

SEISMIC AND STRESS ANALYSIS OF LACBWR  
MAIN STEAM PIPING SYSTEM

Prepared Under NES Project 5101 for  
DAIRYLAND POWER COOPERATIVE

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### VOLUME II

COMPUTER OUT - PIPESD Static and Dynamic Analysis of LACBWR Main Steam Piping System.

## 1. SUMMARY

This report, prepared for Dairyland Power Cooperative, presents the results of seismic and stress analyses of the main steam piping system for the LACBWR Nuclear Power Station. The seismic and stress analyses are performed in accordance with the design requirements for Class 2 piping components of the ASME Boiler and Pressure Vessel Code, Section III, Division 1, "Nuclear Power Plant Components", 1974. By providing adequate seismic restraints (snubbers) at critical locations of the main steam system, the stresses in the piping due to a seismic event have been reduced to acceptable values. It is concluded that the stresses due to seismic, dead weight, pressure and thermal expansion loadings, combined according to the ASME Code rules for Class 2 components, satisfy the design requirements given in the Code.

## 2. INTRODUCTION

In response to AEC/DL's request to review the effects of an earthquake event on the LaCrosse Boiling Water Reactor, Dairyland Power Cooperative requested Gulf United Nuclear Fuels Corporation to evaluate the adequacy of the major structures and equipment to withstand seismic loadings. The seismic study performed by Gulf United (GU) Nuclear Fuels Corporation (Ref. 1) included an analysis of the main steam line which indicated that high stresses would be generated in the main steam line during a seismic event. It was also evident from these analyses that the LACBWR piping systems, in general, were not designed to accommodate horizontal accelerations, the primary earthquake induced loading condition. Anticipating the possibility of a seismically induced loss of coolant accident, it was, therefore, concluded that analyses of the major Class 1 piping systems should be performed to evaluate their structural integrity.

In order to verify that the seismic stresses are acceptable, it is necessary to show that the combined stresses in the piping system are within ASME Boiler and Pressure Vessel Code allowable values. This requires that the seismic stresses be combined with the stresses due to deadweight, pressure and thermal loadings in accordance with the ASME Code Section III rules (Ref. 2).

The rules for a Class I (Section III) analysis require that thermal stress and fatigue due to thermal cycling be considered. A review of the available main steam piping system flexibility and stress analyses indicated that only thermal expansion was considered together with the pressure and deadweight loads in the original design. Consequently, it is not possible to perform a Class I analysis with the existing analytical data.

The existing analytical data, however, is sufficient to perform a Class 2 (Section III) analysis. Therefore, in the subject analysis, the adequacy of the main steam piping system to withstand an earthquake event is evaluated by combining the stresses due to deadweight, pressure, thermal and seismic loadings in accordance with ASME Code requirements for the design of Class 2 components. It should be noted that the requirements of the ASME Code, Section III, for the design of Class 2 components are much more rigorous than the design requirements given in the Power Piping Code, USAS B31.1.0 (The applicable code for the LACBWR Project).

Section 3.0 of this report describes the scope of the main steam piping system considered in the analysis. The loading criteria, design criteria and analytical methods used in the analyses are given in Sections 4.0, 5.0 and 6.0 respectively. The results of the analysis are discussed in Section 7.0. The conclusions and recommendations are summarized in Section 8.0.



### 3. PIPING SYSTEM DESCRIPTION

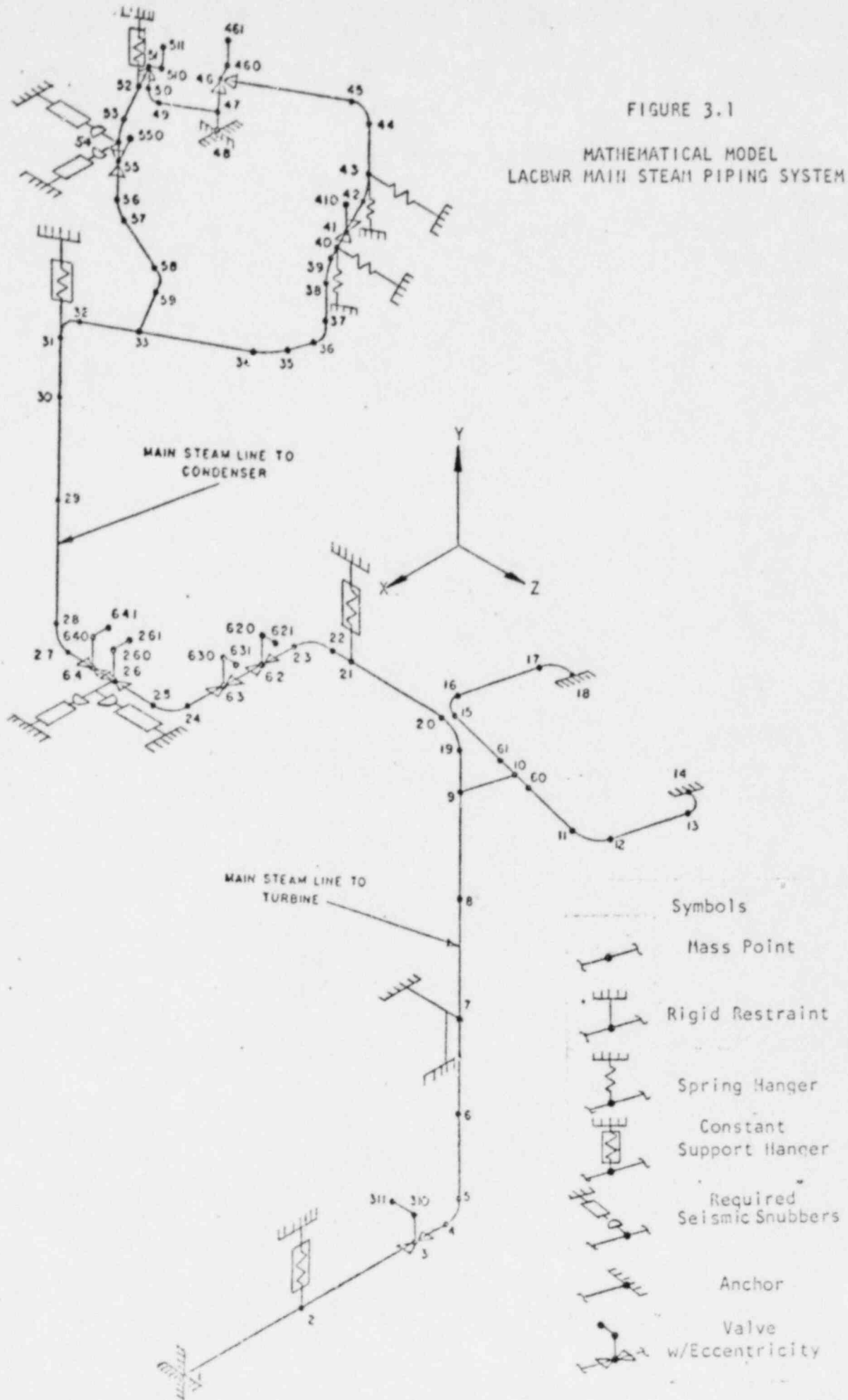
The main steam piping system within the containment shell carries steam from the reactor vessel to either the turbine building or the shutdown condenser. Steam is withdrawn from the reactor vessel through two 8-inch steam lines leading to a single 10-inch line. The steam passes out of the biological shield and through a rotoport steam isolation valve in the 10-inch line before leaving the containment shell for the turbine building. Within the biological shield, the 10-inch steam line branches upward and out of the biological shield to the main steam safety valves. The line then continues upward in the form of a 6-inch line to the shutdown condenser via a redundant system of control valves.

The governing design specification used in the analysis of the main steam piping system is given in Reference 3. The piping arrangement analyzed and piping suspension (hangers, etc.) characteristics have been taken from the drawings listed in Reference 4. Piping properties have been taken from the information given in Reference 5 and from the piping specification (Ref.3). This information is summarized in Table A-1 of Appendix A.


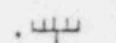
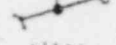




An isometric drawing showing the main steam piping system as analyzed, including the suspension system and recommended seismic snubbers, is given in Figure 3.1.

FIGURE 3.1

MATHEMATICAL MODEL  
LACBWR MAIN STEAM PIPING SYSTEM



Symbols

-  Mass Point
-  Rigid Restraint
-  Spring Hanger
-  Constant Support Hanger
-  Required Seismic Snubbers
-  Anchor
-  Valve w/Eccentricity

## 4. LOADING CRITERIA

The load cases which must be considered in performing a Class 2 stress analysis include: dead loads and sustained mechanical loads, internal pressure, thermal expansion loading, seismic inertia loads and seismic anchor movement loading. The static and dynamic load cases are summarized in Tables A-III and A-IV of Appendix A.

### 4.1 Dead Weight and Other Sustained Mechanical Loads (Static Load Case 1)

The dead weight of the piping system is calculated assuming the system to be insulated and filled with water. The weight of valves, valve operators, and branch piping are included in the analysis. Valve weights and dimensions are taken from vendor drawings and specifications supplied by DPC and are given in Table A-II of Appendix A. Sustained loads imposed on the piping system by constant load hangers are also considered in the dead weight analysis. These loads are taken from Ref. 4 drawings.

### 4.2 Internal Pressure (Static Load Cases 2 and 3)

System normal operating pressure, Load Case 2, and peak pressure, Load Case 3, used in the analysis are taken from Refs. 3 and 6. A value of 1300 psia for operating pressure and 1415 psia for peak pressure are used for most of the piping system. A peak pressure of 1300 psia is used in the section between the containment vessel and the rotoport isolation valve (Nodes 1 through 3).

### 4.3 Thermal Loading (Static Load Case 4)

The thermal expansion stresses are based on the thermal loading resulting from the normal operating temperature of 577.5°F.

Thermal anchor movements at the nozzle connections to the pressure vessel are calculated based on the thermal expansion of the pressure vessel at the design temperature of 577.5°F.

### 4.4 Seismic Loading

A dynamic analysis of the piping system is performed using the response spectrum method of analysis (Section 6.4). Two seismic loading events are considered: the safe shutdown earthquake (SSE), and the operating basis earthquake (OBE). The established design criteria (Ref. 7, Reg. Guide 1.48, May 1973) for Class 2 analysis considers the OBE (or 1/2 SSE) to be the normal and upset condition while the SSE is considered the faulted condition.

Seismic inertia loading is imposed on the piping system in the form of seismic acceleration spectra which were derived for the LACBWR plant (Ref. 1). The horizontal acceleration spectrum used for the main steam line is that corresponding to the reactor vessel at an elevation of 664.5 feet. The vertical response spectrum for the SSE loading is taken as 2/3 of the horizontal SSE ground response spectrum assuming no amplification of vertical response in the structure. For the operating basis earthquake the vertical piping response spectrum is taken as 1/2 of the SSE vertical response spectrum. Damping values used are 1 percent for the OBE and 2 percent for the SSE.

The horizontal spectra in either the global X- direction (Dynamic Load Cases 8 and 10) or the global Z- direction (Dynamic Load Cases 9 and 11) are applied simultaneously with the vertical spectra in the global Y- direction. Load Cases 8 and 9 represent the operating bases earthquake while 10 and 11 represent the SSE earthquake. The applicable response spectra used in the analysis for dynamic load cases are shown in Table A-V of Appendix A.

Seismically induced anchor movements (Static Load Cases 6,7,12, and 13) for points 7, 14,18, 40, 42, and 48 were estimated by calculating low frequency displacements from the containment vessel response spectra at the different anchor point elevations.

## 5. STRESS ACCEPTANCE CRITERIA

The requirements for acceptability of a Class 2 piping system are given in AEC regulatory position 8 of Reference 7 and Section NC-3611 of Reference 2. Calculated stresses resulting from specified load combinations must meet the stress limits of equations 8 through 11 (Section 6.5).

### 5.1 Normal Operating Conditions

Under normal operating conditions, the combined stresses due to design pressure, weight, and other sustained loads (load Cases 1 and 2) must not exceed the basic material allowable stress at maximum temperature,  $S_H$ , and the requirements of Equation 8, Section 6.5. Additionally, either the stress range due to thermal expansion and seismic anchor movements (Load Cases 4 and 6) as calculated by Equation 10, Section 6.5, must not exceed the allowable expansion stress range  $S_A$  (Reference 2), or the combined stresses due to design pressure, weight, other sustained loads and the stress range due to thermal expansion (Load Cases 1, 2, 4 and 6 or 7) must not exceed the sum of  $S_A$  and  $S_H$  as required by Equation 11, Section 6.5.

### 5.2 Upset Conditions

The requirements for operation under upset conditions include compliance with the requirements of Equations 8, 10 and 11 as described above as well as Equation 9, Section 6.5. Equation 9 requires that the combined stresses produced by peak pressure (Load Case 3), live and dead loads (Load Case 1), and those produced by occasional loads -- in this analysis defined as the OBE earthquake -- (Load Cases 8 and 9), must not be greater than 1.2 times the allowable stress value  $S_H$ .

### 5.3 Faulted Conditions

During faulted conditions, the requirements of Equation 9 must be met using a stress limit of  $1.8 S_H$ . For the purpose of satisfying this criteria, the faulted conditions are specified as peak pressure loads (Load Case 3), live and dead loads (Load Case 1), the SSE seismic inertia loadings (Load Cases 1 and 11) and the seismic anchor movement loads associated with the SSE (Load Cases 12 and 13).

## 6. ANALYTICAL METHODS

### 6.1 Mathematical Model

In order to perform static, dynamic and stress analyses, the continuous piping system is mathematically modeled as an assembly of elastic structural elements interconnected at discrete nodal points (Figure 3.1). Nodal points are located at all points of interest in the piping system such as elbows, valves, anchorages, hangers, tee intersections, load points, all structural and material discontinuities, etc. This three dimensional multidegree-of-freedom model of the piping system is attached to the "ground" (structure) by means of rigid hangers, support springs, hydraulic snubbers and anchors. Stiffness characteristics of structural elements are related to the moment of inertia and the axial and effective shear area of the pipe cross section. The stiffness characteristics of the elbows and tee connections are modified to account for local deformation by using the flexibility factors given in the ASME Code (Ref. 2).

For the seismic analysis the distributed mass of the piping system is lumped at the system nodal points. Masses are lumped so that the lumped mass, multi-degree-of-freedom model represents the dynamic characteristics of the piping system. In order to reduce the number of dynamic degrees-of-freedom, only translational degrees-of-freedom are considered at each mass point (the masses associated with the rotational degrees-of-freedom are set to zero). This assumption has been shown to be completely satisfactory for accurate analysis of seismic response. Special items such as valves and actuators are modeled by lumping their masses at an appropriate offset from the center-line of the piping system.

### 6.2 Static Load Analysis

The static load analysis involves the application of the following loading conditions and their combinations:

- . Design Pressure
- . Gravity Loading (dead weight) and Sustained Mechanical Loads
- . Support Displacement
- . Thermal Expansion

For the pressure loadings, the hoop and longitudinal stresses in the affected piping are calculated using the formulae given in the Code (see Section 6.5).

For the deadweight, support displacement, or thermal expansion loading conditions the following equations of equilibrium written in matrix form are solved:

$$KU = P \quad (1)$$

where:

$K$  = System stiffness matrix

$U$  = Nodal point displacement vector

$P$  = External forces, dead weight or equivalent thermal load vector.

The system stiffness matrix is obtained from element stiffness matrices using direct stiffness methods. The unknown nodal displacements  $U$  are obtained as follows:

$$U = K^{-1}P \quad (2)$$

The inversion of the stiffness matrix is performed using the Gauss-Siedel technique.

From the nodal displacements  $U$ , the member internal forces are determined using the member stiffness matrix. Finally the member internal forces are used in calculating the stresses.

### 6.3 Eigenvalue Analysis

The eigenvalues (natural frequencies) and the eigenvectors (mode shapes) for each of the natural modes of vibration are calculated by solving the following frequency equation:

$$\left[ K - \omega_n^2 M \right] \left\{ \phi_n \right\} = \left\{ 0 \right\} \quad (3)$$

where:

$\omega_n$  = Natural angular frequency for the  $n^{\text{th}}$  mode

$M$  = System mass matrix

$\phi_n$  = Mode shape vector for the  $n^{\text{th}}$  mode

$0$  = Null vector

The eigenvalue/eigenvector extraction is performed using the Householder-QR technique.

#### 6.4 Dynamic (Seismic) Load Analysis

Considering only translational degrees of freedom and assuming viscous (velocity proportional) form of damping, the equation of motion in matrix form can be expressed as follows:

$$M(\ddot{U}_t + \ddot{U}_{gt}) + C\dot{U}_t + KU_t = 0 \quad (4)$$

where:

$\ddot{U}_t$  = Relative acceleration time history vector

$\ddot{U}_{gt}$  = Ground acceleration time history vector

C = Damping matrix

$\dot{U}_t$  = Velocity time history vector

$U_t$  = Relative displacement time history vector

Rearranging equation (4)

$$M\ddot{U}_t + C\dot{U}_t + KU_t = -M\ddot{U}_{gt} = P_{eff} \quad (5)$$

To uncouple equation (5), assume

$$U = \Phi Y_t$$

where:

$\Phi$  = Characteristic free vibration mode shapes matrix.

$Y_t$  = Generalized coordinate displacement time history vector.

Pre-and post-multiplying equation (5) by the transpose of  $\Phi$  and by  $\Phi$  respectively and using orthogonality conditions, the following uncoupled equations of motion are obtained:

$$\ddot{Y}_{nt} + 2\omega_n \lambda_n \dot{Y}_{nt} + \omega_n^2 Y_{nt} = M_n^{*-1} R_n \ddot{U}_{gt} \quad (6)$$

where:

$Y_{nt}$  = Generalized displacement coordinate time history for nth mode

$\lambda_n$  = Damping ratio for the nth mode expressed as percent of critical damping

$M_n^*$  = Generalized mass for the nth mode

$$= \Phi_n^T M \Phi_n = M_i \Phi_{in}^2$$



The mode shape  $\phi_n$  is normalized such that  $M_n^* = 1$

$R_n$  = Participation factor for the  $n^{\text{th}}$  mode

$$= \phi_n^T M I = \sum M_i \phi_{i,n}$$

$I$  = Column vector whose elements are generally unity

The solution for the differential equation (6) is given by the Duhamel Integral

$$Y_{nt} = \frac{R_n}{M_n^* \omega_n} \int_0^t \ddot{u}_{gt} e^{-\lambda_n \omega_n (t-\tau)} \sin \omega_n (t-\tau) d\tau$$

Using the response spectrum method of analysis, the maximum values of the generalized response for each mode is given by:

$$\ddot{Y}_{n \max} = \frac{R_n S_{an}}{M_n^*} \quad (7)$$

where:

$\ddot{Y}_{n \max}$  = Maximum generalized coordinate acceleration response for the  $n^{\text{th}}$  mode.

$S_{an}$  = Spectral acceleration value for the  $n^{\text{th}}$  mode (from the applicable response spectrum curve)

From the maximum generalized coordinate response, the maximum acceleration ( $\ddot{U}_{n \max}$ ) and maximum inertia forces ( $F_{n \max}$ ) at each mass point are given by:

$$\ddot{U}_{n \max} = \ddot{Y}_{n \max} \phi_{i,n}$$

$$F_{n \max} = M_n \ddot{U}_{n \max}$$

The inertia forces ( $F_{n \max}$ ) for each of the system natural modes are applied as external static forces, and the piping system response (displacements, member internal forces and stresses) are calculated using the procedure described in Section 4.2. Total system response is then obtained by combining the individual modal response values by the square-root of the sum of the squares method; lower modes having large contribution to the response (all modes having natural frequency under 30 cycles per second) are considered and higher modes with negligible participation are neglected.

## 6.5 Stress Analysis

The design requirements of the ASME Code for Class 2 piping systems are satisfied when the calculated stresses in the piping system due to thermal expansion, weight, and other sustained and occasional loads are combined in accordance with and meet the limitations of, equations 8,9,10,and 11 of Subsection NC-3652 of Reference 8. These requirements are described below:

### A. Sustained Loads

The effects of pressure weight and other sustained mechanical loads must meet the requirements of equation (8).

$$S_{SL} = \frac{PD_o}{4t_n} + \frac{0.75iM_A}{Z} \leq 1.0S_h \quad (8)$$

where:

P = Internal design pressure, psi

D<sub>o</sub> = Outside diameter of pipe, in.

t<sub>n</sub> = Nominal wall thickness, in.

M<sub>A</sub> = Resultant moment loading on cross section due to weight and other sustained loads, in. (See NC-3652.4, Ref.8)

Z = Section modulus of pipe, in.<sup>3</sup> (See NC-3652.4, Ref.8)

i = Stress intensification factor (NC-3673.2 (b), Ref.8)  
The product of 0.75i shall never be taken as less than 1.0

S<sub>h</sub> = Basic material allowable stress at design temperature

### B. Occasional Loads

The effects of pressure, weight, other sustained loads and occasional loads including earthquake must meet the requirements of Equation (9).

$$S_{OL} = \frac{P_{max}D_o}{4t_n} + \frac{0.75i(M_A + M_B)}{Z} \leq 1.2S_h \quad (9)$$

where:

P<sub>max</sub> = Peak pressure, psi

M<sub>B</sub> = Resultant moment loading on cross section due to occasional loads such as earthquake loads

C. Thermal Expansion

The requirements of either Equation (10) or Equation (11) must be met.

1. The effects of thermal expansion must meet the requirements of Equation (10)

$$S_{TE} = \frac{iM_C}{Z} \leq S_A \quad (10)$$

where:

$M_C$  = Range of resultant moments due to thermal expansion. Also include moment effects of anchor displacements due to earthquake if anchor displacement effects were omitted from Equation (9)

$S_A$  = Allowable stress range for expansion stresses (NC-3611.2, Ref.8)

2. The effects of pressure, weight, other sustained loads and thermal expansion shall meet the requirements of Equation (11)

$$S_{TE} = \frac{PD_o}{4t_n} + 0.75i \frac{M_A}{Z} + \frac{iM_C}{Z} \leq (S_h + S_A) \quad (11)$$

The above mentioned static, dynamic and stress analyses are carried out using the PIPESD computer code. PIPESD was developed by URS/John A. Blume and Associates, Engineers, San Francisco, California and has been extensively used in the seismic and stress analysis of piping system for a number of nuclear power plants. PIPESD is available to Nuclear Energy Services through the Control Data Corporation CYBERNET Service.

## 7. DISCUSSION OF RESULTS

A preliminary seismic analysis of the main steam piping system with its existing support configuration indicated that the stresses due to the operating basis earthquake would be substantially greater than the allowable stress values at critical locations (particularly in the vicinity of nodes 53 and 54). In addition, this preliminary analysis indicated that, in the relatively long steam line leading to the shutdown condenser, lateral deflections due to the seismic inertia loads would be of the order of 5 to 6 inches. In order to reduce the seismic stresses and deflections to acceptable values four seismic snubbers were located at critical locations in the piping system as shown in Figure 3.1. The results presented in this report represent the response of this modified system configuration.

The natural frequencies for the first 32 modes of vibration of the piping system are summarized in Table 7-1, from which it may be seen that the piping system is a fairly flexible (low frequency) system.

The deflections at each node point due to the various load cases are summarized in Table B-1, pages B-1 through B-10 of Appendix B. The maximum deflection due to the SSE seismic inertia loading (Load Case 10) is 0.58 inches at node point 31. For a flexible piping system this deflection should be acceptable. The maximum deflection due to thermal expansion (Load Case 4) is 1.8 inches at node 29. Table B-11, pages B-11 through B-14 of Appendix B, summarizes the elastic support reaction forces. The seismic restraints and anchors should be designed (sized) using these restraint forces. The maximum reaction force in these seismic restraints is 980 pounds (Load Case 11).

The results of the detailed stress analysis in accordance with the requirements of Subarticle NC 3652 of the ASME Code for the Class 2 piping system are given in Table B-111, pages B-15 through B-41 of Appendix B. Figures 7.1 through 7.9 indicate node points with maximum stresses or stresses exceeding 10.0 ksi for specified Class 2 load conditions. From these stress results summaries, it may be seen that code allowable stress values are not exceeded.

TABLE 7-1

## NATURAL FREQUENCIES OF VIBRATION

<u>Mode No.</u>	<u>Frequency (CPS)</u>
1	3.0511
2	4.1689
3	4.5762
4	4.8482
5	5.5088
6	6.1582
7	6.5564
8	7.4169
9	8.9696
10	9.6125
11	10.7147
12	11.3881
13	12.4584
14	13.2577
15	14.0559
16	14.3915
17	15.0682
18	16.6528
19	17.3994
20	17.5007
21	19.0081
22	21.1871
23	21.9415
24	22.5624
25	23.5551
26	23.7430
27	26.4039
28	27.1295
29	28.5522
30	29.5071
31	31.1632
32	31.3518

FIGURE 7.2

COMPLIANCE WITH ASME CODE EQUATION 9  
Upset Conditions

Applied Loads	
Peak Pressure Dead Weight & Other Sustained Mechanical Loads X + Y Earthquake ( $\frac{1}{2}$ SSE)	
Allowable Stress, $1.2 S_h$	= 18.0 KSI
Maximum Stress at Node $h_1$	= 11.8 KSI

(Stresses Greater Than 10.0 KSI Indicated)

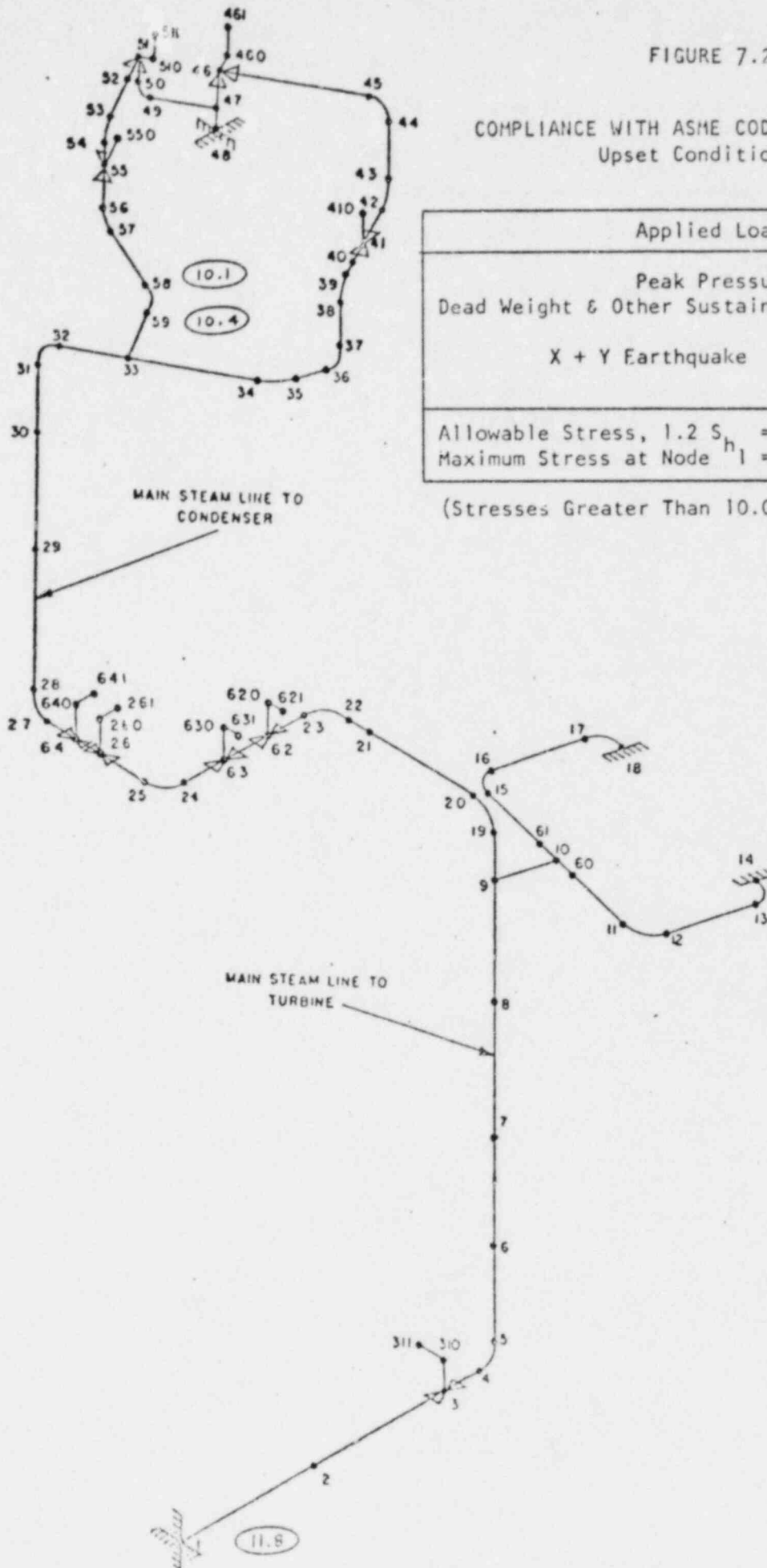


FIGURE 7.3

COMPLIANCE WITH ASME CODE EQUATION 9  
Upset Conditions

Applied Loads
Peak Pressure Dead Weight & Other Sustained Mechanical Loads Z + Y Earthquake ( $\frac{1}{2}$ SSE)
Allowable Stress, $1.2 S_h = 18.0$ KSI Maximum Stress at Node 59 = 10.4 KSI

(Stresses Greater Than 10.0 KSI Indicated)

