OFFSITE DOSE CALCULATION MANUAL

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Commonwealth Edison Company

LA SALLE COUNTY STATION

OFFSITE DOSE CALCULATION MANUAL

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OFFSITE DOSE CALCULATION MANUAL

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1.0 INTRODUCTION

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Flow Chart for Offsite Dose Calculations

1.0 INTRODUCTION

This document provides a concise description of the environmental dose models and techniques used to calculate the offsite doses resulting from the release of radioactive material from Commonwealth Edison's nuclear power plants. A flow chart of these dose models and techniques is given in Figure 1.0-1. Documentation for both airborne (Sections 2.1 and 3.0) and aquatic pathways (Sections 2.2 and 4.0) are included.

The models consider two release modes: airborne and liquid.
Airborne releases are further subdivided into two subclasses:

(1) radioiodines, particulates, and other nonnoble gas nuclides, and (2) noble gases.

Radioiodines, Particulates, and Other Nuclides

In this model it is assumed that there is an adult and infant living in each of 16 sectors around the station. Infant exposure occurs through inhalation and any actual milk pathway. Adult exposure derives from inhalation, assumed leafy vegetable and produce pathways, and any actual milk and meat pathways. Doses to each of seven organs listed in Regulatory Guide 1.10 (bone, liver, total body, thyroid, kidney, lung, and GI-LLI) are computed from individual nuclide contributions in each of the sectors. Searching over sector and organ, the largest organ dose is compared to the 10 CFR 50, Appendix I design objectives. This dose calculation is performed monthly for infants and annually for adults. (The adult dose is computed annually to confirm the premise that the infant is the critical person. The adult will be substituted for the infant in the monthly schedule if found to be the critical person.) As necessary, the release rates of these nuclides will be converted to dose rates for comparison to the limits of 10 CFR 20.

Noble Gases

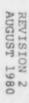
Exposure to the beta and gamma radiations of the noble gases will result in a whole body and skin dose. The maximum whole body and skin doses for each offsite sector are determined from the individual nuclide contributions and the maximum dose values are compared to the 10 CFR 50, Appendix I design objectives. This calculation is performed monthly. As necessary, the noble gas release rate will be converted to dose rates for comparison to the limits of 10 CFR 20.

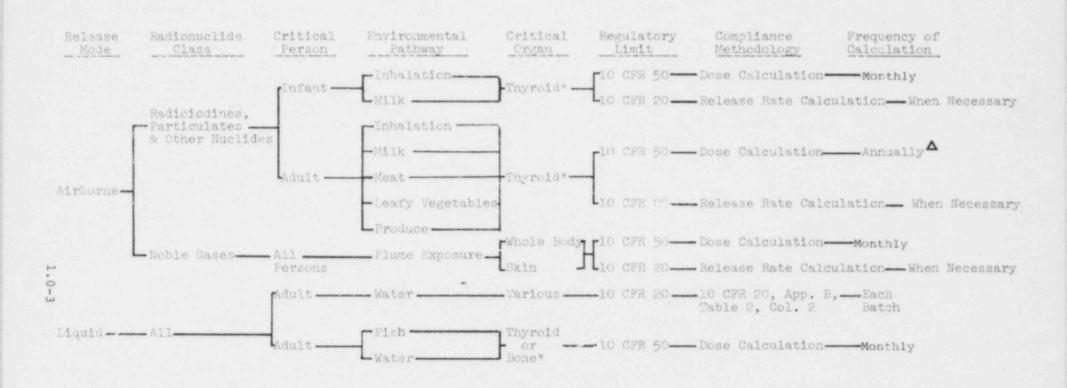
For liquid releases it is assumed that liquid effluents discharged into a river undergo mixing prior to consumption as either potable water or fish by adults. For releases to Lake Michigan a finite plume dilution factor is computed for the potable water pathway and a hypothetical river model is created for the fish pathway. Doses to the seven critical organs are determined from individual nuclide contributions and the largest organ dose is compared to the 10 CFR 50 design objectives. Compliance with the 10 CFR 20 maximum permissible concentrations is done on a batch-by-batch basis prior to discharge.

Compliance with the various regulatory limits for offsite doses is demonstrated with the techniques of Section 5.0.

All site independent data used in the calculations are given in Section 7.1. Site specific data are given in Section 7.2.

The models and techniques used to establish the alarm and trip setpoints of the gaseous and liquid effluent monitors are described in Section 8.0.





^{*} Most likely "ritical organ; however, dose is computed for 7 organs.

[△] The computation of dose to the adult is performed annually to confirm the premise that the infant is the critical person.

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2.0 OFFSITE DOSE LIMITS

2.1 AIRBORNE RELEASES

2.1.1 Noble Gases

2.1.1.1 10 CFR 50, Appendix I Design Objectives

2.1.1.1.1 Air Dose

The average air dose in unrestricted areas due to noble gases released in gaseous effluents from each reactor shall be limited to the following expressions:

2.1.1.1.1.1 Gamma Air Dose

2.1.1.1.1.1 Gamma Air Dose, Calendar Quarter

$$3.17 \times 10^{-8} \sum_{i} \left[s_{i} A_{is} + v_{i} A_{iv} + G_{i} A_{ig} \right] \leq 5 \text{ mrad}$$
 (2.1)

 3.17×10^{-8} Conversion Constant (years/second) Converts seconds to years.

Si Gamma Dose Constant, (mrad/yr per pci/sec)

The gamma ray air dose constant for each identified noble gas radionuclide released from a stack (Tables 7.2-8 or 7.2-11). The constant is evaluated for a finite plume using the methods explained in Subsection 3.3.1.2.

A_{is} Accumulative Radionuclide (μCi) Release, Stack Release

The accumulative release of radionuclide i from a stack. Releases shall be cumulative

over the calendar quarter or year (four consecutive quarters) as appropriate.

Vi

Gamma Dose Constant, Vent Release (mrad/yr per µCi/sec)

The gamma ray air dose constant for each identified noble gas radionuclide released from a vent (Tables 7.2-8 or 7.2-11). The plume may be elevated part of the time as determined by the criteria of Regulatory Guide 1.111 (Reference 6.4), part C.2.b. The constant is evaluated for a finite plume using the method explained in Subsection 3.3.1.2.

Aiv

Accumulative Radionuclide (µCi) Release, Vent Release

The accumulative release of radionuclide i from a vent. Releases shall be cumulative over the calendar quarter or year (four consecutive quarters) as appropriate.

Gi

Gamma Dose Constant, Ground Level Release (mrad/yr per µCi/sec)

The gamma ray air dose constant for each identified noble gas radionuclide released from a ground level release point (Tables 7.2-8 or 7.2-11). The constant is evaluated for a finite plume using the method explained in Subsection 3.3.1.2.

Aig

Accumulative Radionuclide (µCi)
Release, Ground Level Release

The accumulative release of radionuclide i from a ground level release point. Releases

shall be cumulative over the calendar quarter or year (four consecutive quarters) as appropriate.

2.1.1.1.1.2 Gamma Air Dose, Calendar Year (Four Consecutive Quarters)

$$3.17 \times 10^{-8} \sum_{i} \left[s_{i} A_{is} + V_{i} A_{iv} + G_{i} A_{ig} \right] \leq 10 \text{ mrad}$$
(2.2)

2.1.1.1.1.2 Beta Air Dose

2.1.1.1.2.1 Beta Air Dose, Calendar Quarter

$$3.17 \times 10^{-8} \sum_{i} L_{i} \left[(X/Q)_{s} A_{is}^{i} + (X/Q)_{v} A_{iv}^{i} + (X/Q)_{g} A_{ig}^{i} \right]$$

$$\leq 10 \text{ mrad}$$
(2.3)

L_i Beta Air Dose Constant (mrad/yr per μCi/m³)

The air dose factor due to beta emissions for each identified noble gas radionuclide (Table 7.1-13).

(X/Q)_S Relative Effluent (sec/m³)
Concentration, Stack Release

The highest calculated annual average relative concentration in a given direction at or beyond the restricted area boundary for stack releases (Table 7.2-6 or Table 7.2-9).

A'is Accumulative Radionuclide (μCi)
Release from Stack,
Adjusted for Radiodecay

The accumulative release of radionuclide i from a stack, adjusted to account for radiodecay in transit.

$$A_{is}' = A_{is} \times exp (-\lambda_i R/3600 u_s)$$
 (2.3a)

Ai Radiological Decay (hr⁻¹)
Constant
The radiological decay constant for radionuclide i. See Tables 7.1-9 and 7.1-11.

R Downwind Range (m)

The distance downwind to the point of interest. See Tables 7.2-6, 7.2-7, and 7.2-8.

3600 Constant (sec/hr)
Converts hours to seconds

us Average Wind Speed (m/sec)

The average wind speed for a stack release. See Table 7.2-6.

(X/Q) Relative Effluent (sec/m³)
Concentration, Vent Release

The highest calculated annual average relative concentration in a given direction at or beyond the restricted area boundary for vent releases. The partially elevated plume model of Regulatory Guide 1.111, part C.2.b

(Reference 6.4) is used when necessary. See Subsection 3.2.2.3 and Table 7.2-6 or Table 7.2-9.

Aiv

Accumulative Radionuclide (µCi)
Release from Vent, Adjusted
for Radiodecay

The accumulative release of radionuclide i from a vent, adjusted for radiodecay in transit.

$$A'_{iv} = A_{iv} \times \exp(-\lambda_i R/3600 u_v)$$
 (2.3b)

u_v Average Wind Speed (m/sec)

The average wind speed for a vent release. See Table 7.2-6.

(X/Q)_g Relative Effluent (sec/m³) Concentration, Ground Level Release

The highest calculated annual average relative concentration in a given direction at or beyond the restricted area boundary for ground level releases. (See Table 7.2-6 or Table 7.2-9.)

Aig

Accumulative Radionuclide (µCi)
Release at Ground Level,
Adjusted for Radiodecay

The accumulative release of radionuclide i from ground level, adjusted for radiodecay in transit.

$$A'_{ig} = A_{ig} \times \exp(-\lambda_i R/3600 u_g)$$
 (2.3c)

ug Average Wind Speed (m/sec)

The average wind speed for a ground level release. See Table 7.2-6.

2.1.1.1.2.2 Beta Air Dose, Calendar Year (Four Consecutive Quarters)

3.17 x 10⁻⁸
$$\sum_{i} L_{i} \left[(X/Q)_{s} A'_{is} + (X/Q)_{v} A'_{iv} + (X/Q)_{g} A'_{ig} \right]$$

$$\leq 20 \text{ mrad} \qquad (2.4)$$

2.1.1.1.2 Whole Body Dose

The average dose to individuals in unrestricted areas due to noble gases released in gaseous effluents from each reactor shall be limited to the following expressions:

2.1.1.1.2.1 Whole Body Dose, Calendar Quarter

(0.7) (1.11) (3.17 x 10⁻⁸)
$$\sum_{i} \left[\overline{s}_{i} A_{is} + \overline{v}_{i} A_{iv} + \overline{G}_{i} A_{ig} \right]$$

$$\leq 2.5 \text{ mrem}$$
(2.5)

- O.7 Shielding and Occupancy Factor

 The shielding and occupancy factor for protection against gamma radiation.
- 1.11 Conversion Constant (mrem/mrad)
 Converts rads in air to rems in tissue.
- \overline{S}_i Gamma Whole Body Dose (mrad/yr per Constant, Stack Release $\mu \text{Ci/sec}$) \overline{S}_i is the constant S_i multiplied by the shielding factor afforded by 5 cm of tissue; used to evaluate whole body dose. (See Subsection 3.3.1.2; also, see Tables 7.2-8 or 7.2-11.)

 \overline{v}_{i}

Gamma Whole Body Dose Constant, Vent Release

(mrad/yr per µCi/sec)

The constant V_i multiplied by the shielding factor afforded by 5 cm of tissue; used to evaluate whole body dose. (See Subsection 3.3.1.2; also, see Tables 7.2-8 or 7.2-11.)

G,

Gamma Whole Body Dose (mrad/yr per Constant, Ground Level Release µCi/sec)

The constant G_i multiplied by the shielding factor afforded by 5 cm of tissue; used to evaluate whole body dose. (See Subsection 3.3.1.2; also, see Tables 7.2-8 or 7.2-11.)

2.1.1.1.2.2 Whole Body Dose, Calendar Year (Four Consecutive Quarters)

(0.7) (1.11) (3.17 x 10⁻⁸)
$$\sum_{i} \left[\overline{s}_{i} A_{is} + \overline{v}_{i} A_{iv} + \overline{G}_{i} A_{ig} \right] \le 5 \text{ mrem}$$
 (2.6)

2.1.1.1.3 Skin Dose

The average skin dose to individuals in unrestricted areas due to noble gas released in gaseous effluents from each reactor shall be limited to the following expressions:

2.1.1.3.1 Skin Dose, Calendar Quarter

$$3.17 \times 10^{-8} \sum_{i} \left[1.0 \ \overline{L}_{i} \left((X/Q)_{s} \ A'_{is} + (X/Q)_{v} \ A'_{iv} + (X/Q)_{g} \ A'_{ig} \right) + (0.7) (1.11) (S_{i} \ A_{is} + V_{i} \ A_{iv} + G_{i} \ A_{ig}) \right] \leq 7.5 \text{ mrem}$$

$$(2.7)$$

- 1.0 Shielding and Occupancy Factor

 The shielding and occupancy factor for protection against beta radiation.
- \overline{L}_i Beta Skin Dose Constant (mrem/yr per $\mu \text{Ci/m}^3$)

 The skin dose factor due to beta emissions for each identified noble gas radionuclide (Table 7.1-13). Accounts for attenuation of beta radiation during passage through 7 mg/cm² of dead skin.

2.1.1.3.2 Skin Dose, Calendar Year (Four Consecutive Quarters)

$$3.17 \times 10^{-8} \sum_{i} \left[1.0 \ \overline{L}_{i} \left((\chi/Q)_{s} \ A'_{is} + (\chi/Q)_{v} \ A'_{iv} + (\chi/Q)_{g} A'_{ig} \right) + (0.7) (1.11) (S_{i} \ A_{is} + V_{i} \ A_{iv} + G_{i} \ A_{ig}) \right] \leq 15 \text{ mrem}$$

$$(2.8)$$

2.1.1.2 10 CFR 20 Release Rate Limits

The maximum dose rate to individuals in unrestricted areas due to noble gases released in gaseous effluents from the site shall be limited to the following expressions:

2.1.1.2.1 Whole Body Dose Rate

1.11 x
$$\sum_{i}$$
 $\left[\overline{s}_{i} Q_{is} + \overline{V}_{i} Q_{iv} + \overline{G}_{i} Q_{ig}\right] < 500 \text{ mrem/yr}$
(10 CFR 20.105 limit)

 Q_{is} Release Rate, Stack Release ($\mu\text{Ci/sec}$)

The release rate for radionuclide i due to a stack release.

Q_{iv} Release Rate, Vent Release (μCi/sec)

The release rate for radionuclide i due to a vent release.

Q_{ig} Release Rate, Ground Level (μCi/sec) Release

The release rate for radionuclide i due to a ground level release.

2.1.1.2.2 Skin Dose Rate

$$\sum_{i} \left[\overline{L}_{i} \left((X/Q)_{s} Q'_{is} + (X/Q)_{v} Q'_{iv} + (X/Q)_{g} Q'_{ig} \right) + (X/Q)_{s} Q'_{is} + V_{i} Q_{iv} + G_{i} Q_{ig} \right] \le 3000 \text{ mrem/yr}$$

(10 CFR 20.105 limit)

(2.10)

Q'is Release Rate, Stack Release, (μCi/sec)
Adjusted for Radiodecay

The release rate for radionuclide i from a stack adjusted for radiodecay in transit.

$$Q'_{is} = Q_{is} \times \exp(-\lambda_i R/3600 u_s)$$
 (2.10a)

Q'iv Release Rate, Vent Release, (μCi/sec)
Adjusted for Radiodecay

The release rate for radionuclide i from a vent, adjusted for radiodecay in transit.

$$Q'_{iv} = Q_{iv} \times \exp(-\lambda_i R/3600 u_v)$$
 (2.10b)

Q'ig Release Rate, Ground Level, (μCi/sec)
Adjusted for Radiodecay

The release rate for radionuclide i from ground level, adjusted for radiodecay in transit.

$$Q'_{ig} = Q_{ig} \times \exp(-\lambda_i R/3600 u_g)$$
 (2.10c)

2.1.2 Radioiodines, "Particulates", and Other (Nonnoble Gas) Radionuclides

2.1.2.1 10 CFR 50, Appendix I Design Objectives

The average dose to an individual in the unrestricted area from radioiodines, radioactive materials in particulate form, and radionuclides other than noble gases in gaseous effluents released from each reactor with half-lives greater than 8 days, shall be limited to the following expressions:

2.1.2.1.1 Inhalation + Food Pathways Dose, Calendar Quarter

$$3.17 \times 10^{-8} \times 10^{6} R_{a} \sum_{i} DFA_{ija} \left[(\chi/Q)_{s} A_{is}' + (\chi/Q)_{v} A_{iv}' + (\chi/Q)_{g} A_{ig}' \right] + \frac{t_{r}}{365} \sum_{i} DFI_{ija} \left[U_{a}^{P} f_{p} C_{i}^{P} + U_{a}^{M} C_{i}^{M} + U_{a}^{V} C_{i}^{M} + U_{a}^{V} C_{i}^{F} \right] \leq 7.5 \text{ mrem}$$

$$(2.11)$$

10⁶ Conversion Constant (pCi/μCi) Converts μCi to pCi.

