

SEISMIC AND STRESS ANALYSIS OF THE LACBWR  
HIGH PRESSURE CORE SPRAY  
SUCTION LINE PIPING SYSTEM

Prepared Under NES Project 5101 for  
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## TABLE OF CONTENTS

	<u>PAGE</u>
1. SUMMARY .....	1-1
2. INTRODUCTION .....	2-1
3. PIPING SYSTEM DESCRIPTION .....	3-1
4. LOADING CRITERIA .....	4-1
4.1 Dead Weight and Other Sustained Mechanical Loads .....	4-1
4.2 Internal Pressure .....	4-1
4.3 Thermal Loading .....	4-1
4.4 Seismic Loading .....	4-1
5. STRESS ACCEPTANCE CRITERIA .....	5-1
5.1 Design Conditions .....	5-1
5.2 Normal Conditions .....	5-1
5.3 Upset Conditions .....	5-2
5.4 Emergency Conditions .....	5-2
5.5 Faulted Conditions .....	5-2
6. ANALYTICAL METHODS .....	6-1
6.1 Mathematical Model .....	6-1
6.2 Static Load Analysis .....	6-1
6.3 Eigenvalue Analysis .....	6-2
6.4 Dynamic (Seismic) Load Analysis .....	6-2
6.5 Stress Analysis .....	6-4
6.6 Pressure Design Check .....	6-4
6.6.2 Consideration of Design Conditions .....	6-5
6.6.3 Consideration of Normal Conditions .....	6-5
6.6.3.1 Determination of Primary Plus Secondary Stress Intensity Range Limitations .....	6-6
6.6.3.2 Determination of Peak Stress Intensity .....	6-7
6.6.3.3 Simplified Elastic-Plastic Discontinuity Analysis .....	6-7
6.6.3.4 Fatigue Evaluation .....	6-8
6.6.3.5 Stress Range Calculations .....	6-9

TABLE OF CONTENTS

	<u>PAGE</u>
6.6.4 Consideration of Upset Conditions .....	6-9
6.6.5 Consideration of Emergency Conditions .....	6-9
6.6 Consideration of Faulted Conditions .....	6-9
7. DISCUSSION OF RESULTS .....	7-1
8. CONCLUSION .....	8-1
9. REFERENCES .....	9-1
APPENDIX A	
APPENDIX B	

LIST OF FIGURES

		<u>PAGE</u>
3.1.1	Mathematical Model LACBWR HPCS Suction Line 1 .....	3-2
3.1.1	Mathematical Model LACBWR HPCS Suction Line 2 .....	3-3
7.1	HPCS Suction Line 1 .....	7-3
7.2	HPCS Suction Line 1 .....	7-4
7.3	HPCS Suction Line 1 .....	7-5
7.4	HPCS Suction Line 1 .....	7-6
7.5	HPCS Suction Line 1 .....	7-7
7.6	HPCS Suction Line 1 .....	7-8
7.7	HPCS Suction Line 1 .....	7-9
7.8	HPCS Suction Line 1 .....	7-10
7.9	HPCS Suction Line 2 .....	7-11
7.10	HPCS Suction Line 2 .....	7-12
7.11	HPCS Suction Line 2 .....	7-13
7.12	HPCS Suction Line 2 .....	7-14
7.13	HPCS Suction Line 2 .....	7-15
7.14	HPCS Suction Line 2 .....	7-16
7.15	HPCS Suction Line 2 .....	7-17
7.16	HPCS Suction Line 2 .....	7-18



LIST OF TABLES

		<u>PAGE</u>
7.1	Natural Frequencies of Vibration .....	7-2
A-1	Pipe Data .....	A-1
A-11	Valve Weights .....	A-2
A-III-1	Static Load Cases .....	A-3
A-III-2	Static Load Cases .....	A-5
A-IV	Dynamic Load Cases .....	A-7
A-V	Spectrum Response Spectrum .....	A-8
B-1	Joint Displacements .....	B-1
B1-1	ECCS Suction Line 1 Joint Displacements .....	B-2
B1-2	ECCS Suction Line 1 Joint Displacements .....	B-6
B-II	Elastic Support Reactions .....	B-14
B-II-1	ECCS Suction Line 1 Elastic Support Reactions .....	B-15
B-II-2	ECCS Suction Line 1 Elastic Support Reactions .....	B-19
B-III	Class 1 Component Stress Analysis PIPESD Results .....	B-23
B-III-1	Seismic and Stress Analysis of ECCS Suction Line 1 .....	B-24
B-III-2	Seismic and Stress Analysis of ECCS Suction Line 2 .....	B-33

I, the undersigned, being a registered Professional Engineer in the State of California, competent in the design and analysis of structures, have examined this seismic and stress report and referenced drawings and specification and certify that to the best of my knowledge the stress report presented herein is in compliance with the criteria set forth in this report.

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## 1. SUMMARY

This report, prepared for Dairyland Power Cooperative, presents the results of seismic and stress analyses of the High Pressure Core Spray (HPCS) piping system suction line for the LACBWR Nuclear Power Station. The seismic and stress analyses are performed in accordance with the design requirements for Class I piping components of the ASME Boiler and Pressure Vessel Code, Section III, Division I, "Nuclear Power Plant Components", 1974. By providing seismic restraints (snubbers) at critical locations of the HPCS suction line, the stresses in the piping due to a seismic event can be reduced to acceptable values. That is, the stresses due to seismic, dead-weight, pressure and thermal expansion loadings, combined according to the ASME Code rules for Class I components would satisfy the design requirements given in the Code with the addition of seismic restraints.

## 2. INTRODUCTION

In response to AEC/DL's request to review the effects of an earthquake event on the LaCrosse Boiling Water Reactor, Dairyland Power Cooperative requested Gulf United Nuclear Fuels Corporation to evaluate the adequacy of the major structures and equipment to withstand seismic loadings. The seismic study performed by Gulf United (GU) Nuclear Fuels Corporation (Ref. 1) included an analysis of the main steam line which indicated that high stresses would be generated in the main steam line during a seismic event. It was also evident from these analyses that the LACBWR piping systems, in general, were not designed to accommodate horizontal accelerations, the primary earthquake induced loading condition. Anticipating the possibility of a seismically induced loss of coolant accident, it was, therefore, concluded that analyses of the major Class I piping systems should be performed to evaluate their structural integrity.

This report presents the seismic and stress analysis for the suction line of the High Pressure Core Spray (HPCS) System. (The HPCS discharge line analyses is presented in a separate report). The High Pressure Core Spray System is the principal emergency core cooling system. In order to verify that the seismic stresses in the HPCS suction line are acceptable, it is necessary to show that the combined stresses in the piping system are within ASME Boiler and Pressure Vessel Code allowable values for Class I Component. This requires that the seismic stresses be combined with the stresses due to deadweight, pressure and thermal loadings in accordance with the ASME Code Section III, Subsection NB rules (Ref. 2).

For the static and dynamic analysis, the High Pressure Core Spray suction line has been mathematically modeled as a finite element model. The static response of the HPCS Suction Line to the dead weight, thermal expansion and anchor movement loadings have been calculated using direct stiffness displacement methods of structural analysis. The seismic response of the HPCS Suction Line to the operating basis earthquake (OBE) and safe shutdown earthquake (SSE) have been determined using response spectrum, modal superposition methods. Stresses due to various loadings have been calculated and combined in accordance with the ASME Code Section III, Subsection NB rules.

Section 3.0 of this report describes the High Pressure Core Spray (HPCS) Suction Line considered in the analysis. The loading criteria, design criteria and analytical methods used in the analyses are given in Section 4.0, 5.0 and 6.0 respectively. The results of the analyses are discussed in Section 7.0. The conclusions are summarized in Section 8.0.

### 3. DESCRIPTION OF PIPING SYSTEM

The High Pressure Core Spray (HPCS) System of the LACBWR power plant is designed to provide an emergency coolant spray to the reactor core in the event that reactor water level drops accidentally. This is done by either direct gravity feed of water from an overhead storage tank to the core spray header under low reactor pressure conditions, or by means of high pressure water injection under high reactor pressure conditions.

In order to simplify the piping system analysis, the long and complex HPCS piping system was divided into two sections: the first consisting generally of the suction piping which runs from the overhead storage tank to the high pressure core spray pumps and the second consisting of the discharge piping which runs from the high pressure core spray pumps to the core spray header inlet. The HPCS discharge piping analysis is presented in a separate report. The subject analysis of this report is, therefore, the HPCS suction line.

To further simplify the analysis the suction line was divided into two subsections: Line 1 as shown in Figure 3.1-1 and Line 2 as shown in Figure 3.1-2. Line 1 consists of the 4" Schedule 40S stainless steel pipe line leading from the 42,000 gallon overhead water storage tank to a 4" X 4" reducer at node point 19. A section of the 4" fuel storage well flooding line connecting at node point 18 is included in the analysis of Line 1. Line 2 begins at node 19, Figure 3.1-2 and consists mostly of 3" schedule 40S stainless steel piping up to the two ECCS high pressure pumps. Rigid anchors located at points of expected large seismic deflections, serve to isolate the suction lines for analytical purposes. The governing design specification used in the analysis of the HPCS piping system is given in Reference 3. The piping arrangement has been taken from the drawings listed in Reference 4. Piping properties have been taken from the information given in the piping specification (Reference 3). The location of piping suspension (hangers, etc.) and their dimensional characteristics were determined from actual visual inspection and measurements at the LACBWR site. This information is summarized in Table A-1 of Appendix A.

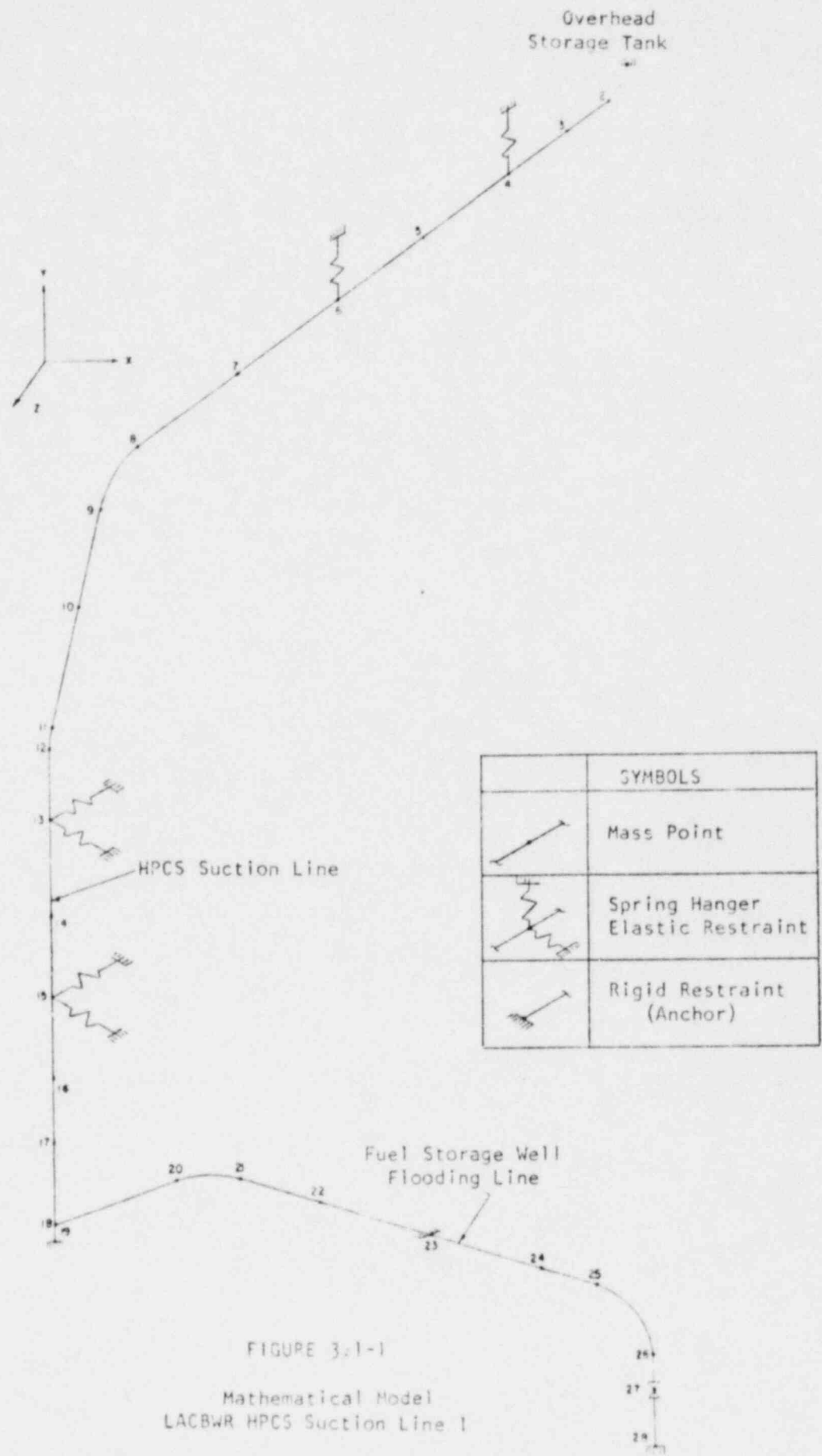
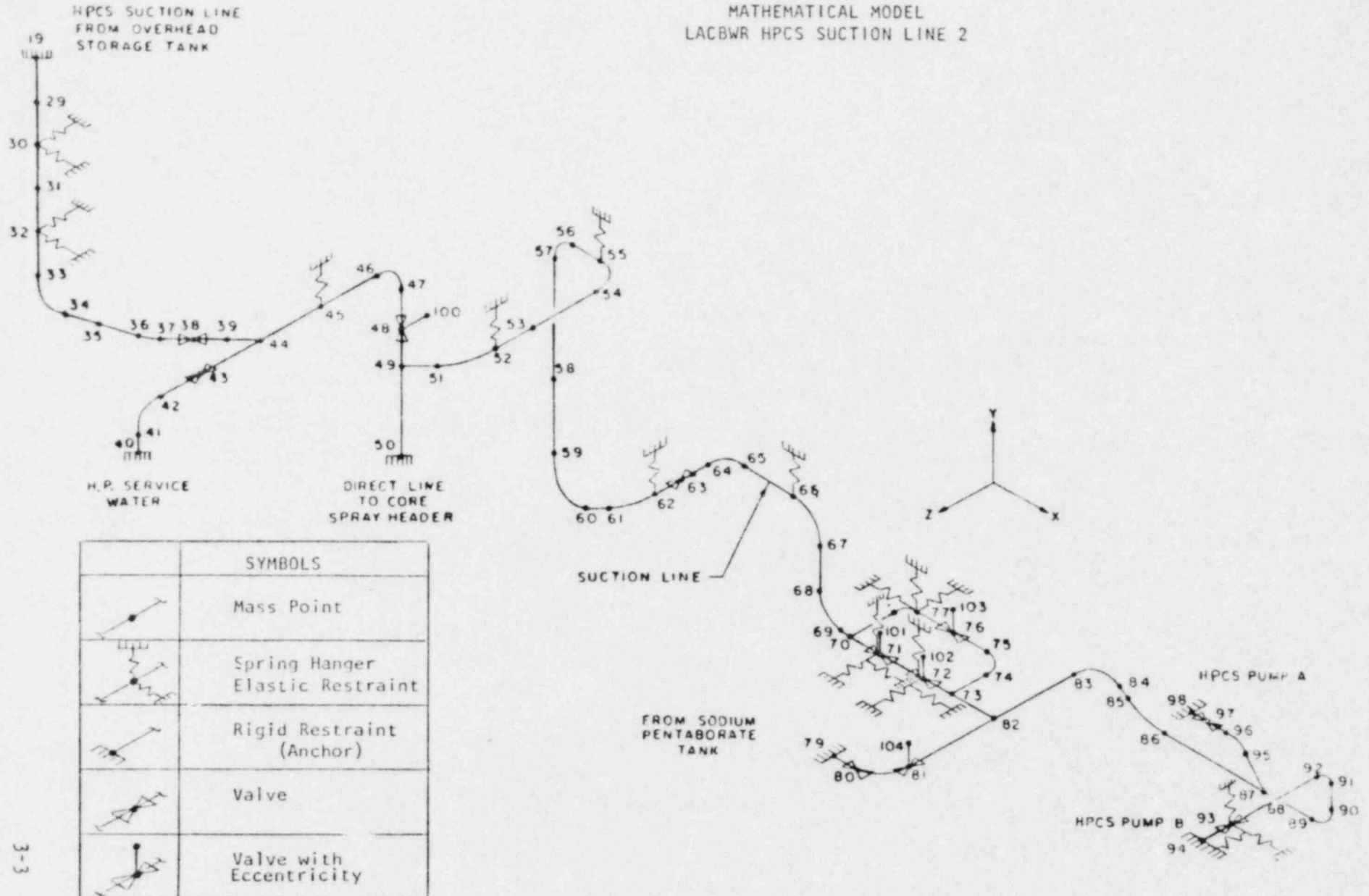


FIGURE 3.1-2  
 MATHEMATICAL MODEL  
 LACBWR HPCS SUCTION LINE 2





#### 4. LOADING CRITERIA

The loading conditions which must be taken into account in performing a Class 1 analysis of a piping system are specified in Subsection NB-3110 of Reference 2. These include dead weight, internal pressure, thermal effects; and earthquake loads. Design, operating, upset, emergency and faulted condition loadings must be considered in the analysis as specified in the stress acceptance criteria (Section 5 of this report). The static and dynamic load cases considered in the analysis are described below and the detail input data are summarized in Table A-III and A-IV of Appendix A.

##### 4.1 Dead Weight Loading (Static Load Case 1)

The dead weight of the piping system is calculated assuming the system to be insulated and filled with water. The weights of valves and valve operators, with appropriate eccentricities are included in the analysis. Valve weight and dimensions are taken from vendor drawings and information supplied by DPC and are summarized in Table A-II of Appendix A.

##### 4.2 Thermal Loading (Static Load Case 2)

The HPCS suction line is basically a cold line containing room temperature water from the overhead storage tank. Thermal expansion stresses are calculated assuming the design temperature of 120°F to be the normal operating condition. Thermal discontinuity and thermal gradient secondary bending stresses are negligible at this temperature and are, therefore, not considered in the analysis.

##### 4.3 Internal Pressure (Static Load Cases 3 and 4)

The normal operating pressure for the HPCS system is the static head resulting from the overhead water storage tank. Constant internal operating pressures of 20 psi and 50 psi, Load Case 3, are conservatively assumed for suction lines 1 and 2 respectively. A pressure of 100 psig taken from reference 3 is used as the design condition (Load Case 4) for the complete HPCS Suction Line.

##### 4.4 Seismic Loading

A dynamic analysis of the piping system is performed using the response spectrum modal superposition method of analysis (Section 6.4). Two seismic loading events are considered: the safe shutdown earthquake (SSE), and the operating basis earthquake (OBE). The established design criteria (Ref. 5, Regulatory Guide 1.48, May, 1973) for class 1 analysis specifies that the OBE (or 1/2 SSE) must be considered in conjunction with the normal and upset plant condition while the SSE must be considered in conjunction with the faulted plant condition.



Seismic inertia loading is imposed on the piping system in the form of seismic acceleration spectra which were derived for the LACBWR plant (Ref. 1). The horizontal acceleration spectra used for the HPCS lines 1 and 2 are those corresponding respectively to the subsystem support points on the reactor containment shell at elevations of 745 feet (Water Storage Tank) and 700 feet (upper floor). The vertical response spectrum for the SSE loading is taken as  $2/3$  of the horizontal SSE ground response spectrum assuming no amplification of vertical response in the structure. For the Operating Basis Earthquake the vertical piping response spectrum is taken as  $1/2$  of the SSE vertical response spectrum. Damping values used are 1 percent for the OBE and 2 percent for the SSE.

The horizontal spectra in either the global X- direction (Dynamic Load Cases 7 and 9) or the global Z- direction (Dynamic Load Cases 8 and 10) are applied simultaneously with the vertical spectra in the global Y- direction. Load cases 7 and 8 represent the Operating Basis Earthquake while 9 and 10 represent the SSE earthquake. The applicable response spectra used in the analysis for dynamic load cases are shown in Table A-V of Appendix A.

Seismically induced anchor movements (Static Load Cases 5 and 6) for the OBE were estimated by calculating low frequency displacements from the containment vessel response spectra at the different anchor point elevations.

## 5. STRESS ACCEPTANCE CRITERIA

The requirements for acceptability of a Class 1 piping system are given in AEC Regulatory Position 1 of Reference 7 and Subsections NB 3600 of Section III of the ASME Boiler and Pressure Vessel Code, Reference 2. Calculated stresses resulting from the design and operating loading conditions given in Subsection NB-3110 and NB-3620 must meet the stress limits of equations 9 through 14 of Subsection NB-3650 of the ASME Code.

### 5.1 Design Conditions

The primary stress intensity, resulting from the combined effects of the design pressure (Load Case 4) and the resultant moment loading due to loads caused by dead weight (Load Case 1) and the Operating Basis Earthquake (Load Cases 7 and 8), and calculated in accordance with equation 9 of Subsection NB-352 of the Code must be less than 1.5 times the allowable design stress intensity,  $S_m$ , at maximum temperature.

### 5.2 Normal Conditions

The primary plus secondary stress intensity range resulting from the combined effects of thermal expansion, linear thermal gradient and discontinuity, (Load Case 2), operating pressure (Load Case 3), anchor movements (Load Cases 5 or 6) and earthquake effects (Load Cases 7 or 8), calculated in accordance with equation 10 of the Code must be less than 3 times  $S_m$ . In the event that the above requirement is not met the piping product may still be acceptable provided the requirements of a simplified Elastic-plastic discontinuity analysis are met. This requirement is met if 1) the nominal expansion stress resulting from thermal expansion and thermal anchor movements, (Load Case 2), calculated in accordance with equation 12 of the Code is less than 3  $S_m$  and 2) if the range of primary plus secondary membrane plus bending stress intensity, resulting from the combined loading of operating pressure (Load Case 3), dead weight (Load Case 1), one-half the range of the earthquake (Load Cases 7 or 8) and thermal discontinuity stresses, calculated according to equation 13 of the code is less than 3  $S_m$ .

The requirements for acceptability under cyclic loading conditions are met by first calculating the peak stress intensity by means of equation 11 of the Code, resulting from the loadings specified for equation 10 plus the loadings resulting from the non-linear portion of the thermal gradient through the wall thickness (considered negligible in this analysis), and then calculating the alternating stress intensity in accordance with equation 14 of the Code. The total number of operating stress cycles must then be less than those determined from the fatigue curves from Appendix I-9 of the Code for the calculated alternating stress intensity in accordance with the requirements of paragraphs NB 3653.4 and NB 3653.5 of the Code.

### 5.3 Upset Conditions

The requirements for acceptability under upset conditions (not specified in this analysis) are the same as for Normal Conditions.

### 5.4 Emergency Conditions

The requirement for acceptability under emergency conditions (not specified in this analysis) is that the primary stress intensity, as calculated by equation 9 of the Code, must be less than  $2.25 S_m$ .

### 5.5 Faulted Conditions

Under faulted conditions the primary stress intensity resulting from the combined effects of design pressure (Load Case 4), dead weight (Load Case 1) and the vibratory motion of the full Safe Shutdown Earthquake (Load Cases 9 or 10) as calculated by equation 9 of the Code must be less than  $3 S_m$ .

## 6. ANALYTICAL METHODS

### 6.1 Mathematical Model

In order to perform static, dynamic and stress analyses, the continuous piping system is mathematically modeled as an assembly of elastic structural elements interconnected at discrete nodal points (Figure 3.1). Nodal points are located at all points of interest in the piping system such as elbows, valves, anchorages, hangers, tee intersections, load points, all structural and material discontinuities, etc. This three dimensional multidegree-of-freedom model of the piping system is attached to the "ground" (structure) by means of rigid hangers, support springs, hydraulic snubbers and anchors. Stiffness characteristics of structural elements are related to the moment of inertia and the axial and effective shear area of the pipe cross section. The stiffness characteristics of the elbows and tee connections are modified to account for local deformation by using the flexibility factors given in the ASME Code (Ref. 2).

For the seismic analysis the distributed mass of the piping system is lumped at the system nodal points. Masses are lumped so that the lumped mass, multi-degree-of-freedom model represents the dynamic characteristics of the piping system. In order to reduce the number of dynamic degrees-of-freedom, only translational degrees-of-freedom are considered at each mass point (the masses associated with the rotational degrees-of-freedom are set to zero). This assumption has been shown to be completely satisfactory for accurate analysis of seismic response. Special items such as valves and actuators are modeled by lumping their masses at an appropriate offset from the center-line of the piping system.

### 6.2 Static Load Analysis

The static load analysis involves the application of the following loading conditions and their combinations:

- . Design Pressure
- . Gravity Loading (dead weight) and Sustained Mechanical Loads
- . Support Displacement
- . Thermal Expansion

For the pressure loadings, the hoop and longitudinal stresses in the affected piping are calculated using the formulae given in the Code (see Section 6.5).

For the deadweight, support displacement, or thermal expansion loading conditions the following equations of equilibrium written in matrix form are solved:

$$KU = P \quad (1)$$

where:

- K = System stiffness matrix
- U = Nodal point displacement vector
- P = External forces, deadweight or equivalent thermal load vector.

The system stiffness matrix is obtained from element stiffness matrices using direct stiffness methods. The unknown nodal displacements U are obtained as follows:

$$U = K^{-1}P \quad (2)$$

The inversion of the stiffness matrix is performed using the Gauss-Seidel technique.

From the nodal displacements U, the member internal forces are determined using the member stiffness matrix. Finally the member internal forces are used in calculating the stresses.

### 6.3 Eigenvalue Analysis

The eigenvalues (natural frequencies) and the eigenvectors (mode shape) for each of the natural modes of vibration are calculated by solving the following frequency equation:

$$(K - \omega_n^2 M) \{\phi_n\} = \{0\} \quad (3)$$

where:

- $\omega_n$  = Natural angular frequency for the  $n^{\text{th}}$  mode
- M = System mass matrix
- $\phi_n$  = Mode shape vector for the  $n^{\text{th}}$  mode
- 0 = Null vector

The eigenvalue/eigenvector extraction is performed using the Householder-QR technique.

### 6.4 Dynamic (Seismic) Load Analysis

Considering only translational degrees of freedom and assuming viscous (velocity proportional) form of damping, the equation of motion in matrix form can be expressed as follows:

$$M(\ddot{U}_t + \ddot{U}_{gt}) + C\dot{U}_t + KU_t = 0 \quad (4)$$

where:

$\ddot{U}_t$  = Relative acceleration time history vector

$\ddot{U}_{gt}$  = Ground acceleration time history vector

$\dot{C}$  = Damping matrix

$\dot{U}_t$  = Velocity time history vector

$U_t$  = Relative displacement time history vector

Rearranging equation (4)

$$M\ddot{U}_t + C\dot{U}_t + KU_t = -M\ddot{U}_{gt} = P_{eff} \quad (5)$$

To uncouple equation (5), assume

$$U = \phi Y_t$$

where:

$\phi$  = Characteristic free vibration mode shapes matrix

$Y_t$  = Generalized coordinate displacement time history vector

Pre-and post-multiplying equation (5) by the transpose of  $\phi$  and by  $\phi$  respectively and using orthogonality conditions, the following uncoupled equations of motion are obtained:

$$\ddot{Y}_{nt} + 2\omega_n \lambda_n \dot{Y}_{nt} + \omega_n^2 Y_{nt} = M_n^{-1} R_n \ddot{U}_{gt} \quad (6)$$

where:

$Y_{nt}$  = Generalized displacement coordinate time history for  $n^{\text{th}}$  mode.

$\lambda_n$  = Damping ratio for the  $n^{\text{th}}$  mode expressed as percent of critical damping

$M_n^{-1}$  = Generalized mass for the  $n^{\text{th}}$  mode

$$= \phi_n^T M \phi_n = M_i \phi_{in}^2$$

The mode shape  $\phi_n$  is normalized such that  $M_n^{-1} = 1$

$R_n$  = Participation factor for the  $n^{\text{th}}$  mode

$$= \phi_n^T M I = \sum M_i \phi_{in}$$

$I$  = Column vector whose elements are generally unity

The solution for the differential equation (6) is given by the Duhamel Integral

$$Y_{nt} = \frac{R_n}{M_n^* \omega_n} \int_0^t \ddot{U}_{gt} e^{-\lambda_n \omega_n (t-T)} \sin \omega_n (t-T) dT$$

Using the response spectrum method of analysis, the maximum values of the generalized response for each mode is given by:

$$\ddot{Y}_{n \max} = \frac{R_n S_{an}}{M_n^*}$$

where:

$\ddot{Y}_{n \max}$  = Maximum generalized coordinate acceleration response for the  $n$ th mode.

$S_{an}$  = Spectral acceleration value for the  $n$ th mode (from the applicable response spectrum curve)

From the maximum generalized coordinate response, the maximum acceleration ( $\ddot{U}_{n \max}$ ) and maximum inertia forces ( $F_{n \max}$ ) at each mass point are given by:

$$\ddot{U}_{n \max} = \ddot{Y}_{n \max} \phi_{In}$$

$$F_{n \max} = M_n \ddot{U}_{n \max}$$

The inertia forces ( $F_{n \max}$ ) for each of the system natural modes are applied as external static forces, and the piping system response (displacements, member internal forces and stresses) are calculated using the procedure described in Section 4.2. Total system response is then obtained by combining the individual modal response values by the square-root of the sum of the squares method; lower modes having large contribution to the response (all modes having natural frequency under 30 cycles per second) are considered and higher modes with negligible participation are neglected.

## 6.5 Stress Analysis

The design requirements of Section III of the ASME Boiler and Pressure Vessel Code, Reference 2 (henceforth referred to as the "Code") for Class I piping systems are satisfied when the calculated stresses in the piping system due to thermal expansion, weight, and other sustained and occasional loads are combined in accordance with, and meet the limitations of Subsection NB-3600 of the Code. These requirements are described below.

## 6.6 Pressure Design Check

The minimum pipe wall thickness requirements for the design pressure are met by satisfying equation (1).



$$t_m = \frac{PD_o}{2(S_m + YP)} \quad (1)$$

where

$t_m$  = the minimum required wall thickness, in.

$P$  = internal design pressure, psi.

$D_o$  = outside diameter of pipe, in.

$S_m$  = maximum allowable stress in the material at the design temperature from Tables 1-1.0 of the Code, psi.

$Y$  = 0.4

#### 6.6.2 Consideration of Design Conditions

The primary stress intensity limit is satisfied by meeting the requirements of equation (9)

$$B_1 \frac{PD_o}{2t} + B_2 \frac{D_o}{2I} M_i \leq 1.5S_m \quad (9)$$

where:

$B_1, B_2$  = primary stress indices for the specific product under investigation (From Subsection NB-3680 of the Code)

$P$  = design pressure, psi

$D_o$  = outside diameter of pipe, in.

$t$  = nominal wall thickness of component

$I$  = moment of inertia, in.<sup>4</sup>

$M_i$  = resultant moment loading due to loads caused by (1) weight, (2) earthquake, considering only one-half the range of the earthquake and excluding the effects of anchor displacement due to earthquake, and (3) other sustained design mechanical loads.

$S_m$  = allowable design stress intensity value, psi

#### 6.6.3 Consideration of Normal Conditions

Protection against fatigue failure is provided for by means of one of the two analyses dependent on whether the structure is subjected to elastic cycling or plastic cycling. The criterion for establishing whether the structure cycles



in the elastic range or the plastic range is set forth in equation (10) (Paragraph 6.6.3.1 below) of the ASME Code. Compliance with equation (10) assures that, after a few cycles of load application, the maximum stress will remain within the range of tensile and compressive yield strengths, i.e. within the elastic range. If this criterion is met, the fatigue evaluation (Section 6.6.3.4) is based on purely elastic behaviour. If the criterion is not met, an elastic-plastic discontinuity analysis must be made. (Section 6.6.3.3 below).

#### 6.6.3.1 Determination of Primary Plus Secondary Stress Intensity Range Limitations

This calculation is based upon the effect of changes which occur in mechanical or thermal loadings which take place as the system goes from one load set, such as pressure, temperature, moment, and force loading, to any other load set which follows it in time. It is the range of pressure, temperature, moment, between two load sets which is to be used in the calculations.

The primary plus secondary stress intensity range limitations are satisfied by meeting the requirements of equation (10).

$$S_n = C_1 \frac{P_0 D_0}{2t} + C_2 \frac{D_0}{2l} M_i + \frac{1}{2(1-\nu)} E \alpha |\Delta T_1| + C_3 E_{ab} [\alpha_a T_a - \alpha_b T_b] \leq 3S_m$$

where:

$C_1, C_2, C_3$  = secondary stress indices for the specific component under investigation (NB-3680)

$D_0, t, l, S_m$  = are as defined for Equation (9)

$M_i$  = range of moment loading due to (1) thermal expansion (2) anchor movements from any cause, (3) earthquake effects, and (4) other mechanical loads.

$|\Delta T_1|$  = range of absolute value (without regard to sign) of the temperature difference between the temperature of the outside surface ( $T_0$ ) and the temperature of the inside surface ( $T_i$ ) of the piping product assuming moment generating equivalent linear temperature distribution.

$T_a(T_b)$  = range of average temperature on side a(b) of gross structural discontinuity or material discontinuity.

$\alpha_a(\alpha_b)$  = coefficient of thermal expansion on side a(b) of a gross structural discontinuity or material discontinuity at room temperature.

$E_{ab}$  = average modulus of elasticity of the two sides of a gross structural discontinuity or material discontinuity at room temperature, psi.

$E\alpha$  = modulus of elasticity ( $E$ ) times the mean coefficient of thermal expansion ( $\alpha$ ) both at room temperature, psi.

$\nu$  = poisson's ratio = 0.3

$P_o$  = range of operating pressure, psi

### 6.6.3.2 Determination of Peak Stress Intensity

The peak stress intensity is calculated by means of equation (11) of the Code for every pair of load sets. This is the maximum stress intensity at a point including any local structural discontinuity (or notch) effects and any local thermal stresses.

$$S_p = K_1 C_1 \frac{P_o D_o}{2t} + K_2 C_2 \frac{D_o}{2l} M_i + \frac{1}{2(1-\nu)} K_3 E\alpha |\Delta T_1| + K_3 C_3 E_{ab} |\alpha_a T_a - \alpha_b T_b| + \frac{1}{1-\nu} E\alpha |\Delta T_2|$$

where:

$K_b, K_2, K_3$  = local stress indices for the specific component under investigation (NB-3680)

$E\alpha$  = same as in Equation (10)

$\Delta T_2$  = range of absolute value (without regard to sign) for that portion of the nonlinear thermal gradient through the wall thickness not included in  $\Delta T_2$  of Equation 10 °F below.

For a quantitative definition of  $|\Delta T_1|$  and  $|\Delta T_2|$ , see NB-3653.2(b) of the Code. All other terms are as defined in Equation (10).

The peak stress,  $S_p$ , is used to calculate the alternating stress intensity,  $S_{alt}$ , for the fatigue evaluation (see Section 6.6.3.4)

### 6.6.3.3 Simplified Elastic-Plastic Discontinuity Analysis

If the primary plus secondary stress intensity requirements of equation (10) are not met, the fatigue evaluation must include the effects of plastic cycling by means of the simplified elastic-plastic discontinuity analysis as described below. Only those pairs of load sets not satisfying equation (10) need be considered. Equation (12) imposes a limitation of  $3 S_m$  on the magnitude of the thermal expansion stress to prevent possible collapse due to the development of a hinge moment.

$$S_e = C_2 \frac{D_o}{2t} M_i^* \leq 3S_m \quad (12)$$

where:

$S_e$  = nominal value of expansion stress

$M_i^*$  = same as  $M_i$  in Equation (10) except it includes only moments due to thermal expansion and thermal anchor movements

The range of primary plus secondary membrane plus bending stress intensity, excluding thermal bending and thermal expansion stresses shall be  $\leq 3S_m$ . This requirement is satisfied by meeting Equation (13) below.

$$C_1 \frac{P_o D_o}{2t} + C_2 \frac{D_o M_i}{2t} + C_3 E_{ab} |d_b T_a - d_b T_b| \leq 3S_m \quad (13)$$

#### 6.6.3.4 Fatigue Evaluation

If the conditions of equation (10) are met, or alternatively the conditions of equations (12) and (13) are met, the value of the alternating stress intensity,  $S_{alt}$ , is calculated by equation (14) of the Code.

$$S_{alt} = K_e \frac{S_p}{2} \quad (14)$$

where:

$S_{alt}$  = alternating stress intensity

$S_p$  = peak stress intensity value calculated by Equation (11)

$K_e$  = 1.0 for  $S_n \leq 3S_m$  (i.e. when equation 10 is satisfied)

$$= 1.0 + \frac{(1-n)}{n(m-1)} \left( \frac{S_n}{3S_m} - 1 \right) \text{ for } 3S_m < S_n$$

<  $3_m S_m$

$$= \frac{1}{n} \text{ for } S_n \geq 3_m S_m$$

$S_n$  = primary plus secondary stress intensity value calculated in Equation (10)

$m$  and  $n$  = material parameters given in NB-3228.3 (b) of the Code

The number of allowable cycles,  $N$ , for a given stress cycle is then determined from applicable design fatigue curves given in Appendix I-9.0 of the Code for the calculated values of  $S_{alt}$ . If more than one operational cycle is being considered which produces significant fluctuating stresses, a cumulative usage factor must be determined in accordance with Subsection NB-3222.4 of the Code.

The cumulative usage factor, U, is defined as:

$$U = \sum U_i = \sum \frac{n_i}{N_i}$$

where:

- $U_i$  = usage factor for each type of stress cycle, i
- $n_i$  = specified number of times a given stress cycle, i, will be repeated during the life of the component
- $N_i$  = allowable number of repetitions for a given stress cycle, i, from table I-90 of the Code.

The cumulative usage factor, U, must not exceed 1.0.

#### 6.6.3.5 Stress Range Calculations

The stress range evaluation is carried out by means of one or both of two analyses. The first analysis is a maximum stress range calculation in which the maximum range of stresses from each load set pair is used to form a "worst load case" which is assumed to occur over the total number of system cycles. If this conservative check results in an allowable number of cycles not exceeding the total number of system cycles, then no further analysis is required for the component. If the maximum stress range check fails, an individual stress range calculation can be made to establish component acceptability. In this evaluation the stress ranges for individual load sets are calculated, pair by pair, in such a manner as to maximize stress ranges and the cumulative usage factor, which must be less than 1.0.

#### 6.6.4 Consideration of Upset Conditions

The procedure and stress limits for evaluating upset conditions are the same as for operating conditions.

#### 6.6.5 Consideration of Emergency Conditions

The primary stress intensity requirements of equation (9) above (Section 5.2) must be met using a stress limit of  $2.25 S_m$ .

#### 6.6.6 Consideration of Faulted Conditions

The primary stress intensity requirements of equation (9) above (Section 6.6.2) for the combined loading effects of system design pressure, deadweight and the vibratory motion of the Safe Shutdown Earthquake must be met using a stress limit of  $3S_m$ .

## 7. DISCUSSION OF RESULTS

The results of the HPCS suction line piping analysis are based on the assumption that restraints are located at node points 19, 28, 40, 50 and 79 of Figure 3.1. These additional restraints, located at positions of expected large seismic deflections, can be made rigid anchors due to low thermal expansion effects.

The natural frequencies, of the lower modes of vibration of the piping systems up to 35 cycles per second, are given in Table 7-1 and indicate generally flexible (low frequency) systems.

The deflections at each node point due to the various load cases are summarized in Table B-1, pages B-1 through B-13 of Appendix B. The maximum deflection due to the SSE seismic inertia loading (Load Case 9) is 1.20 inches at node point 8 in HPCS line. For a flexible piping system this deflection should be acceptable. The maximum deflection due to thermal expansion (Load Case 2) is 0.18 inch at node 65. Table B-11, pages B-14 through B-22 of Appendix B, summarize the elastic support reaction forces.

The results of the detailed stress analyses in accordance with the requirements of Subsection NB-3650 of the ASME Code for Class I piping systems are given in Table B111, pages B-23 through B-59 of Appendix B. Class I stresses are summarized in Figures 7.1 through 7.16 indicating node points with stresses exceeding 5 ksi for specified Class I loading conditions. The maximum allowable number of stress cycles based on the maximum peak stress determined from Figure I-9.2 of Section III of the ASME Code, is in excess of  $10^6$  cycles. Consequently, in accordance with paragraph NB-3653.5 of the ASME Code, the maximum usage factor for stress cycling between the X and Z direction earthquakes, occurring at node point 18 of Line 1, may be taken as 0.0. From these results it can be concluded that maximum and cyclic Code stress requirements are met for the specified loading conditions.

