
Technical Guidance for Siting Criteria Development

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Commission

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FOREWORD

On July 29, 1980 an advance notice of rulemaking was published for the siting of nuclear power reactors. One of the principle elements contained in the advance notice was the development of a comprehensive analysis of all technical issues relevant to siting. Sandia National Laboratories was contracted by the Nuclear Regulatory Commission to perform the analysis and document the technical guidance to support the formulation of new regulations. This report completes the effort to provide the technical guidance.

The work has been primarily focused toward the development of generic siting criteria, uncoupled from specific plant design. To achieve this end, the NRC staff developed a representative set of severe accident release source terms which covers the full spectrum of postulated severe accident releases for typical light water reactors. NUREG-0773, "The Development of Severe Reactor Accident Source Terms: 1975-1981," provides the detailed description of the considerations that went into the development of the spectrum of source terms (SSTs) in general terms; a more specific discussion of the concept of a representative or generic spectrum of source terms is given in pages 6 through 21 of NUREG-0771, "Regulatory Impact of Nuclear Reactor Accident Source Term Assumptions." From the results of Probabilistic Risk Assessments available at the time of the preparation of this report, the NRC staff would assign typical probability values to the source terms for a range of light water reactor designs as follows:

Probability of SST1 release	1×10^{-5} /reactor year
Probability of SST2 release	2×10^{-5} /reactor year
Probability of SST3 release	1×10^{-4} /reactor year

Table 2.3.1-3 presents the comparative impact of these releases in terms of public health effects. These ratios indicate the relative importance of the source terms given equal probability of occurrence. Their absolute and relative probabilities of occurrence affect their significance for the selection of siting criteria.

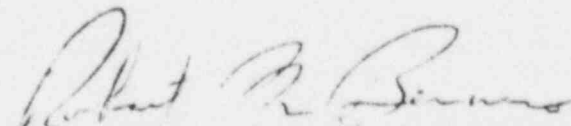
There are very large uncertainties associated with these numbers. The absolute values and the ratios of these probabilities for a given facility are design specific. To accurately portray the risk, very specific accident sequence probabilities and source terms are needed. Thus, the results presented in this report do not represent nuclear power risk.

The siting source terms were used to calculate accident consequences at 91 U. S. reactor sites using site specific meteorology and population data and assuming an 1120 MWe reactor. These calculations treat siting factors such as weather conditions and emergency response probabilistically but postulate the siting source term release. The results are thus conditional consequence values.

Currently there is significant controversy about the realism of accident source terms, that is, the accuracy with which they describe potential releases of radioactivity for a given sequence of events in a core melt accident. The work done to date on siting uses the source terms developed for the Reactor Safety Study, held unchanged by newer projections as explained in NUREG-0772, "Technical Bases for Estimating Fission Product Behavior During LWR Accidents." The staff expects newer information to be available by mid 1983 to modify these source terms. In the meanwhile, sensitivity analyses are given to explore how the calculated consequence values would change with various source term reductions.

Contained in this report are sensitivity studies for the major parameters important to siting decision making. Only through consideration of material such as this can reasoned decisions be made concerning recommendations for improved siting regulations.

This report represents some of the work being done to support the expanding use of probabilistic risk assessment in the regulatory process. The NRC must be careful with the results of such analyses, considering the very large uncertainties in the results. The studies shown in this report must be used in a manner that is consistent with the stated objectives. The results are to provide technical perspective on siting-related issues. Results presented in this report are not significantly different than results of consequence studies that have been available in the open literature for decades. Given the source term assumptions, large consequences are calculated. However, the risks (probabilities times consequences) posed by such accidents are very small. Therefore, the absolute numbers should only be quoted with the associated probabilities and with the stated assumptions recognizing the uncertainties in the analyses.



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Abstract

Technical guidance to support the formulation and comparison of possible siting criteria for nuclear power plants has been developed for the Nuclear Regulatory Commission by Sandia National Laboratories. Information has been developed in four areas: (1) consequences of hypothetical severe nuclear power plant accidents, (2) characteristics of population distributions about current reactor sites, (3) site availability within the continental United States, and (4) socioeconomic impacts of reactor siting.

The impact on consequences of source term magnitude, meteorology, population distribution and emergency response have been analyzed. Population distributions about current sites were analyzed to identify statistical characteristics, time trends, and regional differences. A site availability data bank was constructed for the continental United States. The data bank contains information about population densities, seismicity, topography, water availability, and land use restrictions. Finally, the socioeconomic impacts of rural industrialization projects, energy boomtowns, and nuclear power plants were examined to determine their nature, magnitude, and dependence on site demography and remoteness.

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1. Introduction and Summary

1.1 Introduction

At the request of the Nuclear Regulatory Commission, Sandia National Laboratories has performed a study to develop technical guidance to support the formulation of new regulations for siting nuclear power reactors [1]. Guidance was requested regarding (1) criteria for population density and distribution surrounding future sites, and (2) standoff distances of plants from offsite hazards. Studies were performed in each of these two areas of concern.

The study of offsite hazards had two areas of concern: (1) determination of which classes of offsite hazards are amenable to regulation by fixed standoff distances, and (2) review of available methods for the determination of appropriate standoff distances. The hazards considered included aircraft, hazardous chemicals, dams, faults, adjacent nuclear power plants, tsunamis, meteorite impact, etc. The study concluded that none of the hazards are suitable to treatment by fixed standoff distances and that sufficient methods exist for evaluating the risk for most types of hazards. Because they have been published elsewhere [2], the results of the study of offsite hazards are not included in this report.

The studies of site characteristics, which are presented in this report, involved analyses in four areas, each of which could play a role in evaluating the impact of a siting policy. The four areas were: (1) consequences of possible plant accidents, (2) population distribution characteristics for existing sites, (3) availability of sites, and (4) socioeconomic impacts.

Accident consequence analyses were performed to help define the risks associated with existing sites and with alternative siting criteria. Consequence analyses also help to evaluate the dependence of risk on factors such as meteorology, population distribution, and emergency response which can be mandated or constrained by regulations. Population distributions at existing sites were examined to provide perspective on demographic characteristics as well as to determine whether there have been trends with time or regional differences in site selection. The site availability

analysis examined the impact of various population distribution criteria on the amount of land restricted from siting. Impacts of environmental and legal constraints were also examined. In addition, studies were performed to evaluate the extent of socioeconomic impacts and the degree to which they are dependent on site demographic characteristics. These four areas of analysis provide information that could be used to assess and compare alternative siting criteria.

The information developed by this study is presented in four chapters and six appendices. Chapter 2 presents the results of the consequence analyses that were performed to identify factors that have a significant impact upon risk. The factors examined include source term magnitude (Section 2.3), meteorology (Section 2.4.1), population (Section 2.4.2), emergency response (Section 2.5), consequence distances (Section 2.6), reactor size (Section 2.7.1), plume heat content (Section 2.7.2), dry deposition velocity (Section 2.7.3), characteristics of population distributions (Section 2.7.4), and criteria for the interdiction of contaminated land (Section 2.7.5). CRAC2 [3,4], the computer model used to perform these consequence analyses, is described briefly in Section 2.2.1 and more fully in Appendix E. Model input data are described in Section 2.2.2. Site specific input data are presented in Appendix A and core radionuclide inventory data in Appendix B. Data and model uncertainties are discussed in Section 2.2.4. Finally, a series of site specific calculations were made using a standard set of source terms uncorrected for the characteristics of the reactor at the site. The results of these calculations are presented in Appendix C.

Chapter 3 and Appendix D present an examination of the population distributions surrounding existing sites to provide perspective on demographic characteristics and to determine (1) whether there is evidence of a trend over time to less-dense siting and (2) whether site characteristics differ significantly in different regions of the country. The site availability analyses developed a capability for measuring the impact of population criteria on the availability of reactor sites. Also considered in these analyses were the seismicity, topographic character, availability of surface and ground water at potential sites, and the restriction of power plant siting because of the presence of

national parks or wilderness areas. This study, which was performed by Dames and Moore [5] under contract to Sandia, is presented in full in Chapter 4 and Appendix F. Finally, a study was performed to examine the socioeconomic impacts of reactor siting and the dependence of the magnitude of these impacts on site demography. The study examined impacts caused by large construction projects, energy boomtowns, and the construction of nuclear power plants. Also examined was the impact of site remoteness on transmission costs. The study, performed by Battelle-HARC under contract to Sandia, is summarized in Chapter 5 and presented in full in a separate report [6].

1.2 Summary

This report contains the results of numerous calculations and analyses performed at Sandia National Laboratories, Dames and Moore, and Battelle-HARC. The principal results or conclusions reached are:

- o Estimates of the number of early fatalities are very sensitive to source term magnitude. Mean early fatalities (average result for many weather sequences) are decreased dramatically (about two orders-of-magnitude) by a one order-of-magnitude decrease in source term SST1 (large core melt, loss of most safety systems). Because the core melt accident source terms SST1-3 used in this study neglect or underestimate several depletion mechanisms, which may operate efficiently within the primary loop or the containment, consequence magnitudes calculated using these source terms may be significantly overestimated.
- o The weather conditions at the time of a large release will have a substantial impact on the health effects caused by that release. In marked contrast to this, mean health effects (average result for many weather sequences) are relatively insensitive to meteorology. Over the range of meteorological conditions found within the continental United States (1 year meteorological records from 29 National Weather Service stations), mean early fatality values for a densely populated site show a range (highest value/lowest value) of only a factor of 2, and mean latent cancer fatalities a factor of 1.2.

- o Peak early fatalities (maximum value calculated for any weather sequence) are generally caused by rainout of the radioactive plume onto a population center. For an SST1 release, the peak result is about 10-times less probable in a dry locale than in a wet one.
- o The distances to which consequences might occur depend principally upon source term magnitude and meteorology. Frequency distributions of these distances, calculated using large numbers of weather sequences, yielded expected (mean), 99 percentile, and maximum calculated distances (expressed in miles) for early fatalities, early injuries, and land interdiction as follows:

Source Term	Consequence	Mean	99%	Maximum Calculated
SST1	Early Fatalities	<5	≤15	<25
	Early Injuries	~10	~30	≤50
	Land Interdiction	~20	>50	>50
SST2	Early Fatalities	~0.5	<2	<2
	Early Injuries	<2	<5	~5
	Land Interdiction	<2	~7	~10

The maximum calculated distances are associated with improbable events, (e.g., rain-out of the plume onto a population center). For the SST1 release reduced by a factor of 10, early fatalities are confined to ~5 miles, early injuries to ~20 miles, and interdiction of land to ~25 miles.

- o Calculated consequences are very sensitive to site population distribution. For each of the 91 population distributions examined, early fatality, early injury, and latent cancer fatality CCDFs were calculated assuming an SST1 release from an 1120 MWe reactor. The resulting sets of CCDFs had the following ranges:

Early Fatalities. ~3 orders-of-magnitude in the peak and mean numbers of early fatalities and in the probability of having at least one early fatality.

Early Injuries. ~ 3 orders-of-magnitude in the means, ~2 in the peaks, and ~1 in the probability of having at least one early injury.

Latent Cancer Fatalities. ~1 order-of-magnitude in the peaks and the means and in the probability of having at least one latent cancer fatality.

Generally, mean results are determined by the average density of the entire exposed population, while peak results (especially for early fatalities) are determined by the distance to and size of exposed population centers.

- o Early fatalities and early injuries can be significantly reduced by emergency response actions. Both sheltering (followed by relocation) and evacuation can be effective provided the response is expeditious. Access to basements or masonry buildings significantly enhances the effectiveness of sheltering. Expeditious response requires timely notification of the public. If the evacuation is expeditious (timely initiation), evacuation speeds of 10 mph are effective. Evacuation before containment breach within 2 miles, after release within 10 miles, and sheltering from 10 to 25 miles appears to be a particularly effective response strategy.
- o Population densities (people/sq mi) about the 91 sites have the following maximum, 90th percentile and median values within the indicated distance intervals:

<u>Distance (mi)</u>	<u>0-5</u>	<u>0-10</u>	<u>0-20</u>
<u>Full Circle</u>			
Maximum	790	660	710
90th percentile	190	230	380
Median	40	70	90
<u>Most Populated 22.5° Sector</u>			
Maximum	4200	3800	4500
90th percentile	950	1000	1800
Median	330	270	480

- o At the 91 sites examined, the distance to the nearest exclusion zone boundary ranges from 0.1 to 1.3 miles and averages about 0.5 miles.
- o There appears to be a slight trend with time towards selection of reactor sites in less densely populated locations.
- o A site availability data base has been constructed on a 5 x 5 km grid cell for the continental United States. For each grid cell the data base contains information on population density, seismicity, topographic character, surface and ground water availability, and land use restrictions (wetlands, national parks, etc.)
- o Analysis of boomtown literature, studies of large non-nuclear energy projects, and economic data from existing nuclear power plant sites suggests that only siting in very remote regions has the potential for significant socioeconomic impacts, that these impacts may be both beneficial or detrimental and that the detrimental impacts can be mitigated by advance planning.
- o Outside of the Rocky Mountains, few potential reactor sites are located at a large distance from the national power grid. Consequently, site remoteness and transmission line costs are not strongly correlated.

This study examined a number of factors which could impact the development of siting criteria. The analyses, which are reported in the following chapters, can be used to determine many of the impacts of alternative criteria, and provide guidance in evaluating tradeoffs among criteria. In addition, the data and analyses contained in the study should be useful to the wider community of users interested in evaluating the consequences of reactor accidents.

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2. Consequences of Potential Reactor Accidents

2.1 Introduction

During this study, a large number of calculations were performed to provide a basis for understanding the dependence of reactor accident consequences on site characteristics. Some characteristics were examined because of the possibility of their inclusion in reactor siting criteria (e.g., population distribution, reactor power level). A number of additional parameters were investigated to determine the sensitivity of predicted consequences to variation or uncertainty in data used as input.

All consequence calculations for this study were performed using CRAC2, an improved version of CPAC,^a the Reactor Safety Study [1] consequence model. Section 2.2.1 provides a brief overview of the CRAC2 model, while Section 2.2.2 describes the data used as input to the consequence calculations. Section 2.2.3 is a qualitative discussion of the sources and impacts of uncertainties associated with the consequence model. Section 2.2.4 defines the "base case" calculation which was used as a reference case for examination of the impact of variations in parameters and assumptions.

Section 2.3 briefly describes the five accident source terms used in the calculations. These source terms, denoted SST1-5, were developed by NRC and range from a full core-melt with uncontrolled release to a gap release with minimal leakage. Section 2.3.1 presents results of consequence calculations for each of the five source terms, and Section 2.3.2 examines the potential impact on consequences of reductions in the magnitude of the most severe accident (SST1).

Section 2.4 examines the impact of meteorology and population on consequence estimates. Meteorological data from 29 National Weather Service stations and wind rose and population data from each of the 91 currently approved reactor sites in the United States are examined. Section 2.5 presents the impact on consequences of various emergency response assumptions; both evacuation and sheltering scenarios are evaluated. Section 2.6 discusses the distances to which various consequences occur and the sensitivity of these distances to input

a. CRAC stands for Calculation of Reactor Accident Consequences.

data and assumptions. Section 2.7 examines the sensitivity of consequences to variations in reactor size, energy-release rate, dry deposition velocity, population distribution, and land-interdiction criteria. Finally, Section 2.8 presents a summary of the insights gained from these calculations.

2.2 Background

2.2.1 Overview of Consequence Model

The accident consequence calculations described in this chapter were performed using CRAC2 [2,3], an improved version of the Reactor Safety Study (WASH-1400) consequence model, CRAC [1,4]. Modifications made in the upgrade from CRAC to CRAC2 are briefly described in Appendix E.^a The model describes the progression of the cloud of radioactive material released from the containment structure during and following a reactor accident, and predicts its interaction with and influence on the environment and man. A schematic outline of the computational steps taken in the model is presented in Figure 2.2.1-1.

Analyses of potential plant system failures and accident phenomenology provide an estimate of accident probabilities and release characteristics (magnitudes, timing, etc.) that are used as input to the consequence model.^b Given these estimates, a standard Gaussian dispersion model is used to calculate ground-level concentrations of airborne radioactive material downwind of the reactor site. Weather data for a 1-year period are input to the dispersion model in the form of hourly recordings of wind speed, thermal stability, and accumulated precipitation. The wind direction is assumed to be invariant during and following the release. Radionuclide concentrations within the cloud are depleted by deposition (both wet and dry) and radioactive decay, and integrated air and ground contamination are calculated for downwind distances.

a. Results calculated using the two models are similar, as shown in the recent International Comparison Study of Reactor Accident Consequence Models [5,6].

b. Specific release characteristics assumed in this study are described in Section 2.3.

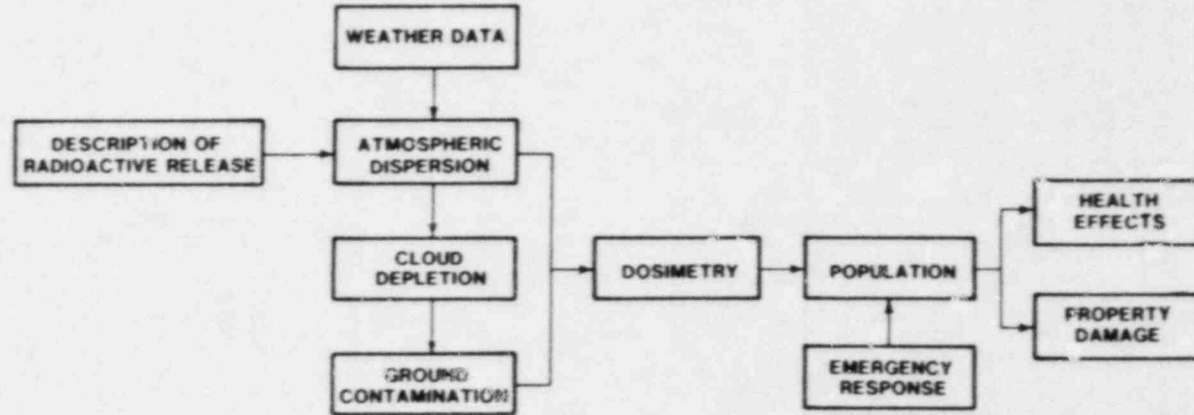


Figure 2.2.1-1. Schematic Outline of Consequence Model, CRAC2.

Hourly weather recordings are used to account for weather variations during the progression of the accident. Beginning at a selected hour within the year's data, the dispersion model uses the subsequent meteorological conditions to predict the dispersion, downwind transport, and deposition of the released cloud of radioactive material. Hourly recordings are sequentially incorporated until all of the released radioactive material (excluding the noble gases) has been deposited. By using an appropriate sample of weather sequences from the year's data, a frequency distribution of estimated consequences can be produced.

The consequence model uses the calculated airborne and ground radionuclide concentrations to estimate the public's exposure to external radiation from (1) airborne radionuclides in the cloud and (2) radionuclides deposited from the cloud onto the ground, and internal radiation from (1) radionuclides inhaled directly from the passing cloud, (2) inhaled resuspended radionuclides, and (3) the ingestion of contaminated food and milk. Radiation exposure from sources external to the body is calculated for time periods over which individuals are exposed to those sources, while the exposure from sources internal to the body is calculated over the remaining life of the exposed individual.

The consequence model allows the input of either site-specific or hypothetical population data as a function of distance and direction from the reactor site. A simple evacuation model is incorporated, which is based on a statistical analysis of evacuation data assembled by the U.S. Environmental Protection Agency [7-9] (see Appendix E). The model incorporates a delay time before public movement, followed by evacuation radially away from the reactor. A range of evacuation delay times, speeds, and distances have been assumed in this study, as is described in later sections.

Based on the calculated radiation exposure to downwind individuals, the consequence model estimates the number of public health effects that would result from the accidental release. Early injuries and fatalities, latent cancer fatalities, and thyroid and genetic effects may be computed. Early fatalities are defined to be those fatalities that occur within 1 year of the exposure period. They are estimated on the basis of exposure to the bone marrow, lung and gastrointestinal tract. Bone marrow damage is the dominant contributor to early

fatalities. In both the Reactor Safety Study and this study, early fatalities are calculated assuming an $LD_{50/60}^a$ of 510 rads to the bone marrow. Supportive medical treatment of the exposed individual is also assumed. Early injuries are defined as non-fatal, non-carcinogenic illnesses, that appear within 1 year of the exposure and require medical attention or hospital treatment. The late somatic effects considered include latent cancer fatalities plus benign and malignant thyroid nodules.

The consequence model also includes an economic model to estimate the potential extent of property damage associated with the release of radioactive material. The total offsite dollar cost of the accident is estimated as the sum of (1) the evacuation cost, (2) the value of condemned crops and milk, (3) the cost of decontaminating land and structures, (4) the cost of interdicting land and structures, and (5) relocation costs (moving costs and temporary loss of income).

2.2.2 Input Data for Consequence Model

CRAC2 requires a large set of input data, including accident release characteristics and source terms, various site-related data (e.g., meteorology, population), reactor core radionuclide inventories, and emergency response scenarios. The accident release characteristics and source terms assumed in this study are described in Section 2.3.

The site-related data, gathered for use in this study, are presented in Appendix A. The data gathered includes:

1. General site and reactor data (e.g., reactor size, vendor, start-up date, site location) for each of the 91 U.S. sites at which a reactor is operating or a construction permit has been obtained.
2. Regional shielding factors for sheltered populations.
3. Site population data derived from the 1970 census.

a. The dose that would be lethal to 50 percent of the population within 60 days.

4. Meteorological data consisting of hourly recordings of weather conditions from 29 National Weather Service stations plus mixing heights from Holzworth [10].
5. Annual site wind roses obtained from either Environmental Impact Reports or Safety Analysis Reports.
6. Site economic data, updated from those used in WASH-1400 to reflect inflation and changing economic conditions.

A core radionuclide inventory for a 3412 MWt (1120 MWe) reactor was calculated for this study using the SANDIA-ORIGEN [11] computer code. This calculation assumed an end-of-cycle fuel burnup of 33,000 MWd/MTU (about 25 percent greater than was assumed in WASH-1400) which is representative of the current generation of larger reactors. Differences in reactor size were accommodated by linearly scaling the inventory with rated thermal power level. A description of the inventory calculations and a discussion of the impact of inventories on predicted consequences are presented in Appendix B. The sensitivity of consequences to reactor size is examined in Section 2.7.1.

The emergency response submodel incorporated in CRAC2 is described in Section 2.5 and Appendix E. The model allows specification of up to six emergency response scenarios plus a weighted sum of these scenarios termed "Summary Evacuation." Unless otherwise specified, calculations were performed using the scenarios presented in Table 2.2.2-1. The scenarios range from a prompt evacuation to sheltering to no emergency response. The response distance of 10 miles was selected to coincide with the Emergency Planning Zone (EPZ) recommended by the NRC [12]. The delay times and speeds assumed were based on a statistical analysis of evacuation data gathered by the EPA (see Appendix E). The "Summary Evacuation" was defined as a 30 percent, 40 percent, 30 percent weighting^a of scenarios 1, 2, and 3, and

a. Thirty percent of the time, all people within 10 miles evacuate with a 1 hour delay and 10 mph speed; 40 percent of the time, all people within 10 miles evacuate with a 3-hour delay and 10 mph speed; and 30 percent of the time all people within 10 miles evacuate with a 5-hour delay and 10 mph speed.

represents a "best estimate" for consequence predictions. Most of the results presented in the following sections assumed this "Summary Evacuation." The sensitivity of predicted consequences to emergency response assumptions is examined in Section 2.5. Differences in emergency response due to site-specific characteristics were not addressed.

Table 2.2.2-1. Emergency Response Scenarios

Scenario Number	Type of Response	Response Distance	Delay Time Before Response	Response Speed
1	Evacuation	10 miles	1-hour	10 mph
2	Evacuation	10 miles	3-hours	10 mph
3	Evacuation	10 miles	5-hours	10 mph
4	Evacuation	10 miles	5-hours	1 mph
5	Sheltering, Relocation	10 miles	none, 6-hours	---
6	No Emergency Response	--	--	---

2.2.3 Uncertainties

Uncertainties in offsite consequence predictions stem principally from uncertainties in two areas: modeling and input data. Modeling uncertainty arises from (1) an incomplete understanding of the phenomena involved in the transport of released radionuclides to man and the consequent health impacts, and (2) simplifications of phenomena made in the modeling process to reduce costs or model complexity. Input data uncertainty arises from problems associated with the quality and availability of

data, selection or determination of appropriate values for model input (including radioactive source terms), and statistical variations in data. To date, a comprehensive assessment of these uncertainties in consequence predictions has not been performed. However, a number of partial uncertainty estimates have been derived using sensitivity analysis techniques [1,13,14].

Improvements in a number of model areas could substantially reduce current uncertainties. The most important of these include source terms (see Section 2.3), plume depletion processes (see Section 2.7.3), the effect of wind trajectories on population exposures, and the effectiveness of emergency response (see Section 2.5). Each of these areas is briefly described below.

Radioactive source terms for atmospheric releases are subject to a number of important uncertainties, including uncertainties about release magnitude and timing, and about aerosol size distributions. It has been suggested [15,16] that removal processes within the primary coolant system and containment could reduce the amount of material released to the atmosphere to levels significantly below those currently estimated. Possible removal processes include plate-out of hot vapors on cooler surfaces, agglomeration and deposition of aerosols, and dissolution in water. Better specification of the timing of a release is important for two reasons: (1) a longer warning period increases the chance of an effective emergency response and (2) a long, slow release spreads the radioactive material over a larger area, thereby decreasing individual doses and (usually) health effects. The particle-size distribution of the released material, and thus the efficiency of dry deposition processes during downwind transport, is determined principally by aerosol agglomeration rates. Resolution of these source-term uncertainties by ongoing or future research activities may require a reevaluation of some of the conclusions reached by this study. For example, some of the conclusions about emergency planning and response presented in Section 2.5 could be significantly altered.

A plume of radioactive material may be depleted during transport by dry deposition and/or washout processes. The dry-deposition removal rate is strongly dependent on the size distribution of particulate matter in the plume. Therefore, the current lack of information about this size distribution prevents reliable modeling

of dry deposition. Since washout of material by rainfall is a very efficient removal mechanism, it is important to account for the frequency, intensity, and spatial variability of rainfall. Moreover, because high-consequence events are usually associated with rainfall over population centers, failure to adequately model rainfall can lead to large inaccuracies in predicted peak consequences.

Wind trajectories determine the specific population exposed by downwind transport of the plume of radioactive material. With the exception of the computer code CRACIT [17,18], current consequence models neglect wind trajectories. Although results obtained with CRACIT indicate that treatment of wind trajectories may affect risk less than intuition suggests [6], a thorough examination of this subject (perhaps using a Gaussian puff model), particularly for sites with complex terrain, seems essential [19].

The sensitivity of predicted consequences to different emergency response scenarios is examined in Section 2.5. If consequence models are to be applied to evaluate the risk at specific sites, consideration should be given to those characteristics of the site and of local organizations that could influence the effectiveness of offsite emergency response. For example, local and utility emergency response plans, available mechanisms for warning the public, and characteristics of the surrounding road network should be examined. Road networks could be particularly important if population densities are sufficient to result in "traffic jams" or "bottleneck" conditions, or if terrain features are likely to cause evacuation routes and the plume trajectory to overlap.

Another area of uncertainty is the estimation of the late somatic effects, of which the incidence of cancer is the most important. The recent BEIR III report [20] discusses these uncertainties, which are largest for low doses (and dose rates) of low-LET radiation. In addition, Loewe and Mendelsohn [21] have recently conducted a reassessment of the dosimetry data for the populations exposed by the detonations at Hiroshima and Nagasaki. These new findings have led to major changes in the estimates of the neutron and gamma-ray doses received by survivors. Efforts are currently underway at the Los Alamos National Laboratory to redefine the source terms from the two detonations

and at Oak Ridge National Laboratory to recalculate dose estimates. When completed, these reassessments may result in some changes in estimates for late somatic effects.

2.2.4 Base Case Calculation

The results of a large number of calculations are presented in Sections 2.3 through 2.7 of this report. These calculations examine the impact on predicted consequences of a wide variety of parameters and assumptions. To simplify the examination of the impact of variations in input parameters and assumptions, a "base case" calculation was defined. Assumed in the base case were:

- * a standard 1120 MWe PWR
- * an SST1 release (defined in Section 2.3)
- * New York City meteorology
- * the Indian Point wind rose and population
- * Summary Evacuation

The values of all other input parameters were those typically used in CRAC2. The sensitivity of predicted consequences to the base case assumptions and to other input parameter values is discussed in later sections.

2.3 Reactor Accident Source Terms

This section describes the reactor accident source terms used to perform the consequence calculations. Consequences that might result from these source terms are compared and the most important source terms are identified. In addition, source term uncertainties are addressed. Results that show the impacts of these uncertainties on reactor accident consequences are presented and discussed.

2.3.1 Accident Release Characteristics and Source Terms

The Nuclear Regulatory Commission recently sponsored an evaluation of the technical bases for reactor accident source term assumptions and the potential impact of possible source term changes on the regulatory process [16,22]. These studies found that the Design Basis Accidents (DBAs), which have been the basis for regulatory policies governing nuclear power plant siting and design, do not constitute a realistic representation

of the full spectrum of possible accident source terms for any reactor design. Therefore, they do not provide an adequate estimate of reactor risk at specific sites. Consequently, after review of current source term information, the NRC defined a spectrum of accidents [22], which more adequately spans the range of possible accident source terms and better reflects current understanding of fission product behavior during reactor accidents.

The spectrum of accidents that was defined ranges from accidents within the design basis envelope to core melt accidents which may release large quantities of radioactive material to the environment. Five accident groups were designated as being representative of the spectrum of potential accident conditions. Each group represents a different degree of core degradation and of failure of containment safety features. Brief descriptions of the characteristics of the accident types included in each group are presented in Table 2.3.1-1.

For the purpose of decision-making in such areas as siting and emergency response, NRC defined a set of five Siting Source Terms (denoted SST1-5) to represent the five accident groups. By adjusting the probabilities associated with each of the five source terms, the set can be made to approximately represent any current LWR design.^a Table 2.3.1-2 summarizes the five NRC-defined source terms used in this study.

The consequences that could potentially result from each of the five source terms were determined by performing a series of CRAC2 calculations. Table 2.3.1-3 compares the relative magnitudes (normalized to 100 for source term SST1) of the mean values^b of selected consequences, given the occurrence of each of the five source terms and assuming an 1120 MWe PWR, Indian Point population distribution and wind rose, New York City meteorology, and Summary Evacuation (see Sections 2.2.2 and 2.5 and Appendix E). These results indicate that source terms SST2 through SST5 would not be expected to produce substantial numbers of offsite consequences

a. Detailed Probabilistic Risk Assessments (PRAs) have not been performed for all reactors. Based on currently available PRAs, NRC has suggested that representative probabilities for the SSTs are: P_1 for SST1 = 1×10^{-5} , P_2 for SST2 = 2×10^{-5} , and P_3 for SST3 = 1×10^{-4} . There are very large variations (factors of 10 to 100) in the accident probabilities associated with a specific design.

b. Using approximately 100 sampled weather sequences, the CRAC2 code calculates frequency distributions for consequences that might result from a radioactive release. The means of these distributions are the mean values referred to in the text.

compared to the SST1 source term. The mean consequences calculated for the SST1 release exceed those from the SST2 release by 1 to 4 orders of magnitude and exceed those from releases SST3, SST4, and SST5 by 4 to 7 orders of magnitude. Early fatalities, early injuries, and land interdiction do not result from releases SST3, SST4, and SST5 because these accidents do not release enough radioactivity to produce doses that exceed the dose thresholds for these consequences.

Table 2.3.1-1. Brief Descriptions Characterizing the Accident Groups Within the NRC "Accident Spectrum" [22]

Group 1	Severe core damage. Essentially involves loss of all installed safety features. Severe direct breach of containment.
Group 2	Severe core damage. Containment fails to isolate. Fission product release mitigating systems (e.g., sprays, suppression pool, fan coolers) operate to reduce release.
Group 3	Severe core damage. Containment fails by basement melt-through. All other release mitigation systems function as designed.
Group 4	Modest core damage. Containment systems operate in a degraded mode.
Group 5	Limited core damage. No failures of engineered safety features beyond those postulated by the various design basis accidents. The most severe accident in this group assumes that the containment functions as designed following a substantial core melt.

Table 2.3.1-2. NRC Source Terms for Siting Analysis

<u>Release Characteristics^a</u>	<u>Source Term</u>				
	<u>SST1</u>	<u>SST2</u>	<u>SST3</u>	<u>SST4</u>	<u>SST5</u>
Accident Type	Core Melt	Core Melt	Core Melt	Gap Release	Gap Release
Containment Failure Mode	Overpressure	H ₂ Explosion of Loss of Isolation	-	-	-
Containment Leakage	Large	Large	1%/day	1%/day	0.1%/day
Time of Release (hr)	1.5	3	1	0.5	0.5
Release Duration (hr)	2	2	4	1	1
Warning Time (hr)	0.5	1	0.5	-	-
Release Height (meters)	10	10	10	10	10
Release Energy	0	0	0	0	0
<u>Inventory Release Fractions</u>					
Xe-Kr Group	1.0	0.9	6 x 10 ⁻³	3 x 10 ⁻⁶	3 x 10 ⁻⁷
I Group	0.45	3 x 10 ⁻³	2 x 10 ⁻⁴	1 x 10 ⁻⁷	1 x 10 ⁻⁸
Cs-Rb Group	0.67	9 x 10 ⁻³	1 x 10 ⁻⁵	6 x 10 ⁻⁷	6 x 10 ⁻⁸
Te-Sb Group	0.64	3 x 10 ⁻²	2 x 10 ⁻⁵	1 x 10 ⁻⁹	1 x 10 ⁻¹⁰
Ba-Sr Group	0.07	1 x 10 ⁻³	1 x 10 ⁻⁶	1 x 10 ⁻¹¹	1 x 10 ⁻¹²
Ru Group	0.05	2 x 10 ⁻³	2 x 10 ⁻⁶	0	0
La Group	9 x 10 ⁻³	3 x 10 ⁻⁴	1 x 10 ⁻⁶	0	0

a. As defined in the Reactor Safety Study [1].

Table 2.3.1-3. Comparison of Conditional Mean Consequences Predicted for Five Source Terms^{a,b}

<u>Source Term</u>	<u>Mean Early Fatalities</u>	<u>Mean Early Injuries</u>	<u>Mean Latent Cancer Fatalities</u>	<u>Mean Thyroid Nodules</u>	<u>Mean Interdicted Land Area</u>
SST1	100 ^b	100	100	100	100
SST2	1 x 10 ⁻²	0.5	7	3	1
SST3	0	0	2 x 10 ⁻²	5 x 10 ⁻²	0
SST4	0	0	4 x 10 ⁻⁴	8 x 10 ⁻⁵	0
SST5	0	0	4 x 10 ⁻⁵	8 x 10 ⁻⁶	0

a. Assumptions: 1120 MWe PWR, population distribution and wind rose for Indian Point, New York City meteorology, "Summary Evacuation" of persons within 10 miles.

b. All consequences are normalized to 100 for source term SST1.

Figures 2.3.1-1 and 2.3.1-2 present mean bone marrow dose and mean thyroid dose to exposed individuals as a function of distance for each of the five source terms.^a The doses were calculated assuming no emergency response, an 1120 MWe PWR, and New York City meteorology. The mean doses at any distance vary by nearly 8 orders of magnitude over the spectrum of five releases. For any pair of releases, relative doses are roughly proportional to the ratios of curies of released radioactivity excluding noble gases (Xe-Kr group). These figures also show that individual bone marrow and thyroid doses would generally not be expected to exceed a few tens of millirem for the SST4 release and a few millirem for the SST5 release.

Figure 2.3.1-3 displays the variation with distance of the mean individual risks (averaged over 360 degrees^b) of early fatality and early injury for source terms SST1 and SST2, and of latent cancer fatality (from early exposure only^c) for all five source terms. These curves were calculated assuming an 1120 MWe PWR, New York City meteorology, a uniform wind rose, and no emergency response. Because early fatalities and injuries have dose thresholds, their risks of occurrence decrease rapidly with distance for large source terms (e.g., SST1 and SST2) and are zero offsite (≥ 0.25 mi) for small source terms (e.g., SST3, SST4, and SST5). Since no offsite risk of early fatality or injury was predicted for source terms SST3, SST4, or SST5, in Figures 2.3.1-3a and 2.3.1-3b no curves were plotted for these source terms. In contrast to this, because no dose threshold is assumed for latent cancer fatalities, the risk of latent cancer fatality decreases more slowly with distance and is non-zero for all five source terms. Therefore, in Figure 2.3.1-3c a

- a. The doses are the means of the frequency distributions of estimated individual dose calculated using an appropriate sample of weather sequences from a single year of meteorological data.
- b. Individual risks shown are the product of two probabilities: (1) the probability of exposure to the plume given that the release occurs, and (2) the probability that the individual dies following the exposure.
- c. Early exposure includes exposure to the radioactive plume, all exposures resulting from inhalation of radioactive materials from the plume, and short-term exposure to radioactivity deposited on the ground from the plume.

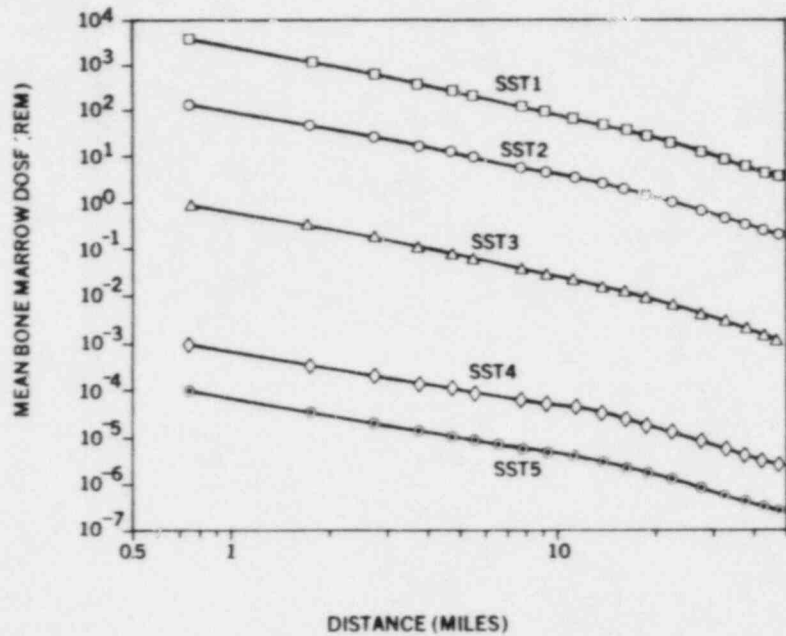


Figure 2.3.1-1. Comparison of Predicted Mean Bone Marrow Dose to Exposed Individuals vs Distance for the Five Source Terms.

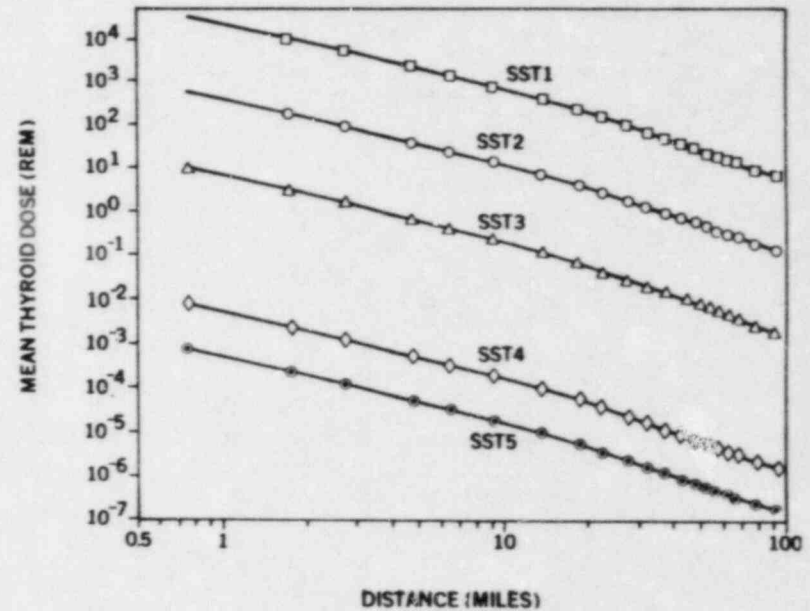


Figure 2.3.1-2. Comparison of Predicted Mean Thyroid Dose to Exposed Individuals vs Distance for the Five Source Terms.

Assumptions: 1120 MWe reactor, New York City meteorology, no emergency response, one day exposure to radionuclides deposited on the ground.

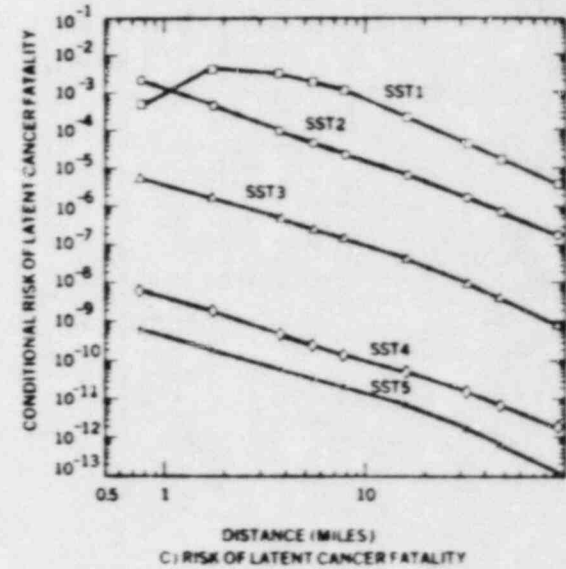
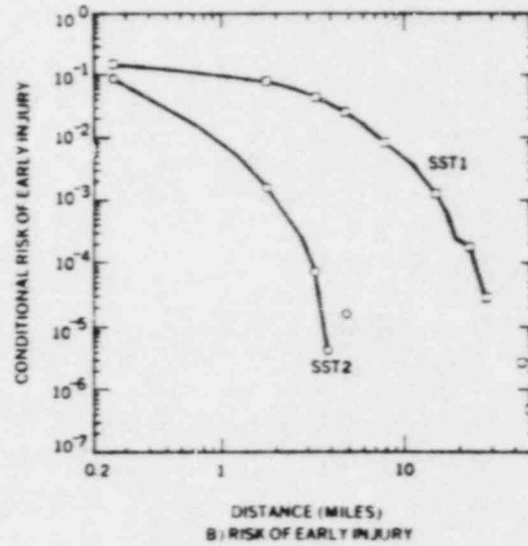
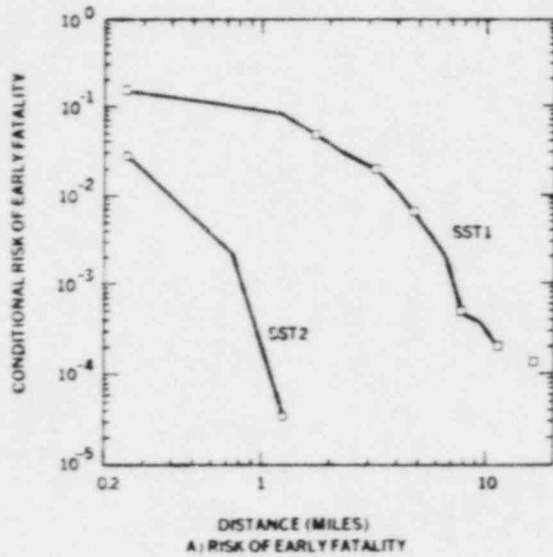


Figure 2.3.1-3. Risk to an Individual of a) Early Fatality, b) Early Injury, and c) Latent Cancer Fatality (from early exposure only) vs Distance Conditional on Each of the Five Siting Source Terms. Assumptions: 1120 MWe PWR, New York City meteorology, no emergency response, and a uniform wind rose.

risk curve is plotted for each source term. The latent cancer risk curve for the SST1 release crosses the risk curve for the SST2 release at short distances. The falloff in the latent cancer fatality risk at short distances (≤ 2 mi) for SST1 is caused by the very high risk of early fatality at these distances. Because of the high early fatality risk, the latent cancer fatality risk is essentially conditional on surviving the high early radiation doses produced close to the reactor by SST1. Finally, comparison of Figure 2.3.1-3c with Figures 2.3.1-1 and 2.3.1-2 shows that the relative differences between the five latent cancer fatality risk curves are similar to those between the five dose vs distance curves for bone marrow or thyroid doses.

Together, the results presented in Table 2.3.1-3 and Figures 2.3.1-1 through 2.3.1-3 show that the SST1 accident would likely dominate overall reactor risk to the public.^a Furthermore, consequences resulting from the SST4 and SST5 accidents were shown to be much smaller than those resulting from the core melt accidents (source terms SST1, SST2, and SST3). Therefore, because these non-melt releases probably have little influence on off-site reactor risk, the SST4 and SST5 releases will not be considered further. In addition, because offsite risk is dominated by the most severe core-melt accidents, the remainder of this chapter will concentrate principally on the SST1 release, although results for the SST2 and SST3 releases will be presented when appropriate.

2.3.2 Uncertainty in Source Term Magnitudes

At present there is a great deal of controversy over the magnitude and nature of source terms for severe reactor accidents. A recent study [15] suggested that source terms for atmospheric releases could be substantially smaller than those assumed in WASH-1400 (or also in this report). The study cited evidence that removal processes, which have generally been neglected but which should operate within the primary coolant system and containment, would decrease the amount of material released following an accident to amounts substantially below those usually assumed. Such removal processes include plate-out of hot vapors, agglomeration and deposition of aerosols, and dissolution of soluble materials in water.

a. This conclusion depends on the relative probabilities of releases.

The effectiveness of these removal processes would be strongly dependent on the conditions inside the coolant system and containment and on the chemical and physical form of the fission products. For example, Campbell et al. [23] suggest that under accident conditions in LWRs, fission product iodine would be in the form of a soluble metallic iodide (probably CsI) rather than volatile, molecular iodine, as is currently assumed. Also, Morewitz [24], after review of past reactor accidents and destructive tests, concluded that in all cases where water was present, no fission product tellurium had been released. Morewitz proposed two explanations for this observation: Either tellurium remains in solution in the form of soluble CsTe₂, or tellurium particles are efficiently scavenged by rapid droplet growth caused by condensation of water vapor. Morewitz further noted that even in the absence of water droplet formation, the generation of large quantities of aerosol from structural materials (steel, concrete, etc.) would produce rates of aerosol agglomeration rapid enough to ensure that a large fraction of the radioactive particles would quickly settle out inside the containment.

These suggestions have received substantial support in a recent NRC report [16]. The significance of these proposals is that the solubility of volatile fission products and potential aerosol removal mechanisms could limit the quantity of released radionuclides to levels one to two orders of magnitude below those currently assumed.

To evaluate the impact on predicted consequences of significant reductions in the amount of released material, a series of calculations was performed with arbitrary reductions in the quantities of released fission products. The impact of potential reductions due to the solubility of fission products in water was evaluated by arbitrarily reducing the release fractions of iodine, cesium, and tellurium^a to 50, 10 and 0 percent of the standard SST1 level, singly,

a. The tellurium release fraction includes both tellurium and antimony and the cesium release fraction includes both cesium and rubidium (see Table 2.3.1-2). Cesium and tellurium, however dominate the predicted consequences for each release group.

in pairs (Cs and I only), and all simultaneously (50 percent reduction only). To evaluate the impact on predicted consequences of potential reductions in source terms due to efficient aerosol removal processes, calculations were performed with the release fraction of all isotopes except noble gases arbitrarily reduced to 50, 10, 5, and 1 percent of the SST1 release.

The results of the calculations are summarized in Tables 2.3.2-1 and 2.3.2-2. Assumed in these calculations were the Indian Point site, New York City meteorology, an 1120 MWe reactor, and Summary Evacuation. The results in Table 2.3.2-1 indicate that a factor of 10 reduction in the release fraction of either iodine or tellurium results only in about a factor of 2 reduction in early effects. Because of the dose-threshold for early effects, this does not imply that iodine or tellurium "account" for half of the early effects.

Table 2.3.2-1 does, however, present a measure of the relative doses resulting from exposure to individual elements. Iodine isotopes account for about 35 percent of the expected acute bone marrow dose and for about 80 percent of the thyroid dose. Bone-marrow dose has been shown to be the dominant cause of early fatalities. Tellurium isotopes account for about 35 percent of the acute bone marrow dose and about 20 percent of the thyroid dose. Because of the long half-lives of Cs¹³⁴ (2 years) and Cs¹³⁷ (30 years), cesium is the dominant element for long-term exposure. However, a factor of 10 reduction in the release fraction of cesium reduces the mean number of latent cancer fatalities by only 25 percent.

The small reduction in the number of latent cancer fatalities is a result of the assumption in CRAC2 that land will be interdicted to reduce long-term exposure. Thus, reducing the release fraction of cesium reduces the amount of interdicted land but does not significantly alter the total population exposure. The amount of interdicted land is very sensitive to the release fraction of cesium. A factor of ten reduction in the cesium release fraction results in an 85% reduction in the interdicted land area. The sensitivity of latent cancer fatalities to the criterion used for the interdiction of land is discussed in Section 2.7.5.

Table 2.3.2-2 presents the impact on consequences of reductions in the SST1 release fractions of all

Table 2.3.2-1. Sensitivity of Mean Consequences to Reductions in SST1 Release Fractions of Iodine, Cesium, and Tellurium^{a,b}

Accident Release	Early Fatalities	Early Injuries	Latent Cancer Fatalities	Acute Dose ^c		Area of Land Interdiction
				Bone Marrow	Thyroid	
SST1 (Standard)	100 ^b	100	100	100	100	100
50% I	75	75	98	85	60	100
10% I	60	55	95	70	30	100
0% I	50	55	95	65	20	100
50% Cs	95	95	90	95	100	55
10% Cs	90	95	75	90	100	15
0% Cs	85	90	60	90	100	1
50% Te	75	65	95	85	90	100
10% Te	50	45	90	70	80	100
0% Te	45	40	90	65	80	100
50% I,Cs	70	70	90	80	60	55
10% I,Cs	45	55	70	60	30	15
0% I,Cs	40	50	55	55	20	1
50% I,Cs,Te	40	45	85	60	50	55

a. Assumptions: 1120 MWe reactor, Indian Point site, New York City meteorology, Summary Evacuation.

b. All consequences normalized to 100 for source term SST1.

c. Relative doses are approximately independent of distance.

Table 2.3.2-2. Sensitivity of Mean Consequences to Reductions in SST1 Release Fractions of All Elements Except Noble Gases^{a,b}

Accident Release	Early Fatalities	Early Injuries	Latent Cancer Fatalities	Acute Doses ^c		Interdicted Land Area
				Bone Marrow	Thyroid	
SST1 (Standard)	100 ^b	100	100	100	100	100
50% SST1 ^d	30	35	74	53	50	55
10% SST1 ^d	1	4	32	16	10	10
5% SST1 ^d	0.2	2	19	11	5	5
1% SST1 ^d	0.03	1	5	8	1	1

a. Assumptions: 1120 MWe reactor, Indian Point Site, New York City meteorology, Summary Evacuation.

b. All consequences normalized to 100 for source term SST1.

c. Relative doses are approximately independent of distance.

d. Release fractions reduced for all isotopes except noble gases.

elements except the noble gases. The results indicate that an order-of-magnitude decrease in the release fractions causes the mean number of early fatalities to decrease by about 2 orders-of-magnitude and other consequences to decrease by about 1 order-of-magnitude. The 99th percentile^a of the calculated distribution of early fatalities for the standard SST1 release was 8,300. When the SST1 release fractions for elements other than noble gases were reduced to 10 and 1 percent of the standard values, the 99th percentile values for early fatalities fell to 100 and 0, respectively.

Only the impact on consequences of potential reductions in the magnitude of source terms has been examined in this section. Two other areas of large uncertainty, the energy release rate accompanying a radioactive release and the physical characteristics of the released material (as reflected in the dry deposition velocity) are discussed in Sections 2.7.2 and 2.7.3, respectively. Other areas of uncertainty, such as release timing (including variable and long duration releases) and release height, have not been addressed in this study.

In summary, if resolution of present uncertainties concerning source term magnitudes determines that the amount of material released to the atmosphere is significantly less than that currently assumed, there could be large decreases in the predicted consequences of large core melt accidents (e.g., SST1 and SST2). Therefore, the reader should bear in mind that the consequences presented in this report may be significantly overestimated and, thus, some conclusions drawn may not remain valid.

2.4 Site Meteorology and Population

In very general terms, the predicted consequences of an accidental release of radioactive material are dependent on four factors: 1) the assumed source term, 2) the meteorological conditions during and following the release, 3) the number of people exposed to the released material, and 4) the effectiveness of population protective measures. In the previous section, the sensitivity of consequences to the source term was discussed. In this section, the impact on consequences of the mete-

a. Those consequences that would be equalled or exceeded by 1 out of every 100 releases.

investigated. The impact of emergency protective measures on consequences is discussed in Section 2.5.

2.4.1 Sensitivity to Meteorological Record

Predictions of the potential consequences of reactor accidents normally assume that an accident may occur at any time, day or night, under any possible weather conditions. So that all possible weather conditions are adequately represented in the calculations, CRAC2 samples weather sequences from an actual record of meteorological conditions. The meteorological record required by CRAC2 consists of the site wind rose and 8760 hourly observations (1 year) of wind speed, atmospheric stability, and accumulated precipitation. As described in Section 2.2.1 and Appendix E, approximately 100 weather sequences are sampled from the meteorological record and used in the calculations to generate frequency distributions for various consequences. Current regulatory policy requires a licensee to monitor meteorological conditions for at least 1 year as part of the site approval process [25]. Data from reactor sites, however, are often of poor quality. Some site meteorological files do not include observations of precipitation and there are often "gaps" in the recordings. For this study, meteorological records from 29 National Weather Service (NWS) stations were used with the site wind rose. The 29 records represent the broad range of climatic conditions found in the United States, ranging from arid climates, such as Phoenix, AZ, to wet climates, such as Apalachicola, FL. NWS data have several potential advantages over reactor site data in that they are generally of higher quality, are readily available, contain more detailed observations, and are of durations of up to 30 years. A description of the 29 meteorological records may be found in Section A.3 of Appendix A.

A sensitivity analysis was performed to examine the impact that the meteorological record used in the calculations has on predicted consequences. Each of the 29 records was used as input for calculations at the Indian Point and Diablo Canyon sites (i.e., the population distributions and wind rose for each site were used with each of the 29 NWS records). Indian Point was selected because it has one of the highest population densities surrounding the site, while Diablo Canyon has one of the lowest.

The calculations assumed Summary Evacuation (see Section 2.5), an 1120 MWe plant, and an SST1 release.

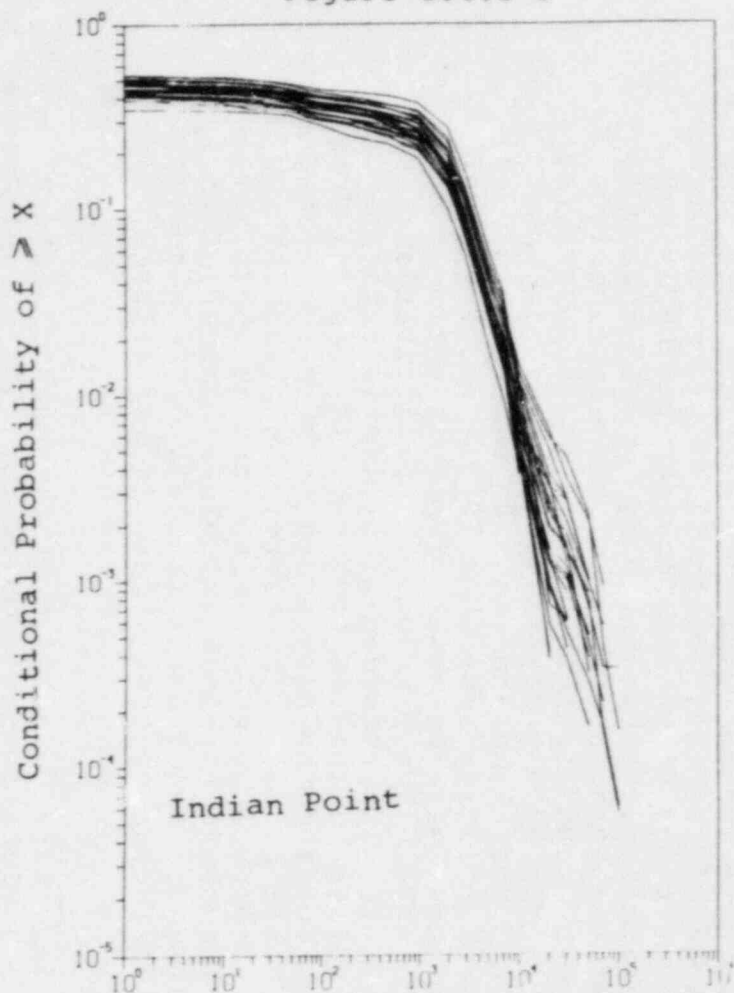
Any observed variation in the predicted consequences at either of the two sites must be due either to differences in the 29 meteorological records or to inadequacies in the procedure used to sample weather sequences.

The weather sequence sampling procedure currently used with CRAC2 has several deficiencies. Because only one year of data is sampled, very low probability sequences (e.g., intense rain at a specific distance) may not be adequately represented. Sequences that contain rain events are currently properly weighted as to frequency of occurrence only when the rain event occurs within 30 miles of the site. This is probably adequate for early fatalities, which typically do not occur beyond 25 miles. However, consequences such as early injuries and interdiction of land, that have dose thresholds and which occur to distances substantially greater than 30 miles, are probably not properly represented by a sampling procedure that does not characterize weather sequences beyond 30 miles. Finally, because rainfall sequences are not weighted for rainfall intensity, ground contamination also may not be adequately characterized by the current sampling procedure.

Figure 2.4.1-1 presents the 29 early fatality CCDFs^a for the Indian Point site obtained using the 29 meteorological records. Probabilities are conditional on the occurrence of an SST1 accident. The means of the 29 conditional distributions vary by less than a factor of 2. At the 90th percentile of the distributions, the consequences range from about 2000 to 4000 early fatalities. At the 99th percentile, the range is about 7000 to 14,000. The higher-consequence events with conditional probabilities less than 10^{-2} typically result from sequences with an onset of precipitation over a populated area. The frequency of precipitation (fraction of hours with recorded precipitation) in the 29 records varies by about a factor of 10, ranging from 1 percent for the Phoenix record to 10 percent at Caribou, ME (see Table A.3-3). Therefore, the probabilities of the high-consequence events also vary by about a factor of 10. The peaks (maximum calculated number of early fatalities) of the 29 early fatality CCDFs also vary by about a factor of ten (10^4 to 10^5 fatalities). This

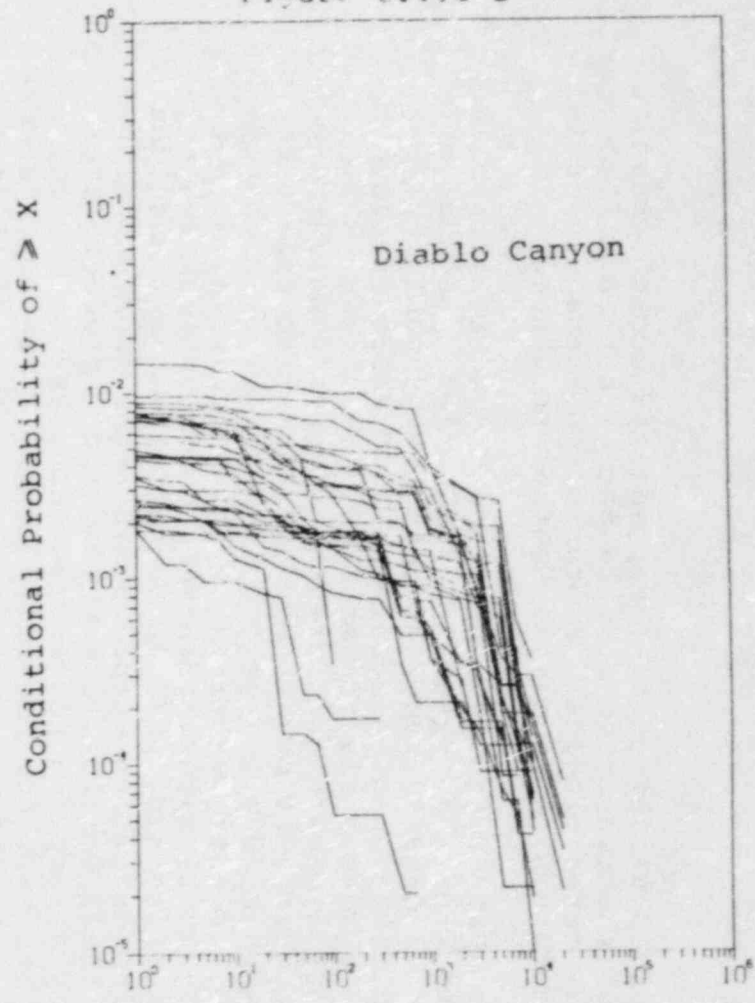
a. Complementary Cumulative Distribution Functions are log-log plots of the probability that a consequence of a given magnitude will be equalled or exceeded.

Figure 2.4.1-1



X , Early Fatalities

Figure 2.4.1-2



X , Early Fatalities

Early Fatality Complementary Cumulative Distribution Functions (CCDFs) Generated With Meteorological Data From 29 National Weather Service Stations. Probabilities are conditional on an SST1 accident occurring. The means of the distributions have the following ranges: Indian Point 710-1300, Diablo Canyon 0.1-18. Assumptions: Summary Evacuation, 1120 MWe reactor.

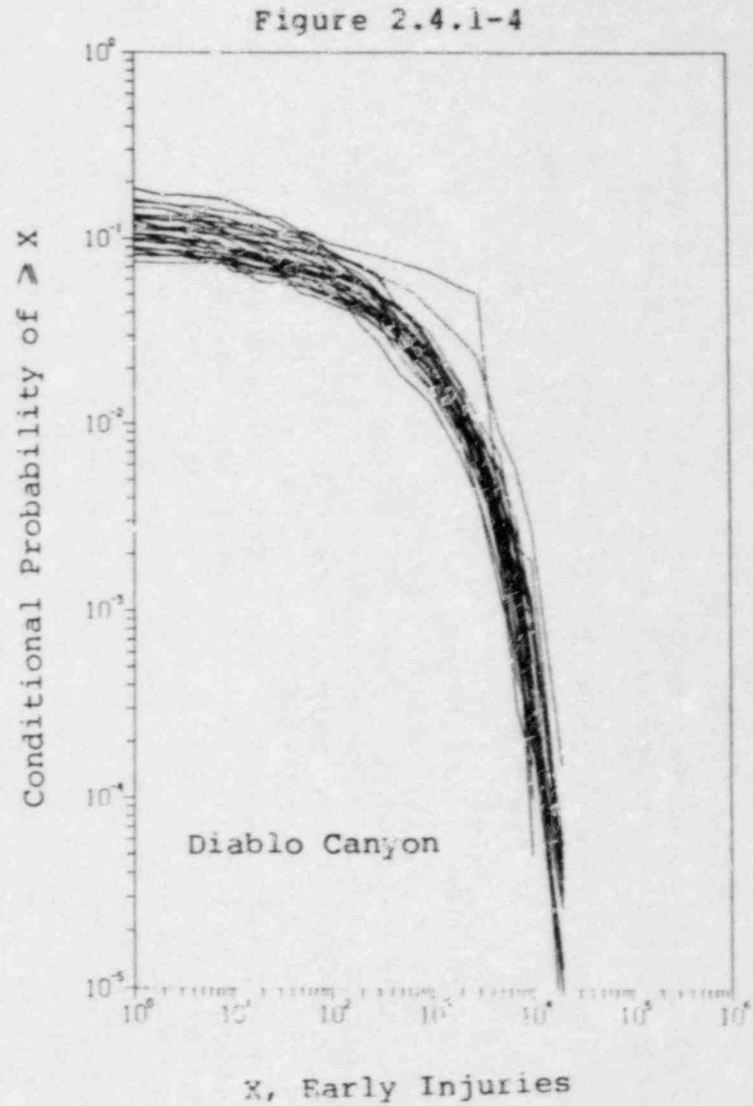
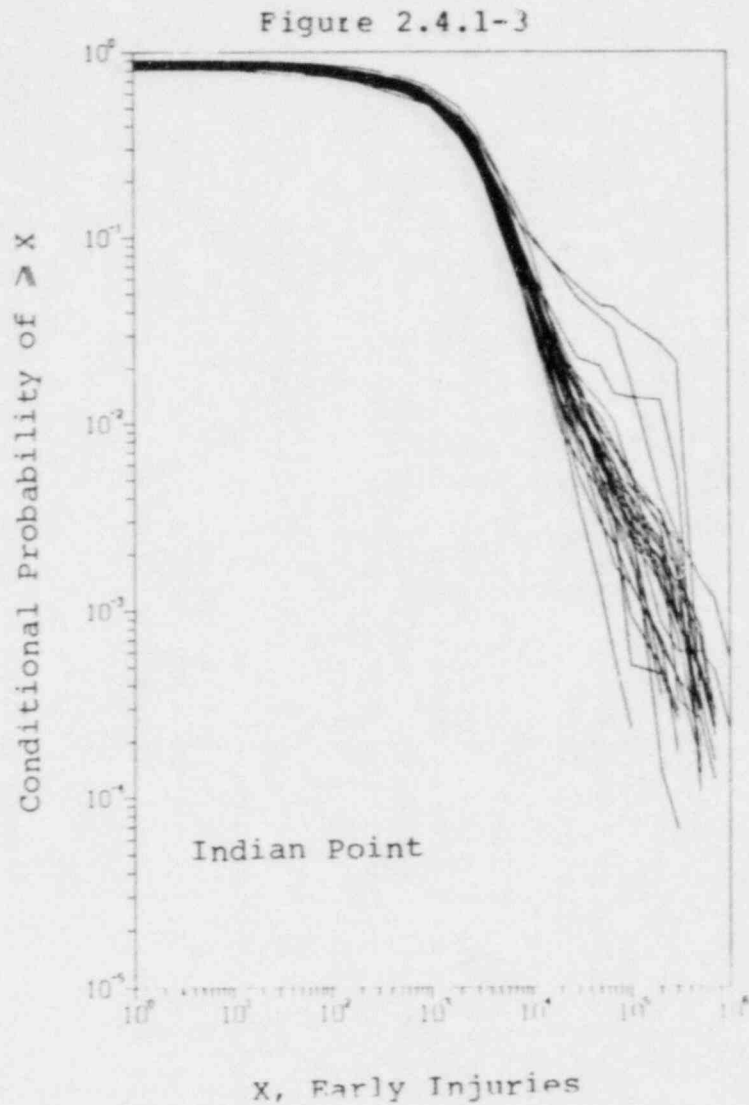
range probably is caused by inadequacies in the weather sequence sampling procedure used in the calculations.

In marked contrast to the Indian Point result, the 29 early fatality CCDFs for the Diablo Canyon site (Figure 2.4.1-2) are not closely clustered. Because of the very low population density surrounding the Diablo Canyon site, early fatalities occur above the 99th percentile of the distributions^a for only one of the 29 meteorological records. Examination of the sequences which produced any early fatalities showed that almost all were sequences containing precipitation. The spread of the distributions (as much as 2 orders of magnitude in both probabilities and consequences) is caused by variations in the frequency of precipitation among the 29 records and inadequacies in the weather sequence sampling procedure.

Results similar to those presented in Figure 2.4.1-2 were found by Sprung [26] for calculations with buoyant plumes where, again, the occurrence of precipitation is required to produce significant numbers of early fatalities (Note that all releases in the present study are assumed to be non-buoyant. The effect of plume buoyancy on predicted consequences is discussed in Section 2.7.2.)

Figures 2.4.1-1 and 2.4.1-2 indicate that out to the 99th percentile of the conditional distributions, the meteorological record used in the calculations does not have a significant impact on the predicted distributions of early fatalities (CCDF mean values differ by less than a factor of 2). Figures 2.4.1-3 and 2.4.1-4 show the 29 early-injury CCDFs for the two sites. Except for three of the meteorological records, there is again very little variation among consequences with conditional probabilities greater than 10^{-2} . The outlying curves are for the Apalachicola, Seattle, and El Paso meteorological records at the Indian Point site and the Apalachicola and Seattle records at Diablo Canyon. Apalachicola and Seattle are two of the "wetter" meteorological records; inexplicably, El Paso is one of the driest. The source of these anomalies is not certain, but is probably due to inadequacies of the weather sequence sampling procedure (i.e., rain events beyond 30 miles are not appropriately weighted).

a. Those consequences that would be equalled or exceeded by 1 out of every 100 releases.



Early Injury Complementary Cumulative Distribution Functions (CCDFs) Generated With Meteorological Data From 29 National Weather Service Stations. Probabilities are conditional on an SST1 accident occurring. The means of the distributions have the following ranges: Indian Point 2400-14,000 (2,400 - 5,000 without the 3 high outlying CCDFs), Diablo Canyon 64-240. Assumptions: Summary Evacuation, 1120 MWe reactor.

Figures 2.4.1-5 and 2.4.1-6 present the 29 latent cancer fatality CCDFs for the two sites. Both figures show variations only in the probabilities of the high-consequence events, most likely a reflection of the different probability of precipitation in each meteorological record. These two figures clearly indicate that the meteorological record does not have a significant impact on predicted distributions of latent cancer fatalities.

Figure 2.4.1-7 shows the interdicted-land area CCDFs for the 29 records. Interdicted land is a measure of the potential offsite economic consequences of an accident and is calculated independent of population distribution and wind rose. At the 90th percentile, the predicted areas vary by about a factor of 3. There is a 2-order of magnitude spread in the probabilities of the CCDF maxima (high-consequence sequences). The different probabilities of precipitation among the 29 meteorological records can account for about 1 order of magnitude. The remaining factor of 10 most likely is caused by inadequacies in the weather-sequence categorization procedure (see Appendix E).

This section has examined the sensitivity of consequence magnitudes to meteorological record. The sensitivity to meteorological record of the distances to which consequences occur is discussed in Section 2.6.

The following conclusions can be drawn from this sensitivity analysis:

- o Given a specific release, the one-year meteorological record used in the calculations does not have a significant impact on predicted consequences out to the 99th percentile of the distributions. Therefore, when suitable meteorological data is not available from the site, the use of substitute meteorological data, such as that available from a nearby National Weather Service station, is probably adequate for performing consequence calculations with CRAC2.
- o Major differences in predicted consequences among the 29 meteorological records occur at probabilities less than 10^{-2} and probably arise from variations in the frequency of precipitation and inadequacies in the procedure used to sample weather sequences.

Figure 2.4.1-5

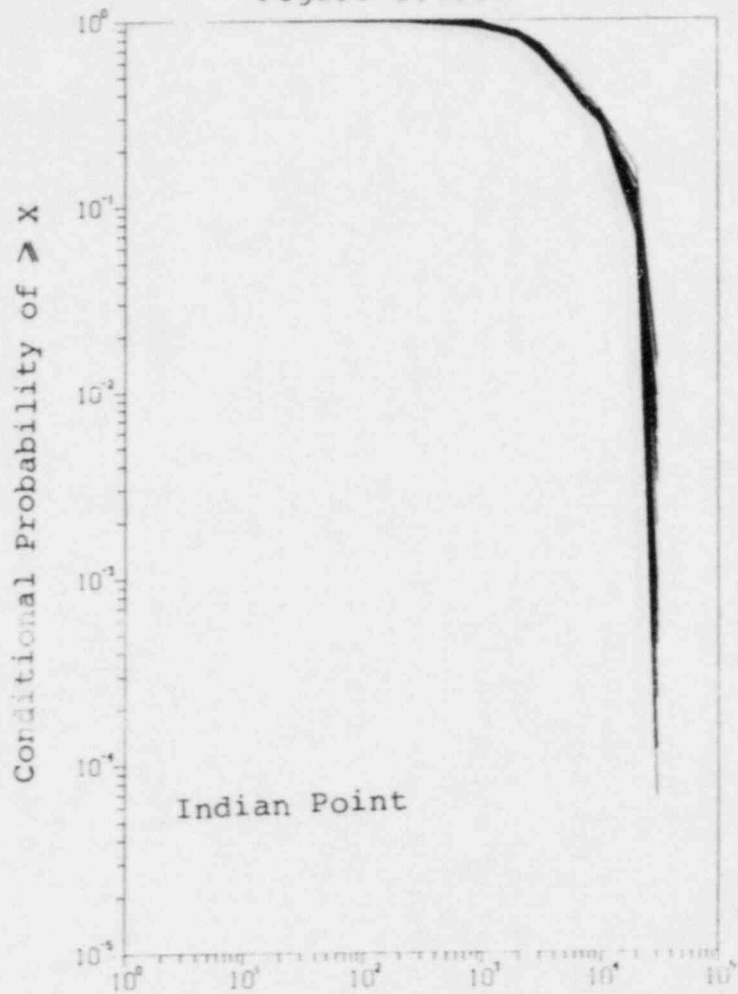
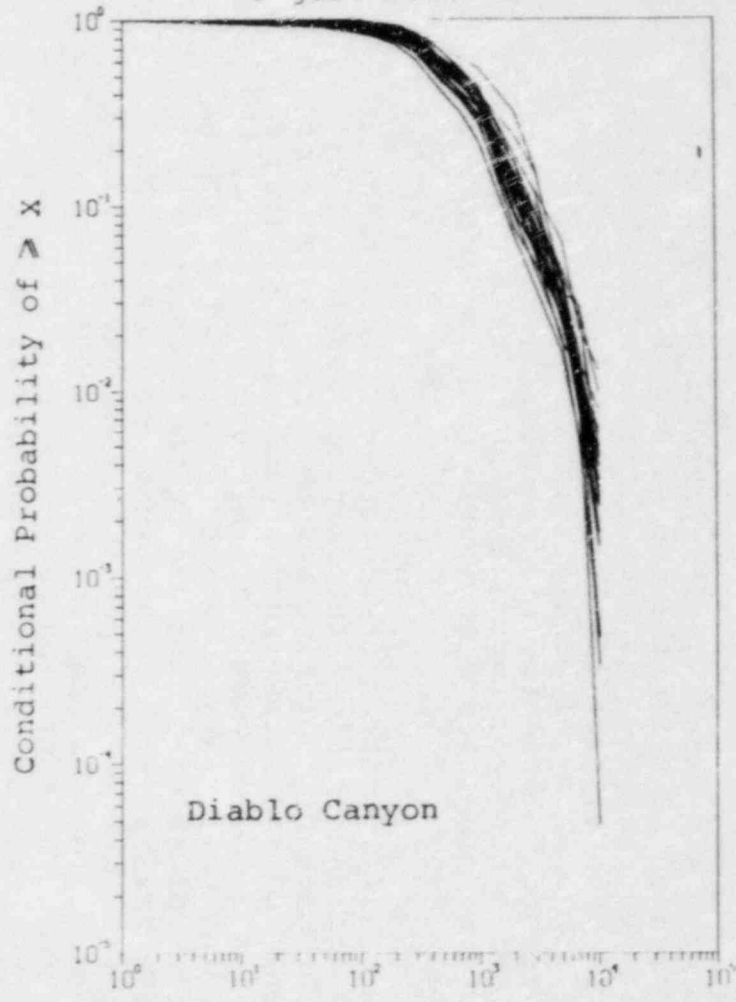


Figure 2.4.1-6



Latent Cancer Fatality Complementary Cumulative Distribution Functions (CCDFs) Generated With Meteorological Data From 29 National Weather Service Stations. Probabilities are conditional on an SST1 accident occurring. The means of the distributions have the following ranges: Indian Point 7600-9300, Diablo Canyon 750-1600. Assumptions: Summary Evacuation, 1120 MWe reactor.

- o Further refinement is needed in the CRAC2 treatment of meteorological data. Possible improvements include the use in the weather sequence sampling procedure of more than 1 year of weather data and the consideration of precipitation intensity. In addition, sequences with an onset of precipitation may need to be categorized to distances beyond the present 30 miles, perhaps to 100 miles.

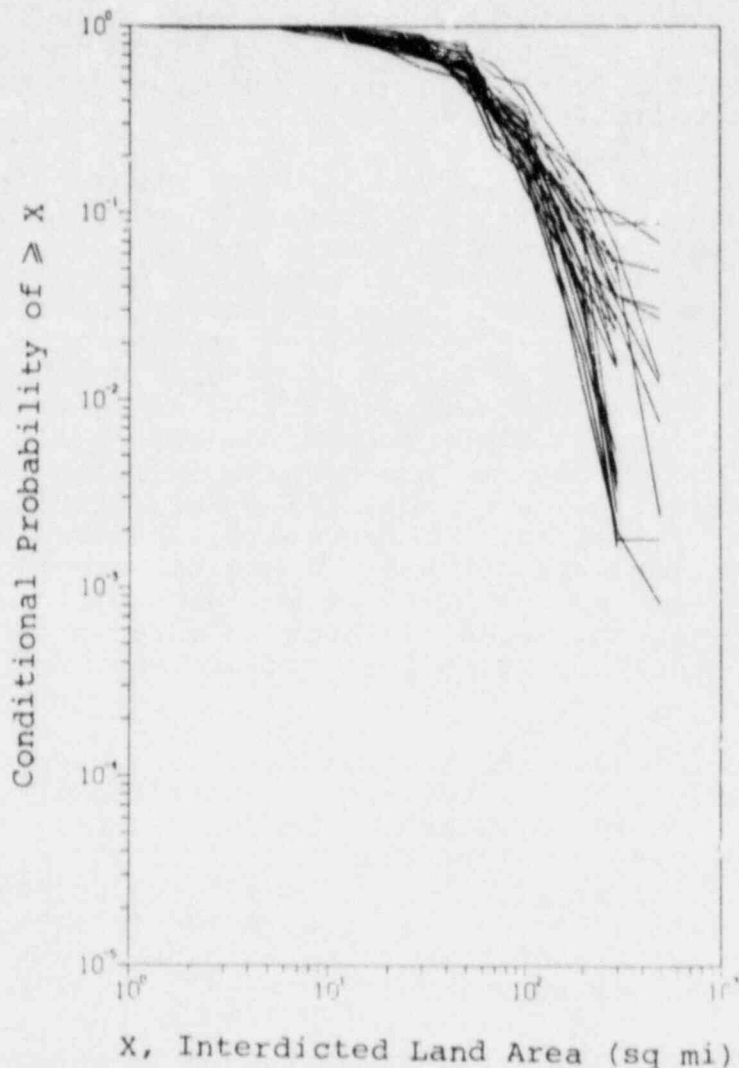


Figure 2.4.1-7. Interdicted Land Area Complementary Cumulative Distribution Functions (CCDFs) Generated with Meteorological Data from 29 National Weather Service Stations. Probabilities are conditional on an SST1 accident occurring. The means of the distributions range from 72 to 140 square miles. Assumption: 1120 MWe reactor.

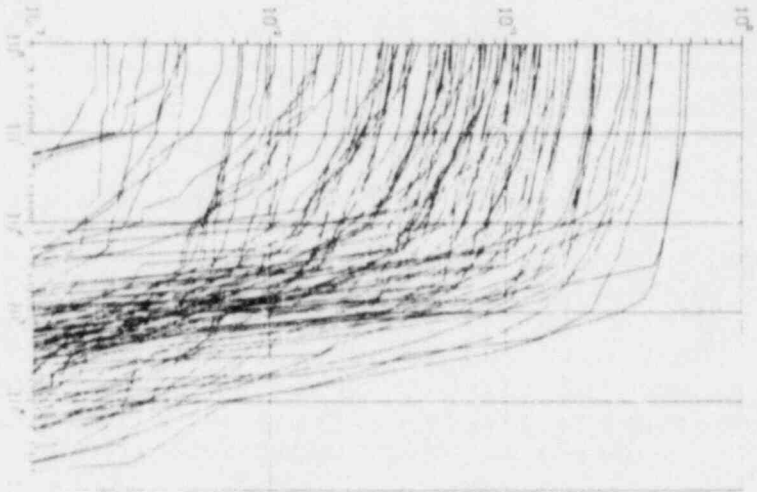
2.4.2 Sensitivity to Site Population Distribution

To examine the role of population distribution in determining reactor accident consequences, a sensitivity study was performed using the actual population distribution and 1-year average wind rose from each of the 91 U.S. reactor sites having either an operating license or a construction permit. Calculations performed using actual site population distributions also provide a better understanding of past siting policy and a reference against which the consequences of proposed siting policies can be compared.

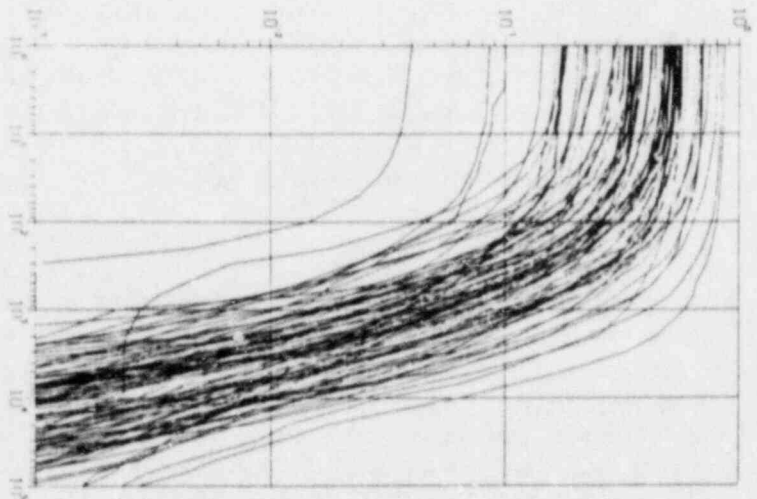
For each of the 91 sites, a representative meteorological record was selected from the 29 National Weather Service records used in this study (see Appendix A). As discussed in the previous section, the meteorological record used in the calculations has only a marginal impact on the predicted distribution of consequences. Thus, the uncertainty resulting from using a substitute record (rather than one obtained at the site) is probably not significant. Since the purpose of this study was to examine the impact on consequences of specific site characteristics, a standard 1120 MWe reactor was assumed at all 91 sites. Consequently, the results of these calculations are not assessments of existing reactor-site combinations, and it would be misleading to use them as such. Finally, each calculation also assumed the occurrence of an SST1 release and of Summary Evacuation.

Figures 2.4.2-1a through 2.4.1-1c show early fatality, early injury, and latent cancer fatality CCDFs for all of the 91 sites. The figures have been truncated at conditional probabilities of 10^{-3} (one in a thousand releases). This was done because consequence probabilities and magnitudes for improbable events (those with conditional probabilities less than 10^{-3}) are very uncertain. A large part of this uncertainty is due to the assumption of an evacuation only within 10 miles. Because of this assumption, all persons beyond 10 miles were assumed to be exposed to deposited radionuclides for 1 day, regardless of dose rate^a. Any emergency actions taken beyond 10 miles

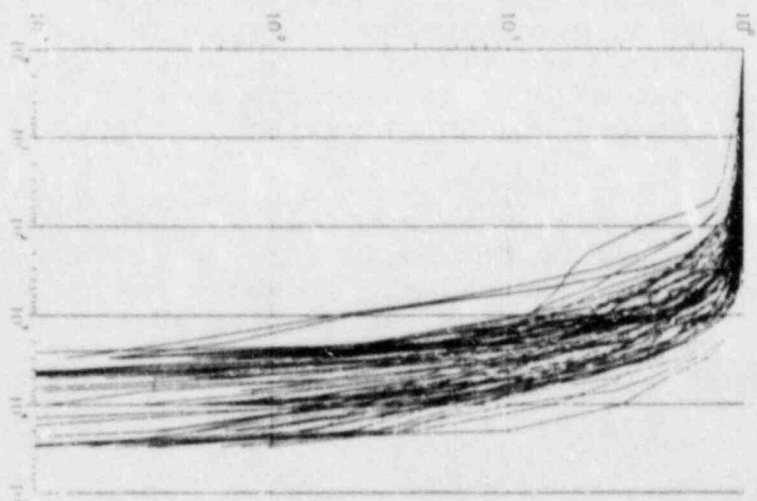
a. Under some meteorological conditions, the 1-day bone marrow dose at 10 miles can exceed 1000 rem.

Conditional Probability of $\geq X$ 

X, Early Fatalities

Conditional Probability of $\geq X$ 

X, Early Injuries

Conditional Probability of $\geq X$ 

X, Latent Cancer Fatalities

Figure 2.4.2-1.

(a) Early Fatality, (b) Early Injury, and (c) Latent Cancer Fatality CCDFs Conditional on an SSTI Release at all 91 Current U.S. Reactor Sites. Assumptions: 1120 Mwe reactor, Summary Evacuation, representative meteorology. Range of means: early fatalities 0.4 to 970, early injuries 4 to 3600, and latent cancer fatalities 230 to 8100.

(e.g., sheltering or prompt relocation) would significantly mitigate the consequences of low-probability, high consequence events [27]. The effect on consequences of different emergency response scenarios is discussed in Section 2.5.

The 91 early fatality CCDFs range (on the probability axis) over almost 3 orders of magnitude in the conditional probability of any early fatalities [i.e., $P(\geq 1)$] and over nearly 4 orders of magnitude in consequences at a conditional probability of 10^{-3} (consequence axis). The conditional means of the 91 CCDFs range from 0.4 to 970 fatalities. Figure 2.4.2-2 presents a histogram of the conditional means of the early fatality CCDFs versus number of sites. Only four sites have means above 250 fatalities; over half are less than 50. Table C-1 in Appendix C lists the conditional mean number of early fatalities, early injuries, and latent cancer fatalities for each of the 91 sites. The 99th percentile^a of the conditional distributions of early fatalities range from zero to 8000. Figure 2.4.2-3 presents a histogram of the 99th percentile of the distributions versus number of sites.

The 91 early injury CCDFs (Figure 2.4.2-1b) range over approximately 1 order of magnitude in the conditional probability of having any injuries [$P(\geq 1)$] and over 2 orders in consequence magnitude at a conditional probability of 10^{-3} . The conditional mean numbers of early injuries range from 4 to 3600. The latent cancer fatality CCDFs (Figure 2.4.2-1c) show less than 1 order of magnitude spread on both axes. The conditional means of the latent cancer fatality CCDFs range from 230 to 8100.

In Section 2.4.1, it was shown that the meteorological record does not significantly affect the calculated distributions of consequences. Therefore, the wide variability in calculated distributions displayed in Figures 2.4.2-1a through c (early fatalities, early injuries, latent cancer fatalities) can be due only to differences in the 91 population distributions since all other factors were either held constant or have no significant effect on predicted consequences.

a. Those consequences that would be equalled or exceeded by 1 out of every 100 releases.

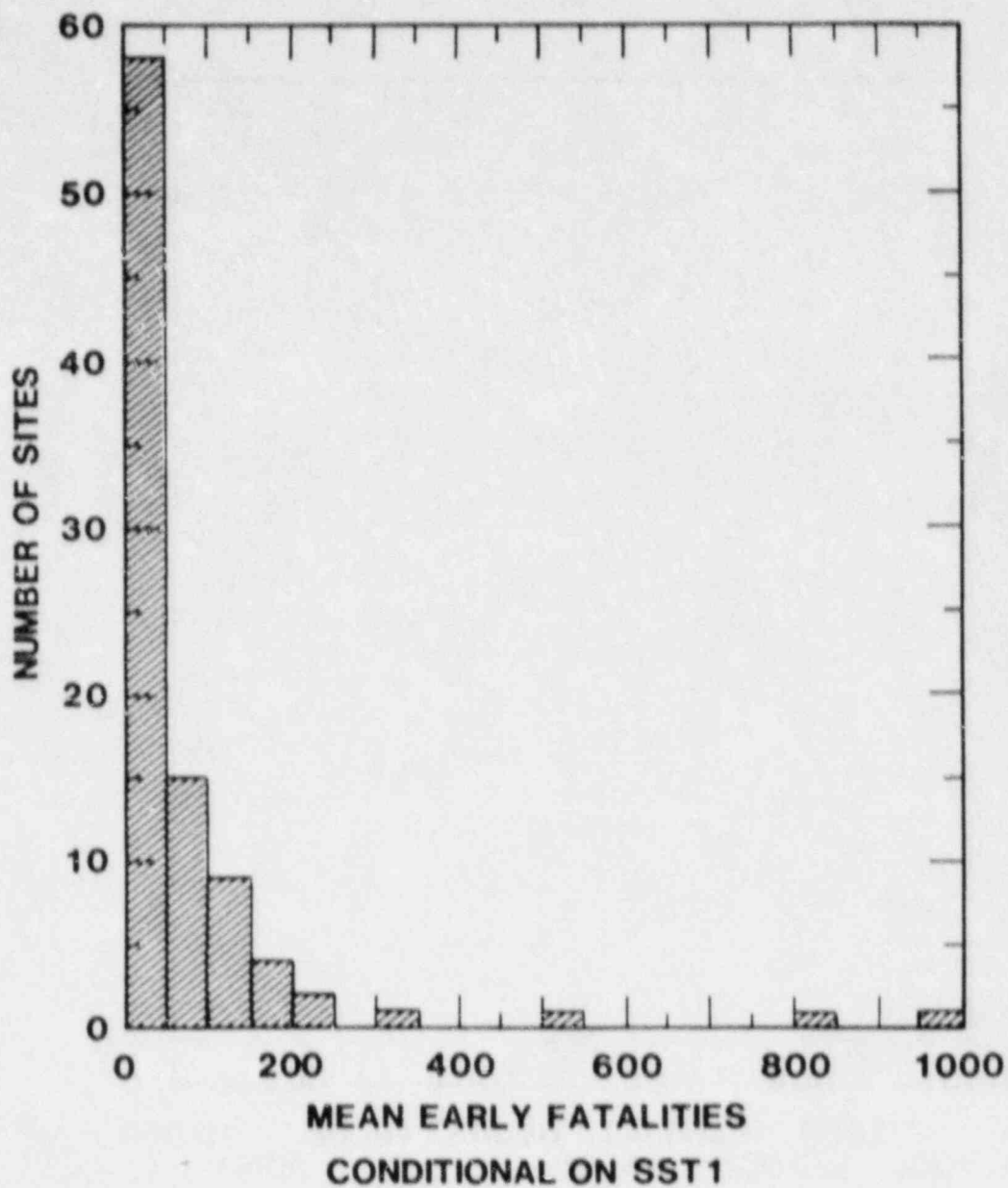


Figure 2.4.2-2. Histogram of Mean Early Fatalities for 91 Sites, Conditional on an SST1 release. Assumptions: 1120 MWe reactor, a representative meteorological record, and Summary Evacuation.

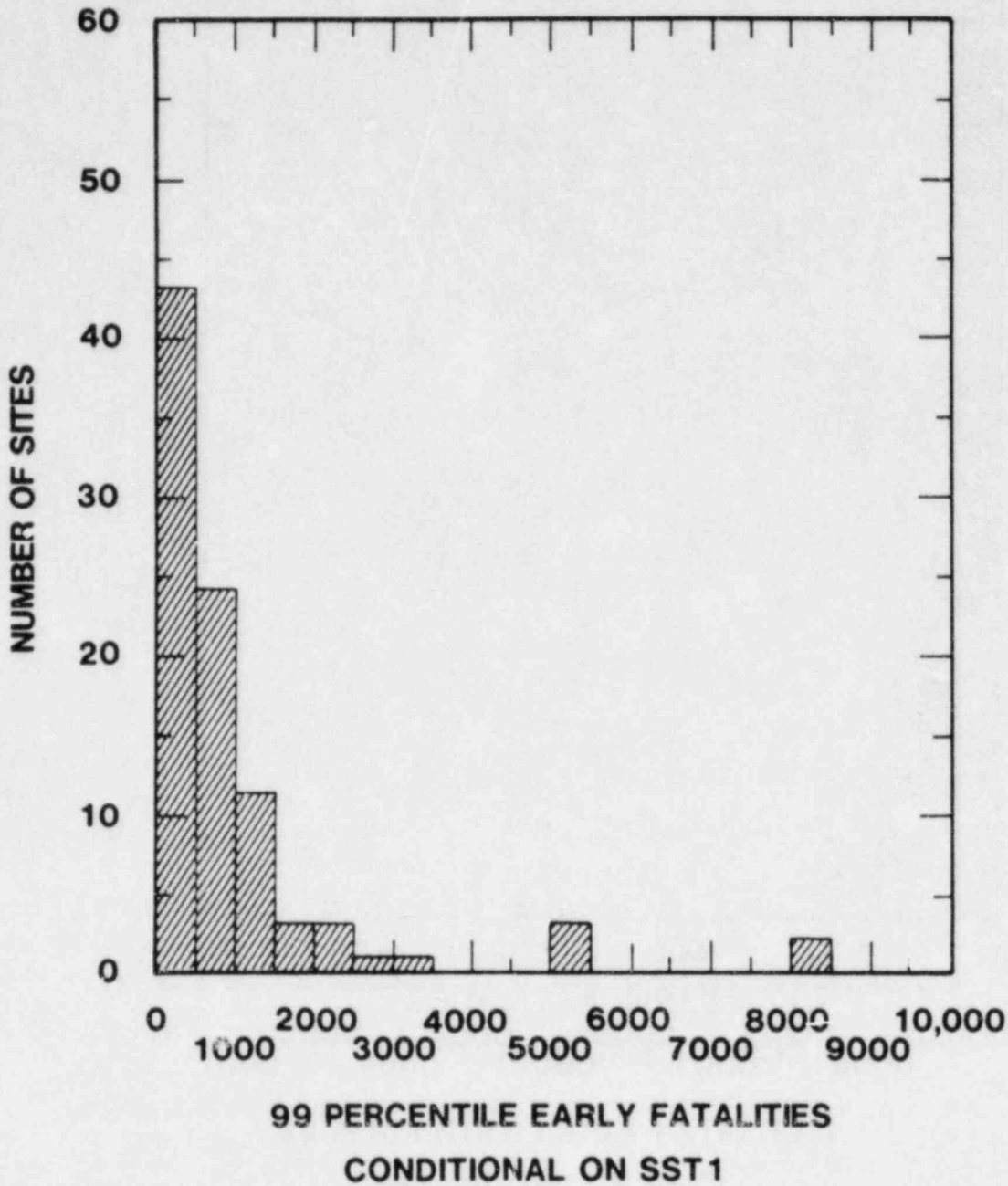


Figure 2.4.2-3. Histogram of the 99th Percentile of the Distribution of Early Fatalities for 91 Sites, Conditional on an SST1 Release. Assumptions: 1120 MWe reactor, a representative meteorological record, and Summary Evacuation.

The different degrees of variability of the three consequences are primarily due to the different distances to which each consequence occurs. Within 20 miles of the reactor there is tremendous variability in the 91 population distributions. Within this distance, the population densities range from 1 to 710 people per square mile (see Section 3). Therefore, the distributions of early fatalities, which are confined to areas within a few tens of miles of the site (most occur within a few miles, see Section 2.6), show the greatest variability. Early injuries can occur to many tens of miles, but most occur within about 30 miles. Within 50 miles of the 91 sites, average population densities range from 10 to 2100 people per square mile. Since this range (factor of 210) is less than that observed to 20 miles (factor of 710), the variability in the 91 early injury CCDFs is less than that obtained for early fatalities. Finally, when averaged over very large areas, the variability in the 91 population distributions is greatly reduced. The population densities within 200 miles of the 91 sites vary between 14 and 335 people per square mile (factor of 24). Thus, the distributions of latent cancer fatalities, which can occur over very large areas, show the least variability.

Some specific characteristics of population distributions which might impact the variability of consequences are discussed in Section 2.7.4. Finally, for each of the 91 sites examined in this report, early fatality, early injury, and latent cancer fatality CCDFs conditional on an SST1 release are presented in Appendix C. When examining these CCDFs, it is important to remember that they are not truly site specific. Although each CCDF was calculated using the site's wind rose, the population distribution about the site, and an appropriate substitute meteorological record, the SST1 release assumed in each calculation was not modified to reflect the specific design of the site's reactor. Instead, a standard 1120 MWe PWR was assumed in each calculation.

2.5 Sensitivity to Emergency Response

Should an accident at a nuclear power plant lead to a significant release of radioactivity, public radiation exposures could be mitigated by evacuation, sheltering, relocation, or medical prophylaxis^a. Summary Evacuation within 10 miles was assumed in most of the calculations presented in other sections of this report. In this section the sensitivity of early fatalities and early injuries to emergency response is examined by a series of parametric calculations. All of these calculations assume an SST1 release from an 1120 MWe reactor, Indian Point population and wind rose, and New York City meteorology.

The emergency response submodel in CRAC2 was briefly described in Section 2.2.2 and is more fully described in this section and in Appendix E. The model allows for the mitigation of radiation exposures by evacuation or by sheltering followed by relocation. Evacuation is characterized by the delay time between accident warning and the initiation of evacuation, by the distance within which people evacuate, and by the evacuation speed [8]. Sheltering is characterized by the distance within which all people take shelter, the shielding factors afforded by the structures in which they take shelter [29-31], and the delay time between cloud passage and the relocation of sheltered population. The parameters that describe these emergency response scenarios are first defined and then the results of the parametric calculations are presented.

a. Evacuation is the expeditious movement of people to avoid exposure to the passing cloud of radioactive material. Sheltering is the expeditious movement of people indoors, if possible, into basements or masonry buildings which afford enhanced shielding from radiation. Relocation is the movement of exposed persons out of contaminated areas after the passage of the radioactive cloud. Medical Prophylaxis is the administration of agents which decrease or block internal exposures (e.g., KI prophylaxis decreases thyroid exposures [28]).

The following eight parameters essentially determine the impact of the CRAC2 emergency response model on consequence predictions:

Warning Time: Time from accident notification by plant personnel to release of radioactivity due to containment failure (e.g., 0.5 hr for SST1).

Delay Time: Time from accident notification to the initiation of emergency response (0 hr for sheltering; 1-5 hr for evacuation).

Evacuation Radius: The radius within which all occupants of a 90° sector (centered on the plume centerline) evacuate (10 mi in the base case calculation).

Evacuation Speed: The effective speed at which evacuees move radially away from the reactor (10 mph in the base case calculation).

Evacuation Distance: The radial distance to which the evacuees move (5 mi beyond the evacuation radius; therefore, 15 mi for the base case calculation) before they are removed from the calculation because they are assumed to have enough information to avoid additional exposure.

Sheltering Radius: The radius within which all non-evacuating occupants of a 90° sector (centered on the plume) take shelter. If the sheltering radius is less than or equal to the evacuation radius, only evacuation takes place. If the sheltering radius is larger than the evacuation radius, then all persons between the evacuation radius and the sheltering radius take shelter. Beyond the sheltering radius, normal activity is assumed to continue (i.e., some people are outdoors).

Shielding Factor [29]: The fraction of the dose to an unsheltered individual received by an individual sheltered in a building or in a vehicle (i.e., during evacuation). Shielding factors for buildings depend on the housing stock (percent brick, availability of basements) and, therefore, vary by geographic region. Different shielding factors are used to decrease unshielded exposures to the radioactive plume and to contaminated ground (see Appendix A).

Relocation Time: The period which elapses after passage of the radioactive plume before non-evacuating individuals are moved from contaminated areas (24 hr in the base case calculation)

Relationships between several of these eight emergency response model parameters are schematically depicted in Figure 2.5-1.

The CRAC2 emergency response submodel allows for the specification of up to six different emergency response scenarios and will calculate a weighted average of the results for any designated set of scenarios. CRAC2 calculations presented in other sections of this report generally assume "Summary Evacuation," which is the weighted summation of three different evacuation scenarios as follows:

<u>Scenario Number</u>	<u>Weight^a</u>	<u>Type of Response</u>	<u>Response Distance</u>	<u>Response Speed</u>	<u>Delay Before Response</u>
1	30%	evacuation	10 miles	10 mph	1 hour
2	40%	evacuation	10 miles	10 mph	3 hours
3	30%	evacuation	10 miles	10 mph	5 hours

- a. The 30%/40%/30% weighting provides a best fit to EPA evacuation data [7] (See Appendix E).

The sensitivity of the CRAC2 evacuation model to evacuation speed has been previously investigated by Aldrich, et al. [9], who found that, for evacuation within 10 miles after a 3 hour delay, early fatalities were minimally affected by effective evacuation speed provided that the evacuation speed was at least 10 mph. The impact of delay time on early health effects is illustrated in Figure 2.5-2, which presents early fatality CCDFs for 10 mph evacuations within 10 miles after delays of 1, 3, and 5 hours, respectively (scenarios 1, 2, and 3). Also plotted is the CCDF for Summary Evacuation, which is the 30:40:30 weighted summation of the CCDFs for scenarios 1, 2, and 3. Figure 2.5-2 shows (1) that early fatalities are substantially decreased by short delay times (≤ 1 hr); and (2) that Summary Evacuation yields results nearly identical to those obtained for scenario 2 (3 hr delay).

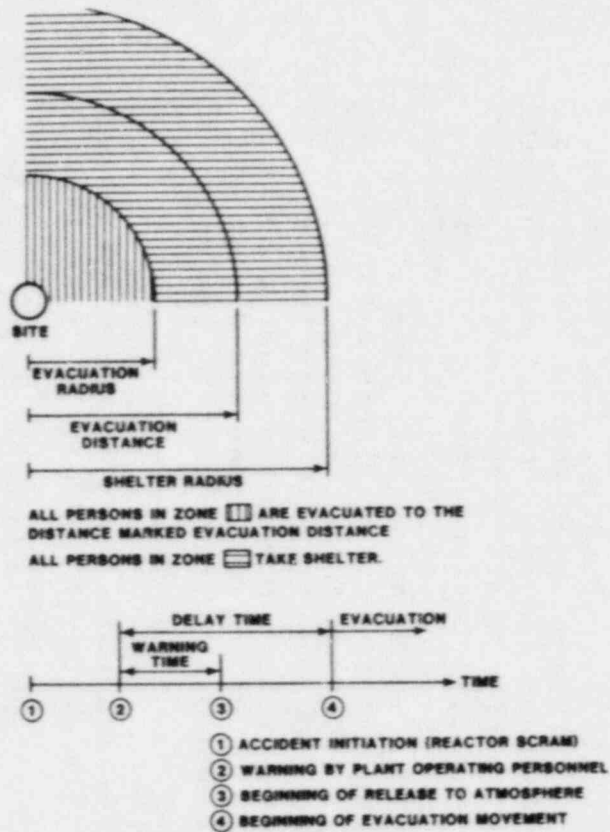


Figure 2.5-1.

Relationships Between
Evacuation Model Parameters.

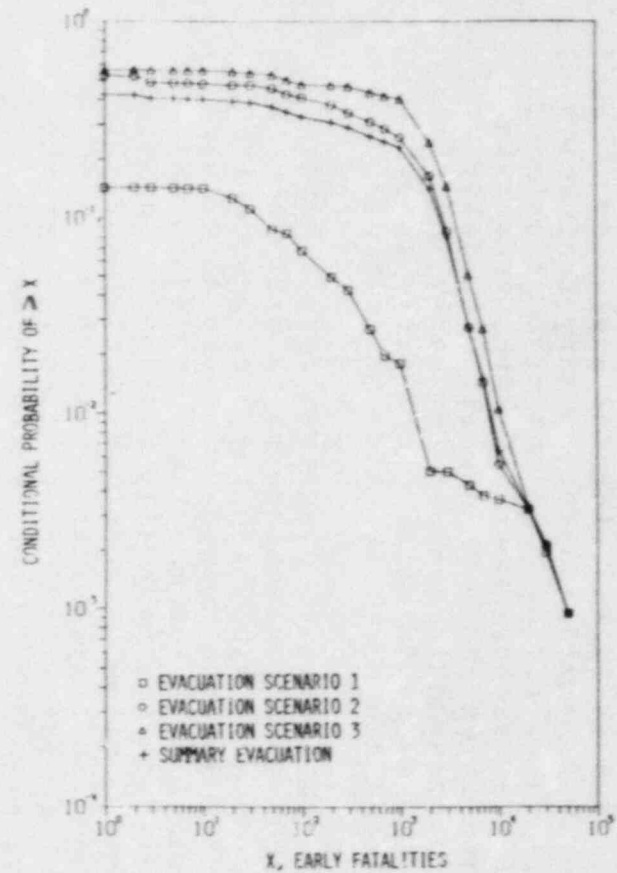


Figure 2.5-2.

Early Fatality Complementary Cumulative Distribution Functions for 10 mph Evacuations within 10 Miles after Delays of 1, 3, and 5 Hours (Scenarios 1, 2, and 3, respectively) and for Summary Evacuation. Assumptions: 1120 MWe reactor, Indian Point population and wind rose, New York City meteorology.

Table 2.5-1 presents mean and 99th percentile^a values of early fatalities and early injuries for emergency response scenarios 1, 2, and 3 and for Summary Evacuation. The table shows (1) that, for evacuations of population within 10 miles of the reactor, mean and 99th percentile values of early fatalities are more sensitive to delay time than are the corresponding values for early injuries; and (2) that for both early fatalities and early injuries, 99th percentile values are about 10 times mean values.

The different sensitivities displayed result largely from the fact that each consequence has a different characteristic distance within which the consequence is calculated to occur (distance dependencies are discussed in detail in Section 2.6). For most weather sequences, fatal doses of radiation are generally confined to distances of less than 10 miles. Therefore, for almost all of the weather sequences sampled, the entire population potentially subject to fatal radiation doses is evacuating. Consequently, mean and 99 percentile values for early fatalities are highly sensitive (factors of $8 \approx 1400/180$ and $7 \approx 10,000/1400$) to delay time. In contrast to this, doses of radiation sufficient to cause early injuries frequently occur to distances significantly greater than 10 miles. Therefore, because a significant fraction of the population potentially subject to doses sufficient to cause injuries (i.e., the population beyond 10 miles) is not evacuating, mean and 99th percentile values of early injuries are less sensitive (factors of 1.7 and 1.1) to delay time than are the corresponding values for early fatalities. Finally, for evacuations of population within 10 miles, peak values (worst case calculated for any weather sequence, conditional probabilities of $\lesssim 10^{-3}$) of early fatalities and early injuries are essentially insensitive to evacuation delay time e.g., in Figure 2.5-2 the four early fatality CCDFs have identical tails). This is because early fatality and injury worst case results (CCDF tails) are caused by rainout of radioactivity from the plume onto population centers (cities) located more than 10 miles from the reactor. Since these cities were not evacuated in this set of calculations, these calculations yield peak values of early fatalities and early injuries that are not affected by evacuation delay time.

Table 2.5-2 presents the effect of the distance within which population is evacuated upon early fatalities

a. Consequence magnitude that would be equalled or exceeded following 1 out of every 100 releases.

Table 2.5-1. Effect of Delay Time on Early Fatalities and Early Injuries for Evacuation to 10 Miles. Results are Conditional on an SST1 Release.

Delay Time (hr)	Early Fatalities		Early Injuries	
	Mean	99th Percentile	Mean	99th Percentile
1	180	1,400	2500	30,000
3	920	8,000	4000	32,000
5	1400	10,000	4300	34,000
Summary	830	8,300	3600	33,000

Assumptions: 1120 MWe reactor, SST1 release, Indian Point population and wind rose, New York City meteorology.

Table 2.5-2. Effect of Evacuation Distance on Early Fatalities and Early Injuries for Summary Evacuation. Results are Conditional on an SST1 Release.

Evacuation Distance (mi)	Early Fatalities		Early Injuries	
	Mean	99th Percentile	Mean	99th Percentile
0 ^a	3600	18,000	6300	41,000
5	1100	11,000	5500	40,000
10	830	8,300	3600	33,000
25	700	7,200	1800	9,400

a. No evacuation

Assumptions: 1120 MWe reactor, SST1 release, New York City meteorology, Indian Point population and wind rose.

and early injuries for Summary Evacuation. The table shows that mean and 99th percentile values of early fatalities and injuries are all quite sensitive to the distance within which population is evacuated. Because worst case results (conditional probabilities of $\leq 10^{-3}$) for early fatalities are generally caused by rainout of the radioactive plume onto a city located further than 10 but less than 25 miles from the reactor, evacuation within 25 miles lowers the worst case number of early fatalities from 57,000 (for evacuation within 10 mi) to 15,000 (for evacuation within 25 mi).

The next three tables examine the sensitivity of early health effects to sheltering parameters. Table 2.5-3 displays the effect of the distance within which population takes shelter in preferred locations (building interiors, basements if available) on early fatalities and early injuries. Examination of the table shows that the effect of response distance for sheltering is similar to that for evacuation. Mean and 99th percentile values of early fatalities and injuries are all quite sensitive to sheltering distance. As before, 99th percentile values are about 10 times the mean result and a 25 mile response distance significantly decreases (by about a factor of 5) the worst case result (conditional probability of $\leq 10^{-3}$) below the result obtained with a 10 mile response distance.

Table 2.5-4 illustrates the impact of the availability of basements upon the degree of shielding (and thereby the reductions in consequences) afforded by sheltering. The table shows that mean and 99th percentile values of early fatalities are substantially decreased, if Northeast regional shielding factors (building characteristics: 87% basements, 47% brick) are used rather than Pacific Coast regional shielding factors (building characteristics: 23% basements, 27% brick) [29]. Because sheltering was assumed to take place only to 10 miles, mean and 99th percentile values of early injuries show a lessened sensitivity. These results are consistent with results previously obtained by Aldrich et al. [27].

Table 2.5-3. Effect of Sheltering Distance on Early Fatalities and Early Injuries for Preferential Sheltering Followed by Relocation. Results are Conditional on an SST1 Release.

Sheltering Distance (mi)	Early Fatalities		Early Injuries	
	Mean	99th Percentile	Mean	99th Percentile
5	830	9,300	5600	40,000
10	560	5,500	3700	32,000
15	490	4,900	2700	25,000
25	420	4,500	1800	11,000

Assumptions: 1120 MWe reactor, SST1 release, Indian Point population and wind rose, New York City meteorology, no evacuation, Northeast regional shielding factors, relocation after 6 hr.

Table 2.5-4. Effect of Early Fatalities and Early Injuries for Sheltering to 10 Miles Followed by Relocation. Results are Conditional on an SST1 Release.

Number of Basements	Early Fatalities		Early Injuries	
	Mean	99th Percentile	Mean	99th Percentile
Few ^a	1200	9,300	4100	34,000
Many ^b	560	5,500	3700	32,000

a. 23% basements (Pacific Coast regional shielding factors used, see Appendix A).

b. 87% basements (Northeast regional shielding factors used, see Appendix A).

Assumptions: 1120 MWe reactor, SST1 release, Indian Point population and wind rose, New York City meteorology, no evacuation, relocation after 6 hr.

After plume passage, relocation of sheltered populations decreases exposure to contaminated ground. The effect upon early fatalities and early injuries of decreasing relocation time from 24 to 6 hours is presented in Table 2.5-5. As before, because sheltering was assumed to take place only to 10 miles, mean and 99th percentile early injury values show little sensitivity, while mean and 99th percentile values for early fatalities decrease by a factor of two.

Table 2.5-5. Effect of Relocation Time on Early Fatalities and Early Injuries for Sheltering to 10 Miles. Results are Conditional on an SST1 Release.

Relocation Time (hr)	Early Fatalities		Early Injuries	
	Mean	99th Percentile	Mean	99th Percentile
6	560	5,500	3700	32,000
12	750	7,500	3800	33,000
24	1200	9,300	4100	34,000

Assumptions: 1120 MWe reactor, SST1 release, Indian Point population and wind rose, New York City meteorology, no evacuation, Northeast regional shielding factors.

Table 2.5-6 gathers together in a single table the results of all the calculations which examined evacuation or sheltering separately. The table presents the variation with response distance of early health consequences for five evacuation scenarios and three sheltering scenarios. Examination of Table 2.5-6 shows that for any response distance, expeditious evacuation (1 hr delay, 10 mph) and sheltering with expeditious relocation (after 6 hr) yield the smallest predictions of early health consequences. The table also confirms the strong dependence of mean early health consequences on response time and the less strong dependence on response distance.

Table 2.5-6. Dependence of Early Fatalities and Early Injuries on Response Distance for Eight Emergency Response Scenarios. Results are Conditional on an SSTI Release

Emergency Response		Response Distance (mi)									
Type	Characteristics	0 ^a	5	10	15	25	0 ^a	5	10	15	25
		<u>Mean Early Fatalities</u>					<u>Mean Early Injuries</u>				
Evacuation	5 hr delay, 1 mph	3,600	2,100	1,900	1,800	1,800	6,300	6,200	5,300	5,100	4,700
	5 hr delay, 10 mph	3,600	1,600	1,400	1,300	1,250	6,300	6,000	4,300	3,300	2,500
	3 hr delay, 10 mph	3,600	1,200	920	860	790	6,300	5,800	4,000	3,000	2,200
	Summary Evacuation	3,600	1,100	830	780	700	6,300	5,500	3,600	2,700	1,800
	1 hr delay, 10 mph	3,600	440	180	110	40	6,300	4,600	2,500	1,500	700
Sheltering ^b	24 hr relocation	3,600	c	1,200	c	c	6,300	c	4,100	c	c
	12 hr relocation	3,600	c	750	c	c	6,300	c	3,800	c	c
	6 hr relocation	3,600	830	560	490	420	6,300	5,600	3,700	2,700	1,800
		<u>99th Percentile Early Fatalities^d</u>					<u>99th Percentile Early Injuries^d</u>				
Evacuation	5 hr delay, 1 mph	18,000	16,000	14,000	12,000	11,000	41,000	41,000	40,000	41,000	28,000
	5 hr delay, 10 mph	18,000	14,000	10,000	9,400	8,800	41,000	40,000	34,000	26,000	10,000
	3 hr delay, 10 mph	18,000	11,000	8,000	7,300	7,000	41,000	40,000	32,000	26,000	10,000
	Summary Evacuation	18,000	11,000	8,300	7,600	7,200	41,000	40,000	33,000	26,000	9,400
	1 hr delay, 10 mph	18,000	7,000	1,400	1,200	1,000	41,000	39,000	30,000	24,000	5,200
Sheltering ^b	24 hr relocation	18,000	c	9,300	c	c	41,000	c	34,000	c	c
	12 hr relocation	18,000	c	7,500	c	c	41,000	c	33,000	c	c
	6 hr relocation	18,000	9,300	5,500	4,900	4,500	41,000	40,000	32,000	25,000	11,000

Assumptions: 1120 MWe reactor, SSTI release, Indian Point population and wind rose, New York City Meteorology.

- a. No emergency response. b. Northeast Regional Shielding Factors. c. Not calculated. d. Consequence magnitude equalled or exceeded following 1 out of every 100 releases.

Figures 2.5-3 and 2.5-4 present the variation with distance of the risk to an individual of early health effects (death or injury) for seven emergency response scenarios. The figures show that, as distance decreases, the different scenarios predict increasingly similar individual risks (the seven risk curves converge). The curves converge at short distances because many weather sequences result in radiation doses large enough to have fatalities or injuries for each of the seven emergency response scenarios. For example, expeditious evacuation (1 hr delay) is not always adequate because for many weather sequences the radioactive plume reaches people before they begin to evacuate. And sheltering with expeditious relocation is inadequate because for many weather sequences fatal or injury causing doses are still received by sheltered persons even with expeditious relocation. Accordingly, because at short distances each of the seven scenarios fails to provide sufficient protection for a substantial number of weather sequences, at these distances little sensitivity to differences in emergency response is observed. In agreement with Table 2.5-6, both figures show that individual risk of early health consequences decreases most rapidly with distance for expeditious evacuation (1 hr delay, 10 mph) or sheltering with expeditious relocation (after 6 hr).

The emergency response submodel in CRAC2 is able to apply one emergency response scenario to an inner region and a second scenario to an outer region. Using this option, the impact of emergency response scenarios, which call for both evacuation and sheltering, and the effect of response beyond 10 miles were briefly examined. Table 2.5-7 presents some evacuation data from Table 2.5-2 and contrasts that data with results obtained for emergency response scenarios which call for evacuation of population within 10 miles and sheltering of population from 10 to 25 miles. The table shows that for Summary Evacuation, increasing the response distance from 10 to 25 miles decreases mean and 99th percentile early injury values by factors of 2 and 3.5, respectively, while mean and 99th percentile early fatality values are somewhat lowered (mean, 19%; 99th, 15%). The table also shows (1) that Summary Evacuation to 10 miles in combination with sheltering (relocation after 24 hr) from 10 to 25 miles is as effective as Summary Evacuation to 25 miles; and (2) that in comparison to Summary Evacuation, expeditious evacuation (1 hr delay, 10 mph)

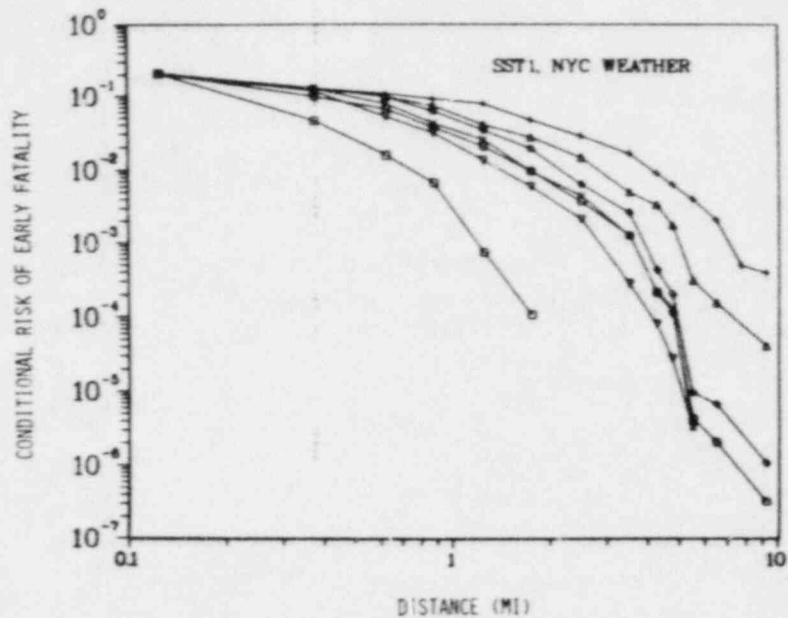


Figure 2.5-3. Conditional Risk of Early Fatality

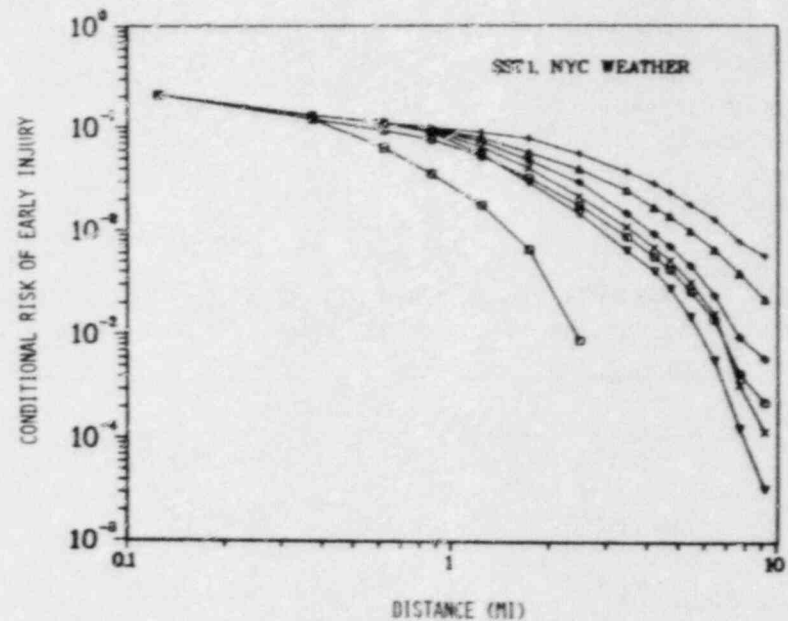


Figure 2.5-4. Conditional Risk of Early Injury

Legend

- + - No evacuation
- Δ - 5 hr delay, 1 mph, within 10 mi
- ◊ - 5 hr delay, 10 mph, within 10 mi
- × - 3 hr delay, 10 mph, within 10 mi
- - Summary Evacuation, within 10 mi
- ▽ - Sheltering within 10 mi, 6 hr relocation
- - 1 hr delay, 10 mph, within 10 mi

Assumptions: 1120 MWe reactor, uniform wind rose, New York City meteorology, results conditional on an SST1 release.

Table 2.5-7. Impact of Emergency Response Beyond 10 Miles on Early Fatalities and Early Injuries. Results are Conditional on an SST1 Release.

<u>Evacuation Distance (mi)</u>	<u>Evacuation Delay</u>	<u>Sheltering Distance (mi)</u>	<u>Early Fatalities</u>		<u>Early Injuries</u>	
			<u>Mean</u>	<u>99th Percentile</u>	<u>Mean</u>	<u>99th Percentile</u>
0 - 10	Summary	None	830	8,300	3600	33,000
0 - 25	Summary	None	700	7,200	1800	9,400
0 - 10	Summary	10 - 25	690	5,400	1900	8,400
0 - 10	1 hr	10 - 25	40	750	750	5,800

Assumptions: 1120 MWe reactor, SST1 release, Indian Point population and wind rose, New York City Meteorology, Northeast regional shielding factors, relocation of sheltered individuals after 24 hr.

to 10 miles combined with the sheltering (relocation after 24 hr) from 10 to 25 miles substantially reduces mean and 99th percentile values for early fatalities (factors of 17 and 7, respectively) and significantly reduces mean and 99th percentile values for early injuries (factors of 2.5 and 1.5, respectively). Further, peak early fatalities (conditional probabilities $\leq 10^{-3}$) are reduced by a factor of almost 10 (peak 15,000 to 1,600). Because of the substantial impact of emergency response beyond 10 miles upon peak early fatalities, it should be noted that most results presented in other sections of this report assume no immediate emergency response beyond 10 miles and consequently may significantly overestimate early fatality peaks.

Finally, Figure 2.5-5 indicates the sensitivity of early fatalities to the range of emergency response scenarios examined. In Figure 2.5-5 the CCDF for Summary Evacuation is the "base case" (see Section 2.2.4) result. The two bounding early fatality CCDFs for no emergency response and for expeditious evacuation to 25 miles show that the emergency response scenario selected has a substantial impact on consequence magnitude.

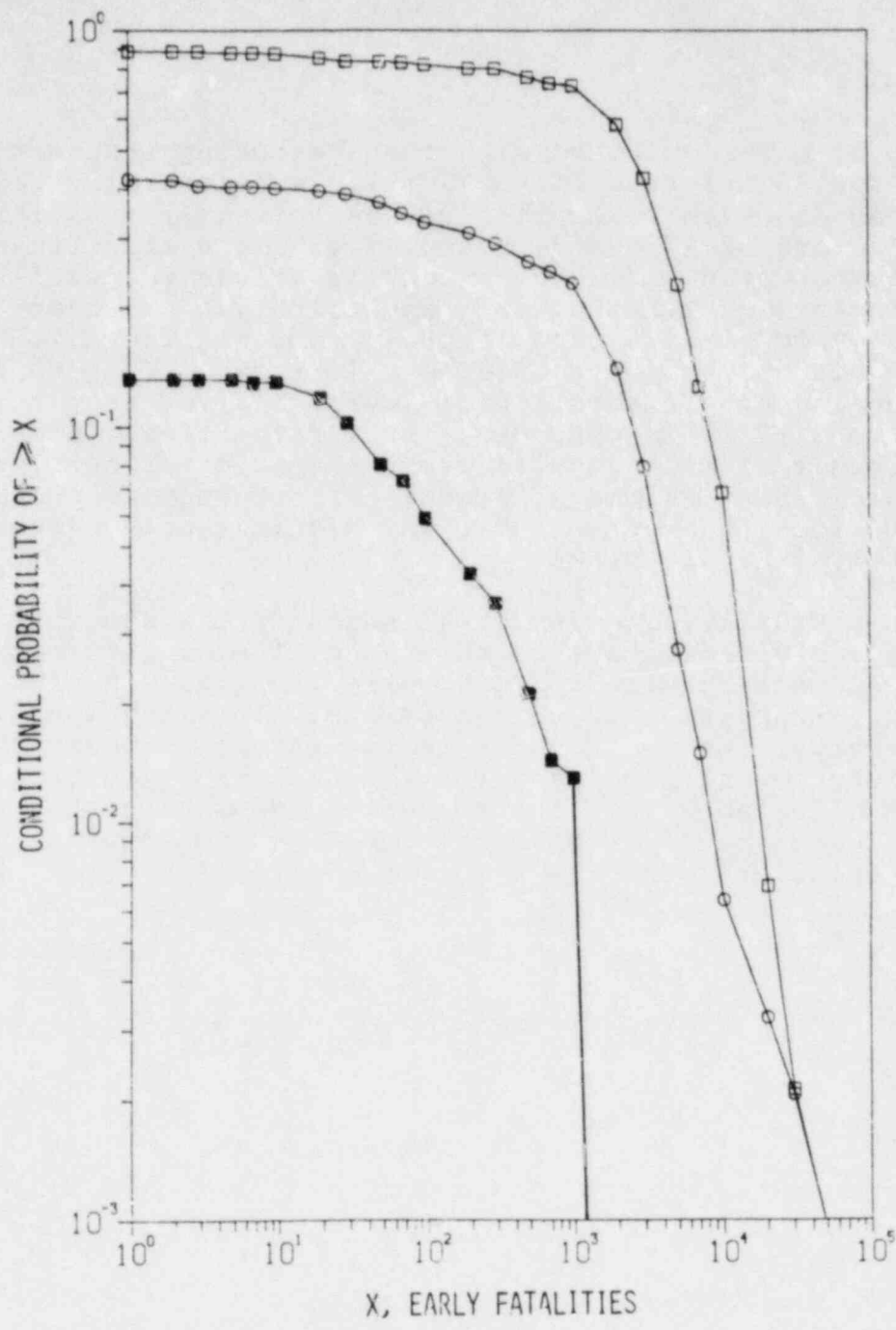


Figure 2.5-5. Impact of Range of Emergency Response Scenarios upon Early Fatalities. Results Conditional upon an SST1 Release

- - No emergency response
- - Summary Evacuation, within 10 mi
- - 1 hr delay, 10 mph, within 25 mi

Assumptions: 1120 MWe reactor, SST1 release, Indian Point population and wind rose, New York City meteorology.

2.6 Distance Dependencies of Reactor Accident Consequences

This section considers distances within which selected consequences might occur, as well as distances within which Protective Action Guides (PAGs) for radiation exposure [32] might be exceeded following a severe reactor accident. The sensitivities of these distances to meteorological conditions at the time of the accident, to differences between meteorological records, to accident severity, and to emergency response are examined. Because of the current controversy concerning the magnitudes of source terms for severe accidents (see Section 2.3.2), the impact of source term reductions on distance estimates is also considered.

The consequences that could result from a severe reactor accident include short-term effects such as early fatalities and injuries and long-term effects such as delayed cancer deaths and interdiction of land. Because early consequences would occur only after large, acute doses of radiation, these effects would be limited to areas close to the reactor (a few tens of miles). Population restrictions within these areas could therefore significantly impact the number of early consequences. As a result, estimates of distances to which fatal or injury-causing doses of radiation could be received are of interest for the development of reactor siting criteria. Following a severe reactor accident, contamination could be sufficiently high to require interdiction of property (buildings and land) to substantial distances (several tens of miles). Because interdiction of large areas could be a significant, and possibly dominant, contributor to the offsite costs of a reactor accident, distances to which land might be interdicted could also be an important consideration for the development of siting criteria. Since latent cancers can be induced by small doses of radiation, they can occur at large distances from the reactor. As a result, latent cancers would generally be less affected by population restrictions close to a reactor than would early fatalities or early injuries.

For each sampled meteorological sequence, the CRAC2 code calculates the maximum distances at which selected consequences might occur. These distances will depend on the magnitude and characteristics of

the source term as well as plume dispersion and depletion processes. By using the weather sequence sampling technique discussed in Section 2.2.1, the CRAC2 code can generate CCDFs of "maximum" consequence distances for any given source term. These curves illustrate the impact that radionuclide dispersion, which is determined by the weather conditions at the time of the accident, has on distances to which consequences occur.

Figures 2.6-1, 2.6-2, and 2.6-3 show SST1 and SST2 early fatality distance, early injury distance, and interdiction distance^a CCDFs for the 29 meteorological records discussed in Section 2.4. The figures show that for an SST1 release early fatality distances range from 1 to 20 miles, early injury distances from 1 to 80 miles, and interdiction distances from 1 to 100 miles. Thus, for a single event, consequence distances are strongly influenced by the weather at the time of the release. However, the figures also show that for a specific release (e.g., SST1), CCDFs calculated using different meteorological records are quite similar. For example, the 90th percentile values of the 29 early fatality CCDFs calculated assuming an SST1 release range only from 6 to 9 miles.

These results also show that for the SST1 release, early fatalities would be limited to about 20 miles, injuries to about 50 miles, and land interdiction to about 100 miles. For the SST2 release, early fatalities would generally be limited to about 2 miles, injuries to about 8 miles, and land interdiction to about 10 miles. For each set of CCDFs, the variation in the peaks, and probabilities of the peaks, is principally due to a combination of (1) the order of magnitude variation in rain frequencies for the 29 meteorological records and (2) errors inherent in the weather sequence sampling procedure (see Section 2.4).

- a. Fatality and injury distances are defined to be distances within which individuals are at risk of being an early fatality or injury given the assumed release (SST1 or SST2). The interdiction distance is defined to be the distance within which land would be interdicted following the assumed release. The SST3 release is not large enough to cause early fatalities, early injuries, or interdiction of land offsite.

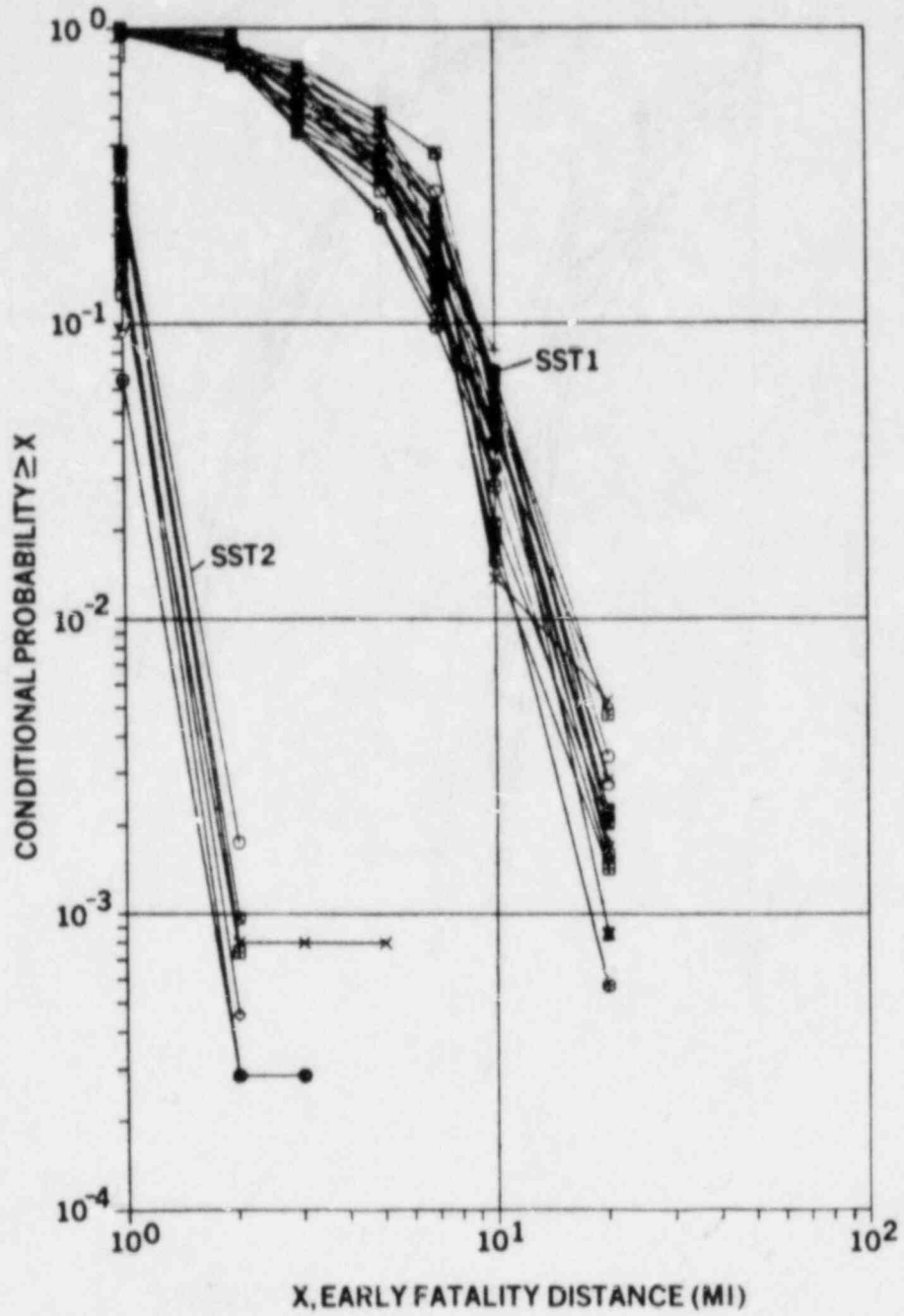


Figure 2.6-1. Conditional CCDFs of Early Fatality Distance for 29 Meteorological Records Calculated Assuming SST1 and SST2 Releases from an 1120 MWe PWR and No Emergency Response.

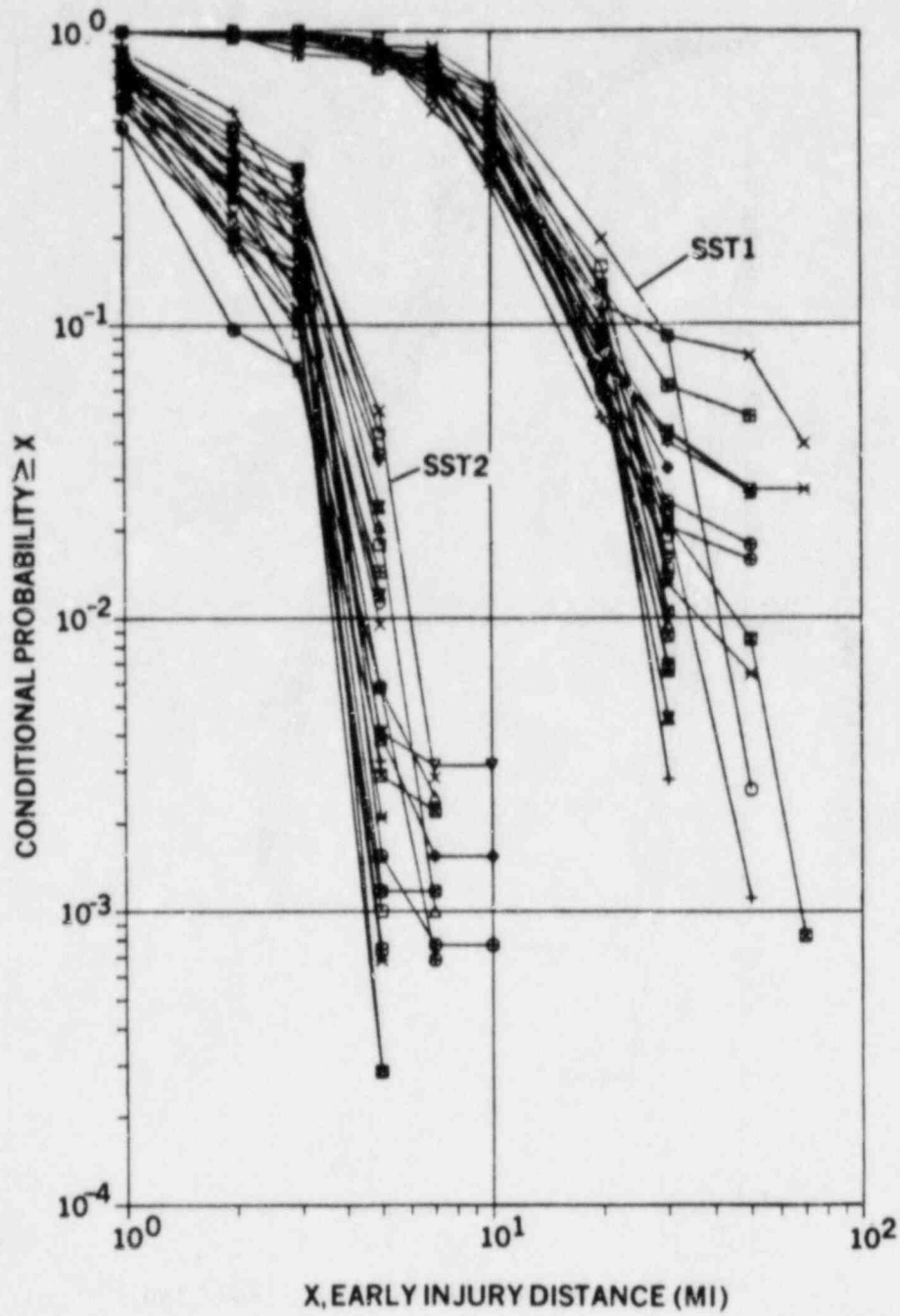


Figure 2.6-2. Conditional CCDFs of Early Injury Distance for 29 Meteorological Records Calculated Assuming SST1 and SST2 Releases from an 1120 MWe PWR and No Emergency Response.

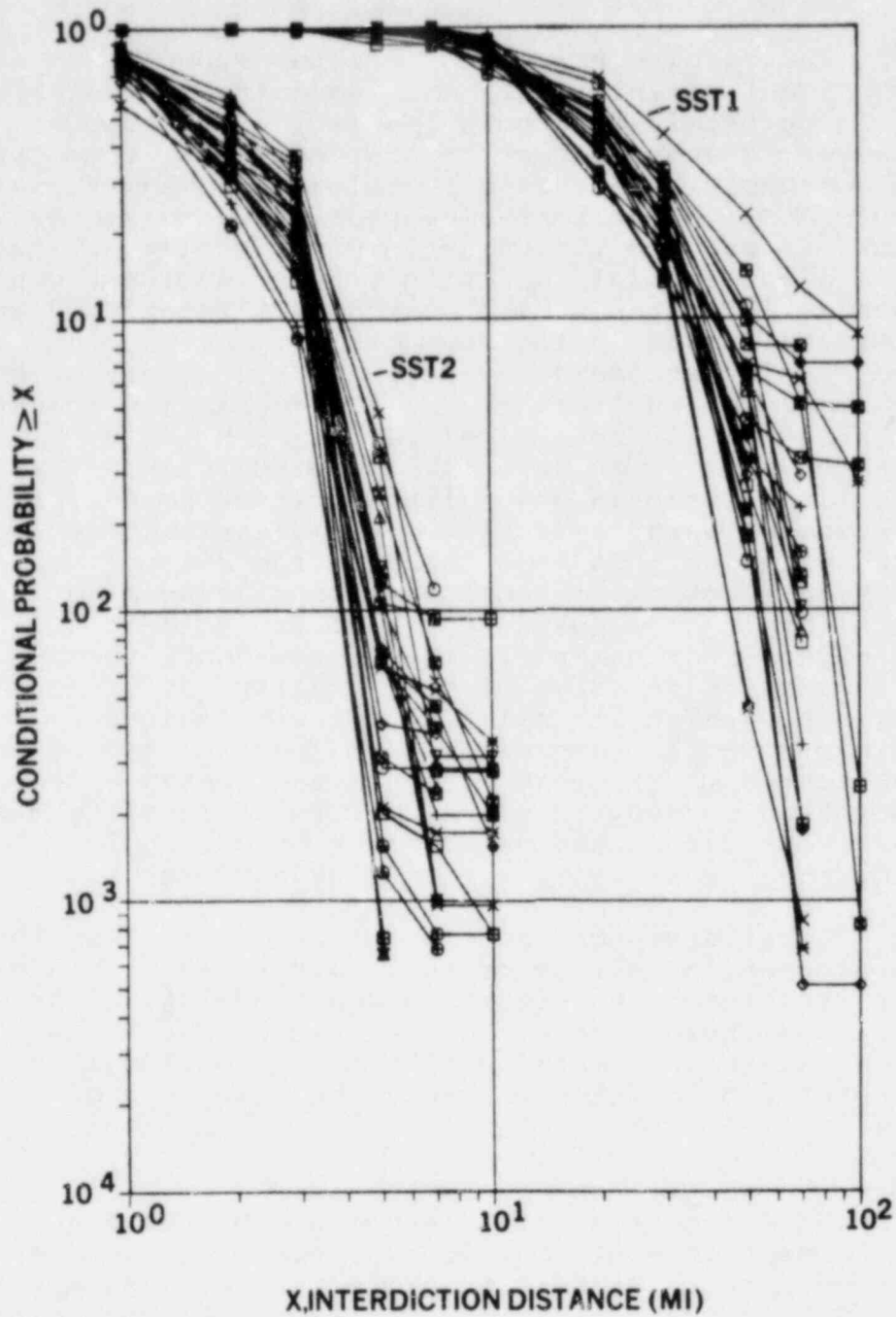


Figure 2.6-3. Conditional CCDFs of Interdiction Distance for 29 Meteorological Records Calculated Assuming SST1 and SST2 Releases from an 1120 MWe PWR.

The results presented thus far show the distances to which fatal or injury-causing doses of radiation could be received assuming no emergency response. However, given a severe reactor accident, some type of emergency response would be expected and therefore, acute doses close to the reactor could be reduced. As shown in Section 2.5, emergency protective actions can have a substantial impact on reactor accident consequences. Figure 2.6-4 compares SST1 fatality distance CCDFs calculated using New York City meteorology and four different emergency response scenarios: no emergency response, sheltering, and two evacuation scenarios (1 hr delay, 10 mph, within 25 mi; 5 hr delay, 10 mph, within 25 mi). In general, these CCDFs show that early fatality distances are quite sensitive to emergency response. Thus, effective implementation of emergency protective actions in areas near the reactor could result in substantial reductions in distances to which fatal or injury-causing doses of radiation could be received. For example, with no emergency response the 90th percentile value of the fatality radius for an SST1 release is ≥ 8 miles, while with sheltering the 90th percentile distance is 4 miles and with expeditious evacuation (1 hr delay, 10 mph) the distance is further decreased to about 2 miles. CCDFs of fatality distance that were calculated using other meteorological records show the same sensitivity to emergency response.

Other distances that might be of interest for the development of siting criteria are those within which the EPA Protective Action Guides (PAGs) [32] for whole body and thyroid dose might be exceeded. A PAG is defined as the projected dose^a to an individual in the general public which warrants the initiation of emergency

a. The "projected dose" is defined by the EPA as the dose that would be received within a few days following the release if no protective actions are taken. PAGs range from 1 to 5 rem for whole body exposure and from 5 to 25 rem for projected dose to the thyroid. The lower value of these ranges should be used if there are no major local constraints limiting the ability to provide protection at that level. However, when determining the need for protective action, in no case should the higher value be exceeded.

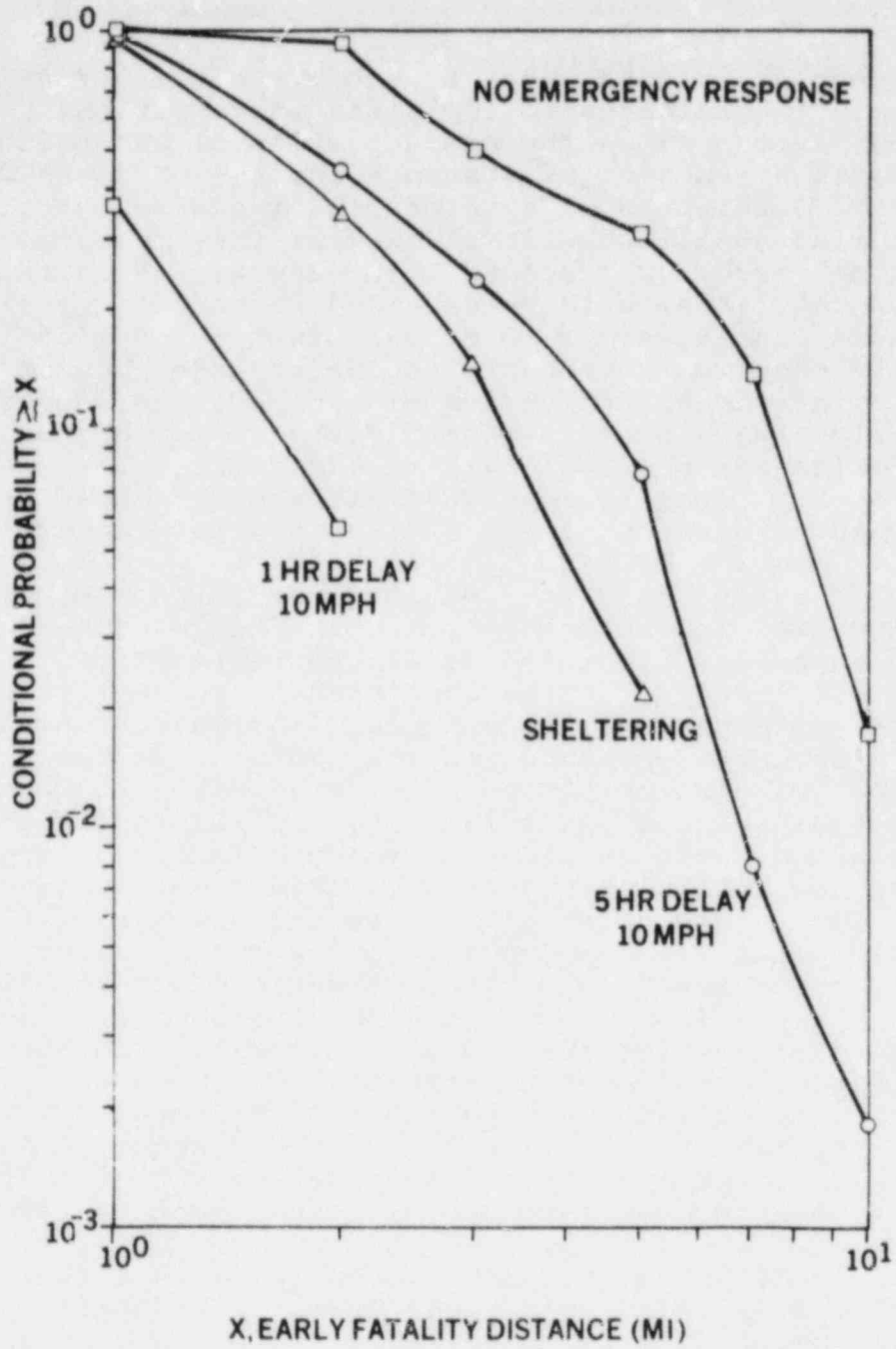
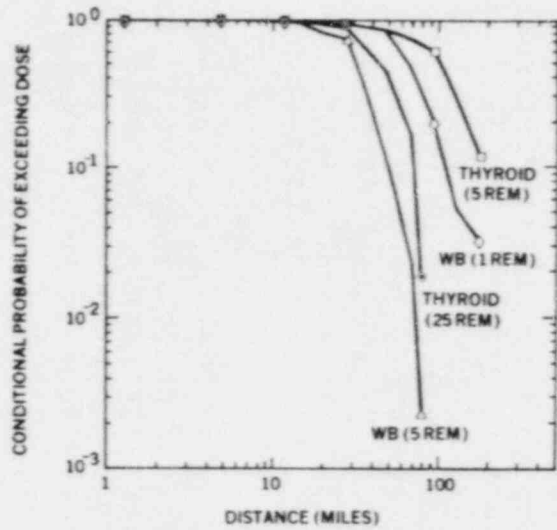


Figure 2.6-4. Sensitivity of SST1 Early Fatality Distances to Emergency Response. Assumptions: New York City meteorology, 1120 MWe PWR, and 25 Mile Response Radius.

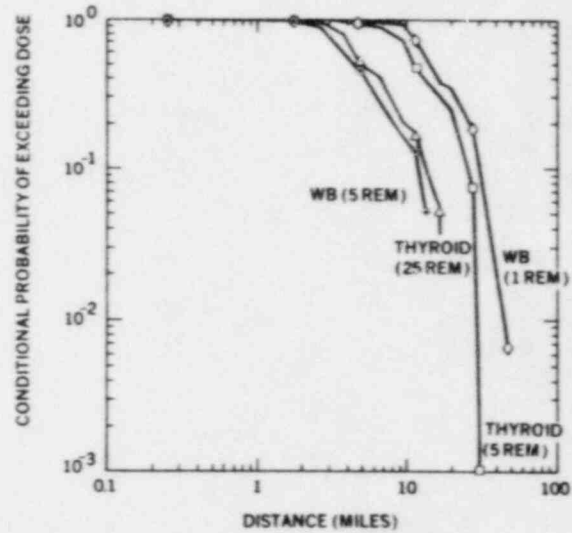
protective actions and, as such, is a trigger value to aid in decisions to implement these actions. Figure 2.6-5 shows the probabilities of exceeding the PAGs as a function of distance for the SST1, SST2, and SST3 releases. The probabilities were calculated assuming an 1120 MWe PWR, New York City meteorology, and no emergency response. In general, these results show that PAGs could be exceeded to very large distances (in excess of 50 miles) given an SST1 accident while they would probably not be exceeded beyond about 30 miles for an SST2 release. In addition, doses would nearly always exceed PAGs to distances of approximately 30 miles for the SST1 release and 2 miles for the SST2 release. Doses from an SST3 release are shown not to exceed PAGs beyond about 3 miles of the reactor.