1 365 Conversion Constant (yrs/day) Converts days to years.

 R_a Individual Air Intake Rate (m^3/yr) The air intake rate for individuals in group a. See Tables 7.1-2 and 7.1-3.

tr Deposition Time or Release (days)
Period
Length of time for deposition.

DFA
ija Inhalation Dose Factor (mrem/pCi)

The inhalation dose commitment factor for radionuclide i. organ i. and age group a.

radionuclide i, organ j, and age group a. See Table 7.1-1.

(X/Q) See Table 7.2-6 or Table 7.2-9.

(X/Q), See Table 7.2-6 or Table 7.2-9.

(X/Q) See Table 7.2-6 or Table 7.2-9.

See Table 7.1-1.

DFI ija Ingestion Dose Factor (mrem/pCi)

The ingestion dose commitment factor for radionuclide i, organ j, and age group a.

 \mathbf{U}_{a}^{P} , \mathbf{U}_{a}^{M} , \mathbf{U}_{a}^{V} , \mathbf{U}_{a}^{F} Foodstuff Consumption Rates (kg/yr, liters/yr, kg/yr, kg/yr, respectively)

The annual consumption rates (usages) of produce (nonleafy vegetables, fruits, and grain); milk; leafy vegetables; and meat (flesh), respectively, for individuals in age group a. See Tables 7.1-2 and 7.1-3.

 f_p , f_V Produce, Leafy Vegetable Fractions

The respective fractions of the ingested produce and leafy vegetables that are grown in the garden of interest; dimensionless. See Table 7.1-2.

 c_i^P , c_i^M , c_i^V , c_i^F Foodstuff Concentrations (pCi/kg, pCi/liter, pCi/kg, pCi/kg, respectively)

The average concentrations of radionuclide i in produce (nonleafy vegetables, fruits, and grain); milk; leafy vegetables; and meat (flesh), respectively. C_{i}^{p} and C_{i}^{V} are calculated from Equation 2.12 below.

C_i Concentration in Vegetation (pCi/kg)

The concentration of radionuclide i in vegetation.

$$C_{i} = d_{i} \times r \frac{\left[1 - \exp\left(-\lambda_{Ei} t_{e}\right)\right]}{Y_{v} \lambda_{Ei}} \exp\left(-\lambda_{i} t_{h}\right) \times f_{f}$$
(2.12)

 d_i Deposition Rate (pCi/m^2-hr) The deposition rate of radionuclide i onto the ground.

$$d_{i} = \frac{10^{6}}{24 \times t_{r}} \begin{bmatrix} A'_{is} (D/Q)_{s} + A'_{iv} (D/Q)_{v} + A'_{ig} (D/Q)_{g} \end{bmatrix}$$

$$A'_{ig} (D/Q)_{g}$$
(2.13)

Converts days to hours.

(D/Q)_s Relative Deposition (m⁻²)
Factor, Stack Release

The calculated annual average relative deposition factor in a given direction at or beyond the restricted area boundary for stack releases. (See Subsection 3.2.3.3; see Table 7.2-6 or Table 7.2-9 for

produce and leafy vegetable pathways; and see Table 7.2-7 or Table 7.2-10 for milk and meat pathways.)

 (D/Q_v) Relative Deposition (m^{-2}) Factor, Vent Release

The calculated annual average relative deposition factor in a given direction at or beyond the restricted area boundary for vent releases. The partially elevated plume model of Regulatory Guide 1.111, part C.2.b is used. (See Subsection 3.2.3.3; see Table 7.2-6 or Table 7.2-9 for produce and leafy vegetable pathways; and see Table 7.2-7 or Table 7.2-10 for milk and meat pathways.)

(D/Q)_g Relative Deposition (m⁻²) Factor, Ground Level Release

The calculated annual average relative deposition factor in a given direction at or beyond the restricted area boundary for ground level releases. (See Subsection 3.2.3.3; see Table 7.2-6 or Table 7.2-9 for produce and leafy vegetable pathways; and see Table 7.2-7 or Table 7.2-10 for milk and meat pathways.

- The fraction of deposited activity retained on crops; dimensionless; see Tables 7.1-2 and 7.1-3.
- Effective Decay Constant (hr⁻¹)

 The effective removal rate constant for radionuclide i from crops.

 $\lambda_{Ei} = \lambda_i + \lambda_w$ (2.13a)

- Weathering Decay Constant (hr⁻¹)
 The removal constant for physical loss by weathering. See Tables
 7.1-2 and 7.1-3.
- te Effective Crop Exposure Time (hr)

 The effective crop exposure time. See Tables
 7.1-2 and 7.1-3.
 - th Harvest to Consumption Time (hr)

 The time between harvest and consumption.

 See Tables 7.1-2 and 7.1-3.
 - f Seasonal Growing Factor
 A factor which accounts for seasonal growth of vegetation. See Tables 7.1-2 and 7.1-3.
 - y_v Productivity Yield (kg/m²)

 The agricultural productivity yield. See
 Tables 7.1-2 and 7.1-3.

C^M Milk Concentration

(pCi/liter)

The concentration of radionuclide i in milk.

c^M is calculated from the following equation
 (after Regulatory Guide 1.109 [Reference 6.5]):

$$C_{i}^{M} = F_{M} C_{i}^{f} W_{f} \exp \left(-\frac{\lambda_{i} t_{M}}{M}\right)$$
 (2.14)

F_M Milk Fraction

(days/liter)

The average fraction of the animal's daily intake of radionuclide i which appears in each liter of milk. See Table 7.1-4.

Cf Feed Concentration

(pCi/kg)

The average concentration of radionuclide i in animal feed.

For milk and meat pathways, the following expression is to be used (after Regulatory Guide 1.109, [Reference 6.5]):

$$C_{i}^{f} = f_{f} f_{g} C_{i}^{g} + (1-f_{f}) C_{i}^{s} + f_{f} (1-f_{g}) C_{i}^{s}$$
 (2.15)

fg Pasture Grass Fraction

The fraction of daily feed that is pasture grass when the animal grazes on the pasture. See Tables 7.1-2 and 7.1-3.

Ci Pasture Grass Concentration

(pCi/kg)

The concentration of radionuclide i is pasture grass (calculated using Equation 2.12 for c_i with f_f = 1; other parameters, including f_f for use in Equation 2.15, are given in Tables 7.1-2 and 7.1-3).

Cs Stored Feed
Concentration

(pCi/kg)

The concentration of radionuclide i in stored feed (calculated using Equation 2.12 for C_i with f_f = 1; other parameters, including f_f for use in Equation 2.15, are given in Tables 7.1-2 and 7.1-3.

- W_f Feed Consumption (kg/day)
 The amount of feed consumed by the
 animal each day. See Tables 7.1-2
 and 7.1-3.
- The average time from the production of milk to its consumption. See Tables 7.1-2 and 7.1-3.
- C_i^F Meat Concentration (pCi/kg) The concentration of radionuclide i in meat.

$$C_i^F = F_F C_i^f W_f \exp(-\lambda_i t_s)$$
 (2.16)

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(days/kg)

F_F Meat Fraction

The fraction of the animal's daily intake of radionuclide i which appears in each kilogram of flesh. See Table 7.1-4.

The time from slaughter consumption,
See Table 7.1-2.

2.1.2.1.2 <u>Inhalation + Food Pathways Dose, Calendar Year</u> (Four Consecutive Quarters)

3.17 x
$$10^{-8}$$
 x 10^{6} R_a \sum_{i} DFA_{ija} $\left[(\chi/Q)_{s} A_{is}' + (\chi/Q)_{v} A_{iv}' + (\chi/Q) A_{ig}' \right] +$

$$\frac{t_{r}}{365} \sum_{i} DFI_{ija} \left[u_{a}^{P} f_{p} C_{i}^{P} + u_{a}^{M} C_{i}^{M} + u_{a}^{V} f_{V} C_{i}^{V} + u_{a}^{F} C_{i}^{F} \right] \leq 15 mrem$$
(2.17)

2.1.2.2 10 CFR 20 Release Rate Limit

The maximum dose rate to an organ of an infant from all radionuclides, radioactive materials in particulate form, and radionuclides other than noble gases with half-lives greater than 8 days shall be limited to the values given by the equations which follow. For purposes of demonstrating compliance with the Technical Specifications, the dose to the infant shall be considered limiting.

$$10^6 R_a \sum_{i} DFA_{ija} \left[(\chi/Q)_s Q'_{is} + (\chi/Q)_v Q'_{iv} + (\chi/Q)_g Q'_{ig} \right] +$$

$$K\sum_{i} DFI_{ija} U_{a}^{M} C_{i}^{M} < 1500 mrem/yr$$

(2.18)

K Seasonal Adjustment Factor

K is a seasonal adjustment factor to account for nongrazing during the winter and partial grazing during the summer; K = 0 for November to April and 0.5 for May to October.

- C_i^M Milk Concentration (pCi/liter)

 The concentration of radionuclide i in milk. $C_i^M = F_M C_i^f W_f \exp(-\lambda_i t_M)$ (2.19)
- C_i^f Feed Concentration (pCi/kg)

 The concentration of radionuclide i in feed.

$$C_i^f = d_i \times r \left[1 - \exp\left(-\lambda_{Ei} t_e\right)\right]$$
 (2.20)

(Note that this assumes feed to be 100% pasture grass.)

d_i Deposition Rate
$$(pCi/m^2 \times hr)$$

$$d_i = 3600 \times 10^6 \times \left[Q'_{is} (D/Q)_s + Q'_{iv} (D/Q)_v + Q'_{ig} (D/Q)_g\right] \qquad (2.21)$$

- $(D/Q)_S$ See Table 7.2-7 or Table 7.2-10 for milk pathway.
- (D/Q) See Table 7.2-7 or Table 7.2-10 for milk pathway.
- $(D/Q)_g$ See Table 7.2-7 or Table 7.2-10 for milk pathway.

2.1.3 Symbols Used In Section 2.1

SYM	BOL	NAME	Ī	NIT	
si		Gamma Dose Constant, Stack Release	(mrad/yr	per	μCi/sec)
Ais		Accemulative Radionuclide Release			
15		Stack Release	(µCi)		
Vi		Gamma Dose Constant, Vent Release	(mrad/yr	per	μCi/sec)
Aiv		Accumulative Radionuclide Release,			
		Vent Release	(µCi)		
Gi		Gamma Dose Constant, Ground			
		Level Release	(mrad/yr	per	μCi/sec)
Aig		Accumulative Radionuclide Release,			
		Ground Level Release	(µCi)		2
Li		Beta Dose Constant	(mrad/yr	per	μCi/m³)
(X/		Relative Effluent Concentration,	2		
,		Stack Release	(sec/m^3)		
A'is		Accumulative Radionuclide Release			
		from Stack, Adjusted for Radiodecay	(µCi)		
(X/	(Q) _V	Relative Effluent Concentration,	3		
,		Vent Release	(sec/m^3)		
Aiv		Accumulative Radionuclide Release			
		from Vent, Adjusted for Radiodecay	(µCi)		
-(x/	(Q) _g	Relative Effluent Concentration,	3		
1		Ground Level Release	(sec/m^3)		
A'ig		Accumulative Radionuclide Release			
		from Ground Level, Adjusted for	(µCi)		
		Radiodecay			
R		Downwind Range	(m)		
' "v'	ug	Average Wind Speed, Stack, Vent, or			
-		Ground Level Release	(m/sec)		
Si		Gamma Whole Body Dose Constant			
		Stack Release	(mrad/yr	per	μCi/sec)
Vi		Gamma Whole 5 7 0 e Constant,	1	-13	.01 ()
-		Vent Release	(mrad/yr	per	μCi/sec)
Gi		Gamma Whole Body Dose Constant,	1		01/
-		Ground Level Release			μCi/sec)
Li		Beta Skin Dose Constant	(mrem/yr	per	DCI/M)

SYMBOL	NAME	UNIT
Q _{is}	Release Rate, Stack Release	(µCi/sec)
Qiv	Release Rate, Vent Release	(µCi/sec)
Qig	Release Rate, Ground Level Release	(µCi/sec)
Q'is	Release Rate from Stack,	
	Adjusted for Radiodecay	(µCi/sec)
Qiv	Release Rate from Vent,	(µCi/sec)
,	Adjusted for Radiodecay	
Q'ig	Release Rate at Ground Level,	
	Adjusted for Radiodecay	(µCi/sec)
Ra	Individual Air Intake Rate	(m ³ /yr)
DFA	Inhalation Dose Factor	(mrem/pCi)
DFI	Ingestion Dose Factor	(mrem/pCi)
r	Deposition Time	(day)
U a	Produce Consumption Rate	(kg/yr)
U _a ^M	Milk Consumption Rate	(liters/yr)
tr Va Wa Va Va Va Va	Leafy Vegetable Consumption Rate	(kg/yr)
ua F	Meat Consumption Rate	(kg/yr)
fp	Produce Fraction	
f _V	Leafy Vegetable Fraction	
c _i ^P	Produce Concentration	(pCi/kg)
c ^M _i c ^V _i c ^F _i	Milk Concentration	(pCi/liter)
c ^V _i	Leafy Vegetable Concentration	(pCi/kg)
c _i ^F	Meat Concentration	(pCi/kg)
ďi	Deposition Rate	(pCi/m ² .hr)
Ci	Vegetation Concentration	(pCi/kg)
(D/Q) _S	Relative Deposition Factor, Stack Release	(m^{-2})
(D/Q),	Relative Deposition Factor, Vent	(m^{-2})
V	Release	(11)
(D/Q) _g	Relative Deposition Factor, Ground Level Release	(m^{-2})

SYMBOL	NAME	UNIT
r	Crop Retention Fraction	
λ _{Ei}	Effective Decay Constant	(hr ⁻¹)
λi	Radiological Decay Constant	(hr ⁻¹)
λ _w	Weathering Decay Constant	(hr ⁻¹)
t _e	Effective Crop Exposure Time	(hr)
th	Harvest to Consumption Time	(hr)
	Productivity Yield	(kg/m^2)
F _M	Milk Fraction	(days/liter)
Y _v F _M C _i	Feed Concentration	(pCi/kg)
f	Seasonal Growing Factor	
fg	Pasture Grass Fraction	
f _g c _i c _i	Pasture Grass Concentration	(pCi/kg)
cis	Stored Feed Concentration	(pCi/kg)
Wf	Feed Consumption	(kg/day)
t _M	Milk Transport Time	(hr)
FF	Meat Fraction	(day/kg)
ts	Slaughter to Consumption Time	(hr)
K	Seasonal Adjustment Factor	

2.1.4 Constants Used In Section 2.1

NUMERICAL VALUE	NAME	UNIT
3.17 x 10 ⁻⁸	Conversion Constant	(years/second)
0.7	Gamma Radiation Shielding	
	and Occupancy Factor	
1.0	Beta Radiation Shielding	
	and Occupancy Factor	
1.11	Conversion Constant	(mrem/mrad)
10 ⁶	Conversion Constant	(pCi/µCi)
24	Conversion Constant	(hr/day)
365	Conversion Constant	(day/yr)
3600	Conversion Constant	(sec/hr)

2.2 RADIOACTIVITY IN LIQUID RELEASES

2.2.1 10 CFR 50, Appendix I Design Objectives

The dose contributions from measured quantities of radioactive materials identified in liquid effluents released to unrestricted areas from each reactor shall be calculated using the following expression:

$$D_{j} = (1.1 \times 10^{-3} \times 8760) \left[\frac{U^{W}M^{W}}{F^{W}} \sum_{i} A_{i} DFI_{ija} exp (-\lambda_{i} t^{W}) + \right]$$

$$\frac{U^{f}M^{f}}{F^{f}} \sum_{i} A_{i} DFI_{ija} B_{i} exp \left(-\lambda_{i} t^{f}\right)$$
(2.22)

D; Cumulative dose (mrem)

The cumulative dose or dose commitment to the total body or an organ j due to an adult consuming water and fish.

U^w, U^f Usage Factor (liters/hr, kg/hr)

Average consumption rate of water or fish.

See Table 7.2-1.

- 1/M^W, 1/M^f Additional Dilution Factor
 Additional dilution factor prior to withdrawal
 of potable water or fish. See Table 7.2-1.
 - FW Average Flow Rate (ft³/sec)

 Average flow of receiving body of water. See
 Table 7.2-1.
 - Ff Near-Field Flow Rate (ft³/sec)
 Near-field flow of receiving body of water.
 See Table 7.2-1.
 - A_i Total Radionuclide Release (µCi)

 Total release of radionuclide i during period of release.
 - DFI
 ija Ingestion Dose Factor (mrem/pCi)
 The ingestion dose commitment factor for each identified gamma and beta emitter i, organ j, and age group a. See Table 7.1-1.
 - λ_{i} Decay Constant (hr⁻¹)

 Radiological decay constant of ith radionuclide.

 See Table 7.1-11.
 - tw, tf Elapsed Time (hr)

 Average elapsed time between release and consumption of potable water or fish. See Table 7.2-1.

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Bioaccumulation Factor (liters/kg)
Bioaccumulation factor. See Table 7.1-12.

1.1 x 10^{-3} = factor to convert from $(\mu \text{Ci/yr})/(\text{ft}^3/\text{sec})$ to pCi/liters

8760 = number of hours per year

2.2.2 10 CFR 20 Maximum Permissible Concentrations in the Unrestricted Area

The concentration of nonnoble gas radioactive material released from the site to unrestricted areas (C_i) shall be limited to the concentrations specified in 10 CFR 2C, Appendix B, Table II, Column 2 (MPC_i). The concentrations of dissolved or entrained noble gases shall be limited to the concentrations specified in Table 7.1-10. The sum of the fractional limits (\sum_{i} [C_i \div MPC_i]) must not exceed 1.0 for each release.

