

March 10, 1994

Docket No. 50-443  
Serial No. SEA-94-007

Mr. Ted C. Feigenbaum  
Senior Vice President  
and Chief Nuclear Officer  
North Atlantic Energy Service Corporation  
Post Office Box 300  
Seabrook, New Hampshire 03874

Dear Mr. Feigenbaum:

SUBJECT: REQUEST FOR ADDITIONAL INFORMATION: CORE THERMAL LIMIT PROTECTION  
FUNCTION SETPOINT METHODOLOGY (TAC M86959)

A preliminary review of Yankee Atomic Electric Company Topical Report YAEC-1854P, Core Thermal Limit Protection Function Setpoint Methodology, reveals that the information identified in the enclosure to this letter is required for us to continue with the review. The proposed methodology for Seabrook is based on use of the Maine Yankee setpoint methodology which has been approved by the NRC. The proposed application to Seabrook would be an extension of this approved methodology.

Because we are certain that you understand that time is of the essence, we are not requesting the information by a specific date, but you should be aware that if there is a delay in satisfying the staff's needs, we might not be able to complete the review in a timely manner, and the staff has the option of rejecting the application for incompleteness.

The requirements of this letter affect fewer than 10 respondents, and, therefore, are not subject to Office of Management and Budget review under P.L. 96-511.

Sincerely,

Original signed by:

Albert W. De Agazio, Sr. Project Manager  
Project Directorate I-4  
Division of Reactor Projects - I/II  
Office of Nuclear Reactor Regulation

9403140354 940310  
PDR ADOCK 05000443  
P PDR

Enclosure:

As stated

cc w/enclosure:

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Docket File SNorris  
NRC & Local PDRs ADeAgazio  
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Albert W. De Agazio, Sr. Project Manager  
Project Directorate I-4  
Division of Reactor Projects - I/II  
Office of Nuclear Reactor Regulation

Enclosure:  
As stated  
cc w/enclosure:  
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| NAME:   | SNorris  | ADeAgazio:bp | OGC:for  |  |  |
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UNITED STATES  
NUCLEAR REGULATORY COMMISSION

WASHINGTON, D.C. 20555-0001

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Sincerely,

A handwritten signature in cursive script that reads "Albert W. De Agazio, Sr.".

Albert W. De Agazio, Sr. Project Manager  
Project Directorate I-4  
Division of Reactor Projects - I/II  
Office of Nuclear Reactor Regulation

Enclosure:  
As stated

cc w/enclosure:  
See next page

Mr. Ted C. Feigenbaum

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Request for Additional Information  
Review of YAEC-1854P

1. Provide a flow chart depicting steps (including computer codes used) taken to determine OPDT and OTDT trip setpoints. Indicate on the chart which variables are transferred onto the next block. In addition, indicate on the diagram those steps which are cycle-dependant (redone with each cycle).
2. Statistical allowance for uncertainties is discussed only with respect to generation of the MSSV Limit Lines. In all other formulations, there was no mention of any uncertainties. This stands in contrast to the approved methodology (which is proposed to simply be extended to Seabrook by this submittal) in which uncertainties were incorporated at each step. Discuss how uncertainties (and their sizes) are accounted for with each step in this proposed methodology.
3. Since the statistical DNB methodology documented in YAEC-1869P is to be used in generation of TLLs, discuss thoroughly and quantitatively differences in the overall setpoints introduced by the use of the RTDP in DNB analysis from the current setpoints being used.
4. Explain how crediting the effects of fuel and moderator temperature reactivity feedback at overpower conditions is equivalent to crediting the action of the VOPT.
5. Explain, using illustrations, how the proposed methodology addresses overpower events from reduced power at Seabrook by expanding the last full paragraph on p.23 for  $P_L$  and the full paragraph on p.35 for  $P_D$ .
6. The formulation of the "tent" as shown on Figure 3-1 is based upon 23 data points. Justify that this constitutes a complete set of cases to be considered for this purpose.
7. Explain the method of determining the base (overpower Trip equation line on Figure 3-3. Explain thoroughly how  $K_4$  was "fitted".
8. Discuss and justify the process used to determine a set of thermal-hydraulic conditions used for the determination of  $P_D$ .
9. Ref. Figure 3-5. The overpower DT line on the top figure of Figure 3-5 appears to be a straight line. Demonstrate that this line is equivalent to the line corresponding to the OPDT line on the bottom figure. In addition, discuss the difference between the OPDT lines on Figure 3-3 and 3-5.
10. Discuss criteria by which a "judicious" choice of the reference power distribution is made.

11. Discuss and justify the process by which an "artificial power distribution" is chosen for cycle independence. Provide a table listing all parameters (in the methodology) which are cycle-independent and justify the cycle-independence of each.
12. Discuss how three constant coefficients were fitted for the OTDT trip setpoint equation.
13. Provide a detailed discussion of how the coefficients are reduced to account for the power overshoot.
14. Explain thoroughly how the uncertainties in delta-I measurements are accounted for in the development of the delta-I LCO band (p.64).
15. Provide a detailed discussion of the first paragraph regarding the selection of initial power distributions on p.72.
16. Indicate on Figure 3-11 the selected limiting drops, and similarly draw a curve on Figure 3-12 indicating the conservative lower bounding curve to envelope the tilt versus dropped worth data.
17. Discuss the method and the codes used to simulate the multi-dimensional core physics due to rod position when determining the LCO band.
18. Provide details of (1) the RETRAN auxiliary DNBR calculation as used by YAEC and (2) modeling of the dropped rod reactivity insertion.
19. Explain and justify the YAEC hot channel search algorithm used in the Seabrook methodology and the method of ranking the candidate hot subchannel locations by their closed channel MDNBR values.