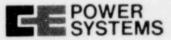
C-E Power Systems Combustion Engineering, Inc. 1000 Prospect Hill Road Windsor, Connecticut 06095 Tel. 203/688-1911 Telex: 99297





Docket No.: STN-50-470F

March 3, 1982 LD-82-028

Mr. Darrell G. Eisenhut, Director Division of Licensing U. S. Nuclear Regulatory Commission Washington, D. C. 20555

Subject: Confirmatory Issue No. 2, Pump and Valve Operability

Dear Mr. Eisenhut:

The Safety Evaluation Report for CESSAR-F requested that C-E provide confirmatory information for a pump and valve operability assurance program. This information was provided informally to the Staff in draft form and was found acceptable. The information is now being provided formally, and is to be included in the next amendment to CESSAR-F.

If we can be of any additional assistance, please feel free to contact either myself or Mr. G. A. Davis of my staff at (203)688-1911, Extension 2803.

Very truly yours,

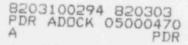
COMBUSTION ENGINEERING, INC.

A. E. Scherer Director Nuclear Licensing

E003

AES:ctk

Attachment



limits for active components, consistent with the recommendations of Regulatory Guide 1.48. The specification requires that the manufacturer demonstrate operability by analysis or test (footnotes 6 and 11 of Regulatory Guide 1.48). The results are independently reviewed by the NSSS Supplier considering the effects of postulated failure modes on operability.

- B. Analysis and/or test demonstrating the operability of each design under the most severe postulated loadings which are combined in a manner consistent with the recommendations of Regulatory Guide 1.48. Methods/results of operability demonstration programs are detailed in Sections 3.9.3.2.2.2 and 3.9.3.2.2.3.
- C. Inspection of each component to assure compliance of critical parameters with specifications and drawings. This inspection confirms that specified materials and processes were used, that wall thicknesses met code requirements, and that fits and finishes met the manufacturer's requirements based on design clearance requirements.
- D. Shop testing of each component to verify "as built" conditions as defined in Sections 3.9.3.2.2.2 and 3.9.3.2.2.3.
- E. Startup and periodic inservice testing in accordance with ASME Boiler and Pressure Vessel Code, Section XI to demonstrate that the active pumps and valves are in operating condition throughout the life of the plant.

NSSS active pumps are listed below with a brief description of active safety function of each. NSSS active valves are listed in Table 3.9.3-3.

#### Active Components

High-pressure safety injection pumps

Low-pressure safety injection pumps

Charging pumps

Active Safety Function

Operate at flowrates to runout

Operate at flowrates to runout

Operate

### 3.9.3.2.2.2 Operability Assurance Program Results for Active Pumps

3.9.3.2.2.2.1 <u>High- and Low-Pressure Safety Injection Pumps</u>. Operability of the high- and low-pressure safety injection (HPSI and LPSI) pumps under faulted conditions has been demonstrated by analyses of the assemblies and by analyses and tests of the motors in accordance with the recommendations of Regulatory Guide 1.48. For the HPSI pumps, the manufacturer has shown that allowable stresses are not exceeded, that clearances are acceptable and that shaft and pedestal bolt deflections do not cause stresses to exceed the normal values indicated by past experience for other pumps of the same type.

For the LPSI pumps, the manufacturer has shown that allowable stresses are not exceeded and that clearances remain acceptable under faulted loadings.

Where necessary, lumped mass models are used with the computer programs to determine the natural frequencies and displacements. The models are conservative (i.e., simplifications tend to make them more flexible).

Operability was demonstrated under the following loads;

	HPSI Pump	LPSI Pump
Horizontal seismic, g's	1.1	1.1
Vertical seismic, g's	1.1	1.1
Design pressure, 1b/in.	2050	2050
Suction nozzle max, resultant force, 1b	4000	4000
Suction nozzle max, resultant moment, ft-1b	12000	50000
Discharge nozzle max, resultant force, 1b	2500	6500
Discharge nozzle max, resultant moment, ft-lb	2500	16000 -

To verify "as built" conditions the HPSI and LPSI pumps were hydrostatically tested in accordance with the ASME Boiler and Pressure Vessel Code, Section III to confirm acceptability of structural integrity of pressure retaining parts, tested for seal leakage, and tested for performance and NPSH characteristics in accordance with the Hydraulic Institute Standard to verify operation within specified parameters. The motors were built as Class IE and were tested in accordance with IEEE Standard 112A-1964 to verify operation within specified parameters. Additionally, the motors were qualified to IEEE Standard 323-1974 and IEEE Standard 344-1975 to assure operability during and following design basis events.

