QUAD-CITIES NUCLEAR POWER STATION

UNITS 1 AND 2

MONTHLY PERFORMANCE REPORT

JANUARY 1983

COMMONWEALTH EDISON COMPANY

AND

IOWA-ILLINOIS GAS & ELECTRIC COMPANY

NRC DOCKET NOS. 50-254 AND 50-265

LICENSE NOS. DPR-29 AND DPR-30

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I. INTRODUCTION

Quad-Cities Nuclear Power Station is composed of two Boiling Water Reactors, each with a Maximum Dependable Capacity of 769 MWe net, located in Cordova, Illinois. The Station is jointly owned by Commonwealth Edison Company and Iowa-Illinois Gas & Electric Company. The Nuclear Steam Supply Systems are General Electric Company Boiling Water Reactors. The Architect/Engineer was Sargent & Lundy, Incorporated, and the primary construction contractor was United Engineers & Constructors. The condenser cooling method is a closed cycle spray canal, and the Mississippi River is the condenser cooling water source. The plant is subject to license numbers DPR-29 and DPR-30, issued October 1, 1971, and March 21, 1972, respectively, pursuant to Docket Numbers 50-254 and 50-265. The date of initial reactor criticalities for Units 1 and 2 respectively were October 18, 1971, and April 26, 1972. Commercial generation of power began on February 18, 1973 for Unit 1 and March 10, 1973 for Unit 2.

This report was compiled by Becky Brown and Randall Buss, telephone number 309-654-2241, extensions 127 and 181.

II. SUMMARY OF OPERATING EXPERIENCE

A. UNIT ONE

January 1-31: Unit One began the month increasing load after a load reduction for maintenance. On January 4, load was reduced rapidly to approximately 320 MWe during the unit's flow drop test, followed immediately by a load increase to 820 MWe which was completed by January 6. Three times during this month the load was decreased to approximately 700 MWe to perform weekly Turbine tests. An average load of approximately 820 MWe was maintained at all other times. On January 26, load was decreased to 700 MWe to change Condensate pumps. Load was then increased to 825 MWe by 0700 hours. On January 27, at 2150 hours, load was decreased 100 MWe to 720 MWe due to a steam leak in the 1B Off Gas Recombiner. At 2230 hours, load was increased at 50 MWe/hour for two hours. On January 29, at 0100 hours, load was decreased 100 MWe/hour to 700 MWe for weekly Turbine tests. Load was then increased to 831 MWe by 1420 hours.

B. UNIT TWO

January 1-10: Unit Two began the month holding load at approximately 780 MWe. On January 5 load was decreased to approximately 590 MWe by 2150 hours to change the Steam Jet Air Ejectors due to a steam leak. At 2310 hours, load was dropped to 500 MWe to return the original Steam Jet Air Ejectors to service after the repairs were completed. A load increase was begun at 0500 hours on January 6, beginning at 0500 hours, and the load reached approximately 772 MWe at 1415 hours. Load was then held due to Condensate Demineralizer problems. At 1520 hours, load was dropped to 650 MWe. This was necessitated by high Reactor water conductivity caused by a Condensate Demineralizer failure. On January 7 load was dropped to 550 MWe for control rod pattern adjustment. At 1500 hours, load began increasing at 5 MWe/hour to 790 MWe on January 9.

January 11-16: On January 11, at 1344 hours, the unit scrammed on an erroneous high steam line flow signal and subsequent main steam isolation valve closure caused by contractor personnel jarring an instrument rack. The unit was on line at 0023 hours on January 12 and load was increased to 773 MWe by January 13. On January 14 load was dropped 200 MWe to backwash and precoat a Condensate Demineralizer. Load then increased to 744 MWe. On January 15, load was decreased to 500 MWe to reverse flow through the main Condenser in order to reduce high backpressure. Load was then increased to approximately 780 MWe on January 16.

