. PRICE



Federal Recycling Program

UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D.C. 20555-0001

OFFICIAL BUSINESS  
PENALTY FOR PRIVATE USE, \$300

SPECIAL FOURTH-CLASS RATE  
POSTAGE AND FEES PAID  
USNRC  
PERMIT NO. G-67

120555139531 1 JAN 1 CI  
US NRC-GADM  
CIV FOIA & PUBLICATIONS SVCS  
TPS-POP-NUREG  
P-211  
WASHINGTON DC 20555