3.9.3.2.2.2.2 <u>Charging Pumps</u>. The charging pumps have a relatively complex geometry, which is difficult to analyze. Therefore, a simplified analysis and type test were used to confirm the charging pump operability during and following a DBE.

A sinusoidal test with simultaneous 1.5 g horizontal and vertical accelerations was conducted. The test on the pump assembly, including its supports, showed no significant natural frequencies in the 1 to 33 Hz range. The fundamental linear natural frequency of the rotating parts of the pump was shown to be greater than 73 Hz. The base of the test pump had a fundamental natural frequency above 33 Hz. Therefore, the System 80 pumps are rigid to postulated seismic input.

The test pump was vibration tested with 2410 psig internal pressure, 1825pound axial force and 610 ft-1b moment on the suction nozzle, and 1650pound axial force and 550 ft-1b moment on the discharge nozzle. Simultaneous 1.5g accelerations is applied to the horizontal and vertical axes by driving the assembly in a 45 degree plane. The test was run with the horizontal input parallel to the motor axis. It was repeated with the horizontal input directed 90, 180, and then 270 degrees from the direction for the first test.

The pump was subjected to two sinusoidal sweeps at 1/2 octave per minute in each direction with 1.0g peak accelerations, limited to 12-inch double amplitude, from 1 to 35 Hz. One of the sweeps in each direction was with the pump operating and one with the pump idle. The test shows that no resonances applicable to operability are in the range of concern, and the unit is therefore rigid to the postulated seismic input. The assembly, both operating and nonoperating, was exposed to a 1.5g horizontal and vertical 30-second sinusoidal dwell at 2.5, 10, 12.25, 20, 23.8 and 33 Hz. The pump was shown to operate normally, and no evidence of damage or deterioration to critical parts exists. The 1.5g horizontal and vertical accelerations exceed the applicable response spectra. The successful test on these pumps demonstrates that the System 80 pumps operate during and following the postulated seismic event.

To verify "as built" conditions the charging pumps were hydrostatically tested in accordance with the ASME Boiler and Pressure Vessel Code, Section III to confirm acceptability of structural integrity of pressure retaining parts, tested for seal leakage, and tested for performance and NPSH characteristics in accordance with the Hydraulic Institute Standards to verify operation within specified parameters. The motors were built as Class IE and were tested in accordance with IEEE Standard 112A-1964 to verify operation within specified parameters. Additionally, the motors were qualified to IEEE Standard 323-1974 and IEEE Standard 344-1975 to assure operability during and following design basis events.

#### 3.9.3.2.2.3 Operability Assurance Program for Active Valves

<u>Safety related active valves</u> must perform their mechanical motion in times of an accident. The qualification program assures that these valves will operate during a seismic event. Qualification tests and/or analyses are conducted for all active valves.

Class 1, 2 and 3 valves are designed/analyzed according to the rules of the ASME Boiler and Pressure Vessel Code, Section III, Section NB-3500, NC-3500, and ND-3500 respectively. Procurement specifications for safety related active valves stipulate that vendor shall submit either detailed calculations and/or test data to demonstrate operability when subjected to the specification loading and stress criteria (normal through faulted conditions). The decision to accept actual or prototype test data, or analysis for operability assurance is made during the normal design and procurement process. The decision to test is based on (1) whether the component is amenable to analysis, (2) whether proven analytical methods are available, and (3) whether applicable prototype test data is available. If analysis or prototype test data is not sufficient, testing is conducted to qualify the component or to verify the analytical technique.