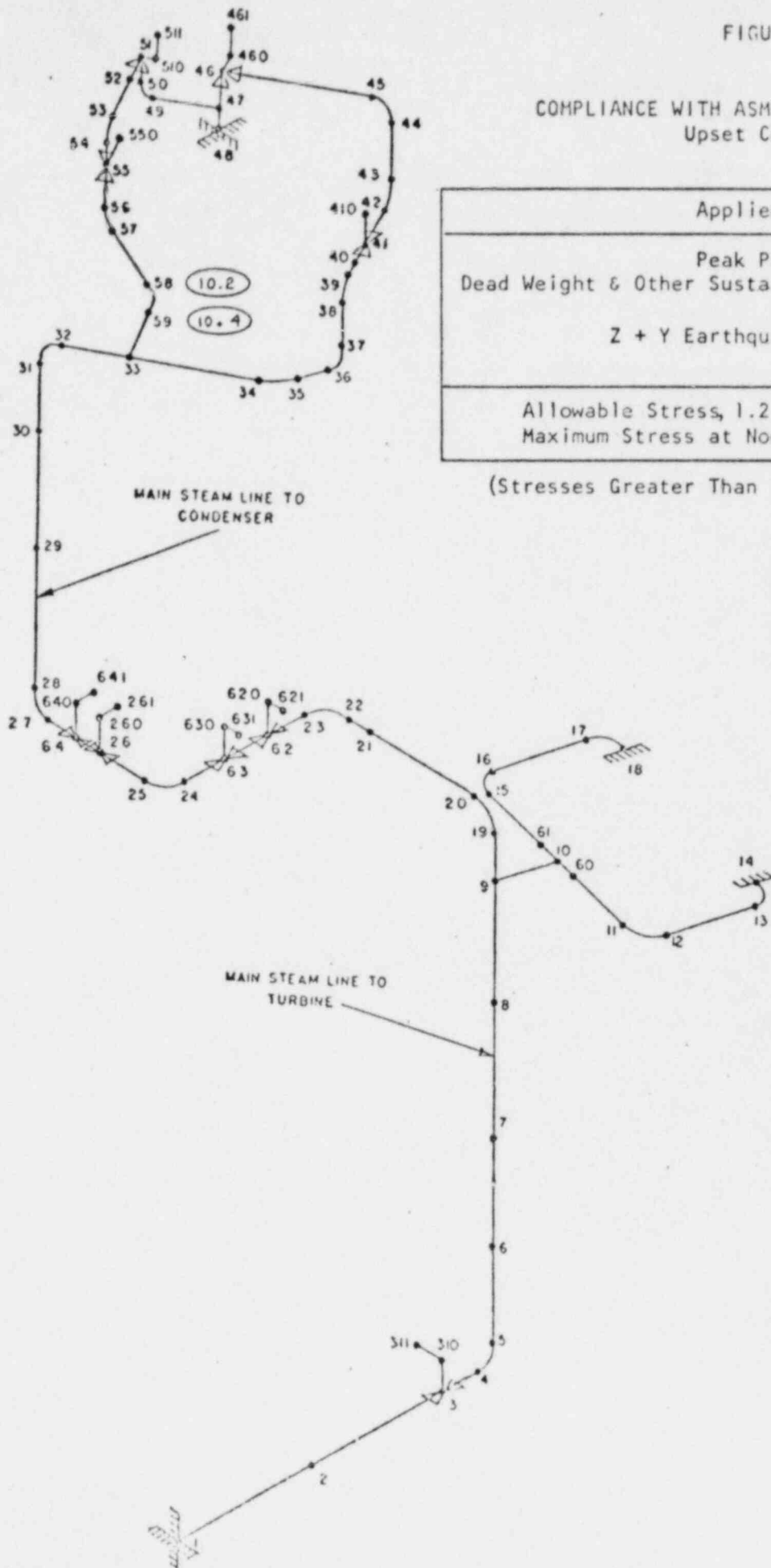


FIGURE 7.4

COMPLIANCE WITH ASME CODE EQUATION 10  
Normal Operating and Upset Conditions

Applied Loads	
Design Temperature	
Thermal Anchor Movements	
Seismic Anchor Movements (X-direction)	
Allowable Stress, $S_A$	= 19.1 KSI
Maximum Stress at Node 1	= 16.6 KSI

(Stresses Greater Than 10.0 KSI Indicated)

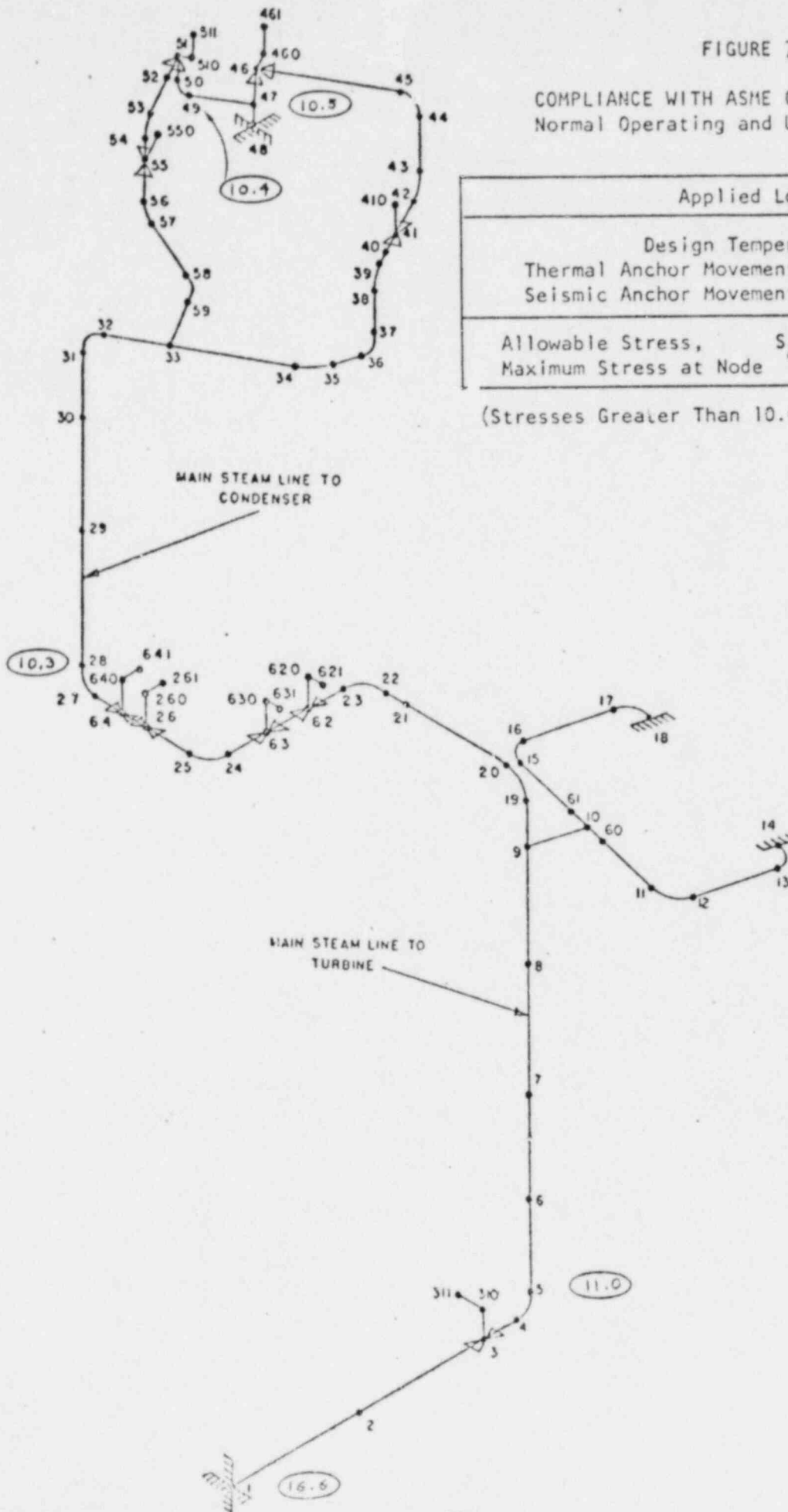
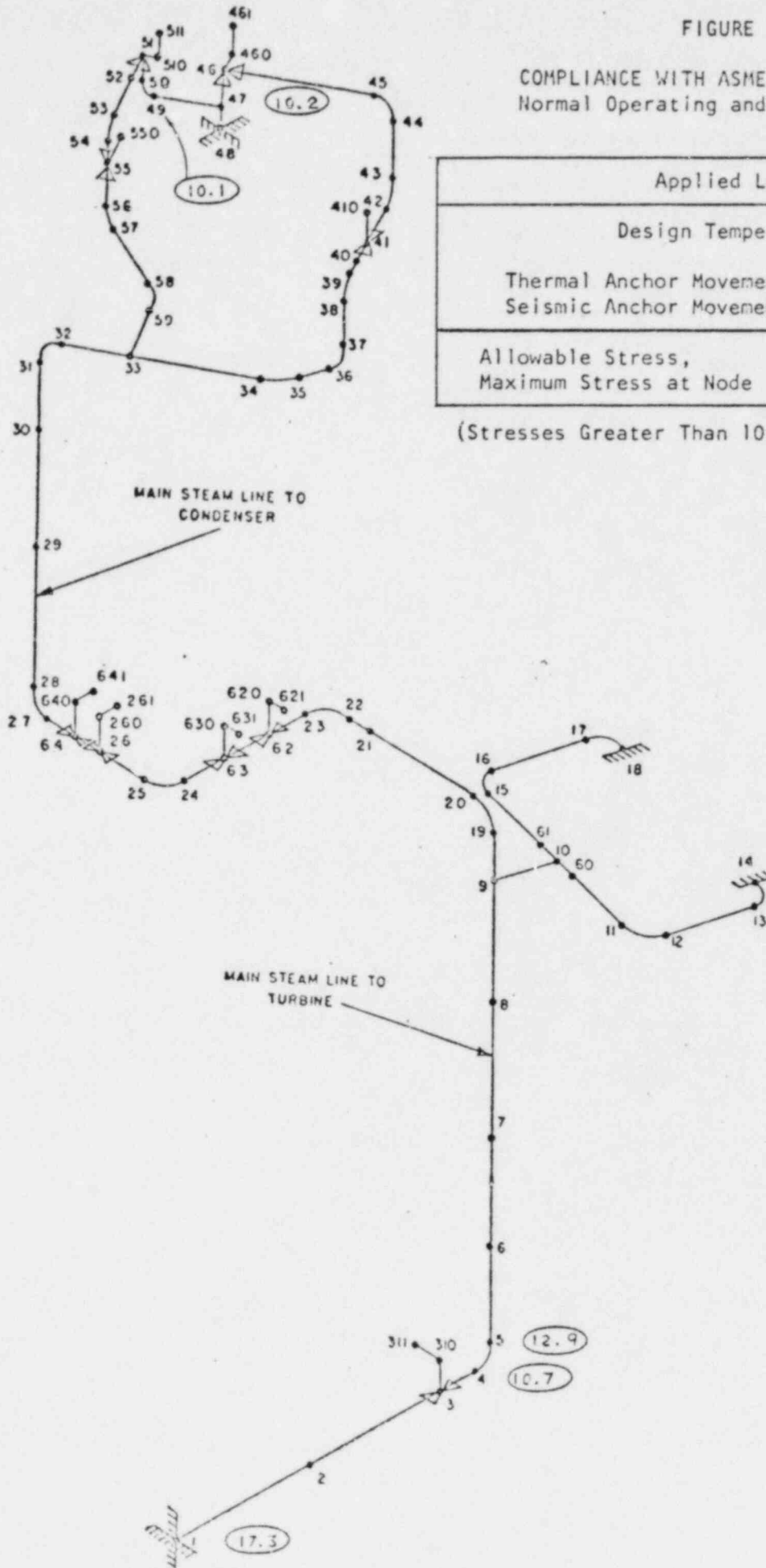




FIGURE 7.5

COMPLIANCE WITH ASME CODE EQUATION 10  
Normal Operating and Upset Conditions



Applied Loads	
Design Temperature	
Thermal Anchor Movements	
Seismic Anchor Movements (Z-direction)	
Allowable Stress, $S_A$	= 19.1 KSI
Maximum Stress at Node 1	= 17.3 KSI

(Stresses Greater Than 10.0 KSI Indicated)

FIGURE 7.6

COMPLIANCE WITH ASME CODE EQUATION 11  
Normal Operating And Upset Conditions

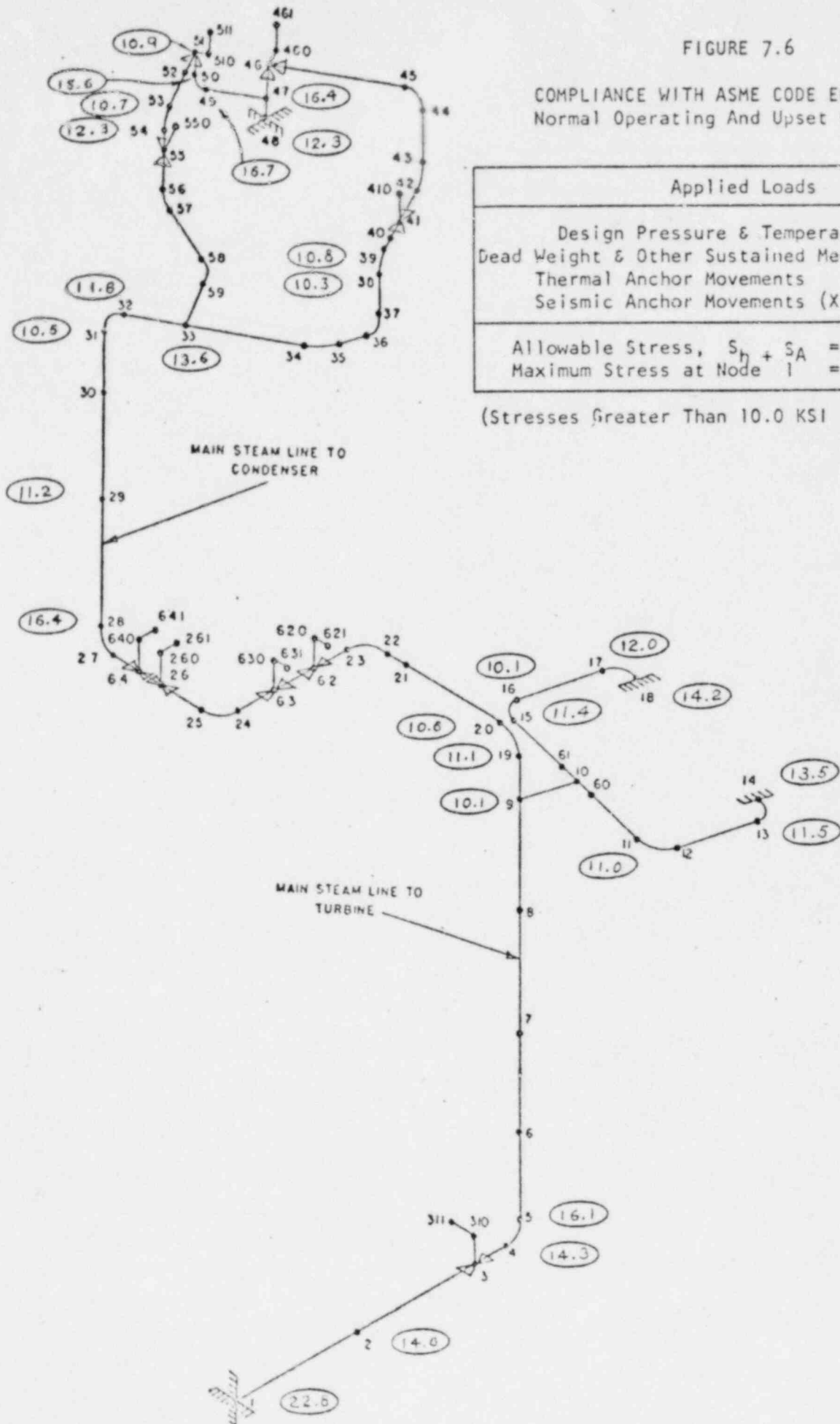


FIGURE 7.7

COMPLIANCE WITH ASME CODE EQUATION 11  
Normal Operating and Upset Conditions

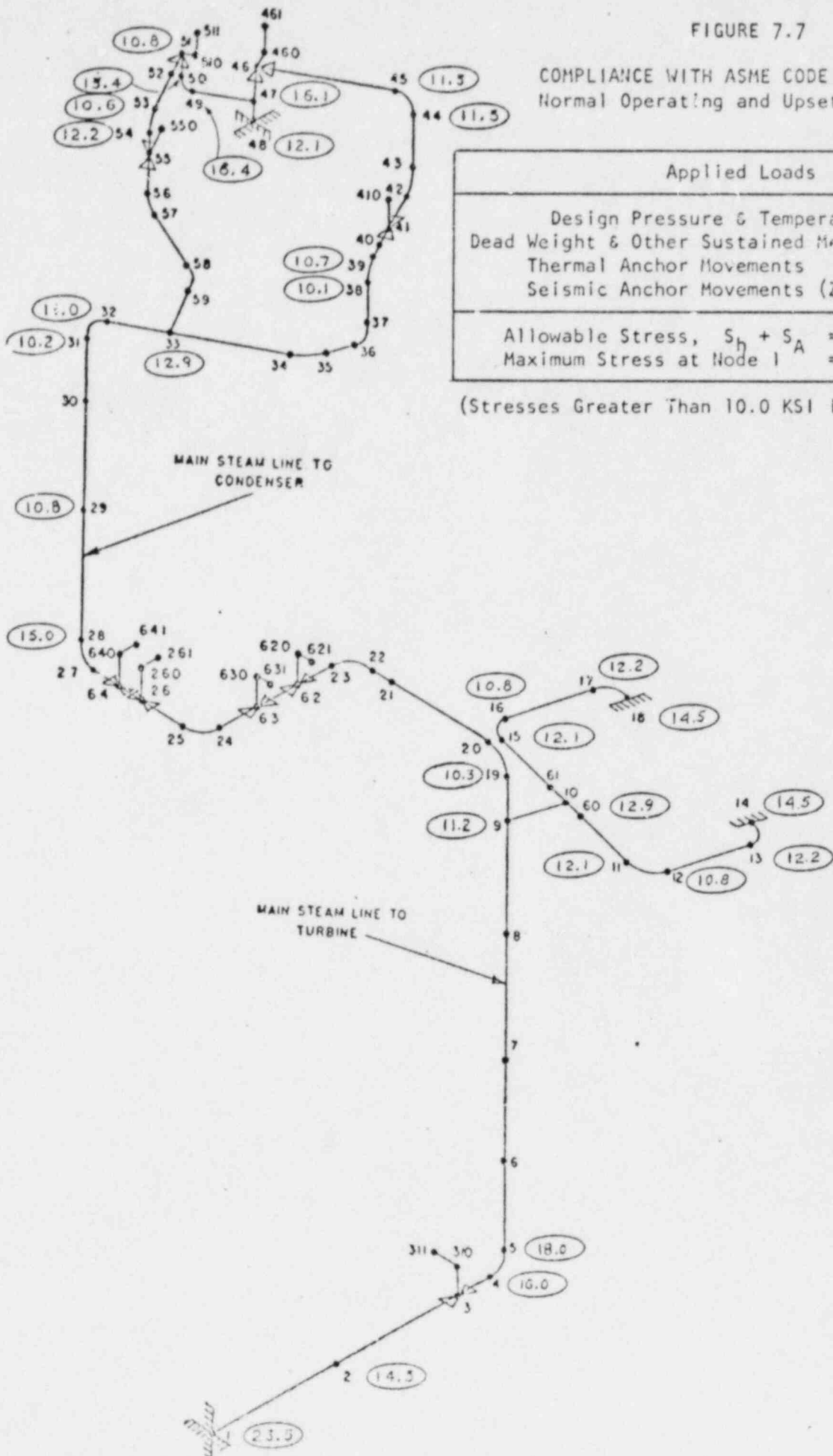


FIGURE 7.8

COMPLIANCE WITH ASME CODE EQUATION 9  
Faulted Conditions

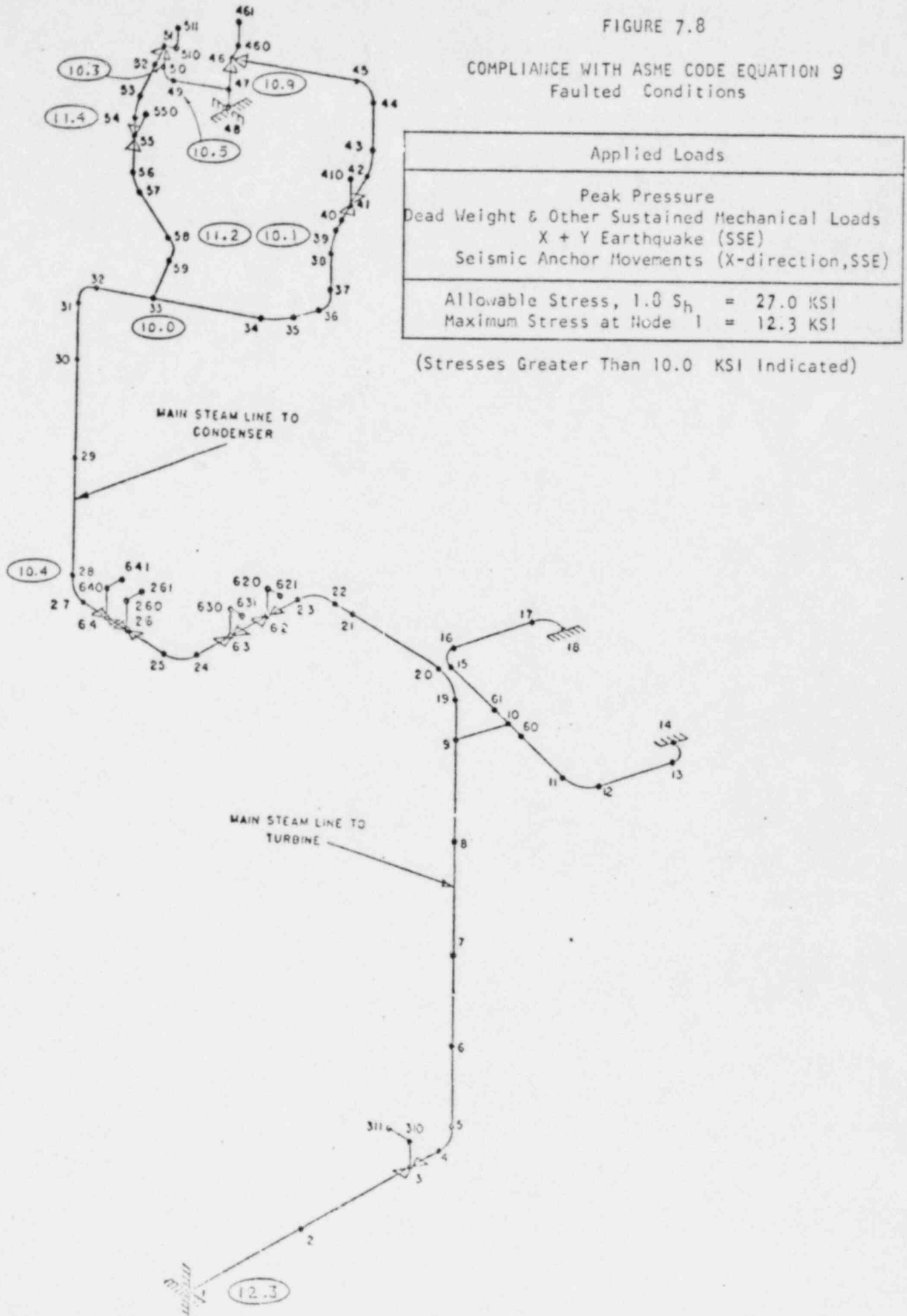
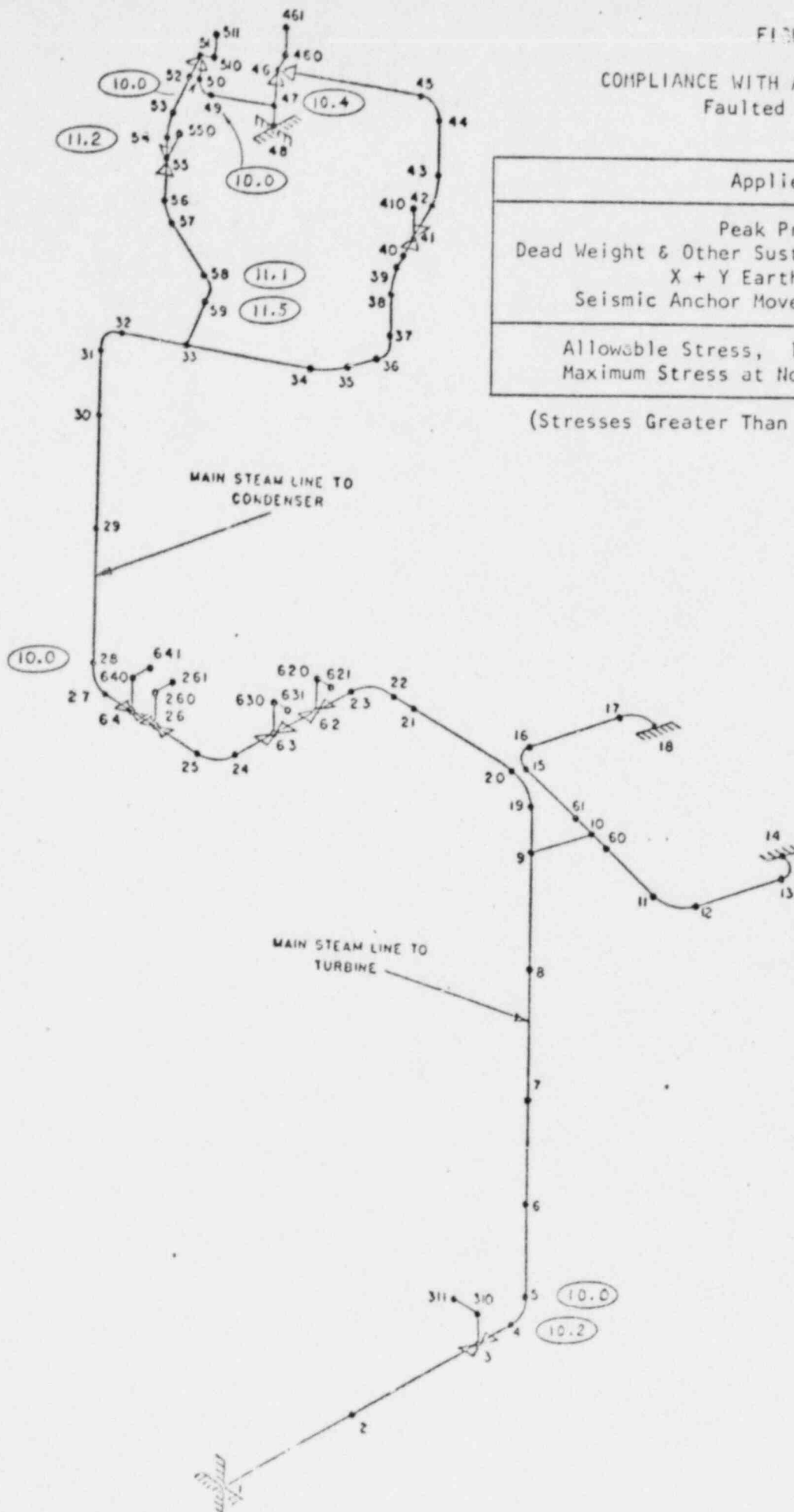


FIGURE 7.9

COMPLIANCE WITH ASME CODE EQUATION 9  
Faulted Conditions



Applied Loads	
Peak Pressure	
Dead Weight & Other Sustained Mechanical Load	
X + Y Earthquake (SSE)	
Seismic Anchor Movements (X-direction, SSE)	
Allowable Stress, $1.8 S_h$	= 23.6 KSI
Maximum Stress at Node 1	= 11.6 KSI

(Stresses Greater Than 10.0 KSI Indicated)

## 8. CONCLUSION AND RECOMMENDATIONS

1. The existing support system of the LACBWR main steam piping system is not adequate to withstand the specified seismic events.
2. The results of the subject analysis, which includes the effects of four additional seismic restraints, indicate that the deflections of the main steam piping system, due to dead weight, thermal expansion and seismic loading are nominal. In addition, the stresses resulting from these loadings, as calculated and combined in accordance with the rules given in Subarticle NC-3652 of Section III of the ASME Code (Ref. 2), satisfy the design requirements of Class 2 piping systems.
3. It is therefore recommended that the main steam piping system be provided with four seismic restraints at the locations indicated in Figure 3.1. The seismic restraints and their attachments should be oriented as shown in Figure 3.1 and designed using the support reaction forces and node displacements given in Appendix B of this report.

## 9. REFERENCES

1. Gulf United Services Report No.SS-1162 "Seismic Evaluation of the LaCrosse Boiling Water Reactor", dated January 11, 1974.
2. ASME Boiler and Pressure Vessel Code, Section III, Division I, 1974 Edition, Nuclear Power Plant Components.
3. Sargent and Lundy Engineers "Specification for Piping System-LaCrosse Boiling Water Reactor" LACBWR No.256.
4. Sargent and Lundy Engineers "LACBWR" Project Drawing Nos.41-503374, 503375, 503376.
5. United Nuclear Corporation "Review of LACBWR Feedwater Nozzle and Recirculation Piping Stress Analysis" Report, dated October 1970.
6. Allis-Chalmers, "LaCrosse Boiling Water Reactor Safeguards Report Volume I and II; LACBWR No.283, dated August 1967.
7. U.S. Atomic Energy Commission - Regulatory Guide 1.48, May 1973.

APPENDIX A  
LACBWR FEEDWATER PIPING ANALYSIS  
ANALYTICAL INPUT DATA

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APPENDIX B

LACBWR FEEDWATER PIPING ANALYSIS

TABULATED RESULTS

TABLE		PAGE
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TABLE A-1 - Pipe Data

Run No.	From Point	To Point	O.D. (in.)	Wall Thick. (in.)	Matl. ASTM	Fluid	Wt. of Pipe and Fluid (lb./in.)	Wt. of Insul. (lb./in.)	Design Temp. (°F)	Design Press. (psia)	Elastic Modulus (psi) X10 <sup>-6</sup>
1	3	21	10.750	0.843	A376		9.76	1.00	577.5	1300	25.1
1	9	60/61	10.750	0.843	A376		9.76	1.00	577.5	1300	25.1
1	60/61	14/18	8.625	0.593 *	A376		5.81	0.85	577.5	1300	25.1
2	21	28	10.750	0.718	A335		8.87	1.00	577.5	1300	27.0
2	28	47	6.625	0.432	A335		3.32	0.71	577.5	1300	27.0
3	1	3	10.750	0.593	A335		7.95	1.00	577.5	1300	27.4

\* .718 was used in the analysis; see Table B-III.