TABLE 7.1

## NATURAL FREQUENCIES OF VIBRATION

## HPCS Suction Line 1

<u>Mode No.</u>	<u>Frequency (CPS)</u>
1	3.62
2	10.27
3	20.20
4	20.33
5	32.83
6	33.11

## HPCS Suction Line 2

<u>Mode</u>	<u>Frequency (CPS)</u>	<u>Mode</u>	<u>Frequency (CPS)</u>
1	3.13	15	20.36
2	3.44	16	20.84
3	6.15	17	21.01
4	6.53	18	21.49
5	7.10	19	22.19
6	8.02	20	22.64
7	8.82	21	24.92
8	10.68	22	27.49
9	12.05	23	28.13
10	12.23	24	28.16
11	14.59	25	28.79
12	15.93	26	30.40
13	19.18	27	33.60
14	19.75	28	34.24

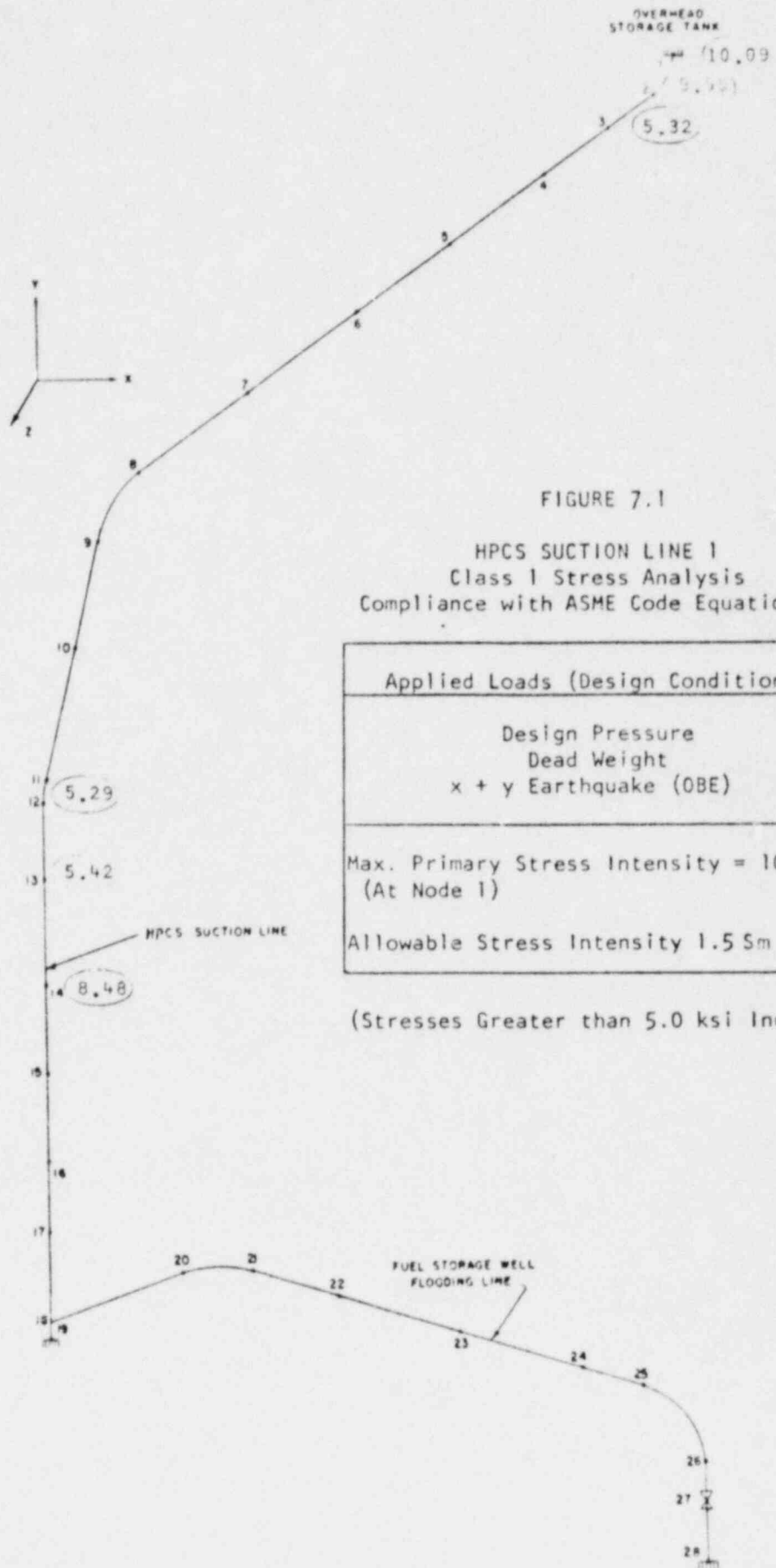


FIGURE 7.1

HPCS SUCTION LINE 1  
 Class 1 Stress Analysis  
 Compliance with ASME Code Equation 9

Applied Loads (Design Conditions)
Design Pressure Dead Weight x + y Earthquake (OBE)
Max. Primary Stress Intensity = 10.99 Ksi (At Node 1)
Allowable Stress Intensity $1.5 S_m = 3.0$ Ksi

(Stresses Greater than 5.0 ksi Indicated)



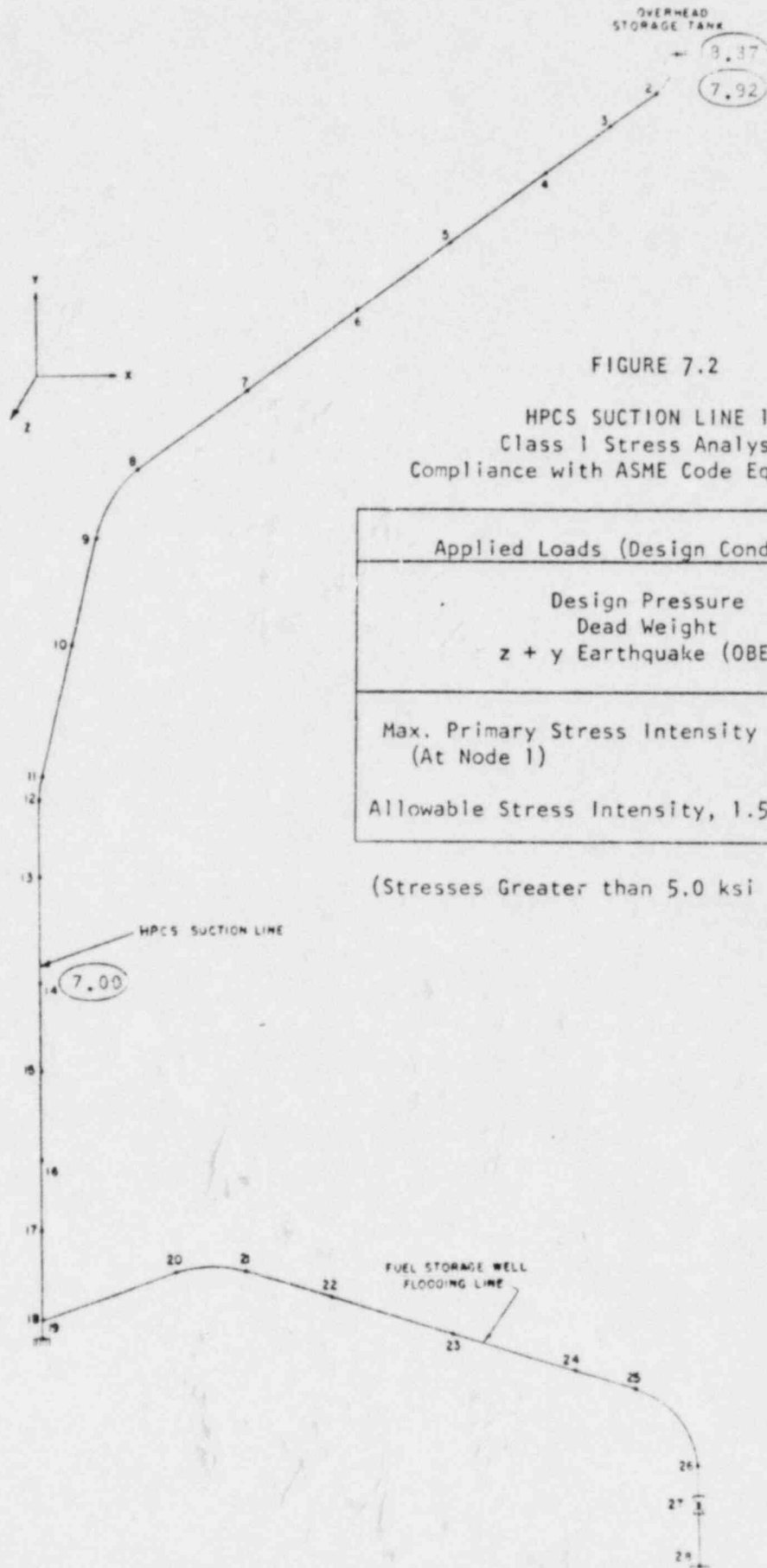


FIGURE 7.2  
 HPCS SUCTION LINE 1  
 Class 1 Stress Analysis  
 Compliance with ASME Code Equation 9

Applied Loads (Design Conditions)
Design Pressure Dead Weight z + y Earthquake (OBE)
Max. Primary Stress Intensity = 8.37 ksi (At Node 1)
Allowable Stress Intensity, $1.5 S_m = 30.0$ ksi

(Stresses Greater than 5.0 ksi Indicated)



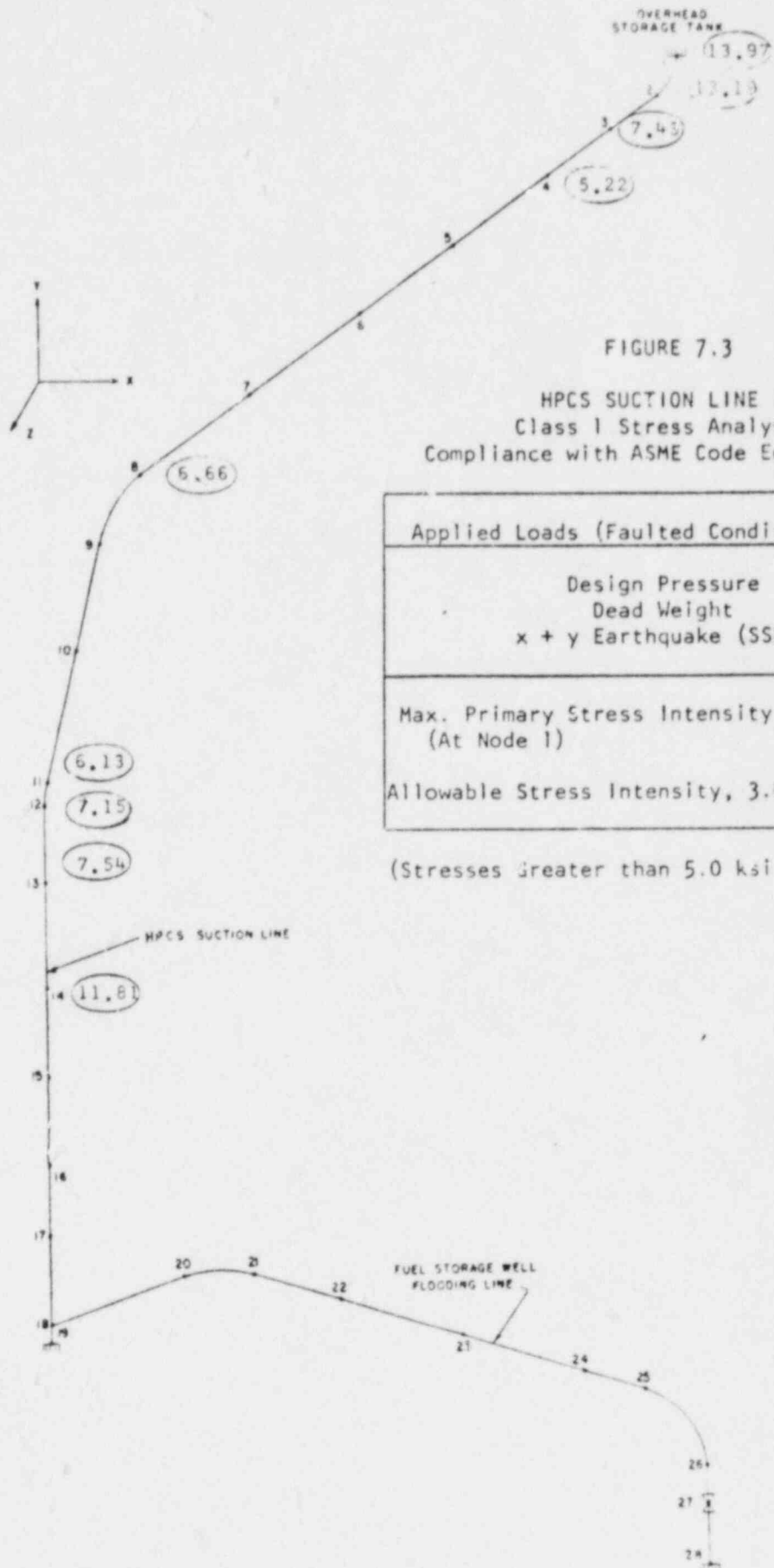


FIGURE 7.3

HPCS SUCTION LINE 1  
 Class 1 Stress Analysis  
 Compliance with ASME Code Equation 9

Applied Loads (Faulted Conditions)
Design Pressure Dead Weight x + y Earthquake (SSE)
Max. Primary Stress Intensity = 13.97 ksi (At Node 1)
Allowable Stress Intensity, $3.0 S_m = 60.0$ ksi

(Stresses Greater than 5.0 ksi Indicated)

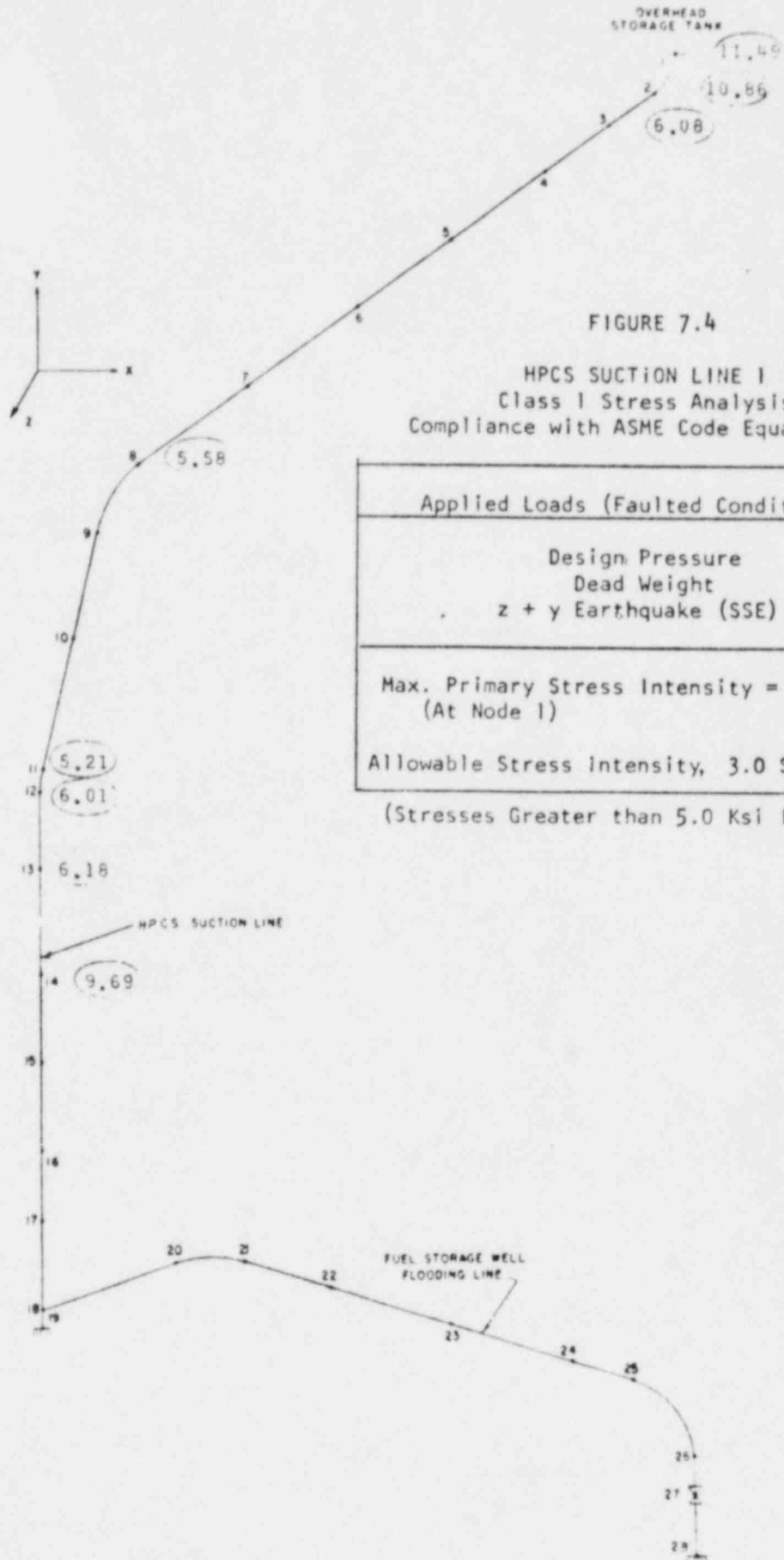


FIGURE 7.4  
 HPCS SUCTION LINE I  
 Class I Stress Analysis  
 Compliance with ASME Code Equation 9

Applied Loads (Faulted Conditions)
Design Pressure Dead Weight z + y Earthquake (SSE)
Max. Primary Stress Intensity = 11.49 ksi (At Node 1)
Allowable Stress Intensity, $3.0 S_m = 60.0$ ksi

(Stresses Greater than 5.0 Ksi Indicated)

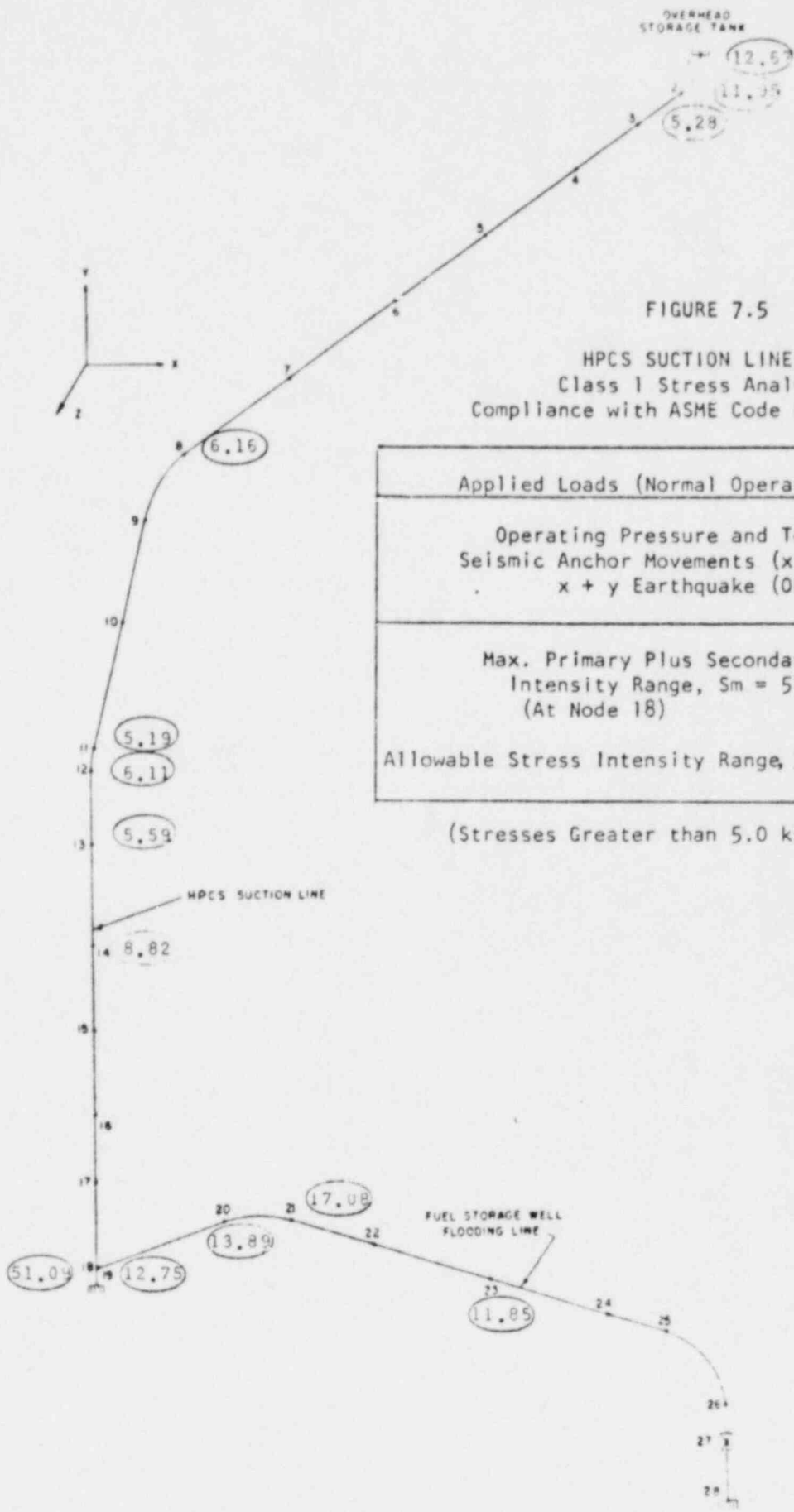


FIGURE 7.5

HPCS SUCTION LINE I  
 Class I Stress Analysis  
 Compliance with ASME Code Equation 10

Applied Loads (Normal Operating Cond.)
Operating Pressure and Temperature Seismic Anchor Movements (x - direction) x + y Earthquake (OBE)
Max. Primary Plus Secondary Stress Intensity Range, $S_m = 51.09$ ksi (At Node 18)
Allowable Stress Intensity Range, $3.0 S_m = 60.0$ ksi

(Stresses Greater than 5.0 ksi Indicated)

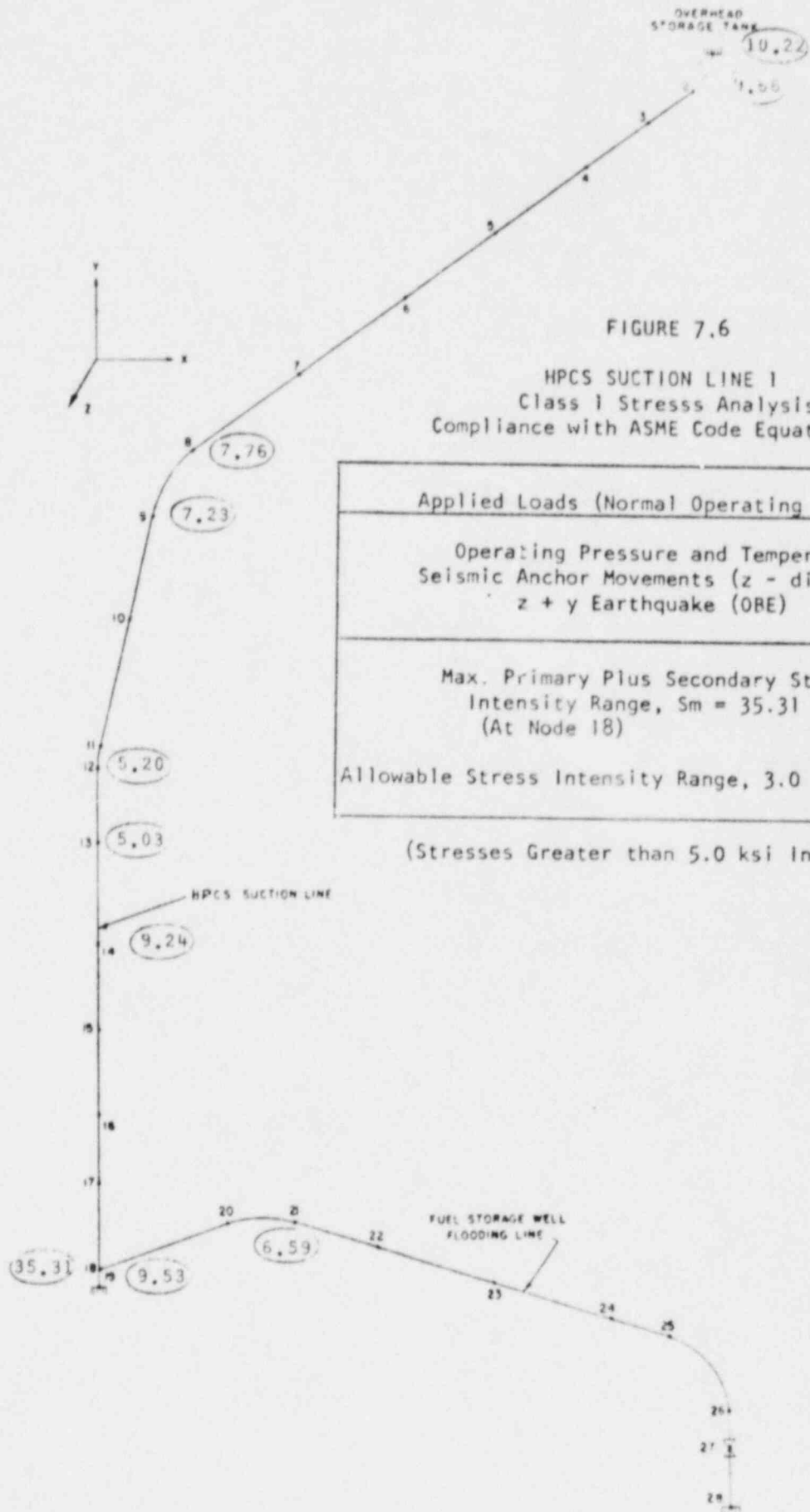


FIGURE 7.6

HPCS SUCTION LINE 1  
 Class 1 Stress Analysis  
 Compliance with ASME Code Equation 10

Applied Loads (Normal Operating Cond.)
Operating Pressure and Temperature Seismic Anchor Movements (z - direction) z + y Earthquake (OBE)
Max. Primary Plus Secondary Stress Intensity Range, $S_m = 35.31$ ksi (At Node 18)
Allowable Stress Intensity Range, $3.0 S_m = 60.0$ Ksi

(Stresses Greater than 5.0 ksi Indicated)

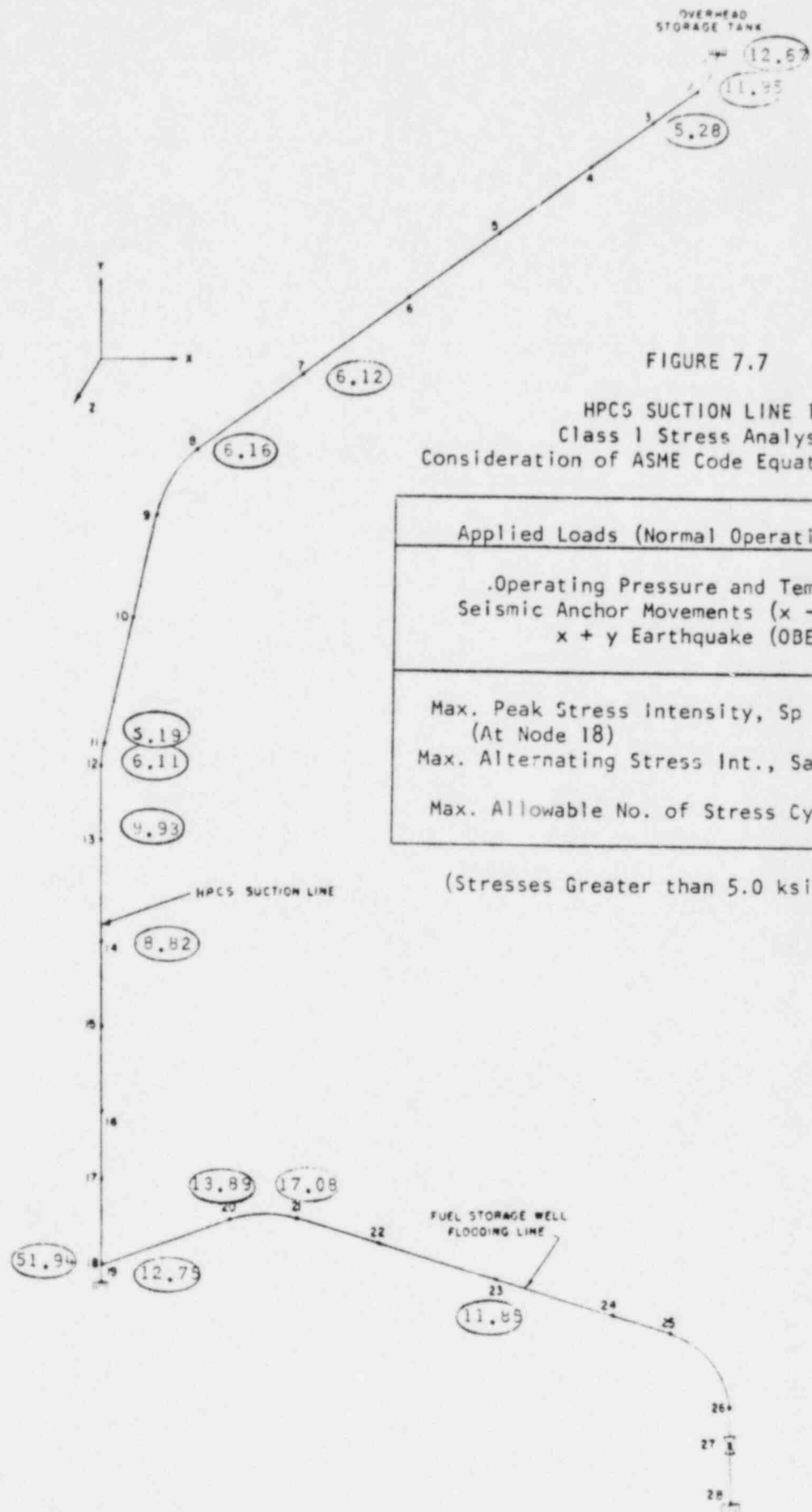


FIGURE 7.7

HPCS SUCTION LINE 1  
 Class 1 Stress Analysis  
 Consideration of ASME Code Equations 11 & 14

Applied Loads (Normal Operation Cond.)
Operating Pressure and Temperature Seismic Anchor Movements (x - direction) x + y Earthquake (OBE)
Max. Peak Stress Intensity, $S_p = 51.94$ ksi (At Node 18)
Max. Alternating Stress Int., $S_{alt} = 25.97$ ksi
Max. Allowable No. of Stress Cycles, $N > 10^6$

(Stresses Greater than 5.0 ksi Indicated)

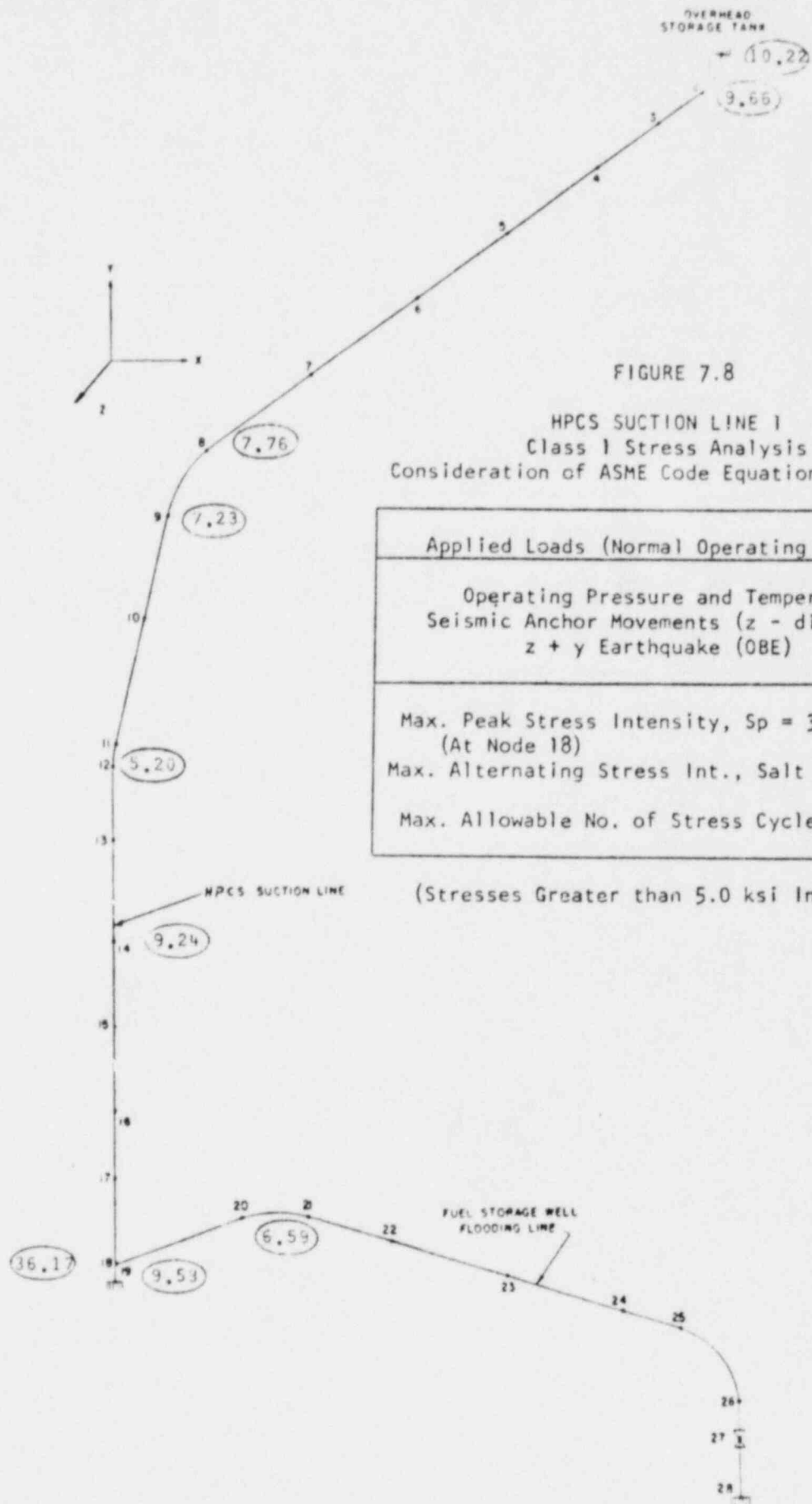


FIGURE 7.7

HPCS SUCTION LINE 2  
 Class 1 Stress Analysis  
 Compliance with ASME Code Equation 9

Applied Loads (Design Conditions)
Design Pressure Dead Weight $x + y$ Earthquake (OBE)
Max. Primary Stress Intensity = 8.89 ksi (At Node 68)
Allowable Stress Intensity, $1.5 S_m = 30.0$ ksi

(Stresses Greater than 5.0 ksi Indicated)

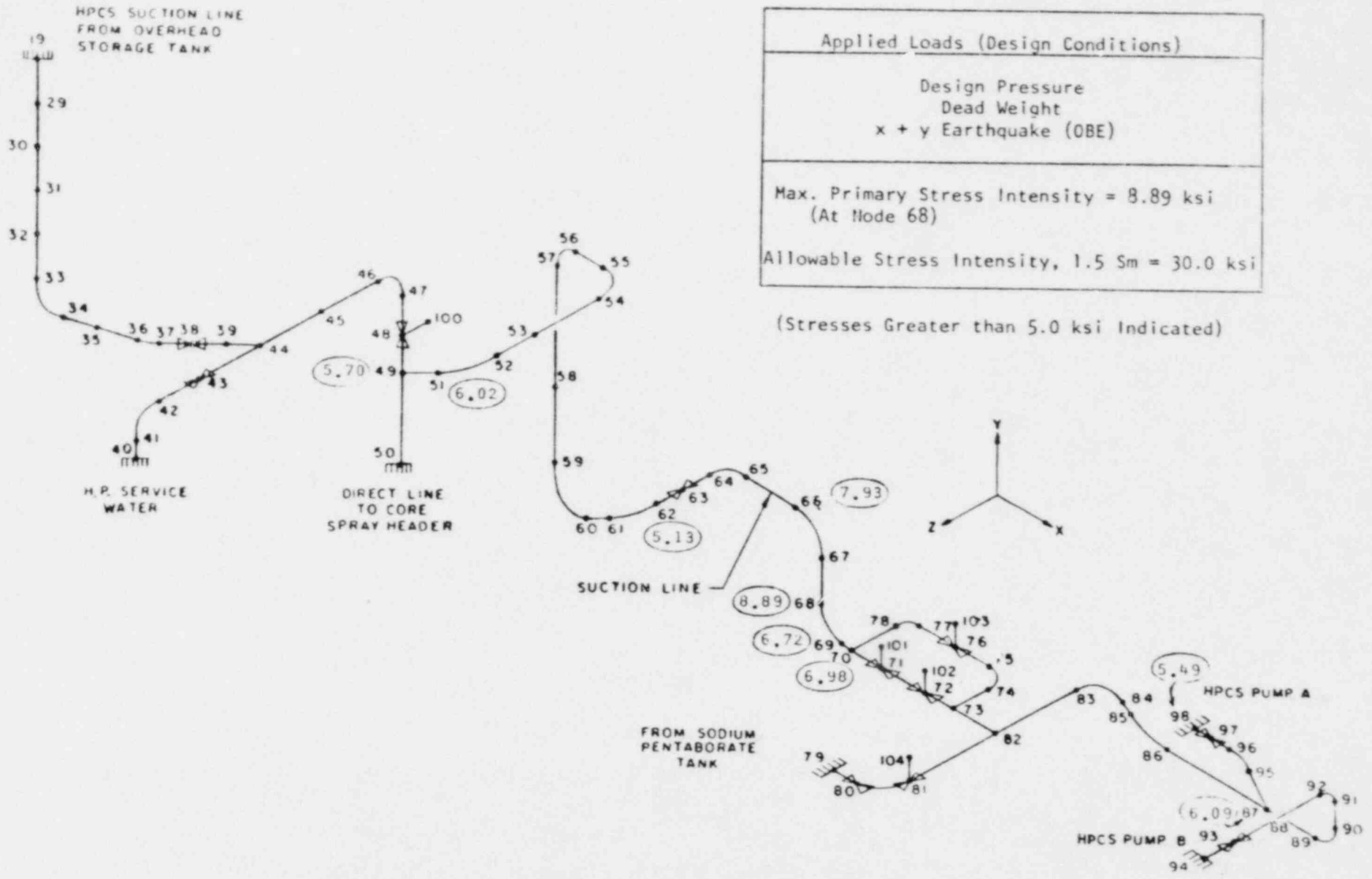


FIGURE 7-11

HPCS SUCTION LINE 2  
 Class I Stress Analysis  
 Compliance with ASME Code Equation 9

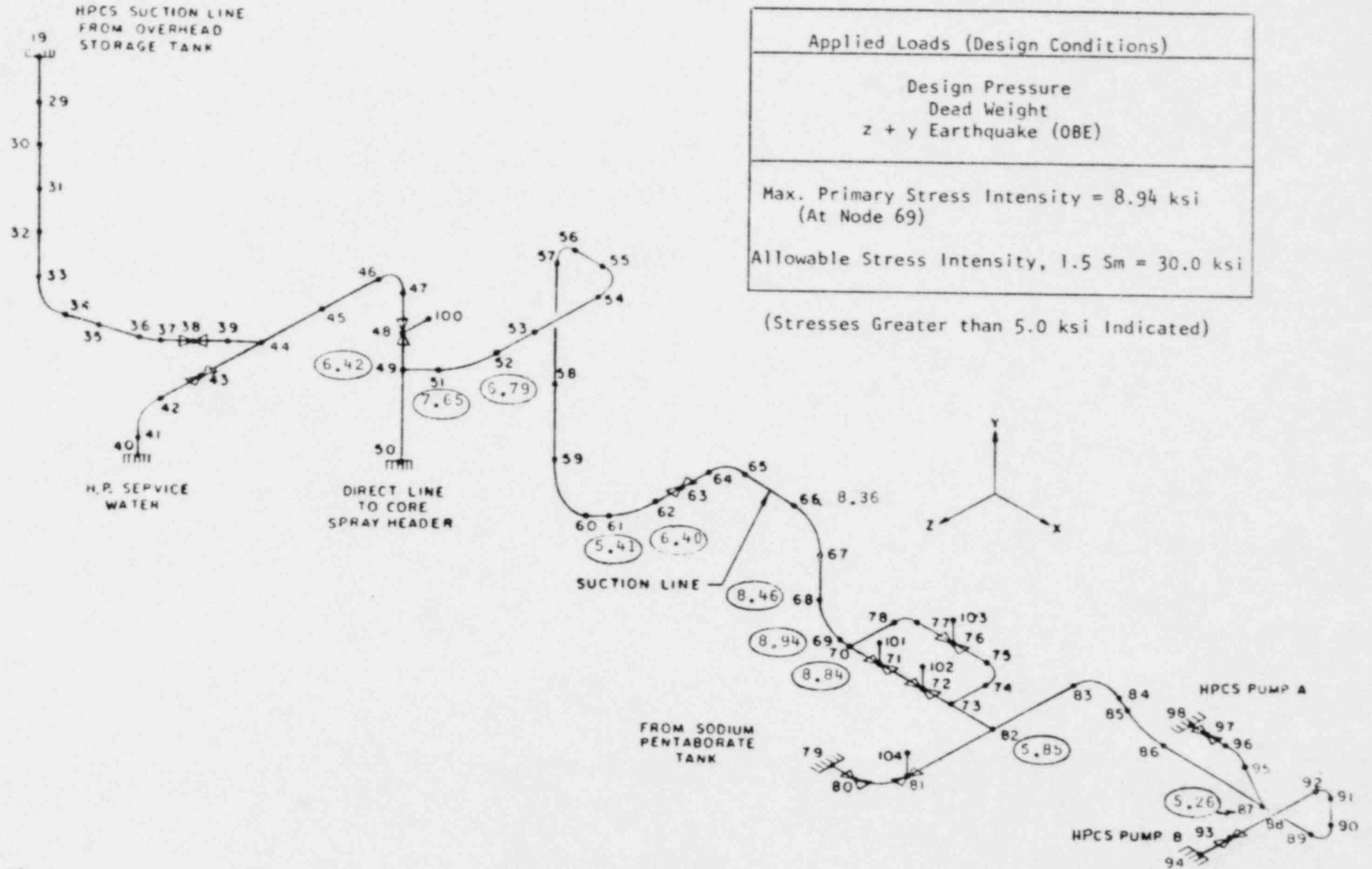




FIGURE 7-11

HPCS SUCTION LINE 2  
 Class 1 Stress Analysis  
 Compliance with ASME Code Equation 9