Where appropriate, valve stem deflection calculations are performed to determine deflections due to short term seismic and other applicable leadings. Deflections so determined are compared to allowable clearances. It must be noted that seismic events are of short duration; thus, contact (if it occurs) does not demonstrate that operability is adversely affected. Cases where contact occurs are reviewed on a case by case basis to determine acceptability.

The operability of active Code Class 1, 2 and 3 components is assured through an extensive program of design verification, qualification testing and thorough surveillance of the manufacturing, assembly and shop testing of each active component. Each aspect of the design related to pressure boundary integrity and operability is either tested or verified by calculations. Procedures for testing are developed by component manufacturers and reviewed and approved by the NSSS supplier before the tests are conducted. The design analyses of the component take into consideration environmental cond tions including loadings developed from seismic, operational effects, and pipe loads. Where necessary and feasible, the conclusions of these analyses are confirmed by test.

On all active valves, an analysis of the extended structure is also performed for static equivalent seismic SSE loads supplied at the center of gravity of the extended structure. The maximum stress limits allowed in these analyses show that structural integrity is within the limits developed and accepted by the ASME Code.

The safety-related values are subjected to a series of tests prior to service and during the plant life. Prior to installation, the following tests are performed; shell hydrostatic test to ASME Sections III requirements, backseat and main seat leakage tests, disc hydrostatic test, functional tests to verify that the value will open and close within the specified time limits, operability qualification of motor operators for the environmental conditions over the installed life (i.e., aging, radiation, accident environment simulation, etc.) according to IEEE 382. Cold hydro malification tests, hot functional qualification tests, periodic inservice inspections, and periodic inservices operation are performed insit. to verify and assure the functional ability of the values. These tests ensure the reliability of the value for the design life of the plant. The values are designed using either stress analyses or the pressure containing mammum wall thickness requirements. All the active valves shall be designed to ave a first natural frequency which is greater than 33 Hz. This is shown by suitable test or analysis.

The above outlines in general the methods used to assure valve operability. Each vendor's specific program is described in the plant specific FSAR.

In addition to the above, the following specific operability assurances are provided for the various type valves:

### 3.9.3.2.2.3.1 Pneumatically Operated Valves

Pneumatic operated valves are furnished by several vendors in CE System 80 Nuclear Power Plants. Methods of operability demonstration are discussed in general but will be discussed in detail in the plant specific FSAR subject to the vendor(s) utilized. Spring actuation of the valve is the required active safety function. Loss of electric power or supply air will result in venting of the actuator and return of the valve to the safe position. Each vendor provides their own method to demonstrate valve operability. The operability for these valves is demonstrated by analysis, test or by a combination of analysis and test. The vendor considers concurrent loads including seismic, design pressure and pipe loads.

The three-way solenoid valve was qualified by test to IEEE-382-1972, IEEE-323-1974 and IEEE-344-1975. Testing included thermal aging, radiation aging, wear aging, vibration endurance, seismic event simulation, and loss of coolant accident. All test results provided satisfactory  $\epsilon$  dence of air solenoid valve operability.

Limit switches, used to determine valve position, were qualified by testing to IEEE-323-1974, IEEE-344-1975 and IEEE-382-1972. Switches were successfully performance tested for aging simulation, wear aging, radiation exposure, seismic qualification, and design basis event environmental conditions. For valves outside of containment and utilizing EA-170 limit switches, the switches were seismically qualified to IEEE-344-1975 and were tested to sustain radiation dosages up to  $2 \times 10^{\circ}$  rads.

### 3.9.3.2.2.3.2 Motor Operated Valves

Motor operated values are qualified by analysis as a minimum as described above. The analysis for each value assembly considers the effects of seismic loads, design pressure, and piping reaction forces to provide assurance of operability.

To provide full qualification of the motor operated valve actuator, environmental and seismic qualification tests were conducted to simulate the following conditions:

- A. Inside Containment (LOCA)
- B. Outside Containment
- C. Seismic Qualification
- D. Steam Line Break Accident

Mid-size valve actuators were subjected to complete environmental qualification consisting of inside containment and outside containment. Each qualification exposed the actuator to thermal and mechanical aging, radiation aging, seismic aging, environmental transient profile test, and steam line break. For the steam line break test an actuator was subjected to a very high superheated temperature to demonstrate that the electrical components of the actuator never exceeded the saturated temperature corresponding to the ambient pressure for the short duration of the test. This short term test proves the existing qualification envelopes the steam line break for superheated temperatures as high as 492°F for a few minutes.