The results discussed thus far in this section are summarized in Table 2.6-1. In the table consequence distances are presented for three releases (SST1, SST2, and SST3) and for three conditional probability levels: mean, 99th percentile, and peak (maximum calculated). The distances presented in the table summarize the large number of distance CCDFs calculated using the 29 meteorological records. The fatality and injury distances presented could be reduced by any effective emergency response action. In general, Table 2.6-1 suggests that: (1) for severe core melt accidents, early fatalities would generally not occur beyond about 15 miles, and in the worst case, would be confined to about 25 miles, while early injuries would probably be confined to downwind distances of about 50 miles; (2) for smaller core melt accidents (on the order of SST2 in severity), early fatalities would be confined to about 2 miles, and injuries and land interdiction to about 7 miles; and (3) for accidents on the order of SST3 in severity, PAGs would probably not be exceeded beyond a few miles.

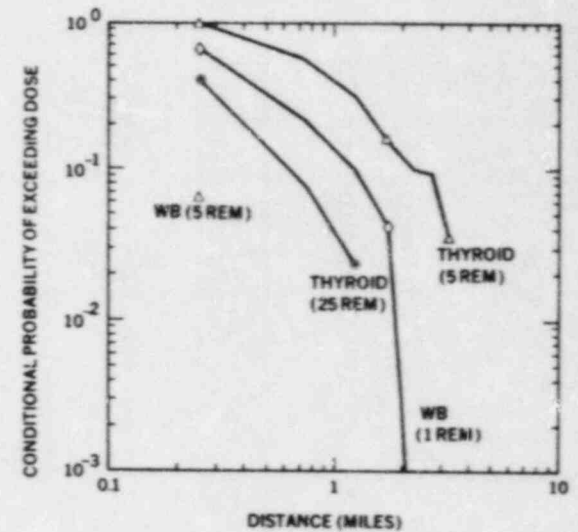
As discussed earlier, latent somatic effects could result from relatively small doses of radiation. Therefore, given a reactor accident, these consequences could occur at large downwind distances from the reactor. Figure 2.6-6 shows the cumulative fraction of latent cancer fatalities versus distance for the SST1, SST2, and SST3 releases. These curves were calculated assuming an 1120 MWe PWR, New York City meteorology, and a one mile per hour evacuation to ten miles after a five hour delay. In general, the results show that significant fractions of latent health effects could occur at large distances from the reactor. For the uniform



a) SST1



b) SST2



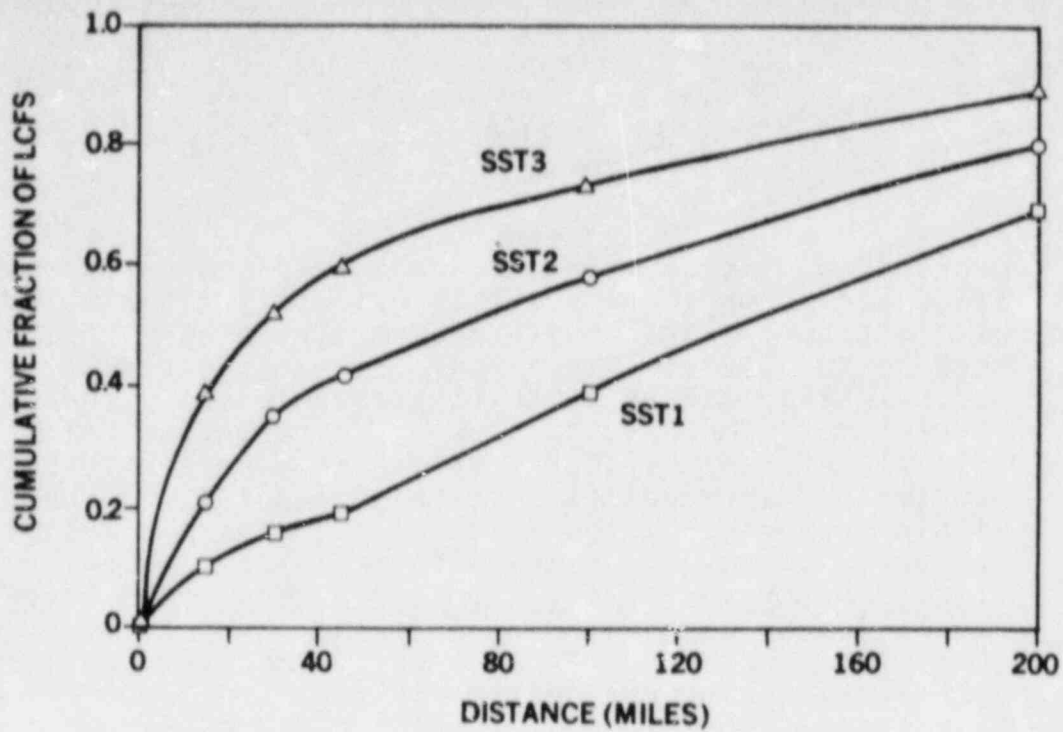
c) SST3

Figure 2.6-5. Conditional Probability of Exceeding PAGs Versus Distance for SST1, SST2, and SST3 Source Terms. Assumptions: 1120 MWe PWR, New York City meteorology, and no emergency response.

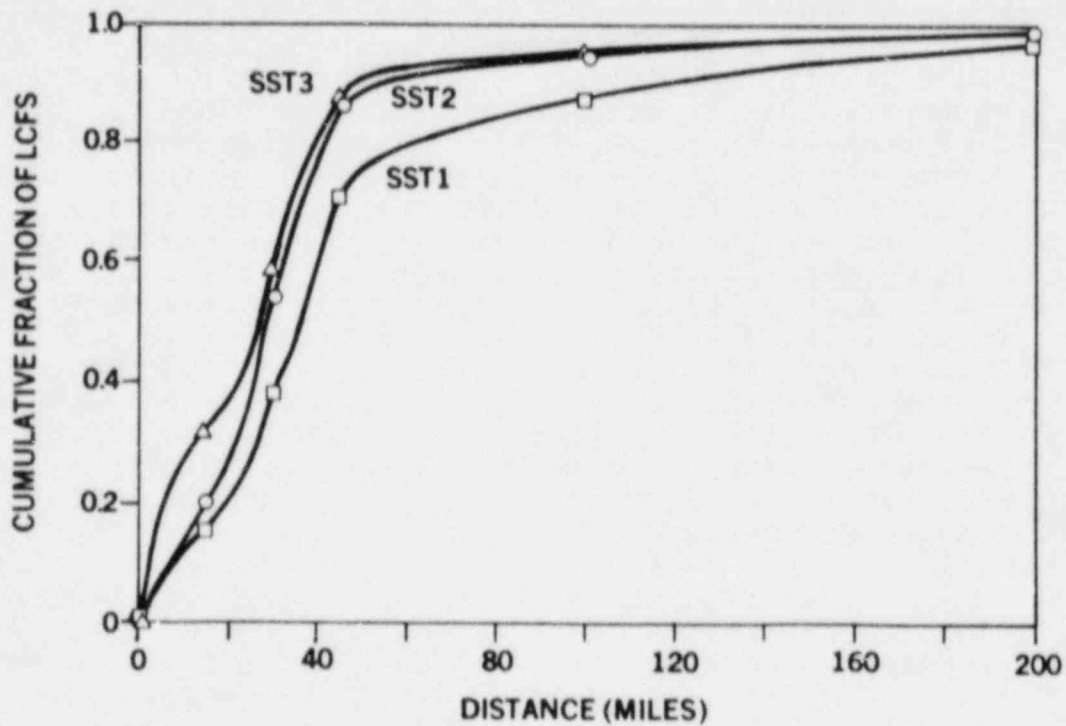
Table 2.6-1. Summary of Consequence Distances^a (miles)

<u>Source Term</u>	<u>Consequence</u>	<u>Conditional Probability Level^b</u>		
		<u>Mean</u>	<u>99%</u>	<u>Calc Max</u>
SST1	Early Fatalities	<5	≤15	<25
	Early Injuries	~10	~30	≥50
	Land Interdiction	~20	>50	>50
	PAGs ^c	≥50	>50	>50
SST2	Early Fatalities	~0.5	<2	≈2
	Early Injuries	<2	<5	~5
	Land Interdiction	<2	~7	~10
	PAGs ^c	≤20	~20	<50
SST3	PAGs ^c	≤0.5	<2	<3

- a. These distances are for a 1120 MWe PWR which is comparable in size to many of the most recently sited nuclear reactors.
- b. Mean distances are the average of the probability distributions of distance; 99% distances refer to those beyond which a consequence or dose is calculated to occur in 1 in 100 accidents; and the calculated maxima represent the largest distances calculated.
- c. A PAG is defined as the "projected" dose to an individual in the general public which warrants the initiation of emergency protective actions. PAGs range from 1 to 5 rem for whole body exposure and from 5 to 25 rem for projected dose to the thyroid.



a) Uniform Population Distribution



b) Indian Point Population Distribution

Figure 2.6-6. Cumulative Fraction of Latent Cancer Fatalities as a Function of Distance from the Reactor a) for a Uniform Population Distribution and b) for the Indian Point Population Distribution.

Assumptions: 1120 MWe PWR, New York City meteorology, and a slow evacuation (5 hr delay, 1 mph, 10 mi response distance).

population distribution, the calculated cancer fatalities are shown to be somewhat uniformly distributed with distance. This uniform distribution results because the decrease in cancer risk with distance is approximately offset by the increase in the exposed population. The results shown for the Indian Point site illustrate the impact of a highly non-uniform population distribution. The high population densities within approximately 50 miles of the Indian Point site (relative to lower densities further away) cause a significantly larger fraction of the predicted cancer fatalities to occur within 50 miles of the reactor. Thus, the high non-uniformity of the exposed population distribution also causes the distribution of cancer fatalities to be non-uniform with distance.

Section 2.3.2 discussed recent reviews of accident phenomenology which indicate that the magnitudes of current source terms for severe reactor accidents may be significantly too large. To investigate the impact of source term reductions on distances to which consequences might occur, a series of calculations was performed for the SST1 release reduced by arbitrary factors of 2, 10, 20, and 100. Important assumptions for the calculations included New York City meteorology, an 1120 MWe PWR, and no emergency response. Table 2.6-2 summarizes the results and in general shows that reductions in severe accident source terms substantially reduce consequence distances. An order of magnitude reduction in the SST1 release reduced the peak fatal distance from about 20 miles to 5 miles while a two-order of magnitude reduction reduced the peak distance to 1 mile. Similar reductions are shown for early injury and land interdiction distances.

This section has examined the impact of meteorological conditions, accident severity, and emergency response on consequence distances. Four factors, that also could influence consequence distances, are discussed in other sections of this report. They are reactor size (i.e., size of radionuclide inventory, see Section 2.7.1), plume heat content (determines plume rise, see Section 2.7.2), dry deposition velocity (see Section 2.7.3) and interdiction criteria (see Section 2.7.5).

Table 2.6-2. Sensitivity of Fatal, Injury, and Interdiction Distances to Release Magnitude^a

<u>Source Term</u>	<u>Fatal Distance (mi)</u>			<u>Injury Distance (mi)</u>			<u>Interdiction Distance (mi)</u>		
	<u>Mean</u>	<u>99%</u> ^b	<u>Peak</u> ^b	<u>Mean</u>	<u>99%</u> ^b	<u>Peak</u> ^b	<u>Mean</u>	<u>99%</u> ^b	<u>Peak</u> ^b
SST1	3.9	12	18	11	35	50	19	55	85
1/2 SST1 ^c	2.5	10	18	7.0	20	25	14	45	50
1/10 SST1 ^c	0.9	2.2	5.0	2.8	10	18	5.5	18	25
1/20 SST1 ^c	0.5	2.0	2.0	1.9	7.0	10	3.6	12	18
1/100 SST1 ^c	0	1.0	1.0	0.9	4.0	5.0	1.1	10	10

- a. Assumptions: New York City meteorology, 1120 MWe PWR, and no emergency response.
- b. The 99 percent distances refer are the distances beyond which a consequence is calculated to occur in only 1 in 100 accidents. The peak result is that obtained for the most unfavorable weather sequence sampled.
- c. Release fractions reduced for all isotopes except noble gases.

2.7 Other Sensitivity Calculations

2.7.1 Reactor Size

All of the calculations presented in previous sections of this report assume an 1120 MWe reactor. This reactor size was selected because many reactors currently operating and most under construction are about this size. Because consequences depend strongly on the amount of radioactivity released (see Section 2.3, Accident Source Terms), which in turn is dependent on reactor size, the sensitivity of consequences to reactor size was examined. Calculations were performed for nine reactor sizes ranging from 11.2 to 1500 MWe. All calculations assumed a 1120 MWe core radionuclide inventory scaled according to reactor size, an SST1 release, New York City meteorology, and the Indian Point population distribution and wind rose. The linear scaling procedure used is described in Appendix B, Core Radionuclide Inventories, which also discusses inventory changes due to annual operating cycle and differences between PWR and BWR inventories.

Figures 2.7.1-1 and 2.7.1-2 present conditional CCDFs of early fatalities, early injuries, latent cancer fatalities, interdiction distance, and interdicted land area for five of the nine reactor sizes examined, assuming Summary Evacuation. Table 2.7.1-1 presents the mean and 99th percentile values of these distributions. The effects of emergency response and reactor size on mean early fatalities are presented in Table 2.7.1-2. Finally, Figure 2.7.1-3 presents plots of the mean values presented in each table versus reactor size.

Several conclusions can be drawn from these results. First, Figure 2.7.1-3 shows that mean values of all five consequences increase roughly linearly with reactor size. The rates of increase are largest for early fatalities and smallest for interdiction distance. Table 2.7.1-1 shows that mean values increase more rapidly than 99th percentile values. The mean early fatality results presented in Table 2.7.1-2 clearly display the significant impact of emergency response, seen previously (see Section 2.5). For an 1120 MWe reactor, No Evacuation yields a mean result of almost 3600 early fatalities, while Best Evacuation (1 hr delay, 10 mph, 10 mi response region) decreases this number to less than 300. Figure 2.7.1-3a shows that for an emergency response of a given effectiveness, there is a reactor size (x-axis

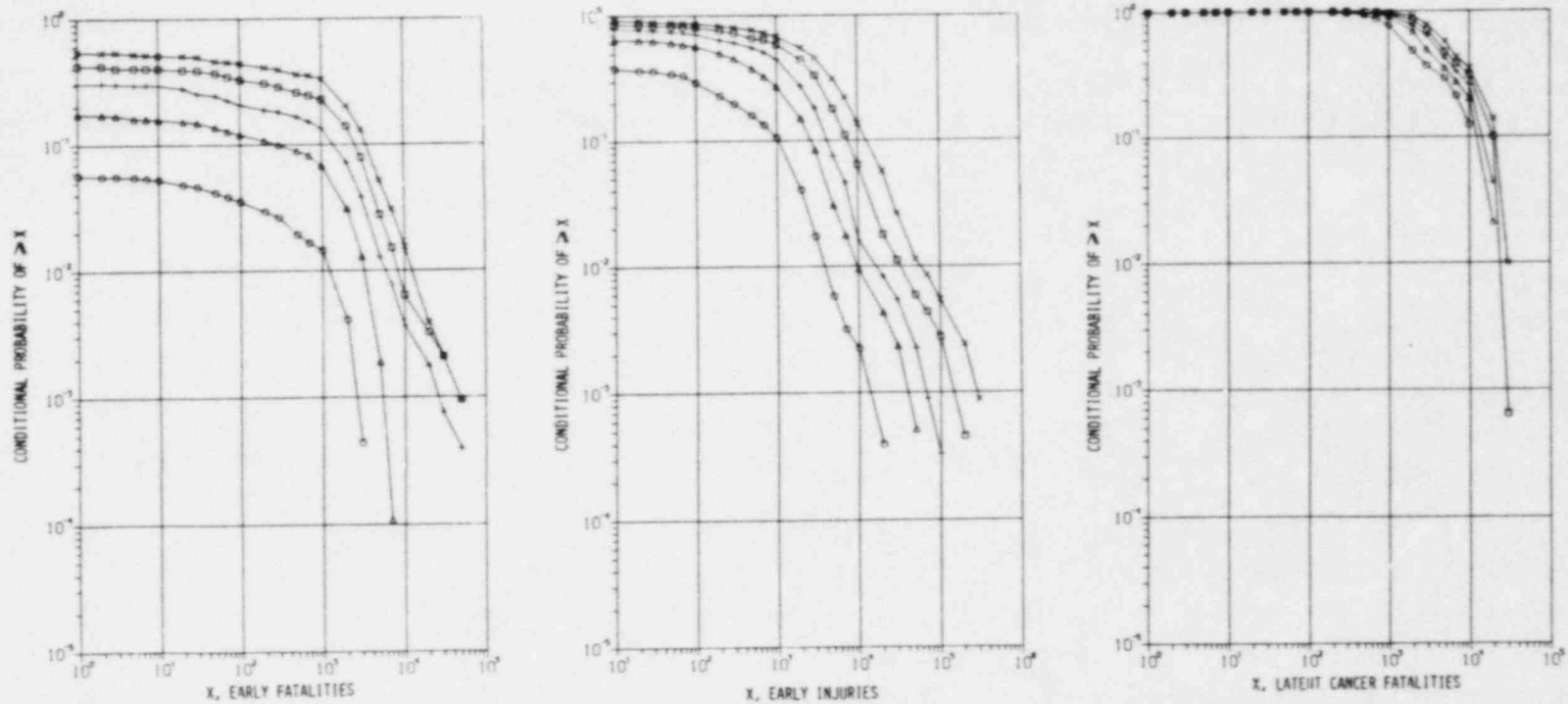


Figure 2.7.1-1. Effect of Reactor Size upon a) Early Fatalities, b) Early Injuries, and c) Latent Cancer Fatalities, Conditional on an SST1 Release.

Legend

- - 1500 MWe reactor
- - 1120 MWe reactor
- + - 750 MWe reactor
- △ - 500 MWe reactor
- - 250 MWe reactor

Assumptions: 1120 MWe core radionuclide inventory scaled to reactor size, SST1 release, New York City Meteorology, Indian Point wind rose and population, Summary Evacuation.

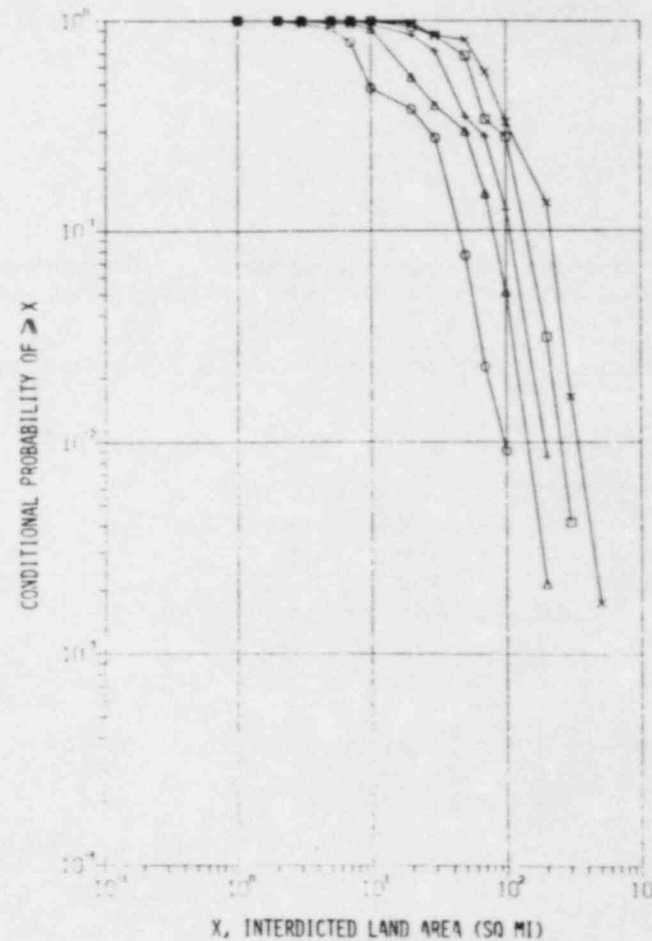
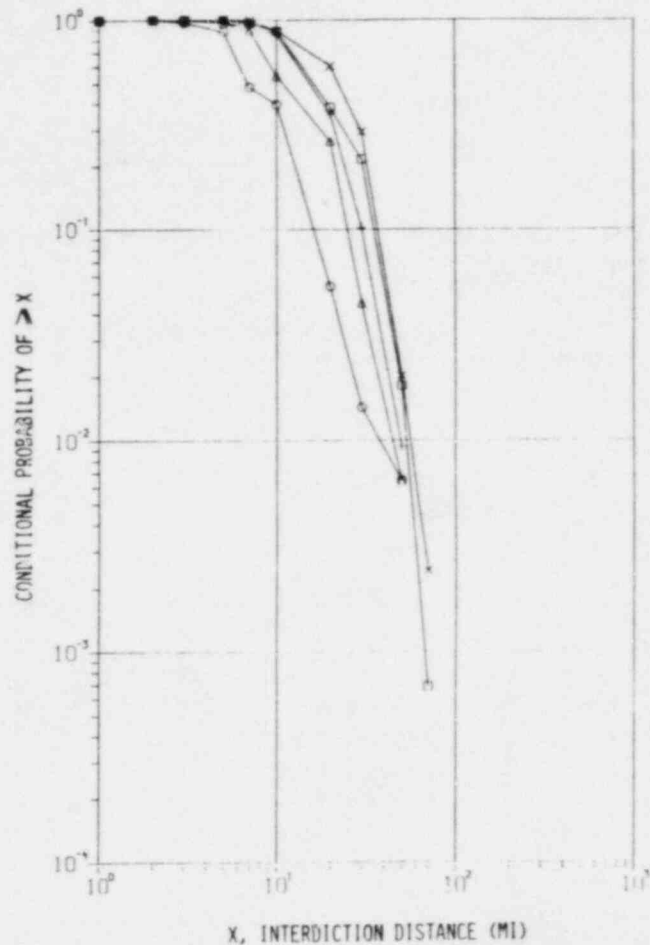


Figure 2.7.1-2. Effect of Reactor size upon a) Interdiction Distance (mi) and b) Interdicted Land Area (sq mi), Conditional on an SST1 Release.

Legend

- x - 1500 MWe reactor
- - 1120 MWe reactor
- + - 750 MWe reactor
- △ - 500 MWe reactor
- - 250 MWe reactor

Assumptions: 1120 MWe core radionuclide inventory scaled to reactor size, SST1 release, New York City meteorology, Indian Point wind rose and population, Summary Evacuation.

Table 2.7.1-1. Dependence of Consequences Upon Reactor Size, Conditional on an SST1 Release^a

Reactor Size (MWe)	Early Fatalities		Early Injuries		Latent Cancer Fatalities		Interdiction Distance (mi)		Interdicted Land Area (sq mi)	
	Mean	99th	Mean	99th	Mean	99th	Mean	99th	Mean	99th
250	34	1,200	323	3,800	3970	10,000	9.7	38	20.8	97
500	172	3,200	1020	9,700	5560	20,000	13.1	45	37.2	120
750	455	5,900	1880	16,000	6710	20,000	16.0	49	53.7	190
1120	831	8,200	3640	33,000	8110	24,000	19.3	54	75.8	250
1500	1250	12,000	6340	57,000	9600	30,000	22.8	56	106	340

a. Assumptions: 1120 MWe core radionuclide inventory scaled according to reactor size, SST1 release, New York City meteorology, Indian Point population and wind rose, Summary Evacuation.

Table 2.7.1-2 Dependence of Mean Early Fatalities Upon Reactor Size and Evacuation Scenario, Conditional on an SST1 Release^a

Reactor Size (MWe)	Evacuation Scenario		
	Best Evacuation ^b	Summary Evacuation	No Evacuation
11.2 ^c	0	0.3	1
56 ^c	0	2	34
112 ^c	0	9	147
250	0.01	34	551
500	6	172	1490
560 ^c	17	224	1700
750	102	455	2380
1120	176	831	3580
1500	287	1250	4880

- a. 1120 MWe core radionuclide inventory scaled according to reactor size, SST1 release, New York City meteorology, Indian Point population and wind rose.
- b. 1 hour delay, 10 mph, 10 mi response region (see Section 2.5).
- c. Noble gas release fractions not scaled; this has no significant impact on early fatalities (see Section 2.3, Accident Source Terms).

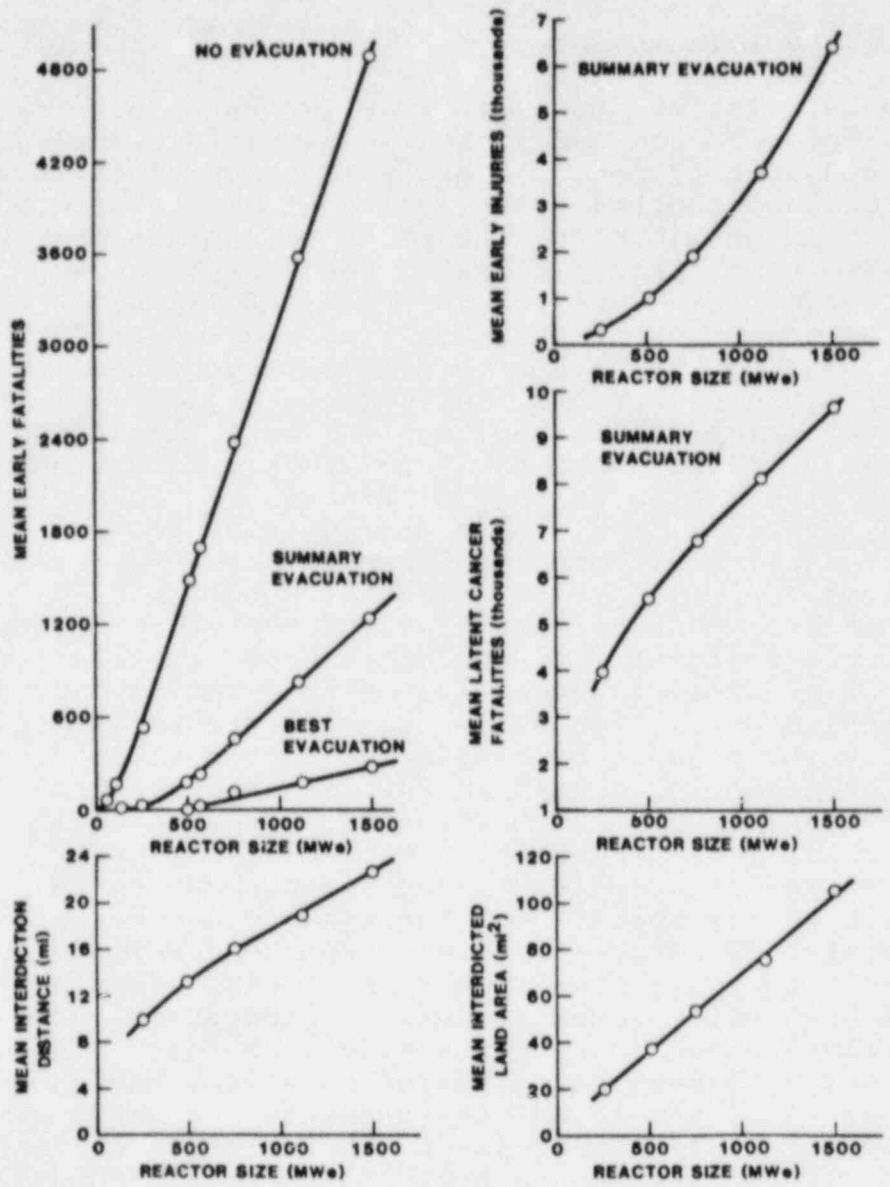


Figure 2.7.1-3. Plots of Mean Values of a) Early Fatalities, b) Early injuries, c) Latent Cancer Fatalities, d) Interdiction Distance (mi), and e) Interdicted Land Area (sq mi) vs Reactor Size, Conditional on an SST1 Release.

Assumptions: 1120 Mwe core radionuclide inventory scaled to reactor size, SST1 release, New York City meteorology, Indian Point population and wind rose.

intercept) for which on the average (mean result) few early fatalities would be expected. For Best Evacuation that size is ~500 MWe; for Summary Evacuation, ~100 MWe; and for no evacuation, ~10 MWe.

2.7.2 Energy Release Rate

The calculations considered so far have been for ground-level releases containing no sensible heat, i.e., nonbuoyant plumes. In an accident where there is a large uncontrolled release directly to the atmosphere, it is possible for the plume to contain a sizable amount of sensible heat. For example, the release categories described in WASH-1400 [1] had energy release rates of up to several hundred million BTUs per hour.^a The rate of energy release determines the final plume height and, therefore, the downwind distance at which the plume first contacts the ground (touchdown). Since under the same weather conditions a buoyant plume would be more dilute at touchdown than a nonbuoyant plume, a significant reduction in the number of early health effects is possible. However, since plume depletion by dry deposition occurs only after touchdown, buoyant plumes might therefore produce ground concentrations high enough to produce early effects at greater distances than nonbuoyant plumes. Furthermore, for highly buoyant plumes, precipitation-washout is the primary mechanism by which radioactive material reaches the ground in sufficient concentrations to cause early health effects. Thus, for a buoyant release the probability of having any early fatalities and injuries is strongly dependent on the occurrence of precipitation. The final plume height is calculated in CRAC2 using the formulae developed by Briggs [33] for emissions from smokestacks. Considerable differences could exist between smokestack plumes and plumes released in a reactor accident [34]. These differences have been investigated by Russo, Wayland, and Ritchie [35] who found that predicted consequences were only marginally sensitive to the moisture content of the plume and atmosphere but, under certain conditions, consequences could be quite sensitive to radioactive heating and initial plume momentum.

For the present study, the sensitivity of predicted consequences to energy release rate was investigated

a. In WASH-1400, an energy release rate of 170×10^6 BTU/hr was assumed for a PWR-2 accident.

by performing calculations for an SST1 release with three arbitrary energy release rates: 17, 170, and 430 million BTU/hour. New York City meteorology and a uniform population density of 50 people per square mile beyond 1 mile were assumed. Table 2.7.2-1 compares selected results for these energy release rates with a cold (no sensible heat) SST1 release (the base case, see Section 2.2.4).

Table 2.7.2-1. Sensitivity of Estimated Consequences to Energy Release Rate^a

<u>Release</u>	SST1	SST1	SST1	SST1
<u>Energy Release Rate (BTU/hr)</u>	0	17x10 ⁶	170x10 ⁶	430x10 ⁶
Mean Early Fatalities				
Summary Evacuation	22	12	9	10
No Evacuation	140	140	47	47
Mean Early Injuries				
Summary Evacuation	140	180	110	85
No Evacuation	350	390	270	150
Mean Latent Cancer Fatalities				
	730	790	830	860
Maximum Calculated Fatal Distance (mi)				
	17.5	17.5	25	25
Maximum Calculated Injury Distance (mi)				
	50	50	50	60
Maximum Calculated Land Interdiction Distance (mi)				
	85	85	85	85

a. Assumptions: New York City meteorology, uniform population of 50 people per square mile beyond 1 mile.

The results for the low-energy release (17×10^6 BTU/hr) differ only slightly from those for the cold release, because this release rate is not large enough to cause substantial differences in the plume touchdown point. The two high-energy release rates result in consequences markedly different from the cold release. Because the occurrence of precipitation is necessary to cause significant numbers of early health effects for hot releases, the mean number of early effects is lower for the high-energy releases.

At very large distances, the amount of initial plume-rise does not significantly affect the transport and deposition of radioactive material. Consequently, latent cancer fatalities, which occur to great distances (see Section 2.6), are not significantly affected by plume buoyancy. The maximum observed fatal distance is 8 miles farther for the high-energy releases, although the maximum calculated injury distance is only slightly increased and interdicted land distance is unaffected. Neither land interdiction nor injury distances are very sensitive to energy release rate because these consequences also occur to distances where initial plume rise is generally not important.

Figure 2.7.2-1 plots the conditional individual risk of early fatality versus distance for the four energy release rates, assuming a uniform wind rose. Within 10 miles, the hot releases have lower risks than the cold releases. However, for low probability events (i.e., precipitation), the hot releases could result in fatalities out to 25 miles. The non-monotonicity in the risk at about 8 miles for the two hot releases (170×10^6 and 430×10^6 BTU/hr) is believed to be an artifact of the weather-sequence sampling procedure used (see Section 2.4.1).

In summary, for an SST1 release the estimated numbers of early fatalities and injuries and the distance to which early fatalities occur are both quite sensitive to the energy release rate. However, consequences which can occur to great distances, such as latent cancer fatalities, are not sensitive to energy release rate. The maximum distances, to which early injuries may occur or land may be interdicted, are also not sensitive to energy release rate. A cautionary note: these conclusions may not hold for source terms significantly smaller than SST1.

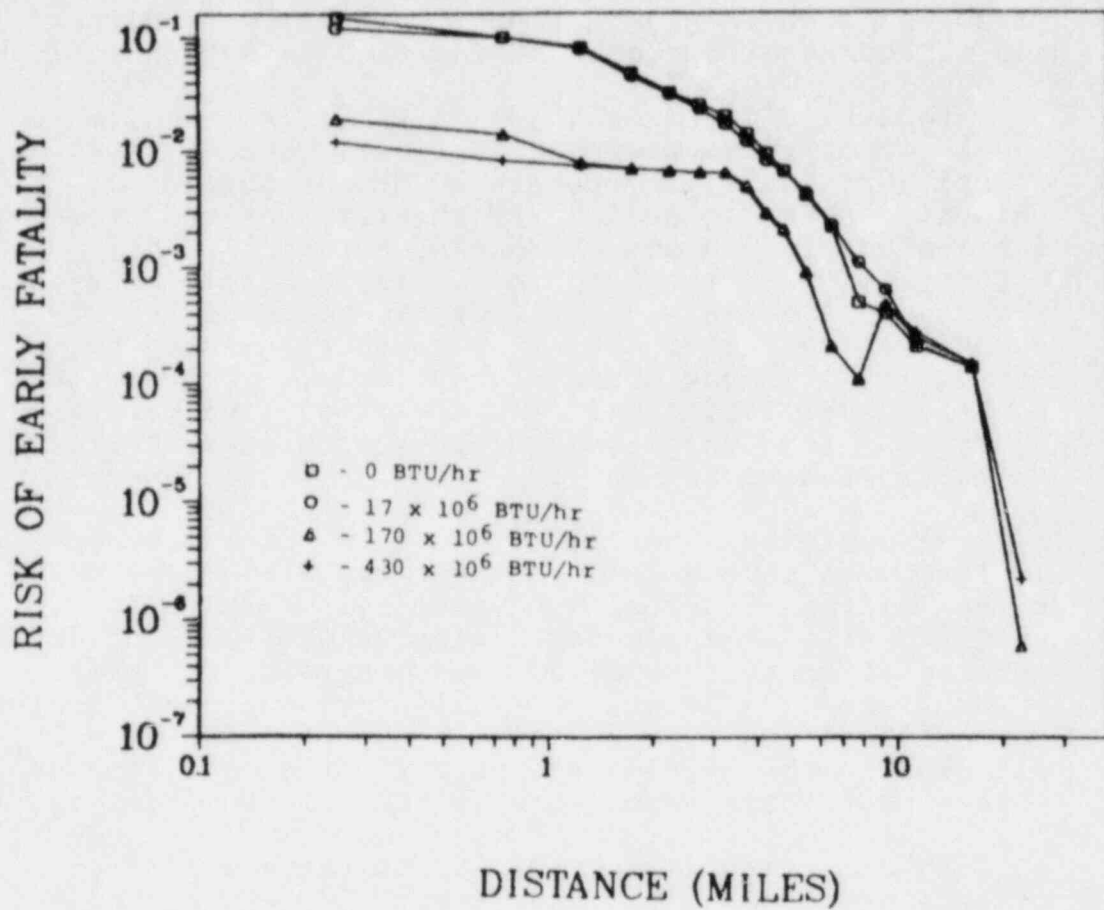


Figure 2.7.2-1. Individual Risk of Early Fatality Versus Distance for 4 Energy Release Rates, Conditional on an SST1 Release. Assumptions: SST1 release, New York City meteorology, uniform wind rose, no emergency response.

2.7.3 Dry Deposition Velocity

The deposition of radioactive material on the ground is the first step in many of the pathways by which radioactive material can reach people. Dry deposition of airborne material onto a surface is a complex process which includes a number of different phenomena such as gravitational settling, turbulent and molecular diffusion, and inertial impaction [36].

Hosker [37] and Kaul [38] have reviewed current models of dry removal processes. All current dry-deposition models incorporate a "dry-deposition velocity" which is defined as the ratio of the time-integrated air concentration of a material to the concentration of the material on the ground. A large number of parameters can affect the value of the deposition velocity. About 80 have been listed by Sehmel [39]. Among these are surface roughness, relative humidity, chemical composition, and particle diameter. Dry deposition velocity is highly sensitive to particle diameter [39].

Radioactive material released to the atmosphere is likely to have a range of particle diameters, each with a different deposition velocity. Despite this, in CRAC2 only a single deposition velocity may be input for each element considered, and generally the same value (1 cm/sec) is used for all elements except noble gases (the deposition velocity of noble gases is zero). All CRAC2 calculations presented in other sections of this report treat deposition velocity in this manner.

As discussed in Section 2.2.3, there are large uncertainties about the characteristics of the radioactive aerosol released from containment. Because predicted ground concentrations can be very sensitive to deposition velocity, a sensitivity analysis was performed to assess the impact of dry deposition velocity on predicted consequences. The analysis was somewhat simplistic in that only a single deposition velocity was used. Thus, no attempt was made to account for a range of particle sizes by use of a distribution of deposition velocities. Also neglected were effects of chemical composition and the possibility that different elements may be associated with particles of different sizes. Gravitational settling of particles, which can be treated by "tilted plume" models [40] was also ignored (gravitational settling would be the dominant

contributor to dry removal for particle diameters greater than about 5 microns).

Calculations were performed for an SST1 release with five deposition velocities: 0.1, 0.3, 1.0, 3.0, and 10.0 cm/sec.^a These values are believed to span the range of possible deposition velocities. Only non-buoyant releases were considered. For buoyant releases, early consequences are dominated by the occurrence of precipitation; therefore, the variation of consequences with dry deposition velocity could be substantially smaller for buoyant releases (see Section 2.7.2). Other assumptions included Summary Evacuation, an 1120 MWE reactor, the Indian Point population distribution and wind rose, and New York City meteorology. Different population distributions and emergency response assumptions could impact the observed variation of early consequences with deposition velocity (see Sections 2.4 and 2.5).

Figure 2.7.3-1 presents the early fatality CCDFs for the set of deposition velocities examined. Except for the low-probability, high-consequence events, there are only very minor differences. Mean numbers of early fatalities vary by less than a factor of 1.5. Deposition velocities of 0.1, 0.3, and 1.0 cm/sec yield the highest consequence events (over 50,000 fatalities) from weather sequences with precipitation beginning between 10 and 20 miles from the reactor. With either a 3 or 10 cm/sec deposition velocity, the particulate matter in the plume is sufficiently depleted before this distance range is reached and, thus, rain does not produce a ground concentration in this interval high enough to cause significant numbers of early fatalities.

Figure 2.7.3-2 shows the conditional individual risk of early fatality versus distance within 10 miles of the reactor. Larger values of deposition velocity result in slightly greater individual risk within 2 miles of the reactor but a much reduced risk farther out. Table 2.7.3-1 lists the means, 90th and 99th percentiles, and maxima of the CCDFs of early fatality distance, early injury distance, and interdicted land

a. In all calculations a single deposition velocity was used for all elements except noble gases. The deposition velocity of the noble gases was assumed to be zero.

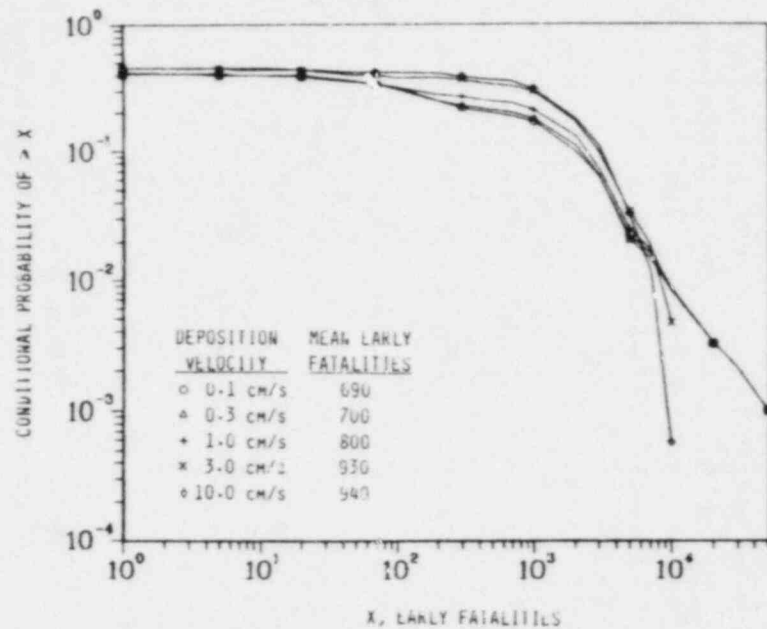


Figure 2.7.3-1. Early Fatality CCDFs for Five Different Deposition Velocities (for particulate matter only), Conditional on an SST1 Release.

Assumptions: 1120 MWe reactor, SST1 release, Indian Point wind rose and population, New York City meteorology, Summary Evacuation.

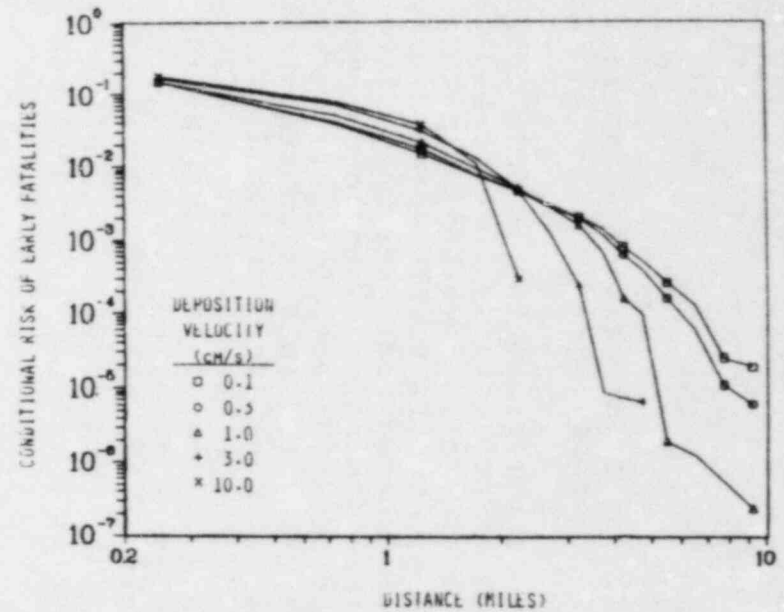


Figure 2.7.3-2. Individual Risk of Early Fatality vs Distance for 5 Deposition Velocities, Conditional on an SST1 Release

Table 2.7.3-1 Sensitivity of the Distances (miles) to which Consequences Occur for Various Deposition Velocities.

Dry- Deposition Velocity (cm/sec)	<u>Early Fatality Distance</u>				<u>Early Injury Distance</u>				<u>Land Interdiction Distance</u>			
	Mean	90%	99%	Maximum Calcu- lated	Mean	90%	99%	Maximum Calcu- lated	Mean	90%	99%	Maximum Calcu- lated
0.1	2.1	4	15	25	7.2	15	55	65	11	30	60	100
0.3	1.9	4	15	25	7.1	20	40	50	16	40	65	85
1.0	1.7	4	12	18	8.3	25	35	50	19	40	60	85
3.0	1.6	3	4	18	6.6	12	23	25	20	25	40	45
10	1.4	3	3	3	3.5	6	15	18	13	22	23	25

Assumptions: 1120 MWe reactor, SST1 release, New York City meteorology, Summary Evacuation within 10 miles.

distance (see Section 2.6). The mean distances for each consequence are only marginally sensitive to deposition velocity. However, the tail of the distributions (99th percentile and maximum calculated) are very sensitive to deposition velocity. As the deposition velocity increases, there is a large reduction in the 99th percentile and maximum calculated distances. Again, the tails of each distribution result from sequences with precipitation beginning some distance from the reactor. Deposition velocities above about 3 cm/sec deplete the plume closer to the reactor, and thus the distance to which precipitation can produce significant ground concentrations is much reduced.

Despite the narrow scope of this sensitivity analysis (only the deposition velocity has been studied rather than trying to account for the more realistic condition of a distribution of deposition velocities), the following conclusions can be drawn:

- o For a single deposition velocity applicable to all particulate matter, the maximum distance to which land is interdicted and early fatalities and injuries occur is very sensitive to deposition velocity. These maximum distances occur for low-probability, worst-case weather conditions.
- o For the population distribution and emergency response scenario assumed (Summary Evacuation), the mean number of early fatalities is only moderately sensitive to deposition velocity and thus may be largely insensitive to the particle-size distribution of the released material.

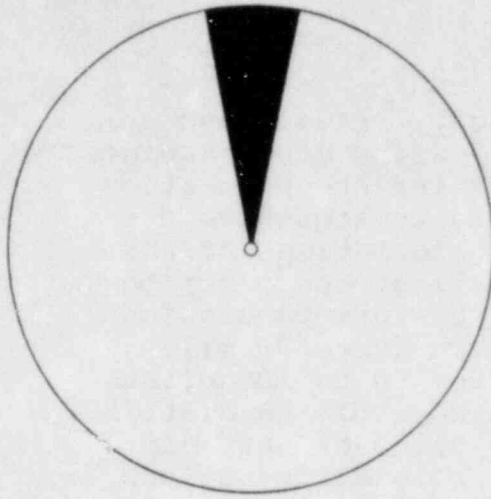
2.7.4 Population Distribution

Results presented in Section 2.4, Site Meteorology and Population, showed that early fatalities and early injuries are strongly sensitive to the characteristics of the surrounding population distribution. Three sets of calculations were performed to better define the sensitivity of early fatalities and injuries to the following features of population distributions: (1) radial and angular variations in population density, (2) the size and distance of population centers, and (3) exclusion zone size.

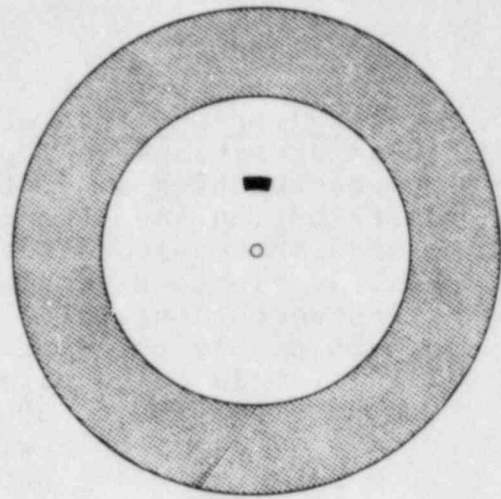
Radial and Angular Variations. Radial and angular variations in population density were examined by constructing a hypothetical reference population distribution and then calculating consequences for that distribution and eight transformations of that distribution. Beyond 20 miles all of the distributions were identical. Each had uniform populations of 750 people per square mile from 20 to 30 miles, 2500 from 30 to 50 miles, 500 from 50 to 100 miles, and 300 from 100 to 500 miles. None of the distributions had any people within 0.5 miles of the reactor (0.5 mile Exclusion Zone). All nine distributions met the following criterion: within 5, 10, 15, 20, and 30 miles of the reactor, the average population density was either zero (the distribution is empty to that radial distance) or 750 people per square mile (if there are any people within a given radial distance, then on average within that distance there are 750 people per sq mi). In addition, all nine distributions had 939,000 people within 20 miles of the reactor, but each had a different distribution of those people, as is schematically depicted in Figure 2.7.4-1.

Figure 2.7.4-1 indicates that the reference distribution (Distribution 1) was uniform from 0.5 to 20 miles. It had 530 people per square mile from 0.5 to 2 miles and 750 people per square mile from 2 to 20 miles. Distribution 2 was constructed from the reference distribution by moving the population within 20 miles forward into 5 high density rings. Distribution 3 moved the population within 20 miles entirely into a single 22.5° sector. Distributions 4 through 8 moved all of the population within 2, 5, 10, 15, or 20 miles, respectively, into a single 22.5° sector toward the back of the vacated region. Distribution 9 was constructed by scaling the actual population distribution around a New England reactor site, so that the resulting distribution had 530 people per square mile from 0.5 to 2 miles and 750 people per square mile in each of four distance intervals: 2-5, 5-10, 10-15, and 15-20 miles.

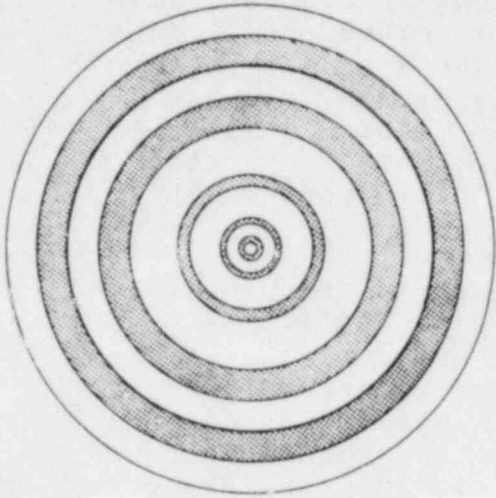
The transformations used to generate Distributions 4 through 8 in effect created population centers by vacating 15 of the 16 sectors of the reference distribution out to 2, 5, 10, 15, or 20 miles, respectively. The population centers thereby created had the following sizes and distances from the reactor:



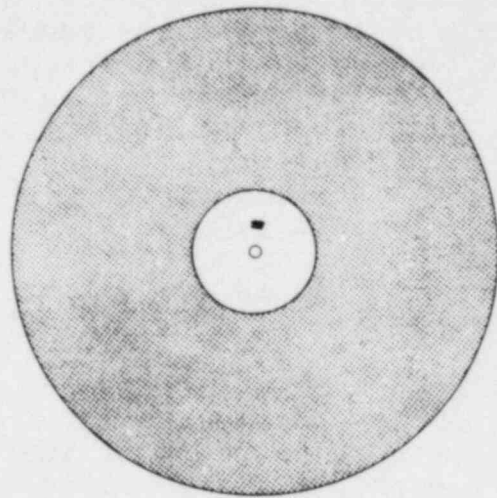
Distribution 3



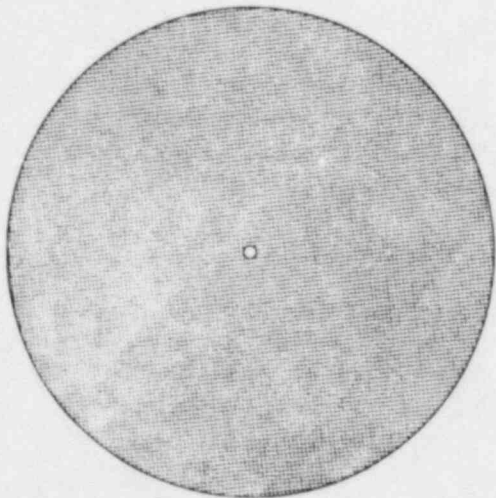
Distribution 6



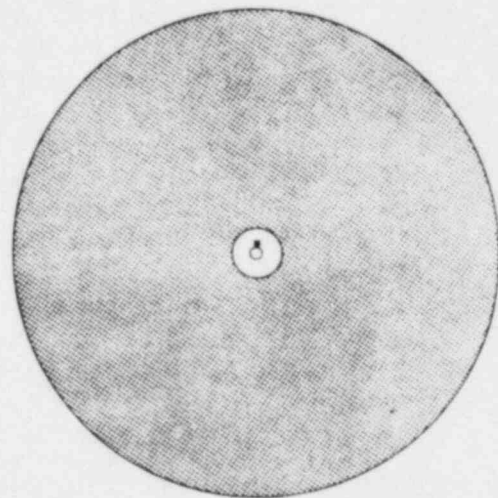
Distribution 2



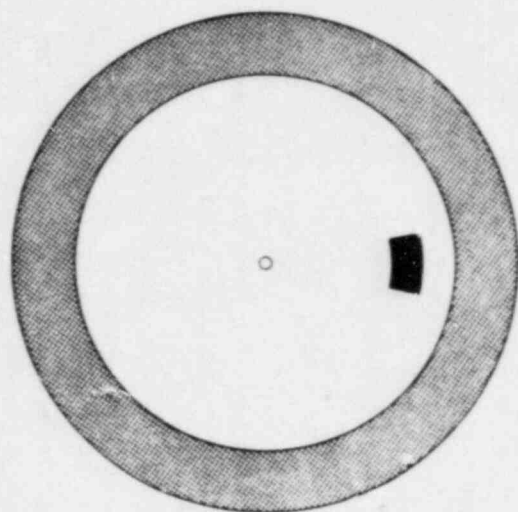
Distribution 5



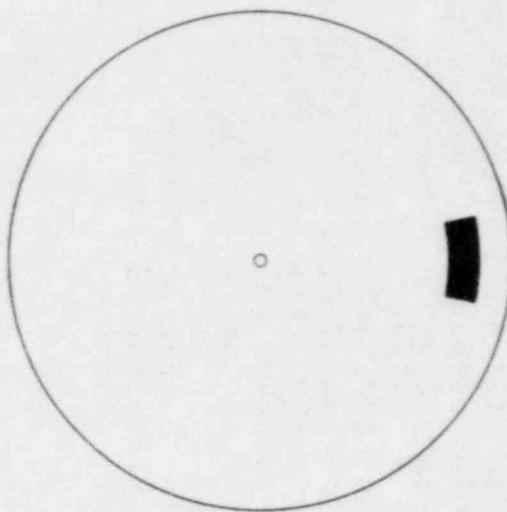
Distribution 1



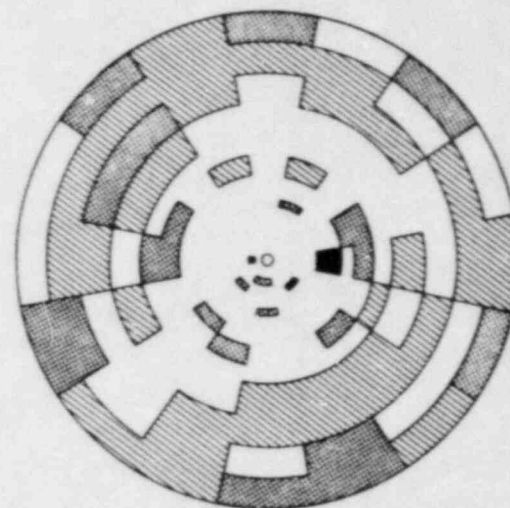
Distribution 4



Distribution 7



Distribution 8



Distribution 9

Figure 2.7.4-1. Schematic Representations of the Nine Hypothetical Population Distributions Used to Examine the Impact on Consequences of Radial and Angular Variations in Population Density.

- 1) Distribution 1 (Reference Distribution): uniform to 20 mi.
- 2) Distribution 2: 4 high density population rings.
- 3) Distribution 3: all population in 1 sector.
- 4) Distribution 4: city at 1.0 mi, uniform beyond 2 mi.
- 5) Distribution 5: city at 3.0 mi, uniform beyond 5 mi.
- 6) Distribution 6: city at 6.8 mi, uniform beyond 10 mi.
- 7) Distribution 7: city at 12.5 mi, uniform beyond 15 mi.
- 8) Distribution 8: city at 16.3 mi, uniform beyond 20 mi.
- 9) Distribution 9: real distribution scaled to match the densities of Distribution 1.

Distribution	City Size	City Distance (mi)
4	6,300	1
5	55,800	3
6	232,000	6.75
7	527,000	12.5
8	940,000	16.25

For each of the nine population distributions, early fatality and early injury CCDFs were calculated assuming an SST1 release from an 1120 MWe reactor, Summary Evacuation, New York City meteorology, and a uniform wind rose. The early fatality CCDFs are presented in Figures 2.7.4-2 through 2.7.4-5. For each early fatality and early injury CCDF, mean (expected) and 99th percentile (consequence magnitude equalled or exceeded following 1 out of every 100 releases) values and the probability of having at least one early fatality or injury are presented in Table 2.7.4-1.

Figure 2.7.4-2 compares the second population distribution to the Reference Distribution. Moving population forward into five high-density rings (densities of 2700, 7000, 5100, 1700, 1600, respectively) increases the number of early fatalities calculated at each probability level (the reference CCDF is shifted toward higher consequences).

Figure 2.7.4-3 compares the third population distribution to the Reference Distribution. Moving all of the population into 1 sector (vacating 15 sectors out to 20 miles) reduces the likelihood of having any early fatalities (the CCDF shifts downward) but increases the number observed, whenever fatalities do occur (the CCDF shifts to the right).

The CCDF shifts downward because, with 15 sectors vacant to 20 miles, many plumes do not intersect any population before plume concentrations fall below fatality dose thresholds. Therefore, the probability of having at least 1 early fatality is substantially decreased. If plumes were always exactly 1 sector wide, then the probability of having at least 1 early fatality would decrease by a factor of exactly 16. Because plume meander frequently causes plumes to be much wider

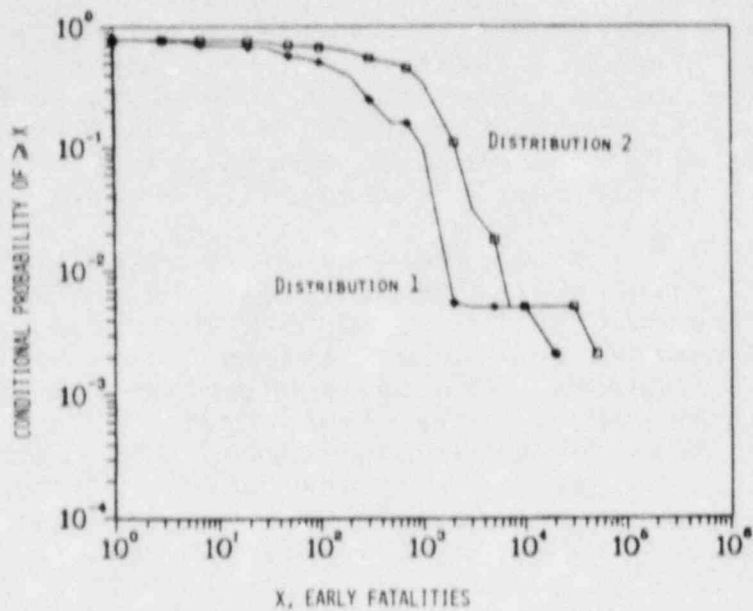


Figure 2.7.4-2. Comparison of the Early Fatality CCDF for Population Distribution 2 (4 high density rings) to that of the Reference Distribution.^a

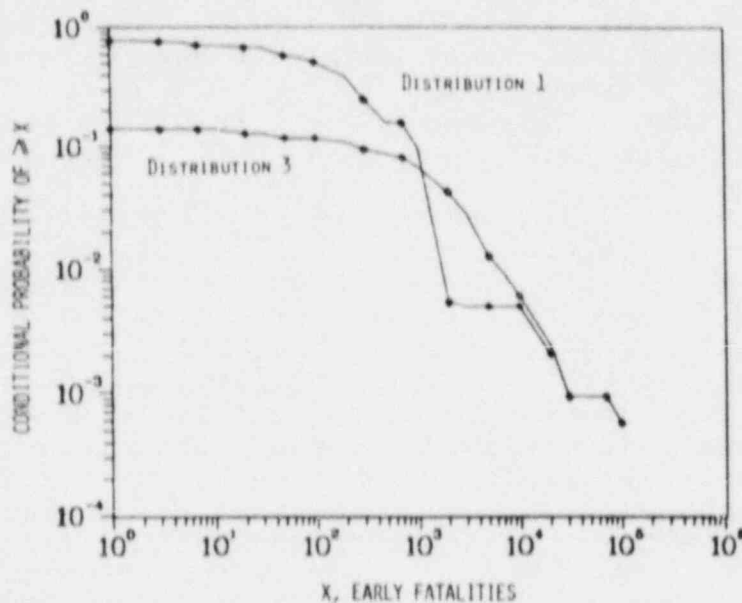


Figure 2.7.4-3. Comparison of the Early Fatality CCDF for Population Distribution 3 (all population in 1 sector) to that of the Reference Distribution.^a

a. Assumptions: 1120 MWe reactor, SST1 release, New York City meteorology, uniform wind rose, Summary Evacuation.

than 1 sector, the probability of observing at least 1 early fatality actually decreases by only a factor of ~6. Conversely, because all of the people out to 20 miles are now in 1 sector, when the plume goes out that sector, consequence magnitudes increase by about the same factor. Therefore, the mean (expected) result (400 early fatalities) is unchanged (see Table 2.7.4-1).

Figure 2.7.4-4 compares the early fatality CCDFs calculated using population distributions 4 through 8 to the Reference Distribution CCDF. The presence of population centers and vacant land in Distributions 4 through 8 produces two effects which are related. First, because increasingly larger areas of land surrounding the reactor are being vacated, the probability of observing any early fatalities decreases from 0.8 for the Reference Distribution to 0.001 for Distribution 8. Second, because the population centers are increasing in size (from 6000 people in Distribution 4 to 1,000,000 in Distribution 8), the maximum number of early fatalities (conditional probabilities of $\lesssim 10^{-3}$, caused by adverse weather) also increases from 2.5×10^4 early fatalities for the Reference Distribution (which contains no population center) to 4.0×10^5 for Distribution 8 (which contains a population center of almost 1 million people). Finally, the mean number of early fatalities for these distributions ranges from a low of 110 for Distributions 6 and 8 to a high of 560 for Distribution 4, while 99th percentile values range from 0 for Distributions 7 and 8 to 8500 for Distribution 5.

Figure 2.7.4-5 compares the CCDF calculated using the Reference Distribution to that calculated using Distribution 9. Figure 2.7.4-5 shows that incorporation into the Reference Distribution of radial and angular irregularities characteristic of a "real" population distribution alters the early fatality CCDF of the Reference Distribution in a predictable way. Because Distribution 9 is not uniform, the probability of having any early fatalities falls to 0.2 from the Reference Distribution value of 0.8, mean early fatalities decrease to 260 from 400, but the 99th percentile result increases from 1200 to 2800. Because Distribution 9 contains population centers (17,700 at 2.75 miles; 62,800 at 5.5 miles; 150,000 at 19 miles), the largest calculated number of early fatalities increased to 6.5×10^4 from the Reference Distribution value of 2.5×10^4 .

Examination of Table 2.7.4-1 and Figures 2.7.4-2 through 2.7.4-4 shows that the chance of having any early fatalities or early injuries, and the numbers that

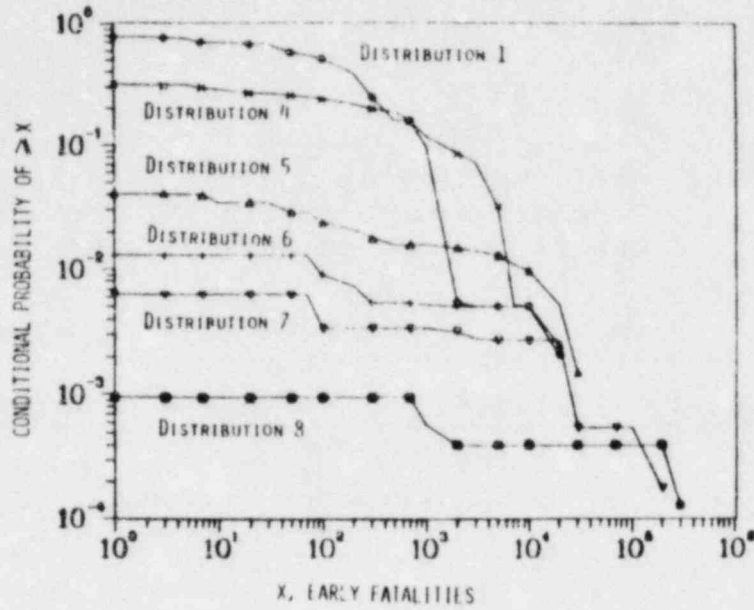


Figure 2.7.4-4. Comparison of the Early Fatality CCDFs for Distributions 4 thru 8 (distributions that contain cities) to that of the Reference Distribution.^a

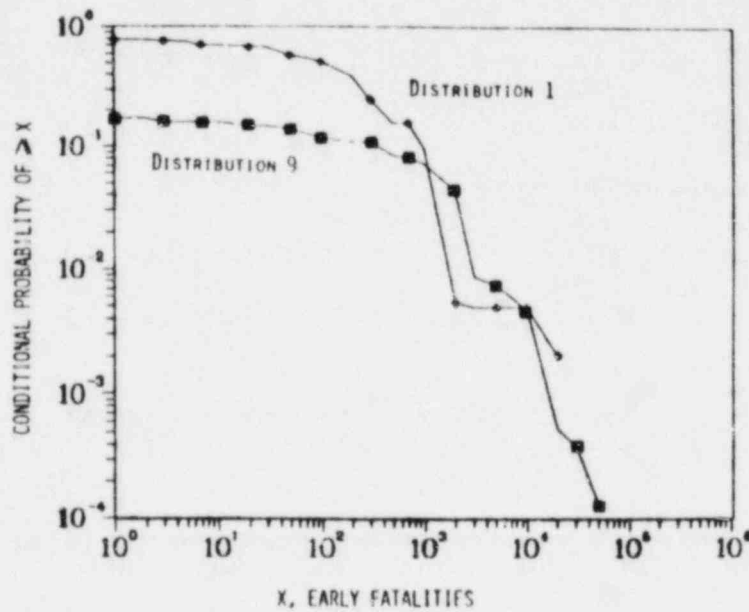


Figure 2.7.4-5. Comparison of the Early Fatality CCDF of Distribution 9 (scaled real population distribution) to that of the Reference Distribution.^a

a. Assumptions: 1120 MWe reactor, SST1 release, New York City meteorology, uniform wind rose, Summary Evacuation.

Table 2.7.4-1. Early Fatalities and Early Injuries for Population Distributions 1 Through 9, Conditional on an SST1 Release

Distri- bution	Early Fatalities			Early Injuries		
	$P(\geq 1)$	Mean	99th Percentile	$P(\geq 1)$	Mean	99th Percentile
1	0.79	400	1200	0.99	2.2×10^3	19,000
2	0.79	1000	2700	0.99	3.9×10^3	30,000
3	0.14	400	5600	0.17	2.2×10^3	67,000
4	0.32	560	5800	0.82	2.3×10^3	17,000
5	0.04	250	8500	0.48	2.2×10^3	26,000
6	0.01	110	90	0.38	1.5×10^3	27,000
7	0.006	160	0	0.20	1.9×10^3	59,000
8	0.001	110	0	0.05	1.2×10^3	34,000
9	0.17	260	2800	0.62	1.8×10^3	24,000

$P(\geq 1)$ = probability of having at least 1 early fatality or early injury (CCDF probability-axis intercept).

Mean = expected number of early fatalities or early injuries.

99th Percentile = consequence magnitude equalled or exceeded following 1 out of every 100 releases.

Assumptions: 1120 MWe reactor, SST1 release, New York City meteorology, uniform wind rose, Summary Evacuation.

might occur, are both highly variable. Therefore, because each of the nine distributions met the same radial population density criterion (populated radial intervals have population densities of 750 people per sq mi), it appears that any siting population criterion that restricts only the number of people within various radial distances may allow population distributions with significantly different risk characteristics. For this reason, consideration should perhaps be given to additional criteria which limit the number of people in any single sector or annular region.

Size and Distance of Population Centers. The effect of the size and distance of population centers upon consequences was further examined by imposing population centers of three sizes (10^4 , 10^5 , and 10^6 people) upon a 50 people per square mile background population density at the distances given in Table 2.7.4-2, thereby generating 13 population distributions, the background distribution and 12 distributions with population centers. Early fatality CCDFs were calculated for each of the 13 distributions assuming an SST1 release from a 1120 MWe reactor, New York City meteorology, a uniform wind rose, a 1-mile population exclusion zone, and evacuation to 10 miles at 10 mph with a distribution of delay times (Summary Evacuation, see Section 2.5). Mean, 90th, 99th, and maximum early fatality values for each CCDF are presented in Table 2.7.4-2.

Four conclusions may be drawn from the results presented in Table 2.7.4-2. First, irrespective of size, population centers beyond 25 miles do not contribute to early fatalities, i.e., these population centers have early fatality CCDFs identical to the background CCDF. Early fatalities are confined to 25 miles because, even for unfavorable meteorological conditions, plume concentrations fall below all early fatality thresholds before that distance.^a

Second, population centers between 10 and 20 miles cause peak early fatality values^b to increase substantially and mean values to increase by up to factors

a. The maximum distance to which early fatalities occur for an SST1 release was shown in Section 2.6 to range from 13 to 25 miles, depending on meteorology, and is 18 miles for New York City meteorology.

b. Improbable events with conditional probabilities of $\leq 10^3$ caused by adverse weather, e.g., rainout of the radioactive plume onto a population center.

Table 2.7.4-2. Effects of Size and Distance of Population Centers on Early Fatalities, Conditional on an SSTI Release

Center Population	Center Distance (mi)	Early Fatalities			
		Mean	90 Per-centile	99 Per-centile	Maximum Calculated ^a
Background ^b	--	23	67	150	1,700
10 ⁶	175.0	23	67	150	1,700
	92.5	23	67	150	1,700
	52.5	23	67	150	1,700
	32.5	23	67	150	1,700
10 ⁵	52.5	23	67	150	1,700
	27.5	23	67	150	1,700
	16.25	37	67	150	51,000
	11.25	44	67	160	49,000
10 ⁴	16.25	26	67	150	11,000
	11.5	27	67	150	10,000
	5.5	24	68	160	1,700
	2.25	120	190	2,300	5,100

a. Maximum value calculated for any weather sequence. An improbable event (conditional probability $\leq 10^{-3}$) typically caused by adverse weather (rainout of the radioactive plume onto a city).

b. Background population density = 50 people per sq mi.

Assumptions: 1120 Mwe reactor, SSTI release, New York City meteorology, uniform wind rose, Summary Evacuation.

of 2, but do not affect 90th or 99th percentile values (only mean and peak values differ from those of the background CCDF). Examination of individual calculations shows that population centers between 10 and 20 miles experience early fatalities principally when rain falls on the radioactive plume after it arrives over the population center. Because this is an improbable event, it affects only the CCDF peak and not its 90th, or 99th percentile values.^a

Third, if effectively evacuated, population centers between 5 and 10 miles probably can avoid early fatalities (the CCDF for the population center at 5.5 miles is almost identical to the background CCDF). The population center at 5.5 miles experiences few early fatalities because the characteristics of Summary Evacuation (delay times, evacuation speed, see Section 2.5) assure that most persons in the population center avoid large exposures to radioactivity by evacuation for most weather sequences sampled.

Fourth, population centers very close to a reactor (≤ 5 miles) are more likely to experience early fatalities even with evacuation (the CCDF of the population center at 2.25 miles differs from the background CCDF at all levels of probability). Early fatalities are likely to occur because only a timely warning followed by a very prompt evacuation could assure that all people in population centers within 5 miles of a reactor will escape plume exposures (see Section 2.5).

Exclusion Zone Size. All existing reactors are surrounded by an exclusion zone, which has no permanent inhabitants and is controlled exclusively by the utility operating the reactor. At current reactor sites exclusion zones are irregularly shaped with minimum exclusion distances which range from 0.1 to 1.3 miles (average 0.6 miles, see Appendix D). Larger exclusion zones would be expected to reduce the incidence of early health effects (those health effects induced by relatively large doses to individuals). The influence of exclusion zone size on early fatalities and injuries was examined for each

a. The effects of rain are discussed more fully in Sections 2.4 and 2.6; the effects of assuming emergency response beyond 10 miles are considered in Section 2.5.

of four emergency response scenarios (Scenarios 1, 5, 6, and 7 as defined in Section 2.2.2). Scenario 1 is an expeditious evacuation (1 hr delay, 10 mph), Scenario 5 is No Emergency Response, Scenario 6 is Poor Evacuation (5 hr delay, 1 mph), and Scenario 7 is Summary Evacuation. All calculations assumed no immediate emergency response beyond 10 miles, a uniform population distribution (100 persons per square mile), an SST1 release from an 1120 MWe reactor, and New York City meteorology.

Table 2.7.4-3 presents for each emergency response scenario the mean number of early fatalities calculated to occur within each of 20 distance intervals to 17.5 miles (for New York City meteorology, early fatalities are confined to 17.5 miles). Without any emergency response, the expected total number of early fatalities is 338, given an SST1 release at a reactor having a surrounding population density of 100 persons per square mile and no exclusion zone. However, if the reactor had a 1-mile exclusion zone, 58 fatalities would be avoided. Alternatively, an effective emergency response within 10 miles (e.g., Best Evacuation) would reduce the mean number of fatalities observed from 338 to 23 without any exclusion zone, and to 14 fatalities (those occurring beyond 10 miles) with a 1-mile exclusion zone.

The combined effects of exclusion zone size and emergency response effectiveness are further illustrated by the data in Table 2.7.4-4, which is drawn from Table 2.7.4-3. Table 2.7.4-4 presents for various combinations of emergency response effectiveness and exclusion zone size the number of early fatalities occurring within and beyond 10 miles and their sum. Table 2.7.4-4 shows that for large core-melt accidents mean early fatalities are reduced 16-fold (from 320 to <20) by an 0.5-mile exclusion zone and a very effective evacuation (Best Evacuation), by a 3-mile exclusion zone and a reasonably effective evacuation (Summary Evacuation), or by a 5-mile exclusion zone and an ineffective evacuation (Poor Evacuation). Alternatively, an 0.5-mile exclusion zone and a very effective evacuation within 2 miles (achieved possibly by early warning [41]) and a reasonably effective evacuation from 2 to 10 miles reduced mean early fatalities 12-fold (320 to 26).

Table 2.7.4-5 shows how the probability of having at least 1 early fatality or early injury varies with

Table 2.7.4-3. Mean Early Fatalities by Distance Intervals for Four Emergency Response Scenarios, All Evacuations^a

<u>Distance Interval</u>	<u>Emergency Response^b</u>			
	None	Poor	Summary	Best
0.0				
0.25	6.3	6.3	5.6	3.9
0.5	11.5	11.4	8.6	2.4

0.75	17.6	16.6	9.9	1.6
1.0	22.2	16.3	8.2	0.6
1.5	51.4	26.1	12.6	0.2
2.0	42.3	25.7	7.7	0.1
2.5	38.9	21.0	4.5	0.0
3.0	29.5	10.0	2.3	0
3.5	26.6	6.5	1.5	0
4.0	19.6	5.1	0.7	0
4.5	14.7	3.9	0.2	0
5.0	11.3	2.1	0.1	0
6.0	15.2	0.6	0.0	0
7.0	7.8	0.2	0.0	0
8.5	3.1	0	0	0
10.0	6.4	0.6	0.0	0

12.5	6.9	6.9	6.9	6.9
15.0	0	0	0	0
17.5	7.1	7.1	7.1	7.1
<u>Total</u>	338	166	76	23

a. Assumptions: SST1 release, 1120 MWe reactor, New York City meteorology, uniform wind rose, 100 people per square mile.

b. No emergency response beyond 10 miles; relocation after 1 day (i.e., 1-day exposure to radioactivity deposited on the ground).

Table 2.7.4-4. Dependence of Mean Early Fatalities on Emergency Response Effectiveness and Exclusion Zone Size^a

<u>Emergency Response</u>	<u>Exclusion Zone (mi)</u>	<u>Mean Early Fatalities</u>		
		>10 mi	≤10 mi	Total
Best Evacuation ^b	0.5	14	2.5	16.5
Summary Evacuation ^b	3.0	14	2.5	16.5
	2.0	14	9.3	23.3
	1.0	14	29.6	43.6
	0.5	14	47.7	61.7
Poor Evacuation ^b	5.0	14	1.4	15.4
	3.0	14	19.0	33.0
	2.0	14	50.0	64.0
	1.0	14	101.8	115.8
	0.5	14	134.7	148.7
No Evacuation	5.0	14	32.5	46.5
	3.0	14	104.7	118.7
	2.0	14	173.1	187.1
	1.0	14	266.8	280.8
	0.5	14	306.6	320.6
Best ≤2 mi Summary >2 mi	0.5	14	11.8	25.8

a. Assumptions: SST1 release, 1120 MWe reactor, New York City meteorology, 100 people per square mile.

b. No emergency response beyond 10 miles; relocation after 1 day (i.e., 1-day exposure to radioactivity deposited on the ground).

Table 2.7.4-5. Probability of Having at Least
1 Early Fatality or Injury^a by
Exclusion Zone Distance^b

Emergency Response	None	Poor	Summary	Best	None	Poor	Summary	Best
<u>Distance</u> (mi)	<u>Early Fatalities</u>				<u>Early Injuries</u>			
0	1.00	1.00	0.96	0.88	1.00	1.00	1.00	1.00
0.25	1.00	1.00	0.81	0.38	1.00	1.00	1.00	1.00
0.5	1.00	0.97	0.76	0.26	1.00	1.00	0.92	0.72
0.75	0.97	0.85	0.55	0.21	1.00	1.00	0.85	0.50
1.0	0.97	0.60	0.37	0.10	1.00	1.00	0.82	0.41
2.0	0.59	0.40	0.19	0.01	0.98	0.97	0.76	0.36
5.0	0.20	0.10	0.02	0.01	0.78	0.57	0.39	0.36

a. CCDF intercept on probability axis (y-axis).

b. Assumptions: SST1 release, 1120 MWe reactor, New York City meteorology, 100 people per square mile.

exclusion zone size. The table shows that the probability of having at least 1 early fatality following a large core-melt accident (SST1 release) can be reduced to 0.2 by the following combinations of an Emergency Response and an Exclusion Zone distance:

<u>Emergency Response</u>	None	Poor	Summary	Best
<u>Exclusion Zone (mi)</u>	5	4	2	0.75

Taken together Tables 2.7.4-3 through 2.7.4-5 suggest that a large Exclusion Zone without an emergency response is not nearly as effective as a substantially smaller Exclusion Zone and a timely emergency response.

Finally, because atmospheric releases of radioactivity of the size of SST1 are improbable (possibly extremely improbable, see Section 2.3.2, Source Term Uncertainties), it is important to note that for smaller releases (e.g., SST1 reduced an order of magnitude or SST2) the mean and peak distances to which early fatalities and injuries are likely to occur is much reduced, even with no emergency response (see Section 2.6, Distance Dependencies). Thus, for SST1 reduced 10-fold, on the average (mean result) fatalities would be confined to 1 mile and injuries to 3 miles, while for SST2 these distances are 0.5 miles and 2 miles, respectively. Thus, for releases substantially smaller than SST1, because early health effects are usually confined to only a few miles, typical Exclusion Zones (~1 mi) can have a substantial impact even without an emergency response.

2.7.5 Interdiction Dose Criterion

Following a nuclear power plant accident, continued usage of land contaminated by radioactive material deposited from the plume would result in increased population exposures, and thus would increase latent health effects. Chronic exposure to contaminated land can be avoided by interdicting the usage of the land until removal processes (decontamination, radioactive decay, weathering, runoff) have decreased exposures to acceptable levels. The dose criterion (allowed groundshine dose to an individual accumulated in 30 years) for interdiction of land is called the "interdiction dose." As interdiction dose increases, latent health effects increase (because more people are continuing to use contaminated land) and interdicted land area

and interdiction costs decrease (because less land is interdicted).

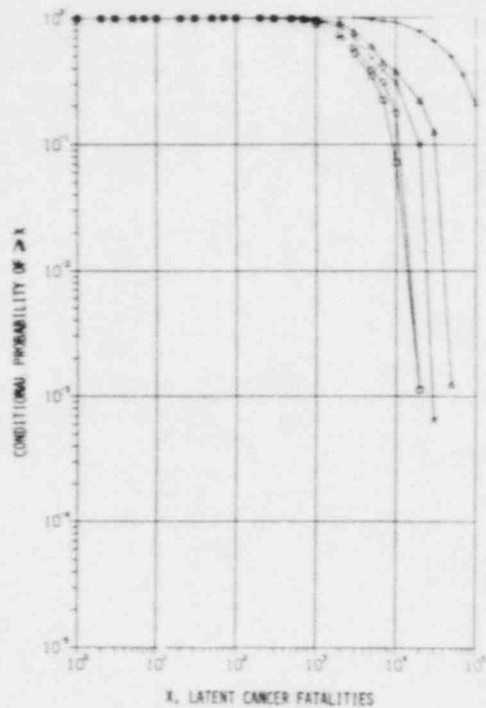
All of the calculations presented in other sections of this report used an interdiction dose of 25 rem due to a 30-year exposure to contaminated land. This section examines the sensitivity of latent cancer fatalities and of interdiction distance (distance to which land is interdicted), area, and costs to interdiction dose. Calculations were performed for four different 30-year interdiction doses (5, 10, 25, and 50 rem) and also for no interdiction. All of these calculations used an 1120 MWe reactor, the SST1 source term, the Indian Point population distribution and wind rose, and New York City meteorology.

Figures 2.7.5-1a through 2.7.5-1c present CCDFs for latent cancer fatalities and the interdiction distance and area. Table 2.7.5-1 presents mean and 90 percentile (conditional probability of 10^{-1}) values of latent cancer fatalities and of interdiction distance, area, and costs as a function of interdiction dose. In Figures 2.7.5-2a through 2.7.5-2c the mean values in Table 2.7.5-1 (except the cost data) are plotted versus interdiction dose. Examination of the CRAC2 code showed that the near linear dependence of mean latent cancer fatalities upon interdiction dose displayed in Figure 2.7.5-2a was to be expected.^a Figure 2.7.5-2a shows that, if all contaminated ground were interdicted (interdiction dose of zero), then 3200 latent cancer fatalities would still result due to the pre-interdiction dose (cloudshine dose; inhalation dose, which includes the chronic dose from

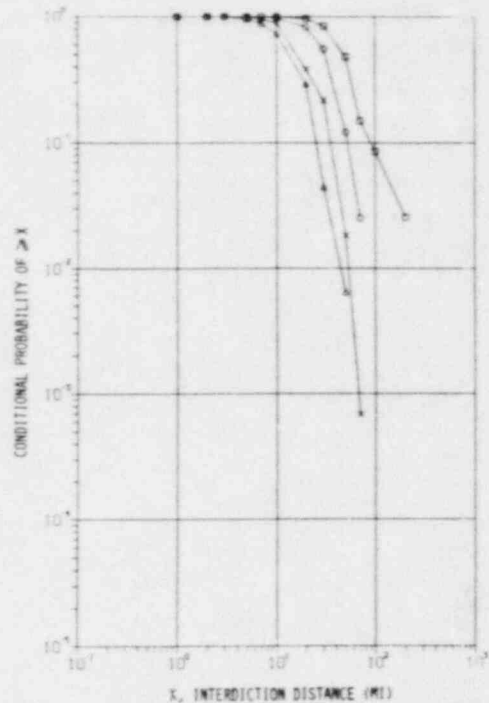
$$a. \text{ Latent cancer fatalities} \sim \text{population dose} \sim \rho \int_0^{500} D(x) dx,$$

where ρ = population density (approximately constant over large areas), $D(x)$ = dose at distance x , x_0 = interdiction distance, and 500 mi = maximum distance for latent cancers (variable but large). From the transport and deposition algorithms used in CRAC2, $D(x) \sim x^{-2}$. So latent cancer fatalities

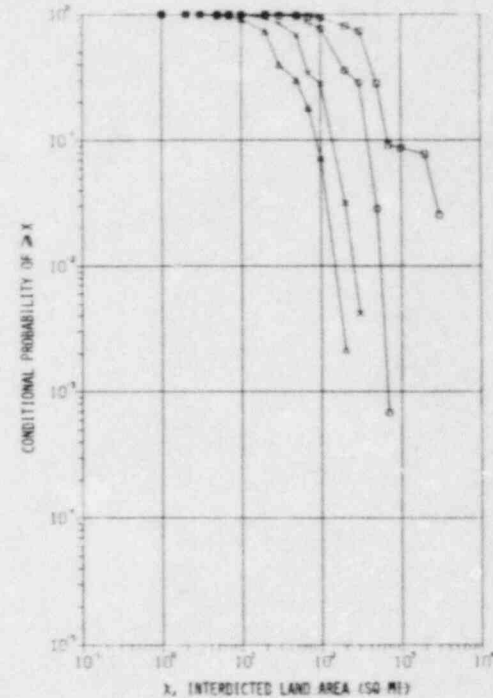
$$\sim \rho \ln x \Big|_{x_0}^{500} \text{ which is approximately linear in } x_0 \text{ for } x_0 \leq 50 \text{ mi.}$$



a)



b)



c)

Figure 2.7.5-1: Impact of 30-Year Interdiction Dose upon a) Latent Cancer Fatalities, b) Interdiction Distance (mi), and c) Interdicted Land Area (sq mi)

Legend

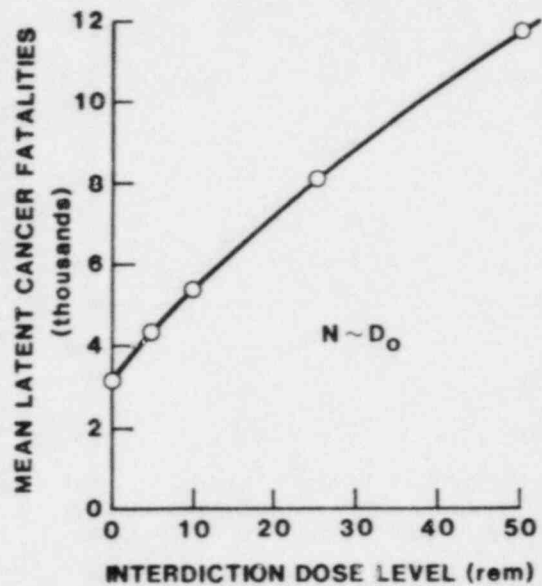
- + - no interdiction
- Δ - 50 rem interdiction dose
- x - 25 rem interdiction dose
- O - 10 rem interdiction dose
- - 5 rem interdiction dose

Assumptions: 1120 MWe reactor, SST1 release, Indian Point population and wind rose, New York City meteorology.

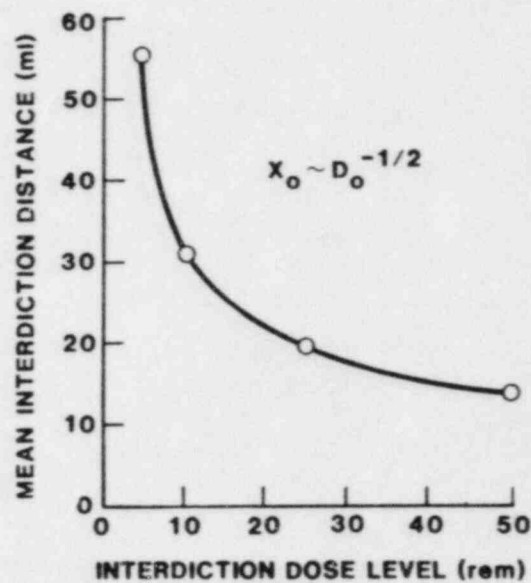
Table 2.7.5-1. Mean and 90th Percentile Values of Several Consequences by Interdiction Dose Level^a

<u>Interdiction Dose (rem)</u>	<u>Latent Cancer Fatalities</u>		<u>Interdiction Distance (mi)</u>		<u>Interdicted Land Area (sq. mi)</u>		<u>Interdiction Costs (billions)</u>
	Mean	90 Per- centile	Mean	90 Per- centile	Mean	90 Per- centile	Mean
5	4,300	9,100	56	90	580	640	36
10	5,400	11,000	32	52	200	380	17
25	8,100	20,000	19	35	76	140	5
50	12,000	31,000	14	25	41	86	2
None	68,000	130,000	0	0	0	0	0

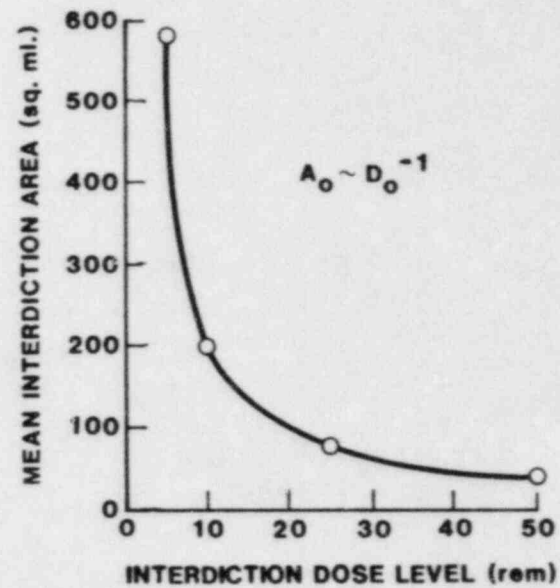
a. SST1 release, 1120 MWe reactor, Indian Point population and wind rose, New York City meteorology.



a)



b)



c)

Figure 2.7.5-2: Plots of a) Mean Latent Cancer Fatalities, b) Mean Interdiction Distance (mi), and c) Mean Interdicted Land Area vs Interdiction Dose Level (rem).

Assumptions: 1120 MWe reactor, SST1 release, Indian Point population and wind rose, New York City meteorology.

radioactivity deposited in the respiratory system; and pre-interdiction groundshine dose, which is assumed to be 1 day in duration). Figure 2.7.5-2b shows that interdiction distance is inversely proportional to the square root of the interdiction dose ($x_0 \sim D_0^{-1/2}$), and Figure 2.7.5-2c shows that interdiction area is inversely proportional to interdiction dose ($A_0 \sim D_0^{-1}$), which is not surprising since interdiction area should be roughly proportional to the square of interdiction distance ($A_0 \sim x_0^{-2}$).

Table 2.7.5-1 and Figures 2.7.5-1a through 2.7.5-1c show that latent cancer fatalities, and interdiction distance, area, and costs are all quite sensitive to interdiction dose. If all contaminated land were interdicted, the mean number of latent cancer fatalities would be reduced by about a factor of 20 from the number that would occur, if no land were interdicted (at the 90 percentile level the reduction factor is 15). Similarly, a 10-fold increase (5 to 50 rem) in interdiction dose produces about a 10-fold decrease in mean interdiction area and nearly a 20-fold decrease in mean interdiction costs.

Data in Table 2.7.5-1 can be used to illustrate the inverse relationship between latent fatalities and interdiction costs. For example, changing the interdiction dose criterion from no interdiction (all doses are tolerated) to an interdiction dose of 50 rem decreases mean latent fatalities by 57,000 and produces interdiction costs of $\$1.9 \times 10^9$ or $\sim \$3 \times 10^4$ per life saved. Further decrease from 50 rem to 25 rem saves an additional 4000 lives at a cost of $\sim \$7 \times 10^5$ per life, while the decrease from 25 rem to 10 rem saves 3000 lives at a cost of $\sim \$5 \times 10^6$ per life. Therefore, because of the inverse relationship between latent cancer fatalities and interdiction area, the high cost of interdicting land may make the interdiction of large areas (selection of a low interdiction dose) unacceptable.

2.8 Summary

This chapter has presented results from a large number of CRAC2 calculations, which characterize the sensitivity of accident consequences to input data and model parameters. Sensitivities were determined by comparison to a Base Case Calculation which assumed an SST1 release from a standard 1120 MWe reactor, meteorology typical of New York City, the Indian Point wind rose and population distribution, and Summary Evacuation. The principal conclusions derived from the results of these calculations are as follows:

- o Estimates of the number of early fatalities are very sensitive to source term magnitude. Mean early fatalities (average result for many weather sequences) are decreased dramatically (about two orders-of-magnitude) by a one order-of-magnitude decrease in source term SST1 (large core melt, loss of most safety systems). Because the core melt accident source terms SST1-3 used in this study neglect or underestimate several depletion mechanisms, which may operate efficiently within the primary loop or the containment, consequence magnitudes calculated using these source terms may be significantly overestimated.
- o The weather conditions at the time of a large release will have a substantial impact on the health effects caused by that release. In marked contrast to this, mean health effects (average result for many weather sequences) are relatively insensitive to meteorology. Over the range of meteorological conditions found within the continental United States (1 year meteorological records from 29 National Weather Service stations), mean early fatality values for a densely populated site show a range (highest value/lowest value) of only a factor of 2, and mean latent cancer fatality values a factor of 1.2.
- o Peak early fatalities (maximum value calculated for any weather sequence) are generally caused by rainout of the radioactive plume onto a population center. For an SST1 release, the peak result is about 10-times less probable in a dry locale than in a wet one.

- o The distances to which consequences might occur depend principally upon source term magnitude and meteorology. Frequency distributions of these distances, calculated using large numbers of weather sequences, yielded expected (mean), 99 percentile, and maximum calculated distances (expressed in miles) for early fatalities and early injuries as follows:

Source Term	Consequence	Mean	99%	Maximum Calculated
SST1	Early Fatalities	<5	≤15	<25
	Early Injuries	~10	~30	≤50
	Land Interdiction	~20	>50	>50
SST2	Early Fatalities	~0.5	<2	<2
	Early Injuries	<2	<5	~5
	Land Interdiction	<2	~7	~10

The maximum calculated distances are associated with very improbable events, (e.g., rain-out of the plume onto a population center). For the SST1 release reduced by a factor of 10, early fatalities are confined to ~5 miles, early injuries to ~20 miles, and interdiction of land to ~25 miles.

- o Calculated consequences are very sensitive to site population distribution. For each of the 91 population distributions examined, early fatality, early injury, and latent cancer fatality CCDFs were calculated assuming an SST1 release from an 1120 MWe reactor. The resulting sets of CCDFs had the following ranges:

Early Fatalities. ~3 orders-of-magnitude in the peak and mean numbers of early fatalities and in the probability of having at least one early fatality.

Early Injuries. ~3 orders-of-magnitude in the means, ~2 in the peaks, and ~1 in the probability of having at least one early injury.

Latent Cancer Fatalities. ~1 order-of-magnitude in the peaks and the means and in the probability of having at least one latent cancer fatality.

Generally, mean results are determined by the average density of the entire exposed population, while peak results (especially for early fatalities) are determined by the distance to and size of exposed population centers.

- o Early fatalities and early injuries can be significantly reduced by emergency response actions. Both sheltering (followed by relocation) and evacuation can be effective, provided the response is expeditious. Access to basements or masonry buildings significantly enhances the effectiveness of sheltering. Expeditious response requires timely notification of the public. If the evacuation is expeditious (timely initiation), evacuation speeds of 10 mph are effective. Evacuation before containment breach within 2 miles, after release within 10 miles, and sheltering from 10 to 25 miles appears to be a particularly effective response strategy.
- o Because accident source terms increase with reactor size, smaller reactors pose lesser risks to the public than are posed by larger reactors.
- o Buoyant plumes (high heat content) can be lofted over close-in populations, thereby decreasing the risk of early health effects at short distances ($\lesssim 10$ mi) but increasing that risk at longer distances (~ 20 mi). Because only rainout of lofted plumes is able to produce fatal exposures, mean early fatality values for buoyant plumes are substantially decreased by comparison to non-buoyant plumes (early fatalities result from fewer weather sequences).
- o Dry deposition velocity has a substantial impact on the distance to which land is interdicted and early health effects occur. However, the number of early health effects calculated are only moderately sensitive to dry deposition velocity.

- o Exclusion zones (unless very large) are unlikely to significantly reduce early health effects for very large core melt accidents such as SST1. However, for smaller accidents (e.g. 1/10 SST1, SST2) early health effects could be significantly mitigated by exclusion zones of 1 to 2 miles.
- o Decreasing the level of contamination at which land is interdicted decreases latent cancer fatalities and increases the amount of land interdicted. As interdiction dose is increased, interdiction costs (value of interdicted land and buildings) increase more rapidly than does the number of latent cancer fatalities avoided.

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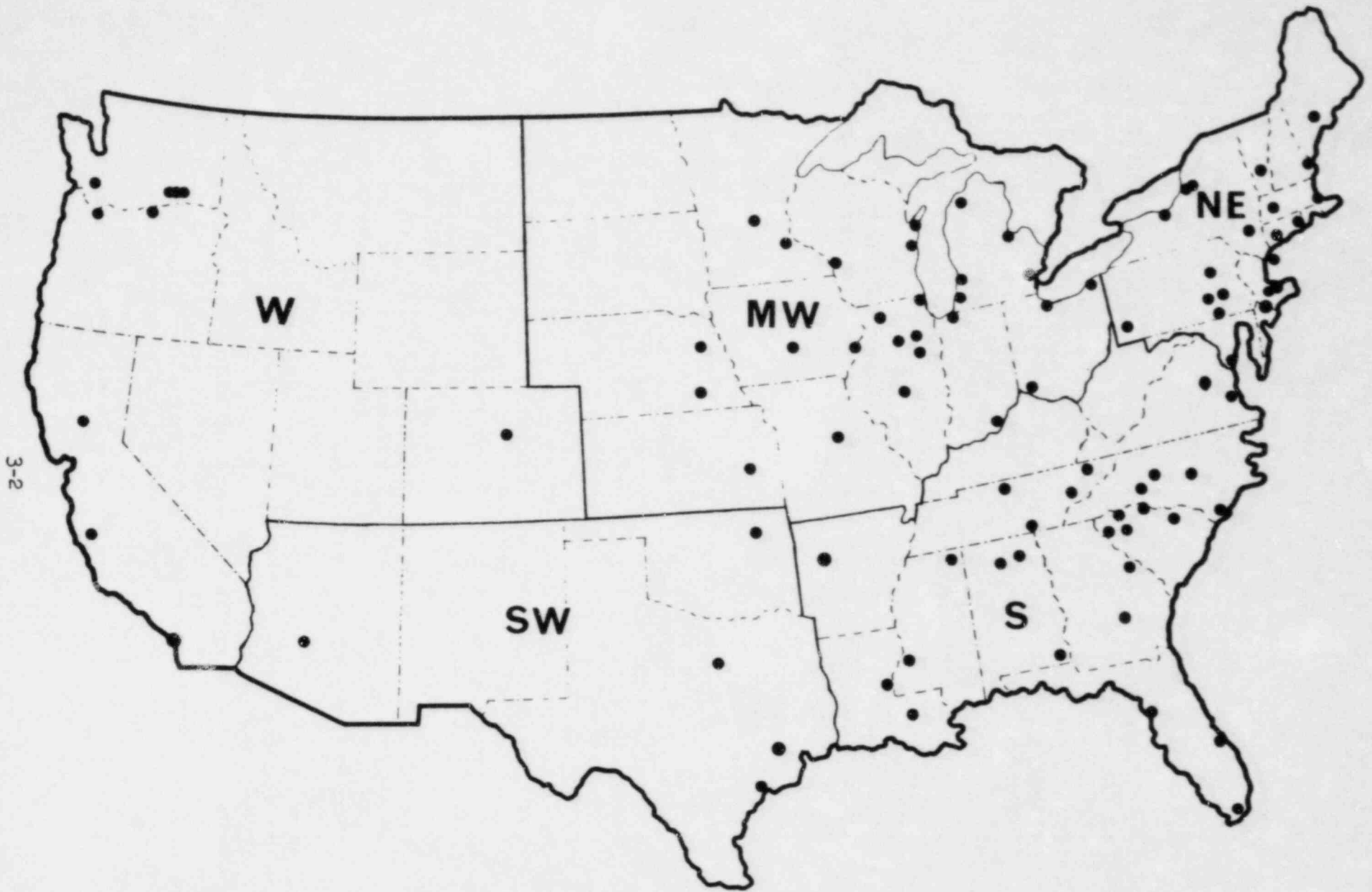
3. Population Statistics for Current Reactor Sites

3.1 Introduction

This chapter examines a variety of characteristics of the population distributions about the 91 reactor sites first discussed in Section 2.4 and described in detail in Appendices A and C. Each of these sites has either an operating license or a construction permit. The site characteristics examined include distance to the boundary of the reactor site exclusion zone, site population factors, the distribution of population densities within different radial annuli, and distances, maximum population densities within 22.5 and 45 sectors, and time-dependent trends in site population densities. As a group these analyses delineate the demographic characteristics of current reactor sites and provide a perspective of past siting decisions.

The population distributions examined in this chapter were derived from 1970 census data. A computer program was used (see Appendix A) to construct from U. S. Census Enumeration District (CED) data, the population distribution (16 sectors, 34 radial intervals) surrounding each of the 91 reactor sites. The procedure used may produce a distribution with significant errors close to the site. Errors may result because the computer program assumes that the entire population of each CED is located entirely at the "centroid" of the CED, when it may actually be dispersed over areas which are substantially larger than the area of the spatial interval in which the centroid is located. Because a CED typically contains about 1000 persons, the magnitude of this error decreases as population density increases. Given the spacing of the circular polar grid, the error is most likely negligible beyond 20 miles even for sparsely populated regions (≤ 40 people per sq mi). Beyond 7 miles, errors are unlikely to be substantial for population densities greater than 500 people per square mile.

Throughout this chapter results are frequently presented for each of the five NRC administrative regions. Figure 3-1 displays the boundaries of these regions and the locations of the 91 reactor sites examined. In Section 3.2 scatter plots of site exclusion zone distances and site population factors are presented by region. Section 3.3 presents population density CCDFs and displays percentile values drawn from the CCDFs for each region. Scatter plots of these data are also



3-2

Figure 3-1. The Five NRC Administrative Regions and the Location of the 91 Reactor Sites.

presented. Time trends of site population characteristics are analyzed by region in Section 3.4. Finally, population characteristics for individual sites and additional regional results are presented in Appendix D, and additional population data are available in NUREG-0348 [1].

3.2 Exclusion Zones and Site Population Factors

Distance to the exclusion zone boundary, distance to nearby cities, and site population factors have all been used by the NRC to describe population distributions about reactor sites. Consequence sensitivity to exclusion zone size and to distance to nearby cities was examined in Section 2.7.4. This section examines regional variation (1) of the minimum distance to the exclusion zone boundary and (2) of site population factors, with and without wind rose weighting.

All reactors are surrounded by an exclusion zone, which has no permanent inhabitants and is controlled exclusively by the utility operating the reactor. Exclusion zones are usually irregularly shaped. For the 91 sites examined in this study, minimum distances to the exclusion zone boundary range from 0.1 to 1.3 miles with 0.5 miles being about average. The value for each of the 91 sites is presented in Appendix D. Figure 3-2 displays these values as scatter plots, one for each NRC administrative region. Median values for each scatter plot are indicated on the figure. The median values increase in the order NE, MW, W, S, SW.

Site population factors were developed by the NRC [2] to provide a way to compare populations around different sites. The factors are intended to be dimensionless measures of the total risk to the population within a specified radial distance. Since correlations between population distribution and wind direction may significantly influence risk at some sites, a wind rose weighted formulation of the site population factor was also developed.

The Site Population Factor (SPF) and Wind Rose weighted Site Population Factor (WRSPF) are defined as follows:

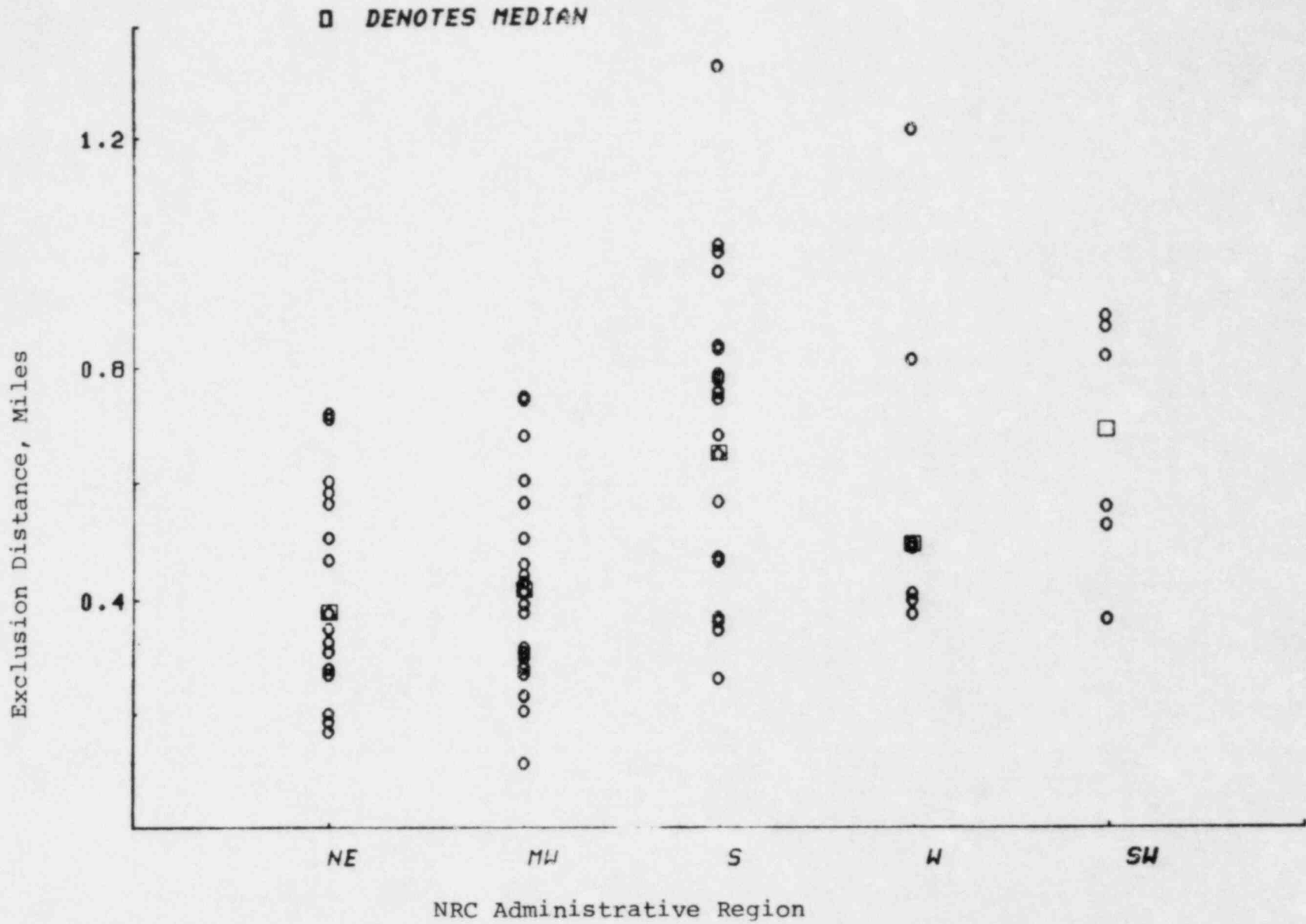


Figure 3-2. Exclusion Distances for 91 Reactor Sites by Geographic Area.

$$SPF_n = \frac{\sum_{i=1}^m P_i / r_i^{1.5}}{\sum_{i=1}^m \bar{P}_i / r_i^{1.5}} \quad WRS PF_n = \frac{16 \sum_{i=1}^m \left[\sum_{j=1}^{16} w_j P_{i,j} \right] / r_i^{1.5}}{\sum_{i=1}^m \bar{P}_i / r_i^{1.5}}$$

- where r_i is the outer radius of annulus i of m concentric annuli ($r_0 = 0, r_m = n$).
- n is the outer radius of the outermost annulus, annulus m .
- \bar{P}_i is the population of annulus i assuming a uniform population density of $2,1000_2$ people per sq mi, i.e., $\bar{P}_i = 10^3 \pi (r_i - r_{i-1})$
- P_i is the actual population of annulus i .
- $P_{i,j}$ is the actual population of the i th radial interval of wind rose sector j .
- w_j is the fraction of time that the wind blows into sector j .

Finally, the power 1.5 to which the radius r_i is raised was selected because it approximates the functional relationship between risk and distance; and $WRS PF_n = SPF_n$ whenever $w_j = 1/16$ for all j , i.e., whenever the wind rose is uniform.

Site population factors (both SPF_n and $WRS PF_n$ for $n = 5, 10, 20,$ and 30 miles) are presented in Appendix D for each of the 91 sites. Table 3-1 presents average values for these factors for each of the five NRC administrative regions. Examination of Table 3-1 shows that, for each distance and for both factors, the regional average values are highest for the Northeast region and lowest for the Southwest region, and decrease in the order NE, MW, S, W, SW.

Table 3-1

SPF and WRS PF Values for the Five
NRC Administrative Regions^a

	<u>NE</u>	<u>MW</u>	<u>S</u>	<u>W</u>	<u>SW</u>
SPF ₅	0.16±0.22	0.09±0.15	0.03±0.04	0.01±0.02	0.01±0.01
SPF ₁₀	0.17±0.19	0.10±0.14	0.05±0.03	0.03±0.03	0.01±0.01
SPF ₂₀	0.20±0.18	0.12±0.12	0.08±0.06	0.04±0.03	0.03±0.02
SPF ₃₀	0.25±0.24	0.14±0.13	0.09±0.06	0.05±0.04	0.04±0.04
WRS PF ₅	0.17±0.29	0.10±0.18	0.04±0.04	0.02±0.02	0.01±0.01
WRS PF ₁₀	0.18±0.22	0.11±0.16	0.05±0.03	0.04±0.06	0.02±0.01
WRS PF ₂₀	0.22±0.20	0.13±0.14	0.08±0.07	0.05±0.04	0.03±0.02
WRS PF ₃₀	0.26±0.26	0.15±0.14	0.09±0.07	0.06±0.06	0.04±0.03

^aStandard Deviations are indicated as bounds

3.3 Site Population Statistics

The 91 population distributions examined in this chapter are all constructed on a 16 sector, circular polar grid. For any specified portion (a circle, an annulus, a sector) of that grid, 91 values of population density are available, one for each of the 91 population distributions. By cumulation of the 91 values for a given portion of the grid, a population density CCDF may be constructed.* Six different sets of population density CCDFs have been constructed for the following areas of the population distribution grid:

- Set 1: eight annuli (0-2, 2-5, 5-10, 10-20, 20-30, 30-50, 50-100, and 100-200 mi).
- Set 2: eight radial distances (0-2, 0-5, 0-10, 0-20, 0-30, 0-50, 0-100, and 0-200 mi).

*Population density CCDFs are Log-Log plots of the fraction of sites vs population density. Any point on the distribution gives the fraction of sites (y-axis value), which have a population density within the specified portion of the grid (annulus, circle, sector), that is greater than or equal to the specified population density (x-axis value).

- Set 3: the most populated 22.5° sector in each of six annuli (0-2, 2-5, 5-10, 10-20, 20-30, and 30-50 mi) on the 16 sector grid.
- Set 4: the most populated 22.5° sector in each of six radial distances (0-2, 0-5, 0-10, 0-20, 0-30 mi, and 0-50 mi) on the 16 sector grid.
- Set 5: the most populated 45° sector (two adjacent 22.5° sectors) in each of six annuli (0-2, 2-5, 5-10, 10-20, 20-30, and 30-50 mi) on the 16 sector grid.
- Set 6: the most populated 45° sector (two adjacent 22.5° sectors) in each of six radial distances (0-2, 0-5, 0-10, 0-20, 0-30, and 0-50 mi) on the 16 sector grid.

Each set of CCDFs contains CCDFs for each of the five NRC administrative regions (NE, MW, S, W, SW) and for all regions combined (All). CCDFs were also calculated for 45° sectors because atmospheric dispersion can produce plumes with an angular dispersion greater than 22.5°.

Because of the large number of CCDFs calculated (total of 240) most of the CCDFs are presented in Appendix D. Also presented in Appendix D are the site specific data from which the CCDFs were constructed. In this section, Figure 3-3 presents CCDFs of population density at the 91 sites for six radial annuli (0-2, 2-5, 5-10, 10-20, 20-30, and 30-50 mi) and Figure 3-4 presents CCDFs for six radial distances (0-2, 0-5, 0-10, 0-20, 0-30, and 0-50 mi). CCDFs of population density, in the most populated 22.5° and 45° sectors at each of the 91 sites, are presented for the same two sets of six annuli and six radial distances in Figures 3-5 through 3-8. Tables 3-2 and 3-3 list maximum, 90th percentile, median, and minimum population densities for each of the five NRC administrative regions and for all regions combined for eight annuli and eight radial distances. Table 3-4 presents population densities for 4 radial distances of the most populated 22.5° sector for each of the five administrative regions and for all regions combined. Finally, Figures 3-9 through 3-11 present scatter plots

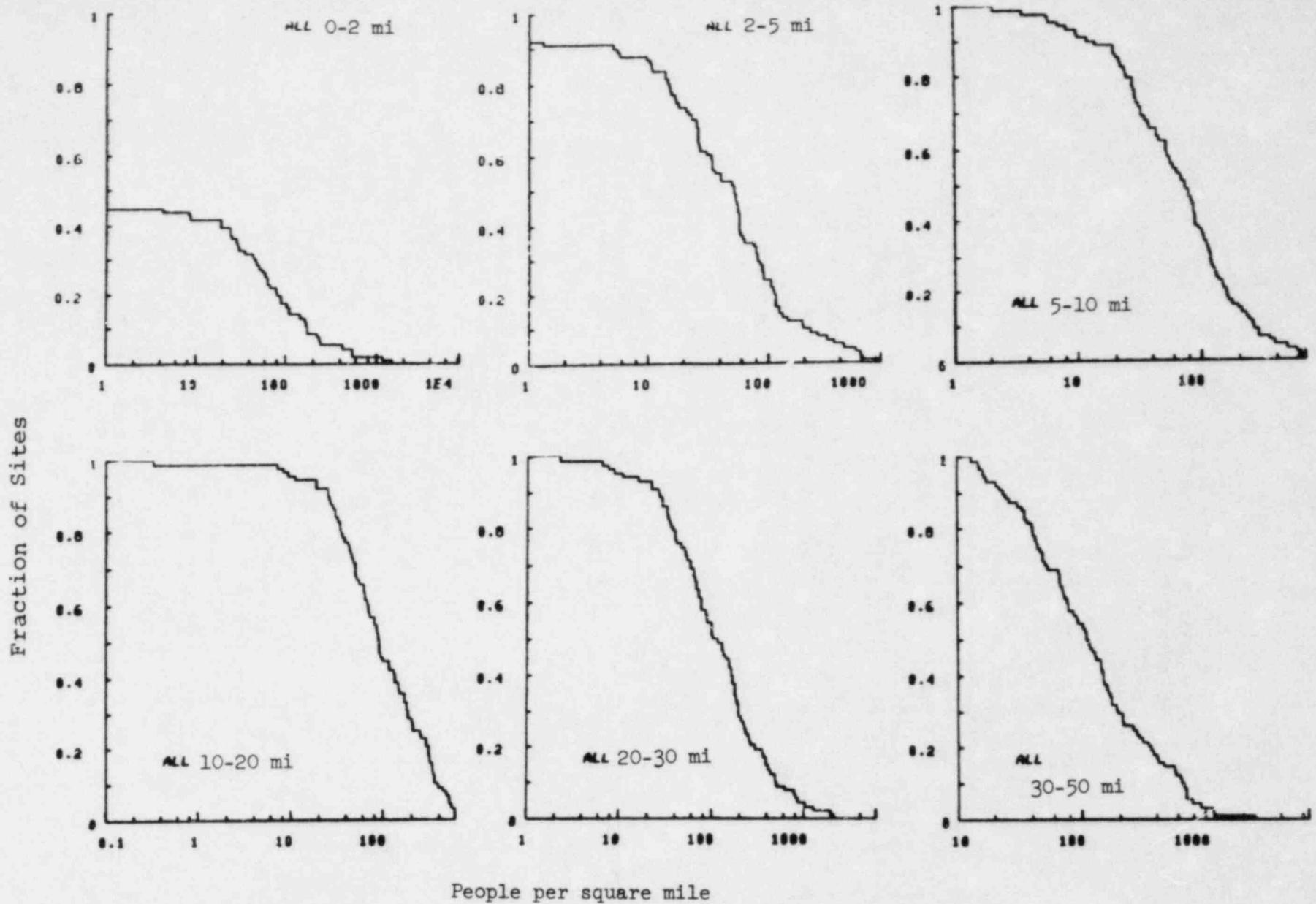


Figure 3-3. CCDFs of Population Density (People/Mile²) at 91 Sites for Six Radial Annuli.

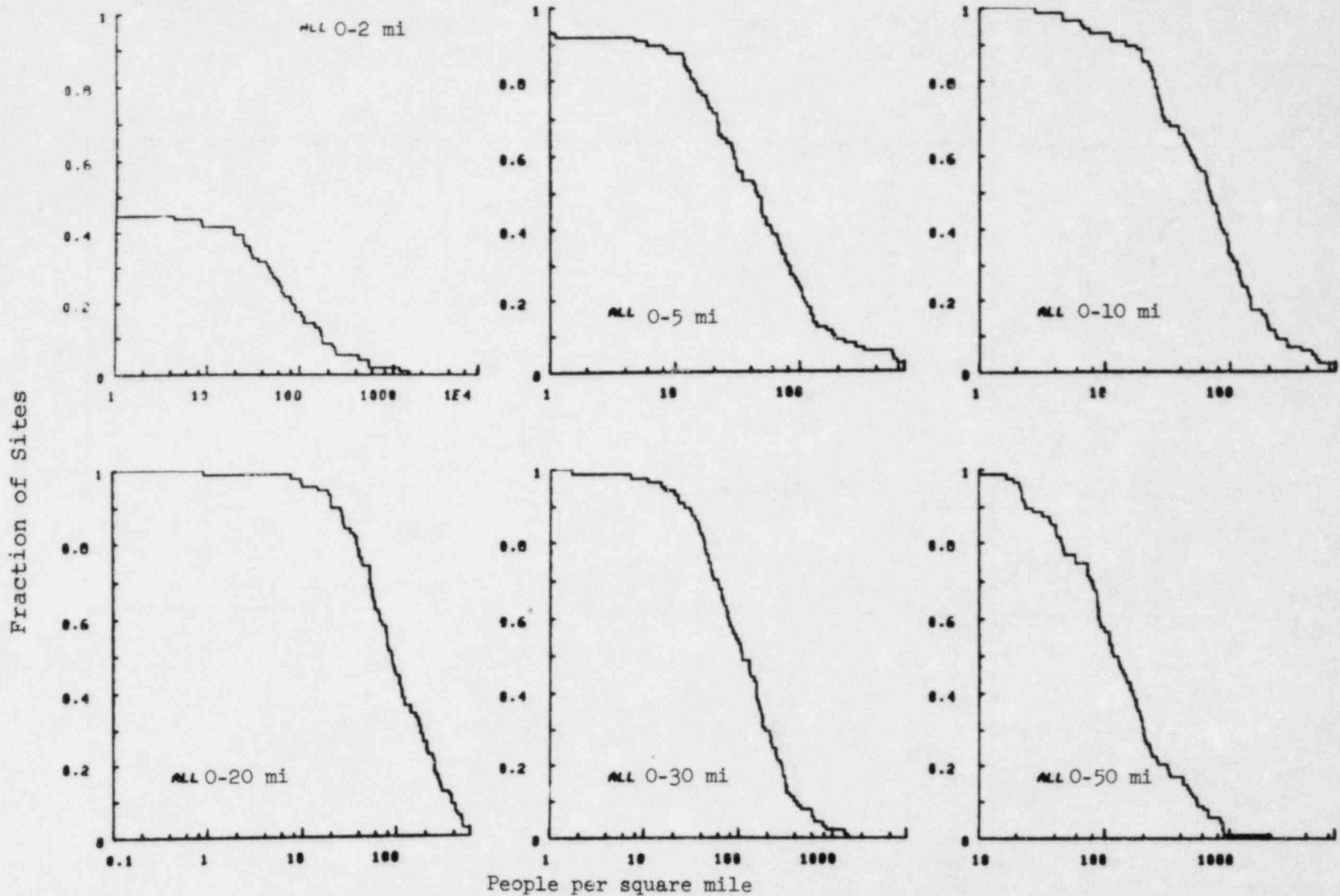


Figure 3-4. CCDFs of Population Density (People/Mile²) at 91 Sites for Six Radial Distances

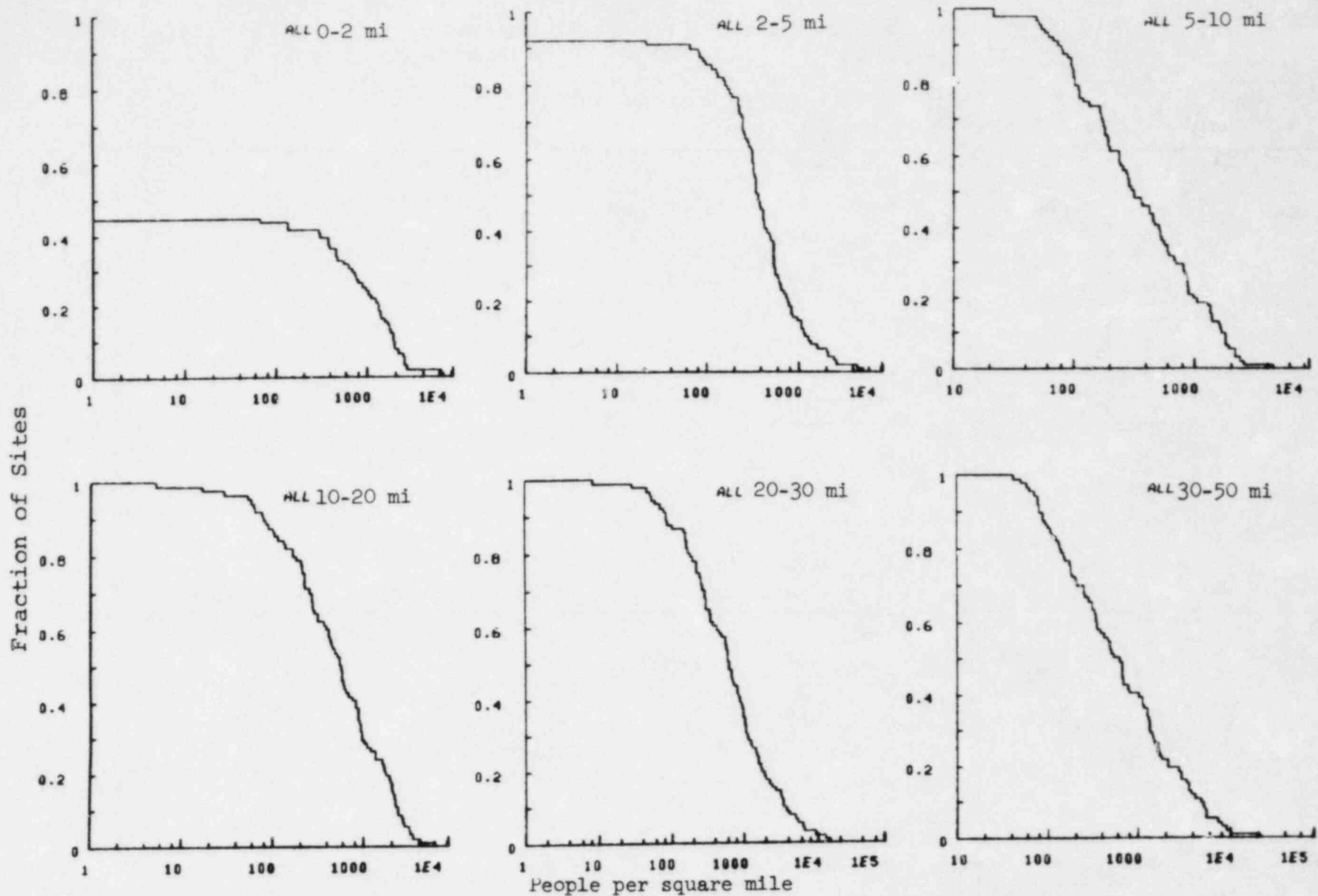


Figure 3-5. CCDFs of Population Density (People/Mile²) in the Most Populated 22.5 Degree Sector at 91 Sites for Six Radial Annuli.

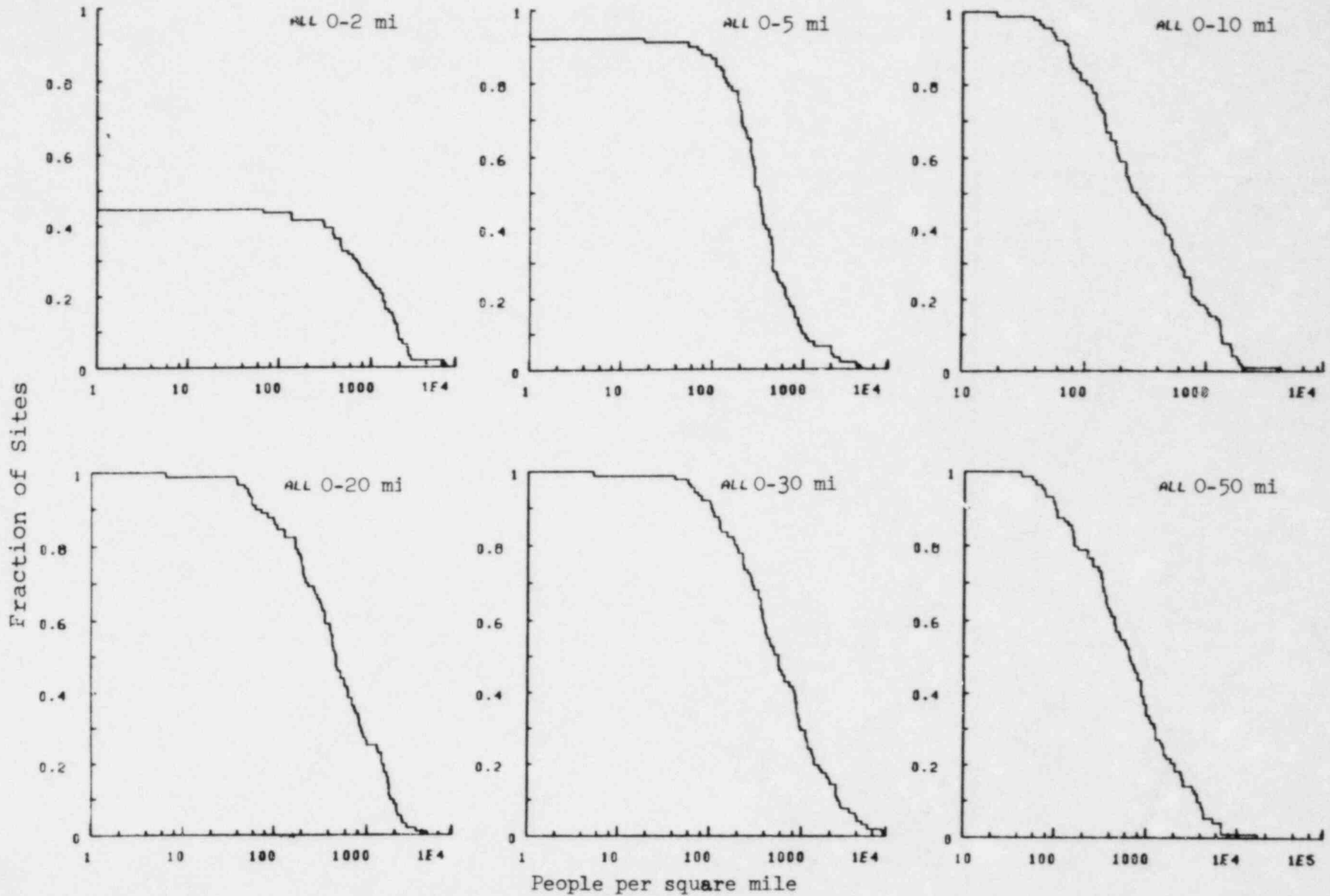


Figure 3-6. CCDFs of Population Density (People/Mile²) in the Most Populated 22.5 Degree Sector at 91 Sites for Six Radial Distances.

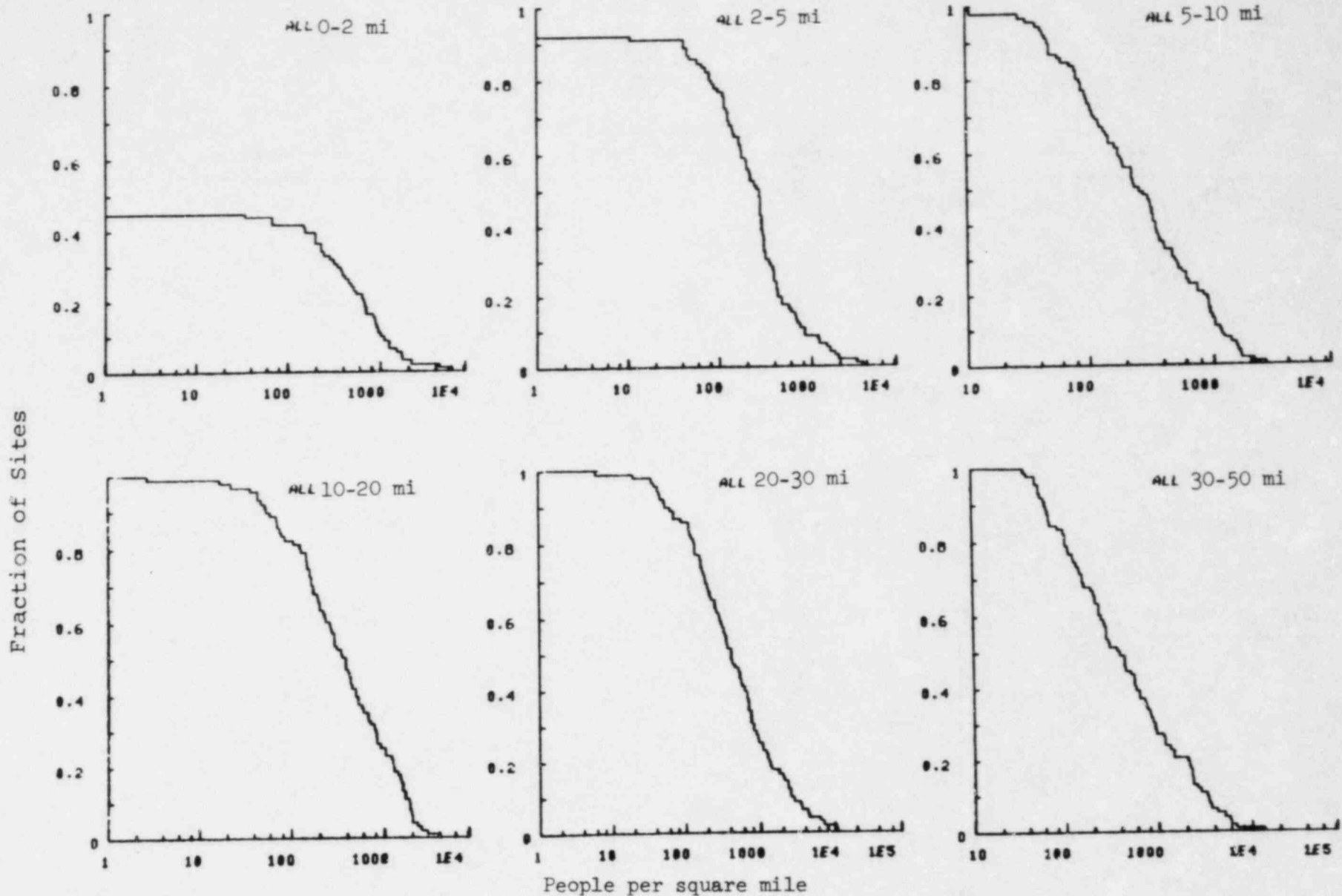


Figure 3-7. CCDFs of Population Density (People/Mile²) in the Most Populated 45 Degree Sector at 91 Sites for Six Radial Annuli.

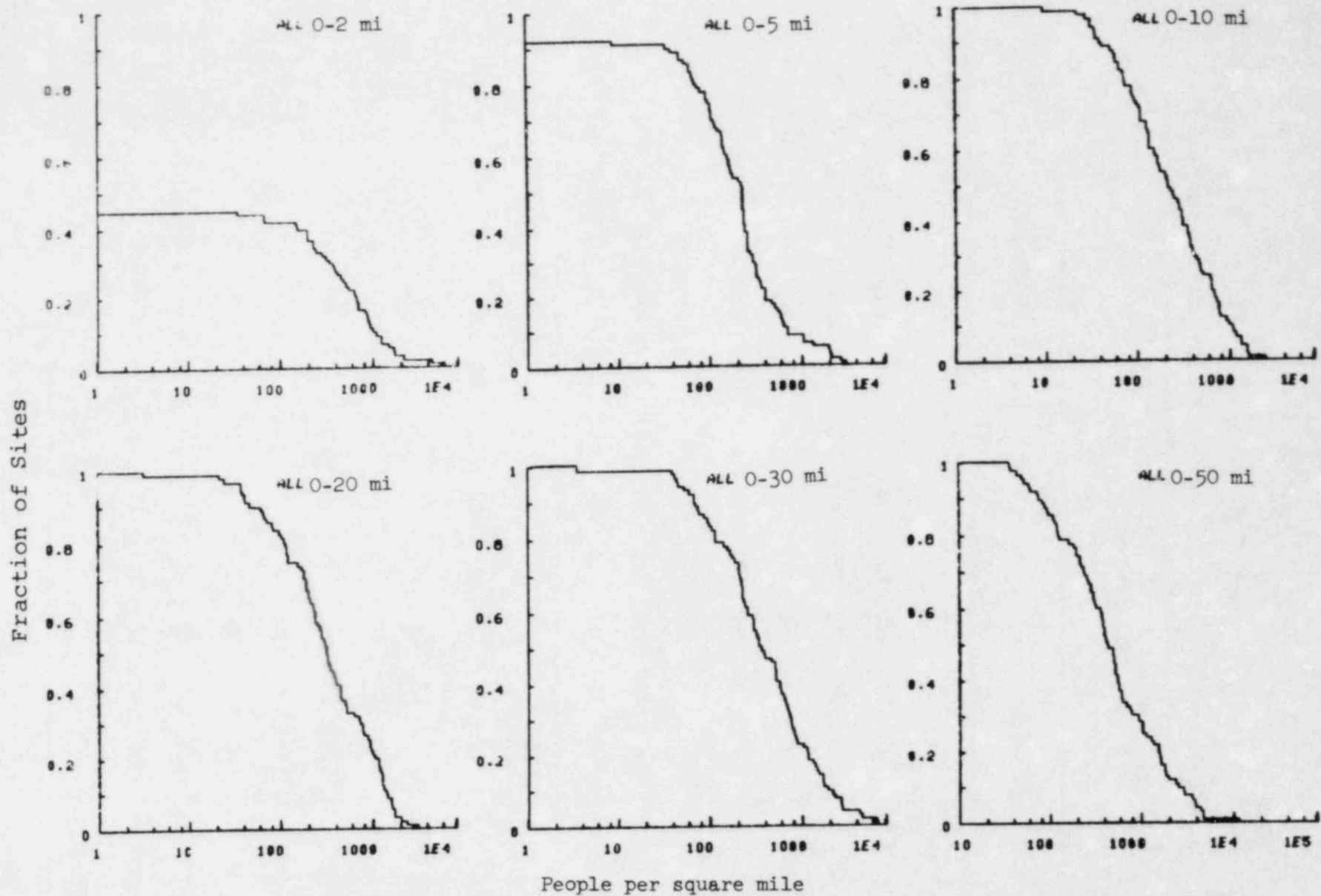


Figure 3-8. CCDFs of Population Density (People/Mile²) in the Most Populated 45 Degree Sector at 91 Sites for Six Radial Distances.

Table 3-2. Maximum, 90th Percentile, Median, and Minimum Population Densities (people/sq mi) for Seven Radial Annuli by Geographic Region and for All Regions Combined.

<u>CCDF Value</u>	<u>Maximum</u>						<u>90th Percentile</u>					
<u>Region</u>	NE	MW	S	W	SW	All	NE	MW	S	W	SW	All
<u>Interval (mi)</u>												
0-5	790	540	180	100	30	790	740	270	100	100	30	190
5-10	620	700	250	100	40	700	550	280	180	200	40	260
10-20	730	530	510	180	150	730	670	340	300	180	150	380
20-30	2000	1300	490	490	230	2000	1800	620	200	490	240	490
30-50	2500	1200	210	630	290	2500	770	940	160	620	280	660
50-100	880	440	180	310	90	880	820	430	110	310	90	420
100-200	350	190	160	150	40	350	280	170	110	150	40	190
<u>CCDF Value</u>	<u>Median</u>						<u>Minimum</u>					
<u>Region</u>	NE	MW	S	W	SW	All	NE	MW	S	W	SW	All
<u>Interval (mi)</u>												
0-5	100	60	30	20	10	40	0	8	0	0	0	0
5-10	130	60	80	30	20	80	6	4	8	2	7	2
10-20	170	90	70	60	30	90	40	9	10	0	7	0
20-30	180	120	100	50	40	110	50	9	8	2	7	2
30-50	400	100	80	40	130	110	50	20	10	20	30	10
50-100	360	130	80	50	40	90	20	10	30	10	20	10
100-200	170	110	70	30	30	80	20	30	8	9	6	6

Table 3-3. Maximum, 90th Percentile, Median, and Minimum Population Densities (people/sq mi) for Seven Radial Distances by Geographic Region and for All Regions Combined.

<u>CCDF Value</u>	<u>Maximum</u>						<u>90th Percentile</u>					
<u>Region</u>	NE	MW	S	W	SW	All	NE	MW	S	W	SW	All
<u>Interval (mi)</u>												
0-5	790	540	180	100	30	790	740	270	100	100	30	190
0-10	650	660	200	170	30	660	470	270	150	170	280	230
0-20	710	470	410	160	110	710	630	340	250	160	110	380
0-30	1500	850	380	320	180	1500	1300	460	290	330	180	420
0-50	2100	890	210	460	200	2100	880	830	200	460	200	530
0-100	760	370	170	350	100	760	750	350	130	360	100	440
0-200	350	210	160	120	50	350	340	200	100	120	50	290
<u>CCDF Value</u>	<u>Median</u>						<u>Minimum</u>					
<u>Region</u>	NE	MW	S	W	SW	All	NE	MW	S	W	SW	All
<u>Interval (mi)</u>												
0-5	100	60	30	20	10	40	0	8	0	0	0	0
0-10	120	60	70	30	20	70	4	10	6	3	7	3
0-20	210	90	60	50	30	90	30	10	20	1	8	1
0-30	230	120	100	50	30	110	50	20	10	2	7	2
0-50	320	120	90	50	90	120	50	20	20	10	20	10
0-100	330	120	80	70	70	90	80	10	40	10	30	10
0-200	290	130	80	40	40	90	50	30	20	20	10	10

Table 3-4. Maximum, 90th Percentile, Median, and Minimum Population Densities (people/sq mi) for the Most Populated 22.5° Sector within Four Radial Distances by Geographic Region and for All Regions Combined.

<u>CCDF Value</u>		<u>Maximum</u>					<u>90th Percentile</u>						
<u>Region</u>	<u>Interval (mi.)</u>	NE	MW	S	W	SW	ALL	NE	MW	S	W	SW	ALL
	0-5	4200	2000	950	450	320	4200	3500	2000	510	460	310	950
	0-10	2000	3800	1300	1600	140	3800	1300	1400	1000	1500	140	1000
	0-20	4500	3400	2600	800	860	4500	2000	2100	2100	780	860	1800
	0-30	8700	5200	4000	1800	1600	8700	3700	3200	1300	1800	1600	2500
<u>CCDF Value</u>		<u>Median</u>					<u>Minimum</u>						
<u>Region</u>	<u>Interval (mi.)</u>	NE	MW	S	W	SW	ALL	NE	MW	S	W	SW	ALL
	0-5	630	350	240	280	170	330	0	50	0	0	0	0
	0-10	750	220	280	150	70	270	40	40	60	20	50	20
	0-20	880	620	360	430	150	480	170	40	50	6	40	6
	0-30	940	800	430	290	120	550	110	60	40	5	70	5

by administrative region of the site specific population data for population density seven annuli and seven radial distances, and for four radial distances of the most populated 22.5° sector.

In Section 2.7.4 the sensitivity of consequences to population distribution was examined using a number of hypothetical population distributions, all of which had average densities within 30 miles of the reactor of 750 people per square mile. Figure 3-4 shows that, within 30 miles of the reactor, only 4 of the 91 sites (4%) have population densities within that distance which exceed 750 people per square mile. Figure 3-8 shows that for the most populated 45° sector 30 of the 91 sites (33%) have population densities that exceed 750 people per square mile. Finally, Figure 3-6 and Table D1.4 show that for the most populated 22.5° sector 38 of the 91 sites (42%) have densities greater than 750 people per square mile.

Examination of the reactor site population density scatter plots for the five NRC administrative regions presented in Figures 3-9 through 3-11 shows that the densities within any region range across approximately two orders of magnitude and that between regions there is substantial overlap of ranges. Densities are largest in the Northeast and lowest in the Southwest; qualitatively the densities are ordered from largest to smallest: NE, MW, S, W, SW. Tables 3-2 through 3-4 confirm this qualitative ordering, although there are a number of exceptions (S and W are often inverted).

3.4 Time Dependent Trends

Figure 3-12 presents scatter plots by region of the year of site selection (the year in which a construction permit was granted was used as a surrogate for the actual year of site selection) for the 91 reactor sites examined in this study. Only four sites were selected prior to 1960, two each in the Northeast and the Midwest. Not until 1973 was a reactor site selected in the Southwest.

Because the years during which sites were selected are distributed over time quite differently by region, trends by selection year in the density of the population distributions surrounding reactor sites were also examined both by region and for all regions combined. Figure 3-13 presents plots of population density within

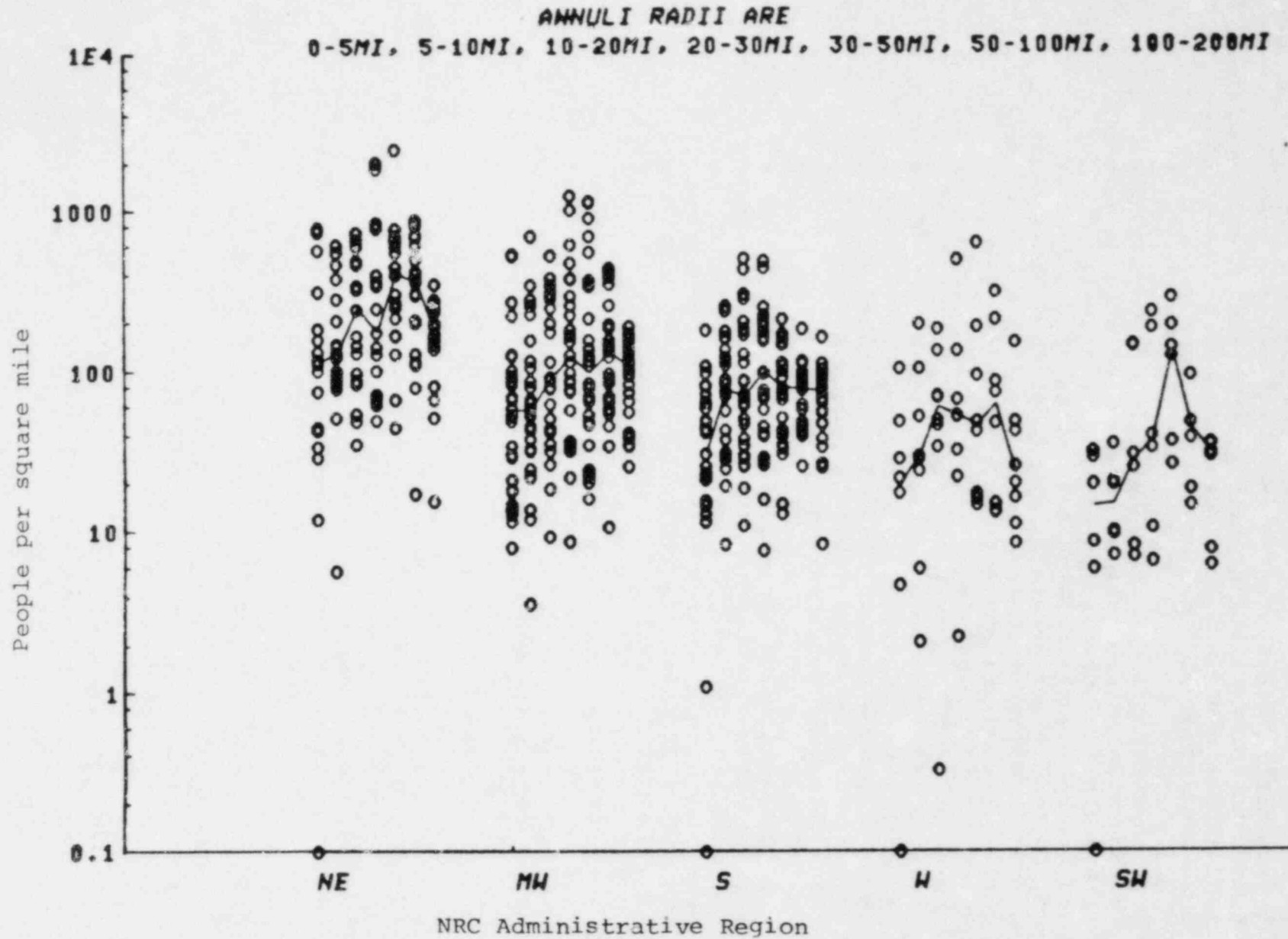


Figure 3-9. Population Density (People/Mile²) at 91 Reactor Sites by Geographic Region for 7 Radial Annuli: 0-5, 5-10, 10-20, 20-30, 30-50, 50-100, and 100-200 Miles (the Lines Connect Median Values).

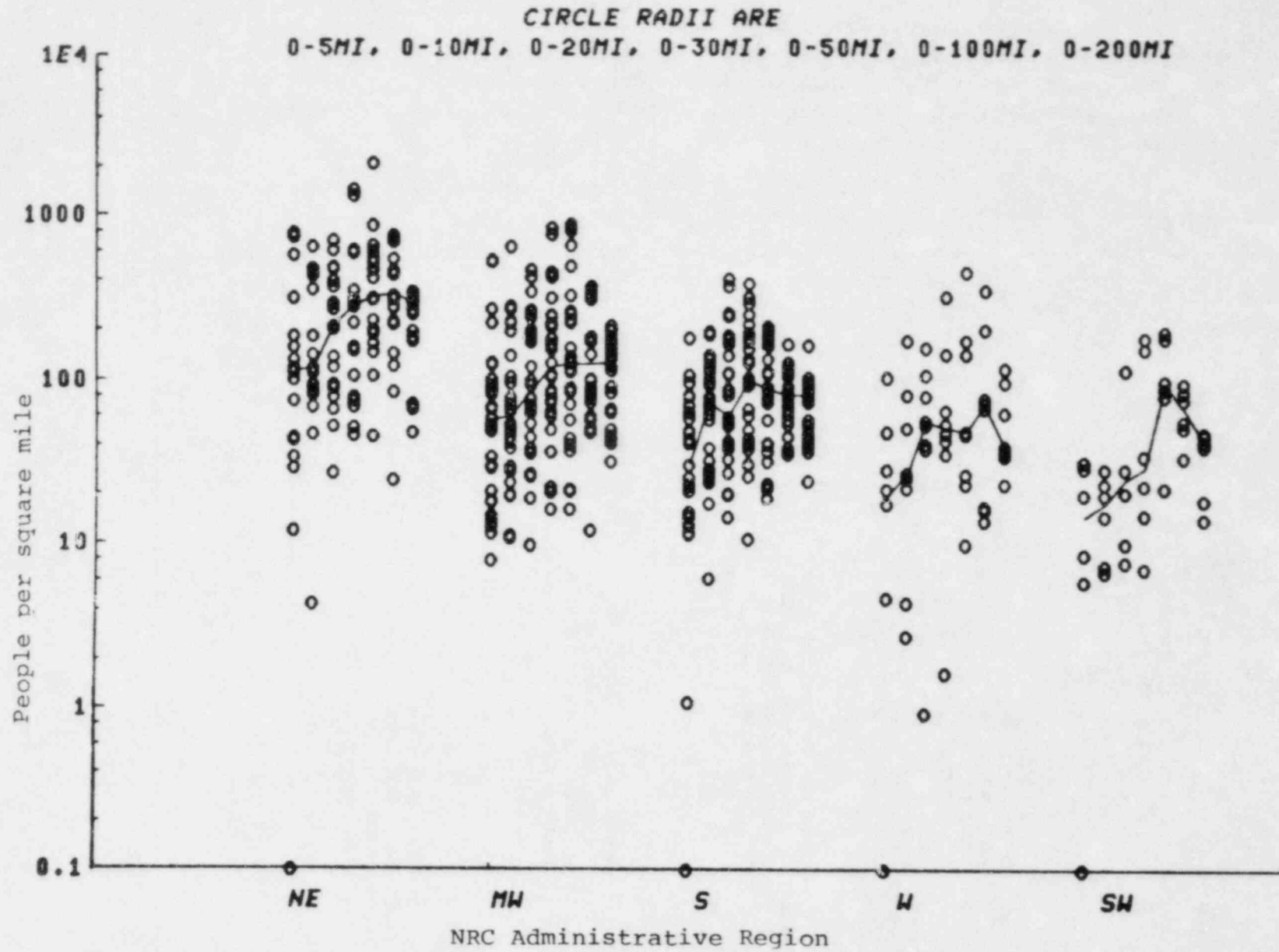


Figure 3-10. Population Density (People/Mile²) at 91 Reactor Sites by Geographic Region for 7 Radial Distances. 0-5, 0-10, 0-20, 0-30, 0-50, 0-100, and 0-200 Miles.

