



UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

APR 16 1982

MEMORANDUM FOR: Thomas A. Ippolito, Chief  
Operating Reactors Assessment Branch  
Division of Licensing

FROM: Keith R. Wichman, Section Leader  
Engineering Section  
Operating Reactors Assessment Branch  
Division of Licensing

SUBJECT: MEETING WITH COMBUSTION ENGINEERING ON STEAM  
GENERATORS

Attached is a summary of the subject meeting that was held on March 18, 1982, in Bethesda. Combustion Engineering presented their views with respect to steam generator tube degradation and steam generator tube rupture accident management. A list of attendees is shown in Enclosure 1 to the summary.

A handwritten signature in cursive script that reads "Keith R. Wichman".

Keith R. Wichman, Section Leader  
Engineering Section  
Operating Reactors Assessment Branch  
Division of Licensing

Attachment:  
As Stated

A large handwritten number "8205100084" is written inside a large, hand-drawn oval. Below the oval, the letters "XA" are written, with a large, bold "X" over the "A".

ATTENDANCE LIST

COMBUSTION ENGINEERING - STEAM GENERATOR MEETING

MARCH 18, 1982

NRC Participants

D. Eisenhut, DL  
G. Lainas, DL  
C. McCracken, DE  
T. Speis, DSI  
E. Sullivan, DE  
R. Vollmer, DE  
P. Norian, DST  
K. Wichman, DL  
R. Martin, DL  
R. Clark, DL  
W. Kennedy, DHFS  
T. Ippolito, DL  
B. Shearon, DSI

Combustion Engineering Participants

G. Bischoff  
V. Callaghan  
H. Williams  
E. Kennedy

Utility Participant

B. Lawson, AP&L

SUMMARY OF MARCH 18, 1982 MEETING WITH  
COMBUSTION ENGINEERING REGARDING STEAM GENERATORS

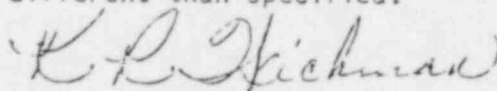
On Thursday, March 18, 1982, representatives of Combustion Engineering (CE) met with members of the NRC staff to present their views with respect to steam generator tube degradation and steam generator tube rupture (SGTR) accident management. A copy of the slides used by CE during the presentation and the attendance list are enclosed.

CE described the steam generator configurations and significant differences between their three models of steam generators, i.e., 2570 Mwt, 3410 Mwt, and System 80 (3817 Mwt). Eight units are currently operating with 2570 Mwt class steam generators and San Onofre Unit 2 which recently received a low power license, has 3410 Mwt class steam generators. There are no operating plants with System 80 steam generators. All CE steam generators have full depth tube expansion in the tubesheet and full or partial eggcrate tube supports; however, the 2570 Mwt class also has two partial drilled support plates where denting has occurred in two plants. In the bend region, batwing spacer assemblies in contact with the tubes in the 2570 Mwt class, have evolved into "V" spacer assemblies with no U-bend contact for the other models of CE steam generators. The System 80 steam generators, in a major design change, incorporate an integral economizer (preheater) section. Ninety percent of feedwater flow is through the two main feedwater nozzles. Feedwater flow is directed down the shroud and does not impinge (e.g. no cross flow) on the steam generator tubes.

CE outlined the steam generator tube degradation experienced to date. Five tube leaks have occurred, four in one plant of which three took place in 1973. The tubes plugged in eight operating units due to inservice degradation is 5476 in a total of 129,131 tubes. The number of preventatively plugged tubes is 576. Generally, 40% tubewall degradation is allowed before plugging. CE stated that some loose parts have been found in certain steam generators in the past, but that CE has issued no specific advisories to their clients concerning loose parts. Four of the eight operating units with CE steam generators have loose parts monitoring systems with offline capability.

An overview of the CE operator guidelines (C-EOG) strategy to mitigate steam generator tube ruptures (SGTR) was presented and major differences between actions taken at Ginna and C-EOG SGTR specified actions were delineated. It was stated that CE guidelines and equipment may have

reduced challenges to steam generator safety valves, but that the Ginna plant response was not significantly different from that of a CE plant. CE emphasized that C-EOG guidance is generic and that utilities may choose to implement it in a manner different than specified.



Keith R. Wichman  
Operating Reactors Assessment Branch  
Division of Licensing

Enclosures:  
As Stated

cc w/enclosures:  
See next page

MEETING WITH NRC STAFF

MARCH 18, 1982

AGENDA

- I. EVOLUTION OF CE STEAM GENERATOR DESIGNS
- II. STEAM GENERATOR LEAKAGE AND PLUGGING EXPERIENCE
- III. STEAM GENERATOR CHEMISTRY RECOMMENDATIONS
- IV. CE EMERGENCY OPERATOR PROCEDURE GUIDELINES FOR STEAM GENERATOR  
TUBE RUPTURE EVENTS

C-E STEAM GENERATORS

2570 MWT CLASS

NUMBER OF TUBES: 8519

TUBE SIZE: 0.750" O.D. X 0.048" WALL

TUBE PITCH: TRIANGULAR PITCH, 1" CENTERS

TUBE SUPPORTS: SIX FULL DISK EGGCRATES  
TWO PARTIAL EGGCRATES  
TWO PARTIAL DRILLED SUPPORT PLATES  
BEND REGION - BATWING SPACER ASSEMBLIES  
WITH INTERLOCKING HORIZONTAL  
STRIPS.

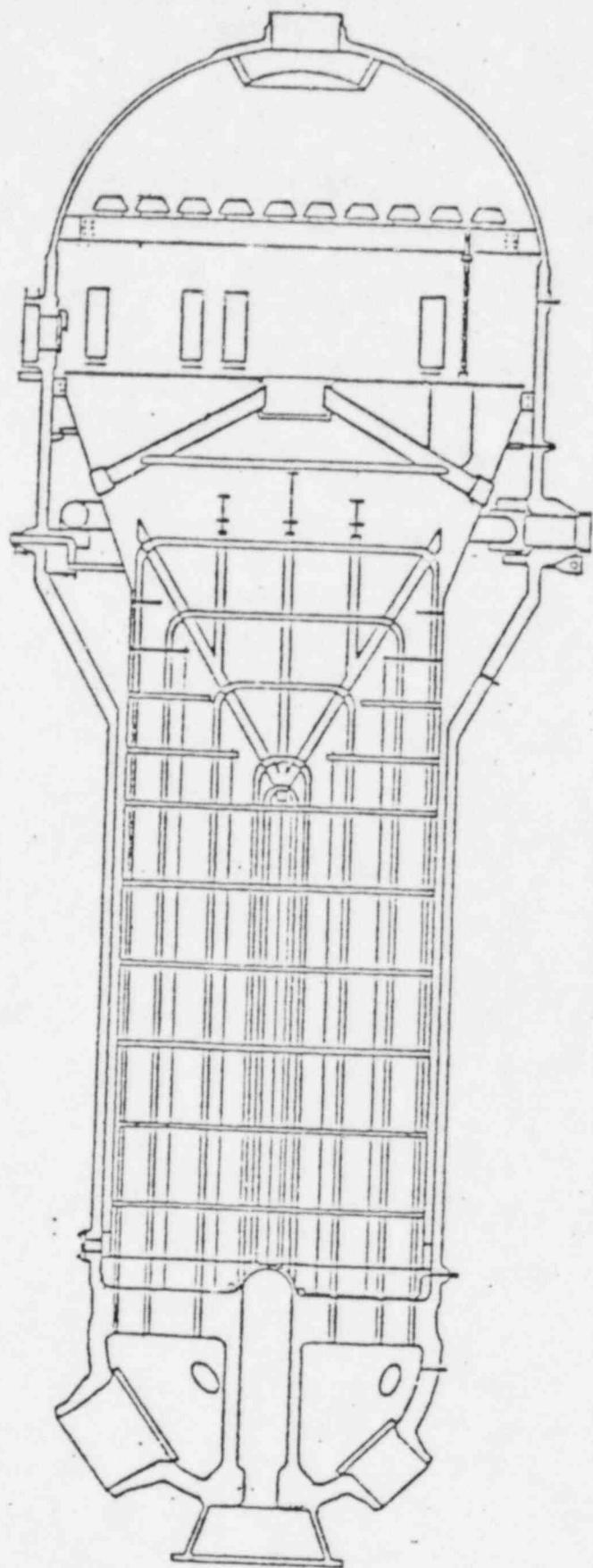
BLOWDOWN ARRANGEMENT: 2" DIAMETER PIPE IN DIVIDER LANE

TUBE TO TUBESHEET JOINT:

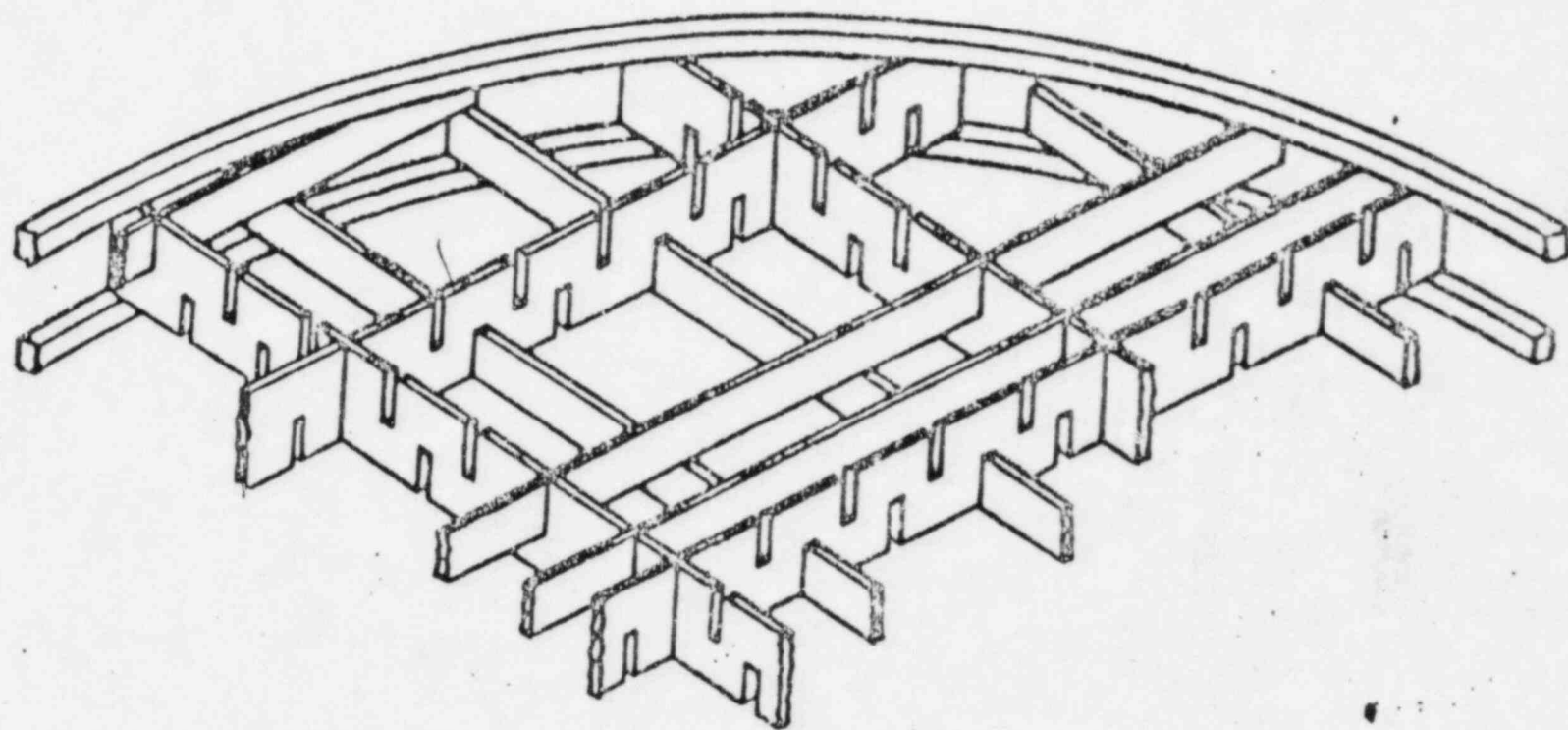
FULL DEPTH EXPANSION (EXPLANSION)  
EDGE WELDED TUBE TO TUBESHEET WELD

NOMINAL OPERATING PARAMETERS:

PRIMARY PRESSURE - 2250 PSIA  
SECONDARY PRESSURE - 815 - 850 PSIA  
PRIMARY TH - 604°F  
PRIMARY TC - 550°F

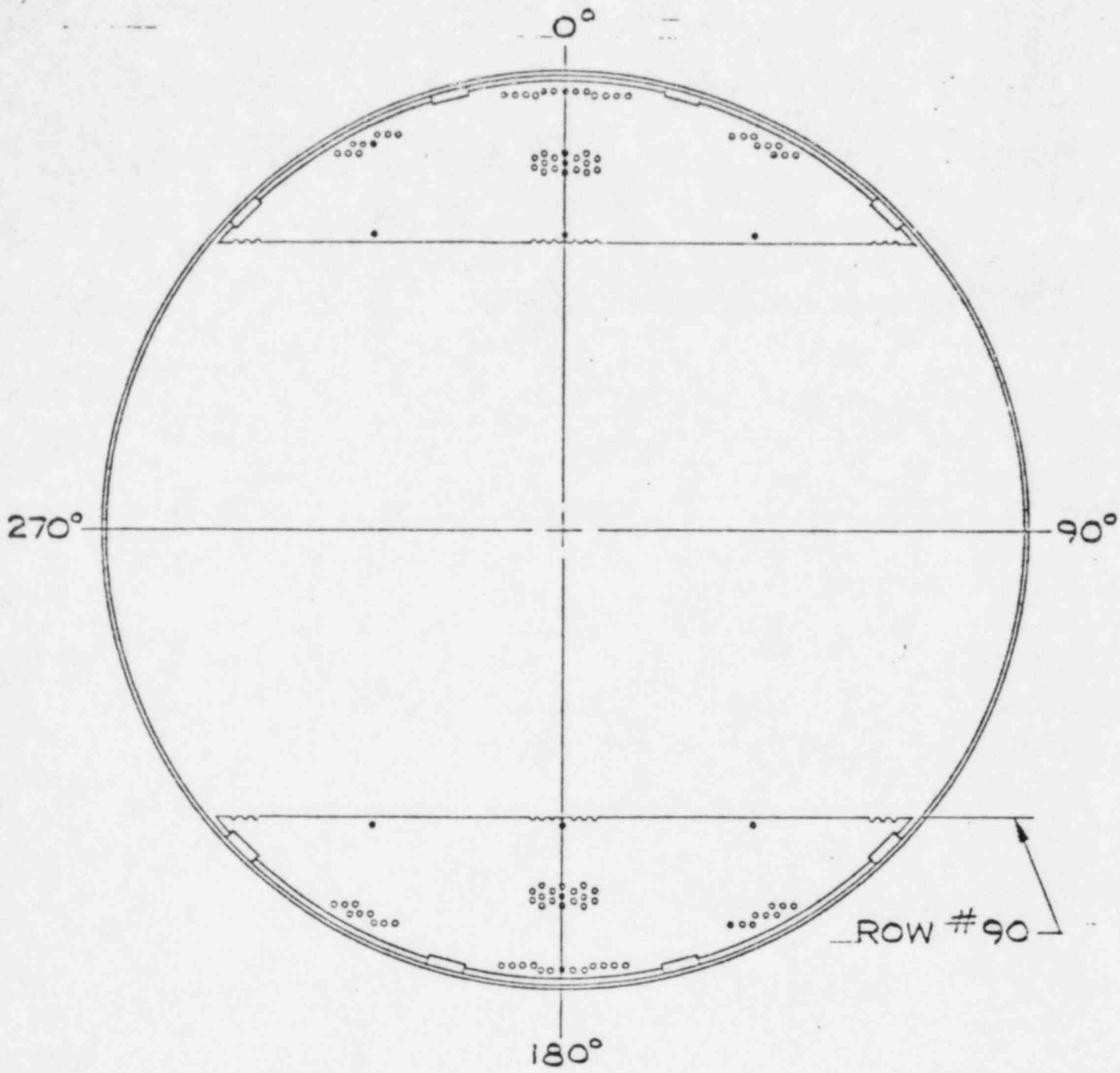


Open Flow Area - 69%  
Flow-Through Design  
Line Contact with Tubes



HORIZONTAL GRID  
"EGGCRATE"  
TUBE SUPPORT

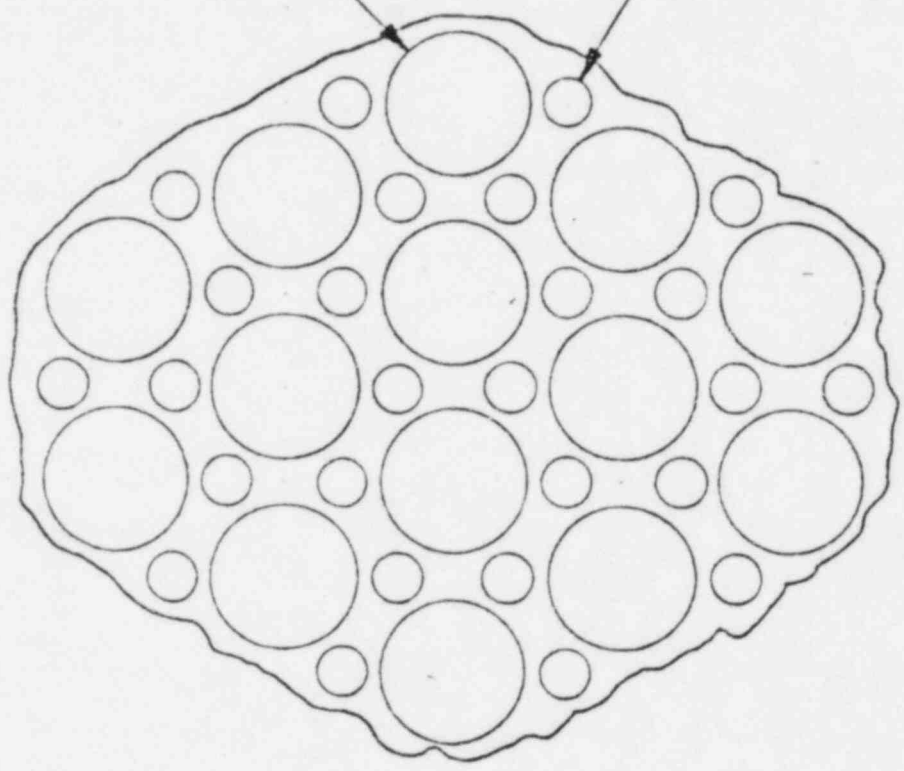




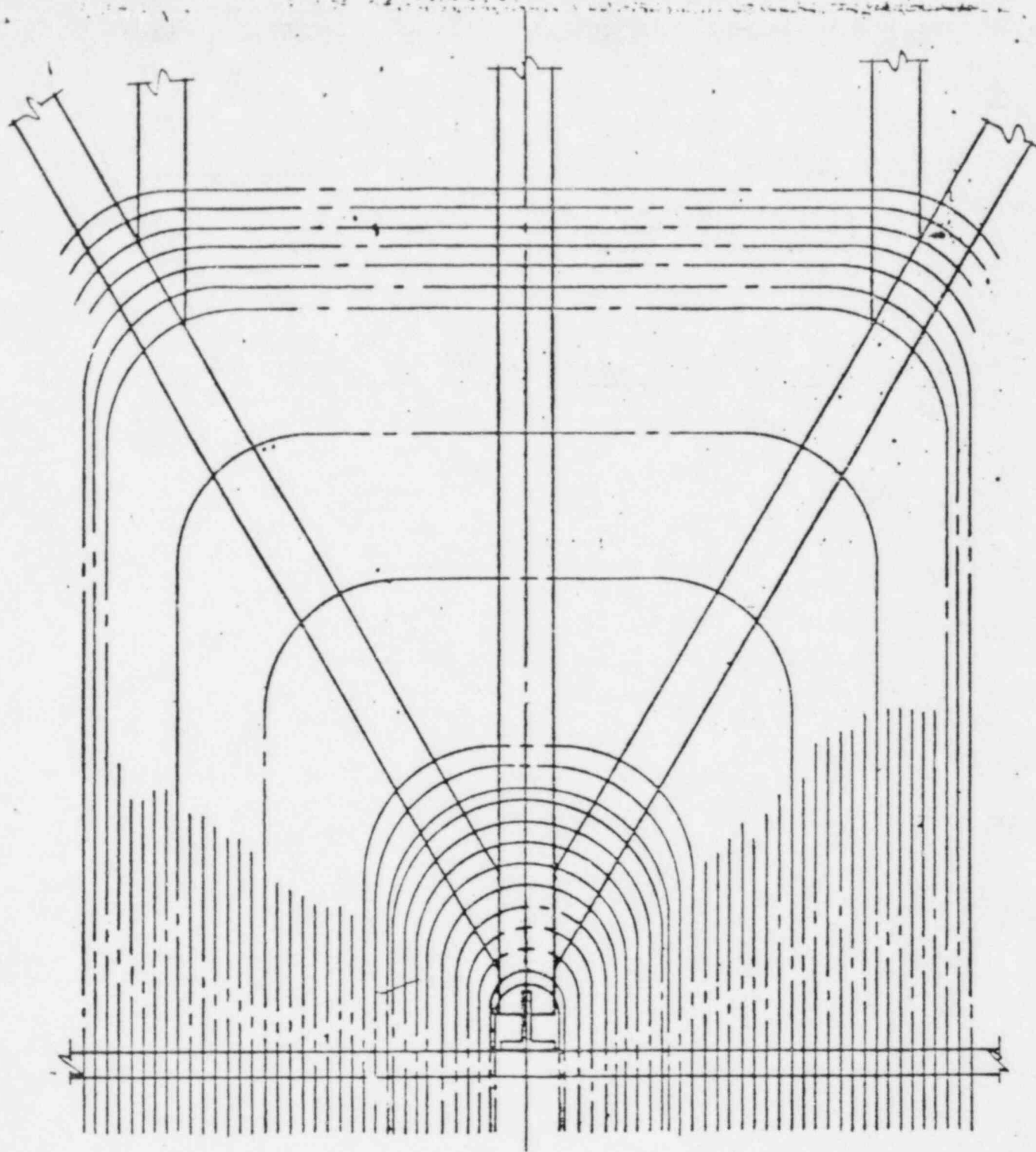
ROW #90

$.765'' + .015''$   
 $-.000$  DIA  
TUBE HOLE

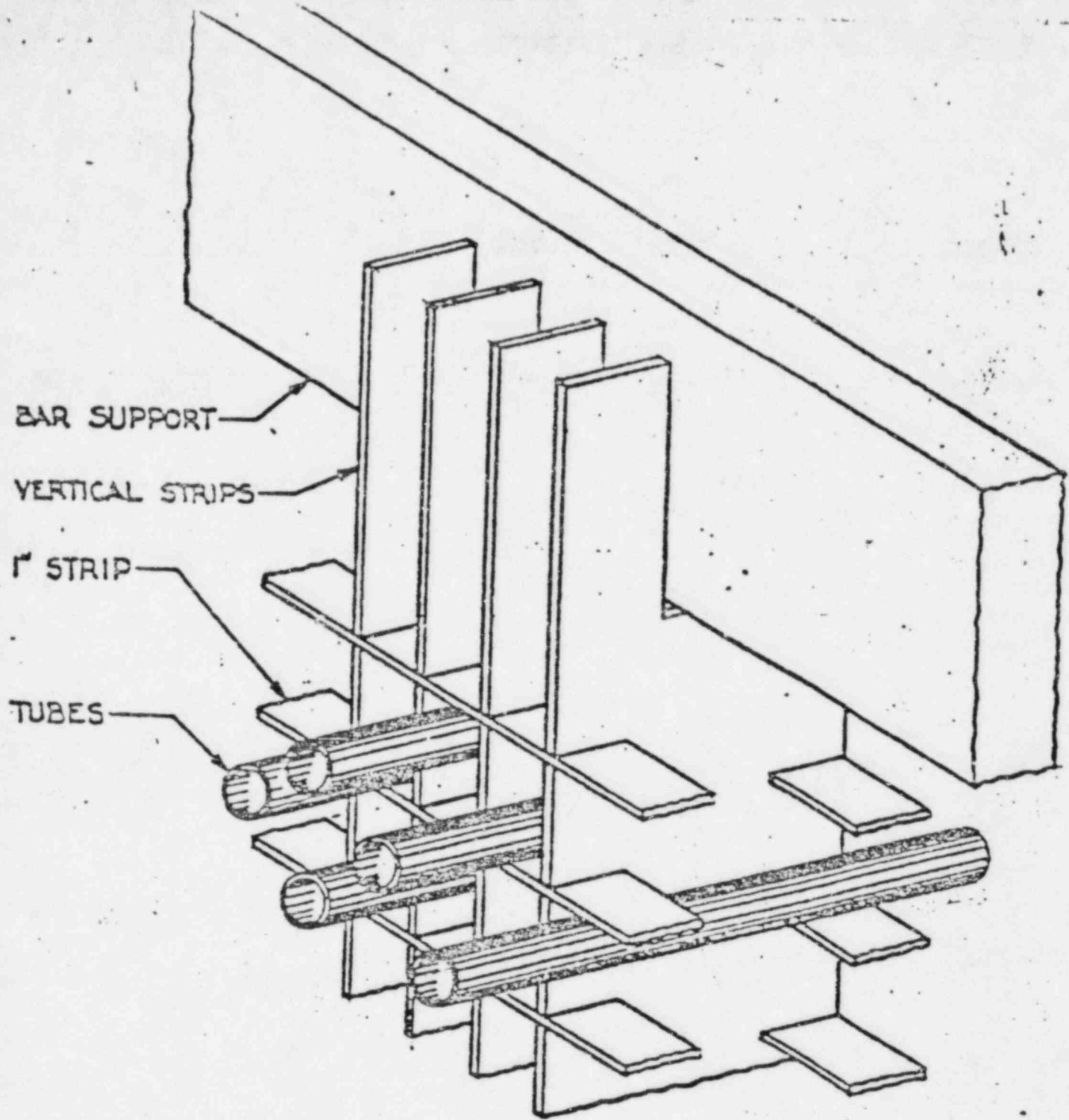
$\frac{1}{4}''$  DIA FLOW HOLE



TYPICAL TUBE SUPPORT  
PLATE PATTERN



ORIGINAL TUBE BUNDLE



TUBE SUPPORT

C-E STEAM GENERATORS

3410 MWT CLASS

NUMBER OF TUBES: 9350

TUBE SIZE: 0.750" O.D. X 0.048" WALL

TUBE PITCH: TRIANGULAR PITCH, 1" CENTERS

TUBE SUPPORTS: SEVEN FULL DISK EGGCRATES  
FOUR PARTIAL EGGCRATES  
BEND REGION - "V" SPACER ASSEMBLIES INTER-  
SECTING TUBES IN VERTICAL  
RUN BELOW BENT TANGENT POINT.