The qualification of the mid-size valve actuator was used to generically qualify all sizes of mid-size valve actuator operators for the environmental test conditions in accordance with IEEE-382-1972. All sizes are constructed of the same materials with components designed to equivalent stress levels, and to the same clearances and tolerances with the only difference being in physical size which varies corresponding to the differences in unit rating.

All the qualifications were conducted per IEEE 382-1972 and meet the requirements of IEEE 323-1974 and IEEE 344-1975 as they apply to valve motor actuators. Further, since the actuators performed satisfactorily without maintenance throughout the various qualifications, the valve actuators are fully qualified for use in CE Nuclear Power Generating Plants.

#### 3.9.3.2.2.3.3 Pressurizer Safety Valves

Pressurizer Safety valves are 6 x 8 valves. Operability has been successfully demonstrated by a combination of dynamic testing and analysis or by static testing. Operability was successfully demonstrated with a 6g seismic load by one vendor or with a 7.1g seismic load by another vendor. Dynamic testing has demonstrated that the natural frequency of both valves was greater than 33 Hz. A summary of the test programs follows:

#### A. Vendor A Safety Valves

1. Natural Frequency Demonstration

Vibration input was in a single, horizontal direction. It was established by previous experience that the horizontal direction was more significant than the vertical direction, and that there was no material difference between teh various horizontal directions. The frequency of vibration was increased from 5 to 75 Hz at a rate of 1 octave per minute. Accelerometers were mounted on the valve assembly. The actual natural frequency under test conditions was 38 Hz.

#### 2. Operability Demonstration

A series of tests demonstrated that the valve would fully open and reseat during and after a seismic acceleration. Vibration input ranged from 3 to 6g and 10 to 33 Hz. The tests were performed using saturated steam. In addition, analysis was used to establish the significance of nozzle loading. The results indicated that deformation was significantly less than the internal clearances. This loading was therefore neglected in the seismic operability tests.

### B. Vendor B Safety Valves

### 1. Natural Frequency Demonstration

A resonance survey was performed along three orthogonal axes with one axis being the centerline of the outlet port. (Vaive mounted on inlet port.) No resonant frequencies were detected in the range of 1-50 Hz on any axis.

#### 2. Operability Demonstration

A series of tests demonstrated that the valve would fully open and reseat during and after applying the following loading combinations: Static seismic loads up to 7.1g were applied to the valve in the direction of least bending stiffness. In addition the maximum permissable piping loads were applied concurrently. The tests were performed using saturated steam. Valve operation was satisfactory.

### C. EPRI Testing of Safety Valves

One manufacturer's valve was tested in the EPRI Test Program under full pressure and full flow conditions. This testing has demonstrated that stable valve operation under these conditions is dependent upon the inlet pipe configuration, built up back pressure range and blowdown setting. Prior to plant startup the inlet pipe configuration and built up back pressure range for each specific plant will be examined by CE and the applicable valve vendor. If necessary, the valves will be adjusted to provide blowdown settings which will result in stable valve operation. These blowdown settings will be recommended by the vendor and approved by CE. These adjustments will be based on the results obtained in the EPRI Test Program. Required adjustments to the valve to assure operability will be documented in the plant specific FSAR.

3.9.3.2.2.3.4 <u>Check Valves</u>. The <u>check valves</u> are characteristically simple in design and their operation will not be affected by seismic accelerations or the maximum applied nozzle loads. The check valve design is compact and there are no extended structures or masses whose motion could cause distortions which could restrict operation of the valve. The nozzle loads due to maximum seismic excitation will not affect the functional ability of the valve since the valve disc is designed to be isolated from the casing wall. The clearance supplied by the design around the disc will prevent the disc from becoming bound or restricted due to any casing distrotions caused by nozzle load. Therefore, the design of these valves is such that once the structural integrity of the valve is assured using standard design or analysis methods, the ability of the valve to operate is assured by the design features. In addition to these design considerations, the valve will also undergo, (1) stress analysis including the SSE loads, (2) in-shop hydrostatic tests, (3) in-shop seet leakage test, and (4) periodic in-situ valve exercising and inspection to assure the functional ability of the valve.