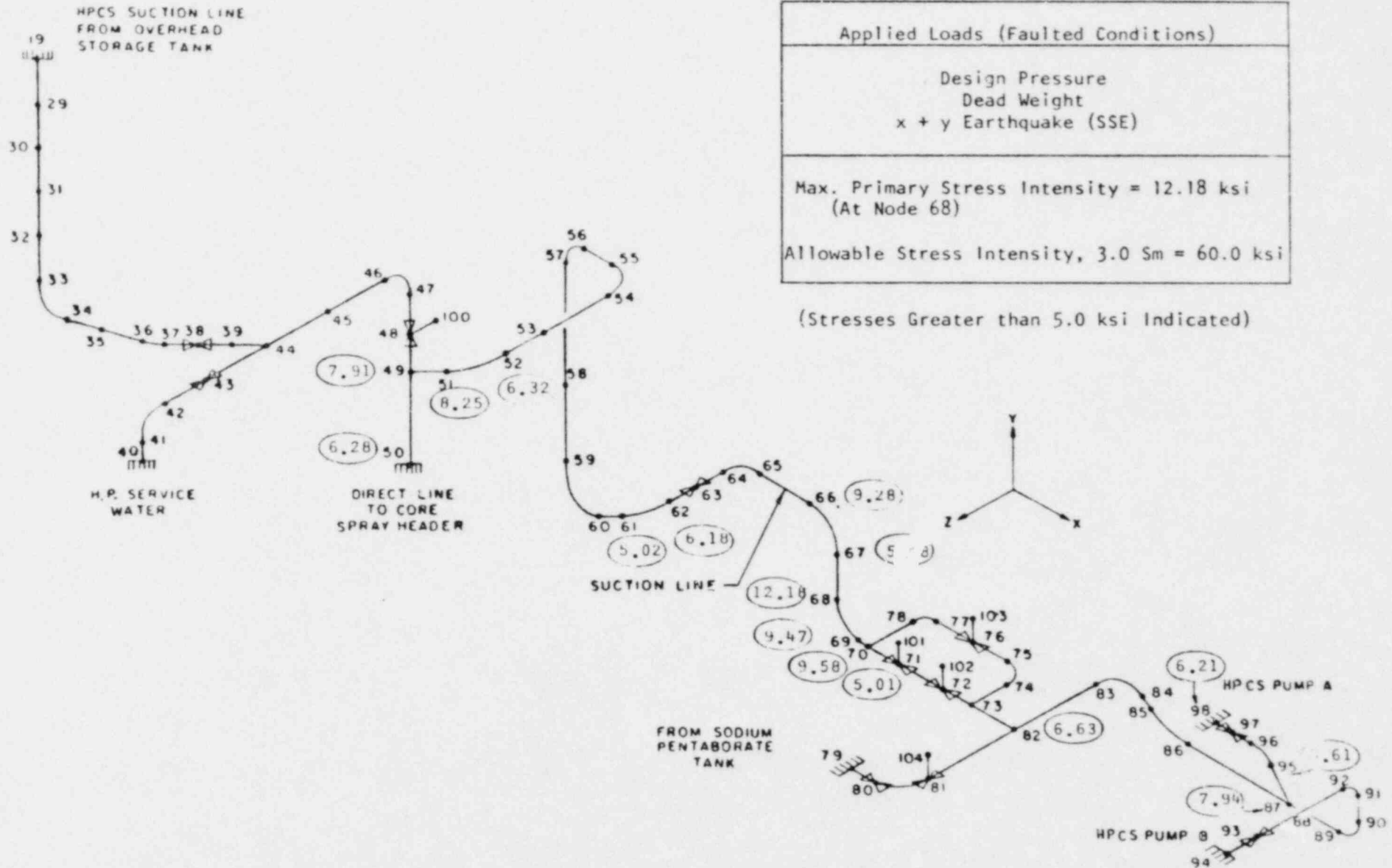


FIGURE 7.1

HPCS SUCTION LINE 2  
 Class 1 Stress Analysis  
 Compliance with ASME Code Equation 9

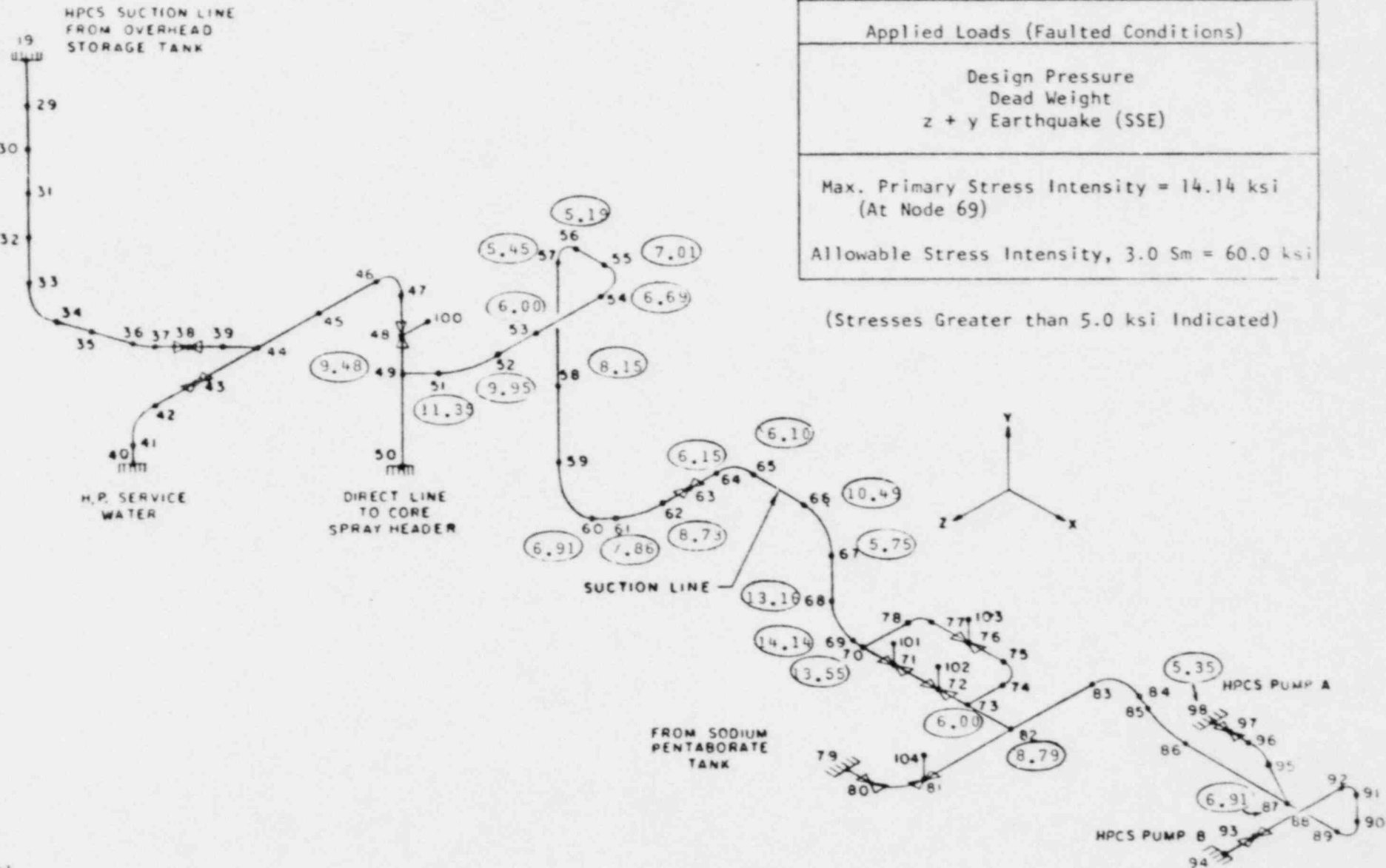


FIGURE 7.12

HPCS SUCTION LINE 2  
 Class 1 Stress Analysis  
 Compliance with ASME Code Equation 10

Applied Loads (Normal Operating Cond.)
Operating Pressure and Temperature Seismic Anchor Movements (x - direction) x + y Earthquake (OBE)
Max. Primary Plus Secondary Stress Intensity Range, $S_m = 13.00$ ksi (At Node 44)
Allowable Stress Intensity Range, $3.0 S_m = 6.00$ ksi

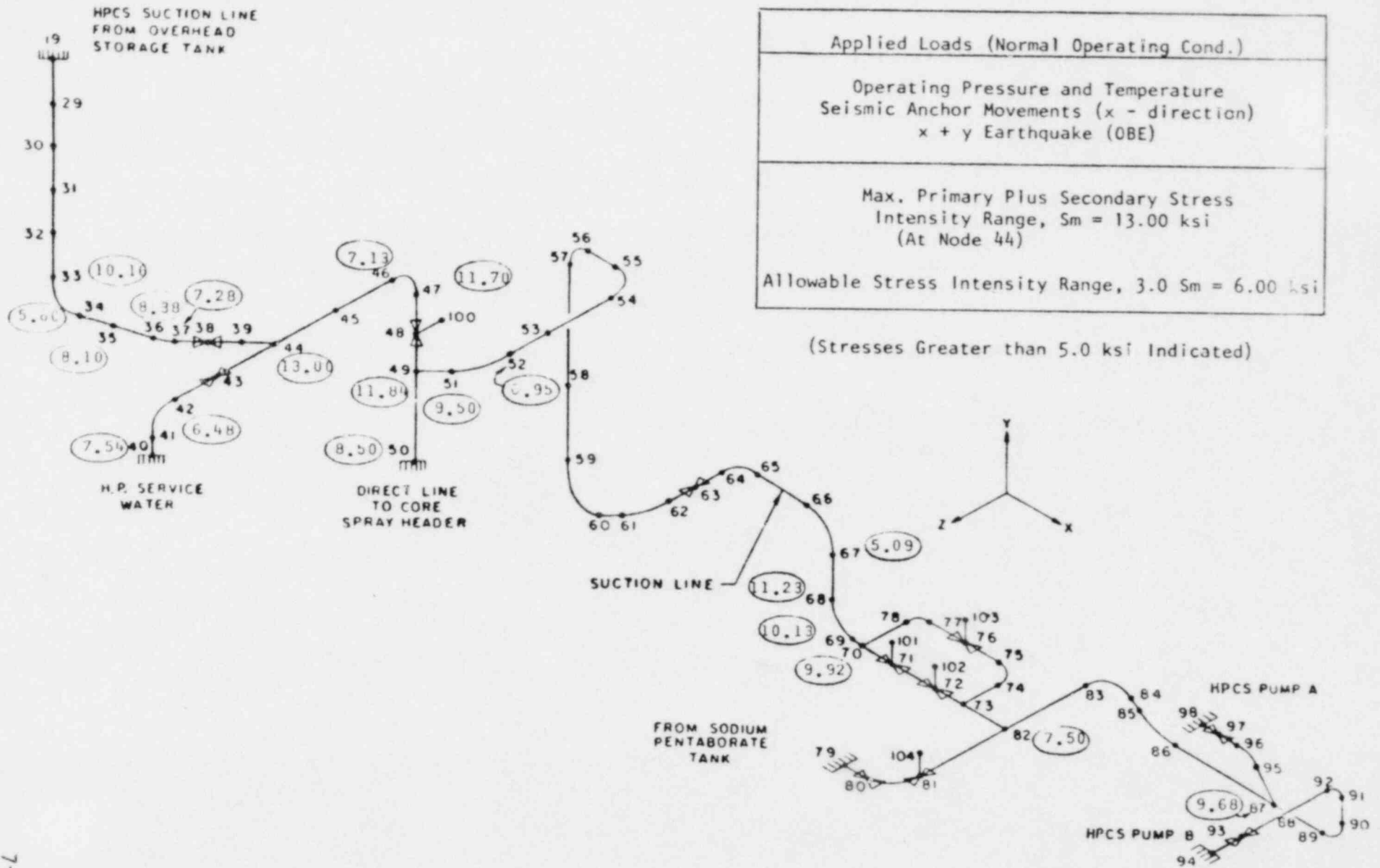


FIGURE 7.14

HPCS SUCTION LINE 2  
 Class 1 Stress Analysis  
 Compliance with ASME Code Equation 10

Applied Loads (Normal Operating Cond.)
Operating Pressure and Temperature Seismic Anchor Movements (z - direction) z + y Earthquake (OBE)
Max. Primary Plus Secondary Stress Intensity Range, $S_n = 24.16$ ksi (At Node 47)
Allowable Stress Intensity Range, $3.0 S_m = 60.0$ ksi

(Stresses Greater than 5.0 ksi Indicated)

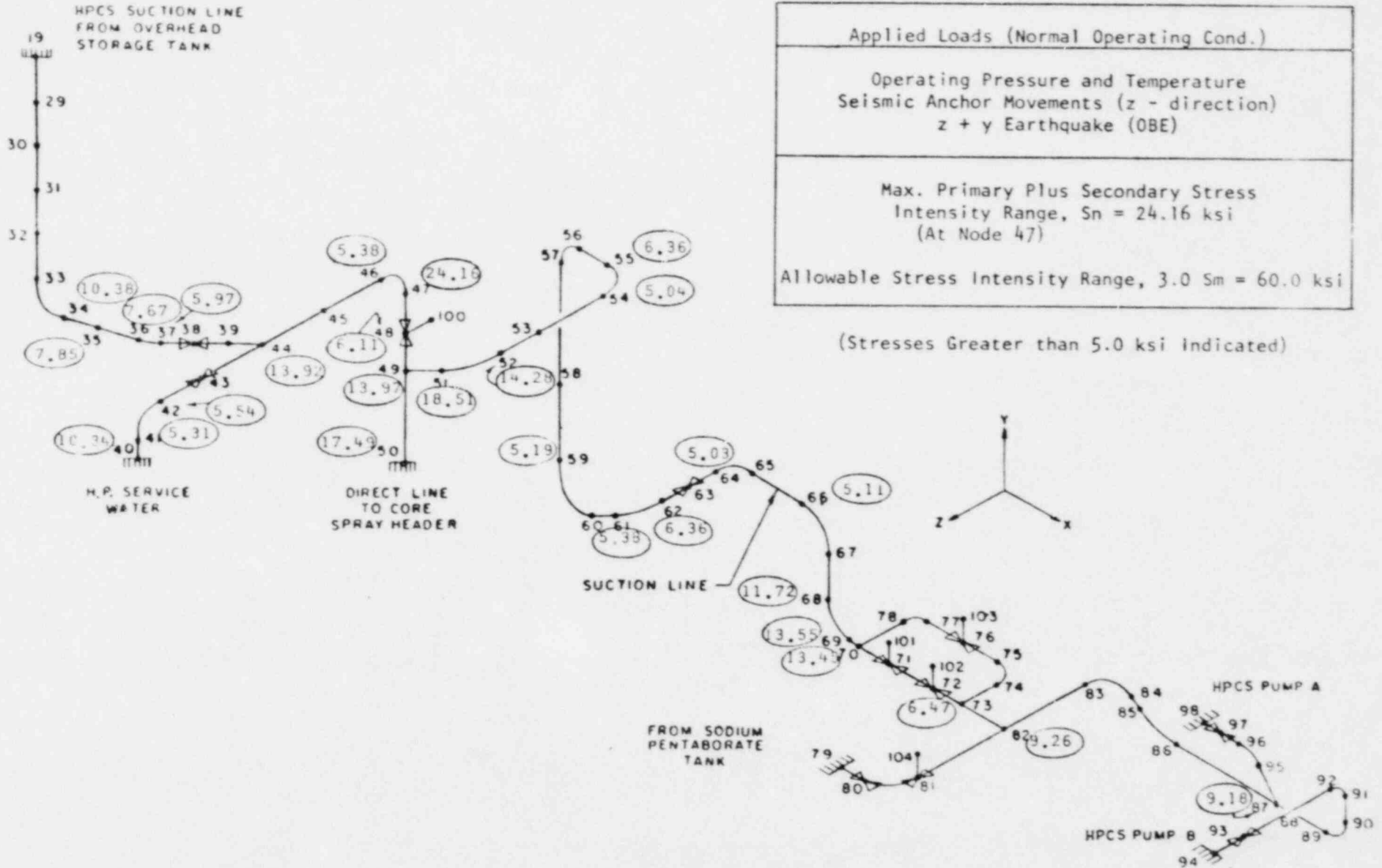


FIGURE 7-15

HPCS SUCTION LINE 2  
 Class 1 Stress Analysis  
 Consideration of ASME Code Equations 11 & 14

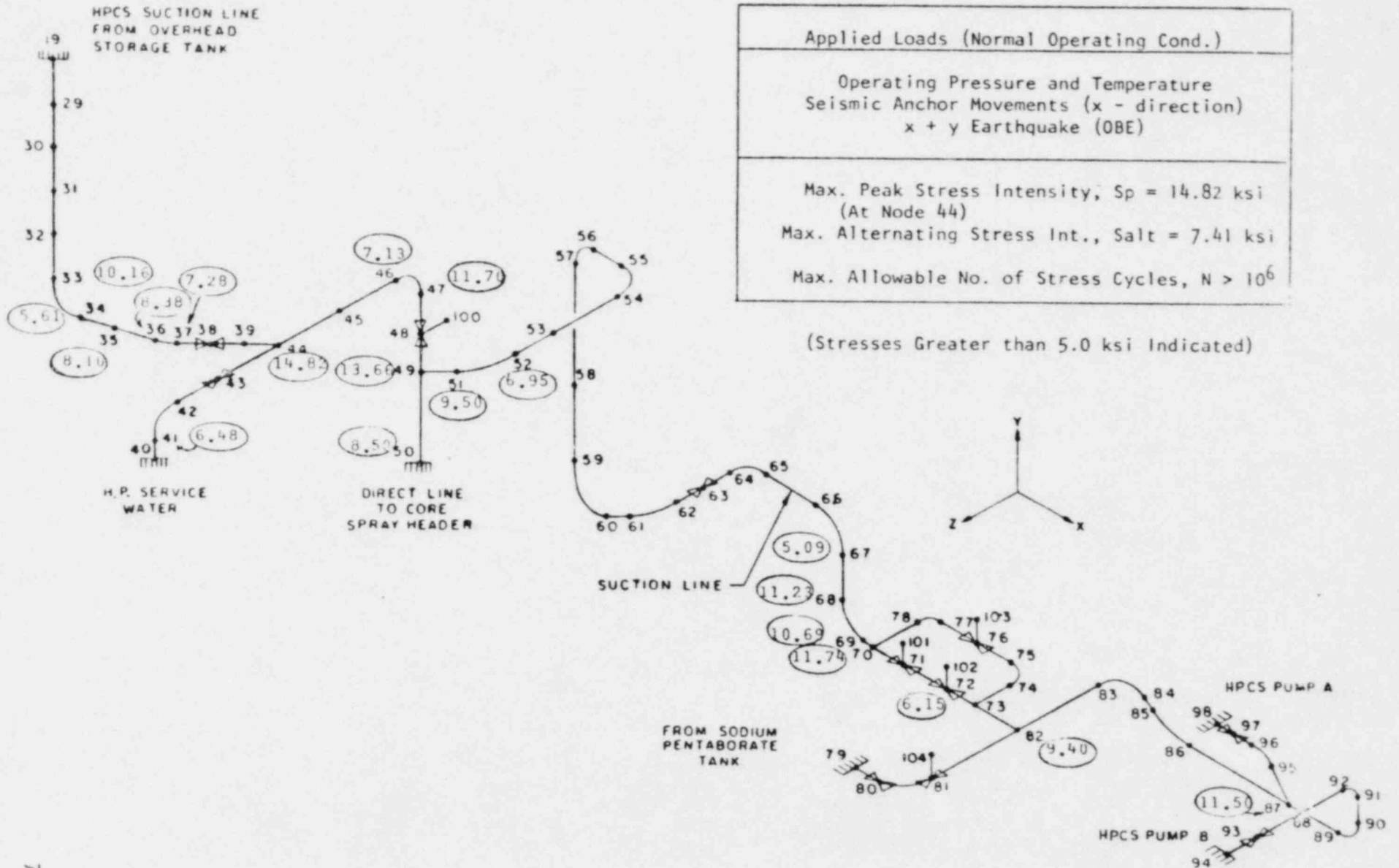
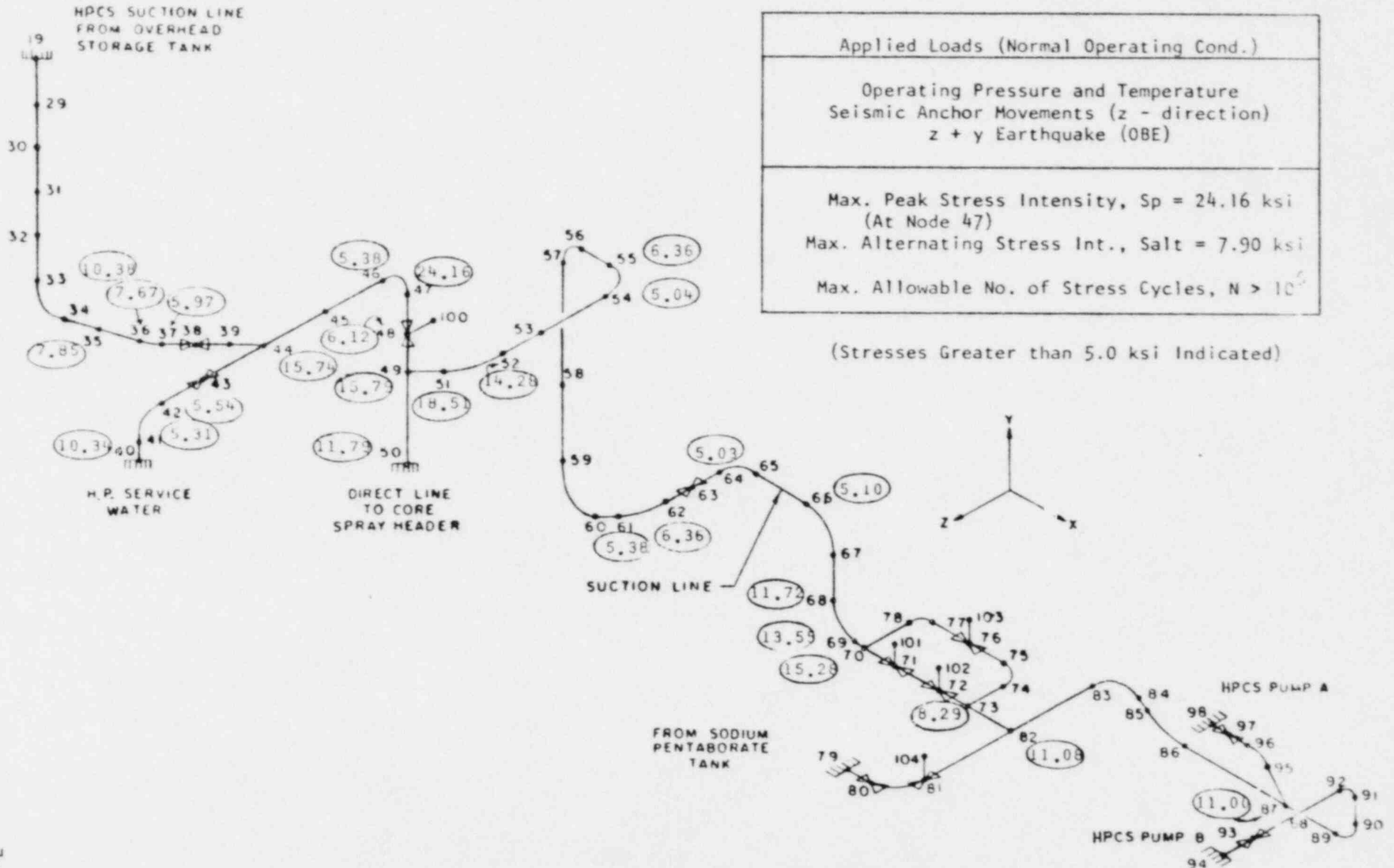


FIGURE 7.10

HPCS SUCTION LINE 2  
 Class 1 Stress Analysis  
 Consideration of ASME Code Equations 11 & 14



## 8. CONCLUSION

By providing rigid seismic restraints at the locations shown in Figure 3.1 the deflections and stresses in the HPCS suction piping due to a seismic event can be reduced to acceptable values.

The results of the subject analysis, which includes effects of five additional rigid restraints indicate that the deflections of the HPCS suction piping system, due to deadweight, thermal expansion and seismic loading are nominal. In addition, the stresses resulting from these loadings as calculated and combined in accordance with the rules given in Subarticle NB-3650 of Section III of the ASME Code (Reference 2), satisfy the design requirements for Class 1 piping systems.

The rigid restraints and their attachments should be designed using the support reaction forces given in Appendix B of this report.

## 9. REFERENCES

1. Gulf United Services Report No. SS-1162 "Seismic Evaluation of the LaCrosse Boiling Water Reactor", dated January 11, 1974.
2. ASME Boiler and Pressure Vessel Code, Section III, Division I, 1974 Edition, Nuclear Power Plant Components
3. Sargent and Lundy Engineers "Specification for Piping System-LaCrosse Boiling Water Reactor" LACBWR #256.
4. Sargent and Lundy Engineers "LACBWR" Project Drawing Nos. 41-503374, 503375, 503376.



APPENDIX A

LACBWR HPCS SUCTION LINE PIPING ANALYSIS

ANALYTICAL INPUT DATA

<u>TABLE</u>		<u>PAGE</u>
A-I	Pipe Properties	A-1
A-II	Valve Weights	A-2
A-III-1	Static Load Cases - Line 1	A-3
A-III-2	Static Load Cases - Line 2	A-5
A-IV	Dynamic Load Cases	A-7
A-V	Seismic Response Spectra	A-8

TABLE A-1 PIPE DATA

HPCS SUCTION LINE

LINE NO.	RUN NO.	FROM POINT	TO POINT	O.D. (IN)	WALL THICK (IN)	MAT'L	FLUID	WT. OF PIPE FLUID (LB/IN)	WT. IN INSUL (LB/IN)	DESIGN TEMP. (°F)	DESIGN PRESS. (PSIG)
1	1	1	2	6.625	0.280	↑	↑	2.62	0.15	↑	↑
		2	28	4.500	0.237			1.36	0.11		
2	1	19	44	3.50	0.216	↑	↓	0.90	0.09	↓	↓
	2	40	33	3.50	0.216			0.90	0.09		
	3	49	82	3.50	0.216			0.90	0.09		
	4	79	88	3.50	0.216			0.90	0.09		
	4	88	94	1.90	0.145			0.30	0.06		
	5	75	98	1.90	0.145			0.30	0.06		
6	73	70	3.50	0.216	0.90	0.09					

TABLE A-11

VALVE WEIGHTS

<u>VALVE</u>	<u>NODE LOCATION</u>	<u>TOTAL WEIGHT (lbs)</u>	<u>ECCENTRIC WEIGHT (lbs)</u>	<u>ECCENTRICITY (in)</u>
4" Gate	27	53.0	0	-
3" Check	38	52.0	0	-
3" Check	43	40.0	0	-
3" Gate	48 - 100	50.0	10.0	10.0
1/2" Relief	63	11.0	0	-
3" Control	71 - 101	234.0	110.0	21.9
3" Control	72 - 102	214.0	90.0	21.9
3" Gate	76 - 103	53.0	13.0	10.0
3" Gate	81 - 104	53.0	13.0	10.0
3" Check	80	52.0	0	-
1 1/2" Globe	93	49.0	0	-
1 1/2" Globe	97	49.0	0	-

TABLE A III - 1

STATIC LOAD CASES  
SUCTION LINE 1

STATIC LOAD CASE : 1  
LOAD CASE TITLE : DEAD WEIGHT AND OTHER SUSTAINED MECHANICAL LOADS

NUMBER OF SINGLE JOINT LOADS-----	0
NUMBER OF SUPPORT DISPLACEMENTS-----	0
NUMBER OF DISCONTINUITY STRESSES-----	0
GRAVITATIONAL MULTIPLIERS : X-----	-0.0000
Y-----	-1.0000
Z-----	-0.0000

STATIC LOAD CASE : 2  
~~LOAD CASE TITLE : THERMAL - NORMAL OPERATING CONDITION~~

THERMAL AND PRESSURE LOADINGS FOR ALL PIPE RUNS

RUN ID	DESIGN PRESSURE PSI	TEMPERATURE CHANGE DEG.	LINEAR	NONLINEAR	LONG.
			TEMPERATURE GRADIENT DEG.	TEMPERATURE GRADIENT DEG.	PRESSURE STRESS
1	0.00	50.00	-0.000	-0.000	NO

STATIC LOAD CASE : 3  
~~LOAD CASE TITLE : OPERATING PRESSURE~~

THERMAL AND PRESSURE LOADINGS FOR ALL PIPE RUNS

RUN ID	DESIGN PRESSURE PSI	TEMPERATURE CHANGE DEG.	LINEAR	NONLINEAR	LONG.
			TEMPERATURE GRADIENT DEG.	TEMPERATURE GRADIENT DEG.	PRESSURE STRESS
1	20.00	0.00	0.000	0.000	NO

TABLE A III - 1 Con'd

STATIC LOAD CASES  
SUCTION LINE 1

~~STATIC LOAD CASE 4~~  
LOAD CASE TITLE : DESIGN PRESSURE

THERMAL AND PRESSURE LOADINGS FOR ALL PIPE RUNS

RUN ID	DESIGN PRESSURE PSI	TEMPERATURE CHANGE DEG.	LINEAR	NONLINEAR	LONG
			TEMPERATURE GRADIENT DEG.	TEMPERATURE GRADIENT DEG.	PRESSURE STRESS
1	100.00	0.00	0.000	0.000	NO

~~STATIC LOAD CASE 5~~  
~~LOAD CASE TITLE : SEISMIC ANCHOR MOVEMENTS X - DIRECTION~~

SUPPORT DISPLACEMENTS

JOINT ID	LOAD TYPE	DISPLACEMENT DIRECTION	DISPLACEMENT MAGNITUDE
1	TRANS.	X	.7200
14	TRANS.	X	.3700
16	TRANS.	X	.2400
19	TRANS.	X	.1300

~~STATIC LOAD CASE 6~~  
~~LOAD CASE TITLE : SEISMIC ANCHOR MOVEMENTS Z - DIRECTION~~

~~SUPPORT DISPLACEMENTS~~

JOINT ID	LOAD TYPE	DISPLACEMENT DIRECTION	DISPLACEMENT MAGNITUDE
1	TRANS.	Z	.7200
14	TRANS.	Z	.3700
16	TRANS.	Z	.2400
19	TRANS.	Z	.1300

TABLE A III - 2

STATIC LOAD CASES  
SUCTION LINE 2

STATIC LOAD CASE : 1  
LOAD CASE TITLE : DEAD WEIGHT AND OTHER SUSTAINED MECHANICAL LOADS

NUMBER OF SINGLE JOINT LOADS-----	0
NUMBER OF SUPPORT DISPLACEMENTS-----	0
NUMBER OF DISCONTINUITY STRESSES-----	0
GRAVITATIONAL MULTIPLIERS : X-----	-0.0000
Y-----	-1.0000
Z-----	-0.0000

~~STATIC LOAD CASE : 2~~  
~~LOAD CASE TITLE : THERMAL - NORMAL OPERATING CONDITION~~

~~THERMAL AND PRESSURE LOADINGS FOR ALL PIPE RUNS~~

<del>PIPE</del> ID	<del>DESIGN</del> PRESSURE PSI	<del>TEMPERATURE</del> CHANGE DEG.	<del>LINEAR</del> TEMPERATURE GRADIENT DEG.	<del>NONLINEAR</del> TEMPERATURE GRADIENT DEG.	<del>LONG.</del> PRESSURE STRESS
1	0.00	50.00	-0.000	-0.000	NO
2	0.00	50.00	-0.000	-0.000	NO
3	0.00	50.00	-0.000	-0.000	NO
4	0.00	50.00	-0.000	-0.000	NO
5	0.00	50.00	-0.000	-0.000	NO
6	0.00	50.00	-0.000	-0.000	NO
7	0.00	0.00	0.000	0.000	NO

STATIC LOAD CASE : 3  
LOAD CASE TITLE : OPERATING PRESSURE

THERMAL AND PRESSURE LOADINGS FOR ALL PIPE RUNS

PIPE	DESIGN	TEMPERATURE	LINEAR	NONLINEAR	LONG.
ID	PRESSURE	CHANGE	TEMPERATURE	TEMPERATURE	PRESSURE
	PSI	DEG.	GRADIENT	GRADIENT	STRESS
			DEG.	DEG.	
1	50.00	0.00	0.000	0.000	NO
2	50.00	0.00	0.000	0.000	NO
3	50.00	0.00	0.000	0.000	NO
4	50.00	0.00	0.000	0.000	NO
5	50.00	0.00	0.000	0.000	NO
6	50.00	0.00	0.000	0.000	NO
7	0.00	0.00	0.000	0.000	NO

TABLE A 111 - 2 Con'd

STATIC LOAD CASES  
SUCTION LINE 2

STATIC LOAD CASE : 4  
LOAD CASE TITLE : DESIGN PRESSURE

THEMAL AND PRESSURE LOADINGS FOR ALL PIPE RUNS

PIPE ID	DESIGN PRESSURE PSI	TEMPERATURE CHANGE DEG.	LINEAR TEMPERATURE GRADIENT DEG.	NONLINEAR TEMPERATURE GRADIENT DEG.	LONG. PRESSURE STRESS
1	100.00	0.00	0.000	0.000	NO
2	100.00	0.00	0.000	0.000	NO
3	100.00	0.00	0.000	0.000	NO
4	100.00	0.00	0.000	0.000	NO
5	100.00	0.00	0.000	0.000	NO
6	100.00	0.00	0.000	0.000	NO
7	0.00	0.00	0.000	0.000	NO

STATIC LOAD CASE : 5  
LOAD CASE TITLE : SEISMIC ANCHOR MOVEMENTS X - DIRECTION

SUPPORT DISPLACEMENTS

JOINT ID	LOAD TYPE	DISPLACEMENT DIRECTION	DISPLACEMENT MAGNITUDE
50	TRANS.	X	.4320

STATIC LOAD CASE : 6  
LOAD CASE TITLE : SEISMIC ANCHOR MOVEMENTS Z - DIRECTION

SUPPORT DISPLACEMENTS

JOINT ID	LOAD TYPE	DISPLACEMENT DIRECTION	DISPLACEMENT MAGNITUDE
50	TRANS.	Z	.4320

TABLE A-IV

## DYNAMIC LOAD CASES

Suction Lines 1 and 2

<u>LOAD CASE NO.</u>	<u>LOAD DESCRIPTION</u>	<u>SPECTRUM NO. IN GLOBAL</u>			<u>SPECTRUM MULTIPLIERS</u>		
		<u>X</u>	<u>Y</u>	<u>Z</u>	<u>X</u>	<u>Y</u>	<u>Z</u>
7	x + y Earthquake (OBE)	1	3	0	386.0	128.7	0
8	z + y Earthquake (OBE)	0	3	1	0	128.7	386.0
9	x + y Earthquake (SSE)	2	3	0	386.0	257.3	0
10	z + y Earthquake (SSE)	0	3	2	0	357.3	386.0



TABLE A-V  
SPECTRUM RESPONSE SPECTRUM

SUCTION LINE 1

SPECTRUM NO. 1 (Horizontal OBE)		SPECTRUM NO. 2 (Horizontal SSE)		SPECTRUM NO. 3 (Vertical Ground SSE)	
Frequency CPS	Acceleration G's	Frequency CPS	Acceleration G's	Frequency CPS	Acceleration G's
40.000	.78000	40.000	.79000	40.000	.12000
<del>15.000</del>	<del>.38000</del>	15.000	.70000	33.000	.12000
12.000	.43000	12.000	.75000	<del>20.000</del>	<del>.23000</del>
10.000	.78000	<del>10.000</del>	<del>1.15000</del>	15.000	.32000
<del>7.000</del>	<del>1.07000</del>	9.000	1.60000	10.000	.52000
6.000	1.33000	6.000	1.90000	<del>9.000</del>	<del>.60000</del>
5.000	1.46000	<del>5.000</del>	<del>2.20000</del>	5.000	.65000
<del>4.000</del>	<del>1.48000</del>	4.000	2.15000	3.000	.70000
3.500	1.26000	3.500	1.80000	<del>2.500</del>	<del>.72000</del>
3.000	1.20000	<del>3.000</del>	<del>1.90000</del>	2.200	.63000
<del>2.500</del>	<del>1.72000</del>	2.500	2.65000	2.000	.59000
2.000	3.18000	2.000	5.75000	<del>1.500</del>	<del>.44000</del>
1.750	4.50000	<del>1.750</del>	<del>6.10000</del>	1.000	.31000
<del>1.500</del>	<del>3.54000</del>	1.500	5.00000	.800	.24300
1.250	1.24000	1.250	2.05000	<del>.600</del>	<del>.19000</del>
1.000	.60000	<del>1.000</del>	<del>1.00000</del>	.400	.13000
<del>.750</del>	<del>.32000</del>	.750	.50000	.200	.05400
.500	.16000	.500	.25000	<del>.100</del>	<del>.01400</del>

SUCTION LINE 2

SPECTRUM NO. 1 (Horizontal OBE)		SPECTRUM NO. 2 (Horizontal SSE)		SPECTRUM NO. 3 (Vertical Ground SSE)	
Frequency CPS	Acceleration G's	Frequency CPS	Acceleration G's	Frequency CPS	Acceleration G's
40.000	.25000	40.000	.43000	40.000	.12000
<del>10.000</del>	<del>.25000</del>	<del>15.000</del>	<del>.43000</del>	<del>33.000</del>	<del>.12000</del>
9.000	.25000	10.000	.43000	20.000	.23000
8.000	.32000	9.000	.50000	15.000	.32000
<del>7.000</del>	<del>.32000</del>	<del>8.000</del>	<del>.58000</del>	<del>10.000</del>	<del>.52000</del>
6.000	.48000	7.000	.60000	9.000	.60000
5.000	.55000	6.000	.63000	5.000	.65000
<del>4.000</del>	<del>.60000</del>	<del>4.000</del>	<del>.95000</del>	<del>3.000</del>	<del>.70000</del>
3.000	.62000	4.000	1.10000	2.500	.72000
2.500	1.00000	3.000	1.10000	2.200	.63000
<del>2.000</del>	<del>1.25000</del>	<del>2.500</del>	<del>1.60000</del>	<del>2.000</del>	<del>.59000</del>
1.800	3.00000	2.000	2.60000	1.500	.44000
1.600	3.00000	1.800	3.95000	1.000	.31000
<del>1.400</del>	<del>1.80000</del>	<del>1.700</del>	<del>3.90000</del>	<del>.800</del>	<del>.24300</del>
1.200	.78000	1.500	3.40000	.600	.19000
1.000	.48000	1.300	1.60000	.400	.13000
<del>.900</del>	<del>.31000</del>	<del>1.100</del>	<del>.90000</del>	<del>.200</del>	<del>.05400</del>
.900	.20000	1.000	.63000	.100	.01400
.600	.16000	.900	.45000		
<del>.500</del>	<del>.16000</del>	<del>.800</del>	<del>.38000</del>		
		.700	.25000		
		.500	.21000		

APPENDIX B

LABWR HPCS SUCTION LINE  
PIPING ANALYSIS TABULATED RESULTS

<u>TABLE</u>		<u>PAGE</u>
B I	Joint Displacements	B-1
B II	Elastic Support Reactions	B-14
B III	Class I Component Stress Analysis PIPESD Results	B-23

TABLE B-1

JOINT DISPLACEMENTS

BI-1 HPCS Suction Line 1	Pages B-2 to B-5
BI-2 HPCS Suction Line 2	Pages B-6 to B-13

Note: Designation "ECCS" in the following tables  
is synonymous with designation "HPCS"

TABLE 1

FCCS SUCTION LINE 1  
JOINT DISPLACEMENTS

(LOAD CASE 1) (LOAD CASE 2)

JOINT	DISPLACEMENTS ( IN. )			THERMAL - NORMAL OPERATING CONDITION
	X	Y	Z	
1	.000000	.000000	.000000	.000000
2	.001063	.000229	.001314	.003274
3	.001149	.000483	.001366	.010738
4	.001308	.000317	.001414	.021202
5	.001605	.002124	.001429	.036473
6	.001973	.003914	.001786	.051939
7	.002463	.012437	.001287	.070389
8	.002984	.008251	.001163	.089783
9	.001499	.003872	.002125	.099819
10	.004791	.001910	.001646	.091494
11	.006699	.000693	.004939	.064358
12	.006466	.000704	.004107	.057064
13	.003986	.000637	.005010	.028517
14	.001105	.000527	.001617	.000547
15	.005006	.000419	.006551	.003925
16	.001020	.000296	.000988	.000452
17	.001101	.000187	.000202	.000479
18	.001063	.000038	.000017	.000024
19	.000000	.000000	.000000	.000000
20	.000075	.008212	.000131	.003086
21	.000689	.009695	.000124	.002368
22	.000035	.005589	.000062	.001048
23	.000600	.000000	.000000	.000000
24	.000078	.001070	.000044	.000000
25	.000117	.000761	.000066	.000000
26	.000359	.000049	.000198	.013249
27	.000280	.000037	.000126	.011725
28	.000000	.000000	.000000	.005546
29	.000000	.000000	.000000	.000000

FCCS SUCTION LINE-1

JOINT DISPLACEMENTS

(LOAD CASE 5)

(LOAD CASE 6)

SEISMIC ANCHOR MOVEMENTS X -- DIRECTION

SEISMIC ANCHOR MOVEMENTS Z -- DIRECTION

JOINT	DISPLACEMENTS ( IN. )		
	X	Y	Z
1	.7200000	-.0000000	.0000000
2	.7194844	-.0000042	-.0003735
3	.7179248	-.0002550	-.0016110
4	.7142854	.0001437	-.0045175
5	.7069250	.0029606	-.0104108
6	.6983644	-.0021592	-.0172689
7	.6887734	-.0267284	-.0249513
8	.6817202	-.0428113	-.0305893
9	.6629976	-.0364406	-.0369816
10	.6102336	-.0246474	-.0377901
11	.5333227	-.0022850	-.0261476
12	.5167146	.0001226	-.0230157
13	.4543271	.0001052	-.0116318
14	.3704982	.0000814	-.0001539
15	.3058842	.0000615	.0009796
16	.2372061	.0000416	-.0009999
17	.1766165	.0000256	-.0010943
18	.1306207	.0000057	-.0001321
19	.1300000	.0000000	-.0000000
20	.0711363	-.0079224	-.0989624
21	.0640642	-.0072521	-.1129815
22	.0347594	-.0034618	-.0613029
23	.0000000	-.0000000	.0000000
24	-.0000003	.0000000	.0000005
25	-.0000002	.0000000	.0000004
26	-.0000001	.0000000	.0000002
27	-.0000000	.0000000	.0000001
28	-.0000000	.0000000	.0000000

JOINT	DISPLACEMENTS ( IN. )		
	X	Y	Z
1	.0000000	.0000000	.7200000
2	-.0003351	.0000056	.7194792
3	-.0014005	.0003150	.7187085
4	-.0039040	-.0001777	.7167685
5	-.0090983	-.0036589	.7125154
6	-.0154331	.0026701	.7073451
7	-.0231884	.0330611	.7010621
8	-.0301590	.0524721	.6953912
9	-.0371865	.0451051	.6789926
10	-.0380694	.0305168	.6267107
11	-.0272072	.0028342	.5443457
12	-.0240522	-.0001501	.5263581
13	-.0121041	-.0001286	.4594201
14	-.0001396	-.0000990	.3705724
15	.0011129	-.0000744	.3050114
16	.0008870	-.0000498	.2376230
17	.0009509	-.0000301	.1765084
18	.0001213	-.0000055	.1316608
19	.0000000	-.0000000	.1300000
20	.0279152	.0084253	.0849073
21	.0287457	.0077991	.0521312
22	.0108930	.0030013	.0198731
23	.0000000	.0000000	.0000000
24	.0000001	-.0000000	-.0000001
25	.0000001	-.0000000	-.0000001
26	.0000000	-.0000000	-.0000000
27	.0000000	-.0000000	-.0000000
28	.0000000	-.0000000	-.0000000

TABLE BI-1, Cont'd

FCCS SUCTION LINE 1

JOINT DISPLACEMENTS

(LOAD CASE 7)

X + Y EARTHQUAKE 1/2 SSE (ORF)

(LOAD CASE 8)

X + Y EARTHQUAKE 1/2 SSE (ORF)