TABLE A-II MAIN STEAM VALVE WEIGHTS

<u>Valve</u>	<u>Total Weight, Lbs.</u>	<u>Nodes</u>	<u>Node Wts, Lbs.</u>	<u>Eccentricity, in.</u>	
				<u>Horizontal</u>	<u>Vertical</u>
Rotoport Isolation Valve	2350	3	784	0	0
		310	784	0	30
		311	784	28	30
Safety Valve	440	62	0	0	0
		620	315	0	30
		621	125	18	30
Safety Valve	440	63	0	0	0
		620	315	0	30
		621	125	18	30
Safety Valve	440	26	0	0	0
		260	315	0	30
		261	125	14	30
Safety Valve	440	64	0	0	0
		640	315	0	30
		641	125	18	30
Gate Valve	425	41	212.5	0	0
		410	212.5	0	13
Gate Valve	425	55	212.5	0	0
		550	212.5	13	0
Pneumatic Control Valve	850	46	284	0	0
		460	283	7.5	0
		461	283	7.5	36
Pneumatic Control Valve	850	51	284	0	0
		510	283	7.5	0
		511	283	7.5	36

TABLE A-111

- A) 1. STATIC LOAD CASE : 1  
LOAD CASE TITLE : DEAD LOAD PLUS SUSTAINED MECHANICAL LOADS

## SINGLE JOINT FORCE AND MOMENT LOADING

JOINT ID	LOAD TYPE	LOAD DIRECTION	LOAD MAGNITUDE
2	FORCE	Y	2600.0000
21	FORCE	Y	1500.0000
31	FORCE	Y	1930.0000
52	FORCE	Y	2145.0000

- B) 2. STATIC LOAD CASE : 2  
LOAD CASE TITLE : NORMAL OPERATING PRESSURE

## THERMAL AND PRESSURE LOADINGS FOR ALL PIPE RUNS

PIPE RUN ID	DESIGN PRESSURE PSI	TEMPERATURE CHANGE DEG.	LINEAR TEMPERATURE GRADIENT DEG.	NONLINEAR TEMPERATURE GRADIENT DEG.	LONG. PRESSURE STRESS
1	1285.00	.00	.000	.000	NO
2	1285.00	.00	.000	.000	NO
3	1285.00	.00	.000	.000	NO

- C) 3. STATIC LOAD CASE : 3  
LOAD CASE TITLE : MAXIMUM PRESSURE

## THERMAL AND PRESSURE LOADINGS FOR ALL PIPE RUNS

PIPE RUN ID	DESIGN PRESSURE PSI	TEMPERATURE CHANGE DEG.	LINEAR TEMPERATURE GRADIENT DEG.	NONLINEAR TEMPERATURE GRADIENT DEG.	LONG. PRESSURE STRESS
1	1400.00	.00	.000	.000	NO
2	1400.00	.00	.000	.000	NO
3	1285.00	.00	.000	.000	NO

- D) 4. STATIC LOAD CASE : 4  
LOAD CASE TITLE : NORMAL OPERATING TEMPERATURE INCL. THERMAL ANCHOR MOVEMENTS

## SUPPORT DISPLACEMENTS

JOINT ID	LOAD TYPE	DISPLACEMENT DIRECTION	DISPLACEMENT MAGNITUDE
14	TRANS.	X	.1810
14	TRANS.	Y	1.2800
14	TRANS.	Z	.0440
18	TRANS.	X	-.1810
18	TRANS.	Y	1.2800
18	TRANS.	Z	-.0440

## THERMAL AND PRESSURE LOADINGS FOR ALL PIPE RUNS

PIPE RUN ID	DESIGN PRESSURE PSI	TEMPERATURE CHANGE DEG.	LINEAR TEMPERATURE GRADIENT DEG.	NONLINEAR TEMPERATURE GRADIENT DEG.	LONG. PRESSURE STRESS
1	.00	507.50	-.000	-.000	NO
2	.00	507.50	-.000	-.000	NO
3	.00	507.50	-.000	-.000	NO

TABLE A-111

- E) 5. STATIC LOAD CASE : 6  
LOAD CASE TITLE : SEISMIC ANCHOR MOVEMENTS X - DIRECTION (1/2 SSE)

## SUPPORT DISPLACEMENTS

JOINT ID	LOAD TYPE	DISPLACEMENT DIRECTION	DISPLACEMENT MAGNITUDE
14	TRANS.	X	.8200
18	TRANS.	X	.8200
40	TRANS.	X	1.3100
43	TRANS.	X	1.3100
48	TRANS.	X	1.3100

- F) 6. STATIC LOAD CASE : 7  
LOAD CASE TITLE : SEISMIC ANCHOR MOVEMENTS Z - DIRECTION (1/2 SSE)

## SUPPORT DISPLACEMENTS

JOINT ID	LOAD TYPE	DISPLACEMENT DIRECTION	DISPLACEMENT MAGNITUDE
14	TRANS.	Z	.8200
18	TRANS.	Z	.8200
40	TRANS.	Z	1.3100
43	TRANS.	Z	1.3100
48	TRANS.	Z	1.3100

- G) 9. STATIC LOAD CASE : 13  
LOAD CASE TITLE : SEISMIC ANCHOR MOVEMENTS Z - DIRECTION (SSE)

## SUPPORT DISPLACEMENTS

JOINT ID	LOAD TYPE	DISPLACEMENT DIRECTION	DISPLACEMENT MAGNITUDE
14	TRANS.	Z	1.5700
18	TRANS.	Z	1.5700
40	TRANS.	Z	2.3800
43	TRANS.	Z	2.3800
48	TRANS.	Z	2.3800

- H) 7. STATIC LOAD CASE : 12  
LOAD CASE TITLE : SEISMIC ANCHOR MOVEMENTS X - DIRECTION (SSE)

## SUPPORT DISPLACEMENTS

JOINT ID	LOAD TYPE	DISPLACEMENT DIRECTION	DISPLACEMENT MAGNITUDE
7	TRANS.	X	.4400
14	TRANS.	X	1.5700
18	TRANS.	X	1.5700
40	TRANS.	X	2.3800
43	TRANS.	X	2.3800
48	TRANS.	X	2.3800

TABLE A-IV - DYNAMIC LOAD CASES

<u>Load Case No.</u>	<u>Load Description</u>	<u>Spectrum IDS</u>			<u>Spectrum Multipliers</u>		
		X	Y	Z	X	Y	Z
8	x + y Earthquake ( $\frac{1}{2}$ SSE)	1	3	0	386.4	128.8	0
9	z + y Earthquake ( $\frac{1}{2}$ SSE)	0	3	1	0	128.8	386.4
10	x + y Earthquake (SSE)	2	3	0	386.4	257.6	0
11	z + y Earthquake (SSE)	0	3	2	0	257.6	386.4

SEISMIC RESPONSE SPECTRA

	SPECTRUM ID	FREQUENCY CPS	PERIOD SEC.	ACCELERATION G's
A)	1	40,000	.025	.16000
		20,000	.050	.16000
		10,000	.100	.16000
		8,000	.125	.16000
		6,000	.167	.27000
		5,200	.192	.48000
		4,200	.238	1.22000
		3,800	.263	1.46000
		3,350	.299	.51000
		2,950	.339	.26000
		2,400	.417	.51000
		2,250	.444	.46000
		2,100	.476	.83000
		2,000	.500	.65000
		1,620	.617	2.17000
		1,600	.625	1.65000
		1,580	.633	1.77000
		1,380	.725	.62000
		1,300	.769	.69000
		1,000	1.000	.35000
.830	1.205	.21500		
.630	1.587	.10800		
.500	2.000	.10800		
B)	2	40,000	.025	.28000
		20,000	.050	.28000
		10,000	.100	.28000
		6,600	.152	.33000
		5,400	.185	.60000
		4,700	.213	.67000
		4,200	.238	1.28000
		4,100	.244	1.15000
		4,000	.250	1.21000
		3,600	.278	.97500
		3,400	.294	.75000
		2,950	.339	.45000
		2,500	.400	.82500
		2,300	.435	.75000
		2,100	.476	1.30000
		2,000	.500	1.05000
		1,750	.571	2.90000
		1,700	.588	2.38000
		1,600	.625	2.55000
		1,350	.741	1.13000
1,320	.758	1.13000		
1,050	.952	.52000		
.920	1.087	.37500		
.840	1.190	.39000		
.720	1.380	.23000		
.500	2.000	.17500		
C)	3	40,000	.025	.12000
		33,000	.030	.12000
		20,000	.050	.23000
		15,000	.067	.32000
		10,000	.100	.52000
		9,000	.111	.60000
		5,000	.200	.65000
		3,000	.333	.70000
		2,500	.400	.72000
		2,200	.455	.63000
		2,000	.500	.59000
		1,500	.667	.44000
		1,000	1.000	.31000
		.800	1.250	.24300
		.600	1.667	.19000
.400	2.500	.13000		
.200	5.000	.05400		

TABLE B-1 (a)

JOINT DISPLACEMENTS

(LOAD CASE 1)

DEAD LOAD PLUS SUSTAINED MECHANICAL LOADS

JOINT (GID)	DISPLACEMENTS ( IN. )				X	Y	Z
	X	Y	Z				
1	.0000000	-.0000000	.0000000	43	.0125768	-.0003042	-.0084104
2	.0031649	-.0067586	.0000030	44	.0036192	-.0003543	.0013240
3	.0100328	-.0203547	.0000058	45	.0012672	-.0018050	.0017063
4	.0170536	-.0070788	.0000077	46	.0013283	-.0001670	.0007390
5	.0174357	-.0009702	.0060028	47	.0002449	-.0000626	.0003371
6	.0169928	-.0003688	.0408575	48	-.0000000	-.0000000	-.0000000
7	.0228730	-.0000000	.0571975	49	.0000223	-.0001261	-.0000220
8	.0236598	-.0010790	.0466081	50	.0047276	.0003152	.0061503
9	.0000021	-.0017021	-.0002408	51	.0131982	.0003178	.0169760
10	-.0004654	-.0146631	-.0003563	52	.0136499	-.0368458	.0167183
11	-.0004944	-.0050188	-.0002388	53	.0119729	-.1195423	.0176899
12	-.0004163	-.0054079	-.0001016	54	.0009923	-.1407334	.0006241
13	-.0000201	-.0009934	.0000010	55	-.0103766	-.1407803	-.0210960
14	.0000000	-.0000000	-.0000000	56	-.0390337	-.1408353	-.0789561
15	-.0005272	-.0317490	-.0001042	57	-.0486398	-.1400177	-.0998255
16	-.0004588	-.0306904	-.0001340	58	-.0673705	-.1343391	-.1486168
17	-.0000321	-.0032431	-.0000292	59	-.0752951	-.1459688	-.1551450
18	-.0000000	-.0000000	.0000000	60	-.0004417	-.0116437	-.0004509
19	-.0144312	-.0017538	-.0194615	61	-.0004914	-.0179904	-.0002513
20	-.0249866	-.0142174	-.0289813	62	-.0181712	-.1123784	-.0183687
21	-.0249781	-.1314585	-.0213495	63	-.0132877	-.0709082	-.0183686
22	-.0249773	-.1441637	-.0203630	64	-.0039897	-.1507280	-.0059608
23	-.0227599	-.1487899	-.0183689	260	-.0701070	-.1044078	-.0603852
24	-.0066576	-.0092266	-.0183684	261	-.0728652	-.1355910	-.0603852
25	-.0039954	-.0123237	-.0157877	310	.0021380	-.0203939	.0006872
26	-.0039916	-.1047969	-.0091197	311	.0021380	-.0280957	-.0027463
27	-.0039888	-.1700189	-.0046441	410	-.0229761	.0005013	.0123530
28	-.0336989	-.2006456	-.0271420	460	.0012185	-.0001301	.0000009
29	-.1673393	-.2002860	-.1760405	461	.0034174	-.0001386	-.0001344
30	-.1445959	-.1996168	-.2009494	510	.0130432	-.0010792	.0167010
31	-.1221263	-.1993180	-.1823349	511	.0399799	-.0010877	.0511456
32	-.1142402	-.1994811	-.1702186	550	-.0074654	-.1148578	-.0227684
33	-.0979524	-.1888488	-.1420467	620	-.0675874	-.1123894	-.0618015
34	-.0614121	-.1111452	-.0787447	621	-.0653369	-.0730453	-.0640519
35	-.0417613	-.0643761	-.0637029	630	-.0656751	-.0709192	-.0669044
36	-.0240545	-.0257952	-.0589785	631	-.0633475	-.0281517	-.0692319
37	-.0190683	-.0074336	-.0400923	640	-.0686983	-.1507390	-.0565889
38	-.0306182	-.0073485	.0082121	641	-.0713537	-.1811398	-.0565889
39	-.0276141	-.0021389	.0142606				
40	-.0256724	-.0013595	.0130844				
41	-.0150733	.0004036	.0071730				
42	.0114137	-.0003924	-.0083533				



TABLE B-1 (b)

## JOINT DISPLACEMENTS

(LOAD CASE 4)

NORMAL OPERATING TEMPERATURE INCL. THERMAL ANCHOR MOVEMENTS

JOINT /-----DISPLACEMENTS ( IN. )-----/  
(GID) X Y Z

JOINT (GID)	X	Y	Z
1	.000000	-.000000	.000000
2	.006168	-.226493	-.253025
3	.019546	-.679030	-.488844
4	.033213	-1.083852	-.765848
5	.038939	-1.106392	-.882551
6	.054139	-.534774	-.904670
7	.052335	-.000000	-.574025
8	-.011997	.754347	.135924
9	-.157632	1.404862	.635384
10	-.122246	1.477206	.484032
11	.237645	1.446077	.546064
12	.295318	1.418622	.482074
13	.239928	1.290394	.112324
14	.181000	1.280000	.044000
15	-.469841	1.392723	.372367
16	-.490257	1.368166	.288632
17	-.265350	1.285910	-.011433
18	-.181000	1.280000	-.044000
19	-.224863	1.576333	.733501
20	-.346748	1.586686	.791015
21	-.842582	1.079848	.853449
22	-.976056	1.027419	.860760
23	-.915709	.840370	.931133
24	-.798560	.201654	1.264572
25	-.834832	.002120	1.339403
26	-.991044	-.257257	1.389961
27	-1.102624	-.435119	1.425201
28	-1.234347	-.459985	1.527585
29	-1.204288	.030451	1.809616
30	-.438973	.520888	1.400901
31	-.156647	.688082	1.154510
32	-.086769	.652899	1.067289
33	-.001744	.395434	.924683
34	.143110	.053652	.622699
35	.151852	-.053254	.520843
36	.134573	-.133371	.450054
37	.146814	-.141016	.376359
38	.215023	-.018202	.245579
39	.221286	.002432	.185202
40	.217070	-.000163	.174970
41	.197472	-.012978	.117632
42	.151643	-.033763	-.071906
43	.168815	-.001011	-.120647
44	.283834	.166209	-.183771
45	.264359	.205473	-.176981
46	-.014973	.116699	-.011974
47	-.001689	.038496	-.003627
48	-.000000	.000000	.000000
49	-.122637	.078529	.054433
50	-.160392	.131277	.017055
51	-.174317	.175903	-.064464
52	-.155530	.368429	.038113

	X	Y	Z
53	-.119493	.660459	.174092
54	-.105252	.690298	.271932
55	-.110585	.645733	.351945
56	.139237	.520157	.562434
57	-.145513	.455874	.633219
58	-.146529	.236542	.790288
59	-.118612	.231881	.850416
60	-.063799	1.482021	.497854
61	-.180611	1.469368	.469879
62	-.882366	.654512	1.030227
63	-.846862	.461022	1.130661
64	-1.069150	-.382674	1.414625
260	-1.172570	-.257257	1.578334
261	-1.193904	-.144174	1.578334
310	.022530	-.679030	-.716753
311	.022530	-.676249	-.723439
410	.234962	-.012978	.085780
460	-.014680	.112036	-.012139
461	-.047926	.112036	-.018831
510	-.169851	.157771	-.055754
511	-.214940	.157771	-.312079
550	-.110942	.575650	.352150
620	-1.071371	.654512	1.242671
621	-1.055016	.644574	1.226316
630	-1.037046	.461022	1.346709
631	-1.020152	.450072	1.329775
640	-1.245134	-.382674	1.596393
641	-1.266319	-.273613	1.596393

JOINT DISPLACEMENTS

(LOAD CASE 6)

SEISMIC ANCHOR MOVEMENTS X - DIRECTION (1/2 SSE)

JOINT /-----DISPLACEMENTS ( IN. )-----/  
(GID) X Y Z

JOINT (GID)	X	Y	Z
1	.000000	.000000	-.000000
2	.009488	.000196	-.000002
3	.030244	.000379	-.000003
4	.051710	.000203	-.000005
5	.077269	-.000004	-.0000286
6	.258305	-.000002	-.003903
7	.444438	-.000000	-.007222
8	.683990	-.000020	-.007866
9	.815242	-.000037	-.000839
10	.815956	-.001704	-.000662
11	.816021	-.020523	-.000883
12	.816270	-.019300	-.000669
13	.819574	-.001710	.000139
14	.820000	-.000000	.000000
15	.816041	.018526	-.000965
16	.816453	.017637	-.001115
17	.819709	.001674	-.000296
18	.820000	.000000	-.000000
19	.835752	-.000045	.003115
20	.843640	.007326	.005805
21	.843648	.047263	.009132
22	.843649	.050766	.009645
23	.845011	.049583	.010805
24	.855686	.000740	.010803
25	.857409	.000511	.012441
26	.857413	.024552	.016529
27	.857416	.042977	.019291
28	.868037	.053113	.026867
29	1.024368	.053096	.047240
30	1.219514	.053080	.026158
31	1.274684	.053074	.015865
32	1.293397	.045522	.014096
33	1.283501	.023233	.014256
34	1.283634	.002716	.014456
35	1.284398	.000357	.014970
36	1.285486	-.000023	.015257
37	1.288333	-.000541	.015262
38	1.296242	-.000531	.013116
39	1.299284	-.000168	.011848
40	1.299435	-.000070	.011636
41	1.301573	.000240	.010511
42	1.307672	.000126	.007031
43	1.309482	-.000010	.005820
44	1.312102	-.000014	.003230
45	1.312988	.000217	.002325
46	1.310001	.000007	-.001154
47	1.310043	.000005	-.000259
48	1.310000	.000000	-.000000
49	1.309293	.003647	-.001438
50	1.309030	.004467	-.004885
51	1.308774	.004472	-.009220
52	1.306053	.014815	-.008116

X	Y	Z	
53	1.304481	.029094	-.006754
54	1.303414	.031727	-.003637
55	1.301952	.031732	-.000667
56	1.296614	.031746	.006053
57	1.294068	.030957	.008183
58	1.285848	.026107	.013010
59	1.283619	.024718	.014193
60	.815922	-.006321	-.000558
61	.815987	.002940	-.000781
62	.840017	.035550	.010804
63	.851268	.020748	.010804
64	.857415	.037332	.018471
260	.875300	.024552	.030561
261	.873609	.032972	.030561
310	.056322	.000370	.000001
311	.056322	.024684	-.010435
410	1.303835	.000240	.009401
460	1.310283	-.000257	-.001267
461	1.310067	-.000257	-.002588
510	1.309099	.003584	-.008644
511	1.308137	.003584	-.022811
550	1.302340	.029952	-.000890
620	.860803	.035550	.026958
621	.862291	.023280	.025470
630	.864830	.020748	.027401
631	.866383	.007960	.025849
640	.876066	.037332	.031964
641	.874418	.045428	.031964

TABLE B-1 (d)

JOINT DISPLACEMENTS

(LOAD CASE 7)

SEISMIC ANCHOR MOVEMENTS Z - DIRECTION (1/2 SSE)

JOINT (GID)	DISPLACEMENTS ( IN. )				X	Y	Z
	X	Y	Z				
1	-.000000	-.000000	.000000				
2	-.000900	-.008018	.000035				
3	-.002968	-.015459	.000068				
4	-.005253	-.008291	.000090				
5	-.006428	.000164	.011619				
6	-.010713	.000079	.172631				
7	-.013535	-.000000	.371187				
8	-.011615	-.000114	.652991				
9	-.000681	-.000211	.817043	53	-.001370	.012873	1.306923
10	-.001904	.019728	.816749	54	-.000565	.013656	1.306929
11	-.002388	.001565	.818690	55	.000262	.013659	1.306096
12	-.001951	.000201	.819505	56	.002126	.013669	1.301874
13	-.000070	-.000039	.819995	57	.002697	.014109	1.299683
14	.000000	.000000	.820000	58	.003447	.016652	1.291616
15	-.002475	.021231	.819074	59	.002822	.014782	1.289970
16	-.002456	.018850	.819191	60	-.001951	.017169	.816538
17	-.000235	.001619	.819754	61	-.001985	.021852	.817080
18	-.000000	.000000	.820000	62	.018417	.029577	.880086
19	.004718	-.000202	.843711	63	.025373	.018549	.880088
20	.008283	.003909	.856532	64	.039542	.001433	.905560
21	.008281	.039486	.874729	260	.040445	.001010	.915983
22	.008280	.042739	.876668	261	.034440	.011425	.915983
23	.011803	.040855	.880083	310	-.003634	-.015459	-.000130
24	.035116	.003706	.880091	311	-.003634	-.016079	.000944
25	.039544	-.001224	.884700	410	.004831	.000242	1.303438
26	.039543	.001010	.898524	460	.000045	-.000134	1.309410
27	.039542	.001516	.908579	461	.000153	-.000134	1.308606
28	.039259	.001380	.923619	510	-.001182	.001884	1.306896
29	.021467	.001320	1.065469	511	-.003990	.001884	1.301483
30	-.000027	.001260	1.235688	550	.000229	.014192	1.306105
31	-.001829	.001239	1.280967	620	.026831	.029577	.892528
32	-.000807	.003227	1.288294	621	.030047	.020734	.889312
33	.000921	.004643	1.291122	630	.032547	.018549	.892326
34	.003782	-.001193	1.294281	631	.035493	.010318	.888981
35	.004620	-.001852	1.296985	640	.039931	.001433	.923906
36	.005027	-.001004	1.297097	641	.033999	.012441	.923906
37	.005928	-.000441	1.297984				
38	.007185	-.000447	1.301275				
39	.006648	-.000035	1.302257				
40	.008431	.000024	1.302389				
41	.005200	.000242	1.303103				
42	.001104	.000045	1.305439				
43	.000110	.000014	1.305939				
44	-.001298	.000014	1.306465				
45	-.001264	-.000145	1.306929				
46	.000136	.000003	1.309359				
47	.000033	.000003	1.309663				
48	.000000	.000000	1.310000				
49	-.000024	.001816	1.302276				
50	-.000276	.001026	1.304693				
51	-.001310	.001127	1.307078				
52	-.001333	.008643	1.306895				

TABLE B-1 (e)

JOINT DISPLACEMENTS

(LOAD CASE 8)

X + Y EARTHQUAKE (1/2 SSE)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 34 BY SQSS SUMMATION

JOINT GID	DISPLACEMENTS (IN.)				X	Y	Z
	X	Y	Z				
1	.0000000	.0000000	.0000000				
2	.1016139	.0030028	.0000518				
3	.3044946	.0053251	.0001001				
4	.4928507	.0025834	.0001211	42	.0425143	.0005623	.1458183
5	.5141111	.0000699	.0036395	43	.0323223	.0003889	.1271615
6	.2412720	.0000338	.0446351	44	.0543489	.0004349	.0976950
7	.0000000	.0000000	.0693995	45	.0507060	.0038934	.0808928
8	.0971371	.0000688	.0524927	46	.0045680	.0000589	.0031688
9	.0464719	.0001269	.0142384	47	.0012906	.0000355	.0007485
10	.0410442	.0063383	.0129895	48	.0000000	.0000000	.0000000
11	.0413857	.0155925	.0105630	49	.0051477	.0312201	.0059159
12	.0383057	.0150242	.0071085	50	.0198468	.0472264	.0103181
13	.0041290	.0013529	.0013041	51	.0434408	.0472524	.0325778
14	.0000000	.0000000	.0000000	52	.0416279	.0742826	.0312714
15	.0413060	.0206815	.0108422	53	.0352117	.1305236	.0284515
16	.0375443	.0192892	.0119158	54	.0000000	.1450849	.0000000
17	.0031560	.0017035	.0032515	55	.0403404	.1450984	.0380698
18	.0000000	.0000000	.0000000	56	.1949476	.1451172	.1466032
19	.0411801	.0001403	.0171093	57	.2509354	.1346483	.1895196
20	.0436062	.0116137	.0238193	58	.3772554	.0968553	.2978397
21	.0436124	.1144665	.0338526	59	.4039302	.1079881	.3160575
22	.0436130	.1250948	.0344183	60	.0412247	.0045289	.0122895
23	.0408748	.1263712	.0340281	61	.0400660	.0096418	.0135483
24	.0075498	.0124191	.0340195	62	.0327851	.0925849	.0340306
25	.0000187	.0035225	.0260309	63	.0229904	.0562253	.0340286
26	.0000000	.0847431	.0000000	64	.0000095	.1264922	.0135197
27	.0000136	.1443595	.0193556	260	.0594326	.0847435	.0496651
28	.0290873	.1735097	.0394141	261	.0617336	.1105570	.0496651
29	.2806802	.1736718	.2880079	310	.2774135	.0053251	.0005501
30	.4525297	.1737709	.3714634	311	.2774135	.0225821	.0961373
31	.4712204	.1737902	.3476111	410	.1428320	.0022543	.2067161
32	.4668391	.1723451	.3329447	460	.0070536	.0007377	.0043341
33	.4408882	.1539339	.3103242	461	.0099902	.0007378	.0067835
34	.3928342	.0861873	.3081788	510	.0435372	.0277009	.0321855
35	.3632201	.0511604	.3199634	511	.1172395	.0277015	.1065336
36	.3328748	.0215820	.3257799	550	.0426300	.1288066	.0368730
37	.3046280	.0058096	.3196102	620	.0644937	.0925852	.0582771
38	.2523624	.0057963	.2718476	621	.0607530	.0603710	.0617943
39	.2138372	.0011659	.2475100	630	.0591681	.0562255	.0602347
40	.2061919	.0004829	.2429798	631	.0553726	.0268439	.0643993
41	.1441820	.0022543	.2191587	640	.0596560	.1264928	.0521348
				641	.0615518	.1524160	.0521348

TABLE B-1 (f)

## JOINT DISPLACEMENTS

(LOAD CASE 9)

Z • Y EARTHQUAKE (1/2 SSE)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 34 BY SQSS SUMMATION

JOINT /-----DISPLACEMENTS ( IN. )-----/

JOINT GID	X	Y	Z		X	Y	Z
1	.0000000	.0000000	.0000000				
2	.0282885	.0148099	.0001915				
3	.0847146	.0279660	.0003700				
4	.1370922	.0143213	.0004916	43	.0217860	.0003793	.1258787
5	.1429125	.0002378	.0199244	44	.0523095	.0004254	.0956952
6	.0667866	.0001150	.2416978	45	.0492288	.0038726	.0788814
7	.0000000	.0000000	.3658043	46	.0043671	.0000588	.0031054
8	.0288387	.0001832	.2458536	47	.0012587	.0000358	.0007303
9	.0265951	.0003392	.0189485	48	.0000000	.0000000	.0000000
10	.0248520	.0335459	.0187512	49	.0054769	.0310386	.0064555
11	.0235110	.0093548	.0061522	50	.0197788	.0469241	.0104148
12	.0221701	.0090888	.0039710	51	.0430047	.0466502	.0319677
13	.0026783	.0002391	.0009094	52	.0412310	.0731706	.0307365
14	.0000000	.0000000	.0000000	53	.0349246	.1256919	.0279684
15	.0235658	.0405862	.0060688	54	.0000000	.1387388	.0000000
16	.0206413	.0363697	.0064229	55	.0489591	.1387532	.0375733
17	.0016950	.0031542	.0017537	56	.1934426	.1387751	.1449695
18	.0000000	.0000000	.0000000	57	.2490151	.1280179	.1879606
19	.0393018	.0003300	.0331481	58	.3744752	.0898992	.2961876
20	.0491434	.0125237	.0523068	59	.6007553	.0949257	.3144039
21	.0491906	.1276398	.0482806	60	.0248365	.0286990	.0182544
22	.0491843	.1390408	.0476497	61	.0247715	.0378231	.0184198
23	.0459285	.1379101	.0456595	62	.0373705	.1001738	.0456585
24	.0094336	.0127121	.0456346	63	.0267646	.0608072	.0456517
25	.0000164	.0032549	.0351693	64	.0000094	.1153944	.0183147
26	.0000000	.0774016	.0000000	260	.0541631	.0774019	.0490303
27	.0000135	.1316286	.0262242	261	.0575974	.1022832	.0490303
28	.0263937	.1580197	.0414554	310	.0770061	.0279676	.0006388
29	.2673754	.1581636	.2753707	311	.0770061	.0315586	.0266136
30	.4442728	.1582496	.3649207	410	.1412230	.0020940	.2062087
31	.4644258	.1582657	.3443479	460	.0066482	.0006711	.0041880
32	.4605459	.1568300	.3308042	461	.0090958	.0006711	.0064944
33	.4360522	.1395564	.3095681	510	.0430939	.0276160	.0316097
34	.3903536	.0783426	.3084717	511	.1160125	.0276165	.1045569
35	.3615335	.0468463	.3200727	550	.0423180	.1257686	.0361501
36	.3216435	.0200123	.3258328	620	.0707081	.1001742	.0808234
37	.3035542	.0053299	.3198416	621	.0664557	.06663110	.0852234
38	.2513416	.0053218	.2718963	630	.0617192	.0604074	.0812651
39	.2127569	.0010623	.2473896	631	.0571706	.0298071	.0865698
40	.2050823	.0004517	.2428545	640	.0542566	.1153950	.0471121
41	.1628479	.0020949	.2189599	641	.0571608	.1400817	.0471121
42	.0348158	.0005390	.1440959				



TABLE B-1 (g)

JOINT DISPLACEMENTS

(LOAD CASE 10)

