NRC FOR	U.S. NUCLEAR REGULATORY COMMISSION
	CONTROL BLOCK:
0 1	$ N \ C \ B \ E \ P \ 2 \ 2 \ 0 \ 0 \ - \ 0 \ 0 \ 0 \ 0 \ - \ 0 \ 0$
7 8 CON'T 0 1 7 8	REPORT L 6 0 5 0 - 0 3 2 4 7 0 2 1 5 8 2 8 0 3 0 8 8 2 9 SOURCE 60 61 DOCKET NUMBER 68 69 EVENT DATE 74 75 REPORT DATE 80 9 EVENT DESCRIPTION AND PROBABLE CONSEQUENCES 10
0 2	During plant operation, routine operator surveillance revealed the presence of an
03	Loily film on the inside of the relay mechanism cover window to main steam line tunnel
04	temperature high channel "B" actuation relay, A71B-K2B. This relay receives input
0 5	from PCIS instruments, B21-1S-NO10B, NO11B, NO12B, and NO13B. The remaining main steam
06	line tunnel temperature high channels were operable and would have initiated a Group I
0 7	isolation signal upon receipt of an actual high temperature condition in the "A", "C",
08 78	and "D" main steamlines. Technical Specifications 3.3.2, 6.9.1.9b j   9 SYSTEM CAUSE COMP. VALVE
09 78	CODE CODE UB
	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
10	Melted insulation form the relay coil, which appeared as an oily film in the relay
11	window, dripped down onto the relay contact support armature, preventing deenergization
12	of the relay upon an actuation signal. The channel was tripped in accordance with
13	technical specifications and the relay, Model No. 12HFA51A49F, was replaced. The
14	affected "B" channel was then returned to service.
1 5	FACILITY STATUS 9 0 8 0 29 NA 9 10 12 13 44 45 46 DISCOVERY DESCRIPTION 32 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	ACTIVITY CONTENT ELEASED OF RELEASE AMOUNT OF ACTIVITY 35 2 33 2 34 10 11 10 11 10 11 10 11 10 11 10 10 11 10 10
1 7 7 8	9 PERSONNEL INJURIES 13 80
18	NUMBER DESCRIPTION (4) 9 11 12 NA
19	LOSS OF OR DAMAGE TO FACILITY (43) LYPE DESCRIPTION NA 2 (42) NA 10 NA 80
20	NRC USE ONLY       NRC USE ONLY </td
	NAME OF PREPARER M. J. Pastva, Jr. PHONE (919) 457-9521

## Facility: BSEP Unit No. 2

Event Date: February 15, 1982

While performing routine surveillance during plant operation, the control operator discovered the presence of an oily film on the inside of the relay mechanism window to main steam line tunnel temperature high channel 'B" actuation relay. This continuously energized AC relay receives input from PCIS instruments, B21-TS-NO10B, NO11B, NO12B, and NO13B. An investigation into the oily film determined that the relay insulation had melted in a manner which would prevent the relay from performing its function. At the time of this discovery, the remaining main steam line tunnel temperature high input channels A, C, and D were operable.

Following the discovery of the channel B inoperability, it was tripped in accordance with the action statement outlined in technical specifications and an investigation to determine the cause of the problem was begun.

An inspection of the normally energized B channel actuation relay, A71B-K2B, General Electric Model No. 12HFA51A49F, revealed the relay's movable contacts were held immovable against the stationary contacts due to the relay contact support armature physically adhering to the relay coil core assembly. This occurred when several of the relay coil turns electrically shorted causing a temperature increase in the coils that eventually broke down and melted the coil insulation. The melted insulation then dripped down on the relay contact support armature causing the physical adhering of the armature to the coil assembly.

The exact cause of the shorted relay coil turns is now known. Consultations with the relay supplier indicate that thermal aging of the enamel insulation on the relay coil turns is a definite factor in similar failures experienced by other utilities with this type relay. This problem has been previously documented in General Electric Service Information Letter No. 44 and IE Notice 81-01.

Present intended final corrective action concerning this event is to replace the existing Model HFA51A49F relay coils utilized on continuously energized AC solenoids in the plant with a replacement coil, Kit No. 257A9680G18, during the upcoming Unit No. 2 refueling outage. However, this action is pending relay vendor testing to determine whether relay contactor arm bending observed in some of the failures experienced by other utilities is a factor in causing the excessive currents experienced in the relay coils which lead to breakdown of the coil insulation. If testing shows that relay contactor arm bending is not a factor in the relay coil failures, the replacement coil kit will be utilized. However, if testing shows relay contactor arm bending is a contributor to relay coil insulation breakdown, further study of the problem will be performed in order to determine what corrective actions are required.

Until final corrective actions concerning the use of this type relay coil have been made, the AC continuously energized HFA type relay coils utilized in the plant will be inspected on a monthly basis in order to detect and replace with duplicate coils any failing relay coils before complete coil failure is encountered.