The concentration of each radionuclide in the unrestricted area is calculated as follows:

$$C_{i} = C_{i}^{t} \times \frac{F^{r}}{F^{d} + F^{r}}$$
 (2.27)

and the combination of C_i^t , F^r , and F^d must meet the condition that:

$$100 \times \sum_{i} \frac{C_{i}}{MPC_{i}} = 100 \times \frac{F^{r}}{F^{d} + F^{r}} \times \sum_{i} \frac{C_{i}^{t}}{MPC_{i}} \leq 100\%$$
 (2.28)

 C_i Concentration in the Unrestricted (μ Ci/ml) Area

The concentration of radionuclide i at the restricted/unrestricted area boundary.

- Ct Concentration in the Discharge Tank (µCi/ml)
 The concentration of radionuclide i in the (radwaste discharge or other similar) tank.
- F^r Flow Rate, Radwaste Discharge (ft³/sec)
 The flow rate of radwaste from the discharge tank to the initial dilution stream.
- Fd Flow Rate, Initial Dilution Stream (ft³/sec)

 The flow rate of the initial dilution stream which carries the radionuclides to the unrestricted area boundary (e.g., the blowdown from cooling tower or lake or the circulating cooling water flow).
- MPC_i Maximum Permissible Concentration (μCi/ml)

 The maximum permissible concentration of radionuclide i in water in the unrestricted area (from 10 CFR 20, Appendix B, Table II, Column 2 or Table 7.1-10).

2.2.3 10 CFR 20 Maximum Permissible Concentrations at the Nearest Surface Water Supply

The quantity of radionuclides, excluding tritium and dissolved or entrained noble gases, in outdoor tanks without overflow pipes connected to other storage tanks shall be limited to ensure that in the case of an overflow, the annual average concentration of radioactivity in the potable water of the nearest surface water supply is less than the 10 CFR 20, Appendix B, Table II, Column 2 limits.

The annual average concentration of each radionuclide in the potable water of the nearest surface water supply is calculated as follows:

$$C_{i}^{W} = C_{i}^{t} \left(\frac{F^{t}}{F_{O}^{W} + F^{t}} \right) M_{O}^{W} \exp \left(-\lambda_{i} \times t_{O}^{W} \right) \times \frac{t_{O}}{8760}$$
 (2.29)

- C_i Concentration in Water Supply (µCi/ml)

 The annual average concentration of radionuclide i in the surface water supply due to tank overflow.
- Ci Concentration in Tank (µCi/ml)

 The concentration of radionuclide i
 in the outdoor tank of interest.
- The maximum rate of overflow from the outdoor tank of interest (usually equal to the maximum tank feed rate). See
- Fo Flow Rate, Receiving Body of Water (ft³/sec)

 The minimum flow rate (from the most recent 10 year record) of the receiving body of water during overflow conditions.

 See Table 7.2-1.
- 1/M_O Additional Dilution Factor
 Additional dilution factor of overflowed
 water prior to use as potable water.
 See Table 7.2-1.
 - The total time between overflow release and consumption of water, equal to the transit time, discharge point to intake, plus the process time at the water treatment plant. See Table 7.2-1.

(hr)

Release Time

The total period of the overflow conditions, assumed to be no greater than one work shift of 8 hours.

Hence the maximum quantity of radionuclide i (Ai, curie) in each tank of interest, excluding tritium and the dissolved or entrained noble gases, which satisfies the limiting condition:

$$\sum_{i} \frac{C_{i}^{W}}{MPC_{i}} \leq 1 \tag{2.30}$$

is:

$$\sum_{i} \frac{\Lambda_{i}^{t}}{MPC_{i}} \exp \left(-\frac{\lambda_{i}}{i} \times t_{O}^{w}\right) \leq 4 \left(\frac{F_{O}^{w} + F^{t}}{F^{t}}\right) \frac{V^{t}}{M_{O}^{w}}$$
 (2.31)

At Tank Radioactivity (Ci)

The quantity of radionuclide i in the tank of interest.

V^t Tank Volume (gal)

The volume of each tank without overflow pipes connected to other storage tanks.

See Table 7.2-1.

Equation 2.31 may also be written in terms of the concentration of radionuclide i in the tank of interest.

$$\sum_{i} \frac{c_{i}^{t}}{MPC_{i}} \exp \left(-\frac{\lambda_{i}}{x} \times t_{O}^{w}\right) \leq \left(\frac{F_{O}^{w} + F^{t}}{F^{t}}\right) \frac{1100}{M_{O}^{w}} \tag{2.32}$$

Derivation of Equation 2.31

Since, by Equation 2.30,

$$\sum_{i} \frac{c_{i}^{w}}{MPC_{i}} \leq 1$$

where C_i^{W} is given by Equation 2.29 and C_i^{t} in Equation 2.29 is given by:

$$C_{i}^{t} = \frac{A_{i}^{t} \times 10^{6} \, \mu \text{Ci/Ci}}{v^{t} \times 3785 \, \text{ml/gal}}$$
 (2.33)

then:

$$\sum_{i} \frac{C_{i}^{w}}{MPC_{i}} = \sum_{i} \frac{C_{i}^{t}}{MPC_{i}} \left(\frac{F^{t}}{F_{O}^{w} + F^{t}} \right) M_{O}^{w} t_{O} / 8760 \exp \left(-\frac{\lambda}{i} t_{O}^{w} \right) \leq 1$$
(2.34)

$$= \left(\frac{F^{t}}{F_{O}^{w} + F^{t}}\right) \left(\frac{M_{O}^{w}}{V^{t}}\right) \frac{8}{8760} \times \frac{10^{6}}{3785} \sum_{i} \frac{A_{i}^{t}}{MPC_{i}} exp \left(-\lambda_{i} t_{O}^{w}\right) < 1$$

(2.35)

$$= \frac{1}{4} \left(\frac{F^{t}}{F_{O}^{w} + F^{t}} \right) \left(\frac{M_{O}^{w}}{V^{t}} \right) = \sum_{i} \frac{A_{i}^{t}}{MPC_{i}} = \exp \left(-\lambda_{i} t_{O}^{w} \right) \leq 1$$
(2.36)

Equation 2.36 on rearrangement gives:

$$\sum_{i} \frac{A_{i}^{t}}{MPC_{i}} \exp \left(-\frac{\lambda_{i}}{i} t_{O}^{w}\right) \leq 4 \left(\frac{F_{O}^{w} + F^{t}}{F^{t}}\right) \left(\frac{V^{t}}{M_{O}^{w}}\right)$$
(2.37)

2.2.4 Symbols Used In Section 2.2

SYMBOL	NAME	UNIT
Dj	Cumulative Dose	(mrem)
uw,uf	Usage Factor	(liters/hr, kg/hr)
1/M ^w ,1/M ^f ,1/M ^w	Additional Dilution Factor	
FW	Average Flow Rate	(ft ³ /sec)
F ^f	Near-Field Flow Rate	(ft ³ /sec)
Ai	Total Radionuclide Release	(µCi)
DFI _{ija}	Ingestion Dose Factor	(mrem/pCi)
$^{\lambda}$ i	Decay Constant	(hr ⁻¹)
cW,tf,tw	Elapsed Time	(hr)
Bi	Bioaccumulation Factor	(liters/kg)
ci	Concentration at Unre-	
	stricted Area	(µCi/ml)
c ^t i	Concentration in Discharge	
	Tank	(UCi/ml)
Fr	Flow Rate, Radwaste	
화기하는 연극	Discharge	(ft ³ /sec)
Fd	Flow Rate, Initial	
	Dilution Stream	(ft ³ /sec)
MPCi	Maximum Permissible	
	Concentration	(µCi/ml)
c _i ^w	Concentration in Water	
	Supply	(uCi/ml)
F ^t	Maximum Tank Overflow Rate	(ft ³ /sec)
F _O	Minimum Flow Rate, Receiving	
	Body of Water	(ft ³ /sec)
to	Release Time	(hr)
t _o A ^t vt	Tank Radioactivity	(Ci)
V ^t	Tank Volume	(gal)

2.2.5 Constants Used In Section 2.2

NUMERICAL VALUE	NAME	UNIT
1.1 x 10 ⁻³	Conversion Factor	(pCi/liter)/ [(µCi/yr)/(ft ³ /sec)]
8760	Conversion Factor	(hrs/yr)
106	Conversion Constant	(pCi/μCi)

2.3 ENVIRONMENTAL STANDARDS FOR THE URANIUM FUEL CYCLE

In accordance with the requirements of 40 CFR 190 (Reference 6.12), the annual dose commitment to any member of the public in the general environment (i.e., the unrestricted area) from all uranium fuel cycle sources, except those specifically excluded by the regulation, is limited to 25 millirems to the whole body, 25 millirems to any organ but the thyroid, and 75 millirems to the thyroid. On the basis of results projected by the NRC for all multi-unit sites presently committed, the conservative nature of the design dose calculations as opposed to the applicability of these standards to exposures actually received, and the operational flexibility available to sites with multiple units, it is concluded that the standards can be readily achieved at all CECo sites by demonstrating compliance with 10 CFR 50 Appendix I objectives.

2.3.1 Sources of Radiation and Radioactivity

2.3.1.1 Uranium Fuel Cycle - Definition

The uranium fuel cycle is defined in 40 CFR 190 (Reference 6.12) to include:

- a. operations of milling of uranium ore,
- b. chemical conversion of uranium,
- c. isotopic enrichment of uranium,
- d. fabrication of uranium fuel,
- e. generation of electricity by a nuclear power plant using uranium fuel, and
- f. reprocessing of spent uranium fuel.

Specifically excluded are:

- a. mining operations,
- b. operations at waste disposal sites,
- c. transportation of ra' pactive material, and

d. the use of recovered nonuranium special nuclear or by-product materials from the cycle.

2.3.1.2 Radiological Impact of Uranium Fuel Cycle Operation

Environmental Radiation Protection Standards, 40 CFR 190, require that the radiation dose resulting from all operations of the uranium fuel cycle (except the specific exclusions noted) be considered in determining compliance. Therefore, each of the operations will be discussed and the radiological impact in the Commonwealth Edison Company (CECo) service area will be considered.

2.3.1.2.1 Milling

Reference 6.13 (Page 4), Reference 6.14 (Section 2.4), and Reference 6.15 (Page IV F-29) indicate that the maximum individual doses due to milling will be less than 10 CFR 20 limits. Therefore, the dose contribution to any person living in this service area due to milling operations, all more than 100 kilometers distant, is expected to be negligible compared to 40 CFR 190 limits.

2.3.1.2.2 Conversion

Reference 6.14 (Section 3.4) and Reference 6.15 (Page IV F-40 and Table IV F-10) indicate that the maximum individual doses due to UF $_6$ conversion will be less than 10 CFR 20 limits. Therefore, the dose contribution to any person living in this service area due to UF $_6$ conversion operations, all more than 100 kilometers distant, is expected to be negligible compared to 40 CFR 190 limits.

2.3.1.2.3 Enrichment

Reference 6.14 (Section 4.4) and Reference 6.15 (Page IV F-51) indicate that the maximum individual doses due to uranium

enrichment will be less than 10 CFR 20 limits. Therefore, the dose contribution to any person living in this service area due to uranium enrichment operations, all more than 100 kilometers distant, is expected to be negligible compared to 40 CFR 190 limits.

2.3.1.2.4 Fabrication

Reference 6.14 (Section 5.4) and Reference 6.15 (Page IV F-63) indicate that the maximum individual doses due to fuel element fabrication will be less than 10 CFR 20 limits. Therefore, the dose contribution to any person living in this service area due to fuel fabrication operations, all more than 100 kilometers distant, is expected to be negligible compared to 40 CFR 190 limits.

2.3.1.2.5 Generation of Electricity

The generation of electricity, using a nuclear power plant, results in radioactivity released in gaseous and liquid effluents. The radiological impact of these requires assessment (using the methodology of Sections 2.1 and 2.2 of this report) and comparison with 40 CFR 190 limits.

Also, boiling water reactors (BWR's) contain radioactive nitrogen-16 (N-16) in their steamlines and turbines in sufficient enough quantities to result in measurable offsite doses. The magnitude of this so-called skyshine dose must also be considered in determining 40 CFR 190 compliance. Offsite doses due to other contained sources in the nuclear power plant are negligible compared to those due to effluents and N-16 skyshine.

Measurements of the radiation environment due to N-16 have been made at the Dresden Station (Reference 6.19). An empirical fit to the measured data is given in Equation 2.38:

 $D(R,P) = SF OF (2.28 \times 10^{-5}) P exp (-0.007 R)$ (2.38)

D(R,P) Dose Due to N-16

(mrem)

Skyshine

The gamma dose due to BWR N-16

skyshine.

SF

Shielding Factor

The shielding factor for protection

against gamma radiation.

SF = 0.7 for a home.

OF

Occupancy Factor

The at-home occupancy factor:

For fisherman 0.95

For all others 1.0

 2.28×10^{-5}

Constant

(mrem/MWe-hr)

A constant to fit the equation to measured

data.

P

Electric Power Generated (MWe-hr)

The total electric energy generated in the

time period of interest.

0.007

Constant

 (m^{-1})

A constant to fit the equation to

measured data.

R

Distance

(m)

Distance from the turbine to the dose point

of interest.

This equation will be used at all CECo BWR's up to a distance of 1100 meters. Beyond that distance the fit (and data) are considered unreliable and, further, the dose at this range is, at most, 0.1 mrem/yr for CECo Stations.

In certain situations, more than one nuclear power plant site may contribute to a radiological dose to be considered in making 40 CFR 190 dose assessment. At present (July 1979), the nuclear power stations in CECo's service area are sufficiently distant from one another that the radiological dose, if not negligible compared to 40 CFR 190 limits, is due to only one site. Hence, adding dose components from several stations is not required.

However, within CECo's service area the following future additive combination is considered. At some point within the triangle formed by the La Salle, Dresden, and Braidwood Stations, an additive dose from airborne releases may be postulated. However, the distances are such (La Salle to Dresden, 39 kilometers; Dresden to Braidwood, 18 kilometers; Braidwood to La Salle, 37 kilometers) that at any intermediate point postulated, the station-combined dose is less than that maximum calculated for an individual station. Therefore, the combined effect of airborne releases will not be considered further.

Such is not the case for future releases of radioactivity into the aquatic environment, where, if more than one facility uses the same receiving body of water, the station-combined dose must be considered. Dresden and (the future) La Salle County Stations discharge their liquid waste into the Illinois River and (the future) Braidwood Station discharges into the Kankakee River which flows into the Illinois at Dresden. Quad Cities and (the future) Carroll County Stations use the Mississippi River and (the future) Byron Station uses the Rock River which flows into the Mississippi at Moline, Illinois, downstream of Quad Cities. For these two situations the combined impact from upstream liquid waste discharges must be considered at each downstream location.

The dose contribution of nuclear power plants in other service areas need not be considered in CECo's 40 CFR 190 assessment. The Duane Arnold Station is about 135 kilometers from Quad Cities; the Clinton Station is about 125 kilometers from Braidwood and La Salle; and the Bailly Station is about 100 kilometers from Dresden.

2.3.1.2.6 Reprocessing

Reference 6.15 (Table IV E-12) indicates that maximum individual doses due to fuel reprocessing will be less than 10 CFR 20 limits. Therefore, the dose contribution to any person living in this service area due to fuel reprocessing operations, all more than 100 kilometers distant, is expected to be negligible compared to 40 CFR 190 limits.

2.3.1.2.7 Waste Disposal Sites

The radiation dose associated with the burial of low level radioactive radwaste need not be considered in determining compliance with 40 CFR 190 as this source is specifically excluded by the law. Inasmuch as the licensed burial facility at Sheffield, Illinois, is near CECo's service area, at least a comment regarding it as a potential source is warranted.

The radiological impact of burial sites is discussed briefly in Chapter IV, Section H, Part 3.1.2.1 of Reference 6.15 (Page IV H-28 ff). No significant movement of radioactivity into the general environment is expected, though some tritium has been found in groundwater near the Sheffield facility. However, no significant dose contribution to a person living in the vicinity of CECo's nuclear power plants is expected. (The Quad Cities Station is about 60 kilometers from Sheffield; Byron and La Salle are each about 90 kilometers from Sheffield.)

2.3.1.2.8 Transportation

The radiation dose associated with the transport of low level radioactive waste and spent fuel is also excluded from consideration by the requirements of 40 CFR 190. This subject has been reviewed in References 6.16 and 6.17, and summarized again in Reference 6.15 (Chapter IV, Section G). The expected dose associated with transportation is 3.4×10^{-3} mrem/person/reactor/year.

2.3.1.2.9 Storage of Spent Fuel in Offsite Facilities

The radiation doses associated with releases of radioactivity by independent spent fuel storage facilities (ISFSF) should also be considered in determining compliance with 40 CFR 190. One ISFSF is being operated within CECo's service area; that is, General Electric Company's Morris Operations Plant at Morris, Illinois, adjacent to CECo's Dresden Station. Minute quantities of Kr-85 and other radioactive particulates are released in airborne effluents. A dose assessment was performed using typical release data provided by the General Electric Company and the Offsite Dose Calculation Manual (ODCM) environmental dose assessment models for Dresden. (The effluent is released through a 300-foot vent stack; hence the similarity between the two facilities. However, no adjustments were made for differences in site boundary ranges or ranges to dairies. These differences are not expected to affect the conclusion from the dose assessment.)