TOTAL RESPONSE EQUALS MORE THROUGH BY SQSS - SUMMATION

JOINT NO	DISPLACEMENTS ( IN. )			JOINT NO	DISPLACEMENTS ( IN. )		
	X	Y	Z		X	Y	Z
1	.000000	.000000	.000000	1	.000000	.000000	.000000
2	.0045782	.000068	.0036874	2	.0036882	.0000100	.0029707
3	.0393999	.0000210	.0117310	3	.0317485	.0000304	.0255610
4	.1305932	.0000195	.1052197	4	.1052384	.0000283	.0877013
5	.3145716	.0003440	.2536845	5	.2535083	.0004990	.2042793
6	.5128872	.0003687	.4132468	6	.4133344	.0005364	.3303346
7	.7073251	.0029846	.5694975	7	.5700318	.0043412	.4592791
8	.8303786	.0024499	.6603380	8	.6692000	.0041434	.5391760
9	.7670556	.0014645	.6180546	9	.6181700	.0021259	.4980404
10	.5604957	.0004669	.4521002	10	.4520301	.0006686	.3643675
11	.3110202	.0000162	.2509632	11	.2506589	.0000221	.2023144
12	.2661100	.0000191	.2148043	12	.2144659	.0000278	.1731783
13	.1259181	.0000164	.1018926	13	.1014833	.0000238	.0821638
14	.0046516	.0000126	.0040230	14	.0037471	.0000183	.0032431
15	.0165073	.0000095	.0133248	15	.0133051	.0000138	.0107491
16	.0038089	.0000063	.0032838	16	.0030692	.0000092	.0026467
17	.0009041	.0000038	.0005966	17	.0007309	.0000055	.0004864
18	.0001200	.0000007	.0000954	18	.0007309	.0000055	.0004864
19	.0000000	.0000000	.0000000	19	.0000969	.0000009	.0000772
20	.0000513	.0004301	.0000243	20	.0000000	.0000000	.0000000
21	.0000424	.0005244	.0000723	21	.0000416	.0004471	.0000207
22	.0000246	.0003019	.0000491	21	.0000345	.0005506	.0000588
23	.0000000	.0000000	.0000000	22	.0000231	.0003139	.0000398
24	.0000000	.0000000	.0000000	23	.0000000	.0000000	.0000000
25	.0000000	.0000000	.0000000	24	.0000000	.0000000	.0000000
26	.0000000	.0000000	.0000000	25	.0000000	.0000000	.0000000
27	.0000000	.0000000	.0000000	26	.0000000	.0000000	.0000000
28	.0000000	.0000000	.0000000	27	.0000000	.0000000	.0000000
29	.0000000	.0000000	.0000000	28	.0000000	.0000000	.0000000



## ECCS SECTION LINE 1-

## JOINT DISPLACEMENTS-

(LOAD CASE 9)-

X + Y EARTHQUAKE SSE

(LOAD CASE 10)-

Z + Y EARTHQUAKE SSE

TOTAL RESPONSE EQUALS MODE 1 THROUGH 6 BY SOSS SUMMATION

JOINT ID	DISPLACEMENTS ( IN. )			JOINT ID	DISPLACEMENTS ( IN. )		
	X	Y	Z		X	Y	Z
1	.0000000	.0000000	.0000000	1	.0000000	.0000000	.0000000
2	.0065754	.0000128	.0052960	2	.0052959	.0000186	.0042658
3	.0565631	.0000392	.0455534	3	.0455753	.0000565	.0367046
4	.1874612	.0000364	.1510386	4	.1510604	.0000527	.1217105
5	.4515177	.0006434	.3638369	5	.3638685	.0009309	.2932048
6	.7361427	.0006902	.5931297	6	.5932569	.0009992	.4786029
7	1.0152112	.0055857	.8172837	7	.8181580	.0080860	.6591063
8	1.1918286	.0053319	.9602591	8	.9604931	.0077169	.7738715
9	1.1009412	.0027372	.8870830	9	.8872515	.0039582	.7149034
10	.8050555	.0008655	.6489062	10	.6488072	.0012416	.5230039
11	.4464501	.0000293	.3602579	11	.3598150	.0000407	.2904853
12	.3819956	.0000358	.3083641	12	.3078711	.0000518	.2486746
13	.1807725	.0000306	.1462805	13	.1456999	.0000443	.1180244
14	.0066911	.0000236	.0057786	14	.0053805	.0000341	.0046593
15	.0236998	.0000177	.0191331	15	.0191044	.0000256	.0154451
16	.0054681	.0000118	.0047143	16	.0044058	.0000171	.0038000
17	.0012994	.0000071	.0008595	17	.0010528	.0000103	.0007060
18	.0001725	.0000012	.0001371	18	.0001394	.0000017	.0001112
19	.0000000	.0000000	.0000000	19	.0000000	.0000000	.0000000
20	.0000739	.0008174	.0000375	20	.0000603	.0008588	.0000328
21	.0000511	.0010103	.0001044	21	.0000500	.0010669	.0000855
22	.0000412	.0005764	.0000708	22	.0000335	.0006051	.0000577
23	.0000000	.0000000	.0000000	23	.0000000	.0000000	.0000000
24	.0000000	.0000000	.0000000	24	.0000000	.0000000	.0000000
25	.0000000	.0000000	.0000000	25	.0000000	.0000000	.0000000
26	.0000000	.0000000	.0000000	26	.0000000	.0000000	.0000000
27	.0000000	.0000000	.0000000	27	.0000000	.0000000	.0000000
28	.0000000	.0000000	.0000000	28	.0000000	.0000000	.0000000

TABLE BI-2

EGGS SECTION LINE 2

JOINT DISPLACEMENTS

DEAD WEIGHT AND OTHER SUSTAINED MECHANICAL LOADS

(LOAD CASE 1)

JOINT (GID)	DISPLACEMENTS ( IN )				X	Y	Z
	X	Y	Z				
10	-.0000000	-.0000000	.0000000	70	.0001238	.0044922	-.0013438
20	-.0000009	-.0002295	.0001097	71	.0001225	.0004512	-.0011255
30	.0000001	-.0003856	-.0000031	72	.0001206	-.0007876	-.0005932
31	.0000043	-.0005153	-.0006028	73	.0001186	-.0065907	-.0001400
32	-.0000037	-.0005686	-.0000025	74	.0002968	-.0104673	-.0001401
33	.0000346	-.0005773	.0023118	75	.0005073	-.0105589	-.0003700
34	.0001439	-.0005439	.0028465	76	.0005073	-.0074145	-.0005975
35	.0001439	-.0002670	.0022580	77	.0005071	-.0001780	-.0011020
36	.0001636	-.0046421	-.0001589	78	.0002900	.0035066	-.0013434
37	.0000128	-.0057597	-.0005513	79	.0000000	-.0000000	-.0000000
38	-.0002906	-.0082040	-.0000399	80	.0000008	-.0011463	-.0000376
39	-.0003312	-.0084719	-.0009298	81	.0000336	-.0056795	-.0000404
40	.0000000	.0000000	-.0000000	82	.0001178	-.0092363	-.0000413
41	-.0003148	.0000117	-.0005748	83	-.0002824	-.0263671	-.0000418
42	-.0008531	-.0003707	-.0003952	84	-.0013280	-.0300094	.0024167
43	-.0005150	-.0024449	-.0008983	85	-.0011747	-.0298561	.0041423
44	-.0003318	-.0078192	-.0009915	86	-.0007147	-.0285128	.0062360
45	-.0007405	-.0230964	-.0009168	87	-.0007184	-.0134610	.0043400
46	-.0084739	-.0017524	-.0007329	88	-.0007180	-.0105111	.0045323
47	-.0009571	-.0000363	-.0021553	89	-.0007148	-.0052382	.0042403
48	-.0072075	-.0000581	-.0030706	90	-.0010003	-.0049081	.0030768
49	-.0055988	-.0000732	-.0024816	91	-.0014001	-.0049066	.0010005
50	-.0000000	-.0000000	-.0000000	92	-.0013642	-.0039252	-.0000010
51	-.0105442	-.0005158	-.0074346	93	-.0002800	-.0000926	-.0000004
52	-.0285971	.0003676	-.0128962	94	-.0000000	.0000000	-.0000000
53	-.1149280	.0002231	-.0129065	95	-.0013296	-.0134323	.0010663
54	-.1757054	.0127305	-.0129137	96	.0000052	-.0115185	-.0000068
55	-.2075071	-.0011732	.0174634	97	.0000024	-.0036250	.0000407
56	-.2075118	-.0379957	.0524736	98	.0000000	-.0000000	.0000000
57	-.1737276	.0713007	.0670771	100	.0119160	-.0001066	-.0030706
58	.0033868	-.0712965	.0117966	101	.0058952	.0004344	-.0061782
59	.2299704	-.0712260	.0034501	102	.0035673	-.0008015	-.0077666
60	.2913468	-.0053205	.0002952	103	.0045850	-.0074155	-.0020307
61	.2850015	.0075696	-.0060488	104	.0031750	-.0056806	-.0036607
62	.2594429	-.0048833	.0188023				
63	.0303990	-.2480000	-.0187825				
64	.0003904	-.2777073	-.0197799				
65	-.0167765	-.2285204	-.0341788				
66	-.0167848	-.0094534	-.0692167				
67	-.0029099	.0092211	-.0584009				
68	.0030856	.0088261	-.0035760				
69	.0001241	.0056236	-.0013777				



TABLE BI-2, Cont'd

FOOS SECTION LINE 2

JOINT DISPLACEMENTS

~~THERMAL - NORMAL OPERATING CONDITION~~

(LOAD CASE 2)

JOINT		DISPLACEMENTS ( IN )			DISPLACEMENTS ( IN )		
(G1)	X	Y	Z	X	Y	Z	
10	-.0000000	.0000000	.0000000	70	-.0189679	-.0033119	.0045609
20	-.0000176	-.0267053	.0011643	71	-.0146880	-.0002782	-.0022399
30	.0000058	-.0507410	-.0000333	72	-.0068358	.0002222	-.0021601
31	-.0002303	-.0801174	-.0053983	73	.0010349	.0005013	-.0073116
32	-.0021045	-.1041526	.0000190	74	-.0016229	.0014866	-.0114733
33	.0304293	-.1228466	.0223857	75	-.0080645	.0025297	-.0133454
34	.1089877	-.0467786	.0282647	76	-.0117536	.0021328	-.0111671
35	.1124262	-.0115530	.0239917	77	-.0197135	-.0000857	-.0062091
36	.1287153	.0575631	.0032286	78	-.0213542	-.0034413	.0003994
37	.1305866	.0486366	-.0033293	79	-.0000000	-.0000000	.0000000
38	.1313407	.0150049	-.0126149				
39	.1342527	-.0004506	-.0140173	80	.0055484	-.0001536	-.0002258
40	.0000000	-.0000000	.0000000	81	.0076325	-.0000984	-.0057212
41	.0269582	.0110427	.0079446	82	.0041328	.0004769	-.0098787
42	.0955920	.0145290	.0006523	83	-.0139733	.0030730	-.0237357
43	.1210708	.0027073	-.0057759	84	-.0155685	.0003860	-.0280909
44	.1372234	-.0115523	-.0123032	85	-.0148511	-.0017500	-.0281270
45	.1334135	-.0596040	-.0402598	86	-.0108406	-.0057073	-.0272329
46	.0859795	.0132430	-.0696376	87	.0118781	-.0061426	-.0141007
47	.0630238	.0396280	-.0993293	88	.0167275	-.0055161	-.0123366
48	.0401719	.0303933	-.0952250	89	.0305477	-.0048044	-.0135928
49	.0267584	.0237970	-.0749581	90	.0303074	-.0021563	-.0131835
50	.0000000	-.0000000	-.0000000	91	.0259620	.0006143	-.0137216
51	.0292999	.0059820	-.0797709	92	.0210792	.0019123	-.0124600
52	.0409054	-.0062205	-.0808974	93	.0044611	.0000329	-.0048428
53	.0507293	-.0097634	-.0985768	94	.0000000	-.0000000	-.0000000
54	.0517898	-.0093151	-.1110583	95	.0097047	-.0019710	-.0100401
55	.0452257	.0010791	-.1150300	96	.0076764	-.0009627	-.0071416
56	.0369044	.0282876	-.1000901	97	.0034893	-.0004403	-.0020764
57	.0121513	.0415664	-.0837706	98	.0000000	-.0000000	-.0000000
58	-.0101834	.0097569	.0003879	100	.0368983	.0205451	-.0952250
59	.0274923	-.0192867	.0520960	101	-.0190242	-.0002782	-.0146229
60	.0429804	-.0079824	.0397511	102	-.0066382	.0002222	-.0015546
61	.0399956	-.0028483	.0339930	103	-.0124503	.0021328	-.0100635
62	.0218138	-.0020498	.0180604	104	.0078564	-.0000884	-.0051680
63	-.1548751	-.0902269	-.0360246				
64	-.1769773	-.1160705	-.0457321				
65	-.1814659	-.1098509	-.0622726				
66	-.1024393	.0033977	-.0751013				
67	-.1166250	.0264587	-.0581002				
68	-.0272596	-.0054662	.0043635				
69	-.0199554	-.0042956	.0051946				

TABLE B1-2, Cont'd

FCES SECTION LINE 2  
 JOINT DISPLACEMENTS  
 SEISMIC ANCHOR MOVEMENTS - X - DIRECTION  
 (LOAD CASE 5)

JOINT (GID)	DISPLACEMENTS ( IN )						
	X	Y	Z				
10	.0000000	-.0000000	-.0000000	70	-.0001088	-.0002971	-.0000538
20	.0011394	-.0000555	-.0014717	71	-.0001070	-.0000283	-.0000300
30	-.0000983	-.0001054	.0000422	72	-.0001037	.0000148	.0000422
31	-.0064029	-.0001665	.0080623	73	-.0001005	-.0000013	.0000018
32	.0004115	-.0002164	-.0001009	74	-.0000754	.0000520	-.0000019
33	.0174149	-.0002553	-.0246461	75	-.0000230	.0000684	-.0000426
34	.0206650	.0009895	-.0366472	76	-.0000223	.0000468	-.0000572
35	.0206699	.0004360	-.0366065	77	-.0000200	.0000144	-.0000571
36	.0206930	-.0027152	-.0276603	78	-.0000301	-.0000719	-.0000539
37	.0231328	-.0024222	-.0222636	79	-.0000000	-.0000000	.0000000
38	.0333284	-.0005889	-.0121438				
39	.0382224	.0000581	-.0057168	80	-.0000011	-.0000142	.0000097
40	-.0000000	-.0000000	.0000000	81	-.0000477	-.0000244	-.0000151
41	-.0007953	-.0000055	.0005099	82	-.0000998	.0000004	-.0000146
42	.0100723	.0001185	.0009149	83	-.0000982	.0001034	-.0000147
43	.0232968	.0002024	.0000175	84	-.0000699	.0001252	-.0000191
44	.0306856	.0007040	.0008200	85	-.0000691	.0001259	-.0000233
45	.1611174	.0011340	.0008072	86	-.0000701	.0001205	-.0000222
46	.3154092	-.0001330	.0007937	87	-.0000693	-.0000154	.0000081
47	.3520495	.0000101	.0004418	88	-.0000693	-.0000514	.0000134
48	.3776137	.0000046	-.0006430	89	-.0000691	-.0000419	.0000188
49	.3941120	.0000007	-.0010535	90	-.0000707	-.0000391	.0000134
50	.4320000	.0000000	-.0000000	91	-.0000693	-.0000391	.0000056
51	.3956589	.0072273	.0004980	92	-.0000597	-.0000327	-.0000000
52	.3777411	.0195323	-.0035800	93	-.0000124	-.0000004	-.0000000
53	.2822438	.0000519	-.0035019	94	-.0000000	.0000000	-.0000000
54	.2165793	-.0035166	-.0036003	95	-.0000162	-.0000156	.0000173
55	.1849036	-.0002024	.0260552	96	-.0000006	-.0000041	.0000151
56	.1847946	.0159315	.0559418	97	-.0000003	.0000010	.0000041
57	.1624771	.0353789	.0674782	98	-.0000000	.0000000	.0000000
5	.0164416	.0353433	.0069455	100	.3853870	.0004425	-.0006830
58	-.1138340	.0353107	-.0270068	101	-.0005023	-.0000283	.0004072
60	-.1478695	.0065796	-.0333192	102	-.0000486	.0000148	.0004513
61	-.1463365	.0007033	-.0317868	103	-.0000478	.0000468	-.0000391
62	-.1390979	.0006681	-.0283118	104	-.0000383	-.0000244	.0000049
63	-.0370729	.0173154	-.0283178				
64	-.0193854	.0218459	-.0283184				
65	-.0083250	.0172710	-.0173800				
66	-.0083182	-.0000187	.0114044				
67	-.0084593	-.0007867	.0132104				
68	-.0006362	-.0007867	.0001641				
69	-.0001041	-.0003781	-.0000972				

TABLE BI-2, Cont'd

FOUR SECTION LINE-2

JOINT DISPLACEMENTS

SEISMIC ANCHOR MOMENTS 2 - DIRECTION

(LOAD CASE 6)

JOINT (610)	DISPLACEMENTS ( IN )				DISPLACEMENTS ( IN )		
	X	Y	Z		X	Y	Z
1	-.0000000	.0000000	.0000000	70	.0002742	-.0002560	-.0026410
20	-.0001432	.0000000	.0000000	71	.0002959	-.0000263	-.0019458
30	.0000153	.0000170	-.0000141	72	.0002992	.0000193	-.0008862
31	.0010295	.0000269	-.0026900	73	.0003027	.0000808	-.0000721
32	-.0000652	.0000349	.0000315	74	.0007202	.0001735	-.0000720
33	-.0028051	.0000412	.0083253	75	.0013712	.0003183	-.0006677
34	-.0033407	-.0001767	.0173833	76	.0013727	.0002811	-.0011604
35	-.0033414	-.0000992	.0194100	77	.0013767	-.0000292	-.0021582
36	-.0033451	.0005936	.0272471	78	.0008955	-.0004906	-.0026405
37	-.0029755	.0004837	.0282693	79	-.0000000	.0000000	.0000000
38	-.0025474	-.0001435	.0286784				
39	-.0026293	-.0000956	.0285597	80	-.0000007	.0000047	.0000510
40	.0000000	-.0000000	.0000000	81	.0001200	.0000476	.0001498
41	-.0001546	-.0000884	.0163988	82	.0003026	.0000966	.0001502
42	-.0011687	.0054597	.0281239	83	.0004368	.0002493	.0001503
43	-.0018230	.0022482	.0281966	84	.0003658	.0002284	.0001033
44	-.0026951	.0002327	.0232703	85	.0003293	.0001921	.0000762
45	-.0174786	.0076685	.0285934	86	.0002929	.0000924	.0000130
46	-.0452037	.0100905	.0249329	87	.0002792	.0001515	-.0001080
47	-.0439286	-.0015640	.0523423	88	.0002792	.0002330	-.0001272
48	-.0310929	-.0011851	.1465060	89	.0002786	.0001580	-.0001135
49	-.0207219	-.0009145	.2276708	90	.0002820	.0001498	-.0000759
50	-.0000000	-.0000000	.4320000	91	.0002725	.0001497	-.0000270
51	-.0233726	-.0360725	.2250123	92	.0002325	.0001216	.0000001
52	-.0241006	-.0155879	.2241545	93	.0000477	.0000014	.0000000
53	-.0158782	-.0011360	.2241347	94	.0000000	-.0000000	.0000000
54	-.0023676	.0079540	.2241208	95	.0000785	.0001518	-.0000635
55	.0098162	.0005498	.2102678	96	.0000031	.0000897	-.0000400
56	.0098129	-.0123584	.1901490	97	.0000014	.0000126	-.0000109
57	.0141985	-.0185600	.1485851	98	.0000000	-.0000000	-.0000000
58	.0028782	-.0185600	.0170742	100	-.0746462	-.0531889	.1465060
59	-.0226496	-.0185600	-.0681952	101	.0000370	-.0000263	-.0027362
60	-.0291255	-.0185600	-.0826452	102	.0002814	.0000193	-.0012154
61	-.0280694	-.0185600	-.0815983	103	.0012936	.0002811	-.0009945
62	-.0244340	-.0185600	-.0796902	104	.0001061	.0000476	.0001981
63	-.0031783		-.0796766				
64	.0024386		-.0796741				
65	.0078432		-.0736783				
66	.0078384		.0419310				
67	.0065950		-.0286667				
68	.0003287	-.0004144	-.0045067				
69	.0002943	-.0003275	-.0028177				

TABLE B1-2, Cont'd

~~CROSS SECTION LINE 2~~

~~JOINT DISPLACEMENTS~~

~~X + Y EARTHQUAKE 1/2-SSS (OPE)~~

(LOAD CASE 7)

~~TOTAL RESPONSE EQUALS MODE 1 THROUGH 25 BY SSS SUMMATION~~

JOINT /-----DISPLACEMENTS ( IN )-----/

<del>GIN</del>	<del>X</del>	<del>Y</del>	<del>Z</del>	<del>X</del>	<del>Y</del>	<del>Z</del>	
10	.0000000	.0000000	.0000000	70	.0044454	.0038507	.0098316
20	.0046466	.0000922	.0027046	71	.0044354	.0006295	.0075903
30	.0002768	.0001762	.0000599	72	.0044149	.0002161	.0039990
31	.0107421	.0002781	.0113180	73	.0043915	.0015919	.0026233
32	.0005780	.0003615	.0001182	74	.0057359	.0030512	.0026244
33	.0247168	.0004264	.0289737	75	.0074424	.0033222	.0032550
34	.0290697	.0013645	.0380866	76	.0074458	.0023537	.0046233
35	.0290752	.0010140	.0362253	77	.0074469	.0001184	.0080432
36	.0291012	.0007617	.0226844	78	.0058574	.0026933	.0098294
37	.0313605	.0012313	.0173820	79	.0000000	.0000000	.0000000
38	.0403939	.0024846	.0038803	80	.0000222	.0001911	.0010810
39	.0438458	.0020110	.0040411	81	.0024660	.0008556	.0032592
40	.0000000	.0000000	.0000000	82	.0043671	.0022150	.0032653
41	.0030266	.0000111	.0015224	83	.0045517	.0107091	.0032713
42	.0199849	.0004674	.0025675	84	.0039018	.0123892	.0029680
43	.0319290	.0002247	.0026747	85	.0036051	.0120877	.0033755
44	.0449529	.0010674	.0026814	86	.0032495	.0103218	.0045685
45	.1083684	.0043266	.0026989	87	.0032352	.0039090	.0051622
46	.1494746	.0003473	.0027173	88	.0032352	.0039080	.0052603
47	.1317273	.0000566	.0029896	89	.0032365	.0027963	.0032073
48	.0912990	.0000549	.0036217	90	.0033340	.0026702	.0021141
49	.0640723	.0000549	.0033139	91	.0033379	.0026689	.0006532
50	.0000000	.0000000	.0000000	92	.0028930	.0020023	.0000047
51	.0672147	.0111165	.0082810	93	.0006104	.0000207	.0000018
52	.0755949	.0317865	.0132848	94	.0000000	.0000000	.0000000
53	.1338845	.0014324	.0132977	95	.0009987	.0039032	.0022942
54	.1826509	.0108134	.0133068	96	.0000321	.0030605	.0012483
55	.2087412	.0007009	.0212550	97	.0000146	.0002264	.0003571
56	.2087370	.6306762	.0542574	98	.0000000	.0000000	.0000000
57	.1789047	.0597424	.0684738	100	.0050162	.0005316	.0036217
58	.0350111	.0537579	.0372262	101	.0054831	.0006295	.0118433
59	.2151553	.0597721	.1681304	102	.0047572	.0002161	.0000419
60	.2744039	.0227959	.2135418	103	.0070405	.0023537	.0046030
61	.2710026	.0212592	.2151672	104	.0025860	.0008556	.0039318
62	.2573250	.0011573	.2183349				
63	.1640212	.1319718	.2184130				
64	.1562284	.1420335	.2184100				
65	.1538700	.1145476	.2014577				
66	.1538203	.0093750	.1393196				
67	.1379273	.0051255	.1063532				
68	.0073332	.0047580	.0155033				
69	.0044477	.0045657	.0103790				



TABLE B1-2, Cont'd

SOFT STORY LINE 2

JOINT DISPLACEMENTS

Z + Y EARTHQUAKE 1/2 SSE (DRF)

(LOAD CASE - 8)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 25 BY SQSS SUMMATION

JOINT GID	DISPLACEMENTS ( IN )				DISPLACEMENTS ( IN )		
	X	Y	Z		X	Y	Z
10	.0000000	.0000000	.0000000	70	.0022078	.0019058	.0255953
20	.0012953	.0000346	.0045032	71	.0022108	.0002432	.0202139
30	.0000743	.0000656	.0000929	72	.0022161	.0001177	.0106777
31	.0047413	.0001036	.0090140	73	.0022182	.0009991	.0027927
32	.0002144	.0001347	.0000822	74	.0059149	.0018487	.0027941
33	.0096711	.0001588	.0169952	75	.0107633	.0021752	.0076533
34	.0112458	.0004975	.0184780	76	.0107733	.0016934	.0120279
35	.0112475	.0003740	.0165815	77	.0107902	.0002243	.0211019
36	.0112554	.0008451	.0110410	78	.0064666	.0022611	.0255899
37	.0116705	.0007817	.0105714	79	.0000000	.0000000	.0000000
38	.0139081	.0008969	.0101426	80	.0000148	.0001361	.0006126
39	.0148460	.0008593	.0100447	81	.0009352	.0006386	.0014044
40	.0000000	.0000000	.0000000	82	.0022148	.0013744	.0014106
41	.0016325	.0000300	.0058499	83	.0037372	.0058912	.0014133
42	.0077577	.0019783	.0100484	84	.0032500	.0069117	.0017603
43	.0114208	.0007230	.0100942	85	.0070750	.0068387	.0021906
44	.0151515	.0007301	.0101146	86	.0029219	.0063554	.0021487
45	.0330452	.0027266	.0101754	87	.0028898	.0017485	.0030716
46	.0561078	.0004969	.0102394	88	.0028893	.0024324	.0030730
47	.0546763	.0000901	.0110595	89	.0028856	.0020001	.0018416
48	.0393186	.0000816	.0128200	90	.0029523	.0019087	.0012300
49	.0285120	.0000776	.0118539	91	.0029010	.0019074	.0003971
50	.0000000	.0000000	.0000000	92	.0025092	.0015373	.0000036
51	.0379944	.0041448	.0198135	93	.0005317	.0000173	.0000014
52	.0720197	.0130029	.0295464	94	.0000000	.0000000	.0000000
53	.2448283	.0015163	.0295812	95	.0007318	.0017472	.0015787
54	.3672246	.0246096	.0296057	96	.0000281	.0011181	.0009761
55	.4311394	.0010622	.0490288	97	.0000128	.0003682	.0002798
56	.4311388	.0689418	.1231229	98	.0000000	.0000000	.0000000
57	.3645558	.1335859	.1543648	100	.0484792	.0008049	.0124200
58	.0362213	.1336322	.0776309	101	.0041344	.0002432	.0280717
59	.4912774	.1336744	.3656818	102	.0024608	.0001177	.0159712
60	.6092450	.0438189	.4697327	103	.0109265	.0016934	.0117960
61	.6021057	.0392803	.4744729	104	.0011120	.0006386	.0015493
62	.5720248	.0013592	.4831759				
63	.1895498	.1472349	.4833453				
64	.1144012	.1514986	.4833734				
65	.0655606	.1119270	.4462047				
66	.0655183	.0018982	.2954705				
67	.0652183	.0050570	.2192920				
68	.0049314	.0050485	.0364493				
69	.0022085	.0024996	.0262744				

TABLE B1-2. Cont'd

FCCS SUCTION LINE 2

X + Y EARTHQUAKE CASE

(LOAD CASE 9)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 25 BY SQSS SUMMATION

JOINT NO	DISPLACEMENTS ( IN )				X	Y	Z
	X	Y	Z				
19	.0000000	.0000000	.0000000	70	.0073561	.0057373	.0175151
20	.0079228	.0001482	.0046895	71	.0073427	.0009272	.0135040
30	.0004657	.0002814	.0000973	72	.0073134	.0003329	.0071177
31	.0173721	.0004442	.0184241	73	.0072608	.0027787	.0044759
32	.0009298	.0005775	.0001922	74	.0095804	.0052305	.0044779
33	.0395444	.0006811	.0466341	75	.0125898	.0055549	.0057705
34	.0465008	.0021799	.0610616	76	.0125963	.0038958	.0082665
35	.0465095	.0016183	.0580124	77	.0125993	.0002122	.0143567
36	.0465508	.0012630	.0362072	78	.0098083	.0040962	.0175113
37	.0501308	.0019789	.0277563	79	.0000000	.0000000	.0000000
38	.0644596	.0039889	.0141424	80	.0000365	.0003192	.0018379
39	.0699366	.0032724	.0066473	81	.0041020	.0015103	.0054865
40	.0000000	.0000000	.0000000	82	.0072375	.0038731	.0054974
41	.0050140	.0000183	.0027073	83	.0076342	.0186960	.0055081
42	.0320162	.0008176	.0045564	84	.0065789	.0216666	.0050981
43	.0510140	.0003972	.0045686	85	.0060989	.0211564	.0058885
44	.0716930	.0018415	.0045798	86	.0055670	.0189780	.0080107
45	.1721247	.0075617	.0045099	87	.0055095	.0067709	.0090036
46	.2374660	.0006067	.0046416	88	.0055094	.0067151	.0091573
47	.2094418	.0000976	.0051167	89	.0055087	.0048122	.0055519
48	.1452178	.0000934	.0062811	90	.0056839	.0045944	.0036583
49	.1019519	.0000927	.0058195	91	.0056097	.0045922	.0011282
50	.0000000	.0000000	.0000000	92	.0049451	.0035819	.0000082
51	.1072982	.0176544	.0145751	93	.0010458	.0000357	.0000032
52	.1227284	.0505339	.0235813	94	.0000000	.0000000	.0000000
53	.2328621	.0023465	.0236041	95	.0017001	.0067596	.0039911
54	.3236695	.0197613	.0236202	96	.0000540	.0053191	.0021474
55	.3720647	.0011877	.0386450	97	.0000246	.0014426	.0006206
56	.3720588	.0558650	.0988580	98	.0000000	.0000000	.0000000
57	.3179662	.1086591	.1245758	100	.1514359	.0009142	.0062811
58	.0576393	.1086897	.0565669	101	.0092557	.0009272	.0210457
59	.4020580	.1087178	.3037299	102	.0079059	.0003329	.0139894
60	.4983801	.0400917	.3873208	103	.0120173	.0038958	.0081192
61	.4923722	.0370293	.3905977	104	.0043238	.0015103	.0065867
62	.4677678	.0018512	.3968053				
63	.2538890	.2104027	.3969467				
64	.2314535	.2251670	.3969411				
65	.2234939	.1799007	.3661333				
66	.2234204	.0135424	.2512274				
67	.2008222	.0081221	.1907677				
68	.0113902	.0076245	.0273232				
69	.0073592	.0064263	.0186915				

TABLE B1-2, Cont'd

FLOOR SECTION LINE 2

JOINT DISPLACEMENTS

Z + Y EARTHQUAKE SSE

(LOAD CASE 10)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 25 BY SQSS SUMMATION

JOINT GID	DISPLACEMENTS ( IN )				DISPLACEMENTS ( IN )		
	X	Y	Z		X	Y	Z
10	.0000000	.0000000	.0000000	70	.0039303	.0034401	.0451855
20	.0023158	.0000611	.0077833	71	.0039354	.0004375	.0356196
30	.0001311	.0001160	.0000603	72	.0039449	.0002123	.0187562
31	.0083971	.0001832	.0156746	73	.0039484	.0017862	.0040836
32	.0003812	.0002381	.0001434	74	.0104615	.0032921	.0048961
33	.0170485	.0002808	.0296523	75	.0190453	.0038879	.0134790
34	.0199099	.0002817	.0323531	76	.0190522	.0030376	.0212138
35	.0199128	.0006606	.0290712	77	.0190932	.0004049	.0372517
36	.0199269	.0014791	.0193333	78	.0114595	.0040885	.0451760
37	.0206892	.0013750	.0184479	79	.0000000	.0000000	.0000000
38	.0246473	.0015974	.0176280	80	.0000267	.0002446	.0010750
39	.0263662	.0015307	.0174386	81	.0016921	.0011453	.0024950
40	.0000000	.0000000	.0000000	82	.0039423	.0024544	.0025055
41	.0028905	.0000520	.0101553	83	.0065982	.0105283	.0025104
42	.0137745	.0034339	.0174782	84	.0057241	.0123487	.0030374
43	.0202857	.0012557	.0175229	85	.0054135	.0122127	.0039105
44	.0269061	.0013000	.0175534	86	.0051410	.0113362	.0052617
45	.0583305	.0049054	.0176646	87	.0050846	.0031125	.0054252
46	.0993229	.0008873	.0177763	88	.0050837	.0042923	.0054162
47	.0969730	.0001606	.0192256	89	.0050771	.0035057	.0032326
48	.0698460	.0001457	.0223742	90	.0051947	.0033442	.0021569
49	.0508703	.0001390	.0207285	91	.0051038	.0033419	.0006956
50	.0000000	.0000000	.0000000	92	.0044146	.0026944	.0000062
51	.0678038	.0073122	.0352467	93	.0009356	.0000303	.0000024
52	.1294456	.0230613	.0529337	94	.0000000	.0000000	.0000000
53	.4412050	.0027255	.0529953	95	.0012888	.0031101	.0027660
54	.6618711	.0443552	.0530388	96	.0000494	.0023532	.0017034
55	.7770702	.0019151	.0881364	97	.0000225	.0006586	.0004884
56	.7770691	.1242419	.2218200	98	.0000000	.0000000	.0000000
57	.6570971	.2407342	.2781656	100	.0864613	.0014532	.0223742
58	.0656713	.2408175	.1402667	101	.0074371	.0004375	.0497199
59	.8860767	.2408936	.6605900	102	.0043657	.0002123	.0281677
60	1.0990495	.0791021	.8485231	103	.0193029	.0030376	.0207836
61	1.0862062	.0709838	.8570590	104	.0019960	.0011453	.0027320
62	1.0320683	.0024643	.8727096				
63	.3423362	.2665951	.8730159				
64	.2065590	.2742604	.8730034				
65	.1183030	.2026128	.8057751				
66	.1182266	.0033817	.5333132				
67	.1177790	.0091548	.3950498				
68	.0088979	.0091399	.0656269				
69	.0039317	.0043522	.0474439				

TABLE B 11

ELASTIC SUPPORT REACTIONS

B 11-1	HPCS Suction Line 1	Pages B-15 to B-18
B 11-2	HPCS Suction Line 2	Pages B-19 to B-22

Note: Designation "ECCS" in the following tables  
is synonymous with designation "HPCS"



TABLE B 11-1

FEES SUCTION LINE 1  
ELASTIC SUPPORT REACTIONS

(LOAD CASE 1)

DEAD WEIGHT AND OTHER SUSTAINED MECHANICAL LOADS

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN.-LB.)		
	X	Y	Z	X	Y	Z
1	-25.355	63.988	31.460	-477.459	-1.596	-383.942
4	0.000	109.118	0.000	0.000	0.000	0.000
6	0.000	168.136	0.000	0.000	0.000	0.000
10	17.527	571.248	-14.896	947.707	-16.506	1229.724
23	16.230	161.296	9.710	1122.204	25.677	-1213.693
24	-17.514	173.957	-9.741	-173.644	-.002	312.231

INCLINED AXIS SUPPORT REACTIONS

SUPPORT JOINT	REACTION TYPE	REACTION MAGNITUDE	DIRECTION COSINES (INCLINED AXIS)		
			X	Y	Z
14	FORCE	-67.958	-.6690	0.0000	.7433
14	FORCE	3.124	-.7433	0.0000	-.6690
16	FORCE	49.574	-.6690	0.0000	.7433
16	FORCE	1.163	-.7433	0.0000	-.6690

(LOAD CASE 2)

THERMAL - NORMAL OPERATING CONDITION

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN.-LB.)		
	X	Y	Z	X	Y	Z
1	-65.92	-53.31	83.47	183.30	76.45	192.66
4	0.00	143.32	0.00	0.00	0.00	0.00
6	0.00	-197.38	0.00	0.00	0.00	0.00
10	722.21	113.46	43.77	-58.45	-11901.28	-3678.61
23	-341.78	-226.00	132.09	3558.74	14779.61	-6366.34
24	-370.47	219.90	-206.05	-6306.58	.07	11339.16

INCLINED AXIS SUPPORT REACTIONS

SUPPORT JOINT	REACTION TYPE	REACTION MAGNITUDE	DIRECTION COSINES (INCLINED AXIS)		
			X	Y	Z
14	FORCE	-224.501	-.6690	0.0000	.7433
14	FORCE	17.845	-.7433	0.0000	-.6690
16	FORCE	151.870	-.6690	0.0000	.7433
16	FORCE	-23.299	-.7433	0.0000	-.6690

TABLE B 11-1 Cont'd

SEISMIC ANCHOR MOVEMENTS

E L A S T I C S U P P O R T R E A C T I O N S

(LOAD CASE 5)

SEISMIC ANCHOR MOVEMENTS X - DIRECTION

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN.-LB.)		
	X	Y	Z	X	Y	Z
1	41.70	15.59	-44.63	-307.27	627.72	753.63
4	0.00	-49.37	0.00	0.00	0.00	0.00
6	0.00	92.74	0.00	0.00	0.00	0.00
10	1288.09	-84.85	185.45	1124.33	-27759.36	9494.02
20	-1709.60	25.98	-163.75	634.67	26651.22	-1032.11
20	.00	-.00	-.00	-.09	-.01	-.05

INCLINED AXIS SUPPORT REACTIONS

SUPPORT JOINT	REACTION TYPE	REACTION MAGNITUDE	DIRECTION COSINES (INCLINED AXIS)		
			X	Y	Z
14	FORCE	156.692	-.6690	0.0000	.7433
14	FORCE	32.000	-.7433	0.0000	-.6690
14	FORCE	-394.015	-.6690	0.0000	.7433
14	FORCE	-329.471	-.7433	0.0000	-.6690

(LOAD CASE 6)

SEISMIC ANCHOR MOVEMENTS Z - DIRECTION

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN.-LB.)		
	X	Y	Z	X	Y	Z
1	-45.06	-19.27	59.92	-596.43	415.95	284.25
4	0.00	61.04	0.00	0.00	0.00	0.00
6	0.00	-114.68	0.00	0.00	0.00	0.00
10	186.32	81.86	-227.48	-18240.78	-10398.31	-1000.90
20	-163.75	-9.95	-160.87	-851.18	-6551.73	532.33
20	-.00	.00	.00	.02	.00	.01

INCLINED AXIS SUPPORT REACTIONS

SUPPORT JOINT	REACTION TYPE	REACTION MAGNITUDE	DIRECTION COSINES (INCLINED AXIS)		
			X	Y	Z
14	FORCE	-181.607	-.6690	0.0000	.7433
14	FORCE	33.500	-.7433	0.0000	-.6690
14	FORCE	411.627	-.6690	0.0000	.7433
14	FORCE	-269.932	-.7433	0.0000	-.6690

TABLE B 11-1, Cont'd

SCSS SUCTION LINE 1

ELASTIC SUPPORT REACTIONS

(LOAD CASE 7) X + Y EARTHQUAKE 1/2 SSE (DRF)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 6 BY SCSS SUMMATION

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN.-LB.)		
	X	Y	Z	X	Y	Z
1	145.1	2.2	117.6	2320.	20205.	2884.
4	0.0	6.7	0.0	0.	0.	0.
4	0.0	15.8	0.0	0.	0.	0.
10	85.3	9.8	66.8	943.	90.	1184.
23	2.7	3.5	.7	74.	24.	99.
20	.0	.0	.0	0.	0.	0.

INCLINED AXIS SUPPORT REACTIONS

SUPPORT JOINT	REACTION TYPE	REACTION MAGNITUDE	DIRECTION COSINES (INCLINED AXIS)		
			X	Y	Z
14	FORCE	53.3	-.6690	0.0000	.7433
14	FORCE	737.8	-.7433	0.0000	-.6690
14	FORCE	40.9	-.6690	0.0000	.7433
14	FORCE	603.3	-.7433	0.0000	-.6690

(LOAD CASE 8) Z + Y EARTHQUAKE 1/2 SSE (DRF)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 6 BY SCSS SUMMATION

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN.-LB.)		
	X	Y	Z	X	Y	Z
1	117.1	3.1	95.6	1870.	14281.	2323.
4	0.0	9.7	0.0	0.	0.	0.
4	0.0	23.0	0.0	0.	0.	0.
10	68.8	13.9	53.9	763.	70.	956.
23	2.2	3.4	.9	80.	19.	101.
20	.0	.0	.0	0.	0.	0.

INCLINED AXIS SUPPORT REACTIONS

SUPPORT JOINT	REACTION TYPE	REACTION MAGNITUDE	DIRECTION COSINES (INCLINED AXIS)		
			X	Y	Z
14	FORCE	57.7	-.6690	0.0000	.7433
14	FORCE	504.4	-.7433	0.0000	-.6690
14	FORCE	38.3	-.6690	0.0000	.7433
14	FORCE	486.2	-.7433	0.0000	-.6690

TABLE B 11-1, Cont'd

~~FOSS SUCTION LINE 1-~~

~~ELASTIC SUPPORT REACTIONS~~

(LOAD CASE 9) ~~X + Y EARTHQUAKE SSE~~

~~TOTAL RESPONSE EQUALS MODE 1 THROUGH 6 BY SSS SUMMATION~~

SUPPORT JOINT	/-----FORCE ( LB. )-----/			/-----MOMENT (IN.-LB.)-----/		
	X	Y	Z	X	Y	Z
1	209.	4.	170.	3333.	29006.	4143.
4	0.	13.	0.	0.	0.	0.
6	0.	30.	0.	0.	0.	0.
10	123.	18.	96.	1356.	141.	1702.
23	4.	7.	1.	147.	34.	184.
28	0.	0.	0.	0.	0.	0.

INCLINED AXIS SUPPORT REACTIONS

SUPPORT JOINT	REACTION TYPE	REACTION MAGNITUDE	/-----DIRECTION COSINES-----/ (INCLINED AXIS)		
			X	Y	Z
14	FORCE	85.7	-.6690	0.0000	.7433
14	FORCE	1059.6	-.7433	0.0000	-.6690
16	FORCE	61.9	-.6690	0.0000	.7433
16	FORCE	866.1	-.7433	0.0000	-.6690

(LOAD CASE 10) ~~Z + Y EARTHQUAKE SSE~~

~~TOTAL RESPONSE EQUALS MODE 1 THROUGH 6 BY SSS SUMMATION~~

SUPPORT JOINT	/-----FORCE ( LB. )-----/			/-----MOMENT (IN.-LB.)-----/		
	X	Y	Z	X	Y	Z
1	168.6	5.9	138.4	2687.	23372.	3336.
4	0.0	18.1	0.0	0.	0.	0.
6	0.0	42.9	0.0	0.	0.	0.
10	98.8	25.8	77.6	1101.	106.	1376.
23	3.2	6.8	.2	156.	28.	190.
28	.0	.0	.0	0.	0.	0.