VERTICAL SPACER ASSEMBLIES  
(VENTILATED) WITH INTERLOCKING  
HORIZONTAL STRIPS.

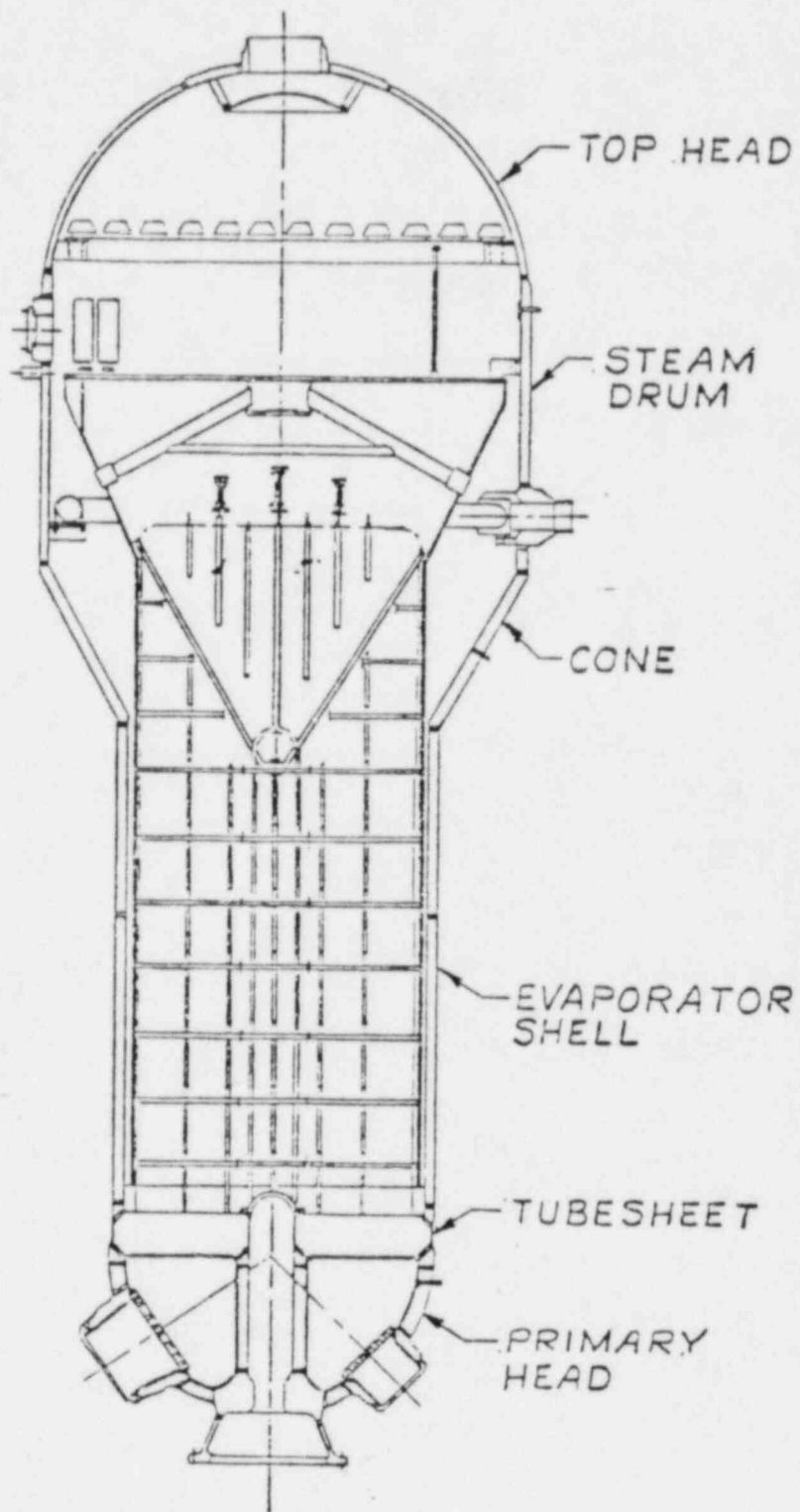
BLOWDOWN ARRANGEMENT: 2" DIAMETER PIPE IN DIVIDER LANE

TUBE TO TUBESHEET JOINT:

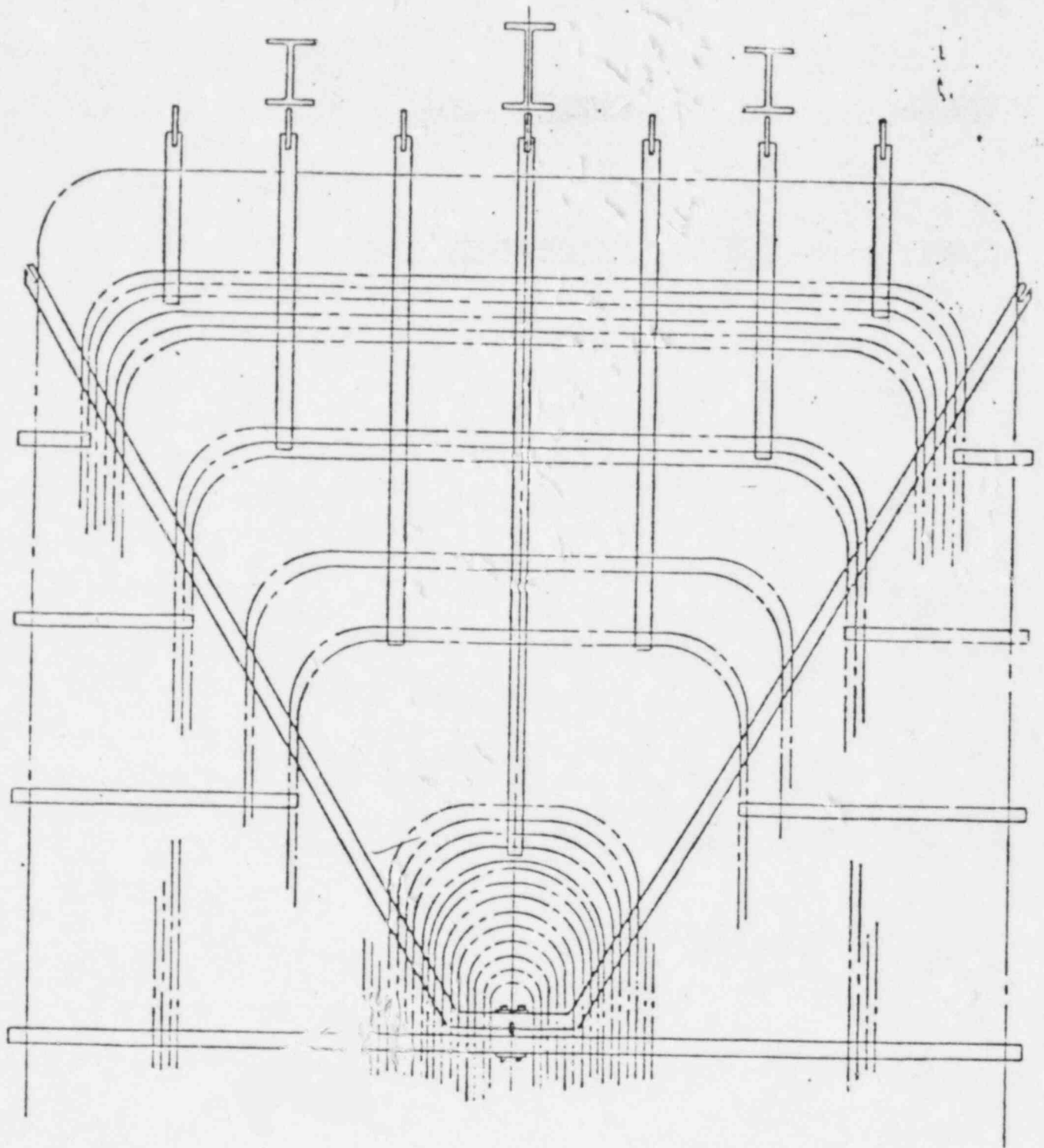
FULL DEPTH EXPANSION (EXPLANSION)  
EDGE WELDED TUBE TO TUBESHEET WELD

NOMINAL OPERATING PARAMETERS:

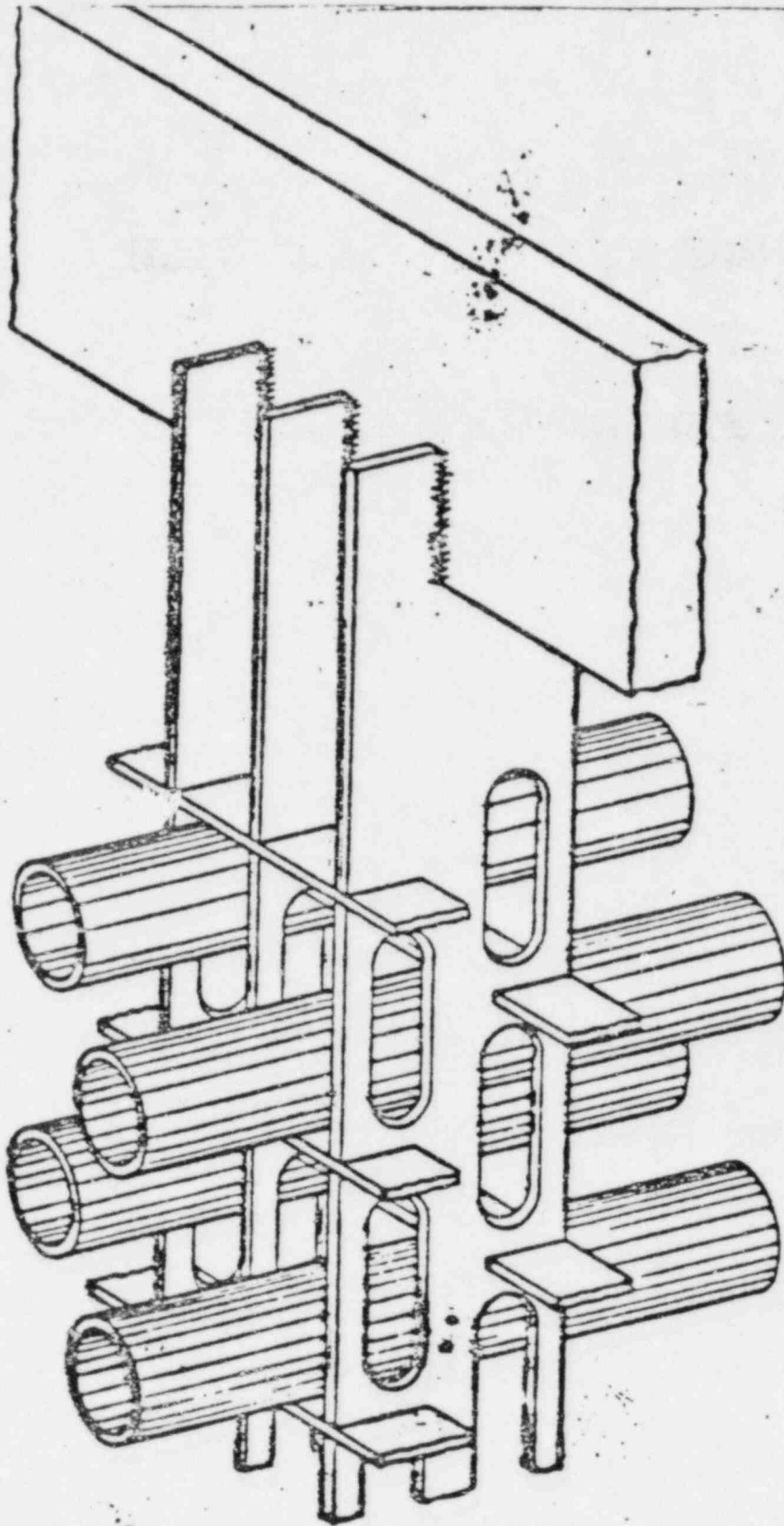
PRIMARY PRESSURE - 2250 PSIA  
SECONDARY PRESSURE - 900 PSIA  
PRIMARY TH - 611°F  
PRIMARY TC - 553°F



3,410 MWT.