The estimated annual airborne releases from the GE Morris Operation plant are 6 x 10 4 µCi of tritium, <55 x 10 6 µCi of Kr-85, 3 µCi of Co-60, and 1 µCi of Cs-137. The maximum whole body dose from these radionuclides is 4 x 10 $^{-4}$ mrem/yr. So long as this plant remains a spent fuel storage facility and does not reprocess the fuel the dose contribution to any person living in its vicinity will be negligible and not considered further in the Dresden 40 CFR 190 analysis.

2.3.1.2.10 Long-Term Storage of High Level Radioactive Wastes

The dose associated with the long-term storage of high level radioactive wastes is excluded from consideration as far as 40 CFR 190 is concerned. The radiological impact is discussed in Reference 6.15 (Chapter IV, Section H, Part 3.2) and should be negligible in the CECo service area.

2.3.1.3 Summary

The magnitude of radiological dose due to various operations of the uranium fuel cycle and its impact in the Commonwealth Edison Company service area has been reviewed with respect to the requirements of 40 CFR 190. The only dose components requiring consideration are those due to:

- radioactivity in nuclear power plant liquid and gaseous effluents, and
- b. the direct radiation due N-16 in BWR steam piping, turbines, and associated equipment.

2.3.2 Numerical Models

2.3.2.1 Airborne Releases and Direct Radiation

2.3.2.1.1 Whole Body Dose

The maximum whole body (WB) dose from airborne releases and direct radiation will be determined by adding, for each sector, the dose contributions, if applicable, from all (1) noble gases; (2) airborne radioiodines, "particulates", and other nonnoble gas radionuclides with half-lives greater than 8 days; (3) direct radiation from BWR turbine N-16 skyshine as computed at the nearest actual residence in each sector

(Table 7.2-4); and at Dresden only, the contribution from (4) noble gases, and (5) airborne "particulates" from the Morris Operations plant if spent fuel is reprocessed.

At Zion, sectors whose site boundary is over Lake Michigan will not be considered in the 40 CFR 190 analysis.

At Dresden and Quad Cities, Equations 2.39 and 2.40, respectively, will be used to compute the direct radiation dose in sectors whose restricted area boundary is over water. This dose, which accounts for possible fishing activities in the vicinity, will then be added to the nearest residence dose computed with Equation 2.38 using an at-home occupancy factor of 0.95 rather than the usual 1.0. An occupancy factor of 0.05 is used for fishermen (0.025 at each of two locations at Quad Cities) and a boat shielding factor of 1.0.

At Dresden:

$$D(R,P) = (1.0)(0.05) 2.28 \times 10^{-5} \sum_{i=1}^{3} P_i \exp(-0.007 \times R_i)$$
(2.39)

$$R_1 = 488 \text{ m}$$

 R_2 , $R_3 = 610 \text{ m}$

P_i Electric power generated (MWe-hr) by each unit in the year

At Quad Cities:

$$D(R,P) = (1.0)(0.025) 2.28 \times 10^{-5} P \left[exp (-0.007 R_1) + exp (-0.007 R_2) \right]$$
 (2.40)

$$R_1 = 100 \text{ m}$$

 $R_2 = 400 \text{ m}$

P Electric power generated (MWe-hr)
by the station

Table 2.3-1 shows the methodology for determining the maximum whole body dose from airborne releases and direct radiation.

2.3.2.1.2 Thyroid Dose

The maximum thyroid dose from airborne releases and direct radiation will be determined by adding, for each sector, the dose contributions from the various sources in a manner similar to that for the maximum whole body dose, as described above and in Table 2.3-1.

2.3.2.1.3 Any Other Organ Dose

In this class, the dose from airborne releases and direct radiation to the GI-LLI, bone, liver, kidney, lung, and skin will be determined separately in each sector, and the maximum value chosen to represent "any other organ" (AOO) for purposes of determining compliance. The maximum AOO dose will be determined in a manner similar to that for the maximum whole body dose, as described in Subsection 2.3.2.1.1 and in Table 2.3-1.

2.3.2.2 Radioactivity in Liquid Releases

The maximum whole body, thyroid, and AOO doses from radioactivity in individual station liquid releases will be determined using, for the fish pathway, the near-field estimate of dilution at the station; and using, for the drinking water pathway, the average flow of the receiving body of water at the nearest downstream community water system, if the water system is near the station. Otherwise, the drinking water pathway will not be considered. For situations involving combined-station releases, for the fish pathway, for releases from all upstream CECo facilities, the tissue doses will be determined using the average flow of the receiving body of water at the station. Table 2.3-1 shows the methodology for determining these doses.

2.3.3 Symbols Used in Section 2.3

SYMBOL	NAME	UNIT
D(R,P)	Dose Due to N-16 Skyshine	(mrem)
SF	Shielding Factor	
OF	Occupancy Factor	
P, P _i	Electric Power Generated by Station or Unit	(MWe-hr)
R	Distance	(m)

2.3.4 Constants Used in Section 2.3

NUMERICAL VALUE	NAME	UNIT
2.28 x 10 ⁻⁵	Fitted Constant	(mrem/MWe-hr)
0.007	Fitted Constant	(m^{-1})
0.7	Shielding Factor at Home	
1.0	Shielding Factor on a Boat	
0.05	Occupancy Factor While Fishing	
0.95	Occupancy Factor at Home for Fishermen	
1.0	Occupancy Factor at Home for Everyone but Fishermen	

TABLE 2.3-1

NUMERICAL MODELS FOR COMPUTING RADIATION DOSE FROM URANIUM FUEL CYCLE OPERATIONS^a

FUEL CYCLE	CL	ASSIFICATION	WHOLE				ANY OT	HER ORGA	N		FOOT-
OPERATION	OF	RADIATION	BODY	THYROID	GI-LLI	BONE	LIVER	KIDNEY	LUNG	SKIN	NOTES
REACTORS											
	1.	Noble Gases	Equation 2.5	Equation 2.5		- Е	Quation	2.5 —		Equation 2.7	
	2.	Airborne Iodine and Particulates	Equation 2.11			E	Equation	2.11—		Equation 2.11 WB Component	b
	3.	Liquid Waste	Equation 2.22	Equation 2.22		E	Equation	2.22 —		Equation 2.22 WB Component	С
	4.	Direct Radiation	Equation 2.38	Equation 2.38		E	Quation	2.38 —		Equation 2.38	đ
FUEL STORAGE	E FAC	CILITY									
	5.	Noble Gases	N/A	N/A		N	lot Appl	icable		N/A	е
	6.	Airborne Particulates	N/A	N/A		N	ot Appl	icable		N/A	е

a. The maximum sector doses for the whole body, thyroid, and any other organ, summed over all classifications of radiation, will be added to similar tissue doses received from radioactivity in liquid releases, or combined-station releases, if applicable. The maximum dose of each tissue class will be compared to the limits established in 40 CFR 190.10(a).

- b. The dose to all organs will be determined first with Equation 2.11 then adjusted through multiplication by a factor $0.5/fg \le 1$ where fg is given in Table 7.1-2.
- c. Only the fish pathway portion of Equation 2.22 will be used unless the community water system is near the station. For combined aquatic pathway doses from more than one station the dose from each upstream CECo station will be determined with Equation 2.22, using M^W/F^W instead of M^f/F^f at the individual station.
- d. Except for special considerations of fishermen at Dresden and Quad Cities, direct radiation from BWR turbine N-16 will be computed at the nearest actual resident in each sector and not at the site boundary. A shielding and occupancy factor of 0.7 will be used.
- e. So long as this plant remains a spent fuel storage facility and does not reprocess the fuel, its contribution to the total dose will not be considered further.

3.0 ATMOSPHERIC TRANSPORT, DIFFUSION, AND DOSE MODELS

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3.0 ATMOSPHERIC TRANSPORT, DIFFUSION, AND DOSE MODELS

3.1 METEOROLOGICAL DATA FOR MODELS

3.1.1 Current Record

Onsite meteorological data are used as input to all of the airborne dose calculations performed by a contractor. The data are obtained by means of an instrumented meteorological tower that measures wind speed and wind direction at several levels. The stability of the atmosphere is determined by means of the temperature lapse rate (differential temperature) between two levels on the tower. The contractor's analyses are used to supplement dose analyses performed with historical meteorological records.

For elevated releases, a joint frequency table (stability wind rose) of wind speed, wind direction, and stability is developed using the upper level wind data and the average lapse rate measured on the tower.

The mixed-mode model for vent stack releases requires two stability wind roses: one to represent the elevated part of the release and one to represent the ground level portion of the release.

These are developed jointly by considering the wind data hour by hour. The criteria for deciding how to proportion each hour's data between a vent release and ground level release depend on the ratio of the exit speed to the wind speed. When the criteria (Subsection 3.2.2.2) indicate part of the release should be considered as ground level, the 10-meter wind data are used.

For ground level releases, the stability wind rose is developed using the lower level wind data and lapse rate.

The wind direction, wind speed, and atmospheric stability classification schemes are described in Tables 7.1-5 and 7.1-8. Because the dispersion equations are very sensitive to low wind speeds, the hourly record may require editing to reflect the measuring limitations of the wind sensors at low speeds. If the reported wind speed is less than the anemometer's threshold (Table 7.1-6), it is assigned a value equal to one-half of threshold speed. If the reported speed is less than the vane's threshold (calm), Table 7.1-6, a direction is assigned in proportion to the observed wind direction distribution of the lowest noncalm speed class.

Diffusion estimates for monthly, calendar quarter, or annual releases are determined by combining hourly stability and wind data in the form of stability wind rose tables. Wind speed, direction, and stability classifications are used to group the data and calculate the joint occurrences of the groups.

3.1.2 Historical Record

Nuclear station operators will use the dispersion factors of Section 7.2 to demonstrate compliance with the Technical Specifications. Depending on the station, there may be three classes (elevated, mixed mode, and ground level) of effluent release, each with four types of dispersion factors: (1) X/Q, (2) D/Q, (3) S_{i} , V_{i} , or G_{i} , and (4) $\overline{\text{S}_{i}}$, $\overline{\text{V}_{i}}$, or $\overline{\text{G}_{i}}$, where i = 1 to 15 which are wind direction dependent. The first two types of dispersion factors are used with the internal dose models; (X/Q) and the last two types are used with the external dose models.

3.1.2.1 Internal Dose

The recipient of the internal dose can either be an adult

or an infant. If the recipient is an adult, the internal dose can consist of contributions from inhalation (X/Q), leafy vegetables or produce (D/Q), and milk or meat (D/Q). If the recipient is an infant, the total dose consists of contributions from inhalation (X/Q) and milk (D/Q). The dispersion factors for inhalation and leafy vegetable doses are calculated for the 16 wind directions. The dispersion factors for the milk cows and meat animals are only calculated for the direction(s) where these animals are located in the unrestricted area and at a distance no greater than 5 miles.

Historical dispersion factors used in the internal dose models are found in Section 7.2. There is a set of these tables for each station. Section 7.2 contains the dispersion factors for the three possible classes of release and the 16 wind directions for which χ/Q (inhalation) and D/Q (leafy vegetables or produce) are calculated. The radius specifies the location at which the dose is calculated. Only maximum χ/Q and D/Q values are used.

Also in Section 7.2 are the dispersion factors used to calculate the doses resulting from milk and meat consumption. Entries occur only for those directions where the nearby milk cows and meat animals are located.

The internal dose models are:

- 1. adult inhalation;
- 2. adult consuming leafy vegetables;
- 3. adult consuming produce;
- 4. adult consuming meat;
- 5. adult drinking milk;
- any combination of 1, 2, 3, 4, and 5;
- 7. infant inhalation;
- 8. infant drinking milk; and
- 9. sum of 7 and 8.

3.1.2.2 External Dose

The wind direction dispersion factors used in the whole body and gamma air external dose models are found in Section 7.2. For each station, the 15 tables correspond to the 15 radionuclides used to determine total external dose, which is the sum of the dose contributions from each radionuclide. The whole body $(\overline{S}_i, \overline{V}_i, \text{ or } \overline{G}_i)$ and gamma air $(S_i, V_i, \text{ or } G_i)$ dose factors are computed for each of the 16 wind directions and each release class.

The dose factors for beta skin dose (\overline{L}_i) and beta air dose (L_i) , two other types of external dose, are constants which do not vary with wind direction. However, they are combined in the dose models with χ/Q factors, which are wind direction dependent.

3.2 ATMOSPHERIC TRANSPORT AND DIFFUSION MODELS

3.2.1 Numerical Model

The model used is classed as a "constant mean wind direction model" by the NRC. Equation 3.1 shows how the concentration to emission ratio (χ/Q) at any downwind range and direction is calculated.

$$\frac{\chi(R,\theta)}{Q} = \frac{2.032}{R} \sum_{u} \sum_{s} f(u,\theta,s) (uS_{z})^{-1} exp \left[-\frac{1}{2} \left(\frac{h_{e}}{S_{z}} \right)^{2} \right]$$
(3.1)

This model assumes that the effluent is uniformally distributed within each downwind sector and that the release rate is constant during the time period modeled.

- X/Q Relative Effluent Concentration (\sec/m^3)
 The relative concentration within the cloud at point (R, θ).
- R Downwind Range (m)The distance downwind to point (R,θ) .
- θ Direction (degree or sector) The downwind direction to point (R,θ) .
- u Wind Speed (m/sec)
 The wind speed.
- s Stability Class
 The atmospheric stability class.

f Joint Frequency.

The observed frequency in which the wind blows with speed u, downwind direction θ , and atmospheric stability class s.

- S_Z Corrected Vertical Dispersion (m)
 Coefficient

 The vertical dispersion coefficient,
 corrected for building wake effects.
- h_e Effective Stack Height (m)
 The effective height at which effluent is released.

3.2.2 Source Configuration Considerations

The location of the source with respect to the buildings affects how the airborne effluent will disperse. The following describes the criteria used to model airborne releases from nuclear power plants and describes how the model evaluates each case.

3.2.2.1 Elevated Releases

Release locations (chimneys, etc.) that are high enough to be out of the range of the effects caused by neighboring solid structures are classified as elevated releases. The concentrations at any range and direction can be calculated by Equation 3.1 when an appropriate value for the effective stack height $(h_{\rm e})$ is used to represent the height of the plume centerline above the ground.

The effective stack height is calculated by the following equation:

$$h_e = h_s + h_r - h_t$$
 (3.2)

- h_s Physical Stack Height (m)

 The actual height of the stack above grade elevation.
- ${\rm h}_{\rm r}$ Plume Rise (m) The additional rise of the plume due to its bouyancy and/or momentum.
- h_t Terrain Correction Factor (m)

 The elevation to account for ground points of interest being different than grade elevation near the stack.

This equation states that the effective stack height (h_e) is equal to the physical stack height (h_s) plus the plume rise due to buoyancy and momentum (h_r) less a correction for the variation in terrain (h_t).

3.2.2.1.1 Plume Rise (hr)

The rise of an effluent plume is dependent on the stability of the atmosphere, the wind speed, the heat content of the plume, and the exit velocity of the plume. The procedure chosen has been selected to provide a conservative (low) estimate of the plume rise in order to maximize the resulting calculated doses.

Under neutral and unstable atmospheric conditions the momentum-dominated plume rise equations are used. Equation 3.3 shows the basic relationship between $\mathbf{h}_{\mathbf{r}}$ and other parameters.

$$(h_r)_1 = 1.44d (W_0/u)^{2/3} (R/d)^{1/3} - C$$
 (3.3)

W_o Exit Velocity (m/sec)

The effluent stream velocity at the discharge point.

- d Stack Diameter (m)

 The diameter of the stack at the discharge point.
- C Downwash Correction Factor (m)

 The factor to account for stack downwash under certain atmospheric conditions.

Equation 3.3 would allow the plume to continue rising forever which is contrary to observation. In order to limit the rise, Equation 3.4 is evaluated and the lesser of Equations 3.3 and 3.4 is used in the calculations.

$$(h_r)_2 = 3 (W_0/u)d$$
 (3.4)

Therefore, h_r can be represented by the following formula for neutral and unstable conditions:

$$h_r = Min [(h_r)_1, (h_r)_2]$$
 (3.5)

Under stable atmospheric conditions, additional calculations are made as follows:

$$(h_r)_3 = 4 (F/S)^{\frac{1}{4}}$$
 (3.6)

$$(h_r)_4 = 1.5 (F/u)^{1/3} s^{-1/6}$$
 (3.7)

F Momentum Flux Parameter (m⁴/sec²)

$$F = W_C^2 (d/2)^2$$
 (3.8)

S Stability Parameter (\sec^{-2}) See following table.

Table of Values for Stability Parameter (S) (Sec-2)

Stability Class	S			
E	8.7×10^{-4}			
F	1.75×10^{-3}			
G	2.45×10^{-3}			

The smaller value computed from Equations 3.6 and 3.7 is compared to the value obtained from Equation 3.5 and the smallest value is used to represent h_r under stable conditions. In other words,

$$h_r - Min \left[(h_r)_1, (h_r)_2, (h_r)_3, (h_r)_4 \right]$$
 (3.9)

3.2.2.1.2 Terrain Correction (ht)

The topography of each site and immediate environs is characterized as relatively flat, little or no slope, and, with the exception of Zion, rural farmland. Zion terrain is comprised of marshy depressions and sandy ridges. Site-specific terrain correction factors, determined in the manner described below and used in the model to describe the offsite receptor points for each station, may be found in Table 7.2-5 of the site-specific data tables.