X-Y DIRECTION EARTHQUAKE (SSE)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 34 BY SQSS SUMMATION

JOINT GID	DISPLACEMENTS (IN.)				X	Y	Z
	X	Y	Z				
1	.0000000	.0000000	.0000000				
2	.0887294	.0044622	.0000602				
3	.2658581	.0078875	.0001162				
4	.4303111	.0037016	.0001463	43	.0512444	.0005083	.1394091
5	.4488768	.0001006	.0051033	44	.0612953	.0005497	.1096220
6	.2107589	.0000487	.0618442	45	.0563581	.0042453	.0923790
7	.0000000	.0000000	.0950627	46	.0062900	.0000657	.0046820
8	.0886200	.0001139	.0702694	47	.0015986	.0000432	.0010099
9	.0535147	.0002108	.0193349	48	.0000000	.0000000	.0000000
10	.0489152	.0101580	.0182596	49	.0075285	.0347218	.0093909
11	.0496681	.0183294	.0133767	50	.0228675	.0515406	.0143491
12	.0457274	.0177524	.0086172	51	.0483511	.0515742	.0396535
13	.0047275	.0016049	.0014899	52	.0466850	.0905203	.0380364
14	.0000000	.0000000	.0000000	53	.0393664	.1823822	.0362053
15	.0496041	.0265272	.0132109	54	.0000000	.2087627	.0000000
16	.0452722	.0246271	.0143727	55	.0549484	.2087739	.0530713
17	.0038304	.0021769	.0039332	56	.2172439	.2087796	.2108311
18	.0000000	.0000000	.0000000	57	.2794227	.2008844	.2744886
19	.0580107	.0002296	.0280174	58	.4184919	.1713671	.4331198
20	.0663239	.0174232	.0393235	59	.4514419	.1932357	.4541832
21	.0663410	.1814815	.0543630	60	.0490423	.0073885	.0177015
22	.0663426	.1990156	.0554016	61	.0488144	.0141262	.0185380
23	.0622028	.2018788	.0552076	62	.0500684	.1462292	.0552118
24	.0118258	.0173756	.0551914	63	.0351705	.0862988	.0552080
25	.0000297	.0058029	.0424904	64	.0000110	.2254916	.0222391
26	.0000000	.1507412	.0000000	260	.1061883	.1507418	.0785583
27	.0000155	.2575699	.0318569	261	.1096321	.1936378	.0785583
28	.0524181	.3103350	.0627344	310	.2422303	.0078887	.0008243
29	.4244193	.3105910	.4441435	311	.2422303	.0212170	.0839425
30	.5742594	.3107364	.5731867	410	.1539530	.0039449	.2170977
31	.5748672	.3107607	.5342434	460	.0082524	.0013206	.0054055
32	.5619708	.3078824	.5016694	461	.0137766	.0013207	.0101148
33	.5137680	.2755024	.4243465	510	.0483783	.0321976	.0389871
34	.4298176	.1525077	.3376395	511	.1296658	.0321984	.1272934
35	.3872298	.0889443	.3389802	550	.0467629	.1723324	.0543213
36	.3483531	.0361422	.3423836	620	.1078898	.1462297	.0986060
37	.3171131	.0101924	.3321320	621	.1021924	.0904378	.1040934
38	.2656367	.0101536	.2813125	630	.1009295	.0862991	.1016885
39	.2258208	.0020208	.2573918	631	.0951222	.0356518	.1082640
40	.2176253	.0007295	.2527526	640	.1069109	.2254925	.0814325
41	.1732716	.0039449	.2286722	641	.1096510	.2688644	.0814325
42	.0586650	.0011437	.1572729				

TABLE B-1 (h)

JOINT DISPLACEMENTS

(LOAD CASE 11)

Z + Y DRE EARTHQUAKE (SSE) + Z - ANCHOR MOVE. (SSE)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 34 BY SOSS SUMMATION

JOINT GIO	DISPLACEMENTS ( IN. )				X	Y	Z
	X	Y	Z				
1	.0000000	.0000000	.0000000				
2	.0250695	.0136415	.0001737				
3	.0750060	.0255940	.0003356				
4	.1214195	.0129921	.0004459	43	.0363472	.0004851	.1340802
5	.1266260	.0002305	.0180465	44	.0564264	.0005279	.1035666
6	.0594908	.0001115	.2188042	45	.0526063	.0041077	.0863741
7	.0000000	.0000000	.3312665	46	.0056828	.0000651	.0045171
8	.0311171	.0001860	.2234834	47	.0014942	.0000427	.0009717
9	.0387434	.0003444	.0222721	48	.0000000	.0000000	.0000000
10	.0362045	.0308194	.0218163	49	.0075242	.0340194	.0093626
11	.0362808	.0145163	.0102327	50	.0224308	.0505949	.0137633
12	.0334843	.0141169	.0062972	51	.0471905	.0506270	.0383823
13	.0036172	.0012676	.0011550	52	.0456641	.0885400	.0368801
14	.0000000	.0000000	.0000000	53	.0386449	.1749853	.0349710
15	.0363515	.0405414	.0099586	54	.0000000	.1992917	.0000000
16	.0229625	.0365302	.0104596	55	.0540027	.1993040	.0509005
17	.0028109	.0031848	.0029070	56	.2135225	.1993130	.2019205
18	.0000000	.0000000	.0000000	57	.2746746	.1911726	.2629249
19	.0560113	.0003447	.0377783	58	.4116163	.1614510	.4152372
20	.0689784	.0176565	.0569615	59	.4435888	.1809509	.4359138
21	.0690146	.1819253	.0615666	60	.0362399	.0261281	.0212898
22	.0690182	.1990701	.0616675	61	.0361531	.0352280	.0215706
23	.0648224	.2003037	.0600557	62	.0526523	.1449974	.0600583
24	.0128513	.0178171	.0600331	63	.0374229	.0861567	.0600525
25	.0000252	.0054175	.0460539	64	.0000107	.2098341	.0238731
26	.0000000	.1402895	.0000000	260	.0988099	.1402901	.0752818
27	.0000150	.2396723	.0341718	261	.1020762	.1803266	.0752818
28	.0487490	.2887228	.0591864	310	.0683172	.0255960	.0009769
29	.4006552	.2889628	.4166839	311	.0683172	.0293146	.0235882
30	.5541992	.2890991	.5459030	410	.1499851	.0036724	.2134127
31	.5578476	.2891218	.5098835	460	.0073584	.0012285	.0051610
32	.5463161	.2865102	.4797160	461	.0118209	.0012286	.0096282
33	.5017922	.2563088	.4092529	510	.0471959	.0314486	.0377924
34	.4236843	.1417439	.3327073	511	.1263613	.0314492	.1240186
35	.3830402	.0827390	.3351021	550	.0459949	.1671023	.0517777
36	.3452247	.0337090	.3387561	620	.1072493	.1449979	.1080244
37	.3162304	.0094202	.3292398	621	.1013244	.0918890	.1142988
38	.2626725	.0093860	.2787329	630	.0977901	.0861569	.1101490
39	.2227567	.0018635	.2545126	631	.0916743	.0380414	.1176504
40	.2145416	.0005785	.2498591	640	.0994699	.2098350	.0745601
41	.1498132	.0036724	.2255613	641	.1019741	.2501155	.0745601
42	.056189	.0009750	.1525819				

JOINT DISPLACEMENTS

(LOAD CASE 12)

SEISMIC ANCHOR MOVEMENTS X - DIRECTION (SSE)

JOINT /-----DISPLACEMENTS ( IN. )-----/  
(GID) X Y Z

JOINT (GID)	X	Y	Z		X	Y	Z
1	.000000	.000000	-.000000				
2	.018235	.000362	-.000003				
3	.058140	.000698	-.000006				
4	.099430	.000374	-.000008				
5	.148442	-.000007	-.000026				
6	.495200	-.000004	-.007194				
7	.851600	-.000000	-.013223				
8	1.309867	-.000034	-.014559				
9	1.560216	-.000064	-.001698	53	2.371146	.049325	-.011492
10	1.561762	-.003383	-.001316	54	2.369501	.053877	-.006154
11	1.561898	-.038999	-.001779	55	2.367179	.053886	-.000937
12	1.562398	-.036667	-.001359	56	2.358630	.053909	.011079
13	1.569127	-.003248	.000285	57	2.354511	.052578	.014954
14	1.570000	-.000000	.000000	58	2.341081	.044376	.023824
15	1.561943	.035040	-.001970	59	2.337518	.042282	.025909
16	1.562778	.033368	-.002273	60	1.561707	-.012135	-.001086
17	1.569407	.002979	-.000605	61	1.561929	.005442	-.001576
18	1.570000	.000000	-.000000	62	1.620133	.066111	.015923
19	1.599065	-.000077	.005548	63	1.624807	.038971	.015921
20	1.613934	.013784	.010193	64	1.633610	.063831	.026458
21	1.613947	.087780	.013707	260	1.664120	.042056	.049836
22	1.613948	.094169	.014356	261	1.661818	.057664	.049836
23	1.615838	.091839	.015924	310	.108093	.000698	.000003
24	1.631157	.002270	.015920	311	.108093	.047254	-.020066
25	1.633601	.000936	.018220	410	2.370042	.000369	.015481
26	1.633607	.042056	.023822	460	2.380461	-.000434	-.002126
27	1.633611	.073431	.027567	461	2.380085	-.000434	-.004346
28	1.651576	.090612	.041000	510	2.378494	.005985	-.014483
29	1.911276	.090583	.081545	511	2.376777	.005985	-.038406
30	2.232800	.090554	.047020	550	2.367733	.050599	-.001255
31	2.323608	.090544	.029252	620	1.642718	.066111	.045538
32	2.337903	.077988	.026028	621	1.644852	.043978	.043404
33	2.337765	.040673	.025757	630	1.648552	.038971	.046358
34	2.337331	.005558	.024954	631	1.650786	.015999	.044125
35	2.338275	.001259	.025558	640	1.665351	.063831	.051509
36	2.339900	.000224	.025958	641	1.663119	.078861	.051509
37	2.344403	-.000825	.025754				
38	2.357577	-.000209	.021474				
39	2.362567	-.000265	.019517				
40	2.363125	-.000113	.019178				
41	2.366220	.000369	.017382				
42	2.376053	.000202	.011777				
43	2.379039	-.000019	.009772				
44	2.383628	-.000026	.005361				
45	2.383465	.000366	.003949				
46	2.380127	.000012	-.001938				
47	2.380070	.000009	-.000434				
48	2.380000	.000000	-.000000				
49	2.378869	.005757	-.002223				
50	2.378632	.008134	-.007756				
51	2.377971	.008142	-.015411				
52	2.374891	.024990	-.013641				



JOINT DISPLACEMENTS

(LOAD CASE 13)

SEISMIC ANCHOR MOVEMENTS Z - DIRECTION (SSE)

JOINT (GID)	DISPLACEMENTS ( IN. )				X	Y	Z
	X	Y	Z				
1	-.000000	-.000000	.000000				
2	-.001611	-.015362	.000068				
3	-.005293	-.029617	.000130				
4	-.009334	-.015884	.000173				
5	-.011450	.000314	.022261				
6	-.017418	.000152	.330726				
7	-.024725	-.000000	.711040				
8	-.021416	-.000223	1.250523				
9	-.001551	-.000413	1.564067	53	-.001858	.023339	2.374335
10	-.003489	.037666	1.563604	54	-.000349	.024952	2.374622
11	-.004470	.003337	1.567536	55	.001149	.024958	2.373679
12	-.003647	.000715	1.569077	56	.004594	.024974	2.368026
13	-.000130	-.000045	1.569991	57	.005650	.025658	2.364576
14	.000000	.000000	1.570000	58	.007044	.029571	2.352935
15	-.004609	.040278	1.568164	59	.006175	.026770	2.350308
16	-.004649	.035654	1.568447	60	-.003410	.032864	1.563288
17	-.000459	.003061	1.569514	61	-.003625	.041639	1.564160
18	-.000000	.000000	1.570000	62	.030464	.053536	1.675440
19	.008288	-.000397	1.614846	63	.041570	.033193	1.675444
20	.014783	.007091	1.638563	64	.063845	.005855	1.715770
21	.014779	.072092	1.667041	260	.067023	.003994	1.735151
22	.014778	.078073	1.670082	261	.057507	.022315	1.735151
23	.020299	.074469	1.675436	310	-.006534	-.029617	-.000250
24	.056871	.006076	1.675449	311	-.006534	-.030774	.001657
25	.063848	-.002137	1.682725	410	.008329	.000362	2.369030
26	.063846	.003994	1.704616	450	.000065	-.000237	2.378966
27	.063845	.006480	1.720558	491	.000216	-.000237	2.377565
28	.044131	.007031	1.745927	510	-.001992	.003242	2.374499
29	.038265	.006929	1.983837	511	-.006941	.003242	2.364680
30	.002749	.006827	2.263007	550	.000951	.025350	2.373792
31	-.000352	.006792	2.336324	620	.046646	.053536	1.698466
32	.001249	.009886	2.347931	621	.051687	.036996	1.693426
33	.003500	.011282	2.351846	630	.055434	.033193	1.697928
34	.007482	-.000221	2.358789	631	.060683	.017781	1.692680
35	.008424	-.002077	2.359611	640	.066125	.005855	1.747879
36	.008715	-.001282	2.359693	641	.056560	.025120	1.747879
37	.009909	-.000634	2.360952				
38	.012332	-.000644	2.365929				
39	.011396	-.000040	2.367062				
40	.011006	.000045	2.367299				
41	.008915	.000362	2.368571				
42	.001460	.000131	2.372650				
43	.000024	.000017	2.373470				
44	-.002148	.000019	2.374156				
45	-.002077	-.000229	2.374902				
46	.000216	.000005	2.378842				
47	.000054	.000005	2.379761				
48	.000000	.000000	2.380000				
49	.000009	.002631	2.379486				
50	-.000578	.003362	2.377615				
51	-.002075	.003362	2.374440				
52	-.002075	.011858	2.374465				

E L A S T I C   S U P P O R T   R E A C T I O N S

(LOAD CASE 1)

D E A D   L O A D   P L U S   S U S T A I N E D   M E C H A N I C A L   L O A D S

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN.-LB.)		
	X	Y	Z	X	Y	Z
1	-60.04	74.87	-22.68	17670.52	10181.15	-9974.75
7	.00	9578.81	.00	.00	.00	.00
14	-4.54	574.50	25.53	-11479.03	17.18	776.06
1P	8.54	913.53	-6.14	-29139.86	278.15	-17252.12
2P	.00	2797.49	.00	.00	.00	.00
40	-62.13	1481.90	-31.66	-406.40	397.34	-376.86
43	-30.44	331.57	20.35	-158.00	224.92	-181.44
4P	24.35	1397.53	14.60	-6939.87	-89.01	5060.44

B) (LOAD CASE 4)

N O R M A L   O P E R A T I N G   T E M P E R A T U R E   I N C L .   T H E R M A L   A N C H O R   M O V E M E N T S

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN.-LB.)		
	X	Y	Z	X	Y	Z
1	-117.2	5610.7	-1139.7	756253.8	19846.1	3849.6
7	.0	561.0	.0	.0	.0	.0
14	-2133.3	-2668.5	195.0	134604.2	-118404.8	41797.0
1P	1859.7	-1990.6	1080.2	99777.1	119644.3	3810.7
2P	.0	-481.2	.0	.0	.0	.0
40	-525.3	183.3	-423.4	1836.2	312.7	1897.1
43	-408.5	1101.9	292.0	1075.3	405.8	1933.2
4P	1324.6	-2317.4	-4.0	70344.5	15409.6	-32785.2

C) (LOAD CASE 6)

S E I S M I C   A N C H O R   M O V E M E N T S   X - D I R E C T I O N ( 1 / 2   S S E )

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN.-LB.)		
	X	Y	Z	X	Y	Z
1	-174.35	-11.96	13.21	-805.35	30403.00	33649.35
7	.00	99.67	.00	.00	.00	.00
14	81.37	276.17	-68.16	-17358.68	3681.06	153.07
1P	39.07	-212.12	71.97	13036.21	3307.54	8075.46
2P	.00	-116.05	.00	.00	.00	.00
40	25.08	76.69	-23.16	56.25	72.01	132.60
43	1.25	10.52	-14.09	44.79	54.44	53.01
4P	27.58	-115.88	25.27	5275.20	1772.71	917.68

## ELASTIC SUPPORT REACTIONS

(LOAD CASE 7)

SEISMIC ANCHOR MOVEMENTS Z - DIRECTION (1/2 SSE)

SUPPORT JOINT	FORCE ( LB. )			MOMENT ( IN.-LB. )		
	X	Y	Z	X	Y	Z
1	13.20	488.09	-264.54	32863.67	-2814.02	-858.73
7	.00	6.60	.00	.00	.00	.00
14	-34.25	-209.68	131.06	3660.62	-189.20	5362.95
18	38.03	-459.58	82.23	20028.81	2825.93	5224.19
25	.00	277.86	.00	.00	.00	.00
40	-15.56	-26.61	18.42	-24.50	-44.73	-14.75
47	-.27	-15.16	9.83	-8.58	-41.17	-22.69
48	-1.15	-61.51	23.01	2784.26	-83.30	676.13

(LOAD CASE 12)

SEISMIC ANCHOR MOVEMENTS X - DIRECTION (SSE)

SUPPORT JOINT	FORCE ( LB. )			MOMENT ( IN.-LB. )		
	X	Y	Z	X	Y	Z
1	-374.62	-22.04	24.28	-1483.91	58422.02	64455.14
7	.00	170.97	.00	.00	.00	.00
14	167.07	526.25	-143.95	-33004.47	7562.16	250.88
18	78.98	-412.84	149.41	24617.40	6764.44	15303.03
25	.00	-212.47	.00	.00	.00	.00
40	40.84	122.92	-46.41	97.73	114.69	223.32
47	2.33	20.64	-23.65	75.96	88.11	89.94
48	44.61	-193.39	40.72	8850.81	2873.10	1503.23

(LOAD CASE 13)

SEISMIC ANCHOR MOVEMENTS Z - DIRECTION (SSE)

SUPPORT JOINT	FORCE ( LB. )			MOMENT ( IN.-LB. )		
	X	Y	Z	X	Y	Z
1	24.27	935.13	-507.32	62964.62	-5050.09	-1601.17
7	.00	32.63	.00	.00	.00	.00
14	-64.23	-404.87	240.68	7283.25	-335.03	10229.40
18	69.71	-873.10	183.25	37986.93	5665.48	9827.18
25	.00	484.20	.00	.00	.00	.00
40	-26.64	-48.99	30.74	-33.60	-80.22	-18.03
47	-.05	-20.48	13.80	-11.39	-70.93	-34.14
48	-3.06	-105.55	36.84	4857.96	-209.27	1109.55

TABLE B-11

## ELASTIC SUPPORT REACTIONS

(LOAD CASE 8)

X + Y EARTHQUAKE (1/2 SSE)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 34 BY SQSS SUMMATION

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN.-LB.)		
	X	Y	Z	X	Y	Z
1	2549.	202.	389.	12710.	339944.	35355.
7	1705.	391.	.	.	.	.
14	718.	174.	478.	12707.	34457.	2088.
18	432.	313.	893.	16149.	36655.	7896.
25	.	800.	.	.	.	.
26	359.	.	418.	.	.	.
40	499.	526.	588.	820.	1604.	1261.
43	78.	424.	308.	528.	1298.	809.
48	267.	781.	475.	15944.	10259.	26176.
54	885.	.	509.	.	.	.

(LOAD CASE 9)

Z + Y EARTHQUAKE (1/2 SSE)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 34 BY SQSS SUMMATION

SUPPORT JOINT	FORCE ( LB. )			MOMENT (IN.-LB.)		
	X	Y	Z	X	Y	Z
1	714.	927.	1439.	61227.	94698.	10560.
7	528.	1472.	.	.	.	.
14	615.	347.	754.	8927.	24158.	9195.
18	245.	835.	819.	37065.	20165.	11229.
25	.	739.	.	.	.	.
26	329.	.	457.	.	.	.
40	406.	492.	588.	810.	1595.	1256.
43	53.	412.	305.	528.	1298.	803.
48	216.	788.	468.	15598.	11006.	25559.
54	880.	.	575.	.	.	.

## ELASTIC SUPPORT REACTIONS

J) (LOAD CASE 10)

X + Y DRE EARTHQUAKE (SSE)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 34 BY SQSS SUMMATION

SUPPORT JOINT	FORCE ( LB. )			MOMENT ( IN.-LB. )		
	X	Y	Z	X	Y	Z
1	2229.	305.	452.	18956.	296878.	31114.
7	1515.	642.	.	.	.	.
1A	797.	205.	472.	14853.	39317.	3166.
1B	535.	421.	1097.	21162.	44344.	9822.
2A	.	1317.	.	.	.	.
2B	555.	.	644.	.	.	.
4A	527.	735.	612.	975.	1761.	1350.
4B	124.	554.	337.	578.	1363.	873.
4C	383.	950.	563.	21336.	17355.	32390.
5A	998.	.	862.	.	.	.

K) (LOAD CASE 11)

Z + Y DRE EARTHQUAKE (SSE) + Z - ANCHOR MOVE. (SSE)

TOTAL RESPONSE EQUALS MODE 1 THROUGH 34 BY SQSS SUMMATION

SUPPORT JOINT	FORCE ( LB. )			MOMENT ( IN.-LB. )		
	X	Y	Z	X	Y	Z
1	645.	862.	1305.	56565.	84038.	10444.
7	496.	1410.	.	.	.	.
1A	609.	336.	714.	12440.	30551.	8509.
1B	394.	801.	1047.	36180.	33159.	12017.
2A	.	1230.	.	.	.	.
2B	490.	.	675.	.	.	.
4A	519.	740.	605.	950.	1737.	1336.
4B	88.	529.	324.	570.	1354.	852.
4C	284.	940.	540.	20594.	16736.	30358.
5A	980.	.	854.	.	.	.

TABLE B-III

COMPLIANCE WITH ASME CODE EQUATIONS 8, 9, 10 and 11

Pages B-15 through B-32

NOTE: Stresses for members between node points 10 - 14 and 10 - 18 should be increased by a factor of 1.21 to account for the inconsistency between pipe wall thickness used in the analysis and the actual wall thickness of the pipe. In view of the low stresses and low masses of these members, the effect of this inconsistency on the overall analysis is small. Stresses for these members, as shown on Figure 7.6 and 7.7, have already been increased by this factor of 1.21.

JACRWD MAIN STEAM LINE PIPING CLASS 2 ANALYSIS

D.1) CLASS 2 STRESSES FOR ANALYSIS SET NUMBER 1

ASSUMED LOAD COMBINATION IDENTIFIERS  
MA = 1 MB = 7 MC = 3 PD = 1 PHAX = 2

D.1.1) SATISFACTION OF EQUATION A (ANALYSIS SET 1)

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (PHAX)	SUSTAINED LOAD STRESS (SHA)	OCCASIONAL LOAD STRESS (SHI)	THERMAL EXPANSION STRESS (SHC)	TOTAL STRESS (I TR)	MODIFIED ALLOWABLE STRESS (SAMI)	DESIGN STRESS RATIO TB/(1.0*SMI)	MODIFIED STRESS RATIO
15	5	4094.604	.000	1006.063	.000	.000	5102.667	32531.443	.15992	
15	6	4074.604	.000	242.421	.000	.000	4334.424	33140.239	.27242	
25	5	4094.604	.000	176.305	.000	.000	4272.909	33234.777	.26574	
25	6	4054.604	.000	151.332	.000	.000	4247.937	33264.004	.26717	
25	7	4004.604	.000	151.732	.000	.000	4247.937	33264.004	.26717	
35	7	4004.604	.000	174.108	.000	.000	4270.712	33234.844	.26668	
35	8	4094.604	.000	254.524	.000	.000	4353.128	33144.591	.27374	
35	9	4094.604	.000	349.700	.000	.000	4444.345	33034.323	.27965	
35	0	4094.604	.000	394.202	.000	.000	4493.876	33044.865	.28257	
35	10	4094.604	.000	543.403	.000	.000	4634.508	32924.168	.29179	
35	9	4094.604	.000	647.028	.000	.000	4793.433	32794.182	.30149	
35	19	4094.604	.000	710.316	.000	.000	4804.922	32742.866	.30232	
35	10	4094.604	.000	400.409	.000	.000	4497.214	33044.118	.27384	
35	10	4094.604	.000	313.305	.000	.000	4404.409	33124.327	.27734	
35	10	4094.604	.000	257.152	.000	.000	4344.757	33172.287	.27351	
35	61	4094.604	.000	257.157	.000	.000	4344.522	33171.456	.27351	
115	12	3850.027	.000	257.913	.000	.000	4117.940	33372.751	.25868	
115	13	3850.027	.000	124.102	.000	.000	3985.128	33411.391	.25064	
115	14	3850.027	.000	347.940	.000	.000	4242.947	33242.228	.26465	
115	17	3850.027	.000	511.604	.000	.000	4370.431	33153.714	.27488	
125	20	4094.604	.000	404.566	.000	.000	4702.171	32871.905	.29573	
125	21	4094.604	.000	580.033	.000	.000	4676.638	32803.808	.29413	
125	66	3850.027	.000	574.934	.000	.000	4438.961	33045.433	.27914	
145	11	3850.027	.000	242.053	.000	.000	4101.090	33382.632	.25763	
145	61	3850.027	.000	464.156	.000	.000	4327.143	33140.444	.27215	
145	15	3850.027	.000	464.470	.000	.000	4323.497	33143.778	.27192	

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (PHAX)	SUSTAINED LOAD STRESS (SHA)	OCCASIONAL LOAD STRESS (SHI)	THERMAL EXPANSION STRESS (SHC)	TOTAL STRESS (I TR)	MODIFIED ALLOWABLE STRESS (SAMI)	DESIGN STRESS RATIO TB/(1.0*SMI)	MODIFIED STRESS RATIO
10	4	4800.402	.000	435.990	.000	.000	5245.391	27416.078	.34972	
10	5	4800.402	.000	314.559	.000	.000	5124.340	27517.534	.34174	
20	11	3450.027	.000	324.039	.000	.000	4183.042	33313.148	.24364	
20	12	3450.027	.000	339.912	.000	.000	4194.930	33300.452	.24404	
30	13	3450.027	.000	168.811	.000	.000	4077.838	33445.047	.24332	
30	14	3450.027	.000	394.474	.000	.000	4213.501	33247.274	.24507	
40	15	3450.027	.000	421.783	.000	.000	4446.810	33040.042	.24141	
40	16	3450.027	.000	513.578	.000	.000	4373.075	33351.456	.24553	
40	17	3450.027	.000	644.881	.000	.000	4541.998	33004.448	.24574	
40	18	3450.027	.000	1043.327	.000	.000	4902.404	32701.707	.30733	
40	19	4094.604	.000	934.563	.000	.000	5091.148	32541.258	.30020	
40	20	4094.604	.000	847.893	.000	.000	4944.458	32665.927	.31097	

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (PHAX)	SUSTAINED LOAD STRESS (SHA)	OCCASIONAL LOAD STRESS (SHI)	THERMAL EXPANSION STRESS (SHC)	TOTAL STRESS (I TR)	MODIFIED ALLOWABLE STRESS (SAMI)	DESIGN STRESS RATIO TB/(1.0*SMI)	MODIFIED STRESS RATIO
115	21	4800.402	.000	487.255	.000	.000	5467.657	27224.001	.34447	
115	22	4800.402	.000	554.192	.000	.000	5344.093	27313.914	.35773	
115	23	4800.402	.000	544.793	.000	.000	5374.844	27354.403	.35031	
115	24	4800.402	.000	744.047	.000	.000	5531.849	27154.208	.37027	
115	25	4800.402	.000	594.443	.000	.000	5394.244	27244.492	.35994	
115	26	4800.402	.000	175.020	.000	.000	4953.021	27434.002	.33219	
115	27	4800.402	.000	150.207	.000	.000	4905.079	27474.242	.33320	
115	64	4800.402	.000	324.174	.000	.000	5134.175	27504.751	.34241	
115	28	4800.402	.000	1177.057	.000	.000	6104.474	26444.197	.40444	
215	29	4094.604	.000	780.246	.000	.000	5714.423	27074.201	.35740	
215	30	4094.604	.000	493.512	.000	.000	5424.159	27264.007	.34334	
215	31	4094.604	.000	493.512	.000	.000	5424.159	27264.007	.34334	
215	32	4094.604	.000	407.275	.000	.000	5474.812	27244.240	.34820	
215	33	4094.604	.000	1174.025	.000	.000	6094.462	26734.114	.40572	
215	34	4094.604	.000	1357.415	.000	.000	7081.902	26134.007	.44180	
215	35	4094.604	.000	1041.182	.000	.000	6407.439	27184.219	.38443	
215	36	4094.604	.000	474.131	.000	.000	5144.104	27302.388	.35787	
215	37	4094.604	.000	574.789	.000	.000	5304.344	27344.402	.35374	
215	38	4094.604	.000	444.036	.000	.000	4987.113	27474.004	.34247	
215	39	4094.604	.000	444.036	.000	.000	4987.113	27474.004	.34247	
215	37	4094.604	.000	712.150	.000	.000	5444.704	27044.000	.37224	
215	38	4094.604	.000	727.403	.000	.000	5453.048	27044.004	.37044	
215	39	4094.604	.000	1040.114	.000	.000	6014.071	26744.003	.40018	
215	40	4094.604	.000	1011.782	.000	.000	6134.330	26674.400	.40120	



MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE (PI)	PEAK STRESS (PMAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAH)	DESIGN STRESS RATIO (T/SAH)	MODIFIED STRESS RATIO
2A	40	4924,577	.000	1189,914	.000	.000	6116,491	24675,983	.40777	
	41	4924,577	.000	558,256	.000	.000	5478,813	27219,492	.36512	
2A	41	4924,577	.000	558,256	.000	.000	5478,813	27219,492	.36512	
	42	4924,577	.000	374,592	.000	.000	5003,149	27377,304	.35354	
3A	43	4924,577	.000	364,426	.000	.000	4233,203	27374,277	.35771	
	44	4924,577	.000	273,465	.000	.000	5201,042	27454,944	.34457	
31S	45	4924,577	.000	281,734	.000	.000	5219,311	27447,936	.34727	
	46	4924,577	.000	217,967	.000	.000	5144,494	27502,108	.34297	
32S	44	4924,577	.000	294,947	.000	.000	5221,124	27439,144	.34887	
	47	4924,577	.000	261,371	.000	.000	5287,947	27386,245	.34523	
33S	47	4924,577	.000	434,277	.000	.000	5562,854	27144,574	.37026	
	48	4924,577	.000	527,022	.000	.000	5451,599	27214,441	.36087	
34S	47	4924,577	.000	949,843	.000	.000	5474,670	26990,723	.38171	
	49	4924,577	.000	912,441	.000	.000	5733,010	26956,935	.37240	
3A	50	4924,577	.000	799,017	.000	.000	5724,544	27000,245	.37171	
	51	4924,577	.000	779,225	.000	.000	5701,802	27025,068	.36839	
3A	51	4924,577	.000	779,225	.000	.000	5701,802	27025,068	.36839	
	52	4924,577	.000	786,940	.000	.000	5713,117	27019,851	.36987	
37A	52	4924,577	.000	2337,794	.000	.000	7254,371	25704,535	.44394	
	53	4924,577	.000	2337,794	.000	.000	7254,371	25704,535	.44394	
	54	4924,577	.000	272,919	.000	.000	6199,596	27490,103	.34457	
3A	54	4924,577	.000	613,431	.000	.000	5540,008	27145,003	.34933	
	55	4924,577	.000	593,385	.000	.000	5519,961	27183,033	.34700	
3A	55	4924,577	.000	593,385	.000	.000	5519,961	27183,033	.34700	
	56	4924,577	.000	447,584	.000	.000	5374,141	27306,044	.35482	
	56	4924,577	.000	395,780	.000	.000	5207,357	27310,997	.35482	
4A	57	4924,577	.000	389,974	.000	.000	5307,551	27363,582	.35384	
	58	4924,577	.000	347,046	.000	.000	5293,423	27375,420	.35291	
41S	57	4924,577	.000	347,046	.000	.000	5293,423	27375,420	.35291	
	59	4924,577	.000	773,365	.000	.000	5583,187	27129,291	.37221	
41S	59	4924,577	.000	773,365	.000	.000	5583,187	27129,291	.37221	
	63	4924,577	.000	715,091	.000	.000	5524,892	27178,841	.36833	
42S	63	4924,577	.000	715,091	.000	.000	5524,892	27178,841	.36833	
	24	4924,577	.000	745,013	.000	.000	5554,615	27153,408	.37032	
	24	4924,577	.000	267,750	.000	.000	5197,051	27457,507	.34547	
42S	24	4924,577	.000	267,750	.000	.000	5197,051	27457,507	.34547	
	27	4924,577	.000	335,949	.000	.000	5145,801	27501,049	.34305	
	27	4924,577	.000	327,127	.000	.000	5136,928	27508,611	.34246	

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE (PI)	PEAK STRESS (PMAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAH)	DESIGN STRESS RATIO (T/SAH)	MODIFIED STRESS RATIO
7C	22	4924,577	.000	881,383	.000	.000	5691,195	27037,561	.37941	
	23	4924,577	.000	894,932	.000	.000	5704,734	27075,976	.38032	
8C	24	4924,577	.000	613,431	.000	.000	5423,492	27245,041	.36156	
	24	4924,577	.000	932,424	.000	.000	5742,224	26994,108	.37242	
9C	27	4924,577	.000	514,352	.000	.000	5324,151	27046,070	.35721	
	28	4924,577	.000	424,576	.000	.000	5234,377	27432,379	.34993	
13C	31	4924,577	.000	750,201	.000	.000	5685,774	27042,049	.37905	
	32	4924,577	.000	931,858	.000	.000	5854,435	26895,330	.39054	
11C	34	4924,577	.000	481,752	.000	.000	5407,929	27214,240	.34051	
	35	4924,577	.000	40,535	.000	.000	4947,113	27434,954	.33247	
12C	36	4924,577	.000	767,664	.000	.000	5494,241	27031,155	.37977	
	37	4924,577	.000	1702,790	.000	.000	6124,377	26845,048	.42747	
13C	38	4924,577	.000	1194,998	.000	.000	6121,474	26817,641	.42711	
	39	4924,577	.000	1747,500	.000	.000	6714,137	26167,983	.44761	

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE (PI)	PEAK STRESS (PMAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAH)	DESIGN STRESS RATIO (T/SAH)	MODIFIED STRESS RATIO
14C	43	4924,577	.000	618,568	.000	.000	5545,245	27161,542	.34968	
	43	4924,577	.000	614,375	.000	.000	5542,852	27163,576	.34952	
15C	44	4924,577	.000	449,250	.000	.000	5375,827	27305,547	.35630	
	45	4924,577	.000	447,834	.000	.000	5389,411	27294,001	.35729	
14C	49	4924,577	.000	1334,683	.000	.000	6261,290	26942,999	.41742	
	50	4924,577	.000	1319,621	.000	.000	6234,204	26571,674	.41595	
17C	51	4924,577	.000	446,975	.000	.000	5373,457	27307,546	.35423	
	54	4924,577	.000	1007,749	.000	.000	5934,326	26370,673	.35482	
18C	55	4924,577	.000	395,780	.000	.000	5327,357	27250,997	.35482	
	57	4924,577	.000	389,974	.000	.000	5307,551	27363,582	.35384	
19C	58	4924,577	.000	609,986	.000	.000	5529,543	27174,871	.36864	
	59	4924,577	.000	623,924	.000	.000	5550,501	27157,074	.37003	

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE (PI)	PEAK STRESS (PMAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAH)	DESIGN STRESS RATIO (T/SAH)	MODIFIED STRESS RATIO
44C	1	5823,472	.000	373,789	.000	.000	6197,461	26507,159	.41316	
	2	5823,472	.000	584,812	.000	.000	6412,474	26424,349	.42761	
44C	2	5823,472	.000	584,812	.000	.000	6412,474	26424,349	.42761	
	3	5823,472	.000	1327,840	.000	.000	7151,512	25796,215	.47677	



LACROR MAIN STEAM LINE PIPING CLASS 2 ANALYSIS

0.1.2 SATISFACTION OF EQUATION 9 (ANALYSIS SET 1)

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (P/MAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAM)	UPSET STRESS RATIO T9/(1.2*SH)	EMERGENCY STRESS RATIO T9/(1.4*SH)
15	3	.000	4443.227	1004.063	784.796	.000	6254.015	32531.483	.22709	.21866
4	.000	4443.227	242.821	865.771	.000	5571.819	33180.239	.29202	.19444	
25	5	.000	4443.227	176.305	930.415	.000	5630.146	33276.777	.24507	.19677
6	.000	4443.227	151.332	454.415	.000	5044.974	33254.004	.24567	.17711	
75	6	.000	4443.227	174.108	174.108	.000	5066.474	33254.004	.24567	.17711
7	.000	4443.227	174.108	174.108	.000	6330.899	33231.444	.33443	.22294	
45	7	.000	4443.227	254.524	934.501	.000	6330.899	33231.444	.33443	.22294
8	.000	4443.227	254.524	934.501	.000	5654.251	33164.591	.29455	.19775	
65	8	.000	4443.227	349.780	474.537	.000	5927.544	33049.323	.27459	.19309
9	.000	4443.227	394.202	630.841	.000	5494.509	33044.865	.28818	.19212	
75	9	.000	4443.227	697.028	153.144	.000	5093.059	32925.168	.30084	.20591
19	.000	4443.227	710.318	645.736	.000	5313.400	32794.162	.27848	.18565	
95	10	.000	4443.227	400.609	83.390	.000	4927.826	32782.866	.30499	.20333
60	.000	4443.227	313.305	304.820	.000	5072.152	33120.327	.26617	.17219	
95	10	.000	4443.227	252.152	145.509	.000	4861.298	33171.856	.26478	.16944
41	.000	4443.227	252.917	434.450	.000	5154.794	33172.751	.26494	.17597	
105	12	.000	4204.387	253.913	478.870	.000	4924.370	33372.751	.25472	.17243
13	.000	4204.387	126.102	524.337	.000	4854.826	33441.341	.25445	.16963	
115	14	.000	4204.387	383.940	565.502	.000	5153.830	33242.270	.27012	.18004
17	.000	4204.387	511.604	567.353	.000	5274.344	33153.714	.27654	.18443	
175	20	.000	4443.227	695.566	695.439	.000	5674.232	32871.905	.29527	.19694
21	.000	4443.227	530.033	590.472	.000	5633.732	32843.488	.29527	.19694	
115	20	.000	4204.387	579.934	584.710	.000	5359.032	33045.633	.29040	.19694
11	.000	4204.387	242.053	484.205	.000	4931.445	33382.832	.25847	.17231	
145	61	.000	4204.387	468.156	894.547	.000	5477.070	33190.404	.28756	.19137
15	.000	4204.387	464.470	572.956	.000	5241.814	33143.778	.27473	.18315	

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (P/MAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAM)	UPSET STRESS RATIO T9/(1.2*SH)	EMERGENCY STRESS RATIO T9/(1.4*SH)
10	4	.000	4204.387	435.950	1554.409	.000	7230.749	27416.078	.40171	.26741
5	.000	4204.387	316.559	1774.467	.000	7335.477	27517.564	.40753	.27144	
20	11	.000	4204.387	324.035	669.841	.000	5177.943	33313.148	.27138	.18099
12	.000	4204.387	339.912	630.489	.000	5184.288	33299.452	.27171	.18114	
13	.000	4204.387	168.811	701.427	.000	5075.126	33445.087	.26599	.17733	
14	.000	4204.387	354.474	1133.316	.000	5692.177	33287.274	.29833	.19845	

AC	15	.000	4204.387	621.793	767.813	.000	5593.183	33060.662	.29314	.19543
EC	16	.000	4204.387	513.078	767.034	.000	5475.399	33151.696	.28697	.19131
17	.000	4204.387	444.881	752.818	.000	5442.076	33006.428	.29571	.19714	
AC	18	.000	4443.227	1043.377	1257.419	.000	8505.543	32701.707	.34095	.23731
19	.000	4443.227	994.563	924.114	.000	6361.928	32541.258	.33343	.23229	
20	.000	4443.227	847.893	847.715	.000	6158.835	32665.927	.32279	.21519	

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (P/MAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAM)	UPSET STRESS RATIO T9/(1.2*SH)	EMERGENCY STRESS RATIO T9/(1.4*SH)
145	21	.000	6240.251	657.256	640.094	.000	6584.590	27294.001	.34441	.24321
22	.000	6240.251	554.182	640.416	.000	6441.848	27313.914	.34010	.24007	
145	22	.000	6240.251	564.783	700.790	.000	6513.354	27309.603	.34185	.24124
57	.000	6240.251	744.047	700.790	.000	6447.177	27314.229	.34151	.24147	
175	25	.000	6240.251	644.443	644.443	.000	6473.576	27284.492	.34544	.24374
24	.000	6240.251	173.020	502.761	.000	5915.632	27639.602	.32943	.23974	
145	24	.000	6240.251	185.207	492.243	.000	5929.791	27609.202	.32943	.23974
44	.000	6240.251	324.374	511.517	.000	6083.141	27559.251	.32943	.23974	
194	28	.000	6247.477	1177.897	2312.594	.000	8557.843	26646.187	.44211	.30577
29	.000	6247.477	700.346	1394.765	.000	7543.478	27024.201	.41904	.29310	
285	29	.000	6247.477	744.246	1394.765	.000	7543.478	27024.201	.41904	.29310
30	.000	6247.477	421.532	1400.005	.000	7270.014	27247.927	.40194	.28939	
214	30	.000	6247.477	443.432	1400.005	.000	7270.014	27247.927	.40194	.28939
31	.000	6247.477	443.432	1400.005	.000	7270.014	27247.927	.40194	.28939	
225	32	.000	6247.477	443.432	884.434	.000	6714.048	27254.593	.37200	.24947
33	.000	6247.477	443.432	824.480	.000	6754.652	27255.200	.37200	.24947	
230	33	.000	6247.477	1124.225	567.843	.000	7041.748	26735.110	.38337	.25033
34	.000	6247.477	137.415	302.116	.000	7024.008	26733.607	.38337	.25033	
244	34	.000	6247.477	481.352	1044.495	.000	6934.414	27278.240	.38577	.25040
60	.000	6247.477	499.731	1000.403	.000	6794.811	27322.708	.38577	.25040	
245	35	.000	6247.477	379.792	2607.774	.000	8414.642	27304.187	.44741	.31144
36	.000	6247.477	443.432	1524.445	.000	6954.489	27325.954	.38447	.25144	
245	37	.000	6247.477	424.805	1744.169	.000	7189.471	27299.140	.42174	.28119
38	.000	6247.477	724.200	1624.449	.000	7224.575	27064.682	.42174	.28119	
275	39	.000	6247.477	724.200	1624.449	.000	7224.575	27064.682	.42174	.28119
40	.000	6247.477	1044.114	1044.114	.000	7124.724	27044.169	.42174	.28119	
284	40	.000	6247.477	1211.753	1044.114	.000	7504.194	26762.413	.44877	.31554
41	.000	6247.477	1144.914	1021.344	.000	7435.577	26657.420	.44877	.31554	
204	41	.000	6247.477	550.214	820.541	.000	7574.677	26675.893	.44877	.31554
42	.000	6247.477	654.216	814.045	.000	6744.094	27019.402	.37403	.25070	
204	42	.000	6247.477	274.442	200.429	.000	6737.709	27210.664	.37403	.25070
204	43	.000	6247.477	374.442	200.429	.000	6524.147	27247.366	.37301	.25070
44	.000	6247.477	374.442	694.470	.000	6614.270	27304.777	.37301	.25070	
314	44	.000	6247.477	274.442	1144.064	.000	6954.489	27444.994	.37301	.25070
45	.000	6247.477	274.442	1144.064	.000	6954.489	27444.994	.37301	.25070	
324	45	.000	6247.477	274.442	1144.064	.000	6954.489	27444.994	.37301	.25070
46	.000	6247.477	274.442	1144.064	.000	6954.489	27444.994	.37301	.25070	
47	.000	6247.477	274.442	1144.064	.000	6954.489	27444.994	.37301	.25070	
334	47	.000	6247.477	274.442	1144.064	.000	6954.489	27444.994	.37301	.25070
48	.000	6247.477	274.442	1144.064	.000	6954.489	27444.994	.37301	.25070	
344	48	.000	6247.477	274.442	1144.064	.000	6954.489	27444.994	.37301	.25070
49	.000	6247.477	274.442	1144.064	.000	6954.489	27444.994	.37301	.25070	

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PROXIMATE STRESS (P/AX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAM)	UPSET STRESS RATIO T9/(1.2*SH)	EMERGENCY STRESS RATIO T9/(1.8*SH)
375	50	.000	6367,477	799,017	1523,526	.000	7690,070	27008,245	.42722	.28492
	51	.000	6367,477	779,225	1827,494	.000	7774,194	27025,068	.43190	.28793
375	61	.000	6367,477	766,540	1591,646	.000	7747,602	27018,951	.43043	.28694
	62	.000	6367,477	2332,794	1308,702	.000	9008,073	25704,435	.50950	.33367
375	69	.000	6367,477	2132,794	1308,702	.000	9008,073	25704,535	.50950	.33367
	57	.000	6367,477	272,019	1572,399	.000	7216,856	27496,193	.46094	.28730
375	64	.000	6367,477	413,431	1871,665	.000	7052,873	27165,993	.46595	.29084
	65	.000	6367,477	593,385	1306,576	.000	7351,439	27183,033	.48041	.29224
308	66	.000	6367,477	447,584	1306,573	.000	7130,634	27306,844	.39892	.28595
	6A	.000	6367,477	305,780	974,836	.000	6738,893	27350,997	.37434	.28454
408	67	.000	6367,477	380,974	1351,268	.000	7101,709	27363,582	.38454	.28303
	58	.000	6367,477	367,045	2537,831	.000	8272,304	27375,420	.45454	.30878
415	67	.000	6240,251	773,385	691,010	.000	8704,646	27129,291	.37248	.28832
	67	.000	6240,251	715,091	667,857	.000	8623,178	27175,841	.36796	.28590
476	67	.000	6240,251	745,013	656,837	.000	8642,101	27153,408	.36901	.28400
	74	.000	6240,251	387,250	643,149	.000	6270,669	27457,507	.34837	.28224
476	6A	.000	6240,251	335,999	517,740	.000	6088,490	27501,069	.33825	.28550
	27	.000	6240,251	327,127	540,092	.000	6107,470	27508,611	.33930	.28260

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PROXIMATE STRESS (P/AX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAM)	UPSET STRESS RATIO T9/(1.2*SH)	EMERGENCY STRESS RATIO T9/(1.8*SH)
7C	22	.000	6240,251	881,303	1086,082	.000	7207,637	27037,561	.40042	.28695
	23	.000	6240,251	894,932	1121,423	.000	7257,606	27025,976	.40320	.28890
8C	24	.000	6240,251	813,620	1019,140	.000	6873,011	27245,091	.38183	.28454
	25	.000	6240,251	532,624	1021,854	.000	7194,599	26994,108	.39970	.28664
4C	27	.000	6240,251	518,152	851,809	.000	6614,411	27346,070	.36747	.28494
	28	.000	6240,251	428,576	841,408	.000	6510,235	27422,375	.35168	.28112
14C	31	.000	6367,477	759,201	1457,054	.000	7579,632	27042,089	.42107	.28073
	32	.000	6367,477	931,858	1351,590	.000	7652,925	26895,330	.42516	.28344
11C	34	.000	6367,477	481,352	1087,595	.000	6931,414	27278,260	.36547	.28693
	35	.000	6367,477	401,535	1522,405	.000	6956,449	27635,954	.38447	.28785
17C	36	.000	6367,477	749,604	2848,746	.000	9222,196	27033,195	.50123	.33414
	37	.000	6367,477	1202,780	2670,133	.000	9248,390	26865,066	.51335	.34224
13C	38	.000	6367,477	1194,940	1787,174	.000	8344,672	26871,661	.46359	.30904
	39	.000	6367,477	1787,560	1771,900	.000	8924,958	26161,983	.49594	.33063
14C	42	.000	6367,477	618,668	1297,937	.000	7284,072	27161,542	.40467	.28974
	43	.000	6367,477	614,275	1201,703	.000	7593,054	27163,576	.42144	.28122
15C	44	.000	6367,477	442,250	1501,882	.000	7725,469	27305,547	.42513	.28400
	45	.000	6367,477	462,034	1831,065	.000	7679,297	27244,001	.42513	.28400
16C	49	.000	6367,477	1324,883	2730,882	.000	9432,502	26552,929	.57523	.34595
	50	.000	6367,477	1712,631	2502,958	.000	9182,945	26571,674	.51016	.34031
17C	51	.000	6367,477	444,875	2591,297	.000	8405,648	27307,568	.44693	.31132
	54	.000	6367,477	1007,749	3074,784	.000	9450,010	26830,023	.52500	.38000
18C	54	.000	6367,477	395,780	974,836	.000	6738,893	27350,997	.37434	.28454
	57	.000	6367,477	380,974	1351,268	.000	7101,709	27363,582	.38454	.28303
19C	58	.000	6367,477	602,988	4169,264	.000	10139,629	27174,871	.56331	.37554
	59	.000	6367,477	623,924	4381,979	.000	10373,390	27157,074	.57633	.38420

LACROW MAIN STEAM LINE PIPING CLASS 2 ANALYSIS

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PROXIMATE STRESS (P/AX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAM)	UPSET STRESS RATIO T9/(1.2*SH)	EMERGENCY STRESS RATIO T9/(1.8*SH)
445	1	.000	6223,672	373,789	5631,157	.000	11828,618	26607,159	.45715	.43810
	2	.000	6223,672	504,812	2784,423	.000	9174,907	26424,389	.50983	.33989
445	2	.000	6223,672	588,812	2764,423	.000	9174,907	26424,389	.50983	.33989
	3	.000	6223,672	1327,840	643,879	.000	7795,390	25796,215	.40308	.28072

LACRUP MAIN STEAM LINE PIPING CLASS 2 ANALYSIS

0.1.3 SATISFACTION OF EQUATION 10 (ANALYSIS SET 1)

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (P/AX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MA)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TI)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T10/(1.0+SAM)	MODIFIED STRESS RATIO T10/(1.0+SAM)
15	3	.000	.000	.000	.000	666,902	666,902	32531,483	.02884	.03000
	4	.000	.000	.000	.000	5073,207	5073,207	33180,239	.21504	.19130
	5	.000	.000	.000	.000	6172,644	6172,644	33236,777	.24217	.19421
	6	.000	.000	.000	.000	3804,169	3804,169	33254,004	.14974	.11917
	7	.000	.000	.000	.000	2037,442	2037,442	33258,444	.14974	.11919
	8	.000	.000	.000	.000	2037,442	2037,442	33234,644	.08724	.08130
	9	.000	.000	.000	.000	1532,497	1532,497	33164,591	.08562	.06478
	10	.000	.000	.000	.000	3835,610	3835,610	33057,323	.16474	.11592
	11	.000	.000	.000	.000	5627,291	5627,291	33259,845	.24096	.17027
	12	.000	.000	.000	.000	3231,915	3231,915	32925,168	.13139	.08914
	13	.000	.000	.000	.000	4097,612	4097,612	32774,162	.17546	.12446
	14	.000	.000	.000	.000	4305,970	4305,970	32782,684	.18438	.13134
	15	.000	.000	.000	.000	3201,970	3201,970	33044,118	.13711	.08490
	16	.000	.000	.000	.000	2787,892	2787,892	33130,327	.11938	.07417
	17	.000	.000	.000	.000	2930,656	2930,656	33172,307	.12649	.08436
	18	.000	.000	.000	.000	2554,571	2554,571	33171,456	.10941	.07731
	19	.000	.000	.000	.000	2946,141	2946,141	33372,751	.12614	.08924
	20	.000	.000	.000	.000	4050,784	4050,784	33481,391	.17517	.12718
	21	.000	.000	.000	.000	2981,103	2981,103	33240,228	.12766	.09487
	22	.000	.000	.000	.000	4021,501	4021,501	33153,714	.17200	.12135
	23	.000	.000	.000	.000	4069,692	4069,692	32871,905	.17426	.12388
	24	.000	.000	.000	.000	2345,376	2345,376	32893,608	.10043	.07136
	25	.000	.000	.000	.000	5160,453	5160,453	33095,633	.22097	.15593
	26	.000	.000	.000	.000	3686,545	3686,545	33382,832	.15786	.11047
	27	.000	.000	.000	.000	4747,050	4747,050	33190,644	.20327	.14302
	28	.000	.000	.000	.000	3686,787	3686,787	33193,778	.15787	.11107

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (P/AX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MA)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TI)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T10/(1.0+SAM)	MODIFIED STRESS RATIO T10/(1.0+SAM)
1C	4	.000	.000	.000	.000	4019,245	4019,245	27416,078	.47160	.32884
	5	.000	.000	.000	.000	10993,329	10993,329	27517,594	.57481	.39190
	11	.000	.000	.000	.000	4635,153	4635,153	33313,148	.21132	.14814
	12	.000	.000	.000	.000	3043,970	3043,970	33249,452	.14888	.11444
	13	.000	.000	.000	.000	5476,307	5476,307	33445,087	.23449	.16374
	14	.000	.000	.000	.000	6955,449	6955,449	33287,274	.29783	.20895

LACRUP MAIN STEAM LINE PIPING CLASS 2 ANALYSIS

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (P/AX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MA)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TI)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T10/(1.0+SAM)	MODIFIED STRESS RATIO T10/(1.0+SAM)
15	21	.000	.000	.000	.000	2657,625	2657,625	27228,011	.17866	.09741
	22	.000	.000	.000	.000	2592,879	2592,879	27313,914	.17866	.09493
	23	.000	.000	.000	.000	2067,863	2067,863	27306,403	.10812	.07573
	24	.000	.000	.000	.000	1210,252	1210,252	27194,228	.06328	.04467
	25	.000	.000	.000	.000	1365,186	1365,186	27248,442	.07134	.05003
	26	.000	.000	.000	.000	1780,317	1780,317	27430,402	.08361	.05874
	27	.000	.000	.000	.000	1790,357	1790,357	27429,240	.09261	.06486
	28	.000	.000	.000	.000	2100,630	2100,630	27559,251	.10794	.07634
	29	.000	.000	.000	.000	10726,869	10726,869	26684,187	.52842	.37622
	30	.000	.000	.000	.000	5470,321	5470,321	27024,201	.20403	.14249
	31	.000	.000	.000	.000	5470,329	5470,329	27074,201	.20403	.14267
	32	.000	.000	.000	.000	2271,810	2271,810	27217,007	.11479	.08351
	33	.000	.000	.000	.000	2271,810	2271,810	27247,907	.11479	.08321
	34	.000	.000	.000	.000	2915,475	2915,475	27294,553	.15244	.10889
	35	.000	.000	.000	.000	3629,376	3629,376	27285,260	.18977	.13341
	36	.000	.000	.000	.000	7545,637	7545,637	26730,118	.30454	.20009
	37	.000	.000	.000	.000	5174,053	5174,053	26503,407	.27054	.17503
	38	.000	.000	.000	.000	1837,591	1837,591	26874,260	.09660	.06734
	39	.000	.000	.000	.000	5203,190	5203,190	27302,358	.20204	.14244
	40	.000	.000	.000	.000	2130,960	2130,960	27304,587	.11142	.07787
	41	.000	.000	.000	.000	1774,145	1774,145	27435,084	.08297	.05474
	42	.000	.000	.000	.000	1872,691	1872,691	27429,160	.08982	.05715
	43	.000	.000	.000	.000	1948,744	1948,744	27435,080	.09341	.05776
	44	.000	.000	.000	.000	2075,334	2075,334	27435,159	.10100	.06049
	45	.000	.000	.000	.000	2444,704	2444,704	27472,513	.12043	.07031
	46	.000	.000	.000	.000	2347,788	2347,788	27467,420	.12495	.07307
	47	.000	.000	.000	.000	2335,058	2335,058	27467,440	.12214	.07084
	48	.000	.000	.000	.000	1744,478	1744,478	27470,142	.08337	.05507
	49	.000	.000	.000	.000	1744,478	1744,478	27470,142	.08337	.05507
	50	.000	.000	.000	.000	704,008	704,008	27317,306	.02936	.01979
	51	.000	.000	.000	.000	805,703	805,703	27317,327	.03494	.02371
	52	.000	.000	.000	.000	2372,003	2372,003	27414,604	.09200	.06485
	53	.000	.000	.000	.000	3160,714	3160,714	27407,084	.12495	.08400
	54	.000	.000	.000	.000	2301,144	2301,144	27407,109	.09200	.06400
	55	.000	.000	.000	.000	2301,144	2301,144	27407,109	.09200	.06400
	56	.000	.000	.000	.000	4311,187	4311,187	27304,904	.14119	.09741
	57	.000	.000	.000	.000	7600,103	7600,103	27114,044	.26941	.18941
	58	.000	.000	.000	.000	6054,007	6054,007	27114,044	.20744	.14715
	59	.000	.000	.000	.000	10544,703	10544,703	27114,044	.37144	.25715
	60	.000	.000	.000	.000	6249,480	6249,480	26980,803	.30202	.21102

SCREW MAIN STEAM LINE PIPING CLASS 2 ANALYSIS

2.1.3 SATISFACTION OF EQUATION 10 (ANALYSIS SET 1)

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (P)	PEAK PROPOSED STRESS (P+AX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MO)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TIO)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO TIO/(1.0SAM)	MODIFIED STRESS RATIO TIO/(1.0SAM)
15	3	.000	.000	.000	.000	654,902	664,902	32531.403	.08854	.02050
24	4	.000	.000	.000	.000	5023,207	5023,207	33140.239	.21504	.15130
24	5	.000	.000	.000	.000	6122,644	6122,644	33216.777	.20217	.13421
25	6	.000	.000	.000	.000	3984,169	3984,169	33258.004	.18974	.11910
45	7	.000	.000	.000	.000	3984,169	3984,169	33258.004	.18974	.11910
45	8	.000	.000	.000	.000	2037,442	2037,442	33238.644	.08724	.04130
45	9	.000	.000	.000	.000	2037,442	2037,442	33238.644	.08724	.04130
45	10	.000	.000	.000	.000	1532,497	1532,497	33164.591	.06547	.04620
45	11	.000	.000	.000	.000	1532,497	1532,497	33164.591	.06547	.04620
45	12	.000	.000	.000	.000	3835,610	3835,610	33059.323	.16424	.11572
45	13	.000	.000	.000	.000	5627,281	5627,281	33049.845	.24096	.17027
75	14	.000	.000	.000	.000	3231,915	3231,915	32995.168	.13039	.09874
75	15	.000	.000	.000	.000	4097,612	4097,612	32794.162	.17554	.12445
75	16	.000	.000	.000	.000	4305,920	4305,920	32792.046	.18431	.13135
75	17	.000	.000	.000	.000	3201,970	3201,970	33044.118	.13711	.09849
95	18	.000	.000	.000	.000	2787,792	2787,792	33120.327	.11935	.08417
95	19	.000	.000	.000	.000	2933,656	2933,656	33172.307	.12449	.08824
105	20	.000	.000	.000	.000	2544,571	2544,571	33171.456	.10981	.07731
105	21	.000	.000	.000	.000	2546,151	2546,151	33372.751	.12015	.08824
115	22	.000	.000	.000	.000	4098,794	4098,794	33441.351	.17517	.12714
115	23	.000	.000	.000	.000	2981,103	2981,103	33242.228	.12765	.09549
125	24	.000	.000	.000	.000	4021,501	4021,501	33153.714	.17220	.12130
125	25	.000	.000	.000	.000	4069,652	4069,652	32871.945	.17426	.12346
125	26	.000	.000	.000	.000	2345,376	2345,376	32893.403	.10043	.07130
125	27	.000	.000	.000	.000	5160,453	5160,453	33095.433	.22902	.15593
125	28	.000	.000	.000	.000	3625,545	3625,545	33302.832	.15796	.11049
125	29	.000	.000	.000	.000	4747,080	4747,080	33190.644	.20327	.14362
125	30	.000	.000	.000	.000	3686,787	3686,787	33193.778	.15787	.11107

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (P)	PEAK PROPOSED STRESS (P+AX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MO)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TIO)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO TIO/(1.0SAM)	MODIFIED STRESS RATIO TIO/(1.0SAM)
10	4	.000	.000	.000	.000	9019,245	9019,245	27416.078	.47140	.32898
20	11	.000	.000	.000	.000	10993,329	10993,329	27517.594	.57641	.39550
20	12	.000	.000	.000	.000	4935,153	4935,153	27132.148	.21132	.14814
20	13	.000	.000	.000	.000	3943,974	3943,974	33249.452	.18888	.13444
20	14	.000	.000	.000	.000	5476,307	5476,307	33445.087	.23449	.16374
20	15	.000	.000	.000	.000	6955,449	6955,449	33287.274	.29783	.20895