B. UNIT TWO: (continued)

January 17-31: On January 17, load was decreased to 328 MWe to investigate Primary Containment leakage. This leakage was a result of a 2A Recirculation pump loop valve packing leak. Following adjustments, the load was increased to 668 MWe by 2220 hours. Unit load was held here due to high Condenser backpressure. On January 18 load was dropped to 520 MWe to take the 2C Circulating Water pump out of service to repair a casing leak. Load was then increased to approximately 650 MWe. On January 28, load was reduced at 100 MWe/hour in preparation for a scheduled Maintenance Outage to repair the 2C Circulating Water pump. At 1830 hours, the Generator was taken off line. The Reactor was manually scrammed at 1840 hours. The Maintenance Outage continued through the end of the month.

III. PLANT OR PROCEDURE CHANGES, TESTS, EXPERIMENTS, AND SAFETY RELATED MAINTENANCE

A. Amendments to Facility License or Technical Specifications

On December 15, 1982, the NRC issued Amendment 83 to License DPR-29. This Amendment provides changes to the License and Technical Specifications required to operate Unit One with the fuel load for Cycle 7. Unit One began operating in Cycle 7 on December 22, 1982.

On December 23, 1982, the NRC issued Amendments 84 and 77 to Licenses DPR-29 and DPR-39, respectively. This Amendment adds requirements for verifying that the scram discharge volume drain and vent valves are open every month.

B. Facility or Procedure Changes Requiring NRC Approval

There were no Facility or Procedure Changes requiring NRC approval for the reporting period.

C. Tests and Experiments Requiring NRC Approval

There were no Tests or Experiments requiring NRC approval for the reporting period.

D. Corrective Maintenance of Safety Related Equipment

The following represents a tabular summary of the safety related maintenance performed on Unit One and Unit Two during the reporting period. This summary includes the following headings: Work Request Numbers, LER Numbers, Components, Cause of Malfunctions, Results and Effects on Safe Operation, and Action Taken to Prevent Repetition.

UNIT ONE MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q21639		RV-1-4711	The relief valve seat was worn, causing valve to lift at low pressure.	Local Leak Rate Test was found to leak at greater than 10.36 scfh.	The valve seats were relapped and the lifting pressure was adjusted.
Q23549		TIP #5 Ball Valve	The ball valve seats were binding against the ball.	The ball valve sticks. Containment isolation was maintained at all times.	The ball valve was replaced and cycled satisfactorily.
Q23721		Unit 1 Diesel Generator (1-6601)	Leaky Y strainer.	Air leaking from "Y" on starting air header. Diesel Generator operability was unaffected.	Replaced Y strainer.
Q23824		TIP #4 Ball Valve	The valve seats were dirty.	TIP #4 ball valve was sticking. Containment isolation was maintained at all times.	The valve internals were cleaned, and the spring tension was adjusted.
Q23925	83-5/03L	HPCI Signal Converter 1-2306	A resistor in the flow controller power supply had burnt out.	The automatic flow controller was inoperable, but HPCI could be operated manually.	Replaced the flow controller circuit amplifier, and resistor in -15 VDC power supply.

UNIT TWO MAINTENANCE SUMMARY

W.R. NUMBER	LER NUMBER	COMPONENT	CAUSE OF MALFUNCTION	RESULTS & EFFECTS ON SAFE OPERATION	ACTION TAKEN TO PREVENT REPETITION
Q23832	83-2/03L	2-703 TIP #4	The valve internals were dirty, and the spring tension on the solenoid operator was out of adjustment.	#4 TIP ball valve will not close. The manual ball valve was closed to maintain containment isolation.	The valve was cleaned and the spring tension was adjusted.
Q22241		2B RHR Heat Exchanger 2B-1003	The expansion joint on the drain from the tube side had cracked.	Leakage from the crack to the service water did not exceed the release limits. The heat exchanger was still operable.	The expansion joint on the drain line was replaced.
Q23887		2-2001-16	The solenoid operated pilot valve was worn.	The valve will not open when given open signal.	The solenoid valve and pipe elbow were replaced.

IV. LICENSEE EVENT REPORTS

The following is a tabular summary of all licensee event reports for Quad-Cities Units One and Two occurring during the reporting period, pursuant to the reportable occurrence reporting requirements as set forth in sections 6.6.B.1. and 6.6.B.2. of the Technical Specifications.