The average difference in elevation H_{rs} is computed for the point to be evaluated by subtracting the height of the terrain (H_s) at the release point from the height of the terrain at the receptor point (H_r) . The correction factor, h_t , is computed by Equaitons 3.10 and 3.11.

$$H_{rs} = H_r - H_s$$
 (3.10)

$$h_{t} = \begin{cases} H_{rs}; H_{rs} > 0 \\ 0 ; H_{rs} \le 0 \end{cases}$$
 (3.11)

H_{rs} Terrain Height Difference (m) Net difference between grade elevation of source and receiver locations.

- H_r Terrain Height At Reseptor Point (m) Grade elevation at the point of interest.
- H_S Terrain Height At Source (m)
 Grade elevation at the release.

3.2.2.1.3 Downwash Correction (C)

If the ratio of the exit velocity to the wind speed is less than 1.5, the effluent can get caught in the downwash of the stack and the plume rise would be inhibited. This reduction is accounted for by the term (C) in Equation 3.3 and this term is computed by Equation 3.12.

$$C = 3(1.5 - W_0/u)d$$
 (3.12)

3.2.2.2 Vent Stack Releases

The constant mean wind direction model has been modified into a "mixed-mode" model. In a mixed ode model the height of the release is proportioned between an elevated release (stack height equal to the vent height plus momentum plume rise), and a ground level release (stack height equal to zero). Separate wind and stability data are used for each release height and the XQ ratios are calculated. Subsection 3.1.1 describes how the meteorological data are prepared for this calculation. This model is recommended by Regulatory Guide 1.111.

The fraction of the time that the plume is considered to be a ground level release $(G_{\mathbf{t}})$ is determined, from the ratio of the exit velocity of the vent $(\mathbf{W}_{\mathbf{0}})$ to the wind speed (\mathbf{u}) , by the use of the following relationships:

$$G_{t} = \begin{cases} 1.00 & ; W_{o}/u & 1.0 \\ 2.58-1.58 & (W_{o}/u) & ; 1.0 & W_{o}/u & 1.5 \\ 0.3-0.06 & (W_{o}/u) & ; 1.5 & W_{o}/u & 5.0 \\ 0.00 & ; W_{o}/u & 5.0 & (3.13) \end{cases}$$

Ground Release Fraction

Fraction of time a vent release is considered a ground level release.

Therefore, the release can be considered as a ground level release $100G_{\rm t}$ percent of the time and as an elevated release $100(1-G_{\rm t})$ percent of the time.

3.2.2.3 Ground Level Releases

To calculate the downwind concentrations resulting from ground level releases, Equation 3.1 is used with the effective stack height set to zero $(h_e=0)$. If the release is from a structure of maximum height (D_z) , a correction is made to the dispersion parameter to account for the increased mixing caused by the building's wake effect. Equation 3.14 shows how this is accounted for in the model.

$$S_{z} = \begin{cases} \sigma_{z} & \text{; no wake effect} \\ \sigma_{z}^{2} + D_{z}^{2} / (2\pi) \end{cases}$$
; wake effect (3.14)

- The vertical dispersion coefficient (m)

 The vertical dispersion coefficient for use in atmospheric dispersion models. See Table 7.1-7.
- D_z Maximum Height Of Neighboring Structure (m)

 The maximum height of any neighboring structure causing downwind building wake effects.

When the wake effect is used the factor $\mathbf{S}_{\mathbf{Z}}$ will be restricted by the condition:

$$S_{z} \leq \sqrt{3} \sigma_{z} \tag{3.25}$$

3.2.3 Removal Mechanism Considerations

3.2.3.1 Radioactive Decay

The loss of activity with time, due to radioactive decay, is accounted for by adjusting the source term. This adjustment

takes the following form:

$$Q_i' = Q_i \exp(-\lambda_i t) = Q_i \exp(-\lambda_i R/3600u)$$
 (3.16)

- Q_{1}^{\prime} Corrected Release Rate ($\mu Ci/sec$)

 The release rate of radionuclide i corrected for radiodecay in transit.
- $Q_{\dot{1}}$ Release Rate ($\mu Ci/sec$) The release rate of radionuclide i.
- λ_i Radiodecay Constant (hr⁻¹)

 The radioactive decay constant for nuclide i.

 See Table 7.1-9.
- t Transport Time (hr)

 The time required to travel a distance R downwind.
- 3600 Conversion Constant (sec/hr)
 Converts hours to seconds.

3.2.3.2 Plume Depletion and Deposition

As the plume travels downwind, the radioiodines and particulate material are deposited on the ground and thus removed from the plume. At all ranges (R) the model accounts for this depletion by multiplying the (X/Q) ratios by a fraction that is a function of release height and stability.

$$(X/Q) = (X/Q)_{Q} P_{d}(h_{e}, s)$$
 (3.17)

P_d Plume depletion coefficient

The function P_d recommended by the NRC (Regulatory Guide 1.111, Figures 2-5) is given in Section 7.1, Figures 7.1-1 to 7.1-4.

The plume depletion factors for the height closest to the actual release height are used.

3.2.3.3 Relative Deposition Factor (D/Q)

The value of D/Q is determined from one of the following equations:

$$D/Q = \frac{1}{R} \frac{16}{2\pi} D_r(s, R, h_s)$$
 (3.18)

$$D/Q = \frac{1}{R} \frac{16}{2\pi} \sum_{s} f(\theta, s) D_{r}(s, R, h_{s})$$
 (3.19)

- D/Q Relative Deposition Factor (m^{-2}) The calculated relative deposition factor in a given direction.
- D_r Relative Deposition Rate (m^{-1}) The relative deposition rate is the deposition rate per unit downwind distance $(\mu \text{Ci s}^{-1} \text{ m}^{-1})$ divided by the source strength $(\mu \text{Ci s}^{-1})$

For time periods Δt < 8 hours, Equation 3.18 is used. For time period Δt > 8 hours, when the meteorological data are in the form of a stability wind rose, Equation 3.19 is used.

The values of D_r from Regulatory Guide 1.111, Figures 6-9, are reproduced in Section 7.1 as Figures 7.1-5 to 7.1-8. Choose the value of D_r closest to the release height (h_s) .

For mixed mode releases,
$$(D_r)_v = G_t (D_r)_g + (1-G_t) (D_r)_s$$
.
(3.19a)

3.2.4 Symbols Used In Section 3.2

SYMBOL	NAME	UNIT
X/Q	Relative Effluent Concentration	(sec/m^3)
R	Downwind Range	(m)
θ	Direction	(degrees or sector)
u	Wind Speed	(m/sec)
S	Stability Class	
f	Joint Frequency	
Sz	Corrected Vertical Dispersion	(m)
	Coefficient	
h _e	Effective Stack Height	(m)
hs	Physical Stack Height	(m)
hr	Plume Rise	(m)
ht	Terrain Correction Factor	(m)
Wo	Exit Velocity	(m/sec)
đ	Stack Diameter	(m)
C	Downwash Correction Factor	(m)
F	Momentum Flux Parameter	(m^4/sec^2)
S	Stability Parameter	(sec ⁻²)
Hrs	Terrain Height Difference	(m)
Hr	Terrain Height at Receptor Point	(m)
Hs	Terrain Height at Source	(m)
Gt	Ground Release Fraction	
σz	Vertical Dispersion Coefficient	(m)
D _z Q'i	Maximum Height of Neighboring Structure	(m)
Qi	Corrected Release Rate	(µCi/sec)
Qi	Release Rate	(µCi/sec)
λi	Radiodecay Constant	(hr ⁻¹)
t	Transport Time	(hr)
Pd	Plume Depletion Coefficient	

3.2.5 Constants Used In Section 3.2

NUMERICAL VALUE	NAME	UNIT
3600	Conversion Constant	(sec/hr)
16/2π	Sector Width ⁻¹	(Radians ⁻¹)
2.032	Conversion Constant	

3.3 MODELS FOR CALCULATING DOSE FROM NOBLE GASES

3.3.1 Gamma Radiation

3.3.1.1 Gamma Air Dose - Finite Cloud Model

The gamma air dose (D^{Υ}) is calculated from either of the following formulae:

$$D^{\Upsilon}(R,\theta) = \frac{260 \times 10^{-6} \times 86400}{R \times 2\pi/16} \times \sum_{m} t_{r}^{m} \sum_{u} \frac{1}{u} \sum_{i} \sum_{s} f(u,\theta,s) Q_{i}' \quad \mu_{ai} \quad \overline{E}_{\Upsilon i} \quad (\overline{I}_{1} + K_{i}\overline{I}_{2})_{i}$$

$$(3.20)$$

$$D^{Y}(R,\theta) = \frac{260 \times 10^{-6}}{R 2\pi/16} \sum_{u} \frac{1}{u} \sum_{i} \sum_{s} f(u,\theta, s) x$$

$$A_{i}^{\prime} \mu_{ai} \overline{E}_{\gamma i} (\overline{I}_{1} + K_{i}\overline{I}_{2})_{i}$$
 (3.21)

 $D^{\gamma}(R,\theta)$ Gamma Air Dose (mrad) The dose at (R,θ) due to gamma rays.

R Downwind Range (m)The distance downwind to point (R,θ) .

Direction (degree or sector)

The downwind direction to point (R,θ) .

Conversion Constant (mrad-radians-m³-disintegration/sec-MeV-Ci)

Reconciles units of Equation 3.20.

 10^{-6} Conversion Constant (Ci/ μ Ci) Converts Ci to μ Ci.

86400 Conversion Constant (sec/day)
Converts days to seconds.

 $2\pi/16$ Sector Width (radians) The sector width over which the plume meanders.

M Index

An index identifying the release period of interest.

tr Length of Release (days)

The time over which the mth release occurred.

u Wind Speed (m/sec)
The wind speed.

i Index
An index identifying the nuclide of interest.

Stability Class

The atmospheric stability class.

Q'i Corrected Release Rate (µCi/sec)

The release rate of nuclide i corrected for radiodecay in transit.

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Air Energy Absorption Coefficient (m⁻¹)

The gamma ray energy absorption coefficient for air, for nuclide i (see Table 7.1-9).

 E_{γ_i} Average Energy per (MeV/disintegration) The average gamma ray energy per disintegration of nuclide i (see Table 7.1-9).

 $(\overline{I}_1 + K_i \overline{I}_2)$ Dimensionless Numerical Integration Constant The dimensionless parameter resulting from numerical integration over the cloud defined in Section 7.5 of Reference 6.7. (For K_i values, see Table 7.1-9)

 A_i Corrected Release (μ Ci) The release of nuclide i corrected for radiodecay in transit.

The basic form of the above equation was taken from Meteorology and Atomic Energy (Equation 7.63) and is equivalent to Equation 6 in Regulatory Guide 1.109. The summation over the index m represents the summing of the doses from all sources at the station (i.e., elevated releases and vent releases).

Equation 3.20 was used to compute the normalized gamma air dose factors (mrad/yr per μ Ci/sec) S_i (for stack releases); V_i (for vent releases); and G_i (for ground level releases). Site-specific values of S_i , V_i , and G_i , using historical meteorological data, are given in Section 7.2.

3.3.1.2 Whole Body Dose Factors

The whole body dose factors, $\overline{S_i}$ (for stack releases); $\overline{V_i}$ (for vent releases); and $\overline{G_i}$ (for ground level releases), in mrad/yr per $\mu\text{Ci/sec}$, computed from $\text{D}^T(\text{R},\Theta)$ ÷ (1.11 SF $^\gamma$ 3.17 x 10 $^{-8}$), evaluated one nuclide at a time, are given in Section 7.2.

The whole body dose $D^{T}(R,\theta)$, calculated for preselected ranges in each downwind sector, is given by the equation that follows:

$$D^{T}(R,\Theta) = 1.11 \text{ SF}^{\gamma} \sum_{i} D_{i}^{\gamma}(R,\Theta) \exp(-5\mu_{ti})$$
 (3.22)

 $D^{T}(R,\theta)$ Whole Body Dose (mrem) The dose to the whole body at downwind point (R,θ) .

1.11 Conversion Constant (mrem/mrad)
Converts mrad to mrem.

SF^Y Shielding and Occupancy Factor for Gamma Radiation

Accounts for reduction in gamma exposure to building shielding and occupancy at the point of interest.

Tissue Energy Absorption (cm^2/g) Coefficient (Table 7.1-9) The gamma ray energy absorption coefficient in tissue for nuclide i.

 $D_i^{\gamma}(R,\theta)$ Gamma Air Dose (mrad) The gamma air dose at (R,θ) due to nuclide i as evaluated from Equation 3.20.

For this calculation, the shielding factor SFY is set to 0.7 and dose is computed at a depth of 5 cm in the tissue. The factor 1.11 is the ratio of tissue to air energy absorption coefficients.

3.3.2 Beta Radiation

3.3.2.1 Beta Particle Air and Skin Dose Factors

The beta particle air dose factor L_i , (mrad/yr per $\mu \text{Ci/m}^3$) and skin dose factor \overline{L}_i , mrem/yr per $\mu \text{Ci/m}^3$, are given in Reference 6.5 and included in Table 7.1-13.

3.3.3 Symbols Used In Section 3.3

SYMBOL	NAME	UNIT
$D^{\Upsilon}(R, \theta)$	Gamma Air Dose	(mrad)
R	Downwind Range	(m)
Θ	Direction	(degrees or sector)
m	Index	
t _r ^m	Length of Release	(days)
u	Wind Speed	(m/sec)
i	Index	
S	Stability Class	
f	Joint Frequency	
Q'i	Corrected Release Rate	(µCi/sec)
μai	Air Energy Absorption	(m^{-1})
	Coefficient	
Ε _γ ί	Average Energy per	(MeV/disintegration)
	Disintegration	
$(\overline{I}_1 + K_i \overline{I}_2)$	Dimensionless Numerical	
	Integration Constant	
A _i	Corrected Release	(µCi)
$D^{T}(R,\Theta)$	Whole Body Dose	(mrem)
SFY	Shielding and Occupancy	
	Factor for Gamma Radiation	
$D_i^{\gamma}(R,\Theta)$	Gamma Air Dose	(mrad)
^μ ti	Tissue Energy Absorption	(cm^2/g)
	Coefficient	

3.3.4 Constants Used in Section 3.3

NUMERICAL VALUE	NAME	UNIT
260	Conversion Constant	([mrad-radians-m ³ -disintegration]/[sec-MeV-Ci])
10-6	Conversion Constant	(Ci/µCi)
86400	Conversion Constant	(sec/day)
2π/16	Sector Width	(radians)
1.11	Conversion Constant	(mrem/mrad)

3.4 MODELS FOR CALCULATING DOSE FROM RADIOIODINES, "PARTICULATES", AND OTHER RADIONUCLIDES

The specific model for computing the dose to the various organs of an adult or infant is given in Equation 2.11. For the purpose of demonstrating compliance with the Technical Specifications, the dose to an infant who inhales air and drinks milk containing radioactive material shall be limiting. However, the dose model may be used to compute the dose to an adult who inhales radioactivity and ingests meat, milk, produce, or leafy vegetables containing radioactivity. The choice of the infant as the critical person is based on previous calculations of dose reported in semi-annual or annual reports. Annually, the dose to an adult will be computed to confirm the choice of an infant as "critical person".

In the inhalation model, using historical meteorological information, radioactive decay but not plume depletion was considered. Plume depletion was not considered at this time because depletion for the D atmospheric class, a class representative of average meteorology, reduces the inhalation dose by, at most, 10% within the 3 kilometer range considered.

4.0 AQUATIC TRANSPORT AND DOSE MODELS

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4.0 AQUATIC TRANSPORT AND DOSE MODELS

4.1 AQUATIC TRANSPORT

Dose via the aquatic pathway is discussed in Section 2.2. Two dilution factors are considered; F, the flow of the receiving body of water; and 1/M, an additional dilution factor.

4.1.1 River Model

For purposes of calculating the drinking water dose from liquid effluents discharged into a river, it is assumed that total mixing of the discharge in the river flow (F^W) occurs prior to consumption. No additional dilution is assumed to occur; thus 1/M^W equals 1.0. The river flow is taken as the long-term (generally 10 years) average.

For the fish consumption pathway, a near-field dilution flow F^f is used; $1/M^f = 1.0$.

4.1.2 Lake Michigan Model

For purposes of calculating dose from liquid effluents discharged to Lake Michigan, it is assumed that the concentration of radioactivity is diluted initially in the condenser cooling water of flow (F^C) and then by an additional factor $1/M^W$ of 60 prior to consumption as potable water. The dilution factor of 60 is the product of the initial entrainment dilution (factor of 10); the plume dilution (factor of 3 over approximately 1 mile); and the current direction frequency (annual average factor of 2).

For the fish ingestion pathway only, it is assumed the radio-activity is diluted fully in a hypothetical river of flow F^f ; $1/M^f = 1.0$.

4.1.3 Symbols Used In Section 4.1

SYMBOL	NAME	UNIT
F	Flow of the Receiving Body of Water	
1/M	Additional Dilution Factor	
Fw	Average Flow Rate (Drinking Water Pathway)	(ft ³ /sec)
1/M ^W	Additional Dilution Factor (Drinking Water Pathway)	
F ^f	Near-Field Flow Rate (Fish Ingestion Pathway)	(ft ³ /sec)
1/M ^f	Additional Dilution Factor (Fish Ingestion Pathway)	
F ^C	Average Flow of the Condenser Cooling Water During the Period of Discharge	(gal/min)

4.2 AQUATIC DOSE MODEL

The general model used to calculate the dose from radioactive material released in liquid waste is given in Subsection 2.2.1. The maximum consumption rate of fish by an adult, $U^f = 2.4 \times 10^{-3} \text{ kg/hr}$ (21 kg/yr), given in Reference 6.5 (USNRC Regulatory Guide 1.109), is assumed for all nuclear stations except those sited along the Illinois River. For these stations, because of this river's very low productivity of desirable fish, a consumption rate one-tenth the maximum is assumed.

