

## UNITED STATES NUCLEAR REGULATORY COMMISSION WASHINGTON, D. C. 20555

DEC 0 1 1978

Docket Nos. 50-369 and 50-370

Mr. William O. Parker, Jr.
Vice President, Steam Production
Duke Power Company
P. O. Box 2178
422 South Church Street
Charlotte, North Carolina 28242

Dear Mr. Parker:

SUBJECT: LOCA/UHI ANALYSIS

(McGuire Nuclear Station, Units 1 and 2)

As a result of our review of Revision 34 to the McGuire FSAR, we find that some additional information is required to complete our review of the LOCA/UHI analysis for the McGuire Station. This information is described in the Enclosure.

Your prompt response to this request will permit us to complete our review of your application.

Sincerely,

Robert L. Baer, Chief Light Water Reactors

Branch No. 2

Division of Project Management

Inhert & Buen

Enclosure: Request for Additional Information

ccs w/enclosure: See page 2 Mr. William O. Parker, Jr.
Vice President, Steam Production
Duke Power Company
P. O. Box 2178
422 South Church Street
Charlotte, North Carolina 28242

cc: Mr. W. L. Porter
Duke Power Company
P. O. Box 2178
422 South Church Street
Charlotte, North Carolina 28242

Mr. R. S. Howard Power Systems Division Westinghouse Electric Corporation P. O. Box 355 Pittsburgh, Pennsylvania 15230

Mr. E. J. Keith
EDS Nuclear Incorporated
220 Montgomery Street
San Francisco, California 94104

Mr. J. E. Houghtaling NUS Corporation 2536 Countryside Boulevard Clearwater, Florida 33515

Mr. Jesse L. Riley, President The Carolina Environmental Study Group 354 Henley Place Charlotte, North Carolina 28207

J. Michael McGarry, III, Esq. Debevoise & Liberman 700 Shoreham Building 806 15th Street, N. W. Washington, D. C. 20005

Shelley Blum, Esq. 418 Law Building 730 East Trade Street Charlotte, North Carolina 28202 cc: Robert M. Lazo, Esq., Chairman Atomic Safety and Licensing Board U. S. Nuclear Regulatory Commission Washington, D. C. 20555

> Dr. Emmeth A. Luebke Atomic Safety and Licensing Board U. S. Nuclear Regulatory Commission Washington, D. C. 20555

Dr. Cadet H. Hand, Jr., Director Bodega Marine Lab of California P. O. Box 247 Bodega Bay, California 94923

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212.0 REACTOR SYSTEMS BRANCH

212.110 (15.4)

Your response to 212.107 indicated that the LOCA/UHI analysis with the finite mixing model for a DECL with a 0.4 discharge coefficient results in a peak clad temperature of 2126°F which is only 20°F below the previously identified limiting break. This analysis was performed with a cold leg accumulator volume of 1050 ft³ instead of the new accumulator volumes presented in 212.105. The applicant must provide a reanalysis of the limiting break using the finite mixing model and correct cold leg accumulator input. As part of this analysis he should justify that he has identified the most limiting break for the finite mixing model analysis, that dynamic steam cooling (identified in WCAP-9220) will not result in a more limiting peak clad temperature calculation, and that the most conservative cold leg accumulator values have been used.