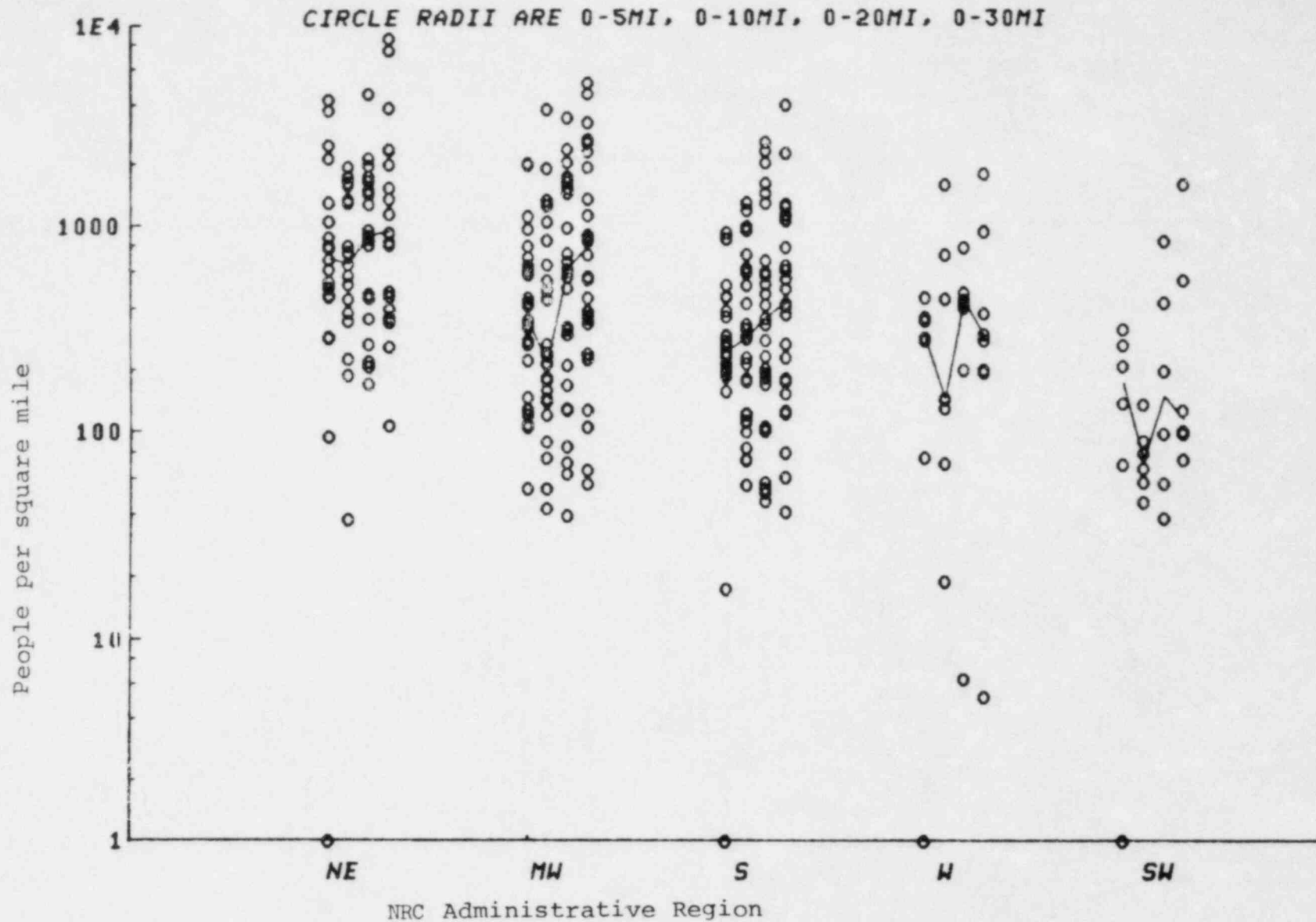


Figure 3-11. Population Density (People/Mile²) in the Most Populated 22.5 Degree Sector at 91 Sites by Geographic Region for 4 Radial Intervals: 0-5, 0-10, 0-20, and 0-30 Miles. (The lines connect median values).

30 miles of the site versus year of site selection, for each region and for all regions combined. The line on each plot is the least squares linear fit of the data. The slope of the line is the change in the logarithm of 30-mile population density with time. The lines for the Northeast, Midwest, and South have slopes which, given the scatter in the data points, are little different from zero (NE = -0.04, MW = -0.01, S = 0.03). Given the narrow time span and considerable scatter of the five Southwest site selection years, the slope of that plot (SW = 0.7), though substantial, is of no importance. Only for the West (W = -0.23) and to a lesser degree for all regions combined (All = -0.08) do the slopes of the plots seem important.

To better define the significance of the time trends displayed in Figure 3-13, an analysis of variance [3] of the logarithm-transformed population density data was performed. The analysis partitioned the variability in the data among four terms: one for the common time trend of all regions combined, one for unique time trends within each region, one for regional differences corrected for regional time trends, and a residual term for variability not attributable to either regional differences or time trends. The results of this analysis are presented in Table 3-5. In the table, the mean square value is obtained by dividing the sum of squares value by its number of degrees of freedom (number of independent terms in the sum of squares). Comparison of the magnitude of the mean square values indicates the relative importance of the three terms (mean square values large by comparison to the residual mean square value are useful in explaining the observed variability).

Table 3-5 Analysis of Variance

Source of Variation	Sum of Squares	Degrees of Freedom	Mean Square
Common time trend	11.2	1	11.2
Regional time trend	18.4	4	4.6
Regional differences corrected for regional time trends	7.1	4	1.8
Residual	<u>82.0</u>	<u>81</u>	1.0
TOTAL	118.7	90	

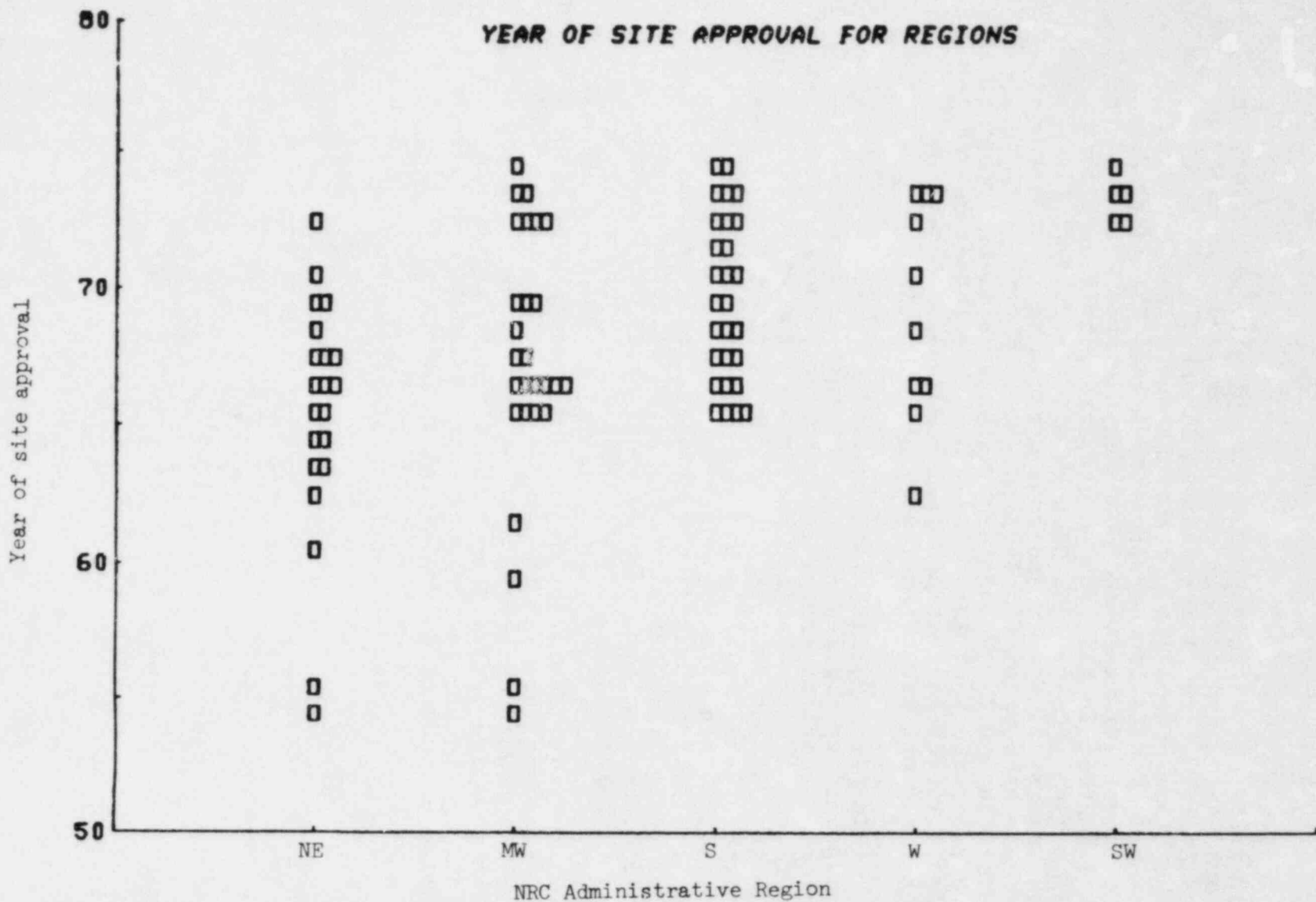
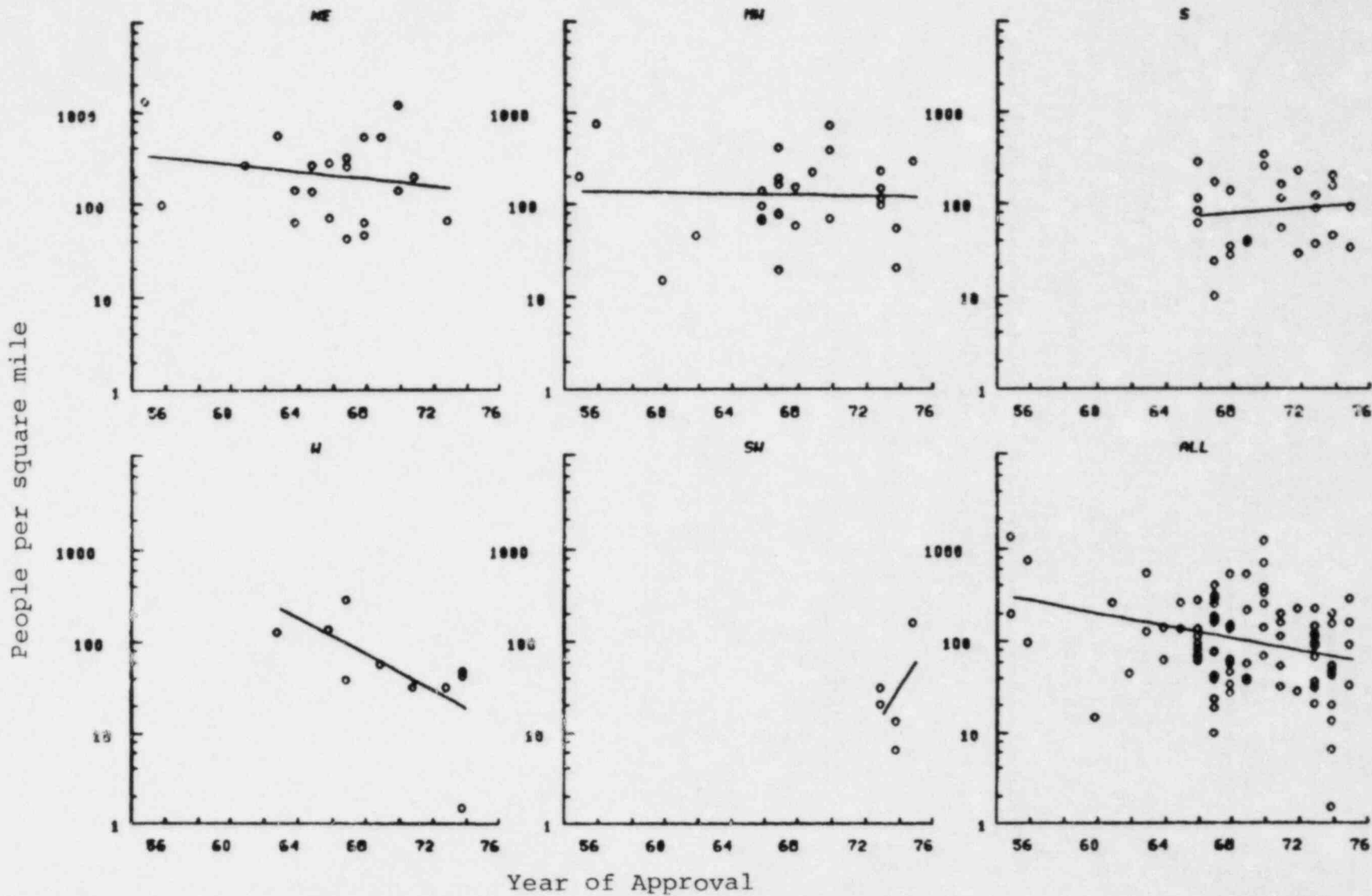


Figure 3-12. Scatter Plot by Region of Year of Site Approval.

POPULATION DENSITY VS APPROVAL YEAR
FOR 91 REACTOR SITES BY REGION



3-23

Figure 3-13. Plots of 30-Mile Population Density vs. Year of Site Approval. The lines are the least squares linear fit to the data. The slope of the lines are: NE = -0.04, MW = -0.01, S = 0.03, W = -0.23, SW = 0.7 and All = -0.08.

Table 3-5 suggests that the variability in logarithm-transformed site population data results principally from a common trend with time. Since this common trend is not strong (the slope of the linear correlation for all regions combined is only -0.08), its importance is unclear. It is possible that the trend toward less dense siting with time is (1) real, or (2) an artifact of the data. If the trend is real, it may result from some factor not addressed by this analysis (e.g., with the passage of time, suitable sites near cities become unavailable, so more remote sites are selected, which are necessarily less densely populated).

References for Chapter 3

1. Demographic Statistics Pertaining to Nuclear Power Reactor Sites, U. S. Nuclear Regulatory Commission, NUREG-0348, October 1979.
2. J. E. Kohler, A. P. Kenneke, and B. K. Grimes, The Site Population Factor: A Technique For Consideration of Population In Site Comparison, U. S. Atomic Energy Commission, WASH-1235, October 1974.
3. P. W. M. John, Statistical Design and Analysis of Experiments, Macmillan, New York, NY, 1971.

4. Site Availability Impacts

4.1 Introduction

The previous chapters of this report have examined the potential consequences of accidents at nuclear power reactors and the relationship of site population distribution to consequences. In addition, the population characteristics of current sites were examined. In order to reduce societal risk from siting, it is desirable to locate reactors in areas of low population density. This, of course, forces a trade-off between reduced risk and site availability. To evaluate more precisely the implications of this trade-off, this chapter reports on work performed by Dames and Moore, under contract to Sandia, to study the impacts of siting criteria alternatives on land availability. The study included consideration of the impacts on site availability of environmental factors (seismicity, topographic character, surface and groundwater availability, and restrictions due to regulations (wetlands, National parks, etc.)) as well as population.

4.2 Methodology

The study was performed in three steps: identification of issues affecting site availability, data collection, and analysis and display of data. The final step was performed iteratively, using Dames and Moore's Geographic Information Management System (GIMS), which manipulates geographical data in a grid cell format.

4.2.1 Issues of Concern

A set of general siting issues was defined and used to identify and discriminate more suitable siting areas from less suitable ones. These issues cover a variety of demographic considerations and a diverse set of environmental siting criteria relating normally to costs.

Three issues were defined for population criteria. These are:

1. Stand-off Zones -- restrictions imposed by distance from urban centers of a particular size;
2. Population Density -- a measure of population density within a specified (circular) area; and
3. Angular Population Distribution -- a measure of the uniformity of population distribution within a specified (circular) area.

Four issues were defined for environmental criteria. These are:

1. Restricted Lands -- those areas in which the development of a nuclear power plant is difficult due to legal constraints or the predominance of wetlands;
2. Seismic Hardening -- the additional cost or difficulty of compliance with seismic design criteria; assumed to be measured by the maximum expected (50 year) horizontal ground acceleration expressed in fractions of gravity (g);
3. Site Preparation -- A relative measure of the ruggedness or topographic character expressed as an index which indicates the percentage of land with access and construction difficulty; and
4. Water Availability -- an index reflecting the relative cost of obtaining water for cooling.

The latter three issues were further combined to define an overall environmental suitability measure.

It is necessary to keep in mind that the goal of this study was to provide information regarding land availability and not to select sites on which to construct nuclear power plants. The defined issues were

analyzed on a nationwide basis to yield trends and indicate areas on a regional basis that could be considered for selection of power plant sites. Site selection analyses are generally conducted at a more specific scale and level of resolution. This is especially true for environmental criteria. Many site selection issues are related to physical features that are not geographically extensive, or consider factors that are important in the site planning process (which includes the precise location of the reactor and other plant facilities within the site). While these factors are important for specific site identification, they are not considered here.

4.2.2 Data Structure Diagram

A data structure diagram describing the flow of data and information through the Dames and Moore study is presented in Figure 4-1. The diagram shows the sources and flow of information on the demographic and environmental issues as well as how these issues are combined to provide assessments of land availability for various siting criteria.

The data structure diagram is principally an aid to help conceptualize the entire impact analysis. For the most part, each box on the diagram represents a map that was created or a data file that could be displayed as a map.

4.2.3 Display of Results

Results are presented as maps which display the impact of a criterion, which when printed on a transparent medium, can be overlaid on other maps to see the effect of composite criteria. Many of the results are displayed for the whole U.S. as well as for the northeastern section of the U.S. (the most populous region of the country).

In addition to maps, results are presented as tabulations of statistics for each state for various categories of information. Most of this statistical work was performed for comparisons of impacts of environmental suitability and population criteria and is described in Section 4.6.

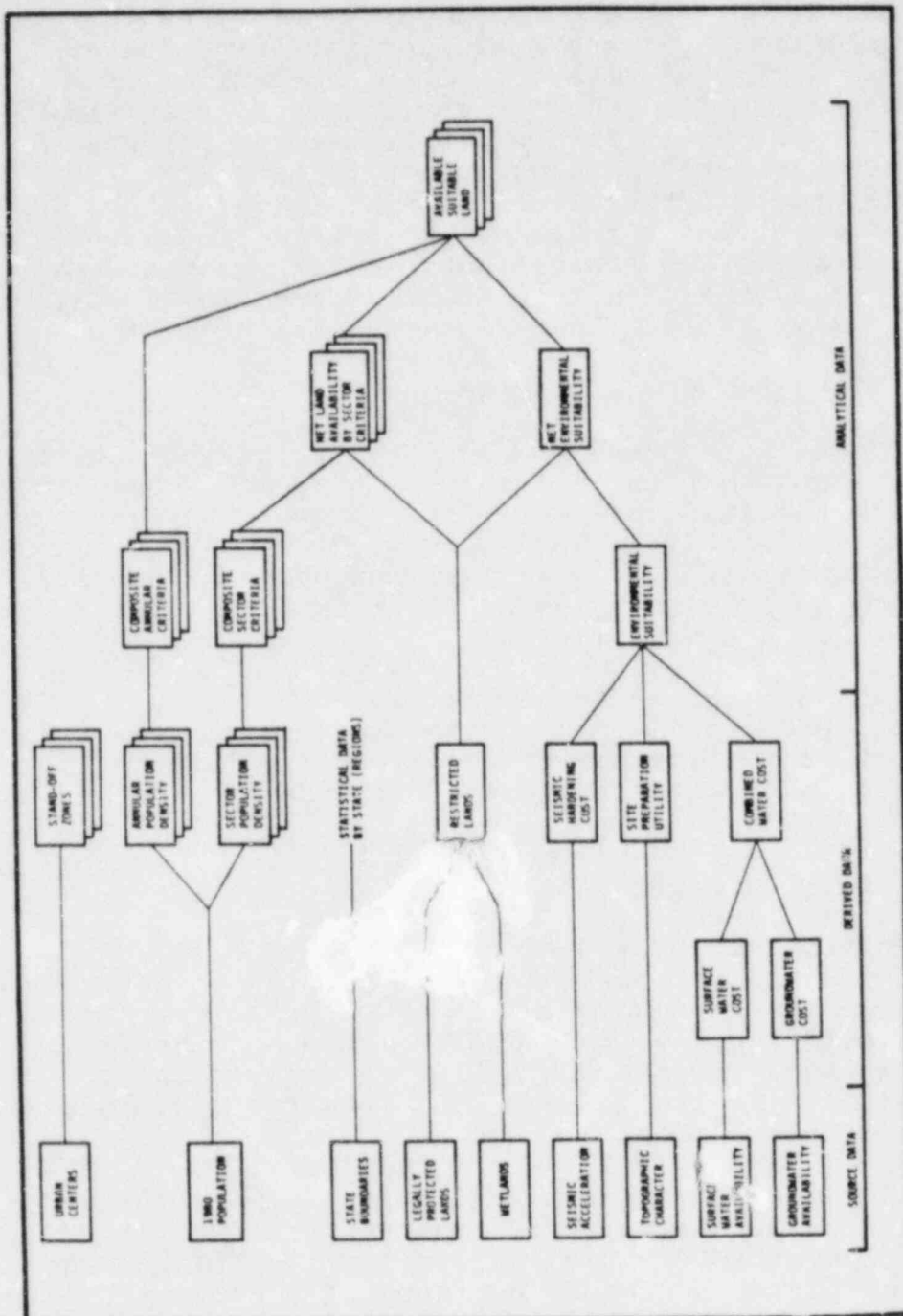


Figure 4-1 Data Structure Diagram for the Dames and Moore Study

4.2.4 Geographic Information Management System

The Dames and Moore Geographic Information Management System (GIMS) was employed for this study. GIMS is a computerized system that provides planners with a comprehensive approach to recording, storing, manipulating and displaying the mappable information used in studies of this nature. The system provides a data base which can be readily updated, and allows evaluation of many alternative criteria that would otherwise be explored by time-consuming manual procedures.

4.2.5 Mapping Approach

The mapping approach is a function of four related factors: (1) characteristics of the study area; (2) nature of the input data; (3) analysis methodology; and (4) desired output or display products. All of these factors are important in determining the base map and grid cell size and shape. Based on these considerations, the Albers Equal Area projection was chosen at a scale of 1:3,168,000 (1 inch = 50 miles) for digitizing input data and displaying output results. In addition, it was decided that data would be analyzed using a grid system consisting of square cells 5 km on a side (each cell represents 25 km² or 9.65 square miles). An artificial equal-area grid was placed on the base map by converting longitude and latitude coordinates into X and Y coordinates given in meters on the ground from an origin in the southwest corner of the map. Using grid cells of this size and shape and the Albers projection ensures that any maps produced from the analysis have several important characteristics:

1. Format is consistent with map projection and level of detail of input data;
2. A reliable sampling of population data (especially for the smaller area annuli) is maintained;
3. Computer time and cost are at an efficient level;
4. Maps are of manageable size while retaining important visible regional patterns;

5. Directional bias of analysis is minimal; and
6. Line printer graphics show area relationships truly, and thus, do not distort the implied impacts of criteria.

4.3 Data Base

The data base consists of those data necessary for analyzing both demographic criteria and net environmental suitability. It includes:

1. Demographic Data
 - o Location and population of urban centers
 - o 1980 population estimated for enumeration districts
2. State and national boundaries
3. Restricted lands
 - o Legally protected
 - o Major wetlands
4. Seismic hardening
 - o Seismic acceleration
5. Site preparation
 - o Topographic character
6. Water availability
 - o Surface water availability
 - o Groundwater availability

4.3.1 Demographic Data

Site availability impacts based on demographic characteristics considered both standoff distances from urban centers and surrounding population density and angular distribution. These analyses required two types of data.

4.3.1.1 Urban Centers

Data concerning urban centers were extracted from NUREG-0348 [1]. This publication categorizes urban centers into three groups: those centers with population in excess of 25,000 people, greater than 100,000 people, and greater than 200,000 people. The data were updated with information provided by the NRC to include population figures for urban centers greater than 250,000 people, greater than 500,000 people and greater than 1,000,000 people.

Populations for these urban centers were identified geographically by latitude and longitude coordinates. The degrees of longitude and latitude were converted into X and Y coordinates which corresponded to the same geographic grid that was applied to the Albers base map as discussed in Section 4.2.5. This conversion prepared the data for eventual use in the production of maps showing how much land would be available after imposing population center standoff zone criteria. The analysis of standoff zones is discussed in Section 4.5.1.

4.3.1.2 Population Density

To calculate population density, analyze various criteria, and ensure that the results are reliable in the face of changing national population trends, it was necessary to obtain the most up-to-date and detailed population figures. Figures from the 1980 decennial census were not available in time for use in this study. In their place, estimates for 1980 population were used. Data were supplied by the National Planning Data Corporation (Ithaca, New York). While it is difficult to give an estimate for the percent error, it is believed that the data are quite reliable, especially when individual data points (which correspond to centroids of enumeration districts or block groups) are taken in groups of 4 or 5. This is typically the case in this study. It is especially true for all areas except the most remote and rural. Thus, the data are considered reliable for its intended function, the analysis of population data around the more urbanized areas of the country.

The 1980 population estimates were obtained formatted on magnetic tapes with population figures geographically referenced by latitude and longitude. As with urban center data, the degrees of longitude and latitude were converted into X and Y coordinates on the Albers grid system. This process prepared the demographic data base for analysis of population density. The analysis is discussed in Section 4.5.2.

4.3.2 State Boundaries

Using the Albers base map at 1:3,168,000 scale, all coastlines, international boundaries, and state boundaries were digitized. The area within each state was assigned a unique code to identify it for further use. The state boundaries map file allows analysis or display of results on an individual state basis or by any group of states.

4.3.3 Restricted Lands

The nature of certain areas of the country causes them to be protected or restricted from development. Two types of lands were considered as restricted: legally protected lands and existing wetlands.

4.3.3.1 Protected Lands

The Energy Reorganization Act of 1974 (Section 207) states that national forests, national parks, national historic monuments and national wilderness areas should be excluded from consideration as potential nuclear energy center sites. While this study did not deal with nuclear energy centers, it is reasonable to consider such lands as protected from the siting of a single nuclear power plant, regardless of a national policy on this matter. Utility industries tend to avoid such areas because of the possibility of time consuming and costly legal battles. The following areas were considered to be protected:

- o National Parks
- o National Forests
- o National Monuments
- o National Wilderness Areas

- o National Grasslands
- o National Wildlife (Game) Refuges
- o National Recreation Areas
- o National Seashores
- o State Parks
- o State Forests
- o State Reserves/Refuges
- o State Recreation Areas
- o Military Reservations
- o Indian Reservations

Three different map sources were used to obtain the locations of these protected lands. The United States base map utilized in this study (compiled by the U.S. Geological Survey, 1965) was used to extract the location of national parks, forests, monuments, wildlife refuges, and Indian reservations. Sectional sheets at a scale of 1:2,000,000 from the National Atlas [2] were used to update the boundary information for the above protected lands as well as to obtain the location of national recreational areas. Because of the relatively small size of protected state areas and some protected national areas, a screening process was used for certain types of land, rather than identifying and digitizing every one. Because this study dealt not with site selection but with the general patterns of land availability, a minimum size screen of 100 square miles was used for the following types of areas: military reservations, national grasslands, state parks, state forests, state monuments, state reserves and refuges, and state recreational areas. Information for these types of lands was obtained from the 1980 Rand McNally Atlas, as this was the most detailed, up-to-date and uniform source of information.

4.3.3.2 Wetlands

Besides the above legally protected lands which would be restricted from development either on the basis of national policy or avoidance on the part

of the utility industry, certain types of environmental restrictions might be imposed as well. For this study, one such environmental constraint was applied -- namely, the location of major wetlands. It is the policy of the Water Resources Council to ensure the protection of wetlands from adverse impacts and degradation [3].

No uniform nationwide data base exists regarding the location of major wetlands. After consideration of several approaches to defining the extent of wetlands in an efficient manner, a source was found to satisfy the needs of this study. The 1:2,000,000 scale sectional sheets of the National Atlas [2] were used to outline the extent of major wetlands. At this scale, only major wetlands can be shown. A comparison of these source data with more detailed map data shows that some of the wetland boundaries have been generalized and most wetlands less than 60 square miles were probably not shown on the sectional sheets.

The locations of both protected lands and wetlands were digitized into separate map files. Each of the 15 different types of protected lands was given a unique identifying code to allow individual consideration of each type of protected land. The two map files were added together to produce a map file called restricted lands (Figure F1 in Appendix F). The restricted lands file was later added to the individual environmental issue map files as well as the environmental suitability map file to produce maps showing the location of restricted lands, and conversely, the net availability of land.

4.3.4 Seismic Hardening

There are generally three major factors to be considered in the seismic evaluation of a nuclear power plant site:

1. Fault Rupture Hazard -- primarily a siting problem;
2. Dynamic Soil Stability (liquefaction) -- both a siting and a design problem; and
3. Strong Ground Motion (vibratory) -- both a siting and design issue.

Siting requirements are specified by the NRC [4] and the evaluation of a site (for design purposes) is based on the additional cost imposed by the site-related conditions. Although a detailed site qualifications study would require the careful consideration of all three factors, their evaluation generally requires effort far beyond the scope of this study. However, after careful consideration of their overall impact, a methodology was developed for a coarse screening process which reflects the overall impact of these factors. The data necessary to evaluate the potential problem from the standpoints of rupture hazard and dynamic soil stability were not uniformly available throughout the United States. For this reason, seismic hardening was evaluated solely on the basis of vibratory ground motion.

Strong ground motion criteria are determined by the postulated Safe Shutdown Earthquake (SSE) which is the largest possible event on the controlling seismogenic feature, which could be a capable fault (not necessarily the closest one) or a tectonic province. The SSE is determined on the basis of historical earthquake data (seismicity) and detailed investigation of the length and capability of nearby faults, according to procedures specified by the NRC [5]. The plant must be able to survive such an earthquake in a manner which will not result in the release of radioactivity in excess of stated limits. An additional design requirement is imposed by the Operating Basis Earthquake (OBE) which is commonly defined as having a peak acceleration equal to 1/2 that of the SSE. The plant must be designed so that it can continue to operate during and after an OBE: alternatively, none of the structural or mechanical components may be stressed beyond their elastic limit by the OBE.

While the detailed investigations required for the determination of the SSE for each 5 km by 5 km grid cell were clearly beyond the scope of this study, it was possible using available data to probabilistically evaluate the relative severity of the strong ground motion hazard in the study area and consider costs of seismic hardening. This was accomplished using probabilistic studies of seismic risk prepared by Algermissen and Perkins [6] and the Applied

Technology Council (ATC) [7] and supplemented with information from a U.S. Geological Survey professional paper [8]. The ATC map represents an adaptation of a comprehensive analysis by Algermissen and Perkins. The map shows accelerations in bedrock expressed as a fraction of gravity. The combination of these three sources resulted in the seismic acceleration source data map illustrated in Figure F2, Appendix F.

The map shows the horizontal acceleration (expressed as a fraction of gravity) in rock with a 90 percent probability of not being exceeded in 50 years. According to Algermissen and Perkins:

"Certain facilities such as nuclear power plants may require design adequate for accelerations with exceedance probability no larger than 0.5 percent in 50 years. For structures for which very low exceedance probabilities are appropriate, it is clear that this source map indicates only a relative idea of the hazards -- the design motions will be high for much smaller exceedance probabilities. In those regions where seismicity is lower than in California, the accelerations shown on this map vary with return period according to the very approximate rule: the level of motion doubles as the return period increases by 5 (exceedance probability decreases by 5)."

This rule was used to modify the values on the source data map. The exceedance probability was decreased by a factor of 5 -- from 10 percent to 2 percent -- and the acceleration values were doubled. Another iteration of this process decreased the exceedance probability from 2 to 0.4 percent and again doubled the acceleration values. The new values were then considered to be four times the values expressed in Figure F2. Thus, the data in the modified map file became consistent with the notion of using a 0.5 percent exceedance probability for nuclear power plants (as suggested by Algermissen and Perkins).

The seismic risk source data file was further adapted by interpolating between the contour levels to develop a more continuous distribution of seismic risk (horizontal acceleration). The continuous distribution was desirable from a siting standpoint,

so that sites falling on either side of a dividing contour would not appear to have greatly differing seismic requirements. (The contours of the source map do not generally have any geological significance which would warrant such sharp distinctions.) It is still recognized that the absolute resolution of the source data map is probably no more precise than the contour intervals given. However, the relative ranking of areas for reactor sites is probably representable to the finer resolution implied by the interpolation.

The general impact of seismic design requirements is assumed to be proportional to the specific cost of the additional design and construction features required to satisfy the seismic design requirements. In NUREG/CR-1508 [9], seismic hardening costs were calculated and shown on a graph relating the Safe Shutdown Earthquake expressed as a fraction of gravity to the estimated cost differential in millions of dollars. The cost curve used in this study is shown in Figure 4-2.

The map shown in Figure F2, Appendix F, indicates that the lowest acceleration contour is equal to 0.05g. Remembering that the exceedance probability was twice decreased by a factor of 5 (thereby twice doubling the ground motion), the lowest acceleration contour may now be considered equivalent to 0.2g. By applying Stevenson's cost information to the modified probabilistic seismic acceleration information, a cost surface that shows the additional cost of seismic hardening was generated.

Using the curve shown in Figure 4-2, acceleration values between 0.2g and 0.6g (0.05 and 0.15 on the source map) were assigned costs ranging from \$23.7 million to \$55.5 million. Acceleration values of less than 0.2g were assigned a cost of \$23.7 million (the same as for 0.2g). This was because nuclear power plants in the U.S. are designed for an SSE of 0.2g, although it may be possible to build them more cheaply. For acceleration values greater than 0.6g, it was felt that there is no reasonable way to accurately estimate the increased costs of seismic hardening. Rather than assign a cost, they were labeled "inestimably high".

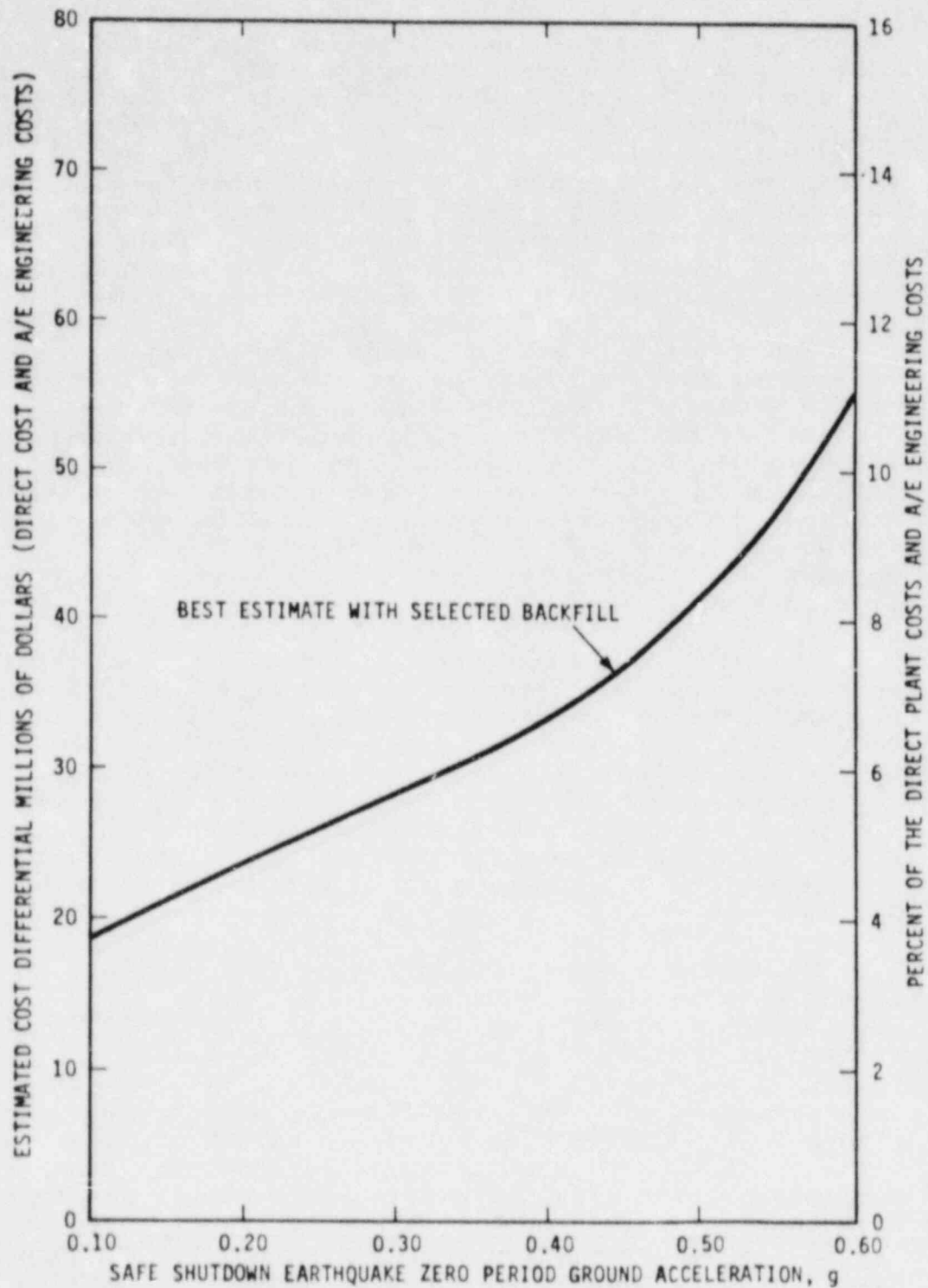


Figure 4-2. Cost Increase As A Function Of Seismic Load for Nominal 1100-MWe Nuclear Power Plant (1977 Dollars)

The costs derived from Figure 4-2 (1977 dollars) were next converted to 1980 dollars yielding a low of \$31.5 million and a high of \$73.9 million. To calculate the cost of seismic hardening that was considered as "additional", the design-basis value of \$31.5 million was subtracted from all the costs. This resulted in a range of costs of 0.0 to \$42.4 million. The graphic display of seismic hardening cost is shown in Figure F3, Appendix F.

4.3.5 Site Preparation

An increase in slope or ruggedness of terrain translates directly into increased cost for construction. This includes the difficulty that may be encountered in excavation for foundations, construction of access roads where low grades are required (due to the transport of large components such as the turbine or pressure vessel), and finally, measures that must be taken to mitigate environmental disturbances such as control of run-off and erosion from cut slopes.

To evaluate the impact of topographic character on site preparation cost over a large regional area, a general index that indicates both the steepness of slopes and the areal extent of such slopes was sought. Such data was found in a paper by E. H. Hammond [10] and his map which was adapted and found in the National Atlas [2]. Regions on the map are characterized by the percentage of their area which is classified with a topographical gradient of less than 8 percent slope (gently sloping). The 8 percent slope is not a critical threshold value for land utilization. It does, however, indicate a value beyond which movement of vehicles becomes impeded, and in general, construction and operation becomes more difficult.

The smallest region delimited and given a classification has an area of about 800 square miles. Smaller areas are omitted or absorbed into the adjacent region that they most resemble. With this level of resolution, it is possible that sites suitable for building a nuclear power plant exist within the area characterized by even the highest proportion of rugged terrain. However, at this regional level of analysis, these special conditions are not practically observed. Because not only site ruggedness but the ruggedness of the access route

for placement of heavy components affects the construction costs, the analysis of site preparation costs is based solely on the general indication of topographic character, as defined by the data. Figure F4, Appendix F, is a map showing the source data with grey tones implying preparation costs. Four terrain classifications are shown: regions with less than 20%, 20 to 50%, 50 to 80%, and greater than 80% gently sloping (less than 8% slope).

4.3.6 Water Availability

Cooling system cost has become a major component of total power plant cost. Several factors are involved in determining cooling system cost: the type of cooling system -- mechanical draft wet towers, natural draft wet towers, cooling ponds, or once through cooling; climatic temperature distributions; existing priorities for use of available water; and restrictions such as wild and scenic rivers. While a detailed analysis of these factors is beyond the scope of this study, a methodology was developed to present a general picture of water availability and the cost involved in its use. Sources of both surface water and groundwater were mapped and costs were determined for each. The two map files were then overlaid, and a map was produced showing the least cost of available water.

4.3.6.1 Surface Water

Hydrological implications of water consumption by nuclear power plants have been discussed by Giusti and Meyer [11]. Many existing power plants are located on sites next to streams and draw their water directly from those streams without provisions for significant storage. In siting plants along rivers one must consider the periods of low flow when the impact on the water resources of total water consumed in the cooling process is at a maximum. This consideration is especially significant for plants that do not use cooling ponds with a large amount of storage capacity. In light of this, it is important to have reliable estimates of the low flow of streams from which plants can draw cooling water. According to Giusti and Meyer there are several reasons for estimating these flows:

1. Safety -- the regulatory staff of the U.S. Atomic Energy Commission (1972) in reference to a safety analysis report for nuclear power plants states:
"Estimate the probable minimum flow rate resulting from the most severe drought considered reasonably possible in the region as such conditions may affect the ability of the ultimate heat sink to perform adequately.";
2. Standards -- most states have issued standards regarding the maximum permissible mineral concentration in surface water to be used for cooling. As is well known, this concentration is at a maximum at a low flow period because the flow consists of groundwater discharge which is normally more concentrated mineralogically than surface water. Additional concentration of the stream flow mineral content is brought about by transpiration which is also at a maximum during low flow periods;
3. Ecology -- maximum ecological impact on fresh water biota can occur on some streams during low flow periods if the mineral concentration exceeds certain limits or if the flow is abruptly reduced by withdrawal at power plants. Furthermore, the withdrawal entails loss of biota by physical entrainment on the intake screens or by physical injury on passage through the water pumps; and
4. Plant Operation -- the conditions described above may be such as to force the shutdown of the plant, with contingent costs and loss of revenue to plant operators and loss of service to consumers. While this may be considered an acceptable operational rule under exceptional circumstances, say once in 10 years, it becomes a serious problem of misdesign when recurring more often, say once every year.

Stankowski, Limerinos, and Euell [12] have examined the low water flow in the United States to provide information regarding potential sources of cooling

water. They have prepared a map which identifies those streams for which the average 7-day low flow with a recurrence interval of 10 years is at least 300 cubic feet per second (cfs). (The 7-day, 10-year low flow or 7Q10, is the average low flow that occurs over 7 consecutive days with a probable recurrence of 10 years.) Their map shows those stream reaches that: (1) have a 7Q10 of at least 300 cfs, or (2) could furnish a sustained flow of at least 300 cfs if storage were provided. For their study, 300 cfs was selected as the needed flow in the stream on the assumption that many states will not permit more than 10 percent of the dependable flow to be withdrawn for a consumption use. Ten percent of 300 cfs equals 30 cfs which is the amount of water that might be considered necessary to cool a 1,000 MWe nuclear power plant if cooling towers, sprays, or ponds are used. The requirement of 30 cfs for cooling is in agreement with the information produced by Giusti and Meyer [11]. The Stankowski, et al., map was digitized and used as a source map to show surface water availability.

To extend the utility of surface water information, the map file showing surface water availability was converted into a map showing surface water cost. First, an estimate was made of the dollar per mile pumping cost to move surface water. These costs were estimated for each of the four terrain types characterized for site preparation (Section 4.3.5). Both an initial capital cost and a 30-year operating and maintenance cost were estimated. In addition to the pumping cost, a penalty cost was added for those streams that required the use of reservoirs in order to sustain a 7Q10 of 300 cfs. Based on this information, a computer model was used to calculate, for each cell, the cost of obtaining surface water as a function of pumping costs over a variety of terrain and the potential use of a reservoir. The model determined the least of the cost alternatives for supplying surface water to a cell. The cost information was mapped and is shown in Figure F5, Appendix F. There are eight equal interval levels between zero and \$300 million. Costs above \$300 million were grouped together -- amounting to about 10 percent of the study area. This grouping at the high cost end allows regional differences in the more reasonable range of costs to be displayed.

4.3.6.2 Groundwater Availability

Groundwater is an important source of cooling water in many parts of the country. Characteristics of groundwater can vary quite dramatically within a small region. Despite this, an attempt was made to locate a source of information that would satisfy the broad scale requirements of this study. Using the USGS Water Supply Paper 1800 [13], and supplementing this with such maps as the Hydrologic Investigations Atlas [14], Tectonic Map of North America [15], and Shaded Relief of U.S. [16], major regions and subregions of the country were mapped as source data. Although variability exists within any one of the regions or sub-regions, regions do show differences regarding their characteristics of quality, quantity, depth to water, and required well field size.

Based on these characteristics, cost information was applied to the map data. Both capital costs and 30-year operating and maintenance costs were calculated for each of the delimited areas on the basis of dollars per well. To obtain the equivalent of 30 cfs from any of the generalized aquifers, it would be necessary to sink several wells. The required number of wells was calculated by dividing 30 cfs by the expected yield per well of the given aquifer. Multiplying this number of wells by the cost per well resulted in the cost associated with bringing 30 cfs to the surface from any of the generalized aquifers. It was observed that several of the generalized aquifer areas require well fields which are too large for practical use. For these areas, groundwater was considered to be unavailable in a practical sense. For reasonably sized well field areas, the cost of collecting the water from numerous wells and bringing it to a single point was estimated. For each of the groundwater regions, the two costs -- that of bringing the water to the surface, and that of collecting the water from a well field, were added together. The cost data were then mapped as is shown in Figure F6, Appendix F.

4.3.6.3 Combined Water Costs

Using the cost information for both surface water and groundwater, a map file was created which indicated

the cost of obtaining cooling water using the least expensive alternative. To do this, the two map files -- surface water costs and groundwater costs, were compared on a cell-by-cell basis. For every cell, the lowest cost value was saved and placed into another map file. This was called "combined water cost" and the map is shown in Figure F7, Appendix F.

4.4 Environmental Suitability Analysis

In order to evaluate the impact of demographic criteria on land availability it was necessary to first establish a base of available land. This base was constructed from the protected area and environmental consideration data bases. The environmental factors were combined by dividing utility functions for each factor, and then summing the utility values within each cell. The protected areas were then overlaid on this data.

4.4.1 Individual Site Availability Issue Assessments (Utility Functions)

To evaluate the suitability of each potential site area, each of the siting issues was first evaluated independently. This evaluation was accomplished by defining a utility function for each issue such that the characteristics of a specific site area could be translated into a value on a defined suitability scale. This was a numeric scale ranging from 1 to 9, where 1 was the lowest level of suitability and 9 was the highest.

4.4.1.1 Seismic Hardening Cost Utility Function

The issue of seismic hardening was assigned a utility function on the basis of additional hardening costs as discussed in Section 4.3.4. Table 4-1 shows the data categories of seismic hardening costs and their corresponding utility value.

A map of the seismic hardening utility function was produced and is shown in Figure F3, Appendix F. (This is the same map used to show the cost of seismic hardening.)

TABLE 4-1

SEISMIC HARDENING UTILITY FUNCTION

<u>Cost in Millions of 1980 Dollars</u>	<u>Utility Value</u>
0.0 to 6.1	8 (high suitability)
6.1 to 12.1	7
12.1 to 18.2	6
18.2 to 24.1	5
24.1 to 30.3	4
30.3 to 36.4	3
36.4 to 42.4	2
No reasonable estimate	1 (low suitability)

4.4.1.2 Site Preparation Utility Function

Actual dollar costs associated with site preparation could not be located as source data. However, discussions with authorities in the construction of nuclear power plants as to how the topographic character of the landscape might affect the site preparation costs have allowed for the assignment of the utility values to terrain classifications which were discussed in Section 4.3.5. These are shown in Table 4-2.

A map of the site preparation utility function was created and is shown in Figure F4, Appendix F. (This is the same map used to show the site preparation source data.)

TABLE 4-2

SITE PREPARATION UTILITY FUNCTION

<u>Topographic Character (percent of area that is gently sloping*)</u>	<u>Utility Value</u>
>80 percent	8 (high suitability)
50 to 80 percent	5
20 to 50 percent	2
< 20 percent	1 (low suitability)

*Gently sloping means 8 percent slope.

4.4.1.3 Water Availability Utility Function

Utility values have also been assigned to data representing the cost of obtaining cooling water. Based on this cost information (described in Section 4.3.6), costs in excess of \$300 million were grouped together and assigned the lowest utility value. For costs less than \$300 million utility values were assigned on the basis of 8 equal intervals as shown in Table 4-3.

TABLE 4-3

WATER AVAILABILITY UTILITY FUNCTION

Combined Water Cost

<u>(in millions of 1980 dollars)</u>	<u>Utility Value</u>
0 to 37.5	9 (high suitability)
37.5 to 75.0	8
75.0 to 112.5	7
112.5 to 150.0	6
150.0 to 187.5	5
187.5 to 225.0	4
225.0 to 262.5	3
262.5 to 300.0	2
>300.0	1 (low suitability)

A map was prepared showing the water availability utility function and is shown in Figure F7, Appendix F. (This is the same map used to show the combined water cost.)

4.4.2 Site Availability Issue Overlay

Using the utility functions, each issue map was translated into a partial suitability map where each potential site area was represented by a utility value. These individual suitability maps are represented in Figures F3, F4 and F7. They are considered partial suitability maps because each includes only one siting issue. They were combined into a composite suitability map by adding the individual map files together. It was felt that the reconnaissance nature of this study, as well as the broad scale representation of environmental data, did not justify a more sophisticated manipulation of the files. For this reason, the three maps were overlaid -- each with an equal importance weighting.

The addition of the three utility value map files resulted in a map file with values ranging from 4 through 25 -- each value having a different frequency of occurrence. Maintaining the relationship that high values represented the most suitable land, the distribution of the composited utility values was divided into five intervals. The intervals were selected to include equal land areas. This resulted in five categories or levels of environmental suitability -- each level representing 20 percent of the data base. The restricted lands file was then added to the composite utility value file. A color-coded version of a map produced from this combined file was supplied to NRC.

4.4.3 Environmental Statistics

Analysis of the impact of various siting criteria on land availability was accomplished in two ways: creation of maps to visually show these impacts and production of statistics to quantify the impacts. The maps concerning environmental factors have been presented elsewhere in this section. To quantify the impacts of various siting criteria, tables were prepared which used the data files created during the visual or map analysis. Statistics regarding the amount of area in each data category were computed for each of the 48 states.

For each of the three environmental issues -- seismic hardening costs, site preparation costs, and water availability costs -- a table was prepared that shows the amount of land in each of the categories that was represented by a utility value. Two additional tables were produced: one for surface water cost and one showing the five different levels of composite environmental suitability. These statistics are shown in Tables F1.1 through F1.5, Appendix F. The numbers in each column indicate the amount of land in the specified category. The area is shown in square miles as well as percent of the total state area.

4.5 Demographic Analysis

As discussed in Section 4.2, three issues were defined as relevant to population criteria - stand-off zones, population density, and angular distribution. Stand-off zones are restrictions on distances from urban centers to nuclear plant sites. Population density is a measure of the persons per square mile within a specified (circular) area surrounding a site. The population density calculations were mapped as single data files or in combination with other annular densities to produce composite population criteria maps. Angular distribution restrictions are limitations on the permissible population within one or more 22 1/2° sectors surrounding a site.

4.5.1 Stand-off Zones

To study the impact of restrictions imposed by distance from urban centers, stand-off zone maps were prepared. As discussed in Section 4.3.1, populations and locations were provided for urban centers of a variety of sizes. The location of these urban centers was indicated by a single latitude/longitude coordinate which was converted to a Y and X coordinate corresponding to grid cells on the Albers base map. Urban centers were grouped according to their size: greater than 25,000, 100,000, 200,000, 250,000, 500,000 and 1,000,000 people. For each grid cell in the study area, its distance from the nearest urban center of a particular size was computed. This resulted in six separate data files. These files were converted into maps by specifying a threshold distance at which a cell would be considered either suitable or unsuitable for siting a nuclear plant. Based on the above data, thirteen such stand-off maps were produced. The maps produced are indicated in Table 4-4 and presented in Figures F8.1 through F8.13, Appendix F. The maps illustrating stand-off zones from the three largest cities were created only for the northeastern U.S.

Maps of stand-off zones are quite self-explanatory. There is a direct relationship between the stand-off distance and the amount of area that is constrained by the specified criteria.

TABLE 4-4
STAND-OFF ZONES

<u>Size of Urban Center</u>	<u>Mapped Stand-Off Distance (in miles)</u>
25,000	5, 10
100,000	10, 15, 25
200,000	25, 30, 40, 50, 100
250,000	12.5
500,000	18
1,000,000	25

An example of these maps is shown in Figure 4-3.

4.5.2 Population Density

A wide variety of population distribution criteria based on density surrounding a prospective site were studied for their impact on land availability. Densities were calculated for both circular areas and annular areas. As described in Section 6.3.1, population source data was identified by a latitude and longitude coordinate system. These coordinates were converted into the Y and X coordinates compatible with the Albers grid base map. This raw data were then converted into a set of map files giving the population density of an area a given radius centered on each cell. Maps of varying thresholds were produced from these files. The matrix shown in Figure 4-4 indicates all of the map files that were produced regarding population density. An "X" in a box means that the map files were produced for both the total US and the northeastern window. An "NE" in a box means that the map file was produced only for the northeast. An example of these maps is shown in Figure 4-5. Maps representative of the variety of population densities are shown in Figures F9.1 through F9.26, Appendix F.

An understanding of the spatial relationships produced by various criteria can be gained by comparing some of the maps. Figure F9.5 shows the areas constrained by a density threshold of 100 people per square mile in the 0-5 mile circle. Figure F9.8, concerning the same circle employs a density threshold of 500 persons per square mile. It is obvious that

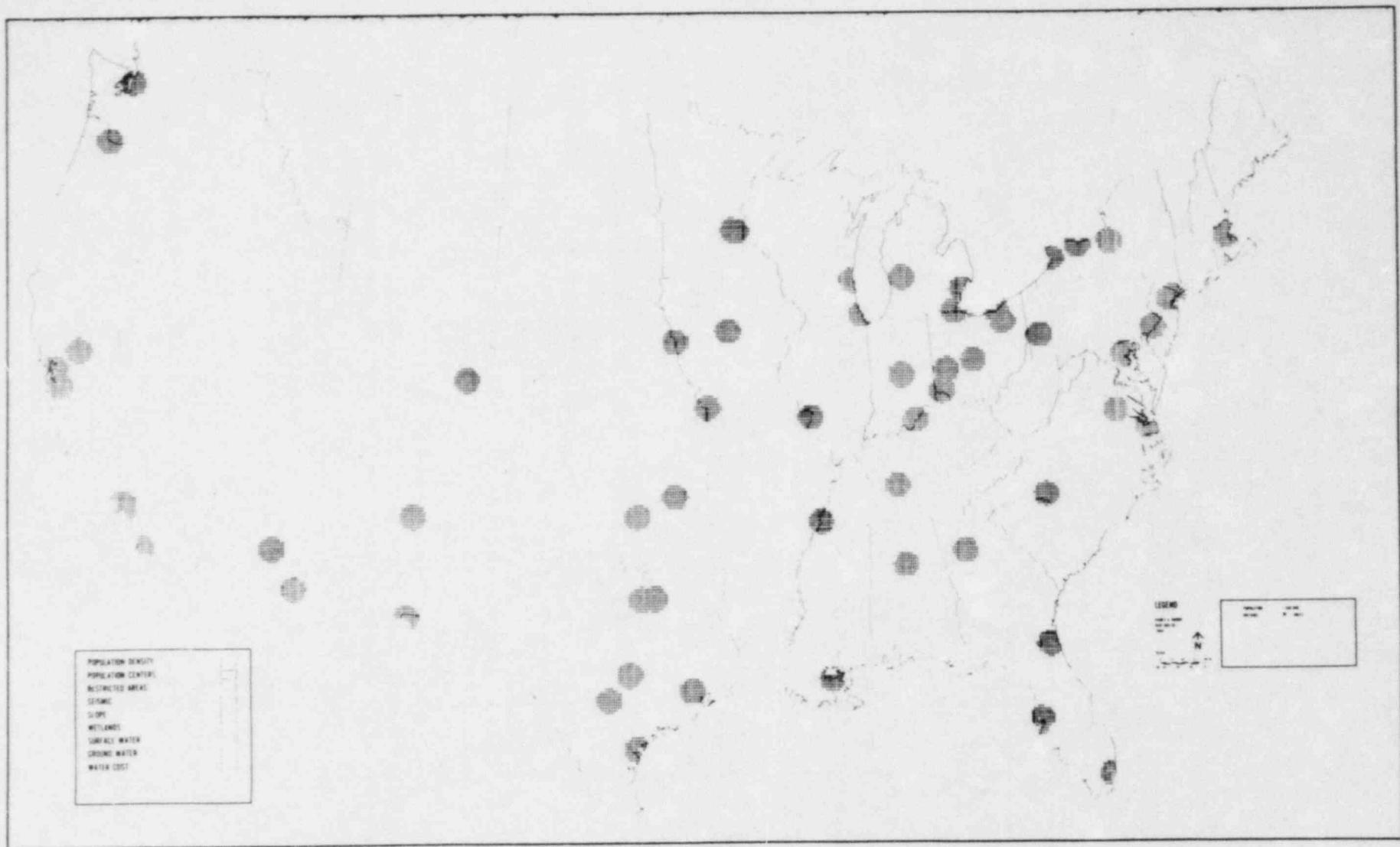


Figure 4-3. Example of Standoff Zone Maps.

ANNULUS RADIUS IN MILES	DENSITY PEOPLE/SQUARE MILE										
	>100	>150	>200	>250	>350	>400	>500	>750	>800	>1000	
0-2	X			X			ME	ME			
0-5	X		X		X		X				
0-10	X		X		X		X				
0-20			X								
0-30							X			X	
5-10		X			X		F				
5-20									X		
10-20						X	X			X	
20-30							X			X	
30-50							X			X	

Figure 4-4. Annular Population Density Data Files



Figure 4-5. Example of Annular Population Density Data Maps.

every area constrained in Figure F9.8 is also constrained in Figure F9.5. If the size of the annulus remains constant, the area constrained using a higher density threshold is always completely contained within the area constrained by a lower threshold. In addition, the use of a lower density threshold as in Figure F9.5, constrains a much greater portion of the suburban and rural land areas.

Spatial differences are also noted through a comparison of circle size while maintaining a constant density threshold. For example, compare Figure F9.8, which shows the areas constrained by a 500 people per square mile density threshold within the 0-5 mile circle, with Figure F9.14 which applies the same threshold to the 0-30 mile circle. Use of the larger radius tends to constrain only the urban and some suburban areas of major cities. None of the rural or smaller urban areas are constrained and the impacts look similar to those which result from stand-off zone criteria.

Another interesting spatial effect of the demographic criteria can be seen on any of the maps in which the annulus is defined using an inner radius greater than zero. In these cases, the annulus surrounding a prospective site is shaped like a ring rather than a circle and the effect is that the shape of some of the constrained areas is also that of a ring. The occurrence of this type of pattern depends upon the specified density threshold in conjunction with the limits of the annulus and the population data itself. For example, Figure F9.23 indicates the amount of land constrained if a criterion of 500 people per square mile in the 20-30 mile annulus were applied. Note that in the St. Louis area the land surrounding the city would be constrained -- but not the land comprising the city. St. Louis' land area is small enough so that a relatively small population is located between 20 and 30 miles of the city center, and yet the city population is large enough to cause the density threshold to be exceeded in the surrounding areas. Chicago, on the other hand, occupies an area large enough so that grid cells at the city center are within 20 to 30 miles of significant population and the pattern of constrained land is solid.

A comparison of the St. Louis area between Figure F9.23 and Figure F9.21, which employs the same density threshold within the 10 to 20 mile annulus indicates not only the absence of a ring structure but also a shrinking of the extent to which land is constrained using the smaller annulus. The pattern of the area constrained near Chicago remains solid in both figures; however, both the extent and amount of land increase with increasing annular radii. Thus, if the density threshold remains constant, the extent from the central city of the criterion's effect increases with increasing annular radius. However, the total amount of land constrained may not increase accordingly due to the possible elimination from constraint of the central city.

4.5.3 Composite Population Densities

When using a criterion of the form of less than 500 people per square mile from 2 to 30 miles, it is possible for a cell to satisfy that criterion, while it doesn't satisfy a 500 people per square mile criterion out to only 15 miles. This occurs when there is a dense population pocket surrounded by low density areas. In order to pinpoint areas for which this occurs, a new set of criteria were developed which restricted population to a given density for all radii from an inner radius to an outer radius. Thus, for the example of 500 people per square mile from 2 to 30 miles, the new criterion is satisfied only if the population density is less than 500 people per square mile from 2 to R miles, where R takes every value from 2 to 30.

Evaluating population density for every radius from the inner radius to the outer radius is impractical in practice, so an approximation is used.

Using the example of mapping any cells that exceed the 500 persons per square mile threshold for the 2-30 mile annulus, density calculations were made for 6 portions of the 2-30 mile annulus and were then composited. First, any cell that exceeded the 500 persons per square mile threshold within the 2-3 mile annulus was recorded. Next, unsuitable cells in the 2-4 mile annulus were recorded and unsuitable cells

in the 2-5 mile annulus were recorded. This process was repeated for the 2-10 mile annulus, 2-20 mile annulus, and the large 2-30 mile annulus. These 6 individual files were then added together, creating a file in which a cell that was shown to be unsuitable in any of the 6 was also considered unsuitable for the 2-30 mile composite annulus. In this manner, data files were created for the 2-30 mile composite annulus for the following densities.

250 persons/square mile
500 persons/square mile
750 persons/square mile
1,000 persons/square mile
1,500 persons/square mile

Example maps for the northeast are shown in Figures F10.1 thru F10.4, Appendix F.

Besides creating a composite map file for a particular annulus (such as 2-30 miles) and a particular density (such as 500 persons per square mile), another type of composite was created. This consisted of two separate annuli -- each with its own given population density threshold. For example, as discussed above, 6 individual data files were added together to create the 2-30 mile composite annulus. Now, a different annulus with a different population density threshold was added to the 2-30 mile composite annulus. Two maps were created in this manner and are shown in Figures F11 and F12, Appendix F. Each map shows cells that are considered unsuitable for the 2-30 mile composite annulus (with density of 500 persons per square mile) as well as for the 0-2 mile annulus for population densities of either 100 persons per square mile or 250 persons per square mile. In addition to these two mapped data files, other complex composite files were created. Some of these were used for statistical analyses in combination with the environmental criteria. (These statistics are discussed in Section 4.6). The six complex composite data files which were created are indicated in Table 4-5. The numbers in the columns underneath the two annuli represent population density figures (persons/mile²).

TABLE 4-5

COMPLEX COMPOSITE POPULATION DENSITIES

<u>0-2 Miles</u>	<u>2-30 Miles (Composite)</u>
(1) 100	250
(2) 100	500
(3) 250	500
(4) 250	750
(5) 500	750
(6) 500	1500

4.5.4 Sector Population Density

To this point in the chapter, any potential demographic criteria addressing population density were analyzed using what might be termed a uniform density distribution. Criteria were stated in terms of the number of persons that would be allowed in an area of a given size -- that is, population density -- and the shape of the area was always circular. Using a circular area allowed relatively dense concentrations of population to exist provided that the total number of people within the circle did not exceed a stated limit.

Results of reactor accident consequence calculations indicate that certain risk characteristics depend strongly on the maximum number of persons within any given direction sector (see Section 2.7.4). Therefore, criteria regarding the maximum allowable population within sectors in addition to total population surrounding a site were considered. The impact on land availability was examined for alternative sector criteria and compared to the impact of uniform density criteria.

Sector criteria were stated in terms of allowing up to a fraction of the allowed number of people to be located in any sector of a particular width. For example, a sector criteria might be stated: no more than 1/6 of the people allowed by a uniform density of 500 persons per square mile can be located in any 45 degree sector at distances within 3 miles of a site.

The impact of sector criteria was investigated with regard to several variables. The parameters were:

- o Distance: Radii of 2, 5, 10, 20, and 30 miles
- o Sector width: 22.5, 45.0, 90.0 degrees, and 360 degrees (for uniform density)
- o Fraction: 1/16, 1/8, 1/4, 1/3, and 1/2 the population allowed by uniform density
- o Density: 250, 500, 750, and 1500 persons per square mile

Population counts were determined within 2, 5, 10, 20, and 30 miles of potential sites (grid cells) and within sector widths of 22.5, 45.0, and 90.0 degrees. The maximum number of persons found in a sector of a stated width and for a particular radius was recorded. For example, investigating a circle of radius 10 miles and using a sector width of 22.5 degrees, the circle was divided into 16 sectors. The number of people was determined within each sector and the maximum of the 16 counts was recorded. This procedure of determining the maximum count was undertaken 15 times -- once for every combination of sector width (3) and radius (5).

Alternative criteria were then applied to the count data on the basis of allowing a certain fraction of the total number of people allowed within the circle to be located in any sector. The total number of people allowed in a circle is dependent upon the radius (for area) and the density that is allowed. For this sector analysis, the previously established densities were analyzed -- 250, 500, 750, and 1500 persons per square mile and five radii were used -- 2, 5, 10, 20, and 30 miles. For 0-2 miles, only one density was used as a part of every criteria -- namely, 250 persons per square mile. To calculate the allowable population threshold out to 5, 10, 20, and 30 miles for each of the densities, the area from 2 miles to r miles (radius) was multiplied by the density and the product added to the threshold for 0-2 miles with its 250 persons per square mile density. For example, at 20 miles using density 750 persons per square mile, the threshold equals:

$$\begin{aligned}
& (\text{Area of 0-2}) \times 250 + (\text{Area of 2-20}) \times 750 \\
& = (12.57 \times 250) + (\text{Area of 2-20}) \times 750 \\
& = (3142 + 933075) \\
& = 936,217 \text{ people}
\end{aligned}$$

Using only one density (250 persons per square mile) for 0-2 miles and four densities for the other four distances resulted in 17 separate thresholds. These thresholds were used not only for uniform density criteria analyses but also for calculating the fractional thresholds applied to sector population distributions. Thus, if a criterion was stated that no more than 1/4 of the people allowed by a uniform density of 750 persons per square mile within 20 miles would be allowed in a sector, the threshold would be $936,217 \times 1/4 = 234,054$ people.

Being consistent with previously computed impacts, the impacts for sector criteria for any particular density or fraction were composited to 30 miles. That is, sites exceeding a threshold at 2 miles were recorded and saved into a map file. Sites exceeding a threshold at 5 miles were also recorded and stored into a map file, as were all sites for 10, 20, and 30 miles. Finally, all five map files were merged resulting in a file that showed sites constrained by any one or more of the thresholds. Spatially, it was found that any criteria at smaller radii tended to eliminate sites in rural areas as well as in cities but only out to their edge. Criteria applied at larger radii tended to eliminate cities and large areas around their edges (similar to a "standoff" criteria) but allow local population concentrations in rural areas. By compositing criteria for all five radii, both urban and rural population concentrations were evaluated for their impact on availability of potential nuclear sites. Additionally, it was found that the effects of sector criteria occurred in the same areas as affected by annular density criteria.

Sector criteria were of interest in regard to their impact on land availability above and beyond that already affected by uniform density criteria. To depict and quantify this information, tables were created to show the amount of land available for siting

in each state if a particular sector criterion was established. The information is shown in Tables F2.1 through F2.24, Appendix F. Each table shows the impact of alternative fractional criteria along with the uniform density criteria on land availability. All of the fractional and uniform density criteria have been composited to 30 miles by adding the individual impacts of a criterion at 2, 5, 10, 20, and 30 miles.

Each table considers a unique combination of allowable annulus population density and sector width. The four population densities and three sector widths resulted in 12 combinations. Twenty-four tables were created as each of the 12 combinations was tabulated using two different formats. Tables F2.1 through F2.12 are formatted such that the numbers in the columns represent the amount of land that is uniquely constrained by the specified criteria.

The columns are arranged so that total magnitude of constrained land decreases from left to right. As an example, Table F2.1 indicates the impacts of alternative fractional criteria applied to 22.5 degree sectors using a density threshold of 250 people per square mile for both the 0-2 mile and 2-30 mile annulus. The leftmost column "Available Land," shows the amount of land available for siting if the criterion stated in the adjacent column is applied; that is, no more than 1/16 of the population allowed in the annulus at a density of 250 people per square mile can be located in any 22.5 degree sector of the annulus. The criterion stated in the second column of these 12 tables always represents the most constraining fractional criterion.

The rightmost column, "Restricted Lands," shows the amount of land that is constrained because it is either legally protected or a major wetland. No demographic criteria affect these numbers.

The numbers in each of the middle columns show the amount of land that is uniquely constrained by the specified criterion which is above the total amount previously constrained by the criteria in all of the columns to the right. In Table F2.1, for example, the column labeled "Uniform Density" shows for Alabama values of 5,703 square miles or 11.0 percent of the state area. This is the area that would be constrained

by applying a uniform (annular) density criterion and it is additional to the area already constrained by restricted lands (2,075 square miles or 4.0 percent). Thus, the application of this particular uniform density criterion in Alabama would constrain a total of 7,778 square miles or 15.0 percent of the state area if no sector criteria were applied. The next column to the left, "1/2 Allowable Pop.," would add another 2,355 square miles or 4.5 percent of constraint if a sector criterion were stated that no more than 1/2 of the total population allowed by a density threshold of 250 people per square mile in both the 0-2 mile and 2-30 mile annuli could be located in any 22.5 degree sector. Similarly, using a criterion of allowing up to 1/3 of the allowable uniform density population to be located in a single sector, would constrain an additional 6,388 square miles or 12.3 percent of the land area. The total constrained land in this case would be 16,521 square miles or 31.8 percent of the state area. Conversely, 68.2 percent (100 minus 31.8) of the land would be available for siting.

To more clearly summarize the information that shows the availability of land when specific sector criteria are applied, Tables F2.13 through F2.24 were created in a different format than the previous 12 tables. On these tables, the numbers in the columns show the amount of land available for siting if the specified criterion is applied. For example, Table F2.13 indicates that 68.2 percent of the land in Alabama would be available for siting if a criterion of allowing up to 1/3 of the population (allowed by a uniform density criteria using a density threshold of 250 people per square mile in both the 0-2 mile and 2-30 mile annuli) to be located in any 22.5 degree sector. This number agrees with the one produced in the above example regarding Table F2.1. The column labeled "Uniform Density" indicates land availability when no sector criteria are applied. The column "No Pop. Criteria" shows the amount of land available when only restricted lands are considered a constraint.

4.6 Impact Analysis

Analysis of the impact of various siting criteria on land availability was accomplished in two ways: creation of maps to visually show these impacts, and production of statistics to quantify the impacts. Many

of the maps produced have already been reviewed in other sections of this chapter. All maps were produced on a transparent base enabling them to be overlaid. This capability allows creation of complex composite population criteria maps. In addition, these population criteria maps can be overlaid on the color-coded environmental suitability map.

To quantify the impacts of various siting criteria, tables were prepared which used the data files created during the visual or map analysis. For a particular subject, whether environmental or demographic, statistics regarding the amount of area impacted were computed for each of the 48 states. Fifteen tables were produced which were grouped into three different types: environmental criteria, environmental suitability levels versus selected population cases, and population criteria versus individual environmental suitability levels.

4.6.1 Environmental Statistics

For each of the three environmental issues -- seismic hardening costs, site preparation costs, and water availability costs -- a table was prepared that showed the amount of land in each of the categories that was represented by a utility value (see Section 4.4). Two additional tables were produced: one for the surface water cost, and one showing the five different levels of composite environmental suitability. As discussed earlier, these statistics are shown in Tables F1.1 through F1.5, Appendix F.

4.6.2 Impact Comparisons

The overlay of transparent maps provided a quick look at potential land availability. A map containing five levels of environmental suitability along with a sixth level showing restricted lands, when overlaid with a variety of population criteria, produces numerous groupings of data. To present these data in statistical form, a method was devised to keep each table simple enough to be understood, while retaining a large amount of information.

First, five population cases were defined on the basis of complex composite criteria. These population cases are shown in Table 4-6. The numbers in the columns underneath the 0-2 and 2-30 mile annuli represent population density figures.

TABLE 4-6

<u>Population Case</u>	<u>0-2 Miles</u>	<u>2-30 Miles (Composite)</u>
1	100	250
2	250	500
3	250	750
4	500	750
5	500	1500

Five tables were produced -- one for each population case -- which compared the environmental suitability levels to an individual population case. These statistics indicate the amount of land in each of the environmental suitability levels that is available for siting nuclear power plants if a given set of population criteria (a population case) is applied. These statistics are shown in Tables F3.1 to F3.5.

To illustrate the effect of applying different population criteria (the five population cases) on land availability in a particular environmental suitability class, five more tables were produced. In these tables, the statistics represent the amount of land available for siting nuclear power plants in a given environmental suitability class as well as the amount of land uniquely constrained by each of the five population cases. These statistics are shown in Tables F3.6 through F3.10. The columns representing population cases have been arranged such that in moving from left to right, the stringency decreases. The leftmost column of the table -- available land -- shows land that is available for the given environmental suitability class even if the most stringent population criterion (population case 1) is applied. The second column -- population case 1 -- represents an additional amount of land considered available if population case 1 were relaxed. The next column -- population case 2 -- represents the additional increment of available land if the criteria for population case 2 were also relaxed. It follows that if no population criteria were established, the amount of land available in a particular environmental suitability class would be equal to the total of the first six columns in the table; the only land considered constrained would be that by a restricted land designation.

4.7 Summary

The analytical methods used in this study were designed to explore the impact of various demographic siting criteria on the availability of land considered suitable for the siting of nuclear power plants. Maps were created so that impacts could be easily visualized and tabular statistics were prepared to allow a more rigorous analysis.

The determination of land considered suitable for siting was accomplished through a multi-objective environmental suitability analysis. The analysis was performed using factors generally related to engineering costs as well as conservation of specific resources. Because this investigation concerned the entire 48 contiguous United States and was not a site selection project, environmental factors were analyzed at a relatively general level of detail and were each considered to be of equal importance. The most suitable areas were characterized by an adequate water supply, low seismicity and gentle topography as well as an absence of protected resources. Although the map of environmental suitability (Figure F8) shows the eastern one-half of the country to be more suitable than the western, it is felt that there are numerous suitable sites available in the western portion.

Three types of population criteria were investigated: stand-off zones, annular density and sector density. The effects of stand-off zone criteria are straightforward. There is a direct relationship between the stand-off distance and the amount of land area constrained.

The analysis of annular density thresholds showed that the use of smaller radii to define the annulus resulted in constraints on sites near both large and small urban populations as well as sites near some locally dense rural areas. Larger radii tended to constrain a greater amount of area near suburban population but only around major cities; small urban and rural areas were not constrained.

Because results of reactor accident consequence calculations indicated (Section 2.7.4, Chapter 2) that certain risk characteristics depended strongly on the maximum number of persons within any given direction

sector, sector population criteria were designed. Their impacts were investigated to determine the amount of land area that would be constrained additional to that affected by annular density criteria. It was found that sector criteria affected the same areas and those adjacent to the areas affected by annular densities. Also, the area of impact responded to changes in annular radius in the same manner as for annular density criteria.

Transparent overlay maps and tabular statistics were provided to NRC for use in establishing siting criteria which would be numerically based upon population density, distribution and exclusion distance. Tabular statistics were used to quantify the impacts on a state-by-state basis. The use of transparent overlays provides a means not only to see the impacts of the generated criteria but also to create and view the effects of complex criteria by overlaying any combination of maps. Maps showing demographic criteria were also overlain onto the map of environmental suitability to visualize the potentially available suitable land. Through both the overlay procedure and a comparison of statistics, it was found that the greatest impacts of demographic criteria occur in the areas of high environmental suitability (i.e., Northeast).

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5. Socioeconomic Impacts

5.1 Introduction

Because the construction and operation of a nuclear power plant can have social and economic impacts on nearby communities, the dependence of socioeconomic impacts on site location was examined by the Battelle Human Affairs Research Centers (Battelle-HARC) under contract to Sandia National Laboratories. The Battelle-HARC study (1) developed a classification scheme for the remoteness of light water reactor (LWR) site locations; (2) calculated average growth rates for several demographic and economic variables during the period of plant construction for two groups of LWR sites of differing remoteness, (3) examined the dependence of transmission line costs on site remoteness; and (4) discussed the significance of these results in the light of previous studies of the socioeconomic impacts of rural industrialization projects, boom towns, and nuclear power plants. This chapter presents a summary of the Battelle-HARC study. Full details are reported in the final report of that study [1].

5.2 Site Remoteness

Conceptually, the degree of remoteness of a nuclear power plant site depends upon both population density (the more sparse the population the more remote the site) and proximity to major population centers (nearby cities of significant size decrease remoteness). To capture this dual dependence, two measures were developed to define the degree of site remoteness, one of population sparseness and the other of proximity to urban centers.

Sparseness was defined in terms of total population and number of communities of population 25,000 or more within 20 miles of the site. Four sparseness categories were defined as follows:

Sparseness Measure

<u>Category</u>	<u>Definition</u>
Most Sparse	1. Less than 50,000 persons and no community with more than 25,000 persons within 20 miles.
	2. From 50,000 to 74,999 persons and no community with more than 25,000 persons within 20 miles.
	3. From 75,000 to 149,999 persons or less than 75,000 persons but with at least one community with more than 25,000 persons within 20 miles.
Least Sparse	4. 150,000 or more persons within 20 miles.

Proximity was defined in terms of total population and the presence of cities with population $\geq 100,000$ within 50 miles of the site. Four proximity categories were defined as follows:

Proximity Measure

<u>Category</u>	<u>Definition</u>
Not in Close Proximity	1. No city with more than 100,000 persons and less than 400,000 persons within 50 miles.
	2. No city with more than 100,000 persons and between 400,000 and 1,499,999 persons within 50 miles.
	3. One or more large cities with more than 100,000 persons and less than 1,500,000 persons within 50 miles.
In Close Proximity	4. 1,500,000 or more persons within 50 miles.

The distance of 20 miles and a community size of 25,000 (sparseness measure) were chosen because the NRC Siting Policy Task Force [2] recommended that population densities around sites be limited out to a distance of 20 miles and because current siting practice requires that the nearest town of 25,000 persons be at least more distant than one and one-third times the distance to the outer boundary of the low population zone surrounding the plant site. The distance of 50 miles (proximity measure) was chosen because workforce commuting distances, which strongly affect the degree of population increase during construction periods and thus the magnitude of socioeconomic impacts, are usually limited to about a one-hour commute [3], or about 50 miles at current speed limits.

Table 5-1 presents the cross-classification by sparseness and proximity of 84 LWR sites in the U.S., where reactors are currently operating or under construction.

Table 5-1. Site Remoteness Matrix

		<u>Proximity</u>				
		1	2	3	4	Total
<u>Sparseness</u>	1	11	1	3	0	15
	2	3	1	4	2	10
	3	4	7	10	4	25
	4	0	0	11	23	34
	Total	18	9	28	29	84

Within this matrix remoteness decreases as one moves from cell (1,1) to cell (4,4) and sites in cells with indices that sum to the same total [e.g., cells (3,1), (2,2), and (1,3)] should be similar in degree of remoteness. 2y

summing the numbers of sites having similar degrees of remoteness, the distribution of remoteness over the 84 sites is obtained. Table 5-2 displays this distribution.

Table 5-2. Distribution of Remoteness

Group	Cell	Number of Sites
1. Most Remote Sites	(1,1)	11
2.	(2,1), (1,2)	4
3.	(3,1), (2,2), (1,3)	8
4.	(4,1), (3,2), (2,3), (1,4)	11
5.	(4,2), (3,3), (2,4)	12
6.	(4,3), (3,4)	15
7. Least Remote Sites	(4,4)	23
		<u>84</u>

Tables 5-1 and 5-2 show that, of the 84 sites, only 15 are not located within 20 miles of a town of 25,000 or within 50 miles of a city of 100,000. By contrast, 23 of the 84 sites have populations of 150,000 within 20 miles of the site and 1,500,000 within 50 miles. Thus, Tables 1 and 2 show that most current U.S. LWFs are not remotely sited.

5.3 Growth Rates

The socioeconomic impacts of large industrial projects usually depend on the size of the project workforce. Since the peak construction workforce (≥ 2000) for a nuclear power plant is substantially larger than the plant's operational staff (~ 200), the socioeconomic impacts of nuclear power plants should be largest during the plant's construction phase. A measure of the magnitude of these impacts can be obtained by calculating average growth rates for population and economic activity in the areas surrounding nuclear power plants during their preconstruction (baseline) and construction periods. Variation of impacts with remoteness can be examined by performing these calculations for two groups of sites, a non-remote group and a remote group, and comparing the results.

Time series data for population, employment (total, retail trade, and construction), payroll (total, retail

trade, and construction), and government revenues (property tax per capita) and expenditures (total, education, highway, health, and welfare) were obtained for the preconstruction and construction periods at 21 nuclear power plant sites. Cross-classification of the 21 sites, according to the sparseness and proximity measures previously defined, yields Table 5-3. Table 5-3 shows that 7 of the sites are relatively remote and the other 14 are nonremote.

Table 5-3. Cross-classification Remoteness Matrix for 7 Remote and 14 Non-Remote Sites.

		<u>Proximity</u>				Total
		1	2	3	4	
<u>Sparseness</u>	1	4	-	-	-	4
	2	1	-	-	-	1
	3	2	-	2	1	5
	4	-	-	5	6	11
	Total	7	0	7	7	21

Population data were available in census publications [4] for the years 1960, 1966, and 1970 through 1978. Employment and payroll data were obtained for the years 1959, 1962, and 1964 through 1978 from County Business Patterns [5]. Government revenue and expenditure data were collected from the County and City Data Book [6] for 1962, 1967, and 1972, and from the Census of Governments [7] for 1977.

Average yearly values of government revenues and expenditures for the preconstruction (baseline) and construction periods for the non-remote group of 14 sites and the remote group of 7 sites are presented in Table 5-4. Table 5-4 also presents the percentage

Table 5-4. Average Yearly Government Revenue and Expenditures for Remote and Non-Remote Groups*

Variable	Remote			Non-Remote		
	Baseline Period	Construction Period	Percentage Increase†	Baseline Period	Construction Period	Percentage Increase†
Property Tax Per Capita	71	88	24	112	139	24
Total Government Expenditures	7,658	12,567	64	78,582	115,478	47
Education Expenditures	3,852	6,566	70	30,274	57,159	89
Highway Expenditures	684	909	33	5,677	6,383	12
Health Expenditures	792	1,687	113	3,626	5,657	56
Public Welfare Expenditures	174	200	15	5,275	9,787	85

*Property tax per capita in dollars, expenditures in thousands of dollars.
 † $[(\text{Construction Period Value}/\text{Baseline Period Value})-1]100$.

increase of each variable for the construction period relative to the baseline period. Table 5-4 shows that the percentage increases in total government, highway, and health expenditures were greater at remote than non-remote sites, that the converse is true for education and welfare expenditures, and that the increase in per capita property tax was the same for both site groups. Therefore, because these data showed no consistent variation and because the amount of data was scant (data were available for only 4 years), average yearly growth rates were not calculated for these government variables.

The exponential growth of the variable X at a rate k per year over the time period t is given by

$$X_t = X_{t_0} e^{kt} \quad (1)$$

Average growth rates for a group of sites can be obtained by linear regression analysis after recasting equation 1 as follows, where k is the yearly average growth rate of the variable X for the site group, i is a site index, and w_i is a site specific difference term.

$$\ln X_{i,t} = \ln X_{i,t_0} + \bar{k}t + \epsilon_i \quad (2)$$

Average growth rates were calculated for both site groups for the preconstruction (baseline) and construction periods for 7 variables (population, and total, retail, and construction employment and payroll). Table 5-5 presents the results of these linear regression analyses.

Examination of Table 5-5 reveals a consistent pattern. For each of the 7 variables and for both periods (baseline and construction), growth rates are higher for the remote site group than for the non-remote group. On the average, during the baseline period growth rates at remote sites exceed those at non-remote sites by about 50 percent. During the construction period growth rates at remote sites are 2 to 3 times larger than are growth rates at non-remote sites. As would be expected, growth rates are largest for construction payroll and employment. In addition, because of the increased demand for labor, the average number of hours worked also increases and therefore payroll growth exceeds employment growth.

Table 5-5. Average Growth Rates for Population, Employment, and Payroll at Remote and Non-Remote Sites.

	Average Yearly Growth Rates (%) ^a				Construction Impacts (%) ^b		Impact Differences (%) ^c
	Preconstruction		Construction		Remote	Non-Remote	
	Remote	Non-Remote	Remote	Non-Remote			
Population	1.7 _± 0.2	1.4 _± 0.2	6.1 _± 0.8	1.6 _± 0.6	4.3 _± 1.0 ^d	0.2 _± 1.4	4.1 _± 2.4 ^d
Total Employment	5.7 _± 0.4	3.9 _± 0.2	12.2 _± 1.5	4.4 _± 0.9	7.1 _± 1.9 ^d	0.5 _± 1.1	6.5 _± 3.0 ^d
Total Payroll	8.4 _± 0.3	5.7 _± 0.3	18.9 _± 2.4	7.3 _± 1.5	10.5 _± 2.7 ^d	1.6 _± 1.8	8.9 _± 4.5 ^d
Retail Employment	5.5 _± 0.3	3.8 _± 0.3	8.8 _± 1.0	4.3 _± 0.6	3.4 _± 1.3 ^d	0.5 _± 0.9	2.8 _± 2.2 ^d
Retail Payroll	8.1 _± 0.2	5.0 _± 0.3	9.9 _± 1.0	4.5 _± 0.6	1.7 _± 1.2	-0.5 _± 0.9	2.2 _± 2.1 ^e
Construction Employment	8.3 _± 0.8	3.9 _± 0.5	33.3 _± 3.5	11.8 _± 2.2	24.9 _± 4.3 ^d	7.9 _± 2.7 ^d	17.1 _± 7.0 ^d
Construction Payroll	10.8 _± 1.0	7.2 _± 0.6	45.9 _± 5.0	17.2 _± 3.1	35.1 _± 6.0 ^d	10.0 _± 3.7 ^d	25.1 _± 9.7 ^d

- a. All values are significant at the 0.01 level by *F*-test
 b. (Construction Growth Rate) - (Preconstruction Growth Rate)
 c. (Remote Impact) - (Non-Remote Impact)
 d. Significant at the 0.01 level by *t*-test
 e. Significant at the 0.05 level by *t*-test

By subtracting baseline period growth rates from construction period growth rates, estimates of the growth rates due only to nuclear power plant construction (construction impact) are obtained. Table 5-5 shows that for the non-remote group of sites, construction impacts were significant only for construction payroll and employment. However, for the remote group of sites, impacts were significant for all variables, being largest for construction payroll (35%) and employment (25%) and substantial for total payroll (10%). Finally, the last column of Table 5-5 shows that, for all variables except retail payroll, impact differences (remote site construction impact minus non-remote site construction impact) are all statistically significant at the 0.01 level.

5.4 Transmission Line Costs

Transmission line costs are comprised of installation and operating costs. Installation costs depend on (1) the length of the right-of-way along which the lines will be strung in order to connect the power plant to the existing national power grid; (2) right-of-way acquisition costs; (3) the number and size (conductor rating) of the lines installed; and (4) installation labor costs (right-of-way preparation, construction of line towers and substations, stringing of lines). Operating costs consist principally of the cost of line losses during transmission and maintenance costs.

Transmission losses are less for shorter line lengths and larger conductors. Larger conductors cost more than smaller conductors, require a wider right-of-way (125 ft wide for 230 kV cable; 200 ft for 500 kV [8]), and are more costly to install. Despite these higher costs, EPRI projections [9] predict an increasing use of higher rated (larger) conductors through the year 2000. This agrees with the findings by Power Transmission, Inc. [10] that utilities currently prefer to minimize future transmission losses by installation of larger conductors.

Unit costs for labor (hourly wages) in suburban areas were found by an EPRI study [11] to exceed those in rural areas by about 25%. Unit costs for the acquisition of land for right-of-way are also likely to be lower in rural areas than in suburban areas. In contrast to this, total costs due to acquisition of right-of-way, purchase of materials and equipment, payment of labor, and transmission line losses all increase with increasing line length. Therefore, since remote siting would seem to require longer transmission lines, remote siting would appear to

entail higher transmission line installation and operating costs. This is not always the case, however.

Maps of the existing national transmission grid show that, except for the more remote regions of the Rocky Mountains, grid transmission lines pass through all regions (both remote and non-remote) of the U.S. [12]. Although consideration of environmental, social, and aesthetic issues as required by NEPA has tended to somewhat lengthen line right-of-ways, the factor that dominates the length of new transmission lines is the gross distance of the power plant site from the nearest leg of the national transmission grid. Because this grid runs through both remote and non-remote areas, remote siting does not necessarily mean a lengthy transmission line. Table 5-6 presents data in support of this conclusion.

Table 5-6 presents data on the conductor rating, length, and acreage of the transmission lines which connect 29 power plant sites (those with all facilities operating as of 1978) of varying remoteness to the national power grid. Examination of the right-of-way lengths, which were drawn from DOE maps [12], shows that for existing sites right-of-way lengths do not correlate with remoteness. Some remote sites are closer to the national grid than are some less remote sites. Thus, it is distance from the national transmission grid and not distance from major population centers (remoteness) that principally determines the costs of transmission line installation and operation.

5.5 Discussion

Major construction projects have large workforce requirements. In rural settings, when workforce requirements can not be met locally or by commuting from nearby cities, in-migration of workers occurs. If this in-migration is substantial, "boomtown" conditions may result and the host area may experience significant socioeconomic impacts. This scenario has been the subject of considerable study. Rural industrial development studies [13,14] have examined the impacts of industrial projects upon small, rural communities. Boomtown studies [15-18] have examined the local impacts of rapid, large-scale energy development projects, located primarily in remote farming and ranching areas of the Rocky Mountains. The impacts of nuclear power plant construction have also been examined by several previous studies [19-21].

Table 5-6. Power Transmission Line Data for 29 Operating Nuclear Sites

Remoteness Index	Total Miles of Right-of-Way	Estimated Acres of Right-of-Way	Average Kilovolts Per Mile of Line
1-1	230	4,182	345
2-1	266	4,030	230
2-1	38	800	399
3-2	52	661	156
3-2	230	4,061	301
3-2	102	1,855	345
3-2	179	2,670	206
2-4	30	545	345
2-4	151	2,655	309
3-3	118	2,675	418
3-3	85	1,370	267
3-3	5	91	345
3-3	95	1,803	316
3-3	84	1,273	230
3-3	123	2,236	337
3-4	17	309	345
3-4	124	2,255	345
3-4	24	291	115
4-3	170	3,576	423
4-3	85	1,455	304
4-3	25	358	198
4-3	67	1,218	345
4-4	409	8,291	147
4-4	60	758	134
4-4	4	61	230
4-4	104	2,545	485
4-4	90	1,636	345
4-4	217	4,561	378
4-4	29	527	345

Significant in-migration to a construction project's host area occurs only if workforce requirements can not be met locally or by commuting from nearby population centers (generally, those located within about a one-hour commute of the site [3]). Even when substantial in-migration does occur, a boomtown can be avoided, if the resulting population growth is spread over several nearby communities [22]. In general, adverse socioeconomic impacts are not observed until the rate of population growth of a single community exceeds 10 to 15 percent per year [23,24]. Under these conditions institutional breakdowns may occur in the labor and housing markets and in the provision of government services (education, health care, recreational facilities, police and fire protection) [23].

The small sizes, undiversified economies, small tax bases, homogeneous populations, and traditional life styles of rural communities tend to increase their susceptibility to socioeconomic impacts resulting from rapid population growth. Mortgage investors tend to find small, economically undiversified, rural communities unattractive investment locales. Lack of mortgage money combined with shortages of building materials and housing construction workers can produce a serious housing shortage. Because of their limited tax bases and because the project under construction generally yields little tax revenue until nearly completed, rural communities are often unable to finance the increased load of government services needed to accommodate rapid population growth. Finally, rural communities having a homogeneous population and life style may be less willing or able to welcome newcomers having different ideas, ways of doing business, and life styles and to accept the changes in personal, social, business, and institutional interactions that incorporation of the newcomers into their communities would entail [16-18,25].

The willingness of rural communities to accept change depends upon community perception of the benefits (and risks) that will accompany the changes, and upon the degree of community involvement in the decisions which determine the nature and rate of the changes. Because the construction of a large industrial or energy facility promises increased tax revenues, new jobs, more retail trade, and therefore improved government services, an end to out-migration of children and friends [14,15], and a higher standard of living [21], many rural communities welcome these projects (at least initially).

However, community resistance may develop, if the economic benefits are unevenly distributed (e.g., business men and land owners profit while the poor, the elderly, and minorities suffer), if the project is perceived to benefit principally distant cities (e.g., electric generating stations [19,25]), if project decisions affecting the community are made without community involvement, and if there are concerns about the safety of the facility (e.g., nuclear power plants [21]).

The degree to which the socioeconomic impacts, characteristic of rural industrialization and boom-towns, have occurred as the result of nuclear power plant siting was examined by gathering data about peak construction employment, number of in-migrants, and socioeconomic impacts at 12 remote nuclear power plant sites. The data, which were extracted from Environmental Impact Statements and post-licensing case studies (where available), are presented in Table 5-7. For the 12 sites listed in Table 5-7, peak construction employment was approximately 2200 (+700), or 5 percent of the surrounding population to 20 miles. For the 9 sites where in-migration data were available, peak construction in-migration (workers plus families) on an average represented only 3 percent of the surrounding population to 20 miles. Examination of the last column in Table 5-7 shows that with scattered exceptions (crowded classrooms, Yellow Creek; stressed government services, Hatch; wage inflation, St. Lucie; safety controversy, Diablo Canyon) the socioeconomic impacts at the 12 sites were largely beneficial (significantly increased tax revenues, increased retail trade). Given the modest increases in total population in the regions surrounding the sites, it is not surprising that detrimental impacts were minimal, while economic impacts were favorable.

Since socioeconomic impacts depend principally on the rate of population growth, which scales with construction workforce growth, additional data on construction workforce growth were developed for 19 non-remote construction projects including 15 nuclear power plants and for 28 remote construction projects including one nuclear power plant. The data are presented in Table 5-8, which shows that an average remote site experiences twice as much in-migration as a non-remote site.

Table 5-7. Socioeconomic Impacts at Selected Remote Sites

Site (Projected Year of Completion for Each Reactor at a Site) ¹	Utility (Total Megawatts at Site) ¹	Remoteness Index ²	Estimated Peak Construction Employment (Workers)	Total Population Within 20 Miles (1980 Projected, provided by James & Moore)	Estimated Number of Immigrants at Peak of Construction	Overall Assessment Social and Economic Impacts
YELLOW CREEK ³ 1985, 1988 (Luka, MS)	TVA 1570 MWe	(1,1) Most Sparse Least Proximate	2,600	55,430	780 workers (470 with families, 310 without fam- ilies)	Increase in students will require seventeen classrooms and teachers; classroom space is currently scarce.
GRAND GULF ⁴ 1982, 1986 (Port Gibson, MS)	Mississippi Power & Light 2,500 MWe	(1,1)	Up to 2,600	27,092	Not provided	1. More electrical power available. 2. Dramatically increases the tax base. 3. Significant direct and indirect increases in employment and income. ⁴ (p. 8-16)
SOUTH TEXAS ⁵ PROJECT 1984, 1986 (Palacios, TX)	Houston Lighting and Power Company 2,500 MWe	(1,1)	2,100	32,307	2,000 persons	Similar to Grand Gulf.
HATCH ^{6,7} 1975, 1979 (Waynesboro, GA)	Georgia Power Company 1,572 MWe	(1,1)	2,300	49,808	920 to 1,150 workers	Some growth impacts on schools, housing, and public services but not serious. No unmanageable strains on community infrastructure. Plant's economic benefits (reduced tax rate, growth and employment) were viewed very positively by host area.
WOOTLE ⁸ 1985, 1988 (Waynesboro, GA)	Georgia Power Company 2,200 MWe	(1,2)	3,800	26,170	815 workers	Construction of the proposed nuclear plant will slow, but not halt, the current trend in population migration from this rural area. For the effects of construction to be most beneficial, efforts to attract new and related commercial activity should continue. ⁸ (p. 27)
CLINTON ⁹ 1982 (Clinton, IL)	Illinois Power Company 1,900 MWe	(2,2)	1,200	47,792	418 persons (191 workers, 121 adults, 106 children)	Minimal impacts anticipated due to close proximity (approximately 60 miles) of large urban areas.
ARKANSAS ¹⁰ 1973, 1976 (Russellville, AK)	Arkansas Power and Light Company 1,748 MWe	(1,1)	973	59,322	200 persons	1. Stabilize area's construction workers. 2. Increases in direct and indirect employment and income. 3. Expansion of electric power provisions to the service area. 4. Increase in property tax payments which aided in reversal of school overcrowding and financial difficulties.
ST. LUCIE ¹¹ 1976, 1983 (Hutchinson Island, FL)	Florida Power and Light Company 1,554 MWe	(3,1)	1,847	121,542	Not provided	1. Increased tax base by approximately 35%. 2. Public construction projects in the county had to be delayed or cancelled due to inflated wage rates resulting from construction of the plant.
CRYSTAL ¹² RIVER 1977 (Crystal River, FL)	Florida Power Corporation 825 MWe	(1,1)	1,790	38,705	Not provided	1. Increased tax base. 2. 50% (85) of operating workforce relocated to Crystal River. 3. Retail sales in area increased due to relocation of non-local construction workforce.
DIABLO ¹³ CANYON 1981, 1981 (Avila Beach, CA)	Pacific Gas and Electric 2,190 MWe	(2,1)	2,470	101,151	3,308 persons ¹⁷	1. Divisiveness of entire Diablo Canyon issue among community residents (not necessarily due to workforce in-migration). Operation of facilities held up due to environmentalists' concerns regarding geologic fault at site.
PARLEY ¹⁴ 1977, 1980 (Dothan, AL)	Alabama Power Company 1,720 MWe	(3,1)	2,250 ¹⁸	93,185	1,057 workers ¹⁹	1. Increase in direct and indirect employment and income.
SURREY ¹⁵ 1972, 1973 (Gravel Neck, VA)	Virginia Electric and Power Company 1,550 MWe	(4,4) ²⁰	1,934	284,669	102 persons ¹⁶	1. Increase in tax base. 2. Increased employment, business income, tourism, traffic and land cost during construction in Surrey and Isle of Wight Counties.

Table 5-7. Footnotes

¹Commercial Nuclear Power Stations in the United States--Operable, Under Construction or Ordered--August 1, 1980, Wallchart, published by Nuclear News, La Grange Park, Illinois.

²The remoteness index as defined by sparseness and proximity measures (see text).

³Tennessee Valley Authority, Final Environmental Statement, Yellow Creek Nuclear Plant Units 1 and 2, Vol. 1, Vol. 2., January 1978.

⁴Mississippi Power & Light Company, Final Environmental Statement Related to Construction of Grand Gulf Nuclear Stations Units 1 and 2, Sec. 8.2, August 1973.

⁵Houston Lighting & Power Company, "Benefits and Costs" Chapter 8 and "Summary Benefit-Cost Analysis" Chapter 11 of South Texas Project-Environmental Report, Vol. 1, amended June 1975.

⁶Altameda Area Planning and Development Commission, Impact of the Georgia Power Company Nuclear Plant on Community Facilities in the Toomb--Appling BiCounty Area, Georgia Institute of Technology, Winter 1969.

⁷Shields, M. A., et al., Socioeconomic Impacts of Nuclear Power Plants: A Paired Comparison of Operating Facilities, NUREG/CR-0916, Oak Ridge, TN: Oak Ridge National Laboratory, July 1979.

⁸Central Savannah Area Planning and Development Commission, Impact of the Georgia Power Company Vogtle Nuclear Power Plant on the Central Savannah River Area, Appendix A, Georgia Institute of Technology, Spring 1972.

⁹Illinois Power Company, "Economic and Social Effects of Plant Construction and Operation," Chapter 8 of Environment Report--Construction Permit Stage for the Clinton Power Station, September 1974.

¹⁰Pijawka, D., Arkansas Nuclear One, Preliminary Site Report, Washington: U.S. Nuclear Regulatory Commission, February 1979.

¹¹Pijawka, D., St. Lucie, Units 1 and 2, Preliminary Site Visit Report, Washington: U.S. Nuclear Regulatory Commission, February 1979.

¹²Pijawka, D., Crystal River, Unit 3, Preliminary Site Visit Report, Washington: U.S. Nuclear Regulatory Commission, February 1979.

¹³York, M. N., Diablo Canyon, Units 1 and 2, Preliminary Site Visit Report, Washington: U.S. Nuclear Regulatory Commission, February 1979.

¹⁴Alabama Power Company, Final Environmental Statement Related to Operation of Joseph M. Farley Nuclear Plant, Units 1 and 2, December 1974.

¹⁵Flynn, J., Surrey Nuclear Plant, Units 1 and 2, Preliminary Site Visit Report, Washington: U.S. Nuclear Regulatory Commission, February 1979.

¹⁶Flynn J., Socioeconomic Impacts of Nuclear Generating Stations, Surry Case Study, Washington: U.S. Nuclear Regulatory Commission, November 1980.

¹⁷Pijawka, D., and Yoquinto, G., Socioeconomic Impacts of Nuclear Generating Stations, Diablo Canyon Case Study, Washington: U.S. Nuclear Regulatory Commission, December 1980.

¹⁸Alabama Power Company, Estimate, February 1979.

¹⁹Based on percentages from a survey at Joseph M. Farley #2. Malhotra, S., Manninen, D., Migration and Residential Location of Workers at Nuclear Power Plant Construction Sites, Vol. 11, Profile Analysis of Worker Survey, Final Report. BHARC-100/80/030, Seattle, WA: Battelle Human Affairs Research Centers, September 1980.

²⁰Based on population size within 20 and 50 miles of the site, Surrey is classified as non-remote. However when natural barriers are taken into consideration the population of the area within 20 miles of the site which has easy access to the site is considerably less. The figure for 50 miles is still appropriate as a representation of the population within commuting distance of the site.

Table 5-8. Variation in Migrant Proportion by Location

Location*	Number of Sites	Migrant Proportion (%) Construction Workers	
		Average	Range
<u>Remote</u>			
Bureau of Reclamation Water Development Projects ^{1,2}	10	59	40-89
Old West Regional Commission Study, Coal-fired Power Plants ³	14	60	21-97
North Dakota State University Leland Olds and Square Butte ⁴	2	50	**
Coal Creek ⁵	1	39	
NRC Labor Migration Study ^{6,7}	1	47	
	—	—	
	N = 28	Weighted Average = 58	
<u>Non-remote</u>			
NRC Labor Migration Study ^{6,7} (excluding TVA)	8	29	15-49
TVA Sites ⁸			
Nuclear ⁹	7	26	11-40
Non-nuclear ⁹	2	34	29-47
Bureau of Reclamation Water Development Projects ²	2	17	12-22
	—	—	
	N = 19	Weighted Average = 27	

*Remoteness assignments were made using the sparseness and proximity measures described in the text.

**Migrant proportions were not provided separately for these sites in the reference document.

Table 5-8. Footnotes

¹J. A. Chalmers, Bureau of Reclamation Construction Worker Survey, Bureau of Reclamation, Engineering and Research Center, October 1977.

²In general the Bureau of Reclamation Water Development Projects were constructed in sparsely settled regions of the western United States. Two sites, however, were located in the Phoenix area and are included in the nonremote group.

³Mountain West Research, Inc., Construction Worker Profile, Final Report, prepared for the Old West Regional Commission, 1975.

⁴A. G. Leholm, F. L. Leistritz and J. S. Wieland, Profile of Electric Power Plant Construction Work Force, Agricultural Economics Statistical Series, Issue No. 22, Department of Agricultural Economics, North Dakota State University, July 1976.

⁵J. S. Wieland and F. L. Leistritz, Profile of the Coal Creek Project Construction Work Force. Agricultural Economics Miscellaneous Report No. 33, Department of Agricultural Economics, North Dakota State University, February 1978.

⁶S. Malhotra and D. Manninen, Migration and Residential Location of Workers at Nuclear Power Plant Construction Sites, Vol. II Profile Analysis of Worker Surveys, Battelle Human Affairs Research Centers, September 1980.

⁷The NRC labor migration study included only one remote site.

⁸TVA has published numerous reports containing the results of construction worker surveys conducted at TVA sites. For example see Tennessee Valley Authority, Hartsville Nuclear Plants Socioeconomic Monitoring and Mitigation Report, March 31, 1978, Knoxville, Tennessee, Tennessee Valley Authority, 1978.

⁹Multiple surveys were conducted at the TVA sites. The average and range of migrant proportions shown are for 35 surveys conducted at the nine TVA sites.

5.6 Conclusions

Classification of current nuclear power plant sites according to remoteness shows that most sites are nonremote, while few are truly remotely sited. In fact, although half of the current sites are located in nonmetropolitan counties, a majority are within 60 miles of [19] and few are more than 100 miles from a major metropolitan area.

The data on growth rates (Table 5-5) and construction workforce in-migration proportions (Table 5-8) show that population and economic growth rates are higher at more remote as opposed to less remote sites. Impacts do increase with site remoteness. However, although the differences in growth rates between more and less remote sites presented in Table 5-5 are all statistically significant, the 6 percent growth rate in total population observed for the more remote sites is significantly below the rate of 10 to 15 percent needed to produce boomtown conditions and thus adverse socioeconomic impacts. This conclusion is supported by the data presented in Table 5-7, which showed that 12 somewhat remotely sited nuclear power plants produced principally favorable socioeconomic impacts (much increased tax revenues, increased retail trade, some strains on government services, stabilization of population) on nearby communities.

Finally, it seems clear (1) that should future nuclear power plants be sited no more remotely than are current plants, then they will have few if any adverse socioeconomic impacts and (2) should they be sited in truly remote locations, then the potential for adverse impacts on nearby small rural communities can be substantially reduced by advance planning.

References for Chapter 5

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2. U.S. Nuclear Regulatory Commission, Report of the Siting Policy Task Force, NUREG-0625, August 1979.
3. W. P. Freudenburg, "The Social Impact of Energy Boom Development on Rural Communities: A Review of Literatures and Some Predictions," Department of Sociology, Yale University, August 1976.
4. U.S. Bureau of the Census, Current Population Reports, Series P-25 and P-26, Washington: Government Printing Office, 1966 and 1971-1978.
5. U.S. Bureau of the Census, County Business Patterns (for individual states), Washington: Government Printing Office, 1959 and 1962 and 1964-1978.
6. U.S. Bureau of the Census, County and City Data Book, Washington: Government Printing Office, 1967 and 1972 and 1977.
7. U.S. Bureau of the Census, Census of Governments, Washington: Government Printing Office, 1977.
8. EPRI Planning and Evaluation Staff, "Technical Assessment Guide," EPRI Rept. No. PS 1201-SR, July 1979, Exhibit 9-1, p. 9-2.
9. Ibid, p. 2-3.
10. I. S. Grant and V. J. Longo, "Economic Incentives for Larger Transmission Conductors," Power Transmission, Inc., Schenectady, NY, p. 1.
11. Commonwealth Associates, Inc., "Cost Components of High Capacity Transmission Options," EPRI Rept. No. EL-1065, Vol. 1, May 1979, p. 2-35.
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18. C. F. Cortese, "Rapid Growth and Social Change in Western Communities," Social Impact Assessment, No. 40/41, April-May 1979.
19. U.S. Nuclear Regulatory Commission, Office of Nuclear Regulatory Research, Socioeconomic Impacts: Nuclear Power Station Siting, NUREG-0150, June 1977.
20. E. Peelle, "Social Effects of Nuclear Power Plants," in C. P. Wolf, ed., 2: Social Impact Assessment, Milwaukee, WI: Environmental Design Research Association, Inc., 1974, p. 114.
21. M. A. Shields et al., Socioeconomic Impacts of Nuclear Power Plants: A Paired Comparison of Operating Facilities, NUREG/CR-0916, Oak Ridge, TN: Oak Ridge National Laboratory, July 1979.
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Appendix A: Site Data

A large body of site-related data was collected for use in performing the consequence calculations discussed in Chapter 2 of this report. These data are summarized in the following sections of this appendix as listed below.

<u>Section</u>	<u>Data Description</u>
A.1	General Site and Reactor Data
A.2	Site Population Data
A.3	Weather Data
A.4	Site Wind Rose Data
A.5	Economic Data

A.1 General Site and Reactor Data

Calculations were performed for 91 sites where reactors are currently operating, are under construction, or have been assigned a construction permit. Table A.1-1 lists the site locations (county/state) and the power level (MWe), type, supplier, and date of startup (actual or expected) for the reactors located at these sites. Table A.1-2 gives the latitude and longitude of each site,* as well as the meteorological station and sheltering region assigned for performing site consequence calculations. The meteorological data used in this study are further described in Section A.3. The sheltering region is based on housing types and is used to determine external exposure shielding factors when population sheltering is assumed to be an emergency protective measure. The important housing characteristics and assumed shielding factors for the seven regions used in this study are described in Table A.1-3. For further information on sheltering regions and shielding factors, see reference [2].

*Latitudes and longitudes were taken from reference [1].

Table A.1-1 General Site and Reactor Data

Plant	Location (County/State)	Power Level (MWe)	Type	Reactor Supplier	Actual or Expected Date of Startup
Allens Creek	Austin, TX	1200	BWR	GE	/87
Arkansas 1,2	Pope, AR	836	PWR	B&W	12/74
		912	PWR	C-E	3/80
Bailly	Porter, IN	645	BWR	GE	6/87
Beaver Valley 1,2	Beaver, PA	833	PWR	W	4/77
		833	PWR	W	5/86
Bellefonte 1,2	Jackson, AL	1213	PWR	B&W	9/83
		1213	PWR	B&W	6/84
Big Rock Pt.	Charlevoix, MI	63	BWR	GL	12/62
Black Fox 1,2	Rogers, OK	1150	BWR	GE	7/85
		1150	BWR	GE	7/88
Braidwood 1,2	Will, IL	1120	PWR	W	10/85
		1120	PWR	W	10/86
Browns Ferry 1,2,3	Limestone, AL	1067	BWR	GE	8/74
		1067	BWR	GE	8/75
		1067	BWR	GE	3/77
Brunswick 1,2	Brunswick, NC	790	BWR	GE	3/77
		790	BWR	GE	11/75
Byron 1,2	Ogle, IL	1120	PWR	W	10/83
		1120	PWR	W	10/84
Callaway 1,2	Callaway, MO	1150	PWR	W	10/82
		1150	PWR	W	4/87
Calvert Cliffs 1,2	Calvert, MD	850	PWR	C-E	5/75
		850	PWR	C-E	5/77
Catawba 1,2	York, SC	1145	PWR	W	7/83
		1145	PWR	W	1/85
Cherokee 1,2,3	Cherokee, SC	1280	PWR	C-E	1/90
		1280	PWR	C-E	1/92
		1280	PWR	C-E	Indef.
Clinton 1,2	Dewitt, IL	950	BWR	GE	12/82
		950	BWR	GE	Indef.
Comanche Peak 1,2	Somervell, TX	1150	PWR	W	/81
		1150	PWR	W	/83
Cooper	Nemaha, NB	778	BWR	GE	7/74
Crystal River 3	Citrus, FL	825	PWR	B&W	3/77
Davis-Besse	Ottawa, OH	906	PWR	B&W	11/77
Diablo Canyon 1,2	San Luis Obispo, CA	1084	PWR	W	/81
		1106	PWR	W	/81
Donald C. Cook 1,2	Berrien, MI	1054	PWR	W	8/75
		1094	PWR	W	6/78
Dresden 1,2,3	Grundy, IL	200	BWR	GE	8/60
		800	BWR	GE	8/70
		800	BWR	GE	10/71
Duane Arnold	Linn, IA	545	BWR	GE	5/74
Fermi 2	Monroe, MI	1100	BWR	GE	3/82
Fitzpatrick*	Oswego, NY	821	BWR	GE	7/75
Forked River **	Ocean, NJ	1120	PWR	C-E	5/86
Ft. Calhoun	Washington, NB	457	PWR	C-E	9/73
Ft. St. Vrain	Weld, CO	330	HTGR	GA	1/79
Ginna (Brookwood)	Wayne, NY	490	PWR	W	3/70
Grand Gulf 1,2	Clairborne, MS	1250	BWR	GE	4/82
		1250	BWR	GE	9/86
Hadden Neck	Middlesey, CT	575	PWR	W	1/68
Hartsville A1,A2, B1,B2	Troysdale & Smith, TN	1233	BWR	GE	7/86
		1233	BWR	GE	7/87
		1233	BWR	GE	Indef.
		1233	BWR	GE	Indef.

*Same site as Nine Mile Point

**Same site as Oyster Creek

Table A.1-1 General Site and Reactor Data (cont)

Plant	Location (County/State)	Power Level (MWe)	Type	Reactor Supplier	Actual or Expected Date of Startup
Hatch 1,2	Appling, GA	786	BWR	GE	12/75
		786	BWR	GE	8/79
Hope Creek 1,2*	Salem, NJ	1070	BWR	GE	12/86
		1070	BWR	GE	12/89
Indian Point 2,3	Westchester, NY	873	PWR	W	7/74
		965	PWR	W	8/76
Joseph M. Farley 1,2	Houston, AL	860	PWR	W	12/77
		860	PWR	W	11/80
Kewaunee	Kewaunee, WI	535	PWR	W	6/74
LaCross	Monroe, WI	50	BWR	Allis	11/69
LaSalle 1,2	LaSalle, IL	1078	BWR	GE	6/81
		1078	BWR	GE	6/82
Limerick 1,2	Montgomery, PA	1055	BWR	GE	4/85
		1055	BWR	GE	4/87
Maine Yankee	Lincoln, ME	790	PWR	C-E	12/72
Marble Hill 1,2	Jefferson, IN	1130	PWR	W	/86
		1130	PWR	W	/87
McGuire 1,2	Mecklenberg, NC	1180	PWR	W	8/80
		1180	PWR	W	4/82
Midland 1,2	Midland, MI	530	PWR	B&W	7/84
		805	PWR	B&W	12/83
Millstone 1,2,3	New London, CT	660	BWR	GE	12/70
		870	PWR	C-E	12/75
		1150	PWR	W	5/86
Monticello	Wright, MN	536	BWR	GE	7/71
Nine Mile Pt. 1,2**	Oswego, NY	610	BWR	GE	12/69
		1080	BWR	GE	10/86
North Anna 1,2,3,4	Louisa, VA	850	PWR	W	6/78
		850	PWR	W	8/80
		934	PWR	B&W	4/87
		934	PWR	B&W	4/88
Oconee 1,2,3	Oconee, SC	860	PWR	B&W	7/73
		860	PWR	B&W	9/74
		860	PWR	B&W	12/74
Oyster Creek ***	Ocean, NJ	620	BWR	GE	12/69
Palisades	VanBuren, MI	740	PWR	C-E	12/71
Palo Verde 1,2,3	Manicopa, AZ	1270	PWR	C-E	5/83
		1270	PWR	C-E	5/84
		1270	PWR	C-E	5/86
Peach Bottom 2,3	York, PA	1065	BWR	GE	7/74
		1065	BWR	GE	12/74
Pebble Springs 1,2	Gilliam, OR	1260	PWR	B&W	9/88
		1260	PWR	B&W	9/90
Perkins 1,2,3	Davie, NC	1280	PWR	C-E	Indef.
		1280	PWR	C-E	Indef.
		1280	PWR	C-E	Indef.
Perry 1,2	Lake, OH	1205	BWR	GE	5/84
		1205	BWR	GE	5/88
Phipps Bend 1,2	Hawkins, TN	1233	BWR	GE	Indef.
		1233	BWR	GE	Indef.
Pilgrim 1,2	Plymouth, MA	670	BWR	GE	12/72
Pt. Beach 1,2	Manitowoc, WI	1150	PWR	C-E	Indef.
		497	PWR	W	12/70

*Same site as Salem
 **Same site as Fitzpatrick
 ***Same site as Forked River

Table A.1-1 General Site and Reactor Data (cont)

Plant	Location (County/State)	Power Level (MWe)	Type	Reactor Supplier	Actual or Expected Date of Startup
Prairie Island 1,2	Goodhue, MN	520	PWR	W	12/73
		520	PWR	W	12/74
Quad Cities 1,2	Rock Island, IL	800	BWR	GE	8/72
		800	BWR	GE	10/72
Rancho Seco	Sacramento, CA	913	PWR	B&W	4/75
River Bend 1,2	West Feliciana, LA	940	BWR	GE	4/84
		940	BWR	GE	Indef
Robinson 2	Darlington, SC	665	PWR	W	3/71
St. Lucie 1,2	St. Lucie, FL	777	PWR	C-E	12/76
		777	PWR	C-E	5/83
Salem 1,2*	Salem, NJ	1090	PWR	W	6/77
		1115	PWR	W	1/81
San Onofre 1,2,3	San Diego, CA	436	PWR	W	1/68
		1100	PWR	C-E	12/81
		1100	PWR	C-E	2/83
Seabrook 1,2	Rockingham, NH	1150	PWR	W	12/83
		1150	PWR	W	/85
Sequoyah 1,2	Hamilton, TN	1148	PWR	W	/80
		1148	PWR	W	6/81
Shearon Harris 1,2, 3,4	Wake & Chatham, NC	900	PWR	W	3/85
		900	PWR	W	3/88
		900	PWR	W	3/94
		900	PWR	W	3/92
Shoreham	Suffolk, NY	820	BWR	GE	3/83
Skagit 1,2	Skagit, WA	1288	BWR	GE	Indef
		1288	BWR	GE	Indef
South Texas 1,2	Matagorda, TX	1250	PWR	W	4/84
		1250	PWR	W	4/86
Surry 1,2	Surry, VA	775	PWR	W	12/72
		775	PWR	W	5/73
Susquehanna 1,2	Luzerne, PA	1050	BWR	GE	1/82
		1050	BWR	GE	1/83
Three Mile Island 1,2	Dauphin, PA	792	PWR	GE	9/74
		880	PWR	W	12/78
Trojan	Columbia, OR	1130	PWR	W	5/76
Turkey Pt. 3,4	Dade, FL	666	PWR	W	12/72
		666	PWR	W	9/73
Vermont Yankee	Windham, VT	514	BWR	GE	11/72
Virgil Summer	Fairfield, SC	900	PWR	W	6/81
Vogtle 1,2	Burke, GA	1100	PWR	W	/85
		1100	PWR	W	/88
WPPSS 1,2,4	Benton, WA	1250	PWR	B&W	6/85
		1100	BWR	GE	1/83
		1250	PWR	B&W	6/86
WPPSS 3,5	Grays Harbor, WA	1240	PWR	C-E	6/86
		1240	PWR	C-E	6/87
Waterford 3	St. Charles, LA	1165	PWR	C-E	/82
Watts Bar 1,2	Rhea, TN	1177	PWR	W	9/81
		1177	PWR	W	6/82
Wolf Creek	Coffey, KS	1150	PWR	W	4/83
Yankee Rowe	Franklin, MA	175	PWR	W	6/61
Yellow Creek 1,2	Tishomingo, MS	1285	PWR	C-E	11/85
		1285	PWR	C-E	4/88
Zimmer	Clermont, OH	810	BWR	GE	/81
Zion 1,2	Lake, IL	1100	PWR	W	6/73
		1100	PWR	W	12/73

*Same site as Hope Creek

Table A.1-2 General Site Data

Plant	Number Site	Latitude	Longitude	Meteorological Station	Sheltering Region	State
Allens Creek	1	29-40-43	96-06-15	Fort Worth (14)	3	TX
Arkansas	2	35-18-42	93-13-15	Columbia (10)	7	AR
Bailly	3	41-38-30	87-07-30	Chicago (9)	2	IN
Beaver Valley	4	40-37-18	80-26-06	Washington, DC (29)	1	PA
Bellefonte	5	34-42-32	85-55-36	Nashville (23)	7	AL
Big Rock Point	6	45-21-32	85-11-45	Milwaukee (21)	2	MI
Black Fox	7	36-07-01	95-32-54	Columbia (10)	3	OK
Braidwood	8	41-14-37	89-13-44	Moline (22)	4	IL
Browns Ferry	9	34-42-13	87-07-16	Nashville (23)	7	AL
Brunswick	10	33-57-32	78-01-15	Cape Hatteras (6)	6	NC
Byron	11	42-04-30	89-16-55	Moline (22)	4	IL
Callaway	12	38-45-42	91-46-52	Columbia (10)	4	MO
Calvert Cliffs	13	38-25-39	76-25-35	Washington, DC (29)	6	MD
Catawba	14	35-03-05	81-04-10	Nashville (23)	6	SC
Cherokee	15	35-02-12	81-30-43	Nashville (23)	6	SC
Clinton	16	40-10-19	88-50-03	Moline (22)	4	IL
Comanche Peak	17	32-17-49	97-47-07	Ft. Worth (14)	3	TX
Cooper	19	40-21-41	95-38-17	Omaha (25)	4	NB
Crystal River	20	28-57-26	82-41-56	Apalachicola (2)	7	FL
Davis-Besse	21	41-35-42	83-05-11	Chicago (9)	2	OH
Diablo Canyon	22	35-12-41	120-51-08	Santa Maria (27)	5	CA
Donald C. Cook	18	41-58-44	86-33-43	Chicago (9)	2	MI
Dresden	23	41-23-23	88-16-17	Moline (22)	4	IL
Duane Arnold	24	42-05-54	91-46-21	Omaha (25)	4	IA
Fermi	26	41-58-41	83-15-34	Chicago (9)	2	MI
Fitzpatrick*	27	43-31-19	76-23-54	Milwaukee (21)	1	NY
Forked River**	28	39-48-36	74-12-36	New York (24)	1	NJ
Ft. Calhoun	29	41-31-12	96-04-50	Omaha (25)	4	NB
Ft. St. Vrain	30	40-14-40	104-52-27	Dodge City (11)	4	CO
Ginna	31	43-16-39	77-18-30	Milwaukee (21)	1	NY
Grand Gulf	32	32-00-27	91-02-53	Lake Charles (17)	7	MS
Haddam Neck	33	41-28-56	72-29-57	New York (24)	1	CT
Hartsville	34	36-21-15	86-05-10	Nashville (23)	7	TN
Hatch	35	31-56-05	82-20-40	Charleston (8)	6	CA
Hope Creek***	92	39-27-46	75-32-08	Washington, DC (29)	1	NJ
Indian Point	36	41-15-57	73-56-06	New York (24)	1	NY
Joseph M. Farley	25	31-13-21	85-06-42	Lake Charles (17)	7	AL
Kewaunee	37	44-19-34	87-31-27	Milwaukee (21)	2	WI
LaCrosse	39	43-33-36	91-13-42	Madison (18)	2	WI
LaSalle	38	41-14-24	88-40-12	Moline (22)	4	IL
Limerick	40	40-13-12	75-35-24	Washington, DC (29)	1	PA
Maine Yankee	42	43-57-02	69-41-48	Caribou (7)	1	ME
Marble Hill	41	38-26-00	85-26-53	Moline (22)	2	IN
McGuire	43	35-25-59	80-56-55	Nashville (23)	6	NC
Midland	44	43-35-10	84-13-08	Milwaukee (21)	2	MI

*Same site as Nine Mile Point

**Same site as Oyster Creek

***Same site as Salem

Table A.1-2 General Site Data (cont)

Plant	Number Site	Latitude	Longitude	Meteorological Station	Sheltering Region	State
Millstone	45	41-18-32	72-10-04	Boston (4)	1	CT
Monticello	46	45-20-03	93-50-55	Madison (18)	2	MN
Nine Mile Point*	47	43-31-19	76-23-54	Milwaukee (21)	1	NY
North Anna	48	38-03-48	77-47-13	Washington, DC (29)	6	VA
Oconee	49	34-47-40	82-53-55	Nashville (23)	6	SC
Oyster Creek**	50	39-48-50	74-12-41	New York (24)	1	NJ
Palisades	51	42-19-24	86-18-52	Chicago (9)	2	MI
Palo Verde	52	33-23-25	112-51-45	Phoenix (26)	3	AZ
Peach Bottom	53	39-45-33	76-16-08	Washington, DC (29)	1	PA
Pebble Springs	54	45-42-05	120-08-17	Medford (19)	5	OR
Perkins	55	35-50-53	80-27-10	Nashville (23)	6	NC
Perry	56	41-48-03	81-08-36	Chicago (9)	2	OH
Phipps Bend	57	36-27-47	82-48-32	Nashville (23)	7	TN
Pilgrim	58	41-56-40	70-34-41	Boston (4)	1	MA
Point Beach	59	44-16-35	87-31-08	Milwaukee (21)	2	WI
Prairie Island	60	44-37-25	92-38-04	Madison (18)	2	MN
Quad Cities	61	41-43-38	90-20-30	Moline (22)	4	IL
Rancho Seco	62	38-21-00	121-07-12	Fresno (15)	5	CA
River Bend	63	30-45-26	91-19-54	Lake Charles (17)	7	LA
Robinson	64	34-24-12	80-09-30	Nashville (23)	6	SC
St. Lucie	65	27-20-55	80-14-47	Miami (20)	7	FL
Salem †	66	39-27-46	75-32-08	Washington, DC (29)	1	NJ
San Onofre	67	33-2-53	117-31-17	Santa Maria (27)	5	CA
Seabrook	68	42-53-53	70-51-05	Boston (4)	1	NH
Sequoyah	69	35-13-31	85-05-13	Nashville (23)	7	TN
Shearon Harris	70	35-38-00	78-57-22	Nashville (23)	6	NC
Shoreham	72	40-57-30	72-52-00	New York (24)	1	NY
Skaqit	71	48-32-00	122-07-26	Seattle (28)	5	WA
South Texas	73	28-47-42	96-02-53	Brownsville (5)	3	TX
Surry	75	37-10-00	76-41-50	Washington, DC (29)	6	VA
Susquehanna	76	41-06-00	76-09-00	Washington, DC (29)	1	PA
Three Mile Island	77	40-09-12	76-43-37	Washington, DC (29)	1	PA
Trojan	78	46-02-24	122-52-06	Medford (19)	5	OR
Tukey Point	79	25-26-02	80-19-54	Miami (20)	7	FL
Vermont Yankee	80	42-46-49	72-30-57	Caribou (7)	1	VT
Virgil Summer	74	34-17-54	81-18-55	Nashville (23)	6	SC
Vogtle	81	33-08-31	81-45-53	Charleston (8)	6	CA
WPPSS 1,2,4††	84	46-28-03	119-18-51	Medford (19)	5	WA
WPPSS 3,5	85	46-57-11	123-28-11	Medford (19)	5	WA
Waterford	82	30-00-00	90-28-12	Lake Charles (17)	7	LA
Watts Bar	83	35-36-10	84-47-25	Nashville (23)	7	TN
Wolf Creek	87	38-14-20	95-41-20	Omaha (25)	4	KN
Yankee Rowe	88	42-43-41	72-55-29	New York (24)	1	MA
Yellow Creek	89	34-57-24	88-12-57	Nashville (23)	7	MS
Zimmer	90	38-51-55	84-13-45	Nashville (23)	2	OH
Zion	91	42-27-34	87-48-23	Chicago (9)	4	IL

*Same site as Fitzpatrick

**Same site as Forked river

†Same site as Hope Creek

††Same site as Skaqit

Table A.1-3 Sheltering Regions

Region Number	Location	% Brick Housing Units	% Homes With Basements	Shielding Factor*	
				Cloud	Ground
1	Northeast	47	87	0.5	0.08
2	Great Lakes	36	77	0.6	0.1
3	Southwest	40	13	0.7	0.3
4	Midwest	35	71	0.5	0.09
5	Pacific Coast	27	23	0.7	0.3
6	Atlantic Coast	45	51	0.6	0.2
7	Southeast	59	16	0.7	0.2

*The ratio of dose received when sheltered to the dose that would be received if outdoors. Cloud refers to gamma exposure from radionuclides dispersed in the atmosphere. Ground refers to gamma exposure from ground-deposited radionuclides.

A.2 Population Data

CRAC2 requires a description of the population distribution surrounding the reactor site being evaluated. Distributions are input as population counts for individual spatial elements. These elements are the cells in a polar grid consisting of up to 34 annuli and 16 sectors (each $22\frac{1}{2}^\circ$ in width). This study used 34 annuli, with radii of 0.5, 1, 1.5, 2, 2.5, 3, 3.5, 4, 4.5, 5, 6, 7, 8.5, 10, 12.5, 15, 17.5, 20, 25, 30, 35, 40, 45, 50, 55, 60, 65, 70, 85, 100, 150, 200, 350, and 500 miles. The population distribution for each site was derived from 1970 census data using a program called SECPOP which was developed by the Office of Radiation Programs, Environmental Protection Agency.* SECPOP constructs a polar grid from user-specified annular radii and number of sectors. This grid is centered on a location specified by latitude and longitude. A data file containing census data is then scanned to determine which enumeration district centroids fall into each spatial element. The population of each enumeration district is considered to be wholly within the spatial element in which its centroid falls. While this is an approximation, especially in sparsely populated areas for which the centroids are widely dispersed, it has an accuracy comparable to much of the other data used as input to CRAC2. In addition, the nature of the inaccuracy is such that it should have a very limited impact on conclusions drawn from exercising the model. The latitudes and longitudes for the 91 sites are provided in Table A.1-2. Summary population statistics for each site are provided in Chapter 3 and Appendix E.

*Technical Memorandum 73-146, U.S. Department of Commerce, Office of Telecommunications.

A.3 Weather Data

CRAC2 requires an input file containing 8760 hourly weather observations (one year). The hourly observations consist of wind speed, wind direction, stability class, and precipitation. These data are used in the dispersion/ deposition submodel to determine the rate at which the radioactive plume travels, disperses, and is depleted.

Past studies have typically employed data gathered by a licensee over a one-year period at a proposed site, usually as part of the license application. For this study we have selected 29 National Weather Service (NWS) stations as the sources of meteorological data. NWS data are available for a large number of sites, cover long periods of time, are generally of higher quality, and are more detailed than actual reactor site data. Each of the NWS stations selected has approximately 25 years of available data. Therefore, rather than select a single year at random, a Typical Meteorological Year (TMY) [3] was used to represent the long-term average behavior of the weather at a station. The technique used to determine a TMY involves comparing the distribution of certain weather characteristics for a given month over the entire period of record. Using statistical techniques described in reference [3], the one month "most typical" of the period is selected as part of the TMY. This procedure was performed for each of the twelve calendar months to obtain the TMY. In addition, a small amount of smoothing is performed at the boundaries between months to avoid abrupt changes in weather conditions.

The criteria used to generate the TMYs were selected based on their relevance to solar heating simulations and include temperature, wind speed, and insolation. Since these parameters are correlated to the data required for the CRAC2 input, the TMYs are considered to be reasonably representative years to use as input to the consequence model. These data are probably better than the single year weather data used in the past which are of uncertain quality and are subject to the anomalies of a single year's weather.

The TMYs are available from the National Climatic Center (NCC), Asheville, NC. The data tapes supplied by the NCC are not compatible with CRAC2 requirements. In addition, these tapes do not contain a classification of stability class. A conversion program, METDAT, was

developed by Science Applications, Inc. (SAI) under contract to Sandia. This program uses CRSTER [4], developed by the National Oceanic and Atmospheric Administration (NOAA), to generate the stability class using the insolation and wind speed data available in the TMY tapes.

CRAC2 requires rainfall intensity data for each hourly observation. Like atmospheric stability, rainfall data are not available on the TMY tapes. Therefore, rainfall statistics were gathered from other NWS data and were merged with the TMY information using the METDAT program.

The diffusion model used in CRAC2 also takes into account mixing height during dispersion calculations. The mixing height can affect the vertical diffusion of the radionuclide plume because mixing is essentially terminated at these levels. The mixing heights used for the 29 NWS stations were determined from the Holzworth isopleths of mean annual afternoon mixing height [5] (see Figure A.3-1). Table A.3-1 lists the 29 NWS stations with the assigned mixing heights. Figure A.3-2 shows the location of these stations in addition to the locations of the 91 reactor sites.

The meteorological data used for each of these 29 stations are summarized in Table A.3-2 in terms of the weather bin categories described in Appendix F. Additional rainfall data for the 29 stations are included in Table A.3-3.

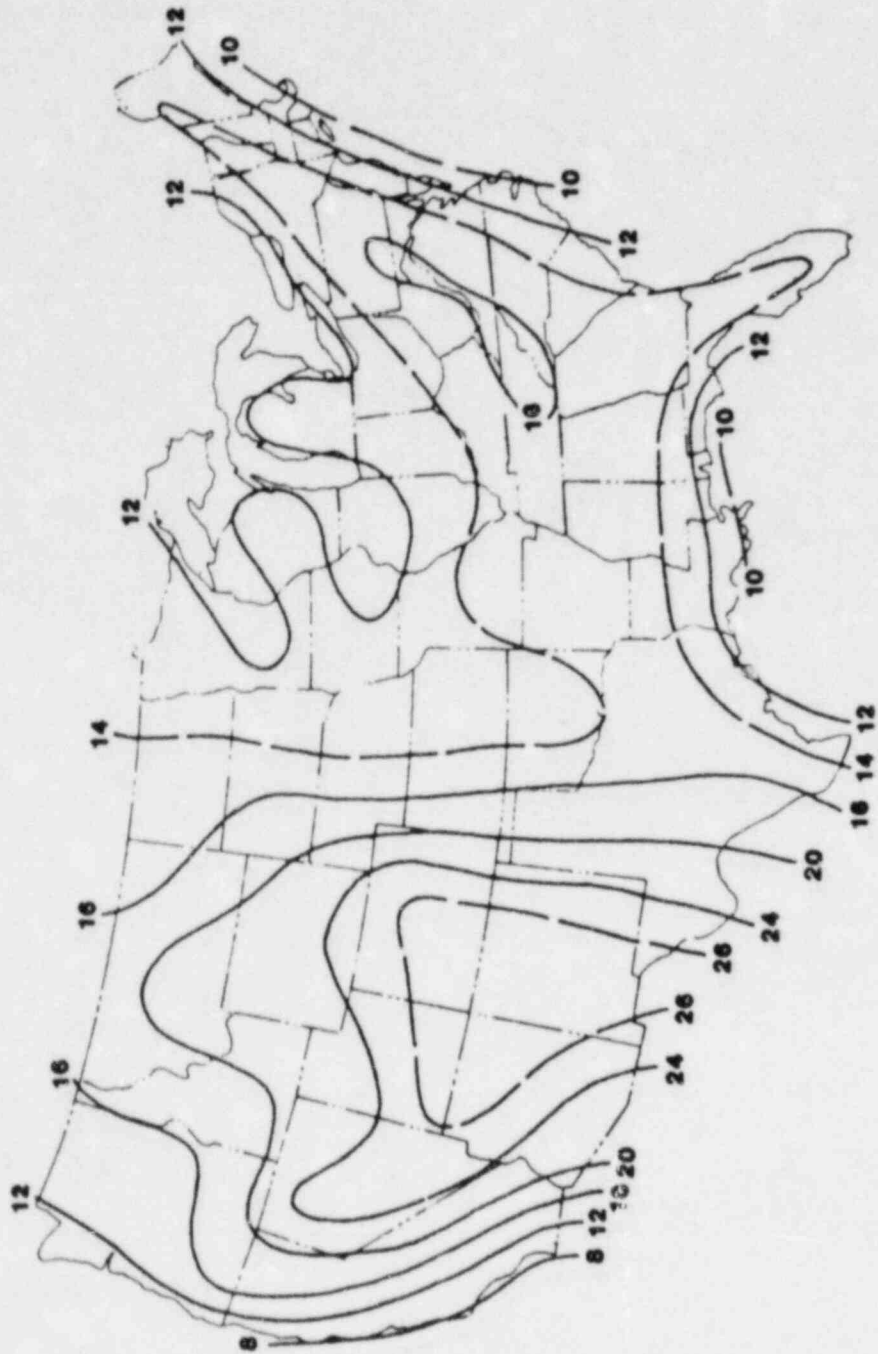


Figure A.3-1 Isopleths ($m \times 10^{-2}$) of Mean Annual Afternoon Mixing Heights. From reference [5].

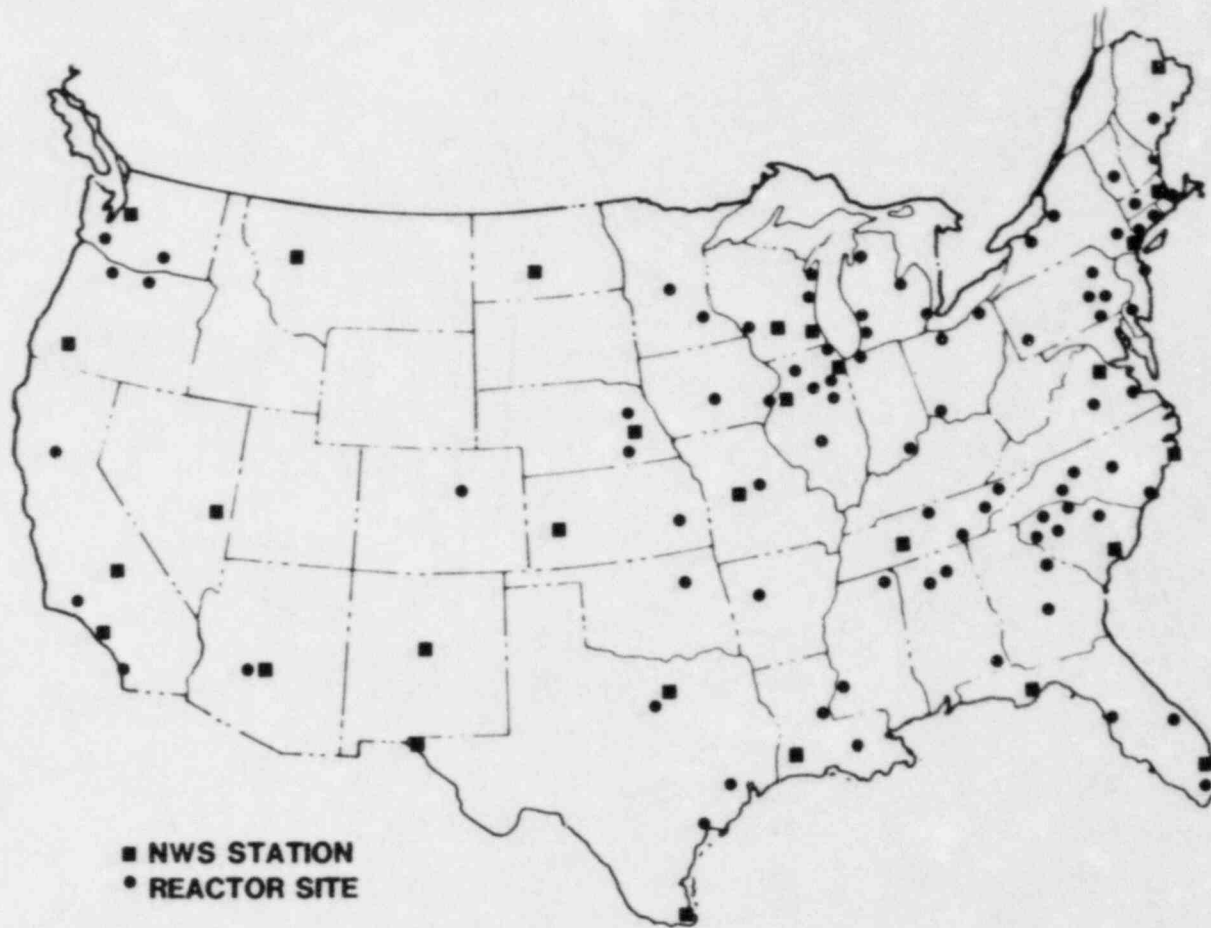


Figure A.3.2 Geographic location of the 29 NWS Stations and the 91 Reactor sites.

Table A.3-1 NWS Station Locations and Mixing Heights

No.	Station	Mixing Height (m)	No.	Station	Mixing Height (m)
1	Albuquerque, NM	2600	16	Great Falls, MT	2000
2	Apalachicola, FL	1200	17	Lake Charles, LA	1100
3	Bismarck, ND	1500	18	Madison, WI	1200
4	Boston, MA	1100	19	Medford, OR	1600
5	Brownsville, TX	1300	20	Miami, FL	1200
6	Cape Hatteras, NC	1000	21	Milwaukee, WI	1200
7	Caribou, ME	1300	22	Moline, IL	1200
8	Charleston, SC	1300	23	Nashville, TN	1600
9	Chicago, IL	1200	24	New York, NY	1200
10	Columbia, MO	1200	25	Omaha, NB	1300
11	Dodge City, KS	1600	26	Phoenix, AZ	2400
12	El Paso, TX	2600	27	Santa Maria, CA	800
13	Ely, NV	2400	28	Seattle, WA	1200
14	Fort Worth, TX	1500	29	Washington, DC	1500
15	Fresno, CA	1600			

Table A.3-2 Meteorological Data for 29 NWS Stations Summarized
Using Weather Bin Categories

Weather Bin Definitions

- R - Rain starting within indicated interval (miles).
- S - Slowdown occurring within indicated interval (miles).
- A-C D E F - Stability categories
- 1(0-1), 2(1-2), 3(2-3), 4(3-5), 5(GT 5) - Wind speed intervals (m/s).

Percent of Weather Sequences

Weather Bin	Albuquerque (1)	Apalachicola (2)	Bismarck (3)	Boston (4)	Brownsville (5)	Cape Hatteras (6)	Caribou (7)	Charleston (8)	Chicago (9)	Columbia (10)	Dodge City (11)	El Paso (12)
1 R (0)	1.46	4.50	3.94	8.89	2.25	6.69	10.14	5.87	6.19	6.26	3.69	1.30
2 R (0-5)	0.09	0.70	0.15	0.17	0.06	0.11	0.38	0.29	0.15	0.11	0.11	0.06
3 R (5-10)	0.31	1.14	0.40	0.79	0.39	0.75	1.26	0.88	0.68	0.75	0.27	0.26
4 R (10-15)	0.55	1.34	0.67	1.24	0.49	1.12	1.60	1.32	1.21	0.91	0.58	0.51
5 R (15-20)	0.33	1.11	0.76	0.82	0.54	1.02	1.28	0.81	0.87	0.91	0.37	0.34
6 R (20-25)	0.37	0.99	0.55	0.90	0.53	0.83	1.12	0.87	0.68	0.76	0.55	0.32
7 R (25-30)	0.00	0.06	0.66	0.94	0.42	0.83	1.29	0.99	0.86	0.76	0.50	0.34
8 S (0-10)	2.00	1.36	1.02	0.55	0.34	0.14	0.53	0.51	0.51	0.53	0.24	0.98
9 S (10-15)	2.01	1.02	0.90	0.43	0.27	0.08	0.42	0.43	0.41	0.42	0.25	0.96
10 S (15-20)	1.78	1.04	0.63	0.50	0.27	0.09	0.40	0.33	0.35	0.39	0.14	0.91
11 S (20-25)	1.55	1.02	0.73	0.37	0.21	0.07	0.29	0.39	0.38	0.32	0.15	0.71
12 S (25-30)	1.62	1.19	0.88	0.45	0.31	0.14	0.33	0.39	0.28	0.45	0.18	0.89
13 A-C 1,2,3	12.97	6.44	4.22	1.51	1.18	1.66	4.29	3.05	2.66	3.32	2.48	11.08
14 A-C 4,5	11.08	15.70	7.11	7.52	11.46	12.48	5.48	13.11	10.98	13.53	13.03	14.74
15 D 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
16 D 2	1.51	2.19	1.71	0.74	0.59	0.21	1.82	1.06	1.02	0.92	0.43	1.31
17 D 3	3.07	2.81	3.18	1.77	1.95	1.67	4.49	3.41	3.62	3.05	1.61	2.91
18 D 4	4.81	7.72	8.56	9.63	7.33	8.50	10.92	12.45	11.90	11.18	7.39	5.89
19 D 5	19.29	12.31	35.99	45.75	43.07	38.66	31.10	19.92	32.15	27.92	49.13	20.50
20 E 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21 E 2	1.26	1.85	1.11	0.23	0.54	0.26	0.53	0.83	0.48	0.50	0.09	1.53
22 E 3	3.15	2.48	1.91	0.79	2.44	1.23	2.43	4.01	2.20	2.00	0.67	3.15
23 E 4	7.87	5.34	6.21	6.36	7.28	9.68	6.71	7.57	7.25	9.06	7.68	6.45
24 E 5	2.35	1.85	1.67	3.13	2.69	3.01	2.09	1.80	2.84	2.23	3.74	2.51
25 F 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
26 F 2	6.94	14.51	7.71	1.13	3.69	1.56	3.11	8.17	2.75	2.32	0.72	9.59
27 F 3	7.50	6.46	5.48	1.80	6.40	4.20	4.75	6.92	4.93	4.73	2.24	8.32
28 F 4	5.78	4.01	3.85	3.58	5.30	5.00	3.28	4.61	4.60	6.74	3.74	4.42
29 F 5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Table A.3-2 Meteorological Data for 29 NWS Stations Summarized
Using Weather Bin Categories (cont)

Weather Bin Definitions

R - Rain starting within indicated interval (miles).

S - Slowdown occurring within indicated interval (miles).

A-C D E F - Stability categories

1(0-1), 2(1-2), 3(2-3), 4(3-5), 5(GT 5) - Wind speed intervals (m/s).

Percent of Weather Sequences

Weather Bin	Ely (13)	Fort Worth (14)	Fresno (15)	Great Falls (16)	Lake Charles (17)	Madison (18)	Medford (19)	Miami (20)	Milwaukee (21)	Moline (22)	Nashville (23)	New York (24)
1 R (0)	3.06	3.97	2.09	5.56	3.73	6.08	4.61	4.37	6.12	5.84	6.60	7.96
2 R (0-5)	0.36	0.10	0.11	0.40	0.32	0.24	1.37	0.32	0.18	0.11	0.18	0.14
3 R (5-10)	0.65	0.47	0.56	0.94	1.00	0.98	1.56	1.14	0.66	0.79	0.79	0.71
4 R (10-15)	0.65	0.66	0.49	1.11	0.98	1.28	1.59	1.34	1.20	1.03	1.04	1.16
5 R (15-20)	0.66	0.45	0.32	0.82	0.68	1.03	1.13	1.15	0.84	0.83	0.90	0.86
6 R (20-25)	0.57	0.45	0.40	0.59	0.76	0.84	1.13	1.02	0.71	0.66	0.01	0.76
7 R (25-30)	0.51	0.48	0.39	0.76	0.66	0.98	1.19	1.31	0.88	0.80	0.73	0.70
8 S (0-10)	0.86	0.49	0.90	0.59	0.51	0.94	1.47	0.62	0.59	0.47	0.73	0.27
9 S (10-15)	0.32	0.33	0.81	0.39	0.43	0.73	1.37	0.50	0.40	0.32	0.66	0.18
10 S (15-20)	0.73	0.25	0.70	0.40	0.35	0.75	1.50	0.49	0.34	0.35	0.65	0.21
11 S (20-25)	0.28	0.33	0.62	0.34	0.38	0.58	1.27	0.41	0.32	0.41	0.68	0.16
12 S (25-30)	0.64	0.33	0.78	0.33	0.42	0.68	1.29	0.53	0.43	0.35	0.70	0.21
13 A-C 1,2,3	9.60	4.12	16.69	4.49	3.97	3.38	15.49	3.46	2.25	3.50	4.40	1.92
14 A-C 4,5	13.70	14.92	7.45	8.12	11.58	8.64	6.06	15.70	9.68	10.73	11.18	10.18
15 D 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
16 D 2	1.54	0.67	4.65	1.36	1.35	2.40	10.54	0.95	1.26	1.71	2.23	0.70
17 D 3	3.12	2.35	5.91	2.92	4.87	3.90	7.31	2.39	2.53	4.68	3.86	2.58
18 D 4	8.57	9.57	4.94	8.64	13.79	11.86	4.50	8.89	10.61	10.82	9.66	10.82
19 D 5	25.41	31.63	7.21	42.24	19.93	29.43	5.27	17.64	36.80	29.33	19.65	37.96
20 E 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21 E 2	0.59	0.43	2.40	0.55	0.75	1.26	2.93	1.16	0.78	1.63	1.36	0.31
22 E 3	1.78	2.10	3.85	2.34	3.89	1.97	3.26	3.73	0.70	2.56	3.36	1.91
23 E 4	10.75	8.80	6.37	6.28	6.29	5.40	2.11	8.20	6.90	5.74	6.06	7.79
24 E 5	3.78	2.88	2.39	2.79	0.99	1.24	0.45	1.97	2.11	1.47	1.07	3.08
25 F 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
26 F 2	2.82	2.90	13.63	2.32	6.95	8.12	13.89	8.06	5.22	8.24	7.25	1.32
27 F 3	4.29	5.14	11.28	3.09	9.62	4.32	7.65	8.54	3.78	5.32	8.26	3.54
28 F 4	4.81	6.18	5.07	2.64	5.75	2.96	1.26	6.12	3.71	3.49	4.41	4.59
29 F 5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Table A.3-2 Meteorological Data for 29 NWS Stations Summarized
Using Weather Bin Categories (cont)

Weather Bin Definitions

- R - Rain starting within indicated interval (miles).
 S - Slowdown occurring within indicated interval (miles).
 A-C D E F - Stability categories
 1(0-1), 2(1-2), 3(2-3), 4(3-5), 5(GT 5) - Wind speed intervals (m/s).