40	15	.000	.000	.000	.000	4035,477	4035,477	33060.062	.21134	.14920
40	16	.000	.000	.000	.000	3090,782	3090,782	33151.695	.17081	.12034
40	17	.000	.000	.000	.000	5383,654	5383,654	33286.424	.23052	.16311
40	18	.000	.000	.000	.000	6872,149	6872,149	32701.707	.29426	.21015
40	19	.000	.000	.000	.000	6029,093	6029,093	32541.258	.25816	.18527
40	20	.000	.000	.000	.000	5698,245	5698,245	32665.927	.24400	.17444

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (P)	PEAK PROPOSED STRESS (P+AX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MO)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TIO)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO TIO/(1.0SAM)	MODIFIED STRESS RATIO TIO/(1.0SAM)
145	21	.000	.000	.000	.000	2657,425	2657,425	27221.001	.13844	.09741
145	22	.000	.000	.000	.000	2592,879	2592,879	27313.914	.13564	.09493
145	23	.000	.000	.000	.000	2067,863	2067,863	27306.603	.10812	.07573
175	24	.000	.000	.000	.000	1210,252	1210,252	27154,228	.06328	.04457
175	25	.000	.000	.000	.000	1365,194	1365,194	27246,482	.07134	.05023
195	26	.000	.000	.000	.000	1790,357	1790,357	27639,468	.09101	.06424
195	27	.000	.000	.000	.000	1790,357	1790,357	27639,468	.09101	.06424
195	28	.000	.000	.000	.000	2100,430	2100,430	27509,251	.10944	.07624
195	29	.000	.000	.000	.000	10324,469	10324,469	26676,197	.50342	.34629
205	30	.000	.000	.000	.000	5470,334	5470,334	27074,201	.26203	.18240
205	31	.000	.000	.000	.000	5470,334	5470,334	27074,201	.26203	.18240
215	32	.000	.000	.000	.000	2271,410	2271,410	27207,507	.11874	.08131
215	33	.000	.000	.000	.000	2271,410	2271,410	27207,507	.11874	.08131
225	34	.000	.000	.000	.000	2915,475	2915,475	27094,793	.15284	.10522
225	35	.000	.000	.000	.000	3629,374	3629,374	27205,740	.19737	.13841
225	36	.000	.000	.000	.000	7548,637	7548,637	26731,118	.34404	.24094
225	37	.000	.000	.000	.000	5174,093	5174,093	26733,407	.27024	.19506
225	38	.000	.000	.000	.000	1433,491	1433,491	27274,740	.07888	.05474
225	39	.000	.000	.000	.000	6063,109	6063,109	27320,340	.27208	.19594
245	40	.000	.000	.000	.000	2130,908	2130,908	2734,707	.11142	.07747
245	41	.000	.000	.000	.000	1774,145	1774,145	27448,044	.09247	.06444
245	42	.000	.000	.000	.000	1872,491	1872,491	27419,100	.09869	.06715
245	43	.000	.000	.000	.000	1872,491	1872,491	27419,100	.09869	.06715
275	44	.000	.000	.000	.000	2074,334	2074,334	27049,109	.10544	.07326
275	45	.000	.000	.000	.000	2074,334	2074,334	27049,109	.10544	.07326
295	46	.000	.000	.000	.000	2371,268	2371,268	26974,113	.12043	.08483
295	47	.000	.000	.000	.000	2371,268	2371,268	26974,113	.12043	.08483
295	48	.000	.000	.000	.000	2371,268	2371,268	26974,113	.12043	.08483
295	49	.000	.000	.000	.000	2371,268	2371,268	26974,113	.12043	.08483
295	50	.000	.000	.000	.000	2371,268	2371,268	26974,113	.12043	.08483
315	51	.000	.000	.000	.000	1744,670	1744,670	27114,000	.09332	.06447
315	52	.000	.000	.000	.000	1744,670	1744,670	27114,000	.09332	.06447
315	53	.000	.000	.000	.000	754,093	754,093	27114,000	.03732	.02647
315	54	.000	.000	.000	.000	894,298	894,298	27114,000	.04414	.03179
315	55	.000	.000	.000	.000	2871,267	2871,267	27448,044	.13038	.09247
315	56	.000	.000	.000	.000	3045,144	3045,144	27448,044	.14094	.09869
315	57	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	58	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	59	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	60	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	61	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	62	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	63	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	64	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	65	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	66	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	67	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	68	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	69	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	70	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	71	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	72	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	73	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	74	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	75	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	76	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	77	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	78	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	79	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	80	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	81	.000	.000	.000	.000	2701,140	2701,140	27448,044	.12564	.08824
315	82	.000	.00							

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PROXIMATE STRESS (P*AX)	SUSTAINED LOAD STRESS (PA)	OCCASIONAL LOAD STRESS (PA)	THERMAL EXPANSION STRESS (TC)	TOTAL STRESS (TI)	MODIFIED ALLOWABLE STRESS (SAMI)	DESIGN STRESS RATIO (TIO/11.0*SAMI)	MODIFIED STRESS RATIO (TIO/11.0*SAMI)
345	54	.000	.000	.000	.000	5711.136	5711.136	27008.745	.26442	.27144
	51	.000	.000	.000	.000	5233.407	5233.407	27025.048	.27344	.17345
345	51	.000	.000	.000	.000	5233.407	5233.407	27014.441	.27344	.16340
	52	.000	.000	.000	.000	2319.040	2319.040	26704.535	.12124	.05022
375	53	.000	.000	.000	.000	2319.040	2319.040	26704.535	.12124	.05022
	53	.000	.000	.000	.000	3257.807	3257.807	27454.193	.17034	.11445
345	54	.000	.000	.000	.000	3444.305	3444.305	27145.993	.20331	.14317
	55	.000	.000	.000	.000	3376.245	3376.245	27143.033	.17454	.12424
305	54	.000	.000	.000	.000	2158.590	2158.590	27301.097	.11247	.07692
	54	.000	.000	.000	.000	1699.493	1699.493	27301.097	.08984	.04211
405	47	.000	.000	.000	.000	2083.794	2083.794	27375.420	.10944	.07612
	48	.000	.000	.000	.000	1210.252	1210.252	27124.291	.06324	.04441
415	A7	.000	.000	.000	.000	344.152	344.152	27174.041	.01924	.01244
	A1	.000	.000	.000	.000	344.152	344.152	27153.408	.01924	.01244
425	A3	.000	.000	.000	.000	831.101	831.101	27457.007	.04344	.03022
	24	.000	.000	.000	.000	2100.430	2100.430	27501.049	.10944	.07634
435	A4	.000	.000	.000	.000	2244.889	2244.889	27506.611	.11734	.08161
	27	.000	.000	.000	.000					

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PROXIMATE STRESS (P*AX)	SUSTAINED LOAD STRESS (PA)	OCCASIONAL LOAD STRESS (PA)	THERMAL EXPANSION STRESS (TC)	TOTAL STRESS (TI)	MODIFIED ALLOWABLE STRESS (SAMI)	DESIGN STRESS RATIO (TIO/11.0*SAMI)	MODIFIED STRESS RATIO (TIO/11.0*SAMI)
7C	22	.000	.000	.000	.000	4105.573	4105.573	27037.561	.21443	.15104
	23	.000	.000	.000	.000	3276.653	3276.653	27025.976	.17133	.12124
7C	24	.000	.000	.000	.000	1315.929	1315.929	27245.091	.06444	.04441
	25	.000	.000	.000	.000	2163.236	2163.236	26994.108	.11311	.08214
8C	27	.000	.000	.000	.000	3557.162	3557.162	27344.070	.14600	.10744
	28	.000	.000	.000	.000	3750.134	3750.134	27422.379	.16604	.12424
10C	31	.000	.000	.000	.000	4789.563	4789.563	27402.049	.22043	.17712
	32	.000	.000	.000	.000	5962.363	5962.363	28445.300	.31176	.22144
11C	34	.000	.000	.000	.000	1837.591	1837.591	27278.260	.09404	.06441
	35	.000	.000	.000	.000	1778.145	1778.145	27635.554	.05297	.04441
12C	37	.000	.000	.000	.000	3010.429	3010.429	27033.145	.15741	.11174
	38	.000	.000	.000	.000	3277.462	3277.462	26665.046	.17032	.12214
13C	39	.000	.000	.000	.000	4225.848	4225.848	26471.861	.22090	.16444
	42	.000	.000	.000	.000	4094.004	4094.004	26167.583	.21427	.15644
14C	43	.000	.000	.000	.000	1244.214	1244.214	27141.642	.05910	.04544
	44	.000	.000	.000	.000	1693.737	1693.737	27143.576	.04966	.04234
14C	45	.000	.000	.000	.000	6352.771	6352.771	27305.547	.33017	.23244
	46	.000	.000	.000	.000	6312.540	6312.540	27204.001	.33007	.23124
14C	50	.000	.000	.000	.000	10431.745	10431.745	25570.429	.54545	.39244
	51	.000	.000	.000	.000	9382.252	9382.252	26571.674	.49055	.36309
17C	54	.000	.000	.000	.000	5351.947	5351.947	27017.565	.27944	.19999
	55	.000	.000	.000	.000	6387.733	6387.733	26810.823	.33400	.23627
18C	57	.000	.000	.000	.000	2158.590	2158.590	27350.497	.11247	.07692
	58	.000	.000	.000	.000	1699.493	1699.493	27363.562	.08984	.04211
18C	54	.000	.000	.000	.000	3423.240	3423.240	27174.871	.17699	.12597
	59	.000	.000	.000	.000	3500.657	3500.657	27157.074	.18304	.12840

1 CURVED MAIN STEAM LINE PIPING CLASS 2 ANALYSIS

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PROXIMATE STRESS (P*AX)	SUSTAINED LOAD STRESS (PA)	OCCASIONAL LOAD STRESS (PA)	THERMAL EXPANSION STRESS (TC)	TOTAL STRESS (TI)	MODIFIED ALLOWABLE STRESS (SAMI)	DESIGN STRESS RATIO (TIO/11.0*SAMI)	MODIFIED STRESS RATIO (TIO/11.0*SAMI)
445	1	.000	.000	.000	.000	16641.350	16641.350	26607.159	.87014	.62544
	2	.000	.000	.000	.000	8172.094	8172.094	26424.389	.42737	.30994
445	2	.000	.000	.000	.000	8172.094	8172.094	26424.389	.42737	.30994
	3	.000	.000	.000	.000	883.121	883.121	25798.215	.04618	.03423



1ACBWR MAIN STEAM LINE PIPING CLASS 2 ANALYSIS

ALL 4 SATISFACTION OF EQUATION 11 (ANALYSIS SET 1)

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (P-MAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T11)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T11/(SH+SA)	MODIFIED STRESS RATIO T11/(SH+SAM)
15	3	4094.604	.000	1704.063	.000	848.002	8769.849	3953.483	.14099	.11917
25	5	4094.604	.000	242.921	.000	8023.207	9362.433	33140.239	.23852	.14074
35	6	4094.604	.000	151.332	.000	3794.169	10395.556	33236.777	.24443	.17156
45	7	4094.604	.000	151.332	.000	3644.169	8212.106	33294.004	.20921	.16704
55	8	4094.604	.000	174.108	.000	2037.442	6304.154	33294.444	.10070	.12937
65	9	4094.604	.000	254.524	.000	1532.497	5804.478	33164.591	.14994	.11995
75	10	4094.604	.000	349.780	.000	3835.610	8201.494	33270.323	.21991	.14904
85	11	4094.604	.000	394.202	.000	5427.291	10120.087	33049.865	.25741	.12674
95	12	4094.604	.000	542.903	.000	3231.915	7071.423	32995.168	.25053	.14122
105	13	4094.604	.000	697.028	.000	4067.612	8891.244	32794.142	.29951	.12929
115	14	4094.604	.000	710.318	.000	4305.420	9112.443	32782.666	.29251	.12719
125	15	4094.604	.000	406.409	.000	3201.970	7699.184	33066.118	.19614	.14693
135	16	4094.604	.000	313.305	.000	2787.892	7197.801	33120.327	.18337	.14693
145	17	4094.604	.000	292.152	.000	2930.696	7274.453	33172.307	.18545	.14934
155	18	4094.604	.000	292.917	.000	2564.571	6914.092	33171.650	.17614	.14020
165	19	3859.027	.000	253.913	.000	2944.141	7059.041	33372.751	.17943	.14327
175	20	3859.027	.000	126.102	.000	4070.784	6070.915	33441.391	.20574	.14354
185	21	3859.027	.000	383.440	.000	2941.103	7224.070	33242.220	.18444	.14394
195	22	3859.027	.000	511.604	.000	4021.501	8302.132	33153.714	.21379	.17164
205	23	4094.604	.000	605.566	.000	4044.692	8771.863	32871.905	.22377	.17946
215	24	4094.604	.000	584.033	.000	2345.376	7029.014	32893.408	.17449	.14301
225	25	3859.027	.000	579.934	.000	5160.453	9594.414	33095.832	.24455	.15507
235	26	3859.027	.000	242.053	.000	3446.545	7787.625	33382.837	.19839	.15067
245	27	3859.027	.000	444.154	.000	4747.089	9074.263	33190.644	.23117	.14444
255	28	3859.027	.000	464.470	.000	3646.787	8010.274	33193.778	.20406	.16316

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (P-MAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T11)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T11/(SH+SA)	MODIFIED STRESS RATIO T11/(SH+SAM)
1C	4	4803.807	.000	435.990	.000	9014.265	14265.056	27410.078	.41802	.33631
2C	11	3859.027	.000	314.559	.000	10993.329	10119.649	27517.544	.47237	.37513
3C	12	3859.027	.000	324.035	.000	4935.153	9114.215	33313.148	.23229	.14824
4C	13	3859.027	.000	339.912	.000	3943.979	8442.918	33299.652	.20744	.16551
5C	14	3859.027	.000	168.811	.000	5476.307	9504.146	33445.087	.24212	.16261
6C	14	3859.027	.000	354.474	.000	6955.449	11164.950	33267.274	.28453	.22707

7C	15	3859.027	.000	621.783	.000	4935.477	9414.277	33060.060	.23988	.19233
8C	16	3859.027	.000	513.974	.000	3992.782	8363.787	33151.696	.21307	.17051
9C	17	3859.027	.000	504.441	.000	5303.556	9427.444	33004.428	.20290	.16299
10C	18	3859.027	.000	1543.377	.000	6374.149	11774.653	32701.707	.29944	.24327
11C	19	4094.604	.000	994.563	.000	8024.003	11120.171	32541.254	.28329	.22954
12C	20	4094.604	.000	847.893	.000	5648.245	10642.742	32665.927	.27113	.21914

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (P-MAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T11)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T11/(SH+SA)	MODIFIED STRESS RATIO T11/(SH+SAM)
15S	21	4804.803	.000	657.256	.000	2497.425	8124.483	27229.401	.23400	.19240
16S	22	4804.803	.000	554.102	.000	2592.479	7458.862	27313.914	.23323	.18490
17S	23	4804.803	.000	544.783	.000	2067.853	7442.447	27304.403	.21809	.17599
18S	24	4804.803	.000	744.447	.000	1210.252	8704.101	27154.229	.19792	.16046
19S	25	4804.803	.000	593.443	.000	1385.146	6101.441	2744.444	.19092	.15994
20S	26	4804.803	.000	173.000	.000	1799.357	8773.178	27431.402	.19444	.15914
21S	27	4804.803	.000	168.000	.000	1792.587	8785.306	27449.402	.19564	.15914
22S	28	4804.803	.000	324.374	.000	2100.430	7204.805	27549.241	.21207	.17094
23S	29	4804.803	.000	1173.007	.000	10306.444	16411.343	26604.197	.44052	.34007
24S	30	4804.803	.000	785.246	.000	5470.339	11177.142	27024.201	.32764	.24607
25S	31	4804.803	.000	447.522	.000	5470.339	11177.142	27024.201	.32764	.24607
26S	32	4804.803	.000	447.522	.000	2971.410	7691.919	27247.807	.29640	.21404
27S	33	4804.803	.000	447.137	.000	2971.410	7691.919	27247.807	.29640	.21404
28S	34	4804.803	.000	947.235	.000	2911.475	8304.119	27254.443	.24330	.19614
29S	35	4804.803	.000	1170.025	.000	3409.376	9122.118	27295.260	.24735	.19614
30S	36	4804.803	.000	1357.445	.000	704.637	13198.439	24730.118	.34849	.25047
31S	37	4804.803	.000	471.752	.000	5174.053	11054.046	24443.407	.33777	.25047
32S	38	4804.803	.000	471.752	.000	1833.001	7944.000	27378.200	.27232	.21114
33S	39	4804.803	.000	471.752	.000	5031.140	10905.210	27321.304	.30943	.24014
34S	40	4804.803	.000	80.136	.000	1120.200	7432.240	27344.547	.21704	.17051
35S	41	4804.803	.000	445.505	.000	1433.140	6744.008	27410.004	.19805	.16047
36S	42	4804.803	.000	730.150	.000	1433.140	7807.074	27241.100	.23104	.17051
37S	43	4804.803	.000	727.412	.000	1543.004	8044.008	27241.100	.20393	.14344
38S	44	4804.803	.000	1040.114	.000	2570.334	10744.004	27241.100	.21304	.17051
39S	45	4804.803	.000	1040.114	.000	2474.814	8729.205	27469.513	.20713	.16047
40S	46	4804.803	.000	1040.114	.000	2347.740	8244.008	27469.513	.20713	.16047
41S	47	4804.803	.000	1170.014	.000	2311.044	8444.008	27469.513	.20713	.16047
42S	48	4804.803	.000	445.505	.000	1244.730	7044.008	27299.402	.20764	.16047
43S	49	4804.803	.000	445.505	.000	1244.730	7044.008	27299.402	.20764	.16047
44S	50	4804.803	.000	324.374	.000	1744.000	7044.008	27299.402	.21274	.16047
45S	51	4804.803	.000	324.374	.000	704.000	6044.008	27299.402	.19744	.14344
46S	52	4804.803	.000	274.443	.000	851.000	6124.008	27299.402	.19744	.14344
47S	53	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
48S	54	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
49S	55	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
50S	56	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
51S	57	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
52S	58	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
53S	59	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
54S	60	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
55S	61	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
56S	62	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
57S	63	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
58S	64	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
59S	65	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
60S	66	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
61S	67	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
62S	68	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
63S	69	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344
64S	70	4804.803	.000	274.443	.000	2044.000	6124.008	27299.402	.19744	.14344

MEMBER NO.	MEMBER ENDS	INTERNAL PIPELINE STRESS (PI)	PEAK PIPELINE STRESS (PI-MAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MCI)	TOTAL STRESS (TII)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO TII/(SAM)	MODIFIED STRESS RATIO TII/(SAM)
345	50	4024,577	.000	799,017	.000	5711,134	11434,738	27008,745	.33514	.27225
345	51	4024,577	.000	774,225	.000	5273,407	10533,209	27075,048	.32958	.26030
345	52	4024,577	.000	746,640	.000	5213,407	10344,574	27075,048	.32958	.26030
345	53	4024,577	.000	2132,744	.000	2319,090	957,411	26744,538	.29678	.24051
345	54	4024,577	.000	2132,744	.000	2619,090	957,411	26744,538	.29678	.24051
345	55	4024,577	.000	272,019	.000	3407,807	8454,403	27450,103	.29149	.23432
345	56	4024,577	.000	613,431	.000	3407,807	8454,403	27450,103	.29149	.23432
345	57	4024,577	.000	603,385	.000	3407,807	8454,403	27450,103	.29149	.23432
345	58	4024,577	.000	447,004	.000	3378,245	8758,605	27305,944	.29047	.23090
445	57	4024,577	.000	345,780	.000	2054,553	7400,946	27305,944	.29047	.23090
415	42	4024,577	.000	367,046	.000	1659,493	7007,044	27305,944	.29047	.23090
415	43	4024,577	.000	773,385	.000	2083,788	7377,411	27375,502	.29192	.23540
415	44	4024,577	.000	715,091	.000	1210,272	4793,459	27179,791	.28908	.23170
415	45	4024,577	.000	745,013	.000	149,152	5874,044	27179,791	.28908	.23170
415	46	4024,577	.000	387,250	.000	349,152	5903,977	27193,408	.28931	.23187
415	47	4024,577	.000	335,959	.000	431,101	6024,152	27457,507	.29165	.23419
415	48	4024,577	.000	327,127	.000	2100,470	7246,431	27501,009	.29235	.23478
415	49	4024,577	.000		.000	2244,889	7381,817	27508,611	.29252	.23500

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PIPELINE STRESS (PI)	PEAK PIPELINE STRESS (PI-MAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MCI)	TOTAL STRESS (TII)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO TII/(SAM)	MODIFIED STRESS RATIO TII/(SAM)
3C	27	4800,802	.000	881,303	.000	4108,573	9799,678	27037,541	.28717	.23312
3C	28	4800,802	.000	894,932	.000	3274,453	8081,307	27037,541	.28717	.23312
3C	29	4800,802	.000	613,620	.000	1316,929	4780,351	27037,541	.28717	.23312
3C	30	4800,802	.000	932,424	.000	2163,236	7905,441	26994,104	.28680	.23280
3C	31	4800,802	.000	514,352	.000	3557,162	8557,315	27444,070	.29030	.23485
3C	32	4800,802	.000	424,576	.000	3750,134	8488,515	27444,070	.29030	.23485
3C	33	4800,802	.000	759,201	.000	4709,543	10475,361	27027,689	.28700	.23300
3C	34	4800,802	.000	931,458	.000	5502,363	11428,798	26995,330	.28680	.23280
3C	35	4800,802	.000	481,752	.000	1877,591	7245,520	27274,260	.28940	.23410
3C	36	4800,802	.000	65,536	.000	1774,145	6755,254	27035,944	.28717	.23312
3C	37	4800,802	.000	769,464	.000	3210,429	8704,669	27035,944	.28717	.23312
3C	38	4800,802	.000	1202,770	.000	3257,462	9386,819	26645,048	.28514	.23029
3C	39	4800,802	.000	1194,998	.000	4225,448	10347,473	26671,051	.28529	.23044
3C	40	4800,802	.000	1787,560	.000	4009,004	10812,142	26187,003	.28169	.22713
3C	41	4800,802	.000	616,668	.000	1244,714	4791,459	27141,542	.28931	.23187
3C	42	4800,802	.000	616,275	.000	1693,737	7256,504	27141,542	.28931	.23187
3C	43	4800,802	.000	447,250	.000	6352,771	11734,598	27055,547	.28908	.23170
3C	44	4800,802	.000	447,034	.000	6317,540	11701,651	27055,547	.28908	.23170
3C	45	4800,802	.000	1336,683	.000	16431,753	18693,075	26952,509	.28817	.23089
3C	46	4800,802	.000	1312,631	.000	9302,292	15621,499	26971,674	.28832	.23104
3C	47	4800,802	.000	444,875	.000	4351,947	11725,399	27077,568	.28931	.23187
3C	48	4800,802	.000	395,780	.000	6337,733	12227,059	26930,823	.28817	.23089
3C	49	4800,802	.000	380,474	.000	2159,090	7480,947	27305,947	.29047	.23432
3C	50	4800,802	.000	502,386	.000	1694,493	7007,044	27305,947	.29047	.23432
3C	51	4800,802	.000	623,924	.000	3423,260	8952,823	27174,071	.28908	.23170
3C	52	4800,802	.000		.000	3500,657	9051,158	27197,074	.28931	.23187

1 ACWR WITH STEAM LINE PIPING CLASS 2 ANALYSIS

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	INTERNAL PIPELINE STRESS (PI)	PEAK PIPELINE STRESS (PI-MAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MCI)	TOTAL STRESS (TII)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO TII/(SAM)	MODIFIED STRESS RATIO TII/(SAM)
445	1	4823,672	.000	373,789	.000	16641,350	22834,671	26607,150	.86097	.64889
445	2	4823,672	.000	544,812	.000	8172,094	14584,578	26424,349	.85211	.63850
445	3	4823,672	.000	584,812	.000	8172,094	14584,578	26424,349	.85211	.63850
445	4	4823,672	.000	1327,840	.000	883,121	8034,633	25796,215	.82545	.61955

LACROR MAIN TEAM LINE PIPING CLASS 2 ANALYSIS

P.2 CLASS 2 STRESSES FOR ANALYSIS SET NUMBER 2

ASSIGNED LOAD COMBINATION IDENTIFIERS

W A \* 1 W R \* R M C \* R P \* 1 P H A \* 2

D.2.1 SATISFACTION OF EQUATION 9 (ANALYSIS SET 2)

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK STRESS (PMAK)	SUSTAINED LOAD STRESS (PMA)	OCCASIONAL LOAD STRESS (PMAO)	THERMAL EXPANSION STRESS (PMT)	TOTAL STRESS (PT)	MODIFIED ALLOWABLE STRESS (SAM)	UPSET RATIO T9/(1.2*SH)	EFFICIENCY STRESS RATIO T9/(1.4*SH)
15	3	.000	4443.227	1607.043	790.739	.000	6262.074	.000	.32820	.21886
15	4	.000	4443.227	242.791	1250.401	.000	5956.648	.000	.31219	.20517
15	5	.000	4443.227	177.305	1120.790	.000	5750.922	.000	.29188	.20174
15	6	.000	4443.227	151.332	990.920	.000	5524.479	.000	.26934	.19363
15	7	.000	4443.227	124.108	850.446	.000	5281.800	.000	.24584	.17357
15	8	.000	4443.227	174.198	190.478	.000	6541.703	.000	.36284	.22557
15	9	.000	4443.227	258.524	927.846	.000	5847.717	.000	.30284	.22557
15	10	.000	4443.227	349.700	114.490	.000	6331.417	.000	.32547	.17233
15	11	.000	4443.227	395.202	124.749	.000	6203.157	.000	.32512	.21674
15	12	.000	4443.227	447.923	123.494	.000	6036.734	.000	.31639	.21057
15	13	.000	4443.227	497.020	114.420	.000	5877.676	.000	.30806	.20534
15	14	.000	4443.227	542.409	307.987	.000	5160.220	.000	.27092	.18027
15	15	.000	4443.227	583.303	490.094	.000	5371.877	.000	.29154	.18769
15	16	.000	4443.227	629.152	480.438	.000	5204.917	.000	.27279	.18197
15	17	.000	4443.227	679.917	90.749	.000	580.493	.000	.24470	.15047
15	18	.000	4204.387	253.513	321.587	.000	5180.287	.000	.27150	.18108
15	19	.000	4204.387	124.152	404.840	.000	4737.079	.000	.24027	.14351
115	14	.000	4204.387	313.940	794.791	.000	5264.649	.000	.28232	.18121
115	17	.000	4204.387	511.404	737.904	.000	5453.450	.000	.29024	.19054
175	20	.000	4443.227	405.468	617.068	.000	5885.801	.000	.29400	.19627
175	21	.000	4443.227	545.033	507.968	.000	5611.228	.000	.29439	.19684
145	10	.000	4204.387	579.034	1107.907	.000	5980.229	.000	.30050	.20057
145	11	.000	4204.387	242.053	895.047	.000	5141.487	.000	.26047	.17965
145	12	.000	4204.387	468.156	1874.414	.000	6350.958	.000	.33286	.22191
145	13	.000	4204.387	464.470	944.666	.000	5613.526	.000	.29421	.19314

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK STRESS (PMAK)	SUSTAINED LOAD STRESS (PMA)	OCCASIONAL LOAD STRESS (PMAO)	THERMAL EXPANSION STRESS (PMT)	TOTAL STRESS (PT)	MODIFIED ALLOWABLE STRESS (SAM)	UPSET RATIO T9/(1.2*SH)	EFFICIENCY STRESS RATIO T9/(1.4*SH)
10	4	.000	4204.387	435.990	2245.473	.000	7921.714	.000	.44010	.27244
10	5	.000	4204.387	314.953	2011.482	.000	7584.491	.000	.42047	.26071
10	11	.000	4204.387	324.025	930.455	.000	5458.877	.000	.28410	.19074
10	12	.000	4204.387	339.912	964.492	.000	5515.791	.000	.28683	.19255
10	13	.000	4204.387	149.911	544.733	.000	4917.431	.000	.25773	.17197
10	14	.000	4204.387	354.474	844.451	.000	5401.413	.000	.28309	.18674
10	15	.000	4204.387	621.743	1244.419	.000	6095.789	.000	.31422	.21229
10	16	.000	4204.387	513.978	1067.707	.000	5787.073	.000	.30331	.20090
10	17	.000	4204.387	684.881	987.427	.000	5677.959	.000	.30070	.20033
10	18	.000	4204.387	1043.377	1045.768	.000	6593.030	.000	.34555	.23034
10	19	.000	4443.227	945.463	944.127	.000	6443.917	.000	.33773	.22519
10	20	.000	4443.227	847.893	851.714	.000	6175.033	.000	.32364	.21574

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK STRESS (PMAK)	SUSTAINED LOAD STRESS (PMA)	OCCASIONAL LOAD STRESS (PMAO)	THERMAL EXPANSION STRESS (PMT)	TOTAL STRESS (PT)	MODIFIED ALLOWABLE STRESS (SAM)	UPSET RATIO T9/(1.2*SH)	EFFICIENCY STRESS RATIO T9/(1.4*SH)
145	21	.000	4204.387	687.044	644.044	.000	6041.520	.000	.36379	.24224
145	22	.000	4204.387	554.180	447.448	.000	6443.701	.000	.35411	.23494
145	23	.000	4204.387	544.793	684.749	.000	6523.377	.000	.36130	.24094
145	24	.000	4204.387	744.047	707.722	.000	6841.500	.000	.37125	.24749
175	25	.000	4204.387	589.643	619.200	.000	6525.429	.000	.37494	.24174
145	26	.000	4204.387	175.707	540.193	.000	5603.473	.000	.31076	.20044
145	27	.000	4204.387	394.324	502.070	.000	614.714	.000	.31131	.20044
145	28	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647
145	29	.000	4204.387	776.746	1240.743	.000	6444.714	.000	.32793	.20647
215	29	.000	4204.387	744.216	1244.243	.000	6444.714	.000	.32793	.20647
215	30	.000	4204.387	453.137	114.412	.000	5679.811	.000	.30404	.20090
215	31	.000	4204.387	440.137	104.412	.000	5579.811	.000	.30070	.20033
215	32	.000	4204.387	447.725	707.740	.000	6041.520	.000	.31076	.20044
215	33	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647
215	34	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647
215	35	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647
215	36	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647
215	37	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647
215	38	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647
215	39	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647
215	40	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647
215	41	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647
215	42	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647
215	43	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647
215	44	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647
215	45	.000	4204.387	1177.807	2401.341	.000	6444.714	.000	.32793	.20647