INCLINED AXIS SUPPORT REACTIONS

SUPPORT JOINT	REACTION TYPE	REACTION MAGNITUDE	/-----DIRECTION COSINES-----/ (INCLINED AXIS)		
			X	Y	Z
14	FORCE	99.4	-.6690	0.0000	.7433
14	FORCE	853.4	-.7433	0.0000	-.6690
16	FORCE	61.6	-.6690	0.0000	.7433
16	FORCE	697.9	-.7433	0.0000	-.6690

TABLE B 11-2

COAST GUARDIAN LINE 2  
ELASTIC SUPPORT REACTIONS  
(LOAD CASE 1)

DEAD WEIGHT AND OTHER SUSTAINED MECHANICAL LOADS

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN -LB.)		
	X	Y	Z	X	Y	Z
10	.003	268.620	-.287	10.816	-17.316	.094
30	-.011	0.000	1.098	0.000	0.000	0.000
32	.444	0.000	.861	0.000	0.000	0.000
35	0.000	93.174	0.000	0.000	0.000	0.000
40	-3.397	-14.503	14.013	272.497	41.620	-67.169
42	0.000	268.941	0.000	0.000	0.000	0.000
44	0.000	193.869	0.000	0.000	0.000	0.000
50	19.155	111.596	1.110	163.480	-671.180	-664.204
52	0.000	-24.541	0.000	0.000	0.000	0.000
55	0.000	129.049	0.000	0.000	0.000	0.000
58	-7.857	0.000	-27.368	0.000	0.000	0.000
62	0.000	244.163	0.000	0.000	0.000	0.000
64	0.000	472.672	0.000	0.000	0.000	0.000
71	-.247	-450.746	2.271	0.000	0.000	0.000
72	-.243	786.819	1.197	0.000	0.000	0.000
77	-1.023	177.805	2.224	0.000	0.000	0.000
79	-4.150	93.753	5.950	763.617	-60.988	1605.049
92	.567	92.546	.001	0.000	0.000	0.000
94	1.854	-25.393	.866	-67.123	-49.994	-9.991
98	-7.078	129.937	-1.937	104.744	16.353	1372.374

(LOAD CASE 2)

THERMAL - NORMAL OPERATING CONDITION

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN -LB.)		
	X	Y	Z	X	Y	Z
10	.051	-1085.931	-3.041	114.755	-119.701	1.824
30	-.821	0.000	11.663	0.000	0.000	0.000
32	252.544	0.000	-6.657	0.000	0.000	0.000
35	0.000	1271.925	0.000	0.000	0.000	0.000
40	-270.492	149.069	-216.421	-3937.729	3297.384	9029.704
42	0.000	-297.859	0.000	0.000	0.000	0.000
44	0.000	-1456.729	0.000	0.000	0.000	0.000
50	-34.351	1361.175	201.090	7910.397	-207.159	2160.547
52	0.000	83.969	0.000	0.000	0.000	0.000
55	0.000	-118.705	0.000	0.000	0.000	0.000
58	23.626	0.000	-.900	0.000	0.000	0.000
62	0.000	102.490	0.000	0.000	0.000	0.000
64	0.000	-169.883	0.000	0.000	0.000	0.000
71	29.640	277.959	-4.518	0.000	0.000	0.000
72	13.725	-221.974	4.359	0.000	0.000	0.000
77	19.782	85.658	12.712	0.000	0.000	0.000
79	8.341	10.724	-35.188	-84.629	-165.514	210.494
92	-9.003	-32.823	9.773	0.000	0.000	0.000
94	-31.866	14.270	-28.762	51.750	401.503	-167.764
98	-61.256	22.672	56.291	-186.721	-751.070	180.523



TABLE B 11-2, Cont'd

SEISMIC ANCHOR MOVEMENTS Z - DIRECTION  
 (LOAD CASE 5)

SUPPORT / JOINT	FORCE ( LB. )			MOMENT ( IN -LB. )		
	X	Y	Z	X	Y	Z
10	.49	-9.31	-1.28	48.39	62.61	18.20
30	-1.90	0.00	4.93	0.00	0.00	0.00
32	7.90	0.00	-11.03	0.00	0.00	0.00
35	0.00	10.91	0.00	0.00	0.00	0.00
40	-1.17	229.92	-323.43	-7209.45	-49.40	-36.64
43	0.00	-247.30	0.00	0.00	0.00	0.00
44	0.00	-1109.96	0.00	0.00	0.00	0.00
50	6.18	1055.67	363.26	18283.19	-388.75	-1310.25
53	0.00	124.96	0.00	0.00	0.00	0.00
55	0.00	-60.44	0.00	0.00	0.00	0.00
58	-6.68	0.00	-39.52	0.00	0.00	0.00
62	0.00	4.44	0.00	0.00	0.00	0.00
64	0.00	-39.85	0.00	0.00	0.00	0.00
71	-1.60	26.32	3.93	0.00	0.00	0.00
72	-1.60	-19.28	1.79	0.00	0.00	0.00
77	-2.78	29.12	4.36	0.00	0.00	0.00
78	3.82	-1.32	-2.98	-10.68	68.23	-6.39
93	-1.10	-1.35	-1.00	0.00	0.00	0.00
94	-1.31	.93	-1.05	2.69	8.47	-1.63
98	-4.25	.56	.24	-1.50	-3.83	-2.78

(LOAD CASE 6)

SUPPORT / JOINT	FORCE ( LB. )			MOMENT ( IN -LB. )		
	X	Y	Z	X	Y	Z
10	-3.023	57.710	3.944	-145.051	-9.778	-113.233
30	11.791	0.000	-14.765	0.000	0.000	0.000
32	-49.379	0.000	35.727	0.000	0.000	0.000
35	0.000	-47.963	0.000	0.000	0.000	0.000
40	5.549	14.290	-11.242	-232.897	1056.673	-274.792
43	0.000	-22.260	0.000	0.000	0.000	0.000
44	0.000	14.631	0.000	0.000	0.000	0.000
50	66.243	-1.764	6.178	170.625	363.443	-3370.410
53	0.000	-5.713	0.000	0.000	0.000	0.000
55	0.000	22.264	0.000	0.000	0.000	0.000
58	-38.144	0.000	-16.113	0.000	0.000	0.000
62	0.000	-33.407	0.000	0.000	0.000	0.000
64	0.000	.934	0.000	0.000	0.000	0.000
71	.216	28.302	-1.041	0.000	0.000	0.000
72	.209	-14.794	-1.045	0.000	0.000	0.000
77	.042	-14.411	.115	0.000	0.000	0.000
78	5.480	1.301	-3.129	-1.739	20.260	20.364
93	.625	.601	.000	0.000	0.000	0.000
94	.013	-1.262	.125	-1.753	-2.204	.135
98	.858	-1.254	-1.093	-1.131	1.449	-1.102

TABLE B 11-2, Cont'd

ECCS SUCTION LINE 2-

ELASTIC SUPPORT REACTIONS

(LOAD CASE 7)

X - Y EARTHQUAKE 1/2 SSE (DRF)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 25 BY SQSS SUMMATION

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN -LB.)		
	X	Y	Z	X	Y	Z
19	19.2	96.5	8.8	303.	52.	596.
30	33.2	0.0	21.0	0.	0.	0.
32	69.4	0.0	41.4	0.	0.	0.
35	0.0	111.5	0.0	0.	0.	0.
40	27.1	28.8	32.6	708.	1124.	1105.
43	0.0	24.7	0.0	0.	0.	0.
46	0.0	38.2	0.0	0.	0.	0.
50	117.0	63.5	18.0	466.	767.	5786.
53	0.0	157.6	0.0	0.	0.	0.
55	0.0	77.1	0.0	0.	0.	0.
58	81.2	0.0	86.4	0.	0.	0.
62	0.0	57.9	0.0	0.	0.	0.
66	0.0	466.8	0.0	0.	0.	0.
71	9.0	628.9	15.3	0.	0.	0.
72	8.9	215.8	8.1	0.	0.	0.
77	15.0	118.3	16.2	0.	0.	0.
79	115.6	22.5	52.8	224.	1409.	284.
93	1.2	20.7	.0	0.	0.	0.
94	4.9	15.0	3.9	44.	111.	5.
99	43.5	21.3	9.6	90.	129.	293.

(LOAD CASE 8)

Z - Y EARTHQUAKE 1/2 SSE (DRF)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 25 BY SQSS SUMMATION

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN -LB.)		
	X	Y	Z	X	Y	Z
19	4.26	35.94	18.98	585.	81.	145.
30	8.91	0.00	32.53	0.	0.	0.
32	25.72	0.00	28.78	0.	0.	0.
35	0.00	41.14	0.00	0.	0.	0.
40	17.45	77.88	114.74	2567.	384.	607.
43	0.00	79.53	0.00	0.	0.	0.
46	0.00	54.65	0.00	0.	0.	0.
50	64.16	89.72	50.79	1565.	1522.	2788.
53	0.00	166.80	0.00	0.	0.	0.
55	0.00	116.89	0.00	0.	0.	0.
58	84.03	0.00	180.10	0.	0.	0.
62	0.00	67.96	0.00	0.	0.	0.
66	0.00	94.91	0.00	0.	0.	0.
71	4.46	242.95	40.79	0.	0.	0.
72	4.47	117.58	21.55	0.	0.	0.
77	21.77	224.11	42.58	0.	0.	0.
79	77.05	14.75	62.09	134.	881.	199.
93	1.07	17.23	.00	0.	0.	0.
94	4.06	11.73	2.45	34.	96.	6.
99	39.09	13.93	7.57	51.	101.	136.



TABLE B 11-2, Cont'd

SOSS SECTION LINE 2

SUPPORT REACTION CONDITIONS

(LOAD CASE 9)

Y • Y EARTHQUAKE CASE

TOTAL RESPONSE EQUALS MODE 1 THROUGH 25 BY SOSS SUMMATION

SUPPORT JOINT	FORCE (LR.)			MOMENT (IN -LB.)		
	X	Y	Z	X	Y	Z
19	33.0	154.1	14.9	513.	88.	1021.
30	55.9	0.0	34.0	0.	0.	0.
32	111.6	0.0	67.3	0.	0.	0.
35	0.0	178.0	0.0	0.	0.	0.
40	44.6	47.6	55.0	1201.	1794.	1799.
42	0.0	43.7	0.0	0.	0.	0.
46	0.0	66.7	0.0	0.	0.	0.
50	186.8	107.1	31.2	821.	1356.	9215.
52	0.0	258.1	0.0	0.	0.	0.
55	0.0	130.7	0.0	0.	0.	0.
58	133.7	0.0	154.4	0.	0.	0.
62	0.0	92.6	0.0	0.	0.	0.
66	0.0	677.1	0.0	0.	0.	0.
71	14.8	926.2	27.3	0.	0.	0.
72	14.8	332.4	14.4	0.	0.	0.
77	25.4	212.0	29.0	0.	0.	0.
79	189.9	38.2	91.9	390.	2404.	476.
93	2.1	35.7	.0	0.	0.	0.
94	8.4	25.9	6.8	75.	191.	8.
94	73.3	37.4	16.7	158.	224.	513.

(LOAD CASE 10)

Z • Y EARTHQUAKE CASE

TOTAL RESPONSE EQUALS MODE 1 THROUGH 25 BY SOSS SUMMATION

SUPPORT JOINT	FORCE (LR.)			MOMENT (IN -LB.)		
	X	Y	Z	X	Y	Z
19	7.6	63.5	32.9	1010.	141.	259.
30	15.7	0.0	56.1	0.	0.	0.
32	45.7	0.0	50.2	0.	0.	0.
35	0.0	72.7	0.0	0.	0.	0.
40	30.9	135.2	199.2	4455.	683.	1075.
42	0.0	138.1	0.0	0.	0.	0.
46	0.0	97.6	0.0	0.	0.	0.
50	114.6	160.6	89.3	2744.	2744.	4965.
52	0.0	299.8	0.0	0.	0.	0.
55	0.0	210.7	0.0	0.	0.	0.
58	152.4	0.0	325.4	0.	0.	0.
62	0.0	123.2	0.0	0.	0.	0.
66	0.0	169.1	0.0	0.	0.	0.
71	7.9	447.0	71.9	0.	0.	0.
72	8.0	212.0	37.9	0.	0.	0.
77	38.5	404.5	75.2	0.	0.	0.
79	132.6	26.4	107.4	240.	1542.	357.
93	1.9	30.3	.0	0.	0.	0.
94	7.2	20.6	5.2	59.	169.	10.
94	67.1	24.7	13.2	91.	177.	243.

TABLE B III

CLASS 1 COMPONENT  
STRESS ANALYSIS PIPES RESULTS

B III-1	HPCS Suction Line 1	Pages B-24 to B-32
B III-2	HPCS Suction Line 2	Pages B-33 to B-59

Note: Designation "ECCS" in the following tables  
is synonymous with designation "HPCS".

B. CLASS I COMPONENT STRESS ANALYSIS

B.0 STRESS INDICES

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE			MOMENT			THERMAL			TEE MOMENTS						STRESS INDEX DESCRIPTION
		R1	C1	K1	R2	C2	K2	C3	K3	C3P	R2R	R2B	C2R	C2B	K2R	K2B	
1A	2	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	TAPERED TRANS. JOINT
2A	3	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
3A	4	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
4A	5	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
5A	6	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
6A	7	.50	1.10	1.70	1.00	1.00	1.00	1.00	1.70	.50	0.00	0.00	0.00	0.00	0.00	0.00	BUTT WELD, AS WELDED
7A	8	.50	1.10	1.70	1.00	1.00	1.00	1.00	1.70	.50	0.00	0.00	0.00	0.00	0.00	0.00	BUTT WELD, AS WELDED
8A	9	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
9A	10	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
10A	11	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
11A	12	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
12A	13	.50	1.10	1.70	1.00	1.00	1.00	1.00	1.70	.50	0.00	0.00	0.00	0.00	0.00	0.00	BUTT WELD, AS WELDED
13A	14	.50	1.10	1.70	1.00	1.00	1.00	1.00	1.70	.50	0.00	0.00	0.00	0.00	0.00	0.00	BUTT WELD, AS WELDED
14A	15	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
15A	16	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
16A	17	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
17A	18	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
18A	19	1.00	1.50	4.00	0.00	0.00	1.00	1.00	1.00	.50	2.17	2.17	2.90	2.90	1.00	1.00	WELDING TEE
19A	20	1.00	1.50	4.00	0.00	0.00	1.00	1.00	1.00	.50	2.17	2.17	2.90	2.90	1.00	1.00	WELDING TEE
20A	21	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
21A	22	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
22A	23	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
23A	24	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
24A	25	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
25A	26	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE

PIPES

PAGE 110.

21A	26	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
22A	27	.50	1.10	1.70	1.00	1.00	1.00	1.00	1.70	.50	0.00	0.00	0.00	0.00	0.00	0.00	BUTT WELD, AS WELDED
23A	28	.50	1.10	1.70	1.00	1.00	1.00	1.00	1.70	.50	0.00	0.00	0.00	0.00	0.00	0.00	BUTT WELD, AS WELDED
24A	29	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE			MOMENT			THERMAL			TEE MOMENTS						STRESS INDEX DESCRIPTION
		R1	C1	K1	R2	C2	K2	C3	K3	C3P	R2R	R2B	C2R	C2B	K2R	K2B	
1C	1	1.00	1.27	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
2C	2	1.00	1.27	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
3C	3	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
4C	4	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
5C	5	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
6C	6	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
7C	7	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
8C	8	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
9C	9	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
10C	10	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
11C	11	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
12C	12	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
13C	13	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
14C	14	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
15C	15	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
16C	16	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
17C	17	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
18C	18	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
19C	19	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
20C	20	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
21C	21	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
22C	22	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
23C	23	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
24C	24	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
25C	25	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
26C	26	1.00	1.04	1.00	1.42	1.49	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF PCCS SUCTION LINE-1 L&C&V

B.1 CONSIDERATION OF EQUATION 9

STRESS FOR EQUATION 9  
LOAD SET 1 - LOAD COMBINATION 1

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (OT)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
14	2	474.68	4002.02	0.00	0.00	0.00	4474.70	.2159	TAPERED TRANS. JOINT
	3	474.68	4449.22	0.00	0.00	0.00	5323.90	.1775	STRAIGHT PIPE
24	3	474.68	4049.21	0.00	0.00	0.00	5323.90	.1775	STRAIGHT PIPE
	4	474.68	3309.41	0.00	0.00	0.00	3744.50	.1261	STRAIGHT PIPE
34	4	474.68	3309.41	0.00	0.00	0.00	3744.50	.1261	STRAIGHT PIPE
	5	474.68	1744.59	0.00	0.00	0.00	2240.27	.0747	STRAIGHT PIPE
44	5	474.68	1744.60	0.00	0.00	0.00	2240.28	.0747	STRAIGHT PIPE
	6	474.68	2201.64	0.00	0.00	0.00	2678.32	.0893	STRAIGHT PIPE
54	6	474.68	2201.65	0.00	0.00	0.00	2678.33	.0893	STRAIGHT PIPE
	7	474.68	3074.57	0.00	0.00	0.00	3511.20	.1170	BUTT WELD, AS WELDED
64	7	474.68	3074.51	0.00	0.00	0.00	3511.20	.1170	BUTT WELD, AS WELDED
	8	474.68	2444.06	0.00	0.00	0.00	3277.22	.1092	STRAIGHT PIPE
74	8	474.68	1817.38	0.00	0.00	0.00	2292.06	.0744	STRAIGHT PIPE
	10	474.68	1014.84	0.00	0.00	0.00	1494.57	.0498	STRAIGHT PIPE
84	10	474.68	1014.93	0.00	0.00	0.00	1494.61	.0498	STRAIGHT PIPE
	11	474.68	2544.13	0.00	0.00	0.00	3024.81	.1010	STRAIGHT PIPE
94	12	474.68	3405.22	0.00	0.00	0.00	3879.90	.1293	STRAIGHT PIPE
	13	474.68	4044.05	0.00	0.00	0.00	5419.74	.1807	BUTT WELD, AS WELDED
104	13	474.68	4044.05	0.00	0.00	0.00	5419.74	.1807	BUTT WELD, AS WELDED
	14	474.68	4044.05	0.00	0.00	0.00	5419.74	.1807	BUTT WELD, AS WELDED
114	14	474.68	4044.05	0.00	0.00	0.00	5419.74	.1807	BUTT WELD, AS WELDED
	15	474.68	3147.82	0.00	0.00	0.00	3642.50	.1214	STRAIGHT PIPE
124	15	474.68	3147.82	0.00	0.00	0.00	3642.50	.1214	STRAIGHT PIPE
	16	474.68	1404.00	0.00	0.00	0.00	2172.77	.0724	STRAIGHT PIPE
134	16	474.68	1404.00	0.00	0.00	0.00	2172.77	.0724	STRAIGHT PIPE
	17	474.68	747.33	0.00	0.00	0.00	1277.01	.0412	STRAIGHT PIPE
144	17	474.68	747.33	0.00	0.00	0.00	1277.01	.0412	STRAIGHT PIPE
	18	949.37	1729.82	0.00	0.00	0.00	2679.19	.0893	WELDING TEE
154	18	949.37	1729.82	0.00	0.00	0.00	2679.19	.0893	WELDING TEE
	19	474.68	214.31	0.00	0.00	0.00	320.00	.0431	STRAIGHT PIPE
164	19	474.68	214.31	0.00	0.00	0.00	320.00	.0431	STRAIGHT PIPE
	20	949.37	1729.82	0.00	0.00	0.00	2679.19	.0893	WELDING TEE
174	20	949.37	1729.82	0.00	0.00	0.00	2679.19	.0893	WELDING TEE
	21	474.68	306.54	0.00	0.00	0.00	412.41	.0260	STRAIGHT PIPE
184	21	474.68	306.54	0.00	0.00	0.00	412.41	.0260	STRAIGHT PIPE
	22	474.68	174.41	0.00	0.00	0.00	633.30	.0211	STRAIGHT PIPE
194	22	474.68	174.41	0.00	0.00	0.00	633.30	.0211	STRAIGHT PIPE
	23	474.68	425.41	0.00	0.00	0.00	1300.00	.0433	STRAIGHT PIPE
204	23	474.68	425.41	0.00	0.00	0.00	1300.00	.0433	STRAIGHT PIPE
	24	474.68	277.43	0.00	0.00	0.00	752.31	.0251	STRAIGHT PIPE
214	24	474.68	277.43	0.00	0.00	0.00	752.31	.0251	STRAIGHT PIPE
	25	474.68	134.19	0.00	0.00	0.00	612.88	.0204	STRAIGHT PIPE
224	25	474.68	134.19	0.00	0.00	0.00	612.88	.0204	STRAIGHT PIPE
	26	474.68	130.58	0.00	0.00	0.00	548.66	.0182	STRAIGHT PIPE
234	26	474.68	130.58	0.00	0.00	0.00	548.66	.0182	STRAIGHT PIPE
	27	474.68	14.78	0.00	0.00	0.00	404.44	.0145	BUTT WELD, AS WELDED

224	27	474.68	19.78	0.00	0.00	0.00	494.46	.0165	BUTT WELD, AS WELDED
	28	474.68	111.14	0.00	0.00	0.00	585.43	.0195	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (OT)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
1C	1	1183.04	4916.84	0.00	0.00	0.00	10093.88	.3265	CURVED PIPE
	2	1183.04	4344.48	0.00	0.00	0.00	9547.51	.3183	CURVED PIPE
2C	8	949.37	1074.15	0.00	0.00	0.00	4928.51	.1643	CURVED PIPE
	9	949.37	2540.41	0.00	0.00	0.00	3529.77	.1177	CURVED PIPE
3C	11	949.37	3624.45	0.00	0.00	0.00	4574.82	.1525	CURVED PIPE
	12	949.37	4317.95	0.00	0.00	0.00	5287.32	.1762	CURVED PIPE
4C	20	949.37	241.02	0.00	0.00	0.00	1230.30	.0410	CURVED PIPE
	21	949.37	434.24	0.00	0.00	0.00	1384.61	.0462	CURVED PIPE
5C	25	949.37	105.03	0.00	0.00	0.00	1054.40	.0351	CURVED PIPE
	26	949.37	142.80	0.00	0.00	0.00	1092.17	.0364	CURVED PIPE

STRESSES FOR EQUATION 8  
LOAD SET 2 = LOAD COMBINATION 2

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (RF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5FSM	CLASS 1 COMMENT / DESCRIPTION
19	2	474.68	4874.94	0.00	0.00	0.00	5311.62	.1721	TAPERED TRANS. JOINT
	3	474.68	3904.34	0.00	0.00	0.00	4383.02	.1461	STRAIGHT PIPE
25	3	474.68	3904.33	0.00	0.00	0.00	4383.01	.1461	STRAIGHT PIPE
	4	474.68	2677.69	0.00	0.00	0.00	3147.34	.1049	STRAIGHT PIPE
31	4	474.68	2677.68	0.00	0.00	0.00	3147.34	.1049	STRAIGHT PIPE
	5	474.68	1424.18	0.00	0.00	0.00	1898.87	.0633	STRAIGHT PIPE
49	5	474.68	1424.19	0.00	0.00	0.00	1898.88	.0633	STRAIGHT PIPE
	6	474.68	1871.64	0.00	0.00	0.00	2296.34	.0765	STRAIGHT PIPE
54	6	474.68	1871.67	0.00	0.00	0.00	2296.36	.0765	STRAIGHT PIPE
	7	474.68	8473.07	0.00	0.00	0.00	2947.75	.0983	BUTT WELD, AS WELDED
62	7	474.68	2473.07	0.00	0.00	0.00	2947.75	.0983	BUTT WELD, AS WELDED
	8	474.68	2270.28	0.00	0.00	0.00	2744.54	.0915	STRAIGHT PIPE
74	8	474.68	1644.15	0.00	0.00	0.00	1942.84	.0648	STRAIGHT PIPE
	10	474.68	466.73	0.00	0.00	0.00	1321.62	.0441	STRAIGHT PIPE
84	10	474.68	466.94	0.00	0.00	0.00	1321.64	.0441	STRAIGHT PIPE
	11	474.68	2104.90	0.00	0.00	0.00	2541.58	.0861	STRAIGHT PIPE
95	12	474.68	2874.31	0.00	0.00	0.00	3301.59	.1101	STRAIGHT PIPE
	13	474.68	4073.04	0.00	0.00	0.00	4474.74	.1492	BUTT WELD, AS WELDED
109	13	474.68	4073.05	0.00	0.00	0.00	4474.74	.1492	BUTT WELD, AS WELDED
	14	474.68	4524.59	0.00	0.00	0.00	7003.28	.2334	STRAIGHT PIPE
115	14	474.68	4524.59	0.00	0.00	0.00	7003.28	.2334	STRAIGHT PIPE
	15	474.68	2074.63	0.00	0.00	0.00	3051.32	.1012	STRAIGHT PIPE
124	15	474.68	2574.63	0.00	0.00	0.00	3051.32	.1012	STRAIGHT PIPE
	16	474.68	1394.24	0.00	0.00	0.00	1870.95	.0624	STRAIGHT PIPE
134	16	474.68	1394.24	0.00	0.00	0.00	1870.95	.0624	STRAIGHT PIPE
	17	474.68	614.84	0.00	0.00	0.00	1094.57	.0365	STRAIGHT PIPE
144	17	474.68	607.79	0.00	0.00	0.00	1092.48	.0361	STRAIGHT PIPE
	18	949.37	1749.92	0.00	0.00	0.00	2659.20	.0886	WELDING-TEE
154	18	949.37	1749.92	0.00	0.00	0.00	2659.20	.0886	WELDING-TEE
	19	474.68	743.81	0.00	0.00	0.00	1214.44	.0406	STRAIGHT PIPE
164	19	474.68	743.81	0.00	0.00	0.00	1214.44	.0406	STRAIGHT PIPE
	20	474.68	191.97	0.00	0.00	0.00	484.64	.0162	STRAIGHT PIPE
175	21	474.68	305.67	0.00	0.00	0.00	740.35	.0246	STRAIGHT PIPE
	22	474.68	154.44	0.00	0.00	0.00	433.12	.0144	STRAIGHT PIPE
185	22	474.68	154.44	0.00	0.00	0.00	433.12	.0144	STRAIGHT PIPE
	23	474.68	824.70	0.00	0.00	0.00	1301.38	.0434	STRAIGHT PIPE
194	23	474.68	824.70	0.00	0.00	0.00	1301.38	.0434	STRAIGHT PIPE
	24	474.68	134.19	0.00	0.00	0.00	612.84	.0204	STRAIGHT PIPE
204	24	474.68	134.19	0.00	0.00	0.00	612.84	.0204	STRAIGHT PIPE
	25	474.68	73.98	0.00	0.00	0.00	548.44	.0183	STRAIGHT PIPE
215	25	474.68	73.98	0.00	0.00	0.00	548.44	.0183	STRAIGHT PIPE
	26	474.68	100.58	0.00	0.00	0.00	375.26	.0125	STRAIGHT PIPE
225	26	474.68	100.58	0.00	0.00	0.00	375.26	.0125	STRAIGHT PIPE
	27	474.68	19.74	0.00	0.00	0.00	494.44	.0165	BUTT WELD, AS WELDED
234	27	474.68	19.74	0.00	0.00	0.00	494.44	.0165	BUTT WELD, AS WELDED
	28	474.68	111.14	0.00	0.00	0.00	545.83	.0185	STRAIGHT PIPE
244	28	474.68	111.14	0.00	0.00	0.00	545.83	.0185	STRAIGHT PIPE

PIPESD

224	27	474.68	19.74	0.00	0.00	0.00	494.44	.0165	BUTT WELD, AS WELDED
	28	474.68	111.14	0.00	0.00	0.00	545.83	.0185	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (RF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5FSM	CLASS 1 COMMENT / DESCRIPTION
16	1	1143.04	7143.03	0.00	0.00	0.00	8346.11	.2749	CURVED PIPE
	2	1143.04	4740.81	0.00	0.00	0.00	7423.45	.2441	CURVED PIPE
2c	4	949.37	3773.42	0.00	0.00	0.00	4172.79	.1391	CURVED PIPE
	5	949.37	2084.56	0.00	0.00	0.00	3033.93	.1011	CURVED PIPE
3c	11	949.37	2981.48	0.00	0.00	0.00	3940.82	.1314	CURVED PIPE
	12	949.37	3547.09	0.00	0.00	0.00	4496.46	.1499	CURVED PIPE
4c	20	949.37	2744.41	0.00	0.00	0.00	3274.78	.1068	CURVED PIPE
	21	949.37	434.00	0.00	0.00	0.00	1383.36	.0461	CURVED PIPE
5c	23	949.37	105.03	0.00	0.00	0.00	1054.40	.0351	CURVED PIPE
	24	949.37	142.00	0.00	0.00	0.00	1092.17	.0364	CURVED PIPE















SEISMIC AND STRESS ANALYSIS OF FACE SUCTION LINE 1 LUBBER

STRESSCS FOR EQUATION 11 & EQUATION 1A  
LOAD SET 2 \* LOAD COMBINATION 5

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	MEMBRANE STRESS (PS)	THERMAL DISCONT. STRESS (QT)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 1A (SA)	CLASS 1 COMPONENT / DESCRIPTION
14	2	398.73	1088.26	0.00	0.00	0.00	11279.88	6439.58	FABRICATION JOINT
	3	189.87	4090.64	0.00	0.00	0.00	4280.51	2140.26	STRAIGHT PIPE
24	3	189.87	4090.64	0.00	0.00	0.00	4780.53	2140.27	STRAIGHT PIPE
	4	189.87	2947.32	0.00	0.00	0.00	3157.14	1578.59	STRAIGHT PIPE
34	4	189.87	2947.32	0.00	0.00	0.00	3157.20	1578.60	STRAIGHT PIPE
	5	189.87	1894.95	0.00	0.00	0.00	2074.42	1037.21	STRAIGHT PIPE
44	5	189.87	1894.95	0.00	0.00	0.00	2074.54	1037.22	STRAIGHT PIPE
	6	189.87	3789.92	0.00	0.00	0.00	3586.69	1793.35	STRAIGHT PIPE
54	6	189.87	3789.92	0.00	0.00	0.00	3586.65	1793.33	STRAIGHT PIPE
	7	250.63	4484.03	0.00	0.00	0.00	4906.70	2453.35	BUTT WELD, AS WELDED
64	7	250.63	4484.07	0.00	0.00	0.00	4906.70	2453.35	BUTT WELD, AS WELDED
	8	189.87	1902.80	0.00	0.00	0.00	4182.67	2091.24	STRAIGHT PIPE
74	8	189.87	1712.67	0.00	0.00	0.00	3787.55	1891.27	STRAIGHT PIPE
	10	189.87	2554.24	0.00	0.00	0.00	2748.11	1374.06	STRAIGHT PIPE
84	10	189.87	2554.24	0.00	0.00	0.00	2748.73	1374.36	STRAIGHT PIPE
	11	189.87	2404.91	0.00	0.00	0.00	2598.45	1299.42	STRAIGHT PIPE
94	11	189.87	2794.67	0.00	0.00	0.00	3184.54	1592.27	STRAIGHT PIPE
	13	250.63	4477.18	0.00	0.00	0.00	4927.82	2443.91	BUTT WELD, AS WELDED
104	13	250.63	4477.18	0.00	0.00	0.00	4927.82	2443.91	BUTT WELD, AS WELDED
	14	189.87	3045.54	0.00	0.00	0.00	4235.52	2117.76	STRAIGHT PIPE
114	14	189.87	3045.54	0.00	0.00	0.00	4235.52	2117.76	STRAIGHT PIPE
	15	189.87	3284.94	0.00	0.00	0.00	3658.81	1829.41	STRAIGHT PIPE
124	15	189.87	3284.94	0.00	0.00	0.00	3658.81	1829.41	STRAIGHT PIPE
	16	189.87	2644.32	0.00	0.00	0.00	2834.14	1414.10	STRAIGHT PIPE
134	16	189.87	2644.32	0.00	0.00	0.00	2834.14	1414.10	STRAIGHT PIPE
	17	189.87	2714.68	0.00	0.00	0.00	2404.56	1202.28	STRAIGHT PIPE
144	17	189.87	2714.68	0.00	0.00	0.00	2525.45	1262.73	STRAIGHT PIPE
	18	1170.24	36074.56	0.00	0.00	0.00	36147.80	18073.90	WELDING TEE
154	18	1170.24	36074.56	0.00	0.00	0.00	36147.80	18073.90	WELDING TEE
	19	189.87	4337.83	0.00	0.00	0.00	4927.70	2463.85	STRAIGHT PIPE
164	19	189.87	4337.83	0.00	0.00	0.00	4927.70	2463.85	STRAIGHT PIPE
	20	189.87	1845.36	0.00	0.00	0.00	2035.23	1017.61	STRAIGHT PIPE
174	20	189.87	1845.36	0.00	0.00	0.00	2035.23	1017.61	STRAIGHT PIPE
	21	189.87	3272.48	0.00	0.00	0.00	3567.35	1783.17	STRAIGHT PIPE
184	21	189.87	3272.48	0.00	0.00	0.00	3567.35	1783.17	STRAIGHT PIPE
	22	189.87	1433.71	0.00	0.00	0.00	1623.59	811.79	STRAIGHT PIPE
194	22	189.87	1433.71	0.00	0.00	0.00	1623.59	811.79	STRAIGHT PIPE
	23	189.87	1394.85	0.00	0.00	0.00	1584.72	792.36	STRAIGHT PIPE
204	23	189.87	1394.85	0.00	0.00	0.00	1584.72	792.36	STRAIGHT PIPE
	24	189.87	2374.52	0.00	0.00	0.00	2545.39	1272.70	STRAIGHT PIPE
214	24	189.87	2374.52	0.00	0.00	0.00	2545.39	1272.70	STRAIGHT PIPE
	25	189.87	340.75	0.00	0.00	0.00	550.82	275.41	STRAIGHT PIPE
224	25	189.87	340.75	0.00	0.00	0.00	550.82	275.41	STRAIGHT PIPE
	26	189.87	340.75	0.00	0.00	0.00	550.82	275.41	STRAIGHT PIPE
234	26	189.87	340.75	0.00	0.00	0.00	550.82	275.41	STRAIGHT PIPE
	27	250.63	4477.85	0.00	0.00	0.00	4931.47	2465.74	BUTT WELD, AS WELDED
244	27	250.63	4477.85	0.00	0.00	0.00	4931.47	2465.74	BUTT WELD, AS WELDED

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (QT)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 1A (SA)	CLASS 1 COMPONENT / DESCRIPTION
17	1	341.91	9914.53	0.00	0.00	0.00	10219.55	5109.77	CURVED PIPE
	2	341.91	9349.79	0.00	0.00	0.00	9660.80	4830.40	CURVED PIPE
27	4	201.17	7444.35	0.00	0.00	0.00	7749.52	3874.76	CURVED PIPE
	9	201.17	7094.49	0.00	0.00	0.00	7230.62	3615.01	CURVED PIPE
37	11	201.17	4544.47	0.00	0.00	0.00	4761.64	2380.82	CURVED PIPE
	12	201.17	4030.12	0.00	0.00	0.00	4201.29	2100.65	CURVED PIPE
47	20	201.17	3404.48	0.00	0.00	0.00	3694.45	1847.33	CURVED PIPE
	21	201.17	4394.50	0.00	0.00	0.00	4550.57	2275.28	CURVED PIPE
57	25	201.17	3244.72	0.00	0.00	0.00	3445.89	1722.95	CURVED PIPE
	26	201.17	3644.95	0.00	0.00	0.00	3939.11	1969.56	CURVED PIPE



B. CLASS 1 COMPONENT STRESS ANALYSIS

TABLE B-111-2

B.1 STRESS INDICES

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE			MOMENT LOADING			THERMAL LOADING			TEE MOMENTS						STRESS INDEX DESCRIPTION
		R1	C1	K1	R2	C2	K2	C3	K3	C3P	B2R	B2C	C2R	C2C	K2R	K2C	
1A	19	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
2A	29	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
3A	30	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
4A	31	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
5A	32	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
6A	33	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
7A	34	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
8A	35	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
9A	36	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
10A	37	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
4A	44	1.00	1.50	4.00	0.00	0.00	1.00	1.00	1.00	.50	1.94	1.94	2.59	2.59	1.00	1.00	WELDING TEE

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE			MOMENT LOADING			THERMAL LOADING			TEE MOMENTS						STRESS INDEX DESCRIPTION
		R1	C1	K1	R2	C2	K2	C3	K3	C3P	B2R	B2C	C2R	C2C	K2R	K2C	
1C	33	1.00	1.05	1.00	1.15	1.53	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
2C	36	1.00	1.08	1.00	1.50	2.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
3C	37	1.00	1.08	1.00	1.50	2.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE			MOMENT LOADING			THERMAL LOADING			TEE MOMENTS						STRESS INDEX DESCRIPTION
		R1	C1	K1	R2	C2	K2	C3	K3	C3P	B2R	B2C	C2R	C2C	K2R	K2C	
11A	40	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
12A	41	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
13A	42	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
14A	43	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
15A	44	1.00	1.50	4.00	0.00	0.00	1.00	1.00	1.00	.50	1.94	1.94	2.59	2.59	1.00	1.00	WELDING TEE
16A	45	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
17A	46	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
18A	47	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
19A	48	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
20A	49	1.00	1.50	4.00	0.00	0.00	1.00	1.00	1.00	.50	1.94	1.94	2.59	2.59	1.00	1.00	WELDING TEE
21A	50	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE			MOMENT LOADING			THERMAL LOADING			TEE MOMENTS						STRESS INDEX DESCRIPTION
		R1	C1	K1	R2	C2	K2	C3	K3	C3P	B2R	B2C	C2R	C2C	K2R	K2C	
3C	41	1.00	1.05	1.00	1.15	1.53	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
4C	46	1.00	1.08	1.00	1.50	2.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
5C	47	1.00	1.08	1.00	1.50	2.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE



CURVED MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE			MOMENT LOADING			THERMAL LOADING			TEE MOMENTS						STRESS INDEX DESCRIPTION	
		R1	C1	K1	R2	C2	K2	R3	K3	C3P	B2R	B2B	C2R	C2B	K2R	K2B		
13C	80	1.00	1.11	1.00	1.82	2.43	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
	81	1.00	1.11	1.00	1.82	2.43	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
14C	83	1.00	1.21	1.00	2.52	3.26	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
	84	1.00	1.21	1.00	2.52	3.26	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
15C	85	1.00	1.06	1.00	1.29	1.73	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
	86	1.00	1.06	1.00	1.29	1.73	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
16C	88	1.00	1.21	1.00	2.14	2.85	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
	89	1.00	1.21	1.00	2.14	2.85	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
17C	91	1.00	1.21	1.00	2.14	2.85	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
	92	1.00	1.21	1.00	2.14	2.85	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 5

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE			MOMENT LOADING			THERMAL LOADING			TEE MOMENTS						STRESS INDEX DESCRIPTION	
		R1	C1	K1	R2	C2	K2	R3	K3	C3P	B2R	B2B	C2R	C2B	K2R	K2B		
45A	87	1.00	1.50	1.00	0.00	0.00	1.00	1.00	1.00	1.00	.50	1.94	1.94	2.59	2.59	1.00	1.00	WELDING TEE
	88	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
46A	95	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
	96	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
47A	97	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
	98	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 5

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE			MOMENT LOADING			THERMAL LOADING			TEE MOMENTS						STRESS INDEX DESCRIPTION	
		R1	C1	K1	R2	C2	K2	R3	K3	C3P	B2R	B2B	C2R	C2B	K2R	K2B		
18C	95	1.00	1.21	1.00	2.14	2.85	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
	96	1.00	1.21	1.00	2.14	2.85	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF EGGS SUCTION LINE 2 LACRVR

STRAIGHT MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE			MOMENT LOADING			THERMAL LOADING			TEE MOMENTS						STRESS INDEX DESCRIPTION	
		R1	C1	K1	R2	C2	K2	R3	K3	C3P	B2R	B2B	C2R	C2B	K2R	K2B		
48A	74	1.00	1.50	1.00	0.00	0.00	1.00	1.00	1.00	1.00	.50	1.94	1.94	2.59	2.59	1.00	1.00	WELDING TEE
	75	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
49A	76	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
	77	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
50A	78	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE
	79	.50	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE			MOMENT LOADING			THERMAL LOADING			TEE MOMENTS						STRESS INDEX DESCRIPTION	
		R1	C1	K1	R2	C2	K2	R3	K3	C3P	B2R	B2B	C2R	C2B	K2R	K2B		
19C	74	1.00	1.11	1.00	1.81	2.42	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
	75	1.00	1.11	1.00	1.81	2.42	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
20C	77	1.00	1.11	1.00	1.82	2.43	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE
	78	1.00	1.11	1.00	1.82	2.43	1.00	1.00	1.00	1.00	.50	0.00	0.00	0.00	0.00	0.00	0.00	CURVED PIPE



SEISMIC AND STRESS ANALYSIS OF EGGS SUCTION LINE 2 - LACROW

B.1 CONSIDERATION OF EQUATION 9

STRESSES FOR EQUATION 9  
LOAD SET 1 - LOAD COMBINATION 2

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS I COMPONENT /-----DESCRIPTION-----/
15	19	405.09	393.17	0.00	0.00	0.00	798.26	.0266	STRAIGHT PIPE
	20	405.09	373.54	0.00	0.00	0.00	778.63	.0253	STRAIGHT PIPE
25	29	405.09	373.54	0.00	0.00	0.00	778.63	.0253	STRAIGHT PIPE
	30	405.09	472.47	0.00	0.00	0.00	877.56	.0269	STRAIGHT PIPE
35	39	405.09	472.47	0.00	0.00	0.00	877.56	.0269	STRAIGHT PIPE
45	49	405.09	573.28	0.00	0.00	0.00	976.31	.0329	STRAIGHT PIPE
	50	405.09	573.28	0.00	0.00	0.00	976.31	.0329	STRAIGHT PIPE
55	59	405.09	674.01	0.00	0.00	0.00	1075.10	.0455	STRAIGHT PIPE
	60	405.09	674.01	0.00	0.00	0.00	1075.10	.0455	STRAIGHT PIPE
65	69	405.09	774.74	0.00	0.00	0.00	1173.83	.0500	STRAIGHT PIPE
	70	405.09	774.74	0.00	0.00	0.00	1173.83	.0500	STRAIGHT PIPE
75	79	405.09	875.47	0.00	0.00	0.00	1272.56	.0545	STRAIGHT PIPE
	80	405.09	875.47	0.00	0.00	0.00	1272.56	.0545	STRAIGHT PIPE
85	89	405.09	976.20	0.00	0.00	0.00	1371.29	.0612	STRAIGHT PIPE
	90	405.09	976.20	0.00	0.00	0.00	1371.29	.0612	STRAIGHT PIPE
95	99	405.09	1076.93	0.00	0.00	0.00	1470.02	.0667	STRAIGHT PIPE
	100	405.09	1076.93	0.00	0.00	0.00	1470.02	.0667	STRAIGHT PIPE
105	109	405.09	1177.66	0.00	0.00	0.00	1568.75	.0722	STRAIGHT PIPE
	110	810.19	1177.66	0.00	0.00	0.00	2653.70	.0885	WELDING TEE