4.2.1 Symbols Used in Section 4.2

 $\frac{\text{SYMBOL}}{\text{U}^{\frac{c}{2}}} \qquad \frac{\text{NAME}}{\text{Usage Factor}} \qquad \frac{\text{UNIT}}{\text{(kg/hr)}}$

4.3 AQUATIC TRANSPORT DURING TANK OVERFLOW CONDITIONS

In Subsection 2.2.3, the limiting quantity of radionuclide i in tanks without overflow pipes connected to other storage tanks was determined to be a function of two dilution factors characteristic of the receiving body of water: F_0^W , the minimum flow of the receiving body of water during overflow conditions, and $1/M_0^W$, an additional dilution factor.

4.3.1 River Model

For purposes of calculating the limiting quantity of tank radioactivity spilled into a river of flow, F_O^W , and with a dam between the release point and the intake, it is assumed that total mixing of the discharge in the river occurs in the minimum river flow of the most recent past 10 years. No additional dilution is assumed to occur; thus $1/M_O^W$ equals 1.0.

4.3.2 Lake Michigan Model

For purposes of calculating he limiting quantity of tank radioactivity spilled into Lake Michigan, it is assumed that F_O^W , the initial dilution water, is zero and that the additional dilution factor, $1/M_O^W$, is 1000. The 1000 factor represents an estimate of the dilution experienced by a shoreline-spilled water mass as it moves north along the shore and east into the lake, having to cross the northward moving lake current to reach the nearest water intake which is 6500 feet northeast (1.1 miles north and 3000 feet out in the lake) at a depth of 35 feet.

4.3.3 Symbols Used in Section 4.3

SYMBOL	NAME	UNIT
F _O	Minimum Flow Rate,	(ft ³ /sec)
· ·	Receiving body of	
	Water	
1/M ^W	Additional Dilution	
	Factor	

5.0 SUMMARY

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5.0 SUMMARY

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5.0 SUMMARY

5.1 AIRBORNE EFFLUENTS

5.1.1 10 CFR 50, Appendix I Design Objectives

The 10 CFR 50, Appendix I technical specification design objectives for the nuclear stations are summarized in Table 5.1-1. To demonstrate compliance with the Appendix I objectives, the dose for each time period of the quarter will be calculated using the dose equations noted in Table 5.1-1. The current quarter dose is the summation of the dose contribution from every effluent release during the quarter. The station will calculate the doses on a monthly basis. Each time the station evaluates the dose equations, the new contribution is added to the current total for the quarter, and the new total is compared with the objective. Next, the new total for the quarter is combined with the totals for the previous three quarters to determine the annual dose.

The results of each calculational run will be summarized in a format similar to that shown in Table 5.1-1. The maximum dose is printed with the associated wind direction. The values calculated for each wind direction and range must be stored for calculation of the maximum period, quarter, and annual dose. For the organ dose, the computer will calculate doses to seven organs for up to 73 radionuclides, and select the maximum period, quarter, and annual organ doses.

For each dose type and maximum value, the compliance status is calculated where the status (%) = $100 \times \text{maximum dose}$ \div dose objective.

5.1.2 10 CFR 20 Release Rate Limits

The compliance status with respect to the 10 CFR 20 limits is determined in the following manner and reported in the format of Table 5.1-2 for periods of unusually high release rate Q.

C.S._{WB} =
$$\frac{\text{(dose rate from Eq. 2.9) x 100}}{500 \text{ mrem/yr}}$$
 (%) whole body (5.1)

C.S._S =
$$\frac{\text{(dose rate from Eq. 2.10)} \times 100}{3000 \text{ mrem/yr}}$$
 (%) skin (5.2)

C.S._o =
$$\frac{\text{(dose rate from Eq. 2.18)} \times 100}{1500 \text{ mrem/yr}}$$
 (%) organ (5.3)

The value of C.S. must not exceed 100%. If it does, the station's release rate is too high and corrective action to reduce the release rate must be taken immediately.

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TABLE 5.1-1

(Name) Unit (number)

MAXIMUM DOSES RESULTING FROM AIRBORNE RELEASES

(PERIOD OF RELEASE FROM (DATE) TO (DATE). DATE OF CALCULATION (DATE))

TYPE	CURRENT PERIOD	CURRENT QUARTER*	THIRD QUARTER	SECOND	FIRST QUARTER	ANNUAL
Gamma Air (mrad)	Eq.2.1 $^{\Delta}$	dose (dir.)	- NOTE:	This format shou 30 entries	ld appear in	all
Beta Air (mrad)	Eq.2.3					
Whole Body (mrem)	Eq.2.5					
Skin (mrem)	Eq.2.7					
Organ (mrem)	Eq.2.11					

Last period of release from (date) to (date), calculated (date).

COMPLIANCE STATUS

TYPE	10 CFR 50 APP. I QUARTERLY OBJECTIVE	% OF APP. I	10 CFR 50 APP. I YEARLY OBJECTIVE	% OF APP. I
Gamma Air (mrad)	5		10	
Beta Air (mrad)	10		20	
Whole Body (mrem)	2.5		5	
Skin (mrem)	7.5		15	
Organ (mrem)	7.5	**	15	***

AThe equation number of the model used to compute the dose for the period is listed here for information only.

^{*}Cumulative dose for the quarter including the current period.

^{**}The critical organ is (Name).
***The critical organ is (Name).

TABLE 5.1-2 (Name) Station

MAXIMUM INSTANTANEOUS RELEASE RATES

(PERIOD OF RELEASE FROM (DATE/TIME) TO (DATE/TIME).

DATE OF CALCULATION (DATE))

ORGAN	DOSE RATE, mrem/year	10 CFR 20 LIMIT, mrem/year	COMPLIANCE STATUS*
Whole Body		500	Eq. 5.1
Skin		3000	Eq. 5.2
(Name) Organ∆		1500	Eq. 5.3

The organ with the maximum dose should be named.

^{*}See text for definition. If C.S. > 100, add this or similar footnote to the table:

[&]quot;Corrective action must be taken immediately to reduce the release rate." Also, perhaps, at the bottom of this table on a separate sheet, the radionuclides and their release rate should be listed.

5.2 LIQUID RELEASES

5.2.1 10 CFR 50, Appendix I Design Objectives

The total quarterly and annual whole body or organ doses due to radioactivity discharged in liquid wastes are computed in a manner similar to that for airborne effluents. The results, based on doses computed with Equation 2.22, are summarized in the manner of Table 5.2-1.

5.2.2 10 CFR 20 Maximum Permissible Concentrations

5.2.2.1 Unrestricted Area

The concentration of nonnoble gas radioactive material released from the site to unrestricted areas (C_i) shall be limited to the concentrations specified in 10 CFR 20, Appendix B, Table II, Column 2 (MPC_i). The concentrations of dissolved or entrained noble gases shall be limited to the concentrations specified in Table 7.1-10. The sum of the fractional limits $(C_i \div \text{MPC}_i)$ must not exceed 1.0 for each release.

Hence:

$$100 \times \sum_{i} \frac{C_{i}}{MPC_{i}} \leq 100%$$
 (5.4)

5.2.2.2 Nearest Surface Water Supply

At Zion, the quantity of radionuclides, excluding tritium and dissolved or entrained noble gases, in outdoor tanks without overflow pipes connected to other storage tanks, shall be limited to ensure that in the case of an overflow, the annual average concentration of radioactivity in the potable water of the nearest surface water supply is less than the 10 CFR 20, Appendix B, Table II, Column 2 limits.

Hence:

$$\sum_{i} \frac{A_{i}^{t}}{MPC_{i}} \exp \left(-\lambda_{i} \times t_{O}^{w}\right) \leq 4 \left(\frac{F_{O}^{w} + F^{t}}{F^{t}}\right) \frac{V^{t}}{M_{O}^{w}}$$
 (5.5)

and

$$\sum_{i} \frac{c_{i}^{t}}{MPC_{i}} \exp \left(-\lambda_{i} \times t_{o}^{w}\right) \leq \left(\frac{F_{o}^{w} + F^{t}}{F^{t}}\right) \frac{1100}{M_{o}^{w}} \tag{5.6}$$

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TABLE 5.2-1

(Name) Unit (number)

MAXIMUM DOSES RESULTING FROM LIQUID EFFLUENTS

(PERIOD OF RELEASE FROM (DATE) TO (DATE). DATE OF CALCULATION (DATE))

TYPE	PERIOD	CURRENT QUARTER*	THIRD QUARTER	SECOND QUARTER		ANNUAL
Whole Body (mrem)		dose - NOTE:	This forma		appear in al	1
Organ (mrem)		dose				
Critical Organ During Period		name				

Last period of release from (date) to (date), calculated (date).

COMPLIANCE STATUS

TYPE	10 CFR 50 QUARTERLY OBJECTIVE	% OF APP. I	10 CFR 50, APP. I YEARLY OBJECTIVE	% OF AFP. I
Whole Body (mrem)	1.5		3	
Organ (mrem)	5	**	10	***

^{*}Cumulative dose in quarter to date

^{**} he critical organ is (name)

^{***} The critical organ is (name)

5.3 URANIUM FUEL CYCLE

The compliance status, with respect to the 40 CFR 190 limits, is determined in the following manner and reported in the format of Table 5.3-1 at the end of each calendar year.

In accordance with the numerical models described in Subsection 2.3.2, the maximum whole body, thyroid, and any other organ (AOO) doses to a member of the public in the general environment, i.e., the unrestricted area, will be determined and compared to the 40 CFR 190 limits to determine the compliance status.

TABLE 5.3-1

	(Name)	STATION (S)
COMPLIANCE STATUS:	URANIUM FUEL CYC	CLE OPERATIONS: 40	CFR 190
Period of Release_	Date of	This Calculation_	
ORGAN	DOSE RATE mrem/year	40 CFR 190 LIMIT (mrem/year)	
Whole Body		25	
Thyroid		75	
Any Other Organ (Name)		25	

^{*}If > 100%, this or a similar footnote must be added to the table.

[&]quot;Corrective action might be needed to bring the facility into compliance with the regulations. If a variance for unusual operations is required, petition the NRC in accordance with the requirements of 40 CFR 190.11."

5.4 PRIMARY DRINKING WATER STANDARDS

The U.S. Environmental Protection Agency has promulgated regulations for the radioactivity content of community water systems (Reference 6.18). One part (40 CFR 141.16(a)) of these regulations involves man-made radioactivity, such as those in liquid waste from a reactor. It reads: "The average annual concentration of beta particle and photon radioactivity from man-made radionuclides in drinking water shall not produce an annual dose equivalent to the whole body or any internal organ greater than 4 millirem per year." In 40 CFR 141.16(b) the method for calculating this dose is described. The EPA dose calculation method differs somewhat from that described in ODCM Subsection 2.2.1. Furthermore, the 40 CFR 141 regulation applies to the operator of the community water system and not to CECo.

If a special report defining corrective actions to reduce the releases of radioactive materials in liquid effluents is required by the technical specifications, it must include an analysis of the radiological impact on the downstream drinking water source also. This analysis may include the data of Table 5.4-1.

If confirmatory measurements of radioactivity attributable to plant operations found at the nearest community water system are available, the following concentrations, taken singularly or in combination (i.e., the sum of the ratios of concentration to limit are ≥ 1), shall define the 40 CFR 141 regulatory limit: strontium-90, 8 pCi/l; tritium, 20,000 pCi/l; gross beta activity, 50 pCi/l; and for any other nuclide, the concentration given in NBS Handbook 69 as amended in August 1963.



(Name) Station

PROJECTED DOSE AT NEAREST COMMUNITY WATER SYSTEM*

(PERIOD OF RELEASE FROM (DATE) TO (DATE). DATE OF CALCULATION (DATE))

CURRENT CURRENT THIRD SECOND FIRST

TYPE PERIOD QUARTER** QUARTER QUARTER QUARTER ANNUAL

Whole Body (mrem) Dose NOTE: This format should appear in all

12 entries

Internal Organ Dose (mrem) ***

Critical Organ Name Name Name Name Name Name Name

Last period of release from (date) to (date), calculated (date).

COMPLIANCE STATUS

TYPE

40 CFR 141
ANNUAL LIMIT

Whole Body (mrem)

4

Internal Organ (mrem) ***

4

Critical Organ
During Year ***

Name

^{*} This calculation of dose is based on techniques described in the Commonwealth Edison Offsite Dose Calculation Manual. These techniques differ from those described in 40 CFR 141. A projected dose of 2 mrem using CECo's techniques is approximately 4 mrem using EPA methods. Any planned action should be based on the requirements of the regulation and not this report.

^{**} Cumulative dose in quarter to date.

^{***} Either thyroid, GI-LLI, bone, liver, kidney, or lung.

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6.0 REFERENCES

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- 6.14 EPA-520/9-73-003-B, "Environmental Analysis of the Uranium Fuel Cycle," Part I, Fuel Supply, October 1973.
- 6.15 NUREG-0002, "Final Generic Environmental Statement on the Use of Recycled Plutonium in Mixed Oxide Fuel in Light Water Cooled Reactors," August 1976.
- 6.16 WASH-1248, "Environmental Survey of the Uranium Fuel Cycle," April 1974.
- 6.17 WASH-1238, "Environmental Survey of Transportation of Radioactive Materials To and From Nuclear Power Plants," December 1972.

- 6.18 U.S. Environmental Protection Agency, 40 CFR 141, Federal Register 41, 133, 28402, July 9, 1976.
- 6.19 W. R. VanPelt, "Environmental Radiation Survey of the Dresden Nuclear Power Station," Environmental Analysis, Inc., December 1971.
- 6.20 G. S. Raynor and P. M. SethuRaman, "Recommendations for Meteorological Measurement Programs and Atmospheric Diffusion Prediction Methods For Use At Coastal Nuclear Reactor Sites," NUREG/CR-0936, BNL-NUREG-51045, October 1979.
- 6.21 J. F. Sagendorf and J. T. Goll, "XOQDOQ Program for the Meteorological Evaluation of Routine Effluent Releases at Nuclear Power Stations," NUREG-0324, Draft, August 1977.

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7.0 DATA FOR DOSE ASSESSMENT MODELS

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7.0 DATA FOR DOSE ASSESSMENT MODELS

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7.2-	Indexes for Section 7.2 Figures will be found preceding the site-specific data for Dresden La Salle, Quad Cities, and Zion Stations, respectively.

7.0 DATA FOR DOSE ASSESSMENT MODELS

Virtually all of the data to be used in the dose assessment models is contained in this section of the ODCM. This organization will permit easy reference and facilitate future changes, should they be necessary.

Section 7.1 contains data which is generically applicable to all stations.

Section 7.2 contains site descriptions and data (particularly meteorological data) which is relevant only to a specific site.

7.1 DATA COMMON TO ALL NUCLEAR STATIONS

This section contains data that is generically applicable to all stations.

TABLE 7.1-1

DOSE COMMITMENT FACTORS

PATHWAY	INFANT	ADULT		
Inhalation	See Table 7.1-E-10	See Table 7.1-E-7		
Ingestion	See Table 7.1-E-14	See Table 7.1-E-11		

The following tables are from Tables E-7, E-10, E-11, and E-14 of Appendix E of Reference 6.5. Each table contains seven organ dose factors for 73 radionuclides. For radionuclides not found in these tables dose factors will be derived from ICRP 2 (1959) or NUREG-0172 (Reference 6.10).