# NSSS SEISMIC I ACTIVE VALVES

(Sheet 1 of 8)

1		LVE D.	SYSTEM NAME (safety functi		LINE	VAL		ASME SECTION III CODE CLASS	ACTUATOR TYPE
\$	SI	134	Safety Injection (Operate)	Sys.	12	Swing	Check	1	None
5	SI	143	Safety Injection (Operate)	Sys.	4	Swing	Check	1	None
5	SI	144	Safety Injection (Gperate)	Sys.	12	Swing	Check	1	None
S	SΙ	164	Safety Injection (Operate)	Sys.	10	Swing	Check	2	None
5	SI	165	Safety Injection (Operate)	Sys.	10	Swing	Check	2	None
S	SI	179	Shutdown Cooling Relief	Suction	6 x 10	Relief		2	None
S	SI	189	(Operate)		6 x 10	Relief		2	None
		215	Safety Injection (Operate)	Sys.	14 -	Swing	Check	1	None
		217	Safety Injection (Operate)	Sys.	14	Swing	Check	1	None
		225	Safety Injection (Operate)		14	Swing	Check	1	None
		227	Safety Injection (Operate)		14		Check	1	None
		235	Safety Injection (Operate)		14		Check	1	None
		237	Safety Injection (Operate)		14		Check	1	None
		245	Safety Injection (Operate)		14		Check	1.	None
		247	Safety Injection (Operate)		14		Check	1	None
		321	Safety Injection (Operate)		3	Globe		2	Motor
		322	Safety Injection (Close)		1	Globe		1	Pneumatic
		331	Safety Injection (Operate)		3	Globe		2	Motor
		332	Safety Injection (Close)		1	Globe	61	1	Pneumatic
		522 523	Safety Injection (Operate)		3		Check	1	None
		532	Safety Injection (Operate)		3	Swing		1	None
			Safety Injection (Operate)		3	Swing		1	None
3		533	Safety Injection (Operate)	sys,	3	Swing	Check	1	None

## NSSS SEISMIC I ACTIVE VALVES

(Sheet 2 of 8)

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	LVE 0.	SYSTEM NAME (safety function)	LINE	VALVE	ASME SECTION III CODE CLASS	ACTUATOR TYPE
SI	605	Safety Injection Tank Vent (Operate)	1	Globe	2	Solenoid
SI	606	Safety Injection Tank Vent (Operate)	1	Globe	2	Solenoid
SI	607	Safety Injection Tank Vent (Operate)	1	Globe	2	Solenoid
SI	608	Safety Injection Tank Vent (Operate)	1	Globe	2	Solenoid
	611	Safety Injection Tank Fill Valve (Close)	2	Globe	2	Pneumatic
	613	Safety Injection Tank Vent (Operate)	1	Globe	2	Solenoid
	614	Safety Injection Tank Isolation (Operate)	14	Gate	1	Motor
	615	LPSI Header Isolation Valve (Operate)	12	Globe	2	Motor
	616	HPSI Header Valve (Operate)	2	Globe	2	Motor
	617	HPSI Header Valve (Operate)	2	Globe	2	Motor
	618	Leakage Return to RWT (Close)	1	Globe	1	Pneumatic
	621	Safety Injection Tank Fill Valve (Close)	2	Globe	2	Pneumatic
	623	Safety Injection Tank Vent (Operate)		Globe	2	Solenoid
	624	Safety Injection Tank Isolation (Operate)	14	Gate	1	Motor
	625	LPSI Header Isolation Valve (Operate)	12	Globe	2	Motor
	626 627	HPSI Header Valve (Operate) HPSI Header Valve	2	Globe	2	Motor
	628	(Operate) Leakage Return to RWT	1	Globe	1	Pneumatic
	631	(Close) Safety Injection Tank	2	Globe	1	Pneumatic
	633	Fill Valve (Close) Safety Injection Tank	1	Globe	2	Solenoid
	634	Vent (Operate) Safety Injection Tank	14	Gate	1	Motor
	635	Isolation (Operate) LPSI Header Isolation	12	Globe	2	Motor
		Valve (Operate)				