U-BEND TUBE SUPPORT SYSTEM



TUBE SUPPORT

(SLIDE NO. 2)



C-E STEAM GENERATORS

SYSTEM 80 (3817 MWT)

NUMBER OF TUBES: 11,000

TUBE SIZE: 0.750" O.D. X 0.042" WALL

TUBE PITCH: TRIANGULAR, 1" CENTERS

TUBE SUPPORTS: TWO HALF EGGCRATES (ECONOMIZER ELEVATION)  
THREE FULL DISK EGGCRATES  
TWO PARTIAL EGGCRATES  
BEND REGION - "V" SPACER ASSEMBLIES INTER-  
SECTING TUBES IN VERTICAL  
RUN BELOW BEND TANGENT POINT.  
  
VERTICAL SPACER ASSEMBLIES  
(VENTILATED) WITH INTERLOCKING  
HORIZONTAL STRIPS).

INTEGRAL ECONOMIZER (PREHEATER):

AXIAL COUNTERFLOW ARRANGEMENT  
180° FEEDWATER DISTRIBUTION DISCHARGING  
VERTICALLY DOWNWARD  
FLOW DISTRIBUTION BAFFLES, HOT AND COLD LEG

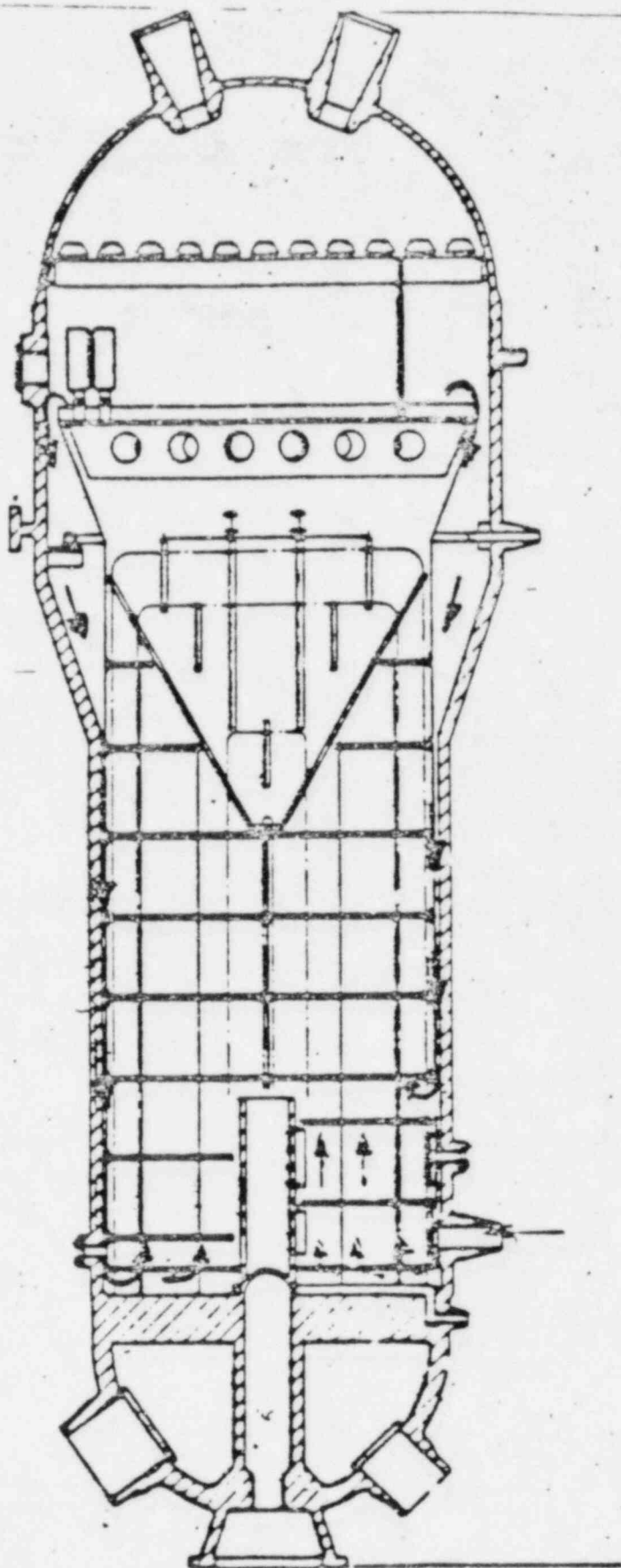
BLOWDOWN ARRANGEMENT: 3" X 6" DUCT, CENTER SUCTION PORTS  
SEPARATE, HOT AND COLD LEGS

TUBE TO TUBESHEET JOINT:

FULL DEPTH EXPANSION (EXPLANSION)  
EDGE WELDED TUBE TO TUBESHEET WELD

NOMINAL OPERATING PARAMETERS:

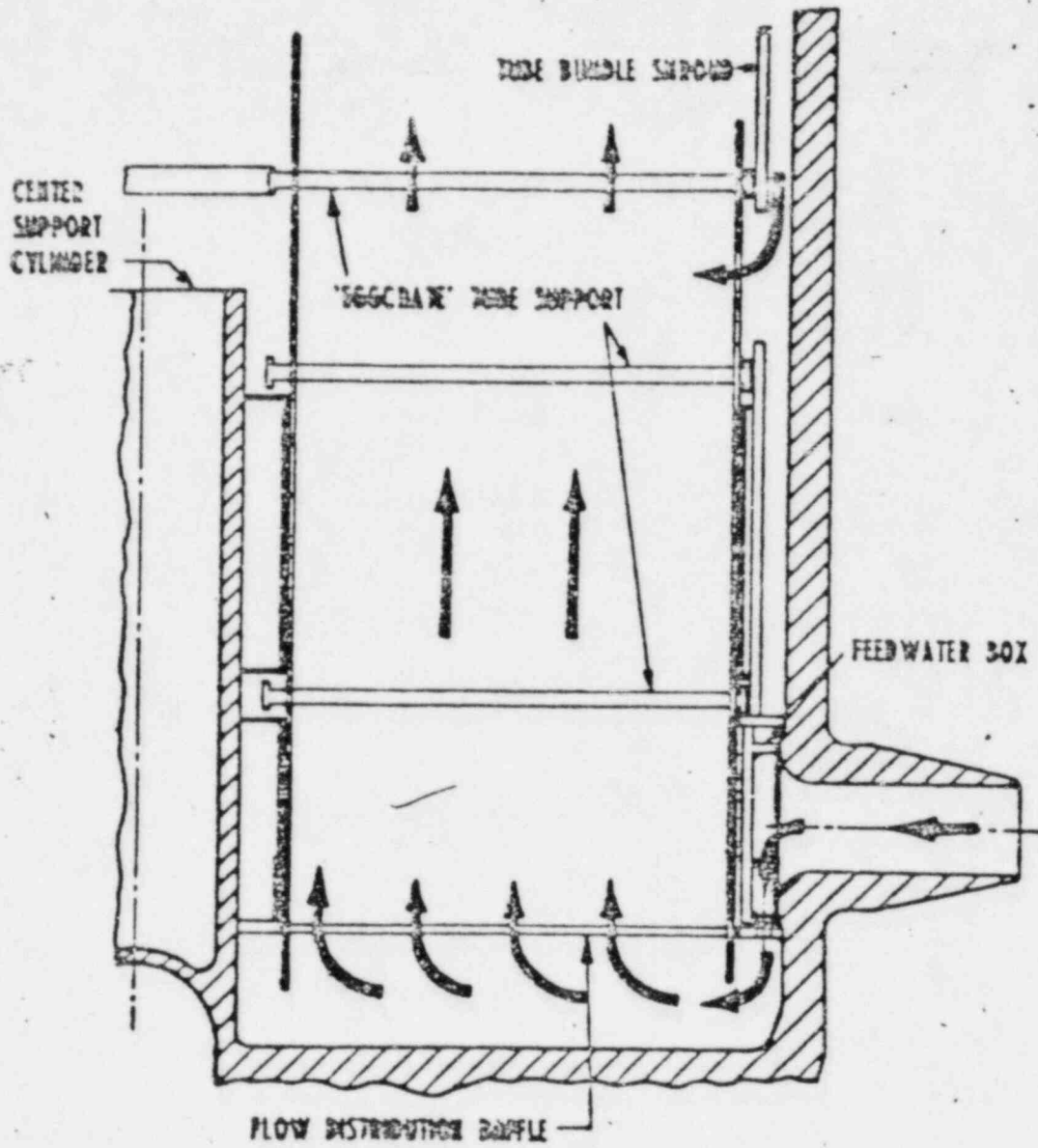
PRIMARY PRESSURE - 2250 PSIA  
SECONDARY PRESSURE - 1070 PSIA  
PRIMARY TH - 621°F  
PRIMARY TC - 564°F