MEMBER NO.	MEMBER TYPE	INTERNAL PRESSURE (PSI)	PEAK STRESS (MPAS)	SUSTAINED LOAD STRESS (MPAS)	OCCASIONAL LOAD STRESS (MPAS)	THERMAL EXPANSION STRESS (MPAS)	TOTAL STRESS (TYP)	MODIFIED ALLOWABLE STRESS (MPAS)	UPSET STRESS RATIO T <sub>9</sub> /(1.2*SM)	EFFICIENCY STRESS RATIO T <sub>9</sub> /(1.4*SM)
245	40	.000	8347.477	1189.914	961.185	.000	7520.746	.000	.41742	.27855
245	41	.000	8347.477	550.256	791.482	.000	6704.714	.000	.37273	.24449
245	42	.000	8347.477	550.256	791.482	.000	6704.714	.000	.37273	.24449
305	43	.000	8347.477	376.592	741.746	.000	6505.915	.000	.37144	.24344
315	44	.000	8347.477	376.592	741.746	.000	6505.915	.000	.37144	.24344
315	45	.000	8347.477	241.734	1167.795	.000	6756.946	.000	.37717	.25149
325	46	.000	8347.477	217.407	1194.194	.000	6781.583	.000	.37519	.25024
325	47	.000	8347.477	294.547	1194.194	.000	6854.647	.000	.37675	.25117
335	47	.000	8347.477	341.371	1217.149	.000	6941.227	.000	.37842	.25244
345	47	.000	8347.477	434.277	1254.409	.000	7094.163	.000	.38274	.25674
345	48	.000	8347.477	527.022	1254.409	.000	7094.163	.000	.38274	.25674
345	49	.000	8347.477	649.043	1271.915	.000	7214.435	.000	.38521	.25841
345	50	.000	8347.477	812.441	1431.415	.000	7814.533	.000	.40314	.27542
345	51	.000	8347.477	794.017	1713.493	.000	7679.187	.000	.39872	.27441
345	52	.000	8347.477	779.225	1817.149	.000	7763.051	.000	.39652	.27441
345	53	.000	8347.477	784.540	1501.170	.000	7735.187	.000	.39823	.27441
375	54	.000	8347.477	2332.794	1284.095	.000	6984.366	.000	.40024	.27441
375	55	.000	8347.477	2732.794	1284.095	.000	6984.366	.000	.40024	.27441
375	56	.000	8347.477	272.019	1501.170	.000	7245.712	.000	.39774	.27441
375	57	.000	8347.477	611.431	1713.493	.000	7911.070	.000	.41525	.29341
375	58	.000	8347.477	593.385	1431.415	.000	7395.917	.000	.40174	.27542
375	59	.000	8347.477	447.584	1431.415	.000	7224.187	.000	.39134	.26744
425	59	.000	8347.477	345.780	954.969	.000	6722.826	.000	.37349	.24949
425	60	.000	8347.477	340.974	1331.581	.000	7083.431	.000	.39302	.27244
425	61	.000	8347.477	347.046	2551.789	.000	8293.012	.000	.44072	.31744
425	62	.000	8347.477	771.385	701.187	.000	6723.401	.000	.37382	.24741
425	63	.000	8347.477	715.091	716.143	.000	6863.524	.000	.37622	.24841
425	64	.000	8347.477	745.813	716.143	.000	6844.647	.000	.37564	.24744
425	65	.000	8347.477	347.250	714.093	.000	6342.494	.000	.35234	.23441
425	66	.000	8347.477	335.999	594.181	.000	6124.413	.000	.34024	.22641
425	67	.000	8347.477	327.127	572.729	.000	6139.597	.000	.34169	.22738

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER TYPE	INTERNAL PRESSURE (PSI)	PEAK STRESS (MPAS)	SUSTAINED LOAD STRESS (MPAS)	OCCASIONAL LOAD STRESS (MPAS)	THERMAL EXPANSION STRESS (MPAS)	TOTAL STRESS (TYP)	MODIFIED ALLOWABLE STRESS (MPAS)	UPSET STRESS RATIO T <sub>9</sub> /(1.2*SM)	EFFICIENCY STRESS RATIO T <sub>9</sub> /(1.4*SM)
7C	22	.000	8240.251	881.303	1057.475	.000	7179.229	.000	.39885	.26552
7C	23	.000	8240.251	894.532	1134.440	.000	7241.843	.000	.40231	.26821
7C	24	.000	8240.251	613.628	1137.450	.000	6734.871	.000	.38811	.26073
7C	25	.000	8240.251	932.424	1107.472	.000	7275.946	.000	.40444	.26743
7C	26	.000	8240.251	518.352	941.717	.000	6864.359	.000	.37035	.24644
11C	31	.000	8347.477	759.201	1370.819	.000	7487.498	.000	.40464	.26733
11C	32	.000	8347.477	931.658	1244.045	.000	7544.320	.000	.41653	.27749
11C	33	.000	8347.477	441.352	1094.216	.000	6937.045	.000	.41913	.27942
11C	34	.000	8347.477	60.536	1531.116	.000	6961.429	.000	.34524	.25841
11C	35	.000	8347.477	789.664	1487.182	.000	6924.323	.000	.40574	.26741
11C	36	.000	8347.477	1202.780	2666.847	.000	9230.344	.000	.50135	.37423
11C	37	.000	8347.477	1194.998	1741.276	.000	8301.751	.000	.48124	.34124
11C	38	.000	8347.477	623.924	1487.367	.000	8842.404	.000	.44132	.30755
11C	39	.000	8347.477	1787.560	1487.367	.000	8842.404	.000	.49124	.32755

14C	42	.000	8347.477	618.658	1251.464	.000	7237.711	.000	.40810	.26804
14C	43	.000	8347.477	418.275	1564.884	.000	7551.639	.000	.41925	.27574
14C	44	.000	8347.477	444.250	1864.592	.000	7708.819	.000	.42722	.28222
14C	45	.000	8347.477	442.834	1514.745	.000	7450.105	.000	.42501	.27534
14C	46	.000	8347.477	1334.643	2601.924	.000	9394.087	.000	.52169	.34745
14C	47	.000	8347.477	1312.431	2445.043	.000	9165.170	.000	.50914	.33944
14C	48	.000	8347.477	446.475	2631.703	.000	8453.055	.000	.44961	.31310
14C	49	.000	8347.477	1007.749	3170.492	.000	9544.104	.000	.51034	.33164
14C	50	.000	8347.477	345.740	594.049	.000	6722.426	.000	.37349	.24949
14C	51	.000	8347.477	340.974	1234.941	.000	7083.431	.000	.39302	.27244
14C	52	.000	8347.477	602.986	4204.417	.000	10174.840	.000	.56272	.37644
14C	53	.000	8347.477	623.924	4424.741	.000	10420.142	.000	.57893	.38553

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER TYPE	INTERNAL PRESSURE (PSI)	PEAK STRESS (MPAS)	SUSTAINED LOAD STRESS (MPAS)	OCCASIONAL LOAD STRESS (MPAS)	THERMAL EXPANSION STRESS (MPAS)	TOTAL STRESS (TYP)	MODIFIED ALLOWABLE STRESS (MPAS)	UPSET STRESS RATIO T <sub>9</sub> /(1.2*SM)	EFFICIENCY STRESS RATIO T <sub>9</sub> /(1.4*SM)
445	1	.000	8491.672	375.789	1864.866	.000	8052.246	.000	.44780	.30205
445	2	.000	8491.672	584.812	771.134	.000	7185.673	.000	.39022	.26613
445	3	.000	8491.672	584.812	771.134	.000	7185.673	.000	.39022	.26613
445	4	.000	8491.672	1327.040	1020.440	.000	8171.944	.000	.45400	.30266

LACROR WITH STEAM LINE PIPING CLASS 2 ANALYSIS

A.2.2 SATISFACTION OF EQUATION 10 (ANALYSIS SET 2)

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (PMAX)	SUSTAINED LOAD STRESS (SM)	OCCASIONAL LOAD STRESS (SM)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TI)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T10/(1.0*SA)	MODIFIED STRESS RATIO
15	3	.000	.000	.000	.000	402,796	402,796	.000	.01725	
	4	.000	.000	.000	.000	599,842	599,842	.000	.25444	
25	5	.000	.000	.000	.000	7157,255	7157,255	.000	.32647	
	6	.000	.000	.000	.000	4493,547	4493,547	.000	.19267	
35	7	.000	.000	.000	.000	4493,547	4493,547	.000	.19267	
	8	.000	.000	.000	.000	2038,898	2038,898	.000	.09730	
45	9	.000	.000	.000	.000	2038,898	2038,898	.000	.09730	
	10	.000	.000	.000	.000	1647,476	1647,476	.000	.07054	
55	11	.000	.000	.000	.000	1647,476	1647,476	.000	.07054	
	12	.000	.000	.000	.000	4773,472	4773,472	.000	.20014	
65	13	.000	.000	.000	.000	4773,472	4773,472	.000	.20014	
	14	.000	.000	.000	.000	3153,695	3153,695	.000	.14927	
75	15	.000	.000	.000	.000	3153,695	3153,695	.000	.14927	
	16	.000	.000	.000	.000	3726,953	3726,953	.000	.16679	
85	17	.000	.000	.000	.000	3726,953	3726,953	.000	.16679	
	18	.000	.000	.000	.000	3455,122	3455,122	.000	.14486	
95	19	.000	.000	.000	.000	3455,122	3455,122	.000	.14486	
	20	.000	.000	.000	.000	3263,095	3263,095	.000	.13943	
105	21	.000	.000	.000	.000	3263,095	3263,095	.000	.13943	
	22	.000	.000	.000	.000	2959,078	2959,078	.000	.12742	
115	23	.000	.000	.000	.000	2959,078	2959,078	.000	.12742	
	24	.000	.000	.000	.000	3472,505	3472,505	.000	.14944	
125	25	.000	.000	.000	.000	3472,505	3472,505	.000	.14944	
	26	.000	.000	.000	.000	4512,190	4512,190	.000	.19301	
135	27	.000	.000	.000	.000	4512,190	4512,190	.000	.19301	
	28	.000	.000	.000	.000	3353,207	3353,207	.000	.14487	
145	29	.000	.000	.000	.000	3353,207	3353,207	.000	.14487	
	30	.000	.000	.000	.000	4151,079	4151,079	.000	.17775	
155	31	.000	.000	.000	.000	4151,079	4151,079	.000	.17775	
	32	.000	.000	.000	.000	3531,202	3531,202	.000	.15120	
165	33	.000	.000	.000	.000	3531,202	3531,202	.000	.15120	
	34	.000	.000	.000	.000	2030,482	2030,482	.000	.08844	
175	35	.000	.000	.000	.000	2030,482	2030,482	.000	.08844	
	36	.000	.000	.000	.000	6262,169	6262,169	.000	.26814	
185	37	.000	.000	.000	.000	6262,169	6262,169	.000	.26814	
	38	.000	.000	.000	.000	4329,773	4329,773	.000	.18540	
195	39	.000	.000	.000	.000	4329,773	4329,773	.000	.18540	
	40	.000	.000	.000	.000	5792,220	5792,220	.000	.24141	
205	41	.000	.000	.000	.000	5792,220	5792,220	.000	.24141	

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (PMAX)	SUSTAINED LOAD STRESS (SM)	OCCASIONAL LOAD STRESS (SM)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TI)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T10/(1.0*SA)	MODIFIED STRESS RATIO
1C	4	.000	.000	.000	.000	10754,876	10754,876	.000	.56235	
	5	.000	.000	.000	.000	12640,989	12640,989	.000	.67195	
2C	11	.000	.000	.000	.000	5796,238	5796,238	.000	.24819	
	12	.000	.000	.000	.000	4672,708	4672,708	.000	.20008	
3C	13	.000	.000	.000	.000	6040,449	6040,449	.000	.29885	
	14	.000	.000	.000	.000	7729,733	7729,733	.000	.33048	

4C	15	.000	.000	.000	.000	5558,425	5558,425	.000	.23547	
	16	.000	.000	.000	.000	4529,076	4529,076	.000	.19093	
5C	17	.000	.000	.000	.000	5557,031	5557,031	.000	.23505	
	18	.000	.000	.000	.000	7047,786	7047,786	.000	.30178	
6C	19	.000	.000	.000	.000	5218,353	5218,353	.000	.22245	
	20	.000	.000	.000	.000	4944,269	4944,269	.000	.21171	

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (PMAX)	SUSTAINED LOAD STRESS (SM)	OCCASIONAL LOAD STRESS (SM)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TI)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T10/(1.0*SA)	MODIFIED STRESS RATIO
195	21	.000	.000	.000	.000	2300,809	2300,809	.000	.10000	
	22	.000	.000	.000	.000	2221,910	2221,910	.000	.11619	
195	23	.000	.000	.000	.000	1793,090	1793,090	.000	.08164	
	24	.000	.000	.000	.000	1081,008	1081,008	.000	.04647	
175	25	.000	.000	.000	.000	1022,216	1022,216	.000	.04345	
	26	.000	.000	.000	.000	1379,794	1379,794	.000	.05215	
175	27	.000	.000	.000	.000	1379,794	1379,794	.000	.05215	
	28	.000	.000	.000	.000	1714,271	1714,271	.000	.06964	
195	29	.000	.000	.000	.000	1714,271	1714,271	.000	.06964	
	30	.000	.000	.000	.000	5045,727	5045,727	.000	.21457	
205	31	.000	.000	.000	.000	5045,727	5045,727	.000	.21457	
	32	.000	.000	.000	.000	2506,924	2506,924	.000	.10158	
215	33	.000	.000	.000	.000	2506,924	2506,924	.000	.10158	
	34	.000	.000	.000	.000	2739,486	2739,486	.000	.11325	
225	35	.000	.000	.000	.000	2739,486	2739,486	.000	.11325	
	36	.000	.000	.000	.000	3153,186	3153,186	.000	.13428	
235	37	.000	.000	.000	.000	3153,186	3153,186	.000	.13428	
	38	.000	.000	.000	.000	4235,204	4235,204	.000	.17647	
245	39	.000	.000	.000	.000	4235,204	4235,204	.000	.17647	
	40	.000	.000	.000	.000	1584,805	1584,805	.000	.06307	
245	41	.000	.000	.000	.000	1584,805	1584,805	.000	.06307	
	42	.000	.000	.000	.000	2061,706	2061,706	.000	.08571	
245	43	.000	.000	.000	.000	2061,706	2061,706	.000	.08571	
	44	.000	.000	.000	.000	1590,129	1590,129	.000	.06708	
245	45	.000	.000	.000	.000	1590,129	1590,129	.000	.06708	
	46	.000	.000	.000	.000	1400,003	1400,003	.000	.05843	
245	47	.000	.000	.000	.000	1400,003	1400,003	.000	.05843	
	48	.000	.000	.000	.000	1894,502	1894,502	.000	.07970	
245	49	.000	.000	.000	.000	1894,502	1894,502	.000	.07970	
	50	.000	.000	.000	.000	2427,225	2427,225	.000	.10070	
245	51	.000	.000	.000	.000	2427,225	2427,225	.000	.10070	
	52	.000	.000	.000	.000	2412,933	2412,933	.000	.10013	
245	53	.000	.000	.000	.000	2412,933	2412,933	.000	.10013	
	54	.000	.000	.000	.000	2335,810	2335,810	.000	.10013	
245	55	.000	.000	.000	.000	2335,810	2335,810	.000	.10013	
	56	.000	.000	.000	.000	2094,409	2094,409	.000	.08944	
245	57	.000	.000	.000	.000	2094,409	2094,409	.000	.08944	
	58	.000	.000	.000	.000	1774,809	1774,809	.000	.07344	
245	59	.000	.000	.000	.000	1774,809	1774,809	.000	.07344	
	60	.000	.000	.000	.000	701,054	701,054	.000	.02851	
245	61	.000	.000	.000	.000	701,054	701,054	.000	.02851	
	62	.000	.000	.000	.000	802,150	802,150	.000	.03209	
245	63	.000	.000	.000	.000	802,150	802,150	.000	.03209	
	64	.000	.000	.000	.000	3744,194	3744,194	.000	.15004	
245	65	.000	.000	.000	.000	3744,194	3744,194	.000	.15004	
	66	.000	.000	.000	.000	3735,154	3735,154	.000	.14951	
245	67	.000	.000	.000	.000	3735,154	3735,154	.000	.14951	
	68	.000	.000	.000	.000	2704,687	2704,687	.000	.10804	
245	69	.000	.000	.000	.000	2704,687	2704,687	.000	.10804	
	70	.000	.000	.000	.000	1400,003	1400,003	.000	.05843	
245	71	.000	.000	.000	.000	1400,003	1400,003	.000	.05843	
	72	.000	.000	.000	.000	6100,607	6100,607	.000	.23744	
245	73	.000	.000	.000	.000	6100,607	6100,607	.000	.23744	

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (P)	PEAK PRESSURE STRESS (PMAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TI)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T10/(1.0+SAM)	MODIFIED STRESS RATIO
345	58	.000	.000	.000	.000	5555.539	5555.539	.000	.29049	
345	61	.000	.000	.000	.000	5045.872	5045.872	.000	.25593	
345	62	.000	.000	.000	.000	5045.872	5045.872	.000	.25593	
375	57	.000	.000	.000	.000	2209.804	2209.804	.000	.11555	
375	53	.000	.000	.000	.000	2209.804	2209.804	.000	.11555	
375	54	.000	.000	.000	.000	3155.660	3155.660	.000	.16509	
375	55	.000	.000	.000	.000	3737.165	3737.165	.000	.19502	
375	56	.000	.000	.000	.000	3292.665	3292.665	.000	.17217	
375	57	.000	.000	.000	.000	2115.435	2115.435	.000	.11035	
405	58	.000	.000	.000	.000	1649.308	1649.308	.000	.08624	
415	42	.000	.000	.000	.000	1900.334	1900.334	.000	.10407	
415	43	.000	.000	.000	.000	1203.804	1203.804	.000	.05567	
425	43	.000	.000	.000	.000	478.894	478.894	.000	.02504	
425	24	.000	.000	.000	.000	478.894	478.894	.000	.02504	
435	44	.000	.000	.000	.000	722.156	722.156	.000	.03774	
435	27	.000	.000	.000	.000	1714.271	1714.271	.000	.07964	
						1872.301	1872.301	.000	.09790	

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (P)	PEAK PRESSURE STRESS (PMAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TI)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T10/(1.0+SAM)	MODIFIED STRESS RATIO
7C	22	.000	.000	.000	.000	3520.750	3520.750	.000	.18400	
7C	23	.000	.000	.000	.000	2777.876	2777.876	.000	.14525	
8C	24	.000	.000	.000	.000	1144.300	1144.300	.000	.05903	
8C	25	.000	.000	.000	.000	1819.763	1819.763	.000	.09449	
9C	27	.000	.000	.000	.000	2966.901	2966.901	.000	.15513	
9C	28	.000	.000	.000	.000	3234.715	3234.715	.000	.16940	
10C	31	.000	.000	.000	.000	4500.705	4500.705	.000	.23533	
10C	32	.000	.000	.000	.000	5186.613	5186.613	.000	.27120	
11C	34	.000	.000	.000	.000	1588.405	1588.405	.000	.08307	
11C	35	.000	.000	.000	.000	1598.129	1598.129	.000	.08356	
12C	36	.000	.000	.000	.000	2784.582	2784.582	.000	.14560	
12C	37	.000	.000	.000	.000	3063.165	3063.165	.000	.16017	
13C	38	.000	.000	.000	.000	3087.461	3087.461	.000	.16049	
13C	39	.000	.000	.000	.000	3963.983	3963.983	.000	.20727	
14C	41	.000	.000	.000	.000	1155.654	1155.654	.000	.06054	
14C	42	.000	.000	.000	.000	1514.342	1514.342	.000	.07918	
14C	44	.000	.000	.000	.000	6154.262	6154.262	.000	.32174	
14C	45	.000	.000	.000	.000	6133.146	6133.146	.000	.32069	
14C	50	.000	.000	.000	.000	10130.671	10130.671	.000	.52971	
17C	53	.000	.000	.000	.000	9126.476	9126.476	.000	.47721	
17C	54	.000	.000	.000	.000	5105.783	5105.783	.000	.27116	
19C	56	.000	.000	.000	.000	6221.560	6221.560	.000	.32531	
19C	57	.000	.000	.000	.000	2110.435	2110.435	.000	.11035	
19C	58	.000	.000	.000	.000	1649.308	1649.308	.000	.08624	
19C	59	.000	.000	.000	.000	3269.734	3269.734	.000	.17097	
						3387.133	3387.133	.000	.17710	

1 ACRRR MAIN STEAM LINE PIPING CLASS 2 ANALYSIS

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (P)	PEAK PRESSURE STRESS (PMAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MR)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TI)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T10/(1.0+SAM)	MODIFIED STRESS RATIO
445	1	.000	.000	.000	.000	17327.623	17327.623	.000	.90602	
445	2	.000	.000	.000	.000	8088.426	8088.426	.000	.42292	
445	3	.000	.000	.000	.000	8088.426	8088.426	.000	.42292	
						533.375	533.375	.000	.02784	

1 ACVR MAIN STEAM LINE PIPING CLASS 2 ANALYSIS

D.7.3 SATISFACTION OF EQUATION 11 (ANALYSIS SET 2)

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PSI)	PEAK PRESSURE STRESS (PHAX)	SUSTAINED LOAD STRESS (SMA)	OCCASIONAL LOAD STRESS (OMA)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T11)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T11/(SAM*SA)	MODIFIED STRESS RATIO
15	3	4094.604	.000	1006.763	.000	402.786	5504.453	.000	14025	.2514
16	4	4094.604	.000	242.421	.000	5909.842	16329.247	.000	25314	.2514
17	5	4094.604	.000	174.305	.000	7157.255	11435.144	.000	29119	.2514
18	6	4094.604	.000	151.332	.000	4499.587	8747.523	.000	22285	.2514
19	7	4094.604	.000	151.332	.000	4499.587	8747.523	.000	22285	.2514
20	8	4094.604	.000	174.108	.000	2078.898	6309.611	.000	16074	.2514
21	9	4094.604	.000	174.108	.000	2078.898	6309.611	.000	16074	.2514
22	10	4094.604	.000	255.424	.000	1647.426	6005.554	.000	15267	.2514
23	11	4094.604	.000	255.424	.000	1647.426	6005.554	.000	15267	.2514
24	12	4094.604	.000	340.760	.000	4473.972	9170.357	.000	23734	.2514
25	13	4094.604	.000	340.760	.000	4473.972	9170.357	.000	23734	.2514
26	14	4094.604	.000	394.202	.000	6704.198	11199.004	.000	29510	.2514
27	15	4094.604	.000	394.202	.000	6704.198	11199.004	.000	29510	.2514
28	16	4094.604	.000	447.903	.000	3953.095	8592.543	.000	21890	.2514
29	17	4094.604	.000	447.903	.000	3953.095	8592.543	.000	21890	.2514
30	18	4094.604	.000	710.318	.000	3724.953	8531.876	.000	21740	.2514
31	19	4094.604	.000	408.407	.000	3895.122	8397.336	.000	21380	.2514
32	20	4094.604	.000	313.309	.000	3383.085	7795.044	.000	19553	.2514
33	21	4094.604	.000	252.152	.000	3260.981	7609.734	.000	19386	.2514
34	22	3850.027	.000	253.013	.000	2850.078	7204.600	.000	18364	.2514
35	23	3850.027	.000	124.102	.000	3490.500	7603.440	.000	19370	.2514
36	24	3850.027	.000	343.940	.000	4512.194	8497.327	.000	21547	.2514
37	25	3850.027	.000	343.940	.000	4512.194	8497.327	.000	21547	.2514
38	26	4094.604	.000	511.404	.000	4151.079	8521.710	.000	21709	.2514
39	27	4094.604	.000	605.466	.000	3531.202	8233.372	.000	20975	.2514
40	28	4094.604	.000	443.033	.000	2070.482	6707.120	.000	17067	.2514
41	29	3850.027	.000	579.934	.000	6282.169	10701.130	.000	27261	.2514
42	30	3850.027	.000	242.053	.000	6329.773	8430.843	.000	21478	.2514
43	31	3850.027	.000	444.156	.000	5242.020	9619.453	.000	24505	.2514
44	32	3850.027	.000	444.156	.000	5242.020	9619.453	.000	24505	.2514

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PSI)	PEAK PRESSURE STRESS (PHAX)	SUSTAINED LOAD STRESS (SMA)	OCCASIONAL LOAD STRESS (OMA)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T11)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T11/(SAM*SA)	MODIFIED STRESS RATIO
1C	4	4094.602	.000	475.990	.000	10754.874	16000.667	.000	44748	.2514
2C	11	3850.027	.000	316.559	.000	12850.999	17977.309	.000	521	.2514
3C	12	3850.027	.000	324.035	.000	5796.234	9979.269	.000	25423	.2514
4C	13	3850.027	.000	330.912	.000	4672.708	8871.647	.000	22501	.2514
5C	14	3850.027	.000	164.811	.000	6040.449	10064.287	.000	25649	.2514
6C	15	3850.027	.000	354.474	.000	7729.733	11943.234	.000	30426	.2514

7C	16	3850.027	.000	421.783	.000	5504.425	9989.235	.000	25448	.2514
8C	17	3850.027	.000	511.978	.000	4529.076	8902.041	.000	22778	.2514
9C	18	3850.027	.000	684.841	.000	4557.621	10100.379	.000	25732	.2514
10C	19	4094.604	.000	1043.377	.000	7047.764	11950.190	.000	32443	.2514
11C	20	4094.604	.000	994.563	.000	5214.353	10309.521	.000	26264	.2514
12C	21	4094.604	.000	847.893	.000	4944.269	9884.766	.000	25192	.2514

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PSI)	PEAK PRESSURE STRESS (PHAX)	SUSTAINED LOAD STRESS (SMA)	OCCASIONAL LOAD STRESS (OMA)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T11)	MODIFIED ALLOWABLE STRESS (SAM)	DESIGN STRESS RATIO T11/(SAM*SA)	MODIFIED STRESS RATIO
135	21	4094.602	.000	467.256	.000	2300.409	7767.866	.000	22743	.2514
136	22	4094.602	.000	554.182	.000	2221.910	7587.893	.000	22236	.2514
137	23	4094.602	.000	544.783	.000	1753.090	7127.674	.000	20487	.2514
138	24	4094.602	.000	744.047	.000	1081.808	6635.657	.000	19448	.2514
139	25	4094.602	.000	683.443	.000	1022.214	6420.461	.000	18815	.2514
140	26	4094.602	.000	173.020	.000	1374.794	6397.615	.000	18440	.2514
141	27	4094.602	.000	185.207	.000	1374.794	6397.615	.000	18441	.2514
142	28	4094.602	.000	324.374	.000	1714.071	6808.446	.000	20075	.2514
143	29	4094.602	.000	1177.497	.000	4954.024	15009.498	.000	43981	.2514
144	30	4094.602	.000	783.249	.000	5005.727	10772.500	.000	31564	.2514
145	31	4094.602	.000	783.249	.000	5005.727	10772.500	.000	31564	.2514
146	32	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
147	33	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
148	34	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
149	35	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
150	36	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
151	37	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
152	38	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
153	39	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
154	40	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
155	41	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
156	42	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
157	43	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
158	44	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
159	45	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
160	46	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
161	47	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
162	48	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
163	49	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
164	50	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
165	51	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
166	52	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
167	53	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
168	54	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
169	55	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
170	56	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
171	57	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
172	58	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
173	59	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
174	60	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
175	61	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
176	62	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
177	63	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
178	64	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
179	65	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
180	66	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
181	67	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
182	68	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
183	69	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
184	70	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
185	71	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
186	72	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
187	73	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
188	74	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
189	75	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
190	76	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
191	77	4094.602	.000	493.632	.000	2504.924	7027.033	.000	20289	.2514
192	78	4094.602	.000	493.632	.000	250				

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PSI)	PEAK POINT STRESS (PSI MAX)	SUSTAINED LOAD STRESS (PSI)	OCCASIONAL LOAD STRESS (PSI)	THERMAL EXPANSION STRESS (PSI)	TOTAL STRESS (PSI)	MODIFIED ALLOWABLE STRESS (SAW)	DESIGN STRESS RATIO T11/(S1+S4)	MODIFIED STRESS RATIO
305	50	4924.577	.000	309.017	.000	5555.539	11991.113	.000	.33958	
	51	4924.577	.000	774.729	.000	5085.872	10791.674	.000	.31674	
305	81	4924.577	.000	744.940	.000	5085.872	10791.949	.000	.31690	
	82	4924.577	.000	2332.394	.000	2209.004	9449.195	.000	.27744	
375	49	4924.577	.000	9322.354	.000	2209.004	9449.195	.000	.27744	
	51	4924.577	.000	272.219	.000	3155.658	835.216	.000	.27744	
306	54	4924.577	.000	613.431	.000	3707.168	9397.173	.000	.27332	
	55	4924.577	.000	693.345	.000	3292.065	864.876	.000	.25425	
306	55	4924.577	.000	447.654	.000	2110.436	7432.792	.000	.21367	
	56	4924.577	.000	396.790	.000	1449.308	6054.849	.000	.21781	
406	57	4924.577	.000	390.974	.000	1990.374	7203.497	.000	.20384	
	58	4924.577	.000	367.048	.000	1081.808	6564.204	.000	.21345	
416	67	4924.577	.000	773.346	.000	474.984	9001.777	.000	.17553	
	63	4924.577	.000	715.091	.000	478.984	9033.690	.000	.17461	
475	63	4924.577	.000	745.013	.000	722.154	5919.208	.000	.17346	
	24	4924.577	.000	387.250	.000	1714.271	6042.072	.000	.20103	
475	64	4924.577	.000	335.499	.000	1872.381	7009.399	.000	.20540	
	27	4924.577	.000	327.127	.000			.000		