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS I COMPONENT /-----DESCRIPTION-----/
11	31	810.19	809.72	0.00	0.00	0.00	1619.91	.0540	CURVED PIPE
	34	810.19	647.07	0.00	0.00	0.00	1457.26	.0449	CURVED PIPE
21	36	810.19	1747.98	0.00	0.00	0.00	2558.15	.0788	CURVED PIPE
	37	810.19	1322.68	0.00	0.00	0.00	2132.86	.0671	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF EGGS SUCTION LINE 2 - LACROW

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS I COMPONENT /-----DESCRIPTION-----/
114	40	405.09	1114.42	0.00	0.00	0.00	1519.51	.0507	STRAIGHT PIPE
	41	405.09	744.56	0.00	0.00	0.00	1149.65	.0371	STRAIGHT PIPE
124	42	405.09	713.56	0.00	0.00	0.00	1118.64	.0373	STRAIGHT PIPE
	43	405.09	1702.40	0.00	0.00	0.00	2405.50	.0748	STRAIGHT PIPE
134	44	405.09	1302.40	0.00	0.00	0.00	1705.50	.0518	STRAIGHT PIPE
	45	810.19	1843.51	0.00	0.00	0.00	2653.70	.0885	WELDING TEE
144	46	810.19	1843.51	0.00	0.00	0.00	2653.70	.0885	WELDING TEE
	47	405.09	1179.40	0.00	0.00	0.00	1558.84	.0519	STRAIGHT PIPE
154	48	405.09	1179.40	0.00	0.00	0.00	1558.84	.0519	STRAIGHT PIPE
	49	405.09	1444.11	0.00	0.00	0.00	1849.20	.0578	STRAIGHT PIPE
164	50	405.09	1444.11	0.00	0.00	0.00	1849.20	.0578	STRAIGHT PIPE
	51	405.09	1139.40	0.00	0.00	0.00	1444.11	.0455	STRAIGHT PIPE
174	52	405.09	1139.40	0.00	0.00	0.00	1444.11	.0455	STRAIGHT PIPE
	53	810.19	1724.41	0.00	0.00	0.00	2444.51	.0748	WELDING TEE
184	54	810.19	1724.41	0.00	0.00	0.00	2444.51	.0748	WELDING TEE
	55	405.09	3444.30	0.00	0.00	0.00	4249.39	.1410	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS I COMPONENT /-----DESCRIPTION-----/
31	41	810.19	872.51	0.00	0.00	0.00	1682.70	.0514	CURVED PIPE
	42	810.19	817.44	0.00	0.00	0.00	1627.63	.0493	CURVED PIPE
41	46	810.19	1712.75	0.00	0.00	0.00	2520.94	.0763	CURVED PIPE
	47	810.19	734.35	0.00	0.00	0.00	1544.55	.0515	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF ECCS SUCTION LINE 2 - LACRU

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (QT)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SB)	RATIO SB / 1.5*SM	CLASS 1 COMPONENT	DESCRIPTION
194	49	810.19	4893.80	0.00	0.00	0.00	5703.99	1.901	WELDING TEE	
	51	405.09	1484.31	0.00	0.00	0.00	1873.40	0.631	STRAIGHT PIPE	
204	50	405.09	1471.74	0.00	0.00	0.00	1874.87	0.640	STRAIGHT PIPE	
	53	405.09	2943.82	0.00	0.00	0.00	3344.91	1.123	STRAIGHT PIPE	
214	53	405.09	2943.82	0.00	0.00	0.00	3344.91	1.123	STRAIGHT PIPE	
	54	405.09	1484.31	0.00	0.00	0.00	1874.87	0.640	STRAIGHT PIPE	
224	55	405.09	2054.14	0.00	0.00	0.00	2443.73	0.821	STRAIGHT PIPE	
	54	405.09	1345.41	0.00	0.00	0.00	1770.50	0.590	STRAIGHT PIPE	
234	57	405.09	1717.00	0.00	0.00	0.00	1817.09	0.610	STRAIGHT PIPE	
	58	405.09	3084.50	0.00	0.00	0.00	3409.49	1.137	STRAIGHT PIPE	
244	54	405.09	1004.60	0.00	0.00	0.00	1409.69	0.470	STRAIGHT PIPE	
	59	405.09	2782.03	0.00	0.00	0.00	2947.72	0.980	STRAIGHT PIPE	
254	60	405.09	2394.24	0.00	0.00	0.00	2603.35	0.874	STRAIGHT PIPE	
	61	405.09	2554.39	0.00	0.00	0.00	2963.44	0.988	STRAIGHT PIPE	
264	62	405.09	2474.26	0.00	0.00	0.00	2679.36	0.903	STRAIGHT PIPE	
	63	405.09	2417.47	0.00	0.00	0.00	2422.57	0.814	STRAIGHT PIPE	
274	63	405.09	2417.47	0.00	0.00	0.00	2622.57	0.881	STRAIGHT PIPE	
	64	405.09	1714.01	0.00	0.00	0.00	2141.10	0.714	STRAIGHT PIPE	
284	65	405.09	1574.75	0.00	0.00	0.00	1983.34	0.661	STRAIGHT PIPE	
	64	405.09	1497.29	0.00	0.00	0.00	1907.78	0.647	STRAIGHT PIPE	
294	67	405.09	2917.79	0.00	0.00	0.00	3217.88	1.064	STRAIGHT PIPE	
	68	405.09	3389.03	0.00	0.00	0.00	3794.12	1.265	STRAIGHT PIPE	
304	69	405.09	2479.34	0.00	0.00	0.00	2884.43	0.961	STRAIGHT PIPE	
	70	810.19	6147.87	0.00	0.00	0.00	6974.05	2.326	WELDING TEE	
314	70	810.19	6147.87	0.00	0.00	0.00	6974.05	2.326	WELDING TEE	
	71	405.09	3777.75	0.00	0.00	0.00	4164.45	1.388	STRAIGHT PIPE	
324	71	405.09	3777.75	0.00	0.00	0.00	4164.45	1.388	STRAIGHT PIPE	
	72	405.09	2024.50	0.00	0.00	0.00	2429.59	0.810	STRAIGHT PIPE	
334	72	405.09	1587.64	0.00	0.00	0.00	2392.73	0.798	STRAIGHT PIPE	
	73	810.19	1484.31	0.00	0.00	0.00	1674.40	0.563	WELDING TEE	
344	73	810.19	1484.31	0.00	0.00	0.00	1674.40	0.563	WELDING TEE	
	82	810.19	4073.34	0.00	0.00	0.00	4883.52	1.628	WELDING TEE	

CURVED MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (QT)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SB)	RATIO SB / 1.5*SM	CLASS 1 COMPONENT	DESCRIPTION
5c	51	810.19	4711.67	0.00	0.00	0.00	4091.84	1.363	CURVED PIPE	
	52	810.19	3031.67	0.00	0.00	0.00	3491.84	1.161	CURVED PIPE	
6c	54	810.19	2754.65	0.00	0.00	0.00	3376.84	1.126	CURVED PIPE	
	55	810.19	2447.84	0.00	0.00	0.00	2433.02	0.814	CURVED PIPE	
7c	54	810.19	1764.57	0.00	0.00	0.00	2574.74	0.859	CURVED PIPE	
	57	810.19	1544.10	0.00	0.00	0.00	2378.28	0.793	CURVED PIPE	

8c	59	810.19	2404.27	0.00	0.00	0.00	3218.44	1.073	CURVED PIPE	
	60	810.19	2574.79	0.00	0.00	0.00	3385.94	1.129	CURVED PIPE	
9c	61	810.19	1044.43	0.00	0.00	0.00	1474.46	0.491	CURVED PIPE	
	62	810.19	4322.50	0.00	0.00	0.00	4874.46	1.628	CURVED PIPE	
10c	64	810.19	2244.04	0.00	0.00	0.00	3137.44	1.031	CURVED PIPE	
	65	810.19	2044.94	0.00	0.00	0.00	3054.24	1.019	CURVED PIPE	
11c	64	810.19	7121.87	0.00	0.00	0.00	2652.14	0.881	CURVED PIPE	
	67	810.19	3773.45	0.00	0.00	0.00	7932.05	2.644	CURVED PIPE	
12c	64	810.19	4079.26	0.00	0.00	0.00	4543.43	1.528	CURVED PIPE	
	69	810.19	5910.60	0.00	0.00	0.00	6909.43	2.303	CURVED PIPE	
							6729.79	2.240	CURVED PIPE	

STRAIGHT MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (QT)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SB)	RATIO SB / 1.5*SM	CLASS 1 COMPONENT	DESCRIPTION
354	79	405.09	1501.81	0.00	0.00	0.00	1906.90	0.636	STRAIGHT PIPE	
	80	405.09	814.12	0.00	0.00	0.00	1244.22	0.415	STRAIGHT PIPE	
364	81	405.09	733.34	0.00	0.00	0.00	1144.43	0.381	STRAIGHT PIPE	
	82	810.19	4073.34	0.00	0.00	0.00	4883.52	1.628	WELDING TEE	
374	83	405.09	417.31	0.00	0.00	0.00	823.00	0.274	STRAIGHT PIPE	
	84	405.09	437.73	0.00	0.00	0.00	842.82	0.281	STRAIGHT PIPE	
384	84	405.09	444.09	0.00	0.00	0.00	849.18	0.285	STRAIGHT PIPE	
	87	405.09	491.40	0.00	0.00	0.00	904.50	0.303	STRAIGHT PIPE	
404	83	405.09	5281.99	0.00	0.00	0.00	6092.17	2.031	STRAIGHT PIPE	
	88	810.19	4281.99	0.00	0.00	0.00	4302.17	1.431	WELDING TEE	
414	88	405.09	163.77	0.00	0.00	0.00	544.85	0.185	STRAIGHT PIPE	
	89	327.59	817.73	0.00	0.00	0.00	1140.71	0.380	STRAIGHT PIPE	
424	90	327.59	244.04	0.00	0.00	0.00	591.42	0.197	STRAIGHT PIPE	
	91	327.59	314.73	0.00	0.00	0.00	643.32	0.214	STRAIGHT PIPE	
434	92	327.59	271.31	0.00	0.00	0.00	544.41	0.182	STRAIGHT PIPE	
	93	327.59	299.21	0.00	0.00	0.00	625.79	0.209	STRAIGHT PIPE	
444	93	327.59	1041.75	0.00	0.00	0.00	1309.34	0.443	STRAIGHT PIPE	
	94	327.59	1041.75	0.00	0.00	0.00	1309.34	0.443	STRAIGHT PIPE	
							928.49	0.309	STRAIGHT PIPE	

CURVED MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (QT)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SB)	RATIO SB / 1.5*SM	CLASS 1 COMPONENT	DESCRIPTION
13c	80	810.19	1524.40	0.00	0.00	0.00	2336.40	0.779	CURVED PIPE	
	81	810.19	1044.43	0.00	0.00	0.00	2144.43	0.712	CURVED PIPE	
14c	81	810.19	1044.43	0.00	0.00	0.00	2077.10	0.692	CURVED PIPE	
	84	810.19	1344.21	0.00	0.00	0.00	2144.19	0.715	CURVED PIPE	
15c	84	810.19	1444.21	0.00	0.00	0.00	1434.50	0.479	CURVED PIPE	
	89	810.19	744.21	0.00	0.00	0.00	1074.92	0.358	CURVED PIPE	
16c	89	810.19	744.21	0.00	0.00	0.00	1074.92	0.358	CURVED PIPE	
	91	810.19	1044.43	0.00	0.00	0.00	1394.44	0.464	CURVED PIPE	

DISPER AND STRESS ANALYSIS OF PC6 SUCTION LINE 2 - LACR2

STRAIGHT MEMBERS FOR RUN 5

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
45A	87	655.17	5241.99	0.00	0.00	0.00	5937.16	.1979	WELDING TEE
	95	327.59	1943.36	0.00	0.00	0.00	2290.94	.0744	STRAIGHT PIPE
46A	96	327.59	1802.12	0.00	0.00	0.00	1727.72	.0576	STRAIGHT PIPE
	97	327.59	1834.66	0.00	0.00	0.00	2166.25	.0722	STRAIGHT PIPE
47A	97	327.59	1834.66	0.00	0.00	0.00	2166.25	.0722	STRAIGHT PIPE
	98	327.59	2162.84	0.00	0.00	0.00	2489.43	.0825	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 5

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
18C	95	655.17	4207.56	0.00	0.00	0.00	4857.74	.1619	CURVED PIPE
	96	655.17	2496.98	0.00	0.00	0.00	3052.16	.1217	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
48A	73	810.19	1848.36	0.00	0.00	0.00	2678.49	.0893	WELDING TEE
	74	405.09	346.29	0.00	0.00	0.00	771.38	.0257	STRAIGHT PIPE
	75	405.09	443.72	0.00	0.00	0.00	848.81	.0283	STRAIGHT PIPE
50A	76	405.09	540.09	0.00	0.00	0.00	945.18	.0315	STRAIGHT PIPE
	76	405.09	540.33	0.00	0.00	0.00	945.42	.0315	STRAIGHT PIPE
	77	405.09	775.95	0.00	0.00	0.00	1181.05	.0394	STRAIGHT PIPE
51A	77	405.09	1044.56	0.00	0.00	0.00	1466.64	.0489	STRAIGHT PIPE
	78	810.19	6167.87	0.00	0.00	0.00	6978.05	.2326	WELDING TEE

CURVED MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
19C	74	810.19	443.56	0.00	0.00	0.00	1473.74	.0491	CURVED PIPE
	75	810.19	404.24	0.00	0.00	0.00	1214.43	.0438	CURVED PIPE
20C	77	810.19	1411.49	0.00	0.00	0.00	2221.68	.0741	CURVED PIPE
	78	810.19	1931.01	0.00	0.00	0.00	2741.19	.0914	CURVED PIPE

SECTION AND STRESS ANALYSIS OF EGGS SUCTION LINE 2 - LACWR

STRESSES FOR EQUATION 9  
LOAD SET 2 \* LOAD COMBINATION 2

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (PS)	RATIO SB / 1.5*SM	CLASS 1 COMPONENT DESCRIPTION
14	18	405.09	346.19	0.00	0.00	0.00	742.19	.0255	STRAIGHT PIPE
	29	405.09	337.60	0.00	0.00	0.00	742.69	.0248	STRAIGHT PIPE
25	29	405.09	337.60	0.00	0.00	0.00	742.69	.0248	STRAIGHT PIPE
	30	405.09	330.51	0.00	0.00	0.00	735.61	.0245	STRAIGHT PIPE
35	30	405.09	330.51	0.00	0.00	0.00	735.61	.0245	STRAIGHT PIPE
	31	405.09	454.17	0.00	0.00	0.00	859.26	.0286	STRAIGHT PIPE
49	31	405.09	454.17	0.00	0.00	0.00	859.26	.0286	STRAIGHT PIPE
	32	405.09	482.17	0.00	0.00	0.00	887.26	.0296	STRAIGHT PIPE
54	32	405.09	482.17	0.00	0.00	0.00	887.26	.0296	STRAIGHT PIPE
	33	405.09	473.68	0.00	0.00	0.00	874.77	.0276	STRAIGHT PIPE
65	33	405.09	473.68	0.00	0.00	0.00	874.77	.0276	STRAIGHT PIPE
	34	405.09	349.29	0.00	0.00	0.00	794.39	.0265	STRAIGHT PIPE
74	34	405.09	349.29	0.00	0.00	0.00	794.39	.0265	STRAIGHT PIPE
	35	405.09	529.49	0.00	0.00	0.00	934.58	.0312	STRAIGHT PIPE
79	35	405.09	529.49	0.00	0.00	0.00	934.58	.0312	STRAIGHT PIPE
	36	405.09	515.15	0.00	0.00	0.00	920.25	.0307	STRAIGHT PIPE
85	36	405.09	515.15	0.00	0.00	0.00	920.25	.0307	STRAIGHT PIPE
	37	405.09	595.20	0.00	0.00	0.00	1000.37	.0333	STRAIGHT PIPE
94	37	405.09	595.20	0.00	0.00	0.00	1000.37	.0333	STRAIGHT PIPE
	38	405.09	611.06	0.00	0.00	0.00	1016.45	.0339	STRAIGHT PIPE
99	38	405.09	611.06	0.00	0.00	0.00	1016.45	.0339	STRAIGHT PIPE
	39	405.09	624.87	0.00	0.00	0.00	1029.96	.0343	STRAIGHT PIPE
104	39	405.09	624.87	0.00	0.00	0.00	1029.96	.0343	STRAIGHT PIPE
	40	405.09	554.89	0.00	0.00	0.00	955.98	.0319	STRAIGHT PIPE
	44	810.19	1173.97	0.00	0.00	0.00	1984.16	.0661	WELDING TEE

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (PS)	RATIO SB / 1.5*SM	CLASS 1 COMPONENT DESCRIPTION
1r	33	810.19	485.39	0.00	0.00	0.00	1295.57	.0432	CURVED PIPE
	34	810.19	444.00	0.00	0.00	0.00	1254.19	.0419	CURVED PIPE
2r	34	810.19	444.00	0.00	0.00	0.00	1254.19	.0419	CURVED PIPE
	37	810.19	895.92	0.00	0.00	0.00	1706.11	.0569	CURVED PIPE

SECTION AND STRESS ANALYSIS OF EGGS SUCTION LINE 2 - LACWR

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (PS)	RATIO SB / 1.5*SM	CLASS 1 COMPONENT DESCRIPTION
114	40	405.09	1710.42	0.00	0.00	0.00	2115.51	.0705	STRAIGHT PIPE
	41	405.09	390.65	0.00	0.00	0.00	755.74	.0252	STRAIGHT PIPE
124	41	405.09	390.65	0.00	0.00	0.00	755.74	.0252	STRAIGHT PIPE
	43	405.09	1240.19	0.00	0.00	0.00	1655.28	.0552	STRAIGHT PIPE
134	43	405.09	1240.19	0.00	0.00	0.00	1655.28	.0552	STRAIGHT PIPE
	44	810.19	1173.97	0.00	0.00	0.00	1984.16	.0661	WELDING TEE
144	44	810.19	1173.97	0.00	0.00	0.00	1984.16	.0661	WELDING TEE
	45	405.09	874.94	0.00	0.00	0.00	1284.05	.0428	STRAIGHT PIPE
154	45	405.09	874.94	0.00	0.00	0.00	1284.05	.0428	STRAIGHT PIPE
	46	405.09	1049.25	0.00	0.00	0.00	1474.34	.0491	STRAIGHT PIPE
164	46	405.09	1049.25	0.00	0.00	0.00	1474.34	.0491	STRAIGHT PIPE
	47	405.09	681.40	0.00	0.00	0.00	1086.50	.0362	STRAIGHT PIPE
174	47	405.09	681.40	0.00	0.00	0.00	1086.50	.0362	STRAIGHT PIPE
	48	405.09	1044.04	0.00	0.00	0.00	1449.13	.0483	STRAIGHT PIPE
175	48	405.09	1044.04	0.00	0.00	0.00	1449.13	.0483	STRAIGHT PIPE
	49	810.19	641.53	0.00	0.00	0.00	1387.57	.0463	STRAIGHT PIPE
184	49	810.19	641.53	0.00	0.00	0.00	1387.57	.0463	STRAIGHT PIPE
	50	810.19	2543.20	0.00	0.00	0.00	2988.29	.0996	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (PS)	RATIO SB / 1.5*SM	CLASS 1 COMPONENT DESCRIPTION
3c	41	810.19	481.72	0.00	0.00	0.00	1211.91	.0404	CURVED PIPE
	42	810.19	1070.82	0.00	0.00	0.00	1840.91	.0630	CURVED PIPE
4c	46	810.19	1605.42	0.00	0.00	0.00	2415.80	.0805	CURVED PIPE
	47	810.19	1023.09	0.00	0.00	0.00	1833.28	.0611	CURVED PIPE

DESIGN AND STRESS ANALYSIS OF COOL SUCTION LINE 2 LAGUNA

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT / DESCRIPTION
19x	49	810.19	5411.53	0.00	0.00	0.00	6421.72	.2141	WELDING TEE
	51	405.09	1491.19	0.00	0.00	0.00	1896.79	.0632	STRAIGHT PIPE
20x	52	405.09	2127.96	0.00	0.00	0.00	2533.95	.0844	STRAIGHT PIPE
	53	405.09	3574.62	0.00	0.00	0.00	3979.71	.1327	STRAIGHT PIPE
21x	53	405.09	3574.62	0.00	0.00	0.00	3979.71	.1327	STRAIGHT PIPE
	54	405.09	2998.74	0.00	0.00	0.00	3313.33	.1104	STRAIGHT PIPE
	55	405.09	3155.54	0.00	0.00	0.00	3550.47	.1184	STRAIGHT PIPE
22x	56	405.09	2074.49	0.00	0.00	0.00	2479.58	.0827	STRAIGHT PIPE
23x	57	405.09	2081.70	0.00	0.00	0.00	2464.80	.0822	STRAIGHT PIPE
	58	405.09	4784.04	0.00	0.00	0.00	5181.13	.1720	STRAIGHT PIPE
24x	58	405.09	4784.04	0.00	0.00	0.00	5181.13	.1720	STRAIGHT PIPE
	59	405.09	2867.74	0.00	0.00	0.00	3272.84	.1091	STRAIGHT PIPE
25x	60	405.09	3057.42	0.00	0.00	0.00	3462.51	.1121	STRAIGHT PIPE
	61	405.09	3725.33	0.00	0.00	0.00	4135.42	.1377	STRAIGHT PIPE
26x	62	405.09	4323.03	0.00	0.00	0.00	4732.12	.1572	STRAIGHT PIPE
	63	405.09	2867.77	0.00	0.00	0.00	3262.86	.1088	STRAIGHT PIPE
27x	63	405.09	2867.77	0.00	0.00	0.00	3262.86	.1088	STRAIGHT PIPE
	64	405.09	2418.48	0.00	0.00	0.00	2823.49	.0948	STRAIGHT PIPE
28x	65	405.09	2591.81	0.00	0.00	0.00	2996.91	.0999	STRAIGHT PIPE
	66	405.09	3874.03	0.00	0.00	0.00	4229.12	.1406	STRAIGHT PIPE
29x	67	405.09	2487.84	0.00	0.00	0.00	2902.66	.0968	STRAIGHT PIPE
	68	405.09	3210.92	0.00	0.00	0.00	3614.91	.1205	STRAIGHT PIPE
30x	68	405.09	3210.92	0.00	0.00	0.00	3614.91	.1205	STRAIGHT PIPE
	70	810.19	4025.19	0.00	0.00	0.00	4435.38	.1476	WELDING TEE
31x	70	810.19	4025.19	0.00	0.00	0.00	4435.38	.1476	WELDING TEE
	71	405.09	3077.45	0.00	0.00	0.00	3487.74	.1160	STRAIGHT PIPE
32x	71	405.09	3077.45	0.00	0.00	0.00	3487.74	.1160	STRAIGHT PIPE
	72	405.09	1981.96	0.00	0.00	0.00	2354.82	.0789	STRAIGHT PIPE
33x	72	405.09	1981.96	0.00	0.00	0.00	2354.82	.0789	STRAIGHT PIPE
	73	810.19	3084.82	0.00	0.00	0.00	3377.50	.1114	WELDING TEE
34x	73	810.19	3084.82	0.00	0.00	0.00	3377.50	.1114	WELDING TEE
	82	810.19	5043.05	0.00	0.00	0.00	5453.24	.1818	WELDING TEE

CURVED MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT / DESCRIPTION
5P	51	810.19	6844.74	0.00	0.00	0.00	7464.43	.2552	CURVED PIPE
	52	810.19	4977.68	0.00	0.00	0.00	6787.86	.2262	CURVED PIPE
6C	54	810.19	3742.70	0.00	0.00	0.00	4572.89	.1524	CURVED PIPE
	55	810.19	4049.78	0.00	0.00	0.00	4427.66	.1482	CURVED PIPE
7F	58	810.19	2883.98	0.00	0.00	0.00	3444.17	.1165	CURVED PIPE
	67	810.19	2687.45	0.00	0.00	0.00	3477.63	.1151	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT / DESCRIPTION
35x	70	405.09	3790.10	0.00	0.00	0.00	4165.19	.1371	CURVED PIPE
	80	405.09	3005.89	0.00	0.00	0.00	3311.88	.1072	CURVED PIPE
36x	81	405.09	4401.49	0.00	0.00	0.00	4811.67	.1572	CURVED PIPE
	82	810.19	5544.87	0.00	0.00	0.00	6099.05	.2033	CURVED PIPE
37x	84	810.19	3747.71	0.00	0.00	0.00	4147.80	.1369	CURVED PIPE
	85	810.19	3743.31	0.00	0.00	0.00	4143.56	.1364	CURVED PIPE
38x	86	810.19	7545.18	0.00	0.00	0.00	8355.37	.2785	CURVED PIPE
	87	810.19	3271.91	0.00	0.00	0.00	3645.09	.1240	CURVED PIPE
39x	88	810.19	7654.65	0.00	0.00	0.00	8444.83	.2822	CURVED PIPE
	89	810.19	8125.94	0.00	0.00	0.00	8936.13	.2979	CURVED PIPE
39x	88	405.09	545.79	0.00	0.00	0.00	595.80	.0200	STRAIGHT PIPE
	87	810.19	4599.95	0.00	0.00	0.00	5410.14	.1803	WELDING TEE
40x	87	810.19	4599.95	0.00	0.00	0.00	5410.14	.1803	WELDING TEE
	88	405.09	147.83	0.00	0.00	0.00	552.92	.0184	STRAIGHT PIPE
41x	88	327.59	781.33	0.00	0.00	0.00	1108.92	.0370	STRAIGHT PIPE
	89	327.59	253.64	0.00	0.00	0.00	581.23	.0194	STRAIGHT PIPE
42x	89	327.59	202.29	0.00	0.00	0.00	619.88	.0207	STRAIGHT PIPE
	91	327.59	235.92	0.00	0.00	0.00	583.51	.0188	STRAIGHT PIPE
43x	92	327.59	274.24	0.00	0.00	0.00	562.66	.0182	STRAIGHT PIPE
	93	327.59	942.82	0.00	0.00	0.00	1310.40	.0437	STRAIGHT PIPE
44x	93	327.59	942.82	0.00	0.00	0.00	1310.40	.0437	STRAIGHT PIPE
	94	327.59	544.81	0.00	0.00	0.00	874.60	.0291	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT / DESCRIPTION
13x	80	810.19	1398.84	0.00	0.00	0.00	2009.05	.0670	CURVED PIPE
	81	810.19	1317.86	0.00	0.00	0.00	2128.04	.0709	CURVED PIPE
14x	83	810.19	1049.30	0.00	0.00	0.00	1494.52	.0473	CURVED PIPE
	84	810.19	1207.10	0.00	0.00	0.00	2217.36	.0720	CURVED PIPE
15x	85	810.19	807.08	0.00	0.00	0.00	1417.24	.0452	CURVED PIPE
	86	810.19	374.22	0.00	0.00	0.00	1568.42	.0523	CURVED PIPE
76x	89	815.17	545.92	0.00	0.00	0.00	1134.10	.0369	CURVED PIPE
	90	815.17	875.64	0.00	0.00	0.00	1293.82	.0427	CURVED PIPE
13x	81	815.17	404.99	0.00	0.00	0.00	1144.74	.0364	CURVED PIPE



SEISMIC AND STRESS ANALYSIS OF FCCG SUCTION LINE 3 LACANS

STRAIGHT MEMBERS FOR RUN 5

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (D)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SB)	RATIO SB / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
454	87	455.17	4509.95	0.00	0.00	0.00	5255.12	+1752	WELDING TEE
	95	327.59	1775.24	0.00	0.00	0.00	2102.83	+0701	STRAIGHT PIPE
466	94	327.59	1364.29	0.00	0.00	0.00	1691.88	+0564	STRAIGHT PIPE
	97	327.59	1554.54	0.00	0.00	0.00	1881.17	+0628	STRAIGHT PIPE
474	97	327.59	1554.54	0.00	0.00	0.00	1881.17	+0628	STRAIGHT PIPE
	94	327.59	1364.29	0.00	0.00	0.00	1691.88	+0564	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 5

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (D)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SB)	RATIO SB / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
18C	95	455.17	3799.90	0.00	0.00	0.00	4455.07	+1485	CURVED PIPE
	94	455.17	2909.56	0.00	0.00	0.00	3564.73	+1180	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (D)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SB)	RATIO SB / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
484	73	405.09	3044.43	0.00	0.00	0.00	3844.41	+1288	WELDING TEE
	74	405.09	527.37	0.00	0.00	0.00	927.46	+0309	STRAIGHT PIPE
495	75	405.09	430.78	0.00	0.00	0.00	835.88	+0279	STRAIGHT PIPE
	76	405.09	544.96	0.00	0.00	0.00	949.05	+0310	STRAIGHT PIPE
504	74	405.09	544.96	0.00	0.00	0.00	949.05	+0310	STRAIGHT PIPE
	77	405.09	937.72	0.00	0.00	0.00	1342.81	+0448	STRAIGHT PIPE
514	76	405.09	1542.89	0.00	0.00	0.00	2048.00	+0683	STRAIGHT PIPE
	79	405.09	8075.19	0.00	0.00	0.00	8835.38	+2945	WELDING TEE

CURVED MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (D)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SB)	RATIO SB / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
19C	74	405.09	944.54	0.00	0.00	0.00	1756.72	+0586	CURVED PIPE
	74	405.09	740.83	0.00	0.00	0.00	1591.01	+0530	CURVED PIPE
20C	77	405.09	1705.75	0.00	0.00	0.00	2515.94	+0839	CURVED PIPE
	78	405.09	2879.35	0.00	0.00	0.00	3689.53	+1222	CURVED PIPE

EISEMIC AND STRESS ANALYSIS OF EGGS SUCTION LINE 2 LACARA

STRESSES FOR EQUATION 9  
LOAD SET 3 \* LOAD COMBINATION 3

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT / DESCRIPTION
1A	19	405.09	888.45	0.00	0.00	0.00	1073.60	.0358	STRAIGHT PIPE
2A	20	405.09	805.39	0.00	0.00	0.00	1010.48	.0337	STRAIGHT PIPE
3A	29	405.09	805.39	0.00	0.00	0.00	1010.48	.0337	STRAIGHT PIPE
4A	30	405.09	888.72	0.00	0.00	0.00	1063.80	.0355	STRAIGHT PIPE
5A	31	405.09	854.77	0.00	0.00	0.00	1063.80	.0355	STRAIGHT PIPE
6A	31	405.09	949.37	0.00	0.00	0.00	1354.46	.0451	STRAIGHT PIPE
7A	32	405.09	949.37	0.00	0.00	0.00	1354.46	.0451	STRAIGHT PIPE
8A	32	405.09	1529.97	0.00	0.00	0.00	1931.06	.0644	STRAIGHT PIPE
9A	33	405.09	1529.97	0.00	0.00	0.00	1931.06	.0644	STRAIGHT PIPE
10A	34	405.09	829.10	0.00	0.00	0.00	1234.28	.0411	STRAIGHT PIPE
11A	35	405.09	909.33	0.00	0.00	0.00	1314.42	.0438	STRAIGHT PIPE
12A	35	405.09	909.33	0.00	0.00	0.00	1314.42	.0438	STRAIGHT PIPE
13A	36	405.09	1195.67	0.00	0.00	0.00	1601.72	.0534	STRAIGHT PIPE
14A	37	405.09	1253.76	0.00	0.00	0.00	1658.86	.0553	STRAIGHT PIPE
15A	38	405.09	1192.26	0.00	0.00	0.00	1593.36	.0532	STRAIGHT PIPE
16A	38	405.09	1246.02	0.00	0.00	0.00	1651.11	.0550	STRAIGHT PIPE
17A	39	405.09	1204.99	0.00	0.00	0.00	1610.09	.0537	STRAIGHT PIPE
18A	39	405.09	1247.12	0.00	0.00	0.00	1644.21	.0548	STRAIGHT PIPE
19A	44	810.19	2598.21	0.00	0.00	0.00	3404.40	.1135	WELDING TEE

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT / DESCRIPTION
1C	33	810.19	1471.67	0.00	0.00	0.00	2281.85	.0761	CURVED PIPE
2C	34	810.19	1796.44	0.00	0.00	0.00	2606.63	.0869	CURVED PIPE
3C	37	810.19	1888.58	0.00	0.00	0.00	2698.68	.0900	CURVED PIPE

EISEMIC AND STRESS ANALYSIS OF EGGS SUCTION LINE 2 LACARA

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT / DESCRIPTION
11A	40	405.09	1747.20	0.00	0.00	0.00	2147.29	.0716	STRAIGHT PIPE
12A	41	405.09	1189.81	0.00	0.00	0.00	1594.90	.0532	STRAIGHT PIPE
13A	42	405.09	1467.66	0.00	0.00	0.00	1962.36	.0646	STRAIGHT PIPE
14A	43	405.09	1491.25	0.00	0.00	0.00	1894.35	.0632	STRAIGHT PIPE
15A	43	405.09	1491.25	0.00	0.00	0.00	1894.35	.0632	STRAIGHT PIPE
16A	44	810.19	2598.21	0.00	0.00	0.00	3404.40	.1135	WELDING TEE
17A	44	810.19	2598.21	0.00	0.00	0.00	3404.40	.1135	WELDING TEE
18A	45	405.09	1572.84	0.00	0.00	0.00	1977.73	.0659	STRAIGHT PIPE
19A	45	405.09	1572.84	0.00	0.00	0.00	1977.73	.0659	STRAIGHT PIPE
20A	46	405.09	1439.70	0.00	0.00	0.00	1844.79	.0615	STRAIGHT PIPE
21A	47	405.09	888.99	0.00	0.00	0.00	1091.09	.0344	STRAIGHT PIPE
22A	48	405.09	1010.99	0.00	0.00	0.00	1435.99	.0479	STRAIGHT PIPE
23A	48	405.09	1017.31	0.00	0.00	0.00	1422.41	.0474	STRAIGHT PIPE
24A	49	810.19	7104.68	0.00	0.00	0.00	7914.45	.2638	WELDING TEE
25A	49	810.19	7104.68	0.00	0.00	0.00	7914.45	.2638	WELDING TEE
26A	50	405.09	5870.76	0.00	0.00	0.00	6275.85	.2092	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT / DESCRIPTION
3C	41	810.19	1363.12	0.00	0.00	0.00	2173.30	.0724	CURVED PIPE
4C	42	810.19	1491.19	0.00	0.00	0.00	1807.38	.0634	CURVED PIPE
5C	46	810.19	2181.62	0.00	0.00	0.00	2971.81	.0991	CURVED PIPE
6C	47	810.19	1029.93	0.00	0.00	0.00	1840.17	.0613	CURVED PIPE



SEISMIC AND STRESS ANALYSIS OF 800S SUCTION LINE 2 - LACARB

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT / ---DESCRIPTION---
19s	49	810.19	7104.06	0.00	0.00	0.00	7914.85	-.2638	WELDING TEE
	51	405.09	2772.14	0.00	0.00	0.00	2627.23	-.0876	STRAIGHT PIPE
20s	52	405.09	2618.54	0.00	0.00	0.00	2473.65	-.0808	STRAIGHT PIPE
	53	405.09	4245.14	0.00	0.00	0.00	4650.24	-.1550	STRAIGHT PIPE
21s	54	405.09	4245.14	0.00	0.00	0.00	4650.24	-.1550	STRAIGHT PIPE
	55	405.09	2801.27	0.00	0.00	0.00	3204.36	-.1049	STRAIGHT PIPE
22s	56	405.09	2825.76	0.00	0.00	0.00	3230.85	-.1077	STRAIGHT PIPE
	5A	405.09	2037.00	0.00	0.00	0.00	2437.09	-.0812	STRAIGHT PIPE
23s	57	405.09	1943.40	0.00	0.00	0.00	2368.49	-.0789	STRAIGHT PIPE
	58	405.09	4475.41	0.00	0.00	0.00	4880.50	-.1627	STRAIGHT PIPE
24s	5A	405.09	4475.41	0.00	0.00	0.00	4880.50	-.1627	STRAIGHT PIPE
	60	405.09	2811.80	0.00	0.00	0.00	3236.40	-.1079	STRAIGHT PIPE
25s	60	405.09	3350.40	0.00	0.00	0.00	3745.57	-.1249	STRAIGHT PIPE
	61	405.09	3492.38	0.00	0.00	0.00	3897.47	-.1299	STRAIGHT PIPE
26s	62	405.09	4251.56	0.00	0.00	0.00	4656.84	-.1552	STRAIGHT PIPE
	63	405.09	3299.41	0.00	0.00	0.00	3703.50	-.1235	STRAIGHT PIPE
27s	63	405.09	3299.41	0.00	0.00	0.00	3703.50	-.1235	STRAIGHT PIPE
	64	405.09	2440.89	0.00	0.00	0.00	2865.98	-.0955	STRAIGHT PIPE
28s	64	405.09	2247.97	0.00	0.00	0.00	2673.06	-.0891	STRAIGHT PIPE
	65	405.09	6537.96	0.00	0.00	0.00	6943.05	-.2314	STRAIGHT PIPE
29s	67	405.09	3414.36	0.00	0.00	0.00	4370.43	-.1460	STRAIGHT PIPE
	68	405.09	4744.12	0.00	0.00	0.00	5173.22	-.1724	STRAIGHT PIPE
30s	69	405.09	3434.01	0.00	0.00	0.00	4039.10	-.1346	STRAIGHT PIPE
	70	810.19	8770.00	0.00	0.00	0.00	9580.19	-.3193	WELDING TEE
31s	70	810.19	8770.00	0.00	0.00	0.00	9580.19	-.3193	WELDING TEE
	71	405.09	4576.94	0.00	0.00	0.00	4982.05	-.1661	STRAIGHT PIPE
32s	71	405.09	4576.94	0.00	0.00	0.00	4982.05	-.1661	STRAIGHT PIPE
	72	405.09	2377.42	0.00	0.00	0.00	2782.51	-.0920	STRAIGHT PIPE
33s	72	405.09	2304.53	0.00	0.00	0.00	2709.62	-.0903	STRAIGHT PIPE
	73	810.19	2954.66	0.00	0.00	0.00	3768.84	-.1256	WELDING TEE
34s	73	810.19	2954.66	0.00	0.00	0.00	3768.84	-.1256	WELDING TEE
	82	810.19	5824.72	0.00	0.00	0.00	6634.53	-.2212	WELDING TEE

CURVED MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT / ---DESCRIPTION---
5c	51	810.19	7434.32	0.00	0.00	0.00	8268.51	-.2740	CURVED PIPE
	52	810.19	4513.35	0.00	0.00	0.00	4323.54	-.1460	CURVED PIPE
6c	54	810.19	3474.30	0.00	0.00	0.00	4039.10	-.1346	CURVED PIPE
	55	810.19	3454.99	0.00	0.00	0.00	4044.18	-.1348	CURVED PIPE
7c	56	810.19	2429.31	0.00	0.00	0.00	3439.20	-.1146	CURVED PIPE
	57	810.19	2540.26	0.00	0.00	0.00	3350.45	-.1117	CURVED PIPE

8c	59	810.19	3310.63	0.00	0.00	0.00	4120.81	-.1374	CURVED PIPE
	60	810.19	3425.74	0.00	0.00	0.00	4435.96	-.1479	CURVED PIPE
9c	61	810.19	4211.49	0.00	0.00	0.00	5021.68	-.1674	CURVED PIPE
	62	810.19	5304.77	0.00	0.00	0.00	6176.96	-.2059	CURVED PIPE
10c	64	810.19	3183.90	0.00	0.00	0.00	3384.10	-.1130	CURVED PIPE
	65	810.19	2934.32	0.00	0.00	0.00	3744.59	-.1248	CURVED PIPE
11c	66	810.19	4470.05	0.00	0.00	0.00	4780.23	-.1593	CURVED PIPE
	67	810.19	4077.08	0.00	0.00	0.00	4282.27	-.1461	CURVED PIPE
12c	68	810.19	11044.94	0.00	0.00	0.00	12177.13	-.4059	CURVED PIPE
	69	810.19	8663.20	0.00	0.00	0.00	9473.46	-.3158	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT / ---DESCRIPTION---
35s	79	405.09	1984.91	0.00	0.00	0.00	2392.01	-.0797	STRAIGHT PIPE
	80	405.09	1175.73	0.00	0.00	0.00	1530.80	-.0510	STRAIGHT PIPE
36s	81	405.09	1074.39	0.00	0.00	0.00	1439.48	-.0480	STRAIGHT PIPE
	82	810.19	5824.72	0.00	0.00	0.00	6634.51	-.2212	WELDING TEE
37s	82	810.19	5824.72	0.00	0.00	0.00	6634.51	-.2212	WELDING TEE
	83	405.09	531.57	0.00	0.00	0.00	936.45	-.0312	STRAIGHT PIPE
38s	84	405.09	630.73	0.00	0.00	0.00	935.82	-.0312	STRAIGHT PIPE
	85	405.09	540.30	0.00	0.00	0.00	895.49	-.0288	STRAIGHT PIPE
39s	86	405.09	742.36	0.00	0.00	0.00	1157.46	-.0385	STRAIGHT PIPE
	87	810.19	7124.79	0.00	0.00	0.00	7934.97	-.2644	WELDING TEE
40s	87	810.19	7124.79	0.00	0.00	0.00	7934.97	-.2644	WELDING TEE
	88	405.09	270.14	0.00	0.00	0.00	425.23	-.0138	STRAIGHT PIPE
41s	88	327.59	1143.52	0.00	0.00	0.00	1471.10	-.0487	STRAIGHT PIPE
	89	327.59	974.66	0.00	0.00	0.00	1281.73	-.0426	STRAIGHT PIPE
42s	90	327.59	457.53	0.00	0.00	0.00	785.12	-.0262	STRAIGHT PIPE
	91	327.59	414.52	0.00	0.00	0.00	746.11	-.0249	STRAIGHT PIPE
43s	92	327.59	442.21	0.00	0.00	0.00	769.70	-.0253	STRAIGHT PIPE
	93	327.59	1341.35	0.00	0.00	0.00	1668.94	-.0556	STRAIGHT PIPE
44s	93	327.59	1341.35	0.00	0.00	0.00	1668.94	-.0556	STRAIGHT PIPE
	94	327.59	679.32	0.00	0.00	0.00	1085.91	-.0355	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT / ---DESCRIPTION---
13c	81	810.19	2047.75	0.00	0.00	0.00	2857.94	-.0953	CURVED PIPE
	81	810.19	1899.46	0.00	0.00	0.00	2709.85	-.0903	CURVED PIPE
14c	83	810.19	1554.61	0.00	0.00	0.00	2404.89	-.0804	CURVED PIPE
	84	810.19	1614.44	0.00	0.00	0.00	2474.67	-.0824	CURVED PIPE
15c	85	810.19	744.21	0.00	0.00	0.00	1274.49	-.0425	CURVED PIPE
	85	810.19	473.89	0.00	0.00	0.00	1284.19	-.0435	CURVED PIPE
16c	86	810.19	800.85	0.00	0.00	0.00	1458.32	-.0485	CURVED PIPE
	86	810.19	974.34	0.00	0.00	0.00	1634.52	-.0545	CURVED PIPE
17c	87	810.19	896.85	0.00	0.00	0.00	1581.62	-.0517	CURVED PIPE