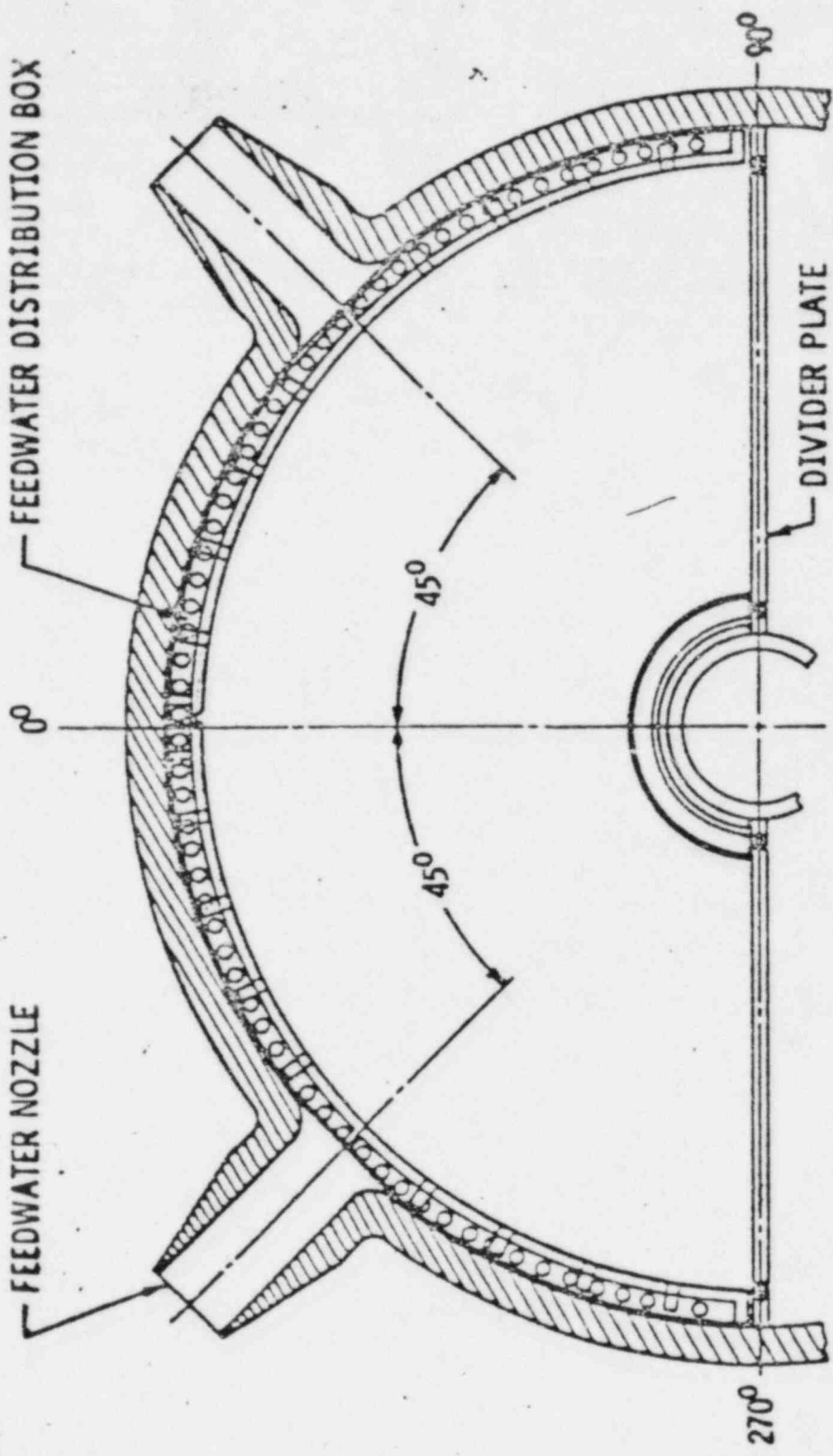


SYSTEM 80

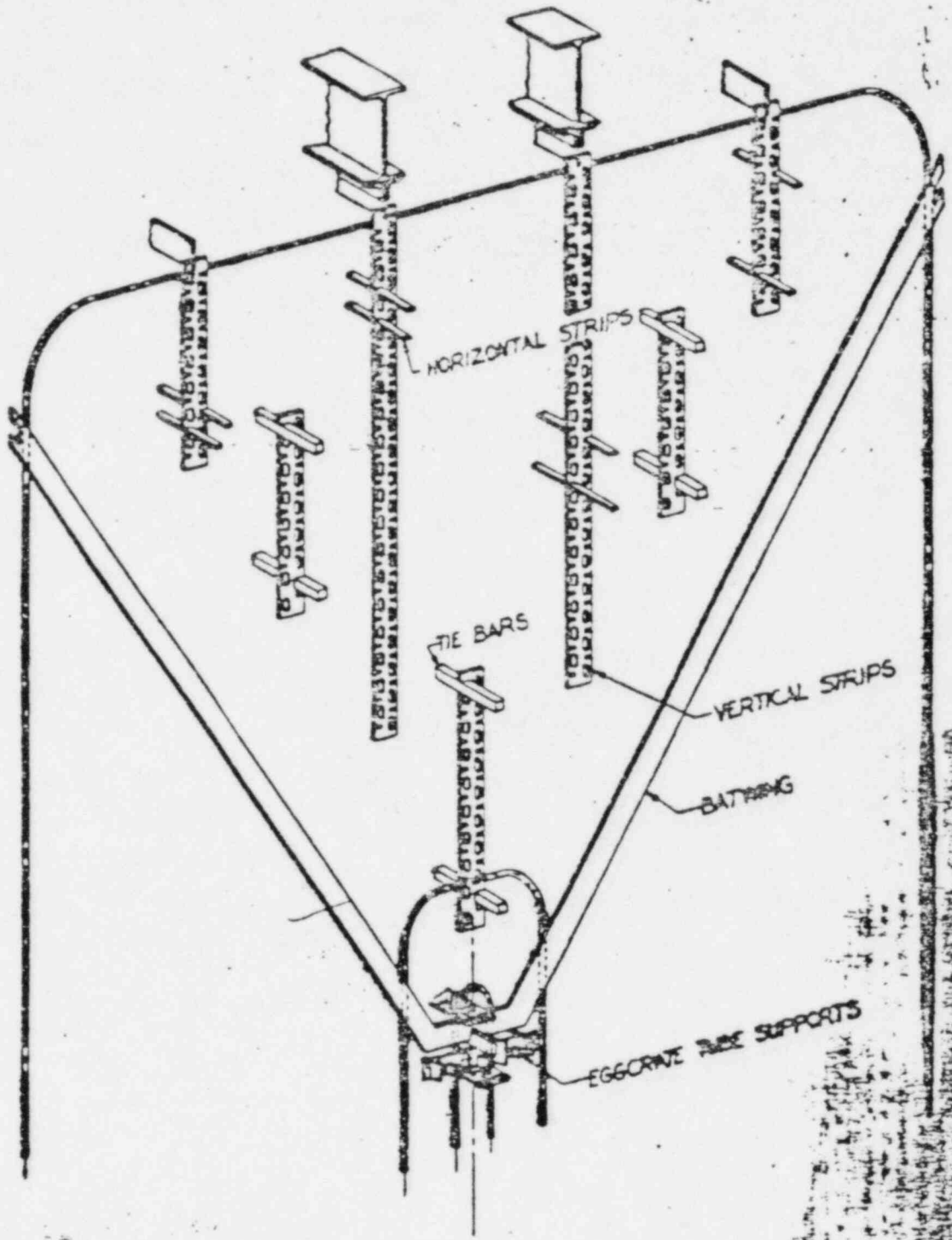
SUBJECT

# ECONOMIZER ELEVATION VIEW





ECONOMIZER (PLAN VIEW)



BOND REGION TUBE SUPPORTS

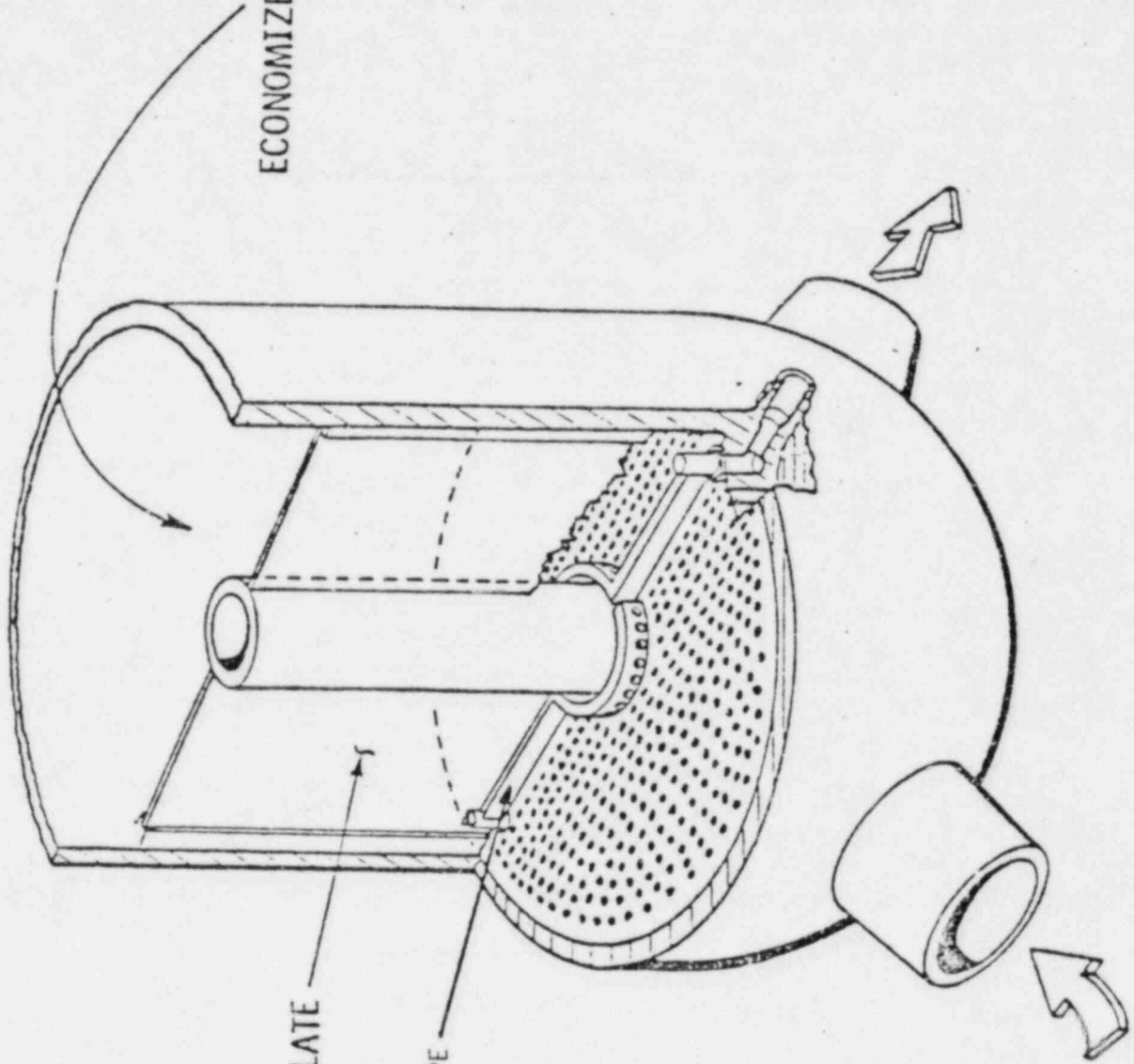
FIGURE 30-28

ECONOMIZER REGION

ECONOMIZER REGION

DIVIDER PLATE

BLOWDOWN PIPE



C-E STEAM GENERATORS  
TUBE LEAK TABULATION

PLANT	NO. S.G.'S	PLANT TOTAL TUBES	TUBE LEAKS				VIBRATION/WEAR
			TUBE WASTAGE	TUBE CRACKING	TUBE DENTING	TUBE PITTING	
A	2	17038	3 (1973)	1			
B	3	17109					
C	2	10010					
D	2	17038					
E	2	17038					
F	2	17038		1 (?)			
G	2	17038					
H	2	16822					
TOTAL	17	129,131	3	2			

C-E STEAM GENERATORS  
TUBE PLUGGING TABULATION

PLANT	NO. S.G.'S	TOTAL NO. TUBES	TUBES PLUGGED						TOTAL
			WASTAGE	CRACKING	DENTING	PITTING	VIBRATION/WEAR	PREVENTATIVE	
A	2	17038	3747		11				3758
B	3	17109						15	15
C	2	10010	3**					48	51
D	2	17038							
E	2	17038			331	731		437	1499
F	2	17038		77**				50	127
G	2	17038							
H	2	16822						26	26
TOTAL	17	129,131	3750	77**	331	731		576	5476

\*\* CAUSE NOT SPECIFICALLY DETERMINED  
 \*\*\* THOUGHT TO BE MECHANICAL, NOT CONFIRMED



## TUBE PLUGGING CRITERIA

BASIS: REGULATORY GUIDE 1.121  
ASME CODE, SECTIONS III AND XI

### TUBE PLUGGING LIMITS:

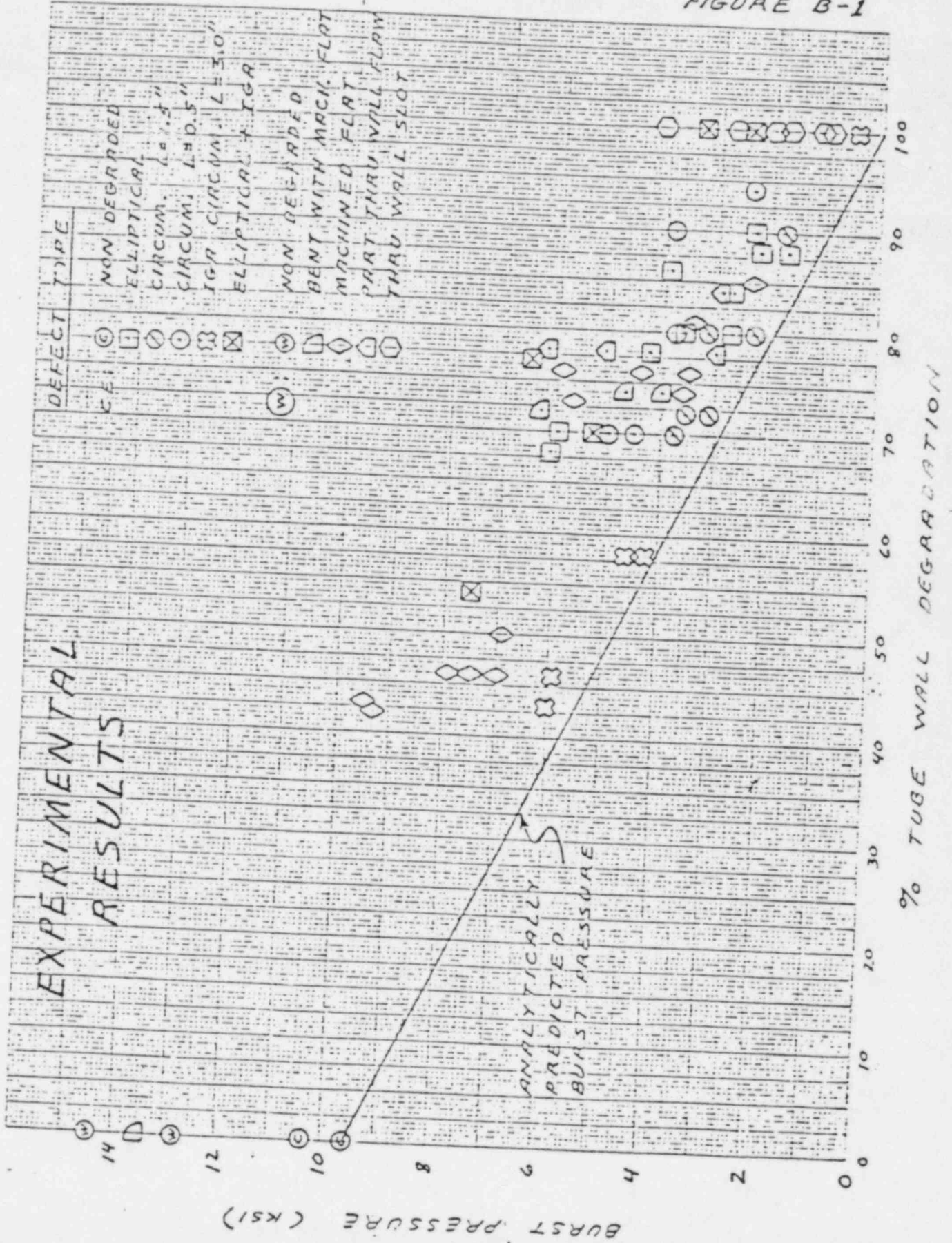
GENERALLY 40% TUBE WALL DEGRADATION ALLOWED.