UNIT ONE

Licensee Event Report Number	Date	Title of Occurrence
83-1/03L	1-04-83	1/2 Diesel Generator Failure to Run
83-2/03L	1-09-83	'A' RHR Heat Exchanger Leak
83-3/03L	1-18-83	1-263-58A Level Switch Out of Calibration
83-4/03L	1-19-83	Unit One HPCI Speed Changer
83-5/03L	1-15-83	Unit One HPCI Motor Gear Unit Failure to Stay at High Speed Stop

UNIT TWO

83-1/03L	1-02-83	Off Gas Monitor Failure
83-2/03L	1-06-83	Reactor Water Conductivity Greater than 10 umho
83-3/03L	1-10-83	TIP #4 Ball Valve Failure
83-4/03L	1-16-83	2B RHR Heat Exchanger Out of Service for Tube Leak

V. DATA TABULATIONS

The following data tabulations are presented in this report:

A. Operating Data Report

B. Average Daily Unit Power Level

C. Unit Shutdowns and Power Reductions

OPERATING DATA REPORT

DOCKET NO. 50-254

UNIT ONE

DATE February 01 1983

COMPLETED BY Randall D Buss

TELEPHONE 309-654-2241x181

OPERATING STATUS

0000 010183

1. Reporting period: 2400 013183 Gross hours in reporting period: 744

2. Currently authorized power level (MWt): 2511 Max.Depend capacity (MWe-Net): 769* Design electrical rating (MWe-Net): 789

3. Power level to which restricted(if any)(MWe-Net): NA

4. Reasons for restriction (if any):

	This Month	Yr.to Date	Cumulative
5. Number of hours reactor was critical	744.0	744.0	75915.2
6. Reactor reserve shutdown hours	0.0	0.0	3421.9
7. Hours generator on line	744.0	744.0	72830.6
8. Unit reserve shutdown hours.	0.0	0.0	909.2
9. Gross thermal energy generated(MWH)	1816962	1816962	148029953
10. Gross electrical energy generated(MWH)	598456	598456	47720337
11. Net electrical energy generated(MWH)	563374	563374	44392282
12. Reactor service factor	100.0	100.0	80.7
13. Reactor availability factor	100.0	100.0	84.4
14. Unit service factor	100.0	100.0	77.5
15. Unit availability factor	100.0	100.0	78.4
16. Unit capacity factor (Using MDC)	98.5	98.5	61.4
17. Unit capacity factor (Using Des.MWe)	96.0	96.0	59.8
18. Unit forced outage rate	0.0	0.0	6.7

19. Shutdowns scheduled over next 6 months (Type,Date,and Duration of each):

20. If shutdown at end of report period,estimated date of startup NA

*The MDC may be lower than 769 MWe during periods of high ambient temperature due to the thermal performance of the spray canal.

*UNOFFICIAL COMPANY NUMBERS ARE USED IN THIS REPORT

OPERATING DATA REPORT

DOCKET NO. 50-265

UNIT TWO

DATE February 01 1983

COMPLETED BY Randall D Buss

TELEPHONE 309-654-2241x181

OPERATING STATUS

0000 010183

1. Reporting period: 2400 013183 Gross hours in reporting period: 744

2. Currently authorized power level (MWt): 2511 Max.Depend capacity (MWe-Net): 769* Design electrical rating (MWe-Net): 789

3. Power level to which restricted(if any)(MWe-Net): NA

4. Reasons for restriction (if any):

	This Month	Yr.to Date	Cumulative
5. Number of hours reactor was critical	659.7	659.7	72923.1
6. Reactor reserve shutdown hours	0.0	0.0	2985.8
7. Hours generator on line	655.9	655.9	70244.0
8. Unit reserve shutdown hours.	0.0	0.0	702.9
9. Gross thermal energy generated(MWH)	1447122	1447122	146038616
10. Gross electrical energy generated(MWH)	450236	450236	46487771
11. Net electrical energy generated(MWH)	422541	422541	4360610[illegible]
12. Reactor service factor	88.7	88.7	78.3
13. Reactor availability factor	88.7	88.7	81.5
14. Unit service factor	88.2	88.2	75.4
15. Unit availability factor	88.2	88.2	76.2
16. Unit capacity factor (Using MDC)	73.9	73.9	60.9
17. Unit capacity factor (Using Des.MWe)	72.0	72.0	59.4
18. Unit forced outage rate	11.9	11.9	9.2