DESIGN AND STRESS ANALYSIS OF EGGS SUCTION LINE 2 - LACRYD

STRAIGHT MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SB)	RATIO SB / 1.5*SM	CLASS I COMPONENT DESCRIPTION
459	87	485.17	7124.79	0.00	0.00	0.00	7783.96	.2595	WELDING TEE
	94	327.59	2312.50	0.00	0.00	0.00	2640.08	.0880	STRAIGHT PIPE
464	94	327.59	1749.43	0.00	0.00	0.00	2077.06	.0692	STRAIGHT PIPE
	97	327.59	2249.35	0.00	0.00	0.00	2576.93	.0859	STRAIGHT PIPE
474	97	327.59	2249.35	0.00	0.00	0.00	2576.93	.0859	STRAIGHT PIPE
	98	327.59	5841.85	0.00	0.00	0.00	6200.43	.2070	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SB)	RATIO SB / 1.5*SM	CLASS I COMPONENT DESCRIPTION
19F	95	455.17	4949.90	0.00	0.00	0.00	5405.07	.1868	CURVED PIPE
	96	455.17	3744.74	0.00	0.00	0.00	4399.91	.1467	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SB)	RATIO SB / 1.5*SM	CLASS I COMPONENT DESCRIPTION
484	74	810.19	2954.64	0.00	0.00	0.00	3764.84	.1256	WELDING TEE
	75	405.09	574.47	0.00	0.00	0.00	979.56	.0313	STRAIGHT PIPE
494	75	405.09	574.59	0.00	0.00	0.00	940.48	.0314	STRAIGHT PIPE
	76	405.09	669.30	0.00	0.00	0.00	1074.39	.0358	STRAIGHT PIPE
504	76	405.09	669.13	0.00	0.00	0.00	1074.22	.0358	STRAIGHT PIPE
	77	405.09	1045.40	0.00	0.00	0.00	1450.53	.0484	STRAIGHT PIPE
514	78	405.09	1434.94	0.00	0.00	0.00	1840.03	.0648	STRAIGHT PIPE
	79	810.19	8770.00	0.00	0.00	0.00	9580.19	.3193	WELDING TEE

CURVED MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SB)	RATIO SB / 1.5*SM	CLASS I COMPONENT DESCRIPTION
19F	74	810.19	948.30	0.00	0.00	0.00	1778.49	.0593	CURVED PIPE
	75	810.19	979.40	0.00	0.00	0.00	1740.08	.0594	CURVED PIPE
20F	77	810.19	1901.70	0.00	0.00	0.00	2711.88	.0904	CURVED PIPE
	78	810.19	2799.40	0.00	0.00	0.00	3609.59	.1203	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF PCCS SUCTION LINE 2 - LACOUR

STRESSES FOR EQUATION 9  
LOAD SET A \* LOAD COMBINATION 4

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SB)	RATIO SB / 1.5*SM	CLASS I COMPONENT / DESCRIPTION
1A	19	405.09	517.54	0.00	0.00	0.00	1022.65	.0341	STRAIGHT PIPE
2A	29	405.09	579.43	0.00	0.00	0.00	984.52	.0328	STRAIGHT PIPE
3A	39	405.09	547.12	0.00	0.00	0.00	967.21	.0322	STRAIGHT PIPE
4A	49	405.09	777.91	0.00	0.00	0.00	1183.00	.0394	STRAIGHT PIPE
5A	59	405.09	817.50	0.00	0.00	0.00	1222.60	.0408	STRAIGHT PIPE
6A	69	405.09	894.46	0.00	0.00	0.00	1303.56	.0438	STRAIGHT PIPE
7A	79	405.09	515.67	0.00	0.00	0.00	920.76	.0307	STRAIGHT PIPE
8A	89	405.09	644.41	0.00	0.00	0.00	1050.50	.0350	STRAIGHT PIPE
9A	99	405.09	644.41	0.00	0.00	0.00	1050.50	.0350	STRAIGHT PIPE
10A	109	405.09	714.12	0.00	0.00	0.00	1119.21	.0373	STRAIGHT PIPE
11A	119	405.09	815.79	0.00	0.00	0.00	1220.47	.0407	STRAIGHT PIPE
12A	129	405.09	844.74	0.00	0.00	0.00	1253.33	.0418	STRAIGHT PIPE
13A	139	405.09	845.95	0.00	0.00	0.00	1271.05	.0424	STRAIGHT PIPE
14A	149	405.09	787.94	0.00	0.00	0.00	1188.03	.0396	STRAIGHT PIPE
15A	159	405.09	790.79	0.00	0.00	0.00	1195.87	.0399	STRAIGHT PIPE
16A	169	810.19	1616.96	0.00	0.00	0.00	2427.14	.0809	WELDING TEE

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SB)	RATIO SB / 1.5*SM	CLASS I COMPONENT / DESCRIPTION
17C	33	810.19	800.20	0.00	0.00	0.00	1610.39	.0537	CURVED PIPE
18C	34	810.19	590.79	0.00	0.00	0.00	1400.98	.0442	CURVED PIPE
19C	36	810.19	1072.01	0.00	0.00	0.00	1882.19	.0627	CURVED PIPE
20C	37	810.19	1277.05	0.00	0.00	0.00	2037.24	.0679	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF PCCS SUCTION LINE 2 - LACOUR

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SB)	RATIO SB / 1.5*SM	CLASS I COMPONENT / DESCRIPTION
11A	40	405.09	2892.25	0.00	0.00	0.00	3257.34	.1096	STRAIGHT PIPE
12A	41	405.09	544.40	0.00	0.00	0.00	963.77	.0321	STRAIGHT PIPE
13A	42	405.09	1394.13	0.00	0.00	0.00	1733.78	.0578	STRAIGHT PIPE
14A	43	405.09	1470.40	0.00	0.00	0.00	1825.50	.0609	STRAIGHT PIPE
15A	44	810.19	1414.96	0.00	0.00	0.00	1825.50	.0609	STRAIGHT PIPE
16A	45	810.19	1616.96	0.00	0.00	0.00	2427.14	.0809	WELDING TEE
17A	46	405.09	1171.49	0.00	0.00	0.00	1528.59	.0510	STRAIGHT PIPE
18A	47	405.09	1331.49	0.00	0.00	0.00	1678.58	.0560	STRAIGHT PIPE
19A	48	405.09	1351.20	0.00	0.00	0.00	1756.29	.0585	STRAIGHT PIPE
20A	49	405.09	1531.31	0.00	0.00	0.00	1443.40	.0481	STRAIGHT PIPE
21A	50	405.09	1574.34	0.00	0.00	0.00	1481.40	.0490	STRAIGHT PIPE
22A	51	405.09	1517.83	0.00	0.00	0.00	1918.02	.0629	STRAIGHT PIPE
23A	52	810.19	2473.75	0.00	0.00	0.00	2838.93	.0945	WELDING TEE
24A	53	810.19	2673.59	0.00	0.00	0.00	3191.78	.1061	WELDING TEE
25A	54	405.09	4187.85	0.00	0.00	0.00	4587.94	.1529	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SB)	RATIO SB / 1.5*SM	CLASS I COMPONENT / DESCRIPTION
30C	41	810.19	440.04	0.00	0.00	0.00	1450.24	.0483	CURVED PIPE
31C	42	810.19	1473.59	0.00	0.00	0.00	2331.79	.0777	CURVED PIPE
32C	43	810.19	2074.75	0.00	0.00	0.00	2838.93	.0945	CURVED PIPE
33C	44	810.19	1548.97	0.00	0.00	0.00	2369.15	.0790	CURVED PIPE

STATIC AND STRESS ANALYSIS OF PCCS SURFION LINE 2 - EACH

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (QT)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT DESCRIPTION
19A	49	810.19	8473.59	0.00	0.00	0.00	9483.78	.3161	WELDING TEE
51	405.09	2317.69	0.00	0.00	0.00	0.00	2722.79	.0900	STRAIGHT PIPE
20A	47	405.09	3732.99	0.00	0.00	0.00	3638.04	.1213	STRAIGHT PIPE
53	405.09	5593.18	0.00	0.00	0.00	0.00	5998.27	.1999	STRAIGHT PIPE
21A	53	405.09	5593.18	0.00	0.00	0.00	5998.27	.1999	STRAIGHT PIPE
54	405.09	4543.46	0.00	0.00	0.00	0.00	4948.73	.1650	STRAIGHT PIPE
22A	64	405.09	4794.03	0.00	0.00	0.00	5199.12	.1733	STRAIGHT PIPE
54	405.09	5792.42	0.00	0.00	0.00	0.00	3787.51	.1263	STRAIGHT PIPE
23A	67	405.09	3444.59	0.00	0.00	0.00	3991.59	.1331	STRAIGHT PIPE
58	405.09	7742.45	0.00	0.00	0.00	0.00	8147.75	.2718	STRAIGHT PIPE
24A	58	405.09	7742.45	0.00	0.00	0.00	8147.75	.2718	STRAIGHT PIPE
59	405.09	7742.45	0.00	0.00	0.00	0.00	4778.23	.1593	STRAIGHT PIPE
25A	68	405.09	5588.75	0.00	0.00	0.00	5993.45	.1970	STRAIGHT PIPE
61	405.09	5470.69	0.00	0.00	0.00	0.00	6075.78	.2051	STRAIGHT PIPE
26A	61	405.09	4044.31	0.00	0.00	0.00	4453.40	.1511	STRAIGHT PIPE
63	405.09	4414.31	0.00	0.00	0.00	0.00	4820.40	.1607	STRAIGHT PIPE
27A	63	405.09	4414.31	0.00	0.00	0.00	4820.40	.1607	STRAIGHT PIPE
64	405.09	4129.43	0.00	0.00	0.00	0.00	4533.79	.1511	STRAIGHT PIPE
28A	65	405.09	4088.80	0.00	0.00	0.00	4493.98	.1498	STRAIGHT PIPE
65	405.09	7468.57	0.00	0.00	0.00	0.00	7873.45	.2625	STRAIGHT PIPE
29A	67	405.09	3811.48	0.00	0.00	0.00	4214.47	.1408	STRAIGHT PIPE
68	405.09	5127.05	0.00	0.00	0.00	0.00	5587.09	.1862	STRAIGHT PIPE
30A	69	405.09	4500.57	0.00	0.00	0.00	5995.66	.1999	STRAIGHT PIPE
70	810.19	12737.00	0.00	0.00	0.00	0.00	13547.19	.4516	WELDING TEE
31A	70	810.19	12737.00	0.00	0.00	0.00	13547.19	.4516	WELDING TEE
71	405.09	3843.74	0.00	0.00	0.00	0.00	4268.43	.1423	STRAIGHT PIPE
32A	71	405.09	3812.43	0.00	0.00	0.00	4210.72	.1406	STRAIGHT PIPE
72	405.09	2332.09	0.00	0.00	0.00	0.00	2737.19	.0912	STRAIGHT PIPE
33A	72	405.09	2274.02	0.00	0.00	0.00	2681.12	.0894	STRAIGHT PIPE
73	810.19	5188.13	0.00	0.00	0.00	0.00	5999.36	.2000	WELDING TEE
34A	73	810.19	5188.13	0.00	0.00	0.00	5999.35	.2000	WELDING TEE
74	810.19	7977.91	0.00	0.00	0.00	0.00	8788.10	.2929	WELDING TEE

CURVED MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (QT)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT DESCRIPTION
50	51	810.19	10544.76	0.00	0.00	0.00	11354.45	.3785	CURVED PIPE
52	810.19	9142.61	0.00	0.00	0.00	0.00	9952.80	.3318	CURVED PIPE
54	810.19	5878.80	0.00	0.00	0.00	0.00	6658.79	.2230	CURVED PIPE
55	810.19	4202.56	0.00	0.00	0.00	0.00	7012.24	.2338	CURVED PIPE
56	810.19	4374.21	0.00	0.00	0.00	0.00	5188.29	.1729	CURVED PIPE
57	810.19	4649.24	0.00	0.00	0.00	0.00	5459.43	.1817	CURVED PIPE

80	59	810.19	4109.62	0.00	0.00	0.00	5910.41	.1970	CURVED PIPE
60	810.19	6103.90	0.00	0.00	0.00	0.00	6913.09	.2305	CURVED PIPE
61	810.19	3044.84	0.00	0.00	0.00	0.00	3457.02	.1151	CURVED PIPE
62	810.19	7917.33	0.00	0.00	0.00	0.00	8727.04	.2869	CURVED PIPE
64	810.19	5343.63	0.00	0.00	0.00	0.00	6151.51	.2009	CURVED PIPE
65	810.19	4208.23	0.00	0.00	0.00	0.00	4828.62	.1608	CURVED PIPE
66	810.19	6575.73	0.00	0.00	0.00	0.00	7445.72	.2495	CURVED PIPE
67	810.19	4934.53	0.00	0.00	0.00	0.00	5744.71	.1916	CURVED PIPE
68	810.19	12353.88	0.00	0.00	0.00	0.00	13163.74	.4388	CURVED PIPE
69	810.19	13327.61	0.00	0.00	0.00	0.00	14137.80	.4713	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (QT)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT DESCRIPTION
35A	79	405.09	1520.41	0.00	0.00	0.00	1985.51	.0662	STRAIGHT PIPE
80	405.09	774.41	0.00	0.00	0.00	0.00	1179.79	.0393	STRAIGHT PIPE
36A	81	405.09	1084.78	0.00	0.00	0.00	1471.87	.0491	STRAIGHT PIPE
82	810.19	7977.91	0.00	0.00	0.00	0.00	8788.10	.2929	WELDING TEE
37A	82	810.19	7977.91	0.00	0.00	0.00	8788.10	.2929	WELDING TEE
83	405.09	444.73	0.00	0.00	0.00	0.00	478.10	.0159	STRAIGHT PIPE
38A	84	405.09	646.17	0.00	0.00	0.00	849.20	.0283	STRAIGHT PIPE
84	405.09	547.53	0.00	0.00	0.00	0.00	871.27	.0290	STRAIGHT PIPE
39A	84	405.09	744.57	0.00	0.00	0.00	972.42	.0326	STRAIGHT PIPE
87	810.19	6103.90	0.00	0.00	0.00	0.00	6913.09	.2305	STRAIGHT PIPE
40A	87	810.19	6103.90	0.00	0.00	0.00	6913.09	.2305	STRAIGHT PIPE
88	405.09	210.95	0.00	0.00	0.00	0.00	210.95	.0070	STRAIGHT PIPE
41A	88	327.59	1114.92	0.00	0.00	0.00	1442.51	.0481	STRAIGHT PIPE
89	327.59	341.79	0.00	0.00	0.00	0.00	480.37	.0159	STRAIGHT PIPE
42A	90	327.59	473.51	0.00	0.00	0.00	751.20	.0250	STRAIGHT PIPE
91	327.59	354.07	0.00	0.00	0.00	0.00	685.45	.0229	STRAIGHT PIPE
43A	92	327.59	234.89	0.00	0.00	0.00	462.44	.0151	STRAIGHT PIPE
93	327.59	1217.57	0.00	0.00	0.00	0.00	1545.54	.0515	STRAIGHT PIPE
44A	93	327.59	1217.57	0.00	0.00	0.00	1545.15	.0515	STRAIGHT PIPE
94	327.59	774.58	0.00	0.00	0.00	0.00	1106.13	.0369	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 5

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (QT)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT DESCRIPTION
130	80	810.19	1409.04	0.00	0.00	0.00	2219.23	.0740	CURVED PIPE
81	810.19	1944.32	0.00	0.00	0.00	0.00	2155.59	.0719	CURVED PIPE
140	81	810.19	1409.04	0.00	0.00	0.00	2132.13	.0711	CURVED PIPE
84	810.19	1474.59	0.00	0.00	0.00	0.00	2215.17	.0738	CURVED PIPE
150	85	810.19	734.73	0.00	0.00	0.00	1544.91	.0515	CURVED PIPE
86	810.19	944.14	0.00	0.00	0.00	0.00	1774.69	.0582	CURVED PIPE
160	89	810.19	774.40	0.00	0.00	0.00	1429.78	.0477	CURVED PIPE
89	810.19	944.14	0.00	0.00	0.00	0.00	1541.41	.0521	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF PCCS SUCTION LINE 2 - LACOMB

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
45A	87	655.17	6100.22	0.00	0.00	0.00	6755.39	.2252	WELDING TEE
	85	327.59	1946.55	0.00	0.00	0.00	2314.14	.0771	STRAIGHT PIPE
46A	95	327.59	1496.53	0.00	0.00	0.00	2022.12	.0667	STRAIGHT PIPE
	97	327.59	1770.71	0.00	0.00	0.00	2098.29	.0699	STRAIGHT PIPE
47A	97	327.59	1770.71	0.00	0.00	0.00	2098.29	.0699	STRAIGHT PIPE
	96	327.59	5923.02	0.00	0.00	0.00	5356.41	.1784	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
18C	95	655.17	4252.22	0.00	0.00	0.00	4907.39	.1636	CURVED PIPE
	96	655.17	3627.14	0.00	0.00	0.00	4282.32	.1427	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
48A	73	810.19	5189.12	0.00	0.00	0.00	5999.35	.2000	WELDING TEE
	74	405.09	847.33	0.00	0.00	0.00	1252.42	.0417	STRAIGHT PIPE
49A	75	405.09	535.94	0.00	0.00	0.00	941.03	.0314	STRAIGHT PIPE
	76	405.09	788.74	0.00	0.00	0.00	1193.85	.0398	STRAIGHT PIPE
50A	76	405.09	795.94	0.00	0.00	0.00	1201.03	.0400	STRAIGHT PIPE
	77	405.09	1783.45	0.00	0.00	0.00	1793.55	.0598	STRAIGHT PIPE
51A	76	405.09	2533.45	0.00	0.00	0.00	2936.74	.0979	STRAIGHT PIPE
	70	810.19	12737.00	0.00	0.00	0.00	13547.19	.4516	WELDING TEE

CURVED MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SR)	RATIO SR / 1.5*SM	CLASS 1 COMPONENT /-----DESCRIPTION-----/
19C	74	810.19	1535.52	0.00	0.00	0.00	2345.70	.0782	CURVED PIPE
	75	810.19	911.43	0.00	0.00	0.00	1281.62	.0544	CURVED PIPE
20C	77	810.19	2525.66	0.00	0.00	0.00	3335.84	.1112	CURVED PIPE
	78	810.19	4605.19	0.00	0.00	0.00	5415.37	.1805	CURVED PIPE



SEISMIC AND STRESS ANALYSIS OF FCCS SUCTION LINE 2 LAGUNA

B.2 CONSIDERATION OF EQUATION 10

STRESSES FOR EQUATION 10  
LOAD SET 1 - LOAD COMBINATION 5

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (T)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT /---DESCRIPTION---
15	19	405.09	444.81	0.00	0.00	0.00	871.10	.0145	STRAIGHT PIPE
	29	405.09	401.74	0.00	0.00	0.00	804.85	.0135	STRAIGHT PIPE
25	29	405.09	411.74	0.00	0.00	0.00	808.85	.0135	STRAIGHT PIPE
	30	405.09	512.44	0.00	0.00	0.00	937.53	.0154	STRAIGHT PIPE
35	30	405.09	512.44	0.00	0.00	0.00	937.53	.0154	STRAIGHT PIPE
	31	405.09	741.82	0.00	0.00	0.00	1146.91	.0191	STRAIGHT PIPE
45	31	405.09	741.82	0.00	0.00	0.00	1146.91	.0191	STRAIGHT PIPE
	32	405.09	1314.76	0.00	0.00	0.00	1741.86	.0290	STRAIGHT PIPE
55	32	405.09	1314.76	0.00	0.00	0.00	1741.86	.0290	STRAIGHT PIPE
	33	405.09	8375.99	0.00	0.00	0.00	8780.99	.1130	STRAIGHT PIPE
65	33	405.09	3762.74	0.00	0.00	0.00	3762.74	.0463	STRAIGHT PIPE
	35	405.09	7405.55	0.00	0.00	0.00	8100.44	.1030	STRAIGHT PIPE
75	35	405.09	3944.04	0.00	0.00	0.00	4371.13	.0558	STRAIGHT PIPE
	37	405.09	3413.04	0.00	0.00	0.00	3818.28	.0484	STRAIGHT PIPE
85	37	405.09	3754.08	0.00	0.00	0.00	4149.18	.0529	STRAIGHT PIPE
	38	405.09	3817.39	0.00	0.00	0.00	4222.49	.0540	STRAIGHT PIPE
95	38	405.09	4209.32	0.00	0.00	0.00	4604.41	.0582	STRAIGHT PIPE
105	39	405.09	4335.91	0.00	0.00	0.00	4742.00	.0599	STRAIGHT PIPE
	44	607.64	12392.97	0.00	0.00	0.00	12998.41	.1666	WELDING TEE

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (T)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT /---DESCRIPTION---
10	31	425.42	8719.50	0.00	0.00	0.00	10144.92	.1494	CURVED PIPE
	34	425.42	5142.40	0.00	0.00	0.00	5468.20	.0735	CURVED PIPE
20	35	437.20	7979.40	0.00	0.00	0.00	8375.60	.1194	CURVED PIPE
	37	437.20	6849.03	0.00	0.00	0.00	7232.62	.1013	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF FCCS SUCTION LINE 2 LAGUNA

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (T)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT /---DESCRIPTION---
115	40	405.09	7130.65	0.00	0.00	0.00	7535.74	.1256	STRAIGHT PIPE
	41	405.09	3941.20	0.00	0.00	0.00	4366.37	.0720	STRAIGHT PIPE
125	42	405.09	5749.25	0.00	0.00	0.00	2145.24	.0350	STRAIGHT PIPE
	43	405.09	2000.72	0.00	0.00	0.00	2405.81	.0401	STRAIGHT PIPE
135	43	405.09	2073.72	0.00	0.00	0.00	2405.81	.0401	STRAIGHT PIPE
	44	607.64	12392.97	0.00	0.00	0.00	12998.41	.1666	WELDING TEE
145	44	405.09	5274.85	0.00	0.00	0.00	2431.94	.0405	STRAIGHT PIPE
155	45	405.09	2024.85	0.00	0.00	0.00	2431.94	.0405	STRAIGHT PIPE
	46	405.09	3341.85	0.00	0.00	0.00	3746.55	.0524	STRAIGHT PIPE
165	46	405.09	5474.13	0.00	0.00	0.00	6229.22	.1025	STRAIGHT PIPE
	48	405.09	3394.23	0.00	0.00	0.00	3799.23	.0633	STRAIGHT PIPE
175	48	405.09	3500.52	0.00	0.00	0.00	3905.42	.0651	STRAIGHT PIPE
	49	607.64	11733.12	0.00	0.00	0.00	11840.76	.1573	WELDING TEE
185	49	607.64	11733.12	0.00	0.00	0.00	11840.76	.1573	WELDING TEE
	50	405.09	4094.85	0.00	0.00	0.00	4524.76	.1417	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (T)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT /---DESCRIPTION---
30	41	425.42	4081.05	0.00	0.00	0.00	4474.47	.1079	CURVED PIPE
	42	425.42	2555.31	0.00	0.00	0.00	3083.24	.0814	CURVED PIPE
40	46	437.20	6593.16	0.00	0.00	0.00	7127.36	.1180	CURVED PIPE
	47	437.20	11259.00	0.00	0.00	0.00	11696.23	.1549	CURVED PIPE



SEISMIC AND STRESS ANALYSIS OF PCCS SUCTION LINE 2 - LACROW

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (T)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (PI)	SUM (SN)	RATIO SN / 3.0*SM	CLASS I COMPONENT DESCRIPTION
195	49	407.64	11237.12	0.00	0.00	0.00	11840.76	.1973	WELDING TEE
51	51	405.09	1844.86	0.00	0.00	0.00	2251.95	.0375	STRAIGHT PIPE
200	52	405.09	1844.86	0.00	0.00	0.00	2149.49	.0345	STRAIGHT PIPE
53	53	405.09	2925.29	0.00	0.00	0.00	3330.39	.0555	STRAIGHT PIPE
214	54	405.09	1911.55	0.00	0.00	0.00	2316.66	.0386	STRAIGHT PIPE
55	55	405.09	2224.42	0.00	0.00	0.00	2629.72	.0438	STRAIGHT PIPE
5A	5A	405.09	1502.23	0.00	0.00	0.00	1997.33	.0333	STRAIGHT PIPE
57	57	405.09	1785.09	0.00	0.00	0.00	1659.14	.0276	STRAIGHT PIPE
58	58	405.09	2649.69	0.00	0.00	0.00	3054.78	.0509	STRAIGHT PIPE
5R	5R	405.09	2649.69	0.00	0.00	0.00	3054.78	.0509	STRAIGHT PIPE
59	59	405.09	2020.19	0.00	0.00	0.00	2425.28	.0404	STRAIGHT PIPE
60	60	405.09	1717.03	0.00	0.00	0.00	2122.12	.0354	STRAIGHT PIPE
61	61	405.09	1627.32	0.00	0.00	0.00	2032.42	.0339	STRAIGHT PIPE
62	62	405.09	1944.74	0.00	0.00	0.00	2349.85	.0392	STRAIGHT PIPE
63	63	405.09	1941.99	0.00	0.00	0.00	2347.08	.0391	STRAIGHT PIPE
63	63	405.09	1941.99	0.00	0.00	0.00	2347.08	.0391	STRAIGHT PIPE
64	64	405.09	1444.27	0.00	0.00	0.00	1891.36	.0315	STRAIGHT PIPE
65	65	405.09	1343.73	0.00	0.00	0.00	1768.82	.0295	STRAIGHT PIPE
6A	6A	405.09	2373.23	0.00	0.00	0.00	2778.32	.0463	STRAIGHT PIPE
67	67	405.09	2700.72	0.00	0.00	0.00	3105.41	.0518	STRAIGHT PIPE
AR	AR	405.09	3341.00	0.00	0.00	0.00	3786.14	.0631	STRAIGHT PIPE
69	69	405.09	3034.98	0.00	0.00	0.00	3440.07	.0573	STRAIGHT PIPE
70	70	607.64	9317.00	0.00	0.00	0.00	9919.63	.1653	WELDING TEE
71	71	405.09	3215.07	0.00	0.00	0.00	3620.16	.0603	STRAIGHT PIPE
71	71	405.09	3233.95	0.00	0.00	0.00	3639.05	.0607	STRAIGHT PIPE
72	72	405.09	844.90	0.00	0.00	0.00	1250.00	.0208	STRAIGHT PIPE
72	72	405.09	804.30	0.00	0.00	0.00	1213.40	.0202	STRAIGHT PIPE
73	73	607.64	3716.47	0.00	0.00	0.00	4324.11	.0721	WELDING TEE
73	73	607.64	3716.47	0.00	0.00	0.00	4324.11	.0721	WELDING TEE
82	82	607.64	6964.50	0.00	0.00	0.00	7576.14	.1263	WELDING TEE

CURVED MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (T)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (PI)	SUM (SN)	RATIO SN / 3.0*SM	CLASS I COMPONENT DESCRIPTION
5C	51	446.19	9015.91	0.00	0.00	0.00	9502.10	.1564	CURVED PIPE
52	52	446.19	6461.66	0.00	0.00	0.00	6947.45	.1160	CURVED PIPE
54	54	429.99	3287.80	0.00	0.00	0.00	3727.59	.0621	CURVED PIPE
55	55	429.99	1837.65	0.00	0.00	0.00	2447.44	.0411	CURVED PIPE
56	56	429.99	2744.73	0.00	0.00	0.00	3176.72	.0529	CURVED PIPE
57	57	429.99	2161.67	0.00	0.00	0.00	2591.46	.0432	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (T)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (PI)	SUM (SN)	RATIO SN / 3.0*SM	CLASS I COMPONENT DESCRIPTION
59	59	424.97	3374.10	0.00	0.00	0.00	3753.17	.0624	CURVED PIPE
60	60	424.97	2537.32	0.00	0.00	0.00	2947.30	.0494	CURVED PIPE
61	61	427.58	2621.25	0.00	0.00	0.00	3044.43	.0504	CURVED PIPE
62	62	427.58	2090.01	0.00	0.00	0.00	2417.59	.0407	CURVED PIPE
64	64	429.99	2543.93	0.00	0.00	0.00	2993.97	.0499	CURVED PIPE
65	65	429.99	2352.54	0.00	0.00	0.00	2782.53	.0464	CURVED PIPE
6A	6A	430.05	4099.39	0.00	0.00	0.00	4529.44	.0755	CURVED PIPE
67	67	410.05	4444.87	0.00	0.00	0.00	5094.92	.0849	CURVED PIPE
6A	6A	441.41	10745.96	0.00	0.00	0.00	11228.37	.1871	CURVED PIPE
69	69	441.41	9644.95	0.00	0.00	0.00	10128.36	.1688	CURVED PIPE
74	74	405.09	944.30	0.00	0.00	0.00	1371.40	.0229	STRAIGHT PIPE
75	75	405.09	869.56	0.00	0.00	0.00	1244.45	.0211	STRAIGHT PIPE
81	81	405.09	910.32	0.00	0.00	0.00	1315.42	.0219	STRAIGHT PIPE
82	82	607.64	8944.50	0.00	0.00	0.00	9576.14	.1263	WELDING TEE
83	83	607.64	8944.50	0.00	0.00	0.00	9576.14	.1263	WELDING TEE
87	87	405.09	894.72	0.00	0.00	0.00	1233.81	.0206	STRAIGHT PIPE
8A	8A	405.09	949.23	0.00	0.00	0.00	1354.38	.0226	STRAIGHT PIPE
85	85	405.09	904.82	0.00	0.00	0.00	1309.91	.0210	STRAIGHT PIPE
84	84	405.09	849.37	0.00	0.00	0.00	1274.47	.0212	STRAIGHT PIPE
87	87	607.64	9047.87	0.00	0.00	0.00	9675.54	.1613	WELDING TEE
88	88	607.64	9047.87	0.00	0.00	0.00	9675.54	.1613	WELDING TEE
8R	8R	405.09	279.35	0.00	0.00	0.00	384.40	.0064	STRAIGHT PIPE
89	89	327.59	1474.45	0.00	0.00	0.00	1804.20	.0301	STRAIGHT PIPE
89	89	327.59	1347.32	0.00	0.00	0.00	1644.00	.0242	STRAIGHT PIPE
90	90	327.59	1354.47	0.00	0.00	0.00	1844.06	.0301	STRAIGHT PIPE
91	91	327.59	1215.74	0.00	0.00	0.00	1543.32	.0257	STRAIGHT PIPE
92	92	327.59	1041.11	0.00	0.00	0.00	1358.78	.0223	STRAIGHT PIPE
93	93	327.59	1045.59	0.00	0.00	0.00	2194.18	.0368	STRAIGHT PIPE
93	93	327.59	1045.59	0.00	0.00	0.00	2194.18	.0368	STRAIGHT PIPE
94	94	327.59	1045.59	0.00	0.00	0.00	2194.18	.0368	STRAIGHT PIPE
94	94	327.59	2805.23	0.00	0.00	0.00	3182.41	.0520	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (T)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (PI)	SUM (SN)	RATIO SN / 3.0*SM	CLASS I COMPONENT DESCRIPTION
80	80	450.29	2044.74	0.00	0.00	0.00	2535.05	.0423	CURVED PIPE
81	81	450.29	2215.42	0.00	0.00	0.00	2665.72	.0444	CURVED PIPE
83	83	491.05	2924.62	0.00	0.00	0.00	3420.47	.0570	CURVED PIPE
84	84	491.05	1079.27	0.00	0.00	0.00	1570.32	.0265	CURVED PIPE
85	85	450.01	1457.04	0.00	0.00	0.00	1987.10	.0331	CURVED PIPE
86	86	450.01	1447.12	0.00	0.00	0.00	1977.31	.0327	CURVED PIPE
89	89	395.30	3027.34	0.00	0.00	0.00	4297.64	.0716	CURVED PIPE
90	90	395.30	3071.78	0.00	0.00	0.00	4246.68	.0711	CURVED PIPE
91	91	395.30	3449.71	0.00	0.00	0.00	3865.01	.0644	CURVED PIPE
92	92	395.30	2845.71	0.00	0.00	0.00	3281.02	.0547	CURVED PIPE

WEIGHT AND STRESS ANALYSIS OF FOS SUGTION LINE 2 LACR

STRAIGHT MEMBERS FOR RUN 5

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT DESCRIPTION
454	87	491.35	9067.87	0.00	0.00	0.00	9559.25	.1593	WELDING TEE
	95	327.59	1394.72	0.00	0.00	0.00	1722.31	.0287	STRAIGHT PIPE
464	96	327.59	1447.44	0.00	0.00	0.00	1775.05	.0295	STRAIGHT PIPE
	97	327.59	1546.79	0.00	0.00	0.00	1874.38	.0312	STRAIGHT PIPE
474	97	327.59	1546.79	0.00	0.00	0.00	1874.38	.0312	STRAIGHT PIPE
	98	327.59	2175.99	0.00	0.00	0.00	2503.58	.0584	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 5

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT DESCRIPTION
180	95	395.30	1980.54	0.00	0.00	0.00	4375.84	.0729	CURVED PIPE
	96	395.30	4118.70	0.00	0.00	0.00	4512.99	.0752	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT DESCRIPTION
484	73	607.64	3716.17	0.00	0.00	0.00	4323.81	.0721	WELDING TEE
	74	405.09	434.49	0.00	0.00	0.00	839.58	.0140	STRAIGHT PIPE
	75	405.09	304.70	0.00	0.00	0.00	709.79	.0118	STRAIGHT PIPE
	76	405.09	459.15	0.00	0.00	0.00	864.24	.0144	STRAIGHT PIPE
504	76	405.09	458.27	0.00	0.00	0.00	863.36	.0144	STRAIGHT PIPE
	77	405.09	901.57	0.00	0.00	0.00	1308.66	.0218	STRAIGHT PIPE
	78	405.09	1053.03	0.00	0.00	0.00	1458.12	.0243	STRAIGHT PIPE
514	78	607.64	4312.00	0.00	0.00	4919.64	.1653	WELDING TEE	

CURVED MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT DESCRIPTION
190	74	450.00	1050.25	0.00	0.00	0.00	1500.25	.0250	CURVED PIPE
	75	450.00	2099.36	0.00	0.00	0.00	1549.36	.0250	CURVED PIPE
200	77	450.29	2191.51	0.00	0.00	0.00	2641.80	.0440	CURVED PIPE
	78	450.29	2554.02	0.00	0.00	0.00	3004.31	.0501	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF EGGS SUCTION LINE 2 - LACROW

STRESS FOR EQUATION 10  
 1.00 100.0 0.0 100.0 0.0 0.0

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (PQ)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT / DESCRIPTION
18	18	405.09	451.41	0.00	0.00	0.00	856.50	.0143	STRAIGHT PIPE
	29	405.09	393.51	0.00	0.00	0.00	798.60	.0133	STRAIGHT PIPE
24	29	405.09	393.51	0.00	0.00	0.00	798.60	.0133	STRAIGHT PIPE
	34	405.09	510.30	0.00	0.00	0.00	915.39	.0153	STRAIGHT PIPE
34	39	405.09	510.30	0.00	0.00	0.00	915.39	.0153	STRAIGHT PIPE
	31	405.09	714.56	0.00	0.00	0.00	1123.46	.0187	STRAIGHT PIPE
45	31	405.09	714.56	0.00	0.00	0.00	1123.46	.0187	STRAIGHT PIPE
	32	405.09	1094.97	0.00	0.00	0.00	1504.06	.0251	STRAIGHT PIPE
54	32	405.09	1094.97	0.00	0.00	0.00	1504.06	.0251	STRAIGHT PIPE
	33	405.09	1515.53	0.00	0.00	0.00	1920.62	.0315	STRAIGHT PIPE
64	34	405.09	1515.53	0.00	0.00	0.00	1920.62	.0315	STRAIGHT PIPE
	35	405.09	2730.84	0.00	0.00	0.00	3144.97	.0524	STRAIGHT PIPE
74	35	405.09	2730.84	0.00	0.00	0.00	3144.97	.0524	STRAIGHT PIPE
	45	405.09	7447.67	0.00	0.00	0.00	7852.57	.1309	STRAIGHT PIPE
84	45	405.09	7447.67	0.00	0.00	0.00	7852.57	.1309	STRAIGHT PIPE
	36	405.09	3611.69	0.00	0.00	0.00	4016.79	.0669	STRAIGHT PIPE
84	36	405.09	3611.69	0.00	0.00	0.00	4016.79	.0669	STRAIGHT PIPE
	37	405.09	2743.43	0.00	0.00	0.00	3168.52	.0528	STRAIGHT PIPE
94	37	405.09	2743.43	0.00	0.00	0.00	3168.52	.0528	STRAIGHT PIPE
	38	405.09	2992.97	0.00	0.00	0.00	3342.53	.0561	STRAIGHT PIPE
94	38	405.09	2992.97	0.00	0.00	0.00	3342.53	.0561	STRAIGHT PIPE
	39	405.09	3341.74	0.00	0.00	0.00	3746.83	.0628	STRAIGHT PIPE
104	39	405.09	3341.74	0.00	0.00	0.00	3746.83	.0628	STRAIGHT PIPE
	44	607.64	13311.33	0.00	0.00	0.00	3746.83	.0628	STRAIGHT PIPE
	44	607.64	13311.33	0.00	0.00	0.00	13918.97	.2320	WELDING TEE

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (PQ)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT / DESCRIPTION
1C	33	425.42	9957.79	0.00	0.00	0.00	10378.21	.1730	CURVED PIPE
	34	425.42	4144.30	0.00	0.00	0.00	4610.32	.0768	CURVED PIPE
2C	36	437.20	7278.64	0.00	0.00	0.00	7665.88	.1278	CURVED PIPE
	37	437.20	5532.61	0.00	0.00	0.00	5969.80	.0995	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF EGGS SUCTION LINE 2 - LACROW

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (PQ)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT / DESCRIPTION
114	40	405.09	9915.41	0.00	0.00	0.00	10340.50	.1723	STRAIGHT PIPE
	41	405.09	3199.43	0.00	0.00	0.00	3604.51	.0601	STRAIGHT PIPE
124	42	405.09	3391.33	0.00	0.00	0.00	3744.42	.0626	STRAIGHT PIPE
	43	405.09	2714.79	0.00	0.00	0.00	3121.84	.0520	STRAIGHT PIPE
134	43	405.09	2714.79	0.00	0.00	0.00	3121.84	.0520	STRAIGHT PIPE
	44	607.64	13311.33	0.00	0.00	0.00	13918.97	.2320	WELDING TEE
144	44	607.64	13311.33	0.00	0.00	0.00	13918.97	.2320	WELDING TEE
	45	405.09	1901.22	0.00	0.00	0.00	2306.31	.0384	STRAIGHT PIPE
154	45	405.09	1901.22	0.00	0.00	0.00	2306.31	.0384	STRAIGHT PIPE
	46	405.09	2447.41	0.00	0.00	0.00	2874.50	.0479	STRAIGHT PIPE
164	46	405.09	2447.41	0.00	0.00	0.00	2874.50	.0479	STRAIGHT PIPE
	47	405.09	11944.51	0.00	0.00	0.00	12254.61	.2042	STRAIGHT PIPE
	48	405.09	6713.03	0.00	0.00	0.00	6112.09	.1020	STRAIGHT PIPE
174	48	405.09	6713.03	0.00	0.00	0.00	6112.09	.1020	STRAIGHT PIPE
	49	405.09	5707.49	0.00	0.00	0.00	6112.58	.1019	STRAIGHT PIPE
	49	607.64	13311.33	0.00	0.00	0.00	13918.97	.2320	WELDING TEE
184	49	607.64	13311.33	0.00	0.00	0.00	13918.97	.2320	WELDING TEE
	50	405.09	17042.39	0.00	0.00	0.00	17487.48	.2915	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (PQ)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT / DESCRIPTION
3C	41	425.42	4447.27	0.00	0.00	0.00	5312.69	.0845	CURVED PIPE
	42	425.42	1119.32	0.00	0.00	0.00	5544.74	.0924	CURVED PIPE
4C	44	437.20	4943.58	0.00	0.00	0.00	5780.78	.0897	CURVED PIPE
	47	437.20	2371.84	0.00	0.00	0.00	2415.04	.0402	CURVED PIPE