TABLE 7.1-E-7

INHALATION DOSE FACTORS FOR ADULTS

(mrem per pCi Inhaled)

NUCLICE BONE	LIVER	T.80CY	THYROID	KIDNEY	LUNG	GI-LLI
H 3 NO DATA	1.58E-07	1.58F-07	1.586-07	1.58E-07	1.58E-07	1.58E-07
C 14 2.27E-06	4.26E-07	4.26E-07	4.268-07	4.26E-07	4.26E-07	4.26E-07
NA 24 1.28E-06	1.28E-06	1.26E-06	1.288-06	1.28E-06	1.28E-06	1.28F-06
P 32 1.65E-04	9.64E-06	6.26E-06	NO DATA	NC DATA	NO DATA	1.08E-05
CR 51 NO DATA	NO DATA	1.25E-08	7.44E-09	2.85E-09	1.80E-06	4.15E-07
MN 54 NO DATA	4.95E-06	7.87E-07	NO DATA	1.23E-06	1.75E-04	9.67E-06
MN 56 NO DATA	1.55F-10	2.23E-11	NO DATA	1.63E-10	1.18E-06	2.53E-06
FE 55 3.07E-06	2.12E-06	4.33E-07	NO DATA	NO DATA	9.01E-06	7.54E-07
FE 59 1.47E-06	3.47E-06	1.32E-06	NO DATA	NO DATA	1.27E-04	2.35E-05
CO 58 '10 DATA	1.98E-07	2.59E-07	NO DATA	NC DATA	1.16E-04	1.33E-05
CO 60 NO DATA	1.94E-06	1.85E-06	NO DATA	NC DATA	7.46E-04	3.56E-05
'11 63 5.406-05	3.93E-0a	1.81E-06	NO DATA	NO DATA	2.23E-05	1.67E-06
VI 65 1.92E-10	2.625-11	1.14F-11	NO DATA	NC DATA	7.00E-07	1.54E-06
CU 64 NO DATA	1.936-10	7.63F-11	NO DATA	5.78E-10	8.48E-07	6.12E-06
ZN 65 4.05E-06	1.296-05	5.82E-06	NO DATA	8.62E-06	1.08E-04	6.68E-06
ZN 69 4.23E-12	B.14C-12	5.65E-13	NO DATA	5.27E-12	1.15E-07	2.04E-09
AR 83 NO DATA	4U DATA	3.01E-08	NO DATA	NO DATA	NO DATA	2.90E-08
AR 84 NO DATA	NO DATA	3.91E-08	NO DATA	NO DATA	NO DATA	2.05E-13
0R 85 NO DATA RB 86 NO DATA RB 88 NO DATA	NO DATA	1.60E-09	NO DATA	NO DATA	NO DATA	LT E-24
	1.676-05	7.37E-06	NO DATA	NO DATA	NO DATA	2.08E-06
	4.845-08	2.415-78	NO DATA	NO DATA	NO DATA	4.18E-19
98 89 NO DATA	3.2CE-08	2.12E-08	NO DATA	NO DATA	NO DATA	1.16E-21
58 89 3.80E-05	NO DATA	1.09E-96	NO DATA	NO DATA	1.75E-04	4.37E-05
58 90 1.24E-02	NO DATA	7.62E-04	NO DATA	NO DATA	1.20E-03	9.02E-05
SR 91 7.74E-09	NO DATA	3.13E-10	NO DATA	NU DATA	4.56E-06	2.39F-05
SR 92 8.43E-10	NO GATA	3.64E-11	NO DATA	NO DATA	2.06E-06	5.38E-06
Y 90 2.61E-07	NO DATA	7.01E-09	NO DATA	NI DATA	2.12E-05	6.32E-05
Y 91M 3.26E-11	NO DATA	1.27E-12	NO DATA	NC DATA	2.40E-07	1.66E-10
Y 91 5.78E-05	NO DATA	1.55E-06		NO DATA	2.13E-04	4.81E-05
Y 92 1.29E-09	NO DATA	3.77E-11		NO DATA	1.96E-06	9.19E-06

TABLE 7.1-E-7 (Cont'd)

NUCLISE	BONE	LIVER	T.BUDY	THYROID	KIONEY	LUNG	GI-LLI
Y 93	1.186-05	NO DATA	3.26E-10	NO DATA	NC DATA	6.06E-06	5.27E-05
ZR 95	1.346-05	4.305-06	2.91E-06	NO DATA	6.776-06	2.21E-04	1.38E-05
ZR 97	1.716-08	2.450-09	1.13E-09	NO DATA	3.716-09	9.84 -06	6.54E-05
NB 95 MO 99 TC 99M	1.76E-06 MO DATA 1.29E-13	0.17L-07 1.51E-08 3.64E-13	5.26E-07 2.87E-09 4.65E-12	NO DATA NO DATA	9.67E-07 3.64E-08 5.52E-12	6.31E-05 1.14E-05 9.55E-08	1.30E-05 3.10E-05 5.20E-07
fC101 .RU103 RU105	5.22E-15 1.91E-07 9.88E-11	7.526-'S NU DATH NO DATA	7.38E-14 8.23E-08 3.89E-11	NO DATA NO DATA	1.35c-13 7.29E-07 1.27E-10	4.99E-08 6.31E-05 1.37E-06	1.36F-21 1.38E-05 6.02E-06
RU106	8.64E-06	NO DATA	1.03E-06	NO DATA	1.67£-05	1.17E-0;	1.14E-04
ACILOM	1.35E-06	1.256-06	7.43E-07	NU DATA	2.46E-06	5.79E-04	3.78E-05
TE1254	4.27E-07	1.996-07	5.84E-08	1.31E-07	1.55£-06	3.92E-05	8.83E-06
TE127M	1.58E-06	7.215-07	1.96E-07	4.11E-07	5.72E-06	1.20E-04	1.87E-05
TE127	1.75E-10	8.035-11	3.87E-11	1.32E-10	6.37E-10	8.14E-07	7.17E-06
TE127	1.22E-06	5.845-07	1.96E-07	4.30E-07	4.57E-06	1.45E-04	4.79E-03
TE127	6.22E-12	2.79E-12	1.55E-12	4.87t-12	2.34E-11	2.42E-07	1.96E-08
TE131M	8.74E-09	5.45E-07	3.63E-09	6.88F-09	3.86E-08	1.82E-05	6.95E-05
TF131	1.39E-12	7.44E-13	4.49E-13	1.17E-12	5.46E-12	1.74E-07	2.30E-09
TE132	3.25E-08	2.69E-08	2.02E-08	2.37E-08	1.82E-07	3.60E-05	6.37F-05
1 130	5.72E-07	1.68E-06	6.60E-07	1.42E-04	2.61E-06	NO DATA	9.61E-07
1 131	3.15E-06	4.47E-06	2.56E-06	1.49E-03	7.66E-06	NO DATA	7.85E-07
1 132	1.45E-07	4.07E-07	1.45E-07	1.43E-05	6.48E-07	NO DATA	5.08F-08
1 133	1.08E-06	1.85E-06	5.65E-07	2.69E-04	3.23E-06		1.11E-06
1 134	8.05E-09	2.16E-07	7.69E-08	3.73E-06	3.44E-07		1.26E-10
1 135	3.35E-C7	8.73E-07	3.21E-07	5.60E-05	1.39E-06	NO DATA	6.56E-07
CS134	4.66E-05	1.06E-04	7.10E-05	NO DATA	3.59E-05	1.22E-05	1.30E-06
CS136	4.88E-06	1.83E-05	1.38E-05	NO DATA	1.07E-05	1.50E-06	1.46E-06
CS138	5.98E-05	7.76E-05	5.35E-05	NO DATA	2.78E-05	9.40E-06	1.05F-06
CS138	4.14E-08	7.76E-08	4.05E-08	NO DATA	6.00E-08	6.07E-09	2.33E-13
BA139	1.17E-10	8.32E-14	3.42E-12	NO DATA	7.78E-14	4.70E-07	1.12E-07

TABLE 7.1-E-7 (Cont'd)

MUCTICE	BONE	LIVER	T. BUCY	THYROTO	KIDNEY	LUNG	GI-LLI
HA140 HA141 RA142	4.88E-C6 1.25E-11 3.29E-12	6.13F-09 9.4.F-15 3.38F-15	3.21E-07 5.20E-13 2.076-13	NO DATA NO DATA NO DATA	2.09E-09 8.75E-15 2.96E-15	1.59E-04 2.42E-07 1.49E-07	2.73F-05 1.45E-17 1.96E-26
LA140 LA142 CE141	4.30E-FP 8.54E-(1 2.49E-06	3.88E-11 1.69E-06	5.7s[-07 9.69E-12 1.91L-07	NO DATA NO DATA NO DATA	NO DATA NO DATA 7.836-07	1.70E-05 7.91E-07 4.52E-05	5.73E-05 2.64E-07 1.50E-05
CE144 PR143	2.33E-08 4.29£-04 1.17E-06	1.72L-08 1.79E-04 4.69E-07	1.916-07 2.30F-05 5.806-08	NO DATA NO DATA NO DATA	7.60E-09 1.06E-04 2.70E-07	9.97E-06 9.72E-04 3.51E-05	2.83E-05 1.02E-04 2.50E-05
PR14" VD:47 W 187	3.76E-12 6.59E-07 1.06E-09	1.565-12 7.625-07 8.850/10	1.91E-13 4.56E-08 3.10E-10	NO DATA NO DATA	8.816-13 4.45E-07 NC DATA	1.27F-07 2.76E-05 3.63E-06	2.69E-18 2.16E-05 1.94E-05
NP239	2.87E-08	2.825-09	1.556-09	NO DATA	8.75E-09	4.70F-06	1.49E-05

TABLE 7.1-E-10

INHALATION DOSE FACTORS FOR INFANTS

(mrem per pCi Inhaled)

NUCL	IDE - E	UNE	LIVER	TLANCY	THYRO	10 K1	DNEY	LUNG	G1-LL1
H C 14 NA 24	4 1.89	E-05 3.	62E-07 79L-06 54E-06	4.62F-07 3.77E-06 7.54E-06	4.62F- 3.796- 7.54E-	06 5.7	9E-06	4.67E-07 3.79E-06 7.54E-06	4.62F-07 3.79E-06 7.54E-06
0 3, CR 5 MN 5	2 1.45 1 NO 6	ATA NO	03E-05 0ATA 61E-05	5.53E-05 6.17E-08 3.56E-06	NO DAT 4.11E- NO DAT	08 9.4	5E-09	0 DATA 7.17E-06 7.14E-04	1.15F-05 2.55E-07 5.04E-06
MN 51 FE 51 FE 5	5 1.41	E-05 8.	105-09 39E-06 68E-05	1.58E-10 2.38E-06 6.77E-36	NO DAT	A NO	DATA 6	2.95E-06 3.21E-05 7.25E-04	5.12E-05 7.82E-07 1.77E-05
CO 51	0 40 0	ATA 5.		1.30E-35 8.41E-06 8.29E-06	NO DAT NO DAT NO DAT	A NO	DATA 3	5.55E-04 5.22E-03 1.49E-04	7.95F-06 2.28E-05 1.73E-06
41 65 CU 64 Z4 65	 NO D 	ATA 1.	34c-09	8.77E-11 5.54F-10 2.22F-05	TAG OF TAG OF TAG OF	A 2.8	4E-09 6	0.80E-06 0.64E-06 0.62E-04	3.58E-05 1.07E-05 3.67E-05
7N 69 BR 8: BR 86	3 NO D	ATA NO	DATA	5.13E~12 2.72E-07 2.86E-07	NO DAT	A NO	DATA N	.05E-06 10 DATA 10 DATA	9.44E-06 LT E-24 LT E-24
78 86 78 86	NO D	ATA 1.	361-04	1.46E-08 6.30E-05 2.05E-07	NO DAT	A NO	DATA N	DATA O DATA	LT E-24 2.17E-06 2.42E-07
RB 89 SR 89	2.84	E-04 NI)	DATA	1.47E-07 8.15E-06 1.85E-03	NO DAT NO DAT NO DAT	A NO	DATA 1	0 DATA .45E-03	4.87E-08 4.57E-05 9.36E-05
SR 91 SR 92 Y 90	7.50	E-09 NU	DATA	2.47E-09 2.79E-10 6.30E-08	NO DAT NO DAT NO DAT	A NO I	DATA I	.76E-05 .70E-05 .92E-04	5.24E-05 1.00E-04 7.43E-05
Y 91 Y 91 Y 92	4.20	E-04 NO	DATA	9.90E-12 1.12E-05 3.23E-10	NO DAT	A NO I	DATA 1	.99E-06 .75E-03	1.68E-06 5.02E-05 9.04E-05

TABLE 7.1-E-10 (Cont'd)

MOCLICE	BONE	LIVER	1.8009	THYROID	KIDNEY	LUNG	GI-LLI
Y 93	1.07E-07	NO DATA	2.91E-09	NO DATA	NO DATA	5.46E-05	1.19E-04
ZR 95	8.24E-05	1.775-05	1.45E-05	NO DATA	2.22t-05	1.25E-03	1.55E-05
ZR 97	1.07E-07	1.636-08	8.36E-09	NU DATA	1.85E-08	7.88E-05	1.00E-04
NB 35	1.120-05	4.59E-06	2.70E-06	NO DATA	3.57E-06	3.42E-04	9.05E-06
MD 39	NO DATA	1.18E-07	2.31E-08	NO DATA	1.89E-07	9.63E-05	3.48E-05
TC 33M	9.785-13	2.06E-12	2.66E-11	NO DATA	2.22E-11	5.79E-07	1.45E-06
TC101	4.65E-14	5.99E-14	5.80F-13	NO DATA	6.77E-13	4.17E-07	6.03E-07
RU103	1.44E-06	NO DATA	4.85E-07	NO DATA	3.03E-06	3.94E-04	1.15E-05
RU105	8.74E-10	NO DATA	2.93E-10	NO DATA	6.42E-10	1.12E-05	3.46E-05
RU106	6.201-05	NU DATA	7.77E-06	NO DATA	7.61E-05	8.26E-03	1.17E-04
AG110*	7,13F-06	5.16E-06	3.57E-06	NO DATA	7.80E-06	2.62E-03	2.36E-05
TE125*	3.401-06	1.42C-06	4.70E-07	1.16E-06	NO DATA	3.19E-04	9.22E-06
TE127#	1.19E-05	4.93E-06	1.45£-06	3.48E-06	2.68E-05	9.37E-04	1.95E-05
TE127	1.59E-09	6.81E-10	3.47£-10	1.33E-09	3.47E-09	7.39E-06	1.74E-05
TE127#	1.01E-05	4.35E-06	1.57£-06	3.91E-06	2.27E-05	1.20E-03	4.93E-05
TE131M TE131	5.63E-11 7.62E-08 1.245-11	2.485-11 3.73E-08 5.87E-12	1.34E-11 2.59E-08 3.57E-12	4.82E-11 6.38E-08 1.13E-11	1.25E-10 1.89E-07 2.85E-11	7.14E-06 1.42E-04 1.47E-06	1.98E-05 8.51E-05 5.87E-06
TE132	2.66E-07	1.698-07	1.26E-07	1.79E-07	7.396-07	2.43E-04	1.15E-05
1 130	4.54E-06	9.718-06	3.9HF-06	1.14E-03	1.996-05	NO DATA	1.42E-06
1 131	2.71E-05	3.175-05	1.47E-05	1.06E-02	3.706-05	NO DATA	7.56E-07
T 132	1.71E-06	2.53E-06	8.99E-07	1.21E-04	2.#2E-06	NO DATA	1.36E-06
T 133	9.46E-06	1.37E-05	4.00E-06	2.54E-03	1.60E-05	NO DATA	1.54E-06
T 134	6.58E-07	1.34E-06	4.75E-07	1.18E-05	1.49E-06	NO DATA	9.21E-07
1 135	2.76E-06	5.43F-06	1.99E-06	4.97E-04	6.05E-06	NO DATA	1.31E-06
CS134	2.83E-04	5.02E-04	5.32E-05	NO DATA	1.36E-04	5.69E-05	9.53E-07
CS136	3.45E-05	9.61E-05	3.78E-05	NO DATA	4.03E-05	8.40E-06	1.02E-06
CS137 CS138 BA139	3.92F-04 3.61E-07 1.06E-09	4.37F-04 5.58E-07 7.03E-13	3.25E-05 2.84E-07 3.07E-11	NO DATA NO DATA	1.23E-04 2.93E-07 4.23E-13	5.09E-05 4.67E-08 4.25E-06	9.53F-07 6.26F-07 3.54F-05

TABLE 7.1-E-10 (Cont'd)

NUCLICE	BONE	r i vc R	T. HUUY	THYRDID	KIONEY	LUNC	GI-LL1
MA140	4.00E-05	4.00E-08	2.07F-96	NO DATA	9.59E-09	1.14f=03	2.740-05
MA141	1.12E-10	7.70F-14	3.55±-12	NO DATA	4.64L-14	2.12f=06	3.39F-06
MA142	2.84E-11	2.30F-19	1.40±-12	NO DATA	1.36L-14	1.11f=06	4.955-07
LA140	3.61E-07	1.43E-07	1.602-08	NO DATA	NO DATA	\$.20E-04	6.96E-05
LA142	7.36E-10	2.69E-10	6.402-11	NO DATA	NO DATA	5.67E-06	4.25E-05
CE141	1.38E-00	1.19E-05	1.4/2-06	NO DATA	1.75E-06	3.69E-04	1.54E-05
CE143	2.09E-07	1.39E-07	1.54E-08	ATAC UV	4.03E-08	8.3CE-05	3.55E-05
CE144	2.28E-03	8.05E-04	1.26E-04	ATAC UV	3.84E-04	7.03E-03	1.36E-04
PR143	1.00E-05	3.74E-00	4.97E-07	ATAU OV	1.41E-06	3.09F-04	2.66E-05
PR144	3.42E-11	1.32E-11	1.7/E-12	NO DATA	4.80E-12	1.15F-06	3.06F-06
VD147	5.67E-00	5.81E-06	3.57E-07	NO DATA	2.25E-06	2.30E-04	2.23E-05
W 187	9.26E-09	6.44E-09	2.23E-03	NO DATA	NO DATA	2.33E-05	2.54F-05
18239	2.65E-07	2.376-08	[.34E-09	NO DATA	4.731-08	4.25E-05	1.786-05

TABLE 7.1-E-11

INGESTION DOSE FACTORS FOR ADULTS

(mrem per pCi Ingested)