GREATER DEGRADATION ALLOWED WHEN JUSTIFIED ON A PLANT BASIS USING SAME CRITERIA AND METHODOLOGY.

ALLOWABLE DEGRADATION OF 56% OR GREATER CAN BE JUSTIFIED FOR CURRENTLY OPERATING C-E PLANTS.

PLUGGING LIMIT FOR TUBE DENTING BASED ON "PLUG GAGE" (0.540" DIAMETER ECT PROBE) RELATED TO HOOP TENSILE STRAIN.

FIGURE B-1



C-E STEAM GENERATOR  
CHEMISTRY CONTROL SPECIFICATIONS

	<u>NORMAL</u>	<u>ABNORMAL</u>	<u>IMMEDIATE SHUTDOWN</u>
pH	8.2 - 9.2	7.5 - 8.2 9.2 - 9.5	10.5
CONDUCTIVITY (SPECIFIC)	< 7 $\mu$ MHOS/CM*	7 - 15 $\mu$ MHOS/CM	
SUSPENDED SOLIDS	< 1.0 PPM	1 - 10 PPM	
FREE HYDROXIDE	-----	-----	5 PPM
SILICA	< 1.0 PPM	1 - 10 PPM	
CHLORIDE	< 0.1 PPM	-----	-----

\* SPECIFIC CONDUCTIVITY ALARM SET POINT 4  $\mu$ MHOS/CM

JWK/3/82

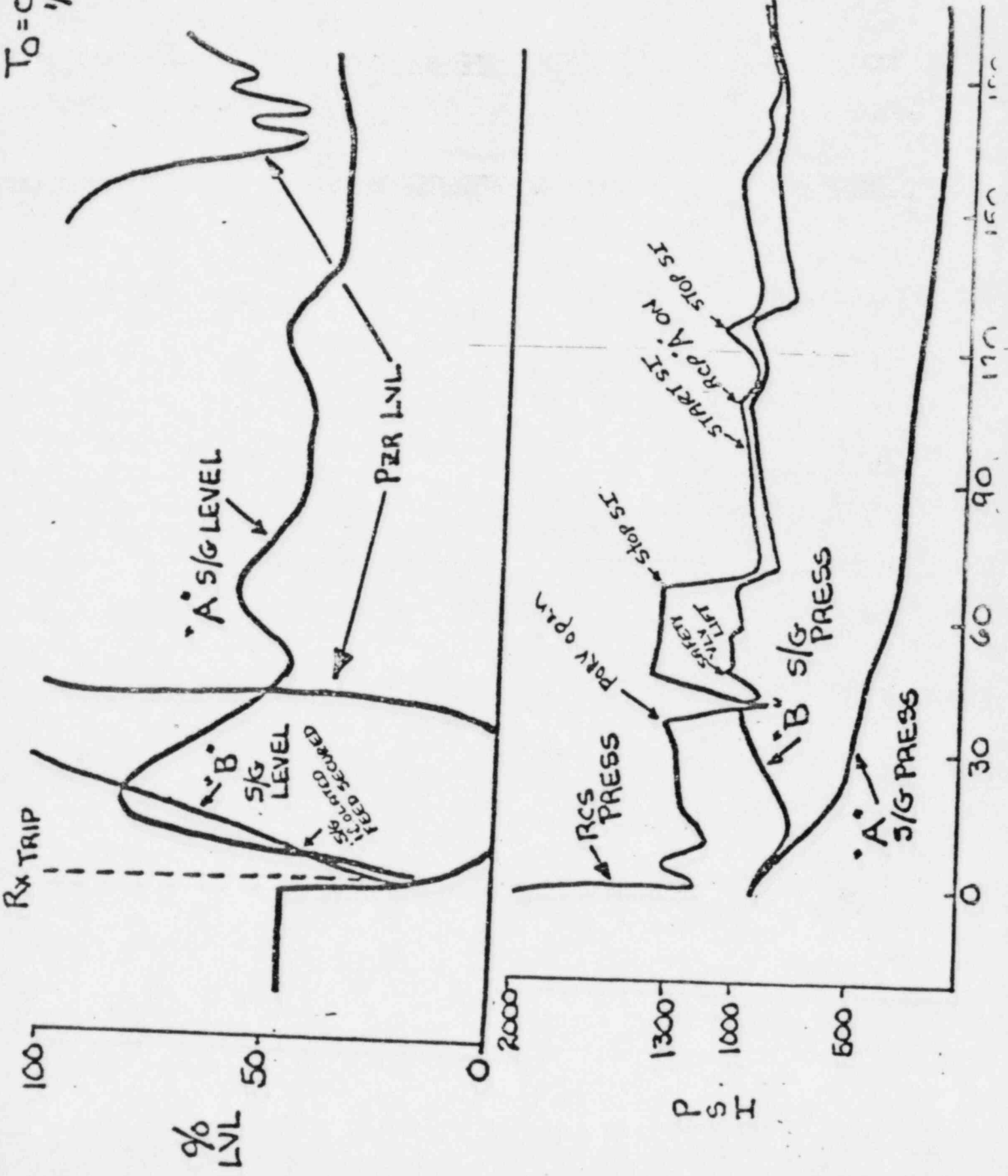
0213b

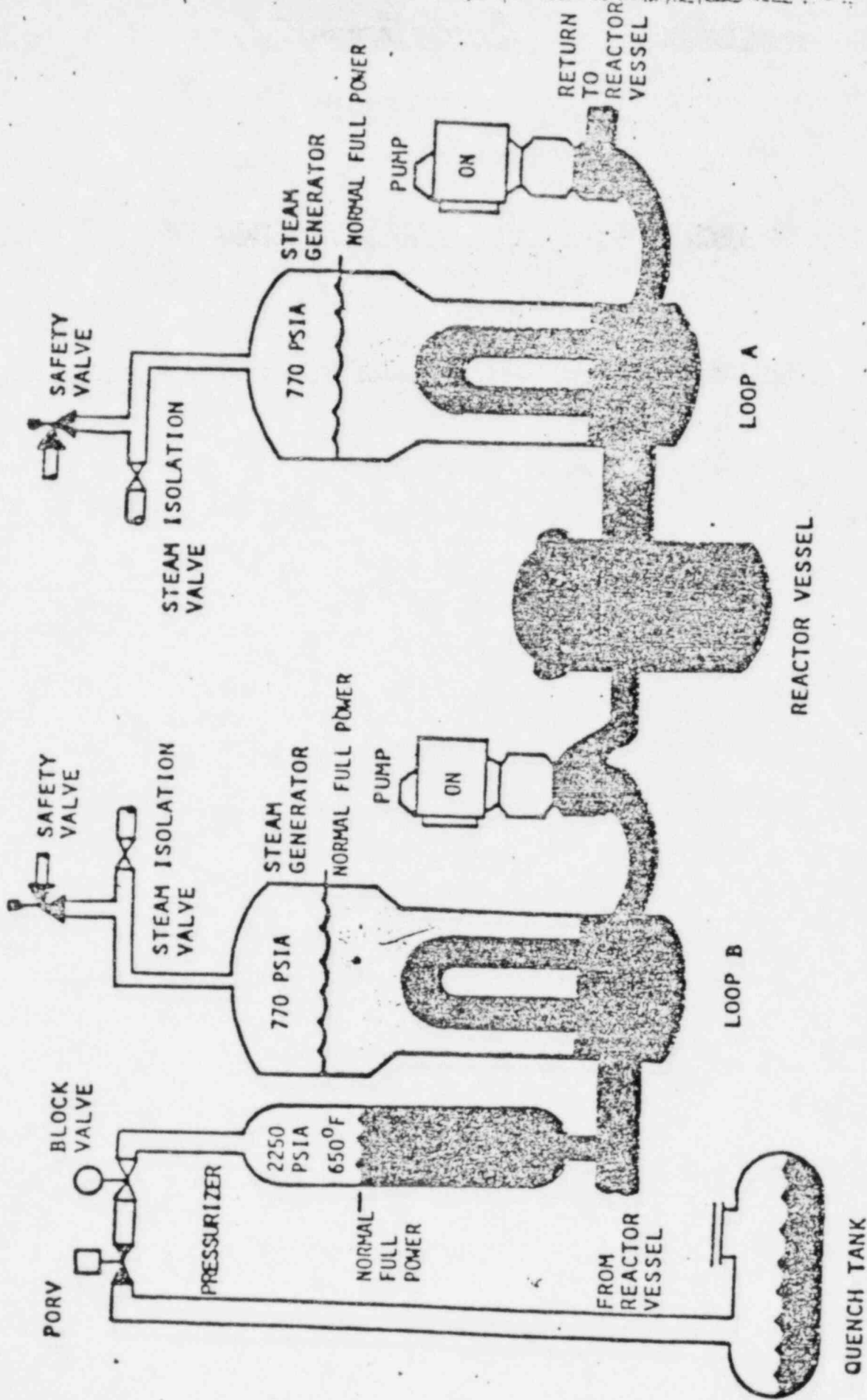
## PURPOSE

- PROVIDE AN OVERVIEW OF THE C-EOG STRATEGY TO MITIGATE SGTRs
  
- POINT OUT MAJOR DIFFERENCES BETWEEN ACTIONS TAKEN AT GINNA AND ACTIONS SPECIFIED IN THE C-EOG SGTR GUIDELINE

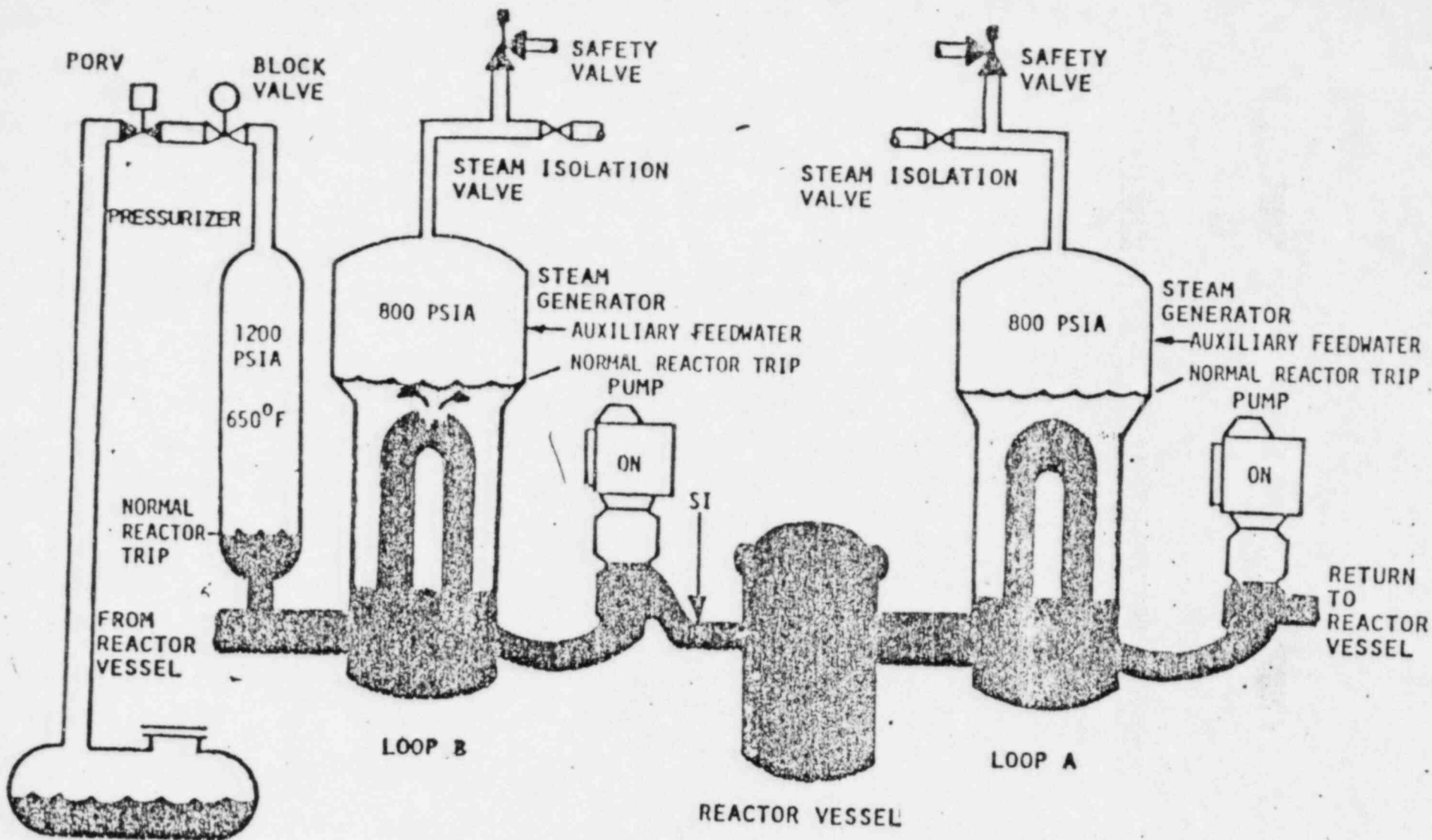
- C-EOG GUIDANCE IS GENERIC
- UTILITIES MAY CHOOSE TO IMPLEMENT  
IT DIFFERENTLY THAN STATED
- C-E CANNOT SPEAK FOR UTILITIES