19. Shutdowns scheduled over next 6 months (Type,Date,and Duration of each):

20. If shutdown at end of report period,estimated date of startup 2-4-83

*The MDC may be lower than 769 MWe during periods of high ambient temperature due to the thermal performance of the spray canal.

*UNOFFICIAL COMPANY NUMBERS ARE USED IN THIS REPORT

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-254

UNIT ONE

DATE February 01 1983

COMPLETED BY Randall D Buss

TELEPHONE 309-654-2241x181

MONTH January 1983

DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)	DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)
1.	696.5	17.	777.9
2.	754.0	18.	772.3
3.	768.6	19.	764.8
4.	700.1	20.	772.6
5.	631.2	21.	772.6
6.	766.2	22.	776.8
7.	772.0	23.	726.7
8.	771.0	24.	774.8
9.	735.5	25.	769.0
10.	752.7	26.	767.7
11.	809.0	27.	773.6
12.	754.4	28.	755.1
13.	783.0	29.	768.1
14.	769.3	30.	749.4
15.	777.1	31.	779.9
16.	732.0		

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly

APPENDIX B
AVERAGE DAILY UNIT POWER LEVEL

DOCKET NO. 50-265

UNIT TWO

DATE February 01 1983

COMPLETED BY Randall D Buss

TELEPHONE 309-654-2241x181

MONTH January 1983

DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)	DAY	AVERAGE DAILY POWER LEVEL (MWe-Net)
1.	743.0	17.	579.1
2.	651.1	18.	602.9
3.	730.7	19.	590.3
4.	742.9	20.	615.0
5.	714.0	21.	629.0
6.	606.4	22.	641.1
7.	640.3	23.	637.4
8.	526.5	24.	644.8
9.	711.9	25.	638.0
10.	735.3	26.	648.0
11.	411.8	27.	639.5
12.	484.8	28.	394.0
13.	653.4	29.	-7.7
14.	655.0	30.	-5.8
15.	640.1	31.	-5.4
16.	718.5		

INSTRUCTIONS

On this form, list the average daily unit power level in MWe-Net for each day in the reporting month. Compute to the nearest whole megawatt.

These figures will be used to plot a graph for each reporting month. Note that when maximum dependable capacity is used for the net electrical rating of the unit, there may be occasions when the daily average power level exceeds the 100% line (or the restricted power level line). In such cases, the average daily unit power output sheet should be footnoted to explain the apparent anomaly

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APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 6
August 1982

DOCKET NO. 050-254

UNIT NAME Quad-Cities Unit One

COMPLETED BY Randall Buss

DATE Feb 1, 1983

REPORT MONTH January 1983

TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
83-1	830104	S	0.0	B	5		CB	ZZZZZZ	Load reduction in preparation for performance of Recirculation Flow Drop Test
83-2	830109	S	0.0	B	5		HA	XXXXXX	Reduced load to perform weekly Turbine tests
83-3	830116	S	0.0	B	5		HA	XXXXXX	Reduced load to perform weekly Turbine tests
83-4	830123	S	0.0	B	5		HA	XXXXXX	Reduced load to perform weekly Turbine tests
83-5	830126	F	0.0	B	5		HH	PUMPXX	Load reduction to change Condensate pumps
83-6	830127	F	0.0	B	5		MB	RECOMB	Load reduction due to steam leak in 1B Off Gas Recombiner
83-7	830129	S	0.0	B	5		HA	XXXXXX	Reduced load to perform weekly Turbine tests

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AUG 16 1982
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APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 6
August 1982