STATIC AND STRESS ANALYSIS OF FCCB SUCTION LINE 2 - 24000

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT DESCRIPTION
195	4W	807.64	13343.93	0.00	0.00	0.00	13371.57	.2329	WELDING TEE
	51	405.09	2501.91	0.00	0.00	0.00	2906.90	.0584	STRAIGHT PIPE
205	52	405.09	2525.48	0.00	0.00	0.00	2930.56	.0589	STRAIGHT PIPE
	53	405.09	4128.14	0.00	0.00	0.00	4533.23	.0756	STRAIGHT PIPE
215	53	405.09	4128.14	0.00	0.00	0.00	4533.23	.0756	STRAIGHT PIPE
	54	405.09	2672.65	0.00	0.00	0.00	3077.74	.0613	STRAIGHT PIPE
225	55	405.09	3425.28	0.00	0.00	0.00	3848.37	.0740	STRAIGHT PIPE
	56	405.09	2213.94	0.00	0.00	0.00	2618.07	.0517	STRAIGHT PIPE
235	57	405.09	2525.48	0.00	0.00	0.00	2932.08	.0589	STRAIGHT PIPE
	58	405.09	4273.97	0.00	0.00	0.00	4679.07	.0780	STRAIGHT PIPE
245	58	405.09	4273.97	0.00	0.00	0.00	4679.07	.0780	STRAIGHT PIPE
	59	405.09	2891.14	0.00	0.00	0.00	3296.23	.0649	STRAIGHT PIPE
255	60	405.09	2813.54	0.00	0.00	0.00	3218.67	.0636	STRAIGHT PIPE
	61	405.09	2959.17	0.00	0.00	0.00	3363.75	.0661	STRAIGHT PIPE
265	62	405.09	7622.24	0.00	0.00	0.00	8027.33	.1438	STRAIGHT PIPE
	63	405.09	2632.85	0.00	0.00	0.00	3037.94	.0606	STRAIGHT PIPE
275	63	405.09	2632.85	0.00	0.00	0.00	3037.94	.0606	STRAIGHT PIPE
	64	405.09	2645.23	0.00	0.00	0.00	3070.32	.0612	STRAIGHT PIPE
285	65	405.09	2807.43	0.00	0.00	0.00	3067.52	.0601	STRAIGHT PIPE
	66	405.09	2708.49	0.00	0.00	0.00	3113.59	.0619	STRAIGHT PIPE
295	67	405.09	2517.40	0.00	0.00	0.00	2942.69	.0590	STRAIGHT PIPE
	68	405.09	3574.65	0.00	0.00	0.00	3939.74	.0717	STRAIGHT PIPE
305	68	405.09	4111.50	0.00	0.00	0.00	4515.66	.0753	STRAIGHT PIPE
	69	405.09	12444.50	0.00	0.00	0.00	13452.22	.2242	WELDING TEE
315	70	807.64	12444.50	0.00	0.00	0.00	13452.22	.2242	WELDING TEE
	71	405.09	2544.67	0.00	0.00	0.00	2951.76	.0592	STRAIGHT PIPE
325	71	405.09	2544.67	0.00	0.00	0.00	2922.09	.0587	STRAIGHT PIPE
	72	405.09	463.74	0.00	0.00	0.00	1365.83	.0228	STRAIGHT PIPE
335	72	405.09	463.74	0.00	0.00	0.00	1361.97	.0227	STRAIGHT PIPE
	73	807.64	4857.55	0.00	0.00	0.00	5765.19	.1070	WELDING TEE
345	73	807.64	4857.55	0.00	0.00	0.00	5765.19	.1070	WELDING TEE
	82	807.64	4850.48	0.00	0.00	0.00	974.12	.1543	WELDING TEE

CURVED MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT DESCRIPTION
80	51	448.19	14025.64	0.00	0.00	0.00	14511.86	.3085	CURVED PIPE
	52	448.19	13794.65	0.00	0.00	0.00	14282.85	.2980	CURVED PIPE
80	54	429.99	4810.53	0.00	0.00	0.00	5040.52	.0940	CURVED PIPE
	55	429.99	6074.12	0.00	0.00	0.00	6356.11	.1059	CURVED PIPE
70	56	429.99	3819.29	0.00	0.00	0.00	4249.28	.0798	CURVED PIPE
	57	429.99	4359.15	0.00	0.00	0.00	4789.14	.0798	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT DESCRIPTION
355	79	405.09	627.94	0.00	0.00	0.00	1033.03	.0172	STRAIGHT PIPE
	80	405.09	428.29	0.00	0.00	0.00	833.38	.0156	STRAIGHT PIPE
365	81	405.09	944.12	0.00	0.00	0.00	1371.21	.0229	STRAIGHT PIPE
	82	807.64	8450.40	0.00	0.00	0.00	9258.12	.1543	WELDING TEE
375	82	807.64	8450.40	0.00	0.00	0.00	9254.12	.1543	WELDING TEE
	83	405.09	795.02	0.00	0.00	0.00	1200.11	.0200	STRAIGHT PIPE
385	84	405.09	954.64	0.00	0.00	0.00	1359.73	.0227	STRAIGHT PIPE
	85	405.09	913.83	0.00	0.00	0.00	1314.62	.0220	STRAIGHT PIPE
395	86	405.09	872.41	0.00	0.00	0.00	1277.50	.0213	STRAIGHT PIPE
	87	807.64	8472.37	0.00	0.00	0.00	9189.01	.1530	WELDING TEE
405	87	807.64	8472.37	0.00	0.00	0.00	9185.01	.1529	WELDING TEE
	88	405.09	270.64	0.00	0.00	0.00	675.73	.0113	STRAIGHT PIPE
415	88	327.59	1430.39	0.00	0.00	0.00	1757.98	.0243	STRAIGHT PIPE
	89	327.59	1379.78	0.00	0.00	0.00	1701.37	.0234	STRAIGHT PIPE
425	90	327.59	1354.34	0.00	0.00	0.00	1685.93	.0231	STRAIGHT PIPE
	91	327.59	1207.93	0.00	0.00	0.00	1538.52	.0256	STRAIGHT PIPE
435	92	327.59	983.16	0.00	0.00	0.00	1210.75	.0210	STRAIGHT PIPE
	93	327.59	1847.00	0.00	0.00	0.00	2175.44	.0343	STRAIGHT PIPE
445	93	327.59	1847.00	0.00	0.00	0.00	2175.44	.0343	STRAIGHT PIPE
	94	327.59	2041.67	0.00	0.00	0.00	2369.25	.0378	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	SUM (SN)	RATIO SN / 3.0*SM	CLASS 1 COMPONENT DESCRIPTION
130	80	440.29	1281.31	0.00	0.00	0.00	1731.60	.0278	CURVED PIPE
	81	440.29	2344.88	0.00	0.00	0.00	2785.18	.0446	CURVED PIPE
140	82	440.29	2779.43	0.00	0.00	0.00	3220.67	.0545	CURVED PIPE
	84	440.29	3279.30	0.00	0.00	0.00	3729.35	.0655	CURVED PIPE
150	85	440.29	1572.58	0.00	0.00	0.00	2005.59	.0334	CURVED PIPE
	86	440.29	1589.50	0.00	0.00	0.00	1912.50	.0322	CURVED PIPE
160	89	395.30	3474.49	0.00	0.00	0.00	4271.79	.0770	CURVED PIPE
	90	395.30	3874.71	0.00	0.00	0.00	4272.01	.0772	CURVED PIPE
170	91	395.30	3444.88	0.00	0.00	0.00	3840.14	.0640	CURVED PIPE
	92	395.30	2805.94	0.00	0.00	0.00	3201.24	.0534	CURVED PIPE

SECTION AND STRESS ANALYSIS OF ECCO SUCTION LINE 2 - LACRO

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (T)	LINEAR TEMPERATURE GRADIENT (TF)	NONLINEAR TEMPERATURE GRADIENT (TF)	SUM (SN)	RATIO SN / 3.0*SM	CLASS I COMPONENT / DESCRIPTION
455	87	491.38	8572.37	0.00	0.00	0.00	9063.75	.1511	WELDING TEE
	95	327.59	1283.98	0.00	0.00	0.00	1611.57	.0269	STRAIGHT PIPE
469	94	327.59	1404.14	0.00	0.00	0.00	1735.73	.0289	STRAIGHT PIPE
	97	327.59	1388.86	0.00	0.00	0.00	1716.45	.0286	STRAIGHT PIPE
474	97	327.59	1388.86	0.00	0.00	0.00	1716.45	.0286	STRAIGHT PIPE
	98	327.59	2091.21	0.00	0.00	0.00	2318.79	.0386	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (T)	LINEAR TEMPERATURE GRADIENT (TF)	NONLINEAR TEMPERATURE GRADIENT (TF)	SUM (SN)	RATIO SN / 3.0*SM	CLASS I COMPONENT / DESCRIPTION
18C	95	395.30	3664.49	0.00	0.00	0.00	4059.79	.0677	CURVED PIPE
	96	395.30	4018.95	0.00	0.00	0.00	4414.25	.0736	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (T)	LINEAR TEMPERATURE GRADIENT (TF)	NONLINEAR TEMPERATURE GRADIENT (TF)	SUM (SN)	RATIO SN / 3.0*SM	CLASS I COMPONENT / DESCRIPTION
484	74	607.64	5857.45	0.00	0.00	0.00	6465.19	.1078	WELDING TEE
	75	405.09	681.10	0.00	0.00	0.00	1086.19	.0181	STRAIGHT PIPE
494	74	405.09	344.75	0.00	0.00	0.00	749.84	.0125	STRAIGHT PIPE
	76	405.09	487.87	0.00	0.00	0.00	892.96	.0145	STRAIGHT PIPE
504	76	405.09	590.51	0.00	0.00	0.00	995.60	.0166	STRAIGHT PIPE
	77	405.09	1194.72	0.00	0.00	0.00	1599.81	.0267	STRAIGHT PIPE
514	74	405.09	1711.24	0.00	0.00	0.00	2116.33	.0353	STRAIGHT PIPE
	78	607.64	1284.59	0.00	0.00	0.00	13452.22	.2242	WELDING TEE

CURVED MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (T)	LINEAR TEMPERATURE GRADIENT (TF)	NONLINEAR TEMPERATURE GRADIENT (TF)	SUM (SN)	RATIO SN / 3.0*SM	CLASS I COMPONENT / DESCRIPTION
19C	74	450.00	1446.06	0.00	0.00	0.00	2096.06	.0349	CURVED PIPE
	75	450.00	833.17	0.00	0.00	0.00	1283.17	.0214	CURVED PIPE
20C	77	450.29	2807.66	0.00	0.00	0.00	3247.96	.0558	CURVED PIPE
	77	450.29	4150.42	0.00	0.00	0.00	4600.71	.0767	CURVED PIPE



SEISMIC AND STRESS ANALYSIS OF ECCS SUCTION LINE 2 - LACRU

3.3 CONSIDERATION OF EQUATION 11 & EQUATION 14

STRESSES FOR EQUATION 11 & EQUATION 14  
LOAD SET 1 - LOAD COMBINATION 5

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT / DESCRIPTION
18	19	405.09	444.01	0.00	0.00	0.00	871.10	435.55	STRAIGHT PIPE
	20	405.09	403.76	0.00	0.00	0.00	804.85	404.42	STRAIGHT PIPE
20	20	405.09	443.76	0.00	0.00	0.00	804.85	404.42	STRAIGHT PIPE
	30	405.09	532.44	0.00	0.00	0.00	937.53	468.77	STRAIGHT PIPE
30	30	405.09	532.44	0.00	0.00	0.00	937.53	468.77	STRAIGHT PIPE
	31	405.09	741.82	0.00	0.00	0.00	1146.91	573.46	STRAIGHT PIPE
44	31	405.09	741.82	0.00	0.00	0.00	1146.91	573.46	STRAIGHT PIPE
	34	405.09	1337.76	0.00	0.00	0.00	1741.86	870.93	STRAIGHT PIPE
54	34	405.09	1337.76	0.00	0.00	0.00	1741.86	870.93	STRAIGHT PIPE
	33	405.09	6375.00	0.00	0.00	0.00	6780.92	3390.50	STRAIGHT PIPE
64	34	405.09	3392.94	0.00	0.00	0.00	3799.03	1899.02	STRAIGHT PIPE
	35	405.09	7495.55	0.00	0.00	0.00	8100.84	4050.32	STRAIGHT PIPE
74	34	405.09	7495.55	0.00	0.00	0.00	8100.84	4050.32	STRAIGHT PIPE
	36	405.09	3766.04	0.00	0.00	0.00	4371.13	2185.56	STRAIGHT PIPE
84	37	405.09	3766.04	0.00	0.00	0.00	4371.13	2185.56	STRAIGHT PIPE
	38	405.09	3744.08	0.00	0.00	0.00	4159.18	2079.59	STRAIGHT PIPE
94	38	405.09	3744.08	0.00	0.00	0.00	4159.18	2079.59	STRAIGHT PIPE
	39	405.09	4249.32	0.00	0.00	0.00	4504.41	2252.21	STRAIGHT PIPE
104	39	405.09	4249.32	0.00	0.00	0.00	4504.41	2252.21	STRAIGHT PIPE
	44	2430.56	12390.97	0.00	0.00	0.00	12821.52	7410.76	WELDING TEE

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT / DESCRIPTION
1C	33	425.42	4739.56	0.00	0.00	0.00	10164.92	5082.46	CURVED PIPE
	34	425.42	5182.88	0.00	0.00	0.00	5608.30	2804.15	CURVED PIPE
2C	3A	437.20	7938.40	0.00	0.00	0.00	8375.40	4187.80	CURVED PIPE
	3F	437.20	6849.03	0.00	0.00	0.00	3222.42	1611.21	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF ECCS SUCTION LINE 2 - LACRU

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT / DESCRIPTION
114	40	405.09	7170.65	0.00	0.00	0.00	7535.74	3767.87	STRAIGHT PIPE
	41	405.09	3941.28	0.00	0.00	0.00	4344.37	2172.19	STRAIGHT PIPE
124	42	405.09	1740.25	0.00	0.00	0.00	2145.30	1072.65	STRAIGHT PIPE
	43	405.09	2000.72	0.00	0.00	0.00	2405.81	1202.91	STRAIGHT PIPE
134	43	405.09	2000.72	0.00	0.00	0.00	2405.81	1202.91	STRAIGHT PIPE
	44	2430.56	12390.97	0.00	0.00	0.00	12821.52	7410.76	WELDING TEE
144	44	2430.56	12390.97	0.00	0.00	0.00	12821.52	7410.76	WELDING TEE
	45	405.09	2424.84	0.00	0.00	0.00	2431.96	1215.98	STRAIGHT PIPE
154	46	405.09	2424.84	0.00	0.00	0.00	2431.96	1215.98	STRAIGHT PIPE
	46	405.09	3341.84	0.00	0.00	0.00	3746.95	1873.48	STRAIGHT PIPE
164	47	405.09	3341.84	0.00	0.00	0.00	3746.95	1873.48	STRAIGHT PIPE
	48	405.09	5474.13	0.00	0.00	0.00	6022.22	3011.11	STRAIGHT PIPE
174	48	405.09	5474.13	0.00	0.00	0.00	6022.22	3011.11	STRAIGHT PIPE
	49	2430.56	11732.12	0.00	0.00	0.00	13543.67	6831.84	WELDING TEE
184	49	2430.56	11732.12	0.00	0.00	0.00	13543.67	6831.84	WELDING TEE
	50	405.09	8099.66	0.00	0.00	0.00	8504.76	4252.38	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT / DESCRIPTION
3C	41	425.42	4041.05	0.00	0.00	0.00	4476.47	2238.24	CURVED PIPE
	42	425.42	2444.31	0.00	0.00	0.00	3083.34	1541.67	CURVED PIPE
4C	46	437.20	6490.16	0.00	0.00	0.00	7127.36	3563.68	CURVED PIPE
	47	437.20	11254.00	0.00	0.00	0.00	11894.28	5947.14	CURVED PIPE



SEISMIC AND STRESS ANALYSIS OF ECCS SUCTION LINE 2 - LACBWD

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (D)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS (SP)	ALTERNATING STRESS EQ. 1A (SA)	CLASS 1 COMPONENT DESCRIPTION
19x	49	2430.56	11233.12	0.00	0.00	0.00	13563.67	6831.84	WELDING TEE
	51	405.09	1764.86	0.00	0.00	0.00	2251.95	1125.94	STRAIGHT PIPE
20x	52	405.09	1764.86	0.00	0.00	0.00	2184.49	1094.49	STRAIGHT PIPE
	53	405.09	2925.29	0.00	0.00	0.00	3330.39	1665.19	STRAIGHT PIPE
21x	54	405.09	2925.29	0.00	0.00	0.00	3330.39	1665.19	STRAIGHT PIPE
	55	405.09	1911.50	0.00	0.00	0.00	2314.46	1158.33	STRAIGHT PIPE
22x	56	405.09	2224.62	0.00	0.00	0.00	2629.72	1314.86	STRAIGHT PIPE
	57	405.09	1592.23	0.00	0.00	0.00	1997.73	998.66	STRAIGHT PIPE
23x	58	405.09	1753.09	0.00	0.00	0.00	1654.18	829.09	STRAIGHT PIPE
	59	405.09	2649.69	0.00	0.00	0.00	3054.78	1527.39	STRAIGHT PIPE
24x	60	405.09	2649.69	0.00	0.00	0.00	3054.78	1527.39	STRAIGHT PIPE
	61	405.09	2029.19	0.00	0.00	0.00	2429.28	1212.64	STRAIGHT PIPE
25x	62	405.09	1717.03	0.00	0.00	0.00	2127.12	1061.06	STRAIGHT PIPE
	63	405.09	1677.32	0.00	0.00	0.00	2032.42	1016.21	STRAIGHT PIPE
26x	64	405.09	1866.76	0.00	0.00	0.00	2349.45	1174.93	STRAIGHT PIPE
	65	405.09	1941.99	0.00	0.00	0.00	2347.08	1173.54	STRAIGHT PIPE
27x	66	405.09	1941.99	0.00	0.00	0.00	2347.08	1173.54	STRAIGHT PIPE
	67	405.09	1484.27	0.00	0.00	0.00	1891.36	945.68	STRAIGHT PIPE
28x	68	405.09	1347.73	0.00	0.00	0.00	1768.42	884.41	STRAIGHT PIPE
	69	405.09	2373.23	0.00	0.00	0.00	2778.32	1389.16	STRAIGHT PIPE
29x	70	405.09	2709.42	0.00	0.00	0.00	3105.43	1552.91	STRAIGHT PIPE
	71	405.09	3781.04	0.00	0.00	0.00	3785.14	1893.07	STRAIGHT PIPE
30x	72	405.09	3076.94	0.00	0.00	0.00	3440.07	1720.03	STRAIGHT PIPE
	73	2430.56	9312.00	0.00	0.00	0.00	11742.55	5871.28	WELDING TEE
31x	74	2430.56	9312.00	0.00	0.00	0.00	11742.55	5871.28	WELDING TEE
	75	405.09	3214.07	0.00	0.00	0.00	3520.16	1760.08	STRAIGHT PIPE
32x	76	405.09	2233.96	0.00	0.00	0.00	2639.05	1319.53	STRAIGHT PIPE
	77	405.09	844.99	0.00	0.00	0.00	1250.00	625.00	STRAIGHT PIPE
33x	78	405.09	808.31	0.00	0.00	0.00	1213.40	606.70	STRAIGHT PIPE
	79	2430.56	3716.47	0.00	0.00	0.00	4347.52	2173.76	WELDING TEE
34x	80	2430.56	3716.47	0.00	0.00	0.00	4347.52	2173.76	WELDING TEE
	81	2430.56	6968.59	0.00	0.00	0.00	9399.05	4699.53	WELDING TEE

CURVED MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (D)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS (SP)	ALTERNATING STRESS EQ. 1A (SA)	CLASS 1 COMPONENT DESCRIPTION
5c	51	429.99	6915.49	0.00	0.00	0.00	6502.18	4751.05	CURVED PIPE
	52	429.99	4441.66	0.00	0.00	0.00	4947.45	3473.93	CURVED PIPE
6c	54	429.99	3293.60	0.00	0.00	0.00	3727.59	1863.79	CURVED PIPE
	55	429.99	3637.45	0.00	0.00	0.00	4267.64	2133.82	CURVED PIPE
7c	56	429.99	2746.73	0.00	0.00	0.00	3176.72	1588.36	CURVED PIPE
	57	429.99	2161.67	0.00	0.00	0.00	2591.86	1295.83	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (D)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS (SP)	ALTERNATING STRESS EQ. 1A (SA)	CLASS 1 COMPONENT DESCRIPTION
25x	74	405.09	944.30	0.00	0.00	0.00	1371.40	685.70	STRAIGHT PIPE
	75	405.09	469.54	0.00	0.00	0.00	1264.85	632.42	STRAIGHT PIPE
36x	81	405.09	910.32	0.00	0.00	0.00	1315.42	657.71	STRAIGHT PIPE
	82	2430.56	6948.50	0.00	0.00	0.00	9399.05	4699.53	WELDING TEE
37x	83	2430.56	6948.50	0.00	0.00	0.00	9399.05	4699.53	WELDING TEE
	84	405.09	824.72	0.00	0.00	0.00	1233.81	616.91	STRAIGHT PIPE
38x	85	405.09	949.20	0.00	0.00	0.00	1354.38	677.19	STRAIGHT PIPE
	86	405.09	494.82	0.00	0.00	0.00	1309.91	654.96	STRAIGHT PIPE
39x	87	405.09	849.37	0.00	0.00	0.00	1274.47	637.23	STRAIGHT PIPE
	88	2430.56	9047.87	0.00	0.00	0.00	11498.42	5749.21	WELDING TEE
40x	89	2430.56	9047.87	0.00	0.00	0.00	11498.42	5749.21	WELDING TEE
	90	405.09	279.35	0.00	0.00	0.00	644.44	322.22	STRAIGHT PIPE
41x	91	327.59	1474.45	0.00	0.00	0.00	1804.04	902.02	STRAIGHT PIPE
	92	327.59	1347.32	0.00	0.00	0.00	1694.91	847.45	STRAIGHT PIPE
42x	93	327.59	1354.47	0.00	0.00	0.00	1644.06	822.03	STRAIGHT PIPE
	94	327.59	1215.74	0.00	0.00	0.00	1543.32	771.66	STRAIGHT PIPE
43x	95	327.59	1011.11	0.00	0.00	0.00	1338.70	669.35	STRAIGHT PIPE
	96	327.59	1466.59	0.00	0.00	0.00	2194.18	1097.09	STRAIGHT PIPE
44x	97	327.59	1844.59	0.00	0.00	0.00	2194.18	1097.09	STRAIGHT PIPE
	98	327.59	2856.23	0.00	0.00	0.00	3182.81	1591.41	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (D)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS (SP)	ALTERNATING STRESS EQ. 1A (SA)	CLASS 1 COMPONENT DESCRIPTION
13c	80	440.29	2094.74	0.00	0.00	0.00	2535.05	1267.53	CURVED PIPE
	81	440.29	2215.40	0.00	0.00	0.00	2645.72	1322.86	CURVED PIPE
14c	83	441.05	2094.42	0.00	0.00	0.00	2470.87	1235.44	CURVED PIPE
	84	441.05	1079.27	0.00	0.00	0.00	1579.37	789.69	CURVED PIPE
15c	85	440.01	1587.04	0.00	0.00	0.00	1947.10	973.55	CURVED PIPE
	86	440.01	1497.39	0.00	0.00	0.00	1927.31	963.66	CURVED PIPE
16c	89	345.30	1971.34	0.00	0.00	0.00	4247.44	2123.72	CURVED PIPE
	90	345.30	1871.34	0.00	0.00	0.00	4246.88	2123.44	CURVED PIPE
17c	91	345.30	1449.71	0.00	0.00	0.00	3265.01	1632.51	CURVED PIPE
	92	345.30	2895.71	0.00	0.00	0.00	3281.02	1640.51	CURVED PIPE

DESIGN AND STRESS ANALYSIS OF PIPS SECTION LINE 2 - ESCRIB

STRAIGHT MEMBERS FOR RUN 5

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT DESCRIPTION
454	87	1965.52	9047.87	0.00	0.00	0.00	11073.38	5516.89	WELDING TEE
	95	327.59	1394.72	0.00	0.00	0.00	1722.71	841.15	STRAIGHT PIPE
464	98	327.59	1442.48	0.00	0.00	0.00	1790.05	845.02	STRAIGHT PIPE
	97	327.59	1546.79	0.00	0.00	0.00	1874.38	937.19	STRAIGHT PIPE
474	97	327.59	1546.79	0.00	0.00	0.00	1874.38	937.19	STRAIGHT PIPE
	96	327.59	3179.99	0.00	0.00	0.00	3503.58	1741.78	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 5

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT DESCRIPTION
18C	95	395.38	3989.54	0.00	0.00	0.00	4375.84	2187.92	CURVED PIPE
	96	395.38	4116.74	0.00	0.00	0.00	4512.09	2256.04	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT DESCRIPTION
484	73	2439.56	9716.47	0.00	0.00	0.00	12474.02	3073.51	WELDING TEE
	74	405.09	434.41	0.00	0.00	0.00	834.54	419.79	STRAIGHT PIPE
494	75	405.09	304.70	0.00	0.00	0.00	709.79	354.89	STRAIGHT PIPE
	76	405.09	454.15	0.00	0.00	0.00	864.24	432.12	STRAIGHT PIPE
504	76	405.09	454.27	0.00	0.00	0.00	863.26	431.68	STRAIGHT PIPE
	77	405.09	901.57	0.00	0.00	0.00	1308.66	654.33	STRAIGHT PIPE
514	78	405.09	1051.09	0.00	0.00	0.00	1458.12	729.06	STRAIGHT PIPE
	79	2439.56	9312.00	0.00	0.00	0.00	11742.55	5871.28	WELDING TEE

CURVED MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PB)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT DESCRIPTION
19C	74	450.00	1050.25	0.00	0.00	0.00	1500.25	750.12	CURVED PIPE
	79	450.00	734.38	0.00	0.00	0.00	1186.37	593.19	CURVED PIPE
20C	77	450.29	2191.51	0.00	0.00	0.00	2641.80	1320.90	CURVED PIPE
	78	450.29	2554.02	0.00	0.00	0.00	3004.31	1502.15	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF EGCS SUCTION LINE 2 - LAGUNA

STRESSES FOR EXHAUSTION 11 - EXHAUSTION 14  
LOAD SET 2 \* LOAD COMBINATION 6

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (QR)	LINEAR TEMPERATURE GRADIENT (PER)	NONLINEAR TEMPERATURE GRADIENT (PR)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT DESCRIPTION
15	19	405.09	451.44	0.00	0.00	0.00	856.50	428.26	STRAIGHT PIPE
25	29	405.09	371.51	0.00	0.00	0.00	794.00	399.30	STRAIGHT PIPE
35	39	405.09	371.51	0.00	0.00	0.00	794.00	399.30	STRAIGHT PIPE
45	49	405.09	510.30	0.00	0.00	0.00	916.20	457.70	STRAIGHT PIPE
55	59	405.09	510.30	0.00	0.00	0.00	916.20	457.70	STRAIGHT PIPE
65	69	405.09	714.56	0.00	0.00	0.00	1123.66	561.83	STRAIGHT PIPE
75	79	405.09	714.56	0.00	0.00	0.00	1123.66	561.83	STRAIGHT PIPE
85	89	405.09	1004.97	0.00	0.00	0.00	1504.06	752.03	STRAIGHT PIPE
95	99	405.09	1004.97	0.00	0.00	0.00	1504.06	752.03	STRAIGHT PIPE
105	109	405.09	6519.45	0.00	0.00	0.00	6920.42	3460.21	STRAIGHT PIPE
115	119	405.09	2779.88	0.00	0.00	0.00	3144.07	1572.04	STRAIGHT PIPE
125	129	405.09	7647.47	0.00	0.00	0.00	7852.57	3926.28	STRAIGHT PIPE
135	139	405.09	7647.47	0.00	0.00	0.00	7852.57	3926.28	STRAIGHT PIPE
145	149	405.09	3611.69	0.00	0.00	0.00	4016.79	2008.39	STRAIGHT PIPE
155	159	405.09	2741.43	0.00	0.00	0.00	3168.52	1584.26	STRAIGHT PIPE
165	169	405.09	2937.54	0.00	0.00	0.00	3340.53	1670.27	STRAIGHT PIPE
175	179	405.09	2067.97	0.00	0.00	0.00	3368.26	1684.03	STRAIGHT PIPE
185	189	405.09	3341.74	0.00	0.00	0.00	3766.83	1883.42	STRAIGHT PIPE
195	199	405.09	3341.74	0.00	0.00	0.00	3766.83	1883.42	STRAIGHT PIPE
205	209	2430.56	13311.33	0.00	0.00	0.00	15741.89	7870.95	WELDING TEE

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (QR)	LINEAR TEMPERATURE GRADIENT (PER)	NONLINEAR TEMPERATURE GRADIENT (PR)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT DESCRIPTION
1P	31	425.42	4957.79	0.00	0.00	0.00	10378.21	5189.11	CURVED PIPE
2P	36	437.20	4799.30	0.00	0.00	0.00	9499.72	4749.86	CURVED PIPE
3P	37	437.20	7274.68	0.00	0.00	0.00	10655.88	5327.94	CURVED PIPE
4P	37	437.20	5532.61	0.00	0.00	0.00	5969.80	2984.90	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF EGCS SUCTION LINE 2 - LAGUNA

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (QR)	LINEAR TEMPERATURE GRADIENT (PER)	NONLINEAR TEMPERATURE GRADIENT (PR)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT DESCRIPTION
115	40	405.09	9975.41	0.00	0.00	0.00	10340.50	5170.25	STRAIGHT PIPE
125	41	405.09	3199.42	0.00	0.00	0.00	3804.51	1902.26	STRAIGHT PIPE
135	42	405.09	2711.33	0.00	0.00	0.00	3756.42	1878.21	STRAIGHT PIPE
145	43	405.09	2711.33	0.00	0.00	0.00	3756.42	1878.21	STRAIGHT PIPE
155	44	405.09	2711.33	0.00	0.00	0.00	3756.42	1878.21	STRAIGHT PIPE
165	45	405.09	2711.33	0.00	0.00	0.00	3756.42	1878.21	STRAIGHT PIPE
175	46	405.09	1702.39	0.00	0.00	0.00	15741.89	7870.95	WELDING TEE
185	46	405.09	13311.33	0.00	0.00	0.00	15741.89	7870.95	WELDING TEE
195	47	405.09	1901.22	0.00	0.00	0.00	2306.31	1153.16	STRAIGHT PIPE
205	48	405.09	2453.41	0.00	0.00	0.00	2874.50	1437.25	STRAIGHT PIPE
215	49	405.09	11949.51	0.00	0.00	0.00	12254.61	6127.30	STRAIGHT PIPE
225	49	405.09	6711.99	0.00	0.00	0.00	6117.00	3058.50	STRAIGHT PIPE
235	49	405.09	5707.49	0.00	0.00	0.00	6112.58	3056.29	STRAIGHT PIPE
245	49	2430.56	13311.33	0.00	0.00	0.00	15794.40	7897.20	WELDING TEE
255	49	2430.56	13311.33	0.00	0.00	0.00	15794.40	7897.20	WELDING TEE
265	50	405.09	1702.39	0.00	0.00	0.00	17487.48	8743.74	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (QR)	LINEAR TEMPERATURE GRADIENT (PER)	NONLINEAR TEMPERATURE GRADIENT (PR)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT DESCRIPTION
3P	41	425.42	4897.27	0.00	0.00	0.00	5312.69	2656.35	CURVED PIPE
4P	42	425.42	5199.32	0.00	0.00	0.00	5946.74	2973.37	CURVED PIPE
5P	44	437.20	4947.58	0.00	0.00	0.00	5380.78	2690.39	CURVED PIPE
6P	47	437.20	23721.84	0.00	0.00	0.00	24159.04	12079.52	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF PCCS SECTION LINE 2 - LACOUR

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT /-----DESCRIPTION-----
19A	49	2430.56	13763.93	0.00	0.00	0.00	15794.49	7897.24	WELDING TEE
	51	405.09	2531.41	0.00	0.00	0.00	2904.54	1453.45	STRAIGHT PIPE
20A	52	405.09	2575.44	0.00	0.00	0.00	2930.54	1465.29	STRAIGHT PIPE
	53	405.09	4125.14	0.00	0.00	0.00	4533.23	2266.61	STRAIGHT PIPE
21A	53	405.09	4125.14	0.00	0.00	0.00	4533.23	2266.61	STRAIGHT PIPE
	54	405.09	2672.09	0.00	0.00	0.00	3077.74	1538.82	STRAIGHT PIPE
22A	55	405.09	2435.24	0.00	0.00	0.00	3040.37	1520.19	STRAIGHT PIPE
	54	405.09	2213.94	0.00	0.00	0.00	2619.07	1309.54	STRAIGHT PIPE
23A	57	405.09	2526.93	0.00	0.00	0.00	2932.02	1466.01	STRAIGHT PIPE
	58	405.09	4273.97	0.00	0.00	0.00	4679.07	2339.53	STRAIGHT PIPE
24A	58	405.09	4273.97	0.00	0.00	0.00	4679.07	2339.53	STRAIGHT PIPE
	59	405.09	2891.14	0.00	0.00	0.00	3296.23	1648.12	STRAIGHT PIPE
25A	60	405.09	2813.58	0.00	0.00	0.00	3218.67	1609.33	STRAIGHT PIPE
	61	405.09	2954.17	0.00	0.00	0.00	3363.26	1681.63	STRAIGHT PIPE
26A	62	405.09	2472.74	0.00	0.00	0.00	3027.23	1513.62	STRAIGHT PIPE
	63	405.09	2632.85	0.00	0.00	0.00	3037.94	1518.97	STRAIGHT PIPE
27A	63	405.09	2632.85	0.00	0.00	0.00	3037.94	1518.97	STRAIGHT PIPE
	64	405.09	2444.23	0.00	0.00	0.00	3076.32	1538.16	STRAIGHT PIPE
28A	65	405.09	2402.43	0.00	0.00	0.00	3007.52	1503.76	STRAIGHT PIPE
	66	405.09	2729.44	0.00	0.00	0.00	3113.59	1556.79	STRAIGHT PIPE
29A	67	405.09	2512.44	0.00	0.00	0.00	2942.49	1471.25	STRAIGHT PIPE
	68	405.09	2534.66	0.00	0.00	0.00	2939.76	1469.88	STRAIGHT PIPE
30A	69	405.09	4111.56	0.00	0.00	0.00	4516.46	2258.23	STRAIGHT PIPE
	70	2430.56	17844.58	0.00	0.00	0.00	15275.14	7637.57	WELDING TEE
31A	70	2430.56	17844.58	0.00	0.00	0.00	15275.14	7637.57	WELDING TEE
	71	429.99	2544.67	0.00	0.00	0.00	2951.78	1475.89	STRAIGHT PIPE
32A	72	429.99	2518.91	0.00	0.00	0.00	2922.00	1461.00	STRAIGHT PIPE
	73	429.99	404.74	0.00	0.00	0.00	1365.83	684.92	STRAIGHT PIPE
33A	72	429.99	404.74	0.00	0.00	0.00	1365.83	684.92	STRAIGHT PIPE
	73	2430.56	1097.55	0.00	0.00	0.00	8244.11	4144.05	WELDING TEE
34A	73	2430.56	1097.55	0.00	0.00	0.00	8244.11	4144.05	WELDING TEE
	82	2430.56	8650.48	0.00	0.00	0.00	11081.04	5540.52	WELDING TEE

CURVED MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT /-----DESCRIPTION-----
5C	51	405.09	14075.86	0.00	0.00	0.00	14511.45	7255.93	CURVED PIPE
	52	405.09	13794.64	0.00	0.00	0.00	14282.85	7141.42	CURVED PIPE
6C	54	429.99	4410.51	0.00	0.00	0.00	5049.52	2520.26	CURVED PIPE
	55	429.99	4324.12	0.00	0.00	0.00	4956.41	2478.04	CURVED PIPE
7C	56	429.99	3819.29	0.00	0.00	0.00	4249.28	2124.64	CURVED PIPE
	57	429.99	4359.15	0.00	0.00	0.00	4789.14	2394.57	CURVED PIPE

8C	59	424.97	4742.25	0.00	0.00	0.00	5187.22	2593.61	CURVED PIPE
	60	424.97	4271.23	0.00	0.00	0.00	4694.20	2349.10	CURVED PIPE
9C	61	427.50	4952.89	0.00	0.00	0.00	5378.27	2649.13	CURVED PIPE
	62	427.50	5029.43	0.00	0.00	0.00	6357.41	3178.70	CURVED PIPE
10C	64	429.99	4597.73	0.00	0.00	0.00	5027.72	2513.86	CURVED PIPE
	65	429.99	4449.40	0.00	0.00	0.00	4919.39	2459.19	CURVED PIPE
11C	66	430.05	4674.75	0.00	0.00	0.00	5108.79	2554.40	CURVED PIPE
	67	430.05	4392.29	0.00	0.00	0.00	4812.33	2406.17	CURVED PIPE
12C	68	431.42	11239.09	0.00	0.00	0.00	11716.46	5858.23	CURVED PIPE
	69	431.42	13044.90	0.00	0.00	0.00	13550.39	6775.20	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT /-----DESCRIPTION-----
35A	79	405.09	637.94	0.00	0.00	0.00	1033.03	516.51	STRAIGHT PIPE
	80	405.09	424.29	0.00	0.00	0.00	931.34	465.67	STRAIGHT PIPE
36A	81	405.09	964.12	0.00	0.00	0.00	1371.21	685.61	STRAIGHT PIPE
	82	2430.56	8650.48	0.00	0.00	0.00	11081.04	5540.52	WELDING TEE
37A	83	405.09	6650.48	0.00	0.00	0.00	11043.04	5540.52	WELDING TEE
	84	405.09	795.02	0.00	0.00	0.00	1203.11	600.06	STRAIGHT PIPE
38A	84	405.09	964.12	0.00	0.00	0.00	1359.73	679.87	STRAIGHT PIPE
	85	405.09	4134.27	0.00	0.00	0.00	4318.92	2159.46	STRAIGHT PIPE
39A	86	405.09	872.41	0.00	0.00	0.00	1277.50	638.75	STRAIGHT PIPE
	87	2430.56	872.37	0.00	0.00	0.00	11002.93	5501.46	WELDING TEE
40A	87	2430.56	872.37	0.00	0.00	0.00	11002.93	5501.46	WELDING TEE
	88	405.09	279.54	0.00	0.00	0.00	675.73	337.86	STRAIGHT PIPE
41A	88	405.09	1638.39	0.00	0.00	0.00	1757.98	878.94	STRAIGHT PIPE
	89	327.50	4379.73	0.00	0.00	0.00	4799.37	2399.69	STRAIGHT PIPE
42A	90	327.50	1354.34	0.00	0.00	0.00	1485.93	742.96	STRAIGHT PIPE
	91	327.50	1207.03	0.00	0.00	0.00	1316.75	658.38	STRAIGHT PIPE
43A	92	327.50	404.16	0.00	0.00	0.00	1135.44	567.73	STRAIGHT PIPE
	93	327.50	1847.84	0.00	0.00	0.00	2175.44	1087.73	STRAIGHT PIPE
44A	93	327.50	1847.84	0.00	0.00	0.00	2175.44	1087.73	STRAIGHT PIPE
	94	327.50	2041.42	0.00	0.00	0.00	2169.25	1084.63	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 4

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PE)	NONLINEAR TEMPERATURE GRADIENT (PF)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 14 (SA)	CLASS 1 COMPONENT /-----DESCRIPTION-----
13C	81	450.29	1291.31	0.00	0.00	0.00	1731.60	865.80	CURVED PIPE
	81	450.29	2344.64	0.00	0.00	0.00	2794.98	1397.49	CURVED PIPE
14C	83	491.05	4778.43	0.00	0.00	0.00	3270.47	1635.24	CURVED PIPE
	84	491.05	3079.30	0.00	0.00	0.00	3070.35	1535.17	CURVED PIPE
15C	85	450.01	1572.58	0.00	0.00	0.00	2002.59	1001.29	CURVED PIPE
	86	450.01	1404.50	0.00	0.00	0.00	1932.52	966.26	CURVED PIPE
16C	89	327.30	3221.49	0.00	0.00	0.00	4371.79	2185.89	CURVED PIPE
	91	327.30	3474.71	0.00	0.00	0.00	4772.01	2386.00	CURVED PIPE
17A	91	327.30	3474.71	0.00	0.00	0.00	4772.01	2386.00	CURVED PIPE
	92	327.30	2405.94	0.00	0.00	0.00	3201.24	1600.62	CURVED PIPE

SEISMIC AND STRESS ANALYSIS OF FCCS SUCTION LINE 2 - LACARB

STRAIGHT MEMBERS FOR RUN 5

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 1A (SA)	CLASS 1 COMPONENT / DESCRIPTION
454	87	1945.52	2572.37	0.00	0.00	0.00	10537.49	5244.94	WELDING TEE
	95	327.59	1243.98	0.00	0.00	0.00	1611.57	805.74	STRAIGHT PIPE
465	94	327.59	1404.10	0.00	0.00	0.00	1735.72	847.88	STRAIGHT PIPE
	97	327.59	1344.84	0.00	0.00	0.00	1716.45	854.22	STRAIGHT PIPE
475	97	327.59	1344.84	0.00	0.00	0.00	1716.45	854.22	STRAIGHT PIPE
	98	327.59	2491.21	0.00	0.00	0.00	3218.70	1494.40	STRAIGHT PIPE

CURVED MEMBERS FOR RUN 5

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 1A (SA)	CLASS 1 COMPONENT / DESCRIPTION
18C	95	395.30	3644.41	0.00	0.00	0.00	4059.79	2029.89	CURVED PIPE
	96	395.30	4018.95	0.00	0.00	0.00	4414.25	2207.13	CURVED PIPE

STRAIGHT MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 1A (SA)	CLASS 1 COMPONENT / DESCRIPTION
484	73	2430.56	5457.55	0.00	0.00	0.00	8244.11	4144.05	WELDING TEE
	74	405.09	681.10	0.00	0.00	0.00	1046.19	543.10	STRAIGHT PIPE
494	75	405.09	344.75	0.00	0.00	0.00	749.04	374.92	STRAIGHT PIPE
	76	405.09	447.43	0.00	0.00	0.00	992.96	496.48	STRAIGHT PIPE
505	76	405.09	590.51	0.00	0.00	0.00	995.60	497.80	STRAIGHT PIPE
	77	405.09	1194.72	0.00	0.00	0.00	1599.81	799.91	STRAIGHT PIPE
514	76	405.09	1714.24	0.00	0.00	0.00	2116.33	1058.17	STRAIGHT PIPE
	70	2430.56	12844.50	0.00	0.00	0.00	15275.14	7637.57	WELDING TEE

CURVED MEMBERS FOR RUN 6

MEMBER NO.	MEMBER ENDS	LOCAL MEMBRANE STRESS (PL)	BENDING STRESS (PR)	THERMAL DISCONT. STRESS (Q)	LINEAR TEMPERATURE GRADIENT (PF)	NONLINEAR TEMPERATURE GRADIENT (F)	PEAK STRESS EQ. 11 (SP)	ALTERNATING STRESS EQ. 1A (SA)	CLASS 1 COMPONENT / DESCRIPTION
19C	74	450.00	1444.04	0.00	0.00	0.00	2054.06	1048.03	CURVED PIPE
	79	450.00	237.17	0.00	0.00	0.00	1283.47	641.58	CURVED PIPE
207	77	450.29	2897.46	0.00	0.00	0.00	3347.94	1673.98	CURVED PIPE
	78	450.29	4150.42	0.00	0.00	0.00	4600.71	2300.36	CURVED PIPE