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PSI)	PEAK POINT STRESS (PSI MAX)	SUSTAINED LOAD STRESS (PSI)	OCCASIONAL LOAD STRESS (PSI)	THERMAL EXPANSION STRESS (PSI)	TOTAL STRESS (PSI)	MODIFIED ALLOWABLE STRESS (SAW)	DESIGN STRESS RATIO T11/(S1+S4)	MODIFIED STRESS RATIO
70	22	4924.577	.000	881.303	.000	3920.750	9011.856	.000	.28904	
	23	4924.577	.000	894.932	.000	2777.876	8482.410	.000	.28457	
70	24	4924.577	.000	613.420	.000	1144.300	6567.722	.000	.19248	
	25	4924.577	.000	972.424	.000	1619.763	7301.649	.000	.21574	
90	27	4924.577	.000	514.312	.000	2964.901	8299.674	.000	.24308	
	28	4924.577	.000	476.574	.000	3239.715	8474.602	.000	.24444	
140	31	4924.577	.000	759.201	.000	4500.705	10186.443	.000	.29380	
	32	4924.577	.000	931.858	.000	5154.613	11045.048	.000	.32366	
110	34	4924.577	.000	481.352	.000	1534.805	6994.734	.000	.20533	
	35	4924.577	.000	65.425	.000	1594.129	6564.204	.000	.19297	
120	36	4924.577	.000	769.644	.000	2744.582	8482.410	.000	.28457	
	37	4924.577	.000	1209.790	.000	3083.165	9172.522	.000	.29934	
140	38	4924.577	.000	1194.958	.000	3987.461	10109.036	.000	.29824	
	39	4924.577	.000	1787.060	.000	3983.983	10178.120	.000	.31201	
140	47	4924.577	.000	614.668	.000	1154.654	6704.899	.000	.19544	
	43	4924.577	.000	614.275	.000	1514.342	7057.193	.000	.20640	
180	44	4924.577	.000	649.250	.000	4154.263	11530.099	.000	.33788	
	45	4924.577	.000	449.874	.000	6133.146	11598.597	.000	.33766	
140	49	4924.577	.000	1338.443	.000	10130.471	16291.931	.000	.47005	
	50	4924.577	.000	1312.031	.000	9126.876	15365.494	.000	.45028	
170	53	4924.577	.000	444.878	.000	5155.763	10559.238	.000	.30943	
	54	4924.577	.000	1007.749	.000	6221.590	12154.906	.000	.35622	
140	56	4924.577	.000	396.790	.000	2110.436	7432.792	.000	.21367	
	57	4924.577	.000	390.974	.000	1649.328	6954.899	.000	.20384	
190	58	4924.577	.000	602.948	.000	3269.734	8799.297	.000	.25785	
	59	4924.577	.000	623.924	.000	3387.133	8937.634	.000	.26191	

JACOB MAIN STEAM LINE PIPING CLASS 2 ANALYSIS

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PSI)	PEAK POINT STRESS (PSI MAX)	SUSTAINED LOAD STRESS (PSI)	OCCASIONAL LOAD STRESS (PSI)	THERMAL EXPANSION STRESS (PSI)	TOTAL STRESS (PSI)	MODIFIED ALLOWABLE STRESS (SAW)	DESIGN STRESS RATIO T11/(S1+S4)	MODIFIED STRESS RATIO
445	1	4923.672	.000	373.789	.000	17327.623	23525.094	.000	.68938	
	2	4923.672	.000	583.812	.000	8071.426	14500.910	.000	.42494	
445	2	4923.672	.000	583.812	.000	8084.426	14500.910	.000	.42494	
	3	4923.672	.000	1327.840	.000	533.375	7684.697	.000	.22920	

1 ACROSS MAIN STEAM LINE PIPING CLASS 2 ANALYSIS

D.3 CLASS 2 STRESSES FOR ANALYSIS SET NUMBER 3

ASSIGNED LOAD COMBINATION IDENTIFIERS  
MA = 1 MB = 9 MC = 0 PD = 0 PHAX = 2

D.3.1 SATISFACTION OF EQUATION 9 (ANALYSIS SET 3)

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (PHAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MB)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TD)	MODIFIED ALLOWABLE STRESS (SMA)	UPSET STRESS RATIO T9/(1.2*SM)	EFFICIENCY STRESS RATIO T9/(1.8*SM)
15	3	.000	4443,227	1004,063	1527,092	.000	6994,341	.000	.36660	.24444
	4	.000	4443,227	742,421	1554,142	.000	6269,109	.000	.32921	.21889
	5	.000	4443,227	174,305	1611,495	.000	6256,347	.000	.32742	.21841
	6	.000	4443,227	151,332	671,050	.000	5284,509	.000	.27714	.18474
	7	.000	4443,227	174,108	1781,496	.000	6419,230	.000	.33644	.22420
	8	.000	4443,227	254,524	1684,318	.000	6404,069	.000	.33575	.22343
	9	.000	4443,227	254,524	1704,778	.000	6429,528	.000	.33551	.22434
	10	.000	4443,227	349,780	2193,779	.000	7004,755	.000	.34723	.24482
	11	.000	4443,227	394,202	1793,172	.000	6952,800	.000	.34804	.23244
	12	.000	4443,227	697,023	1933,641	.000	6934,821	.000	.34767	.23245
	13	.000	4443,227	710,318	1427,007	.000	6651,907	.000	.34393	.23243
	14	.000	4443,227	400,609	949,025	.000	5833,741	.000	.30575	.20384
	15	.000	4443,227	313,305	872,146	.000	5594,677	.000	.29343	.19542
	16	.000	4443,227	252,152	1134,716	.000	5854,045	.000	.30402	.20444
	17	.000	4443,227	252,917	644,704	.000	5665,878	.000	.29634	.19747
	18	.000	4204,387	253,913	734,402	.000	5197,192	.000	.27239	.18160
	19	.000	4204,387	174,102	1024,099	.000	5420,418	.000	.28409	.19439
	20	.000	4204,387	393,940	844,052	.000	5452,409	.000	.29577	.20051
	21	.000	4443,227	511,404	1144,707	.000	5760,294	.000	.30714	.20474
	22	.000	4443,227	400,546	1344,441	.000	6454,273	.000	.33844	.22544
	23	.000	4443,227	580,033	1244,449	.000	6261,719	.000	.33818	.21874
	24	.000	4204,387	242,053	504,073	.000	6304,133	.000	.33051	.22034
	25	.000	4204,387	468,156	1744,017	.000	5347,413	.000	.28204	.18444
	26	.000	4204,387	464,470	994,612	.000	6430,540	.000	.33763	.22444
	27	.000	4204,387	464,470	994,612	.000	5663,470	.000	.29683	.19789

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (PHAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MB)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TD)	MODIFIED ALLOWABLE STRESS (SMA)	UPSET STRESS RATIO T9/(1.2*SM)	EFFICIENCY STRESS RATIO T9/(1.8*SM)
1C	4	.000	4204,387	435,990	274,082	.000	8470,322	.000	.47957	.31372
	5	.000	4204,387	314,559	259,400	.000	8450,204	.000	.44444	.31247
	6	.000	4204,387	324,035	1204,126	.000	5734,544	.000	.30055	.20032
	7	.000	4204,387	330,912	984,150	.000	5531,449	.000	.29001	.19334
	8	.000	4204,387	164,411	1454,041	.000	5834,279	.000	.30564	.20374
	9	.000	4204,387	304,474	204,447	.000	6627,548	.000	.34734	.23157
	10	.000	4204,387	621,743	1331,441	.000	6157,451	.000	.32273	.21014
	11	.000	4204,387	513,478	1154,740	.000	5875,104	.000	.30797	.20524
	12	.000	4204,387	424,441	1531,776	.000	6421,144	.000	.33554	.22434
	13	.000	4204,387	1043,377	2251,430	.000	7459,204	.000	.39204	.24203
	14	.000	4443,227	944,563	2054,441	.000	7512,771	.000	.39375	.24254
	15	.000	4443,227	847,893	1944,503	.000	7256,423	.000	.38033	.25355

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PI)	PEAK PRESSURE STRESS (PHAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MB)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (TD)	MODIFIED ALLOWABLE STRESS (SMA)	UPSET STRESS RATIO T9/(1.2*SM)	EFFICIENCY STRESS RATIO T9/(1.8*SM)
16	21	.000	4204,387	437,256	1384,377	.000	7774,143	.000	.44434	.24044
	22	.000	4204,387	544,182	1424,474	.000	7221,913	.000	.44122	.24744
	23	.000	4204,387	544,182	1444,014	.000	7221,914	.000	.44332	.24444
	24	.000	4204,387	744,047	1344,011	.000	7247,717	.000	.44444	.24217
	25	.000	4204,387	544,443	1244,045	.000	7124,049	.000	.43507	.24331
	26	.000	4204,387	174,000	944,041	.000	6341,444	.000	.35284	.24544
	27	.000	4204,387	174,000	924,016	.000	6341,370	.000	.34945	.24544
	28	.000	4204,387	324,174	844,049	.000	6444,444	.000	.35414	.24544
	29	.000	4204,387	1177,497	3444,100	.000	10411,714	.000	.57474	.34444
	30	.000	4204,387	744,246	2444,047	.000	8771,000	.000	.44744	.24444
	31	.000	4204,387	244,246	2444,047	.000	8771,000	.000	.44744	.24444
	32	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	33	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	34	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	35	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	36	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	37	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	38	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	39	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	40	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	41	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	42	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	43	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	44	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	45	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	46	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	47	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	48	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	49	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	50	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	51	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	52	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	53	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	54	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	55	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	56	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	57	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	58	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	59	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	60	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	61	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	62	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	63	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	64	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	65	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	66	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	67	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	68	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	69	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	70	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	71	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	72	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	73	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	74	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	75	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	76	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	77	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	78	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	79	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	80	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	81	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	82	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	83	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	84	.000	4204,387	431,532	2344,049	.000	8227,304	.000	.44707	.24444
	85	.000	4204,387							



MEMBER NO.	MEMBER ENDS	INTENTIONAL STRESS (P)	BEAK STRESS (P-MAX)	SUSTAINED LOAD STRESS (MAX)	OCCASIONAL LOAD STRESS (MAX)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAW)	UPSET STRESS RATIO T9/(1.25SH)	EMERGENCY STRESS RATIO T9/(1.25SH)
205	40	.000	8347,477	1149,914	1787,0A3	.000	8344,453	.000	.46154	.31055
205	41	.000	8347,477	554,256	1-37,755	.000	7355,670	.000	.46437	.27225
205	42	.000	8347,477	554,256	1420,587	.000	7342,774	.000	.46790	.27101
205	43	.000	8347,477	774,592	1044,443	.000	6834,941	.000	.37972	.25116
205	44	.000	8347,477	764,474	1149,914	.000	6914,549	.000	.38389	.25193
205	45	.000	8347,477	271,724	1411,505	.000	7052,537	.000	.36141	.24121
205	46	.000	8347,477	271,724	133,544	.000	6987,794	.000	.37021	.24191
205	47	.000	8347,477	217,497	1477,684	.000	7074,470	.000	.35234	.24147
205	48	.000	8347,477	994,547	1477,684	.000	7134,407	.000	.35956	.24434
205	49	.000	8347,477	781,371	1874,544	.000	7584,471	.000	.47158	.24184
205	50	.000	8347,477	434,277	377,855	.000	9274,549	.000	.54025	.24177
205	51	.000	8347,477	949,943	4370,849	.000	9056,445	.000	.50240	.24150
205	52	.000	8347,477	412,441	2310,840	.000	10087,399	.000	.60445	.44304
205	53	.000	8347,477	747,017	271,4491	.000	8,34,915	.000	.47142	.24145
205	54	.000	8347,477	770,225	271,4491	.000	8,34,915	.000	.48543	.24155
205	55	.000	8347,477	704,540	2289,840	.000	846,474	.000	.47024	.24157
205	56	.000	8347,477	2310,794	177,044	.000	8423,677	.000	.46794	.24157
205	57	.000	8347,477	2130,794	177,044	.000	9474,317	.000	.52844	.27097
205	58	.000	8347,477	271,019	2541,411	.000	9474,318	.000	.52844	.27097
205	59	.000	8347,477	411,431	1947,843	.000	8100,927	.000	.45441	.24107
205	60	.000	8347,477	591,705	240,035	.000	4074,571	.000	.50159	.23439
205	61	.000	8347,477	447,584	237,719	.000	8161,776	.000	.46446	.24177
205	62	.000	8347,477	394,780	1444,435	.000	8197,294	.000	.46446	.24177
205	63	.000	8347,477	380,974	164,412	.000	7204,892	.000	.40049	.24159
205	64	.000	8347,477	347,046	320,447	.000	7397,243	.000	.41054	.24157
205	65	.000	8347,477	771,345	1341,744	.000	8041,018	.000	.46672	.24114
205	66	.000	8347,477	714,091	121,040	.000	7357,070	.000	.46872	.24144
205	67	.000	8347,477	745,013	121,040	.000	7197,325	.000	.39957	.24104
205	68	.000	8347,477	347,250	121,040	.000	7203,850	.000	.40021	.24104
205	69	.000	8347,477	335,999	894,713	.000	8839,679	.000	.37908	.24139
205	70	.000	8347,477	327,127	914,947	.000	8484,503	.000	.35934	.23944
205	71	.000	8347,477	327,127	914,947	.000	6485,925	.000	.36633	.24022

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTENTIONAL STRESS (P)	BEAK STRESS (P-MAX)	SUSTAINED LOAD STRESS (MAX)	OCCASIONAL LOAD STRESS (MAX)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAW)	UPSET STRESS RATIO T9/(1.25SH)	EMERGENCY STRESS RATIO T9/(1.25SH)
7C	27	.000	8246,251	481,303	2254,746	.000	8380,310	.000	.44557	.31034
7C	28	.000	8246,251	494,932	2307,931	.000	8437,414	.000	.44476	.31251
7C	29	.000	8246,251	411,429	1920,102	.000	7774,543	.000	.43192	.24704
7C	30	.000	8246,251	619,424	2044,103	.000	8227,778	.000	.45710	.31473
7C	31	.000	8246,251	514,352	1444,494	.000	7214,074	.000	.40879	.24719
7C	32	.000	8246,251	420,576	1407,408	.000	7074,374	.000	.39313	.24100
7C	33	.000	8347,477	759,201	3436,444	.000	9562,132	.000	.53123	.39410
7C	34	.000	8347,477	491,048	3479,779	.000	9211,714	.000	.53554	.39444
7C	35	.000	8347,477	491,048	1744,414	.000	7184,443	.000	.39441	.24124
7C	36	.000	8347,477	60,528	1711,438	.000	7159,701	.000	.39774	.24117
7C	37	.000	8347,477	764,664	3441,656	.000	9580,736	.000	.53224	.39444
7C	38	.000	8347,477	1207,740	1337,725	.000	9907,942	.000	.55374	.34114
7C	39	.000	8347,477	1194,494	2724,001	.000	9284,476	.000	.51603	.34407
7C	40	.000	5347,477	1787,540	2985,535	.000	10140,572	.000	.56337	.37554

MEMBER NO.	MEMBER ENDS	INTENTIONAL STRESS (P)	BEAK STRESS (P-MAX)	SUSTAINED LOAD STRESS (MAX)	OCCASIONAL LOAD STRESS (MAX)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAW)	UPSET STRESS RATIO T9/(1.25SH)	EMERGENCY STRESS RATIO T9/(1.25SH)
14C	42	.000	8347,477	618,668	1709,133	.000	7778,278	.000	.43210	.29843
14C	43	.000	8347,477	618,668	2090,498	.000	8074,450	.000	.44888	.29905
14C	44	.000	8347,477	440,250	2314,136	.000	8134,043	.000	.45200	.29134
14C	45	.000	8347,477	460,834	2194,749	.000	8024,270	.000	.44407	.29771
14C	46	.000	8347,477	1334,663	3744,550	.000	10501,710	.000	.58343	.34885
14C	47	.000	8347,477	1314,431	3574,110	.000	10257,218	.000	.58995	.34591
14C	48	.000	8347,477	444,475	417,453	.000	9999,705	.000	.55515	.27011
14C	49	.000	8347,477	1007,749	4987,793	.000	11704,519	.000	.63175	.44043
14C	50	.000	8347,477	349,780	1374,746	.000	7134,342	.000	.39656	.24437
14C	51	.000	8347,477	380,974	1644,412	.000	7397,243	.000	.41054	.24157
14C	52	.000	8347,477	409,686	5264,470	.000	11220,443	.000	.67405	.41603
14C	53	.000	8347,477	621,924	5591,230	.000	11582,631	.000	.64348	.42894

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	INTENTIONAL STRESS (P)	BEAK STRESS (P-MAX)	SUSTAINED LOAD STRESS (MAX)	OCCASIONAL LOAD STRESS (MAX)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAW)	UPSET STRESS RATIO T9/(1.25SH)	EMERGENCY STRESS RATIO T9/(1.25SH)
443	1	.000	8427,672	371,780	4047,179	.000	12764,440	.000	.68137	.45435
443	2	.000	8427,672	444,412	1334,100	.000	8744,444	.000	.44109	.24104
443	3	.000	8427,672	444,412	1334,100	.000	9344,444	.000	.54154	.24104
443	4	.000	8427,672	1327,440	1667,794	.000	8819,306	.000	.48196	.32664

FACTORY MAIN STEAM LINE PIPEST CLASS 2 ANALYSIS

CLASS 2 STRESSES FOR ANALYSIS SET NUMBER 4

ASSIGNED LOAD COMBINATION IDENTIFIERS  
MA \* 1 MR \* 10 MC \* 0 PD \* 0 PHAX \* 2

CLASS 2 SATISFACTION OF EQUATION 9 (ANALYSIS SET 4)

STRAIGHT MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PSI)	PEAK PROXIMATE STRESS (PHAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MO)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAH)	UPSET STRESS RATIO T9/(1.2*SAH)	EMERGENCY STRESS RATIO T9/(1.4*SAH)
15	3	.000	4443.227	1004.663	1494.131	.000	6941.470	.000	.30469	.24371
24	6	.000	4443.227	242.421	2537.472	.000	7237.919	.000	.37045	.28297
34	4	.000	4443.227	174.305	2444.767	.000	7129.208	.000	.37345	.28416
45	7	.000	4443.227	151.332	1594.406	.000	6710.215	.000	.32544	.23100
55	4	.000	4443.227	151.332	1594.406	.000	6710.215	.000	.32544	.23100
65	7	.000	4443.227	174.108	1827.703	.000	6494.727	.000	.33882	.23548
75	8	.000	4443.227	174.108	1827.703	.000	6494.727	.000	.33882	.23548
85	8	.000	4443.227	756.524	1720.732	.000	6444.473	.000	.33707	.23571
95	9	.000	4443.227	365.789	3197.473	.000	6432.678	.000	.33714	.23474
105	10	.000	4443.227	365.789	3197.473	.000	6432.678	.000	.33714	.23474
115	0	.000	4443.227	642.503	2090.091	.000	7094.221	.000	.37192	.24704
125	10	.000	4443.227	642.503	2090.091	.000	7094.221	.000	.37192	.24704
135	10	.000	4443.227	710.318	1452.119	.000	6624.644	.000	.34726	.23159
145	10	.000	4443.227	400.139	1147.563	.000	6511.341	.000	.34504	.23044
155	10	.000	4443.227	313.305	941.743	.000	6754.275	.000	.36193	.24020
165	10	.000	4443.227	252.917	1491.647	.000	6407.192	.000	.34475	.23317
175	12	.000	4204.387	203.913	1244.249	.000	6407.192	.000	.34475	.23317
185	13	.000	4204.387	174.102	864.346	.000	6130.817	.000	.32488	.21995
195	14	.000	4204.387	330.940	1544.346	.000	6154.674	.000	.32691	.21927
205	17	.000	4204.387	511.404	1454.146	.000	6170.137	.000	.32244	.21512
215	20	.000	4443.227	625.566	1364.947	.000	6424.340	.000	.32339	.21594
225	21	.000	4443.227	581.033	1214.711	.000	6257.991	.000	.32657	.22445
235	20	.000	4204.387	579.934	1817.230	.000	6521.551	.000	.32789	.21164
245	11	.000	4204.387	242.053	1294.432	.000	6741.272	.000	.36589	.23044
255	11	.000	4204.387	242.053	1294.432	.000	6741.272	.000	.36589	.23044
265	15	.000	4204.387	464.156	3130.168	.000	7892.712	.000	.46895	.27243
275	15	.000	4204.387	464.156	3130.168	.000	7892.712	.000	.46895	.27243

CURVED MEMBERS FOR RUN 1

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PSI)	PEAK PROXIMATE STRESS (PHAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MO)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAH)	UPSET STRESS RATIO T9/(1.2*SAH)	EMERGENCY STRESS RATIO T9/(1.4*SAH)
1C	4	.000	5244.251	435.990	4544.415	.000	10227.456	.000	.54810	.37874
2C	11	.000	4204.387	316.459	4470.424	.000	10527.223	.000	.55707	.37134
3C	12	.000	4204.387	374.005	1731.762	.000	6261.804	.000	.32815	.21875
4C	13	.000	4204.387	330.912	1865.722	.000	6210.021	.000	.32547	.21404
5C	14	.000	4204.387	149.411	1071.594	.000	5444.552	.000	.28534	.19024
6C	15	.000	4204.387	354.474	1277.044	.000	5834.478	.000	.30580	.20347
7C	16	.000	4204.387	421.782	2544.813	.000	7374.683	.000	.38653	.26740
8C	17	.000	4204.387	413.883	2094.655	.000	6817.909	.000	.35733	.23922
9C	18	.000	4204.387	424.883	1944.655	.000	6835.974	.000	.35822	.23865
10C	19	.000	4443.227	1043.377	2864.674	.000	7917.342	.000	.41449	.27444
11C	20	.000	4443.227	904.583	2074.645	.000	7530.375	.000	.39483	.24322
12C	20	.000	4443.227	847.682	1904.942	.000	7214.112	.000	.37823	.23214

STRAIGHT MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE STRESS (PSI)	PEAK PROXIMATE STRESS (PHAX)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MO)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAH)	UPSET STRESS RATIO T9/(1.2*SAH)	EMERGENCY STRESS RATIO T9/(1.4*SAH)
175	21	.000	5244.251	457.356	1374.463	.000	7071.909	.000	.40411	.27041
185	22	.000	5244.251	504.102	1827.189	.000	7292.572	.000	.40124	.26756
195	23	.000	5244.251	744.143	1444.432	.000	7244.644	.000	.40381	.24491
205	24	.000	5244.251	744.143	1307.244	.000	7373.544	.000	.40997	.24974
215	24	.000	5244.251	744.143	1307.244	.000	7373.544	.000	.40997	.24974
225	24	.000	5244.251	273.170	957.998	.000	6371.245	.000	.35304	.23567
235	24	.000	5244.251	187.207	947.701	.000	6371.245	.000	.35304	.23567
245	24	.000	5244.251	324.734	877.150	.000	6441.394	.000	.36744	.23404
255	28	.000	5367.477	1127.497	144.747	.000	10831.771	.000	.54757	.37111
265	29	.000	5367.477	744.143	817.477	.000	8734.200	.000	.44321	.30047
275	30	.000	5367.477	281.048	2147.477	.000	8354.398	.000	.44701	.30047
285	31	.000	5367.477	401.537	2477.167	.000	8344.177	.000	.44374	.30110
295	31	.000	5367.477	401.537	2477.167	.000	8344.177	.000	.44374	.30110
305	32	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
315	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
325	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
335	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
345	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
355	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
365	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
375	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
385	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
395	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
405	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
415	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
425	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
435	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
445	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
455	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
465	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
475	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
485	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
495	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
505	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
515	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
525	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
535	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
545	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
555	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
565	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
575	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
585	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
595	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
605	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
615	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
625	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
635	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
645	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
655	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
665	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
675	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
685	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
695	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
705	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
715	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
725	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
735	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
745	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304	.29644
755	33	.000	5367.477	442.177	2107.477	.000	7574.194	.000	.44304</	



225	40	.000	5367,477	1189,914	1845,149	.000	8702,860	.000	445570	.36344
	41	.000	5367,477	590,256	1310,280	.000	7228,714	.000	440180	.26773
226	41	.000	5367,477	590,256	1301,483	.000	7221,276	.000	440178	.26774
	42	.000	5367,477	376,592	977,956	.000	6722,085	.000	377284	.26152
365	43	.000	5367,477	356,626	1004,959	.000	6751,041	.000	377284	.26152
	44	.000	5367,477	273,465	1307,772	.000	6944,714	.000	38493	.26774
315	45	.000	5367,477	251,704	1255,268	.000	6806,259	.000	38493	.26774
	46	.000	5367,477	217,307	1328,221	.000	6927,735	.000	38493	.26774
325	46	.000	5367,477	204,567	1308,498	.000	7018,722	.000	38493	.26774
	47	.000	5367,477	161,371	1704,703	.000	7431,410	.000	44227	.27511
335	47	.000	5367,477	136,277	3272,574	.000	9276,329	.000	51535	.34387
	48	.000	5367,477	577,022	2744,777	.000	8644,775	.000	48004	.32013
345	47	.000	5367,477	945,043	4097,453	.000	10414,178	.000	57357	.34387
	49	.000	5367,477	812,441	2924,413	.000	8215,170	.000	48446	.32013
355	50	.000	5367,477	749,017	3025,930	.000	8195,424	.000	48530	.32013
	51	.000	5367,477	779,225	2133,102	.000	8205,304	.000	48002	.32013
365	51	.000	5367,477	786,540	2122,140	.000	8274,577	.000	48591	.32013
	52	.000	5367,477	2332,794	1691,025	.000	9304,394	.000	52190	.34743
375	52	.000	5367,477	2332,794	1691,025	.000	9304,394	.000	52190	.34743
	53	.000	5367,477	277,019	2431,074	.000	8072,570	.000	44248	.26484
385	54	.000	5367,477	611,431	2924,413	.000	8073,218	.000	44248	.26484
	55	.000	5367,477	591,385	2244,759	.000	8243,570	.000	44731	.26574
395	55	.000	5367,477	447,546	2255,938	.000	8073,218	.000	44248	.26484
	56	.000	5367,477	304,740	1395,724	.000	7151,901	.000	33744	.26484
405	57	.000	5367,477	180,474	1634,906	.000	7387,357	.000	41041	.27321
	58	.000	5367,477	357,046	3150,464	.000	8884,977	.000	49361	.32577
415	62	.000	5746,251	773,195	1301,216	.000	7395,852	.000	41041	.27321
	63	.000	5746,251	715,091	1301,217	.000	7254,749	.000	40315	.26477
425	63	.000	5746,251	745,013	1292,095	.000	7277,360	.000	40432	.26551
	64	.000	5746,251	387,750	1321,426	.000	6940,326	.000	38670	.26720
435	64	.000	5746,251	335,999	878,232	.000	8446,442	.000	35814	.23574
	27	.000	5746,251	327,127	373,255	.000	6446,672	.000	35781	.23574

CURVED MEMBERS FOR RUN 2

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE (PSI)	PEAK STRESS (PSI/EAK)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MA)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAH)	UPSET STRESS RATIO T9/(1.25SH)	EFFICIENCY STRESS RATIO T9/(1.65TH)
7C	22	.000	5746,251	881,103	2259,435	.000	8381,300	.000	44563	.31027
	23	.000	5746,251	894,932	2310,214	.000	8454,347	.000	44964	.31213
8C	24	.000	5746,251	813,620	2094,513	.000	7944,314	.000	44154	.27429
	25	.000	5746,251	932,424	2210,824	.000	8303,499	.000	44579	.31027
9C	27	.000	5746,251	518,352	1383,725	.000	7142,327	.000	33680	.24449
	28	.000	5746,251	428,576	1261,176	.000	6936,493	.000	33539	.24603
10C	31	.000	5367,477	759,201	3482,411	.000	9609,299	.000	53395	.35574
	32	.000	5367,477	931,858	3257,410	.000	9557,145	.000	51885	.35327
11C	34	.000	5367,477	481,352	1271,798	.000	7120,627	.000	33559	.24371
	35	.000	5367,477	601,536	1704,358	.000	7212,371	.000	40049	.24717
12C	34	.000	5367,477	769,664	3419,010	.000	9554,150	.000	53290	.35321
	37	.000	5367,477	1202,780	3310,449	.000	9880,946	.000	54494	.34584
13C	34	.000	5367,477	1194,498	2675,523	.000	9237,958	.000	51322	.34210
	39	.000	5367,477	1787,560	2764,478	.000	9940,016	.000	55222	.36815

14C	43	.000	5367,477	618,688	1601,461	.000	7592,886	.000	42182	.28122
	44	.000	5367,477	616,275	1901,544	.000	7889,338	.000	43230	.29221
15C	44	.000	5367,477	449,250	2144,427	.000	7967,334	.000	43234	.29404
	45	.000	5367,477	462,834	2061,402	.000	7927,112	.000	43045	.29235
14C	49	.000	5367,477	1334,683	3344,432	.000	10047,572	.000	55429	.37213
	50	.000	5367,477	1312,631	3322,549	.000	10003,054	.000	55373	.37044
17C	53	.000	5367,477	444,875	1997,020	.000	9811,470	.000	54504	.36377
	54	.000	5367,477	1007,749	4784,277	.000	11164,503	.000	62025	.41321
18C	56	.000	5367,477	375,780	1354,544	.000	7121,804	.000	39566	.26377
	57	.000	5367,477	370,874	1637,806	.000	7387,357	.000	41041	.27321
19C	58	.000	5367,477	602,886	5175,069	.000	11145,532	.000	61920	.41241
	59	.000	5367,477	623,924	5496,181	.000	11487,592	.000	63820	.42547

STRAIGHT MEMBERS FOR RUN 3

MEMBER NO.	MEMBER ENDS	INTERNAL PRESSURE (PSI)	PEAK STRESS (PSI/EAK)	SUSTAINED LOAD STRESS (MA)	OCCASIONAL LOAD STRESS (MA)	THERMAL EXPANSION STRESS (MC)	TOTAL STRESS (T)	MODIFIED ALLOWABLE STRESS (SAH)	UPSET STRESS RATIO T9/(1.25SH)	EFFICIENCY STRESS RATIO T9/(1.65TH)
445	1	.000	5923,672	373,709	2463,519	.000	8659,990	.000	49111	.37074
	2	.000	5923,672	588,812	754,557	.000	7167,041	.000	36017	.26544
445	2	.000	5923,672	588,812	754,557	.000	7167,041	.000	36017	.26544
	3	.000	5923,672	1327,840	1965,628	.000	9117,140	.000	50651	.33767