Percent of Weather Sequences

Weather Bin	Omaha (25)	Phoenix (26)	Santa Maria (27)	Seattle (28)	Washington (29)
1 R (0)	5.43	1.00	2.24	8.72	5.79
2 R (0-5)	0.13	0.08	0.19	0.42	0.39
3 R (5-10)	0.62	0.31	0.40	1.87	1.28
4 R (10-15)	0.89	0.25	0.62	2.12	1.14
5 R (15-20)	0.70	0.23	0.41	1.90	0.88
6 R (20-25)	0.51	0.24	0.32	1.53	0.87
7 R (25-30)	0.59	0.22	0.43	1.77	0.86
8 S (0-10)	1.16	1.27	2.41	1.36	0.71
9 S (10-15)	0.90	1.21	1.84	1.44	0.67
10 S (15-20)	0.75	1.20	1.63	1.02	0.48
11 S (20-25)	0.67	0.91	1.45	0.98	0.63
12 S (25-30)	0.86	1.13	1.77	1.21	0.63
13 A-C 1,2,3	3.79	16.02	7.96	5.15	7.33
14 A-C 4,5	12.36	15.92	12.53	6.87	11.30
15 D 1	0.00	0.00	0.00	0.00	0.00
16 D 2	1.26	1.52	11.16	2.95	2.98
17 D 3	3.23	3.18	8.66	6.55	6.08
18 D 4	8.87	6.69	6.97	16.12	10.64
19 D 5	30.39	6.30	13.40	19.46	16.20
20 E 1	0.00	0.00	0.00	0.00	0.00
21 E 2	0.99	1.96	2.44	0.72	1.85
22 E 3	2.24	3.57	2.41	2.07	3.52
23 E 4	6.53	6.35	2.42	4.82	5.27
24 E 5	1.77	0.92	0.81	1.02	1.23
25 F 1	0.00	0.00	0.00	0.00	0.00
26 F 2	7.63	11.20	11.16	3.46	9.81
27 F 3	4.17	12.09	4.81	3.80	6.38
28 F 4	3.56	6.22	1.54	2.68	3.09
29 F 5	0.00	0.00	0.00	0.00	0.00

Table A.3-3 Summary of Rainfall Data for
29 NWS Station TMYs

<u>Station</u>	<u>Hours of Observed Rainfall</u>	<u>Annual Rain (inches)</u>
Albuquerque (1)	128	7
Apalachicola (2)	394	65
Bismarck (3)	345	16
Boston (4)	779	41
Brownsville (5)	197	16
Cape Hatteras (6)	586	49
Caribou (7)	888	31
Charleston (8)	514	52
Chicago (9)	542	37
Columbia (10)	548	37
Dodge City (11)	323	26
El Paso (12)	114	6
Ely (13)	268	10
Fort Worth (14)	348	33
Fresno (15)	183	7
Great Falls (16)	487	16
Lake Charles (17)	327	41
Madison (18)	533	29
Medford (19)	404	17
Miami (20)	383	53
Milwaukee (21)	536	27
Moline (22)	512	37
Nashville (23)	578	49
New York (24)	697	49
Omaha (25)	476	30
Phoenix (26)	88	4
Santa Maria (27)	196	10
Seattle (28)	764	40
Washington (29)	507	32

A.4 Site Wind Rose Data

CRAC2 uses a straight-line trajectory model for plume movement, employing the wind speeds in the weather sequence to determine the rate of travel. To calculate the effects of the accident in different directions, CRAC2 uses the wind rose as an empirical distribution for the probability that the plume trajectory will be in a given direction. All consequences are calculated assuming that the plume follows each of the 16 directions, and the results are weighted by the frequency of wind travel in that direction.

The wind rose data for the 91 sites were taken from either the Environmental Reports or the Preliminary or Final Safety Analysis Reports submitted to the Nuclear Regulatory Commission. The site wind roses used in this study are presented in Table A.4-1. A summary histogram of peak to mean wind rose probability ratios for the 91 sites is presented in Figure A.4-1. This histogram illustrates the importance of wind rose probabilities to reactor accident consequence calculations. (The mean wind rose probability is 1/16.)

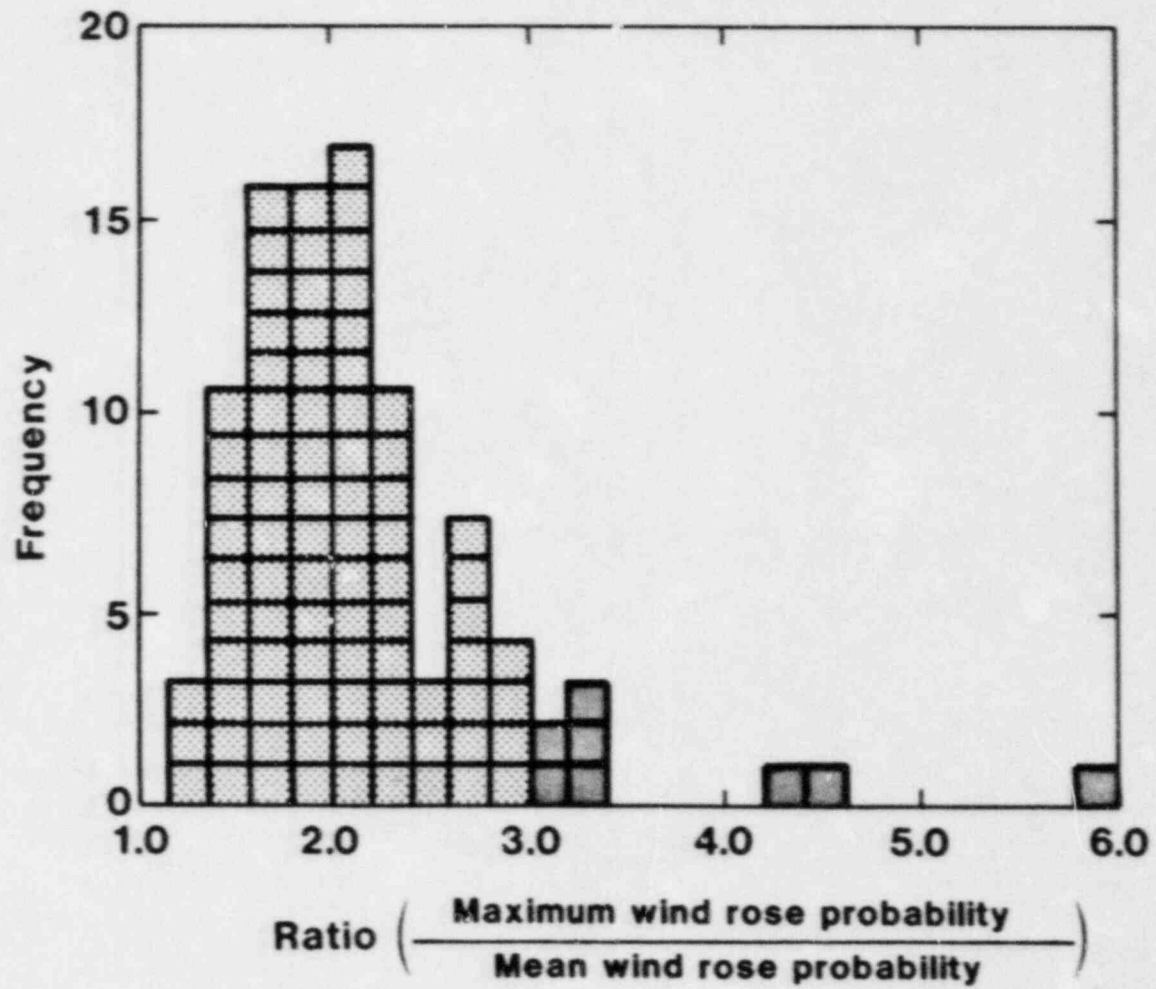
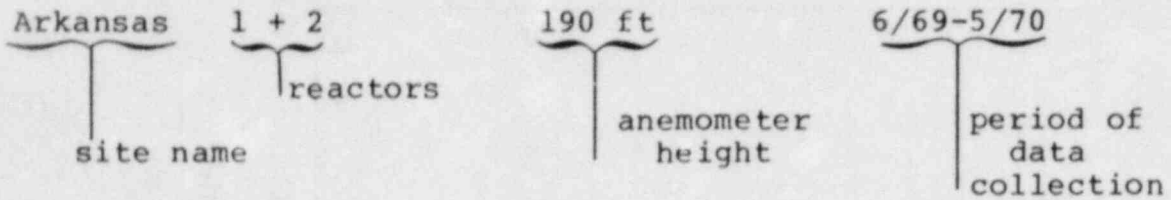


Figure A.4-1 Summary Histogram of Peak to Mean Wind Rose Probability Ratios for the 91 Sites

Table A.4-1
Site Wind Rose Data

Explanation of Titles:



Note: All wind roses in Table A.4-1 are presented as the probability of wind blowing toward the sector indicated. This is the opposite of the conventional definition used by meteorologists.

Table A.4-1 Site Wind Rose Data
Probability of Wind Blowing Towards Sector

Station	N	NNE	NE	ENE	E	ESE	SE	SSE
	S	SSW	SW	WSW	W	WNW	WW	WNW
Allens Creek	<u>10 m</u>				<u>8/1/1972 - 7/31/1973</u>			
	.127	.073	.043	.024	.022	.021	.027	.069
Arkansas 1, 2	<u>190 ft</u>				<u>8/69 - 5/70</u>			
	.103	.074	.052	.074	.126	.087	.053	.021
Bailly	<u>230 ft</u>				<u>12/4/51 - 12/3/57</u>			
	.064	.105	.095	.086	.069	.056	.040	.038
Beaver Valley 1, 2	<u>190 ft</u>				<u>9/15/69 - 9/5/70</u>			
	.087	.078	.051	.041	.083	.137	.123	.050
Beliefonte 1	<u>94 ft</u>				<u>1971</u>			
	.064	.075	.092	.082	.071	.067	.060	.076
Big Rock Point	<u>250 ft</u>				<u>2/61 - 2/63</u>			
	.112	.075	.071	.081	.099	.058	.057	.065
Black Fox	<u>33 ft</u>				<u>12/73 - 11/74</u>			
	.180	.055	.026	.026	.022	.030	.051	.059
Braidwood 1	<u>30 ft</u>				<u>11/1/73 - 10/31/74</u>			
	.105	.112	.077	.065	.061	.070	.065	.045
Browns Ferry 1, 2, 3	<u>300 ft</u>				<u>2/11/67 - 12/31/68</u>			
	.072	.066	.058	.058	.052	.067	.055	.054
Brunswick 1, 2	<u>350 ft</u>				<u>9/25/70 - 1/5/73</u>			
	.055	.077	.145	.088	.053	.037	.036	.041
Byron 1	<u>30 ft</u>				<u>6/11/73 - 5/31/74</u>			
	.097	.089	.081	.065	.075	.063	.076	.057
Callaway	<u>10 m</u>				<u>5/4/73 - 5/4/74</u>			
	.126	.096	.074	.043	.058	.070	.058	.050
Calvert Cliff 1, 2	<u>33 ft</u>							
	.116	.089	.070	.045	.064	.061	.103	.078
Catawba 1	<u>30 ft</u>				<u>6/10/73 - 6/10/72</u>			
	.023	.056	.207	.087	.043	.024	.036	.026
Cherokee	<u>30 ft</u>				<u>9/11/73 - 9/11/74</u>			
	.036	.048	.124	.104	.094	.081	.114	.052
Clinton	<u>10 m</u>				<u>5/72 - 6/73</u>			
	.104	.093	.086	.054	.042	.041	.042	.052
Comanche Peak	<u>10 m</u>				<u>5/12/72 - 5/14/76</u>			
	.151	.084	.041	.025	.024	.029	.067	.076

Table A.4-1 Site Wind Rose Data (cont)
Probability of Wind Blowing Towards Sector

Station	N S	NNE SSW	NE SW	ENE WSW	E W	ESE WNW	SE NW	SSE NNW
Cook DC 1, 2		<u>200 ft</u>			<u>1967</u>			
	.091	.105	.055	.045	.054	.069	.057	.062
	.078	.042	.042	.050	.040	.063	.072	.073
Cooper		<u>318 ft</u>			<u>3/70 - 2/71</u>			
	.116	.117	.079	.037	.030	.041	.060	.100
	.094	.061	.025	.031	.027	.034	.058	.090
Crystal River		<u>33 ft</u>			<u>1/1/75 - 12/31/75</u>			
	.043	.048	.051	.048	.082	.057	.043	.030
	.062	.047	.098	.121	.111	.064	.061	.034
Davis-BE 1		<u>35 ft</u>			<u>8/4/74 - 8/3/75</u>			
	.064	.116	.130	.102	.081	.039	.053	.037
	.030	.039	.058	.057	.077	.041	.038	.039
Diablo Canyon 1, 2		<u>250 ft</u>			<u>10/69 - 9/70</u>			
	.031	.012	.014	.015	.026	.045	.363	.128
	.059	.029	.055	.017	.014	.015	.103	.075
Dresden 2, 3		<u>300 ft</u>						
	.088	.090	.096	.067	.101	.085	.080	.056
	.049	.031	.039	.033	.036	.033	.060	.055
Duane Arnold		<u>165 ft</u>			<u>1972</u>			
	.129	.073	.053	.036	.051	.082	.083	.095
	.075	.040	.032	.034	.039	.060	.061	.076
Farley 1, 2		<u>33 ft</u>						
	.073	.070	.064	.044	.044	.045	.067	.090
	.097	.083	.086	.062	.044	.035	.040	.056
Fermi 2					<u>9/1/73 - 8/31/74</u>			
	.041	.088	.089	.102	.083	.086	.063	.047
	.026	.025	.059	.063	.069	.050	.058	.058
Fitzpatrick		<u>200 ft</u>			<u>1963 - 1964</u>			
	.087	.059	.102	.132	.115	.056	.053	.035
	.040	.047	.033	.014	.018	.037	.101	.088
Forked River		<u>400 ft</u>			<u>2/66 - 2/67</u>			
	.075	.096	.087	.068	.087	.093	.075	.063
	.044	.037	.052	.055	.039	.040	.047	.040
Fort Calhoun		<u>40 ft</u>			<u>10/68 - 9/70</u>			
	.093	.059	.034	.021	.042	.079	.113	.098
	.071	.018	.017	.022	.028	.064	.115	.126
Fort St. Vrain		<u>205 ft</u>			<u>1967 - 1968</u>			
	.063	.069	.076	.057	.040	.029	.035	.039
	.164	.085	.076	.064	.058	.043	.051	.049
Ginna R.E.		<u>50 ft</u>			<u>1966 - 1967</u>			
	.090	.081	.102	.097	.112	.101	.079	.044
	.030	.032	.031	.038	.045	.036	.030	.052
Grand Gulf 1					<u>1951 - 1960</u>			
	.101	.074	.062	.043	.036	.043	.070	.064
	.065	.060	.061	.040	.040	.044	.080	.117
Nadden Neck		<u>129 ft</u>			<u>1963</u>			
	.048	.046	.043	.038	.070	.160	.265	.052
	.013	.006	.009	.013	.035	.092	.055	.055
Hartsville		<u>33 ft</u>			<u>2/1/73 - 1/31/74</u>			
	.045	.058	.048	.056	.151	.034	.044	.025
	.045	.113	.175	.063	.150	.074	.069	.051

Table A.4-1 Site Wind Rose Data (cont)
Probability of Wind Blowing Towards Sector

Station	N S	NNE SSW	NE SW	ENE SSW	E W	ESE WNW	SE NW	SSE NNW
Hatch, E.I. 1, 2	<u>150 ft</u>				<u>6/1/70 - 8/31/74</u>			
	.055 .040	.069 .038	.082 .051	.073 .067	.075 .081	.077 .068	.072 .057	.049 .044
Indian Point 2, 3	<u>100 ft</u>				<u>1/1/71 - 12/31/71</u>			
	.076 .124	.055 .135	.038 .066	.039 .027	.053 .019	.079 .019	.077 .041	.070 .063
Kewaunee	<u>180 ft</u>				<u>8/31/68 - 3/25/70</u>			
	.092 .066	.090 .055	.064 .042	.075 .030	.094 .022	.117 .023	.082 .028	.080 .050
LaSalle 1, 2	<u>300 ft</u>							
	.088 .049	.090 .031	.096 .039	.067 .033	.101 .036	.085 .033	.080 .060	.056 .055
La Crosse	<u>350 ft</u>				<u>1968 - 1970</u>			
	.194 .125	.139 .101	.084 .048	.018 .011	.051 .022	.026 .010	.076 .026	.062 .033
Limerick 1	<u>270 ft</u>				<u>1/72 - 12/74</u>			
	.071 .054	.068 .039	.052 .035	.051 .046	.090 .0670	.150 .040	.109 .037	.059 .040
Marble Hill	<u>33 ft</u>				<u>1/74 - 12/74</u>			
	.058 .045	.141 .044	.124 .063	.074 .060	.062 .047	.060 .030	.044 .030	.037 .041
Mc Yankee	<u>149 ft</u>				<u>7/67 - 6/68</u>			
	.118 .075	.124 .068	.082 .064	.041 .030	.041 .024	.055 .027	.088 .031	.089 .044
McGuire 1, 2	<u>130 ft</u>				<u>10/17/70 - 10/16/71</u>			
	.070 .057	.090 .068	.122 .113	.062 .078	.054 .056	.042 .037	.042 .038	.040 .030
Midland 2					<u>1962 - 1966</u>			
	.060 .045	.082 .046	.123 .061	.106 .043	.124 .045	.066 .024	.064 .028	.051 .032
Millstone 1, 2	<u>152 ft</u>				<u>8/65 - 9/67</u>			
	.038 .066	.060 .060	.076 .036	.170 .035	.078 .058	.070 .035	.078 .025	.073 .041
Monticello	<u>140 ft</u>				<u>2/9/67 - 2/10/68</u>			
	.089 .036	.091 .041	.063 .029	.055 .051	.030 .031	.089 .055	.104 .052	.119 .065
Nine M. Pt. 1, 2	<u>204 ft</u>				<u>1963 - 1964</u>			
	.082 .041	.060 .048	.104 .034	.131 .013	.118 .018	.059 .037	.054 .097	.037 .069
North Anna 1, 2, 3	<u>150 ft</u>				<u>9/16/71 - 9/15/72</u>			
	.141 .100	.095 .048	.058 .044	.047 .035	.055 .041	.047 .035	.074 .042	.084 .054
Oconee 1, 2, 3					<u>6/19/68 - 6/19/69</u>			
	.021 .174	.036 .084	.075 .100	.051 .058	.062 .060	.043 .038	.061 .036	.081 .019
Oyster Creek	<u>400 ft</u>				<u>2/66 - 2/67</u>			
	.075 .044	.096 .037	.087 .052	.068 .055	.087 .039	.093 .040	.075 .047	.063 .040
Pallisades	<u>55 ft</u>				<u>9/67 - 8/68</u>			
	.204 .080	.113 .033	.027 .013	.030 .012	.058 .052	.046 .038	.072 .049	.081 .093

Table A.4-1 Site Wind Rose Data (cont):
Probability of Wind Blowing Towards Sector

Station	N S	NNE SSW	NE SW	ENE WSW	E W	ESE WNW	SE NW	SSE NNW
Palo Verde 1	<u>200 ft</u>				<u>8/13/73 - 8/13/74</u>			
	.055 .048	.073 .059	.144 .068	.082 .048	.068 .073	.047 .059	.052 .056	.035 .041
Peach Bottom 2, 3	<u>120 ft</u>				<u>8/67 - 7/69</u>			
	.085 .060	.064 .043	.046 .031	.052 .032	.069 .034	.095 .046	.115 .054	.109 .064
Pebble Springs	<u>30 ft</u>				<u>1/74 - 12/74</u>			
	.017 .012	.039 .019	.075 .050	.201 .055	.313 .035	.094 .028	.021 .020	.009 .014
Perkins	<u>30 ft</u>				<u>10/12/73 - 10/11/74</u>			
	.036 .068	.067 .066	.125 .104	.066 .067	.058 .063	.047 .037	.064 .044	.053 .034
Perry 1	<u>200 ft</u>				<u>5/1/72 - 4/30/73</u>			
	.105 .045	.095 .030	.092 .057	.084 .045	.081 .048	.054 .037	.057 .054	.042 .073
Phipps Bend	<u>33 ft</u>				<u>2/1/74 - 1/31/75</u>			
	.037 .054	.054 .110	.107 .112	.106 .045	.053 .020	.071 .018	.053 .021	.120 .019
Pilgrim 1	<u>72 ft</u>							
	.051 .051	.185 .038	.118 .042	.085 .035	.094 .048	.060 .031	.053 .033	.046 .030
Point Beach 1, 2	<u>150 ft</u>				<u>4/67 - 4/68</u>			
	.088 .096	.122 .070	.087 .055	.048 .022	.081 .020	.097 .018	.075 .031	.056 .036
Prairie 1, 2	<u>140 ft</u>				<u>6/1/71 - 5/31/72</u>			
	.065 .046	.031 .023	.025 .019	.031 .019	.073 .055	.102 .108	.125 .134	.065 .080
Quad Cities 1, 2	<u>400 ft</u>				<u>4/68 - 9/69</u>			
	.072 .068	.128 .051	.090 .042	.049 .028	.045 .037	.069 .033	.083 .075	.067 .063
Rancho Seco	<u>50 ft</u>				<u>1967 - 1969</u>			
	.066 .049	.073 .034	.069 .029	.107 .021	.114 .029	.078 .039	.100 .057	.074 .062
Riverbend 1	<u>135 ft</u>				<u>10/1/72 - 9/30/73</u>			
	.057 .069	.058 .066	.048 .066	.048 .060	.054 .076	.048 .082	.061 .072	.066 .067
H. B. Robinson 2	<u>120 ft</u>				<u>4/14/67 - 4/19/68</u>			
	.045 .141	.074 .114	.072 .095	.081 .050	.071 .040	.037 .035	.036 .038	.043 .029
Saint Lucie 1	<u>50 ft</u>				<u>11/1/72 - 12/31/73</u>			
	.062 .045	.056 .038	.063 .070	.046 .088	.030 .121	.041 .093	.053 .098	.029 .067
Salem 1, 2	<u>300 ft</u>				<u>6/69 - 5/71</u>			
	.067 .062	.062 .046	.060 .049	.056 .037	.073 .028	.095 .023	.132 .042	.094 .074
San Onofre	<u>10 m</u>				<u>1/25/73 - 1/24/76</u>			
	.066 .034	.061 .111	.054 .134	.045 .028	.088 .016	.109 .022	.060 .049	.031 .070
Seabrook 1	<u>30 ft</u>				<u>11/71 - 10/72</u>			
	.030 .039	.040 .024	.069 .033	.089 .046	.110 .038	.167 .041	.145 .043	.049 .037

Table A.4-1 Site Wind Rose Data (cont)
Probability of Wind Blowing Towards Sector

Station	N S	NNE SSW	NE SW	ENE WSW	E W	ESE WNW	SE NW	SSE NNW
Sequoyah 1, 2		<u>33 ft</u>			<u>4/21/71 - 3/31/72</u>			
	.066 .058	.151 .169	.161 .116	.48 .026	.024 .611	.024 .008	.035 .013	.070 .019
Shearon Harris		<u>10 m</u>			<u>1/76 - 12/76</u>			
	.079 .083	.107 .067	.098 .063	.079 .047	.053 .033	.054 .031	.057 .035	.062 .053
Skagit		<u>10 m</u>						
	.014 .037	.011 .021	.021 .041	.037 .028	.128 .109	.109 .058	.085 .039	.062 .020
Shoreham		<u>150 ft</u>			<u>10/1/73 - 9/30/74</u>			
	.060 .050	.129 .045	.095 .049	.050 .043	.079 .032	.103 .028	.094 .034	.066 .041
South Texas		<u>33 ft</u>			<u>7/20/73 - 7/20/74</u>			
	.148 .075	.046 .078	.029 .080	.010 .047	.015 .053	.014 .059	.020 .137	.037 .153
Virgin C. Sumner		<u>202 ft</u>			<u>1975</u>			
	.068 .029	.090 .042	.118 .080	.087 .070	.064 .059	.046 .041	.055 .052	.043 .056
Surry St 1, 2		<u>150 ft</u>			<u>11/67 - 12/69</u>			
	.064 .072	.082 .051	.082 .046	.062 .045	.059 .057	.061 .052	.087 .055	.081 .043
Susquehanna 1					<u>1956 - 1960</u>			
	.037 .046	.070 .039	.125 .049	.126 .054	.044 .040	.059 .062	.100 .031	.090 .029
Three Mile Island		<u>100 ft</u>			<u>4/71 - 3/72</u>			
	.054 .040	.045 .027	.054 .036	.059 .057	.001 .085	.092 .082	.091 .062	.070 .057
Trojan		<u>30 ft</u>			<u>9/1/71 - 8/31/72</u>			
	.203 .172	.070 .054	.026 .016	.013 .006	.022 .007	.037 .009	.070 .046	.132 .120
Turkey Point 1, 2		<u>30 ft</u>			<u>1969</u>			
	.038 .035	.041 .028	.047 .048	.027 .100	.027 .136	.047 .135	.051 .100	.077 .062
Vermont Yankee 1		<u>140 ft</u>			<u>8/67 - 7/68</u>			
	.072 .070	.027 .025	.018 .017	.023 .019	.069 .024	.086 .066	.117 .085	.196 .086
Vogtle		<u>30 ft</u>			<u>12/73 - 12/74</u>			
	.064 .043	.062 .043	.074 .072	.079 .065	.084 .069	.075 .060	.056 .063	.031 .060
Waterford 3		<u>30 ft</u>			<u>5/72 - 4/73</u>			
	.042 .046	.053 .092	.045 .088	.047 .059	.049 .029	.056 .100	.064 .083	.072 .077
Watts Bar 1, 2		<u>300 ft</u>			<u>7/1/73 - 6/30/75</u>			
	.033 .053	.109 .106	.183 .132	.089 .059	.040 .041	.131 .019	.035 .014	.077 .019
WPPS 1, 4		<u>33 ft</u>			<u>4/74 - 3/75</u>			
	.100 .164	.062 .045	.063 .036	.052 .031	.061 .022	.099 .026	.107 .040	.085 .075
WPPS 2		<u>33 ft</u>			<u>4/74 - 3/75</u>			
	.100 .164	.062 .045	.063 .036	.052 .031	.061 .022	.099 .026	.107 .040	.085 .075

Table A.4-1 Site Wind Ros. Data (cont)

Probability of Wind Blowing Towards Sector

Station	S	SSE	SE	ESE	E	ESE	SE	SSE
	S	SSW	SW	WSW	W	WSW	SW	SSW
WPPS 3, 5	<u>60 m</u> <u>5/73 - 4/74</u>							
	.037	.090	.124	.170	.125	.031	.015	.040
	.014	.019	.062	.074	.047	.052	.050	.037
Wolf Creek	<u>30 m</u> <u>6/3/73 - 5/31/75</u>							
	.080	.100	.040	.024	.030	.041	.044	.069
	.144	.058	.039	.035	.039	.046	.061	.111
Vanlee Howe	<u>30 ft</u> <u>10/71 - 9/72</u>							
	.101	.080	.052	.037	.039	.041	.072	.066
	.086	.054	.065	.063	.047	.036	.052	.061
Yellow Creek	<u>33 ft</u> <u>7/1/74 - 6/30/75</u>							
	.142	.097	.049	.039	.040	.050	.057	.087
	.037	.079	.049	.019	.021	.046	.066	.110
Zimmer	<u>30 ft</u> <u>3/1/72 - 2/28/75</u>							
	.108	.076	.068	.056	.051	.059	.047	.062
	.062	.011	.027	.011	.030	.054	.127	.129
Zion	<u>35 ft</u> <u>10/70</u>							
	.031	.078	.079	.113	.069	.076	.046	.071
	.046	.059	.037	.019	.035	.015	.060	.096

A.5 Economic Data

The input data to the economic model in CRAC2 can be divided into two groups: those which are national in character and those which are applicable to individual states. Appendix VI of WASH-1400 [6] contains a detailed discussion of these parameters.

The national data can be further divided into data which measure costs on a per capita basis, and data which measure costs on a per acre basis. Decontamination costs for business, residential, and public areas, relocation costs, consumed dairy products, and consumed nondairy products, are all measured in dollars per person. The decontamination cost for farm land is measured in dollars per acre. Table A.5-1 lists current figures for these cost parameters and in addition compares these costs with those contained in Appendix VI of WASH-1400.

WASH-1400 Appendix VI describes some of the decontamination techniques considered when the original costs estimates were made. It does not, however, give a detailed breakdown of costs. As an approximation, the decontamination costs were broken down into labor, energy, and durable goods (equipment) components. The breakdown of costs was assumed to be 40% labor, 50% energy, and 10% durable goods for farmland decontamination and 60%, 30%, and 10% for decontamination of public areas. Using data contained in the Statistical Abstract of the US [7], the change in the Consumer Price Index (CPI) from 1972 to 1979 was calculated for each of these areas. These factors are 1.69 for labor, 2.66 for energy, and 1.55 for durable goods. The updated decontamination costs were obtained by multiplying the original WASH-1400 cost figures by the appropriately weighted combinations of these CPI factors.

Relocation costs were calculated in Appendix VI as a combination of lost income, both individual and corporate, and moving costs. These costs, which were calculated on a per capita basis, are \$1,100 for lost individual income, \$940 for lost corporate income, and \$1,300 for transportation expenses. Based on data from the Statistical Abstract, the employee compensation rate has increased by a factor of 1.44 between 1973 and 1978. The nonfarm business gross national product (GNP) has increased by a factor of 1.54 and transportation services by a factor of 1.53 in the same period. The updated relocation cost was obtained by summing the products of each of the three costs and the appropriate factor.

The revised per capita value of residential, business, and public areas, and annual per capita dairy and nondairy consumption costs were derived from data contained in the Statistical Abstract of the U.S. The net value of residential, business, and public assets, less farm assets, was divided by the US population to obtain the updated per capita value of nonfarm assets. The updated agricultural consumption figures were obtained by dividing the total annual market value of these commodities by the US population. Per capita agricultural consumption figures are used by CRAC2 to determine radiation exposure through dairy and nondairy product ingestion.

The data, which are supplied on a state-by-state basis, all relate to farm costs and values. The input parameters are fraction of state area devoted to farming, average annual sale of farm products in dollars per acre, the fraction of farm sales resulting from dairy products, the average value of farmland in dollars per acre, and the major farming season. Table A.5-2 lists the values for all of these fields. The Statistical Abstract of the United States is the source for farmland value and farmland fraction. Farm sales and dairy share are found in reference [8]. The farming seasons are the same as the WASH-1400 figures.

Table A.5-1 National Economics Data

<u>Description</u>	<u>WASH-1400 Data</u>	<u>Current Data</u>
Decontamination cost for farmland (\$/acre)	230	500*
Decontamination cost for residential, business, and public property (\$/person)	1,700	4,400*
Value of residential, business, and public property (\$/person)	17,000	32,000*
Depreciation rate for improvements (yr ⁻¹)	0.2	0.2
Relocation cost (\$/person)	2,900	4,300**
Annual cost of dairy product consumption (\$/person)	--	135**
Annual cost of non-dairy product consumption (\$/person)	--	690**

*Represents 1979 statistics
 **Represents 1978 statistics

Table A.5-2 Agricultural Land Use Characteristics

State	Fraction of State Used as Farm Land*,**	Average Annual Sale of Farm Products† (\$/acre-year)	Average Share of Dairy Products‡ (\$ dairy/\$ products)	Average Value of Farmland† (\$/acre)	Major Farming Season
Maine	0.077	250	0.182	485	May-Sept
New Hampshire	0.097	150	0.444	802	May-Sept
Vermont	0.283	177	0.791	657	May-Sept
Massachusetts	0.123	372	0.283	1366	May-Sept
Rhode Island	0.081	476	0.220	2133	May-Sept
Connecticut	0.140	500	0.313	2158	May-Sept
New York	0.315	188	0.579	642	May-Sept
New Jersey	0.197	376	0.162	2222	May-Sept
Pennsylvania	0.307	239	0.413	669	May-Sept
Ohio	0.618	183	0.153	1516	May-Sept
Indiana	0.728	206	0.067	1498	May-Sept
Illinois	0.795	213	0.041	1786	May-Sept
Michigan	0.285	197	0.238	955	May-Sept
Wisconsin	0.520	194	0.598	807	May-Sept
Minnesota	0.563	160	0.185	854	May-Sept
Iowa	0.944	242	0.050	1458	May-Sept
Missouri	0.724	111	0.079	674	May-Sept
North Dakota	0.922	45	0.047	306	May-Sept
South Dakota	0.922	46	0.074	257	May-Sept
Nebraska	0.967	99	0.027	470	May-Sept
Kansas	0.915	92	0.034	437	May-Sept
Delaware	0.471	508	0.046	1725	April-Oct
Maryland	0.414	273	0.227	1799	April-Oct
Virginia	0.371	126	0.171	864	April-Oct
West Virginia	0.270	44	0.203	472	April-Oct
North Carolina	0.368	261	0.056	819	April-Oct
South Carolina	0.327	148	0.063	635	April-Oct
Georgia	0.417	164	0.058	609	April-Oct
Florida	0.368	233	0.077	930	April-Oct
Kentucky	0.557	141	0.117	792	April-Oct
Tennessee	0.507	118	0.140	669	April-Oct
Alabama	0.400	144	0.041	515	April-Oct
Mississippi	0.475	135	0.047	520	April-Oct
Arkansas	0.494	158	0.030	691	April-Oct
Louisiana	0.332	137	0.087	763	April-Oct
Oklahoma	0.782	68	0.051	442	April-Oct
Texas	0.811	54	0.053	354	April-Oct
Montana	0.658	20	0.026	186	May-Sept
Idaho	0.894	93	0.114	485	May-Sept
Wyoming	0.560	15	0.024	119	May-Sept
Colorado	0.570	69	0.039	332	April-Oct
New Mexico	0.600	21	0.056	100	April-Oct
Arizona	0.556	36	0.069	134	April-Oct
Utah	0.236	36	0.215	265	April-Oct
Nevada	0.127	19	0.117	104	April-Oct
Washington	0.369	132	0.138	586	May-Sept
Oregon	0.300	68	0.093	330	May-Sept
California	0.318	316	0.119	936	April-Oct

*Fraction of total state area (including water areas) devoted to agricultural use

**Reflect 1979 statistics

†Reflect 1978 statistics

References for Appendix A

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4. User's Manual for Single Source (CRSTER) Model, US Environmental Protection Agency, Office of Air and Waste Management, Research Triangle Park, NC, July 1977.
5. G. C. Holzworth, Mixing Heights, Wind Speeds, and Potential for Urban Air Pollution Throughout the Contiguous United States, Publ. No. AP-101, US Environmental Protection Agency, Office of Air Programs, Research Triangle Park, NC, 1972.
6. Reactor Safety Study, Appendix VI: Calculation of Reactor Accident Consequences, WASH-1400 (NUREG 75/014), US Nuclear Regulatory Commission, October 1975.
7. US Department of Commerce, 1979, Statistical Abstract of the United States.
8. US Department of Agriculture, Agricultural Statistics, 1979.

Appendix B: Reactor Core Radionuclide Inventories

B.1 Core Radionuclide Inventory

Reactor accident consequence calculations are often performed using the Reactor Safety Study [1] radionuclide inventory for a 3200 Mwt Westinghouse pressurized water reactor (PWR). This inventory, calculated for an end-of-cycle equilibrium core, has been used to represent both boiling water reactor (BWR) and PWR cores. Recently, however, an end-of-cycle equilibrium inventory for a 3412 Mwt Westinghouse PWR was calculated using the SANDIA-ORIGEN computer code [2]. This inventory, which was calculated using a 25% greater fuel burnup than used for the WASH-1400 inventory, was used to perform the reactor consequence calculations discussed in Chapter 2. (A spent fuel burnup of 26,400 MWd/MTU was assumed to calculate the WASH-1400 inventories.)

The 3412 Mwt PWR inventory was calculated by assuming that the three regions of the reactor core (each initially loaded with uranium enriched to 3.3% U-235) were operated at a constant specific power density of 38.3 MW/MTU charged. A three year refueling cycle and an 80% capacity factor were also assumed. This inventory is representative of an equilibrium core at a time when the three regions have average burnups of 11,000, 22,000, and 33,000 MWd/MTU charged (end-of-cycle).

The SANDIA-ORIGEN code calculates the time dependent activities of approximately 500 radionuclides; including activation products, fission products, and actinides. Of this number, only 54 radionuclides are expected to significantly impact reactor accident consequence calculations and as a result, are input to the CRAC2 code. The elimination of radionuclides from consideration was based on a number of parameters, such as quantity (curies), release fraction, radioactive half-life, dosimetry, and chemical characteristics [1]. Table B.1-1 lists the 54 radionuclides used to perform the consequence calculations. Also given is the activity of each radionuclide at the time the accident is assumed to occur. The reactor core inventories used to perform the power level sensitivity calculations discussed in Chapter 2 were obtained by linearly scaling (by thermal power level) the inventories presented in Table B.1-1.

Table B.1-1 Inventory of Radionuclides in the 3412 Mwt PWR Core

No.	Radionuclide	Radioactive Inventory Source (curies x 10 ⁻⁸)	Half-Life (days)
1	Cobalt-58	0.0075	71.0
2	Cobalt-60	0.000045	1,920
3	Krypton-85	0.0066	3,950
4	Krypton-85m	0.31	0.183
5	Krypton-87	0.57	0.0528
6	Krypton-88	0.77	0.117
7	Rubidium-86	0.00048	18.7
8	Strontium-89	0.96	52.1
9	Strontium-90	0.052	10,300
10	Strontium-91	1.2	0.403
11	Yttrium-90	0.055	2.67
12	Yttrium-91	1.2	59.0
13	Zirconium-95	1.5	65.2
14	Zirconium-97	1.6	0.71
15	Niobium-95	1.4	35.0
16	Molybdenum-99	1.7	2.8
17	Technetium-99m	1.4	0.25
18	Ruthenium-103	1.2	39.5
19	Ruthenium-105	0.82	0.185
20	Ruthenium-106	0.29	366
21	Rhodium-105	0.56	1.50
22	Tellurium-127	0.075	0.391
23	Tellurium-127m	0.0098	109
24	Tellurium-129	0.25	0.048
25	Tellurium-129m	0.067	34.0
26	Tellurium-131m	0.13	1.25
27	Tellurium-132	1.3	3.25
28	Antimony-127	0.077	3.88
29	Antimony-129	0.27	0.179
30	Iodine-131	0.87	8.05
31	Iodine-132	1.3	0.0958
32	Iodine-133	1.8	0.875
33	Iodine-134	2.0	0.0366
34	Iodine-135	1.7	0.280
35	Xenon-133	1.8	5.28
36	Xenon-135	0.38	0.384
37	Cesium-134	0.13	750
38	Cesium-136	0.039	13.0
39	Cesium-137	0.065	11,000
40	Barium-140	1.7	12.8
41	Lanthanum-140	1.7	1.67
42	Cerium-141	1.5	32.3
43	Cerium-143	1.5	1.38
44	Cerium-144	0.92	284
45	Praseodymium-143	1.5	13.7
46	Neodymium-147	0.65	11.1
47	Neptunium-239	19.0	2.35
48	Plutonium-238	0.0012	32,500
49	Plutonium-239	0.00026	8.9 x 10 ⁶
50	Plutonium-240	0.00029	2.5 x 10 ⁶
51	Plutonium-241	0.054	5,350
52	Americium-241	0.000036	1.6 x 10 ⁵
53	Curium-242	0.014	163
54	Curium-244	0.00084	6,630

B.2 Radionuclide Inventory Impacts on Reactor Accident Consequences

The potential impacts of different radionuclide inventories on predicted accident consequences, and the appropriateness of inventory scaling, were examined using the CRAC2 code [3]. Consequence calculations were performed using end-of-cycle equilibrium inventories for the WASH-1400 3200 Mwt Westinghouse PWR, the 3412 Mwt Westinghouse PWR, a 3578 Mwt General Electric (GE) BWR, and a 1518 Mwt Westinghouse PWR. Calculations were also performed for the 3412 Mwt PWR at 1/3 and 2/3 of the way through the annual operating cycle. (The 3578 Mwt BWR and 1518 Mwt PWR inventories, like those for the 3412 Mwt PWR, were generated with the SANDIA-ORIGEN computer code.) The operating characteristics for the four reactors are summarized in Table B.2-1. The 3412 Mwt and 1518 Mwt PWRs and the 3578 Mwt BWR are considered to be representative of current reactor designs and compositions.

Table B.2-2 summarizes the four reactor inventories for selected radionuclides. In general, inventories of short-lived radionuclides are proportional to reactor thermal power level, while inventories of long-lived radionuclides are proportional to burnup; both are influenced by in-core fuel management plans.

Consequences were calculated assuming (1) an SST1 release (large-scale core melt with uncontrolled release directly to the atmosphere), (2) Indian Point population and wind-rose data, (3) New York City weather data, and (4) a distribution of evacuations within 10 miles of the reactor.* Table B.2-3 summarizes the consequence calculation results from which the following observations can be made.

- 1) The 3412 Mwt PWR land interdiction and decontamination results are approximately 30% larger than those for the WASH-1400 PWR. Differences for other consequences are somewhat less (10-17%).

*Consists of a 30%, 40%, 30% weighting of a 10 mile per hour evacuation after 1, 3, and 5 hour delays, respectively.

Table B.2-1 Reactor Operating Characteristics

Characteristic	WASH-1400	3412 MWt PWR	3578 MWt ^a BWR	1518 MWt PWR
Total Uranium in Fresh Core (MT)	---	89.1	136.7	47.5
Initial U-235 Enrichment (percent)	3.3	3.3	2.66, 2.83	3.2
Refueling Cycle	annually	annually	annually	annually
Number of Years an Element Spends in Core (years)	3	3	3,4	3
Capacity Factor (Percent of time at Full Power)	---	80	80	80
Average Fuel Burnup at dis- charge (MWd/MTU)	26,400	33,600	---	28,000
Average Power Density (MW/MTU)	40	38.3	26.1	32.0

^aThe SANDIA-ORIGEN BWR calculations were performed on a per fuel assembly basis. The code generated radionuclide inventories by blending individual assembly results.

Table B.2-2 Inventory of Selected Radionuclides for the Reactors Studied.

Radionuclide	Half-Life (days)	End-of-Cycle 3412 Mwt PWR (Ci)	(Designated Inventory) ÷ (3412 Mwt PWR Inventory)				
			WASH-1400		End-of-Cycle 1518 Mwt PWR	1/3 Cycle 3412 Mwt PWR	2/3 Cycle 3412 Mwt PWR
			End-of-Cycle 3200 Mwt PWR	End-of-Cycle 2578 Mwt BWR			
Kr-85	0.117	6.64 x 10 ⁵	1.03	1.36	0.44	0.68	0.84
Mo-99	2.8	1.66 x 10 ⁸	0.94	1.05	0.45	1.02	1.01
Tc-99m	0.25	1.43 x 10 ⁸	1.00	1.05	0.45	1.03	1.01
Ru-103	39.5	1.25 x 10 ⁸	0.85	1.06	0.44	0.87	0.96
Ru-105	0.185	8.22 x 10 ⁷	0.88	1.07	0.43	0.86	0.94
Ru-106	366	2.90 x 10 ⁷	0.86	1.24	0.42	0.66	0.83
Te-129m	0.34	6.70 x 10 ⁶	0.79	1.06	0.44	0.88	0.96
Te-131m	1.25	1.28 x 10 ⁷	1.00	1.07	0.44	0.97	0.98
Te-132	3.25	1.27 x 10 ⁸	0.92	1.06	0.45	1.00	1.00
Sb-129	0.179	2.72 x 10 ⁷	1.22	1.06	0.44	0.93	0.97
I-131	8.05	8.74 x 10 ⁷	0.98	1.06	0.45	0.99	1.00
I-132	0.096	1.29 x 10 ⁸	0.92	1.05	0.44	0.99	1.00
I-133	0.875	1.84 x 10 ⁸	0.94	1.05	0.45	1.02	1.01
I-134	0.037	2.02 x 10 ⁸	0.95	1.05	0.45	1.02	1.01
I-135	0.28	1.73 x 10 ⁸	0.88	1.06	0.45	1.02	1.01
Cs-134	750	1.26 x 10 ⁷	0.60	1.20	0.38	0.55	0.76
Cs-136	13.0	3.91 x 10 ⁶	0.77	1.04	0.41	0.67	0.84
Cs-137	11,000	6.54 x 10 ⁶	0.72	1.39	0.44	0.67	0.83
Ba-140	12.8	1.68 x 10 ⁸	0.94	1.05	0.45	1.02	1.01
Ce-144	284	9.15 x 10 ⁷	0.92	1.14	0.45	0.77	0.90

Table B.2-3 Summary of CRAC2 Consequence Predictions.

Consequence	End-of-Cycle 3412 Mwt PWR	WASH-1400 End-of-Cycle 3200 Mwt PWR	End-of-Cycle 3578 Mwt BWR	1/3 Cycle 3412 Mwt PWR	2/3 Cycle 3412 Mwt PWR	End-of-Cycle 1518 Mwt PWR	Scaled ¹
							End-of-Cycle 1518 Mwt PW
Mean Early Fatalities	800	690	890	750	780	150	150
Mean Early Injuries	3600	3000	4100	3400	3500	960	970
Mean Latent Cancer Fatalities	7800	7000	8400	6800	7300	5300	5400
Mean Land Interdiction Area (km ²)	200	140	280	130	160	92	97
Mean Land Decontamination Area (km ²)	3800	2800	5900	2800	3100	2000	2100

¹Inventory = (1518 Mwt/3412 Mwt) x (3412 Mwt PWR inventory).

- 2) The 3578 MWt BWR land decontamination and interdiction consequences are approximately 50% larger than those for the 3412 MWt PWR. Again, differences for other consequences are on the order of 10%.
- 3) Comparison of the 3412 and 1518 MWt PWR results indicate reductions in reactor size result in proportionately larger reductions in early consequences.
- 4) Comparison of the 1/3, 2/3, and end-of-cycle 3412 MWt PWR results indicate that differences in radionuclide inventory during the annual operating cycle have little influence on early consequences. However, time of the accident during the cycle does significantly influence predicted latent cancer fatalities and areas of land interdiction and decontamination.
- 5) There is essentially no difference in consequences for the 1518 MWt PWR predicted by using either the calculated or scaled inventories.

Differences in latent cancer fatality, land interdiction, and land decontamination consequences largely result from long-lived radionuclide inventory differences (e.g., Cs-137). Differences in early consequences are primarily due to differences in short-lived radionuclide inventories.

In summary, the results presented above indicate that reactor accident consequences are sensitive to differences in radionuclide inventories due to reactor size and design. Because of in-core fuel management plans, boiling water reactors will likely have larger inventories of long-lived radionuclides than a pressurized water reactor of the same size. Therefore, using PWR inventories for BWR consequence calculations could underestimate latent consequences. The time of a reactor accident during the annual operating cycle has little influence on early consequences; however, it can significantly influence latent effects. Reductions in reactor size will lead to substantial reductions in early consequences, more so than would be expected based on differences in reactor power levels. In addition, linear scaling of radionuclide inventories by thermal power level is adequate for consequence calculations, provided that the reactor of interest has operating and design characteristics similar to those of the reactor from which the inventories are scaled.

References for Appendix B

1. "Reactor Safety Study Appendix VI: Calculation of Reactor Accident Consequences," WASH-1400 (NUREG 75/014), U.S. Nuclear Regulatory Commission, October 1975.
2. D. E. Bennett, Radionuclide Core Inventories for Standard PWR and BWR Fuel Management Plans, SAND82-1111, NUREG/CR-2724, Sandia National Laboratories, Albuquerque, NM, to be published.
3. R. M. Ostmeyer, "Radionuclide Inventory Impacts on Reactor Accident Consequences," Transactions of the American Nuclear Society (November 1981).

Appendix C: Site Specific Consequence Estimates

This appendix presents the consequence estimates for each of the 91 sites analyzed in Chapter 2. It is important to note that in each case the calculations assumed (1) that the site contained an 1120 MWe PWR, (2) meteorology based on the most appropriate regional National Weather Service Station (from among the 29 detailed in Appendix A), (3) actual site wind rose and population, (4) a summary evacuation (all persons within 10 miles evacuate at 10 mph after delays of 1, 3, or 5 hours, with probability .3, .4, .3, respectively) and (5) hypothetical releases of radioactive materials (see Section 2.3, Chapter 2). Thus the estimates presented in this appendix are only a guide to the impact of site characteristics (principally population distribution) on predicted consequences. In no way are these to be taken as estimates of existing/reactor combinations.

Table C.1 provides a summary of the mean early fatalities, early injuries, and latent cancer fatalities for SST1, SST2, and SST3. Figures C-1 through C-18 contain early fatality, early injury, and latent cancer fatality CCDFs for each of the 91 sites, conditional on an SST1 release and assuming the 1120 MWe PWR, summary evacuation, regional meteorology, and actual site population and wind rose. Since some of these characteristics do not exactly duplicate the characteristics of the actual reactor/site combinations, the CCDFs are not to be used in place of actual risk estimates for existing reactor/site combinations.

Table C-1. Mean Number (Per Reactor-Year) of Early Fatalities, Early Injuries and Latent Cancer Fatalities for each of 91 Sites, for SST1, SST2, or SST3 Accident Source Terms.

Assumptions:

- (1) Standard 1120 MWe PWR
- (2) Summary Evacuation
- (3) Actual Site Population and Wind rose
- (4) Best Estimate Meteorology

	Mean Early Fatalities*			Mean Early Injuries*			Mean Latent Cancer Fatalities*		
	SST1	SST2	SST3	SST1	SST2	SST3	SST1	SST2	SST3
Allens Creek	31xP ₁	0xP ₂	0xP ₃	93xP ₁	0.9xP ₂	0xP ₃	620xP ₁	49xP ₂	0.2xP ₃
Arkansas	17xP ₁	0xP ₂	0xP ₃	150xP ₁	0.2xP ₂	0xP ₃	950xP ₁	82xP ₂	0.3xP ₃
Bailly	58xP ₁	0xP ₂	0xP ₃	1200xP ₁	0.5xP ₂	0xP ₃	3300xP ₁	260xP ₂	0.9xP ₃
Beaver Valley	150xP ₁	0xP ₂	0xP ₃	1200xP ₁	0.4xP ₂	0xP ₃	3400xP ₁	200xP ₂	0.6xP ₃
Bellefonte	63xP ₁	0.08xP ₂	0xP ₃	110xP ₁	5.6xP ₂	0xP ₃	1000xP ₁	70xP ₂	0.3xP ₃
Big Rock Pt.	15xP ₁	0xP ₂	0xP ₃	90xP ₁	0.5xP ₂	0xP ₃	680xP ₁	53xP ₂	0.2xP ₃
Black Fox	13xP ₁	0xP ₂	0xP ₃	220xP ₁	0.01xP ₂	0xP ₃	780xP ₁	69xP ₂	0.3xP ₃
Braidwood	160xP ₁	0.05xP ₂	0xP ₃	420xP ₁	10xP ₂	0xP ₃	3200xP ₁	240xP ₂	0.9xP ₃
Browns Ferry	25xP ₁	0xP ₂	0xP ₃	220xP ₁	0.03xP ₂	0xP ₃	970xP ₁	69xP ₂	0.3xP ₃
Brunswick	12xP ₁	0xP ₂	0xP ₃	120xP ₁	0.01xP ₂	0xP ₃	890xP ₁	98xP ₂	0.4xP ₃

*Detailed Probabilistic Risk Assessments (PRAs) have not been performed for all reactors. Therefore, consequence calculations were performed in this study using Siting Source Terms (SSTs) defined by NRC (see Section 2.3.1, Chapter 2). By adjusting the probabilities associated with each of the source terms, the set can be made to approximately represent any current LWR design. Based on currently available PRAs, NRC has suggested that representative probabilities for the SSTs are: P₁ for SST1 = 1 x 10⁻⁵, P₂ for SST2 = 2 x 10⁻⁵, and P₃ for SST3 = 1 x 10⁻⁴. There are very large variations (factors of 10 to 100) in the accident probabilities associated with a specific design.

Caution should be used when applying these numbers. Probability times consequence is not an adequate representation of risk; it provides only a common measure for comparative purposes (i.e., rank ordering). The Complementary Cumulative Distribution Functions (shown in Figure C-1 through C-18) are a better representation of risk.

Table C-1. (continued)

	Mean Early Fatalities*			Mean Early Injuries*			Mean Latent Cancer Fatalities*		
	SST1	SST2	SST3	SST1	SST2	SST3	SST1	SST2	SST3
Byron	54xP ₁	0.09xP ₂	0xP ₃	330xP ₁	4.3xP ₂	0xP ₃	2500xP ₁	190xP ₂	0.7xP ₃
Callaway	10xP ₁	0xP ₂	0xP ₃	100xP ₁	0.04xP ₂	0xP ₃	1200xP ₁	97xP ₂	0.3xP ₃
Calvert Cliffs	18xP ₁	0xP ₂	0xP ₃	170xP ₁	0.08xP ₂	0xP ₃	2400xP ₁	120xP ₂	0.4xP ₃
Catawba	100xP ₁	0xP ₂	0xP ₃	710xP ₁	0.2xP ₂	0xP ₃	1500xP ₁	110xP ₂	0.4xP ₃
Cherokee	27xP ₁	0xP ₂	0xP ₃	250xP ₁	0.1xP ₂	0xP ₃	1200xP ₁	76xP ₂	0.3xP ₃
Clinton	16xP ₁	0xP ₂	0xP ₃	130xP ₁	0.7xP ₂	0xP ₃	2300xP ₁	170xP ₂	0.7xP ₃
Comanche Peak	1.3xP ₁	0xP ₂	0xP ₃	37xP ₁	0xP ₂	0xP ₃	640xP ₁	49xP ₂	0.2xP ₃
Cooper	4.7xP ₁	0xP ₂	0xP ₃	47xP ₁	0.09xP ₂	0xP ₃	900xP ₁	81xP ₂	0.3xP ₃
Crystal River	21xP ₁	0xP ₂	0xP ₃	88xP ₁	0.9xP ₂	0xP ₃	590xP ₁	66xP ₂	0.3xP ₃
Davis-Besse	21xP ₁	0xP ₂	0xP ₃	420xP ₁	0.6xP ₂	0xP ₃	2600xP ₁	160xP ₂	0.5xP ₃
Diablo Canyon	4.7xP ₁	0xP ₂	0xP ₃	50xP ₁	0xP ₂	0xP ₃	1200xP ₁	98xP ₂	0.4xP ₃
Donald C. Cook	55xP ₁	0.04xP ₂	0xP ₃	590xP ₁	2.2xP ₂	0xP ₃	2500xP ₁	120xP ₂	0.4xP ₃
Dresden	42xP ₁	0xP ₂	0xP ₃	540xP ₁	0.3xP ₂	0xP ₃	3300xP ₁	260xP ₂	0.9xP ₃
Duane Arnold	21xP ₁	0xP ₂	0xP ₃	380xP ₁	0.4xP ₂	0xP ₃	1700xP ₁	190xP ₂	0.8xP ₃
Fermi	160xP ₁	0.08xP ₂	0xP ₃	970xP ₁	7.1xP ₂	0xP ₃	3000xP ₁	200xP ₂	0.6xP ₃
Fitzpatrick	5.0xP ₁	0xP ₂	0xP ₃	110xP ₁	0.06xP ₂	0xP ₃	1200xP ₁	57xP ₂	0.2xP ₃
Forked River	84xP ₁	0xP ₂	0xP ₃	530xP ₁	0.8xP ₂	0xP ₃	4400xP ₁	200xP ₂	0.6xP ₃
Fort Calhoun	50xP ₁	0.1xP ₂	0xP ₃	440xP ₁	3.0xP ₂	0xP ₃	1100xP ₁	110xP ₂	0.4xP ₃
Ft. St. Vrain	15xP ₁	0xP ₂	0xP ₃	220xP ₁	0xP ₂	0xP ₃	810xP ₁	82xP ₂	0.3xP ₃
Ginna	11xP ₁	0xP ₂	0xP ₃	370xP ₁	0.1xP ₂	0xP ₃	1900xP ₁	89xP ₂	0.3xP ₃
Grand Gulf	14xP ₁	0xP ₂	0xP ₃	73xP ₁	0.7xP ₂	0xP ₃	700xP ₁	60xP ₂	0.3xP ₃
Haddam Neck	110xP ₁	0xP ₂	0xP ₃	890xP ₁	1.2xP ₂	0xP ₃	2100xP ₁	160xP ₂	0.5xP ₃

*See footnote, page C-2.

Table C-1. (continued)

	Mean Early Fatalities*			Mean Early Injuries*			Mean Latent Cancer Fatalities*		
	SST1	SST2	SST3	SST1	SST2	SST3	SST1	SST2	SST3
Hartsville	19xP ₁	0xP ₂	0xP ₃	140xP ₁	0.04xP ₂	0xP ₃	970xP ₁	64xP ₂	0.2xP ₃
Hatch	4xP ₁	0xP ₂	0xP ₃	62xP ₁	0.04xP ₂	0xP ₃	770xP ₁	64xP ₂	0.2xP ₃
Hope Creek	120xP ₁	0xP ₂	0xP ₃	440xP ₁	0xP ₂	0xP ₃	3000xP ₁	160xP ₂	0.5xP ₃
Indian Pt.	830xP ₁	0.08xP ₂	0xP ₃	3600xP ₁	18xP ₂	0xP ₃	8100xP ₁	590xP ₂	1.8xP ₃
Joseph M. Farley	12xP ₁	0xP ₂	0xP ₃	85xP ₁	0.03xP ₂	0xP ₃	670xP ₁	56xP ₂	0.2xP ₃
Kewaunee	1.2xP ₁	0xP ₂	0xP ₃	78xP ₁	0xP ₂	0xP ₃	1200xP ₁	70xP ₂	0.3xP ₃
LaCrosse	32xP ₁	0xP ₂	0xP ₃	200xP ₁	1.8xP ₂	0xP ₃	850xP ₁	58xP ₂	0.2xP ₃
La Salle	26xP ₁	0xP ₂	0xP ₃	180xP ₁	0.6xP ₂	0xP ₃	2800xP ₁	200xP ₂	0.7xP ₃
Limerick	970xP ₁	2.2xP ₂	0xP ₃	2800xP ₁	6.6xP ₂	0xP ₃	5400xP ₁	370xP ₂	1.3xP ₃
Maine Yankee	4.1xP ₁	0xP ₂	0xP ₃	34xP ₁	0xP ₂	0xP ₃	770xP ₁	29xP ₂	0.1xP ₃
Marble Hill	28xP ₁	0xP ₂	0xP ₃	420xP ₁	0xP ₂	0xP ₃	2400xP ₁	180xP ₂	0.7xP ₃
McGuire	130xP ₁	0xP ₂	0xP ₃	680xP ₁	0xP ₂	0xP ₃	1600xP ₁	130xP ₂	0.5xP ₃
Midland	320xP ₁	0.2xP ₂	0xP ₃	1100xP ₁	1.3xP ₂	0xP ₃	2200xP ₁	130xP ₂	0.5xP ₃
Millstone	240xP ₁	0.02xP ₂	0xP ₃	990xP ₁	4.5xP ₂	0xP ₃	3200xP ₁	160xP ₂	0.6xP ₃
Monticello	12xP ₁	0xP ₂	0xP ₃	200xP ₁	0.08xP ₂	0xP ₃	1100xP ₁	98xP ₂	0.4xP ₃
Nine Mile Pt.	5.2xP ₁	0xP ₂	0xP ₃	110xP ₁	0.06xP ₂	0xP ₃	1200xP ₁	58xP ₂	0.2xP ₃
North Anna	14xP ₁	0xP ₂	0xP ₃	92xP ₁	0.08xP ₂	0xP ₃	1800xP ₁	75xP ₂	0.3xP ₃
Oconee	2.0xP ₁	0xP ₂	0xP ₃	240xP ₁	0.03xP ₂	0xP ₃	1100xP ₁	70xP ₂	0.3xP ₃
Oyster Creek	84xP ₁	0xP ₂	0xP ₃	530xP ₁	0.8xP ₂	0xP ₃	4400xP ₁	200xP ₂	0.6xP ₃
Palisades	37xP ₁	0.02xP ₂	0xP ₃	250xP ₁	1.3xP ₂	0xP ₃	1700xP ₁	90xP ₂	0.3xP ₃
Palo Verde	5.8xP ₁	0xP ₂	0xP ₃	59xP ₁	0.2xP ₂	0xP ₃	450xP ₁	26xP ₂	0.09xP ₃
Peach Bottom	97xP ₁	0xP ₂	0xP ₃	400xP ₁	0.02xP ₂	0xP ₃	2800xP ₁	140xP ₂	0.4xP ₃

*See footnote, page C-2.

Table C-1. (continued)

	Mean Early Fatalities*			Mean Early Injuries*			Mean Latent Cancer Fatalities*		
	SST1	SST2	SST3	SST1	SST2	SST3	SST1	SST2	SST3
Pebble Springs	0.41xP ₁	0xP ₂	0xP ₃	3.7xP ₁	0xP ₂	0xP ₃	230xP ₁	18xP ₂	0.07xP ₃
Perkins	98xP ₁	0xP ₂	0xP ₃	520xP ₁	2.1xP ₂	0xP ₃	1500xP ₁	120xP ₂	0.5xP ₃
Perry	95xP ₁	0.07xP ₂	0xP ₃	520xP ₁	4.2xP ₂	0xP ₃	2500xP ₁	160xP ₂	0.6xP ₃
Phipps Bed	170xP ₁	0.3xP ₂	0xP ₃	300xP ₁	16xP ₂	0xP ₃	1300xP ₁	82xP ₂	0.3xP ₃
Pilgrim	71xP ₁	0.02xP ₂	0xP ₃	300xP ₁	2.4xP ₂	0xP ₃	1500xP ₁	85xP ₂	0.3xP ₃
Pt. Beach	7.7xP ₁	0xP ₂	0xP ₃	110xP ₁	0.3xP ₂	0xP ₃	1400xP ₁	77xP ₂	0.3xP ₃
Prairie Is.	56xP ₁	0xP ₂	0xP ₃	260xP ₁	2.4xP ₂	0xP ₃	1400xP ₁	110xP ₂	0.4xP ₃
Quad Cities	17xP ₁	0xP ₂	0xP ₃	290xP ₁	0.04xP ₂	0xP ₃	1900xP ₁	170xP ₂	0.7xP ₃
Rancho Seco	15xP ₁	0xP ₂	0xP ₃	110xP ₁	0.02xP ₂	0xP ₃	870xP ₁	87xP ₂	0.3xP ₃
River Bend	31xP ₁	0xP ₂	0xP ₃	200xP ₁	0.2xP ₂	0xP ₃	750xP ₁	60xP ₂	0.2xP ₃
Robinson	16xP ₁	0xP ₂	0xP ₃	170xP ₁	0.01xP ₂	0xP ₃	880xP ₁	59xP ₂	0.2xP ₃
St. Lucie	77xP ₁	0xP ₂	0xP ₃	310xP ₁	0.6xP ₂	0xP ₃	700xP ₁	69xP ₂	0.4xP ₃
Salem	120xP ₁	0xP ₂	0xP ₃	440xP ₁	0xP ₂	0xP ₃	3000xP ₁	160xP ₂	0.5xP ₃
San Onofre	11xP ₁	0xP ₂	0xP ₃	150xP ₁	0xP ₂	0xP ₃	1800xP ₁	150xP ₂	0.5xP ₃
Seabrook	13xP ₁	0xP ₂	0xP ₃	210xP ₁	0.04xP ₂	0xP ₃	1000xP ₁	54xP ₂	0.2xP ₃
Sequoyah	110xP ₁	0xP ₂	0xP ₃	690xP ₁	0.6xP ₂	0xP ₃	1300xP ₁	95xP ₂	0.3xP ₃
Shearon Harris	40xP ₁	0xP ₂	0xP ₃	260xP ₁	0.4xP ₂	0xP ₃	1300xP ₁	110xP ₂	0.4xP ₃
Shoreham	140xP ₁	0xP ₂	0xP ₃	870xP ₁	1.9xP ₂	0xP ₃	3400xP ₁	170xP ₂	0.5xP ₃
Skagit	50xP ₁	0xP ₂	0xP ₃	370xP ₁	0.4xP ₂	0xP ₃	500xP ₁	49xP ₂	0.2xP ₃
South Texas	5.2xP ₁	0xP ₂	0xP ₃	32xP ₁	0xP ₂	0xP ₃	610xP ₁	43xP ₂	0.2xP ₃
Surry	65xP ₁	0xP ₂	0xP ₃	330xP ₁	0xP ₂	0xP ₃	1700xP ₁	95xP ₂	0.3xP ₃
Susquehanna	180xP ₁	0xP ₂	0xP ₃	700xP ₁	0.2xP ₂	0xP ₃	3300xP ₁	150xP ₂	0.5xP ₃

*See footnote, page C-2.

Table C-1. (continued)

	Mean Early Fatalities*			Mean Early Injuries*			Mean Latent Cancer Fatalities*		
	SST1	SST2	SST3	SST1	SST2	SST3	SST1	SST2	SST3
Three Mile Island	240xP ₁	0xP ₂	0xP ₃	1200xP ₁	4.5xP ₂	0xP ₃	3500xP ₁	170xP ₂	0.6xP ₃
Trojan	46xP ₁	0.1xP ₂	0xP ₃	350xP ₁	3.8xP ₂	0xP ₃	1100xP ₁	73xP ₂	0.3xP ₃
Turkey Pt.	31xP ₁	0xP ₂	0xP ₃	460xP ₁	0xP ₂	0xP ₃	690xP ₁	83xP ₂	0.4xP ₃
Vermont Yankee	130xP ₁	0xP ₂	0xP ₃	320xP ₁	4.4xP ₂	0xP ₃	1800xP ₁	72xP ₂	0.3xP ₃
Virgil Summer	12xP ₁	0xP ₂	0xP ₃	120xP ₁	0xP ₂	0xP ₃	1000xP ₁	63xP ₂	0.2xP ₃
Vogtle	0.07xP ₁	0xP ₂	0xP ₃	85xP ₁	0xP ₂	0xP ₃	900xP ₁	70xP ₂	0.3xP ₃
WPPSS 1,4	0.1xP ₁	0xP ₂	0xP ₃	110xP ₁	0xP ₂	0xP ₃	310xP ₁	37xP ₂	0.2xP ₃
WPPSS 2	1.0xP ₁	0xP ₂	0xP ₃	120xP ₁	0xP ₂	0xP ₃	720xP ₁	53xP ₂	0.2xP ₃
WPPSS 3,5	0.1xP ₁	0xP ₂	0xP ₃	110xP ₁	0xP ₂	0xP ₃	310xP ₁	37xP ₂	0.2xP ₃
Waterford	170xP ₁	0.2xP ₂	0xP ₃	580xP ₁	8.3xP ₂	0xP ₃	990xP ₁	93xP ₂	0.4xP ₃
Watts Bar	13xP ₁	0xP ₂	0xP ₃	110xP ₁	0.02xP ₂	0xP ₃	1000xP ₁	66xP ₂	0.3xP ₃
Wolf Creek	2.4xP ₁	0xP ₂	0xP ₃	34xP ₁	0.04xP ₂	0xP ₃	760xP ₁	70xP ₂	0.3xP ₃
Yankee Rowe	18xP ₁	0xP ₂	0xP ₃	180xP ₁	0.05xP ₂	0xP ₃	2300xP ₁	100xP ₂	0.2xP ₃
Yellow Creek	5.6xP ₁	0xP ₂	0xP ₃	68xP ₁	0xP ₂	0xP ₃	850xP ₁	63xP ₂	0.3xP ₃
Zimmer	46xP ₁	0xP ₂	0xP ₃	670xP ₁	0.4xP ₂	0xP ₃	2400xP ₁	170xP ₂	0.6xP ₃
Zion	520xP ₁	4.1xP ₂	0xP ₃	1600xP ₁	32xP ₂	0xP ₃	4000xP ₁	330xP ₂	1.2xP ₃

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-7

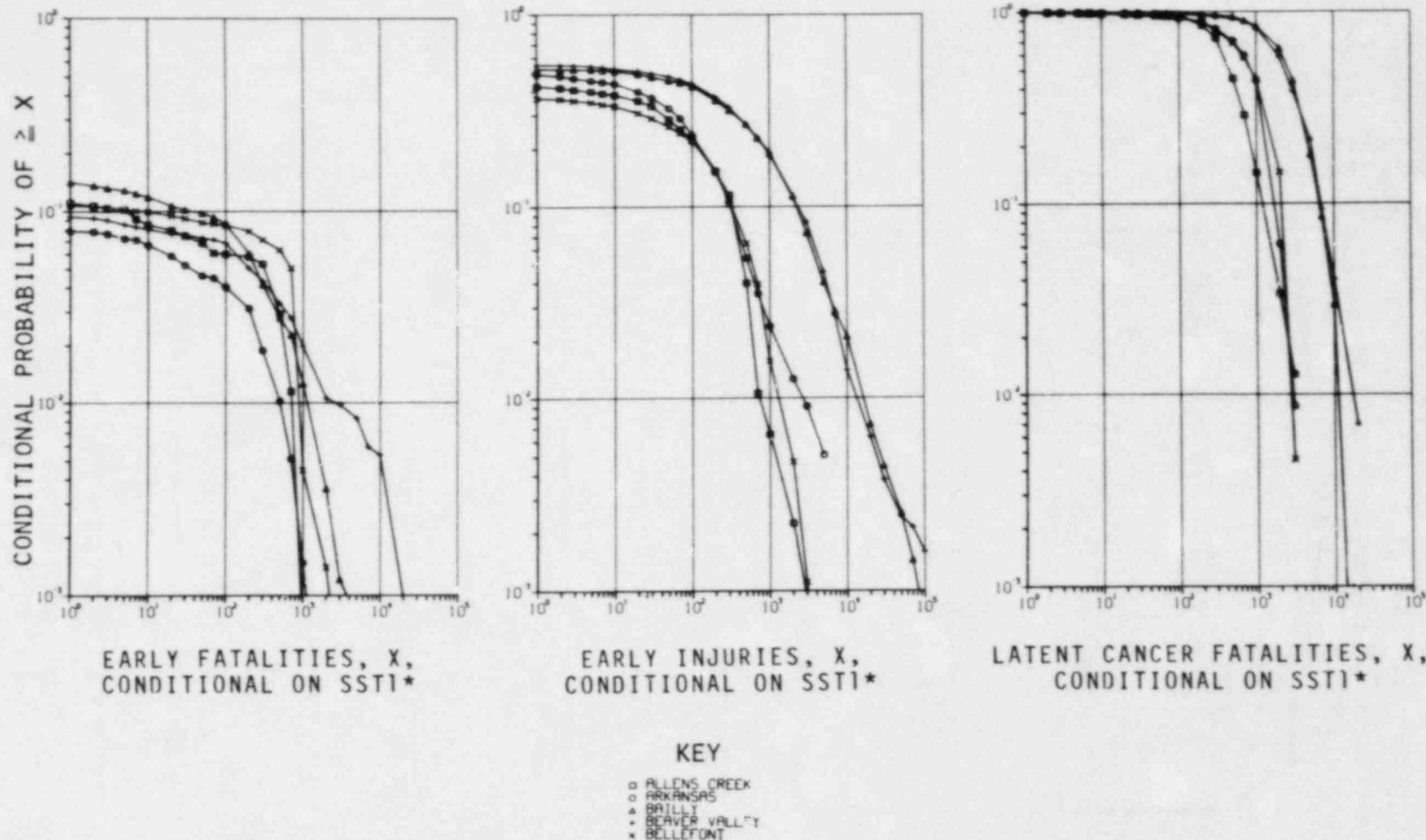


Figure C-1: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release. Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

8-C

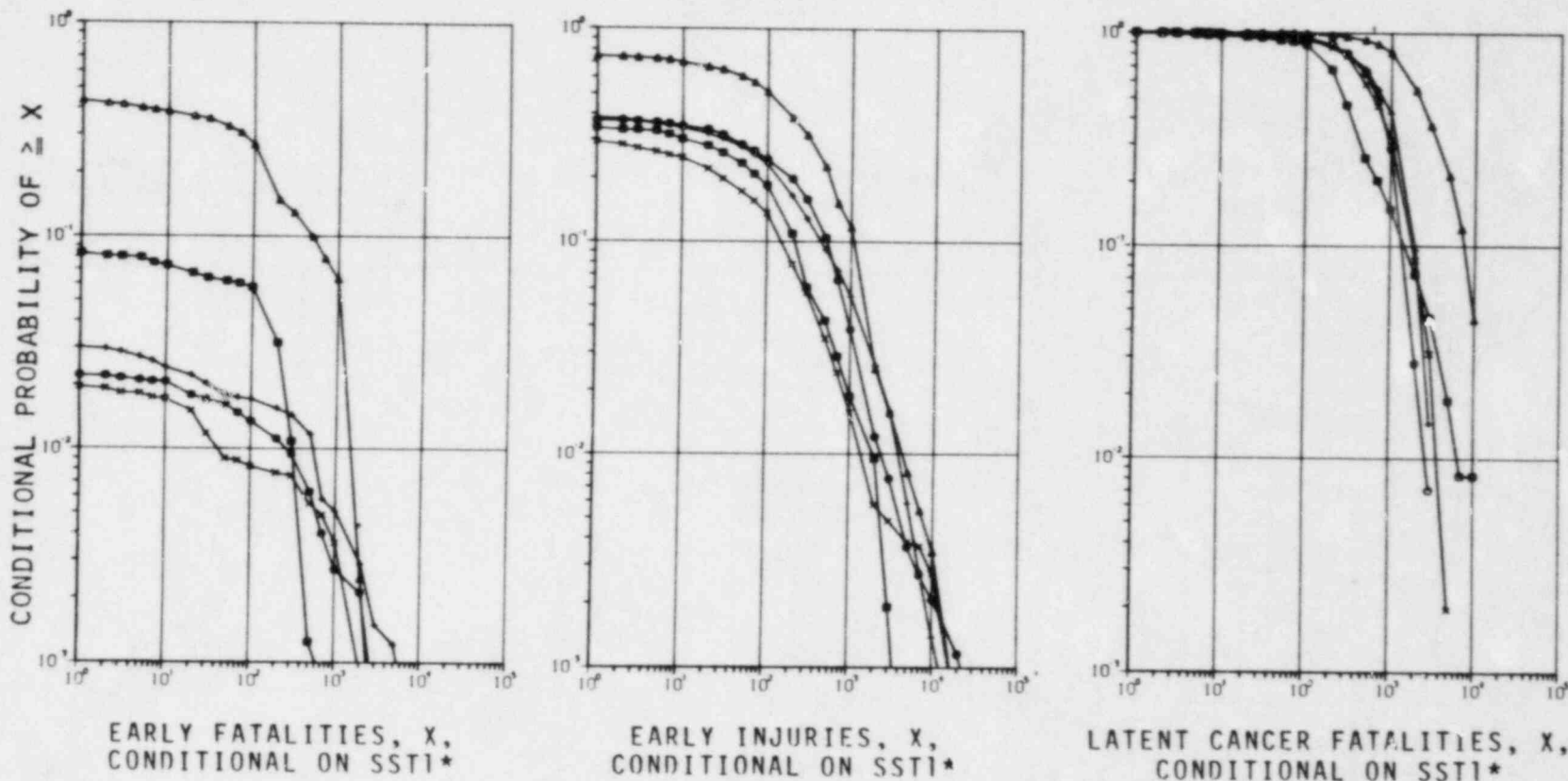


Figure C-2: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release. Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-3

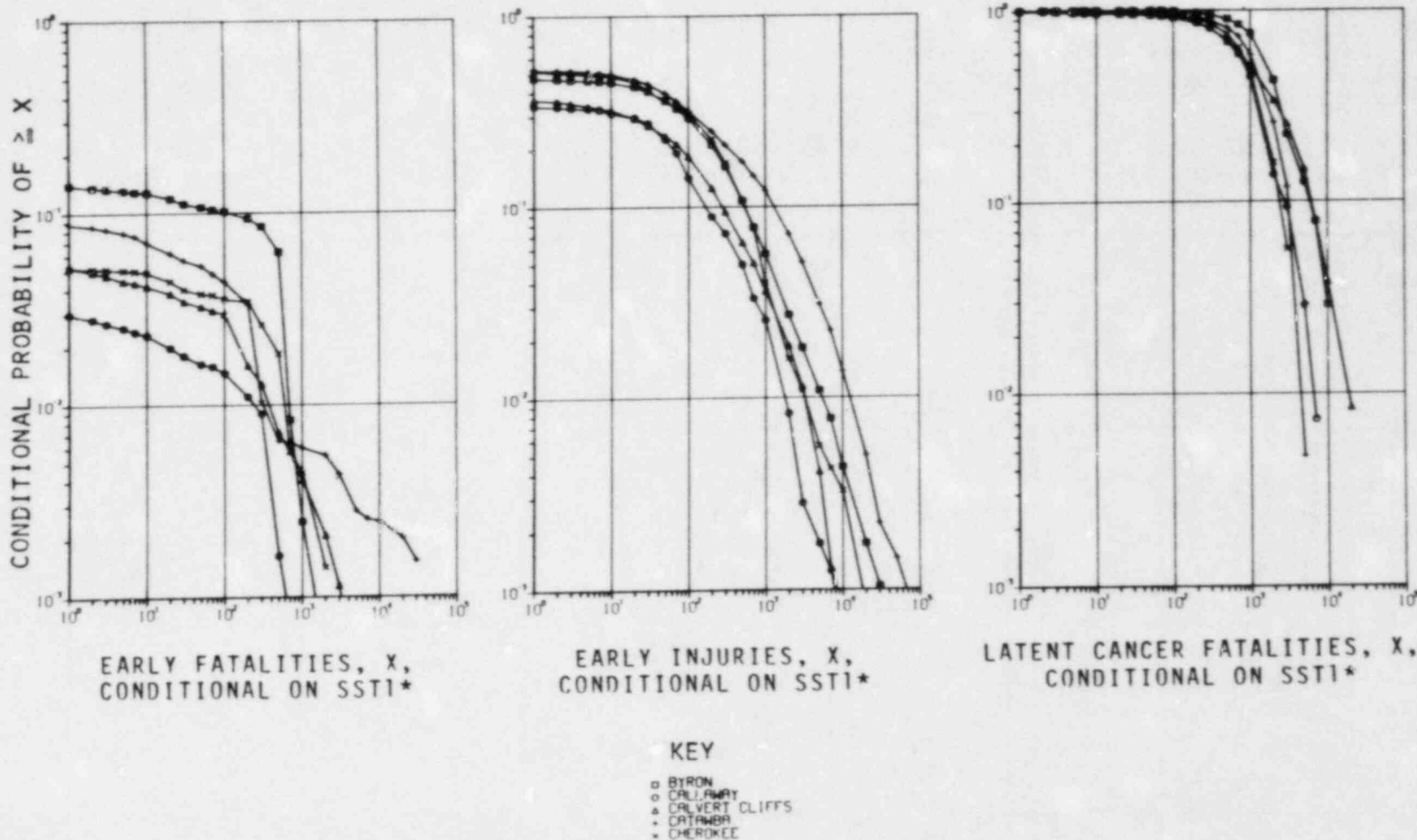


Figure C-3: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release. Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-10

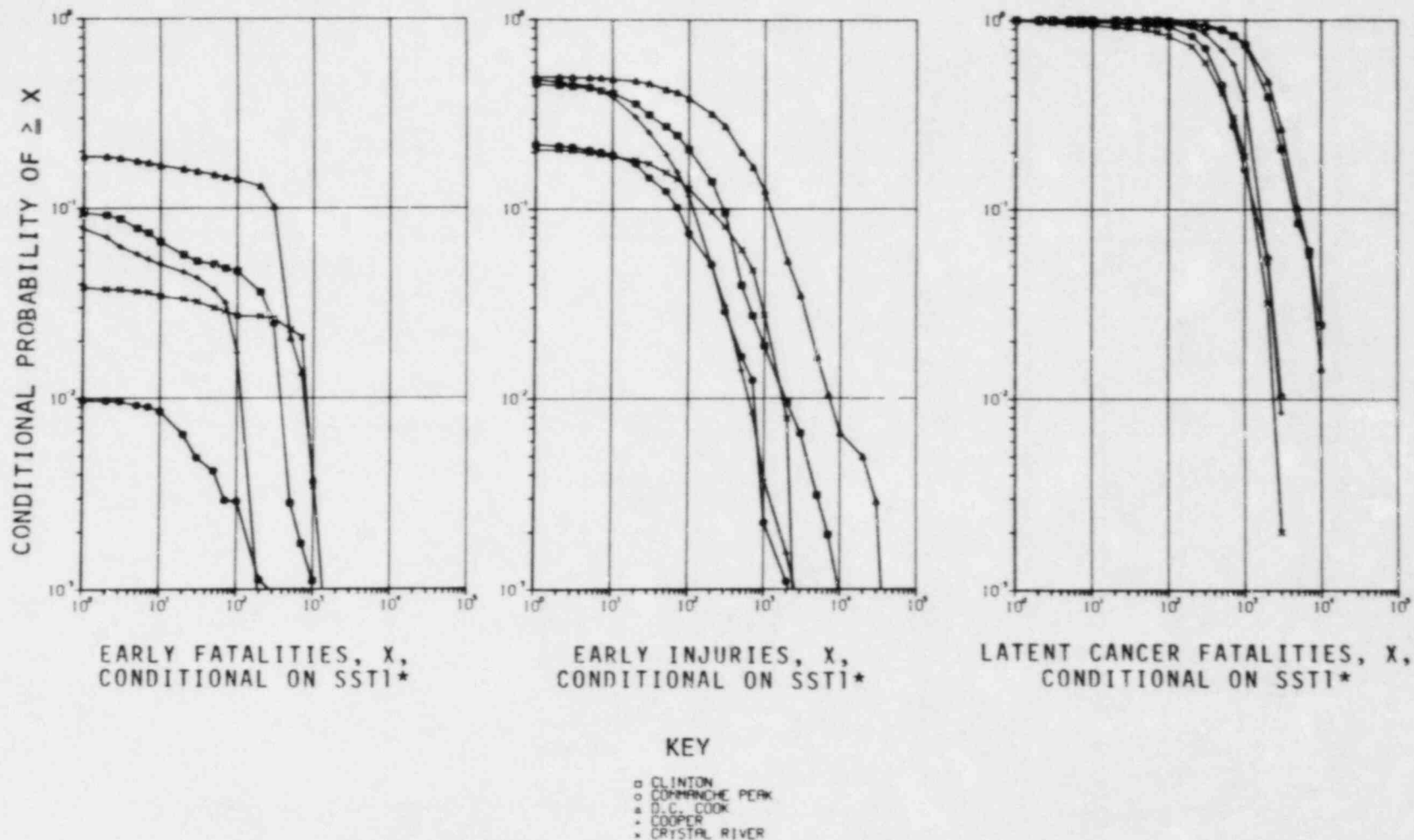


Figure C-4: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release.

Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDPs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-11

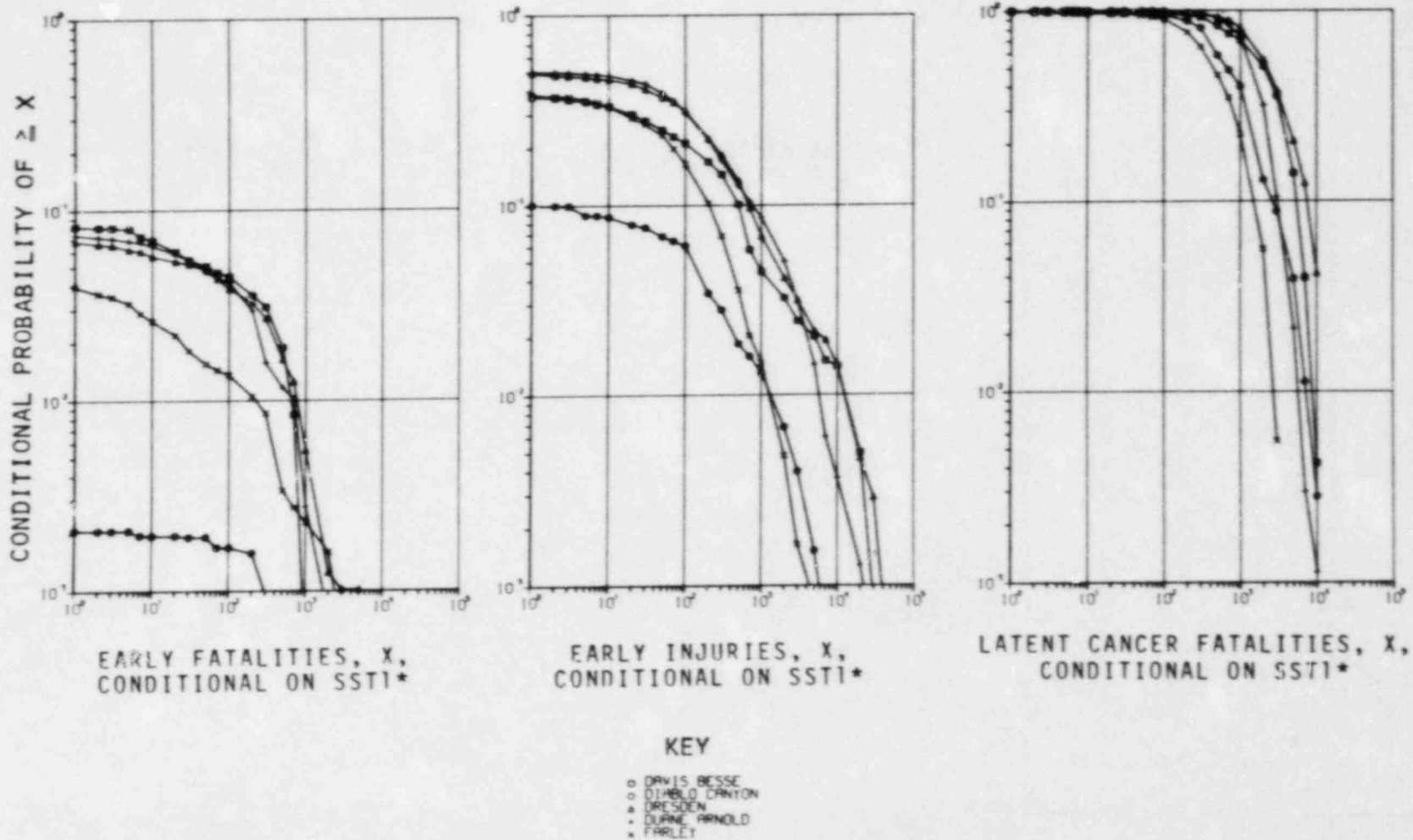


Figure C-5: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release.
Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-12

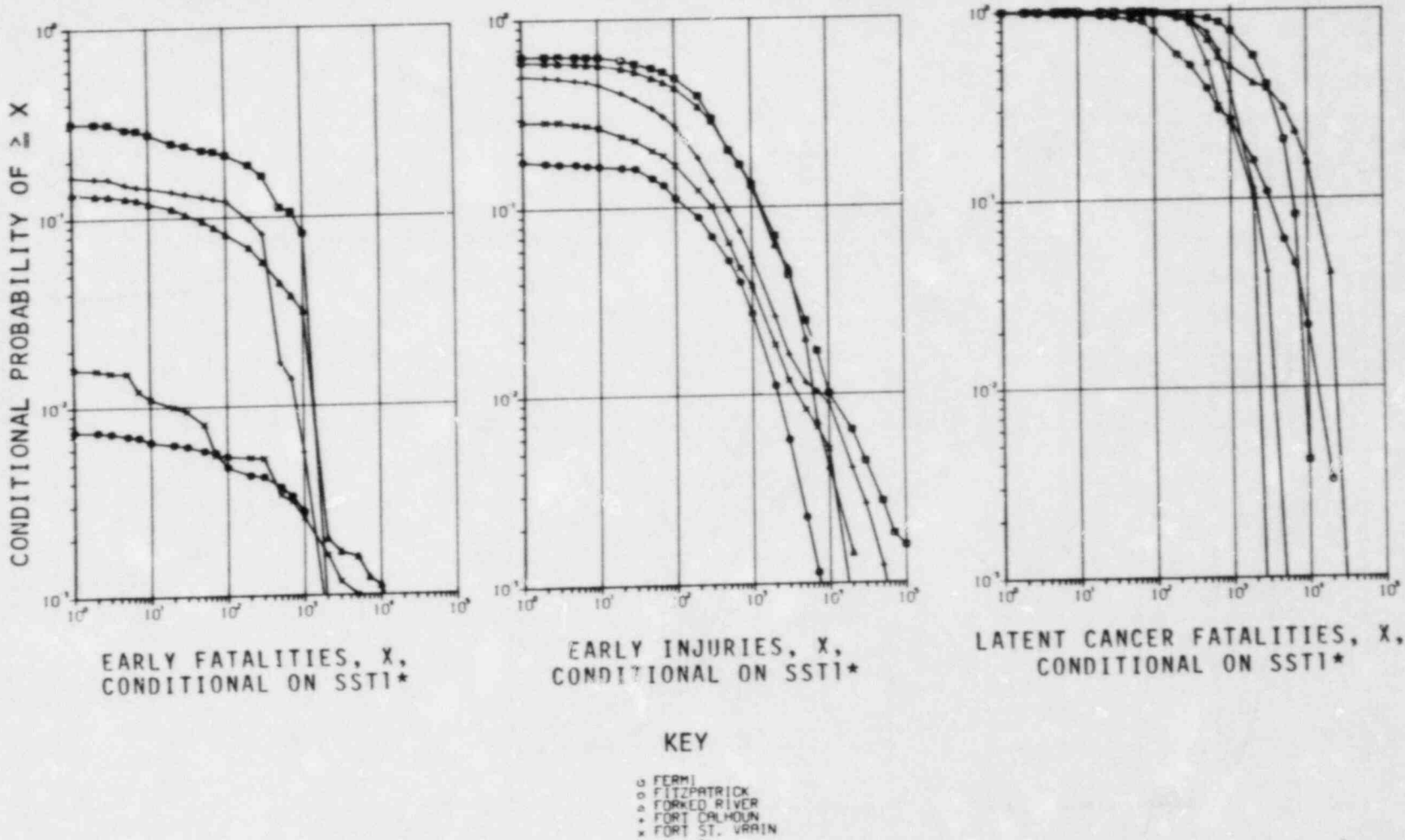


Figure C-6: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release. Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-13

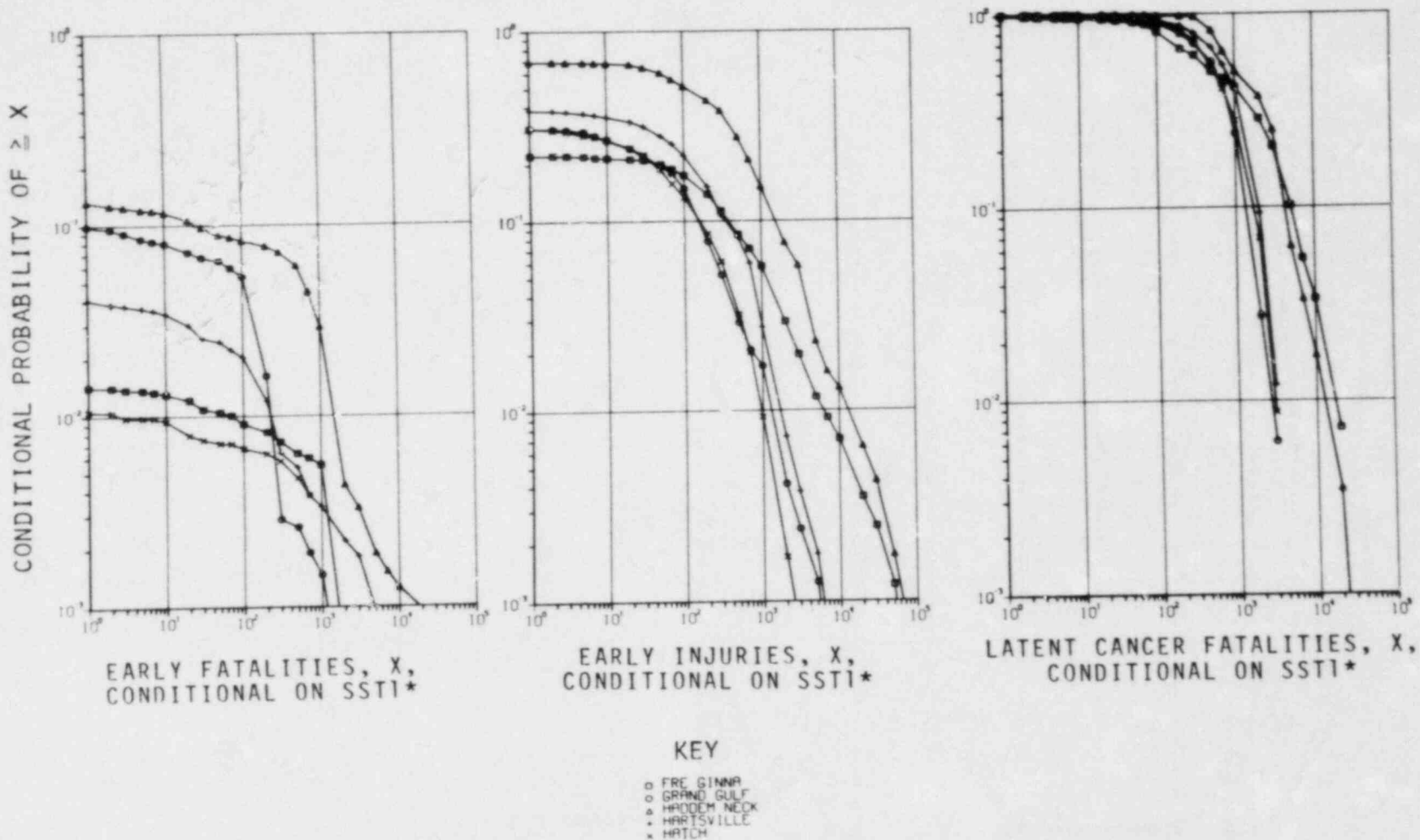


Figure C-7: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release. Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-14

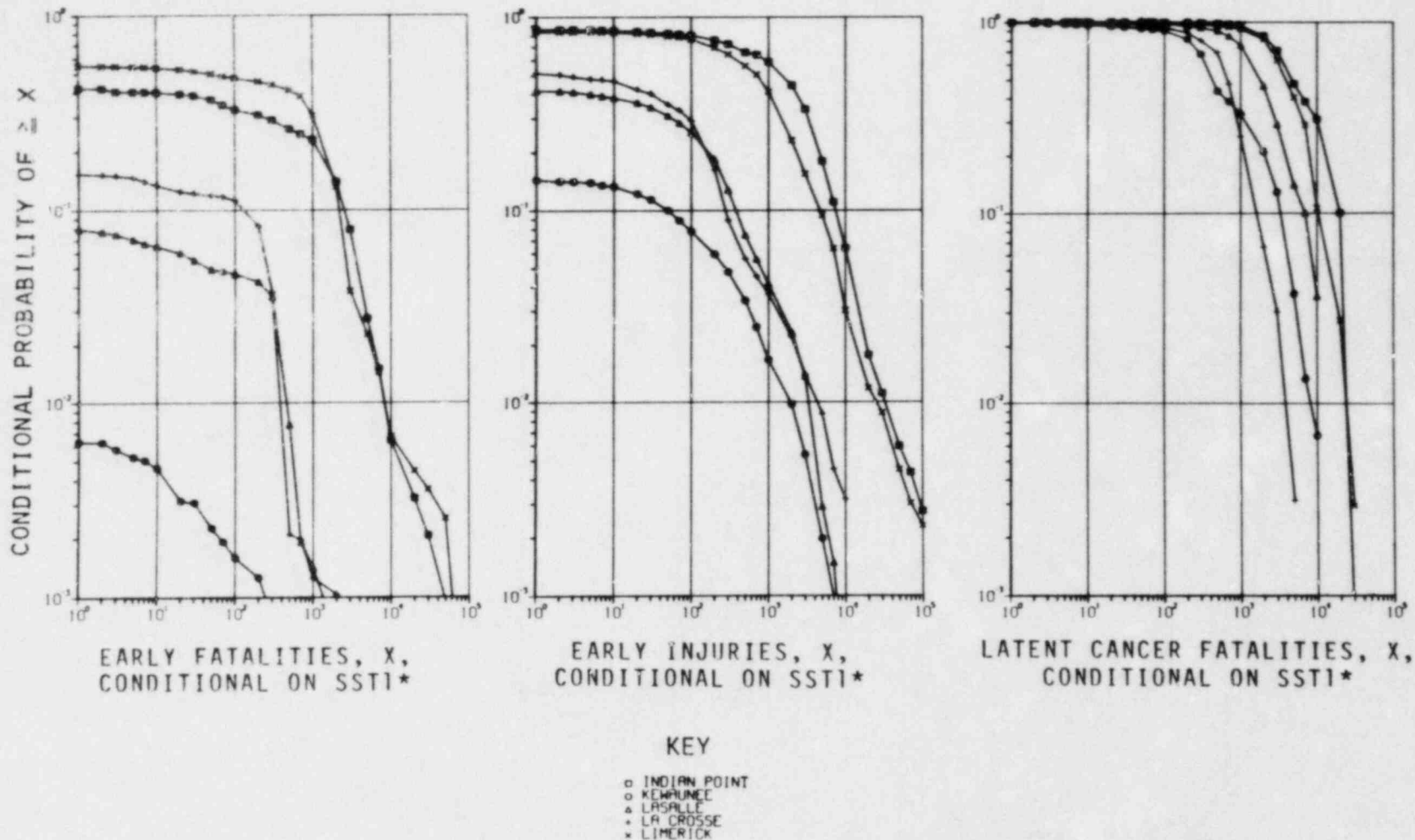


Figure C-8: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release.

Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume a 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-13

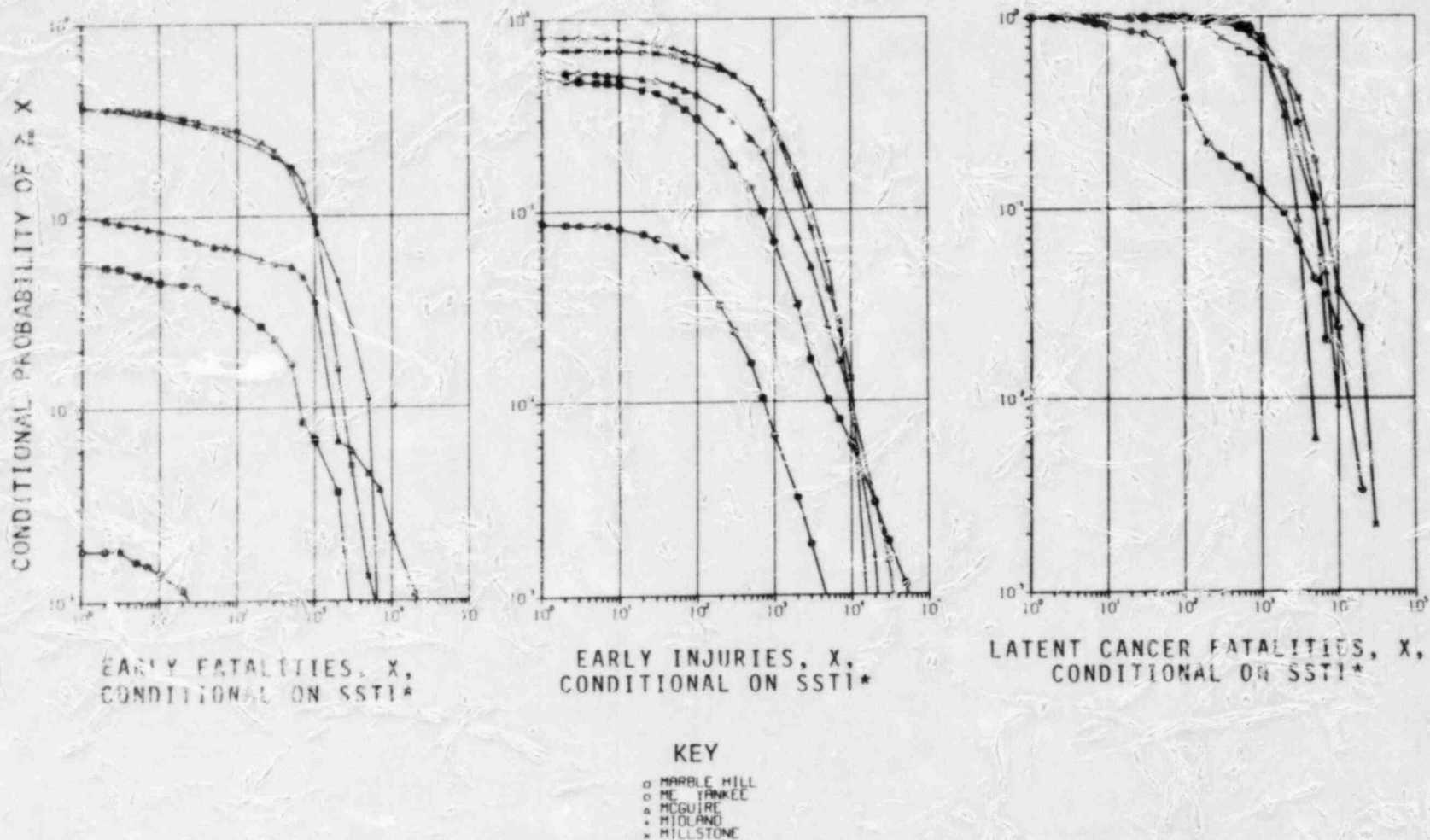


Figure C-9: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release. Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-16

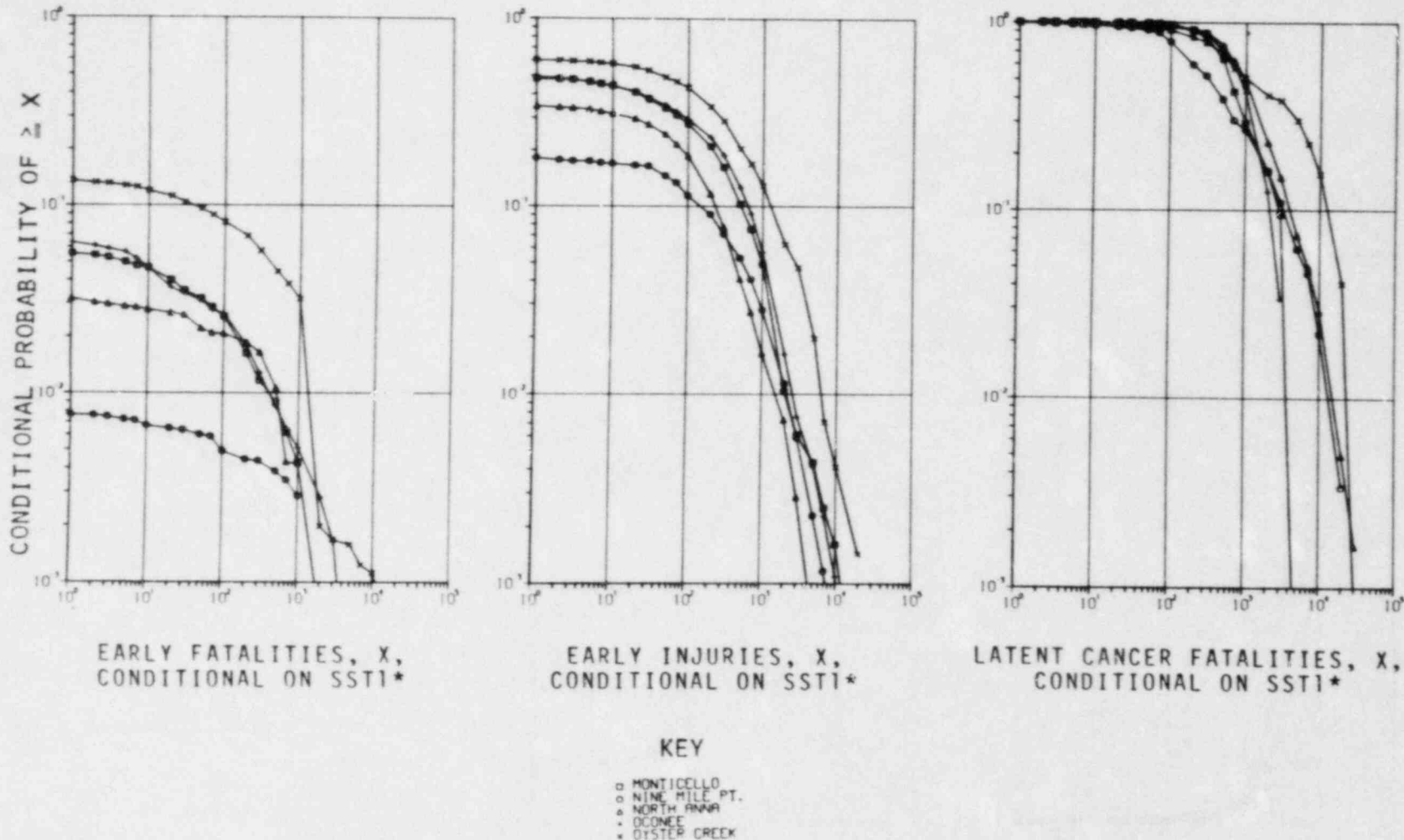


Figure C-10: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release.

Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-17

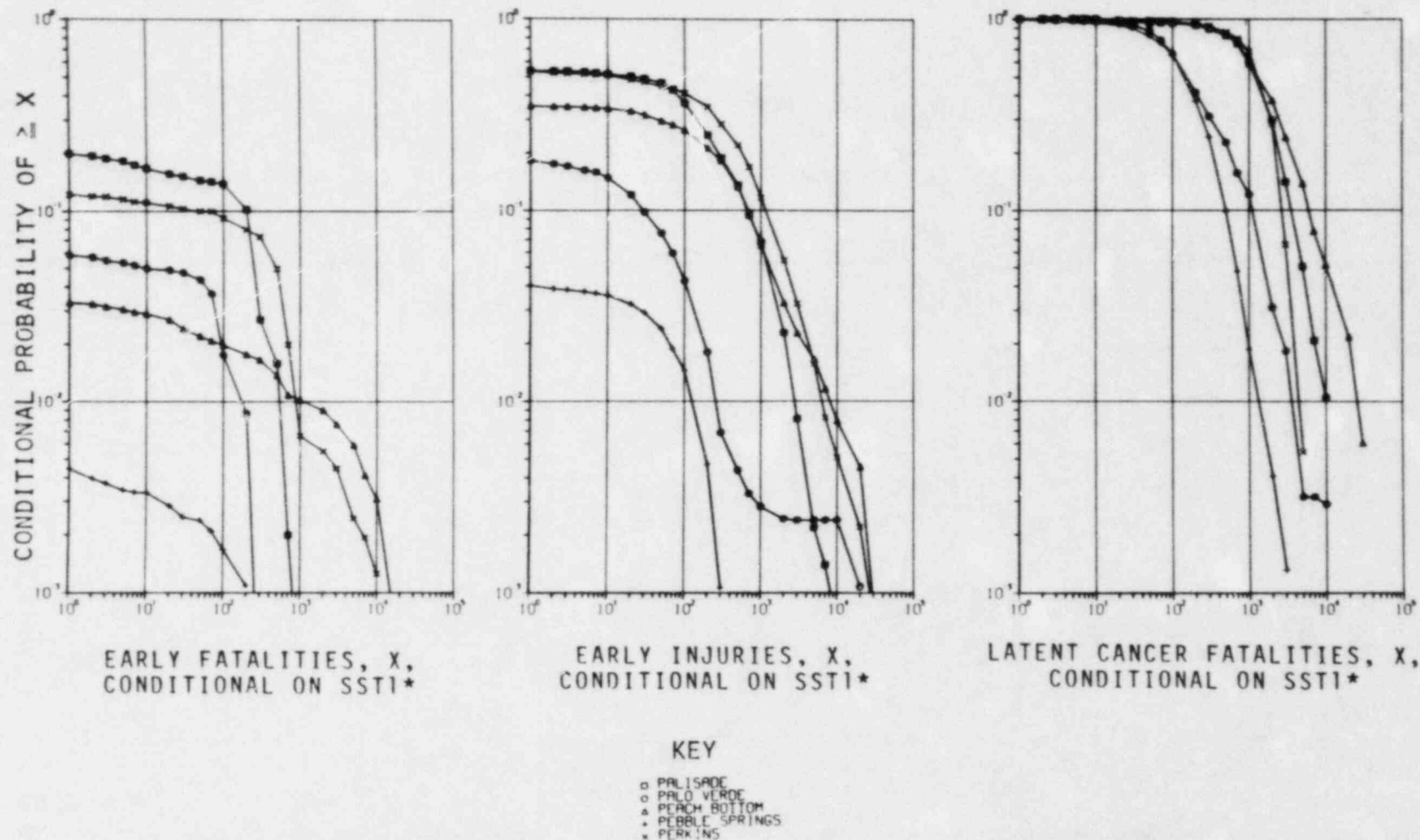


Figure C-11: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release.

Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-18

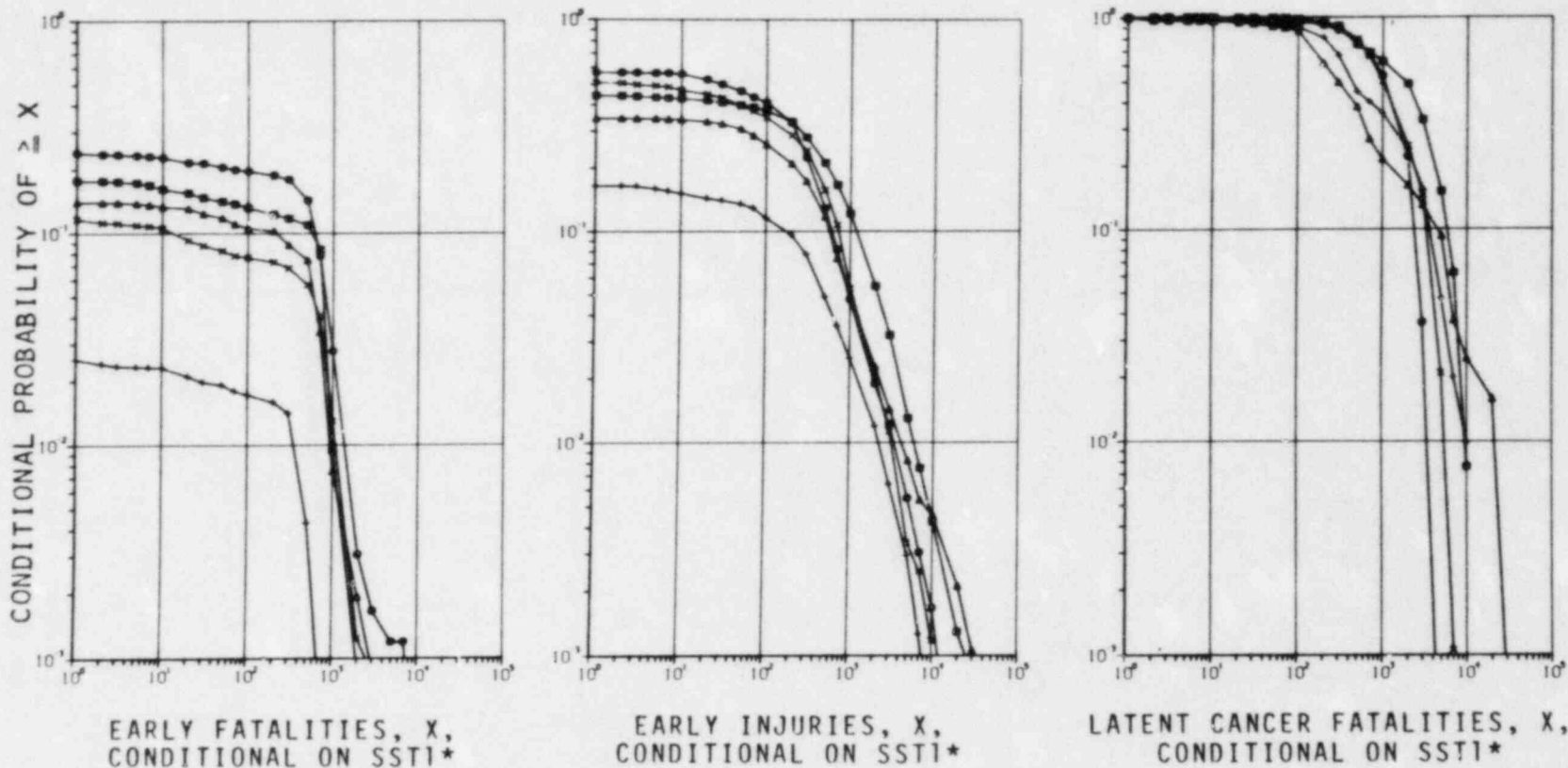


Figure C-12: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release.

Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-19

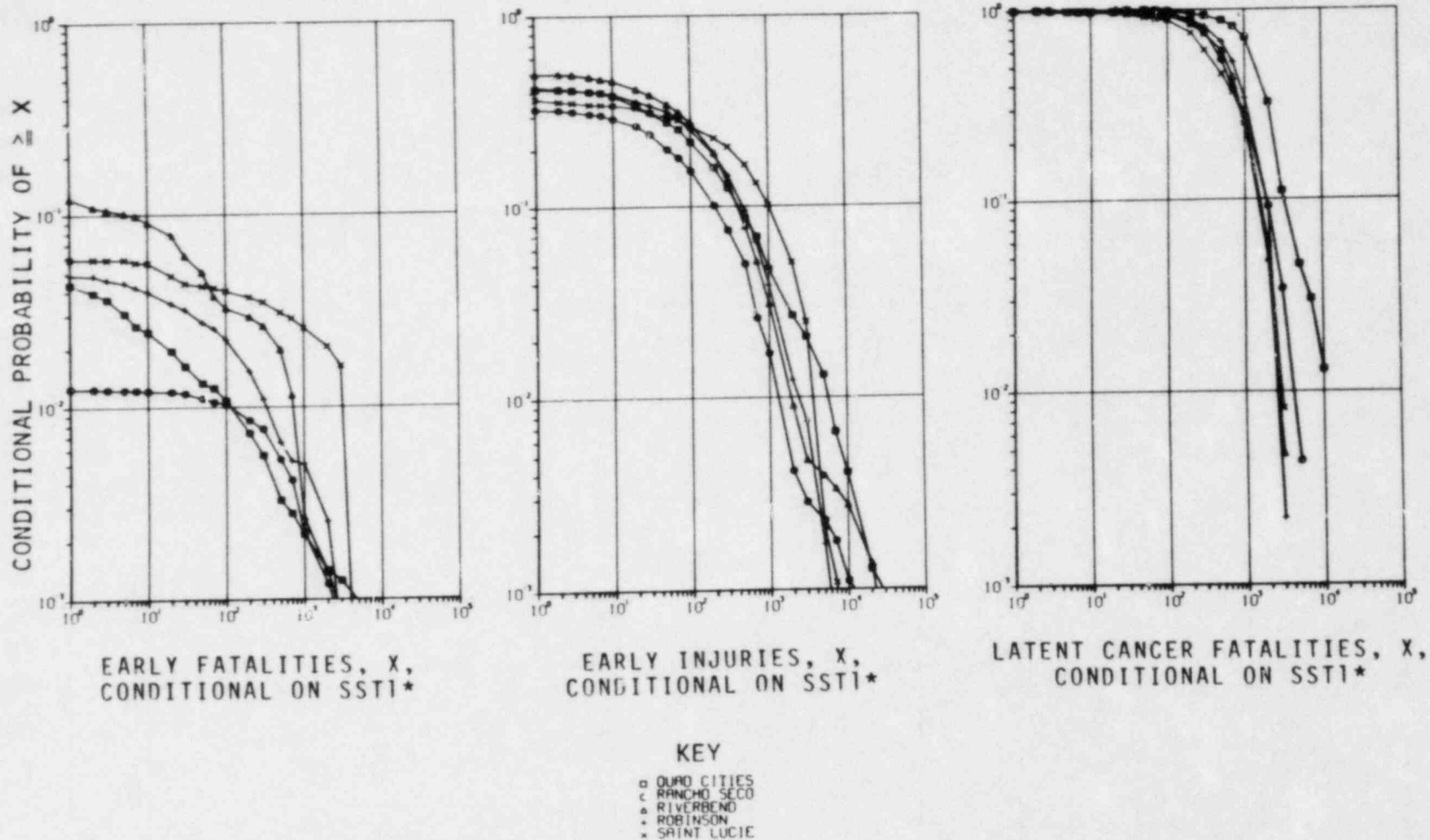


Figure C-13: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release. Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

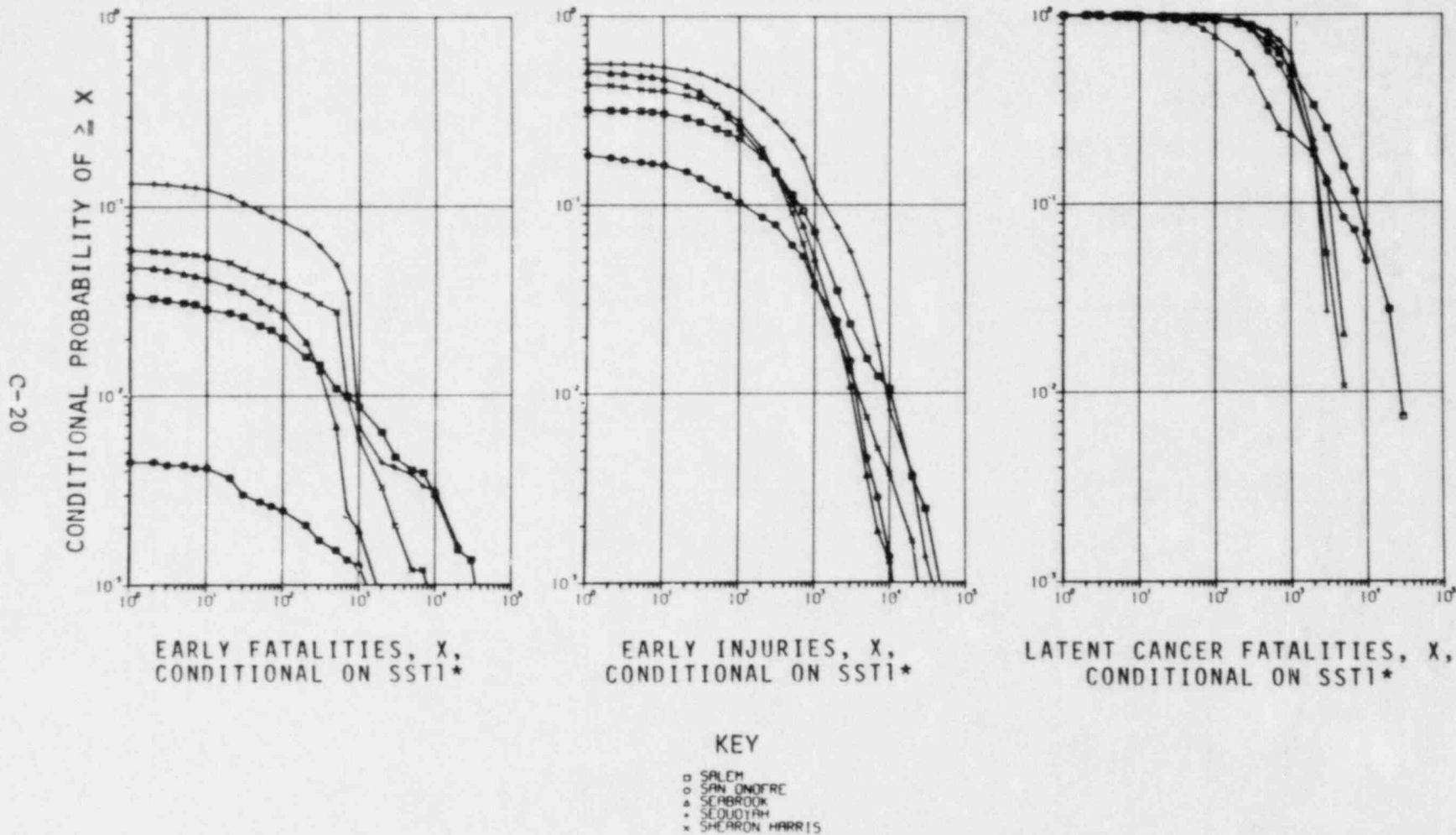


Figure C-14: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release.
 Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-21

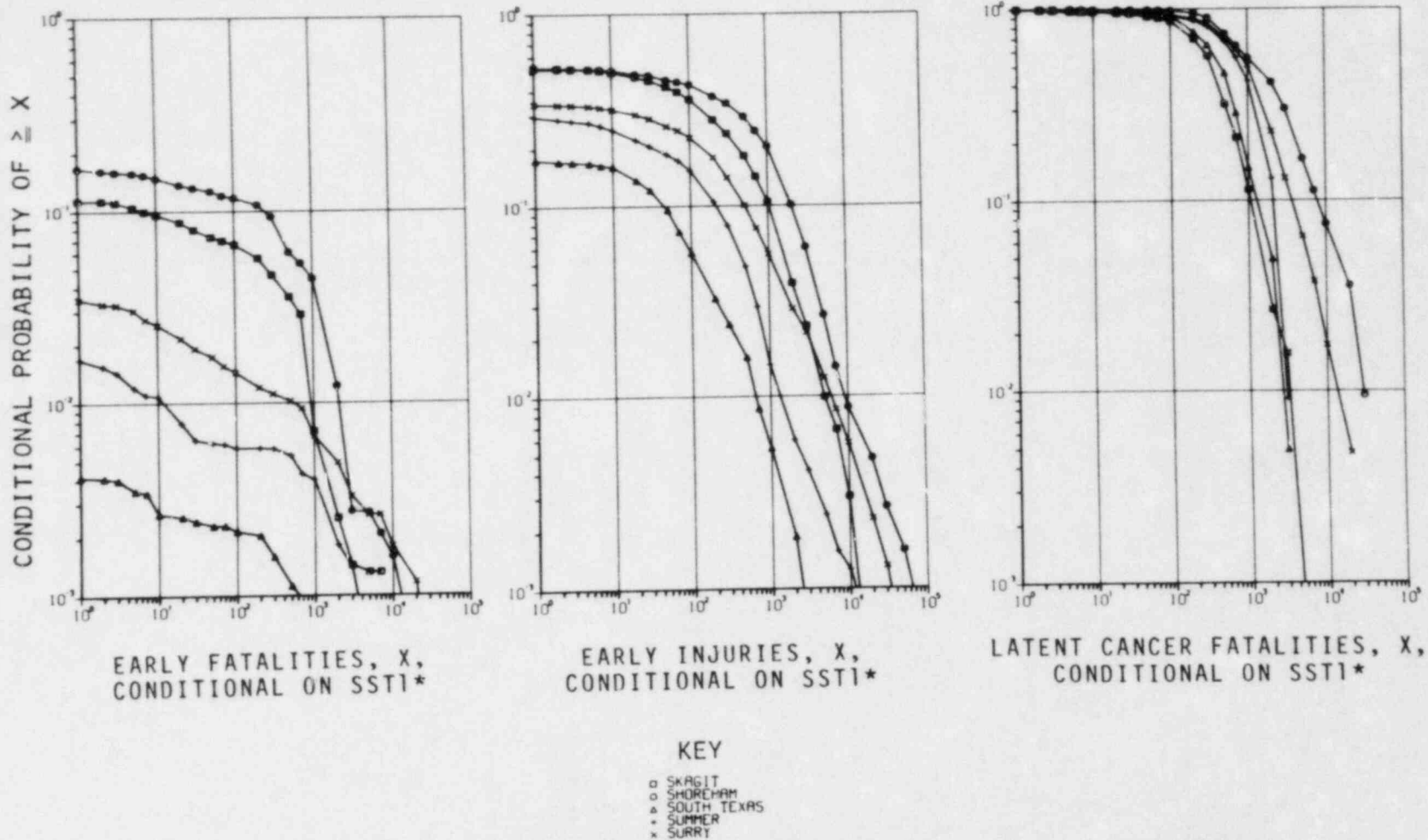


Figure C-15: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release. Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-22

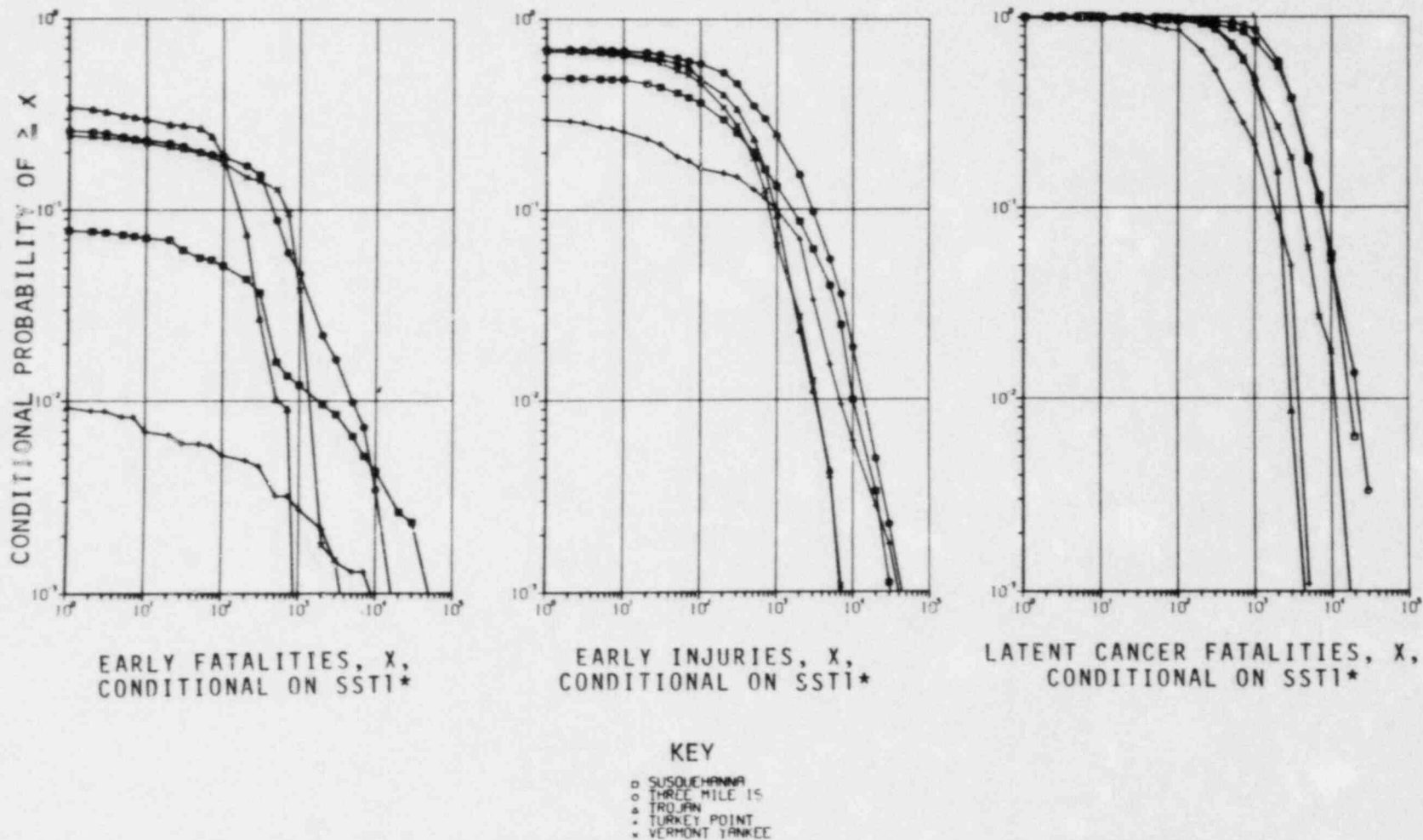
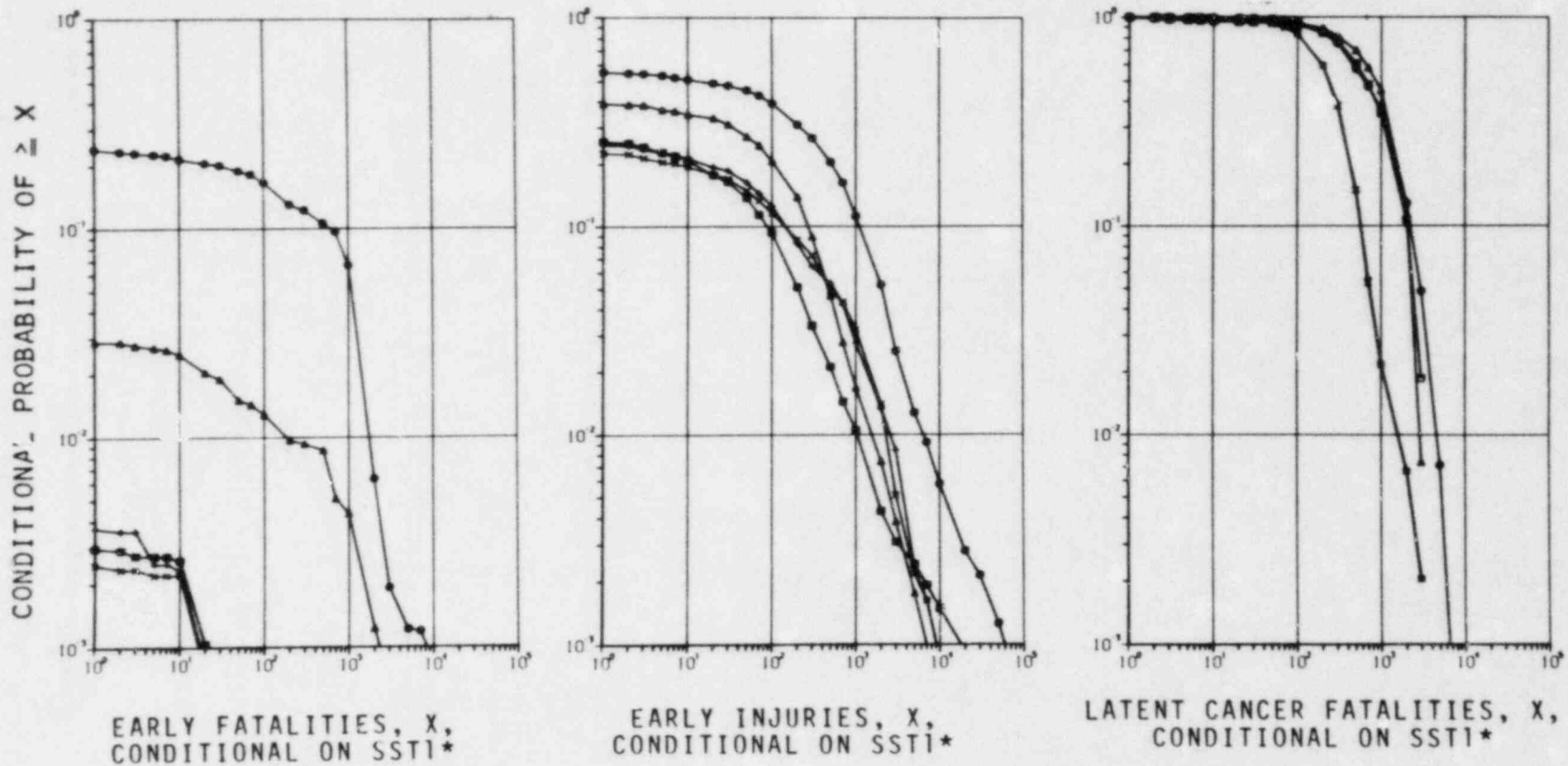


Figure C-16: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release.
Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2.

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-23



KEY

- VOGTLE
- WATERFORD
- △ WATTS BAR
- WPSS 1+4
- * WPSS 3+5

Figure C-17: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release. Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2

Note: These CCDFs do not represent effects from existing reactor/site combinations, all assume an 1120 MWe reactor. In addition, these results are conditional on the occurrence of a hypothetical SST1 release. Recent evidence suggests that the source term magnitude assumed for SST1 may be overestimated by a factor of 10 or more (see section 2.3.2).

C-24

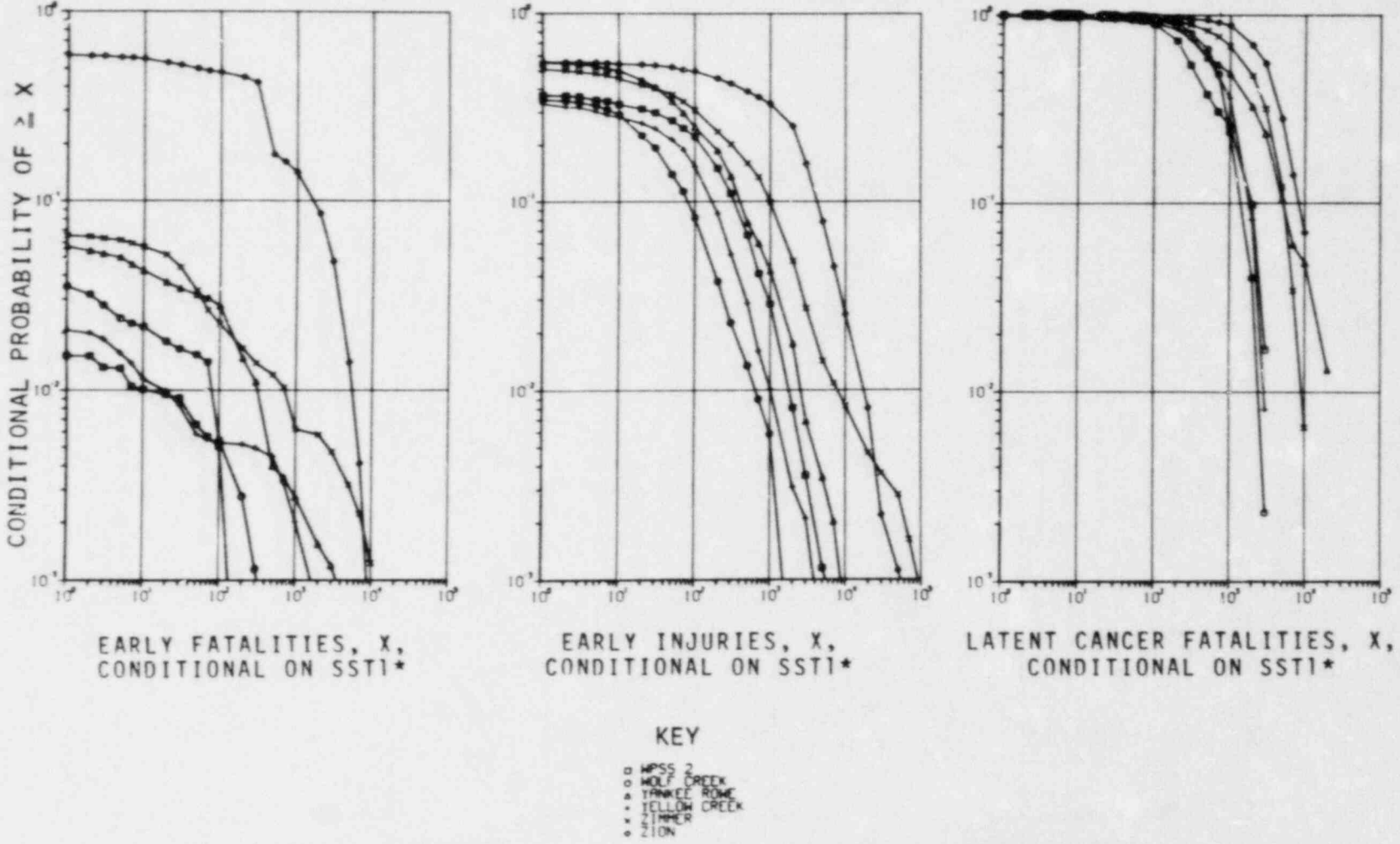


Figure C-18: Early fatality, early injury, and latent cancer fatality CCDFs at named sites, conditional on an SST1 release. Assumptions: 1120 MWe reactor, summary evacuation, representative meteorology (see Appendix A), and actual site population and windrose.

*See footnote, page C-2

Appendix D: Additional Population Statistics for Current Reactor Sites

The demographic characteristics of the 91 reactor sites described in Chapter 2 and Appendix A were analyzed for this study. These data, which were summarized in Chapter 3, provide a perspective of previous siting decisions and delineate the population characteristics of current reactor sites. This appendix contains additional demographic data which complement the data presented in Chapter 3. These data are presented in the following sections.

<u>Section</u>	<u>Data Description</u>
D.1	Site Population Statistics
D.2	Exclusion Distances
D.3	Site Population Factors

D.1 Site Population Statistics

The 91 population distributions examined in this report were all constructed on a 16 sector, circular polar grid. For any specified portion (a circle, an annulus, a sector) of that grid, 91 values of population density are available, one for each of the 91 population distributions. By cumulation of the 91 values for a given portion of the grid, a population density CCDF may be constructed.* Six different sets of population density CCDFs have been constructed for the following areas of the population distribution grid:

Set 1 (Figures D.1-1 thru D.1-8): Eight annuli (0-2, 2-5, 5-10, 10-20, 20-30, 30-50, 50-100, and 100-200 mi).

Set 2 (Figures D.1-9 thru D.1-16): eight radial distances (0-2, 0-5, 0-10, 0-20, 0-30, 0-50, 0-100, and 0-200 mi).

*Population density CCDFs are Log-Log plots of the fraction of sites vs population density. Any point on the distribution gives the fraction of sites (y-axis value), which have a population density within the specified portion of the grid (annulus, circle, sector), that is greater than or equal to the specified population density (x-axis value).

Set 3 (Figures D.1-17 thru D.1-22): the most populated 22.5° sector in each of six annuli (0-2, 2-5, 5-10, 10-20, 20-30, and 30-50 mi) on the 16 sector grid.

Set 4 (Figures D.1-23 thru D.1-28): the most populated 22.5° sector in each of six radial distances (0-2, 0-5, 0-10, 0-20, 0-30 and 0-50 mi) on the 16 sector grid.

Set 5 (Figures D.1-29 thru D.1-34): the most populated 45° sector (two adjacent 22.5° sectors) in each of six annuli (0-2, 2-5, 5-10, 10-20, 20-30, and 30-50 mi) on the 16 sector grid.

Set 6 (Figures D.1-35 thru D.1-40): the most populated 45° sector (two adjacent 22.5° sectors) in each of six radial distances (0-2, 0-5, 0-10, 0-20, 0-30, and 0-50 mi) on the 16 sector grid.

Each figure contains six CCDFs, one for each of the five NRC administrative regions (NE, MW, S, W, SW, see Figure 3-1) and one for all regions combined (All).

Tables D.1-1 thru D.1-4 present the data used to construct the CCDFs in Figures D.1-1 thru D.1-28. Table D.1 presents, for each of the 91 sites, population densities within eight annuli; Table D.2 presents similar data for eight radial distances; Table D.3 for the most populated 22.5° sector of six annuli; and Table D.4 for the most populated 22.5° sector of six radial distances.

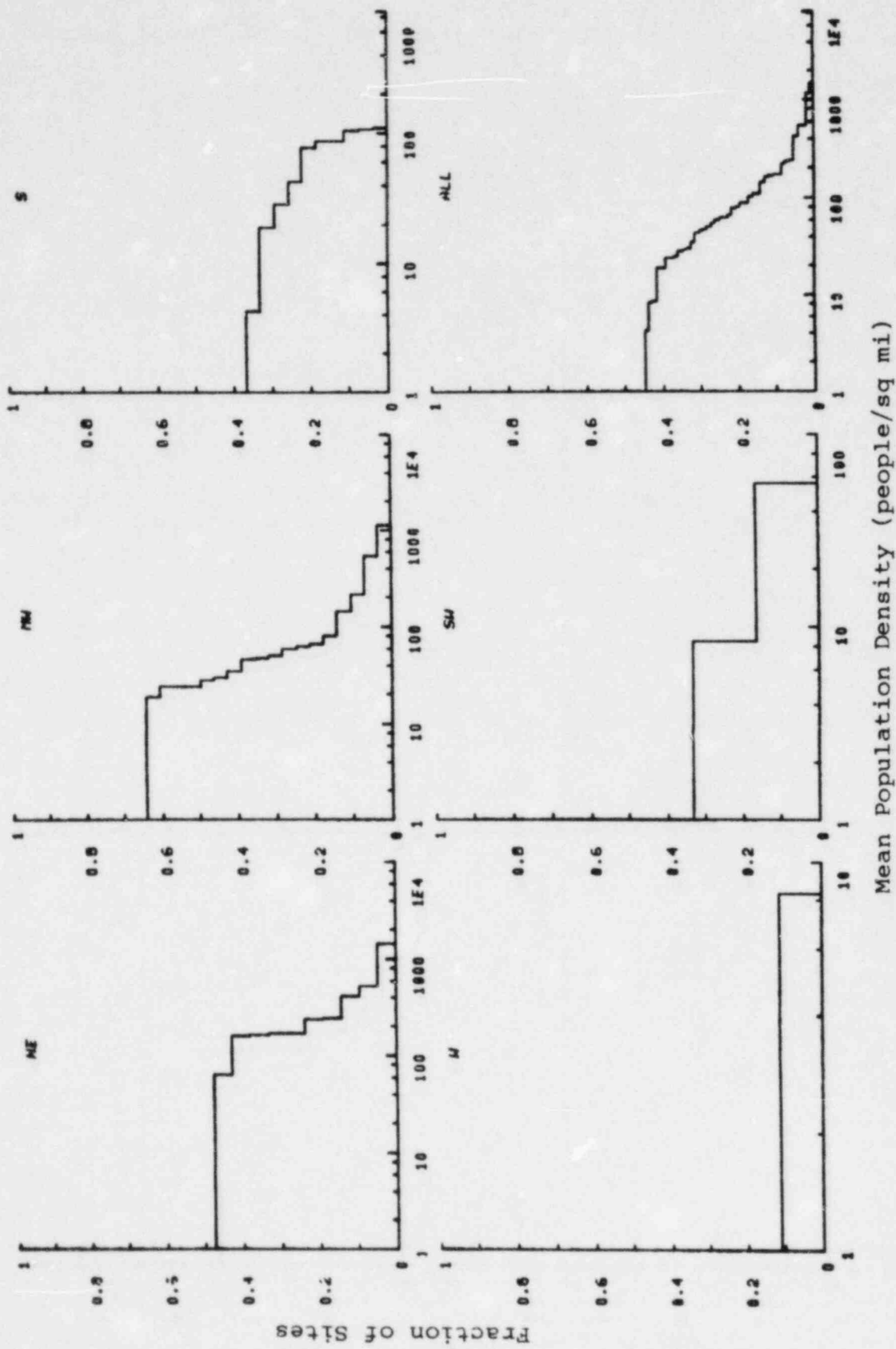


Figure D.1-1. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (ALL): Population Density Within the Annulus Interval 0-2 Miles.

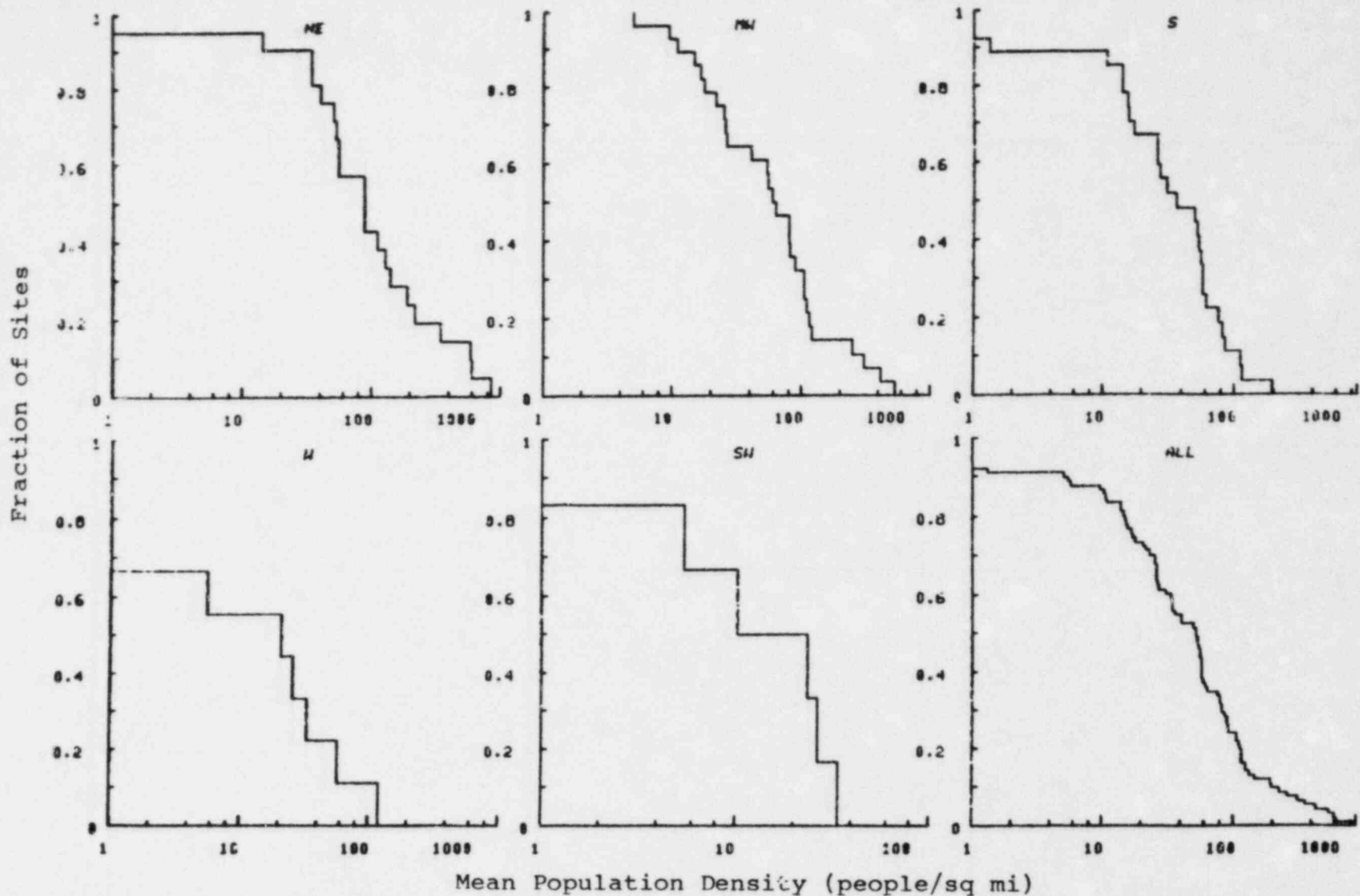
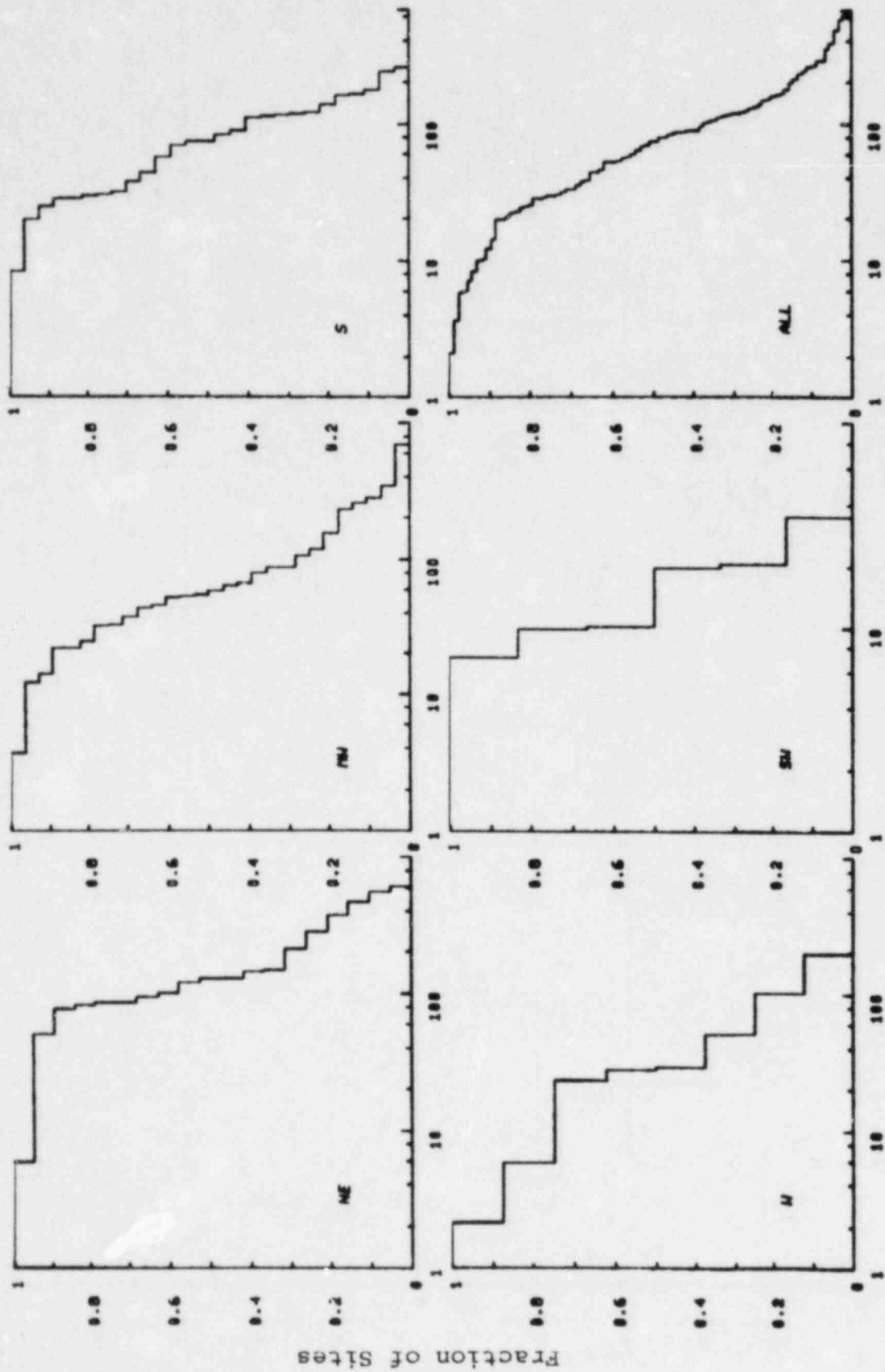


Figure D.1-2. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Annulus Interval 2-5 Miles.