DOCKET NO. 050-265

UNIT NAME Quad-Cities Unit Two

COMPLETED BY Randall Buss

DATE Feb 1, 1983

REPORT MONTH January 1983

TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
83-1	830105	F	0.0	B	5		HC	XXXXXX	Reduced load to change Steam Jet Air Ejectors due to steam leak.
83-2	830105	F	0.0	H	5		HC	XXXXXX	Reduced load to change Steam Jet Air Ejectors after repair of steam leak
83-3	830106	F	0.0	B	5		HG	DEMINX	Load reduction due to Condensate Demineralizer problems
83-4	830106	F	0.0	A	5	83-2/03L	HG	DEMINX	Load reduction due to high Reactor Water Conductivity
83-5	830107	S	0.0	H	5		RB	CONROD	Load reduced to perform Control Rod pattern adjustments
83-6	830111	F	10.7	H	3		ZZ	ZZZZZZ	Reactor isolation signal and subsequent scram on erroneous High Steam Line Flow signal due to contractor personnel jarring an instrument rack

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APPENDIX D
UNIT SHUTDOWNS AND POWER REDUCTIONS

QTP 300-S13
Revision 6
August 1982

DOCKET NO. 050-265

UNIT NAME Quad-Cities Unit Two

COMPLETED BY Randall Buss

DATE Feb 1, 1983

REPORT MONTH January 1983

TELEPHONE 309-654-2241

NO.	DATE	TYPE F OR S	DURATION (HOURS)	REASON	METHOD OF SHUTTING DOWN REACTOR	LICENSEE EVENT REPORT NO.	SYSTEM CODE	COMPONENT CODE	CORRECTIVE ACTIONS/COMMENTS
83-7	830114	F	0.0	B	5		HG	DEMINX	Load reduction due to Condensate Demineralizer problems
83-8	830115	F	0.0	H	5		HC	ZZZZZZ	Load reduction due to high Condenser backpressure
83-9	830115	F	0.0	H	5		HC	ZZZZZZ	Load reduction due to high Condenser backpressure
83-10	830117	F	0.0	B	5		CB	VALVEX	Load reduction to perform maintenance on a Recirculation Loop Crosstie Equalizer valve
83-11	830118	F	0.0	B	5		HF	PUMPXX	Reduced load to take 2C Circulation Water Pump out of service
83-12	830128	S	0.0	B	5		HF	PUMPXX	Load reduced in preparation of unit Maintenance Outage to repair 2C Circulation Pump casing
83-13	830128	S	77.5	B	2		HF	PUMPXX	Unit shutdown for Maintenance Outage

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VI. UNIQUE REPORTING REQUIREMENTS

The following items are included in this report based on prior commitments to the commission:

A. MAIN STEAM RELIEF VALVE OPERATIONS

There were no Main Steam Relief Valve Operations for the reporting period.

B. CONTROL ROD DRIVE SCRAM TIMING DATA FOR UNITS ONE AND TWO

There was no Control Rod Drive Scram Timing Data for Units One and Two for the reporting period.

VII. REFUELING INFORMATION

The following information about future reloads at Quad-Cities Station was requested in a January 26, 1978, licensing memorandum (78-24) from D. E. O'Brien to C. Reed, et al., titled "Dresden, Quad-Cities, and Zion Station--NRC Request for Refueling Information", dated January 18, 1978.

QTP 300-S32
Revision 1
March 1978

QUAD-CITIES REFUELING INFORMATION REQUEST

*

1. Unit: Q1 Reload: 6 Cycle: 7

2. Scheduled date for next refueling shutdown: 9-6-82

3. Scheduled date for restart following refueling: 12-18-82

4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment: Yes

5. Scheduled date(s) for submitting proposed licensing action and supporting information: 8-19-82: Tech. Spec. changes submitted to the NRC.

6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:
   a) All 7x7 fuel assemblies will be removed from the core.
   b) MAPLHGR curves for fuel types in the core are being extended to 40,000 MWD/ST.
   c) MCPR limits will be determined by GE's ODYN computer code.
   d) The vessel pressure safety limit is being modified to accommodate the potential for higher reactor pressures as calculated by ODYN.