T<sub>0</sub> = 0928  
1/25/82





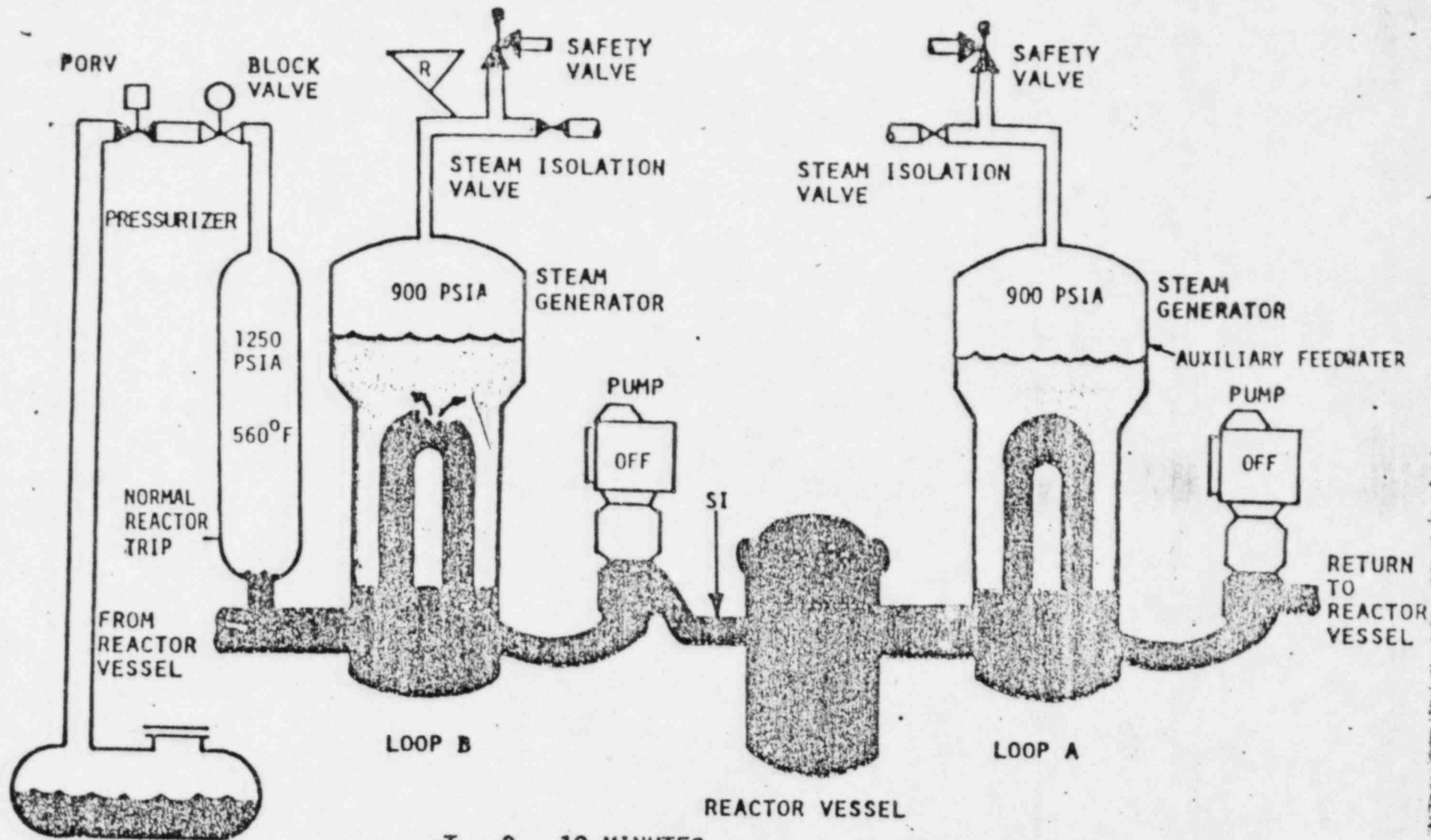
T = 0, INITIAL CONDITIONS, NORMAL POWER



QUENCH TANK

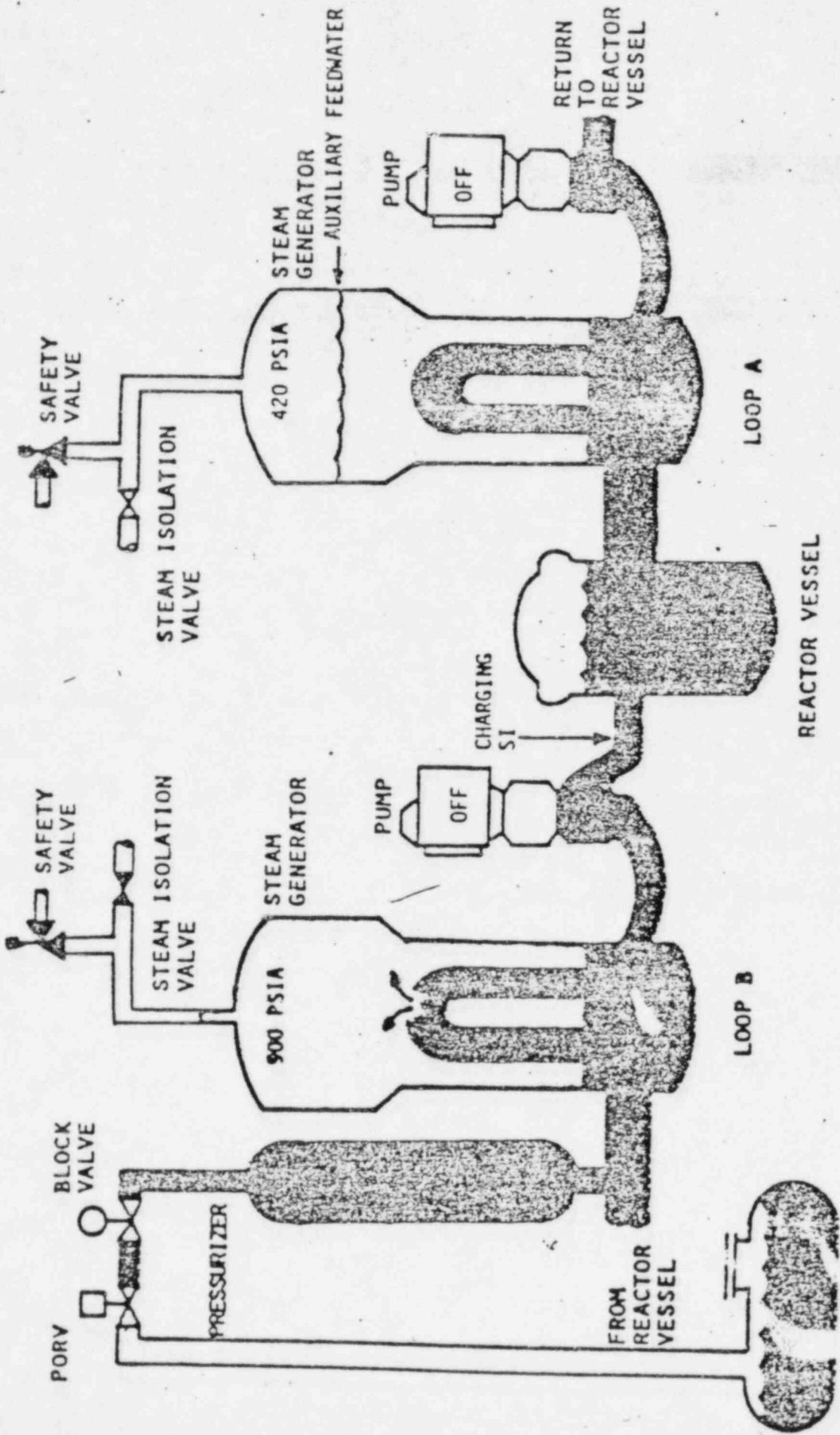
T = 3 MINUTES, STEAM GENERATOR TUBE RUPTURE  
 REACTOR TRIP, COOLANT PUMPS ON  
 SI ACTUATION  
 AUXILIARY FEEDWATER ACTUATION  
 PRESSURIZER LEVEL DEPLETED  
 STEAM GENERATOR LEVEL LOW