# NSSS SEISMIC I ACTIVE VALVES

(Sheet 3 of 8)

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	LVE 0.	SYSTEM NAME (safety function)	LINE	VALVE	ASME SECTION III CODE CLASS	ACTUATOR TYPE
SI	636	HPSI Header Valve (Operate)	2	Globe	2	Motor
SI	637	HPSI Header Valve (Operate)	2	Globe	2	Motor
SI	638	Leakage Return to RWT (Close)	1	Globe	1	Pneumatic
SI	641	Safety Injection Tank Fill Valve (Close)	2	Globe	2	Pneumatic
SI	643	Safety Injection Tank Vent (Operate)	1	Globe	2	Solenoid
SI	644	Safety Injection Tank Isolacion (Operate)	14	Gate	1	Motor
SI	645	LPSI Header Isolation Valve (Operate)	12	Globe	2	Motor
SI	646	HPSI Header Valve (Operate)	2	Globe	2	Motor
SI	647	- HPSI Header Valve (Operate)	2	Globe	2	Motor
SI	648	Leakage Return to RWT (Close)	1	Globe	1	Pneumatic
SI	651	Shutdown Cooling Suction (Operate)	16	Gate	1	Motor
SI	652	Shutdown Cooling Suction (Operate)	16	Gate	1	Motor
	653	Shutdown Cooling Suction (Operate)	16	Gate	1	Motor
	654	Shutdown Cooling Suction (Operate)	16	Gate	1	Motor
	655	Shutdown Cooling Suction (Operate)	16	Gate	2	Motor
	656	Shutdown Cooling Suction (Operate)	16	Gate	2	Motor
	690	Safety Injection Sys. (Operate)	10	Globe	2	Motor
	691	Safety Injection Sys. (Operate)	10	Globe	2	Motor
	157	Safety Injection Sys. (Operate)	18	Swing Check	2	None
SI	158	Safety Injection Sys. (Jperate)	18	Swing Check	2	None

# NSSS SEISMIC I ACTIVE VALVES

(Sheet 4 of 8)

	LVE 0.	SYSTEM NAME (safety function)	LINE	VALVE	ASME SECTION III CODE CLASS	ACTUATOR TYPE
SI	200	Safety Injection Sys. (Operate)	20	Swing Check	2	None
SI	201	Safety Injection Sys. (Operate)	20	Swing Check	2	None
SI	205	Safety Injection Sys. (Operate)	24	Swing Check	2	None
SI	206	Safety Injection Sys. (Operate)	24	Swing Check	2	None
SI	306	Safety Injection Sys. (Operate)	10	Globe	2	Motor
SI	307	Shutdown Cooling Sys. (Operate)	10	Globe	2	Motor
SI	404	Safety Injection Sys. (Operate)	4	Swing Check	2	None
SI	405	Safety Injection Sys. (Operate)	4	Swing Check	2	None
SI	424	Safety Injection Sys. (Operate)	2	Lift Check	2	None
SI	426	Safety Injection Sys. (Operate)	2	-Lift Check	2	None
SI	434	Safety Injection Sys. (Operate)	10	Swing Check	2	None
SI	446	Safety Injection Sys. (Operate)	10	Swing Check	2	None
	448	Safety Injection Sys. (Operate)	2	Lift Check	2	None
	451	Safety Injection Sys. (Operate)	2	Lift Check	2	None
	484	Safety Injection Sys. (Operate)	10	Swing Check	2	None
	485	Safety Injection Sys. (Operate)	10	Swing Check	2	None
	486	Safety Injection Sys. (Operate)	2	Lift Check	2	None
	487	Safety Injection Sys. (Operate)	2	Lift Check	2	None
	604	HPSI Hot Leg Isolation (Operate)	3	Gate	2	Motor
	609	HPSI Hot Leg Isolation (Operate)	3	Gate	2	Motor
	657	Shutdown Cooling (Operate)	16	Butterfly	2	Motor
51	658	Shutdown Cooling (Operate)	16	Butterfly	2	Motor