7. The number of fuel assemblies.

   a. Number of assemblies in core: 724

   b. Number of assemblies in spent fuel pool: 800

8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:

   a. Licensed storage capacity for spent fuel: 3657

   b. Planned increase in licensed storage: 0

9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity: 2003

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Q.C.O.S.R.

QTP 300-S32
Revision 1
March 1978

QUAD-CITIES REFUELING INFORMATION REQUEST

*

1. Unit: Q2 Reload: 6 Cycle: 7

2. Scheduled date for next refueling shutdown: 9-11-83

3. Scheduled date for restart following refueling: 11-20-83

4. Will refueling or resumption of operation thereafter require a technical specification change or other license amendment:
   Depending upon the Licensing analyses, a MCPR limit change may be needed.

5. Scheduled date(s) for submitting proposed licensing action and supporting information: 8-22-83 (if necessary)

6. Important licensing considerations associated with refueling, e.g., new or different fuel design or supplier, unreviewed design or performance analysis methods, significant changes in fuel design, new operating procedures:
   NFS intends to apply 10CFR50.59 to the Q2R6C7 reload unless MCPR Technical Specification change is required.

7. The number of fuel assemblies.

   a. Number of assemblies in core: 724

   b. Number of assemblies in spent fuel pool: 1140

8. The present licensed spent fuel pool storage capacity and the size of any increase in licensed storage capacity that has been requested or is planned in number of fuel assemblies:

   a. Licensed storage capacity for spent fuel: 3897

   b. Planned increase in licensed storage: 0

9. The projected date of the last refueling that can be discharged to the spent fuel pool assuming the present licensed capacity: 2003

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APR 20 1978
Q.C.O.S.R.

VIII. GLOSSARY

The following abbreviations which may have been used in the Monthly Report, are defined below:

ACAD/CAM	-	Atmospheric Containment Atmospheric Dilution/Containment Atmospheric Monitoring
ANSI	-	American National Standards Institute
APRM	-	Average Power Range Monitor
ATWS	-	Anticipated Transient Without Scram
BWR	-	Boiling Water Reactor
CRD	-	Control Rod Drive
EHC	-	Electro-Hydraulic Control System
EOF	-	Emergency Operations Facility
GSEP	-	Generating Stations Emergency Plan
HEPA	-	High-Efficiency Particulate Filter
HPCI	-	High Pressure Coolant Injection System
HRSS	-	High Radiation Sampling System
IPCLRT	-	Integrated Primary Containment Leak Rate Test
IRM	-	Intermediate Range Monitor
ISI	-	Inservice Inspection
LER	-	Licensee Event Report
LLRT	-	Local Leak Rate Test
LPCI	-	Low Pressure Coolant Injection Mode of RHRS
LPRM	-	Local Power Range Monitor
MAPLHGR	-	Maximum Average Planar Linear Heat Generation Rate
MCPR	-	Minimum Critical Power Ratio
MFLCPR	-	Maximum Fraction Limiting Critical Power Ratio
MPC	-	Maximum Permissible Concentration
MSIV	-	Main Steam Isolation Valve
NIOSH	-	National Institute for Occupational Safety and Health
PCI	-	Primary Containment Isolation
PCIOMR	-	Preconditioning Interim Operating Management Recommendations
RBCCW	-	Reactor Building Closed Cooling Water System
RBM	-	Rod Block Monitor
RCIC	-	Reactor Core Isolation Cooling System
RHRS	-	Residual Heat Removal System
RPS	-	Reactor Protection System
RWM	-	Rod Worth Minimizer
SBGTS	-	Standby Gas Treatment System
SBLC	-	Standby Liquid Control
SDC	-	Shutdown Cooling Mode of RHRS
SDV	-	Scram Discharge Volume
SRM	-	Source Range Monitor
TBCCW	-	Turbine Building Closed Cooling Water System
TIP	-	Traveling Incore Probe
TSC	-	Technical Support Center