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J. T. Beckham, Jr. Vice President and General Manager Nuclear Generation

April 5, 1982

the southern electric system.

U. S. Nuclear Regulatory Commission Operating Reactor Branch #4 Division of Licensing Washington, D. C. 20555

ATTENTION: Mr. John F. Stolz



NRC DOCKETS 50-321, 50-366
OPERATING LICENSES DPR-57, NPF-5
EDWIN I. HATCH NUCLEAR PLANT UNITS 1, 2
RESPONSE TO CONTAINMENT SYSTEMS BRANCH REQUEST FOR
ADDITIONAL INFORMATION ON MAIN
STEAM LINE BREAK

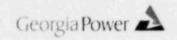
Gentlemen:

The following is submitted in response to your letter of February 25, 1982 which requested additional information regarding peak containment temperatures for equipment qualification purposes at Plant Hatch. The letter requested Georgia Power company (GPC) to perform and submit main steam line break analyses for multiple break sizes since the NRC staff had determined that this type of accident was limiting for peak containment temperatures. A small line break (SLB) analysis in high energy piping for Plant Hatch was performed. Based upon the results of this analysis, we conclude that the design basis accident (DBA) analyses in the FSARs bound the SLB analysis with regard to drywell peak temperature.

The Plant Hatch unique drywell temperature SLB analysis examined a spectrum of three break sizes (.01, 0.1, 0.5 ft²) in high energy lines to determine the maximum drywell temperature. The 0.5 ft² break results in rapid vessel depressurization and produces the highest drywell peak temperature of the three break sizes, which is $274^{\rm OF}$.

The GE SLB analysis was performed in compliance with NUREG-0588 (except for the manner in which heat sink condensate is treated and the assumption of a homogeneous air/steam mixture in the drywell). The assumptions made during the course of the analysis are summarized in Attachment 2.

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The drywell peak temperatures obtained by the DBA analyses in the HNP-FSARs for Units 1 and 2 are conservative and the assumptions documented by GE have been approved by the NRC (NUREG-0661). As shown in Attachment 1, the peak drywell temperature for each SLB case is lower than the FSAR DBA temperatures of 289°F for Unit 1 and 304°F for Unit 2. This confirms that the original drywell temperature analyses contained in the HNP-FSARs are bounding for peak temperatures for equipment qualification purposes.

J. T. Beckham, Jr. states that he is Vice President of Georgia Power Company and is authorized to execute this oath on behalf of Georgia Power Company, and that to the best of his knowledge and belief the facts set forth in this letter are true.

Public

GEORGIA POWER CUMPANY

By: J. J. Beckham, Jr.

Sworn to and subscribed before me this 5th day of April, 1982

CS/mb

Notary Public, Georgia, State at Large My Commission Expires July 26, 1985

Enclosures

xc: M. Manry

R. F. Rogers, III

J. P. O'Reilly (NRC-Region II)

ATTACHMENT 1
SUMMARY OF SLB VERSUS DBA ANALYSIS RESULTS

Break Size	Time to Maximum Temperature	Maximum Temperature
(ft ²)	(sec)	(°F)
.01	676	213.4
.1	623	262.6
.5	7.7	274.3
HNP-2 FSAR-DBA	Approx. 8	304.0
HNP-1 FSAR-DBA	Approx. 8	289.0

ATTACHMENT 2

MAJOR INPUT SLB ANALYSIS ASSUMPTIONS

Scram:

MSIV Closure:

ECCS Systems:

Feedwater flow:

Auto depressurization System:

RHR pool cooling:

Initial suppression pool temp:

Initial reactor power:

Initial drywell relative humidity:

Initial drywell temperature:

Drywell steel liner:

Surface area:

Heat capacity

At time zero

At 3.5 seconds

HPCI plus 1 core spray pump

Coastdown to zero in 7 sec.

Actuated at 10 min.

1 loop initiated at 10 min.

95°F

102% of rated

20%

135°F

15842 ft²

90108 BTU/0F