## NSSS SEISMIC I ACTIVE VALVES

(Sheet 5 of 8)

	LVE	SYSTEM NAME (safety function)	LINE	VALVE	ASME SECTION III CODE CLASS	ACTUATOR TYPE
SI	659	Mini Flow Isolation (Operate)	4	Globe	2	Solenoid
SI	660	Mini Flow Isolation (Operate)	4	Globe	2	Solenoid
SI	664	CSP Mini Flow Isolation (Operate)	2	Globe	2	Motor
SI	665	CSP Mini Flow Isolation (Operate)		Globe	2	Motor
	666	HPSI Pump Mini Flow Isolation (Operate)	2	Globe	2	Motor
	667	HPSI Pump Mini Flow Isolation (Operate)	2	Globe	2	Motor
	668	LPSI Pump Mini Flow Isolation (Operate)	2	Globe	2	Motor
	669	LPSI Pump Mini Flow Isolation (Operate)	2 -	Globe	2	Motor
	671	Containment Spray Isola Valve (Operate)		Gate	2	Motor
	672 673	Containment Spray Isola Valve (Operate) Sump Suction Isolation	24	Gate Butterfly	2	Motor
	674	(Operate) Sump Suction Isolation	24	Butterfly	2	Motor
	675	(Operate) Sump Suction Isolation	24	Butterfly	2	Motor
	676	(Operate) Sump Suction Isolation	24	Butterfly	2	Motor
	678	(Operate) CSP Flow Control Valve	10	Butterfly	2	Motor
	679	(Operate) CSP Flow Control Valve	10	Butterfly	2	Motor
SI	682	(Operate) SIT Fill Line	2	Globe	2	Pneumatic
SI	683	(Close) LPSI Pump Suction	20	Gate	2	Motor
SI	684	(Operate) CSP Discharge (Operate)	10	Gate	2	Motor
SI	685	LPSI Discharge (Operate)	10	Gate	2	Motor
SI	686	SDCHX Discharge (Operate)	20	Gate	2	Motor
SI	687	SDCHX Discharge (Operate)	10	Gate	2	Motor

# NSSS SEISMIC I ACTIVE VALVES

(Sheet 6 of 8)

	LVE 0.		LINE	VALVE	ASME SECTION III CODE CLASS	ACTUATOR TYPE
SI	688	SDCHX Spray Bypass (Operate)	10	Gate	2	Motor
SI	689	CSP Discharge (Operate)	10	Gate	2	Motor
SI	692	LPSI Pump Suction (Operate)	20	Gate	2	Motor
SI	693	SDCHX Spray Bypass (Operate)	10	Gate	2	Motor
SI	694	LPSI Discharge (Operate)	10	Gate	2	Motor
SI	695	SDCHX Discharge (Operate)	10	Gate	2	Motor
	696	SDCHX Discharge (Operate)	20	Gate	2	Motor
	698	HPSI Pump Orifice Bypass (Operate)	4 -	Gate	2	Motor
	699	HPSI Pump Orifice Bypass (Operate)	4	Gate	2	Motor
	113	Safety Injection Sys. (Operate)	4 -	Check	1	None
	114	Safety Injection Sys. (Operate)	12	Check	1	None
	123	Safety Injection Sys. (Operate)	4	Check	1	None
	124	Safety Injection Sys. (Operate)	12	Check	1	None
	133	Safety Injection Sys. (Operate)	4	Check	1	None
	118 190	VCT Outlet Check (Operate)	4	Swing Check	2	None
	203	Gravity Feedline Check (Operate) Auxiliary Spray	3 2	Swing Check Globe	2	None
	205	(Operate) Auxiliary Spray	2	Globe		Solenoid
	240	(Operate) Charging Line Backpressure	2-1/2	Globe	,	Solenoid Pneumatic
	255	(Close) Seal Inj. Containment	1-1/2	Globe	2	Motor
	305	Isolation (Open)	20	Swing Check	2	None
	306	(Operate) RWT Suction Check	20	Swing Check	2	
		(Operate)	20	Saring Check	2	None