Mean Population Density (people/sq mi)

Figure D.1-3. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (ALL): Population Density Within the Annulus Interval 5-10 Miles.

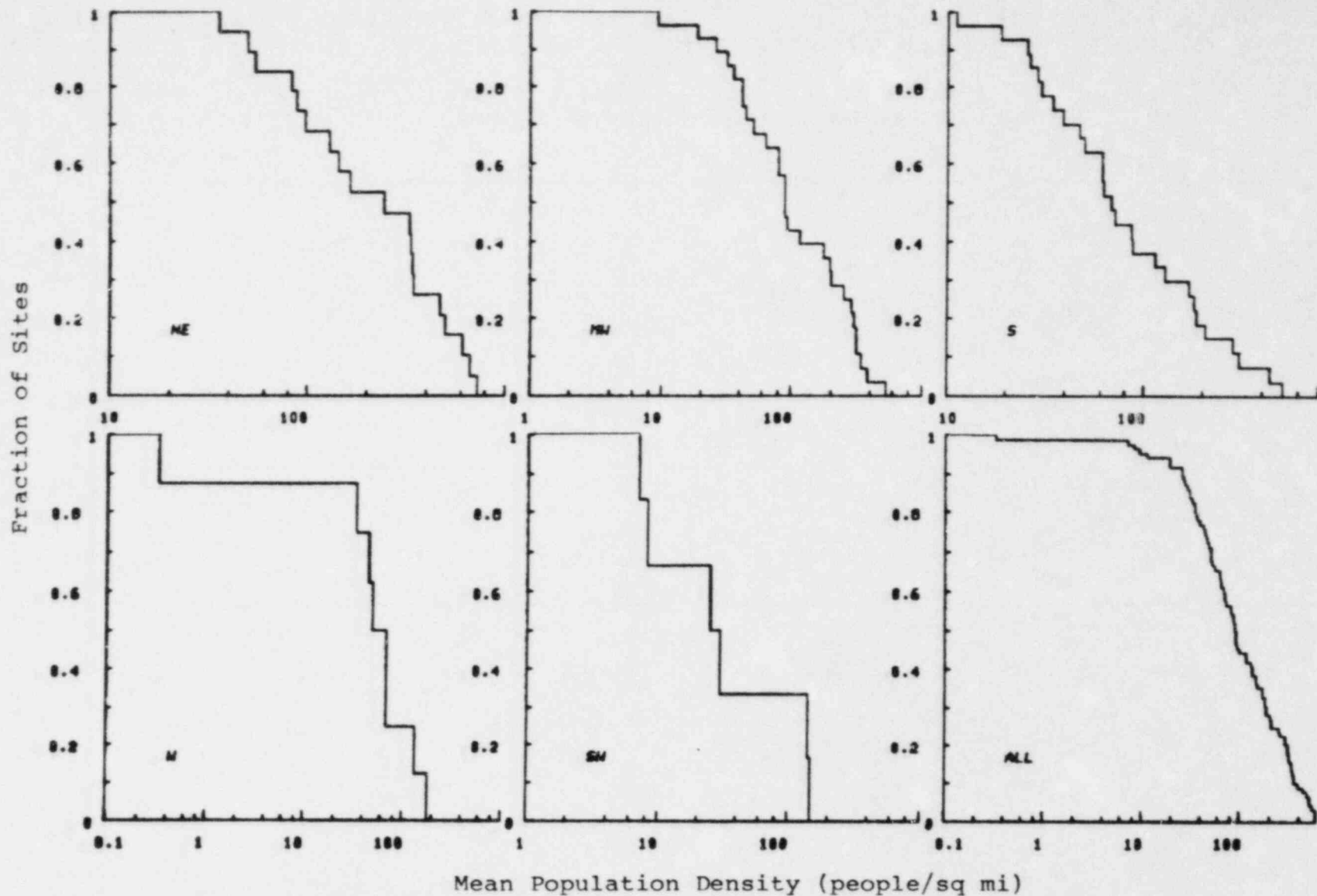


Figure D.1-4. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Annulus Interval 10-20 Miles.

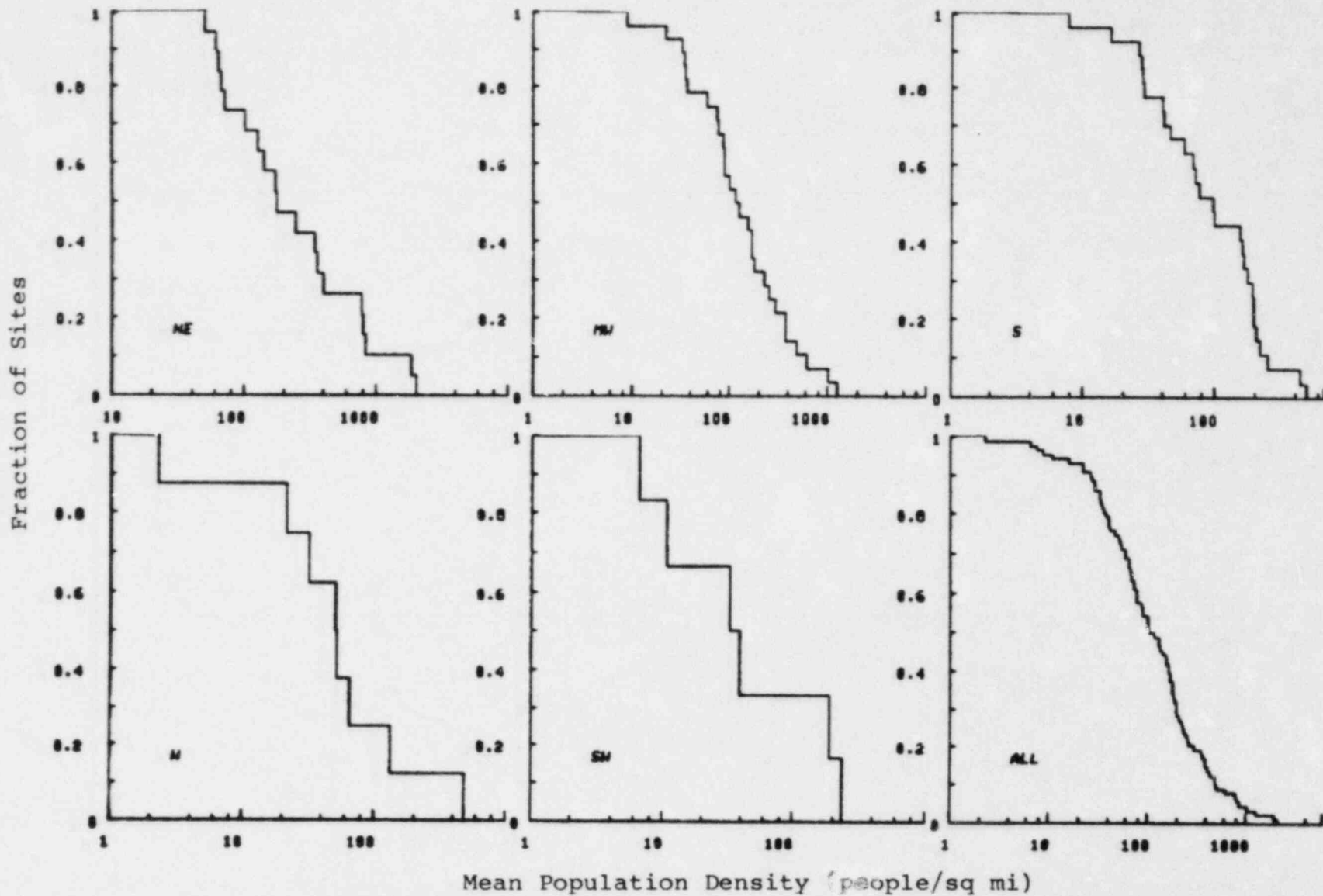


Figure D.1-5. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Annulus Interval 20-30 Miles.

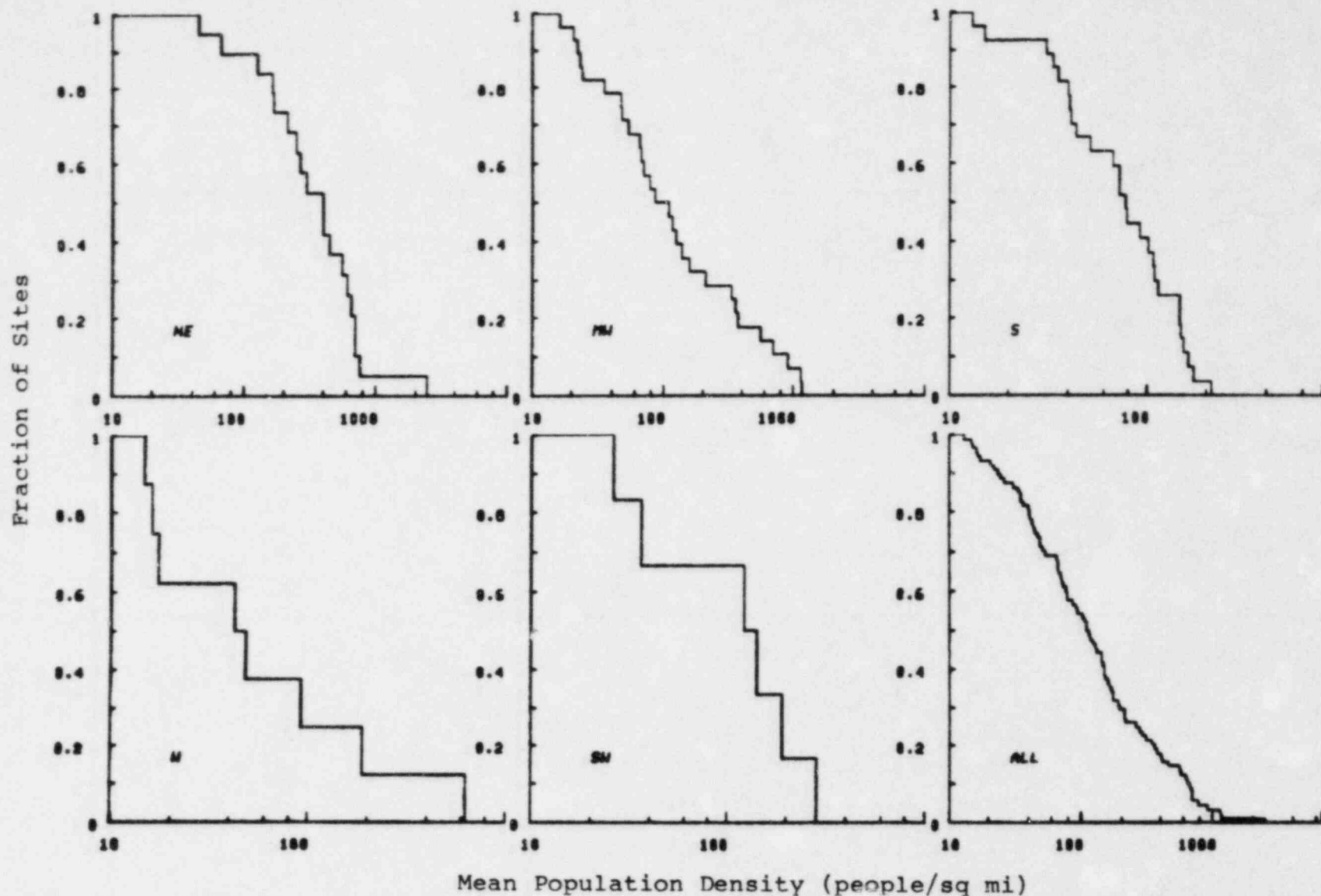


Figure D.1-6. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Annulus Interval 30-50 Miles.

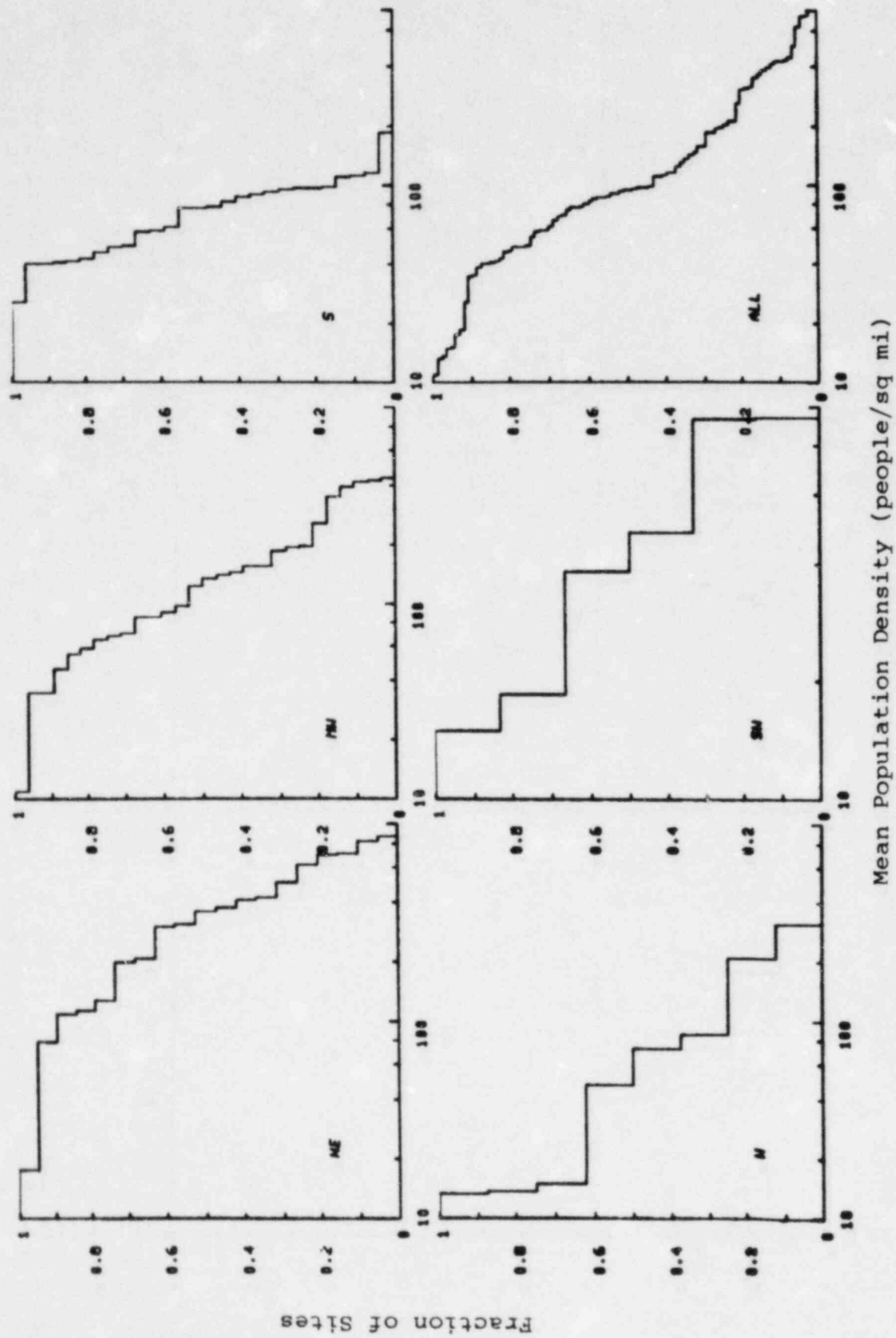


Figure D.1-7. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (ALL): Population Density Within the Annulus Interval 50-100 Miles.

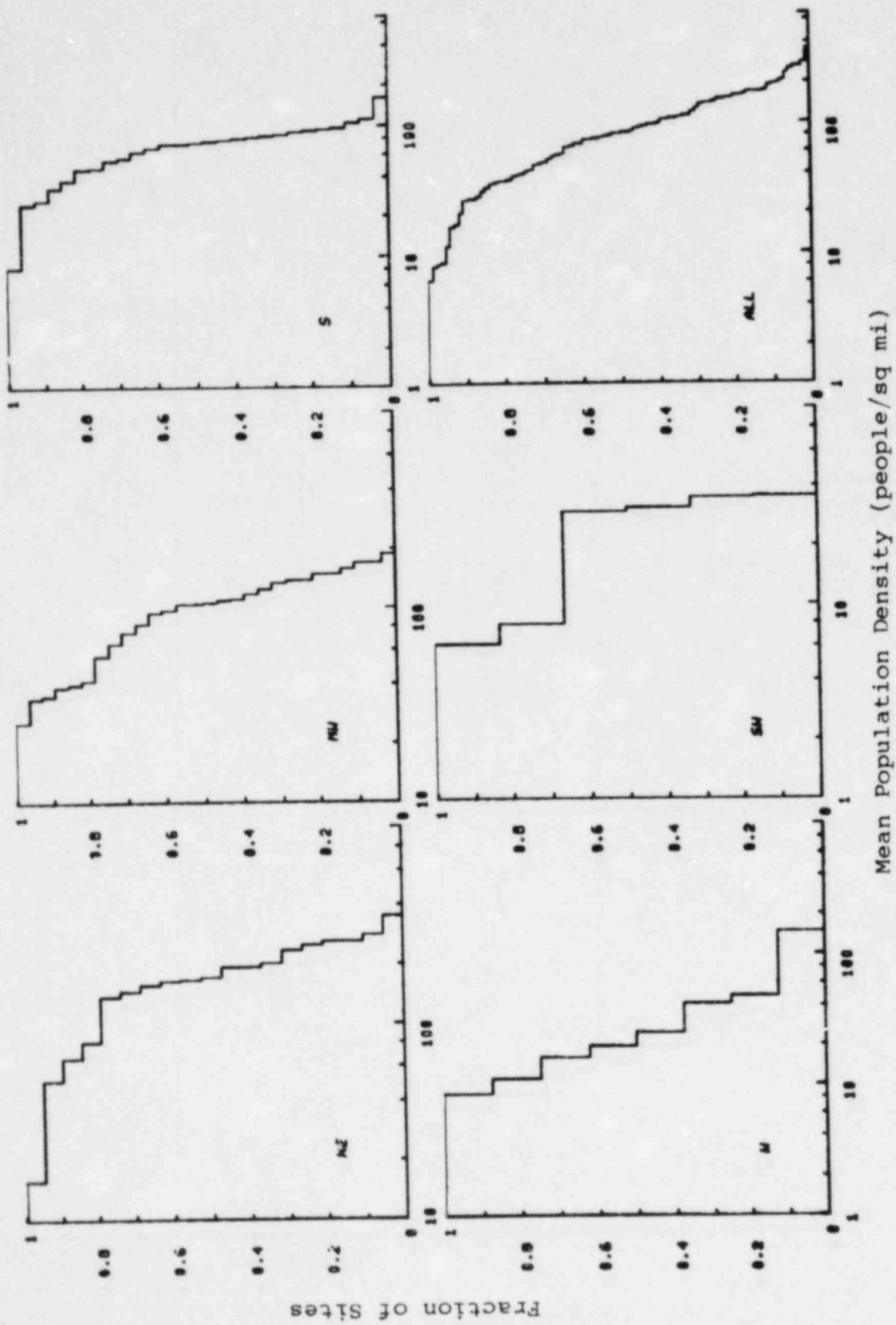


Figure D.1-8. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (ALL): Population Density Within the Annulus Interval 100-200 Miles.

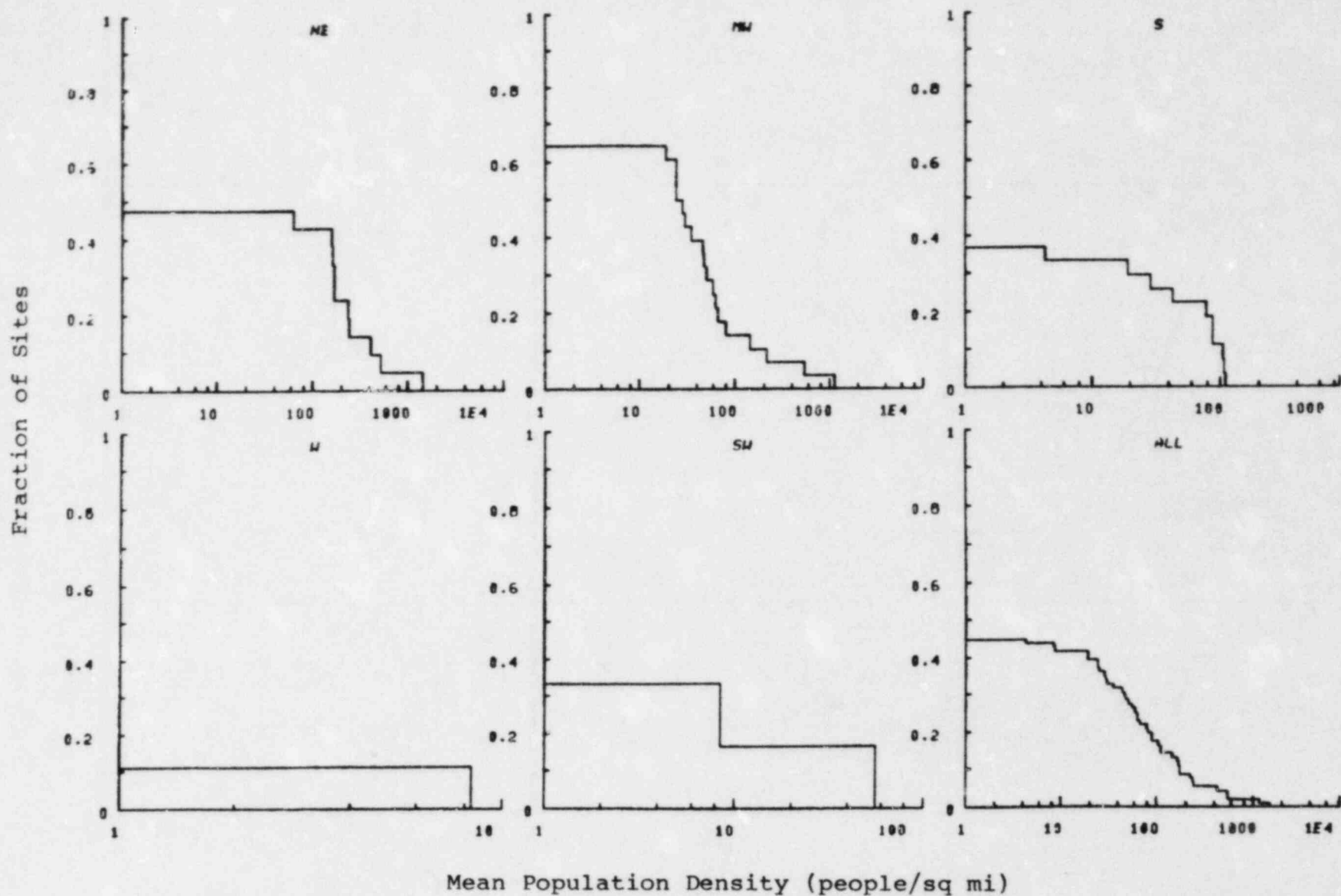


Figure D.1-9. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Radial Distance 0-2 Miles.

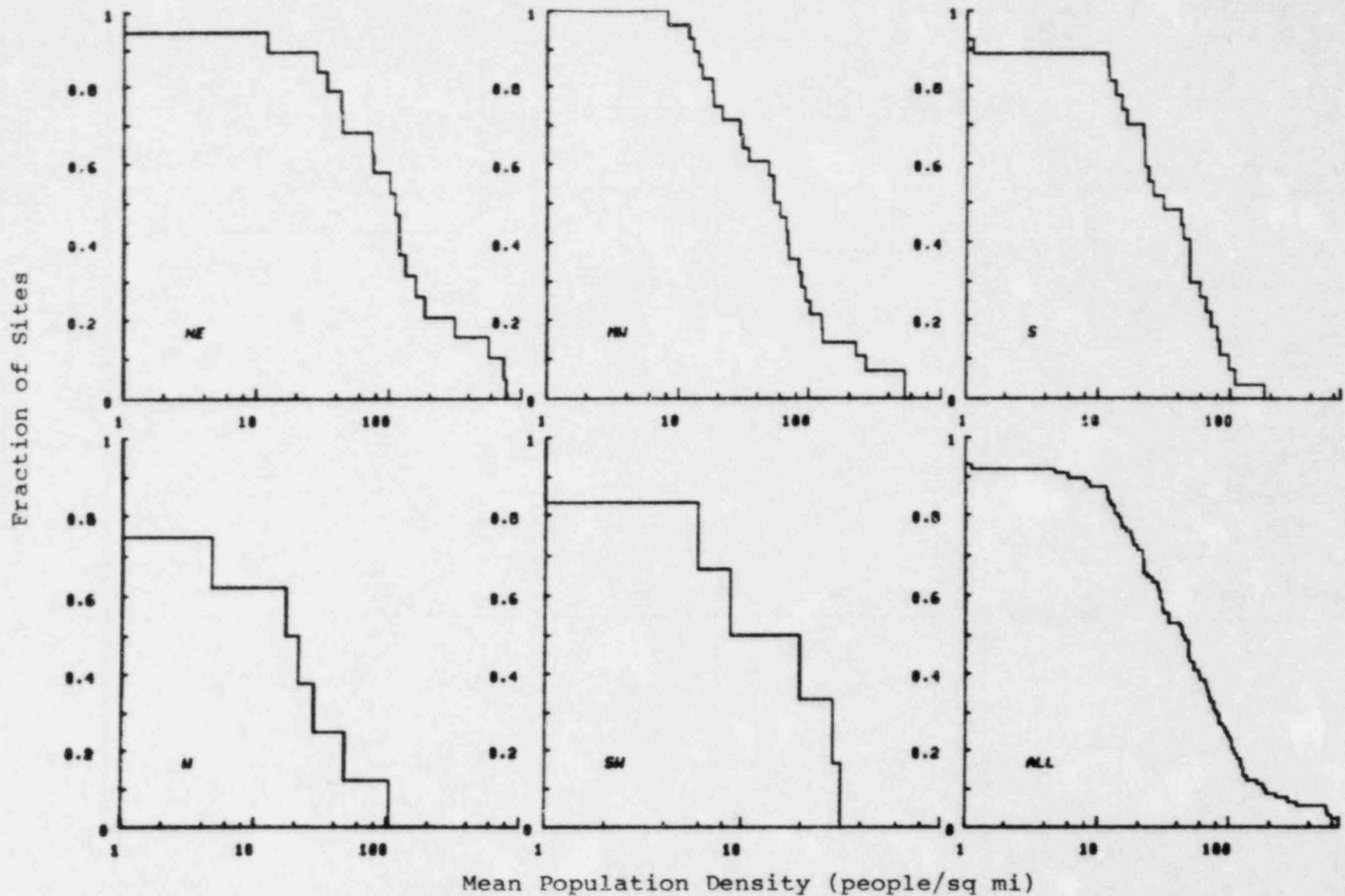


Figure D.1-10. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Radial Distance 0-5 Miles.

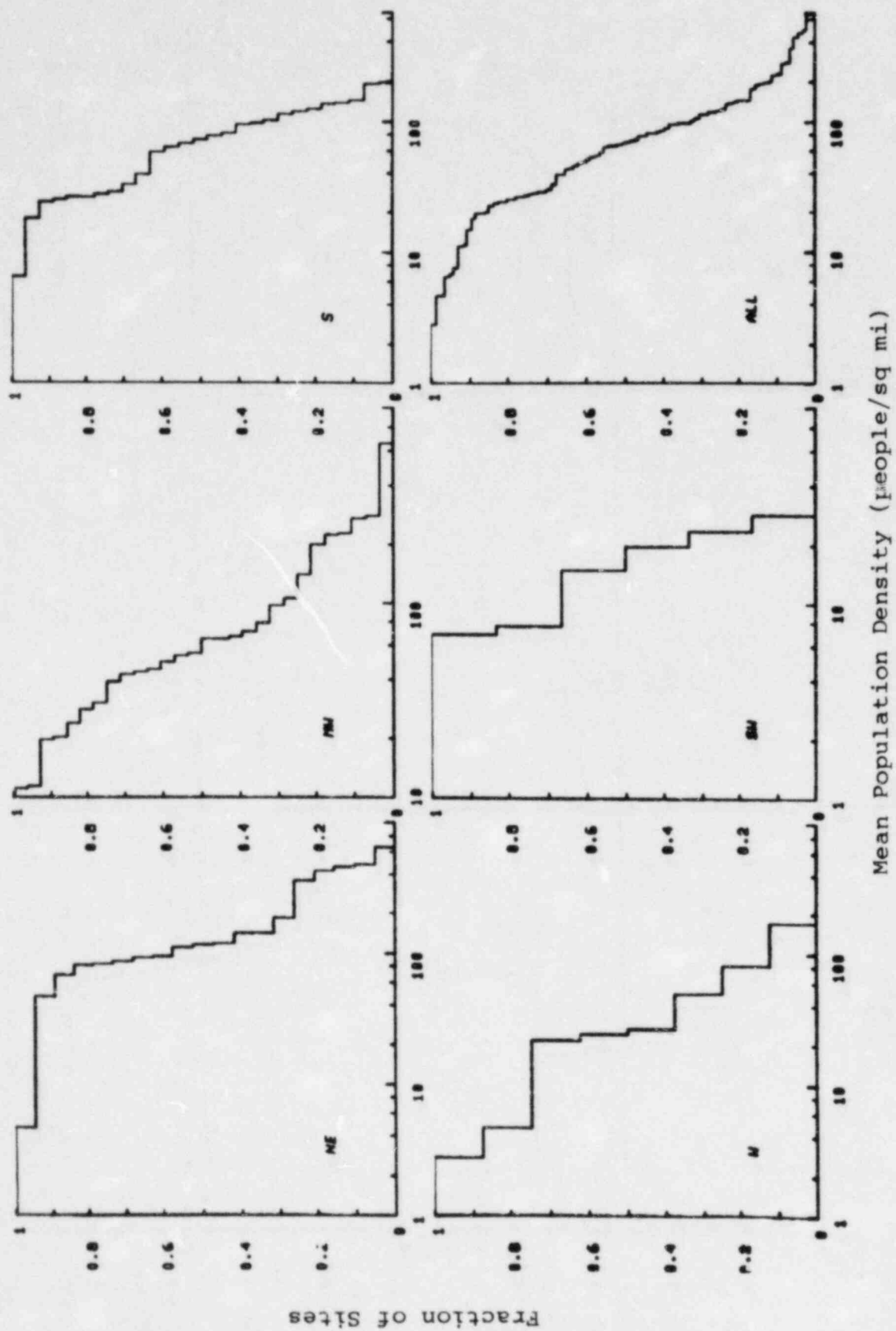


Figure D.1-11. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (ALL): Population Density Within the Radial Distance 0-10 Miles.

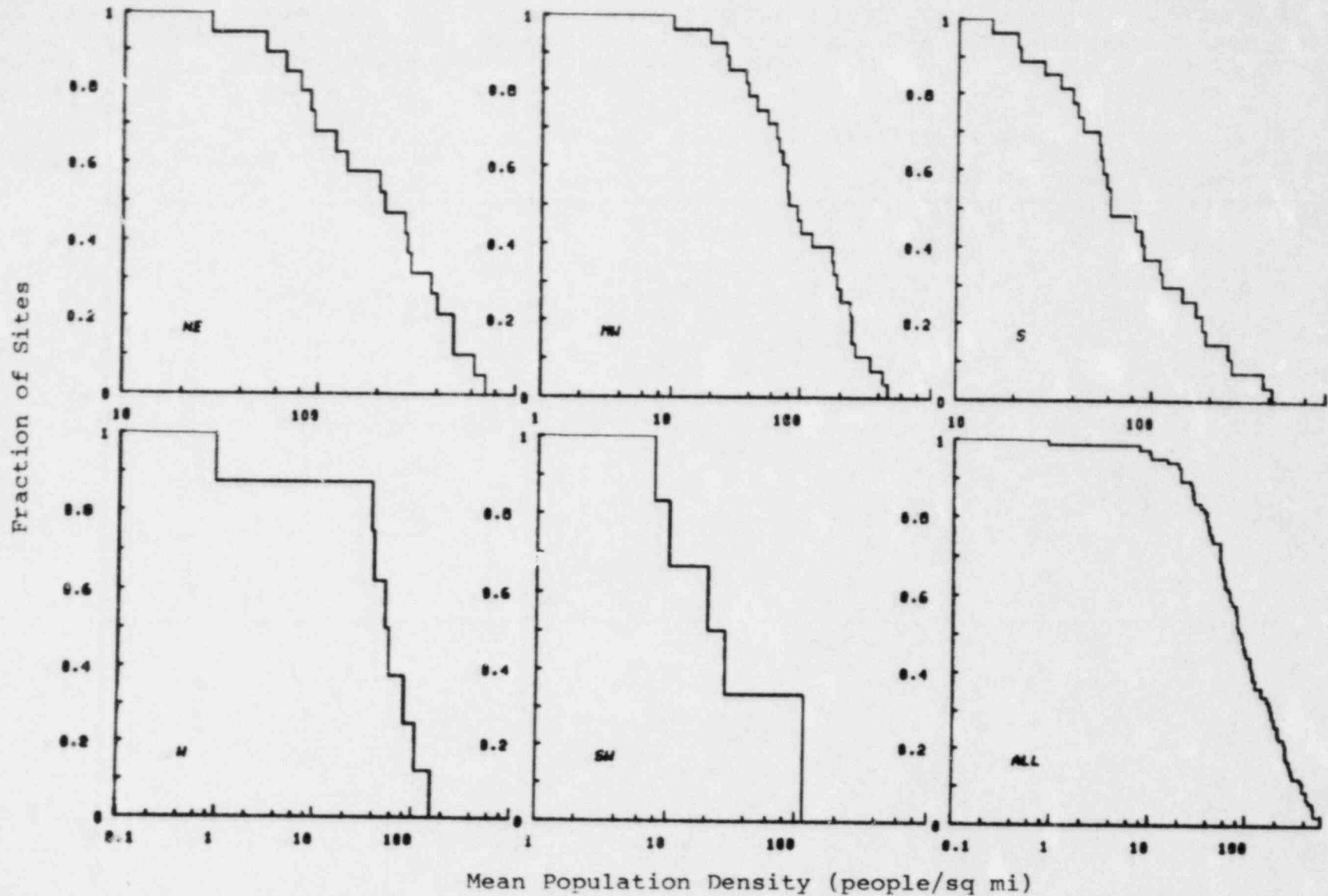


Figure D.1-12. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Radial Distance 0-20 Miles.

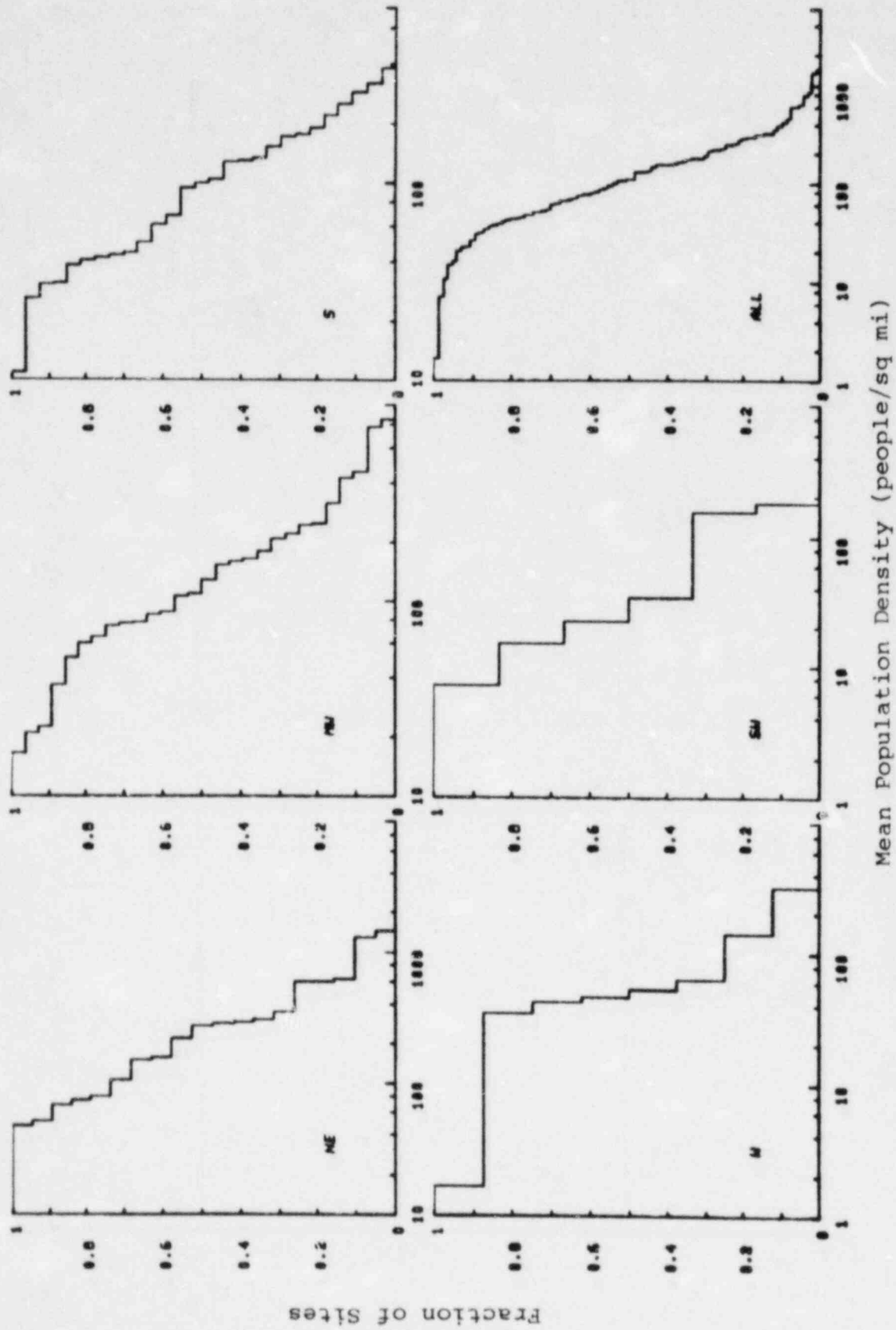


Figure D.1-13. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (ALL): Population Density Within the Radial Distance 0-30 Miles.

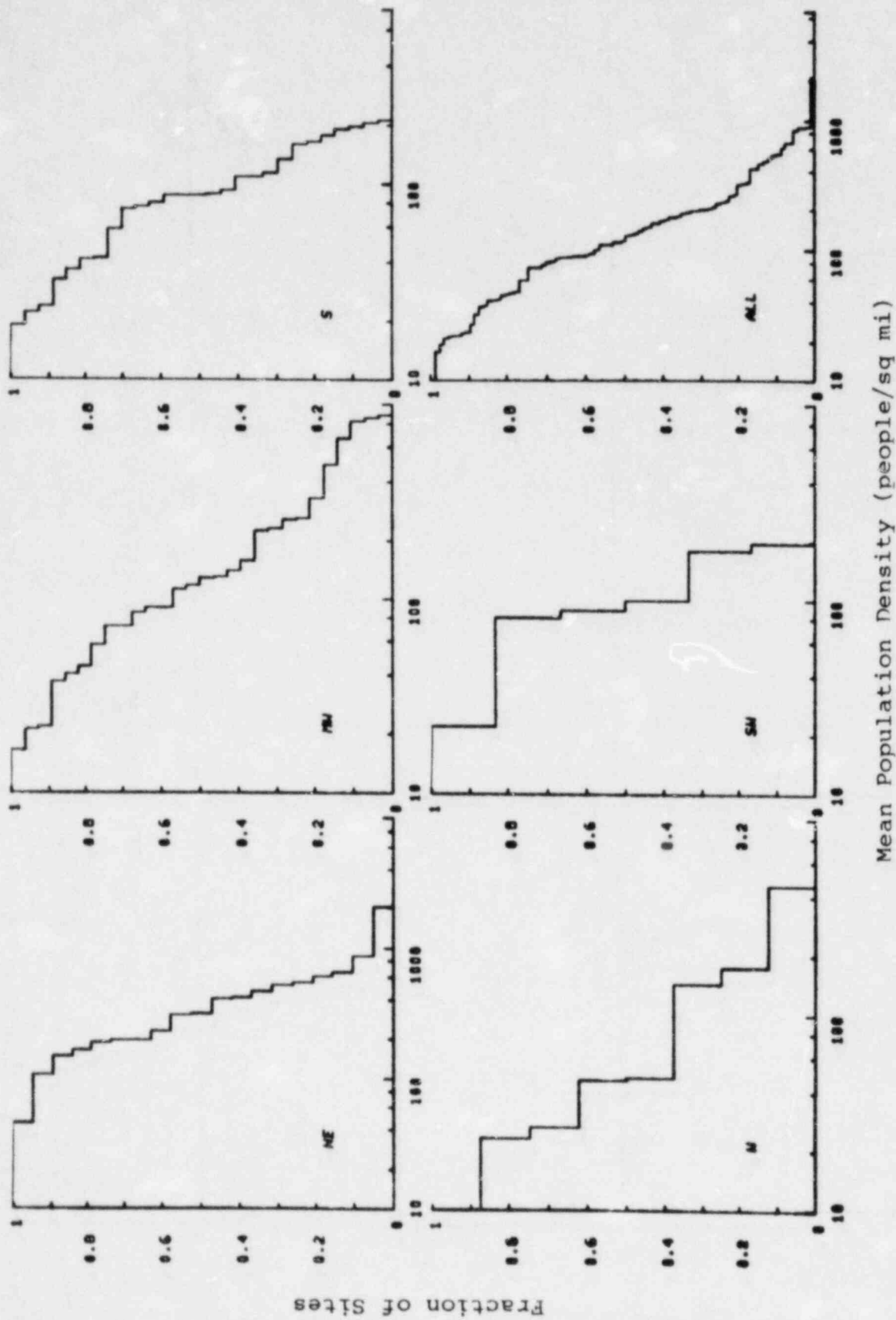


Figure D.1-14. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Radial Distance 0-50 Miles.

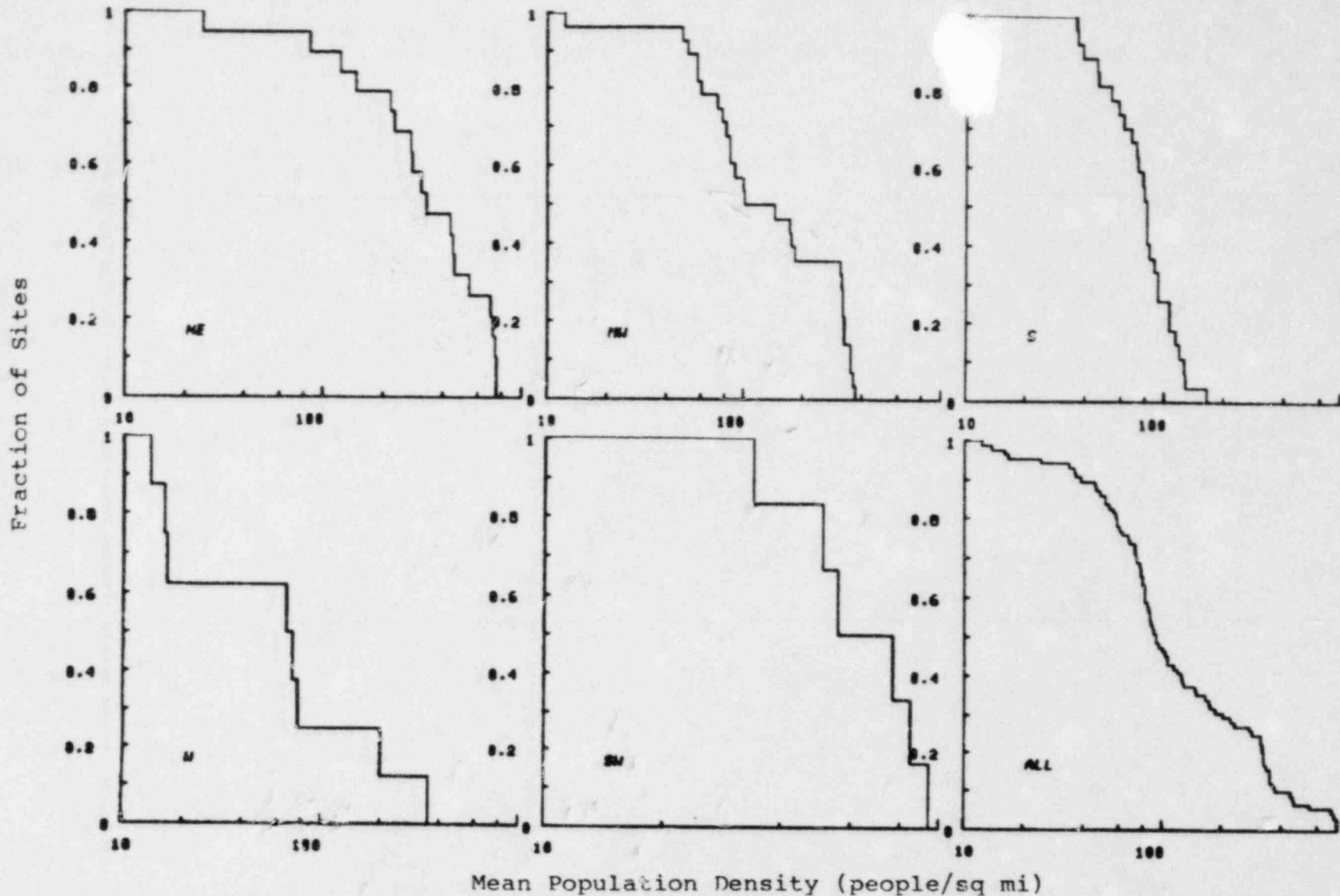


Figure D.1-15. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Radial Distance 0-100 Miles.

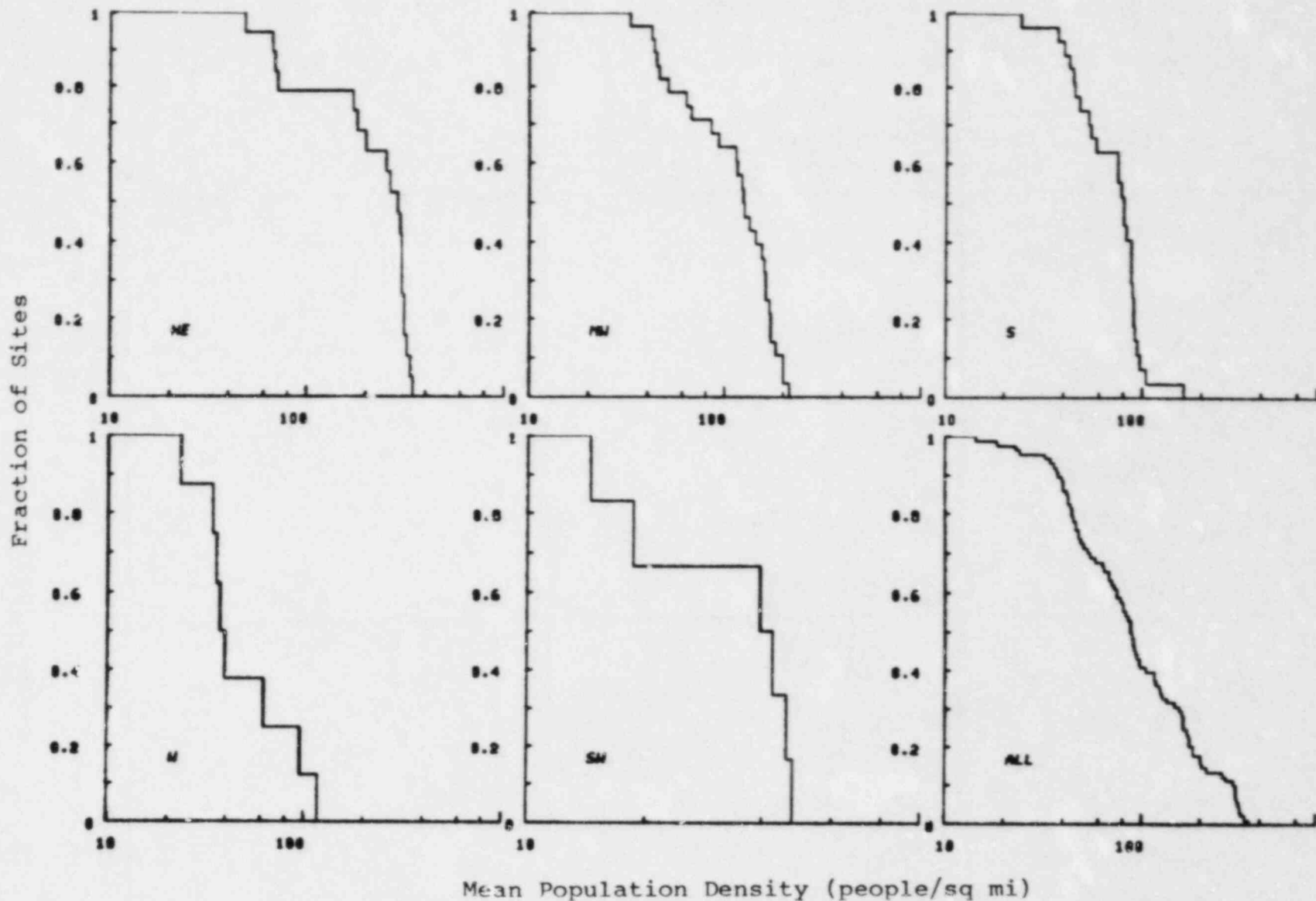


Figure D.1-16. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Radial Distance 0-200 Miles.

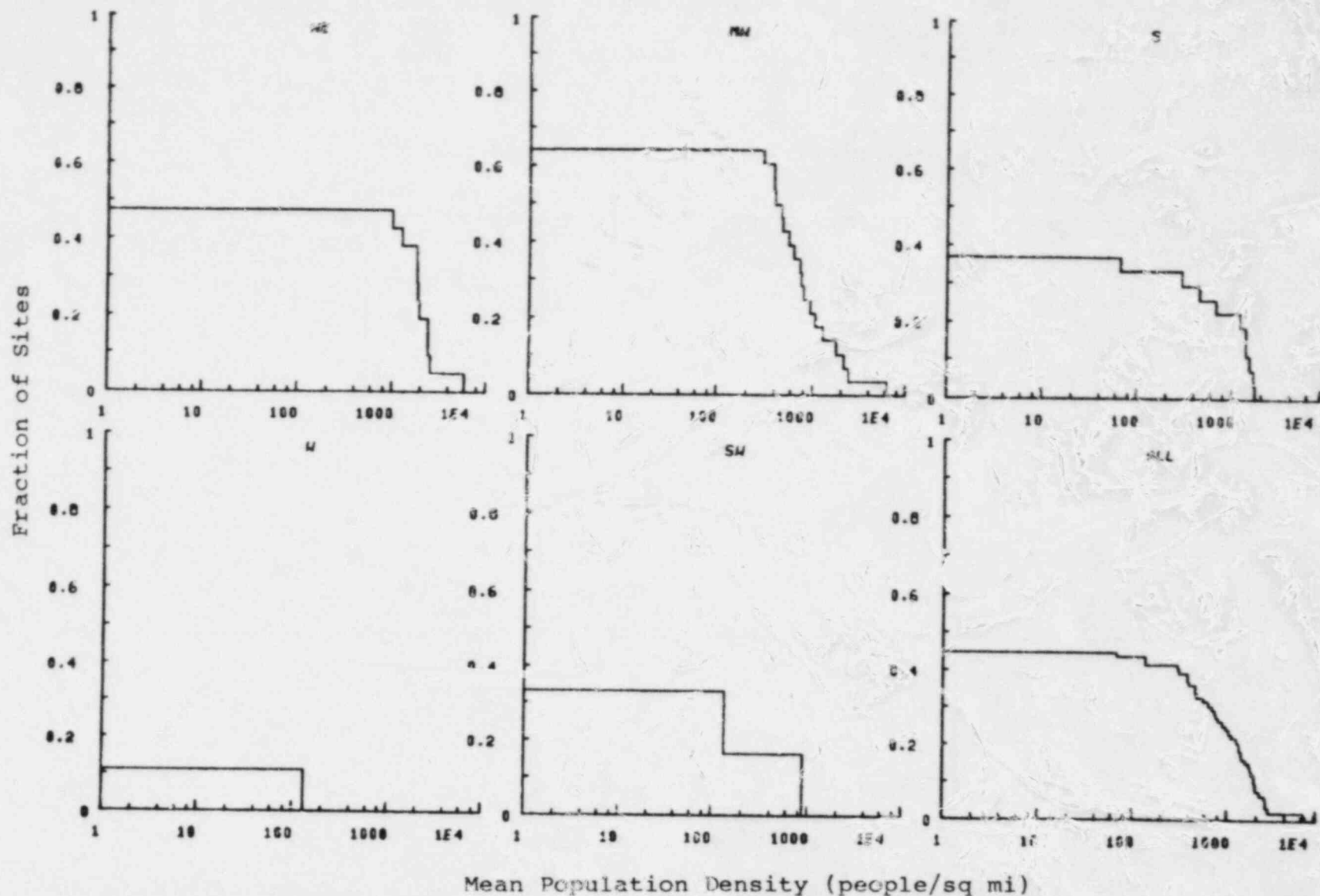
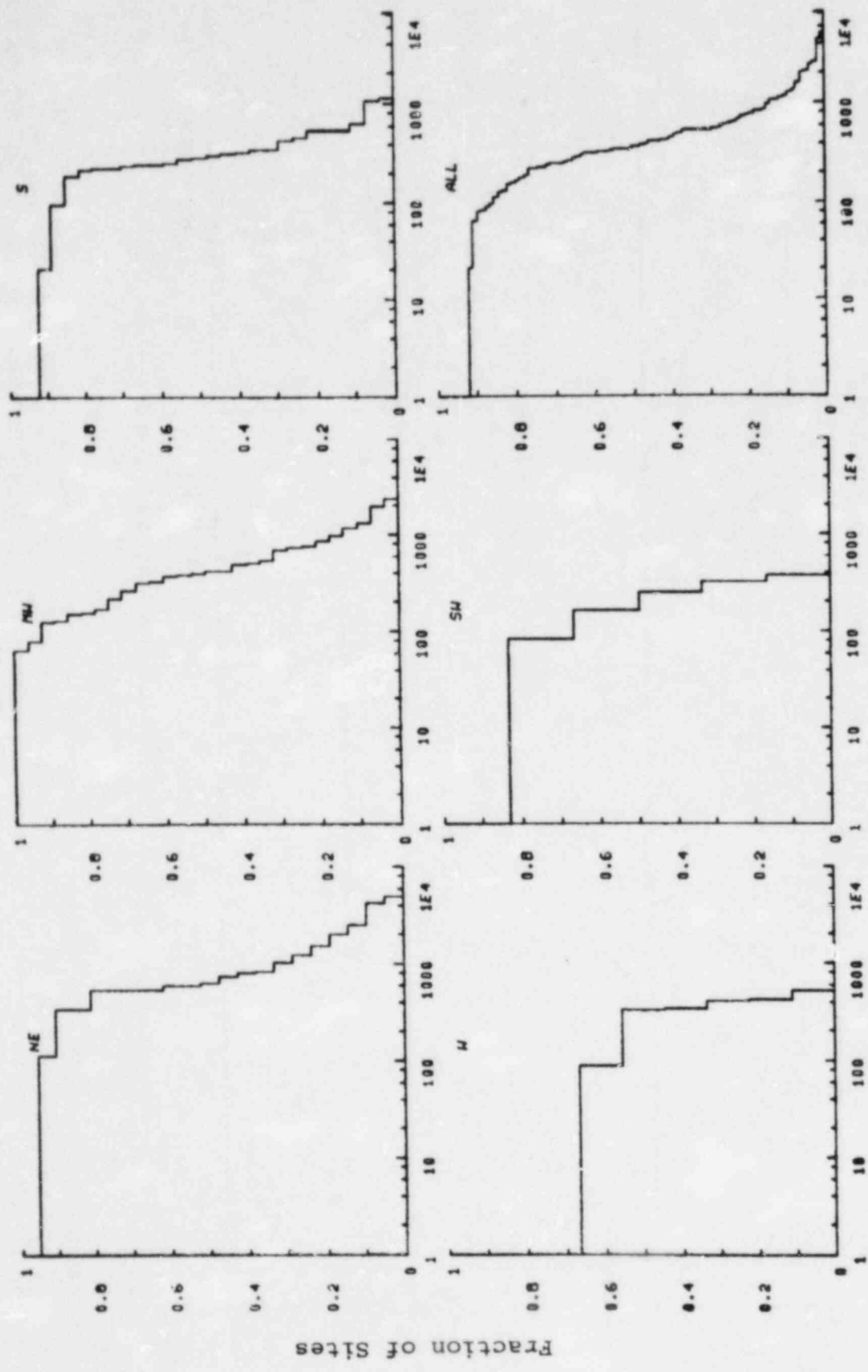


Figure D.1-17. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 22.5° Sector of the Annular Interval 0-2 Miles.



Mean Population Density (people/sq mi)

Figure D.1-18. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (ALL): Population Density Within the Most Populated 22.5° Sector of the Annular Interval 2-5 Miles.

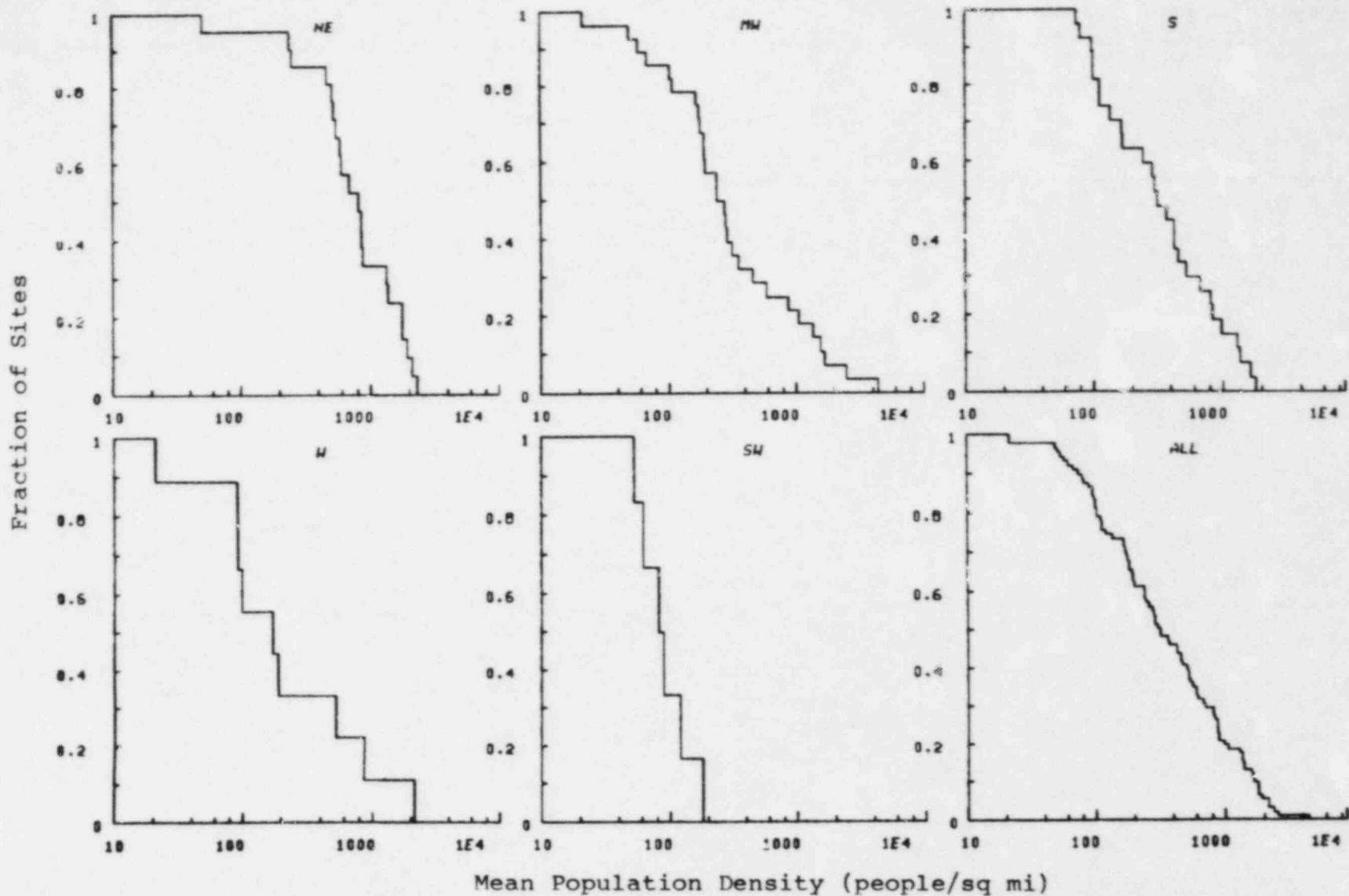


Figure D.1-19. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 22.5° Sector of the Annular Interval 5-10 Miles.

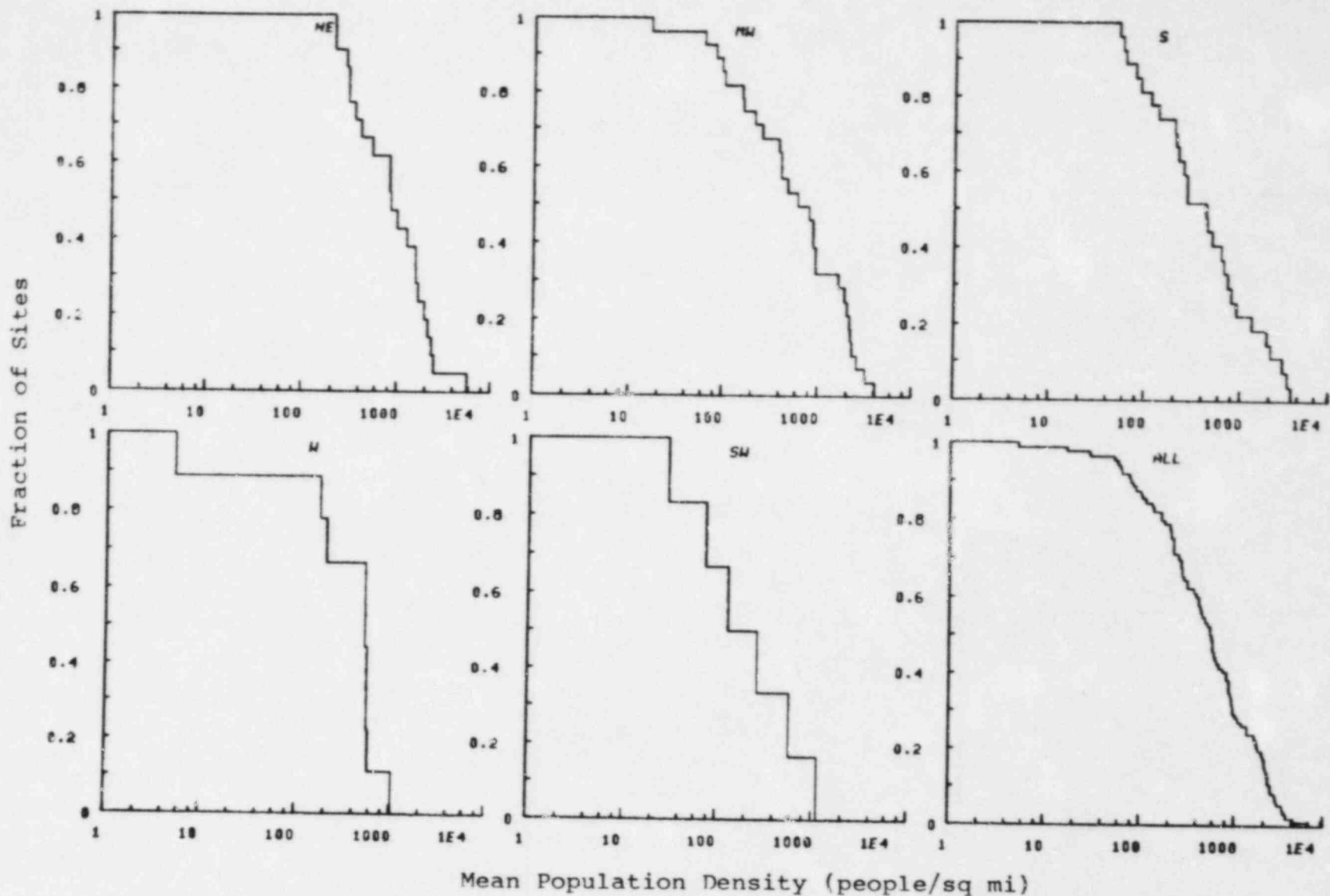


Figure D.1-20. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 22.5° Sector of the Annular Interval 10-20 Miles.

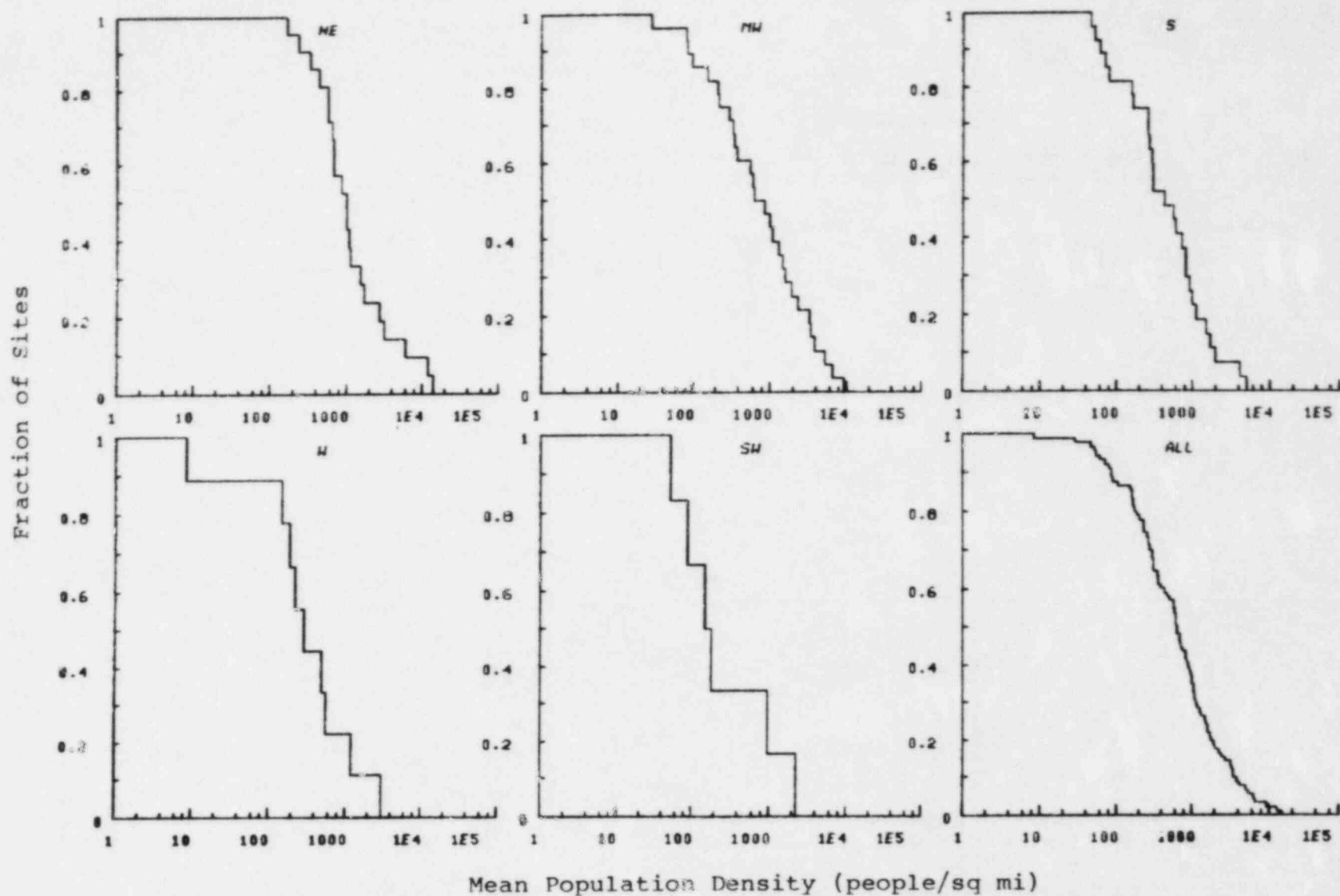


Figure D.1-21. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 22.5° Sector of the Annular Interval 20-30 Miles.

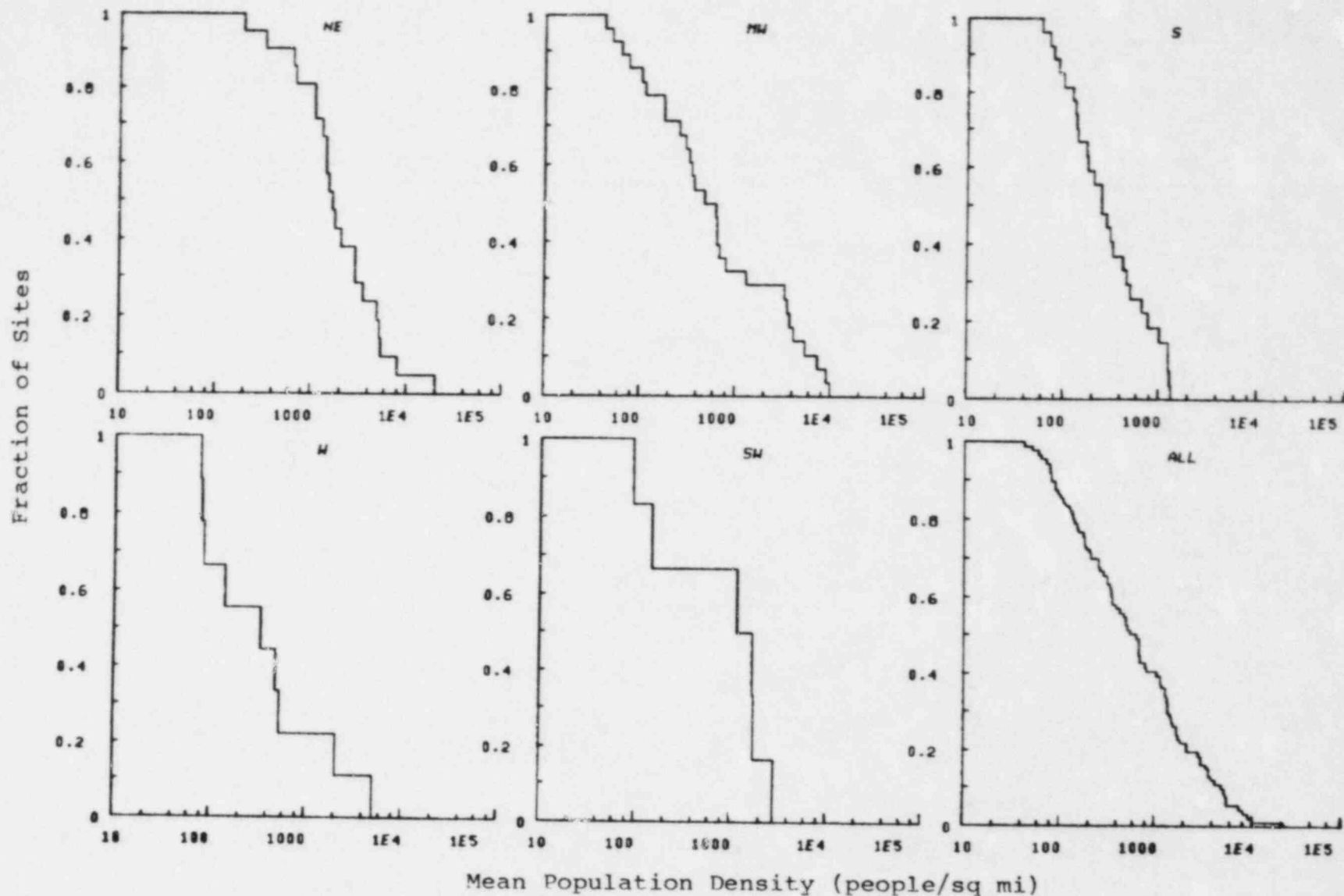


Figure D.1-22. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 22.5° Sector of the Annular Interval 30-50 Miles.

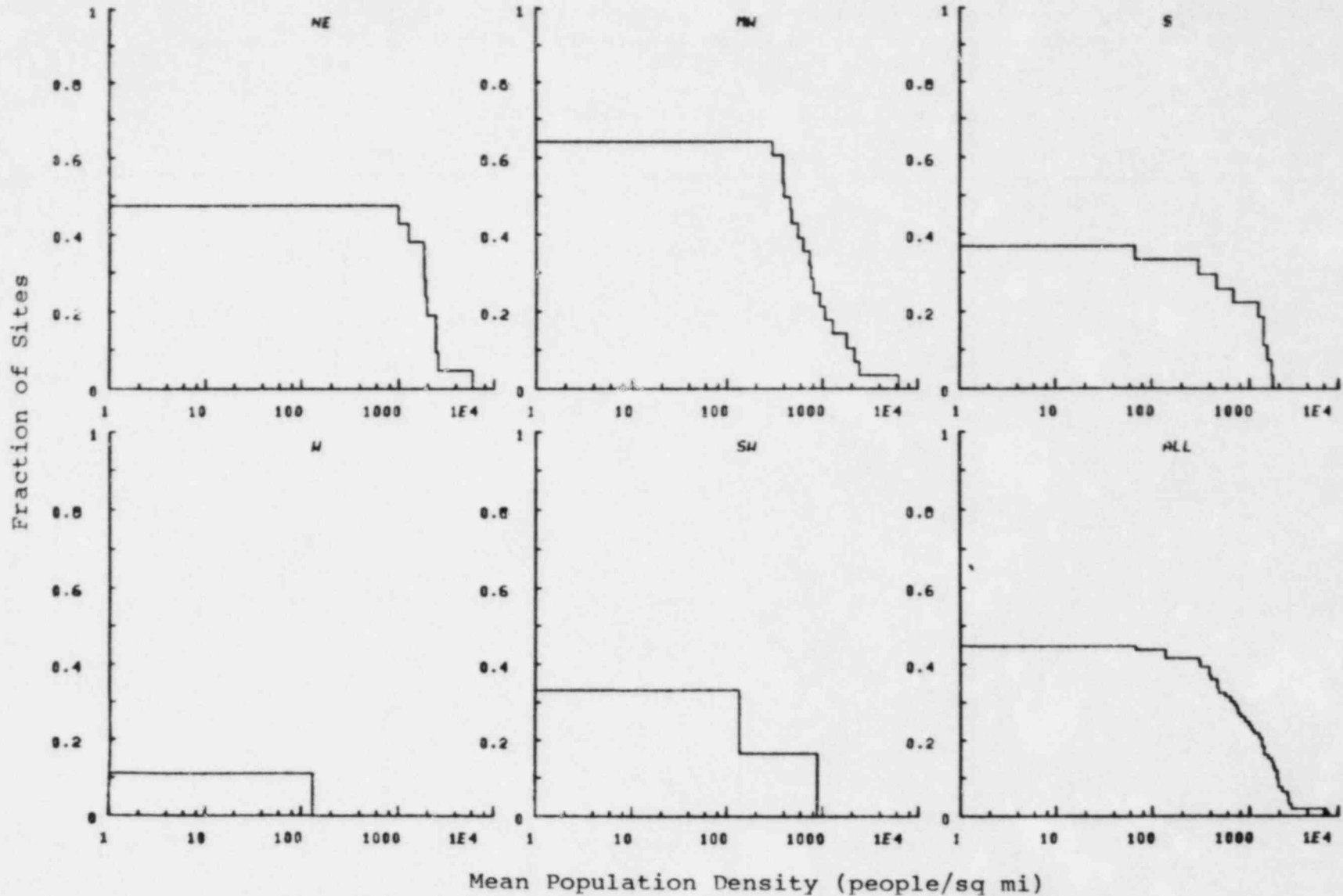


Figure D.1-23. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 22.5° Sector of the Radial Distance 0-2 Miles.

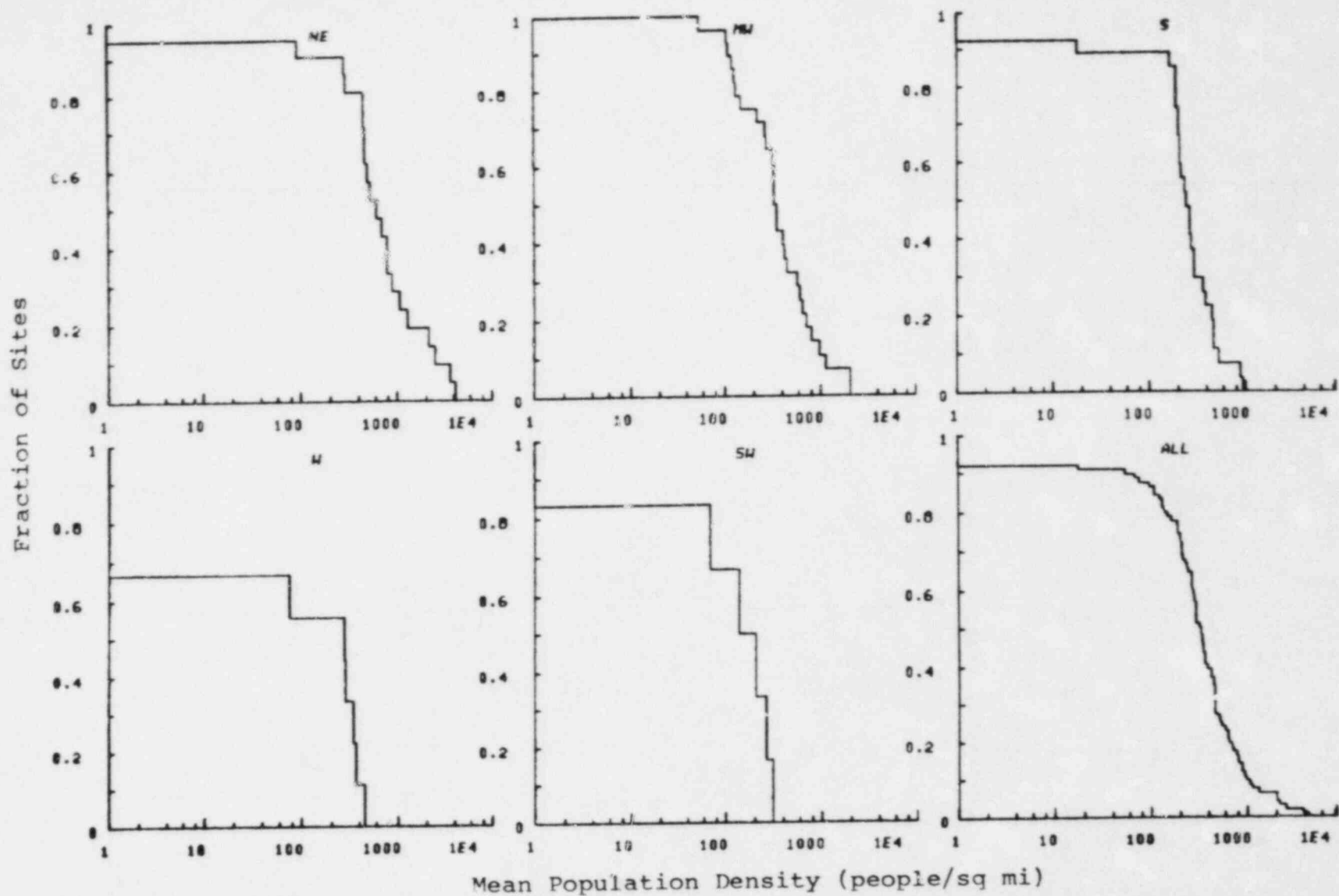


Figure D.1-24. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 22.5° Sector of the Radial Distance 0-5 Miles.

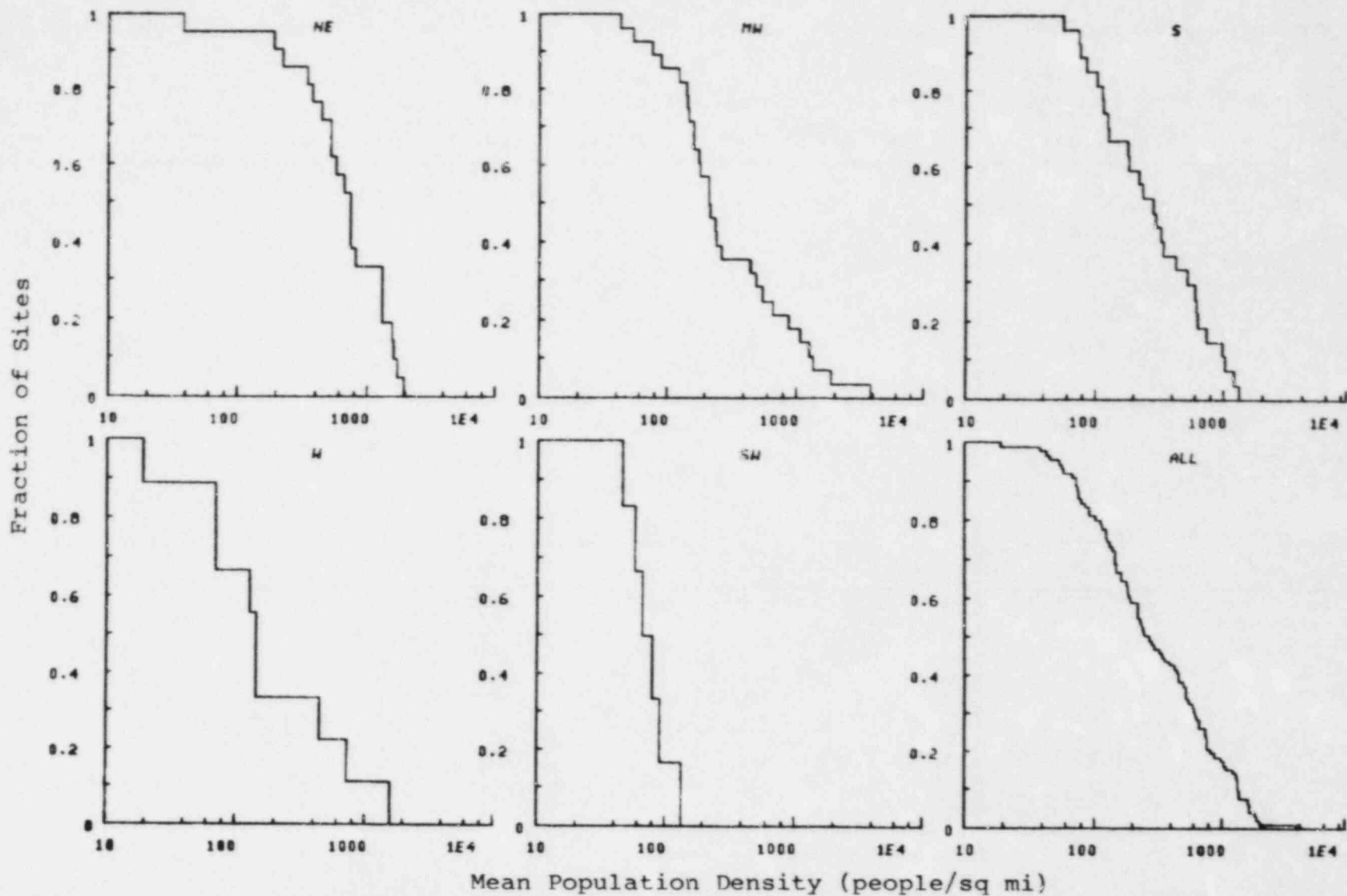


Figure D.1-25. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 22.5° Sector of the Radial Distance 0-10 Miles.

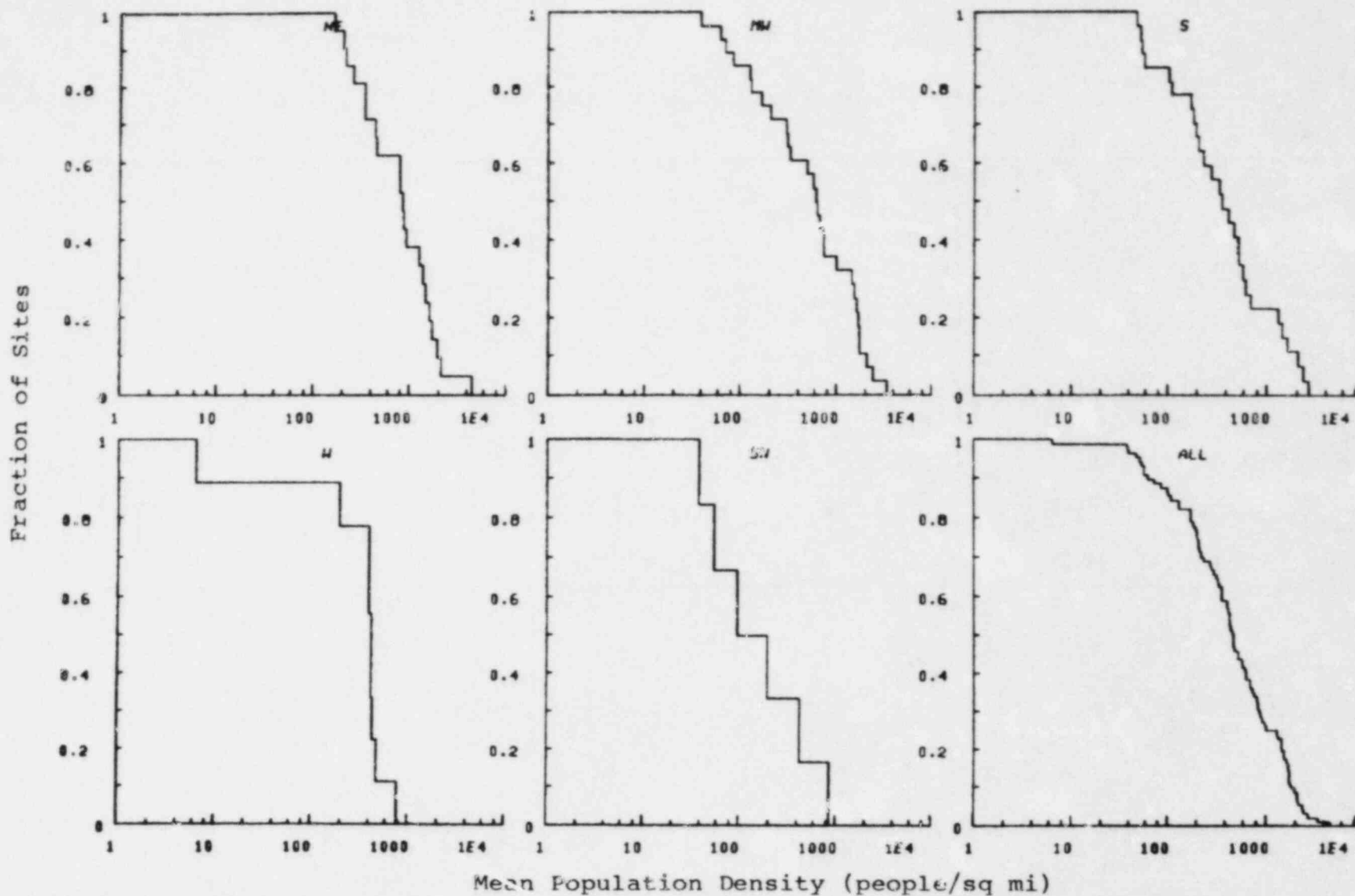


Figure D.1-26. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 22.5° Sector of the Radial Distance 0-20 Miles.

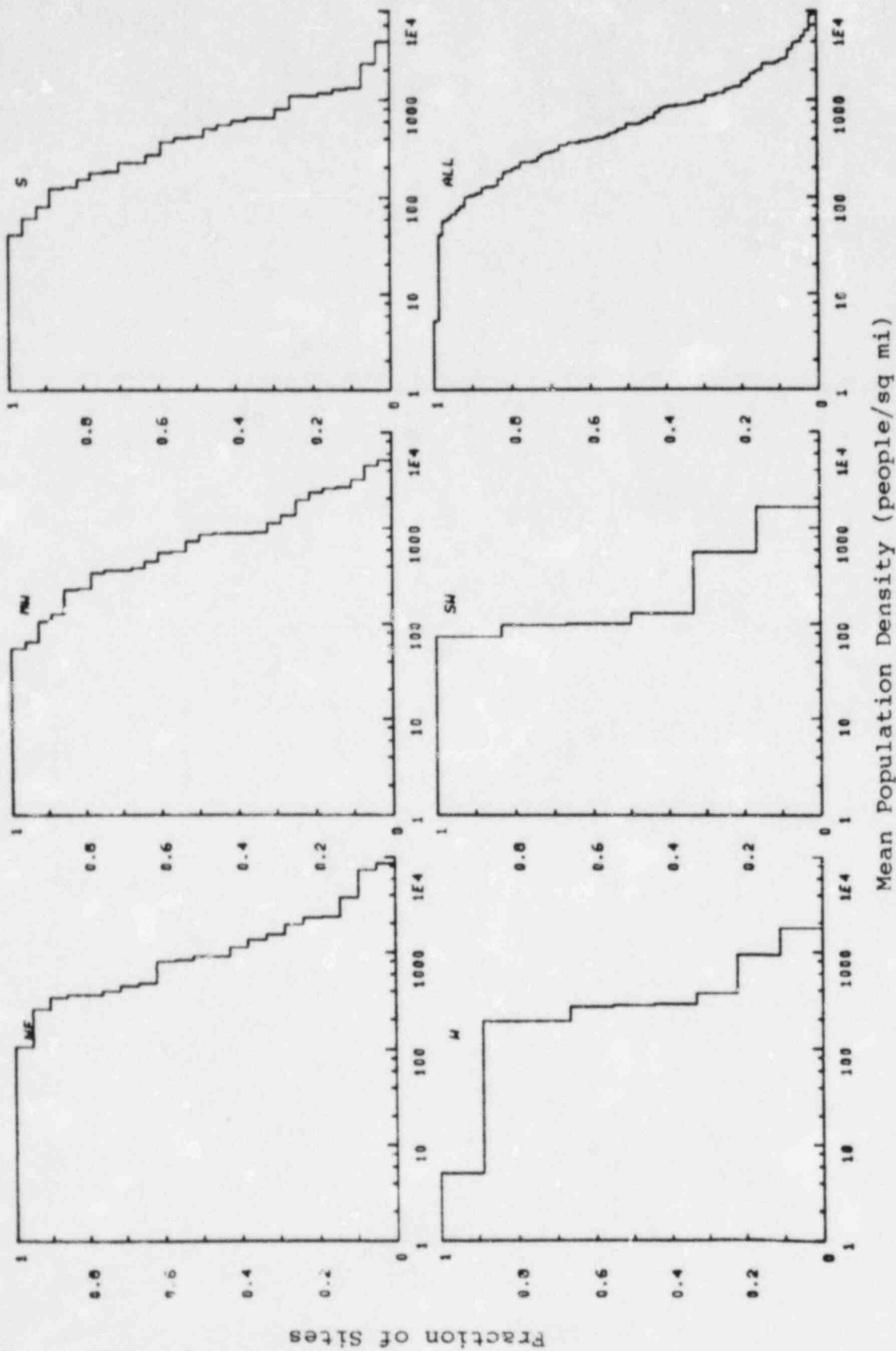


Figure D.1-27. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 22.5° Sector of the Radial Distance 0-30 Miles.

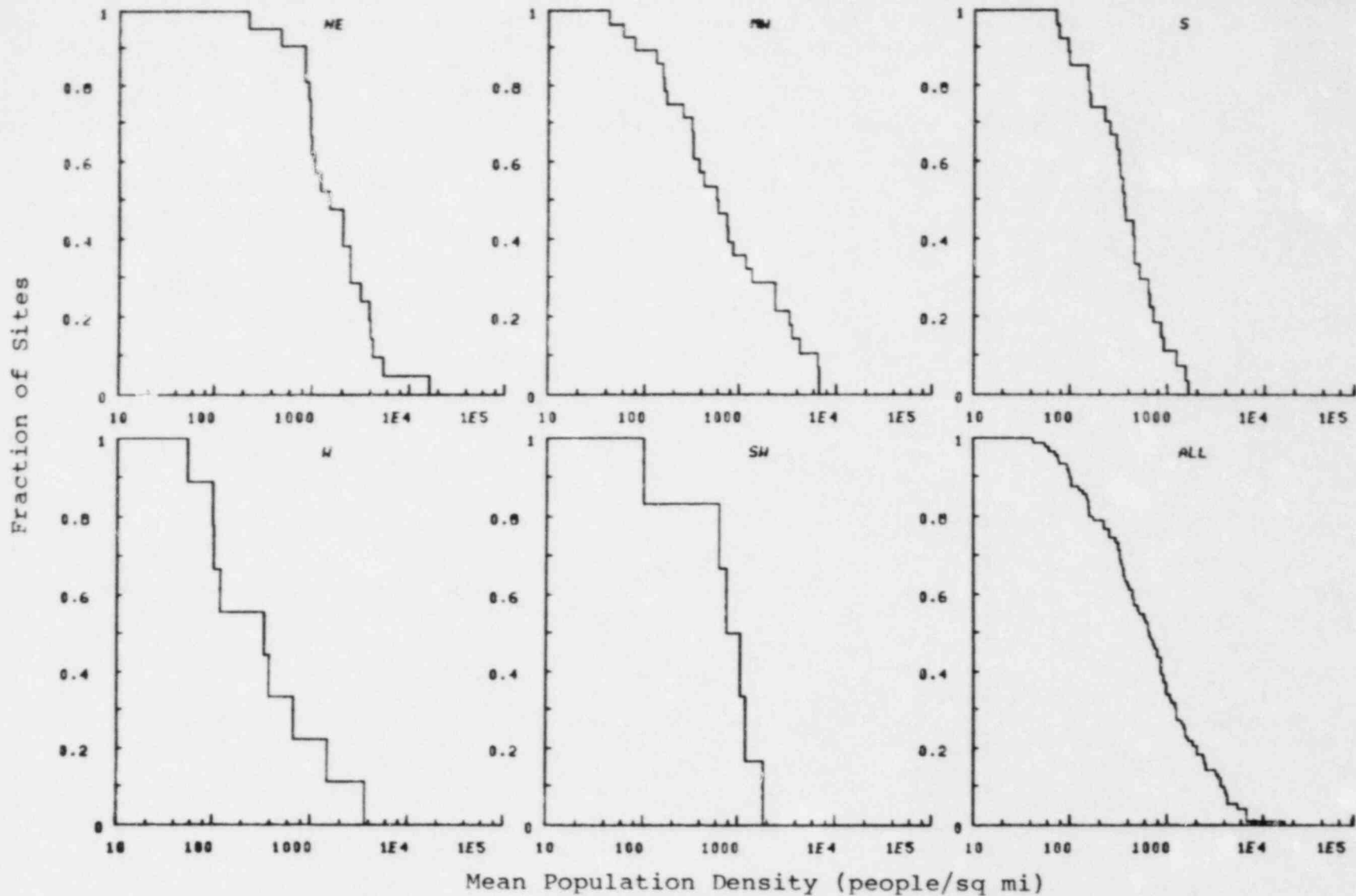


Figure D.1-28. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 22.5° Sector of the Radial Distance 0-50 Miles.

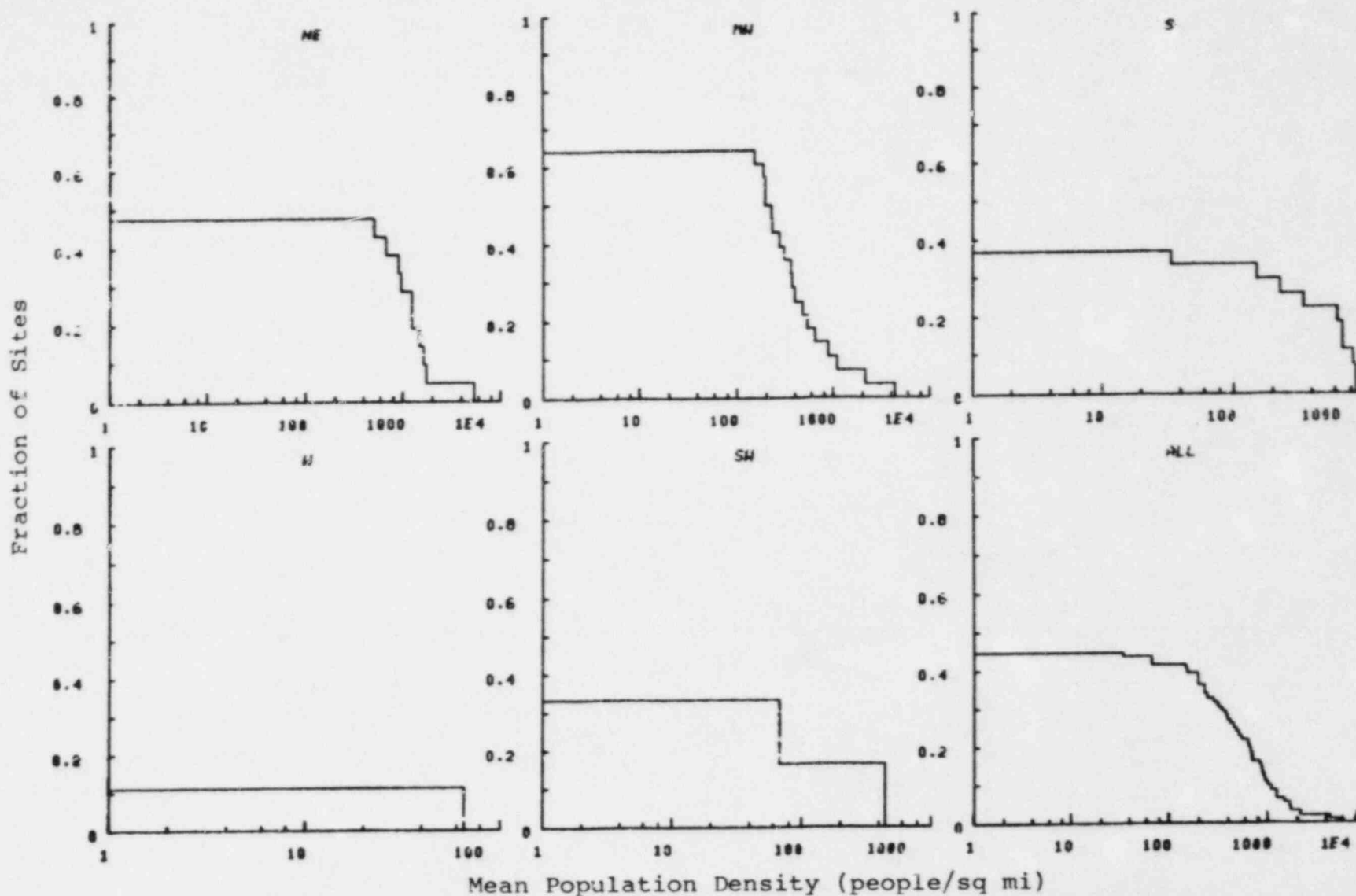


Figure D.1-29. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 45° Sector (two adjacent 22.5° sectors) of the Annular Interval 0-2 Miles.

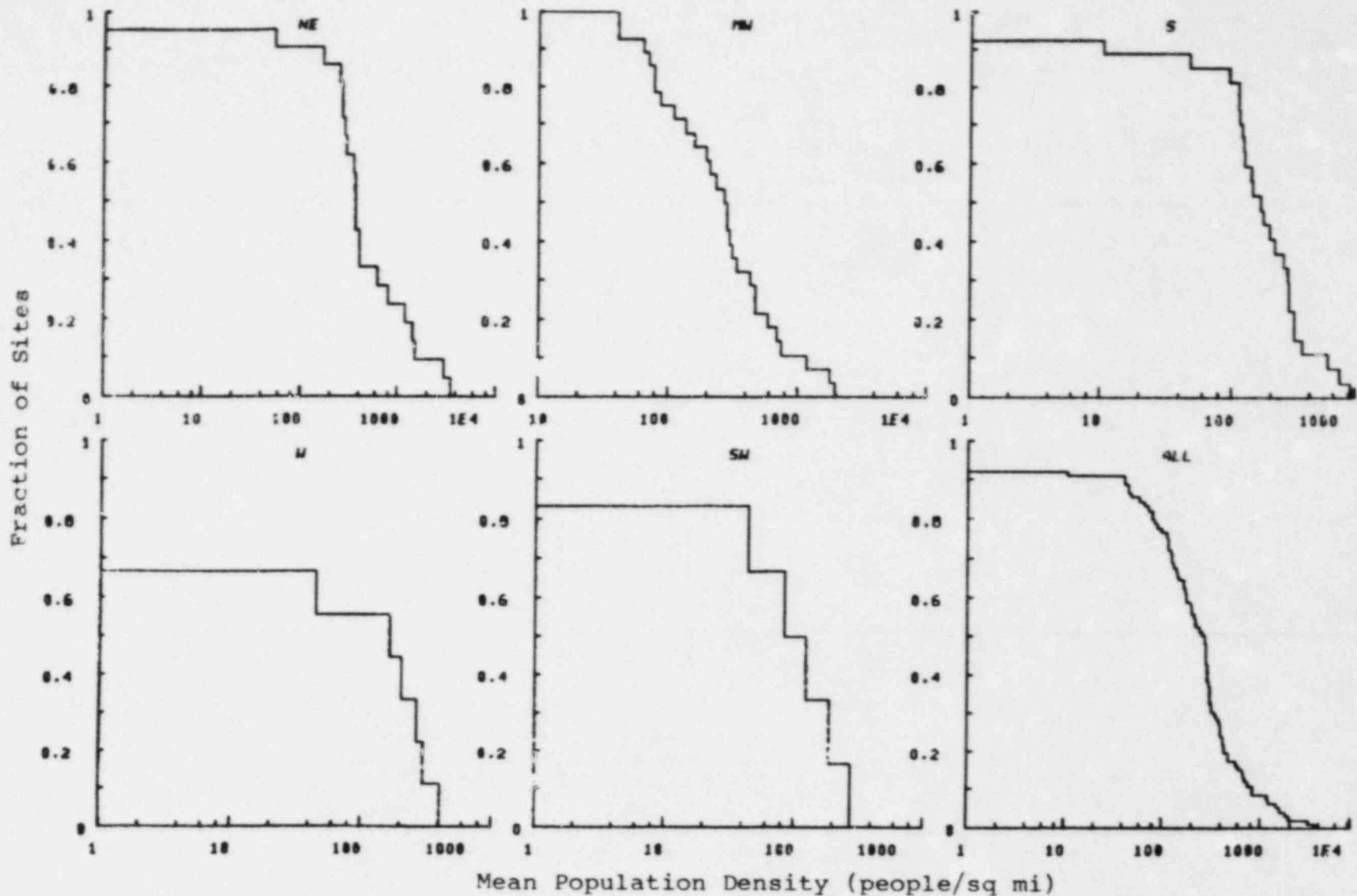


Figure D.1-30. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 45° Sector (two adjacent 22.5° sectors) of the Annular Interval 2-5 Miles.

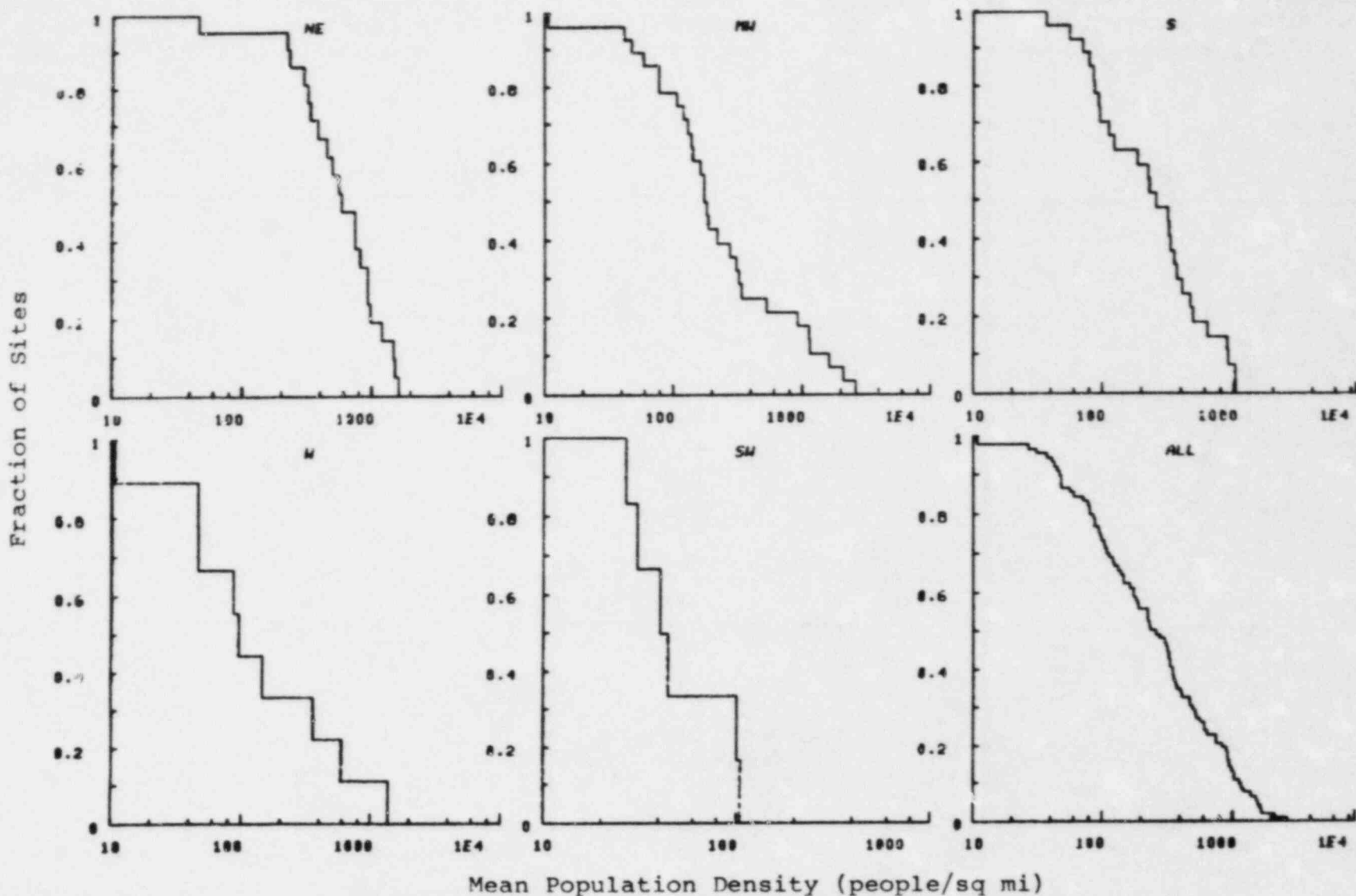


Figure D.1-31. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 45° Sector (two adjacent 22.5° sectors) of the Annular Interval 5-10 Miles.

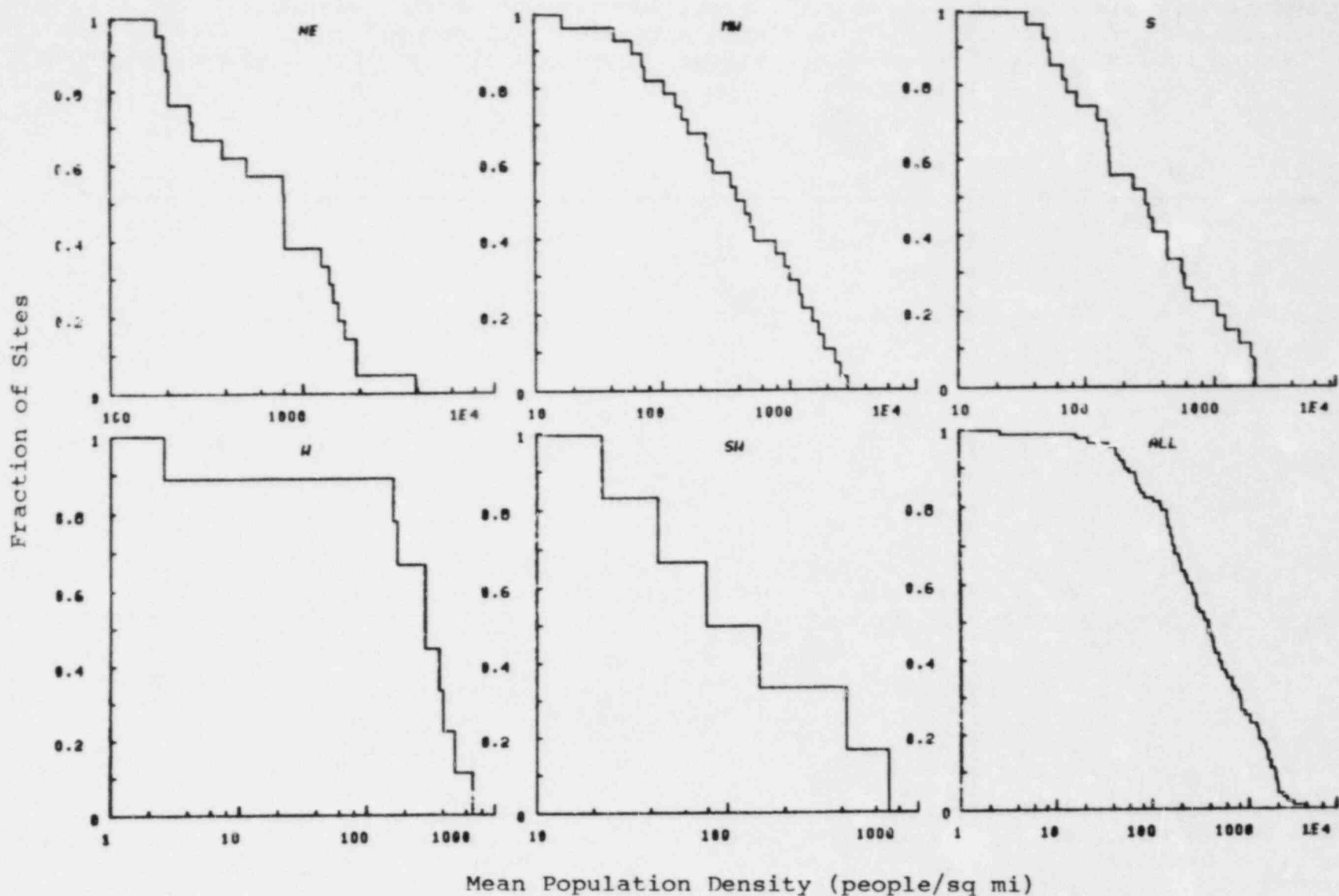


Figure D.1-32. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 45° Sector (two adjacent 22.5° sectors) of the Annular Interval 10-20 Miles.

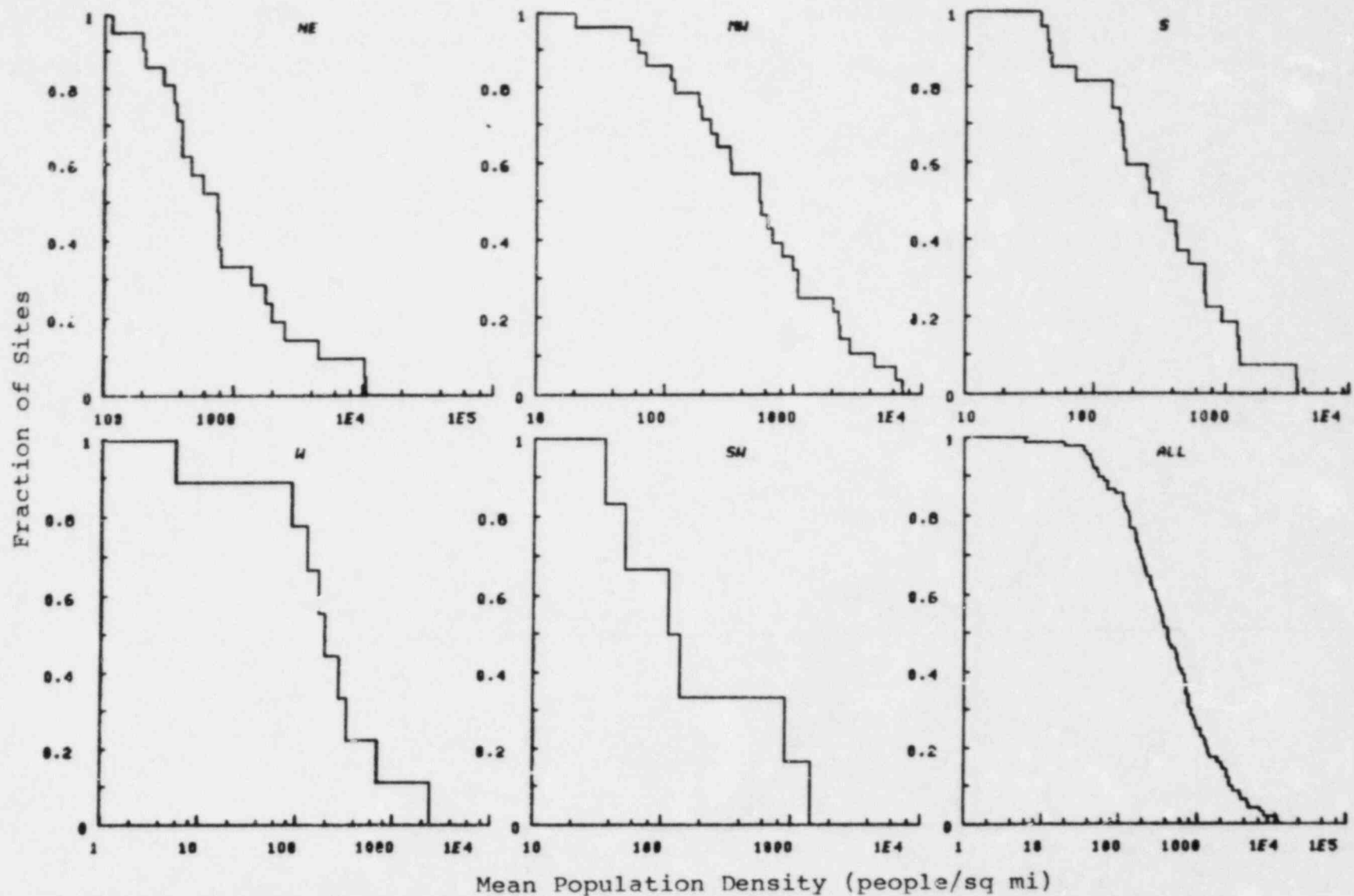


Figure D.1-33. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 45° Sector (two adjacent 22.5° sectors) of the Annular Interval 20-30 Miles.

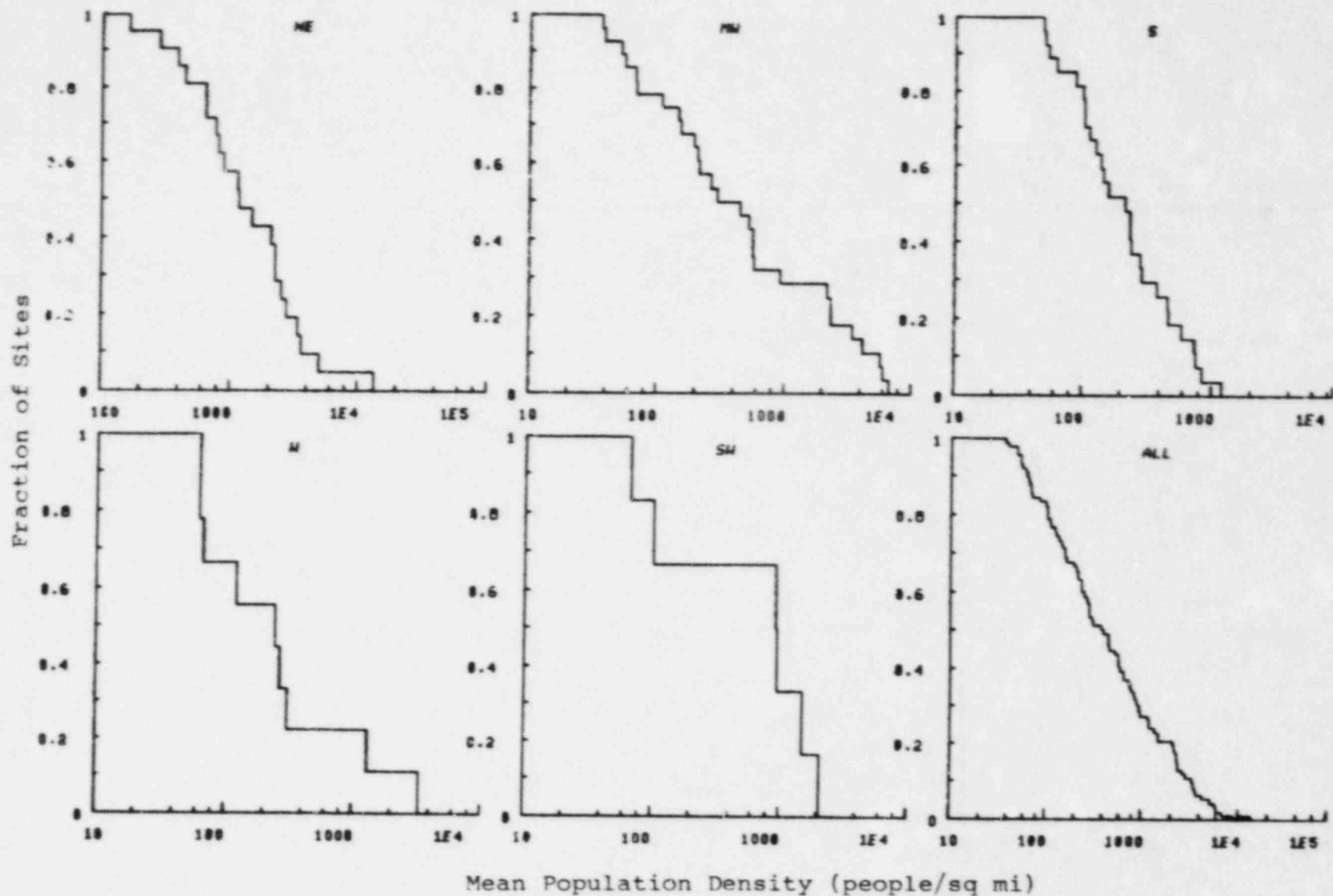


Figure D.1-34. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 45° Sector (two adjacent 22.5° sectors) of the Annular Interval 30-50 Miles.

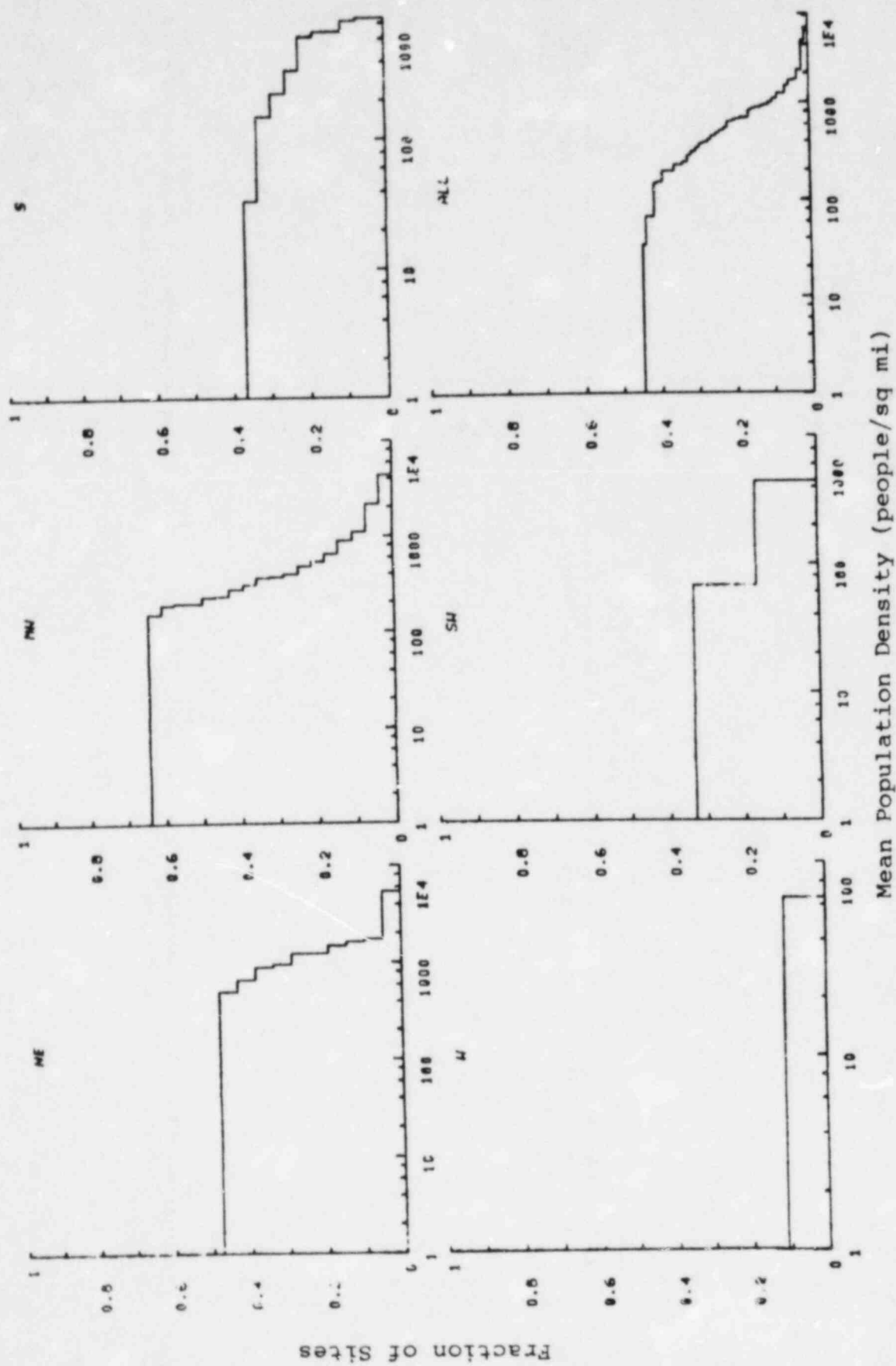


Figure D.1-35. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (ALL): Population Density Within the Most Populated 45° Sector (two adjacent 22.5° sectors) of the Radial Distance 0-2 Miles.

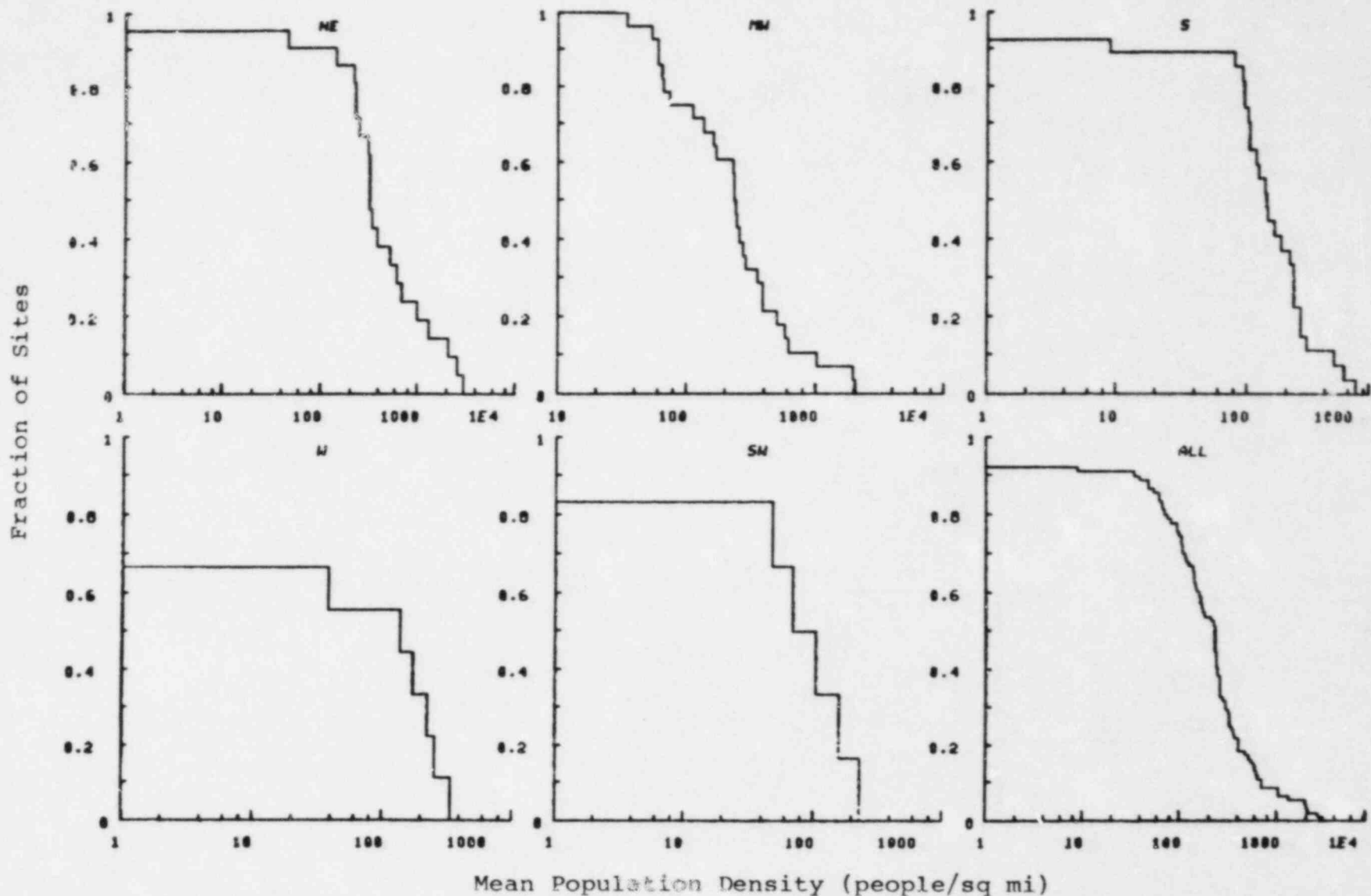


Figure D.1-36. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 45° Sector (two adjacent 22.5° sectors) of the Radial Distance 0-5 Miles.

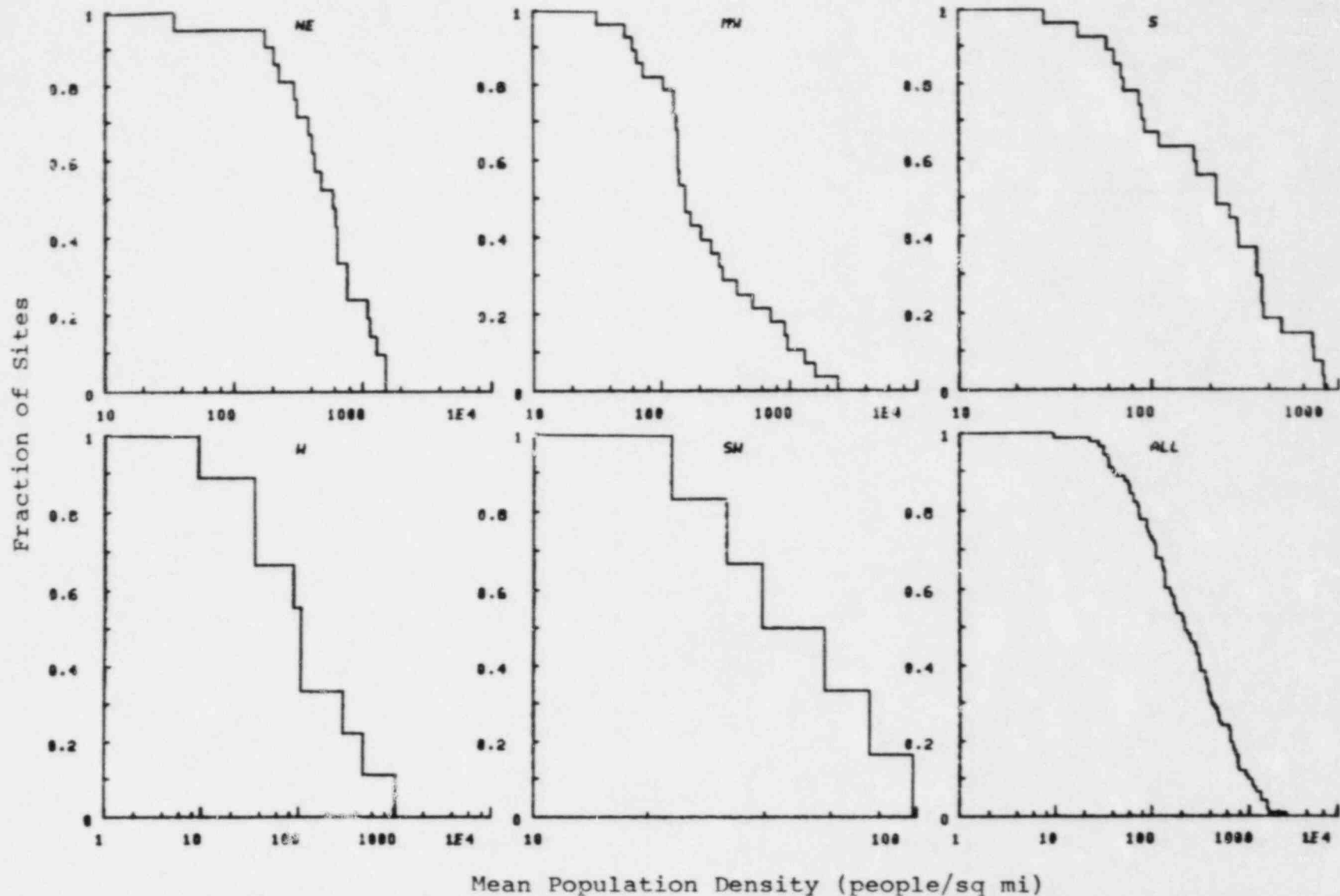


Figure D.1-37. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 45° Sector (two adjacent 22.5° sectors) of the Radial Distance 0-10 Miles.

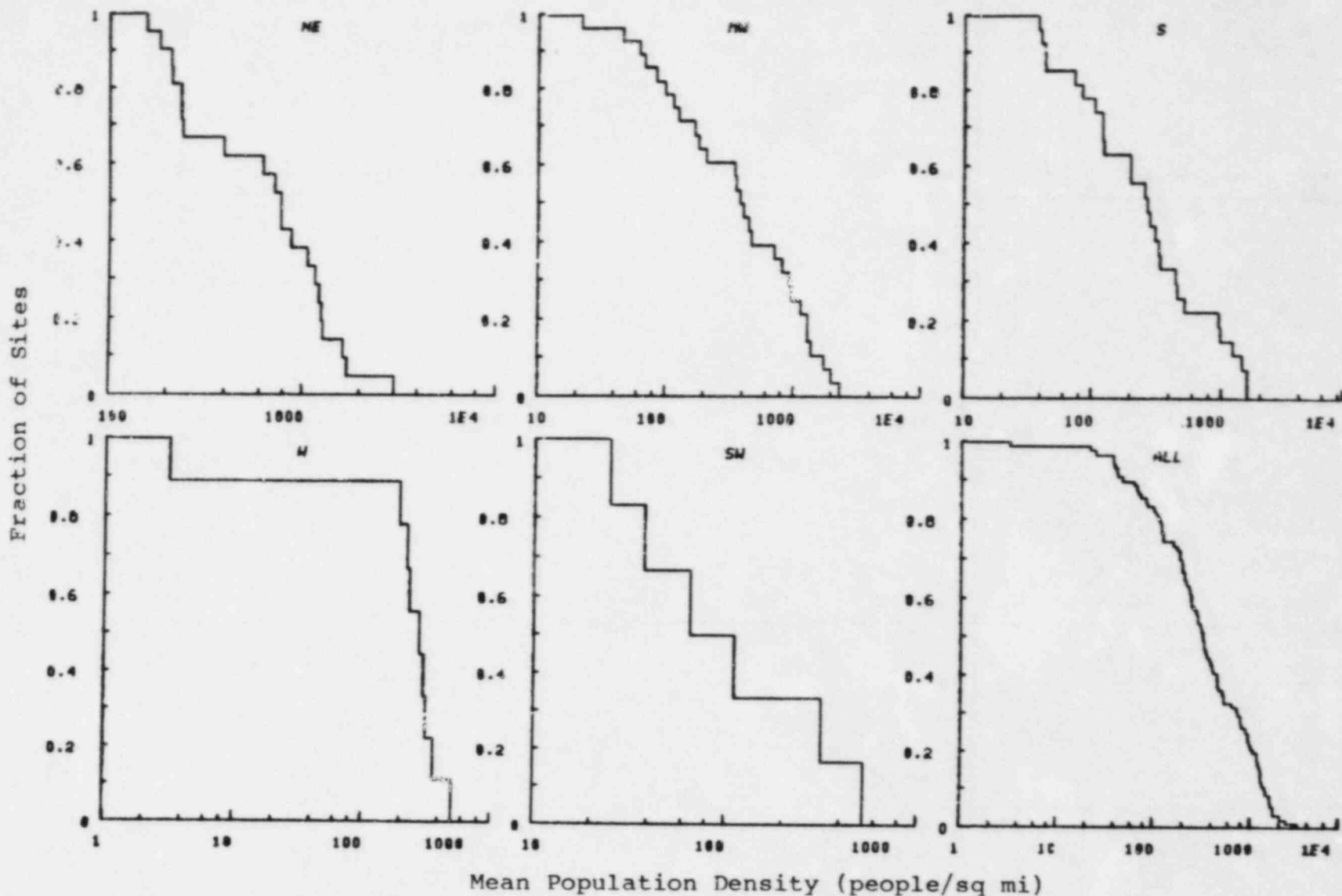


Figure D.1-38. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 45° Sector (two adjacent 22.5° sectors) of the Radial Distance 0-20 Miles.

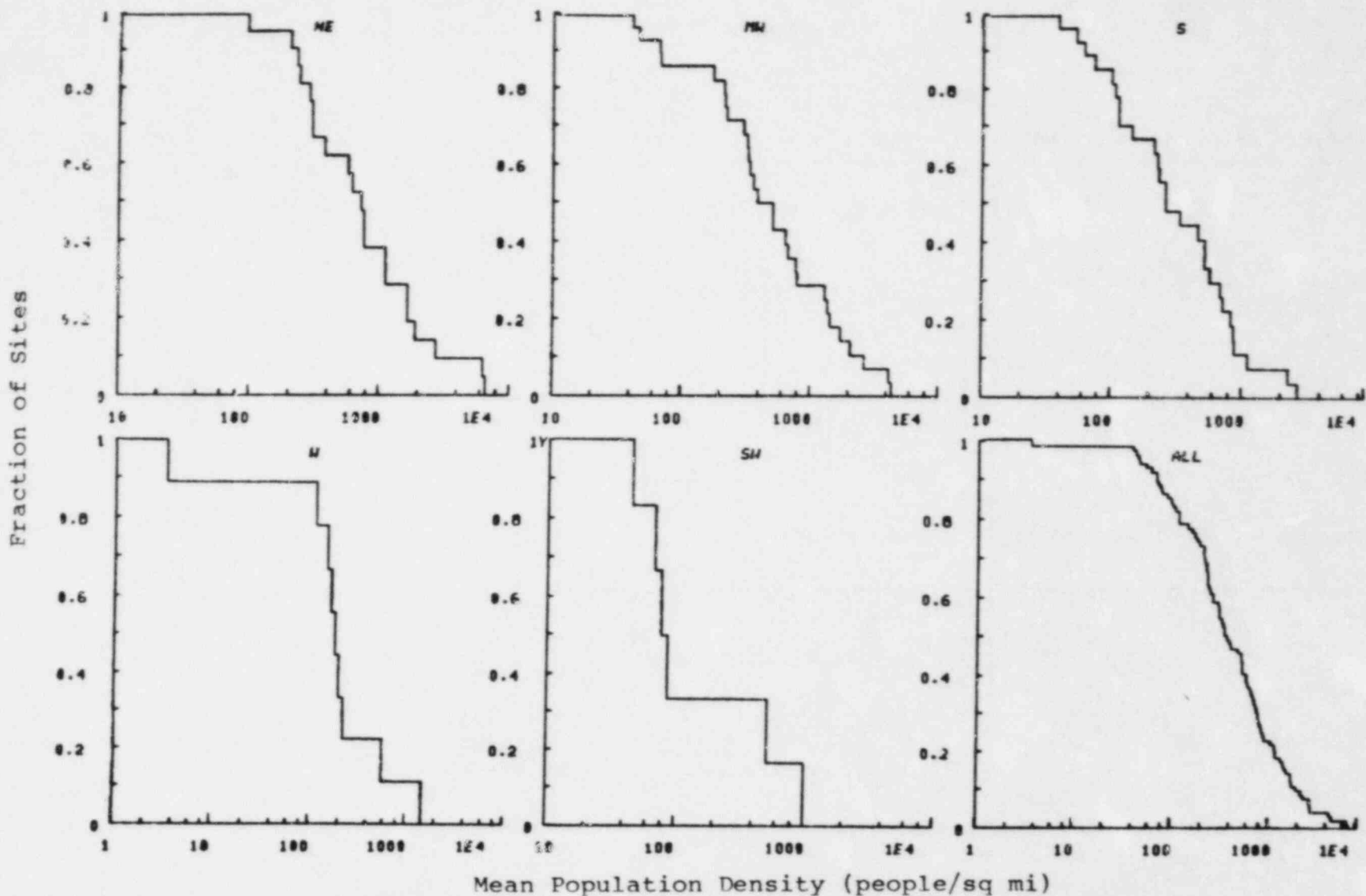


Figure D.1-39. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 45° Sector (two adjacent 22.5° sectors) of the Radial Distance 0-30 Miles.

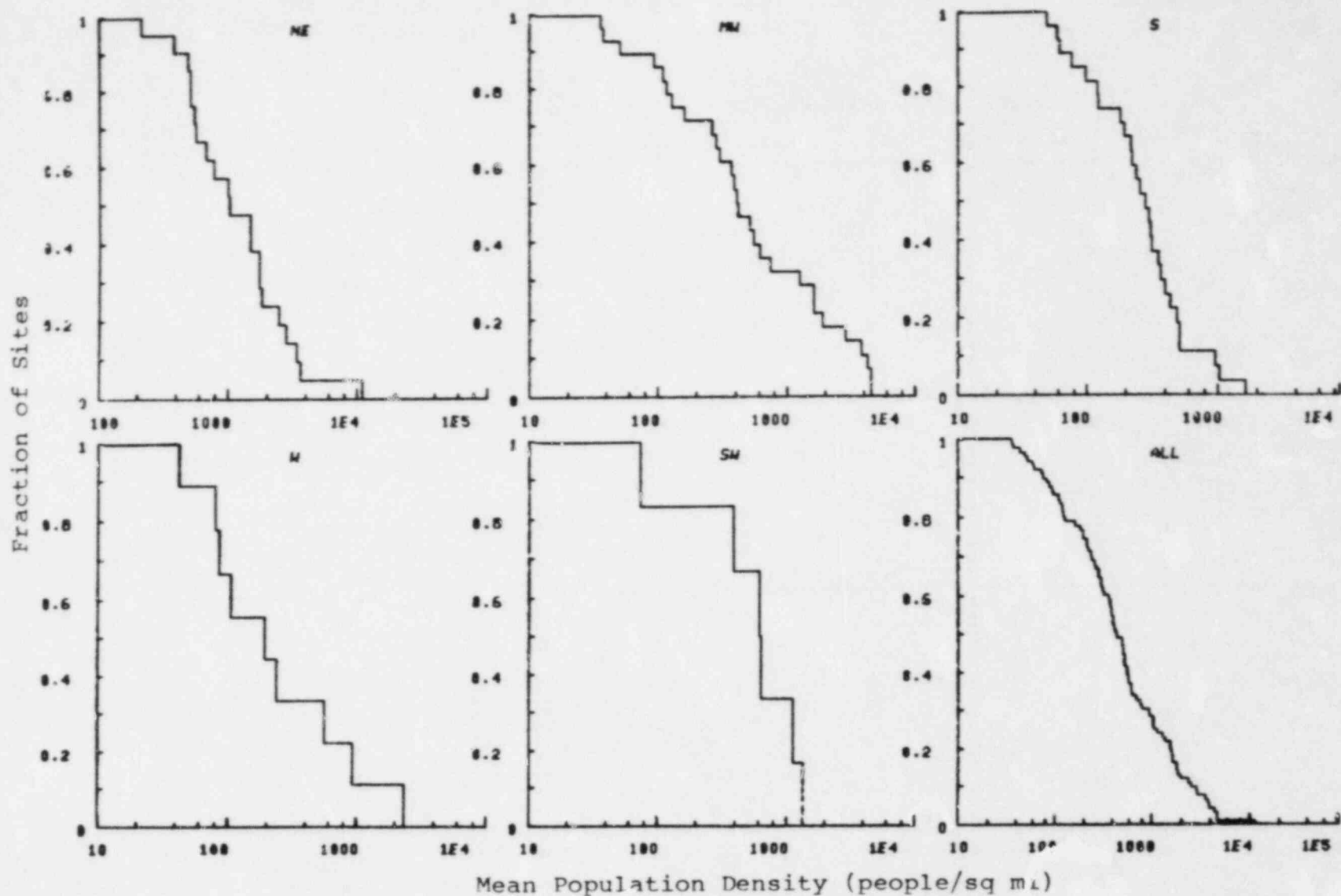


Figure D.1-40. CCDFs of Population Density (people/sq mi) at 91 Reactor Sites for the Five NRC Administrative Regions (NE, MW, S, W, SW) and for All Regions Combined (All): Population Density Within the Most Populated 45° Sector (two adjacent 22.5° sectors) of the Radial Distance 0-50 Miles.