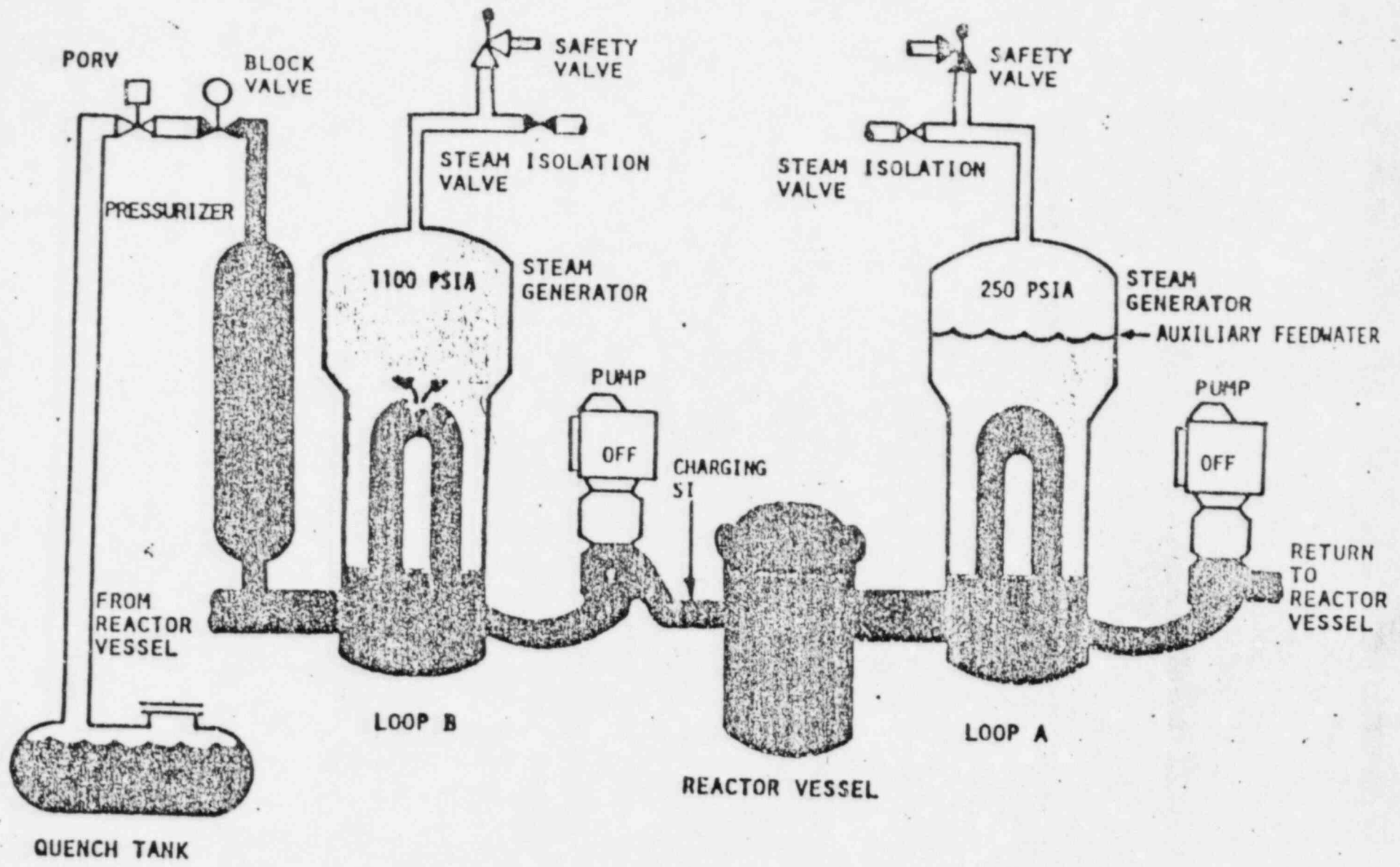


QUENCH TANK

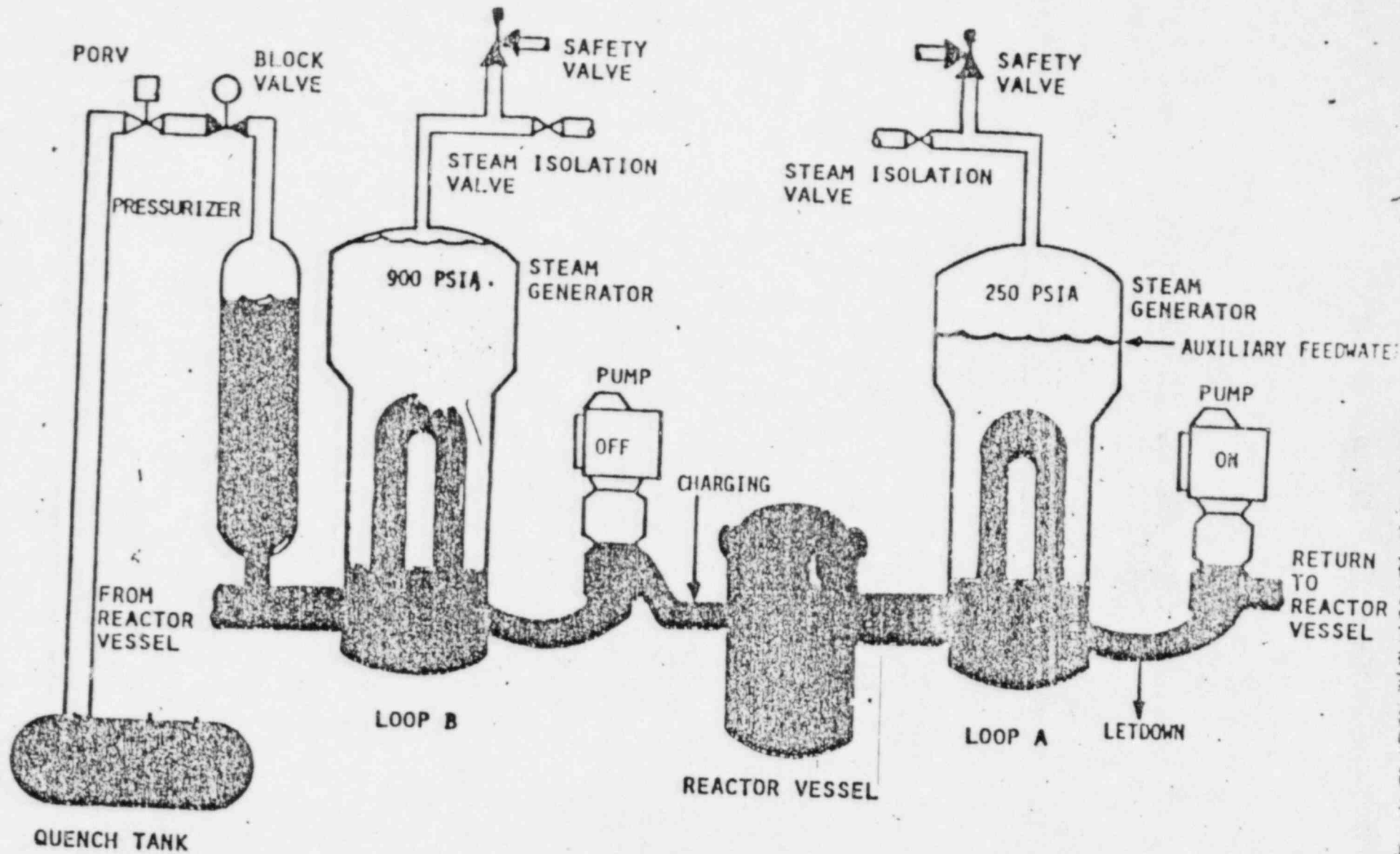
T - 8 - 12 MINUTES, STEAM GENERATOR TUBE RUPTURE IDENTIFIED  
 STEAM GENERATOR B LEVEL INCREASING FASTER THAN A  
 STEAM GENERATOR B ISOLATED  
 AUXILIARY FEEDWATER TO STEAM GENERATOR A  
 REACTOR COOLANT PUMPS OFF  
 HIGH RADIATION LEVELS ON "B" SG PIPING



T - 43 MINUTES, PORV STUCK OPEN  
 VOID FORMS IN REACTOR VESSEL HEAD  
 PRESSURIZER LEVEL FULL

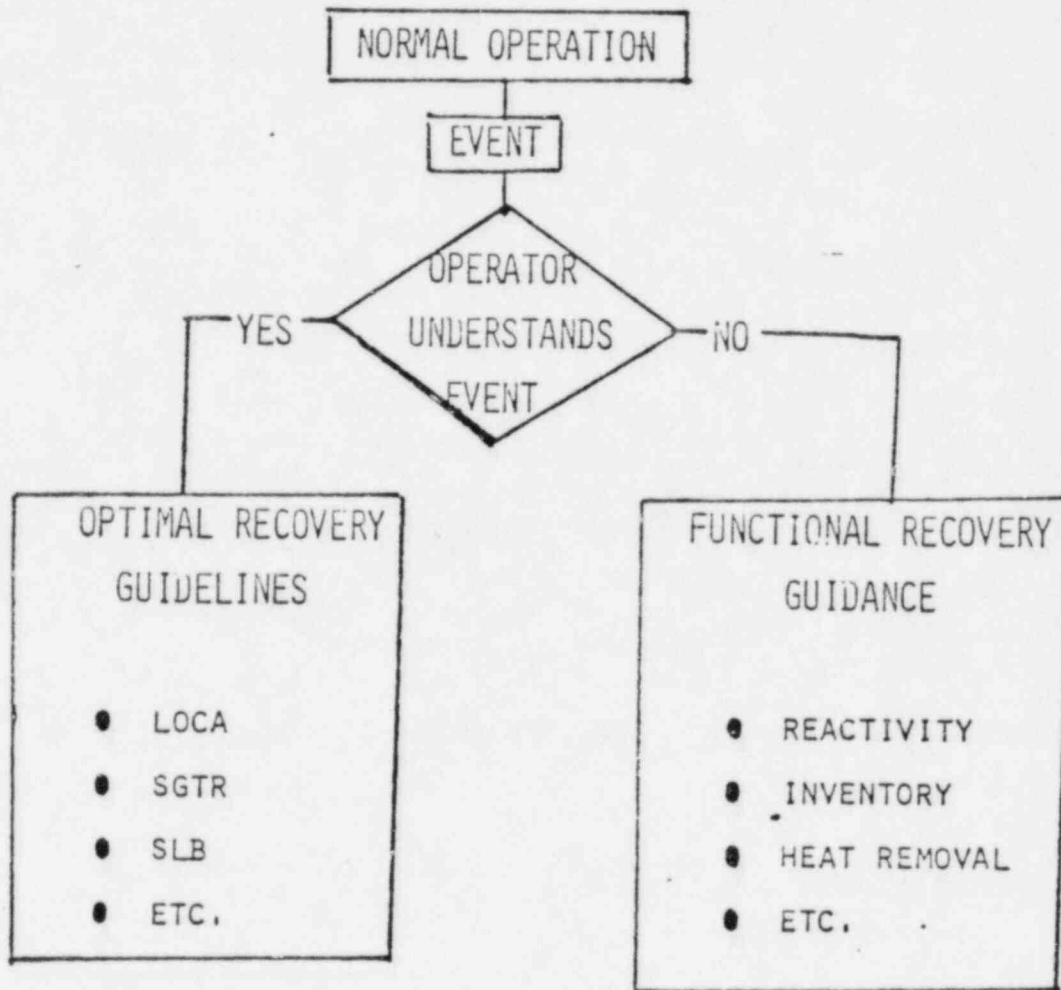


T - MINUTES, SI AND CHARGING LIFT STEAM GENERATOR B SAFETY VALVE

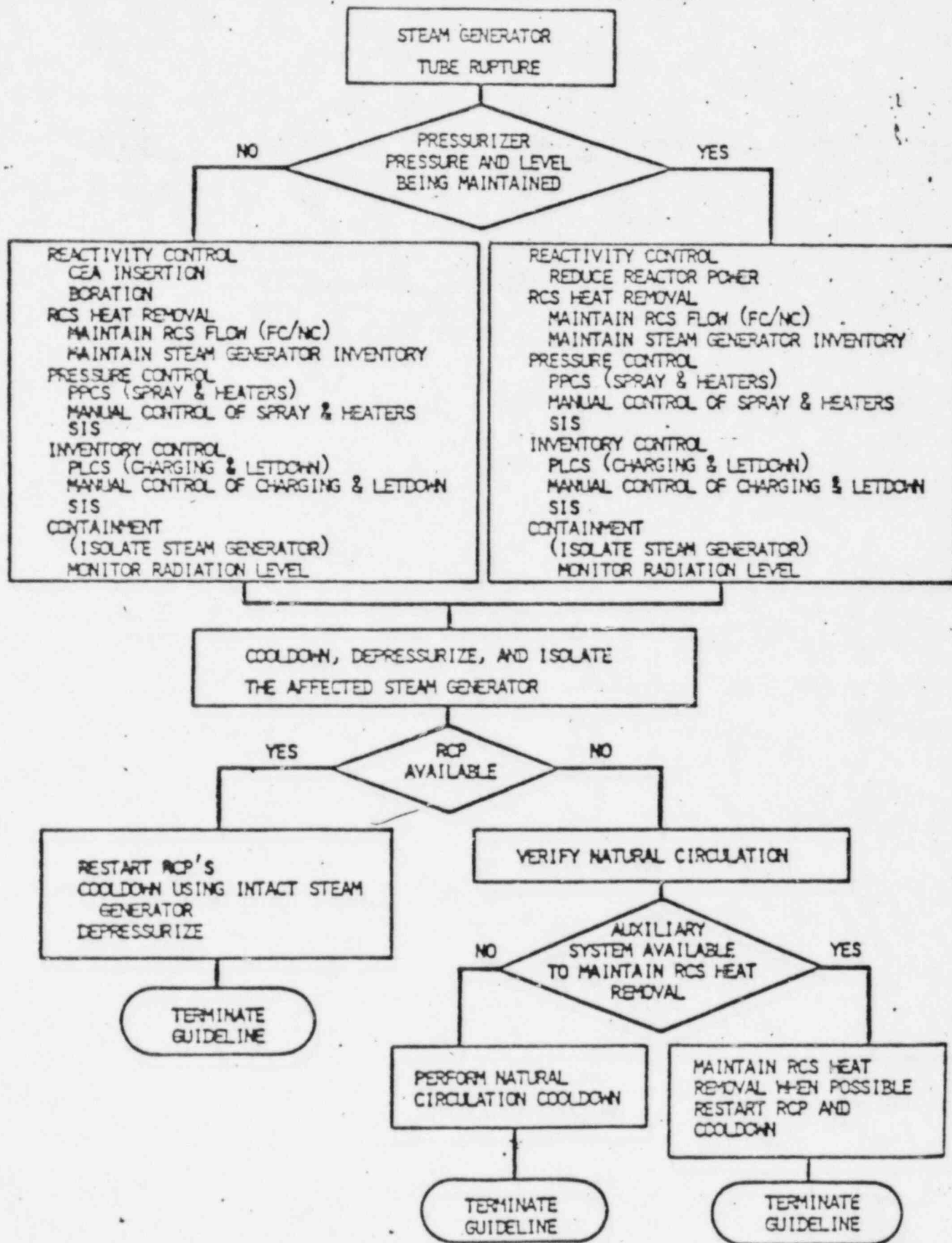


T = 155 MINUTES, BUBBLE IN PRESSURIZER  
 REACTOR VESSEL VOID CONDENSED  
 LETDOWN ESTABLISHED

C-EOG  
EMERGENCY PROCEDURE GUIDELINE SYSTEM



STEAM GENERATOR TUBE RUPTURE STRATEGY CHART



	GINNA	CE	POTENTIAL IMPACT
RCS DEPRESSURIZATION	PORV	AUX. SPRAY	1) EARLIER DEPRESSURIZATION MIGHT BE ENCOURAGED 2) NO ADDITIONAL CHALLENGE TO RCS PRESSURE BOUNDARY INTEGRITY
RCP OPERATION	--	SPECIFIC RESTART CRITERIA PROVIDED	EARLIER RESTART OF RCPS - FORCED CIRCULATION COOLDOWN
HPSI PUMP TERMINATION	CRITERIA PROVIDED	CRITERIA PROVIDED	EARLIER DEPRESSURIZATION WOULD HAVE SATISFIED TERMINATION CRITERIA EARLIER - REDUCED CHALLENGE TO S.G. SAFETIES
S.G. LEVEL CONTROL	--	CRITERIA PROVIDED ON CONTROL ON AFFECTED S.G.	REDUCED CHALLENGE TO S.G. SAFETY VALVES

- GINNA PLANT RESPONSE NOT SIGNIFICANTLY DIFFERENT FROM CE PLANT
- CE GUIDELINES & CE EQUIPMENT MAY HAVE REDUCED CHALLENGES TO S.G. SAFETY VALVES