# NSSS SEISMIC I ACTIVE VALVES

(Sheet 7 of 8)

	LVE D.			LINE	VALVE	ASME SECTION III CODE CLASS	ACTUATOR
СН	328		Charging Line Check (Operate)	2	Lift Check	2	None
СН	331		Charging Line Check (Operate)	2	Lift Check	2	None
СН	334		Charging Line Check (Operate)	2	Lift Check	2	None
СН	431		Auxiliary Spray Check (Operate)	2	Lift Check	1	None
СН	433		Charging Line Check (Operate)	2-1/2	Lift ineck	1	None
СН	440		HPSI Header Check (Operate)	2	Lift Check	2	None
СН	494		RMW Supply Line to RDT Check (Operate)	1-1/2	Lift Check	2	None
СН	505		RCP Controlled Bleed-Off Containment Isolation	1 -	Globe	2	Pneumatic
СН	506	,	(Close)	1	Globe	2	Pneumatic
СН	515		Letdown Isolation Valve		Globe	1	Pneumatic
СН	516		(Close)	2	Globe	1	Pneumatic
СН	523			2	Globe	2	Pneumatic
СН	524		Charging Line Isolation Valve (Open)	2-1/2	Globe	2	Motor
СН	530		RWT Suction Isolation	20	Gate	2	Motor
СН	531		(Operate)	20	Gate	2	Motor
CH	560		RDT Suction Isolation (Close)	3	Globe	2	Pneumatic
CH	561		RDT Suction Isolation (Close)	3	Globe	2	Pneumatic
СН	580		RMW Supply Isclation to RDT Isc. (Close)	1-1/2	Globe	2	Pneumatic
СН	639		Charging Line Check Valve (Operate)	2-1/2	Lift Check	2	None
CH	787		Seal Injection Check (Operate)	1	Lift Check	1	None
CH	802		Seal Injection Check (Operate)	1	Lift Check	1	None
CH	807		Seal Injection Check (Operate)	1	Lift Check	1	None

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### NSSS SEISMIC ACTIVE VALVES

(Sheet 8 of 8)

	LVE 0.	SYSTEM NA (safety func		LINE	VALVE	ASME SECTION III CODE CLASS	ACTUATOR TYPE
СН	812	Seal Injection (Operate)		1	Lift Check	1	None
СН	835	Seal Injection (Operate)	Check	1-1/2	Lift Check	2	None
СН	866	Seal Injection (Operate)	Check	1	Lift Check	1	None
СН	867	Seal Injection (Operate)	Check	1	Lift Check	1	None
СН	868	Seal Injection (Operate)	Check	1	Lift Check	1	None
СН	-869	Seal Injection (Operate)	Check	1	Lift Check	1	None
RC	200	RCS (Operate)		6 x 8	Safety	1	Nche
RC	201	RCS (Operate)		6 x_8	Safety	1	None
RC	202	RCS (Operate)		6 x 8	Safety	1	· None
RC	203 .	RCS (Operate)		6 x 8	Safety	1	None
RC	244	RCS (Operate)		4	Check	1	None
IR	100	Iodine Removal (Operate)	Sys.	1	Vacuum Breaker	2	None
IR	118	Iodine Removal (Operate)	Sys.	1	Vacuum Breaker	2	None
IR	120	Iodine Removal (Operate)	Sys.	1/2	Check	2	None
IR	130	Iodine Removal (Operate)	Sys.	1/2	Check	2	None
IR	680	Iodine Removal (Operate)	Sys.	1/2	Globe	2	Solenoid
IR	681	Iodine Removal (Operate)	Sys.	1/2	Globe	2	Solenoid
IR	682	Iodine Removal (Operate)	Sys.	1/2	Globe	2	Solenoid
IR	683	Iodine Removal (Operate)	Sys.	1/2	Globe	2	Solenoid

NOTE:

- (Operate) is defined as valve being capable of both opening and closing.
- (Close) is defined as valve being capable of moving to or maintaining a closed position.

 (Open is defined as valve being capable of moving to or maintaining an open position.