TABLE D.1-1

POPULATION DENSITIES (PEOPLE PER SQ. MI.) FOR 91 REACTOR SITES
INNER AND OUTER ANNULAR RADII ARE GIVEN IN MILES

SITE	0-5	5-10	10-20	20-30	30-50	50-100	100-200
1 ALLENS CREEK	31	21	30	39	286	48	35
2 ARKANSAS 1 + 2	58	83	26	16	15	42	47
3 BAILLY S	271	283	534	1024	906	145	134
4 BEAVER VALLEY 1 + 2	160	565	342	787	403	210	139
5 BELLEFONTE 1	21	89	30	41	147	87	76
6 BIG ROCK POINT	54	14	27	9	16	11	39
7 BLACK FOX	29	10	147	234	36	38	35
8 BRAIDWOOD 1	127	53	79	168	700	258	111
9 BROWNS FERRY 1, 2, +	12	121	88	98	71	76	80
10 BRUNSWICK 1 + 2	31	25	62	26	13	40	48
11 BYRON 1	83	59	250	127	85	439	74
12 CALLAWAY	8	12	32	87	24	123	56
13 CALVERT CLIFF 1 + 2	34	52	55	51	456	201	167
14 CATAWBA 1	49	237	431	154	107	116	73
15 CHEROKEE	48	113	113	220	162	95	91
16 CLINTON	18	46	36	168	79	68	188
17 COMMANCHE PEAK	20	20	7	33	142	94	30
18 COOK DC 1 + 2	93	157	115	226	117	418	169
19 COOPER S	14	22	19	22	22	70	40
20 CRYSTAL RIVER	15	30	11	8	31	89	25
21 DAVIS-BE 1	31	55	89	380	212	350	158
22 DIABLO CANYON 1 + 2	0	30	69	32	17	13	151
23 DRESDEN 2 + 3	68	118	199	259	1157	156	108
24 DUANE ARNOLD	50	346	42	37	54	58	94
25 FARLEY 1 + 2	22	29	71	27	41	48	55
26 FERMI 2	126	259	386	1254	562	194	125
27 FITZPATRICK	29	150	50	72	129	79	67
28 FORKED RIVER 1	76	131	146	176	565	875	148
29 FORT CALHOUN	101	25	312	182	23	34	42
30 FORT ST VRAIN	9	35	143	188	192	15	6
31 R. E. GINNA	77	124	611	143	67	114	52
32 GRAND GULF 1	16	28	19	40	40	49	57
33 HADDEM NECK	113	211	473	803	305	822	158
34 HARTSVILLE	44	37	61	46	148	46	83
35 HATCH, E.I. 1 + 2	13	20	38	28	33	41	64
36 INDIAN PT 2 + 3	752	617	732	2046	2462	304	196
37 KEWAUNEE	21	33	80	99	66	84	139
38 LASALLE 1 + 2	12	53	90	75	140	391	118
39 LA CROSSE	13	22	89	34	35	55	106
40 LIMERICK 1	792	381	668	1877	619	705	169
41 MARBLE HILL	88	44	301	379	67	141	104
42 ME YANKEE	0	6	36	63	45	18	82
43 MCGUIRE 1 + 2	64	137	505	193	113	111	73
44 MIDLAND 2	535	87	289	85	109	185	97
45 MILLSTONE 1 + 2	582	284	167	102	410	624	204
46 MONTICELLO	67	38	45	155	340	35	26

TABLE D.1-1 (cont'd)

SITE	0-5	5-10	10-20	20-30	30-50	50-100	100-200
47 NINE M. PT. 1 + 2	29	150	50	72	129	79	67
48 NORTH ANNA 1, 2, + 3	12	28	29	58	146	183	161
49 OCONEE 1, 2 + 3	42	176	68	163	72	77	94
50 OYSTER CREEK	76	131	146	176	565	875	148
51 PALISADE	70	106	92	58	158	423	148
52 PALO VERDE 1	6	7	8	7	122	18	8
53 PEACH BOTTOM 2 + 3	44	96	246	362	659	428	63
54 PEBBLE SPRINGS	5	2	0	2	15	15	48
55 PERKINS	79	109	203	251	172	96	78
56 PERRY 1	224	230	178	296	374	135	170
57 PHIPPS BEND	82	57	128	98	78	78	92
58 PILGRIM 1	119	85	132	407	699	110	194
59 POINT BEACH 1 + 2	30	80	63	88	70	90	139
60 PRAIRIE 1 + 2	60	67	51	114	358	46	34
61 QUAD CITIES 1 + 2	18	64	313	77	47	85	150
62 RANCHO SECO	22	29	133	492	93	210	16
63 RIVERBEND 1	49	74	86	176	43	92	34
64 H. B. ROBINSON 2	97	75	50	75	77	98	68
65 SAINT LUCIE 1	71	160	34	29	41	58	38
66 SALEM 1 + 2	45	102	334	348	778	410	249
67 SAN ONOFRE	18	103	183	134	632	314	11
68 SEABROOK 1	120	88	89	64	272	129	16
69 SEQUOYAH 1 + 2	108	115	303	71	51	82	89
70 SHEARON HARRIS	23	69	168	205	109	97	74
71 SHOREHAM	135	146	347	847	699	714	173
72 SKAGIT	49	52	34	66	43	74	9
73 SOUTH TEXAS	0	10	25	11	26	94	31
74 VIRGIL C. SUMMER	1	43	47	194	67	110	84
75 SURRY ST 1 + 2	26	253	185	194	212	40	111
76 SUSQUEHANNA 1	188	130	330	178	172	378	354
77 THREE MILE ISLAND	320	470	499	248	168	506	281
78 TROJAN	104	197	50	52	190	48	26
79 TURKEY POINT 1 + 2	0	164	179	437	152	26	8
80 VERMONT YANKEE 1	102	79	99	68	217	363	236
81 VOSTLE	0	8	26	162	35	58	79
82 WATERFORD 3	181	119	282	490	91	40	27
83 WATTS BAR 1 + 2	22	31	61	68	101	61	103
84 WPPSS1+4	0	6	69	22	16	14	43
85 WPPSS 3 + 5	28	24	46	53	49	86	20
86 WPPSS 2	0	6	61	27	16	14	43
87 WOLF CREEK	34	4	9	32	21	97	35
88 YANKEE ROWE	12	88	84	129	255	311	261
89 YELLOW CREEK	15	32	42	35	49	65	65
90 ZIMMER 1	53	87	203	622	126	156	105
91 ZION	538	697	347	484	1130	196	83

TABLE D.1-2

CUMMULATIVE POPULATION DENSITIES (PEOPLE PER SQ. MI.) FOR 91
REACTOR SITES, CIRCLE RADII ARE GIVEN IN MILES

SITE	0-5	0-10	0-20	0-30	0-50	0-100	0-200
1 ALLENS CREEK	31	23	28	35	196	85	48
2 ARKANSAS 1 + 2	58	77	39	26	19	37	44
3 BAILLY S	271	280	471	778	860	324	182
4 BEAVER VALLEY 1 + 2	160	464	373	603	475	277	174
5 BELLEFONTE 1	21	72	41	41	109	92	80
6 BIG ROCK POINT	54	24	26	16	16	12	32
7 BLACK FOX	29	15	114	181	88	51	39
8 BRAIDWOOD 1	127	72	77	128	494	317	163
9 BROWNS FERRY 1, 2, +	12	94	89	94	80	77	80
10 BRUNSWICK 1 + 2	31	26	53	38	22	36	45
11 BYRON 1	83	65	204	161	112	357	145
12 CALLAWAY	8	11	27	61	37	102	67
13 CALVERT CLIFF 1 + 2	34	48	53	52	310	229	182
14 CATAWBA 1	49	190	371	250	159	126	87
15 CHEROKEE	48	97	109	171	165	113	96
16 CLINTON	18	39	37	109	90	74	159
17 COMMANCHE PEAK	20	20	10	23	99	95	46
18 COOK DC 1 + 2	93	141	122	180	139	349	214
19 COOPER S	14	20	19	21	22	58	44
20 CRYSTAL RIVER	15	26	15	11	24	73	37
21 DAVIS-BE 1	31	49	79	246	225	318	198
22 DIABLO CANYON 1 + 2	0	22	57	43	27	17	117
23 DRESDEN 2 + 3	68	105	176	222	821	322	162
24 DUANE ARNOLD	50	272	100	65	58	58	85
25 FARLEY 1 + 2	22	27	60	42	41	46	53
26 FERMI 2	126	226	346	851	666	312	172
27 FITZPATRICK	29	119	67	70	107	86	72
28 FORKED RIVER 1	76	117	139	160	419	761	301
29 FORT CALF UN	101	44	245	210	91	48	43
30 FORT ST PAIN	9	29	114	155	179	56	19
31 R. E. GINNA	77	112	486	295	149	123	70
32 GRAND GULF 1	16	25	20	31	37	46	54
33 HADDEM NECK	113	187	401	624	420	722	299
34 HARTSVILLE	44	39	55	50	113	62	78
35 HATCH, E.I. 1 + 2	13	18	33	31	32	39	58
36 INDIAN PT 2 + 3	752	651	711	1453	2099	752	335
37 KEWAUNEE	21	30	68	85	73	81	124
38 LASALLE 1 + 2	12	42	78	76	117	322	169
39 LA CROSSE	13	20	71	51	41	51	92
40 LIMERICK 1	792	483	622	1319	871	746	313
41 MARBLE HILL	88	55	240	317	157	145	115
42 ME YANKEE	0	4	28	47	46	25	68
43 MCGUIRE 1 + 2	64	119	408	289	176	128	87
44 MIDLAND 2	535	199	266	166	129	171	116
45 MILLSTONE 1 + 2	582	359	215	152	317	547	290
46 MONTICELLO	67	45	45	106	256	90	42

TABLE D.1-2 (cont'd)

SITE	0-5	0-10	0-20	0-30	0-50	0-100	0-200
47 NINE M. PT. 1 + 2	29	119	67	70	107	86	72
48 NORTH ANNA 1, 2, + 3	12	24	28	44	109	165	162
49 OCONEE 1, 2 + 3	42	142	87	129	93	81	91
50 OYSTER CREEK	76	117	139	160	419	761	301
51 PALISADE	70	97	93	74	128	349	198
52 PALO VERDE 1	6	7	8	7	81	34	14
53 PEACH BOTTOM 2 + 3	44	83	205	292	527	452	311
54 PEBBLE SPRINGS	5	3	1	2	10	14	40
55 PERKINS	79	102	178	219	189	119	88
56 PERRY 1	224	228	190	249	329	183	173
57 PHIPPS BEND	82	63	112	104	87	80	89
58 PILGRIM 1	119	94	122	280	548	220	201
59 POINT BEACH 1 + 2	30	67	64	77	73	85	126
60 PRAIRIE 1 + 2	60	65	55	88	261	100	51
61 QUAD CITIES 1 + 2	18	53	248	153	85	85	134
62 RANCHO SECO	22	27	107	321	175	201	63
63 RIVERBEND 1	49	68	81	134	76	88	47
64 H. B. ROBINSON 2	97	80	58	67	73	92	74
65 SAINT LUCIE 1	71	138	60	43	42	54	42
66 SALEM 1 + 2	45	88	272	314	611	460	302
67 SAN ONOFRE	18	82	158	144	456	350	96
68 SEABROOK 1	120	96	91	76	202	147	49
69 SEQUOYAH 1 + 2	108	113	255	153	88	83	87
70 SHEARON HARRIS	23	58	141	176	133	106	82
71 SHOREHAM	135	144	296	602	664	702	305
72 SKAGIT	49	51	38	54	47	67	23
73 SOUTH TEXAS	0	7	21	15	22	76	42
74 VIRGIL C. SUMMER	1	33	43	127	89	105	89
75 SURRY ST 1 + 2	26	196	188	191	204	81	104
76 SUSQUEHANNA 1	188	144	284	225	191	331	348
77 THREE MILE ISLAND	320	433	483	352	234	438	321
78 TROJAN	104	174	81	65	145	72	37
79 TURKEY POINT 1 + 2	0	123	165	316	211	72	24
80 VERMONT YANKEE 1	102	84	95	80	168	314	255
81 VOGTLE	0	6	21	99	58	58	73
82 WATERFORD 3	181	135	245	381	195	79	40
83 WATTS BAR 1 + 2	22	29	53	61	87	68	94
84 WPPSS1+4	0	4	53	36	23	16	36
85 WPPSS 3 + 5	28	25	41	48	48	77	34
86 WPPSS 2	0	4	47	36	23	16	36
87 WOLF CREEK	34	11	10	22	21	78	46
88 YANKEE ROWE	12	69	81	107	202	283	267
89 YELLOW CREEK	15	28	39	37	44	60	64
90 ZIMMER 1	53	78	172	422	232	175	122
91 ZION	538	657	424	457	888	369	154

TABLE D.1-3

POPULATION DENSITIES (PEOPLE PER SQ. MI.) IN
MOST POPULATED 22.5° SECTOR OF EACH ANNULUS

SITE	0-5MI	5-10MI	10-20MI	20-30MI
1 ALLENS CREEK	209.4	182.3	130.8	153.1
2 ARKANSAS 1 + 2	364.2	676.5	112.0	69.4
3 BAILLY S	1123.1	1650.5	4113.3	9294.1
4 BEAVER VALLEY 1 + 2	1073.8	2108.9	1003.9	6199.0
5 BELLEFONTE 1	199.6	420.6	89.1	79.7
6 BIG ROCK POINT	716.9	48.9	160.5	28.7
7 BLACK FOX	267.3	81.0	1148.5	2232.1
8 BRAIDWOOD 1	619.3	283.1	409.3	1462.9
9 BROWNS FERRY 1, 2, + 3	189.1	814.7	502.6	730.4
10 BRUNSWICK 1 + 2	452.3	112.9	809.6	254.8
11 BYRON 1	356.3	173.8	2191.8	355.3
12 CALLAWAY	129.8	57.3	161.3	557.6
13 CALVERT CLIFF 1 + 2	293.4	240.3	220.0	171.7
14 CATAWBA 1	263.0	1613.2	2719.9	607.2
15 CHEROKEE	276.9	981.9	448.0	807.3
16 CLINTON	107.8	287.3	83.1	1001.1
17 COMMANCHE PEAK	316.6	88.5	29.2	183.6
18 COOK DC 1 + 2	335.3	1053.0	474.3	1930.4
19 COOPER S	54.2	108.6	63.1	83.7
20 CRYSTAL RIVER	235.3	164.5	51.7	52.6
21 DAVIS-BE 1	337.6	313.3	417.2	2358.0
22 DIABLO CANYON 1 + 2	0.0	175.2	566.8	295.7
23 DRESDEN 2 + 3	332.7	359.6	2023.6	1093.6
24 DUANE ARNOLD	269.1	2488.4	102.4	86.2
25 FARLEY 1 + 2	160.7	134.5	619.9	46.1
26 FERMI 2	586.9	1364.6	2637.4	6556.7
27 FITZPATRICK	468.3	1758.1	310.2	599.6
28 FORKED RIVER 1	458.6	858.5	847.5	1029.9
29 FORT CALHOUN	976.8	239.0	3212.8	1593.9
30 FORT ST VRAIN	139.1	120.7	574.2	965.4
31 R. E. GINNA	692.2	515.3	5883.2	700.6
32 GRAND GULF 1	207.8	168.7	60.7	301.1
33 HADDEM NECK	789.6	881.2	1725.3	2730.1
34 HARTSVILLE	456.9	79.6	274.1	160.2
35 HATCH, E.I. 1 + 2	210.4	112.9	136.1	61.5
36 INDIAN PT 2 + 3	2513.7	1916.9	2363.0	14617.9
37 KEWAUNEE	225.1	197.0	814.8	1292.6
38 LASALLE 1 + 2	122.2	192.5	383.3	337.7
39 LA CROSSE	148.3	68.0	891.6	160.7
40 LIMERICK 1	4232.5	1340.1	2167.5	12296.5
41 MARBLE HILL	649.0	166.2	2318.0	3443.4
42 ME YANKEE	0.0	50.9	218.8	683.2
43 MCGUIRE 1 + 2	388.5	425.8	3096.1	433.5
44 MIDLAND 2	2006.6	276.6	2221.0	304.1
45 MILLSTONE 1 + 2	3739.0	1369.8	865.4	251.1
46 MONTICELLO	456.3	190.9	98.2	621.0

TABLE D.1-3 (cont'd)

SITE	0-5MI	5-10MI	10-20MI	20-30MI
47 NINE M. PT. 1 + 2	468.3	1758.1	310.2	599.6
48 NORTH ANNA 1, 2, + 3	187.2	98.5	57.2	294.6
49 OCONEE 1, 2 + 3	215.1	821.7	277.7	920.6
50 OYSTER CREEK	458.6	858.5	847.5	1029.9
51 PALISADE	415.8	460.0	944.2	220.5
52 PALO VERDE 1	69.7	53.2	75.4	88.1
53 PEACH BOTTOM 2 + 3	290.1	255.2	1292.9	1092.9
54 PEBBLE SPRINGS	76.4	21.2	5.3	8.6
55 PERKINS	458.8	314.9	675.8	810.2
56 PERRY 1	811.4	1561.6	899.0	3837.3
57 PHIPPS BEND	265.9	287.9	915.8	557.4
58 PILGRIM 1	886.6	611.8	413.4	1773.1
59 POINT BEACH 1 + 2	355.1	876.7	617.3	625.4
60 PRAIRIE 1 + 2	280.3	596.8	219.0	866.5
61 QUAD CITIES 1 + 2	109.8	240.1	1937.6	383.8
62 RANCHO SECO	348.6	101.5	573.9	3087.3
63 RIVERBEND 1	295.8	298.9	440.0	1673.5
64 H. B. ROBINSON 2	525.0	523.0	198.9	262.9
65 SAINT LUCIE 1	947.7	1350.3	221.0	303.3
66 SALEM 1 + 2	626.6	601.1	2014.0	1568.1
67 SAN ONOFRE	280.9	887.1	1061.9	1252.7
68 SEABROOK 1	540.7	469.8	548.7	453.3
69 SEQUOYAH 1 + 2	294.2	372.0	1900.2	274.7
70 SHEARON HARRIS	190.5	242.8	721.1	1106.3
71 SHOREHAM	805.7	816.3	1589.7	3219.4
72 SKAGIT	288.3	525.8	207.1	502.3
73 SOUTH TEXAS	0.0	61.4	265.7	53.3
74 VIRGIL C. SUMMER	17.7	99.8	206.9	1956.7
75 SURRY ST 1 + 2	244.5	1751.9	1320.4	1521.0
76 SUSQUEHANNA 1	1309.7	561.9	2560.7	869.8
77 THREE MILE ISLAND	2157.0	2319.5	1622.8	1158.4
78 TROJAN	365.9	2151.1	176.8	582.6
79 TURKEY POINT 1 + 2	0.0	1689.1	2107.5	4119.7
80 VERMONT YANKEE 1	507.7	532.1	361.2	350.6
81 VOGTLE	0.0	74.4	76.9	991.7
82 WATERFORD 3	880.3	452.7	3399.3	5068.1
83 WATTS BAR 1 + 2	203.1	98.3	248.0	163.3
84 WPPSS1+4	0.0	95.1	581.8	158.1
85 WPPSS 3 + 5	453.7	193.3	540.7	225.5
86 WPPSS 2	0.0	95.1	538.3	197.7
87 WOLF CREEK	427.6	21.5	16.8	225.3
88 YANKEE ROWE	95.5	705.1	286.1	670.6
89 YELLOW CREEK	132.2	101.6	262.6	102.3
90 ZIMMER 1	325.9	180.0	949.5	5331.2
91 ZION	2040.9	4367.4	1665.5	3344.7

TABLE D.1-4

POPULATION DENSITIES (PEOPLE PER SQ. MI.) IN
MOST POPULATED 22.5° SECTOR OF EACH CIRCLE

SITE	0-5MI	0-10MI	0-20MI	0-30MI
1 ALLENS CREEK	209.4	136.7	98.1	128.6
2 ARKANSAS 1 + 2	364.2	598.4	194.6	125.1
3 BAILLY S	1123.1	1355.6	3423.9	5163.4
4 BEAVER VALLEY 1 + 2	1073.8	1594.2	903.2	3845.3
5 BELLEFONTE 1	199.6	335.6	107.7	80.5
6 BIG ROCK POINT	716.9	215.9	132.2	66.2
7 BLACK FOX	267.3	66.8	861.4	1622.9
8 BRAIDWOOD 1	619.3	218.8	316.7	878.7
9 BROWNS FERRY 1, 2, + 3	189.1	611.1	529.7	427.3
10 BRUNSWICK 1 + 2	452.3	113.1	607.2	411.4
11 BYRON 1	356.3	162.6	1656.5	889.0
12 CALLAWAY	129.8	43.0	129.7	341.3
13 CALVERT CLIFF 1 + 2	293.4	229.0	210.1	109.3
14 CATAWBA 1	263.0	1209.9	2075.7	1259.9
15 CHEROKEE	276.9	736.4	361.2	501.1
16 CLINTON	107.8	215.5	72.2	572.2
17 COMMANCHE PEAK	316.6	79.1	38.5	102.0
18 COOK DC 1 + 2	335.3	867.9	572.7	1141.4
19 COOPER S	54.2	90.3	63.3	56.5
20 CRYSTAL RIVER	235.3	123.4	53.5	41.4
21 DAVIS-BE 1	337.6	238.7	327.8	1367.2
22 DIABLO CANYON 1 + 2	0.0	131.4	441.6	201.4
23 DRESDEN 2 + 3	332.7	269.7	1538.2	876.8
24 DUANE ARNOLD	269.1	1922.2	505.8	241.8
25 FARLEY 1 + 2	160.7	100.8	475.8	231.4
26 FERMI 2	586.9	1073.2	2069.3	4507.6
27 FITZPATRICK	468.3	1318.6	362.0	365.6
28 FORKED RIVER 1	458.6	758.5	825.3	939.0
29 FORT CALHOUN	976.8	244.2	2417.8	1960.0
30 FORT ST VRAIN	139.1	90.6	430.7	553.9
31 R. E. GINNA	692.2	386.5	4507.8	2392.7
32 GRAND GULF 1	207.8	178.5	51.8	183.1
33 HADDEM NECK	789.6	660.9	1439.7	2009.7
34 HARTSVILLE	456.9	114.2	205.6	155.2
35 HATCH, E.I. 1 + 2	210.4	84.7	102.1	61.2
36 INDIAN PT 2 + 3	2513.7	1627.5	2161.0	8684.2
37 KEWAUNEE	225.1	147.7	618.5	735.8
38 LASALLE 1 + 2	122.2	144.4	301.9	228.0
39 LA CROSSE	148.3	53.7	682.1	392.5
40 LIMERICK 1	4232.5	1343.5	1758.1	7511.8
41 MARBLE HILL	649.0	184.6	1753.1	2692.1
42 ME YANKEE	0.0	38.1	173.6	404.3
43 MCGUIRE 1 + 2	388.5	319.4	2386.1	1301.3
44 MIDLAND 2	2006.6	549.1	1718.5	911.8
45 MILLSTONE 1 + 2	3739.0	1962.1	877.7	485.5
46 MONTICELLO	456.3	143.2	86.2	368.5

TABLE D.1-4 (cont'd)

SITE	0-5MI	0-10MI	0-20MI	0-30MI
47 NINE M. PT. 1 + 2	468.3	1318.6	362.0	365.6
48 NORTH ANNA 1, 2, + 3	187.2	73.9	47.0	178.5
49 OCONEE 1, 2 + 3	215.1	629.3	235.0	611.8
50 OYSTER CREEK	458.6	758.5	825.3	939.0
51 PALISADE	415.8	448.9	741.4	452.0
52 PALO VERDE 1	69.7	57.3	56.5	74.1
53 PEACH BOTTOM 2 + 3	290.1	191.4	969.7	841.6
54 PEBBLE SPRINGS	76.4	19.1	6.4	5.2
55 PERKINS	458.8	291.7	529.3	651.1
56 PERRY 1	811.4	1276.5	993.4	2573.3
57 PHIPPS BEND	265.9	215.9	688.3	374.3
58 PILGRIM 1	886.6	584.3	456.1	1155.4
59 POINT BEACH 1 + 2	355.1	657.6	627.4	362.0
60 PRAIRIE 1 + 2	280.3	496.1	171.2	557.5
61 QUAD CITIES 1 + 2	109.8	180.1	1456.3	860.5
62 RANCHO SECO	348.6	146.1	430.4	1814.3
63 RIVERBEND 1	295.8	231.9	335.1	1078.7
64 H. B. ROBINSON 2	525.0	523.5	280.0	270.5
65 SAINT LUCIE 1	947.7	1012.7	419.0	230.7
66 SALEM 1 + 2	626.6	450.8	1511.5	1543.0
67 SAN ONOFRE	280.9	735.6	796.4	951.5
68 SEABROOK 1	540.7	352.3	475.5	344.2
69 SEQUOYAH 1 + 2	294.2	283.0	1456.0	799.7
70 SHEARON HARRIS	190.5	182.1	580.4	647.5
71 SHOREHAM	805.7	813.7	1289.1	2361.5
72 SKAGIT	288.3	451.5	201.2	301.2
73 SOUTH TEXAS	0.0	46.0	199.3	98.3
74 VIRGIL C. SUMMER	17.7	74.9	173.9	1091.1
75 SURRY ST 1 + 2	244.5	1313.9	1318.8	1164.1
76 SUSQUEHANNA 1	1309.7	748.9	1979.1	1362.8
77 THREE MILE ISLAND	2157.0	1758.2	1656.6	824.4
78 TROJAN	365.9	1618.7	480.5	382.6
79 TURKEY POINT 1 + 2	0.0	966.8	1628.8	2316.4
80 VERMONT YANKEE 1	507.7	526.0	270.9	261.4
81 VOGTLE	0.0	55.8	57.7	559.2
82 WATERFORD 3	880.3	426.9	2618.1	3979.2
83 WATTS BAR 1 + 2	203.1	124.5	186.0	127.9
84 WPPSS1+4	0.0	71.4	436.3	281.7
85 WPPSS 3 + 5	453.7	145.0	405.5	196.8
86 WPPSS 2	0.0	71.4	403.7	289.3
87 WOLF CREEK	427.6	123.0	39.7	129.5
88 YANKEE ROWE	95.5	528.8	223.7	464.0
89 YELLOW CREEK	132.2	76.2	213.0	107.0
90 ZIMMER 1	325.9	162.0	747.0	3264.5
91 ZION	2040.9	3779.5	1724.0	2349.3

D.2 Exclusion Distances

Table D.2-1 presents the distance to the closest boundary of the exclusion zone surrounding each of the 91 reactor sites, discussed in Chapter 2 and Appendix A. The variability of these distances is displayed in Figure 3-2 in Chapter 3.

TABLE D.2-1

EXCLUSION DISTANCES (MILES) FOR 91 REACTOR SITES

SITE	EX. DIST.
*****	*****
1 ALLENS CREEK	0.82
2 ARKANSAS 1 + 2	0.65
3 BAILLY S	0.12
4 BEAVER VALLEY 1 + 2	0.38
5 BELLEFONTE 1	0.57
6 BIG ROCK POINT	0.51
7 BLACK FOX	0.53
8 BRAIDWOOD 1	0.28
9 BROWNS FERRY 1, 2, + 3	0.76
10 BRUNSWICK 1 + 2	0.57
11 BYRON 1	0.29
12 CALLAWAY	0.68
13 CALVERT CLIFF 1 + 2	0.71
14 CATAWBA 1	0.47
15 CHEROKEE	0.37
16 CLINTON	0.61
17 COMMANCHE PEAK	0.87
18 COOK DC 1 + 2	0.38
19 COOPER S	0.46
20 CRYSTAL RIVER	0.83
21 DAVIS-BE 1	0.39
22 DIABLO CANYON 1 + 2	0.50
23 DRESDEN 2 + 3	0.42
24 DUANE ARNOLD	0.27
25 FARLEY 1 + 2	0.78
26 FERMI 2	0.57
27 FITZPATRICK	0.61
28 FORKED RIVER 1	0.38
29 FORT CALHOUN	0.23
30 FORT ST VRAIN	0.37
31 R. E. GINNA	0.28
32 GRAND GULF 1	0.47
33 HADDEM NECK	0.33
34 HARTSVILLE	0.76
35 HATCH, E.I. 1 + 2	0.78
36 INDIAN PT 2 + 3	0.21
37 KEWAUNEE	0.75
38 LASALLE 1 + 2	0.32
39 LA CROSSE	0.21
40 LIMERICK 1	0.47
41 MARBLE HILL	0.42
42 ME YANKEE	0.38
43 MCGUIRE 1 + 2	0.47
44 MIDLAND 2	0.31
45 MILLSTONE 1 + 2	0.31

TABLE D.2-1 (cont'd)

SITE	EX. DIST.
46 MONTICELLO	0.30
47 NINE M. PT. 1 + 2	0.97
48 NORTH ANNA 1, 2, + 3	0.84
49 OCONEE 1, 2 + 3	1.00
50 OYSTER CREEK	0.25
51 PALISADE	0.42
52 PALO VERDE 1	0.56
53 PEACH BOTTOM 2 + 3	0.51
54 PEBBLE SPRINGS	0.49
55 PERKINS	0.37
56 PERRY 1	0.57
57 PHIPPS BEND	0.47
58 PILGRIM 1	0.27
59 POINT BEACH 1 + 2	0.75
60 PRAIRIE 1 + 2	0.44
61 QUAD CITIES 1 + 2	0.24
62 RANCHO SECO	0.40
63 RIVERBEND 1	0.57
64 H. B. ROBINSON 2	0.26
65 SAINT LUCIE 1	0.97
66 SALEM 1 + 2	0.72
67 SAN ONOFRE	0.50
68 SEABROOK 1	0.57
69 SEQUOYAH 1 + 2	0.36
70 SHEARON HARRIS	1.33
71 SHOREHAM	0.19
72 SKAGIT	0.38
73 SOUTH TEXAS	0.89
74 VIRGIL C. SUMMER	1.01
75 SURRY ST 1 + 2	0.35
76 SUSQUEHANNA 1	0.35
77 THREE MILE ISLAND	0.38
78 TROJAN	0.41
79 TURKEY POINT 1 + 2	0.79
80 VERMONT YANKEE 1	0.17
81 VOGTLE	0.68
82 WATERFORD 3	0.57
83 WATTS BAR 1 + 2	0.75
84 WPPSS1+4	1.21
85 WPPSS 3 + 5	0.81
86 WPPSS 2	1.21
87 WOLF CREEK	0.75
88 YANKEE ROWE	0.59
89 YELLOW CREEK	0.43
90 ZIMMER 1	0.24
91 ZION	0.57

D.3 Site Population Factors

Table D.3-1 presents the Site Population Factor (SPF_n) and the Wind Rose Weighted Site Population Factor ($WRSPF_n$) for each of the 91 reactor sites discussed in Chapter 2 and Appendix A. For every site, the factors have been calculated for each of the following four distances: 5, 10, 20, and 30 miles. The equations used in these calculations are presented in Section 3.2 of Chapter 3.

Table D.3-1. SITE POPULATION FACTORS (SPF) AND WIND ROSE WEIGHTED SITE POPULATION FACTORS (WRWSPF) FOR 91 REACTOR SITES

SITE NAME	REGION	SPF5	SPF10	SPF20	SPF30	WRSPF5	WRSPF10	WRSPF20	WRSPF30
ALLENS CREEK	SW	.31084E-01	.26170E-01	.27085E-01	.29669E-01	.29167E-01	.28190E-01	.29807E-01	.33529E-01
ARKANSAS 1 + 2	S	.34737E-01	.60184E-01	.48306E-01	.41624E-01	.56405E-01	.60023E-01	.48555E-01	.42315E-01
BAILLY S	MM	.17129E+00	.21447E+00	.33316E+00	.46225E+00	.15890E+00	.24294E+00	.40154E+00	.51750E+00
BEAVER VALLEY 1 + 2	NE	.90963E-01	.25042E+00	.24870E+00	.38618E+00	.76206E-01	.22261E+00	.24205E+00	.34474E+00
BELLEFONTA 1	S	.60386E-01	.72908E-01	.58133E-01	.54642E-01	.68453E-01	.84200E-01	.65040E-01	.59119E-01
BIG ROCK POINT	MM	.32287E-01	.25840E-01	.27861E-01	.23975E-01	.33586E-01	.27221E-01	.27626E-01	.23475E-01
BLACK FOX	SW	.17274E-01	.14603E-01	.55139E-01	.93730E-01	.14052E-01	.13323E-01	.41818E-01	.73356E-01
BRAIDWOOD 1	MM	.13580E+00	.10993E+00	.96933E-01	.11376E+00	.12694E+00	.10149E+00	.88696E-01	.99581E-01
BROWNS FERRY 1, 2, +	S	.79286E-02	.44405E-01	.64589E-01	.70623E-01	.83789E-02	.52503E-01	.78023E-01	.77970E-01
BRUNSWICK 1 + 2	S	.20188E-01	.22260E-01	.32303E-01	.31477E-01	.17567E-01	.22345E-01	.32963E-01	.31882E-01
BYRON 1	MM	.71963E-01	.67722E-01	.11826E+00	.12009E+00	.78011E-01	.73461E-01	.10725E+00	.11010E+00
CALLAWAY	MM	.90153E-02	.10237E-01	.19330E-01	.32205E-01	.51928E-02	.83736E-02	.17588E-01	.28591E-01
CALVERT CLIFF 1 + 2	NE	.19608E-01	.30431E-01	.40544E-01	.42677E-01	.25289E-01	.41027E-01	.55162E-01	.53537E-01
CATAWBA 1	S	.28386E-01	.97801E-01	.20199E+00	.19320E+00	.15367E-01	.58678E-01	.24996E+00	.24078E+00
CHEROKEE	S	.32364E-01	.60843E-01	.74998E-01	.10486E+00	.38406E-01	.82775E-01	.90473E-01	.11931E+00
CLINTON	MM	.19499E-01	.31270E-01	.33278E-01	.62732E-01	.15294E-01	.23542E-01	.29824E-01	.65338E-01
COMMANCHE PEAK	SW	.84912E-02	.12700E-01	.10855E-01	.15435E-01	.20515E-01	.20185E-01	.15354E-01	.17798E-01
COOK DC 1 + 2	MM	.84697E-01	.11303E+00	.11942E+00	.14056E+00	.88946E-01	.10599E+00	.10839E+00	.13656E+00
COOPER S	MM	.10078E-01	.14811E-01	.16822E-01	.17901E-01	.10219E-01	.14122E-01	.15045E-01	.17808E-01
CRYSTAL RIVER	S	.16346E-01	.22168E-01	.18219E-01	.16187E-01	.29057E-01	.30043E-01	.24442E-01	.21577E-01
DAVIS-BE 1	MM	.32672E-01	.40451E-01	.55738E-01	.12140E+00	.56239E-01	.59827E-01	.70913E-01	.12767E+00
DIABLO CANYON 1 + 2	N	.0	.98598E-02	.35215E-01	.34517E-01	.0	.57107E-02	.14153E-01	.18607E-01
DRESDEN 2 + 3	MM	.44720E-01	.67169E-01	.11713E+00	.14378E+00	.42523E-01	.70489E-01	.94596E-01	.11579E+00
DUANE ARNOLD	MM	.39515E-01	.12939E+00	.12819E+00	.10952E+00	.31349E-01	.13590E+00	.13519E+00	.11556E+00
FARLEY 1 + 2	S	.11499E-01	.17446E-01	.33556E-01	.32332E-01	.88854E-02	.15052E-01	.28956E-01	.29465E-01
FERMI 2	MM	.15421E+00	.19137E+00	.24531E+00	.44021E+00	.12502E+00	.17859E+00	.18463E+00	.31792E+00
FITZPATRICK	NE	.19642E-01	.68462E-01	.62453E-01	.63600E-01	.18665E-01	.98174E-01	.83399E-01	.82134E-01
FORKED RIVER 1	NE	.80588E-01	.94443E-01	.11249E+00	.12548E+00	.59297E-01	.72795E-01	.88249E-01	.10273E+00
FORT CALHOUN	MM	.73958E-01	.55546E-01	.12552E+00	.14071E+00	.10434E+00	.73081E-01	.20558E+00	.23105E+00
FORT ST VRAIN	W	.73534E-02	.20285E-01	.63295E-01	.86448E-01	.57651E-02	.21997E-01	.60302E-01	.97050E-01
GINNA R.E.	NE	.47184E-01	.72451E-01	.23521E+00	.21771E+00	.46365E-01	.81548E-01	.33809E+00	.31177E+00
GRAND GULF 1	S	.12290E-01	.19601E-01	.19342E-01	.23405E-01	.13523E-01	.22849E-01	.21192E-01	.24940E-01
HADDEN NECK	NE	.12231E+00	.14928E+00	.24484E+00	.36523E+00	.95413E-01	.19216E+00	.39105E+00	.52525E+00
HARTSVILLE	S	.21557E-01	.26881E-01	.37927E-01	.39203E-01	.20832E-01	.26524E-01	.36980E-01	.37850E-01
HATCH, E.I. 1 + 2	S	.11122E-01	.14720E-01	.22731E-01	.23489E-01	.12330E-01	.13566E-01	.21401E-01	.22887E-01
INDIAN PT 2 + 3	NE	.81326E+00	.74045E+00	.73557E+00	.98620E+00	.11763E+01	.95346E+00	.87477E+00	.11167E+01
KEWAUNEE	MM	.93780E-02	.17390E-01	.36593E-01	.47946E-01	.16358E-01	.23622E-01	.49717E-01	.72662E-01
LASALLE 1 + 2	MM	.13544E-01	.29233E-01	.55404E-01	.59426E-01	.90269E-02	.24474E-01	.60214E-01	.64080E-01
LA CROSSE	MM	.17126E-01	.19149E-01	.39487E-01	.38589E-01	.18270E-01	.20467E-01	.50259E-01	.48158E-01
LIMERICK 1	NE	.69580E+00	.58125E+00	.59208E+00	.83770E+00	.82582E+00	.65562E+00	.64060E+00	.77740E+00
MARBLE HILL	MM	.52590E-01	.48820E-01	.12305E+00	.18073E+00	.42417E-01	.45750E-01	.14729E+00	.21629E+00
ME YANKEE	NE	.0	.17540E-02	.14157E-01	.23032E-01	.0	.11468E-02	.11221E-01	.19443E-01
MCGUIRE 1 + 2	S	.68527E-01	.89179E-01	.22294E+00	.21853E+00	.55320E-01	.86377E-01	.20439E+00	.20009E+00
MIDLAND 2	MM	.51550E+00	.36272E+00	.32814E+00	.27855E+00	.47273E+00	.33162E+00	.27610E+00	.20001E+00
MILLSTONE 1 + 2	NE	.44527E+00	.39795E+00	.31930E+00	.27479E+00	.38361E+00	.33459E+00	.27492E+00	.24015E+00
MONTICELLO	MM	.36455E-01	.36888E-01	.40108E-01	.63248E-01	.35786E-01	.34907E-01	.38813E-01	.66259E-01
NINE M. F. 1 + 2	NE	.19642E-01	.68462E-01	.62453E-01	.63600E-01	.18665E-01	.98174E-01	.83399E-01	.82134E-01
NORTH ANNA 1, 2, + 3	S	.74517E-02	.15242E-01	.29497E-01	.28285E-01	.17726E-01	.22356E-01	.24040E-01	.29313E-01
OCONEE 1, 2 + 3	S	.20946E-01	.71083E-01	.71072E-01	.87747E-01	.20376E-01	.54069E-01	.56339E-01	.70761E-01

Table D.3-1. (continued)

SITE NAME	REGION	SPF5	SPF10	SPF20	SPF30	MRSPF5	MRSPF10	MRSPF20	MRSPF30
OYSTER CREEK	NE	.80588E-01	.94443E-01	.11249E+00	.12548E+00	.59297E-01	.72795E-01	.83249E-01	.10273E+00
PALISADE	W	.54980E-01	.74781E-01	.78747E-01	.74770E-01	.64503E-01	.90103E-01	.10466E+00	.10047E+00
PALO VERDE 1	SW	.59341E-02	.57060E-02	.64846E-02	.63884E-02	.72781E-02	.65626E-02	.68223E-02	.67669E-02
PEACH BOTTOM 2 + 3	NE	.21262E-01	.46280E-01	.10392E+00	.15471E+00	.16166E-01	.43229E-01	.10408E+00	.16286E+00
PEBBLE SPRINGS	W	.32039E-02	.26601E-02	.18549E-02	.19379E-02	.10765E-02	.18643E-02	.12494E-02	.16177E-02
PERKINS	S	.56885E-01	.73595E-01	.11950E+00	.14722E+00	.69392E-01	.77501E-01	.12927E+00	.16576E+00
PERRY 1	W	.18134E+00	.19633E+00	.14713E+00	.20736E+00	.19364E+00	.22503E+00	.21854E+00	.25700E+00
PHIPPS BEND	S	.10524E+00	.84886E-01	.97704E-01	.97859E-01	.14545E+00	.11126E+00	.97714E-01	.90997E-01
PILGRIM 1	NE	.11534E+00	.10936E+00	.11597E+00	.17272E+00	.10559E+00	.10456E+00	.12056E+00	.18316E+00
POINT BEACH 1 + 2	W	.27877E-01	.42796E-01	.50634E-01	.56737E-01	.30607E-01	.61374E-01	.78181E-01	.84759E-01
PRAIRIE 1 + 2	W	.52533E-01	.60849E-01	.58239E-01	.68463E-01	.68078E-01	.89779E-01	.81843E-01	.98066E-01
QUAD CITIES 1 + 2	W	.92684E-02	.28898E-01	.11576E+00	.10374E+00	.74518E-02	.26202E-01	.15572E+00	.14606E+00
RANCHO SECO	W	.11965E-01	.16493E-01	.49437E-01	.14276E+00	.21786E-01	.24511E-01	.62468E-01	.18807E+00
RIVERBEND 1	S	.30502E-01	.43767E-01	.55354E-01	.81505E-01	.26084E-01	.38615E-01	.53917E-01	.83519E-01
H. B. ROBINSON 2	S	.44152E-01	.60749E-01	.56364E-01	.59736E-01	.31658E-01	.40944E-01	.40993E-01	.46573E-01
SAINT LUCIE 1	S	.54634E-01	.83901E-01	.69659E-01	.61506E-01	.26940E-01	.57388E-01	.50326E-01	.43984E-01
SALEM 1 + 2	NE	.20414E-01	.44992E-01	.12554E+00	.17034E+00	.10118E-01	.37371E-01	.13494E+00	.17374E+00
SAN ONOFRE	W	.69002E-02	.48712E-01	.83849E-01	.96513E-01	.66242E-02	.33136E-01	.69350E-01	.73546E-01
SEABROOK 1	NE	.67564E-01	.70954E-01	.75767E-01	.74098E-01	.51712E-01	.53509E-01	.61434E-01	.60380E-01
SEQUOYAH 1 + 2	S	.74540E-01	.92644E-01	.15439E+00	.14585E+00	.14089E+00	.99429E-01	.24659E+00	.22043E+00
SHEARON HARRIS	S	.19205E-01	.32954E-01	.71277E-01	.10028E+00	.18313E-01	.27659E-01	.62003E-01	.89401E-01
SKAGIT	W	.34859E-01	.43992E-01	.42008E-01	.47567E-01	.55447E-01	.72359E-01	.61431E-01	.61842E-01
SHOREHAM	NE	.16493E+00	.15862E+00	.22164E+00	.35388E+00	.14089E+00	.14828E+00	.23875E+00	.39069E+00
SOUTH TEXAS	SW	.0	.22669E-02	.11954E-01	.11540E-01	.0	.31599E-02	.11627E-01	.10927E-01
VIRGIL C. SUMNER	S	.50986E-03	.16901E-01	.26477E-01	.59106E-01	.55440E-03	.16344E-01	.27235E-01	.54535E-01
SURRY ST 1 + 2	S	.11499E-01	.10123E+00	.12692E+00	.14067E+00	.14834E-01	.98112E-01	.11710E+00	.12781E+00
SUSQUEHANNA 1	NE	.88449E-01	.10759E+00	.17999E+00	.17990E+00	.13817E+00	.14840E+00	.14670E+00	.18442E+00
THREE AILE ISLAND	NE	.22949E+00	.31201E+00	.39926E+00	.37154E+00	.19179E+00	.30919E+00	.42313E+00	.39465E+00
TRUJAN	W	.60039E-01	.10794E+00	.88903E-01	.80567E-01	.68927E-01	.18613E+00	.15456E+00	.14013E+00
TURKEY POINT 1 + 2	S	.0	.53684E-01	.94549E-01	.16790E+00	.0	.44722E-01	.72504E-01	.10295E+00
VERMONT YANKEE 1	NE	.95964E-01	.94227E-01	.95045E-01	.88440E-01	.10817E+00	.14159E+00	.11733E+00	.10598E+00
VOGTLÉ	S	.0	.36768E-02	.10877E-01	.39824E-01	.0	.34954E-02	.10971E-01	.2954E-01
WATERFORD 3	S	.16326E+00	.14943E+00	.14643E+00	.25577E+00	.14376E+00	.14389E+00	.15424E+00	.20717E+00
WATTS BAR 1 + 2	S	.15094E-01	.22252E-01	.34829E-01	.41281E-01	.10158E-01	.17324E-01	.24514E-01	.37325E-01
WPPSS1+4	W	.0	.33914E-02	.25418E-01	.24944E-01	.0	.14139E-02	.33159E-01	.31951E-01
WPPSS 2	W	.0	.26920E-02	.22569E-01	.23771E-01	.0	.11239E-02	.29395E-01	.30428E-01
WPPSS 3 + 5	W	.11904E-01	.18371E-01	.27064E-01	.31975E-01	.14094E-01	.15227E-01	.19507E-01	.25535E-01
WOLF CREEK	W	.16991E-01	.12359E-01	.11440E-01	.15201E-01	.85718E-02	.66541E-02	.80877E-02	.13311E-01
YANKEE ROWE	W	.12403E-01	.35226E-01	.51955E-01	.67440E-01	.15425E-01	.30277E-01	.44781E-01	.56389E-01
YELLOW CREEK	S	.65005E-02	.14117E-01	.22904E-01	.25371E-01	.66200E-02	.16426E-01	.25084E-01	.26547E-01
ZIEMER 1	W	.27940E-01	.46397E-01	.93655E-01	.20515E+00	.20134E-01	.37355E-01	.79703E-01	.17520E+00
ZION	W	.71363E+00	.70661E+00	.58157E+00	.55685E+00	.87478E+00	.84040E+00	.68575E+00	.65741E+00

Appendix E: CRAC 2: A Brief Description

The accident consequence calculations presented in Chapter 2 were performed using CRAC2 [1,2], an improved version of the WASH-1400 consequence model CRAC. A number of modifications were made in the upgrade from CRAC to CRAC2. These include changes in the treatments of atmospheric dispersion parameters, plume rise, precipitation scavenging (wet deposition), mixing heights, weather sequence sampling, emergency response (evacuation and sheltering), and latent cancer risk factors. These changes are briefly described below. In addition, several errors found in CRAC were corrected in the CRAC2 version.

E.1 Atmospheric Dispersion Parameters

The values of the horizontal dispersion coefficients, σ_y , obtained from the Pasquill-Gifford curves (and parameterized by Tadmor and Gur [3]) correspond to a release duration of three minutes. To correct the standard dispersion coefficients for releases of longer duration, the summary report of the National Commission on Air Quality's Atmospheric dispersion Modeling Panel [4] endorses the method suggested by Gifford [5]. An adjustment for releases of duration t_2 (minutes) is made by means of the formula

$$\frac{\sigma_{y2}}{\sigma_{yPG}} = \left(\frac{t_2}{3 \text{ min}} \right)^Q$$

where Q is within the range 0.25-0.3 for $1 \text{ hr} < t_2 < 100 \text{ hr}$ and equals ~ 0.2 for $3 \text{ min} < t_2 < 1 \text{ hr}$. In CRAC2, Q is equal to 0.2 for release durations between 3 minutes and one hour and 0.25 for release durations greater than one hour. The lower value of 0.25, rather than 0.3, was selected for long-duration releases because it results in higher concentrations.

The vertical dispersion coefficients, σ_z , obtained from the Pasquill-Gifford curves (parameterized by Martin and Tikvart [6]) are based on data from releases over

terrain with very low surface roughness (grasslands with roughness length of approximately 3 cm). In CRAC2 a more typical roughness length of 10 cm (crops, bushes) is assumed. The vertical dispersion coefficients are adjusted using the following recommended equation [7,8]:

$$\sigma_{z2}/\sigma_{z1} = (r_2/r_1)^{0.2} ,$$

where σ_{z1} is the unadjusted parameter, σ_{z2} is the adjusted parameter, $r_1 = 3$ cm, and $r_2 = 10$ cm. Impacts of these changes in the treatment of dispersion parameters were examined in [9].

E.2 Plume Rise

The WASH-1400 consequence model used plume rise equations recommended in Briggs (1969) [10]. The plume rise model used in CRAC2 is based on a more recent paper by Briggs (1975) [11].

E.3 Precipitation Scavenging (Wet Deposition)

The WASH-1400 consequence model (CRAC) used weather data which reported rainfall in terms of the incidence or nonincidence of rain within any clock hour. To calculate precipitation scavenging, the model assumed that rain reported for a clock hour fell at a rate of 1 mm/hr for half the hour. The CRAC2 code contains a more sophisticated wet deposition model which requires as input the amount of rain falling in an hour. Rain is assumed to occur during the entire hour with a constant rate. The hourly rainfall rate is multiplied by a rainout coefficient to determine precipitation scavenging. A coefficient of $1.0 \times 10^{-4} (\text{sec})^{-1} (\text{mm/hr})^{-1}$ is used for stable conditions and $1.0 \times 10^{-3} (\text{sec})^{-1} (\text{mm/hr})^{-1}$ for neutral and unstable conditions.

E.4 Mixing Heights

The WASH-1400 consequence model used Holzworth [12] morning and afternoon mixing heights for all stability conditions. In CRAC2, the treatment is somewhat simplified. For stable conditions (E and F stability), the inversion layer is ground based and no mixing depth

is assumed. For neutral and unstable conditions, the Holzworth afternoon mixing height is assumed. This change has minimal impact on resulting predicted consequences.

E.5 Improved Weather Sequence Sampling Technique

WASH-1400's consequence model (CRAC) used a stratified sampling technique by which sequences are selected every four days \pm thirteen hours to provide coverage of diurnal, seasonal and four-day weather cycles [13]. In this manner, a total of 91 weather sequences were chosen to represent one year of data (8760 hours). Sensitivity studies have shown that considerable variation in predicted consequences result from sampling by this method. Consequences can vary significantly for calculations performed using different sets of weather sequences (see Figure E5-1A). Differences in peak predicted consequences of an order of magnitude or more are not uncommon.

There are several reasons for the large variation in consequences due to the WASH-1400 sampling technique. Given an accident, large consequences are normally associated with relatively low probability weather conditions such as rainfall within a few 10's of kilometers of the site [14], wind-speed slowdowns, or stable weather conditions with moderate wind speeds. Not only is the occurrence of rainfall or a slowdown important, but where it occurs as well. Rain beginning over a densely populated area could result in extremely high consequences. Because of their low probability, such weather conditions will be selected infrequently, if at all, by the WASH-1400 sampling technique. Furthermore, estimated probabilities for adverse weather conditions can be significantly in error. For example, a particularly adverse weather sequence with actual probability of 1/8760 would, if sampled, be assigned a probability of 1/91.

CRAC2 uses a new weather sequence sampling method [15] which produces improved estimates of accident-consequence frequency distributions. Prior to sequence selection, the entire year of weather data is sorted into 29 weather categories (termed "bins"), as defined in Table E.5-1. Each of the 8760 potential sequences is first examined to determine if rain occurs anywhere within 50 kilometers (30 miles) of the accident site.

If not, a similar examination is made for wind-speed slowdowns. If neither of these conditions occurs, the sequence is categorized by the stability and wind speed at the start of the accident. A probability for each weather bin is estimated from the number of sequences placed in the bin. Sequences are then sampled from each of the bins (with appropriate probabilities) for use in risk calculations. In the current analysis, four sequences were selected from each bin. Sampling with this method assures that low probability adverse weather conditions are adequately included.

A comparison of the variation in consequences due to sampling by the two methods is provided in Figure E.5-1. For both methods, early-fatality frequency distributions (CCDF's) for a PWR2 release [15] were calculated with CRAC, using 32 different sets of weather sequences sampled from the New York City weather data summarized in Table E.5-1. Also assumed were a uniform population density of 100 people/mile² and a relatively ineffective evacuation. The results clearly indicate that the weather bin method results in substantially less variation due to sampling than the previous WASH-1400 technique.

E.6 Emergency Response (Evacuation) Model

The CRAC2 evacuation model [16,17] is significantly different from the RSS evacuation model. In lieu of the small "effective" evacuation speeds assumed in the RSS model, the revised treatment incorporates a delay time before public movement, followed by evacuation radially away from the reactor. Both an assumed delay time and evacuation speed are required as input to the model. Different shielding factors and breathing rates are used while stationary or in transit. In addition, all persons within the designated evacuation area move as a group with the same delay time and evacuation speed. Therefore, the possibility that some people may not leave the evacuated area is ignored. This latter assumption results in upper bound estimates of evacuation effectiveness, given a specific delay time and speed.* Unlike the RSS model in which persons continue

*The evacuation effectiveness would decrease linearly with an increasing nonparticipating fraction of the population. In actual evacuations, Civil Defense personnel have observed a nonparticipating minority of approximately 5%.

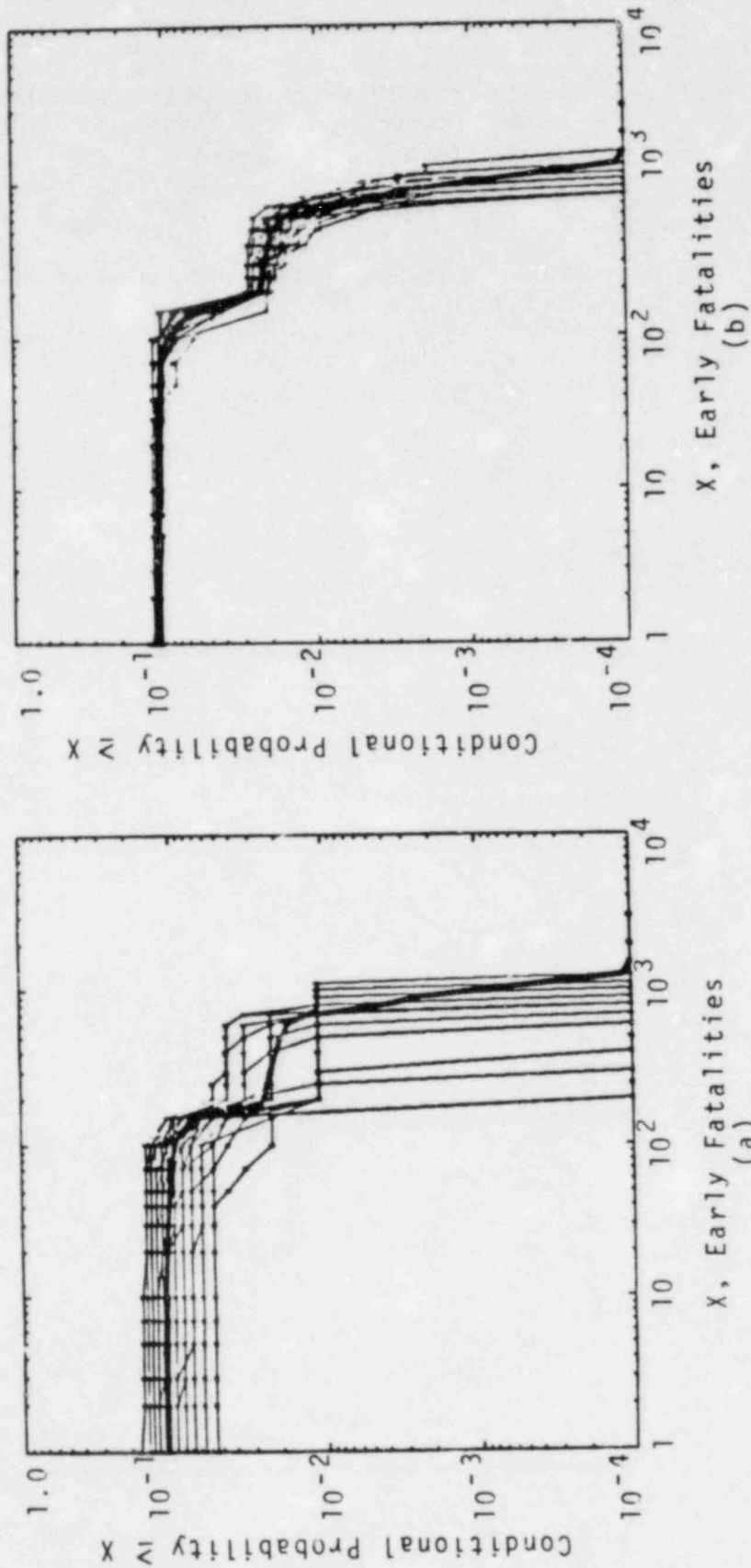


Figure E.5-1. Comparison of Uncertainty Due to Sampling by (A) WASH-1400 and (B) Weather Bin Techniques. For each technique, 32 different sets of weather sequences are used to generate early-fatality frequency distributions for a PWR2 release. A "best estimate" using all 8760 available sequences, is shown by the darkened line.

Table E.5-1 One Year of New York City Meteorological Data Summarized Using Weather Bin Categories

Weather Bin Definitions

R - Rain starting within indicated interval (miles).

S - Slowdown occurring within indicated interval (miles).

A-C D E F - Stability categories.

1(0-1), 2(1-2), 3(2-3), 4(3-5), 5(GT 5) - Wind Speed intervals (m/s).

<u>Weather Bin</u>	<u>Number of Sequences</u>	<u>Percent</u>
1 R (0)	697	7.96
2 R (0-5)	12	.14
3 R (5-10)	62	.71
4 R (10-15)	102	1.16
5 R (15-20)	75	.86
6 R (20-25)	67	.76
7 R (25-30)	61	.70
8 S (0-10)	24	.27
9 S (10-15)	16	.18
10 S (15-20)	18	.21
11 S (20-25)	14	.16
12 S (25-30)	18	.21
13 A-C 1, 2, 3	168	1.92
14 A-C 4, 5	892	10.18
15 D 1	0	0.00
16 D 2	61	.70
17 D 3	226	2.58
18 D 4	948	10.82
19 D 5	3325	37.96
20 E 1	0	0.00
21 E 2	27	.31
22 E 3	167	1.91
23 E 4	682	7.79
24 E 5	270	3.08
25 F 1	0	0.00
26 F 2	116	1.32
27 F 3	310	3.54
28 F 4	402	4.59
29 F 5	0	0.00
	<u>8760</u>	<u>100.00</u>

evacuating until they are either overtaken by the cloud or leave the model grid, all evacuating persons in the new model travel a designated distance from the evacuated area and are then removed from the problem. This treatment allows for the likelihood that after traveling outward for some distance, people may learn their position relative to the cloud and be able to avoid it.

The new model also calculates more realistic exposure durations to airborne and ground-deposited radionuclides than the RSS evacuation model. The RSS consequence model employs an exposure model for an instantaneous point source and thus all released plumes have zero effective lengths. Because of this, evacuating persons overtaken by the cloud in the RSS evacuation model are exposed to the entire cloud at the point overtaken. However, a released cloud of radioactive material would have a finite release duration and a length that depends on the wind speed during and following the release. A person overtaken by the front of the cloud might still escape before being passed by the entire cloud and thus receive only a fraction of the full cloud exposure.* The revised evacuation model assigns the cloud a finite length which is calculated using the assumed release duration and wind speed during the release. To simplify the treatment, the length of the cloud is assumed to remain constant following the release (i.e., the front and back of the cloud travel at the same speed), and the concentration of radioactive material is assumed to be uniform over the length of the cloud. The radial position of evacuating persons, while stationary and in transit, is compared to both the front and the back of the cloud as a function of time to determine a more realistic period of exposure to airborne radionuclides.

The revised treatment calculates the time periods during which people are exposed to radionuclides on the ground while they are stationary and while they

*It is also possible that an evacuating person may travel under the cloud for a long time and thus receive more exposure than if he had remained stationary during the passage of the cloud.

are evacuating. Because radionuclides would be deposited continually from the cloud as it passed a given location, a person while under the cloud would be exposed to ground contamination less concentrated than if the cloud had completely passed. To account for this, the new model assumes that persons completely passed by the cloud are exposed to the total ground contamination concentration, calculated to exist after complete passage of the cloud, to one-half the calculated concentration when anywhere under the cloud, and to no concentration when in front of the cloud. A more detailed discussion of the models is provided in [16] and [17].

The CRAC2 model of public evacuation requires as input estimates of the delay time before evacuation commences and the evacuation speed. Reexamination of the EPA evacuation data used to develop the WASH-1400 model [18] show that, if a constant evacuation speed was assumed, a distribution of delay times could be estimated. For assumed evacuation speeds of 10 mph or greater, delay times were found to be satisfactorily represented by a normal distribution with 15, 50, and 85 percentile delay times of approximately 1, 3, and 5 hours respectively.

The CRAC2 evacuation model can incorporate this distribution of evacuation delay times by calculating a 30:40:30% weighted sum of consequences for 10 mph evacuations after delays of 1, 3, and 5 hours. The weighted distribution of evacuations is denoted "Summary Evacuation", and was discussed in Sections 2.2 and 2.5.

The CRAC2 model is also capable of considering population sheltering as an emergency protective action. Sheltering would involve the expedient movement of people into basements or masonry buildings, if possible, followed by relocation. Table A.1-3 of Appendix A lists sheltering factors for different regions in the U.S. A discussion of sheltering is provided in [19].

E.7 Updated Cancer Risk Factors

The latent cancer fatality risk factors used in CRAC2 are updated versions of those reported in WASH-1400. The RSS factors assumed a latency period during which the risk of cancer was assumed to be zero, followed by a risk period where the individual is assumed to be at a constant risk (risk plateau). Depending on the type of cancer and the age of the exposed individual, the latency periods ranged from 0 to 15 years and the risk periods ranged from 10 to 30 years. Based on recommendations in BEIR III [20], the factors used in CRAC2 were updated to reflect extension of the risk period to the end of an individual's life for all cancers except leukemia and for all age groups (of exposed individuals) other than those exposed in utero. Table E.7-1 compares the updated factors to those from WASH-1400. The 0-1 year factors are used for external exposures.

Table E.7-1 Expected Total Latent Cancer (Excluding Thyroid) Deaths per 10^6 Man-Rem From Internal Radionuclides Delivered During Specified Periods

WASH-1400

	Time Period (years) After Accident								
	0-1	1-10	11-20	21-30	31-40	41-50	51-60	61-70	71-80
Leukemia	28.4	27.2	18.7	13.8	9.7	6.8	4.0	1.7	0.5
Lung	22.2	22.2	22.2	14.5	8.1	4.0	1.5	0.2	0
GI Tract ^(a)	13.5	13.6	13.6	8.9	5.0	2.5	0.9	0.1	0
Pancreas	3.4	3.4	3.4	2.2	1.3	0.6	0.2	0	0
Breast	25.6	25.6	25.6	16.8	9.4	4.6	1.7	0.3	0
Bone	6.9	6.7	5.0	2.6	1.6	0.9	0.4	0.1	0
All Other	21.6	19.8	17.1	11.2	6.3	3.1	1.2	0.2	0

UPDATED WASH-1400 (CRAC2)

Leukemia	28.4	27.2	18.7	13.8	9.7	6.8	4.0	1.7	0.5
Lung	27.5	27.5	27.5	15.8	8.1	4.0	1.5	0.2	0.0
GI Tract ^(a)	16.9	16.9	16.9	9.7	5.0	2.5	0.9	0.1	0.0
Pancreas	4.2	4.2	4.2	2.4	1.3	0.6	0.2	0.0	0.0
Breast	31.7	31.7	31.7	18.3	9.4	4.6	1.7	0.3	0.0
Bone	11.1	10.6	7.0	3.0	1.7	0.9	0.4	0.1	0.0
All Other	28.0	26.3	21.1	12.2	6.3	3.0	1.2	0.2	0.0

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Appendix F: Site Availability Maps and Tables

This appendix contains the site availability data that was discussed in Chapter 4.0. Figure F1 shows legally protected and wetland areas in the U. S. where reactor siting would be restricted. Seismic acceleration contours are shown in Figure F2. Figure F4 shows the topographic character of the U. S. in terms of percent land that is gently sloping (gently sloping was defined as less than 8% slope). Figures F3, F5, F6, and F7 show seismic hardening costs, surface, water availability costs, groundwater availability costs, and combined water availability costs (the lesser of surface water and groundwater costs) for the 48 contiguous United States. Associated with these costs are the utility values discussed in Section 4.4.1 of Chapter 4.0. Tables F1.1-F1.5 show the fractions of land, by state, that fall within each of the environmental suitability categories shown in Figures F3-F7.

Figures F8.1-F8.13 show land that would be restricted from reactor siting by standoff distances to cities. The cities and standoff distances considered in each figure are tabulated below.

Figure	Standoff Distance (mile)	Cities (Population \geq)
F8.1	5	25,000
F8.2	10	25,000
F8.3	10	100,000
F8.4	15	100,000
F8.5	25	100,000
F8.6	25	200,000
F8.7	30	200,000
F8.8	40	200,000
F8.9	50	200,000
F8.10	100	200,000
F8.11	125	250,000
F8.12	18	500,000
F8.13	25	1,000,000

Figures F8.11, F8.12, and F8.13 show the restricted areas for the Northeastern U. S. only.

Figures F9.1-F9.26 show areas that would be restricted from reactor siting by population density criteria. These criteria restrict the number of people that can reside in an annulus surrounding a reactor site. The population density restrictions and the annuli considered in each figure are tabulated below. The population restrictions are shown in terms of average population density (people within the annulus/annulus area).

Figure	Radii of the Annulus (mile)	Average Population Density (people/mile ²)
F9.1	0-2	100
F9.2	0-2	250
F9.3	0-2	500
F9.4	0-2	750
F9.5	0-5	100
F9.6	0-5	200
F9.7	0-5	350
F9.8	0-5	500
F9.9	0-10	100
F9.10	0-10	200
F9.11	0-10	350
F9.12	0-10	500
F9.13	0-20	200
F9.14	0-30	500
F9.15	0-30	1000
F9.16	5-10	150
F9.17	5-10	350
F9.18	5-10	500
F9.19	5-20	800
F9.20	10-20	400
F9.21	10-20	500
F9.22	10-20	1000
F9.23	20-30	500
F9.24	20-30	1000
F9.25	30-50	500
F9.26	30-50	1000

Figures 9.3 and 9.4 show restricted areas for the Northeastern U. S. only.

Figures F10.1-F10.4 show areas in the NE U. S. that would be restricted from siting by composite density criteria between 2 and 30 miles of a prospective site. Each criterion would simultaneously restrict the mean

population densities within six annuli: 2-3 miles, 2-4 miles, 2-5 miles, 2-10 miles, 2-20 miles, and 2-30 miles. The mean population densities in each of the six annuli can not exceed the prescribed density limits for the site to be acceptable. Figures F10.1, F10.2, F10.3 and F10.4 consider density restrictions of 500, 750, 1000, and 1500 people/mile², respectively for the Northeastern U. S.

Figures F11 and F12 show areas in the 48 contiguous United States that would be restricted from reactor siting by the combination of a population density restriction within two miles and a composite population density restriction between 2 and 30 miles of the site. Figure F11 considers a population density restriction of 100 people/mile² within 2 miles and a composite population density of 500 people/mile². Figure F12 is based on a 250 people/mile² density restriction within 2 miles and a composite population density restriction (2-30 miles) of 500 people/mile². The 2-30 mile composite restriction is as defined for Figures F10.1-F10.4.

Tables F2.1-F2.24 show the fractions of land available for reactor siting in each state if sector population restrictions are added to a composite population density criterion. These restrictions would limit the number of people that could reside within any sector in each of the composite annuli (see Section 4.5.4 of Chapter 4.0). For these tables, five annuli were considered: 0-2 miles, 0-5 miles, 0-10 miles, 0-20 miles, and 0-30 miles. The allowable populations in each annuli were calculated assuming 250 people/mile² between zero and two miles and from 250 to 1500 people/mile² in the two to thirty mile region. An acceptable site must satisfy the sector population restriction for each of the composite annuli. The sector population restrictions (fraction of annulus population allowed within the sector), sector widths, and the 2-30 mile average population densities (people within an annulus/annulus area) considered in each table are given below. Tables F2.1-F2.12 show the land areas that are uniquely restricted by the specified criterion. Tables F2.13-F2.24 show the fraction of land available for reactor siting based on the specified criterion.

Table	Width	Sector Population Restrictions							Population Density (2-30 miles) (people/mile ²)
F2.1 & F2.13	22.5°	$\frac{1}{16}$	$\frac{1}{8}$	$\frac{1}{6}$	$\frac{1}{4}$	$\frac{1}{3}$	$\frac{1}{2}$	$\frac{1}{1}$	250
F2.2 & F2.14	22.5°	$\frac{1}{16}$	$\frac{1}{8}$	$\frac{1}{6}$	$\frac{1}{4}$	$\frac{1}{3}$	$\frac{1}{2}$	$\frac{1}{1}$	500
F2.3 & F2.15	22.5°	$\frac{1}{16}$	$\frac{1}{8}$	$\frac{1}{6}$	$\frac{1}{4}$	$\frac{1}{3}$	$\frac{1}{2}$	$\frac{1}{1}$	750
F2.4 & F2.16	22.5°	$\frac{1}{16}$	$\frac{1}{8}$	$\frac{1}{6}$	$\frac{1}{4}$	$\frac{1}{3}$	$\frac{1}{2}$	$\frac{1}{1}$	1500
F2.5 & F2.17	45°		$\frac{1}{8}$	$\frac{1}{6}$	$\frac{1}{4}$	$\frac{1}{3}$	$\frac{1}{2}$	$\frac{1}{1}$	250
F2.6 & F2.18	45°		$\frac{1}{8}$	$\frac{1}{6}$	$\frac{1}{4}$	$\frac{1}{3}$	$\frac{1}{2}$	$\frac{1}{1}$	500
F2.7 & F2.19	45°		$\frac{1}{8}$	$\frac{1}{6}$	$\frac{1}{4}$	$\frac{1}{3}$	$\frac{1}{2}$	$\frac{1}{1}$	750
F2.8 & F2.20	45°		$\frac{1}{8}$	$\frac{1}{6}$	$\frac{1}{4}$	$\frac{1}{3}$	$\frac{1}{2}$	$\frac{1}{1}$	1500
F2.9 & F2.21	90°				$\frac{1}{4}$	$\frac{1}{3}$	$\frac{1}{2}$	$\frac{1}{1}$	250
F2.10 & F2.22	90°				$\frac{1}{4}$	$\frac{1}{3}$	$\frac{1}{2}$	$\frac{1}{1}$	500
F2.11 & F2.23	90°				$\frac{1}{4}$	$\frac{1}{3}$	$\frac{1}{2}$	$\frac{1}{1}$	750
F2.12 & F2.24	90°				$\frac{1}{4}$	$\frac{1}{3}$	$\frac{1}{2}$	$\frac{1}{1}$	1500

Tables F3.1-F3.5 show the environmental suitability of land not restricted by each of 5 population siting criteria. (The environmental suitability classifications were discussed in Section 4.4 of Chapter 4.0). These tables show the fraction of land, by state, that 1) lies within each of the five suitability categories and 2) satisfies the population criteria. The population criteria consist of a population restriction within two miles and a composite population restriction within the 2 to 30 mile region. (The annuli considered by the 2 to 30 mile composite population restriction include 2-3 miles, 2-4 miles, 2-5 miles, 2-10 miles, 2-20 miles, and 2-30 miles.) The population criterion considered by each table are tabulated below.

Table	Population Case	0-2 miles (people/mile ²)	2-30 miles (composite) (people/mile ²)
F3.1	1	100	250
F3.2	2	250	500
F3.3	3	500	750
F3.4	4	500	750
F3.5	5	500	1500

Tables F3.6-F3.10 show the effect of applying different population criteria (the five cases considered in Tables F3.1-F3.5) on land available within each of the suitability categories. The suitability category considered in each table is tabulated below.

Table	Environmental Suitability Category
F3.6	low
F3.7	medium-low
F3.8	medium
F3.9	medium-high
F3.10	high

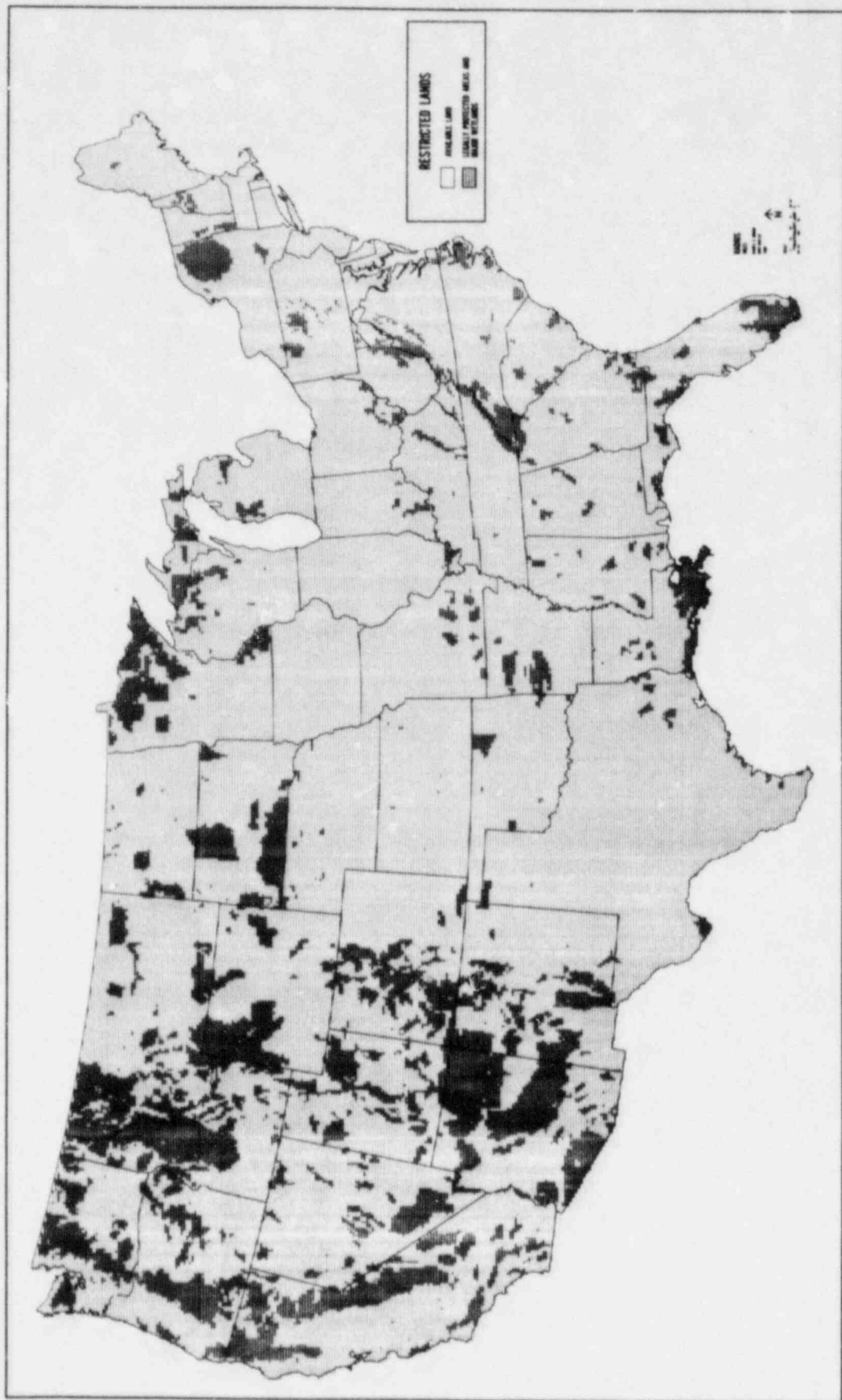


FIGURE F1

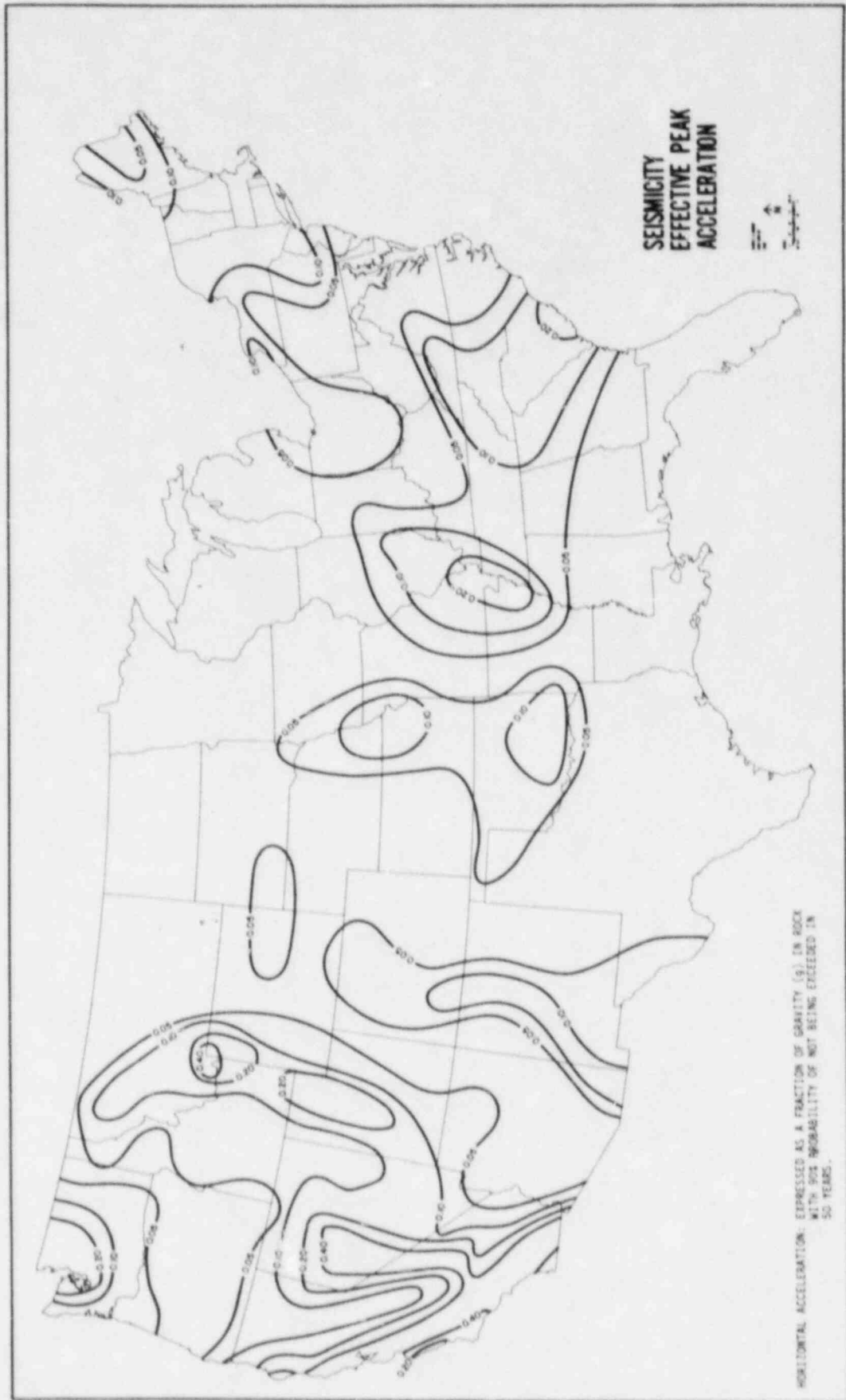


FIGURE F2

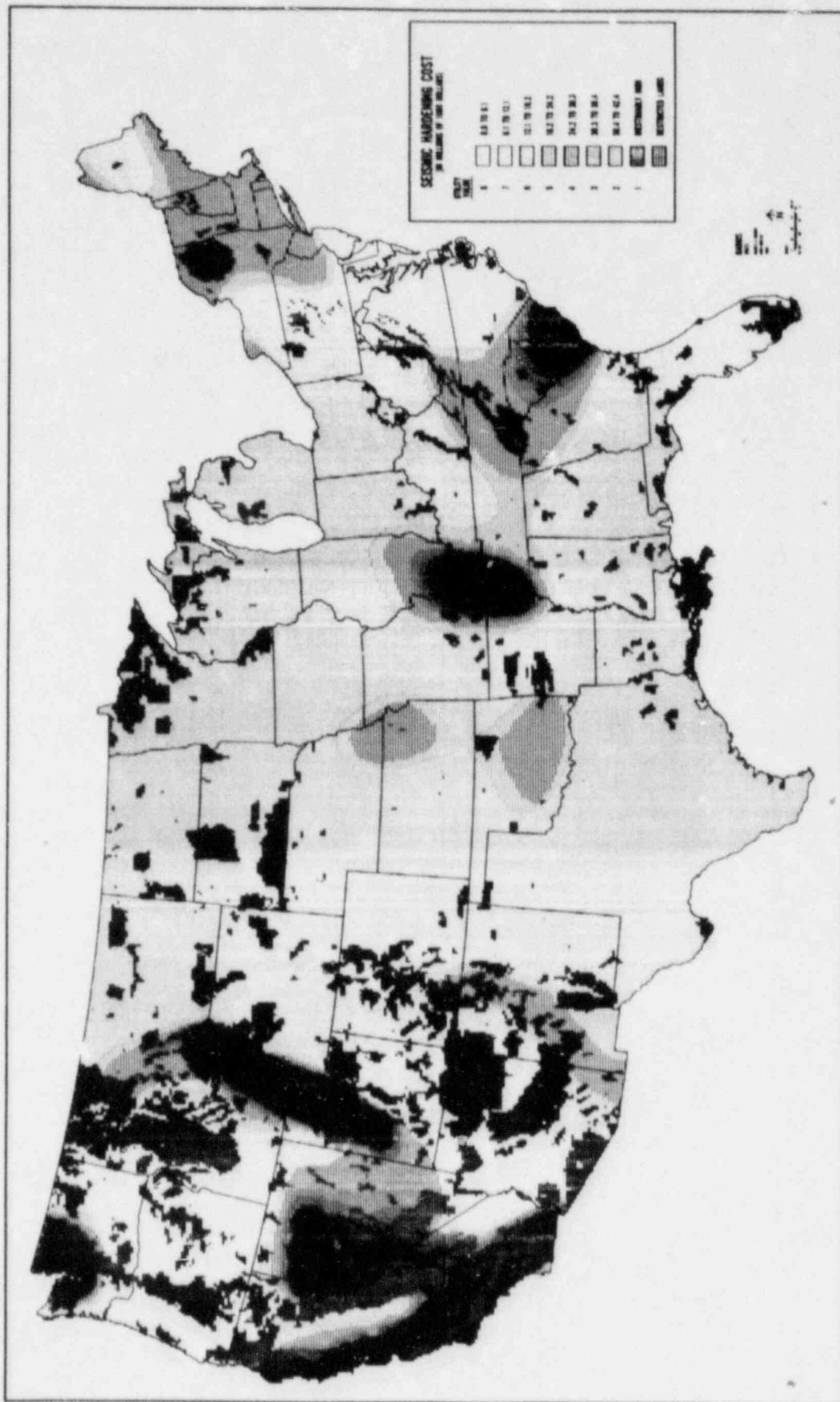


FIGURE F3



FIGURE F4

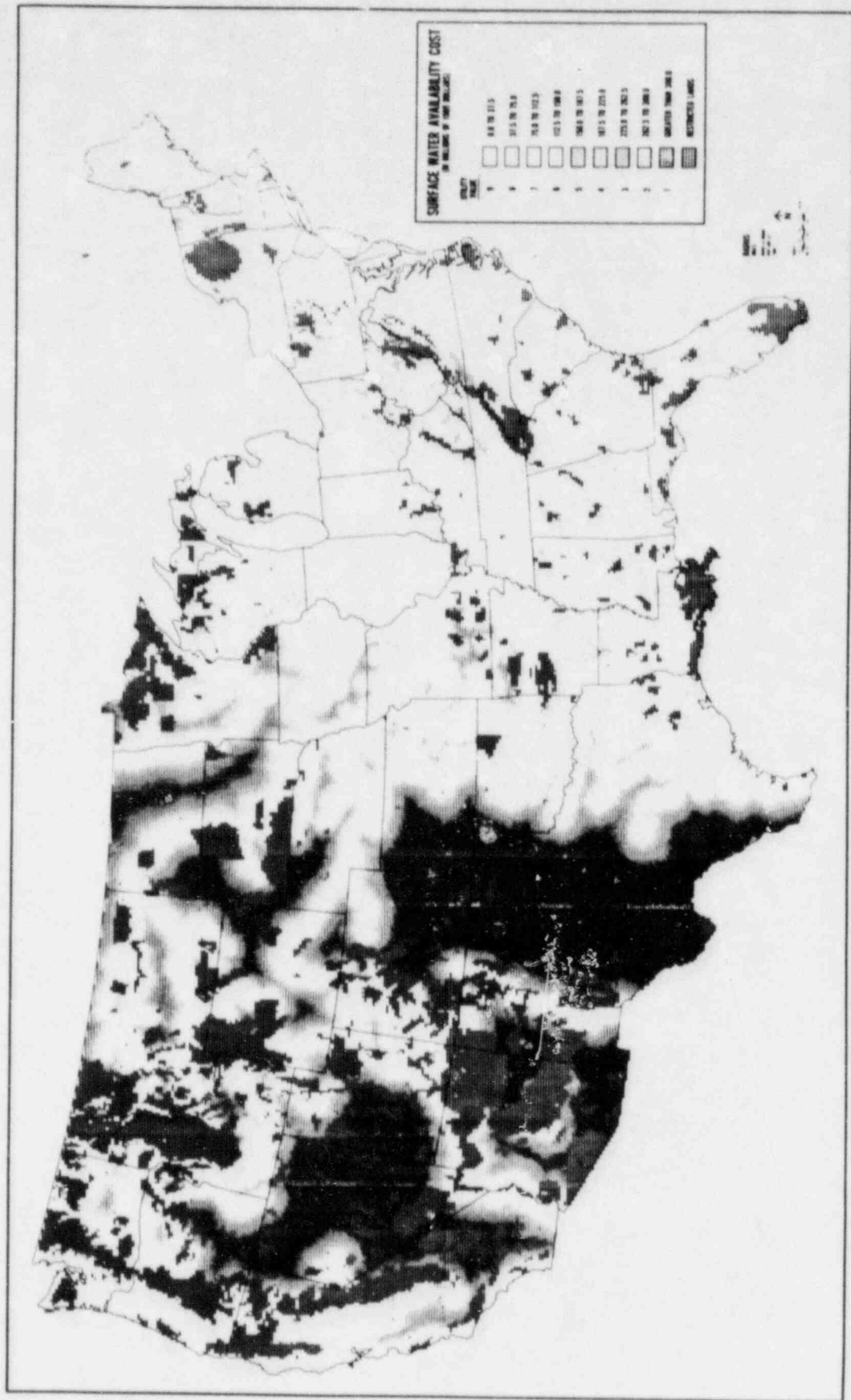


FIGURE F5

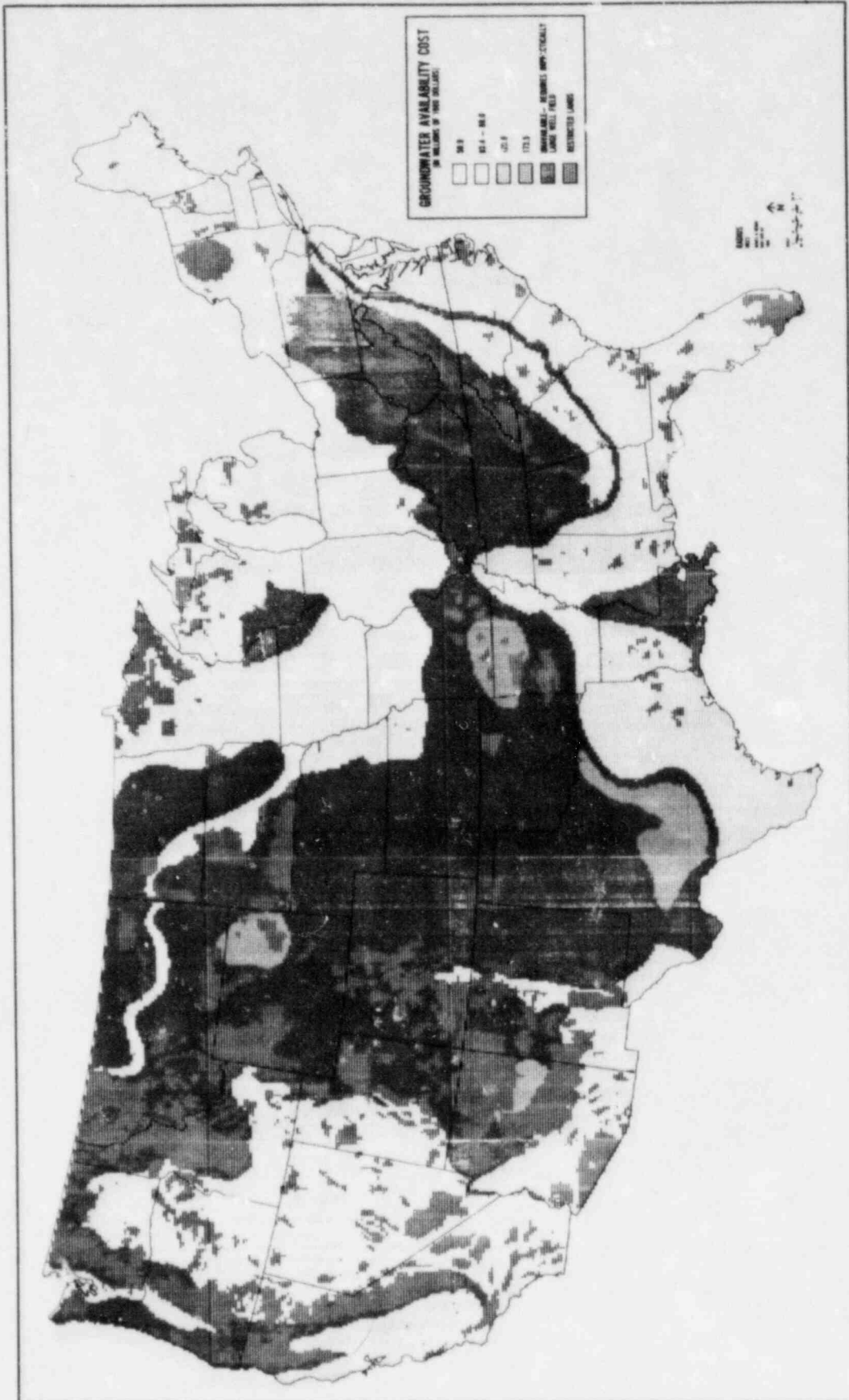


FIGURE F6

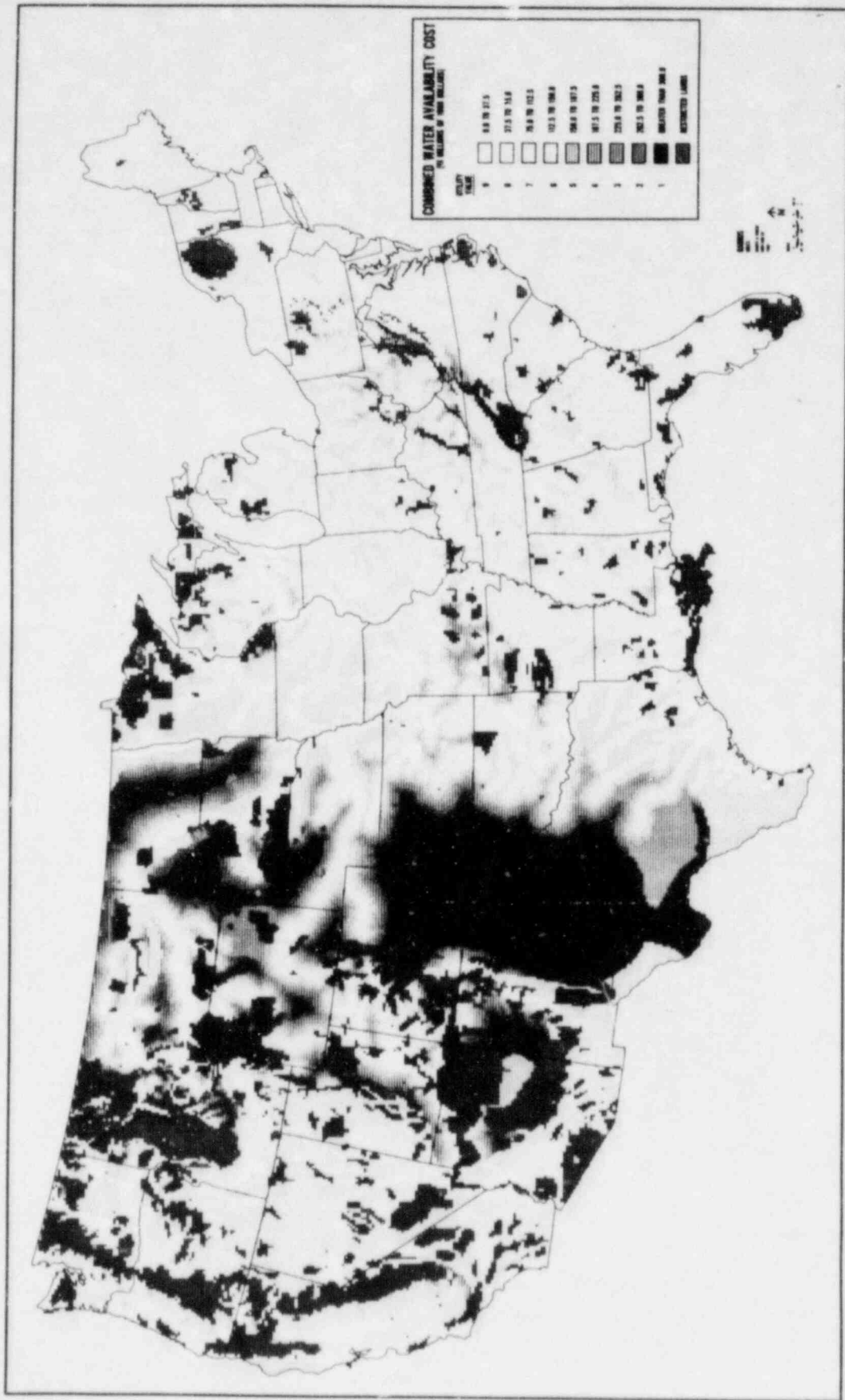


FIGURE F7

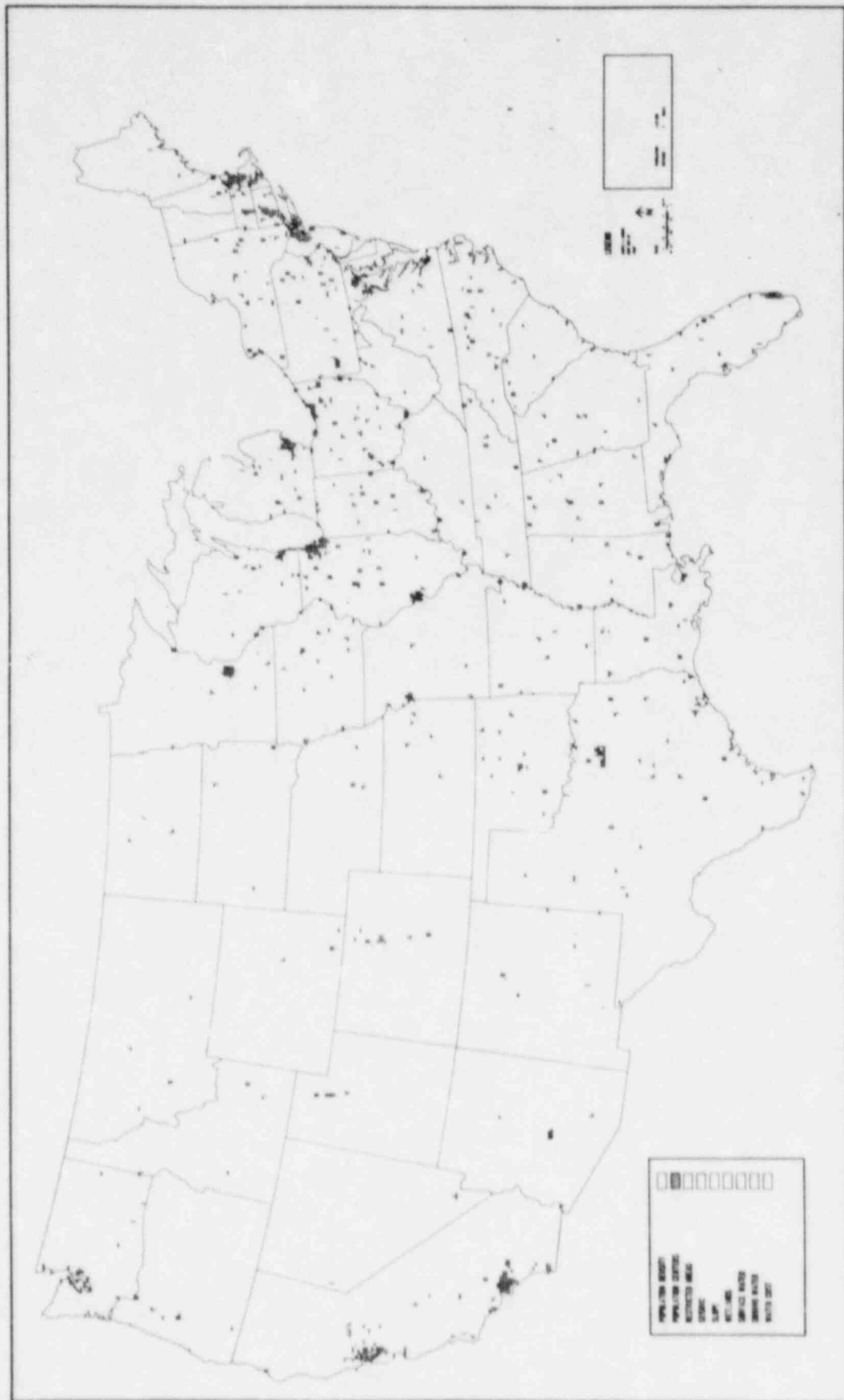


FIGURE F8.1

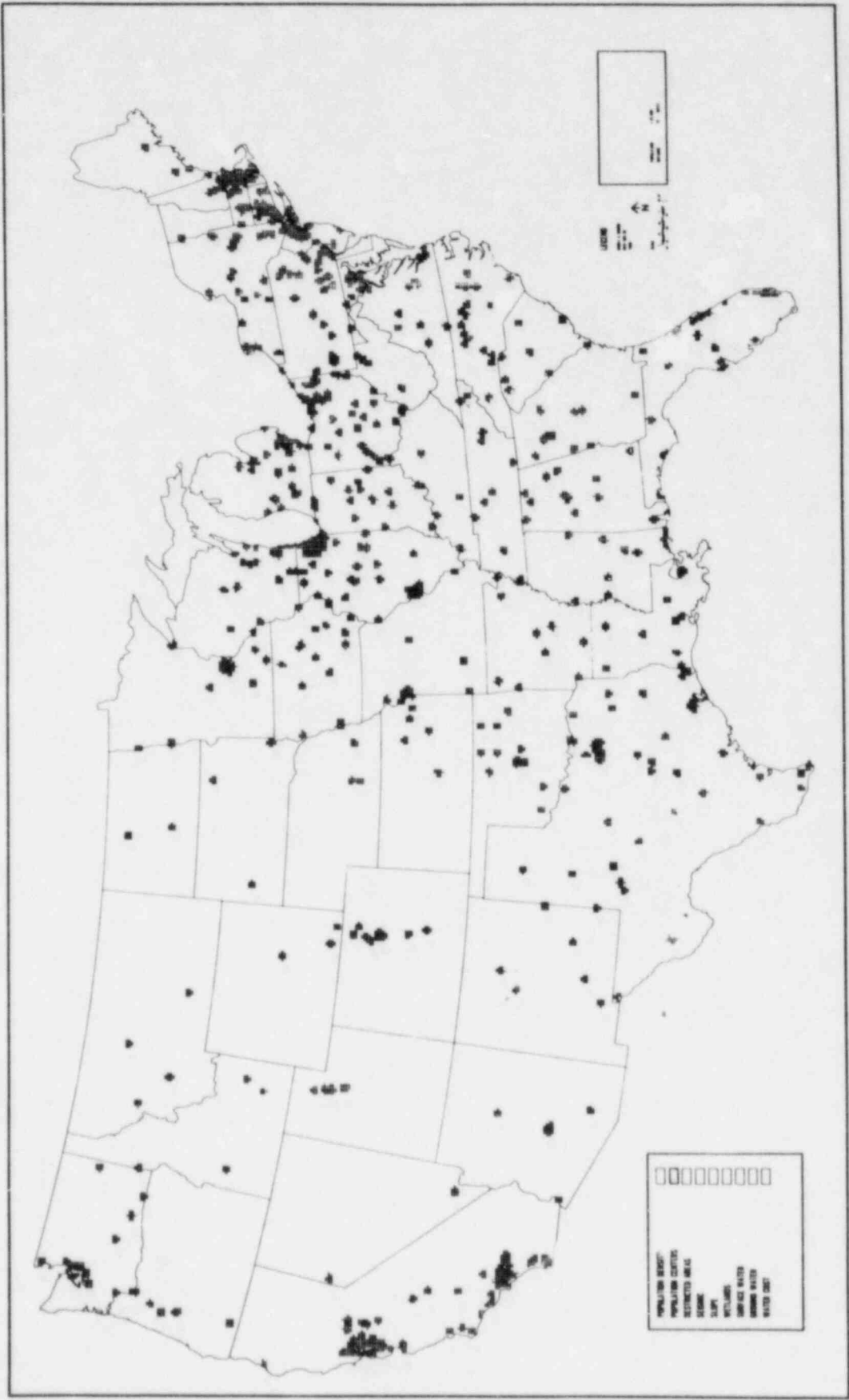


FIGURE F8.2

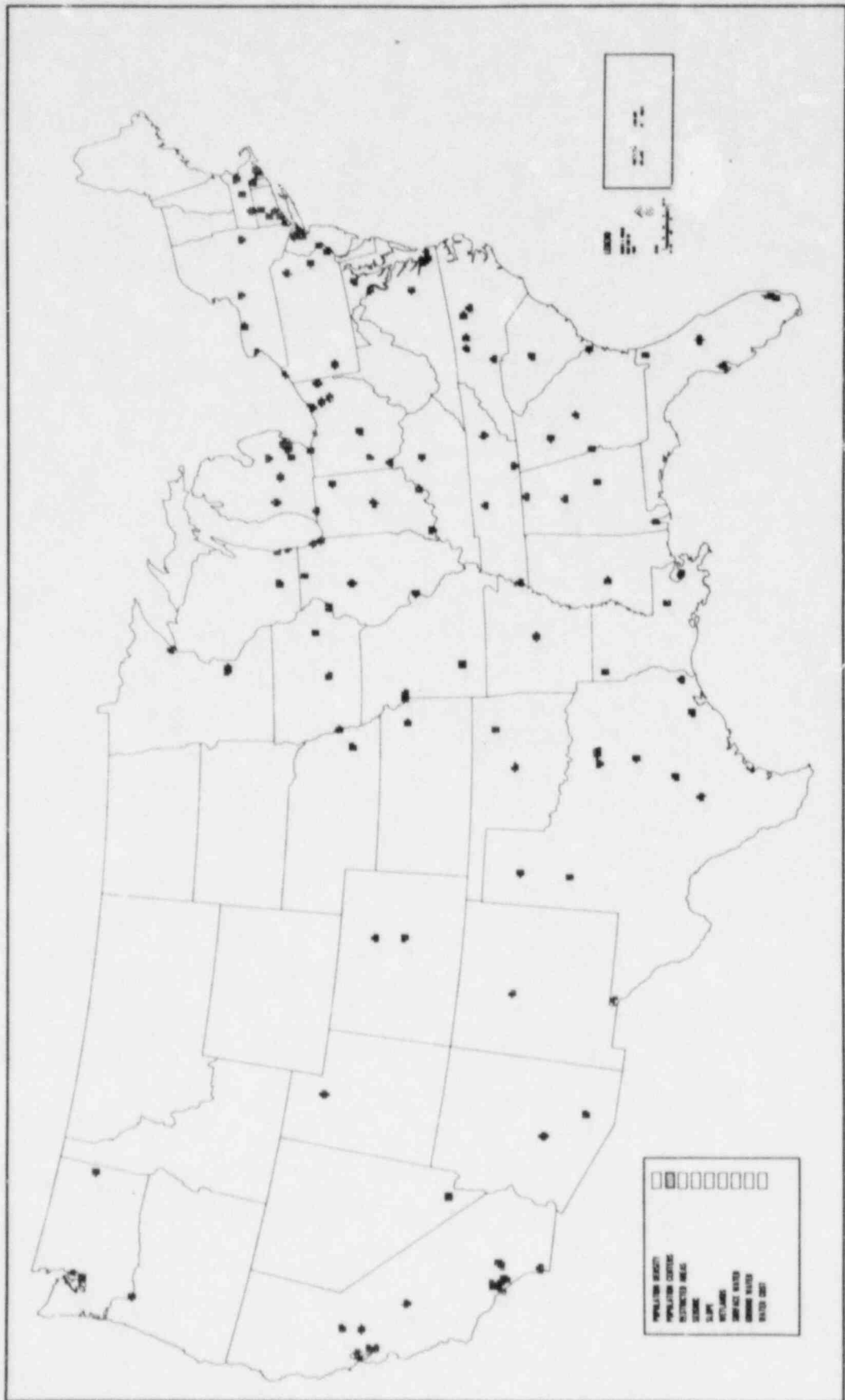


FIGURE F8.3

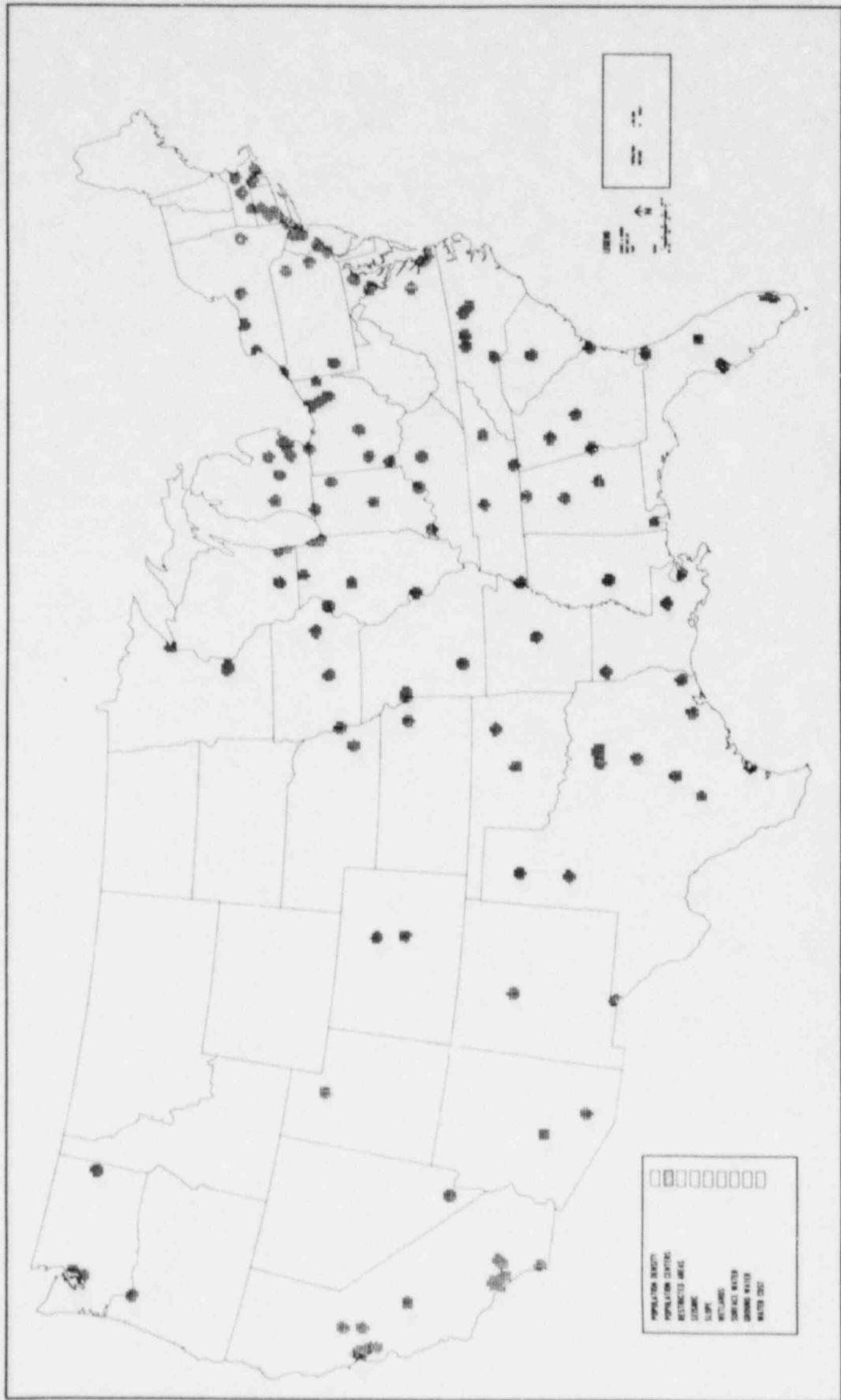


FIGURE F8.4

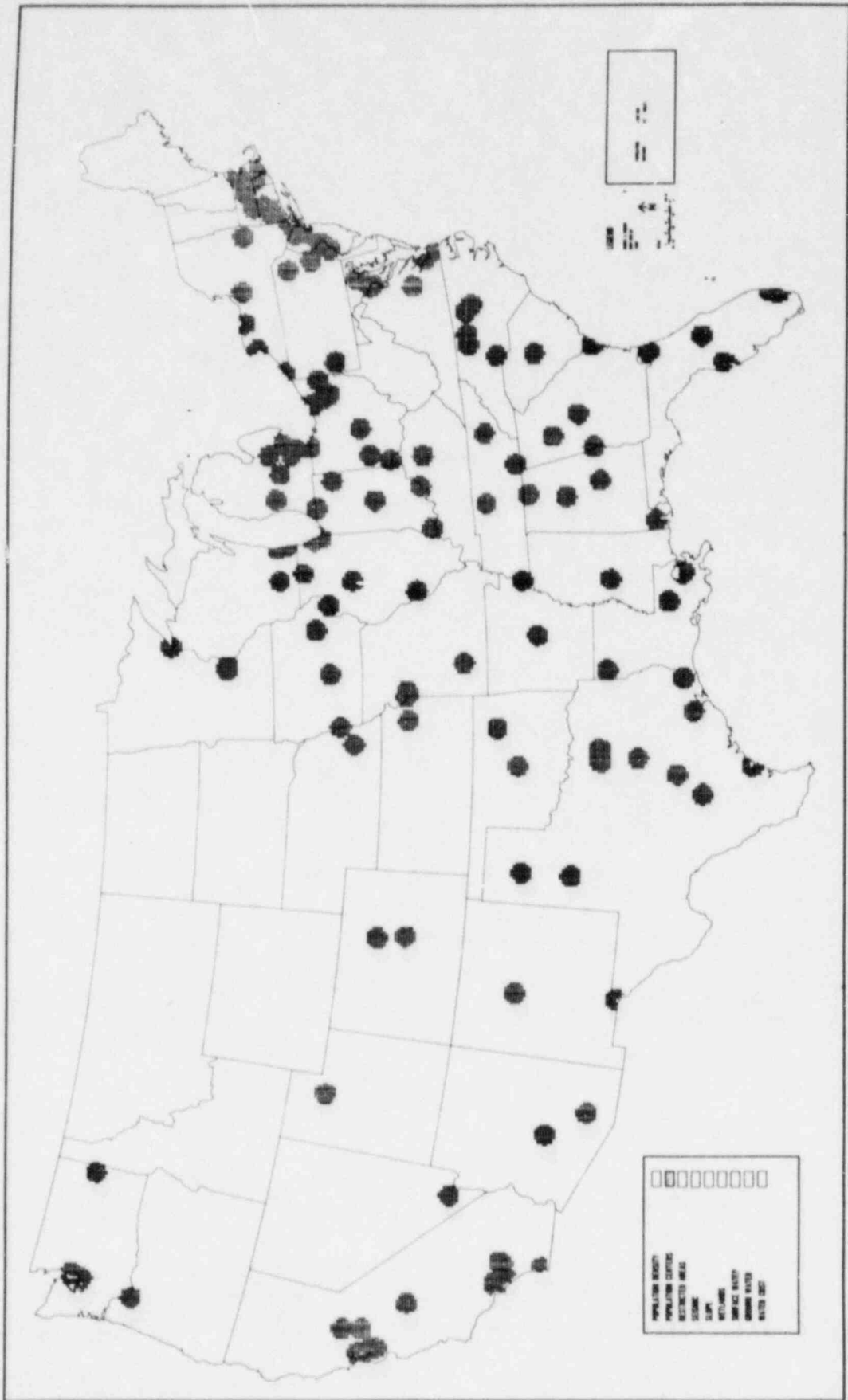


FIGURE F8.5

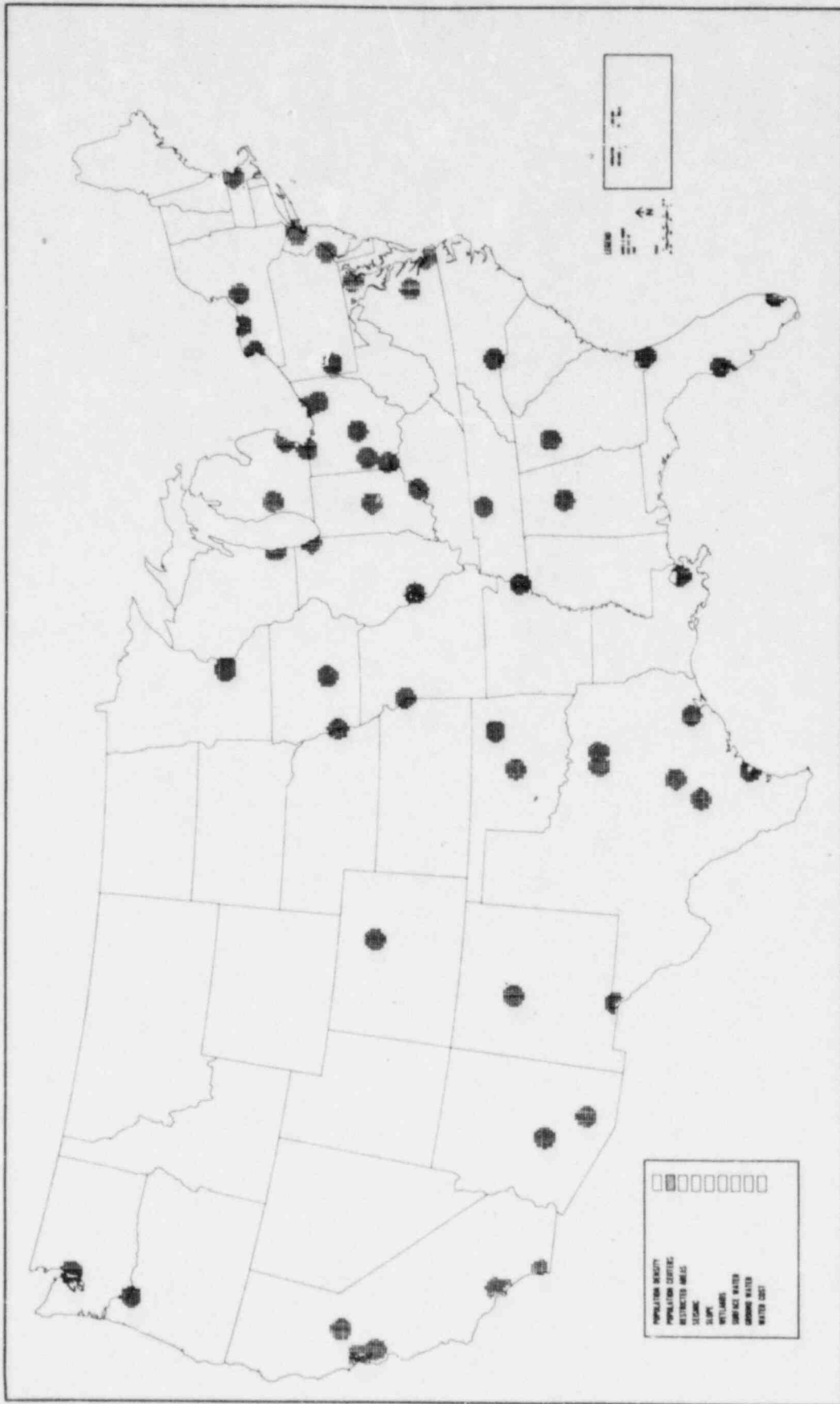


FIGURE F8.6

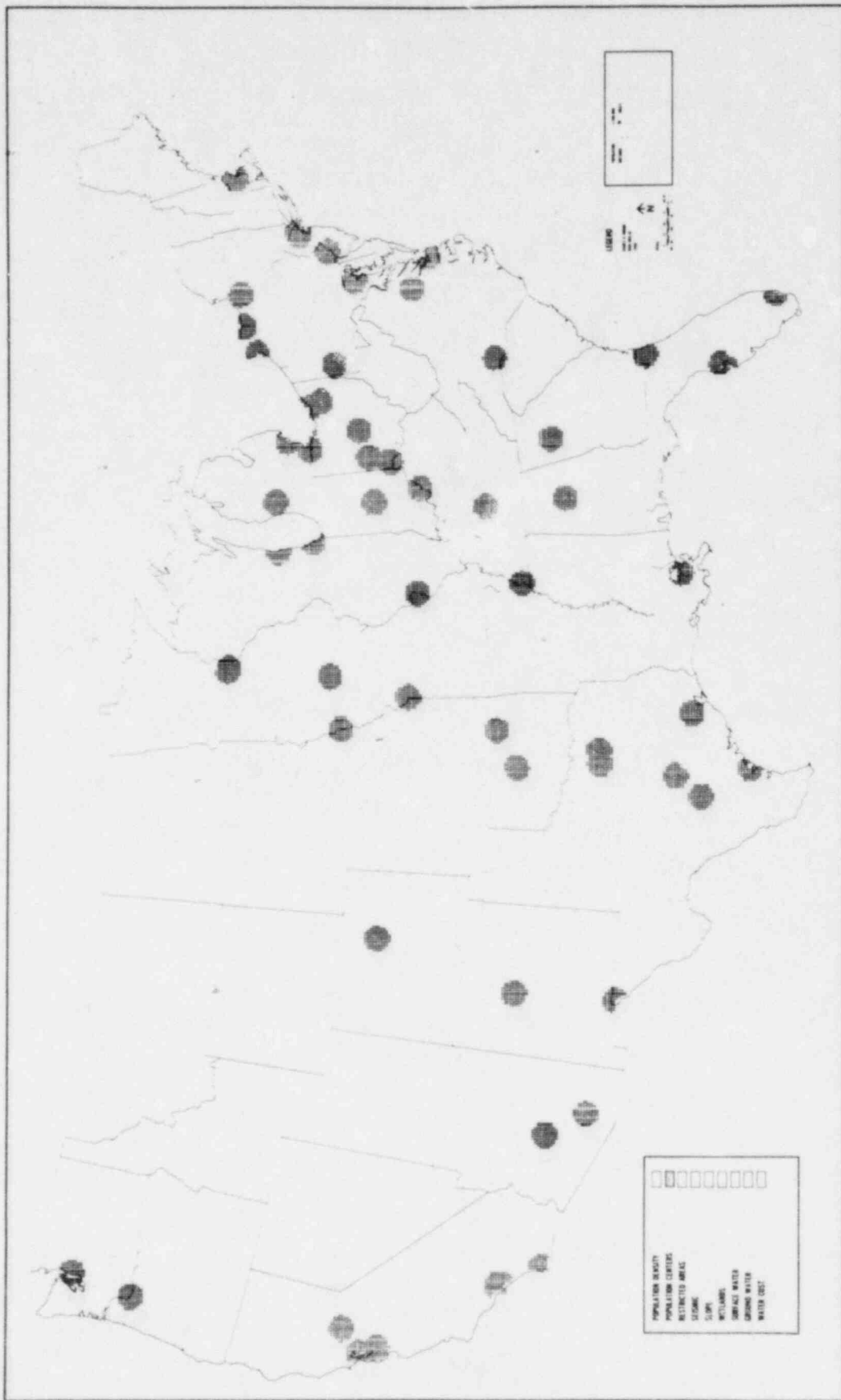


FIGURE F8.7

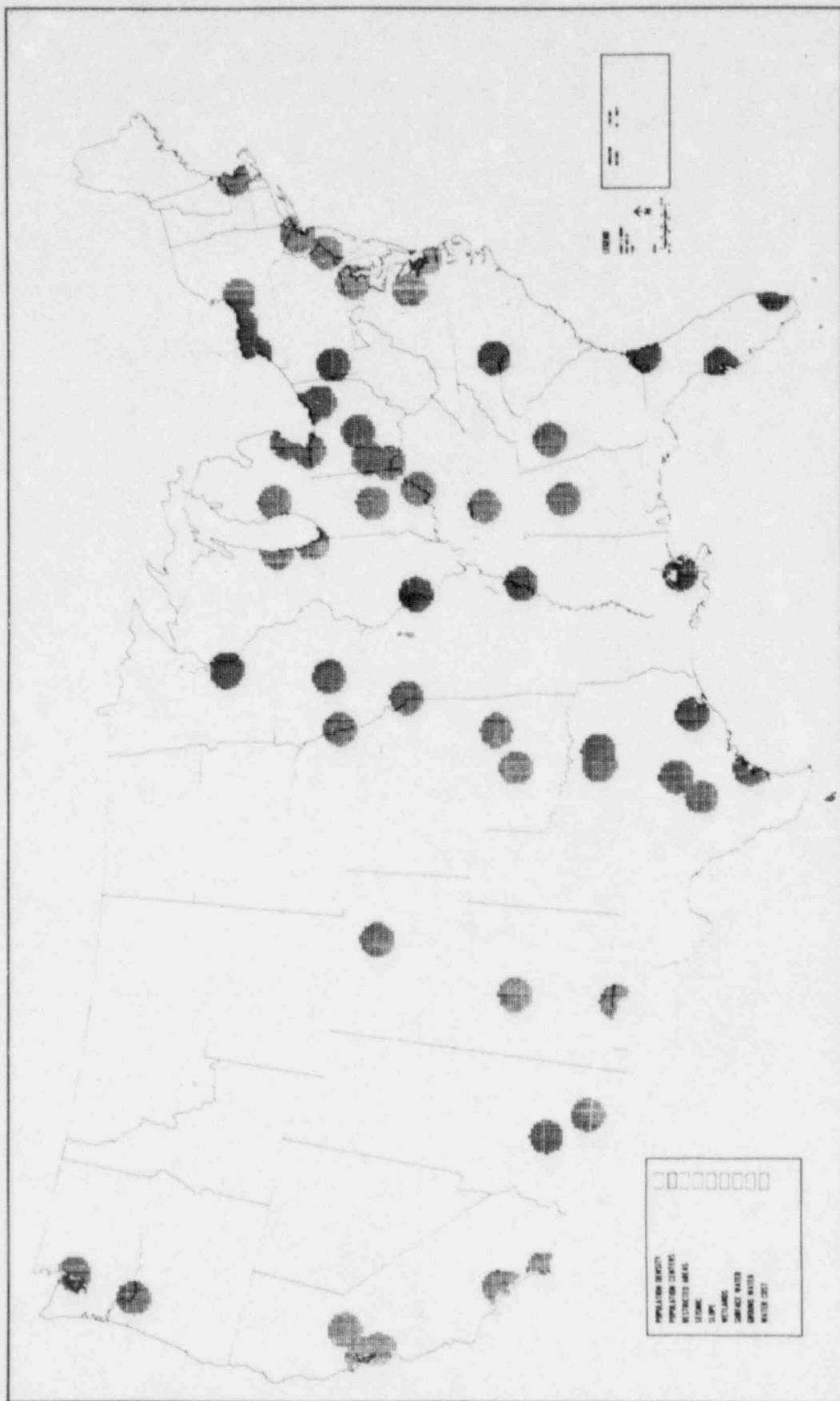


FIGURE F8.8



FIGURE F8.9

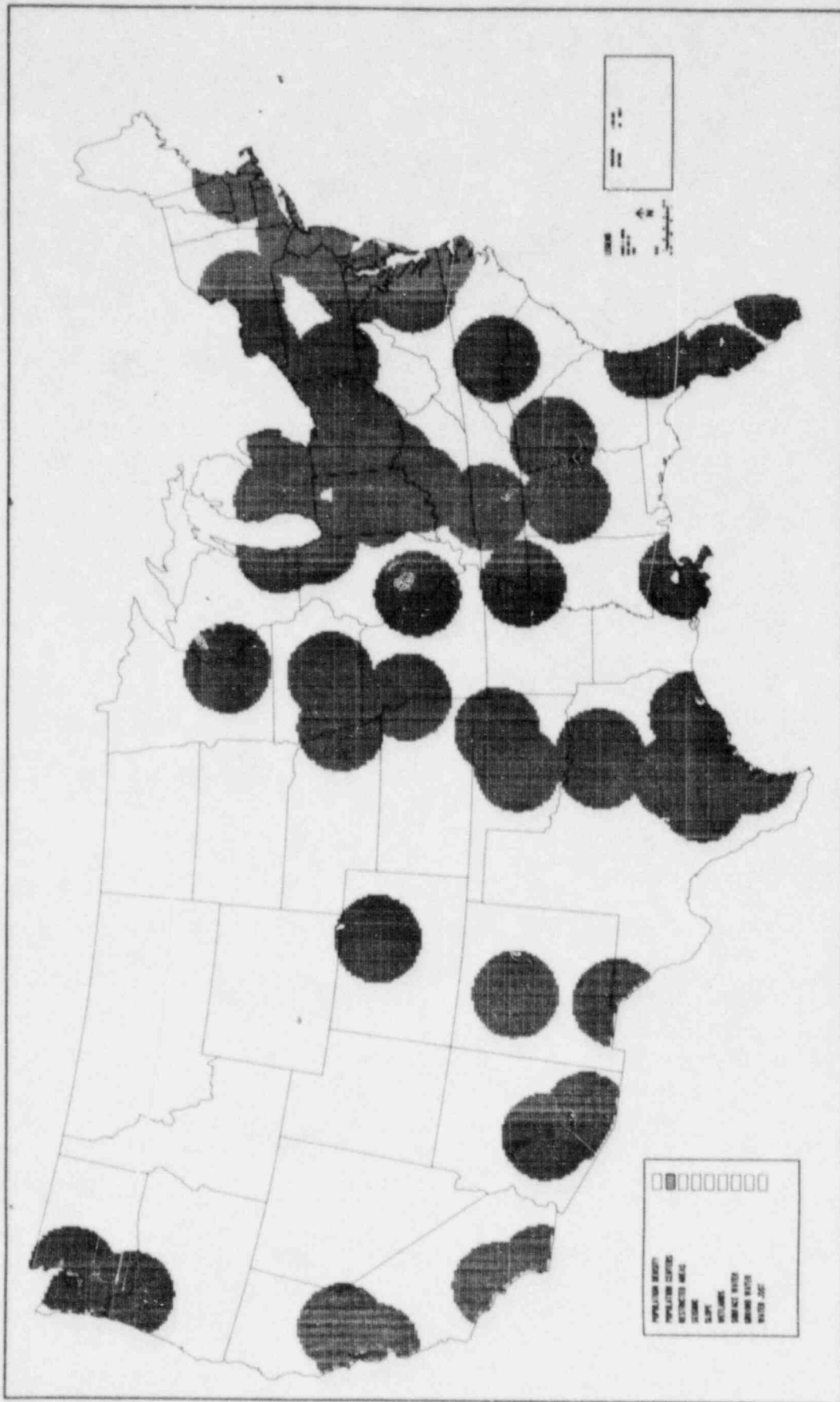


FIGURE F8.10

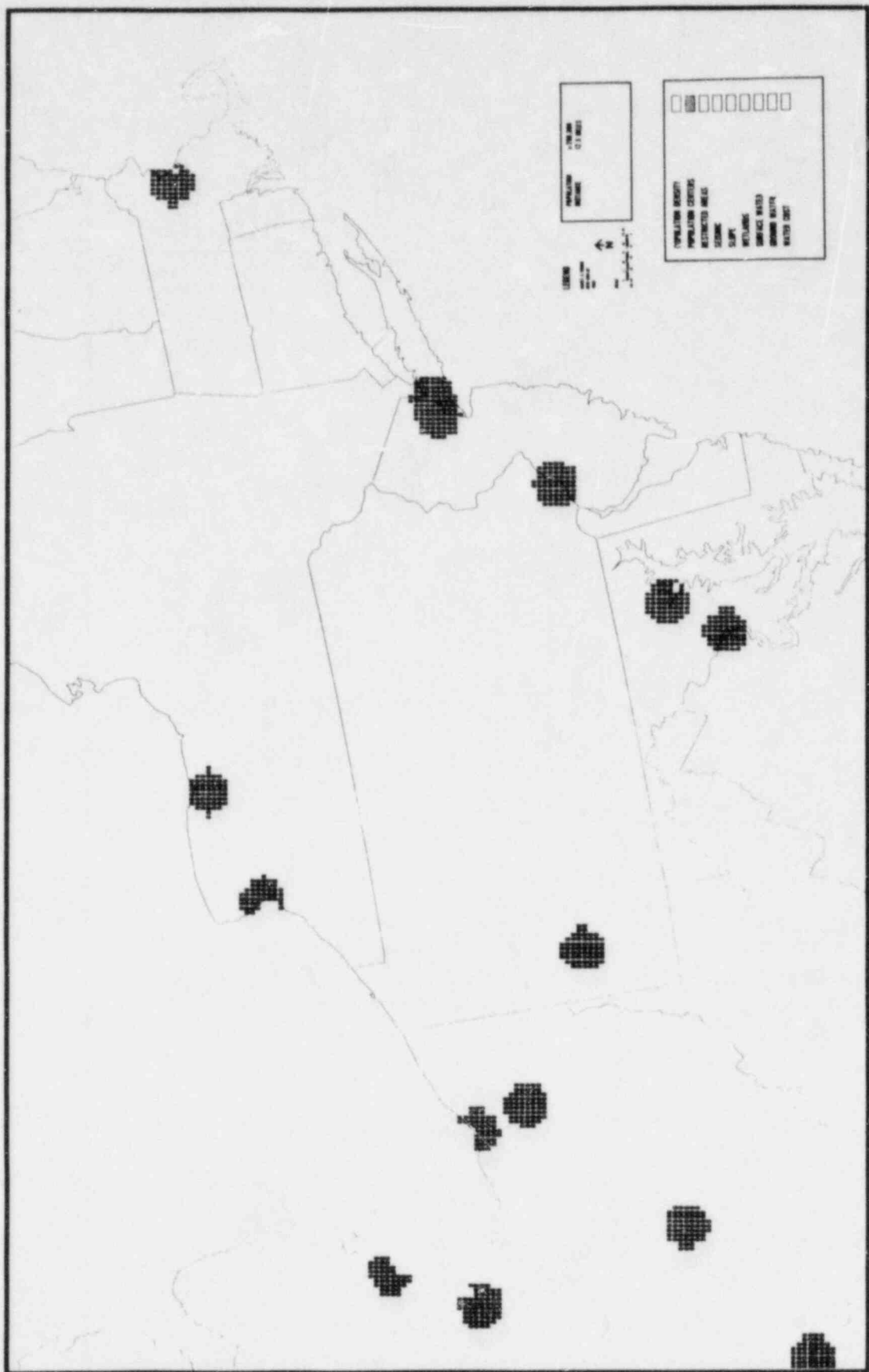


FIGURE F8.11

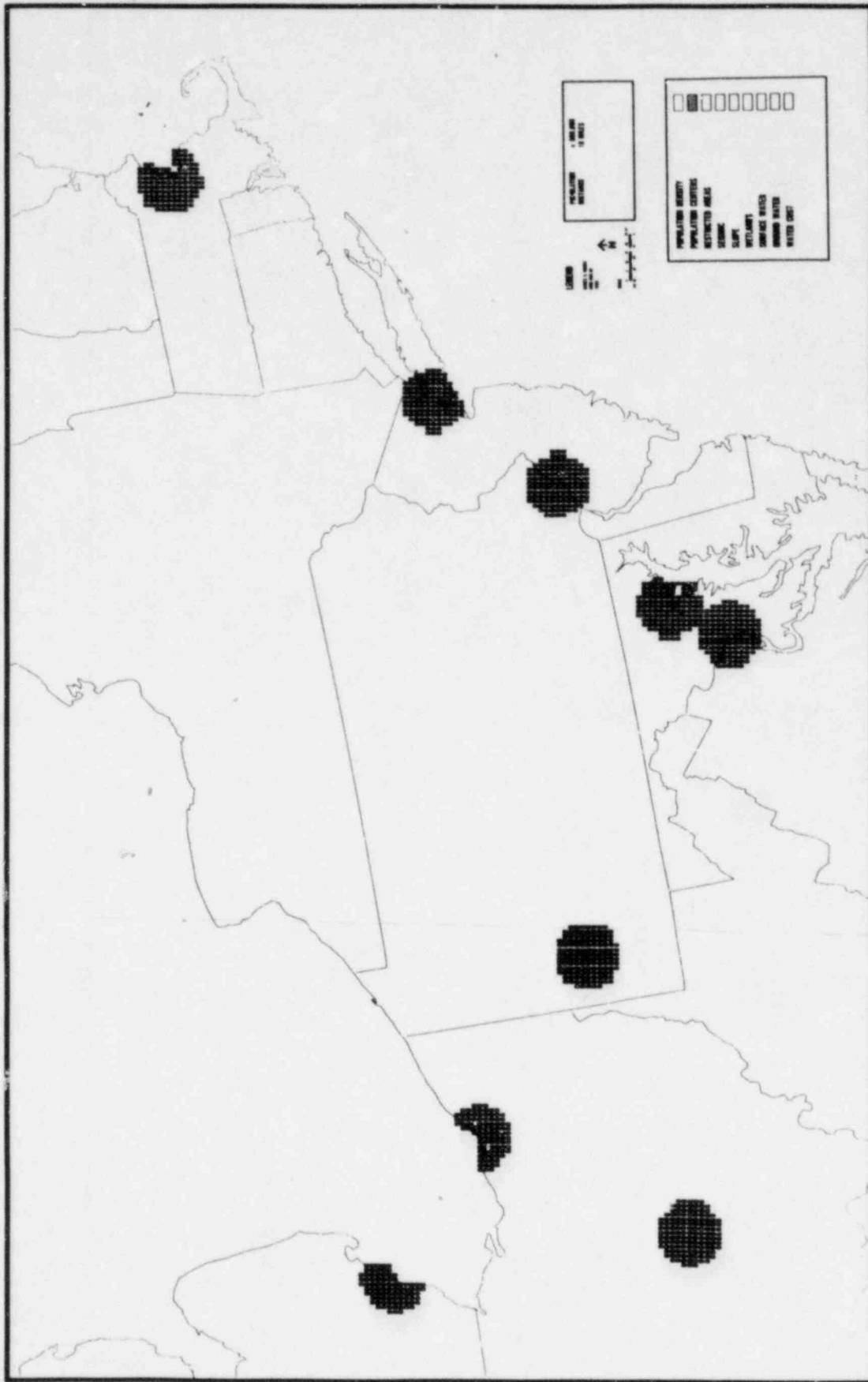


FIGURE F8.12



FIGURE F8.13

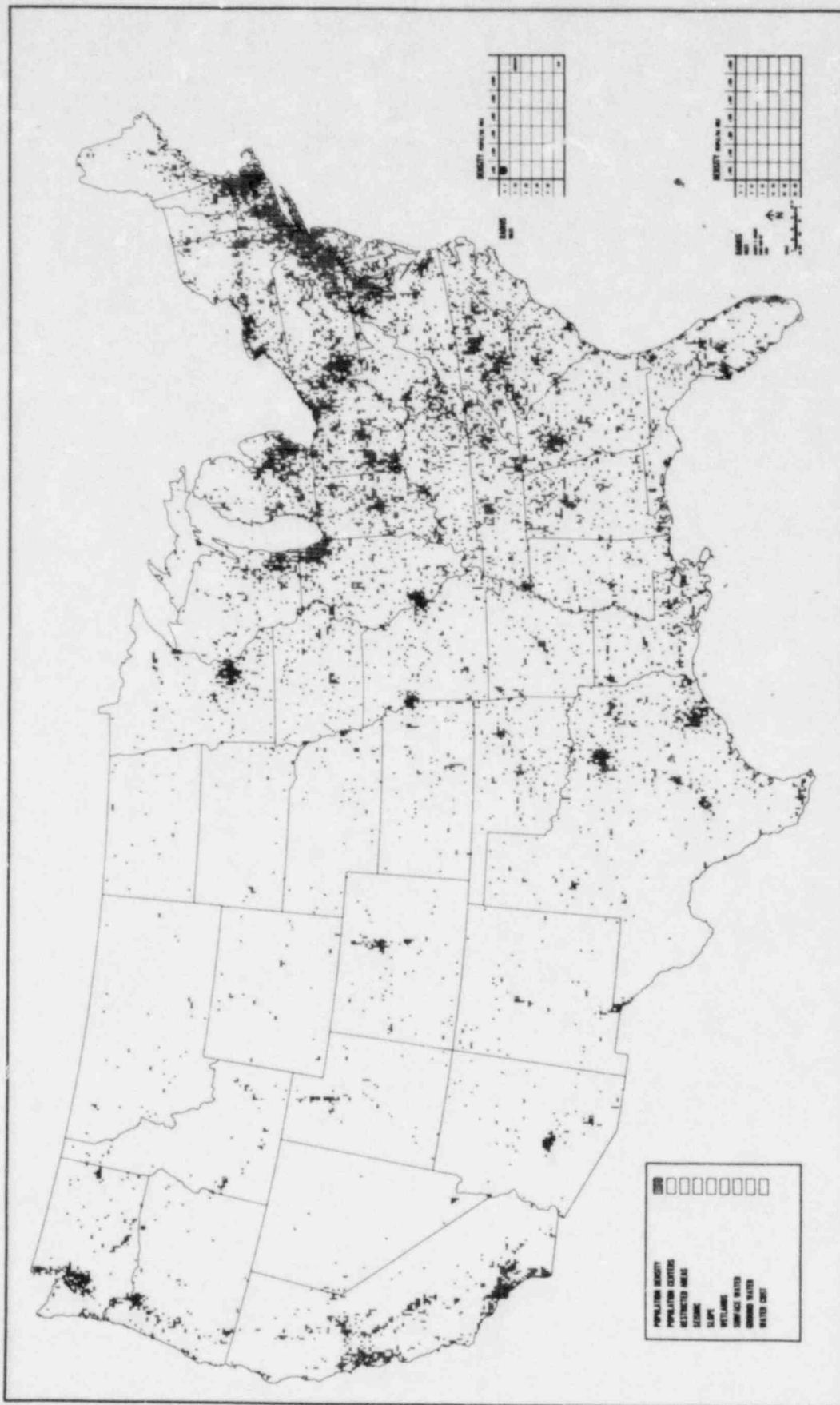


FIGURE F9.1

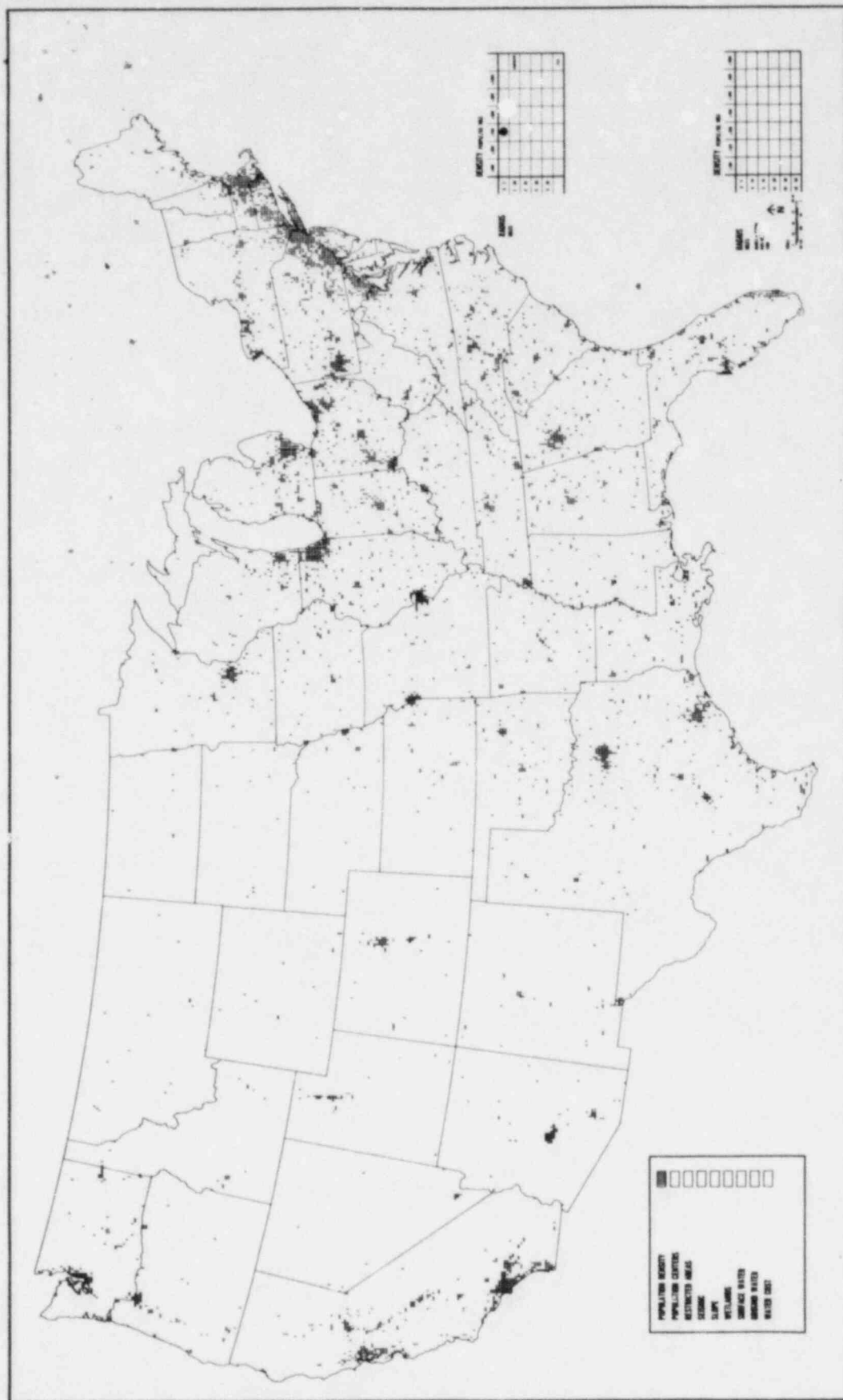


FIGURE F9.2

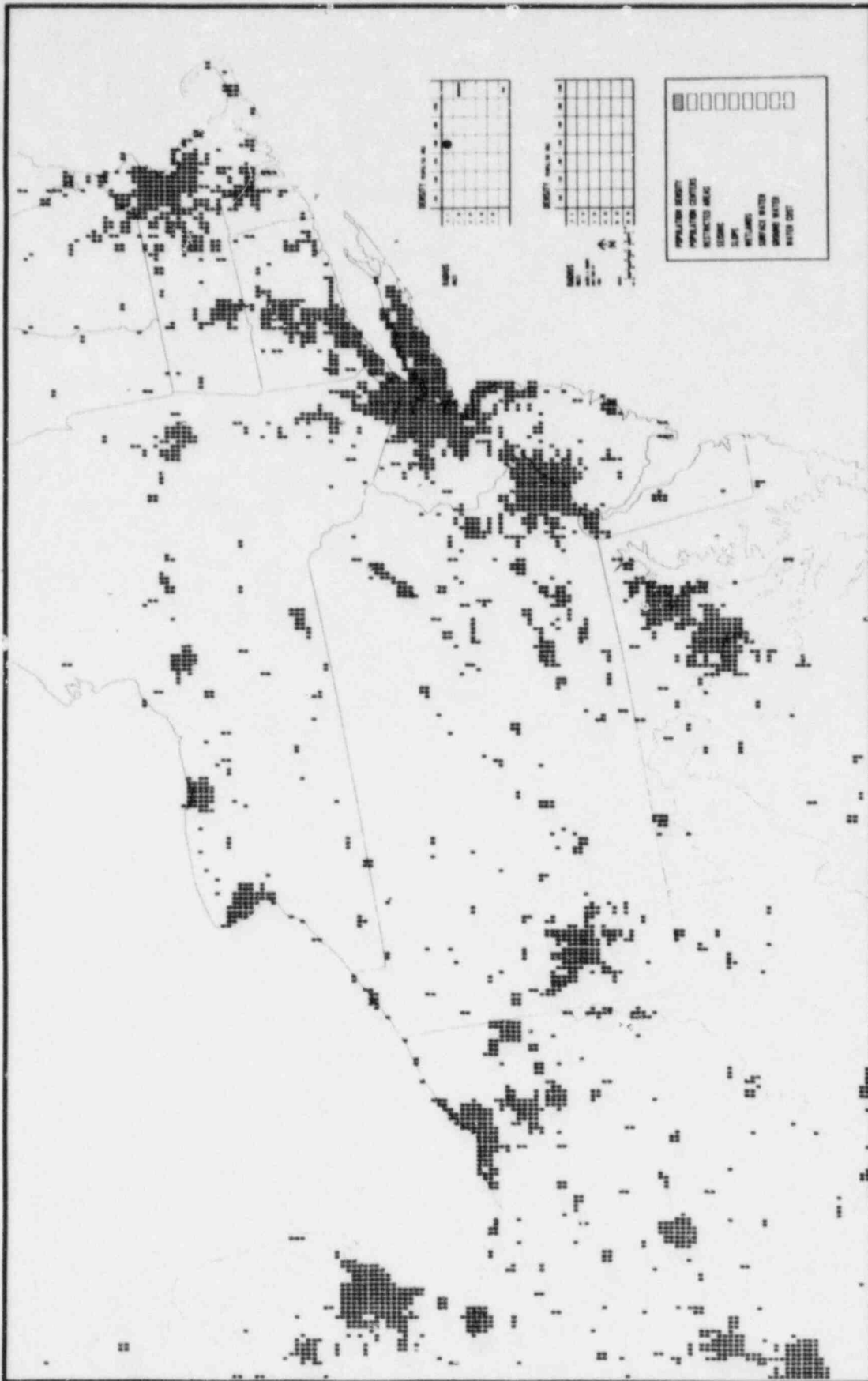


FIGURE F9.3

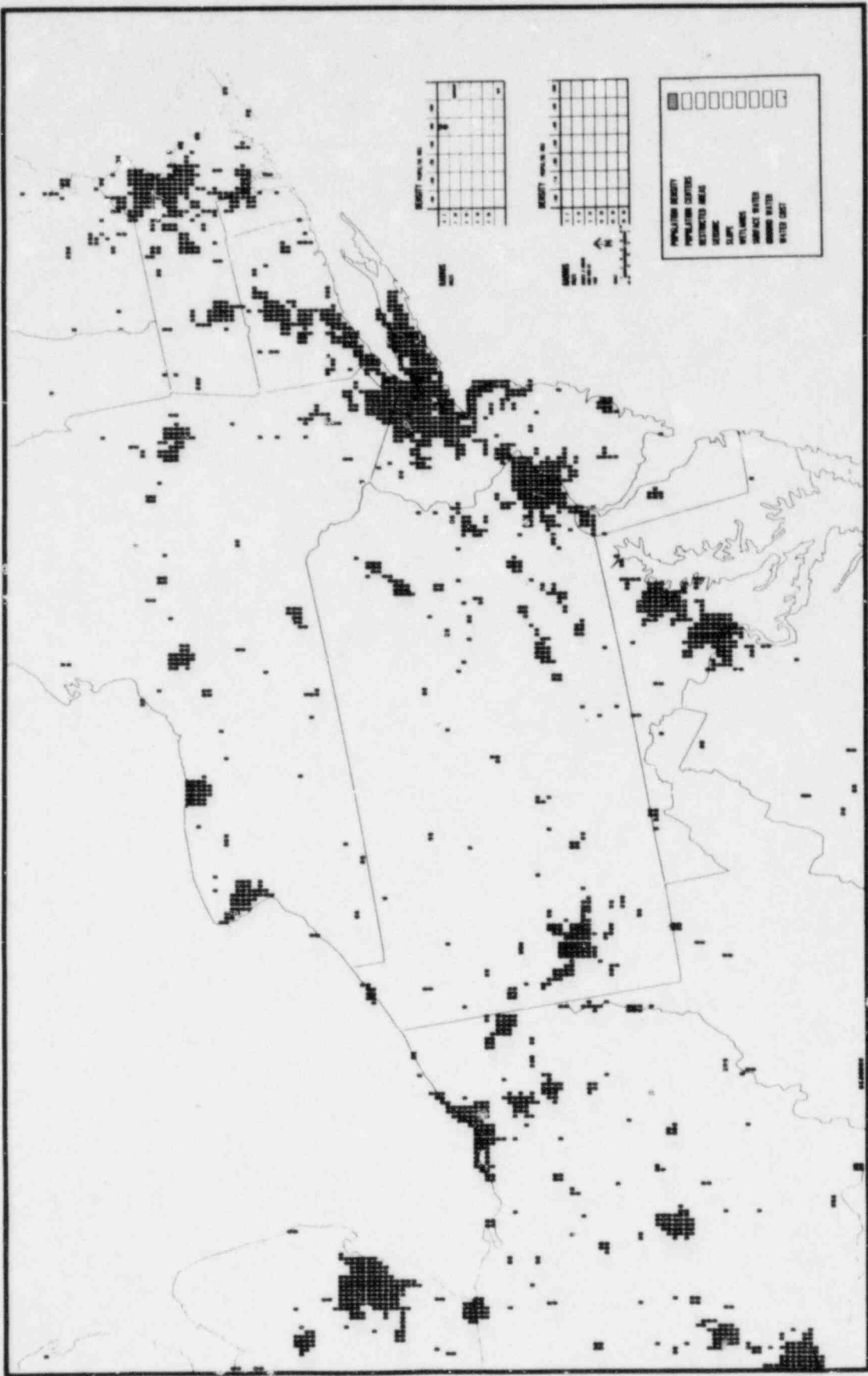


FIGURE F9.4

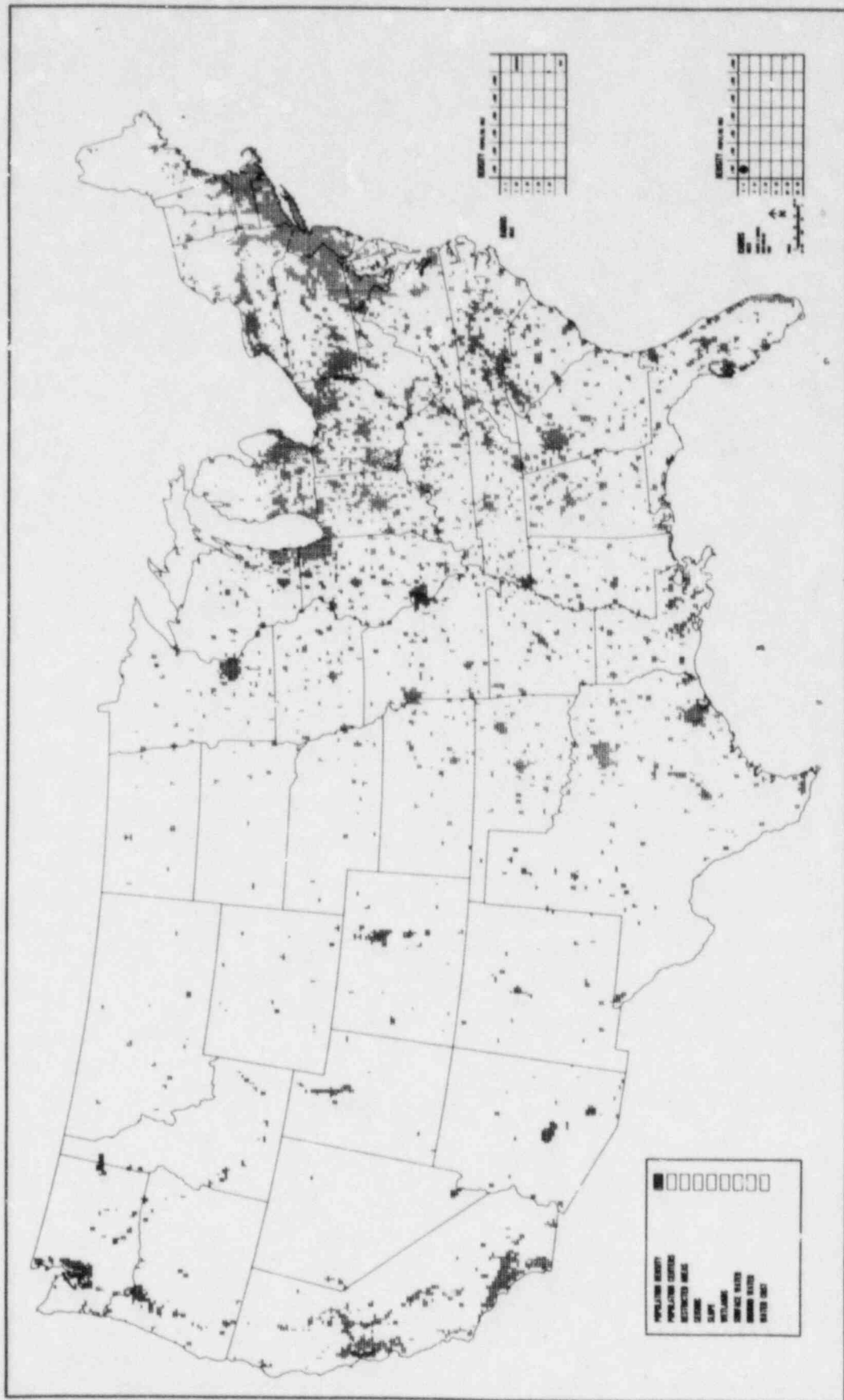


FIGURE F9.5

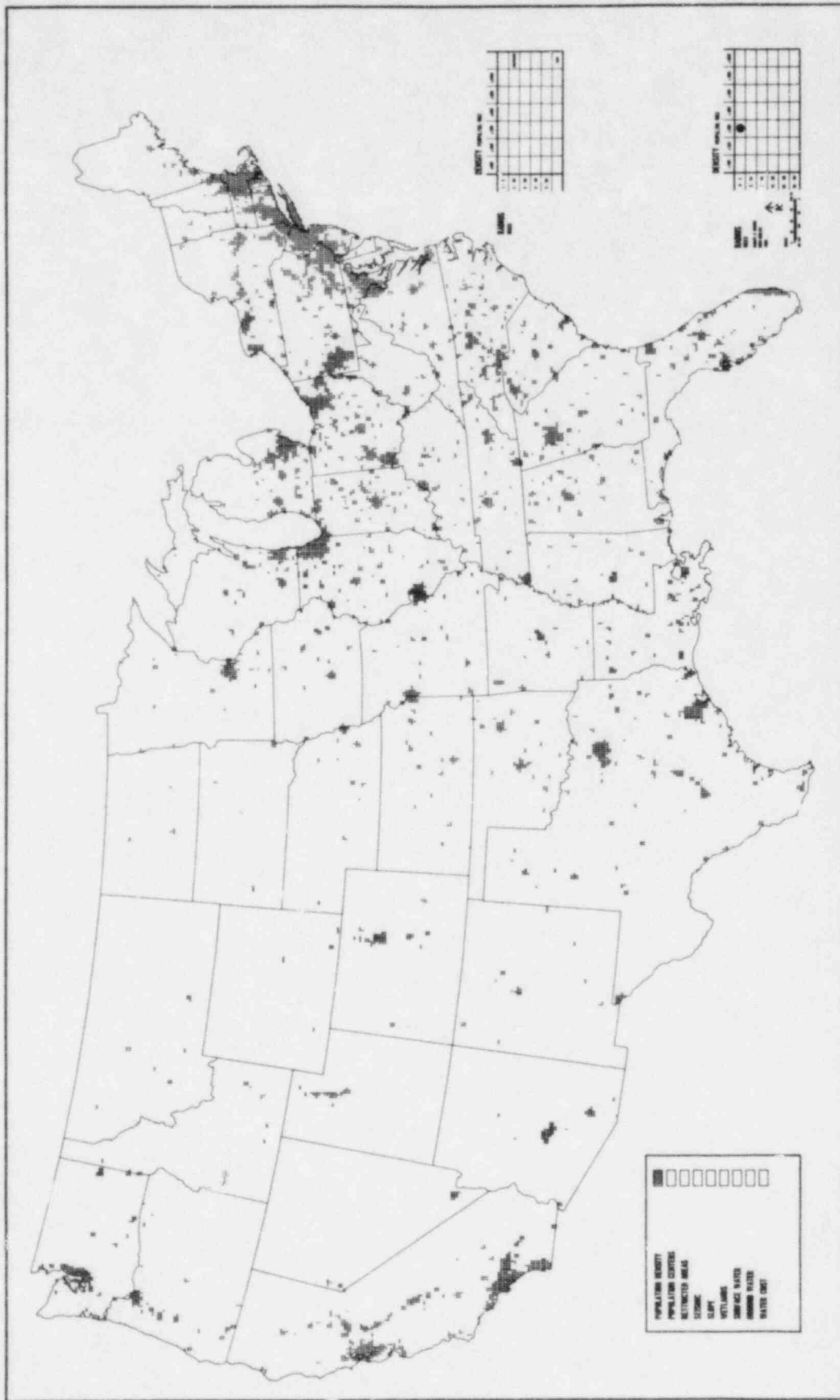


FIGURE F9.6

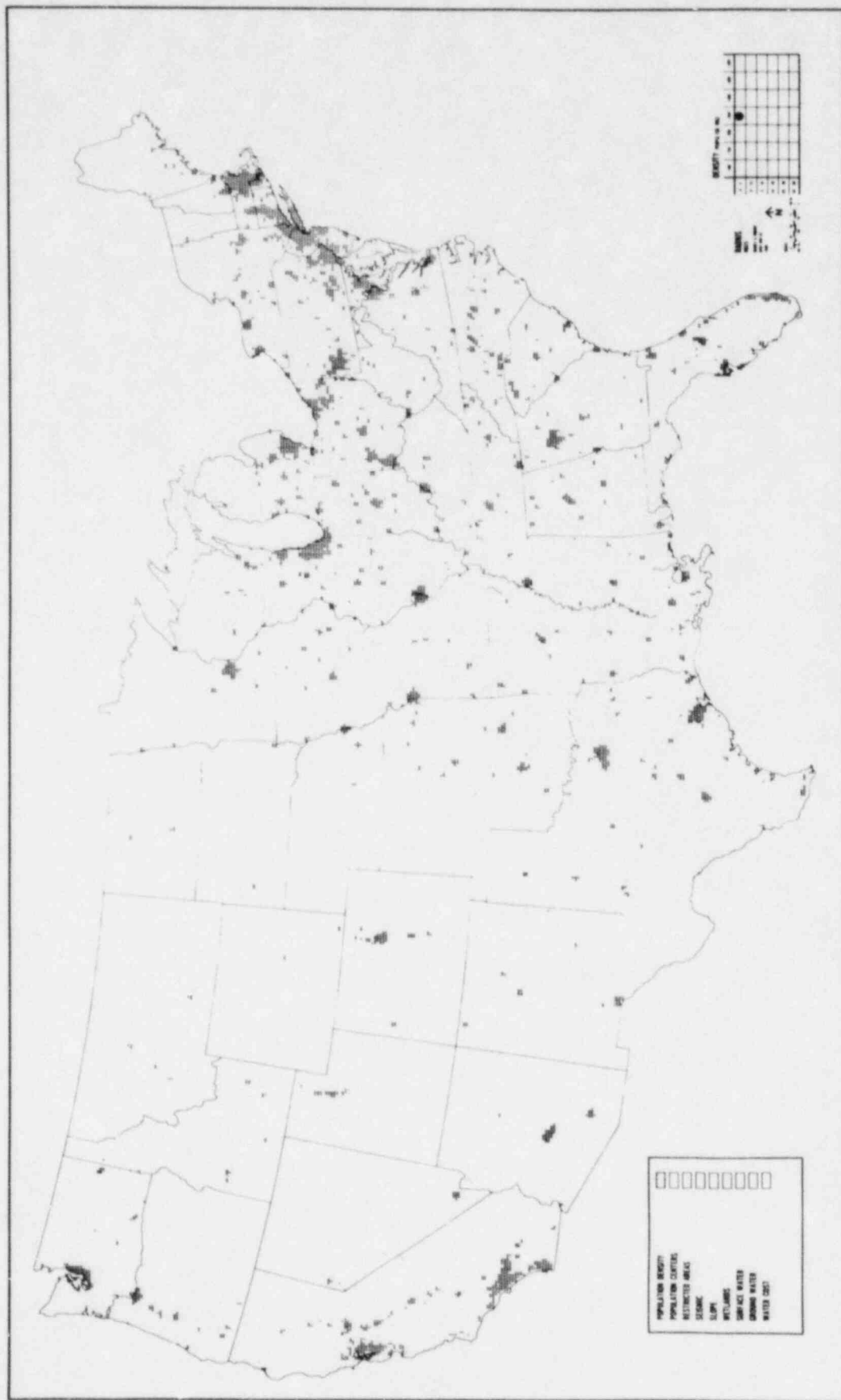


FIGURE F9.7

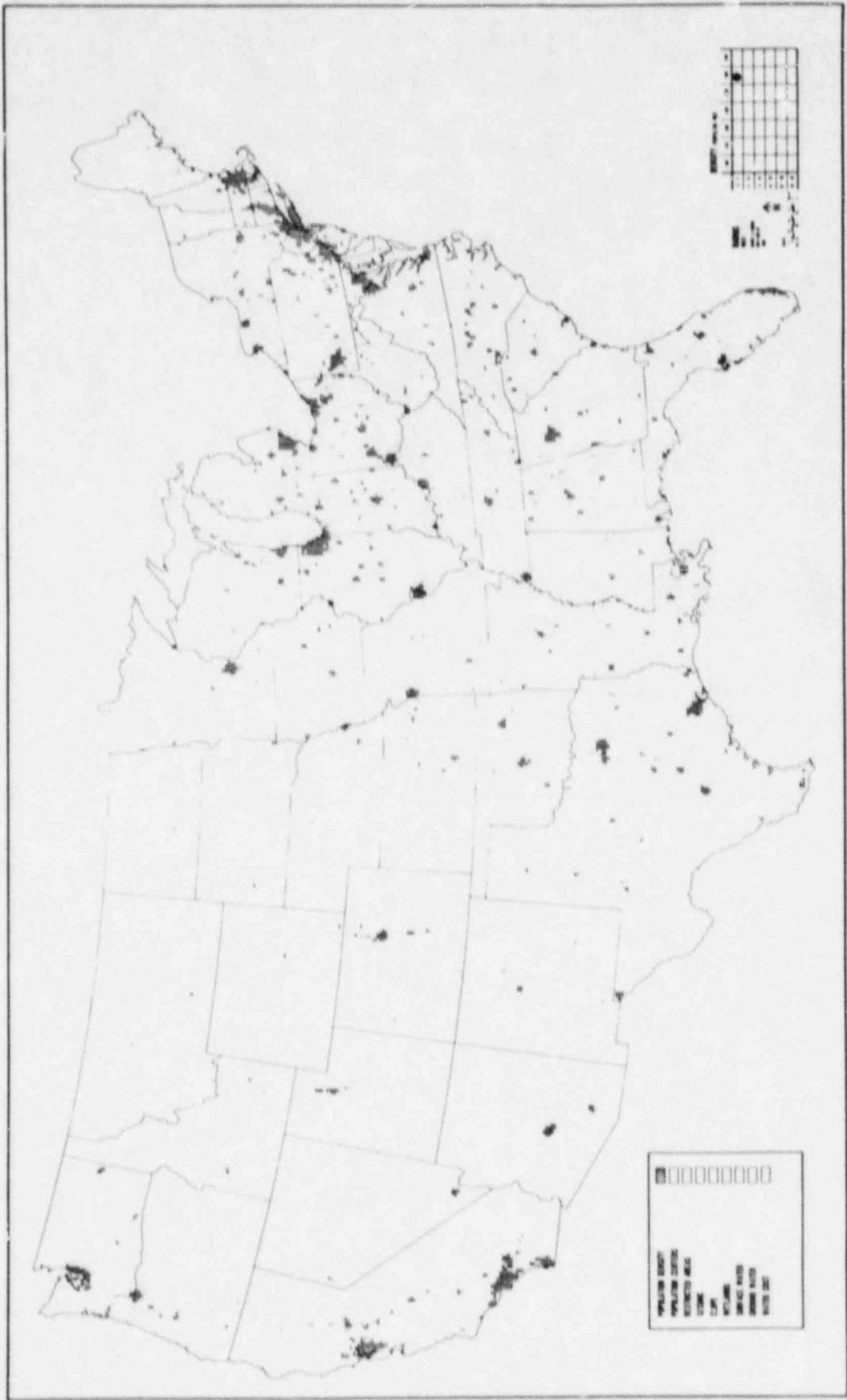


FIGURE F9.8

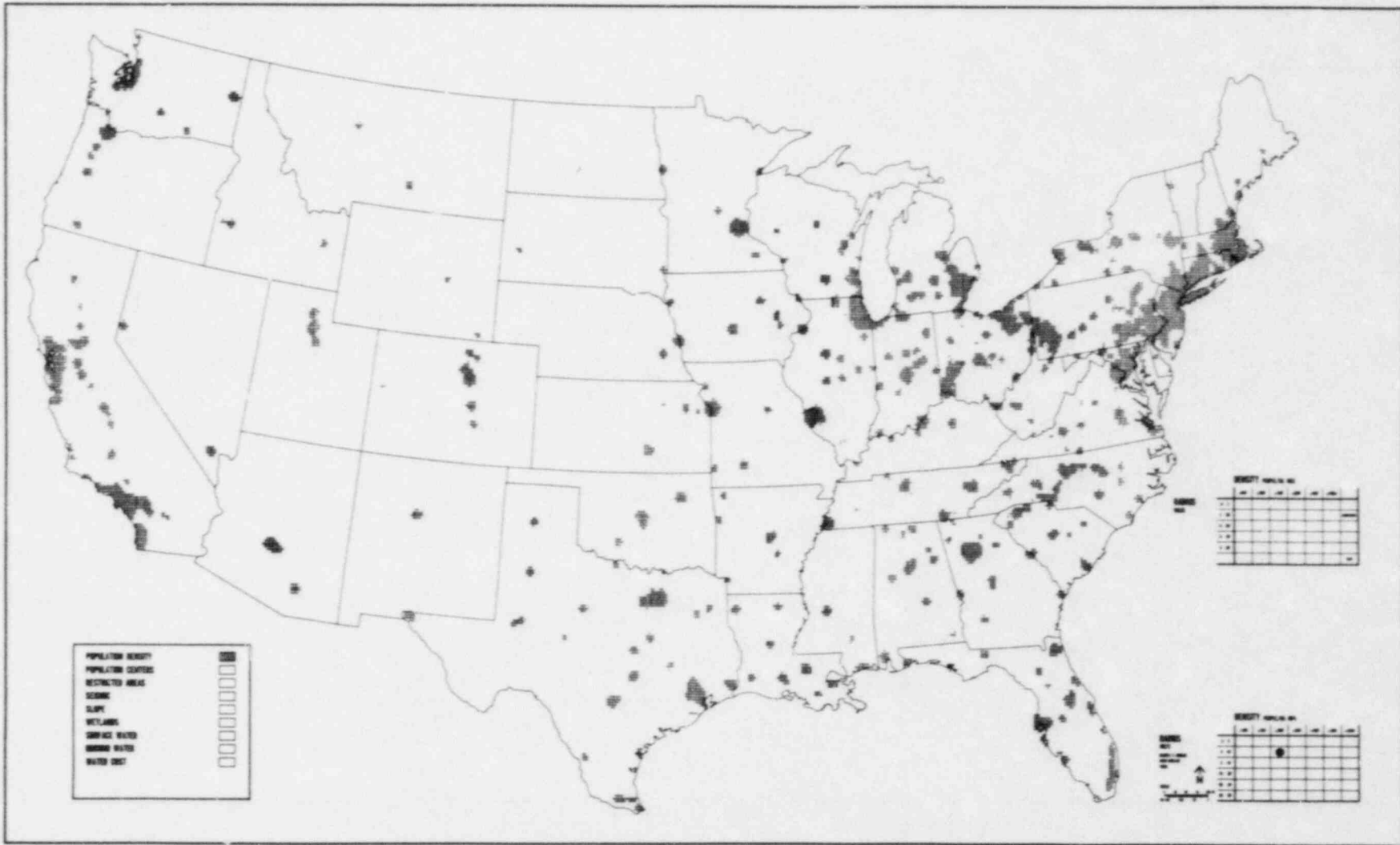


FIGURE F9.10

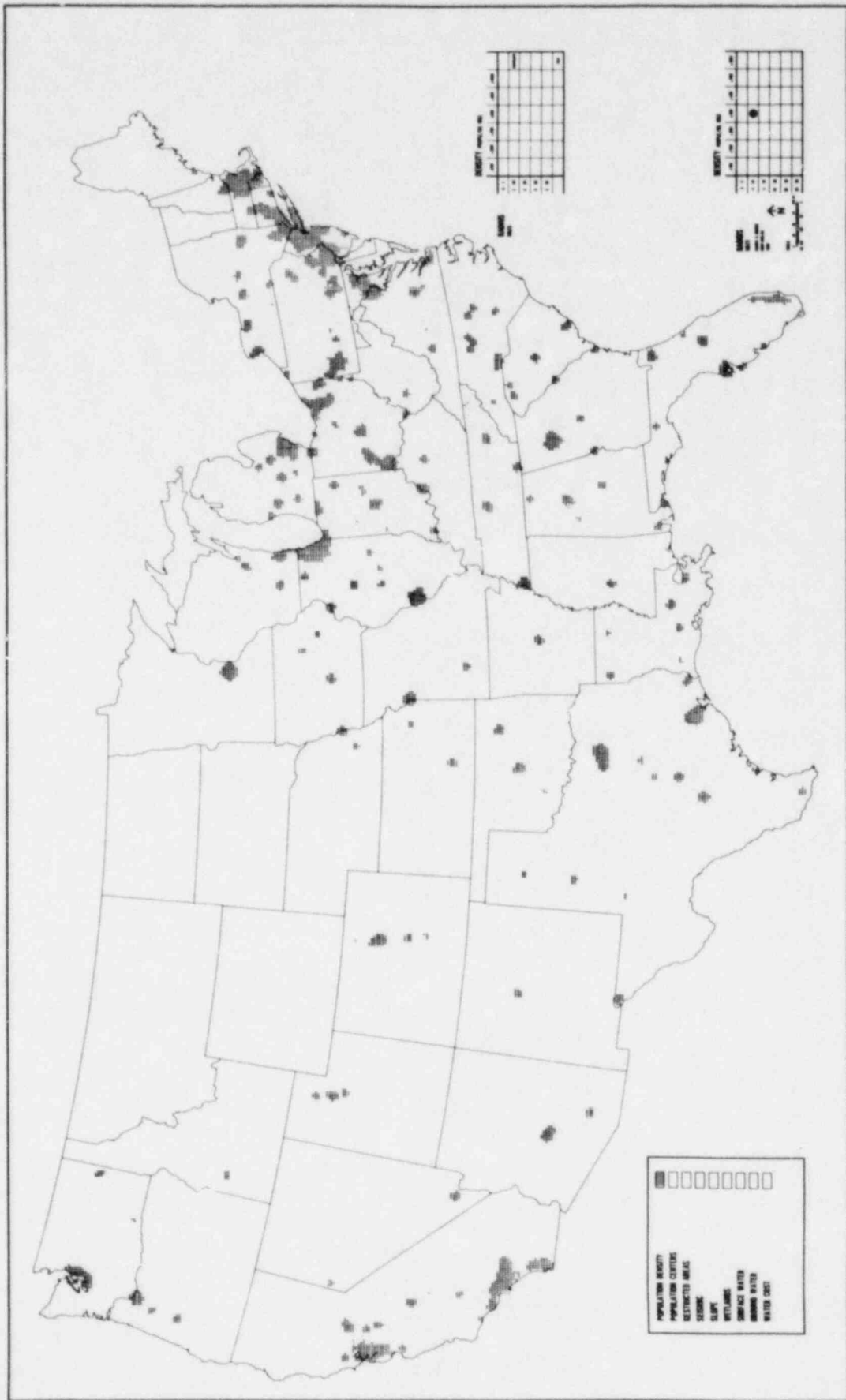


FIGURE F9.11

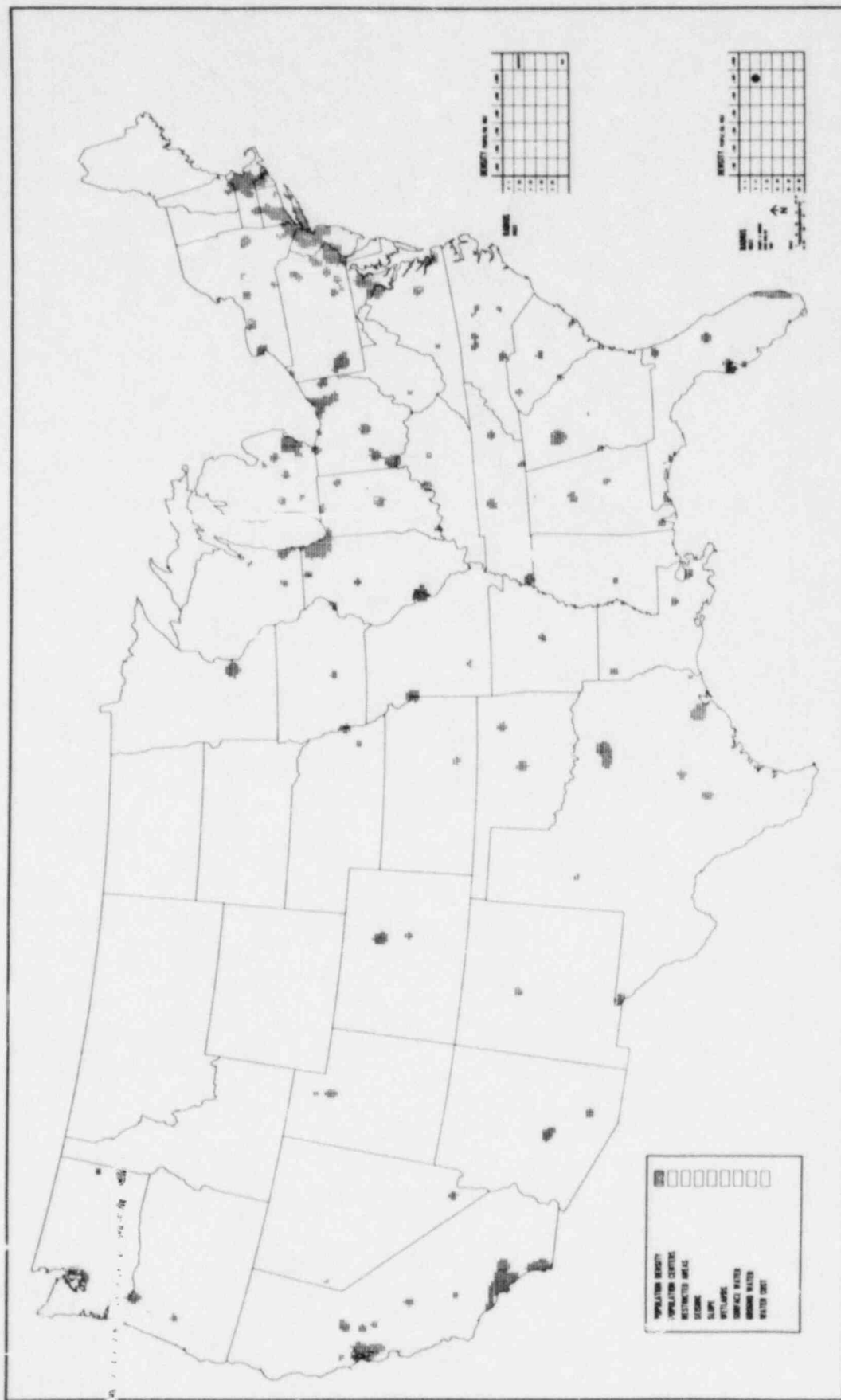


FIGURE F9.12

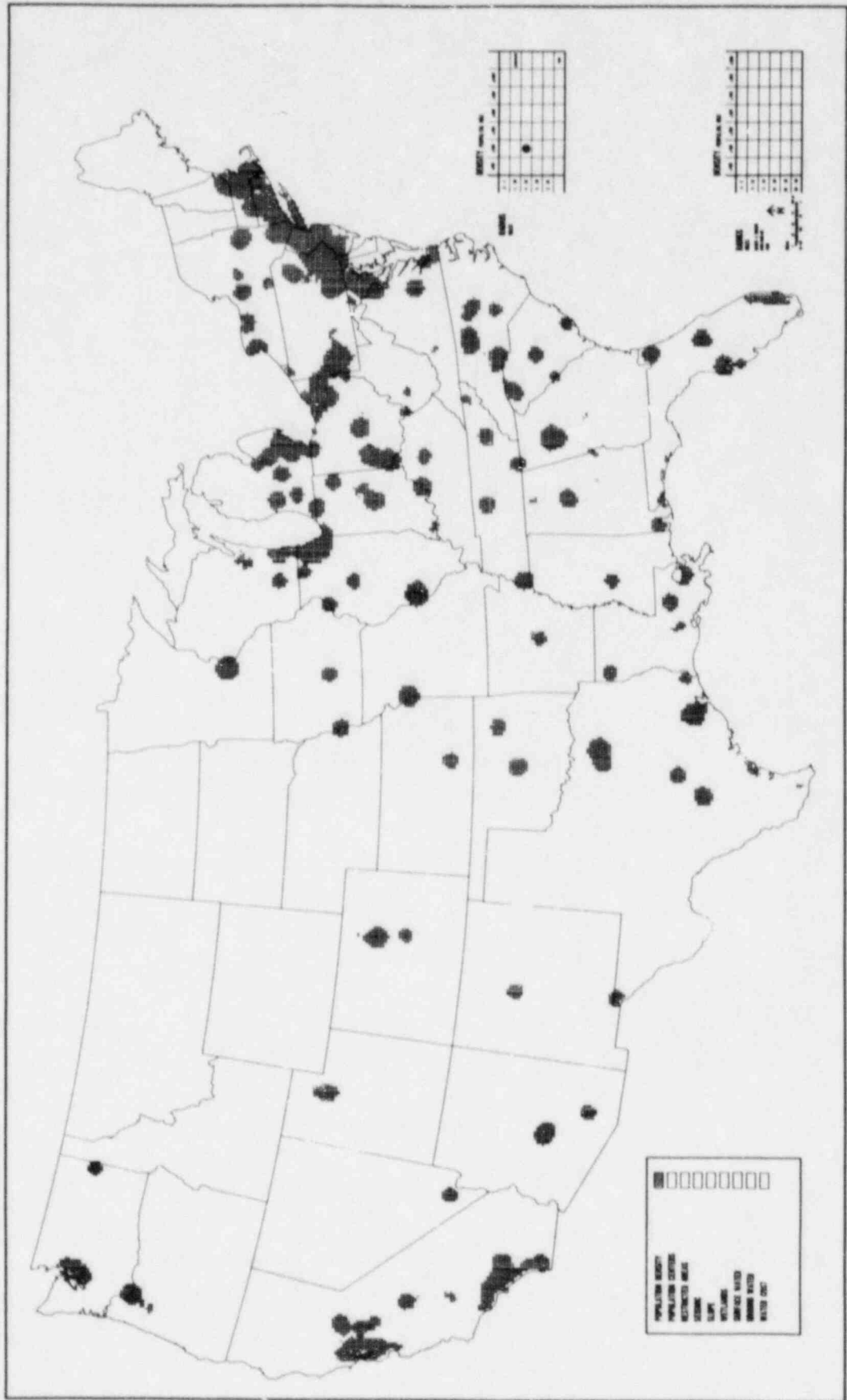


FIGURE F9.13

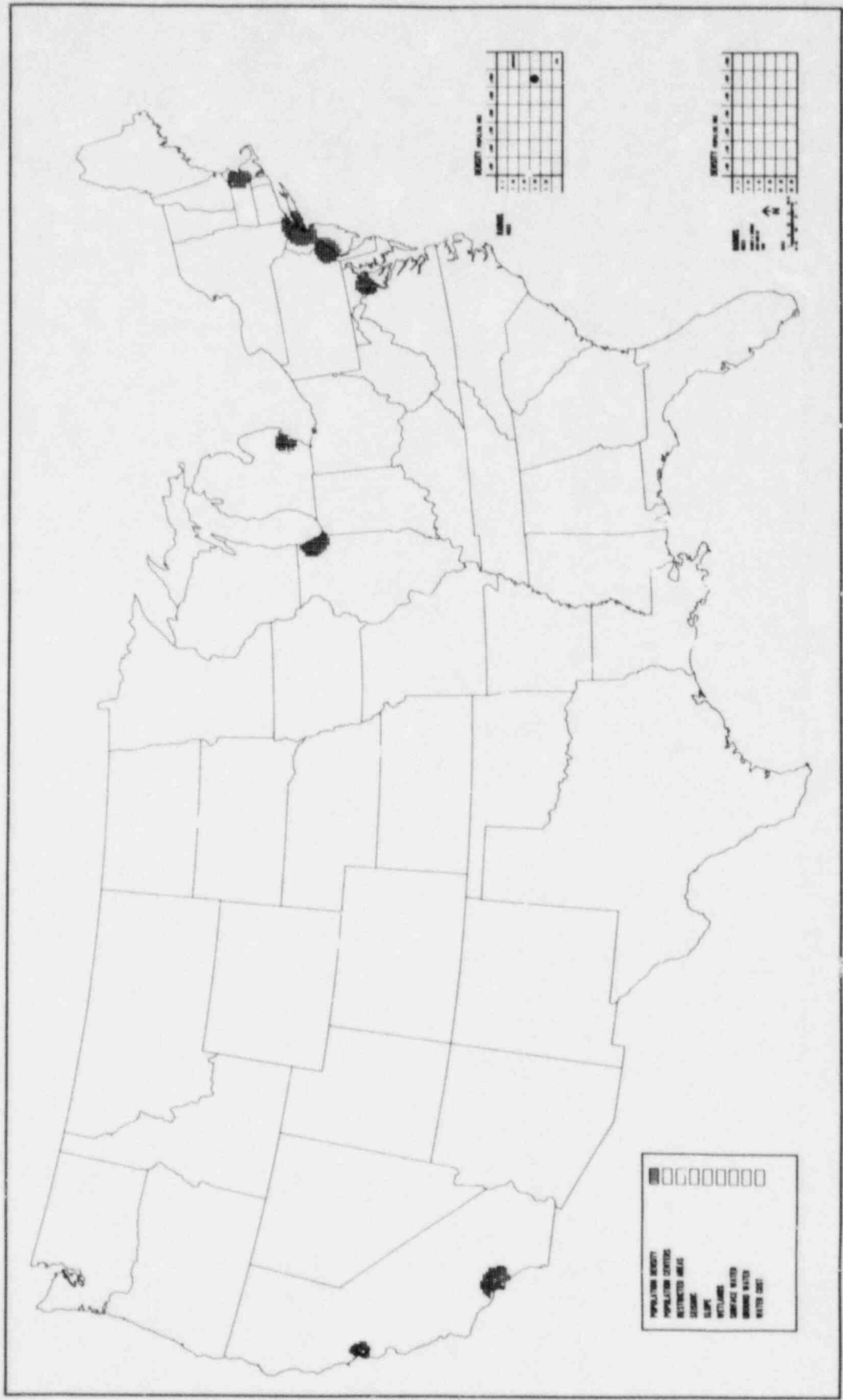


FIGURE F9.15

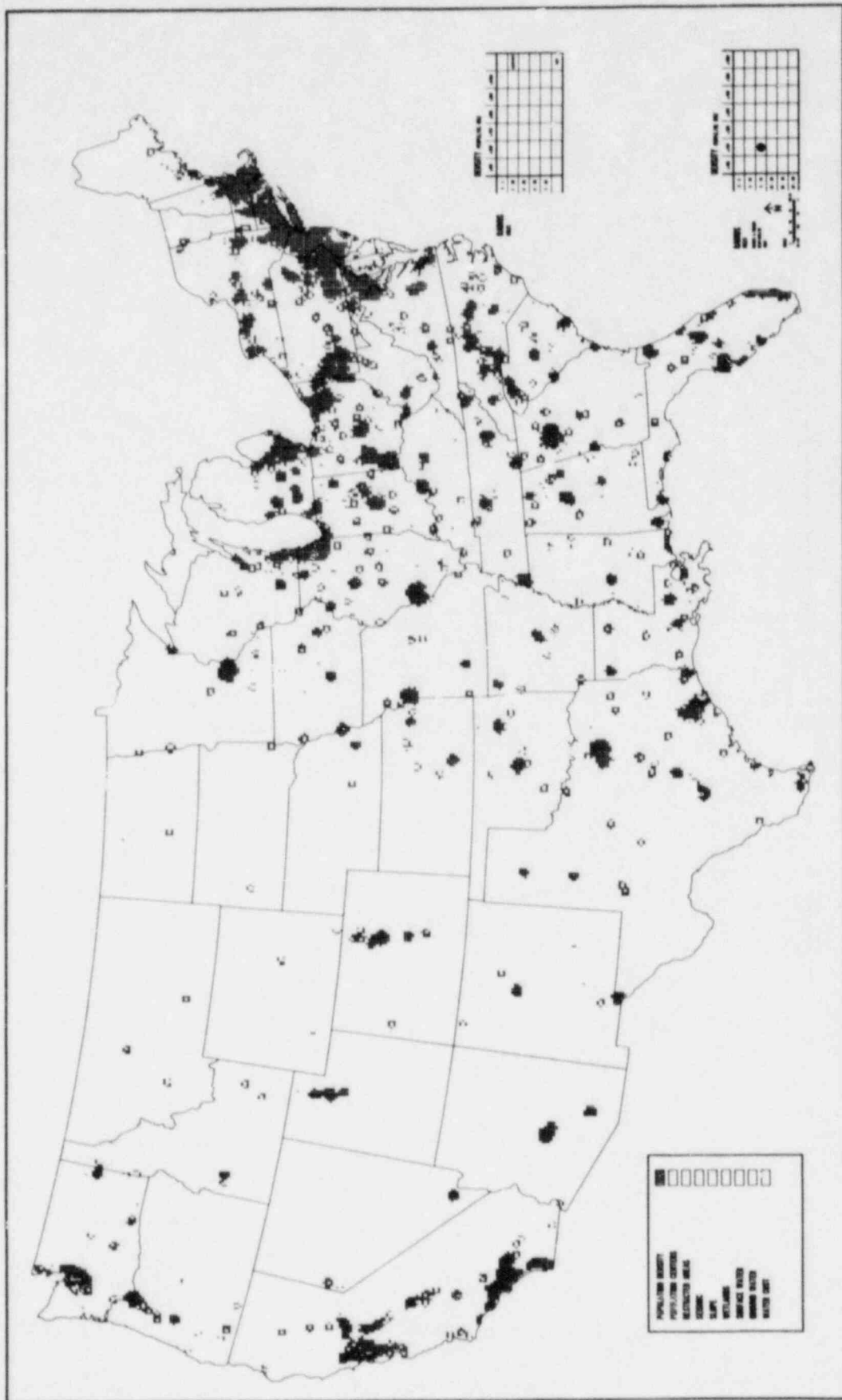


FIGURE F9.16

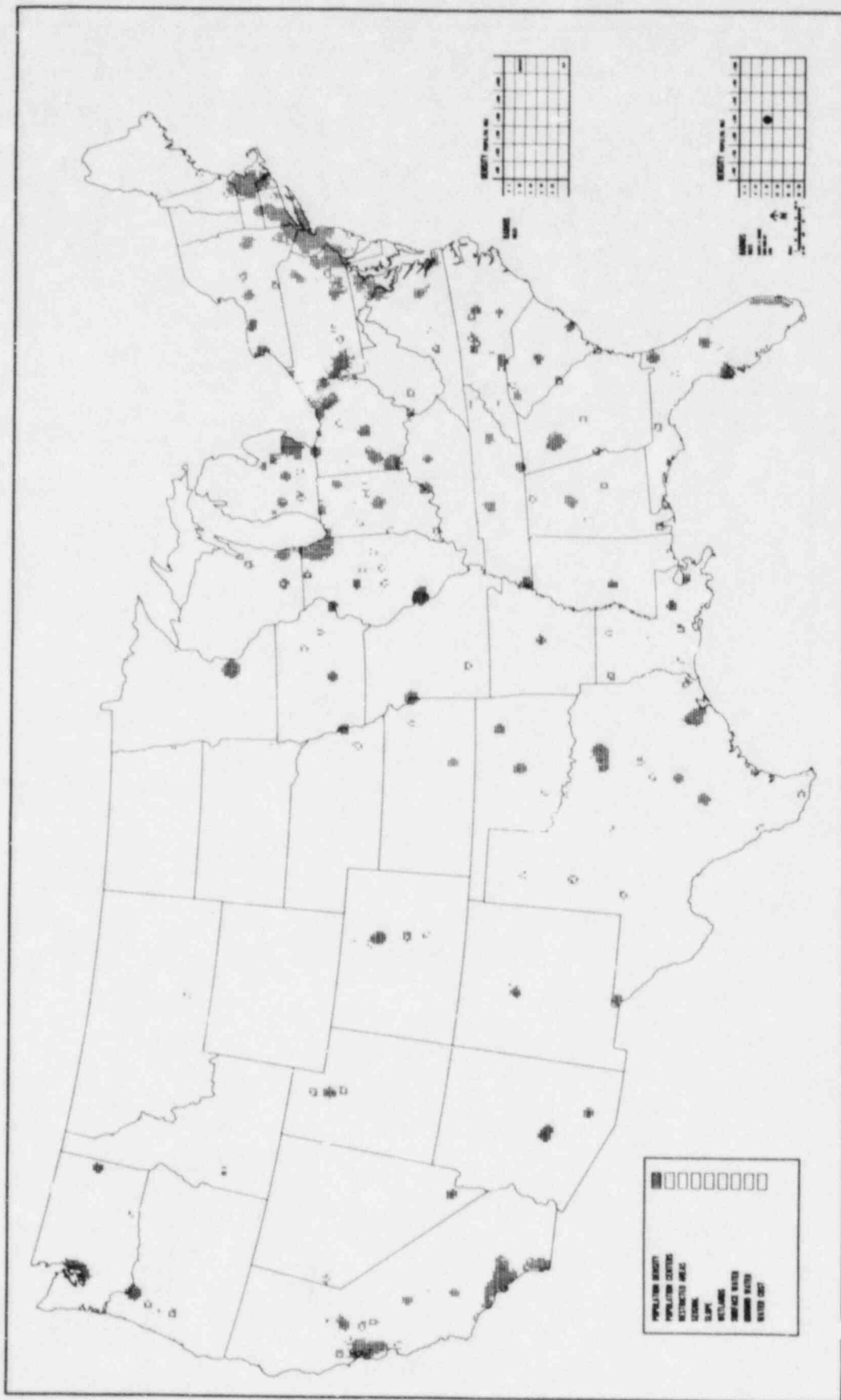


FIGURE F9.17

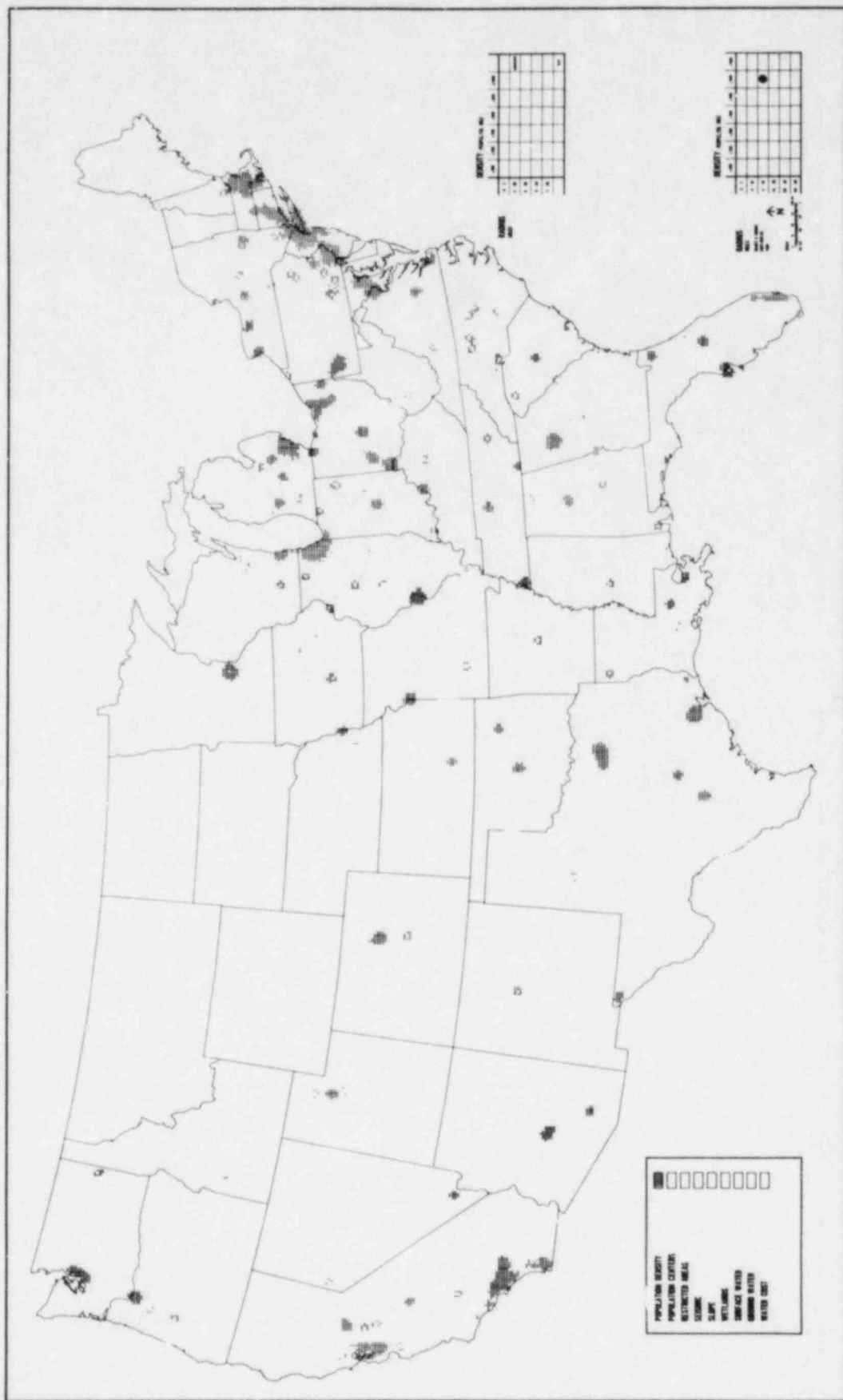


FIGURE F9.18

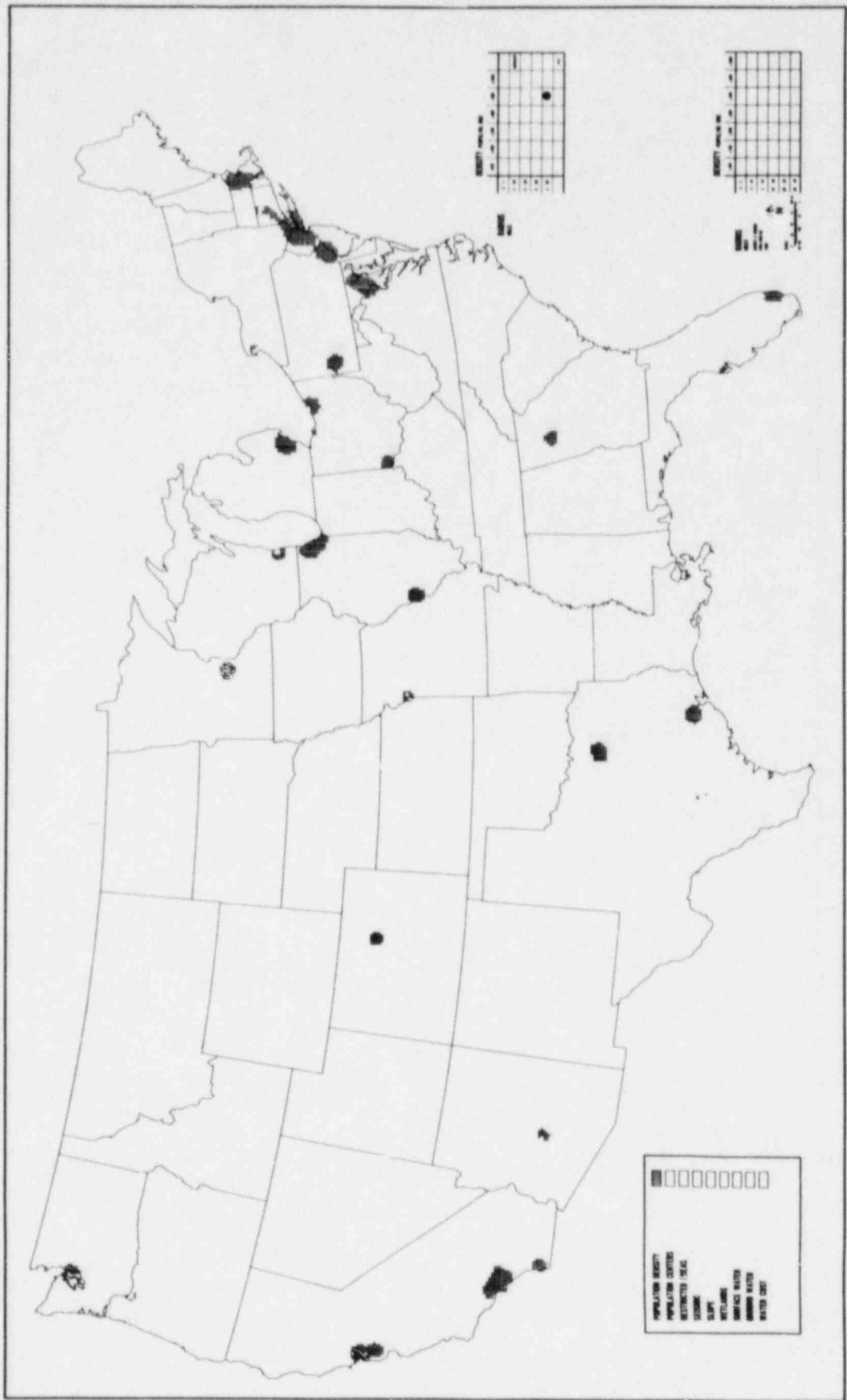


FIGURE F9.19

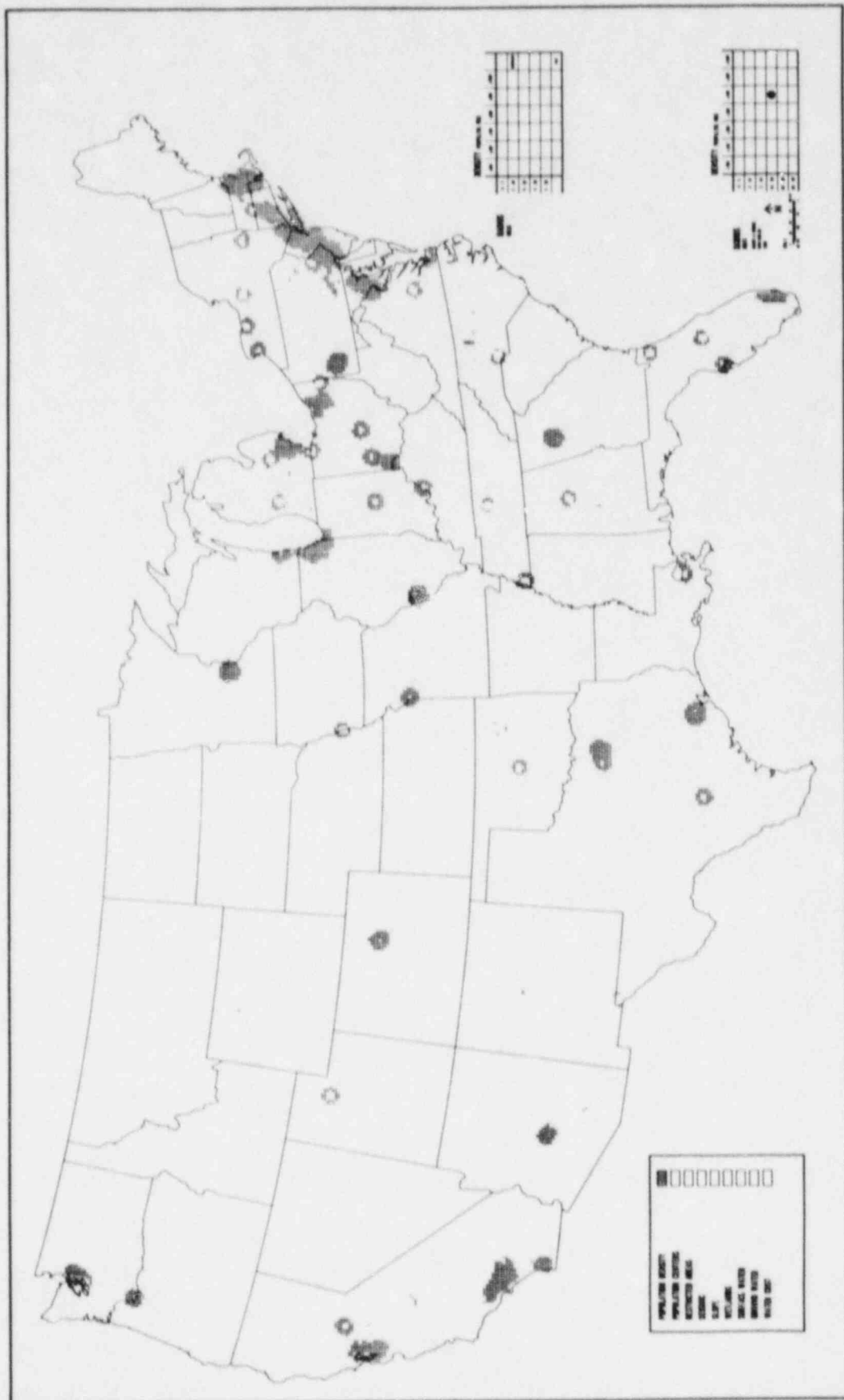


FIGURE F9.20

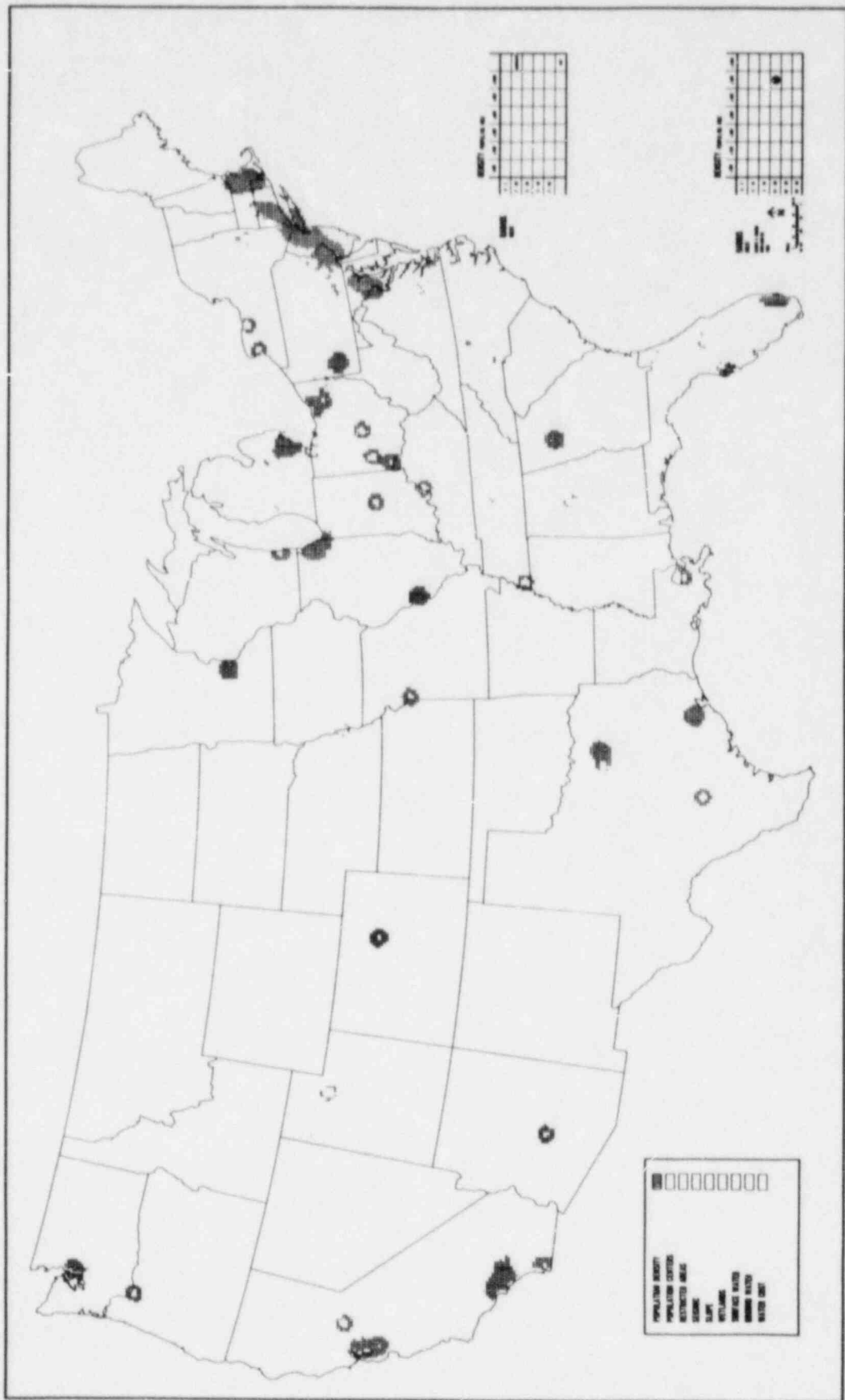


FIGURE F9.21

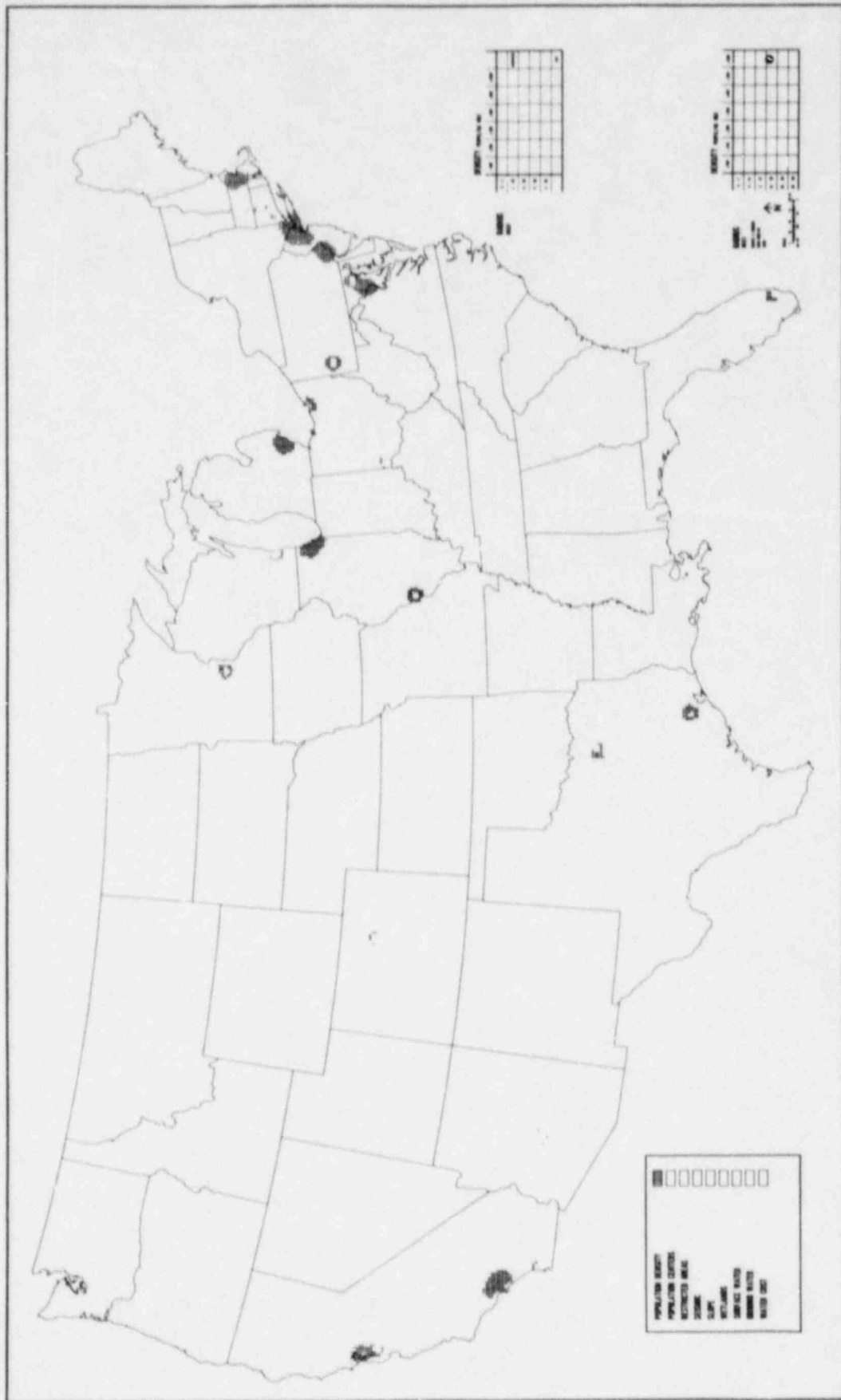


FIGURE F9.22

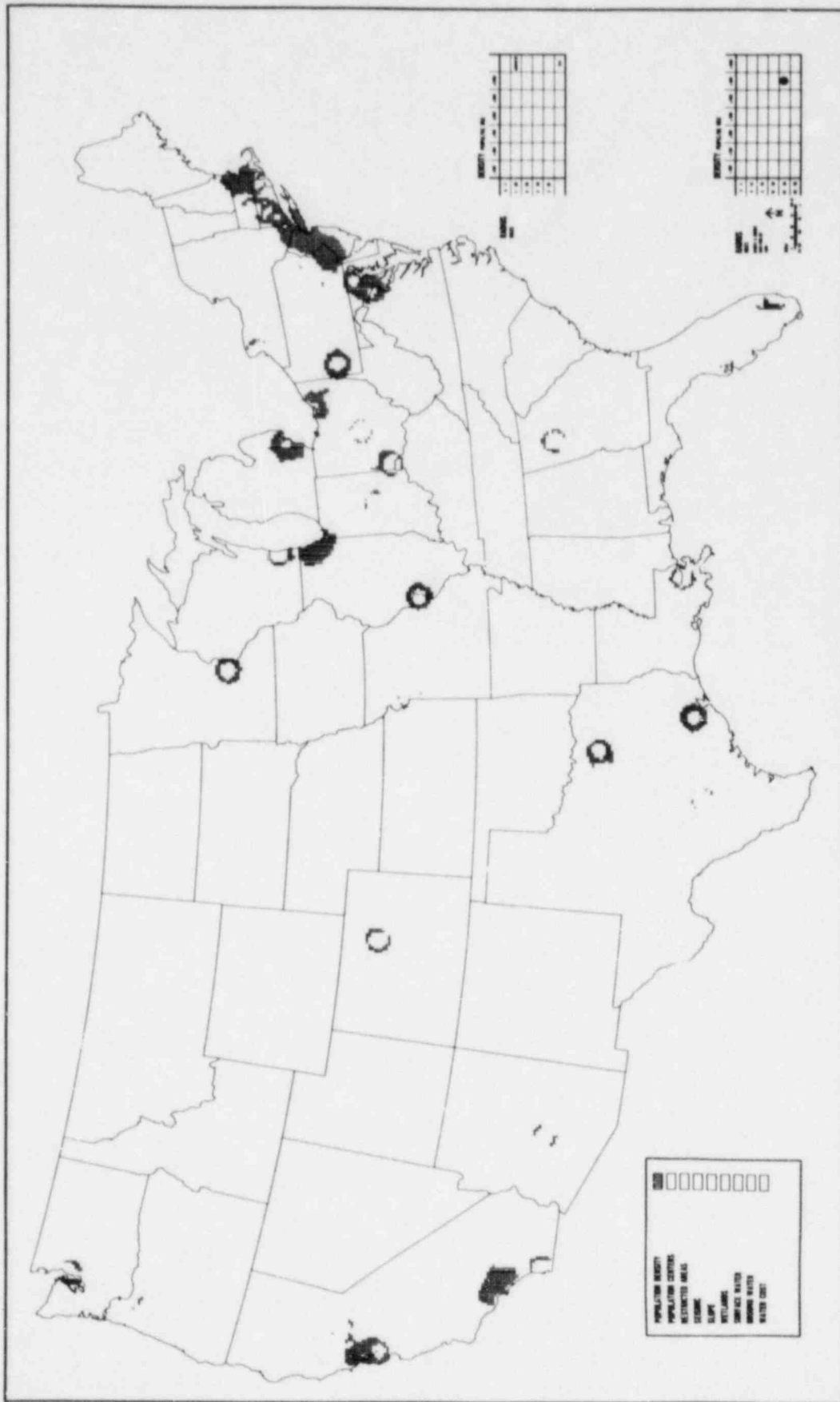


FIGURE F9.23

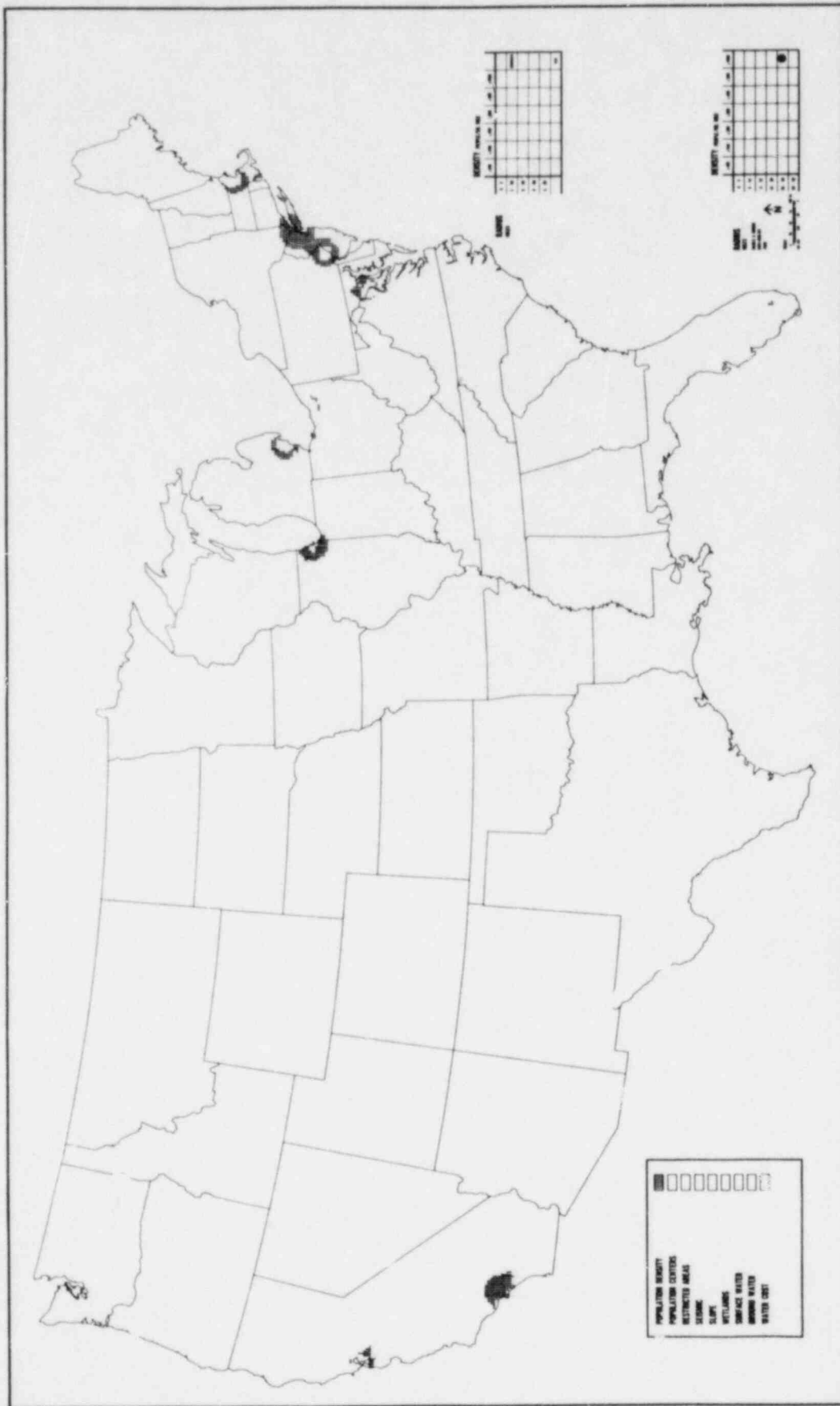


FIGURE F9.24

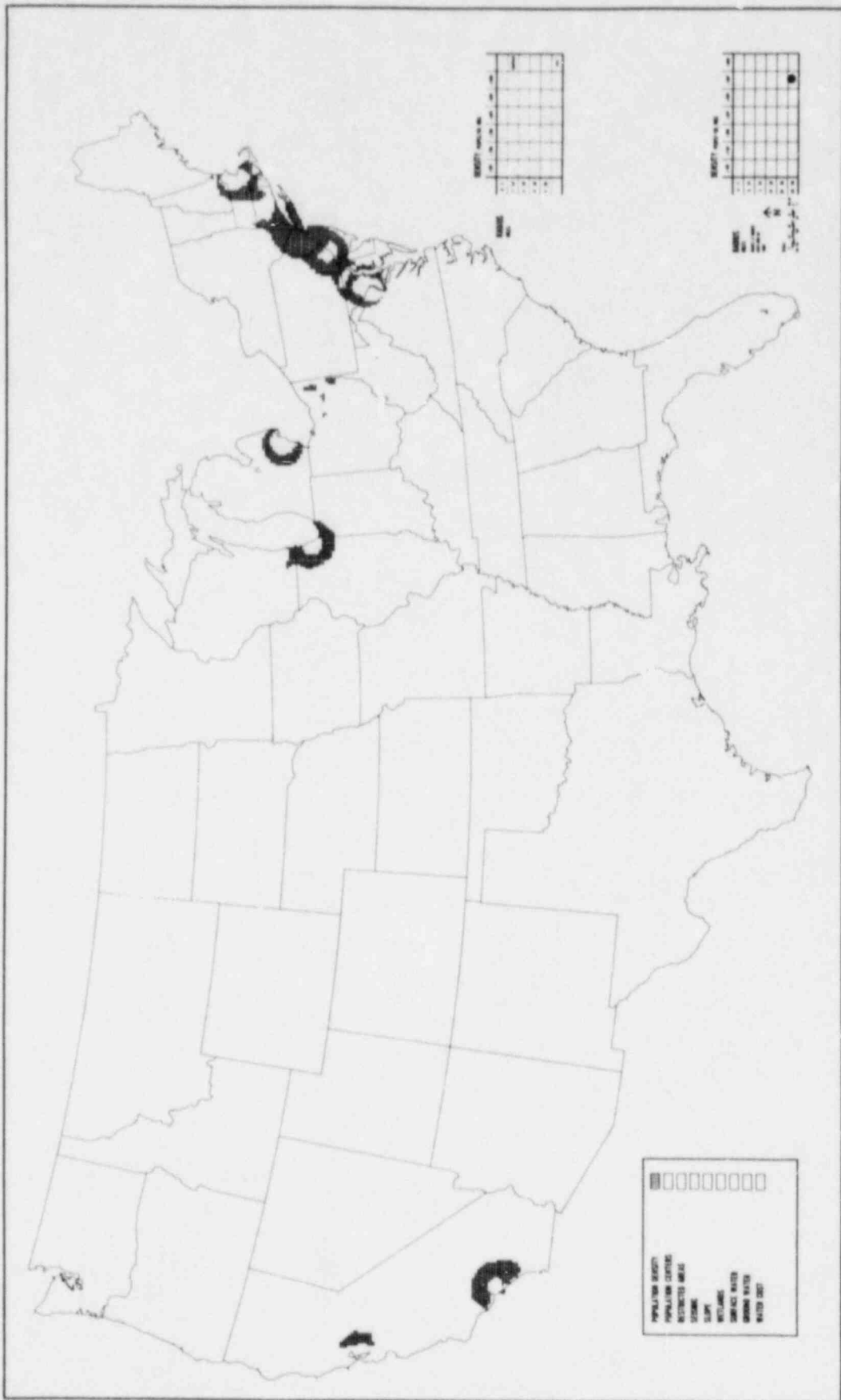


FIGURE F9.25

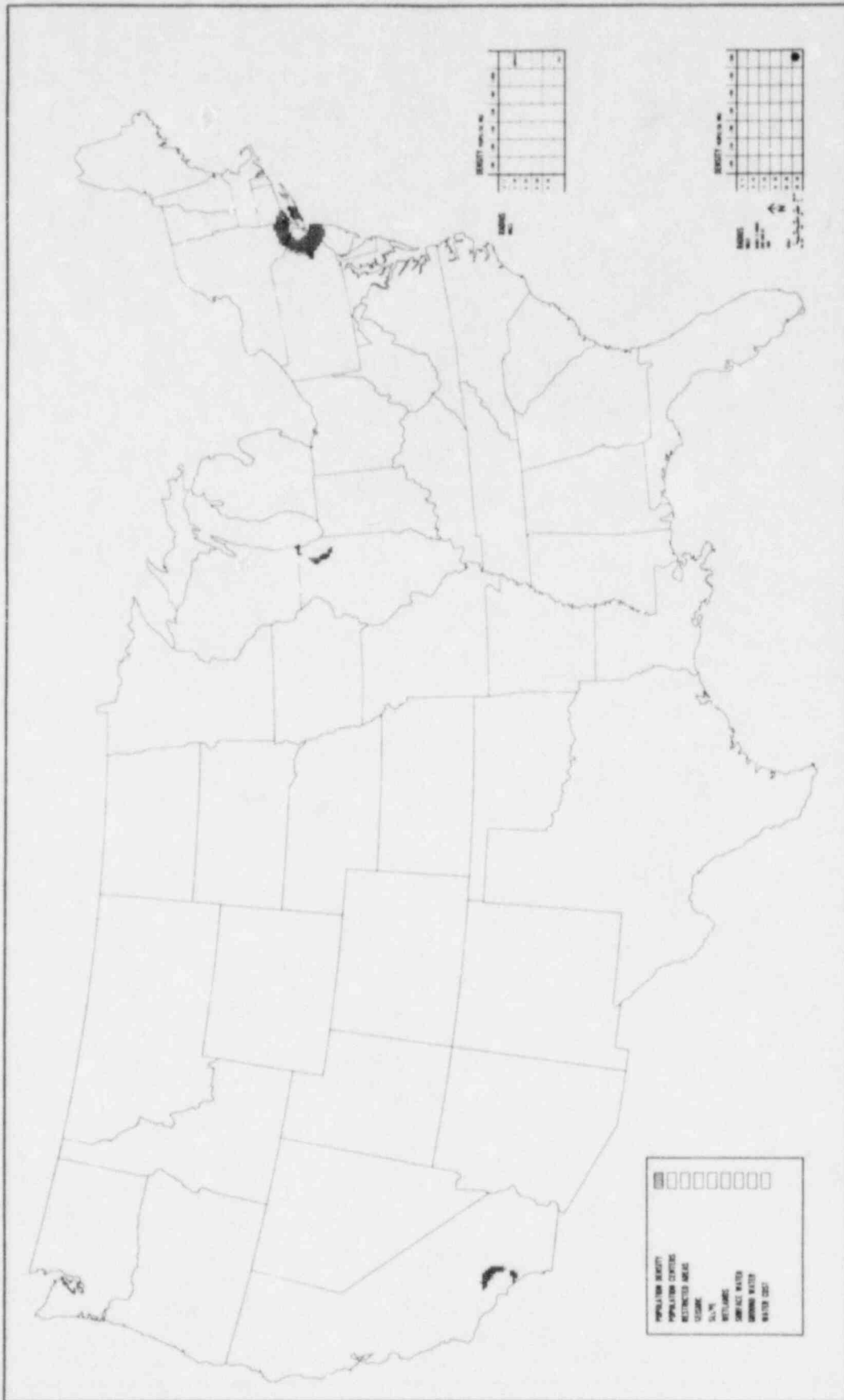


FIGURE F9.26

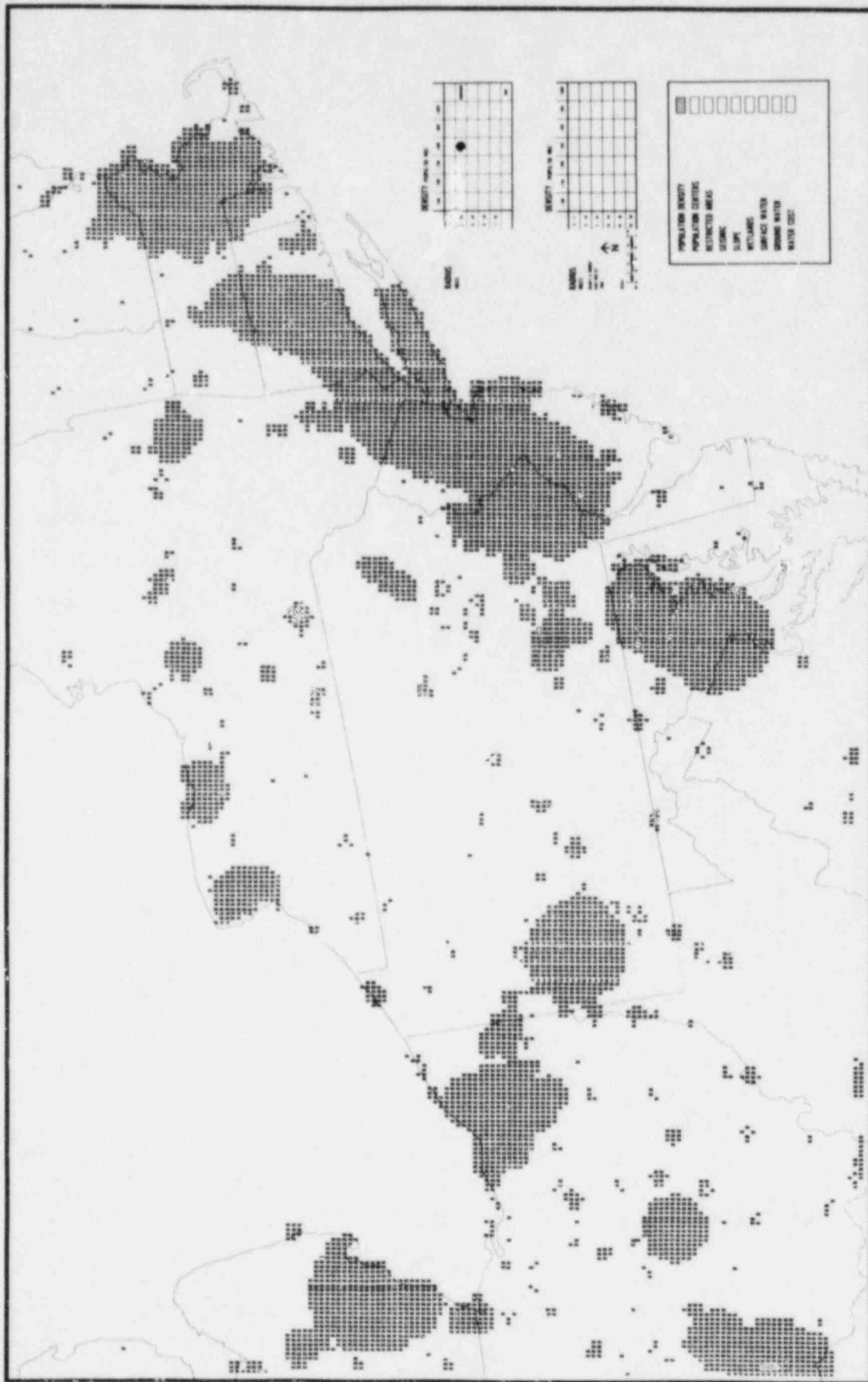


FIGURE F10.1

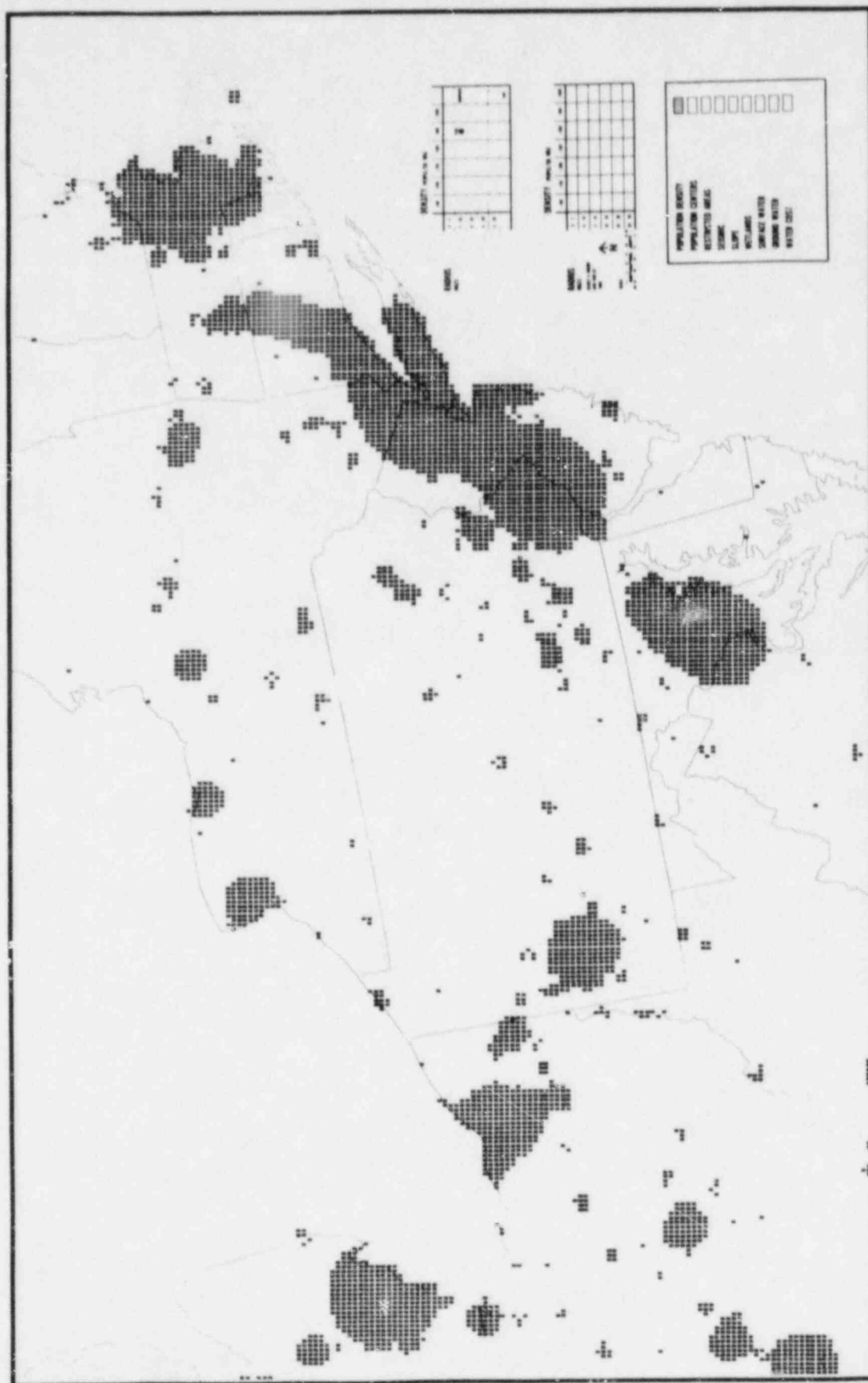


FIGURE F10.2

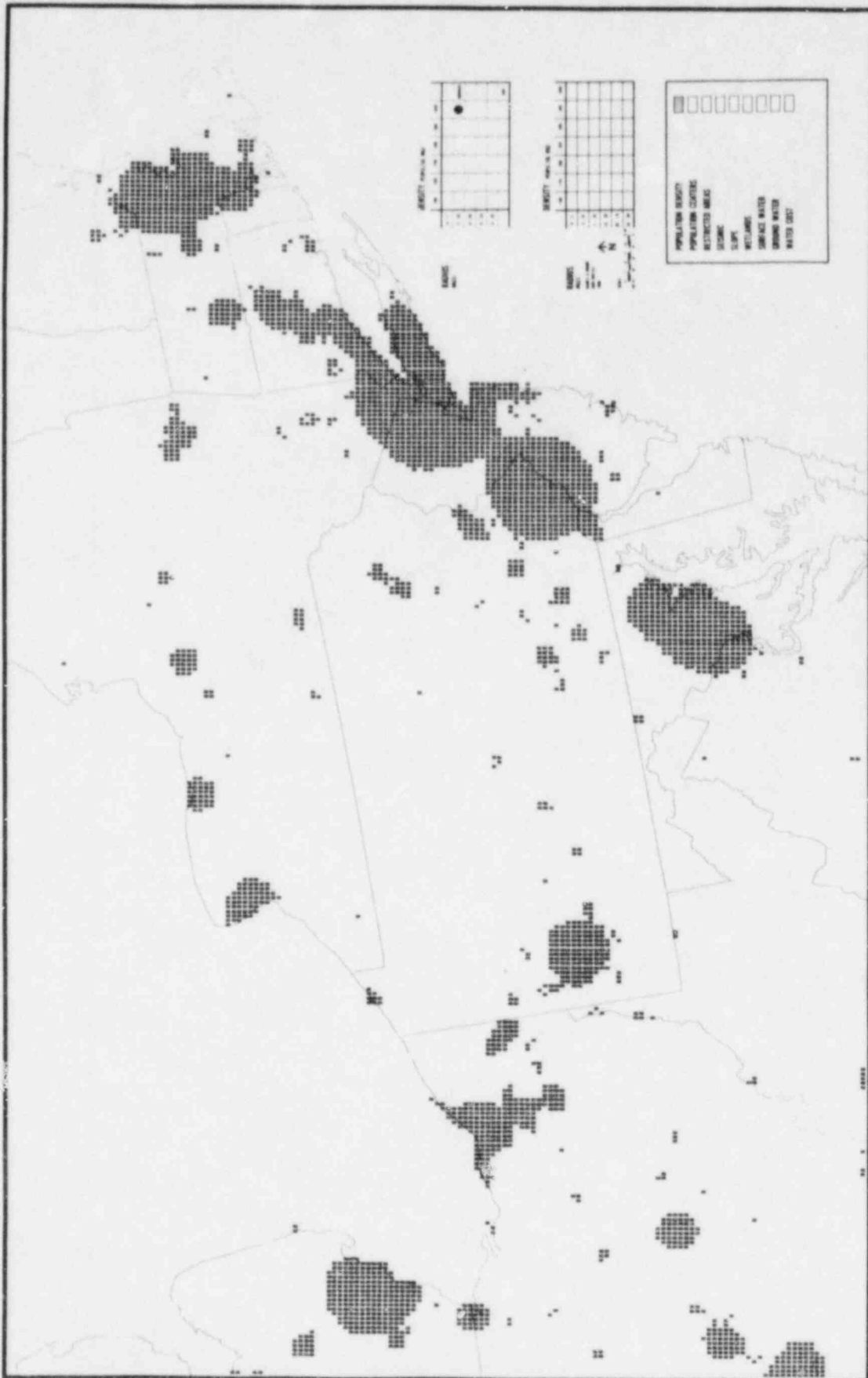


FIGURE F10.3

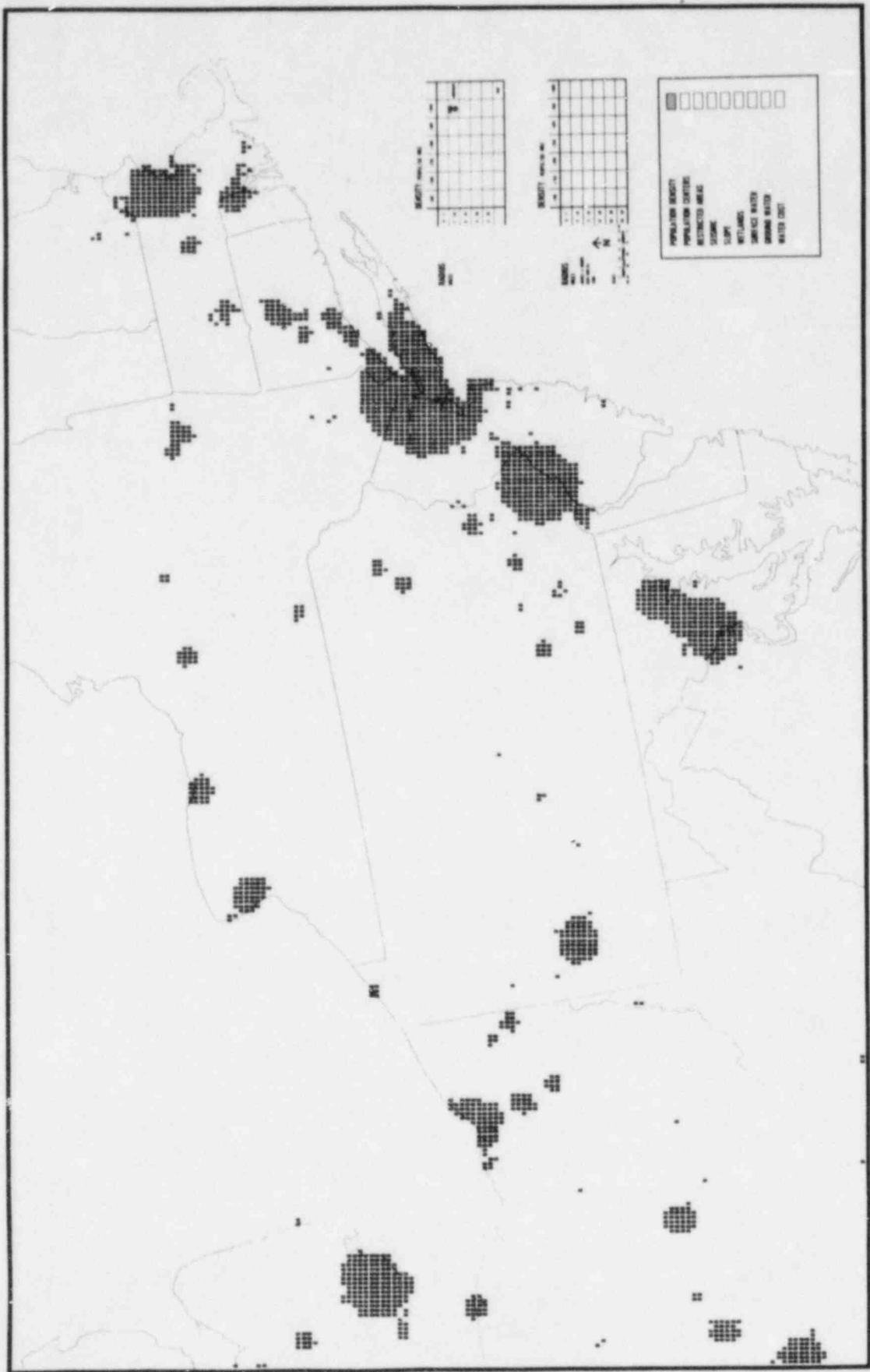


FIGURE F10.4

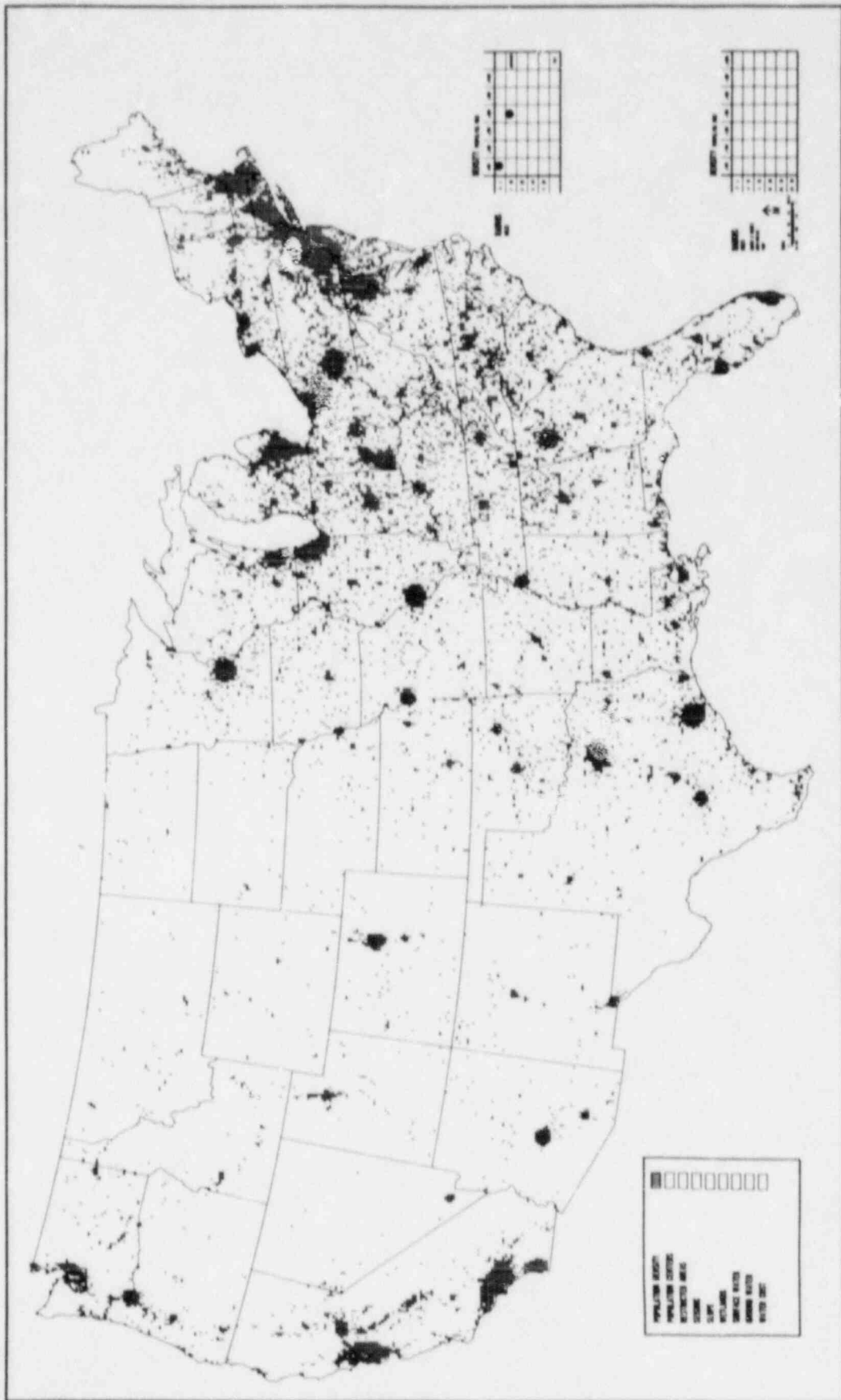


FIGURE F1:

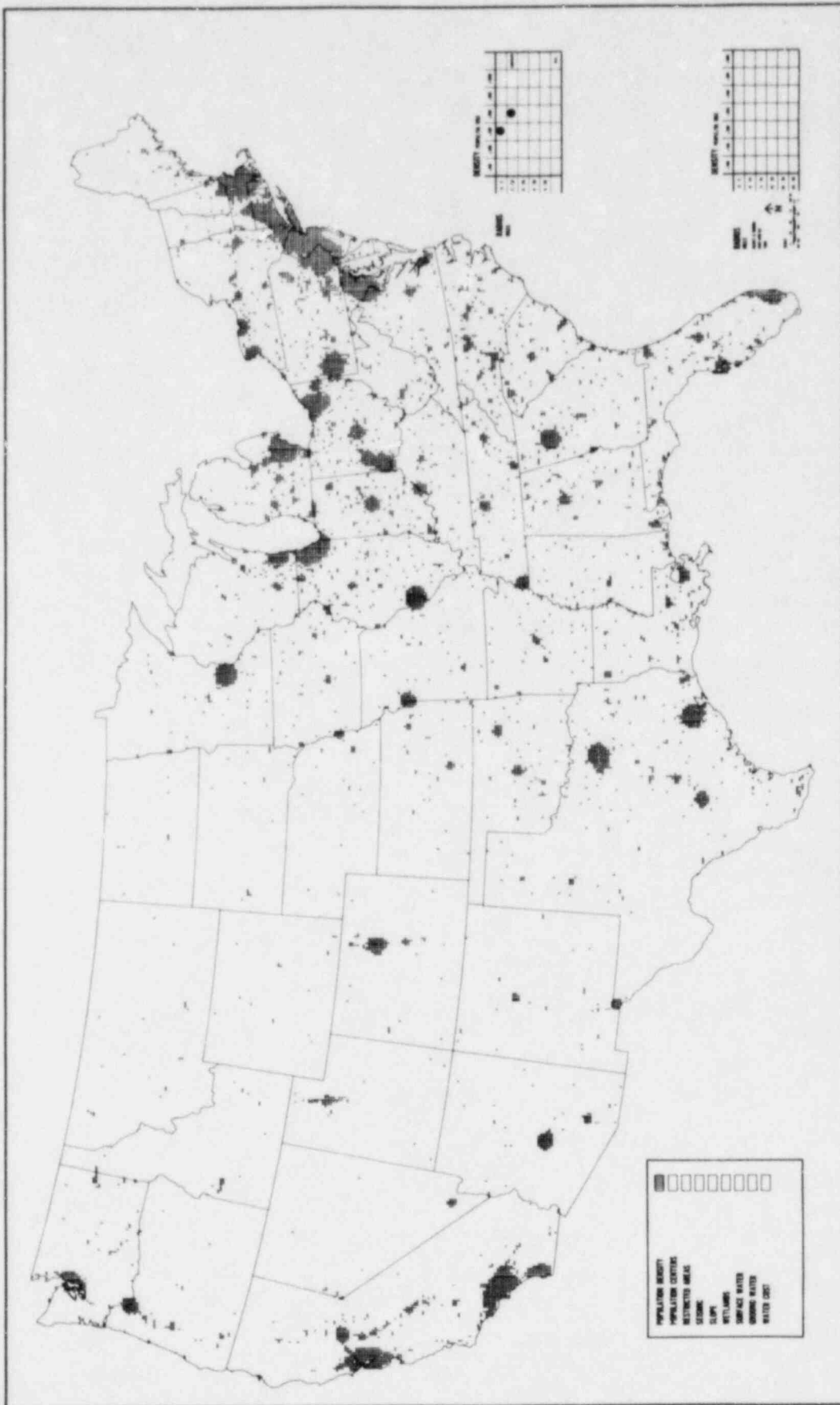


FIGURE F12

TABLE F1.1

SEISMIC HARDENING UTILITY FUNCTION ***
 COSTS IN MILLIONS OF DOLLARS 1980
 STATE AREAS IN SQUARE MILES AND % OF STATE

ACCELERATION	UNESTIMABLY HIGH							
	3e 4 TO 4e 4	3e 3 TO 3e 4	3e 2 TO 3e 3	3e 1 TO 3e 2	3e 0 TO 3e 1	3e -1 TO 3e 0	3e -2 TO 3e -1	3e -3 TO 3e -2
UTILITY VALUE	1	2	3	4	5	6	7	8
ALABAMA	0 0	0 0	0 0	0 0	0 0	164	5701	4243
ALASKA	222	10	48	27	192	5638	2994	4534
ARIZONA	0 2	0 0	0 0	0 1	0 2	5 1	2 3	4 2
ARIZONA-SONORA	6340	479	521	466	724	1969	3749	32142
CALIFORNIA	84328	2200	2142	2673	3416	8378	14171	11657
COLOMBIA	0 0	0 0	0 0	0 0	0 0	0 0	2 1	4 5
CONNECTICUT	0 0	0 0	0 0	0 0	0 0	160 0	0 0	0 0
DELAWARE	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
FLORIDA	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
GEORGIA	0 0	0 7	1 3	2 4	5 8	23 9	11 4	44 3
IDAHO	6736	849	946	1206	967	2336	6771	2617
ILLINOIS	2364	975	1341	1766	2606	8980	5848	31391
INDIANA	0 0	0 0	0 0	0 0	0 0	1 2	4 5	8 6
IOWA	0 0	0 0	0 0	0 0	0 0	0 0	2 6	9 9
KANSAS	0 0	0 0	0 0	0 0	0 0	12188	4795	60051
KENTUCKY	1287	232	174	212	415	2687	4207	28593
LOUISIANA	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
MAINE	0 0	0 0	0 0	0 0	0 0	10721	7931	15015
MARYLAND	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
MASSACHUSETTS	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
MICHIGAN	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
MINNESOTA	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
MISSISSIPPI	0 1	0 2	0 4	0 5	0 7	2 6	6 2	8 1
MISSOURI	7981	589	618	689	926	4648	7324	42754
MONTANA	1351	251	376	521	2036	10995	6272	79593
NEBRASKA	0 0	0 0	0 0	0 0	0 0	3694	3628	6685
NEVADA	31565	2220	2933	4767	14311	17498	10492	5877
NEW HAMPSHIRE	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
NEW JERSEY	0 0	0 0	0 0	0 0	0 0	38 1	11 7	50 2
NEW MEXICO	0 0	0 0	0 0	0 0	0 0	18210	11792	60206
NEW YORK	0 0	0 0	0 0	0 0	0 0	21037	7151	12101
NORTH CAROLINA	0 0	0 0	0 0	0 0	0 0	154	10905	4970
NORTH DAKOTA	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
OHIO	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
OKLAHOMA	0 0	0 0	0 0	0 0	0 0	24617	15932	25601
OREGON	0 0	0 0	0 0	0 0	0 0	0 2	0 5	46 4
PENNSYLVANIA	0 0	0 0	0 0	0 0	0 0	14 9	9 8	67 4
RHODE ISLAND	0 0	0 0	0 0	0 0	0 0	1206	0 0	0 0
SOUTH CAROLINA	12603	1843	2548	2586	3037	3908	0 0	0 0
SOUTH DAKOTA	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
TENNESSEE	3532	540	569	618	637	12342	15508	5780
TEXAS	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
UTAH	17573	1274	1206	1768	2210	4873	3172	25513
VERMONT	0 0	0 0	0 0	0 0	0 0	8830	0 0	0 0
VIRGINIA	0 0	0 0	0 0	0 0	0 0	58	3404	1383
WASHINGTON	7044	396	434	511	647	2528	3 6	67 1
WEST VIRGINIA	10 2	0 6	0 7	0 7	0 9	3 6	7 3	40 3
WISCONSIN	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
WYOMING	608	299	270	241	299	7264	3252	6652
TOTAL	162286	12710	15141	20207	28349	257403	183612	1791572
	5 4%	0 4%	0 5%	0 7%	1 3%	8 5%	6 0%	56 4%

*** UTILITY VALUES ARE DERIVED FROM MAP OF EFFECTIVE PEAK ACCELERATION EXPRESSED AS 1g (GRAVITY) AND ASSOCIATED COSTS OF SEISMIC HARDENING. COSTS ARE RELEVANT TO 1100 MEG PLANT OF SAFE SHUTDOWN EARTHQUAKE. THE 1g HAS A PROBABILITY OF LESS THAN 0.5% OF BEING EXCEEDED IN 50 YEARS. UNESTIMABLY HIGH REFERS TO AREAS WITH GREATER THAN 60% COSTS FOR AREAS WITH 20% TO 60% WERE DIVIDED INTO EQUAL INTERVALS AND ASSIGNED UTILITY VALUES 2-8.

TABLE Fl.2

SITE PREPARATION UTILITY FUNCTION ***
 PER CENT OF AREA LESS THAN 8% SLOPE (GENTLY SLOPING)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	UNDER 20% OF AREA					RESTRICTED LANDS
	UTILITY VALUE	1	2	3	4	
ALABAMA	0	17360	30069	2403	2075	51407
ARIZONA	0%	231	581	0%	4%	114342
ARIZONA	12%	2972	51348	492	59407	114342
ARIZONA	0%	3%	45%	0%	52%	
ARKANSAS	6369	7131	14381	18914	6263	53258
ARKANSAS	7%	13%	27%	36%	12%	
CALIFORNIA	24873	21259	35223	25517	31492	160364
CALIFORNIA	17%	33%	27%	16%	22%	
COLORADO	7286	13625	46822	7925	28860	104326
COLORADO	7%	13%	45%	8%	27%	
CONNECTICUT	0	2673	2538	0	0	5211
CONNECTICUT	0%	31%	49%	0%	0%	
DELAWARE	0	0	68	223	39	2327
DELAWARE	0%	0%	3%	95%	2%	
FLORIDA	0	0	4941	41312	13105	59358
FLORIDA	0%	0%	8%	70%	22%	
GEORGIA	530	5742	20755	15691	5867	38605
GEORGIA	1%	10%	32%	27%	10%	
IDAHO	4362	13809	27860	0	37519	83550
IDAHO	5%	17%	33%	0%	45%	
ILLINOIS	0	1012	29461	24700	1361	56539
ILLINOIS	0%	2%	52%	44%	2%	
INDIANA	0	9537	13717	19166	1322	36342
INDIANA	0%	7%	27%	32%	4%	
IOWA	0	13896	37249	4922	0	56067
IOWA	0%	25%	64%	9%	0%	
KANSAS	0	8502	48540	25032	193	82267
KANSAS	0%	10%	59%	30%	0%	
KENTUCKY	9785	14678	13056	390	2470	40269
KENTUCKY	24%	36%	32%	1%	6%	
LOUISIANA	0	0	973	24164	14417	48154
LOUISIANA	0%	0%	20%	50%	30%	
MAINE	418	11223	21877	0	357	34075
MAINE	2%	33%	64%	0%	1%	
MARYLAND	0	1351	5809	3850	145	11155
MARYLAND	0%	12%	52%	35%	1%	
MASSACHUSETTS	0	2741	5887	0	0	3628
MASSACHUSETTS	0%	30%	68%	0%	0%	
RICHMOND	0	0	30166	21992	9679	61837
RICHMOND	0%	0%	49%	36%	16%	
MINNESOTA	0	1187	34817	24984	24926	85914
MINNESOTA	0%	1%	41%	29%	29%	
MISSISSIPPI	0	4507	29770	9766	3841	47884
MISSISSIPPI	0%	9%	62%	20%	8%	
MISSOURI	7662	26954	18866	12005	4316	69933
MISSOURI	11%	30%	27%	17%	6%	
MONTANA	3542	41427	56327	0	47160	148456
MONTANA	2%	28%	38%	0%	32%	
NEBRASKA	0	27047	31546	17544	1534	77721
NEBRASKA	0%	35%	41%	23%	2%	
NEVADA	0	2490	87844	24	20255	110618
NEVADA	0%	2%	79%	0%	19%	
NEW HAMPSHIRE	772	5269	2239	0	1197	9467
NEW HAMPSHIRE	8%	56%	24%	0%	13%	
NEW JERSEY	0	1013	1554	5443	0	8010
NEW JERSEY	0%	13%	19%	68%	0%	
NEW MEXICO	5250	8849	62638	13471	31336	121744
NEW MEXICO	4%	7%	51%	11%	26%	
NEW YORK	2124	11252	24926	975	9930	50219
NEW YORK	6%	22%	30%	2%	20%	
NORTH CAROLINA	5461	2986	19454	17640	8627	50768
NORTH CAROLINA	5%	5%	36%	35%	17%	
NORTH DAKOTA	0	2432	33370	28632	6572	71006
NORTH DAKOTA	0%	3%	47%	40%	9%	
OHIO	9447	154	14649	15257	2326	41833
OHIO	23%	0%	35%	36%	6%	
ORLANDO	1090	4680	49447	10933	3664	69614
ORLANDO	2%	7%	71%	16%	5%	
OREGON	14495	18789	32096	0	30349	97920
OREGON	17%	19%	33%	0%	31%	
PENNSYLVANIA	7054	24743	9891	39	3551	45279
PENNSYLVANIA	16%	55%	22%	0%	8%	
RHODE ISLAND	0	0	1206	0	0	1206
RHODE ISLAND	0%	0%	100%	0%	0%	
SOUTH CAROLINA	338	376	11985	19826	2663	31188
SOUTH CAROLINA	1%	1%	38%	51%	9%	
SOUTH DAKOTA	1274	4169	31874	16897	22793	77007
SOUTH DAKOTA	2%	5%	41%	22%	30%	
MISSISSIPPI	1312	19522	17727	965	2596	42122
MISSISSIPPI	3%	46%	42%	2%	6%	
TEXAS	5394	8106	174906	74942	5491	248839
TEXAS	2%	3%	65%	28%	2%	
UTAH	1708	8386	43483	6051	25553	85181
UTAH	2%	10%	51%	7%	30%	
VERMONT	14640	5618	1573	0	1023	9852
VERMONT	17%	9%	1%	0%	10%	
VIRGINIA	2982	5501	22957	4063	3665	41168
VIRGINIA	7%	13%	56%	10%	14%	
WASHINGTON	10477	12535	41722	0	24762	69316
WASHINGTON	15%	18%	31%	0%	36%	
WEST VIRGINIA	16936	4072	376	0	2221	2405
WEST VIRGINIA	70%	17%	2%	0%	11%	
WISCONSIN	0	10567	33283	8145	5028	57023
WISCONSIN	0%	19%	36%	14%	9%	
WYOMING	6253	13105	53403	0	25225	97966
WYOMING	6%	13%	55%	0%	26%	
TOTAL	161193	415887	1383039	522176	557673	
TOTAL	5%	14%	45%	17%	18%	

*** SITE PREPARATION UTILITY IS DERIVED FROM A CONSIDERATION OF AN AREA'S TOPOGRAPHIC CHARACTER. SOURCE DATA IS A MAP INDICATING % OF AREA THAT IS GENTLY SLOPING (LESS THAN 8% SLOPE) AND CONTAINS 4 CATEGORIES. UTILITY VALUES WERE ASSIGNED ON THE BASIS OF RELATIVE DEGREE OF DIFFICULTY FOR ACCESS AND CONSTRUCTION.

TABLE 1.3

AGGREGATE WATER (SURFACE & GROUND) UTILITY FUNCTION ***
 COSTS IN MILLIONS OF DOLLARS (1980)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	MERE THAN 4300 HILL										
	262.5 TO 300.0		225.0 TO 262.5		187.5 TO 225.0		150.0 TO 187.5		112.5 TO 150.0		75.0 TO 112.5
	1	2	3	4	5	6	7	8	9	10	11
ALABAMA	0	0	0	0	87	1370	10364	19680	18325	2072	5177
ARIZONA	859	374	447	1119	16.3	8135	36302	3630	2297	5940	11830
ARKANSAS	0	0	0	0	1014	1908	4567	17291	16037	4263	8379
CALIFORNIA	0	0	25	0	35	81	127	375	127	57	117
COLORADO	29974	2441	2490	3065	4449	5462	11906	1976	4574	20665	104321
CONNECTICUT	0	0	0	0	0	0	656	2104	2451	0	5211
DELAWARE	0	0	0	0	0	0	0	0	0	0	0
FLORIDA	0	0	0	0	0	0	0	10	20632	25611	13101
GEORGIA	0	0	0	0	39	374	9905	24125	10692	5867	5867
IDAH0	77	309	409	720	860	1361	17420	15039	9853	0	8046
ILLINOIS	0	0	0	0	0	0	0	0	0	0	0
INDIANA	0	0	0	0	0	0	0	0	0	0	0
IOAH	0	0	0	0	0	0	0	0	0	0	0
KANSAS	25401	3493	3262	3032	3670	4094	12925	14473	5662	193	8706
KENTUCKY	0	0	0	0	360	2171	9322	15353	10393	2470	4026
L0UISIANA	0	0	0	0	0	0	0	0	0	0	0
MAINE	0	0	0	0	0	0	0	0	0	0	0
MARYLAND	0	0	0	0	0	0	0	0	0	0	0
MASSACHUSETTS	0	0	0	0	0	0	0	0	0	0	0
MICHIGAN	0	0	0	0	0	0	0	0	0	0	0
MINNESOTA	0	0	0	0	0	0	0	0	0	0	0
MISSISSIPPI	0	0	0	0	0	0	0	0	0	0	0
MISSOURI	0	0	0	0	0	0	0	0	0	0	0
NEBRASKA	251	924	3621	6410	9544	13327	25013	23382	10422	47160	148450
NEVADA	0	0	0	0	0	0	0	0	0	0	0
NEW HAMPSHIRE	0	0	0	0	0	0	0	0	0	0	0
NEW JERSEY	0	0	0	0	0	0	0	0	0	0	0
NEW MEXICO	51340	3050	2277	2024	1891	1460	19684	4523	1554	31334	12174
NEW YORK	0	0	0	0	0	0	0	0	0	0	0
NORTH CAROLINA	0	0	0	0	0	0	0	0	0	0	0
NORTH DAKOTA	1774	4562	7131	6919	8790	4234	11011	6420	4410	4572	71005
OHIO	0	0	0	0	0	0	0	0	0	0	0
OKLAHOMA	7491	1284	1325	1998	3020	4447	4447	19300	17254	8627	50749
OREGON	113	28	25	35	45	81	189	351	125	55	91928
PENNSYLVANIA	0	0	0	0	0	0	0	0	0	0	0
RHODE ISLAND	0	0	0	0	0	0	0	0	0	0	0
SOUTH CAROLINA	0	0	0	0	0	0	0	0	0	0	0
SOUTH DAKOTA	4139	4555	5084	5279	4893	4254	9194	7102	4709	22793	77008
TENNESSEE	125	65	75	78	65	65	127	91	61	205	42124
TEXAS	80295	3474	3404	3648	29519	9071	70474	42528	18933	5491	26803
UTAH	400	374	1438	2344	2924	4024	35444	7575	4873	25553	8511
VERMONT	15	05	25	35	75	55	425	95	65	305	905
VIRGINIA	0	0	0	0	0	0	0	0	0	0	0
WASHINGTON	0	0	0	0	0	0	0	0	0	0	0
WEST VIRGINIA	0	0	0	0	0	0	0	0	0	0	0
WISCONSIN	0	0	0	0	0	0	0	0	0	0	0
WYOMING	2943	3937	5317	6184	17430	9505	10607	10614	6012	25227	97461
TOTAL	220705	32874	39778	49727	103801	110644	740547	453680	522404	557471	187

*** AGGREGATE WATER COST DERIVATION LEAST COST ALTERNATIVE
 WAS DETERMINED FOR COMPOSITE OF GROUNDWATER COST AND SURFACE
 WATER COST. ESTIMATED GROUNDWATER COSTS FOR MAJOR REGIONS OF
 THE COUNTRY WERE CALCULATED FROM INFORMATION REGARDING
 QUANTITY, QUANTITY, DEPTH AND SIZE OF WELL-FIELD. PLEASE SEE
 SURFACE WATER UTILITY TABLE FOR DESCRIPTION OF SURFACE WATER
 COSTS. AGGREGATE COSTS LESS THAN \$300 MILLION WERE DIVIDED
 INTO 6 EQUAL INTERVALS.

TABLE F1.4

SURFACE WATER UTILITY FUNCTION ***
 COSTS IN MILLIONS OF DOLLARS (1980)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	MORE THAN \$300 MILL									RESTRICTED LAND	
	1	2	3	4	5	6	7	8	9		
ALABAMA	0	0	0	0	125	2731	8965	19686	18225	2675	5107
ALASKA	82012	4777	4364	4223	4140	4813	4362	3638	2297	9405	114343
ARIZONA	0	42	41	41	41	41	41	31	21	82	53254
ARKANSAS	0	0	77	473	1264	2374	6176	17793	18827	6263	53254
CALIFORNIA	0	0	0	18	23	41	127	331	331	107	160364
COLORAADO	13732	4403	6311	7228	8463	10567	15382	20704	21877	51492	140364
CONNECTICUT	29973	2400	2633	3234	4873	9964	10007	11956	4514	28460	104373
DELAWARE	0	0	0	0	0	0	0	0	0	0	5211
FLORIDA	0	0	0	0	0	0	0	0	0	0	2326
GEORGIA	0	0	0	0	0	0	0	0	0	0	2326
IDAHO	0	0	0	0	0	0	0	0	0	0	2326
ILLINOIS	0	0	0	0	0	0	0	0	0	0	2326
INDIANA	0	0	0	0	0	0	0	0	0	0	2326
IOWA	0	0	0	0	0	0	0	0	0	0	2326
KANSAS	0	0	0	0	0	0	0	0	0	0	2326
KENTUCKY	0	0	0	0	0	0	0	0	0	0	2326
LOUISIANA	0	0	0	0	0	0	0	0	0	0	2326
MAINE	0	0	0	0	0	0	0	0	0	0	2326
MARYLAND	0	0	0	0	0	0	0	0	0	0	2326
MASSACHUSETTS	0	0	0	0	0	0	0	0	0	0	2326
MICHIGAN	0	0	0	0	0	0	0	0	0	0	2326
MINNESOTA	0	0	0	0	0	0	0	0	0	0	2326
MISSISSIPPI	0	0	0	0	0	0	0	0	0	0	2326
MISSOURI	0	0	0	0	0	0	0	0	0	0	2326
MONTEANA	0	0	0	0	0	0	0	0	0	0	2326
NEBRASKA	0	0	0	0	0	0	0	0	0	0	2326
NEVADA	0	0	0	0	0	0	0	0	0	0	2326
NEW HAMPSHIRE	0	0	0	0	0	0	0	0	0	0	2326
NEW JERSEY	0	0	0	0	0	0	0	0	0	0	2326
NEW MEXICO	0	0	0	0	0	0	0	0	0	0	2326
NEW YORK	0	0	0	0	0	0	0	0	0	0	2326
NORTH CAROLINA	0	0	0	0	0	0	0	0	0	0	2326
NORTH DAKOTA	0	0	0	0	0	0	0	0	0	0	2326
OHIO	0	0	0	0	0	0	0	0	0	0	2326
OKLAHOMA	0	0	0	0	0	0	0	0	0	0	2326
OREGON	0	0	0	0	0	0	0	0	0	0	2326
PENNSYLVANIA	0	0	0	0	0	0	0	0	0	0	2326
RHODE ISLAND	0	0	0	0	0	0	0	0	0	0	2326
SOUTH CAROLINA	0	0	0	0	0	0	0	0	0	0	2326
SOUTH DAKOTA	0	0	0	0	0	0	0	0	0	0	2326
TENNESSEE	0	0	0	0	0	0	0	0	0	0	2326
TEXAS	0	0	0	0	0	0	0	0	0	0	2326
UTAH	0	0	0	0	0	0	0	0	0	0	2326
VERMONT	0	0	0	0	0	0	0	0	0	0	2326
VIRGINIA	0	0	0	0	0	0	0	0	0	0	2326
WASHINGTON	0	0	0	0	0	0	0	0	0	0	2326
WEST VIRGINIA	0	0	0	0	0	0	0	0	0	0	2326
WISCONSIN	0	0	0	0	0	0	0	0	0	0	2326
WYOMING	0	0	0	0	0	0	0	0	0	0	2326
TOTAL	398680	89912	69191	86117	119619	195086	284340	447940	522404	557473	185

*** SURFACE WATER COST DERIVATION SUITABLE SOURCES ARE OCEANS GREAT LAKES AND NON-INTERNATIONAL BOUNDARY STREAMS WITH 7-DAY, 10-YEAR LOW FLOW GREATER THAN 300 CFS WITH OR WITHOUT RESERVOIR STORAGE DISTANCE FROM SOURCES WAS COMPUTED AND COST APPLIED AS 8/MILE VARYING WITH TERRAIN SLOPE. A PENALTY ADDED FOR RESERVOIR NECESSITY LEAST COST ALTERNATIVE WAS DETERMINED COSTS LESS THAN \$300 MILLION WERE DIVIDED INTO EQUAL INTERVALS

TABLE F1.5

ENVIRONMENTAL SUITABILITY UTILITY FUNCTION ***
STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	ENVIRONMENTAL SUITABILITY UTILITY FUNCTION					RESTRICTED LANDS	
	LOW	MEDIUM-LOW	MEDIUM	MEDIUM-HIGH	HIGH		
UTILITY VALUE	1	2	3	4	5	1	
ALABAMA	98	4871	11387	19657	11860	2673	51908
ARIZONA	0%	13%	82%	38%	33%	4%	114343
ARKANSAS	2020	4101	14048	30755	1814	29405	114343
CALIFORNIA	3%	4%	14%	27%	2%	50%	53259
COLORADO	5211	7414	7784	10190	16103	6207	160743
CONNECTICUT	17%	14%	5%	19%	50%	12%	104324
DELAWARE	29999	29429	10938	13529	8384	51492	104324
FLORIDA	291	12%	7%	8%	9%	32%	5211
GEORGIA	76144	14209	11448	13234	4189	28460	5211
IDaho	31%	14%	11%	12%	4%	57%	2324
ILLINOIS	998	2073	782	1734	0	0	2324
INDIANA	11%	40%	18%	34%	0%	0%	2324
IOWA	0	0	0	0	2287	39	2324
KANSAS	0%	0%	0%	0%	98%	2%	2324
KENTUCKY	0	0	0	2133	44120	13105	2324
LOUISIANA	0%	0%	0%	4%	74%	22%	2324
MAINE	2454	3784	1072	17187	18422	867	2324
MARYLAND	5%	4%	18%	8%	31%	10%	2324
MASSACHUSETTS	10847	7874	12091	10441	4777	27519	2324
MICHIGAN	13%	9%	14%	12%	4%	45%	2324
MINNESOTA	3607	2343	9064	14473	27647	1361	2324
MISSISSIPPI	4%	4%	9%	24%	52%	2%	2324
MISSOURI	0	274	1988	9674	27774	1322	2324
MONTANA	0%	0%	0%	0%	63%	4%	2324
NEBRASKA	0	9474	8124	20740	12314	0	2324
NEVADA	0%	17%	9%	52%	22%	0%	2324
NEW HAMPSHIRE	18824	27802	18461	19131	7252	193	2324
NEW JERSEY	19%	34%	19%	19%	9%	0%	2324
NEW MEXICO	4871	17874	12101	8049	1978	2470	2324
NEW YORK	11%	54%	30%	21%	3%	4%	2324
NORTH CAROLINA	0	0	374	7083	26277	14417	2324
NORTH DAKOTA	0%	0%	1%	1%	9%	30%	2324
OHIO	1845	8443	4979	17274	1784	397	2324
OKLAHOMA	4%	2%	1%	5%	1%	1%	2324
OREGON	0	347	1081	2034	7344	145	2324
PENNSYLVANIA	0%	3%	10%	19%	48%	1%	2324
RHODE ISLAND	903	1774	2258	2439	0	0	2324
SOUTH CAROLINA	11%	21%	24%	42%	0%	0%	2324
SOUTH DAKOTA	0	0	0	17109	25049	0	2324
TENNESSEE	0%	0%	0%	0%	0%	14%	2324
TEXAS	0	241	1978	29093	24454	24974	2324
UTAH	0%	0%	0%	34%	25%	2%	2324
VERMONT	10	2425	4970	20747	15472	2841	2324
VIRGINIA	0%	8%	10%	43%	33%	0%	2324
WASHINGTON	12709	14417	15749	11985	10537	4514	2324
WEST VIRGINIA	17%	21%	22%	17%	1%	4%	2324
WISCONSIN	13887	27387	30098	23973	6449	47140	2324
WYOMING	9%	18%	20%	14%	4%	38%	2324
TOTAL	14214	12294	14772	14434	18431	1534	77721
	18%	14%	22%	19%	24%	2%	110414
	27982	18844	27447	2373	911	20253	110414
	34%	17%	2%	2%	0%	1%	2324
	1474	4448	1090	1235	0	1197	9444
	14%	47%	12%	12%	0%	12%	2324
	347	644	878	474	8442	0	2324
	4%	0%	11%	0%	48%	0%	2324
	47430	18382	19143	4892	328	21234	121743
	39%	15%	14%	4%	0%	24%	2324
	2832	7778	18024	12944	2992	4920	20220
	7%	18%	24%	8%	4%	20%	2324
	2144	1412	4478	12548	19229	8427	20770
	4%	3%	9%	27%	38%	17%	2324
	8238	12410	17973	14378	11734	4972	71005
	12%	17%	29%	20%	17%	9%	2324
	1494	2099	2832	11319	18043	2384	41823
	4%	12%	9%	27%	43%	4%	2324
	8149	12101	23044	14957	7884	3444	49415
	12%	17%	32%	21%	11%	9%	2324
	309	21134	14041	29408	4487	20349	27928
	0%	2%	14%	24%	7%	21%	2324
	2740	14104	14390	4399	2113	3931	45278
	4%	34%	32%	14%	9%	9%	2324
	0	0	434	778	0	0	1204
	0%	0%	34%	44%	0%	0%	2324
	1479	7777	14144	1983	1282	2443	21188
	8%	29%	2%	8%	4%	9%	2324
	11927	7917	11980	12101	11078	22792	77004
	14%	10%	1%	14%	14%	30%	2324
	4483	14514	9978	8094	454	2594	42123
	13%	24%	24%	17%	1%	4%	2324
	24320	43943	28440	98130	28253	3491	248839
	20%	14%	11%	37%	14%	2%	2324
	18873	13220	12984	10113	4825	23553	25180
	22%	14%	1%	12%	4%	20%	2324
	4234	3001	1457	114	0	1023	9853
	43%	30%	1%	1%	0%	10%	2324
	4335	2799	2480	12811	12448	3445	41148
	11%	7%	4%	32%	30%	14%	2324
	9313	28999	12227	9402	4912	24742	49317
	14%	12%	14%	14%	7%	24%	2324
	4121	10344	4523	149	232	2721	24104
	17%	42%	27%	1%	1%	11%	2324
	114	3840	4420	24417	14781	9028	57022
	0%	7%	12%	42%	29%	9%	2324
	17824	13703	20787	19710	4747	25225	27984
	18%	14%	21%	14%	9%	24%	2324
TOTAL	425114	432053	464810	449192	908122	557172	
	14%	14%	15%	21%	17%	12%	

*** ENVIRONMENTAL SUITABILITY DERIVATION: THREE FACTORS --
SEISMIC HARDENING, SITE PREPARATION AND AGGREGATE WATER
AVAILABILITY WERE COMBINED ADDING THEIR MAPPED UTILITY
VALUES (EACH RANGE 1-9) RESULTING IN A NET UTILITY MAP WITH
VALUES FROM 4-25. NET VALUES WERE DIVIDED INTO FIVE CATE-
GORIES OF APPROXIMATELY EQUAL AREA. BEST 20% COMPOSITE UTIL-
ITY WAS ASSIGNED "HIGH" ENVIRONMENTAL SUITABILITY WHILE
WORST 20% NET UTILITY WAS ASSIGNED "LOW" SUITABILITY.

TABLE F2.1

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 290 4/30 MI. *** SINGLE SECTOR (22.5 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	AVAILABLE LAND										
	> 1/16 ALLOWABLE POP	> 1/8 ALLOWABLE POP	> 1/4 ALLOWABLE POP	> 1/2 ALLOWABLE POP	> 1/3 ALLOWABLE POP	> 1/2 ALLOWABLE POP	UNIFORM DENSITY	RESTRICTED LANDS			
ALABAMA	1.0	14930	3002	4072	5674	5288	6398	2325	5703	2075	51907
ARIZONA	2.0	44020	830	1302	1978	1071	1727	464	3329	59405	114342
ARKANSAS	3.0	23944	3444	4940	4979	3647	2043	820	3165	4643	53257
CALIFORNIA	4.0	52478	7180	4417	4485	5365	3501	2142	28803	51492	160363
COLORADO	5.0	38327	3992	2972	2328	2200	1784	1139	3947	28440	104325
CONNECTICUT	6.0	10	0	0	0	0	0	0	0	0	5212
DELAWARE	7.0	309	77	261	399	284	212	133	408	39	2326
FLORIDA	8.0	10749	4757	4101	5510	3397	4034	2287	11397	13105	59357
GEORGIA	9.0	18347	803	493	935	575	485	395	1324	7014	58604
IDAH0	10.0	2797	703	873	1313	973	833	313	1203	1003	80550
ILLINOIS	11.0	11999	355	814	8502	6137	4139	1283	11792	136	56538
INDIANA	12.0	3020	142	314	5407	5008	2974	1486	18547	1322	36311
IOWA	13.0	24238	2398	2119	4230	4792	3300	917	2912	0	56046
KANSAS	14.0	59579	3001	5021	4007	2818	2750	780	3719	193	82244
KENTUCKY	15.0	11348	2844	2818	3302	4275	4543	2094	4314	2470	40270
LOUISIANA	16.0	11455	2123	3127	4391	4945	3300	1071	3723	14417	48154
MAINE	17.0	23234	1438	1978	1843	1421	1402	398	1303	357	54074
MARYLAND	18.0	994	408	454	964	907	742	357	3742	145	11155
MASSACHUSETTS	19.0	98	193	144	423	338	394	280	4774	0	8428
MICHIGAN	20.0	20024	782	2831	4738	4432	3522	1204	13423	9479	61837
MINNESOTA	21.0	35280	3078	7209	4294	3107	2490	897	4432	24926	89913
MISSISSIPPI	22.0	18238	2345	4245	5269	3838	4101	1042	2905	3841	47684
MISSOURI	23.0	33254	3718	7305	4987	4410	3404	984	5356	4314	49923
MONTANA	24.0	92206	2191	1431	2374	955	753	367	820	47160	148457
NEBRASKA	25.0	48113	155	113	143	043	032	022	043	3183	77721
NEVADA	26.0	82192	299	753	830	791	878	241	1177	20255	110617
NEW HAMPSHIRE	27.0	2818	270	878	897	714	950	241	1901	1197	9446
NEW JERSEY	28.0	0	29	48	394	193	241	154	4929	0	8010
NEW MEXICO	29.0	80344	1004	1988	1708	1293	1814	579	1474	31336	121744
NEW YORK	30.0	9703	1737	3184	4410	4719	4342	1447	14707	9930	50219
NORTH CAROLINA	31.0	4919	2347	3444	4041	4902	4794	2345	9110	8627	50749
NORTH DAKOTA	32.0	54088	1930	2937	1949	1004	579	473	473	4572	71005
OHIO	33.0	1872	2229	3204	4700	4403	3725	1399	1775	2324	41833
OKLAHOMA	34.0	39433	2580	5163	4244	4178	4130	1177	4343	3444	49414
OREGON	35.0	49794	2345	2779	3532	1754	2007	1204	4159	30349	97927
PENNSYLVANIA	36.0	3590	2895	3320	4893	4092	4254	1214	17447	3351	45280
RHODE ISLAND	37.0	0	0	0	0	29	39	0	1139	0	1207
SOUTH CAROLINA	38.0	3742	2123	2393	3339	4323	4403	1177	4825	2443	31188
SOUTH DAKOTA	39.0	44918	1805	1489	1737	647	389	212	418	22793	77008
TENNESSEE	40.0	11435	2423	2818	3995	4883	5423	2171	4174	2594	42122
TEXAS	41.0	144143	13254	17003	19397	12477	10394	3457	20941	5491	248839
UTAH	42.0	52264	443	1390	1081	811	1119	415	2084	2353	83180
VERMONT	43.0	3889	579	973	994	994	950	290	540	1023	9834
VIRGINIA	44.0	4774	3001	3213	4234	4442	5452	1583	4401	5443	41147
WASHINGTON	45.0	22890	2750	3117	3339	2874	2142	1139	4301	24742	49314
WEST VIRGINIA	46.0	5074	2519	2287	2874	2741	2741	868	2277	2721	24104
WISCONSIN	47.0	19590	3754	5520	4823	5047	3699	1245	4128	5028	57024
WYOMING	48.0	45330	1833	1737	1543	782	437	328	590	23225	97985
TOTAL		1405512	113194	143114	182502	148233	137771	49348	282411	557473	
		44.2%	2.7%	5.4%	6.0%	4.9%	4.5%	1.4%	9.3%	18.3%	

NOTE: "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST CON-
 STRAINING CRITERIA (I.E. IF > 1/16 OF THE POPULATION ALLOWED
 BY A UNIFORM DENSITY CRITERION IS FOUND IN A SINGLE SECTOR
 OF 22.5 DEGREES). NUMBERS IN THE COLUMNS REPRESENT THAT LAND
 UNUSUALLY CONSTRAINED BY THE GIVEN FRACTIONAL CRITERION. THIS
 LAND IS CONSIDERED AVAILABLE IF THE CRITERION WERE RELATED
 IF SECTOR CRITERION IS APPLIED. ASSUME THAT UNIFORM DENSITY
 CRITERION IS ALSO IN EFFECT. ** COMPOSITE OF 5 RADII **

TABLE F2.2

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 500 #/50 MI *** SINGLE SECTOR (22.5 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION		AVAILABLE LAND									
		> 1/16 ALLOWABLE POP	> 1/8 ALLOWABLE POP	> 1/4 ALLOWABLE POP	> 1/4 ALLOWABLE POP	> 1/3 ALLOWABLE POP	> 1/2 ALLOWABLE POP	UNIFORM DENSITY	RESTRICTED LANDS		
ALABAMA	1 0	24036	3990	3098	4072	4323	4813	2567	3329	2078	5190
ARIZONA	2 0	44600	926	1197	1690	1062	984	844	2026	39403	114342
ARKANSAS	3 0	30677	666	4661	3812	2866	1737	820	1756	4203	53258
CALIFORNIA	4 0	66366	4410	4883	6137	4516	4053	2191	6110	51492	180363
COLORADO	5 0	63427	1631	2490	1698	1544	1766	618	2490	23660	104326
CONNECTICUT	6 0	29758	143	120	357	270	309	251	3723	0	2512
DELAWARE	7 0	565	39	241	367	338	164	145	423	39	2327
FLORIDA	8 0	20149	3739	3069	4140	2741	2625	2663	7131	13105	59358
GEORGIA	9 0	25061	3706	3619	6439	4912	4410	2162	4429	5867	58605
IDAH0	10 0	42 85	4 32	6 25	7 61	8 63	7 55	3 75	7 51	15 02	82350
ILLINOIS	11 0	19570	4333	8724	6350	4178	3173	1013	7836	1361	56540
INDIANA	12 0	7063	2990	2860	4941	3259	4092	1998	5298	1322	36343
IOWA	13 0	32241	2364	8434	5336	3042	1862	311	2075	0	56065
KANSAS	14 0	67994	1867	2754	3049	2248	1534	540	2046	193	82267
KENTUCKY	15 0	14839	1457	2065	2490	3927	6380	2248	2683	2470	40269
LOUISIANA	16 0	10855	2499	2731	3464	3735	2258	994	2200	14417	48153
MAINE	17 0	36229	328	1399	1274	1426	1583	627	849	357	34074
MARYLAND	18 0	2123	270	369	1023	897	926	495	4507	143	11155
MASSACHUSETTS	19 0	434	222	347	830	618	492	369	5113	0	8627
MICHIGAN	20 0	22981	1341	4574	5134	4825	3638	2393	7472	9679	61837
MINNESOTA	21 0	41871	1042	8597	3175	2953	2113	907	3329	24926	89913
MISSISSIPPI	22 0	24123	1197	3136	4072	5230	3368	1129	1785	3641	47883
MISSOURI	23 0	41563	1905	8022	4748	4198	3030	886	3464	4316	69934
MONTANA	24 0	96654	803	1197	1148	753	550	338	454	47160	148457
NEBRASKA	25 0	66327	1197	2490	2084	1438	1032	347	1052	1534	77721
NEVADA	26 0	86039	907	791	878	494	463	222	589	20255	110618
NEW HAMPSHIRE	27 0	77 85	0 85	0 75	0 85	0 43	0 43	0 25	0 53	18 32	9467
NEW JERSEY	28 0	3619	434	476	637	266	801	347	1090	817	1197
NEW MEXICO	29 0	135	328	396	270	241	290	454	3894	0	8010
NEW YORK	30 0	1 71	4 13	4 92	3 43	3 03	3 63	5 73	73 61	0 01	121745
NORTH CAROLINA	31 0	83801	425	1138	1862	917	791	309	946	31536	121745
NORTH DAKOTA	32 0	68 85	0 35	1 03	1 53	0 83	0 63	0 33	0 83	25 92	30219
OHIO	33 0	9669	2298	3223	4111	4835	4864	2528	8801	9930	50219
OKLAHOMA	34 0	19 35	4 53	6 43	8 23	9 63	4 93	5 03	17 53	19 83	30768
OREGON	35 0	12902	2760	3107	4160	4343	4494	3398	5037	8627	30768
PENNSYLVANIA	36 0	25 43	5 43	6 13	8 23	8 43	12 83	8 43	9 93	7 03	45278
RHODE ISLAND	37 0	58315	482	2306	1476	917	425	134	357	4372	71004
SOUTH CAROLINA	38 0	80 13	0 73	3 23	2 13	1 33	0 63	0 23	0 53	9 33	41832
SOUTH DAKOTA	39 0	17 13	4 13	7 33	9 63	13 23	11 83	6 03	25 13	5 63	69616
TENNESSEE	40 0	47353	1940	2783	3985	3001	2538	1197	2355	3464	69616
TEXAS	41 0	68 03	2 83	5 43	5 73	4 33	3 63	1 73	3 43	3 03	97929
UTAH	42 0	55266	2063	1592	1969	1457	1293	1525	2413	30349	97929
VERMONT	43 0	38 43	2 13	1 63	2 03	1 53	1 23	1 63	2 53	31 03	45278
VIRGINIA	44 0	9090	2461	3349	4256	4352	4374	2528	11117	3351	45278
WASHINGTON	45 0	20 13	5 43	7 43	9 43	9 43	10 13	5 63	24 63	7 83	1207
WEST VIRGINIA	46 0	0	0	10	39	87	106	58	907	0	1207
WISCONSIN	47 0	0 03	0 03	0 83	3 23	7 23	8 83	4 83	75 23	0 03	31189
WYOMING	48 0	9756	2133	2519	2461	3339	4169	1505	2644	2663	31189
TOTAL		31 33	6 83	8 13	7 93	10 73	13 43	4 83	8 53	8 53	77008
		45 93	0 13	1 63	1 13	0 73	0 43	0 23	0 53	29 63	42122
		18636	1370	2577	3406	4304	4844	2721	3648	2596	42122
		39 53	3 23	6 13	8 13	10 23	11 53	6 53	8 73	4 23	268839
		194554	10605	12545	12140	9254	8318	3030	12902	5491	85181
		72 43	3 93	4 73	4 53	3 43	3 13	1 13	4 83	2 03	9852
		53480	1129	1004	1226	733	647	338	1071	25553	41167
		5308	0	772	685	878	492	347	347	1023	69316
		53 93	0 03	7 83	7 03	8 93	5 03	3 53	3 53	10 43	12107
		12120	2133	2277	3831	4564	4507	1998	4072	5665	41167
		29 43	5 23	5 33	5 33	11 33	10 93	4 93	9 93	12 83	69316
		28757	1824	2509	2422	2451	1631	1216	3744	24762	24105
		41 53	2 63	3 63	3 53	3 53	2 43	1 83	5 43	35 73	24105
		9399	994	1198	1920	2673	2818	955	1467	2721	57021
		39 03	4 13	4 83	8 03	11 13	11 73	4 03	6 13	11 33	57021
		26366	2229	3153	4970	4391	3184	1592	3908	5028	97985
		46 63	3 93	9 03	8 73	7 73	5 63	2 83	6 93	8 83	97985
		69663	0	955	733	492	290	222	405	25225	25 73
		71 13	0 03	1 03	0 73	0 53	0 33	0 23	0 43	25 73	
		1448335	78720	135711	139287	128934	116370	54769	177165	537673	
		54 23	2 63	4 53	4 63	4 23	3 83	1 93	5 83	18 33	

NOTE "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST CON-
 STRAINING CRITERIA (i.e. IF > 1/16 OF THE POPULATION ALLOWED
 BY A UNIFORM DENSITY CRITERION IS FOUND IN A SINGLE SECTOR
 OF 22.5 DEGREES) NUMBERS IN THE COLUMNS REPRESENT THAT LAND
 UNIQUELY CONSTRAINED BY THE GIVEN FRACTIONAL CRITERION. THIS
 LAND IS CONSIDERED AVAILABLE IF THE CRITERION WERE RELATED
 IF SECTOR CRITERION IS APPLIED. ASSUME THAT UNIFORM DENSITY
 CRITERION IS ALSO IN EFFECT ** COMPOSITE OF 5 RADII **

TABLE F2.3

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 750 #/SQ. MI *** SINGLE SECTOR (22.5 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION		AVAILABLE LAND									
		> 1/16	ALLOWABLE POP	> 1/8	ALLOWABLE POP	> 1/4	ALLOWABLE POP	> 1/2	ALLOWABLE POP	UNIFORM DENSITY RESTRICTED LANDS	
ALABAMA	1 0	27435	2972	2760	2893	3667	4593	2650	2856	2075	51507
ARIZONA	2 0	47459	1419	1255	1554	509	531	454	1679	39405	114345
ARKANSAS	3 0	31845	1062	4217	3423	2566	1407	300	1354	4263	53259
CALIFORNIA	4 0	71592	4333	4736	4393	4468	3513	4306	12327	31492	140363
COLORADO	5 0	65380	1573	1679	1766	1621	1071	704	1362	28660	104324
CONNECTICUT	6 0	87	270	270	309	386	531	415	2962	0	3211
DELAWARE	7 0	637	106	232	309	190	154	164	396	39	2327
FLORIDA	8 0	25012	2248	3175	2615	1698	2268	3770	6449	13109	99257
GEORGIA	9 0	28815	2374	2895	3704	4468	4323	2343	2817	5867	98605
IDAHO	10 0	40839	413	1081	753	562	849	444	685	27519	83550
ILLINOIS	11 0	25167	2490	7768	5201	4198	2731	1216	6417	1361	56539
INDIANA	12 0	9843	1814	3879	4902	4497	3980	2345	4199	1322	26341
IOWA	13 0	35647	1954	9019	4314	2808	1390	840	1795	0	86667
KANSAS	14 0	69557	1554	3281	2461	1727	1156	989	1747	192	82267
KENTUCKY	15 0	18480	1197	1727	2220	3713	3913	2293	2152	2470	40269
LOUISIANA	16 0	18943	1486	1978	3049	3165	2220	1042	1893	14417	48153
MAINE	17 0	26972	10	1148	1235	1391	1943	647	791	297	34074
MARYLAND	18 0	2480	232	618	878	1004	1216	984	3999	145	11156
MASSACHUSETTS	19 0	436	407	618	860	415	998	743	4432	0	8627
MICHIGAN	20 0	24067	1911	5035	4516	4304	3542	2721	6523	9679	61806
MINNESOTA	21 0	43637	261	3472	3040	2876	1998	1148	2957	24926	89915
MISSISSIPPI	22 0	25331	1525	2615	3686	4902	3642	1198	1982	3841	47883
MISSOURI	23 0	43413	1042	3879	4374	4121	2577	926	2856	4516	64923
MONTEANA	24 0	97494	0	917	1023	695	434	318	415	47160	148456
NEBRASKA	25 0	48033	868	2384	1727	1312	676	338	849	1834	77721
NEVADA	26 0	86956	801	732	569	309	309	164	462	20755	116617
NEW HAMPSHIRE	27 0	4169	164	390	569	716	782	276	966	1197	9667
NEW JERSEY	28 0	482	386	261	347	174	405	340	9433	0	6008
NEW MEXICO	29 0	84544	772	1544	899	733	569	318	847	21936	121744
NEW YORK	30 0	12091	1727	3165	3783	4413	4449	2827	7623	9930	90018
NORTH CAROLINA	31 0	15994	2268	2615	3011	4043	6736	3962	4323	8627	30769
NORTH DAKOTA	32 0	99183	0	2229	1954	689	308	145	999	4972	71009
OHIO	33 0	9235	1428	3194	4767	9086	4907	3184	8106	2326	41833
OKLAHOMA	34 0	2213	343	763	1143	1223	1083	763	1943	863	69615
OREGON	35 0	57298	1361	1486	1573	1081	1090	1602	1988	20349	97928
PENNSYLVANIA	36 0	11366	2287	3223	2992	4364	5086	3184	9013	3551	45278
RHODE ISLAND	37 0	0	10	29	154	77	125	125	689	0	1205
SOUTH CAROLINA	38 0	11754	2287	1630	1602	3117	4178	1640	2297	2643	3188
SOUTH DAKOTA	39 0	51193	0	1100	733	434	212	164	376	22793	77005
TENNESSEE	40 0	18142	1814	2094	2702	3936	4777	2827	3213	2594	42121
TEXAS	41 0	208662	3568	9959	10914	8695	4205	3175	10171	5491	268840
UTAH	42 0	54629	811	1100	1052	291	502	357	926	29553	85181
VERMONT	43 0	5481	10	714	608	849	492	338	338	1022	9853
VIRGINIA	44 0	14552	1486	2200	3213	4101	4800	2104	3445	3665	41166
WASHINGTON	45 0	26774	1969	1911	2287	1737	1448	1341	3088	24762	69317
WEST VIRGINIA	46 0	10721	145	926	1843	2615	2827	984	1312	2721	24104
WISCONSIN	47 0	29095	1554	4777	4207	6352	3184	1679	3166	5028	57022
WYOMING	48 0	70262	0	811	492	347	251	232	367	25225	97987
TOTAL		1745298	61812	122845	117671	116880	107473	62288	148018	557673	
		57.4%	2.0%	4.0%	3.9%	3.8%	3.9%	2.0%	4.9%	18.3%	

NOTE "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST CONSTRAINING CRITERIA (i.e. IF > 1/16 OF THE POPULATION ALLOWED BY A UNIFORM DENSITY CRITERION IS FOUND IN A SINGLE SECTOR OF 22.5 DEGREES) NUMBERS IN THE COLUMNS REPRESENT THAT LAND UNIQUELY CONSTRAINED BY THE GIVEN FRACTIONAL CRITERION. THIS LAND IS CONSIDERED AVAILABLE IF THE CRITERION WERE RELAXED. IF SECTOR CRITERION IS APPLIED, ASSUME THAT UNIFORM DENSITY CRITERION IS ALSO IN EFFECT ** COMPOSITE OF 5 RADII **

TABLE F2.4

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 1500 4/80 MI *** SINGLE SECTOR (22 1/2 DEGREES)
 STATE AREAS IN SQUARE MILES AND 1/2 OF STATE

TABULATION		AVAILABLE LAND									
		> 1/16 ALLOWABLE POP	> 1/8 ALLOWABLE POP	> 1/4 ALLOWABLE POP	> 1/2 ALLOWABLE POP	> 1/3 ALLOWABLE POP	> 1/2 ALLOWABLE POP	UNIFORM DENSITY	RESTRICTED LANDS		
ALABAMA	1 0	32482	704	1438	1734	2464	4392	2702	2492	2075	51704
ARIZONA	2 0	49444	1421	743	484	261	472	482	1438	39403	114343
ARKANSAS	3 0	32765	434	3754	2914	2374	1448	830	1474	4263	53258
CALIFORNIA	4 0	79335	2730	3251	2242	3134	3088	2548	11020	51492	140262
COLORADO	5 0	48224	608	1814	1522	848	934	704	1484	28460	104325
CONNECTICUT	6 0	384	309	114	182	408	627	911	2473	0	5210
DELAWARE	7 0	811	48	192	251	270	182	144	247	39	2324
FLORIDA	8 0	29384	2142	1187	1042	1341	2258	2837	4002	13103	39358
GEORGIA	9 0	32279	791	2104	2892	4371	4294	2384	3419	5847	58404
IDAHO	10 0	41804	10	830	389	731	732	4 1/2	4 1/2	10 1/2	8351
ILLINOIS	11 0	29712	714	7244	4449	3503	2384	1303	5445	1341	34329
INDIANA	12 0	13298	1534	3143	3242	3915	3931	2413	3812	1322	34342
IOWA	13 0	34 1/2	4 1/2	8 1/2	9 1/2	11 1/2	9 1/2	4 1/2	10 1/2	3 1/2	54047
KANSAS	14 0	72500	502	2797	4 1/2	4 1/2	1100	389	1431	193	82247
KENTUCKY	15 0	29424	447	1341	1431	2397	2829	2441	2045	2470	40270
LOUISIANA	16 0	51992	39	1399	2297	2972	2210	1042	1744	14417	48154
MAINE	17 0	27194	0	1073	1148	1351	1594	434	732	357	34073
MARYLAND	18 0	2779	274	850	1224	1071	1042	1214	2750	145	11195
MASSACHUSETTS	19 0	1380	472	241	384	443	447	473	4043	0	8428
MICHIGAN	20 0	27438	782	3782	3541	4092	3542	3020	5742	9479	41829
MINNESOTA	21 0	44422	472	3414	2404	2422	2007	1233	2191	24924	89914
MISSISSIPPI	22 0	27792	318	2094	3134	4784	3212	1187	1515	3841	47882
MISSOURI	23 0	45345	742	5742	3879	2704	2432	1012	2537	4514	49923
MONTANA	24 0	47928	0	840	878	340	347	318	403	47140	148454
NEBRASKA	25 0	49403	500	2132	1187	1022	950	338	801	1534	77721
NEVADA	26 0	89 1/2	0 1/2	2 1/2	1 1/2	1 1/2	0 1/2	0 1/2	1 1/2	2 1/2	110417
NEW HAMPSHIRE	27 0	4420	10	840	521	474	782	405	888	1197	9449
NEW JERSEY	28 0	1042	280	341	384	280	340	1012	4184	0	8010
NEW MEXICO	29 0	84145	704	493	443	340	521	318	782	3134	121744
NEW YORK	30 0	14841	1448	2557	2847	4323	4294	2943	4994	4930	50219
NORTH CAROLINA	31 0	29 1/2	2 1/2	5 1/2	5 1/2	8 1/2	8 1/2	5 1/2	13 1/2	1 1/2	8427
NORTH DAKOTA	32 0	19232	104	1774	2434	2934	4448	3512	4217	1847	50749
OHIO	33 0	49801	0	2035	1214	484	270	145	290	4572	71005
OKLAHOMA	34 0	32200	1119	2094	1852	2374	2384	1245	1882	3444	49415
OREGON	35 0	39849	598	907	848	840	1042	1421	1853	30349	97927
PENNSYLVANIA	36 0	13102	241	2422	2731	4448	5124	3532	8087	3551	45278
RHODE ISLAND	37 0	10	194	87	29	48	114	144	398	0	1204
SOUTH CAROLINA	38 0	13082	39	1032	1274	3078	4159	1440	2220	2443	31189
SOUTH DAKOTA	39 0	31999	0	917	579	374	212	144	347	22792	77007
TENNESSEE	40 0	20931	549	1322	2210	3812	4719	2844	3098	2594	42122
TEXAS	41 0	219402	3879	8801	7180	4339	5587	1 1/2	1 1/2	2 1/2	248829
UTAH	42 0	55814	1119	472	347	192	502	374	801	25553	85180
VERMONT	43 0	8407	10	454	349	830	482	338	338	1022	9853
VIRGINIA	44 0	14704	1148	1534	2441	3983	4371	2142	3134	5445	41144
WASHINGTON	45 0	33920	1224	1197	1204	1484	1380	1448	2472	24742	49317
WEST VIRGINIA	46 0	11124	10	811	1708	2412	2827	964	5 1/2	11 1/2	24105
WISCONSIN	47 0	31932	347	4244	3792	4043	3040	1747	2808	5028	57022
WYOMING	48 0	70812	0	502	328	328	192	232	347	25225	97987
TOTAL		1835831	32521	99454	87423	104450	104528	65959	131928	537472	

NOTE: "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST CON-
 STRAINING CRITERIA (I.E. IF > 1/16 OF THE POPULATION ALLOWED
 BY A UNIFORM DENSITY CRITERION IS FOUND IN A SINGLE SECTOR
 OF 22 1/2 DEGREES; NUMBERS IN THE COLUMNS REPRESENT THAT LAND
 UNIQUELY CONSTRAINED BY THE GIVEN FRACTIONAL CRITERION; THIS
 LAND IS CONSIDERED AVAILABLE IF THE CRITERION WERE RELAXED
 IF SECTOR CRITERION IS APPLIED. ASSUME THAT UNIFORM DENSITY
 CRITERION IS ALSO IN EFFECT. ** COMPOSITE OF 9 RADII **

TABLE F2.5

POPULATION SECTOR ANALYSIS - TOTAL U. S.
 DENSITY = 250 #/SQ MI *** DOUBLE SECTOR (45 0 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION		AVAILABLE LAND								
		> 1/8 ALLOWABLE POP	> 1/6 ALLOWABLE POP	> 1/4 ALLOWABLE POP	> 1/3 ALLOWABLE POP	> 1/2 ALLOWABLE POP	UNIFORM DENSITY	RESTRICTED LANDS		
ALABAMA	1 0	19647	1554	5616	3944	6813	4555	5703	2075	51907
ARIZONA	3 0	44947	328	1947	1110	1361	1882	3229	59405	114343
ARKANSAS	3 0	28767	762	5616	3426	3387	1812	3165	6263	53258
CALIFORNIA	4 0	59695	1448	7604	5713	6085	5124	22803	51492	160364
COLORADO	3 0	6702	1004	2625	1380	2953	2055	3947	28660	104326
CONNECTICUT	4 0	10	0	29	68	97	19	4989	0	5212
DELAWARE	7 0	444	0	375	280	376	203	608	29	2326
FLORIDA	8 0	13790	2413	5221	4053	4738	4642	11397	13105	59359
GEORGIA	9 0	20535	1399	7218	7083	5944	3542	7016	5867	58604
IDAHO	10 0	38185	154	2972	975	1679	859	1206	37519	83549
ILLINOIS	11 0	17138	1792	8679	6124	6745	3522	11782	1361	56538
INDIANA	12 0	4749	1003	4989	5240	4960	3271	10547	1322	36341
IOWA	13 0	32347	1361	6620	3860	3414	2654	3812	0	56068
KANSAS	14 0	62166	415	4593	2384	3300	2499	3719	193	82265
KENTUCKY	15 0	14272	590	4140	4534	6686	3329	4314	2470	40269
LOUISIANA	16 0	12931	1448	4593	3870	4757	2413	3725	14417	48154
MAINE	17 0	25399	68	2461	1756	1901	830	1303	357	34075
MARYLAND	18 0	1573	48	1255	772	1081	540	5742	145	11156
MASSACHUSETTS	19 0	174	87	309	328	473	482	6774	0	8627
MICHIGAN	20 0	22562	328	4188	4362	4729	2537	13423	9679	61838
MINNESOTA	21 0	42335	1023	5163	3001	2908	1930	4632	24926	85915
MISSISSIPPI	22 0	21934	444	5442	6080	4613	2386	2905	3841	47885
MISSOURI	23 0	41061	704	7344	4314	4169	2470	5356	4516	69934
MONTANA	24 0	94744	811	1940	1648	897	637	820	47160	148457
NEBRASKA	25 0	65475	415	2577	2441	1515	1592	2171	1534	77720
NEVADA	26 0	85825	135	904	405	975	782	1177	20255	110618
NEW HAMPSHIRE	27 0	3194	116	1090	936	695	338	1901	1197	9467
NEW JERSEY	28 0	0	19	97	290	434	241	6929	0	8010
NEW MEXICO	29 0	82363	123	1882	1013	1708	1440	1474	31536	121743
NEW YORK	30 0	7469	762	4246	4458	4989	2657	14707	9930	50218
NORTH CAROLINA	31 0	8463	1303	5105	4861	7469	3831	9110	8627	50769
NORTH DAKOTA	32 0	58209	618	2586	965	647	936	473	6572	71006
OHIO	33 0	3591	1081	4555	4899	4687	3059	17775	2326	41833
OKLAHOMA	34 0	44081	1727	4526	3677	4487	3609	4043	3464	69614
OREGON	35 0	32149	907	3168	2596	2229	2374	4159	30349	97928
PENNSYLVANIA	36 0	5790	1052	4854	4709	5288	2567	17467	3551	45278
RHODE ISLAND	37 0	0	0	0	0	48	10	1139	0	1207
SOUTH CAROLINA	38 0	7337	434	3426	3735	4031	2519	4825	2663	31190
SOUTH DAKOTA	39 0	48655	724	2036	907	627	447	618	22793	77007
TENNESSEE	40 0	14050	676	4159	4314	6379	3773	6176	2596	42123
TEXAS	41 0	181256	5221	20091	13346	12777	9718	20941	5491	268841
UTAH	42 0	53220	203	1071	714	1226	1110	2084	25552	85181
VERMONT	43 0	4420	311	1090	1177	666	405	560	1023	9852
VIRGINIA	44 0	9525	1110	4178	4999	5722	3368	6601	5665	41168
WASHINGTON	45 0	24974	1592	3175	3156	2885	2470	6301	24762	69315
WEST VIRGINIA	46 0	7181	695	3831	2905	3300	1235	2277	2721	24105
WISCONSIN	47 0	24849	975	7527	4603	5037	2876	6128	5028	57023
WYOMING	48 0	67637	0	2538	676	618	743	550	25225	97987
TOTAL		1544002	39888	189101	152051	166674	107973	282411	557674	557674
		50 8%	1 3%	6 2%	5 0%	5 5%	3 6%	9 3%	18 3%	

NOTE "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST CONSTRAINING CRITERIA I.E. IF > 1/8 OF THE POPULATION ALLOWED BY A UNIFORM DENSITY CRITERION IS FOUND IN A DOUBLE SECTOR OF 45 0 DEGREES 1 NUMBERS IN THE COLUMNS REPRESENT THAT LAND UNIQUELY CONSTRAINED BY THE GIVEN FRACTIONAL CRITERION THIS LAND IS CONSIDERED AVAILABLE IF THE CRITERION WERE RELATED IF SECTOR CRITERION IS APPLIED. ASSUME THAT UNIFORM DENSITY CRITERION IS ALSO IN EFFECT. ** COMPOSITE OF 5 RADII **

TABLE F2.6

POPULATION SECTOR ANALYSIS - TOTAL U. S.
 DENSITY = 500 #/SQ MI *** DOUBLE SECTOR (45 0 DEGREES)
 STATE AREAS IN SQUARE MILES AND 1 OF STATE

TABULATION		AVAILABLE LAND								
		> 1/8 ALLOWABLE POP	> 1/8 ALLOWABLE POP	> 1/8 ALLOWABLE POP	> 1/8 ALLOWABLE POP	> 1/8 ALLOWABLE POP	> 1/8 ALLOWABLE POP	> 1/8 ALLOWABLE POP	> 1/8 ALLOWABLE POP	> 1/8 ALLOWABLE POP
ALABAMA	1 0	26653	1718	3937	5192	5858	3144	3329	2075	51900
ARIZONA	2 0	47353	454	1312	1255	1351	1187	2026	59405	114343
ARKANSAS	3 0	23910	308	4304	2799	2499	1399	1756	6263	53258
CALIFORNIA	4 0	69422	2534	5549	5877	5269	4005	14115	51492	160263
COLORADO	5 0	65224	328	2712	1590	1824	1698	2490	28660	104326
CONNECTICUT	6 0	0 29	48	232	376	482	309	3735	0	5211
DELAWARE	7 0	456	29	386	347	280	164	425	39	2326
FLORIDA	8 0	23170	840	3773	3725	3821	3792	7131	13105	59357
GEORGIA	9 0	28342	1814	4825	5172	5240	2914	4429	5867	58603
IDAHO	10 0	41099	48	1437	1033	840	811	743	37519	83550
ILLINOIS	11 0	27396	1332	7498	4391	4053	2673	7836	1361	56540
INDIANA	12 0	10731	868	4642	4555	5520	3406	5298	1322	36342
IOWA	13 0	39652	415	6427	2895	2982	1631	2075	0	56067
KANSAS	14 0	70397	290	3349	2133	2277	1583	2044	193	82268
KENTUCKY	15 0	18383	917	2986	3937	4369	2924	2683	2470	40269
LOUISIANA	16 0	18653	338	4343	3358	3368	1476	2200	14417	48153
MAINE	17 0	27474	0	1583	1341	1679	791	849	357	34074
MARYLAND	18 0	2319	106	846	926	1081	926	4507	145	11156
MASSACHUSETTS	19 0	589	106	454	868	793	743	5115	0	8628
MICHIGAN	20 0	25650	907	4989	4931	4864	3146	7672	9679	61838
MINNESOTA	21 0	47430	145	3242	2683	2441	1718	3329	24926	88914
MISSISSIPPI	22 0	26055	579	4815	5443	3686	1679	1785	3841	47883
MISSOURI	23 0	47149	376	5105	3783	3339	2181	3444	4516	69933
MONTANA	24 0	97803	0	1081	656	772	531	454	47160	148457
NEBRASKA	25 0	68843	482	1766	1718	1187	1139	1052	1534	77721
NEVADA	26 0	87072	77	907	685	515	618	589	20255	110618
NEW HAMPSHIRE	27 0	78 75	0 15	0 85	0 45	0 45	0 65	0 55	18 35	9466
NEW JERSEY	28 0	45 05	1 65	0 75	7 65	8 15	4 95	11 55	12 65	8009
NEW MEXICO	29 0	84360	203	1505	1583	926	485	946	31536	121744
NEW YORK	30 0	11976	1158	3995	5086	5105	4169	8801	9930	50220
NORTH CAROLINA	31 0	14986	232	8 05	10 15	10 25	8 35	17 55	19 85	50767
NORTH DAKOTA	32 0	60698	0	1505	878	418	376	257	6572	71004
OHIO	33 0	9747	482	3561	5182	5626	4420	10490	2326	41834
OKLAHOMA	34 0	50383	415	3763	3570	3735	1930	2355	3464	69615
OREGON	35 0	56588	1110	1940	1640	1650	2239	2413	30349	97929
PENNSYLVANIA	36 0	11397	1206	4458	5143	5250	3136	11117	3551	45278
RHODE ISLAND	37 0	0	0	10	48	145	97	907	0	1207
SOUTH CAROLINA	38 0	11030	1052	3291	3976	4622	1911	2644	2663	31189
SOUTH DAKOTA	39 0	51408	0	811	521	569	290	415	22793	77007
TENNESSEE	40 0	18017	550	3762	4786	5607	3127	3648	2596	42123
TEXAS	41 0	207629	2876	13182	9563	9322	7894	12902	5491	268839
UTAH	42 0	54387	434	1090	627	1293	724	1071	25553	85179
VERMONT	43 0	5954	0	495	897	511	425	347	1023	9852
VIRGINIA	44 0	14195	782	3551	5008	5201	2692	4072	5665	41166
WASHINGTON	45 0	30571	540	2663	2374	2557	2104	3744	2452	69315
WEST VIRGINIA	46 0	10673	174	2374	2606	2963	1129	1467	2721	24107
WISCONSIN	47 0	31334	685	5423	4593	3648	2403	3908	5028	57022
WYOMING	48 0	70233	0	743	540	502	338	405	25225	97986
TOTAL		1761966	28968	145927	136449	140321	91495	177165	551673	58 05

NOTE: "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST CONSTRAINING CRITERIA (i.e. IF > 1/8 OF THE POPULATION ALLOWED BY A UNIFORM DENSITY CRITERION IS FOUND IN A DOUBLE SECTOR OF 45 0 DEGREES) NUMBERS IN THE COLUMNS REPRESENT THAT LAND UNIQUELY CONSTRAINED BY THE GIVEN FRACTIONAL CRITERION. THIS LAND IS CONSIDERED AVAILABLE IF THE CRITERION WERE RELATED IF SECTOR CRITERION IS APPLIED. ASSUME THAT UNIFORM DENSITY CRITERION IS ALSO IN EFFECT ** COMPOSITE OF 5 RADII **

TABLE F2.7

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 750 #/SQ MI *** DOUBLE SECTOR (45 0 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION		AVAILABLE LAND								
		> 1/8 ALLOWABLE POP	> 1/6 ALLOWABLE POP	> 1/4 ALLOWABLE POP	> 1/3 ALLOWABLE POP	> 1/2 ALLOWABLE POP	UNIFORM DENSITY	RESTRICTED LANDS		
ALABAMA	1 0	29934	850	4024	4190	5143	2895	2856	2073	51907
ARIZONA	2 0	48308	998	1505	897	1293	656	1679	59405	114341
ARKANSAS	3 0	25531	492	4678	2712	1958	1119	1514	6263	53258
CALIFORNIA	4 0	75270	1197	5732	4526	5134	3686	13327	51492	160364
COLORADO	5 0	61174	511	1698	1361	1843	1216	1862	28660	160325
CONNECTICUT	6 0	134	106	376	502	685	444	2943	0	5210
DELAWARE	7 0	702	77	376	297	212	174	396	29	2326
FLORIDA	8 0	26422	753	3763	2328	3136	3179	4465	13105	59357
GEORGIA	9 0	32009	397	4246	4738	4844	2731	3812	3667	58604
IDAHO	10 0	41920	125	830	917	889	666	685	37519	83550
ILLINOIS	11 0	32134	907	5674	3650	3841	2355	4417	1301	56539
INDIANA	12 0	13066	840	4767	4786	1584	3117	4199	1322	36341
IOWA	13 0	42547	1062	4574	2827	2065	1197	1795	0	56067
KANSAS	14 0	72008	963	2548	1911	1747	1148	1747	193	82267
KENTUCKY	15 0	20312	193	2384	2754	4186	2818	2152	2470	40270
LOUISIANA	16 0	20564	811	3098	3570	2413	1428	1853	14417	48154
MAINE	17 0	27989	0	1303	1322	1529	791	791	357	34074
MARYLAND	18 0	2885	106	897	897	1148	1474	3599	143	11153
MASSACHUSETTS	19 0	859	174	830	579	724	830	4632	0	8626
MICHIGAN	20 0	27850	926	4622	4854	4101	3271	6533	9479	61836
MINNESOTA	21 0	48414	114	3088	2584	8441	1785	2857	24926	89913
MISSISSIPPI	22 0	28207	280	4082	3008	3320	1573	1583	3841	47884
MISSOURI	23 0	48983	270	4265	4034	3252	1756	2856	4516	69932
MONTANA	24 0	98179	0	917	733	618	434	412	47180	148456
NEBRASKA	25 0	70040	125	2220	1042	1245	666	849	1534	77721
NEVADA	26 0	87719	193	733	367	550	338	465	20255	110418
NEW HAMPSHIRE	27 0	4661	97	618	704	801	444	946	1197	9468
NEW JERSEY	28 0	4925	105	635	745	835	475	1003	1243	8009
NEW MEXICO	29 0	14678	482	4178	4613	5201	3913	7423	9930	50218
NEW YORK	30 0	2923	105	835	925	1045	705	1725	1985	50768
NORTH CAROLINA	31 0	18403	347	4033	4294	4890	3821	433	8627	50768
NORTH DAKOTA	32 0	61132	0	1573	733	328	357	299	6572	71005
OHIO	33 0	11329	647	4150	3755	5684	4217	8104	2326	41834
OKLAHOMA	34 0	52274	714	3879	2731	2799	1849	2084	3444	69614
OREGON	35 0	58913	135	1756	1293	1698	1795	1988	30349	97927
PENNSYLVANIA	36 0	14378	666	4178	4130	5452	3908	9013	3551	45276
RHODE ISLAND	37 0	3185	193	296	318	463	608	3433	0	1206
SOUTH CAROLINA	38 0	13549	743	2422	3387	4207	1920	2297	2663	31188
SOUTH DAKOTA	39 0	51965	0	840	482	270	280	376	22793	77006
TENNESSEE	40 0	19937	656	3300	4275	4970	3175	3213	2596	42122
TEXAS	41 0	21712	1361	11020	8996	9640	5887	10171	5491	268839
UTAH	42 0	55381	251	1168	656	782	463	926	25537	85180
VERMONT	43 0	6128	0	676	791	502	396	338	1023	9854
VIRGINIA	44 0	16164	473	3599	4362	5095	1364	3445	5665	41167
WASHINGTON	45 0	32192	830	2268	2374	2104	1698	3088	24762	69316
WEST VIRGINIA	46 0	11361	0	1872	2654	2808	1177	1312	2721	24105
WISCONSIN	47 0	34016	125	4719	4130	3590	2268	3146	5028	57022
WYOMING	48 0	70677	0	733	386	328	270	367	25225	97966
TOTAL		1849701	19801	131151	121809	129952	82244	148018	557673	

NOTE: "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST CONSTRAINING CRITERIA (I.E. IF > 1/8 OF THE POPULATION ALLOWED BY A UNIFORM DENSITY CRITERION IS FOUND IN A DOUBLE SECTOR OF 45 0 DEGREES) NUMBERS IN THE COLUMNS REPRESENT THAT LAND UNIQUELY CONSTRAINED BY THE GIVEN FRACTIONAL CRITERION. THIS LAND IS CONSIDERED AVAILABLE IF THE CRITERION WERE RELAXED IF SECTOR CRITERION IS APPLIED. ASSUME THAT UNIFORM DENSITY CRITERION IS ALSO IN EFFECT. ** COMPOSITE OF 5 RADII **

NOTE: AVAILABLE LAND IS THAT WHICH IS NOT CON-
 SIDERED AVAILABLE IN THE FEDERAL CENSUS BY A UNIFORM DENSITY CRITERION IN A 1/2 DEGREE
 OR 1/4 DEGREE SQUARE MILE AREA. UNIFORM DENSITY CRITERION THIS
 LAND IS CONSIDERED AVAILABLE IN THE FEDERAL CENSUS BY A UNIFORM DENSITY
 CRITERION IS ALSO IN EFFECT. ** COMPOSITE OF 3 RADII **

STATE	1/4	1/2	3/4	TOTAL
ALABAMA	1 0	20834	2244	23078
ARIZONA	2 0	47375	473	47848
ARKANSAS	3 0	37452	318	37770
CALIFORNIA	4 0	45988	1805	47793
COLORADO	5 0	43956	302	44258
CONNECTICUT	6 0	43 25	2 75	46
DELAWARE	7 0	40 25	1 25	41 50
FLORIDA	8 0	22147	1033	23180
GEORGIA	9 0	32134	2384	34518
IDAHO	10 0	54 95	1 15	56 10
ILLINOIS	11 0	29449	1218	30667
INDIANA	12 0	12323	1476	13799
IOWA	13 0	42074	820	42894
KANSAS	14 0	71810	544	72354
KENTUCKY	15 0	31124	830	31954
LOUISIANA	16 0	20730	4479	25209
MAINE	17 0	20603	423	21026
MARYLAND	18 0	30594	231	30825
MASSACHUSETTS	19 0	27 45	2 25	29 70
MICHIGAN	20 0	20441	704	21145
MINNESOTA	21 0	50585	212	50797
MISSISSIPPI	22 0	32030	724	32754
MISSOURI	23 0	31314	1255	32569
MONTANA	24 0	20874	0	20874
NEBRASKA	25 0	45517	838	46355
NEVADA	26 0	67139	232	67371
NEW HAMPSHIRE	27 0	4487	347	4834
NEW JERSEY	28 0	20	87	107
NEW MEXICO	29 0	6448	241	6689
NEW YORK	30 0	12819	2108	14927
OHIO	31 0	16330	1428	17758
NORTH CAROLINA	32 0	32 45	2 85	35 30
NORTH DAKOTA	33 0	42144	0	42144
OHIO	34 0	10721	1013	11734
OKLAHOMA	35 0	52630	374	53004
OREGON	36 0	54334	1488	55822
PENNSYLVANIA	37 0	11628	1447	13075
RHODE ISLAND	38 0	0 00	0 00	0
SOUTH CAROLINA	39 0	12533	1013	13546
SOUTH DAKOTA	40 0	15224	0	15224
TENNESSEE	41 0	20919	888	21807
Texas	42 0	21294	2427	23721
UTAH	43 0	54232	618	54850
VERMONT	44 0	63 75	0 75	64 50
VIRGINIA	45 0	1472	1344	2816
WASHINGTON	46 0	30947	502	31449
WEST VIRGINIA	47 0	12631	407	13038
WISCONSIN	48 0	34271	1332	35603
WYOMING	49 0	20242	0	20242
TOTAL	180371	24443	180054	362420

TABLE F.2.9
 POPULATION DENSITY - 1900
 STATE AREAS IN SQUARE MILES AND 1/4 OR STATE
 DENSITY = 250 * SQ MI *** 1/4 DEGREE SECTION (90 0 DEGREES)
 POPULATION SECTION AVAILABLE - TOTAL U S
 AVAILABLE LAND
 > 1/4 ALLOWABLE FOR
 > 1/2 ALLOWABLE FOR
 > 3/4 ALLOWABLE FOR
 UNIFORM DENSITY
 RESTRICTED LANDS

TABLE F2.10

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 500 #/SQ MI *** "QUAD" SECTOR (90.0 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION		AVAILABLE LAND		> 1/4 ALLOWABLE POP		> 1/3 ALLOWABLE POP		> 1/2 ALLOWABLE POP		UNIFORM DENSITY	RESTRICTED LANDS
ALABAMA	1 0	35888	376	6253	3985	3329	2075	51906			
ARIZONA	2 0	49244	936	1168	1563	2026	59405	114342			
ARKANSAS	3 0	40501	87	2779	1872	1756	6263	53258			
CALIFORNIA	4 0	75062	1612	6282	5800	16115	51492	140363			
COLORADO	5 0	49210	193	1776	1991	2490	28630	104327			
CONNECTICUT	6 0	164	164	482	666	2735	0	5211			
DELAWARE	7 0	1206	58	247	251	425	39	2366			
FLORIDA	8 0	28381	811	4642	5288	7131	13105	59358			
GEORGIA	9 0	36687	309	5239	453	4429	5867	58604			
IDAHO	10 0	43435	0	926	926	743	37519	83549			
ILLINOIS	11 0	38166	463	4738	3976	7836	1361	56540			
INDIANA	12 0	18991	704	5182	4844	5298	1322	36341			
INDIA	13 0	48356	193	3291	2152	2075	0	56067			
KANSAS	14 0	75309	434	1949	2335	2046	193	82266			
KENTUCKY	15 0	25080	193	4282	3561	2683	2470	40269			
LOUISIANA	16 0	25765	492	3156	2123	2200	14417	48153			
MAINE	17 0	30224	0	1669	975	849	357	34074			
MARYLAND	18 0	4014	222	1081	1187	4507	145	11156			
MASSACHUSETTS	19 0	1081	261	1139	1033	5115	0	8629			
MICHIGAN	20 0	33852	1409	4902	4023	7672	9679	61827			
MINNESOTA	21 0	52766	164	2566	2142	3329	24926	85913			
MISSISSIPPI	22 0	4145	0	27	301	255	2901	47883			
MISSOURI	23 0	55661	290	3039	2943	3464	4516	69933			
MONTANA	24 0	99491	0	647	704	454	47160	148456			
NEBRASKA	25 0	72385	183	1177	1390	1052	1534	77721			
NEVADA	26 0	80239	434	347	733	589	20255	110617			
NEW HAMPSHIRE	27 0	7981	0	43	0	77	183	9466			
NEW JERSEY	28 0	5833	143	923	693	1131	1263	8010			
NEW MEXICO	29 0	86821	724	782	936	946	31536	121745			
NEW YORK	30 0	19474	1187	5385	5443	8801	9930	50220			
NORTH CAROLINA	31 0	23662	946	7491	4806	5037	8627	50769			
NORTH DAKOTA	32 0	62947	0	685	444	357	6572	71005			
OHIO	33 0	16434	1033	5423	6128	10490	2326	41834			
OKLAHOMA	34 0	56192	1100	3754	2750	2355	3464	69615			
OREGON	35 0	60689	154	1689	2634	2613	30349	97928			
PENNSYLVANIA	36 0	18721	1380	6002	4507	11117	3551	45278			
RHODE ISLAND	37 0	19	10	58	212	907	0	1206			
SOUTH CAROLINA	38 0	18132	145	5018	2586	2644	2663	31188			
SOUTH DAKOTA	39 0	52785	0	608	405	415	22793	77006			
TENNESSEE	40 0	4833	0	0	0	0	2963	42123			
TEXAS	41 0	229207	1891	9003	10345	12902	5491	268839			
UTAH	42 0	55816	482	1293	965	1071	25552	85180			
VERMONT	43 0	7421	29	550	482	347	1023	9852			
VIRGINIA	44 0	21635	637	5452	3706	4072	5665	41167			
WASHINGTON	45 0	34692	386	2712	3020	3744	24762	69316			
WEST VIRGINIA	46 0	15459	0	2750	1708	1467	2721	28105			
WISCONSIN	47 0	40935	193	3937	3020	3908	5028	57021			
WYOMING	48 0	71400	0	579	376	405	25225	97985			
TOTAL		201562	21627	145462	122968	177165	557673				
		66.3%	0.7%	4.8%	4.0%	5.8%	16.3%				

NOTE "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST CON-
 STRAINING CRITERIA (1) * IF > 1/4 OF THE POPULATION ALLOWED
 BY A UNIFORM DENSITY CRITERION IS FOUND IN A "QUAD" SECTOR
 OF 90.0 DEGREE; NUMBERS IN THE COLUMNS REPRESENT THAT LAND
 UNILATERALLY CONSTRAINED BY THE GIVEN FRACTIONAL CRITERION. THIS
 LAND IS CONSIDERED AVAILABLE IF THE CRITERION WERE RELAXED.
 IF SECTOR CRITERION IS APPLIED, ASSUME THAT UNIFORM DENSITY
 CRITERION IS ALSO IN EFFECT ** COMPOSITE OF 5 RADII **

TABLE F2.11

POPULATION SECTOR ANALYSIS - TOTAL U. S.
 DENSITY = 750 #/50 MI *** "QUAD" SECTOR (90 0 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION		AVAILABLE LAND						
			> 1/4 ALLOWABLE POP	> 1/3 ALLOWABLE POP	> 1/2 ALLOWABLE POP	UNIFORM DENSITY RESTRICTED LANDS		
ALABAMA	1 0	37838	482	4950	3706	2896	2075	51907
		72 9%	0 9%	9 5%	7 1%	5 5%	4 0%	
ARIZONA	2 0	50614	328	1226	1090	1679	59405	114342
		44 3%	0 3%	1 1%	1 0%	1 5%	52 0%	
ARKANSAS	3 0	41630	203	2075	1534	1554	6263	53259
		78 2%	0 4%	3 9%	2 9%	2 9%	11 8%	
CALIFORNIA	4 0	83820	1033	5058	5684	13527	51492	160364
		52 3%	0 4%	3 1%	3 5%	8 3%	32 1%	
COLORADO	5 0	70300	174	1457	1872	1062	28660	104325
		67 4%	0 2%	1 4%	1 8%	1 2%	27 5%	
CONNECTICUT	4 0	415	193	1023	637	2943	0	5211
		8 0%	3 7%	19 6%	12 2%	56 3%	0 0%	
DELAWARE	7 0	1080	19	280	212	396	39	2324
		59 3%	0 8%	12 0%	9 1%	17 0%	1 7%	
FLORIDA	8 0	31112	1042	3802	2831	6465	13105	59357
		52 4%	1 8%	6 4%	4 5%	10 9%	22 1%	
GEORGIA	9 0	40086	280	4912	3648	3812	5867	58605
		68 4%	0 5%	8 4%	6 2%	6 3%	10 0%	
IDAHO	10 0	43705	0	849	791	685	37519	83549
		52 3%	0 0%	1 0%	0 9%	0 8%	44 9%	
ILLINOIS	11 0	40791	444	2908	3619	6417	1361	56540
		72 1%	0 8%	6 9%	6 4%	11 4%	2 4%	
INDIANA	12 0	21346	733	4719	4063	6159	1322	36342
		58 7%	2 0%	13 0%	11 2%	11 4%	3 6%	
IOWA	13 0	50093	261	2094	1824	1795	0	56067
		89 3%	0 5%	3 7%	3 3%	3 2%	0 0%	
KANSAS	14 0	74650	135	1911	1631	1747	193	82267
		93 2%	0 2%	2 3%	2 0%	2 1%	0 2%	
KENTUCKY	15 0	26036	241	6031	3039	2152	2470	40249
		64 7%	0 6%	15 0%	8 3%	5 3%	6 1%	
LOUISIANA	16 0	27464	10	2702	1708	1853	14417	48154
		57 0%	0 0%	3 6%	3 3%	3 8%	29 9%	
MAINE	17 0	30494	0	1534	897	791	357	34073
		89 5%	0 0%	4 3%	2 4%	2 3%	1 0%	
MARYLAND	18 0	4439	125	1052	1795	3599	145	11155
		39 8%	1 1%	9 4%	16 1%	32 3%	1 3%	
MASSACHUSETTS	19 0	1785	376	820	1013	4632	0	8626
		20 7%	4 4%	9 5%	11 7%	53 7%	0 0%	
MICHIGAN	20 0	36882	222	4429	4092	6533	9679	61837
		59 6%	0 4%	7 2%	6 6%	10 6%	15 7%	
MINNESOTA	21 0	53529	193	2314	2293	2257	24926	85914
		62 3%	0 2%	2 7%	2 8%	3 0%	29 0%	
MISSISSIPPI	22 0	27027	145	3310	1978	1983	3841	47884
		77 3%	0 3%	6 9%	4 1%	3 3%	8 0%	
MISSOURI	23 0	54674	328	3030	2528	2556	4516	69332
		81 0%	0 5%	4 3%	3 6%	4 1%	6 5%	
MONTANA	24 0	99723	0	647	511	415	47160	148456
		67 2%	0 0%	0 4%	0 3%	0 3%	31 8%	
NEBRASKA	25 0	72771	357	1245	965	849	1534	77721
		93 6%	0 5%	1 6%	1 2%	1 1%	2 0%	
NEVADA	26 0	88905	0	550	444	463	20255	110617
		80 4%	0 0%	0 5%	0 4%	0 4%	18 3%	
NEW HAMPSHIRE	27 0	5819	125	820	560	946	1197	9467
		61 5%	1 3%	8 7%	5 9%	10 0%	12 6%	
NEW JERSEY	28 0	1110	97	560	811	5433	0	8011
		13 9%	1 2%	7 0%	10 1%	67 8%	0 0%	
NEW MEXICO	29 0	87892	0	936	531	849	21536	121744
		72 2%	0 0%	0 8%	0 4%	0 7%	29 9%	
NEW YORK	30 0	21954	926	3356	4429	7623	9930	50218
		43 7%	1 8%	10 7%	8 8%	15 2%	19 8%	
NORTH CAROLINA	31 0	26383	29	6765	4632	4333	8627	50769
		52 0%	0 1%	13 3%	9 1%	8 5%	17 0%	
NORTH DAKOTA	32 0	63362	0	347	425	299	6572	71005
		89 2%	0 0%	0 5%	0 6%	0 4%	9 3%	
OHIO	33 0	18750	1148	5867	5636	8106	2326	41833
		44 8%	2 7%	14 0%	13 5%	19 4%	5 6%	
OKLAHOMA	34 0	58132	637	3223	2075	2084	3864	69615
		83 5%	0 9%	4 6%	3 0%	3 0%	5 0%	
OREGON	35 0	61319	174	1650	2248	1988	30349	97928
		62 8%	0 2%	1 7%	2 3%	2 0%	31 0%	
PENNSYLVANIA	36 0	22041	280	5192	5201	9013	3951	45278
		48 7%	0 6%	11 5%	11 5%	19 9%	7 8%	
RHODE ISLAND	37 0	48	10	193	270	685	0	1206
		4 0%	0 8%	16 0%	22 4%	56 8%	0 0%	
SOUTH CAROLINA	38 0	19628	0	4275	2326	2297	2663	31189
		62 9%	0 0%	13 7%	7 5%	7 4%	8 5%	
SOUTH DAKOTA	39 0	53162	0	347	328	376	22793	77006
		69 0%	0 0%	0 5%	0 4%	0 5%	29 6%	
TENNESSEE	40 0	27309	116	5269	3619	3213	2596	42122
		64 8%	0 3%	12 5%	8 6%	7 6%	6 2%	
TEXAS	41 0	234659	1042	9486	7990	10171	5491	268839
		87 3%	0 4%	3 5%	3 0%	3 8%	2 0%	
UTAH	42 0	56588	666	724	724	926	25553	85181
		66 4%	0 8%	0 8%	0 8%	1 1%	30 0%	
VERMONT	43 0	7556	0	482	454	338	1023	9853
		76 7%	0 0%	4 9%	4 6%	3 4%	10 4%	
VIRGINIA	44 0	23121	647	5211	3078	3445	5665	41167
		56 2%	1 6%	12 7%	7 5%	8 4%	13 8%	
WASHINGTON	45 0	36332	454	2306	2374	3088	24762	69316
		52 4%	0 7%	3 3%	3 4%	4 5%	35 7%	
WEST VIRGINIA	46 0	15729	0	2876	1467	1312	2721	24105
		65 3%	0 0%	11 9%	6 1%	5 4%	11 3%	
WISCONSIN	47 0	42315	174	3213	3146	3146	5028	57022
		74 2%	0 3%	5 6%	5 5%	5 5%	8 8%	
WYOMING	48 0	71786	0	280	308	367	2525	97986
		73 3%	0 0%	0 3%	0 3%	0 4%	25 7%	
TOTAL		2080704	13849	131258	108457	148018	557673	
		68 4%	0 5%	4 3%	3 6%	4 9%	18 3%	

NOTE "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST CON-
 STRAINING CRITERIA (I.E. IF > 1/4 OF THE POPULATION ALLOWED
 BY A UNIFORM DENSITY CRITERION IS FOUND IN A "QUAD" SECTOR
 OF 90 0 DEGREES) NUMBERS IN THE COLUMNS REPRESENT THAT LAND
 UNIQUELY CONSTRAINED BY THE GIVEN FRACTIONAL CRITERION. THIS
 LAND IS CONSIDERED AVAILABLE IF THE CRITERION WERE RELAXED.
 IF SECTOR CRITERION IS APPLIED. ASSUME THAT UNIFORM DENSITY
 CRITERION IS ALSO IN EFFECT ** COMPOSITE OF 5 RADII **

TABLE F2.12

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY * 1500 #/SQ MI *** "QUAD" SECTOR (90.0 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	AVAILABLE LAND		1/4 ALLOWABLE POP		1/3 ALLOWABLE POP		1/2 ALLOWABLE POP		UNIFORM DENSITY RESTRICTED LANDS
	1/4	1/3	1/4	1/3	1/4	1/3	1/2		
ALABAMA	1 0	39391	0	453a	3213	2492	2075	51907	
ARIZONA	2 0	51820	318	772	589	1438	59405	114342	
ARKANSAS	3 0	42499	0	1747	1274	147a	6262	53259	
CALIFORNIA	4 0	88259	92a	4603	4603	11020	51492	180363	
COLORADO	5 0	71275	389	1187	1129	1486	28680	104326	
CONNECTICUT	6 0	1255	10	67a	598	2473	0	5212	
DELAWARE	7 0	1457	0	241	212	367	39	2326	
FLORIDA	8 0	34479	29	2345	3397	6002	13105	59357	
GEORGIA	9 0	41389	241	4323	3165	3619	5867	58604	
IDAHO	10 0	4398a	0	772	637	67a	37519	83550	
ILLINOIS	11 0	42981	454	3464	2634	5449	1361	56539	
INDIANA	12 0	23980	135	3889	3204	3812	1322	36342	
IOWA	13 0	51299	0	1785	1322	1860	0	56066	
KANSAS	14 0	77866	39	1293	1245	1831	193	82267	
KENTUCKY	15 0	27097	48	561a	2972	2065	2470	40268	
LOUISIANA	16 0	28217	0	230a	1448	176a	14417	48154	
MAINE	17 0	30581	0	147a	878	782	357	34074	
MARYLAND	18 0	4854	0	318	1341	1747	2750	11155	
MASSACHUSETTS	19 0	2663	29	685	1177	4063	0	8627	
MICHIGAN	20 0	38571	116	3802	3928	5742	9679	61838	
MINNESOTA	21 0	54214	367	2345	1872	2191	2492a	85915	
MISSISSIPPI	22 0	37503	0	3098	1727	1919	3841	47884	
MISSOURI	23 0	57987	222	2721	1930	2537	491a	69933	
MONTANA	24 0	100051	0	463	37a	405	47160	148455	
NEBRASKA	25 0	73909	0	859	618	801	1534	77721	
NEVADA	26 0	8944a	0	290	251	37a	20255	110618	
NEW HAMPSHIRE	27 0	6118	0	695	349	888	1197	9467	
NEW JERSEY	28 0	1602	145	511	1563	4188	0	8009	
NEW MEXICO	29 0	88404	0	5a9	454	782	3153a	121745	
NEW YORK	30 0	24907	58	4314	4014	697a	9930	50219	
NORTH CAROLINA	31 0	27282	0	6485	4188	4217	8627	50749	
NORTH DAKOTA	32 0	62458	0	357	328	290	6572	71005	
OHIO	33 0	22861	290	452a	4709	7122	232a	41834	
OKLAHOMA	34 0	59878	0	25a7	1824	1882	3464	69615	
OREGON	35 0	62744	0	1206	177a	1853	30349	97928	
PENNSYLVANIA	36 0	23440	318	5172	4709	8087	3951	45277	
RHODE ISLAND	37 0	270	0	145	193	598	0	1206	
SOUTH CAROLINA	38 0	20159	0	3995	2152	2220	2663	31189	
SOUTH DAKOTA	39 0	53297	0	241	309	367	22793	77007	
TENNESSEE	40 0	28342	0	4757	3329	3098	259a	42122	
TEXAS	41 0	241327	975	6880	5481	8685	5491	268839	
UTAH	42 0	57823	0	425	579	801	25553	85181	
VERMONT	43 0	7703	0	473	434	338	1023	9853	
VIRGINIA	44 0	25090	58	4613	2606	313a	5665	41160	
WASHINGTON	45 0	38108	280	1592	1882	2492	24762	6931a	
WEST VIRGINIA	46 0	16038	0	2625	1419	1303	2721	24106	
WISCONSIN	47 0	43319	203	3098	2567	2808	5028	57023	
WYOMING	48 0	71912	0	193	290	367	25225	97987	
TOTAL		214133	6178	112074	90981	131928	557673		
		70.4%	0.2%	3.7%	3.0%	4.3%	18.3%		

NOTE: "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST CONSTRAINING CRITERIA (1) * IF > 1.4 OF THE POPULATION ALLOWED BY A UNIFORM DENSITY CRITERION IS FOUND IN A "QUAD" SECTOR OF 90.0 DEGREES; NUMBERS IN THE COLUMNS REPRESENT THAT LAND UNIQUELY CONSTRAINED BY THE GIVEN FRACTIONAL CRITERION. THIS LAND IS CONSIDERED AVAILABLE IF THE CRITERION WERE RELAXED IF SECTOR CRITERION IS APPLIED. ASSUME THAT UNIFORM DENSITY CRITERION IS ALSO IN EFFECT ** COMPOSITE OF 5 44011 **

TABLE F2.13

POPULATION SECTOR ANALYSIS - TOTAL U. S.
 DENSITY = 250 #/SQ MI *** SINGLE SECTOR (22.5 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	1/16 POP IN SECTOR		1/8 POP IN SECTOR		1/4 POP IN SECTOR		1/2 POP IN SECTOR		UNIFORM DENSITY		NO POP CRITERIA NO RESTRICTIONS
	>	IN SECTOR	>	IN SECTOR	>	IN SECTOR	>	IN SECTOR	>	IN SECTOR	
ALABAMA	1 0	14390	20352	24424	30098	35967	41773	44129	49833	51907	
ARIZONA	2 0	44033	44863	43166	48144	49212	50942	51609	54937	114743	
ARKANSAS	3 0	23994	27059	32019	36998	40665	43010	43830	46999	53298	
CALIFORNIA	4 0	52978	40198	44375	72040	78426	83928	84048	100871	140364	
COLORADO	5 0	98527	61123	64095	66624	67224	70580	71719	75066	104326	
CONNECTICUT	6 0	10	10	19	114	182	263	222	5211	5811	
DELAWARE	7 0	309	386	447	444	1332	1544	1479	2287	2326	
FLORIDA	8 0	10749	15327	19428	23138	28530	32649	34856	46252	59387	
GEORGIA	9 0	14347	20439	25334	33186	38289	43298	45722	52337	88604	
IDAHO	10 0	35486	37809	40019	41736	43098	44380	44824	46031	83573	
ILLINOIS	11 0	11999	15151	23009	31804	37994	42103	43306	53170	56339	
INDIANA	12 0	3020	4642	8294	14002	19011	22986	24472	35020	36342	
INDIA	13 0	24238	28767	36911	43242	48038	51338	52255	56067	86067	
KANSAS	14 0	49379	62980	67801	72008	74824	77576	78358	82073	82266	
KENTUCKY	15 0	11368	14225	17052	20574	24849	31391	33485	37799	40247	
LOUISIANA	16 0	11433	13978	14704	21093	23640	28940	30012	33736	48184	
MAINE	17 0	23334	24772	26750	28593	30214	31814	32414	33717	34074	
MARYLAND	18 0	994	1602	2298	3242	4130	4912	5269	11011	11135	
MASSACHUSETTS	19 0	58	251	415	840	1177	1373	1853	8627	8627	
MICHIGAN	20 0	20024	20809	24436	29329	34007	37329	38735	52158	61827	
MINNESOTA	21 0	37280	38359	43567	49862	52949	55499	56356	60988	85914	
MISSISSIPPI	22 0	18258	20603	24868	30137	35973	40074	41138	44043	4882	
MISSOURI	23 0	33294	36969	44274	51261	55671	59077	60062	65417	69934	
MONTANA	24 0	92204	94296	94622	98401	99356	100109	100476	101294	148436	
NEBRASKA	25 0	63815	64394	66932	70059	71941	73643	74016	76187	77721	
NEVADA	26 0	85792	85492	86445	87275	88064	88944	89185	90363	110618	
NEW HAMPSHIRE	27 0	2818	3088	3766	4865	5570	6128	6369	8270	9467	
NEW JERSEY	28 0	0	0	96	492	685	926	1081	8010	8010	
NEW MEXICO	29 0	0 0%	0 0%	1 2%	4 1%	8 6%	11 6%	13 5%	100 0%	100 0%	
NEW YORK	30 0	80346	81320	83337	85045	86239	88153	88732	90608	121734	
NORTH CAROLINA	31 0	6919	9486	12950	18991	23893	30687	33032	42142	50749	
NORTH DAKOTA	32 0	54088	56018	59955	61905	62908	63487	63960	64433	71005	
OHIO	33 0	1872	4101	7305	12005	18608	20333	21732	29807	41833	
OKLAHOMA	34 0	39433	43213	48375	52621	56800	60930	62107	66151	69615	
OREGON	35 0	49794	52139	54918	58450	60206	62214	62420	65719	97928	
PENNSYLVANIA	36 0	3590	4685	9804	14697	18789	23044	24240	41727	45278	
RHODE ISLAND	37 0	0	0	0	0	29	48	68	1206	1206	
SOUTH CAROLINA	38 0	5742	7865	10258	13577	17920	22523	23700	28529	31189	
SOUTH DAKOTA	39 0	18 4%	29 2%	32 9%	43 6%	57 3%	72 2%	74 0%	91 3%	100 0%	
TENNESSEE	40 0	46918	48723	50412	52149	52993	53384	53596	54214	77007	
TEXAS	41 0	11435	14060	16878	20873	25756	31179	33350	39526	42122	
UTAH	42 0	27 1%	33 4%	40 1%	49 6%	61 1%	74 0%	79 2%	93 8%	100 0%	
VERMONT	43 0	16613	17819	19432	21397	22894	23851	24208	26349	28839	
VIRGINIA	44 0	61 8%	66 8%	73 1%	80 3%	85 0%	88 8%	90 2%	98 0%	100 0%	
WASHINGTON	45 0	52264	52728	54117	55198	56099	57128	57543	59627	85181	
WEST VIRGINIA	46 0	61 4%	61 9%	63 3%	64 8%	65 8%	67 1%	67 4%	70 0%	100 0%	
WISCONSIN	47 0	3889	4468	5443	6437	7431	7981	8270	8830	9853	
WYOMING	48 0	39 5%	45 3%	55 2%	65 7%	75 4%	81 0%	83 9%	89 4%	100 0%	
	49 0	4774	9775	12989	17225	21867	27019	28902	35502	41167	
	50 0	16 5%	23 7%	31 6%	41 8%	53 1%	66 4%	70 2%	86 2%	100 0%	
	51 0	22890	25640	28757	32094	34972	37114	38653	44554	45314	
	52 0	33 0%	37 0%	41 5%	46 3%	50 5%	53 5%	55 2%	64 3%	100 0%	
	53 0	3074	7595	9882	12757	15498	18239	19107	21884	24106	
	54 0	21 1%	31 5%	41 0%	52 9%	64 3%	75 7%	79 3%	88 7%	100 0%	
	55 0	19597	23343	28063	35066	40733	44622	45866	51994	57022	
	56 0	34 4%	40 9%	50 6%	62 6%	71 4%	78 3%	80 4%	91 2%	100 0%	
	57 0	65330	7114	13901	7464	71246	71883	72211	72761	97986	
	58 0	66 7%	68 5%	70 3%	71 9%	72 7%	73 4%	73 7%	74 3%	100 0%	
TOTAL		1405512	1518712	1681820	1844324	2012560	2150329	2199478	2480289	3039964	
		46 2%	50 0%	55 2%	61 3%	66 2%	70 7%	72 4%	81 7%	100 0%	

NOTE: NUMBERS IN THE COLUMNS REPRESENT THE AMOUNT OF LAND THAT IS CONSIDERED TO BE AVAILABLE IF THE GIVEN CRITERION IS APPLIED. WHENEVER A SECTOR CRITERION IS APPLIED, IT IS ASSUMED THAT A UNIFORM DENSITY CRITERION IS ALSO IN EFFECT. CRITERIA WERE APPLIED TO 5 RADII (2.5, 5, 10, 20, 30) INDIVIDUALLY AND THE RESULTS COMPOSITED.

TABLE F2.15

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 750 #/SQ MI *** SINGLE SECTOR / 22.5 DEGREES
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION		31/16 POP IN SECTOR		1/8 POP IN SECTOR		1/4 POP IN SECTOR		1/3 POP IN SECTOR		1/2 POP IN SECTOR		UNIFORM DENSITY NO POP	CRITERIA NO RESTRICTIONS
		>	>	>	>	>	>	>	>	>	>		
ALABAMA	1 0	21435	30407	33667	36062	39709	44322	46976	49633	51907			
ARIZONA	2 0	47459	48877	50132	51483	52270	52803	53256	53637	53983			
ARKANSAS	3 0	31845	32907	37124	40550	43141	44612	45442	46995	53298			
CALIFORNIA	4 0	71543	75426	80664	85258	89726	93208	95545	100871	160364			
COLORADO	5 0	45380	66961	68640	70406	72028	73099	73803	75666	104326			
CONNECTICUT	6 0	87	257	627	936	1322	1873	2268	5211	5211			
DELAWARE	7 0	437	743	975	1283	1573	1727	1891	2287	2326			
FLORIDA	8 0	25013	27261	30436	32031	34750	37017	39787	46212	59357			
GEORGIA	9 0	28815	31109	34084	37789	42257	46391	48926	52737	58604			
IDAH	10 0	40839	41254	42335	43087	44052	44901	45345	46030	83550			
ILLINOIS	11 0	25167	27857	33423	40627	44815	47566	48761	53179	56539			
INDIANA	12 0	9843	11657	15537	20439	24936	28516	30561	35020	36362			
IOWA	13 0	35647	37001	45220	49537	52342	53731	54272	56066	56066			
KANSAS	14 0	69557	71111	74392	76853	78580	79738	80327	82073	82266			
KENTUCKY	15 0	18980	19676	21404	23623	27338	33284	35647	37799	40269			
LOUISIANA	16 0	18943	20429	22407	25457	28622	30841	31884	33736	48154			
MAINE	17 0	26972	26981	28130	29365	30716	32279	32926	33517	34074			
MARYLAND	18 0	2480	2712	3329	4207	5211	6427	7411	11011	11155			
MASSACHUSETTS	19 0	656	1062	1679	2299	2634	3252	3995	8627	8627			
MICHIGAN	20 0	24067	25978	30533	35049	39353	42894	43625	52158	61837			
MINNESOTA	21 0	43637	43898	49369	52409	55285	57282	58431	60988	85914			
MISSISSIPPI	22 0	25231	26856	29471	33157	38060	41302	42460	44043	47883			
MISSOURI	23 0	43415	44458	50354	54928	59048	61625	62561	65417	69034			
MONTANA	24 0	97494	97494	98411	99434	100128	100563	100881	101296	148456			
NEBRASKA	25 0	48033	48901	71285	73012	74324	75000	75338	76187	77721			
NEVADA	26 0	86956	87757	88491	89060	89427	89735	89899	90363	110618			
NEW HAMPSHIRE	27 0	4169	4333	4883	5452	6166	6948	7324	8270	9667			
NEW JERSEY	28 0	682	869	1110	1457	1831	2036	2577	8010	8010			
NEW MEXICO	29 0	84564	85316	86860	87719	88471	89041	89359	90208	121744			
NEW YORK	30 0	12091	13828	16994	20776	25289	29838	32665	40289	50219			
NORTH CAROLINA	31 0	15594	17862	20477	23488	27531	34267	37809	42162	50769			
NORTH DAKOTA	32 0	59183	59183	61422	62976	63661	63989	64134	64433	71003			
OHIO	33 0	9235	10663	13857	18625	23710	28217	31401	39507	41833			
OKLAHOMA	34 0	50180	52013	55410	57929	60380	62841	64066	66151	69615			
OREGON	35 0	57398	58759	60243	61818	62899	63989	65591	67579	97928			
PENNSYLVANIA	36 0	11368	13655	16887	19879	24443	29529	32713	41727	45278			
RHODE ISLAND	37 0	0	10	39	193	270	396	521	1206	1206			
SOUTH CAROLINA	38 0	11754	14041	15691	17293	20410	24588	26229	28525	31189			
SOUTH DAKOTA	39 0	51193	51193	52293	53027	53661	53673	53837	54214	77007			
TENNESSEE	40 0	18142	19956	22050	24752	28709	33486	36313	39526	42122			
TEXAS	41 0	208662	214230	224189	235103	243788	250003	253177	263349	268039			
UTAH	42 0	56629	55439	56539	57591	57842	58344	58701	59627	85181			
VERMONT	43 0	5481	5491	6205	6813	7662	8154	8492	8830	9853			
VIRGINIA	44 0	14552	16038	18238	21452	25553	29954	32057	35027	41167			
WASHINGTON	45 0	30774	32742	36653	36940	38677	40125	41466	44559	69316			
WEST VIRGINIA	46 0	10721	10866	11792	13635	16251	19088	20072	21384	24106			
MISCELLANEOUS	47 0	29095	30648	35425	39633	43985	47169	48848	51994	57022			
WYOMING	48 0	70262	70262	71072	71564	71912	72163	72194	72761	97986			
TOTAL		1745298	1807107	1929952	2047623	2164506	2271978	2334266	2482287	3039963			

NOTE: NUMBERS IN THE COLUMNS REPRESENT THE AMOUNT OF LAND THAT IS CONSIDERED TO BE AVAILABLE IF THE GIVEN CRITERION IS APPLIED. WHENEVER A SECTOR CRITERION IS APPLIED, IT IS ASSUMED THAT A UNIFORM DENSITY CRITERION IS ALSO IN EFFECT. CRITERIA WERE APPLIED TO 5 RADII (2.5, 10, 20, 30) INDIVIDUALLY AND THE RESULTS COMPOSITED.

TABLE F2.16

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 1500 #/SQ MI *** SINGLE SECTOR (22 5 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION		POPULATION SECTOR ANALYSIS										UNIFORM DENSITY NO POP	CRITERIA NO RESTRICTIONS
		31/16 POP	IN SECTOR	> 1/8 POP	IN SECTOR	> 1/4 POP	IN SECTOR	> 1/3 POP	IN SECTOR	> 1/2 POP	IN SECTOR		
ALABAMA	1 0	32482	23106	34624	30291	29045	44438	47140	49233	51907			
ARIZONA	2 0	43484	51067	11820	82944	32344	52017	32500	54937	114343			
ARKANSAS	3 0	33745	34200	37955	40848	43242	44689	45519	46995	53258			
CALIFORNIA	4 0	79533	82284	87837	89079	92518	95303	97851	100871	140365			
COLORADO	5 0	49461	51231	53531	55531	57531	59531	61531	63531	100031			
CONNECTICUT	6 0	384	495	811	994	1399	2027	2938	5211	5211			
DELAWARE	7 0	741	1331	1052	1303	1573	1754	1920	2287	2324			
FLORIDA	8 0	29384	31944	32733	33794	35155	37413	40250	44232	59357			
GEORGIA	9 0	32279	33071	33174	38049	42441	46735	49118	52737	58404			
IDAHO	10 0	41804	41813	42443	43232	44081	44911	45355	46030	83550			
ILLINOIS	11 0	29712	30424	31493	32142	32844	33527	34227	35170	54539			
INDIANA	12 0	13209	14832	17997	21259	25244	28794	31208	35020	36342			
IOWA	13 0	38448	39140	44629	50074	52477	53827	54407	56047	56047			
KANSAS	14 0	72500	73002	75791	77204	78754	79854	80442	82073	82244			
KENTUCKY	15 0	20429	21074	22434	24047	27474	32929	35734	37799	40249			
LOUISIANA	16 0	21992	22031	23430	25277	28499	30909	31970	33736	48154			
MAINE	17 0	27194	27194	28224	29273	30724	32279	32935	33717	34074			
MARYLAND	18 0	2779	3154	3704	4931	6002	7045	8260	11011	11155			
MASSACHUSETTS	19 0	1380	1853	2094	2480	2943	3590	4544	8427	8427			
MICHIGAN	20 0	27438	28419	32202	35743	39859	41411	41411	42158	41837			
MINNESOTA	21 0	44422	45094	50508	53114	55536	57843	58797	60988	85914			
MISSISSIPPI	22 0	27792	28110	30204	32341	38127	41341	42528	44043	47883			
MISSOURI	23 0	45345	46088	51830	55709	59419	61847	62840	65417	69934			
MONTANA	24 0	97928	97928	98748	99748	100204	100372	100891	101294	148454			
NEBRASKA	25 0	69605	70155	72288	73479	74498	75048	75384	76187	77721			
NEVADA	26 0	88365	88732	89108	89417	89639	89822	89984	90363	110416			
NEW HAMPSHIRE	27 0	4420	4429	4989	5520	6195	6977	7382	8270	9447			
NEW JERSEY	28 0	4473	4683	5273	5873	6543	7373	7803	8743	10003			
NEW MEXICO	29 0	86145	86849	87544	88027	88589	89108	89427	90208	121944			
NEW YORK	30 0	14841	14308	18844	21713	24034	30330	33293	40289	50219			
NORTH CAROLINA	31 0	19232	19338	21134	23787	27744	34412	37925	42142	50749			
NORTH DAKOTA	32 0	59801	59801	61854	63072	63729	63999	64144	64433	71003			
OHIO	33 0	11812	12838	14984	18111	21492	26882	32385	39507	41833			
OKLAHOMA	34 0	53200	54320	54414	58247	60441	63024	64249	64151	69119			
OREGON	35 0	59849	60448	61355	62223	63043	64105	65224	67579	97928			
PENNSYLVANIA	36 0	15102	15363	17785	20514	24984	30108	33440	41727	45278			
RHODE ISLAND	37 0	10	144	251	280	328	444	608	1204	1204			
SOUTH CAROLINA	38 0	15083	15122	16154	17428	20504	24444	26307	28525	31489			
SOUTH DAKOTA	39 0	51999	51999	52515	53094	53471	53483	53847	54214	77007			
TENNESSEE	40 0	20921	21500	22822	25032	28844	33543	36429	39524	42122			
TEXAS	41 0	219402	223282	232082	239242	245421	251209	254443	263348	268839			
UTAH	42 0	55814	56723	57408	57753	57948	58450	58824	59427	85181			
VERMONT	43 0	5407	5414	6273	6842	7472	8154	8492	8830	9853			
VIRGINIA	44 0	14704	17872	19404	21848	25833	30204	32344	35502	41147			
WASHINGTON	45 0	32920	35143	36342	37548	39034	40414	41842	44554	49314			
WEST VIRGINIA	46 0	11124	11134	11947	13455	14270	15097	20082	21384	24104			
WISCONSIN	47 0	31932	32299	34545	40337	44400	47439	49184	51984	57522			
WYOMING	48 0	70812	70812	71313	71442	71970	72143	72294	72741	97984			
TOTAL		1855831	1888350	1987803	2075429	2179874	2284405	2350362	2482284	3037943			

NOTE: NUMBERS IN THE COLUMNS REPRESENT THE AMOUNT OF LAND THAT IS CONSIDERED TO BE AVAILABLE IF THE GIVEN CRITERION IS APPLIED. WHENEVER A SECTOR CRITERION IS APPLIED, IT IS ASSUMED THAT A UNIFORM DENSITY CRITERION IS ALSO IN EFFECT. CRITERIA WERE APPLIED TO 5 RADII (2, 5, 10, 20, 30) INDIVIDUALLY AND THE RESULTS COMBINED.

TABLE F2.17

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 250 8/50 MI *** DOUBLE SECTOR (45.0 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	> 1/8 POP IN SECTOR		> 1/4 POP IN SECTOR		> 1/3 POP IN SECTOR		> 1/2 POP IN SECTOR		UNIFORM DENSITY	NO POP	CRITERIA NO RESTRICTIONS
	POP	IN SECTOR	POP	IN SECTOR	POP	IN SECTOR	POP	IN SECTOR			
ALABAMA	1.0	19667	21201	26817	32762	39575	44129	49233	51667		
ARIZONA	2.0	44969	43267	47756	48266	49726	51603	54937	114243		
ARKANSAS	3.0	26767	29521	35143	38571	41758	43930	46491	53258		
CALIFORNIA	4.0	79695	61142	48747	74439	20944	86068	108071	160364		
COLORADO	5.0	61702	62704	63331	66710	69663	71714	75666	104324		
CONNECTICUT	5.0	10	10	29	106	253	222	5311	5211		
DELAWARE	7.0	444	444	820	1100	1476	1670	2507	2326		
FLORIDA	6.0	13790	16202	21423	25676	30314	37856	44252	59357		
GEORGIA	9.0	20570	21934	29132	36236	42180	49260	52727	58604		
IDAHO	10.0	36182	38329	41312	42281	43965	46021	46030	83950		
ILLINOIS	11.0	17128	18923	26943	33119	39844	43286	55179	56539		
INDIANA	12.0	4709	6012	11001	16241	21201	24472	35320	36342		
IOWA	13.0	32347	33707	40327	44187	49601	52255	56666	56666		
KANSAS	14.0	63166	63581	70173	72558	73839	78358	82073	82266		
KENTUCKY	15.0	14272	14822	18942	23498	30154	33486	37799	40269		
LOUISIANA	16.0	12931	14378	18972	22842	27599	30011	33736	48154		
MAINE	17.0	25399	25466	27927	29683	31584	32414	33717	36074		
MARYLAND	18.0	1373	1421	2876	3646	4729	5269	11011	11139		
MASSACHUSETTS	19.0	174	261	549	897	1370	1853	2627	2627		
MICHIGAN	20.0	22562	22899	27088	31449	36178	38735	52188	61837		
MINNESOTA	21.0	48338	43397	48520	51321	54426	56386	60988	89114		
MISSISSIPPI	22.0	21214	22798	27860	32739	38352	41138	44043	47883		
MISSOURI	23.0	41061	41765	49109	53422	57591	60062	65417	69934		
MONTANA	24.0	47444	43554	47494	48941	49839	100476	101296	148456		
NEBRASKA	25.0	65475	63890	68467	70908	72423	74015	76187	77721		
NEVADA	26.0	85883	86020	87024	87428	88404	89156	90363	110618		
NEW HAMPSHIRE	27.0	3194	3310	4400	5336	6021	6369	8270	9467		
NEW JERSEY	28.0	0	19	114	403	840	1081	8009	8009		
NEW MEXICO	29.0	82363	82488	84370	85383	87091	88732	90289	121744		
NEW YORK	30.0	7669	8231	12477	16736	21923	25862	40289	50219		
NORTH CAROLINA	31.0	8463	9766	14871	21732	29201	33032	42142	50769		
NORTH DAKOTA	32.0	58209	58826	61413	62078	63024	63760	64433	71005		
OHIO	33.0	3931	4632	9187	14186	18673	21732	39507	41833		
OKLAHOMA	34.0	44081	43809	50336	54011	58498	62107	66151	69615		
OREGON	35.0	32149	32036	36221	38817	41044	43420	47379	57928		
PENNSYLVANIA	36.0	5790	6842	11696	16403	21693	24260	41727	45278		
RHODE ISLAND	37.0	0	0	0	10	58	68	1206	1206		
SOUTH CAROLINA	38.0	7537	7990	11416	15190	21182	23700	28329	31189		
SOUTH DAKOTA	39.0	48635	49379	51413	52222	52950	53596	54214	77007		
TENNESSEE	40.0	14050	14726	18885	23199	29577	33390	39526	42122		
TEXAS	41.0	181256	186477	206568	219914	232690	242408	262349	268829		
UTAH	42.0	53220	53422	54494	55208	56423	57543	59627	63181		
VERMONT	43.0	4420	4931	6022	7199	7963	8923	9503	9853		
VIRGINIA	44.0	9325	10634	14813	19811	25334	28902	35502	41167		
WASHINGTON	45.0	24974	26566	29741	32897	35822	38253	44554	67316		
WEST VIRGINIA	46.0	7141	7836	11667	14572	17872	19156	21384	24106		
WISCONSIN	47.0	24849	25823	32350	37953	42991	49866	51994	57022		
WYOMING	48.0	67637	67637	70173	70173	70173	71468	72211	72761		
TOTAL		1544002	1583878	1772988	1925028	2091704	2199677	2402286	3009962		
		50 8%	52 1%	58 3%	63 3%	68 8%	72 4%	81 7%	100 0%		

NOTE: NUMBERS IN THE COLUMNS REPRESENT THE AMOUNT OF LAND THAT IS CONSIDERED TO BE AVAILABLE IF THE GIVEN CRITERION IS APPLIED. WHENEVER A SECTOR CRITERION IS APPLIED, IT IS ASSUMED THAT A UNIFORM DENSITY CRITERION IS ALSO IN EFFECT. CRITERIA WERE APPLIED TO 3 RADII (2, 5, 10, 20, 30) INDIVIDUALLY AND THE RESULTS COMPOSITED.

TABLE F2.18

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 300 / SQ MI *** DOUBLE SECTOR (45 0 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	> 1/8 POP IN SECTOR										UNIFORM DENSITY NO POP CRITERIA NO RESTRICTIONS
	> 1/4 POP IN SECTOR					> 1/2 POP IN SECTOR					
	> 1/3 POP IN SECTOR		> 1/3 POP IN SECTOR		> 1/3 POP IN SECTOR		> 1/3 POP IN SECTOR		> 1/3 POP IN SECTOR		
	POP	%	POP	%	POP	%	POP	%	POP	%	
ALABAMA	1 0	26650	29371	32208	37540	41357	46703	49833	51907		
ARIZONA	2 0	47353	47503	49118	50212	51724	52911	54927	54333		
ARKANSAS	3 0	33917	37208	38547	41341	43280	45239	46998	52258		
CALIFORNIA	4 0	69427	72057	77605	85482	89781	92756	101371	140344		
COLORADO	5 0	63214	63552	68144	69654	71179	73176	75666	104321		
CONNECTICUT	6 0	29	77	309	685	1168	1476	5211	5211		
DELAWARE	7 0	0 55	1 53	5 95	13 13	22 45	28 33	100 03	100 03		
FLORIDA	8 0	28 22	29 52	46 17	61 03	73 03	80 13	98 33	103 03		
GEORGIA	9 0	20342	30156	34981	40154	45394	48700	52727	56604		
IDAHO	10 0	48 43	51 53	57 73	68 93	77 53	82 43	90 03	100 03		
ILLINOIS	11 0	49 23	49 23	51 03	52 23	53 23	54 23	55 23	56 23		
INDIANA	12 0	10731	11599	14241	20796	26316	29722	35020	36342		
IDAHO	13 0	29652	40067	46494	49377	52361	53992	56067	56067		
KANSAS	14 0	70397	70686	74035	76167	76445	80027	82073	82266		
KENTUCKY	15 0	83 63	85 93	90 03	92 63	95 43	97 23	99 83	100 03		
LOUISIANA	16 0	18283	19300	21865	25823	32192	35116	37799	40269		
MAINE	17 0	27474	27474	29056	30397	32077	32868	32717	34074		
MARYLAND	18 0	22 63	23 53	32 03	40 33	50 03	58 33	98 73	100 03		
MASSACHUSETTS	19 0	6 83	8 13	13 33	23 43	32 13	40 73	100 03	100 03		
MICHIGAN	20 0	25650	26557	31546	36477	41341	44887	52158	61837		
MINNESOTA	21 0	47430	47979	50817	53900	59441	57459	60988	85914		
MISSISSIPPI	22 0	26055	26634	31449	36892	40578	42257	44043	47883		
MISSOURI	23 0	47149	47546	52650	56433	59772	61953	65817	69934		
MONTANA	24 0	97803	97803	98884	99440	100312	100843	101296	148456		
NEBRASKA	25 0	48843	49326	71092	72809	73996	75125	76187	77721		
NEVADA	26 0	88 63	89 23	91 53	93 73	95 23	96 73	98 03	100 03		
NEW HAMPSHIRE	27 0	87072	87149	88056	88741	89156	89774	90363	110618		
NEW JERSEY	28 0	78 73	78 83	79 63	80 23	80 63	81 23	81 73	100 03		
NEW MEXICO	29 0	4256	4410	5230	5954	6716	7180	8270	9467		
NEW YORK	30 0	45 03	46 63	55 23	62 93	70 93	75 83	87 43	100 03		
NORTH CAROLINA	31 0	3 43	4 83	10 83	14 73	20 13	26 43	100 03	100 03		
NORTH DAKOTA	32 0	84360	84563	86068	87651	88577	89267	90208	121744		
OHIO	33 0	49 33	49 53	70 73	72 03	72 83	73 33	74 13	100 03		
OKLAHOMA	34 0	11976	13134	17129	22214	27319	31488	40289	50219		
OREGON	35 0	23 83	26 23	34 13	44 23	54 43	62 73	80 23	100 03		
PENNSYLVANIA	36 0	14986	16859	20912	26248	33273	37104	42142	50769		
RHODE ISLAND	37 0	29 53	33 23	41 23	51 73	65 53	73 13	83 03	100 03		
SOUTH CAROLINA	38 0	47149	47546	52650	56433	59772	61953	65817	71005		
TENNESSEE	39 0	67 43	68 03	75 33	80 73	85 53	88 63	93 53	100 03		
TEXAS	40 0	97803	97803	98884	99440	100312	100843	101296	148456		
UTAH	41 0	45 93	45 93	66 63	67 13	67 63	67 63	68 23	100 03		
VERMONT	42 0	88 63	89 23	91 53	93 73	95 23	96 73	98 03	100 03		
VIRGINIA	43 0	87072	87149	88056	88741	89156	89774	90363	110618		
WASHINGTON	44 0	78 73	78 83	79 63	80 23	80 63	81 23	81 73	100 03		
WEST VIRGINIA	45 0	4256	4410	5230	5954	6716	7180	8270	9467		
WISCONSIN	46 0	3 43	4 83	10 83	14 73	20 13	26 43	100 03	100 03		
WYOMING	47 0	84360	84563	86068	87651	88577	89267	90208	121744		
TOTAL	48 0	49 33	49 53	70 73	72 03	72 83	73 33	74 13	100 03		

NOTE: NUMBERS IN THE COLUMNS REPRESENT THE AMOUNT OF LAND THAT IS CONSIDERED TO BE AVAILABLE IF THE GIVEN CRITERION IS APPLIED. WHENEVER A SECTOR CRITERION IS APPLIED, IT IS ASSUMED THAT A UNIFORM DENSITY CRITERION IS ALSO IN EFFECT. CRITERIA WERE APPLIED TO 9 RADII (2, 5, 10, 20, 30) INDIVIDUALLY AND THE RESULTS COMPOSITED.

TABLE F2.19

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 750 #/SQ MI *** DOUBLE SECTOR (45 0 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	POPULATION SECTOR ANALYSIS - TOTAL U.S.												
	> 1/8 POP. IN SECTOR		> 1/6 POP. IN SECTOR		> 1/3 POP. IN SECTOR		> 1/2 POP. IN SECTOR		UNIFORM DENSITY		CRITERIA NO RESTRICTIONS		
	1/8	1/6	1/3	1/2	1/8	1/6	1/3	1/2	1/8	1/6	1/3	1/2	
ALABAMA	1.0	29924	30744	34778	38926	44081	44976	49833	51907				
ARIZONA	2.0	48208	48906	30412	51319	52602	53258	54937	114343				
ARKANSAS	3.0	25531	36023	25672	42363	44322	45442	46993	53230				
CALIFORNIA	4.0	75270	76467	42199	84725	91538	93545	100871	140364				
COLORADO	5.0	47174	47483	49384	70744	72587	73803	75666	104326				
CONNECTICUT	6.0	134	261	637	1139	1824	2268	3211	5211				
DELAWARE	7.0	3.0%	5.0%	12.2%	21.9%	35.0%	43.3%	100.0%	100.0%				
FLORIDA	8.0	762	840	1216	1505	1718	1891	2287	2326				
GEORGIA	9.0	32.8%	36.1%	50.3%	64.7%	73.9%	81.3%	98.3%	100.0%				
IDAHO	10.0	26422	27174	34928	33476	36612	39787	46232	59287				
ILLINOIS	11.0	44.5%	45.6%	52.1%	56.4%	61.7%	67.0%	77.9%	100.0%				
INDIANA	12.0	30029	32364	36412	41290	41195	48936	52737	58604				
IOWA	13.0	34.6%	35.2%	42.3%	45.6%	48.8%	53.9%	60.5%	100.0%				
KENTUCKY	14.0	41900	42045	42875	43792	44679	45345	46030	83550				
LILLINOIS	15.0	50.2%	50.3%	51.3%	52.4%	53.5%	54.7%	55.1%	100.0%				
LOUISIANA	16.0	32124	31042	28716	42561	45407	48701	55179	56559				
MAINE	17.0	56.8%	58.4%	68.5%	79.2%	82.1%	86.2%	97.6%	100.0%				
MARYLAND	18.0	13064	13607	18374	23160	27744	30861	35020	36342				
MASSACHUSETTS	19.0	36.5%	37.4%	50.6%	63.7%	76.3%	84.9%	96.4%	100.0%				
MICHIGAN	20.0	42547	43608	48182	51010	53075	54272	56067					
MINNESOTA	21.0	71.9%	77.8%	83.9%	88.7%	94.7%	96.8%	100.0%	100.0%				
MISSISSIPPI	22.0	72058	72973	73521	77432	79178	80327	82073	82266				
MISSOURI	23.0	87.5%	88.7%	91.8%	94.1%	96.2%	97.5%	99.8%	100.0%				
MONTANA	24.0	20313	20506	22890	26644	32829	35447	37799	40269				
NEBRASKA	25.0	30564	21275	24472	28043	30455	31894	33736	48154				
NEVADA	26.0	42.7%	44.4%	50.8%	56.2%	63.2%	66.2%	70.1%	100.0%				
NEW HAMPSHIRE	27.0	27985	27985	29288	30610	32134	32926	33717	34074				
NEW JERSEY	28.0	82.1%	82.1%	86.0%	89.8%	94.3%	96.4%	99.0%	100.0%				
NEW MEXICO	29.0	25.9%	26.8%	34.9%	42.9%	53.2%	66.4%	98.7%	100.0%				
NEW YORK	30.0	259	1033	1862	2441	3165	3995	8627	8627				
NORTH CAROLINA	31.0	27890	28774	33399	38253	42354	45625	52158	61837				
NORTH DAKOTA	32.0	43.0%	46.5%	54.0%	61.9%	68.5%	73.8%	84.3%	100.0%				
OHIO	33.0	48414	48930	51655	54800	56649	58431	60988	89914				
OKLAHOMA	34.0	56.4%	56.5%	60.1%	63.1%	65.9%	68.0%	71.0%	100.0%				
OREGON	35.0	28207	28487	30549	37377	40897	42660	44042	47883				
PENNSYLVANIA	36.0	38.9%	39.3%	48.0%	58.4%	65.4%	68.7%	92.0%	100.0%				
RHODE ISLAND	37.0	48983	49254	53519	57553	60805	62561	65417	69934				
SOUTH CAROLINA	38.0	70.0%	70.4%	76.5%	82.3%	86.9%	89.5%	93.5%	100.0%				
SOUTH DAKOTA	39.0	98179	98179	99046	99529	100447	100881	101296	148456				
TENNESSEE	40.0	66.1%	66.1%	66.8%	67.2%	67.7%	68.0%	68.2%	100.0%				
TEXAS	41.0	70040	70165	72385	73427	74672	75338	76187	77721				
UTAH	42.0	90.1%	90.3%	93.1%	94.5%	96.1%	96.9%	98.0%	100.0%				
VERMONT	43.0	87719	87912	88645	89562	89999	90363	910618					
VIRGINIA	44.0	79.3%	79.3%	80.1%	80.3%	81.0%	81.2%	81.7%	100.0%				
WASHINGTON	45.0	66.1	4737	8275	6080	4880	7324	8270	9467				
WEST VIRGINIA	46.0	49.2%	50.3%	56.8%	64.2%	72.7%	77.4%	87.4%	100.0%				
WISCONSIN	47.0	7.5%	9.9%	14.8%	18.8%	24.6%	30.2%	100.0%	100.0%				
WYOMING	48.0	85394	85711	87255	88105	88944	89359	90208	121744				
TOTAL		70.1%	70.4%	71.7%	72.4%	73.1%	73.4%	74.1%	100.0%				

NOTE: NUMBERS IN THE COLUMNS REPRESENT THE AMOUNT OF LAND THAT IS CONSIDERED TO BE AVAILABLE IF THE GIVEN CRITERION IS APPLIED. WHENEVER A SECTOR CRITERION IS APPLIED, IT IS ASSUMED THAT A UNIFORM DENSITY CRITERION IS ALSO IN EFFECT. CRITERIA WERE APPLIED TO 2 RADII (2, 5, 10, 20, 30) INDIVIDUALLY AND THE RESULTS COMPOSITED.

TABLE F2.20

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 1500 P/50 MI. *** DOUBLE SECTOR (45 0 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	> 1/8 POP. IN SECTOR		> 1/4 POP. IN SECTOR		> 1/3 POP. IN SECTOR		> 1/2 POP. IN SECTOR		UNIFORM DENSITY NO POP. CRITERIA	NO RESTRICTIONS
	1	2	1	2	1	2	1	2		
ALABAMA	1 0	33958	33958	33958	33958	33958	33958	33958	51907	
ARIZONA	2 0	30478	30478	30478	30478	30478	30478	30478	114343	
KANSAS	3 0	37201	37201	37201	37201	37201	37201	37201	53258	
CALIFORNIA	4 0	81842	81842	81842	81842	81842	81842	81842	140364	
COLORADO	5 0	49229	49229	49229	49229	49229	49229	49229	104326	
CONNECTICUT	6 0	350	350	350	350	350	350	350	5211	
DELAWARE	7 0	1013	1013	1013	1013	1013	1013	1013	2326	
FLORIDA	8 0	31527	31527	31527	31527	31527	31527	31527	59357	
GEORGIA	9 0	34250	34250	34250	34250	34250	34250	34250	98604	
IDAHO	10 0	42460	42460	42460	42460	42460	42460	42460	83556	
ILLINOIS	11 0	35664	35664	35664	35664	35664	35664	35664	56339	
INDIANA	12 0	14110	14110	14110	14110	14110	14110	14110	36342	
INDIA	13 0	45741	45741	45741	45741	45741	45741	45741	96067	
KANSAS	14 0	74913	74913	74913	74913	74913	74913	74913	82266	
KENTUCKY	15 0	21598	21598	21598	21598	21598	21598	21598	40269	
LOUISIANA	16 0	23112	23112	23112	23112	23112	23112	23112	48154	
MAINE	17 0	28207	28207	28207	28207	28207	28207	28207	34074	
MARYLAND	18 0	3271	3271	3271	3271	3271	3271	3271	11159	
MASSACHUSETTS	19 0	1824	1824	1824	1824	1824	1824	1824	8627	
MICHIGAN	20 0	31305	31305	31305	31305	31305	31305	31305	61837	
MINNESOTA	21 0	49523	49523	49523	49523	49523	49523	49523	88914	
MISSISSIPPI	22 0	29674	29674	29674	29674	29674	29674	29674	47883	
MISSOURI	23 0	30489	30489	30489	30489	30489	30489	30489	49934	
MONTANA	24 0	98575	98575	98575	98575	98575	98575	98575	148486	
NEBRASKA	25 0	71535	71535	71535	71535	71535	71535	71535	77721	
NEVADA	26 0	88712	88712	88712	88712	88712	88712	88712	110618	
NEW HAMPSHIRE	27 0	4912	4912	4912	4912	4912	4912	4912	9467	
NEW JERSEY	28 0	1187	1187	1187	1187	1187	1187	1187	8010	
NEW MEXICO	29 0	87217	87217	87217	87217	87217	87217	87217	121744	
NEW YORK	30 0	17515	17515	17515	17515	17515	17515	17515	30219	
NORTH CAROLINA	31 0	20863	20863	20863	20863	20863	20863	20863	50749	
NORTH DAKOTA	32 0	61741	61741	61741	61741	61741	61741	61741	11005	
OHIO	33 0	14552	14552	14552	14552	14552	14552	14552	41832	
OKLAHOMA	34 0	35922	35922	35922	35922	35922	35922	35922	67615	
OREGON	35 0	40399	40399	40399	40399	40399	40399	40399	79728	
PENNSYLVANIA	36 0	17274	17274	17274	17274	17274	17274	17274	43278	
RHODE ISLAND	37 0	48	48	48	48	48	48	48	1206	
SOUTH CAROLINA	38 0	15961	15961	15961	15961	15961	15961	15961	31189	
SOUTH DAKOTA	39 0	52438	52438	52438	52438	52438	52438	52438	77007	
TENNESSEE	40 0	22398	22398	22398	22398	22398	22398	22398	42122	
TEXAS	41 0	226061	226061	226061	226061	226061	226061	226061	248839	
UTAH	42 0	56684	56684	56684	56684	56684	56684	56684	85181	
VERMONT	43 0	6253	6253	6253	6253	6253	6253	6253	9853	
VIRGINIA	44 0	18470	18470	18470	18470	18470	18470	18470	41147	
WASHINGTON	45 0	35078	35078	35078	35078	35078	35078	35078	69316	
WEST VIRGINIA	46 0	11898	11898	11898	11898	11898	11898	11898	24106	
WISCONSIN	47 0	35753	35753	35753	35753	35753	35753	35753	57022	
WYOMING	48 0	71227	71227	71227	71227	71227	71227	71227	97986	
TOTAL		1946617	1946617	1946617	1946617	1946617	1946617	1946617	3039964	

NOTE: NUMBERS IN THE COLUMNS REPRESENT THE AMOUNT OF LAND THAT IS CONSIDERED TO BE AVAILABLE IF THE GIVEN CRITERION IS APPLIED. WHENEVER A SECTOR CRITERION IS APPLIED, IT IS ASSUMED THAT A UNIFORM DENSITY CRITERION IS ALSO IN EFFECT. CRITERIA WERE APPLIED TO 5 RADII (2, 5, 10, 20, 30) INDIVIDUALLY AND THE RESULTS COMPOSITED.

TABLE F2.21

POPULATION SECTOR ANALYSIS - TOTAL U. S.
 DENSITY = 250 #/SQ MI *** "QUAD" SECTOR (90 0 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	> 1/4 POP		IN SECTOR		UNIFORM DENSITY		CRITERIA NO RESTRICTIONS
	> 1/3	POP	> 1/2	POP	NO POP	IN SECTOR	
ALABAMA	1 0	28834	31198	38175	44129	49823	51907
ARIZONA	2 0	47575	48047	49324	51608	54937	114313
ARKANSAS	2 0	37162	37481	41466	43630	46993	52258
CALIFORNIA	4 0	49268	11072	78068	86048	108871	140364
COLORADO	3 0	45950	64460	64314	71719	75664	104324
CONNECTICUT	4 0	29	48	125	222	5211	5211
DELAWARE	7 0	930	965	1311	1679	2287	2326
FLORIDA	6 0	22147	23119	28882	34834	44232	59357
GEORGIA	9 0	32151	34537	45200	41112	52737	78404
IDAHO	10 0	41585	47049	43447	44824	44030	83550
ILLINOIS	11 0	29249	37465	38417	42386	53179	56339
INDIANA	12 0	12323	13800	14990	24472	25020	24342
IOWA	13 0	33 92	38 01	33 92	47 23	96 41	100 01
KANSAS	14 0	71410	71979	75077	78398	82073	82264
KENTUCKY	15 0	21124	21954	29027	33486	37799	40269
LOUISIANA	16 0	20738	21732	26711	30012	33734	48134
MAINE	17 0	28603	29027	31227	32414	33717	34074
MARYLAND	18 0	3059	3310	4314	5269	11011	11135
MASSACHUSETTS	19 0	482	569	1062	1833	8627	8627
MICHIGAN	20 0	28641	29346	34547	38725	52138	61837
MINNESOTA	21 0	50985	50798	53741	54354	60988	85914
MISSISSIPPI	22 0	32038	32742	37789	41138	44043	47883
MISSOURI	23 0	51319	52573	56443	60062	65417	69934
MONTANA	24 0	98874	98874	99900	100476	101294	148456
NEBRASKA	25 0	66 61	68 61	67 21	67 71	68 21	100 01
NEVADA	26 0	87199	87390	88105	89185	90363	110618
NEW HAMPSHIRE	27 0	4487	4835	5809	6369	8270	9467
NEW JERSEY	28 0	0 41	1 41	7 01	13 51	100 01	100 01
NEW MEXICO	29 0	84949	85190	86782	88732	90208	121744
NEW YORK	30 0	12813	14919	20217	23582	40289	50219
NORTH CAROLINA	31 0	16530	17959	24817	33032	42142	50749
NORTH DAKOTA	32 0	42144	62144	62966	63960	64433	71005
OHIO	33 0	10721	11734	17264	21732	29507	41833
OKLAHOMA	34 0	52420	53027	57775	62107	66151	69613
OREGON	35 0	56354	58054	60303	63420	67579	97928
PENNSYLVANIA	36 0	11428	13548	19985	24260	41727	45278
RHODE ISLAND	37 0	0	0	39	68	1204	1204
SOUTH CAROLINA	38 0	12535	13549	19860	23700	28525	31189
SOUTH DAKOTA	39 0	52224	52224	52853	53594	54214	77007
TENNESSEE	40 0	20979	21867	28332	33350	39524	42122
TEXAS	41 0	212696	216363	229921	242408	263349	268839
UTAH	42 0	54252	54870	55806	57543	59627	85181
VERMONT	43 0	4938	4938	7729	8270	8830	9853
VIRGINIA	44 0	16772	18171	24241	28902	35502	41147
WASHINGTON	45 0	30967	31449	35020	38253	44534	49314
WEST VIRGINIA	46 0	12651	13598	18938	19107	21384	24104
WISCONSIN	47 0	34721	36052	41488	45864	51994	57022
WYOMING	48 0	70792	70792	71410	72211	72741	97984
TOTAL		1830731	1870373	2050431	2199678	2482288	3079964

NOTE: NUMBERS IN THE COLUMNS REPRESENT THE AMOUNT OF LAND THAT IS CONSIDERED TO BE AVAILABLE IF THE GIVEN CRITERION IS APPLIED. WHENEVER A SECTOR CRITERION IS APPLIED, IT IS ASSUMED THAT A UNIFORM DENSITY CRITERION IS ALSO IN EFFECT. CRITERIA WERE APPLIED TO 5 RADII (2, 3, 10, 20, 30) INDIVIDUALLY AND THE RESULTS COMPOSITED.

TABLE F2.22

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 500 8/50 MI *** "QUAD" SECTOR (90 0 DEGREE)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION		> 1/4 POP IN SECTOR		> 1/3 POP IN SECTOR		> 1/2 POP IN SECTOR		UNIFORM DENSITY NO POP	CRITERIA NO RESTRICTIONS
ALABAMA	1.0	25886	34247	42518	44503	41923	31907		
ARIZONA	2.0	45244	50180	51748	52911	54937	115343		
ARKANSAS	3.0	40501	40548	43347	45209	44994	73280		
CALIFORNIA	4.0	79040	80474	86974	92736	100671	140364		
COLORADO	5.0	49210	47402	71178	73174	75444	104324		
CONNECTICUT	6.0	144	328	811	1474	5211	5211		
DELAWARE	7.0	1204	1244	1412	1862	2287	2324		
FLORIDA	8.0	25281	29191	33833	39121	44252	99357		
GEORGIA	9.0	38487	38994	44255	48308	52737	10404		
IDAHO	10.0	47139	43439	44341	45287	44034	13930		
ILLINOIS	11.0	38144	38429	43307	47343	53179	54539		
INDIANA	12.0	18991	19494	24878	29722	35020	34749		
IOWA	13.0	48394	48549	51840	53992	54044	54044		
KANSAS	14.0	73209	73743	77492	80027	82073	82244		
KENTUCKY	15.0	25080	25273	31554	29114	37799	40249		
LOUISIANA	16.0	29745	24298	29413	31334	32734	48154		
MAINE	17.0	30224	30224	31893	32848	33717	34074		
MARYLAND	18.0	4014	4234	5317	4504	11011	11133		
MASSACHUSETTS	19.0	1081	1341	2480	3512	5427	5427		
MICHIGAN	20.0	33852	35241	40143	44484	52198	41837		
MINNESOTA	21.0	52744	52930	55514	57459	40988	85914		
MISSISSIPPI	22.0	34092	34199	39990	48897	44043	47889		
MISSOURI	23.0	7335	7535	8335	8835	9235	10035		
MONTANA	24.0	99491	99491	100138	100842	101294	148454		
NEBRASKA	25.0	72389	72348	73749	73139	74187	77721		
NEVADA	26.0	88299	88492	89041	89774	90343	110418		
NEW HAMPSHIRE	27.0	9580	9453	4523	7180	8070	9447		
NEW JERSEY	28.0	457	888	1341	2113	3010	3010		
NEW MEXICO	29.0	84821	87545	88324	89242	90208	121744		
NEW YORK	30.0	19474	20441	24049	31488	40289	50219		
NORTH CAROLINA	31.0	23442	24407	32299	37104	42142	50749		
NORTH DAKOTA	32.0	4444	4844	4344	7344	8344	10044		
OHIO	33.0	14434	17447	22890	29018	39507	41833		
OKLAHOMA	34.0	34192	37292	41044	43794	44181	49419		
OREGON	35.0	40489	40843	42532	45144	47279	97928		
PENNSYLVANIA	36.0	18721	20101	24103	30410	41727	45278		
RHODE ISLAND	37.0	19	29	87	299	1204	1204		
SOUTH CAROLINA	38.0	18132	18277	23293	25861	28525	31189		
SOUTH DAKOTA	39.0	52785	52785	53293	53799	54214	77007		
TENNESSEE	40.0	25244	24084	31884	35079	39524	42122		
TEXAS	41.0	229207	231098	240102	250442	243749	248834		
UTAH	42.0	55814	54298	57591	58554	59427	85181		
VERMONT	43.0	7421	7490	8000	8482	8830	9853		
VIRGINIA	44.0	21635	22272	27724	31430	35502	41147		
WASHINGTON	45.0	34492	35079	37789	40810	44554	49314		
WEST VIRGINIA	46.0	19439	19439	18210	19918	21384	24104		
WISCONSIN	47.0	40935	41124	45049	48084	51994	57022		
WYOMING	48.0	71400	71400	71979	72354	72741	97984		
TOTAL		2019442	2034490	2182154	2305121	2482288	3039963		

NOTE: NUMBERS IN THE COLUMNS REPRESENT THE AMOUNT OF LAND THAT IS CONSIDERED TO BE AVAILABLE IF THE GIVEN CRITERION IS APPLIED. WHENEVER A SECTOR CRITERION IS APPLIED, IT IS ASSUMED THAT A UNIFORM DENSITY CRITERION IS ALSO IN EFFECT. CRITERIA WERE APPLIED TO 5, 10, 20, 30, 40, 50, 60, 70, 80, 90, 100 INDIVIDUALLY AND THE RESULTS COMPOSITED.

TABLE F2.23

POPULATION SECTOR ANALYSIS - TOTAL U.S.
 DENSITY = 750 #/SQ MI *** "QUAD" SECTOR (90.0 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	> 1/4 POP. IN SECTOR				> 1/3 POP. IN SECTOR				> 1/2 POP. IN SECTOR				UNIFORM DENSITY NO P.P.	CRITERIA NO RESTRICTIONS
	1	2	3	4	1	2	3	4	1	2	3	4		
ALABAMA	1 0	37828	35320	43271	26976	49833	31907							
ALASKA	2 0	30614	50942	52160	53258	54937	114343							
ARIZONA	3 0	41630	41833	43907	45442	46095	53258							
CALIFORNIA	4 0	63620	64852	67561	69545	70887	140364							
COLORADO	5 0	70300	70474	71931	72803	73664	104328							
CONNECTICUT	6 0	415	428	1471	2268	5211	5211							
DELAWARE	7 0	1380	1399	1474	1891	2307	2307							
FLORIDA	8 0	31112	32134	35954	37787	44252	59757							
GEORGIA	9 0	40084	40344	43278	48724	52737	56434							
IDaho	10 0	43703	43703	44551	45349	44030	83590							
ILLINOIS	11 0	40791	41234	40143	48761	53179	56530							
INDIANA	12 0	21344	22079	24798	26000	35020	36342							
IDAHO	13 0	30093	30354	32448	34272	36647	56067							
KANSAS	14 0	4450	74785	78494	80327	82072	82244							
KENTUCKY	15 0	24070	24277	32308	35447	37799	40249							
LOUISIANA	16 0	27442	27474	30174	31864	32734	48184							
MAINE	17 0	30494	30494	32028	32924	33717	34074							
MARYLAND	18 0	4439	4544	5414	7411	11011	11155							
MASSACHUSETTS	19 0	1789	2162	2782	3999	5627	5627							
MICHIGAN	20 0	34882	37104	41334	45423	52158	61837							
MINNESOTA	21 0	53529	53722	56038	58431	60988	85914							
MISSISSIPPI	22 0	37087	37178	40488	42440	44042	47983							
MISSOURI	23 0	56474	57003	60033	62561	65417	69934							
MONTANA	24 0	99723	99723	100370	100881	101294	148434							
NEBRASKA	25 0	72771	73128	74373	75328	74187	77721							
NEVADA	26 0	88905	88905	89455	89999	90363	110418							
NEW HAMPSHIRE	27 0	9819	9844	1745	7324	8270	9467							
NEW JERSEY	28 0	1110	1204	1744	2577	4010	4010							
NEW MEXICO	29 0	87892	87892	88208	89359	90208	121744							
NEW YORK	30 0	21934	22800	28234	32445	40299	50219							
NORTH CAROLINA	31 0	4373	4543	5423	6303	8023	10023							
NORTH DAKOTA	32 0	26362	26362	27009	27434	28433	71009							
OHIO	33 0	18750	18998	25749	31401	39507	41833							
OKLAHOMA	34 0	98130	98748	11992	14044	14131	18418							
OREGON	35 0	41519	41492	42343	43991	45757	97928							
PENNSYLVANIA	36 0	22041	22300	27932	32713	41727	45278							
RHODE ISLAND	37 0	48	50	251	521	1204	1204							
SOUTH CAROLINA	38 0	19428	19428	20903	24229	28523	31189							
SOUTH DAKOTA	39 0	53162	53162	53509	53837	54214	77007							
TENNESSEE	40 0	27309	27423	32494	36313	39524	42122							
TEXAS	41 0	234439	235701	245187	253177	263349	268839							
UTAH	42 0	54988	57052	57977	58701	59427	85181							
VERMONT	43 0	7934	7934	8038	8492	8830	9833							
VIRGINIA	44 0	23121	23748	28979	32057	35502	41167							
WASHINGTON	45 0	26332	26784	29092	31444	34334	49314							
WEST VIRGINIA	46 0	13729	13729	18403	20072	21384	24104							
WISCONSIN	47 0	42315	42487	43702	48848	51994	57022							
WYOMING	48 0	71784	71784	72044	72394	72761	97984							
TOTAL		2080704	2094548	2225812	2334264	2482288	3079944							

NOTE: NUMBERS IN THE COLUMNS REPRESENT THE AMOUNT OF LAND THAT IS CONSIDERED TO BE AVAILABLE IF THE GIVEN CRITERION IS APPLIED. WHENEVER A SECTOR CRITERION IS APPLIED, IT IS ASSUMED THAT A UNIFORM DENSITY CRITERION IS ALSO IN EFFECT. CRITERIA WERE APPLIED TO 3 RADII (2.5, 10, 20, 30) INDIVIDUALLY AND THE RESULTS COMPOSITED.

TABLE F2.24

POPULATION SECTOR ANALYSIS - TOTAL U. S.
 DENSITY = 1500 N/80 MI *** "QUAD" SECTOR (90 0 DEGREES)
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	> 1/4 POP. IN SECTOR		> 1/3 POP. IN SECTOR		> 1/2 POP. IN SECTOR		UNIFORM DENSITY	NO POP. CRITERIA	NO RESTRICTIONS
	1	2	3	4	5	6			
ALABAMA	1 0	29391	39391	43927	47140	49843	51907		
ARIZONA	2 0	51820	52139	52911	53500	54937	1 47 13		
ARKANSAS	3 0	42499	42499	44245	45919	46705	5 258		
CALIFORNIA	4 0	88299	89125	93760	97951	100871	140344		
COLORADO	5 0	71275	71844	73051	74180	75464	104354		
CONNECTICUT	6 0	1255	1264	1940	2338	5211	5211		
DELAWARE	7 0	1467	1467	1708	1920	2287	2324		
FLORIDA	8 0	34479	34508	34937	40250	44251	58297		
GEORGIA	9 0	41389	41430	43953	49118	52727	88647		
IDAHO	10 0	43944	43944	44718	45375	46030	83850		
ILLINOIS	11 0	42981	43439	44899	47533	55179	56537		
INDIANA	12 0	23790	24115	28004	31228	35020	36342		
IOWA	13 0	51299	51299	53083	54407	56047	56047		
KANSAS	14 0	77844	77904	79198	80442	82073	82244		
KENTUCKY	15 0	27097	27143	32740	35734	37799	40249		
LOUISIANA	16 0	28217	28217	30523	31970	33736	48154		
MAINE	17 0	30581	30581	32057	32935	33717	34074		
MARYLAND	18 0	4854	5172	4514	8240	11011	11155		
MASSACHUSETTS	19 0	2443	2702	3387	4344	5427	5427		
MICHIGAN	20 0	38571	38687	42489	44417	52158	61837		
MINNESOTA	21 0	34214	34580	34925	38797	40988	89914		
MISSISSIPPI	22 0	37703	37703	40800	43288	44042	47883		
MISSOURI	23 0	57907	58209	60930	62840	65417	49934		
MONTANA	24 0	100051	100051	100514	100891	101294	148454		
NEBRASKA	25 0	73909	73909	74748	75384	76187	77721		
NEVADA	26 0	89444	89444	89735	89984	90343	110418		
NEW HAMPSHIRE	27 0	4118	4118	4813	7382	8270	9467		
NEW JERSEY	28 0	1402	1747	2258	3821	8009	8009		
NEW MEXICO	29 0	88404	88404	88973	89427	90208	121744		
NEW YORK	30 0	24707	24943	29278	32293	40289	50219		
NORTH CAROLINA	31 0	27252	27252	33736	37925	42142	50749		
NORTH DAKOTA	32 0	63458	63458	63815	64144	64423	71005		
OHIO	33 0	22841	23150	27474	32085	39907	41833		
OKLAHOMA	34 0	59878	59878	62445	64249	66151	49415		
OREGON	35 0	62744	62744	63951	65724	67979	97928		
PENNSYLVANIA	36 0	23440	23758	28931	33440	41727	49278		
RHODE ISLAND	37 0	270	270	415	408	1204	1204		
SOUTH CAROLINA	38 0	20159	20159	21154	24304	28525	31189		
SOUTH DAKOTA	39 0	53297	53297	53538	53847	54214	77007		
TENNESSEE	40 0	28342	28342	33100	34429	39524	42122		
TEXAS	41 0	241327	242302	249182	254444	263349	268839		
UTAH	42 0	57823	57823	58247	58924	59427	85181		
VERMONT	43 0	7585	7585	8058	8492	8830	9853		
VIRGINIA	44 0	25070	25148	29741	32344	35902	41147		
WASHINGTON	45 0	38108	38388	39980	41842	44554	49314		
WEST VIRGINIA	46 0	14038	14038	18443	20082	21384	24104		
WISCONSIN	47 0	43319	43521	44417	49184	51994	57022		
WYOMING	48 0	71912	71912	72105	72394	72741	97966		
TOTAL		214133	217730	225937	235343	248287	307943		

NOTE: NUMBERS IN THE COLUMNS REPRESENT THE AMOUNT OF LAND THAT IS CONSIDERED TO BE AVAILABLE IF THE GIVEN CRITERION IS APPLIED. WHENEVER A SECTOR CRITERION IS APPLIED, IT IS ASSUMED THAT A UNIFORM DENSITY CRITERION IS ALSO IN EFFECT. CRITERIA WERE APPLIED TO 5, 10, 20, 30, 100-VIDUALLY AND THE RESULTS COMPOSITED.

TABLE F3.1

POPULATION CASE 1 AND ENVIRONMENTAL SUITABILITY LEVELS *** STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	LOW SUITABILITY		MEDIUM SUITABILITY		HIGH SUITABILITY		DENSITY	RESTRICTED DEVELOPMENT	RESTRICTED LANDS
	AREA	%	AREA	%	AREA	%			
ALABAMA	48	5250	8830	15758	8952	10922	184	1911	5192
ARIZONA	2113	3831	15517	27522	1727	4284	191	5704	11404
KANSAS	4687	6958	6321	8972	14192	5877	100	6177	5321
CALIFORNIA	40520	16772	9052	10596	4844	2708	3271	48271	160364
COLORADO	29876	13616	10654	12487	3763	5269	876	2782	104329
CONNECTICUT	290	131	101	121	42	5047	0	0	5211
DELAWARE	0	0	0	0	1216	1071	0	39	2326
FLORIDA	0	0	0	1689	2908	15556	2065	11020	59356
GEORGIA	2220	2625	6890	12873	15739	12391	598	5268	58307
IDAH0	10451	7556	11361	9920	4190	2393	212	37307	83550
ILLINOIS	2799	1457	3792	11831	19618	13681	97	1264	56535
INDIANA	0	434	1216	8321	12506	14543	48	1274	36342
IOWA	10	9023	4803	25756	10094	6391	0	0	56067
KANSAS	15546	26554	15208	13775	5674	5915	0	193	62261
KENTUCKY	3277	8376	9418	5597	917	10113	521	1949	40268
LOUISIANA	0	0	347	4475	20226	6687	3609	10808	48151
MAINE	1197	8309	4374	14784	16027	3252	0	357	34071
MARYLAND	0	212	627	39	3435	6697	29	116	11155
MASSACHUSETTS	203	447	0	347	0	7430	0	0	8627
MICHIGAN	0	0	0	11580	22533	18446	251	9420	61838
MINNESOTA	0	232	1390	25650	26180	7537	704	24222	85915
MISSISSIPPI	0	2355	4294	18036	13249	6108	145	3696	47883
MISSOURI	11406	12400	13579	10171	9235	8666	68	4449	69934
MONTANA	13288	27107	29683	23276	6311	1631	241	46918	148455
NEBRASKA	14157	12036	16019	13365	17196	3213	10	1525	77721
NEVADA	37363	18844	27570	4719	463	1399	425	19831	110618
NEW HAMPSHIRE	141	371	71	13	0	2760	0	1197	9667
NEW JERSEY	0	68	0	0	427	7315	0	0	8010
NEW MEXICO	46831	17929	18258	4449	222	2709	1052	30484	121744
NEW YORK	285	133	13	41	0	21	11	251	50219
NORTH CAROLINA	2374	680	1911	6630	14378	16164	1129	7490	50769
NORTH DAKOTA	8241	12207	17476	16147	11194	1168	29	6543	71005
OHIO	1119	3735	1737	3204	7778	21934	608	1718	41833
OKLAHOMA	7923	11329	19570	12709	7016	7604	290	3175	69616
OREGON	111	161	281	181	101	111	0	51	97929
PENNSYLVANIA	251	19869	12256	24926	4101	6176	232	30118	45278
RHODE ISLAND	1226	9196	7035	1554	376	22340	174	3377	45278
SOUTH CAROLINA	31	201	165	31	11	491	0	0	1207
SOUTH DAKOTA	0	0	0	68	0	1139	0	0	1207
TENNESSEE	1090	5365	11348	965	984	8772	212	2451	31187
TENNESSEE	31	171	361	31	31	281	11	81	81
TENNESSEE	11686	7334	11368	11947	10605	1274	164	22629	77007
TENNESSEE	151	101	191	161	161	21	0	291	42122
TEXAS	4275	9563	7865	5568	125	12130	357	2239	42122
TEXAS	101	231	191	131	0	291	11	51	51
TEXAS	53065	41331	26730	83916	29442	28863	347	5143	268827
UTAH	207	151	101	311	111	111	0	21	21
UTAH	16321	12941	12420	10084	4815	2847	917	24636	85181
VERMONT	191	151	151	121	61	31	11	291	9852
VERMONT	3821	2538	1013	68	0	1390	125	897	9852
VIRGINIA	391	261	101	11	0	141	11	91	91
VIRGINIA	3532	1959	1776	9942	7395	11044	830	4835	41168
WASHINGTON	91	51	61	231	181	271	21	121	121
WASHINGTON	5182	7488	10403	8928	3908	8646	357	24407	69315
WEST VIRGINIA	71	111	131	131	61	121	11	351	351
WEST VIRGINIA	3503	8145	6429	48	68	5192	48	2673	24106
WISCONSIN	151	341	181	0	0	221	0	111	111
WISCONSIN	116	3629	5674	20091	12246	10279	241	4786	57221
WYOMING	0	61	101	351	211	181	0	81	81
WYOMING	17611	13520	20564	15469	4444	1148	134	25071	97966
WYOMING	181	141	211	161	51	11	0	261	261
TOTAL	381399	382005	400812	531015	373547	413209	23024	536650	181
TOTAL	131	131	131	171	121	141	11	181	181

*** POPULATION CASE 1 COMPOSITE

RADIUS 0 - 2 MILES/DENSITY 100 PERSONS PER SQUARE MILE
RADIUS 2 - 30 MILES/DENSITY 250 PERSONS PER SQUARE MILE

POPULATION CASE 1 IS 1% IN THE AMOUNT OF LAND IT CONSTRAINS

POPULATION CASE 2 and ENVIRONMENTAL SUITABILITY LEVELS *** STATE AREAS IN SQUARE MILES AND % OF STATE

TABLE F3.2

TABULATION	LOW SUITABILITY					MEDIUM SUITABILITY		HIGH SUITABILITY		DENSITY RESTRICTIONS	DEN. RESTRICTIONS	LAND RESTRICTIONS	RESTRICTED LAND
ALABAMA	38	4301	105%	185%	106P3	2540	24	202e	4100				
ARIZONA	2171	4082	15855	28922	175e	217e	520	586P4	114200				
ARKANSAS	4979	7392	7373	9843	15411	199e	48	621e	17000				
CALIFORNIA	44590	18924	9968	11918	4502	16907	1640	4905e	117000				
COLORADO	3099e	13925	11040	13143	395e	2e0e	154	2857e	104700				
CONNECTICUT	193	87e	309	203	0	3812	0	0	0				
DELAWARE	0	0	0	0	18e2	427	0	0	0				
FLORIDA	0	0	0	1930	265e4	7759	1032	1207e	5025e				
GEORGIA	259e	342e	91e	15247	17418	4854	18	5e6e	5650e				
IDAHO	10702	77e8	11918	10239	451e	88e	6e	3745e	8351e				
ILLINOIS	3281	1959	4420	13452	23758	8309	10	45e	5e5e				
INDIANA	0	302	177e	8714	18345	5e84	10	1312	3e343				
IOWA	10	9409	4941	27811	11484	2413	0	0	5e05e				
KANSAS	13758	27194	15778	14359	6e10	2374	0	195	827e				
KENTUCKY	4381	10287	11455	735e	1341	2779	77	2393	424e				
LOUISIANA	111	2e1	28e	192	3e	7e	0	0	0				
MAINE	1239	8444	4883	1e415	1727	1013	0	357	34074				
MARYLAND	4e	251	141	481	5e	3e	0	1e	111e				
MASSACHUSETTS	791	1457	135	917	441	411	0	11	8e7				
MICHIGAN	0	0	0	15015	28921	8222	8	9592	4183				
MINNESOTA	0	251	1e40	27753	27831	3513	11e	24810	8541e				
MISSISSIPPI	0	2548	471e	20072	14400	2104	39	3802	4780e				
MISSOURI	12188	13500	14832	11088	100e5	3744	0	451e	e993e				
MONTANA	171	191	211	1e3	141	9e	0	6e	0				
NEBRASKA	13423	27319	29992	23440	6514	408	39	47121	14845e				
NEVADA	181	1e1	211	1e1	231	2e	0	1534	772e				
NEVADA	37732	1894e	27e18	4999	492	67e	20	2022e	110e1e				
NEW HAMPSHIRE	341	17e	251	5e	0	11	0	181	0				
NEW HAMPSHIRE	1457	4188	94e	45e	0	122e	0	1197	94e				
NEW JERSEY	0	318	29	68	1679	9913	0	0	800e				
NEW MEXICO	47198	18181	18702	4490	309	1129	203	31334	1217e				
NEW YORK	391	131	151	41	0	11	0	2e1	0				
NEW YORK	3242	6581	10210	9303	1428	9525	77	9852	5021e				
NORTH CAROLINA	2943	1235	3590	192	31	191	0	201	0				
NORTH CAROLINA	61	131	201	192	31	191	0	201	0				
NORTH DAKOTA	8328	12342	17334	14321	11474	434	0	657e	7100e				
OHIO	121	171	251	201	1e1	11	0	0	0				
OHIO	1448	4719	2770	6147	13259	11165	241	2084	4183				
OKLAHOMA	31	111	71	151	321	271	11	51	0				
OKLAHOMA	8125	11821	21925	14166	7375	2538	68	3397	49e1e				
OREGON	121	171	311	201	111	41	0	51	0				
OREGON	290	20998	13413	25244	507e	2557	29	30320	9792				
PENNSYLVANIA	0	211	1e1	2e1	51	31	0	311	0				
PENNSYLVANIA	2258	12934	10258	3542	1081	11734	48	3503	4527e				
RHODE ISLAND	51	281	231	81	21	2e1	0	81	0				
RHODE ISLAND	0	0	125	212	0	8e8	0	0	120e				
SOUTH CAROLINA	0	0	101	181	0	721	0	0	0				
SOUTH CAROLINA	1544	6871	14552	13e1	1255	2943	29	2e34	3118e				
SOUTH DAKOTA	31	221	471	41	41	91	0	81	0				
SOUTH DAKOTA	11792	7470	11484	12053	10895	540	4E	25785	7700				
TENNESSEE	151	101	151	1e1	141	11	0	31	0				
TENNESSEE	5771	13047	92e4	7083	280	4082	88	2548	4212				
TEXAS	141	311	221	171	101	171	0	61	0				
TEXAS	53934	428e5	279e6	91e17	33138	13828	77	5414	2e822e				
UTAH	201	1e1	101	341	121	51	0	21	0				
UTAH	17833	13192	1251e	10113	4825	1148	3e7	2518e	851e				
VERMONT	211	151	151	121	61	11	0	201	0				
VERMONT	4190	2847	1322	87	0	425	5e	9e5	9e5				
VIRGINIA	421	291	131	11	0	41	11	101	0				
VIRGINIA	4352	25e8	231e	12043	9940	4304	11	121	411e				
WASHINGTON	111	61	81	291	241	101	0	0	0				
WASHINGTON	7044	8029	11590	9341	4294	4254	77	24885	6931e				
WEST VIRGINIA	101	121	171	131	61	61	0	3e1	0				
WEST VIRGINIA	3947	9901	542e	135	183	1592	10	2712	2410e				
WISCONSIN	1e1	411	231	11	11	71	0	111	0				
WISCONSIN	11e	3802	6379	22755	14e97	424e	8	441	5702e				
WYOMING	0	71	111	401	2e1	71	0	91	0				
WYOMING	1772	13e1e	20709	1575e	4e42	511	2e	2514e	9745e				
TOTAL	402791	414228	439406	993990	441227	190657	7374	550321					
	131	141	141	201	151	61	0	1E1					

*** POPULATION CASE 2 COMPOSITE

RADIUS 0 - 3 MILES/DENSITY 250 PERSONS PER SQUARE MILE
RADIUS 2 - 30 MILES/DENSITY 300 PERSONS PER SQUARE MILE

POPULATION CASE 1 IS 2nd IN THE AMOUNT OF LAND IT CONSTRAINS

TABLE F3.3

POPULATION CASE 3 AND ENVIRONMENTAL SUITABILITY LEVELS *** STATE AREAS IN SQUARE MILES AND % OF STATE

POPULATION	LOW SUITABILITY						MEDIUM SUITABILITY			HIGH SUITABILITY		
	MEDIUM-LOW		MEDIUM-HIGH		HIGH		RESTRICTIONS		RESTRICTIONS			
	0	1	0	1	0	1	0	1	0	1	0	1
ALABAMA	38	4396	10751	18527	10874	2943	14	2057	11507			
ARIZONA	0	127	215	315	215	60	0	47				
ARIZONA	2171	4082	15874	29248	1807	1707	420	5878	11407			
ARIZONA	25	41	140	211	25	21	0	51				
ARKANSAS	5047	7421	7538	9291	15577	1812	48	4215	7229			
CALIFORNIA	91	147	140	190	290	50	0	120				
CALIFORNIA	46301	19223	10355	12275	7044	13770	1197	50299	167748			
COLORADO	290	120	65	80	60	90	10	70				
COLORADO	31295	13992	11213	13192	3980	1984	127	28375	14307			
CONNECTICUT	300	130	115	130	40	20	0	270				
CONNECTICUT	377	1023	454	236	0	304	0	2	1210			
DELAWARE	70	200	90	60	0	580	0	0				
DELAWARE	0	0	0	0	180	374	0	29	224			
FLORIDA	0	0	0	0	820	160	0	0				
FLORIDA	0	0	0	1930	37423	6900	550	12355	59350			
GEORGIA	0	0	0	0	0	120	10	210				
GEORGIA	2615	3484	9467	15338	17880	3974	164	5700	56001			
IDAHO	40	60	180	270	300	70	0	100				
IDAHO	10712	7768	11927	10306	4574	743	44	3741	82547			
ILLINOIS	130	90	140	120	50	10	0	40				
ILLINOIS	3349	2142	4574	13693	24675	6767	10	1371	36574			
INDIANA	40	40	80	240	440	120	0	20				
INDIANA	0	511	1805	8907	19319	4478	10	1312	36342			
IOWA	0	10	50	230	530	120	0	40				
IOWA	10	8409	4940	28024	11877	1908	0	0	56068			
KANSAS	0	170	90	500	210	40	0	0				
KANSAS	15778	27300	15787	14494	6784	1930	0	190	80260			
KENTUCKY	190	320	190	180	80	20	0	0				
KENTUCKY	4381	10326	11561	7874	1490	2162	68	2400	40071			
LOUISIANA	110	260	290	200	40	50	0	60				
LOUISIANA	0	0	376	690	24376	2094	950	13462	48107			
MAINE	0	0	10	140	310	40	0	20				
MAINE	1235	8444	4883	16511	1727	917	0	357	34074			
MARYLAND	40	250	140	480	90	30	0	10				
MARYLAND	0	318	946	618	5452	3677	0	147	11150			
MASSACHUSETTS	0	30	80	60	490	300	0	10				
MASSACHUSETTS	830	1554	376	1110	0	4757	0	0	8627			
MICHIGAN	100	180	40	130	0	550	0	0				
MICHIGAN	0	0	0	13343	29867	6948	77	9602	61807			
MINNESOTA	0	0	0	250	480	110	0	180				
MINNESOTA	0	251	1737	28130	28178	2492	106	24820	85914			
MISSISSIPPI	0	0	20	330	330	30	0	200				
MISSISSIPPI	0	2586	4786	20140	14832	1698	38	3802	47880			
MISSOURI	0	50	100	420	310	40	0	80				
MISSOURI	12297	13799	14957	11200	10152	3011	0	4516	49933			
MONTANA	180	200	210	160	150	40	0	60				
MONTANA	13471	27339	29992	23440	6552	502	38	47121	148455			
NEBRASKA	90	180	200	160	40	0	0	300				
NEBRASKA	14205	12775	16550	14088	18130	917	0	1534	77720			
NEVADA	180	160	210	180	230	11	0	20				
NEVADA	37788	18846	27618	5086	492	531	10	20246	110618			
NEW HAMPSHIRE	340	170	250	50	0	0	0	180				
NEW HAMPSHIRE	1457	4217	1023	540	0	1033	0	1197	9467			
NEW JERSEY	150	450	110	60	0	110	0	130				
NEW JERSEY	0	405	97	87	2046	5375	0	0	8010			
NEW MEXICO	0	50	10	10	260	670	0	0				
NEW MEXICO	47227	18248	18760	4738	318	917	134	31382	121744			
NEW YORK	390	150	150	40	0	10	0	260				
NEW YORK	32911	6497	10309	10007	1534	8251	77	9873	50219			
NORTH CAROLINA	70	130	210	200	30	160	0	200				
NORTH CAROLINA	2963	1293	3696	11377	18046	4767	220	8405	50769			
NORTH DAKOTA	60	30	70	220	360	90	0	170				
NORTH DAKOTA	6328	12352	17534	14321	11512	386	0	4572	71005			
OHIO	120	170	250	200	160	10	0	90				
OHIO	1448	4806	2895	7729	14157	8473	212	2113	41833			
OKLAHOMA	30	110	70	190	340	200	10	50				
OKLAHOMA	8135	11860	22031	14301	7404	2220	68	3397	69616			
OREGON	120	170	320	210	110	30	0	50				
OREGON	299	2107	13500	25273	3423	2053	19	30330	97926			
PENNSYLVANIA	0	210	140	260	60	20	0	310				
PENNSYLVANIA	2374	13693	10876	3966	1322	9496	39	3513	45299			
RHODE ISLAND	50	300	240	90	30	210	0	80				
RHODE ISLAND	0	0	261	328	0	618	0	0	1007			
SOUTH CAROLINA	0	0	220	270	0	510	0	0				
SOUTH CAROLINA	1573	7073	14803	1370	125	2451	29	2634	31186			
SOUTH DAKOTA	30	230	470	40	40	80	0	80				
SOUTH DAKOTA	11867	7450	11503	12063	10924	454	48	20745	77004			
TENNESSEE	150	100	150	160	140	10	0	300				
TENNESSEE	5415	13336	9399	7286	290	3300	48	2548	42127			
TEXAS	140	300	220	170	10	80	0	60				
TEXAS	54069	43116	28053	93103	34084	10924	38	5452	268847			
UTAH	200	160	100	300	130	40	0	20				
UTAH	18046	13192	12526	10113	4825	966	230	25320	89180			
VERMONT	210	150	150	120	60	10	0	300				
VERMONT	41748	28534	1341	87	0	367	48	979	9807			
VIRGINIA	420	290	140	10	0	40	0	100				
VIRGINIA	4362	2586	2355	12217	10297	3686	193	5472	41165			
WASHINGTON	110	60	60	300	250	90	0	170				
WASHINGTON	7527	8056	11725	9399	4439	3406	46	24714	49314			
WEST VIRGINIA	110	120	170	140	60	50	0	360				
WEST VIRGINIA	3947	10007	5722	135	183	1390	10	2712	24107			
WISCONSIN	160	420	240	10	10	60	0	110				
WISCONSIN	116	3802	6388	23076	15044	3347	77	4900	57002			
WYOMING	0	70	110	410	260	60	0	90				
WYOMING	17737	13605	20719	15572	4661	434	29	25196	47960			
TOTAL	180	140	210	160	50	0	0	260				
TOTAL	406711	418199	443843	604417	452510	156610	5480	552190				
TOTAL	130	140	150	200	150	50	0	180				

*** POPULATION CASE 3 COMPOSITE

RADIUS 0 - 2 MILES/DENSITY 250 PERSONS PER SQUARE MILE
RADIUS 2 - 30 MILES/DENSITY 750 PERSONS PER SQUARE MILE

POPULATION CASE 1 IS 3x IN THE AMOUNT OF LAND IT CONSTRAINS

TABLE F3.4

POPULATION CASE 4 AND
ENVIRONMENTAL SUITABILITY LEVELS ***
STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	LOW SUITABILITY			MEDIUM SUITABILITY			HIGH SUITABILITY			DENSITY	RESTRICTIVE LAND USE RESTRICTIONS	RESTRICTED LAND
ALABAMA	38	6514	11030	19175	11300	1756	10	2065	7102			
ARIZONA	2210	4092	15980	29481	1805	1370	116	9426	114144			
ARKANSAS	3105	7546	7604	10665	15739	936	19	6244	53210			
CALIFORNIA	47285	19686	10200	12506	7363	11831	1052	50421	160364			
COLORADO	31498	14002	11252	13230	4024	1660	38	28653	10432			
CONNECTICUT	305	1322	940	634	0	2509	0	0	5210			
DELAWARE	0	0	0	0	2007	280	0	39	2326			
FLORIDA	0	0	0	2046	39029	3182	423	12680	39358			
GEORGIA	2644	3667	9930	15990	17930	2577	97	5771	58606			
IDAHO	10779	7797	12014	10354	4642	444	10	37510	87550			
ILLINOIS	3484	2200	4690	14070	25486	5250	10	1351	56541			
INDIANA	0	321	1930	9283	20275	3011	0	1321	36342			
IOWA	10	9457	3018	28477	11918	1187	0	0	56067			
KANSAS	15807	27493	15874	14716	4938	1226	0	193	82267			
KENTUCKY	4355	10490	11773	8145	1544	1293	29	2441	40270			
LOUISIANA	0	0	376	7025	24993	1341	143	13674	48152			
MAINE	1245	8453	4941	16878	1756	444	0	357	38074			
MARYLAND	0	338	1004	743	5761	3165	0	143	1115			
MASSACHUSETTS	817	1640	940	1438	0	4092	0	0	8627			
MICHIGAN	0	0	0	15931	31237	4970	0	9679	41837			
MINNESOTA	0	261	1776	28516	28477	1959	39	24887	85915			
MISSISSIPPI	0	2615	4873	20429	15073	1052	0	3841	47883			
MISSOURI	12516	13983	15112	11258	10335	2123	0	4516	69933			
MONTANA	13529	27340	30069	23409	4581	299	0	47160	148455			
NEBRASKA	14214	12284	18627	14137	18316	608	0	1534	77720			
NEVADA	37847	18846	27638	3105	311	413	10	30246	110618			
NEW HAMPSHIRE	1476	4371	1071	714	0	637	0	1197	9466			
NEW JERSEY	0	311	145	134	2316	4883	0	0	9009			
NEW MEXICO	47324	18996	18866	4777	318	627	48	31488	121744			
NEW YORK	3416	6967	11020	11001	1689	6193	10	9920	50218			
NORTH CAROLINA	3078	1448	4092	12284	18586	2654	87	8540	30769			
NORTH DAKOTA	6338	12381	17544	14321	11341	309	0	4572	71006			
OHIO	1467	8008	3117	8347	15015	4552	106	2220	41832			
OKLAHOMA	8145	11976	22330	14494	7720	1486	19	3445	69615			
OREGON	299	21085	13780	25322	9674	1619	0	30349	97926			
PENNSYLVANIA	2948	14504	11850	4336	1919	6774	19	3532	45278			
RHODE ISLAND	0	0	390	405	0	911	0	0	1206			
SOUTH CAROLINA	1650	7344	15170	1486	1293	1583	0	2663	31189			
SOUTH DAKOTA	11870	7488	11532	12072	11001	251	0	22793	77007			
TENNESSEE	6137	13896	9554	7494	357	1891	14	2579	42122			
TEXAS	34204	43367	28274	94445	34856	8203	39	3452	268840			
UTAH	18200	13201	12564	10113	4835	714	174	25379	85100			
VERMONT	4227	2934	1370	87	0	212	10	1013	9853			
VIRGINIA	4487	2692	2432	12574	10625	2692	68	5997	41167			
WASHINGTON	7826	8183	11870	9534	4555	2586	29	24733	69316			
WEST VIRGINIA	4072	10219	4612	135	203	743	0	2721	24107			
WISCONSIN	116	3831	6523	23758	15392	2774	58	4970	37022			
WYOMING	17775	13655	20738	15623	4690	280	18	25006	47986			
TOTAL	410763	423912	450935	616884	465237	114556	3333	554346				

*** POPULATION CASE 4 COMPOSITE

RADIUS 0 - 2 MILES/DENSITY 500 PERSONS PER SQUARE MILE
RADIUS 2 - 30 MILES/DENSITY 750 PERSONS PER SQUARE MILE

POPULATION CASE 1 IS 4% IN THE AMOUNT OF LAND IT COMBINES

TABLE F3.5

POPULATION CASE 5 AND
ENVIRONMENTAL SUITABILITY LEVELS ***
STATE AREAL IN SQUARE MILES AND % OF STATE

STATE	LOW SUITABILITY		MEDIUM SUITABILITY		HIGH SUITABILITY		DENSITY RESTRICTIONS	RESTRICTED LAND
	AREA	%	AREA	%	AREA	%		
ALABAMA	98	0.352	11117	19232	11435	1478	0	2775
ARIZONA	2210	4.092	15990	29938	1802	1004	69	59256
ARKANSAS	5124	7.566	7662	10062	15817	714	19	5644
CALIFORNIA	49372	19.651	10306	12825	7652	8666	569	50123
COLORADO	31796	14.050	11428	13278	4072	1081	48	28112
CONNECTICUT	473	15.34	647	801	0	179	0	0
DELAWARE	0	0	0	0	2062	222	0	29
FLORIDA	0	0	0	2055	40192	4003	116	12999
GEORGIA	2644	3.676	10200	16222	18046	1920	48	5819
IDaho	10798	7.807	12034	10374	4661	357	10	37510
ILLINOIS	121	0.43	4815	18185	26383	4034	10	1321
INDIANA	62	0.22	1969	9389	20883	2229	0	1322
Idaho	10	0.04	5057	28193	12034	917	0	0
KANSAS	19807	27.628	15884	14871	7054	820	0	193
KENTUCKY	115	0.41	11879	8280	1560	926	29	2461
LOUISIANA	0	0	376	7025	23222	1013	311	13909
MAINE	1245	8.653	4941	16994	1756	328	0	357
MARYLAND	0	0	1013	1351	4446	1862	0	145
MASSACHUSETTS	926	1.698	1148	2104	0	2750	0	0
MICHIGAN	0	0	0	16453	32202	3507	0	9679
MINNESOTA	0	0	1824	28699	28757	1448	19	24907
MISSISSIPPI	10	0.04	4912	20506	15208	782	0	3841
MISSOURI	12574	14.118	15237	11551	10364	1573	0	4516
MONTANA	13558	27.367	30069	23078	4991	232	0	47160
NEBRASKA	14214	12.284	14627	14214	18345	502	0	1534
NEVADA	37886	18.046	27638	5201	511	280	10	20246
NEW HAMPSHIRE	1476	4.371	1081	879	0	482	0	1197
NEW JERSEY	163	0.61	113	93	0	53	0	131
NEW MEXICO	17	0.06	296	357	3561	3059	0	0
NEW YORK	47353	18.306	18933	4796	338	482	29	31907
NORTH CAROLINA	3664	7.199	11064	11580	1776	4806	10	9920
NORTH DAKOTA	67	0.24	81	251	371	41	0	171
OHIO	8328	12.381	17553	14359	11390	212	0	4372
OKLAHOMA	121	0.43	201	143	43	0	0	0
OREGON	1486	9.018	3146	9525	15701	4632	106	2220
PENNSYLVANIA	43	0.16	143	263	67	13	0	311
RHODE ISLAND	2615	15.072	12458	5008	1660	4912	19	3532
SOUTH CAROLINA	63	0.23	285	113	43	113	0	81
SOUTH DAKOTA	0	0	376	470	0	357	0	1206
TENNESSEE	0	0	313	292	0	301	0	0
TEXAS	1669	7.421	15401	1496	1293	1245	0	2660
UTAH	51	0.24	491	51	43	43	0	93
VERMONT	11898	7.488	11541	12072	11030	183	0	22793
VIRGINIA	151	0.55	153	163	143	0	0	301
WASHINGTON	6166	14.050	9660	7778	376	1496	10	2586
WEST VIRGINIA	153	0.55	221	181	13	43	0	63
WISCONSIN	54223	43.483	28790	9318	35840	5876	29	5462
WYOMING	203	0.73	113	363	131	23	0	23
TOTAL	18393	13.201	12564	10113	4825	521	48	25507
	221	0.81	153	123	43	13	0	301
	427	1.53	1399	97	0	164	10	1013
	433	3.03	163	13	0	21	0	103
	4487	27.02	2441	18906	11069	1998	38	3619
	113	0.41	63	313	271	51	0	143
	8309	8.222	12009	9544	4603	1872	0	24762
	123	0.45	171	143	71	31	0	363
	4072	10.248	6195	145	203	521	0	2721
	173	0.63	261	13	13	21	0	113
	116	0.43	6533	24000	15749	1766	29	4999
	0	0	113	421	281	31	0	93
	17783	13.684	20748	15633	4709	203	19	25206
	181	0.66	213	167	51	0	0	263
TOTAL	414601	426238	456642	626314	476193	82339	1901	555775
	143	0.53	133	213	163	31	0	183

*** POPULATION CASE 5 COMPOSITE

RADIUS 0 - 2 MILES/DENSITY 500 PERSONS PER SQUARE MILE
RADIUS 2 - 30 MILES/DENSITY 1500 PERSONS PER SQUARE MILE

POPULATION CASE 1 IS SHOWN IN THE AMOUNT OF LAND IT CONSTRAINS

TABLE F3.6

ENVIRONMENTAL SUITABILITY AND POPULATION CASES 1 - 5 ***
HIGH SUITABILITY
STATE AREAS IN SQUARE MILES AND % BY STATE

TABULATION	AVAILABLE LAND					POPULATION CASE 5	OTHER SUITABLE LAND	TOTAL AVAILABLE LAND	
	POPULATION CASE 1	POPULATION CASE 2	POPULATION CASE 3	POPULATION CASE 4	POPULATION CASE 5				
ALABAMA	8984	1698	193	427	135	425	37972	2071	71954
ARIZONA	1727	29	48	0	0	10	53123	54422	114344
ARKANSAS	14193	1214	108	227	125	328	35821	4223	53251
CALIFORNIA	4844	1718	482	318	290	733	100491	51494	146367
COLORADO	3763	193	29	39	48	87	71507	28667	104326
CONNECTICUT	0	0	0	0	0	0	5211	0	5211
DELAWARE	1214	447	48	97	98	227	0	39	2327
FLORIDA	29008	7554	899	1602	1168	3928	2133	13109	99374
GEORGIA	15739	1679	241	270	114	376	34315	5867	98605
IDAHO	4130	367	98	68	19	116	41234	37519	83511
ILLINOIS	19618	4140	917	811	897	3291	25519	1381	56547
INDIANA	12504	5838	975	955	608	1891	12446	1322	36341
IOWA	10094	1390	193	241	114	482	43530	0	56064
KANSAS	181	21	0	0	0	11	781	0	8221
KENTUCKY	917	425	134	48	114	318	35821	2470	40248
LOUISIANA	20226	3735	415	618	328	955	7459	14417	48155
MAINE	1402	125	0	29	0	0	31941	357	34574
MARYLAND	3435	1474	540	309	485	1100	3444	145	11154
MASSACHUSETTS	311	131	51	31	61	101	311	11	8627
MICHIGAN	22533	6388	944	1370	945	2847	17109	9479	61837
MINNESOTA	24180	1450	347	299	980	897	31334	24926	85913
MISSISSIPPI	13249	1351	232	241	135	463	28371	3841	47883
MISSOURI	9235	830	87	193	29	193	34860	4514	49933
MONTANA	4311	203	39	29	10	38	44647	47180	148457
NEBRASKA	17194	868	87	144	29	104	57736	1534	77720
NEVADA	221	13	0	0	0	0	743	21	8951
NEW HAMPSHIRE	0	0	0	0	0	0	8270	1197	9467
NEW JERSEY	427	1052	367	270	1245	1882	2367	0	8010
NEW MEXICO	222	87	10	0	19	0	89870	31536	121744
NEW YORK	753	474	104	194	87	1214	37297	9930	50219
NORTH CAROLINA	14378	3464	203	940	222	531	22803	8627	50768
NORTH DAKOTA	11194	290	39	29	48	145	52499	4372	71006
OHIO	7778	9481	887	859	485	2364	21442	2326	41832
OKLAHOMA	7014	540	29	114	48	114	38267	3464	49414
OREGON	4101	975	347	251	161	753	60891	30349	97928
PENNSYLVANIA	376	704	241	193	145	454	39613	3551	45277
RHODE ISLAND	0	0	0	0	0	0	1204	0	1204
SOUTH CAROLINA	984	270	0	29	0	29	27203	2662	31188
SOUTH DAKOTA	10405	290	29	77	29	48	43136	2293	77007
TENNESSEE	125	154	10	68	19	77	39073	2594	42122
TEXAS	29442	3674	944	772	984	2413	225076	5491	268841
UTAH	4815	10	0	10	0	0	54793	2553	85181
VERMONT	0	0	0	0	0	0	8830	1023	9853
VIRGINIA	7593	2345	357	328	444	1399	23035	3665	41165
WASHINGTON	3908	388	145	114	48	309	39442	24762	49314
WEST VIRGINIA	48	114	0	19	0	29	21153	2721	24104
WISCONSIN	12246	2451	367	328	357	1033	35213	5026	57023
WYOMING	4449	193	19	29	19	98	47994	25225	97964
TOTAL	373547	47477	11282	12729	10914	31971	197448	557473	121

NOTE "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST CONSTRAINING POPULATION CRITERIA. THE NUMBERS IN THE POPULATION CASE COLUMNS REPRESENT THAT LAND UNLIKELY CONSTRAINED BY THAT CRITERION.

TABLE F3.7

ENVIRONMENTAL SUITABILITY AND POPULATION CASES 1 - 5 ***
 CUMULATIVE MEDIUM-HIGH SUITABILITY
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	AVAILABLE LAND					OTHER SUITABILITIES RESTRICTED LAND			
	POP CASE 1	POP CASE 2	POP CASE 3	POP CASE 4	POP CASE 5				
ALABAMA	15758	2937	232	347	56	427	30176	2071	51909
ARIZONA	27502	1399	367	212	257	917	24103	54401	114342
ARKANSAS	8975	868	48	174	0	120	36877	6207	32150
CALIFORNIA	10596	1322	357	232	318	704	95347	51492	160347
COLORADO	12487	656	48	39	48	77	62017	28667	104304
CONNECTICUT	120	15	0	0	0	0	670	0	5216
DELAWARE	0	0	0	0	0	0	2287	39	2341
FLORIDA	1689	241	0	114	10	73	44127	13105	59358
GEORGIA	12873	2374	290	454	232	967	35555	58667	58665
IDAHO	9920	318	68	48	19	68	35599	37519	83547
ILLINOIS	11831	1621	241	376	116	290	40704	1361	56547
INDIANA	6321	3993	193	376	106	290	25341	1322	36342
INDIA	25725	2053	212	454	114	347	27126	0	58068
KANSAS	13375	934	135	222	134	261	46942	193	82268
KENTUCKY	5997	1959	318	270	135	290	29230	3470	40268
LOUISIANA	6475	396	19	137	0	58	26653	14417	48150
MAINE	14784	1631	97	367	116	280	16444	357	34076
MARYLAND	39	290	290	125	408	685	8975	145	11157
MASSACHUSETTS	347	369	193	328	666	1525	4999	0	8627
MICHIGAN	11580	3435	328	608	302	656	35049	9679	61837
MINNESOTA	25450	2104	376	386	183	396	31893	24026	85914
MISSISSIPPI	18036	2036	68	290	77	261	23276	3841	47887
MISSOURI	10171	917	116	145	203	434	53432	4516	69924
MONTANA	23276	164	0	29	10	97	77721	47160	148457
NEBRASKA	13365	647	77	48	77	241	61731	1534	77720
NEVADA	175	13	0	0	0	0	84988	2025	110619
NEW HAMPSHIRE	58	396	87	174	145	376	7035	1197	9468
NEW JERSEY	0	68	19	68	203	318	7334	0	8010
NEW MEXICO	4449	241	48	39	19	97	85316	31536	121745
NEW YORK	5443	3860	704	994	579	2384	26327	9930	50219
NORTH CAROLINA	111	82	13	25	13	51	525	205	50770
NORTH DAKOTA	14147	174	0	0	39	19	50055	4572	71006
OHIO	3204	2943	1992	608	1177	1793	29188	2326	41833
OKLAHOMA	12709	1457	135	193	145	318	51193	3464	69614
OREGON	24926	218	29	48	19	68	42171	30348	97928
PENNSYLVANIA	1554	1988	625	569	473	1390	35329	3251	45276
RHODE ISLAND	68	145	114	77	68	299	434	0	1207
SOUTH CAROLINA	965	396	10	114	10	87	26943	2663	31190
SOUTH DAKOTA	11947	106	10	10	0	29	42113	22983	77006
TENNESSEE	5568	1513	203	405	87	318	31430	2596	42122
TEXAS	83916	7701	1486	1341	1071	2674	165199	5491	268838
UTAH	10084	29	0	0	0	0	49514	25553	8519
VERMONT	68	19	0	0	10	19	8714	1023	9852
VIRGINIA	9592	2451	174	357	232	405	22292	5665	41187
WASHINGTON	8926	415	58	135	10	58	34952	24762	67316
WEST VIRGINIA	48	87	0	0	10	0	21240	2721	24107
WISCONSIN	20091	2663	521	482	241	618	27077	3029	57027
WYOMING	15449	87	19	48	10	77	57051	25225	47986
TOTAL	531013	62975	10433	12468	9432	22882	1833100	557070	181

NOTE "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST
 CONSTRAINING POPULATION CRITERIA. THE NUMBERS IN THE
 POPULATION CASE COLUMNS REPRESENT THAT LAND UNLIKELY
 CONSTRAINED BY THAT CRITERION.

TABLE F3.8

ENVIRONMENTAL SUITABILITY AND POPULATION CASES 1 - 5 ***
 <<<<< REGION SUITABILITY >>>>>
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	AVAILABLE LAND						OTHER SUITABLE REGIONS	TOTAL SUITABLE REGIONS	
	POP CASE 1	POP CASE 2	POP CASE 3	POP CASE 4	POP CASE 5				
ALABAMA	8830	1766	135	299	87	270	36446	2075	51908
ARIZONA	15517	338	19	106	10	58	38897	59425	114443
ARKANSAS	6321	1052	135	97	58	125	39208	6267	53249
CALIFORNIA	9052	917	87	145	106	232	98334	51492	140367
COLORADO	10654	386	174	39	174	225	64018	28667	104327
CONNECTICUT	29	299	123	87	104	135	4429	0	5211
DELAWARE	0	0	0	0	0	0	2287	29	2326
FLORIDA	0	0	0	0	0	0	46252	13107	59357
GEORGIA	6890	2306	270	463	270	521	42016	5867	58623
IDAHO	11561	357	10	87	19	58	33939	37119	83551
ILLINOIS	3792	627	154	116	125	270	50093	1361	56738
INDIANA	1216	560	29	123	39	19	33032	1322	36344
IOWA	4603	338	19	58	39	68	50942	0	56067
KANSAS	15208	349	10	87	10	77	68112	193	82266
KENTUCKY	9418	2036	106	212	106	222	25698	2470	40268
LOUISIANA	231	29	0	0	0	0	33360	14417	48153
MAINE	4574	309	0	58	0	39	28738	357	34075
MARYLAND	627	270	48	58	10	68	9930	145	11156
MASSACHUSETTS	61	21	0	11	0	11	897	11	9627
MICHIGAN	0	0	0	0	0	0	52158	9679	61837
MINNESOTA	1390	251	97	39	48	154	59010	24926	85915
MISSISSIPPI	4294	425	68	87	39	58	39073	3841	47885
MISSOURI	13539	1293	125	154	125	511	49669	4516	69534
MONTANA	29683	309	0	77	0	29	71198	47180	148456
NEBRASKA	14019	425	106	77	0	145	59415	1534	77721
NEVADA	27570	48	0	19	0	10	62715	20255	110617
NEW HAMPSHIRE	856	290	77	48	10	10	7180	1197	9468
NEW JERSEY	0	29	68	48	251	482	7131	0	8009
NEW MEXICO	18258	44	58	106	68	232	71043	31506	121745
NEW YORK	7189	3020	299	511	444	560	28265	9930	50216
NORTH CAROLINA	1911	1679	106	396	116	270	37664	8627	50769
NORTH DAKOTA	17476	58	0	10	10	19	46860	6572	71005
OHIO	251	0	0	0	0	0	661	91	742
OKLAHOMA	1737	1033	116	232	29	386	35975	2326	41834
OREGON	41	21	0	11	0	11	963	67	1033
PENNSYLVANIA	19570	2355	106	299	164	349	43087	3464	69614
OREGON	281	31	0	0	0	11	621	51	672
OREGON	12256	1158	87	280	106	154	53538	30349	97928
PENNSYLVANIA	135	11	0	0	0	0	551	311	862
RHODE ISLAND	7035	3223	618	973	608	1891	27377	3551	45276
RHODE ISLAND	161	71	11	21	11	41	672	81	753
RHODE ISLAND	0	125	135	29	87	58	772	0	1206
SOUTH CAROLINA	0	101	111	21	71	51	641	0	904
SOUTH CAROLINA	11348	3204	251	367	232	743	12381	2663	31189
SOUTH CAROLINA	361	101	11	11	11	21	401	91	492
SOUTH DAKOTA	11368	116	19	29	10	39	42634	22793	77008
TENNESSEE	151	0	0	0	0	0	551	301	852
TENNESSEE	7865	1399	135	154	106	318	29548	2596	42121
TEXAS	191	31	0	0	0	11	701	61	762
TEXAS	26730	1235	87	222	116	270	234689	5491	268839
UTAH	101	0	0	0	0	0	871	21	892
UTAH	12420	97	10	39	0	19	47044	25553	85182
VERMONT	135	0	0	0	0	0	551	301	852
VERMONT	1013	309	19	29	29	58	7373	1023	9853
VIRGINIA	101	0	0	0	0	11	751	101	852
VIRGINIA	1776	540	39	77	10	39	33022	5665	41168
WASHINGTON	41	11	0	0	0	0	801	141	942
WASHINGTON	10403	1187	135	145	135	222	32327	24762	69316
WEST VIRGINIA	151	21	0	0	0	0	471	361	832
WEST VIRGINIA	4429	1197	97	290	183	328	14861	2721	24161
WISCONSIN	181	51	0	11	11	11	621	111	732
WISCONSIN	5674	704	10	135	10	87	45374	5026	57022
WYOMING	101	11	0	0	0	0	901	91	992
WYOMING	20564	145	10	19	10	10	52064	25225	67989
WYOMING	211	0	0	0	0	0	531	261	792
TOTAL	400812	38592	4440	7094	4713	11165	2015479	557673	6573152
TOTAL	13%	11	0	0	0	0	66%	18%	84%

NOTE: "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST
 CONCENTRATING POPULATION CRITERIA. THE NUMBERS IN THE
 POPULATION CASE COLUMNS REPRESENT THAT LAND UNIQUELY
 CONCENTRATED BY THAT CRITERION.

TABLE F3.9

ENVIRONMENTAL SUITABILITY AND POPULATION CASES 1 - 5 ***
 RESTRICTED LAND SUITABILITY
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	AVAILABLE LAND		POP CASE 1	POP CASE 2	POP CASE 3	POP CASE 4	POP CASE 5	OTHER	SUITABILITY RESTRICTED LAND
	SQ. MI.	% OF STATE							
ALABAMA	5250	1052	97	116	39	318	42962	2075	51905
ARIZONA	101	25	0	0	0	0	10	80	41
ARIZONA	3831	251	0	10	0	0	10	50829	59405
ARIZONA	31	0	0	0	0	0	0	44	52
ARKANSAS	6938	434	29	125	19	48	39387	4262	53251
ARIZONA	135	15	0	0	0	0	74	12	12
CALIFORNIA	16772	2152	299	463	164	574	89442	71492	162310
CALIFORNIA	101	15	0	0	0	0	55	52	52
COLORADO	13616	309	68	10	48	309	61306	28660	104376
CONNECTICUT	131	0	0	0	0	0	59	2	0
CONNECTICUT	106	569	347	299	212	540	313	0	5209
CONNECTICUT	2	115	72	63	43	102	80	0	0
DELAWARE	0	0	0	0	0	0	226	39	232
FLORIDA	0	0	0	0	0	0	46252	13105	59257
FLORIDA	0	0	0	0	0	0	78	22	0
GEORGIA	2625	801	58	183	29	58	40983	587	59674
GEORGIA	41	15	0	0	0	0	84	10	10
IDAHO	7956	212	0	29	10	68	38156	37519	80550
IDAHO	91	0	0	0	0	0	46	49	0
ILLINOIS	1457	502	183	58	48	77	52834	1361	56540
ILLINOIS	35	15	0	0	0	0	93	2	0
INDIANA	439	68	10	10	29	29	34441	1322	36343
INDIANA	13	0	0	0	0	0	95	4	0
IOWA	9023	386	0	48	0	19	46590	0	56066
IOWA	168	15	0	0	0	0	23	0	0
KANSAS	86354	840	106	193	135	174	54272	192	80267
KANSAS	32	15	0	0	0	0	65	0	0
KENTUCKY	8376	1911	39	164	10	77	27223	2470	40270
KENTUCKY	215	9	0	0	0	0	68	63	0
LOUISIANA	0	0	0	0	0	0	33736	14417	48153
LOUISIANA	0	0	0	0	0	0	70	30	0
MAINE	8309	135	0	10	0	10	25254	357	34075
MAINE	241	0	0	0	0	0	74	1	0
MARYLAND	212	106	0	19	0	10	10663	145	11155
MARYLAND	2	15	0	0	0	0	94	1	0
MASSACHUSETTS	647	811	97	87	98	77	4851	0	8626
MASSACHUSETTS	71	95	15	15	15	15	79	0	0
MICHIGAN	0	0	0	0	0	0	52138	9478	61837
MICHIGAN	0	0	0	0	0	0	84	16	0
MINNESOTA	232	19	0	10	0	0	60727	24924	85914
MINNESOTA	0	0	0	0	0	0	71	29	0
MISSISSIPPI	2355	193	39	29	10	0	41418	3841	47885
MISSISSIPPI	51	0	0	0	0	0	86	8	0
MISSOURI	12400	1100	299	183	135	299	81000	4516	69922
MISSOURI	181	2	0	0	0	0	73	6	0
MONTANA	27107	212	19	10	19	19	73909	47160	148455
MONTANA	181	0	0	0	0	0	90	30	0
NEBRASKA	12236	29	0	10	0	10	63893	1374	77722
NEBRASKA	163	0	0	0	0	0	82	2	0
NEVADA	18844	0	0	0	0	0	71516	20255	110617
NEVADA	173	0	0	0	0	0	63	18	0
NEW HAMPSHIRE	3474	714	29	154	0	97	3802	1197	9467
NEW HAMPSHIRE	373	8	0	23	0	13	40	13	0
NEW JERSEY	68	251	87	106	39	116	7344	0	8011
NEW JERSEY	11	2	15	15	15	15	92	0	0
NEW MEXICO	17939	241	68	48	10	77	71823	31536	121744
NEW MEXICO	133	0	0	0	0	0	39	26	0
NEW YORK	4989	1392	116	270	232	574	32511	9930	50219
NEW YORK	101	2	0	15	0	15	62	20	0
NORTH CAROLINA	685	569	39	134	19	145	40530	8627	50768
NORTH CAROLINA	11	15	0	0	0	0	80	17	0
NORTH DAKOTA	12907	139	10	29	0	29	52023	6572	71005
NORTH DAKOTA	173	0	0	0	0	0	73	9	0
OHIO	3725	984	87	207	10	77	34412	2326	41834
OHIO	92	2	0	0	0	0	82	6	0
OKLAHOMA	11329	492	39	114	0	121	54050	3464	64615
OKLAHOMA	163	15	0	0	0	0	78	3	0
OREGON	19849	1129	29	98	0	48	44443	30349	97927
OREGON	203	15	0	0	0	0	47	31	0
PENNSYLVANIA	9196	3657	840	811	549	1033	25621	3951	45278
PENNSYLVANIA	203	8	23	23	13	23	57	8	0
RHODE ISLAND	0	0	0	0	0	0	1206	0	1206
RHODE ISLAND	0	0	0	0	0	0	100	0	0
SOUTH CAROLINA	5245	1505	203	270	77	376	20725	2663	31187
SOUTH CAROLINA	173	5	15	15	15	15	66	9	0
SOUTH DAKOTA	7350	114	0	39	0	29	44496	22793	77007
SOUTH DAKOTA	105	0	0	0	0	0	41	20	0
TENNESSEE	9563	3484	290	560	154	463	29013	2596	42123
TENNESSEE	231	8	15	15	15	15	59	6	0
TEXAS	41331	1534	251	251	116	482	219383	5491	268839
TEXAS	151	15	0	0	0	0	82	2	0
UTAH	12941	251	0	10	0	19	46407	25553	85181
UTAH	151	0	0	0	0	0	84	30	0
VERMONT	2538	309	10	77	10	58	9829	1023	9854
VERMONT	26	2	0	15	0	15	59	10	0
VIRGINIA	1939	589	39	134	10	87	32713	5665	41168
VIRGINIA	51	15	0	0	0	0	79	14	0
WASHINGTON	7488	540	29	125	39	77	36255	24762	69315
WASHINGTON	113	15	0	0	0	0	32	36	0
WEST VIRGINIA	8145	1756	106	212	29	116	11020	2721	24105
WEST VIRGINIA	341	7	0	15	0	15	46	11	0
WISCONSIN	3628	174	0	29	0	29	48134	5026	57022
WISCONSIN	61	0	0	0	0	0	84	6	0
WYOMING	13520	47	19	19	29	19	59058	2522	97986
WYOMING	143	0	0	0	0	0	60	26	0
TOTAL	302005	30221	2981	5715	2328	6812	2049232	557620	
TOTAL	135	15	0	0	0	0	67	18	0

NOTE "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST RESTRICTING POPULATION CRITERIA. THE NUMBERS IN THE POPULATION CASE COLUMNS REPRESENT THAT LAND USUALLY RESTRICTED BY THAT CRITERION.

TABLE F3.10

ENVIRONMENTAL SUITABILITY AND POPULATION CASES 1 - 5 ***
 CO- SUITABILITY
 STATE AREAS IN SQUARE MILES AND % OF STATE

TABULATION	AVAILABLE LAND					OTHER SUITABILITY RESTRICTED LANDS
	POP CASE 1	POP CASE 2	POP CASE 3	POP CASE 4	POP CASE 5	
ALABAMA	48	10	0	0	0	49771 2078 51904
ARIZONA	01	01	01	01	01	961 41 114343
ARIZONA	2113	38	0	39	0	10 12719 39407 114343
ARKANSAS	21	01	01	01	01	01 461 521
ARKANSAS	4880	290	01	01	19	87 41787 8263 53256
CALIFORNIA	91	11	01	01	01	01 781 127
CALIFORNIA	40520	4072	1708	984	2287	4417 32882 51492 140367
COLORADO	291	31	11	11	11	41 32 32
COLORADO	29876	1119	399	203	261	386 43222 28460 104327
CONNECTICUT	291	11	01	01	01	01 421 271
CONNECTICUT	0	193	164	48	48	127 4613 0 5211
DELAWARE	01	41	31	11	11	21 891 01 5211
DELAWARE	0	0	0	0	0	0 2287 39 2326
FLORIDA	01	01	01	01	01	01 44236 13105 59357
FLORIDA	0	0	0	0	0	0 781 271
GEORGIA	01	01	01	01	01	01 44236 13105 59357
GEORGIA	2220	376	19	29	0	10 80083 5867 58604
IDAHO	41	11	01	01	01	01 851 101
IDAHO	10451	251	10	68	19	48 35184 37519 83551
ILLINOIS	131	01	01	01	01	01 421 451
ILLINOIS	2799	482	68	135	10	116 9170 1361 36541
INDIANA	91	11	01	01	01	01 911 21
INDIANA	0	0	0	0	0	0 33020 1322 36342
IOWA	01	01	01	01	01	01 961 41
IOWA	107	0	0	0	0	0 54057 0 36067
KANSAS	01	01	01	01	01	01 1001 01
KANSAS	15346	212	19	29	0	19 46247 193 82263
KENTUCKY	191	01	01	01	01	01 811 01
KENTUCKY	3377	1004	0	174	0	19 33225 2470 40269
LOUISIANA	81	21	01	01	01	01 831 61
LOUISIANA	0	0	0	0	0	0 33336 14417 48153
MAINE	01	01	01	01	01	01 701 301
MAINE	1197	39	0	10	0	0 32472 357 34075
MARYLAND	41	01	01	01	01	01 951 11
MARYLAND	0	0	0	0	0	0 11011 143 11156
MASSACHUSETTS	01	01	01	01	01	01 991 11
MASSACHUSETTS	203	989	39	87	10	39 7662 0 8629
MICHIGAN	21	71	01	11	01	01 871 01
MICHIGAN	0	0	0	0	0	0 56138 9678 41837
MINNESOTA	01	01	01	01	01	01 841 161
MINNESOTA	0	0	0	0	0	0 60988 24920 85914
MISSISSIPPI	01	01	01	01	01	01 711 291
MISSISSIPPI	0	0	0	0	10	0 44033 3841 47884
MISSOURI	01	01	01	01	01	01 951 81
MISSOURI	11406	782	106	222	98	135 82708 4516 69933
MONTANA	161	11	01	01	01	01 751 61
MONTANA	13288	135	48	98	29	29 87709 47160 148456
NEBRASKA	91	01	01	01	01	01 391 321
NEBRASKA	14157	48	0	10	0	0 61972 1534 77721
NEVADA	181	01	01	01	01	01 801 21
NEVADA	27365	367	98	98	39	97 52380 80235 110619
NEW HAMPSHIRE	341	01	01	01	01	01 471 181
NEW HAMPSHIRE	1322	133	0	19	0	0 6794 1197 9467
NEW JERSEY	141	11	01	01	01	01 721 131
NEW JERSEY	0	0	0	0	87	81 7662 0 8010
NEW MEXICO	01	01	01	01	11	11 31 961 01
NEW MEXICO	44831	367	29	97	29	77 42778 21536 121744
NEW YORK	381	01	01	01	01	01 391 261
NEW YORK	2634	989	48	125	48	48 36757 9930 30219
NORTH CAROLINA	91	11	01	01	01	01 731 201
NORTH CAROLINA	2374	849	19	01	01	01 38996 8627 30769
NORTH DAKOTA	81	11	01	01	01	01 771 171
NORTH DAKOTA	8241	87	0	10	0	0 84093 4372 71005
OHIO	121	01	01	01	01	01 791 91
OHIO	1119	308	0	19	19	19 38011 2326 41832
OKLAHOMA	31	11	01	01	01	01 911 61
OKLAHOMA	7923	203	16	10	0	0 98006 3464 69616
OREGON	111	01	01	01	01	01 831 31
OREGON	831	39	10	0	0	0 27270 30349 97929
PENNSYLVANIA	01	01	01	01	01	01 691 311
PENNSYLVANIA	1824	1033	116	174	68	143 38947 3991 45280
RHODE ISLAND	31	81	01	01	01	01 861 81
RHODE ISLAND	0	0	0	0	0	0 1206 0 1206
SOUTH CAROLINA	01	01	01	01	01	01 1001 01
SOUTH CAROLINA	1090	454	29	77	19	19 26846 2663 31188
SOUTH DAKOTA	31	11	01	01	01	01 861 91
SOUTH DAKOTA	11486	106	29	48	29	39 42277 22793 77007
TENNESSEE	131	01	01	01	01	01 891 301
TENNESSEE	4275	1496	145	222	29	318 33042 2996 42123
TEXAS	101	41	01	11	01	11 781 61
TEXAS	33065	868	175	135	19	97 209029 5491 268837
UTAH	201	01	01	01	01	01 781 21
UTAH	14321	1312	212	154	193	482 40752 25553 85179
VERMONT	191	21	01	01	01	11 481 301
VERMONT	3821	308	29	48	0	29 4574 1023 9852
VIRGINIA	391	31	11	01	01	01 861 101
VIRGINIA	3532	820	10	125	0	68 30948 2663 41168
WASHINGTON	91	21	01	01	01	01 751 141
WASHINGTON	5182	1862	482	299	482	1206 35029 24762 69314
WEST VIRGINIA	71	31	11	01	11	21 511 361
WEST VIRGINIA	3903	444	0	125	0	48 17264 2721 24105
WISCONSIN	131	21	01	11	01	01 721 111
WISCONSIN	116	0	0	0	0	0 91878 3028 57021
WYOMING	01	01	01	01	01	01 911 91
WYOMING	17411	116	10	39	10	39 54937 29225 47987
WYOMING	181	01	01	01	01	01 561 261
TOTAL	381599	21192	3919	4054	3842	10512 205717 357673
TOTAL	131	11	01	01	01	01 481 181

NOTE: "AVAILABLE LAND" IS THAT AVAILABLE UNDER THE MOST
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