BUCLILE	BONE	I. I VER	T.CLSY	THYROTO	KIDNEY	LUNG	61-111
H 3	NO DATA	1.05C-0/	1.05E-07	1.05e-07	1.05E-07	1.05E-07	1.05E-07
C 14	2.84E-06	5.68E-D7	5.68E-07	5.68E-07	5.68E-07	5.68F-07	5.68E-07
NA 24	1.70E-06	1.70F-06	1.70E-06	1.70E-06	1.70E-06	1.70E-06	1.70E-06
P 32 CR 51 MN 54	1.936-04 NO DATA NO DATA	1.20F-05 NO DATA 4.575-06	7.46E-06 2.66E-07 8.72E-07	1.59E-09 NO DATA	NC DATA 5.866-10 1.368-06	NO DATA 3.53E-09 NO DATA	2.17E-05 6.69E-07 1.40E-05
MN 56	NO DATA	1.155-07	2.04F-08	NO DATA	1.46E-07	NO DATA	3.67F-06
FE 55	2.75E-06	1.305-06	4.43E-07	NO DATA	NO DATA	1.06E-06	1.09E-06
FE 59	4.34E-06	1.025-05	3.91E-06	NO DATA	NO DATA	2.85E-06	3.40E-05
CO 58	NO DATA	7.456-07	1.67E-05	VO DATA	NO DATA	NO DATA	1.51F-05
CO 50	NO DATA	2.145-06	4.72C-06		NO DATA	NO DATA	4.02E-05
VI 63	1.30E-C4	9.016-06	4.36E-06		NO DATA	NO DATA	1.88E-06
NI 63	5.28E-07	6.86E-08	3.13E-08	NO DATA	NO DATA	NO DATA	1.74E-06
CU 64	NO DATA	9.33E-08	3.91E-08	NO DATA	2.10E-07	NO DATA	7.10E-06
ZN 63	4.84E-06	1.54E-05	5.90E-06	NO DATA	1.03E-05	NO DATA	9.70E-06
ZN 69	1.03E-08	1. 775-08	1.37F-09	NO DATA	1.28E-08	NO DATA	2.96E-09
HR 83	40 DATA	NO DATA	4.02E-08	NO DATA	NO DATA	NO DATA	5.79E-08
HR 84	NO DATA	NO DATA	5.21E-08	NO DATA	NO DATA	NO DATA	4.09E-13
RR 85	NO DATA	NO DATA	2.14E-09	NO DATA	NC DATA	NO DATA	LT E-24
RB 86	NO DATA	2.116-75	9.83E-06	NO DATA	NO DATA	NO DATA	4.16E-06
RB 88	NO DATA	6.050-08	3.21E-08	NO DATA	NO DATA	NO DATA	8.36E-19
RR 89	NO DATA	4.01E-0B	2.82E-08	NO DATA	NO DATA	NO DATA	2.33E-21
SR 89	3.08E-04	NO DATA	8.84E-06	NO DATA	NO DATA	NO DATA	4.94E-05
SR 90	7.58E-03	NO DATA	1.86E-03	NO DATA	NO DATA	NO DATA	2.19E-04
SR 91 SR 92 Y 90	5.67E-06 2.15E-06 9.62E-09	NU DATA NO DATA NU DATA	2.29E-97 9.30E-08 2.58E-10	NO DATA NO DATA	NC DATA NC DATA NC DATA	NO DATA NO DATA NO DATA	2.70E-05 4.26E-05 1.02E-04
Y 91K	9.09E-11	NO DATA	3.52E-12	NO CATA	NO DATA	NO DATA	7.6 'E-10
Y 91	1.41E-07	NO DATA	3.77E-07	NO DATA	NO DATA	NO DATA	. 76E-05
Y 92	8.45E-10	NO CATA	2.47E-11	NO DATA	NO DATA	NO DATA	1. 8E-05

TABLE 7.1-E-11 (Cont'd)

NUCLICE	BONE	LIVER	T.SORY	THAGUIC	KIDNEY	LUNG	G1-LL1
Y 93	2.68E-09	NO DATA	7.40E-11	NO DATA	NO DATA	NO DATA	9.50F-05
18 75	3.04E-08	7.75E-09	6.60E-07		1.5:E-08	NO DATA	3.09E-05
1R 97	1.68E-09	3.39E-10	1.55E-10		5.12E-10	NO DATA	1.05E-04
NR 95 MR 97 TC 99M	6.22E-09 NO DATA 2.47E-10	3.46E-09 4.31E-06 6.98E-10	1.86E-09 8.20E-07 8.89E-09	NO DATA NO DATA	3.42E-09 9.76E-06 1.06E-08	NO DATA NO DATA 3.42E-10	2.10E-05 9.99E-06 4.13E-07
TC101 30103 R0105	2.546-10 1.85E-07 1.54E-08	3.66E-10 NO DATA NU DATA	3.59E-09 7.97E-08 6.08E-09	NO DATA NO DATA	6.59E-09 7.06E-07 1.99E-07	1.87E-10 NO DATA NO DATA	1.10E-21 2.16E-05 9.42E-06
RU106	2.75F-06	NO DATA	3.48E-07	NC 031A	5.31E-06	NO DATA	1.78E-04
AG110M	1.60E-07	1.48E-27	8.79E-08	30 DATA	2.91E-07	NO DATA	6.04E-05
TE125M	2.69E-06	2.71E-07	3.59E-07	8.06F-37	1.09E-05	NO DATA	1.07E-05
TE127M	6.77E-06	2.42E-06	8.25E-07	1.73E-05	2.75E-05	NO DATA	2.27E-05
TE127	1.10E-07	3.95E-08	2.38E-08	8.15E-08	4.48E-07	NO DATA	8.68E-06
TE129M	1.15E-05	4.29E-06	1.82E-06	3.95E-06	4.80E-05	NO DATA	5.79E-05
fE129	3.14E-08	1.186-08	7.65E-09	2.41E-08	1.32E-07	NO DATA	2.37E-08
TE131M	1.73E-06	8.465-07	7.05E-07	1.34E-06	8.57E-06	NO DATA	8.40E-05
TE131	1.97E-08	8.235-09	6.22E-09	1.62E-08	9.63E-08	NO DATA	2.79E-09
16132	2.52E-06	1.63E-06	1.53E-06	1.80E-06	1.57E-05	NO DATA	7.71E-05
1 130	7.56E-07	2.23E-06	8.80E-07	1.89E-04	3.48E-06	NO DATA	1.92E-06
1 131	4.16E-06	5.95E-06	3.41E-06	1.95E-03	1.02E-05	NO DATA	1.57E-06
1 132	2.03E-07	5.43F-07	1.90E-07	1.90E-05	8.65E-07	NO DATA	1.02E-07
1 133	1.42E-06	2.47E-06	7.53E-07	3.63E-04	4.31E-06	NO DATA	2.22E-06
1 134	1.06E-07	2.88E-07	1.03E-07	4.99E-06	4.58E-07	NO DATA	2.51E-10
1 135	4.43E-07	1.166-06	4.29E-07	7.65E-05	1.86E-06	NO DATA	1.31E-06
CS134	6.22E-05	1.480-04	1.21E-04	NO DATA	4.79E-05	1.59E-05	2.59E-06
CS136	6.51E-06	2.576-05	1.85E-05	NO DATA	1.43E-05	1.96E-06	2.92E-06
CS137	7.97E-05	1.69E-04	7.14E-05	NO DATA	3.70E-05	1.23E-05	2.11E-06
CS138	5.52E-08	1.69E-07	5.40E-08	NO DATA	8.01E-08	7.91E-09	4.65E-13
BA139	9.70E-08	6.91ê-11	2.84E-09	NO DATA	6.46E-11	3.92E-11	1.72E-07

TABLE 7.1-E-11 (Cont'd)

NUCL 11 E	BONE	LIVER	T.BODY	THYROID	KIDNEY	LUNG	GI-LLI
3A140	2.030-05	2.555-08	1.336-06	ATAG DATA	8.67E-09	1.46E-08	4.18E-05
0A141	4.71E-08	3.565-11	1.57E-09		3.31E-11	2.02E-11	2.22E-17
9A142	2.13E-08	2.135-11	1.34E-09		1.95E-11	1.24E-11	3.00E-26
LA140	Z.50(-09	1.2607	3.330-10	NO DATA	NC DATA	NO DATA	9.25E-05
LA142	1.280-10	5.821-11	1.455-11	NO DATA	NC DATA	NO DATA	4.25E-07
CE141	9.366-09	6.335-09	7.19E-10	NO DATA	2.94E-09	NO DATA	2.42E-05
CE143	1.65E-07	1.22F-06	1.35E-10	NO DATA	5.37E-10	NO DATA	4.56E-05
CE144	4.88E-07	2.04E-07	2.62E-08	NO DATA	1.21E-07	NO DATA	1.65E-04
PR143	9.20E-09	3.69E-09	4.56E-10	NO DATA	2.13E-09	NO DATA	4.03E-05
PR144	3.01E-11	1.255-11	1.53E-12	NO DATA	7.05E-12	NO DATA	4.33E-18
VD147	6.29E-09	7.276-09	4.35E-10	NO DATA	4.25E-09	NO DATA	3.49E-05
W 197	1.03E-07	5.616-08	3.01E-28	NO DATA	NO DATA	NO DATA	2.82E-05
NP239	1.176-07	1.175-10	6.458-11	WO DATA	3.65E-10	NO DATA	2.408-05

TABLE 7.1-E-14

INGESTION DOSE FACTORS FOR INFANTS

(mrem per pCi Ingested)

WELTEL	BONE	LIVER	T. difficY	THY3010	KIONEY	LUNG	CI-FFI
H 3	NG DATA	3.08°-07	3.636-07	\$.696-07	3.08t-07	3.G8C-07	3.08E-07
L 14	2.376-05	5.06F+06	5.066-06	\$.066-06	5.06t-06	5.06F-06	5.06E-06
NA 24	1.016-05	1.01C-09	1.016-95	1.616-05	1.01t-05	1.01E-05	1.01E-05
H 32	1.706-03	1.000-04	6.59 -05	7.200 UATA	NC DATA	NO DATA	2.30E-05
CR 51	NO UATA	NO DATA	1.41s-08	7.200-09	2.01E-09	1.79E-08	4.11E-07
MN 54	NO DATA	1.995-05	3.51E-06	7.200 OM	4.41E-06	NO DATA	7.31E-06
MN 56	NU DATA	8.18L-07	1.41F-07	NO DATA	7.03E-07	NO DATA	7.43F-05
FE 55	1.39E-05	8.18L-06	2.46E-06	NO DATA	NG DATA	4.39E-06	1.14E-06
FE 59	3.08E-05	5.382-05	2 12E-05	NO CATA	NO DATA	1.59E-05	2.57F-05
CO 58	NO DATA	3.60r-06	8.931-06	NO DATA	VO DATA	NO DATA	8.97E-06
CO 60	NO DATA	1.08r-05	2.55E-05	NO DATA	VC DATA	NO DATA	2.57E-05
NI 61	6.34E-54	3.92r-05	2.20E-05	NO DATA	VO DATA	NO DATA	1.95E-06
71 67 00 64 ZN 67	4.70E-06 VO DATA 1.34E-05	5.325-07 6.091-07 6.311-05	2.42c-07 2.82E-07 2.91E-05	NO DATA NO DATA	1.03E-06 1.06E-05	NO DATA NO DATA NO DATA	4.05E-05 1.25E-05 5.33E-05
ZN 67	9 33E-08	1.08E-07	1.25f-09	NO BATA	6.38E-08	NO DATA	1.37F-05
IR 83	DATA	NO DATA	3.63f-07	NO BATA	NO DATA	NO DATA	Lf E-24
BR 84	NO DATA	NO DATA	3.82f-07	NO DATA	NO DATA	NO DATA	Lf E-24
88 As 88 Bs 88 Bs	NO DATA NO DATA	NO DATA 1.703+04 4.986-07	1.94E-08 8.4JE-05 2.73E-07	NO DATA NO DATA NO DATA	NO DATA NO DATA NO DATA	NO DATA NO DATA NO DATA	LT E-24 4.35E-06 4.85F-07
9P 99	NO DATA	2.86E-07	1.97E-37	NO DATA	NO DATA	NO DATA	9.74E-08
SR 89	2.516-03	NG DATA	7.20E-05	NO DATA	NO DATA	NO DATA	5.16E-05
SR 90	1.856-02	NU DATA	4.71E-03	NO DATA	NO DATA	NO DATA	2.31E-04
SR 91	5.00E-05	NU DATA	1.81E-06	NO DATA	NO DATA	NO DATA	5.92E-05
SR 92	1.92E-05	NU DATA	7.13E-07	NO DATA	NO DATA	NO DATA	2.07E-04
Y 90	8.69E-08	NU DATA	2.33E-09	NO DATA	NO DATA	NO DATA	1.20E-04
Y 91M Y 91 Y 92	8.10E-10 1.13E-06 7.65E-09	NO DATA NO DATA NO DATA	2.76F-11 3.01E-08 2.15E-10	NO DATA NO DATA	NU DATA NO DATA NO DATA	NO DATA NO DATA NO DATA	2.70F-06 8.10E-05 1.46E-04

TABLE 7.1-E-14 (Cont'd)

NUCLICE	BONE	LIVER	T.000Y	THYRDIO	KIDNEY	LUNG	GI-LLI
Y 93	2.43E-08	NO DATA	6.62F-10	NO DATA	YO DATA	NO DATA	1.92F-04
ZR 95	2.06E-07	5.02E-08	3.56E-58	NO DATA	5.41E-08	NO DATA	2.50F-05
ZR 97	1.48E-08	2.54E-09	1.16E-09	NO DATA	2.56E-09	NO DATA	1.62F-04
VB 95	4.20E-08	1.73E-08	1.00E-08	NO DATA	1.24E-08	NO DATA	1.46E-05
MO 99	NO DATA	3.402-05	6.63E-06	NO DATA	5.08E-05	NO DATA	1.12E-05
TC 93M	1.92E-09	3.963-09	5.10E-08	NO DATA	4.26E-08	2.07E-09	1.15E-06
fC101	2.27E-09	2.86E-09	2.83E-08	NO DATA	3.40E-08	1.56E-09	4.80E-07
RU103	1.48E-06	NO UATA	4.95E-07	NO DATA	3.08E-06	NO DATA	1.80E-05
RU105	1.36E-07	NO DATA	4.53E-08	NO DATA	1.00E-06	NO DATA	5.41E-05
QU106	2.415-05	NO DATA	3.01F-06	NO DATA	2.85E-05	NO DATA	1.83F-04
AG110M	9.76E-07	7.275-07	4.81E-07	NO DATA	1.04E-06	NO DATA	3.77E-05
TE125M	2.33E-05	7.795-06	3.15E-06	7.84E-06	NO DATA	NO DATA	1.11E-05
TE127M	5.85E-05	1.94E-05	7.08E-06	1.67E-05	1.44E-04	NO DATA	2.36E-05
TE127	1.00E-06	3.35E-07	2.15E-07	8.14E-67	2.44E-06	NO DATA	2.10E-05
TE127	1.00E-04	3.43E-05	1.54E-05	3.84E-05	2.50E-04	NO DATA	5.97E-05
TE129	2.84E-07	9.77E-08	6.63E-08	2.38E-07	7.07E-07	ATAG ON	2.27E-05
TE131*	1.52E-05	6.12E-06	5.05E-06	1.24E-05	4.21E-05	ATAG ON	1.03E-04
TE131	1.76E-07	6.50E-08	4.94E-08	1.57E-07	4.50E-07	ATAG ON	7.11E-06
fE132	2.08E-05	1.03E-05	9.61E-06	1.52F-05	6.44E-05	NO DATA	3.81E-05
f 130	6.00E-06	1.32E-05	5.30E-06	1.48E-03	1.45E-05	NO DATA	2.83E-06
f 131	3.59E-05	4.23E-05	1.86E-05	1.39F-02	4.94E-05	NO DATA	1.51E-06
1 132 1 133 1 134	1.66E-06 1.25E-05 8.69E-07	3.37E-06 1.82F-05 1.78E-06	1.20E-06 5.33E-06 6.33E-07	1.58E+04 3.31E-03 4.15E-05	3.76E-06 2.14E-05 1.99E-06	NO DATA NO DATA	2.73E-06 3.08E-06 1.84E-06
1 135 CS134 CS136	3.64E-06 3.77E-04 4.59E-05	7.24E-06 7.03E-04 1.35E-04	7.10E-05 5.04E-05	6.49E-04 NO DATA NO DATA	8.07E-06 1.81E-04 5.38L-05	NO DATA 7.42E-05 1.10E-05	2.62E-06 1.71E-06 2.05E-06
C 137	5.22E-04	6.11E-04	4.13E+05	NO DATA	1.64E-04	6.64E-05	1.91E-06
CS138	4.81E-07	7.82E-07	3.77E+07	NO DATA	3.90E-07	6.09E-08	1. 5E-06
BA139	8.81E-07	5.84E-10	2.55E-08	NO DATA	3.51E-10	3.54E-1C	5.58E-05

TABLE 7.1-E-14 (Cont'd)

VUCLIUE	BONE	LIVER	T. ACDY	THYROLO	KIDNEY	LUNG	GI-LLI
3A140 PA141	1.71E-04 4.25E-07	1.716-07 2.715-10	9.815-06 1.346-08	NO DATA	4.06E-08 1.75E-10	1.05E-G7 1.77F-10	4.20E-05 5.19E-06
HA142	1.845-07	1.536-10	9.068-09	NO DATA	8-816-11	7.268-11	7.59E-07
LA140 LA142	2.11E-08 1.10E-09	8.322-09 4.04E-10	2.14E-09 9.67F-11	NO DATA	NO DATA	NO DATA	9.77F-05 6.86F-05
CE141	7.87E-08	4.807-08	5.650-09	NO DATA	1.486-08	NO DATA	2.48E-05
CE144	1.48E-08 2.98E-06	1.226-06	1.17E-09 1.67E-07	NO DATA	2.86E-09 4.93E-07	NO DATA	5.73E-05 1.71E-04
PR143	8.13E-08	3.641-08	4.03E-09	NO DATA	1.136-08	NO DATA	4.298-05
PR144	2.74E-10 5.53E-08	1.06E-10 5.68E-68	1.336-11	NO DATA	3.84E-11 2.19E-08	NO DATA	4.93E-05 3.60E-05
w 187	9.03E-07	6.280-07	7.176-07	NO DATA	NO DATA	NO DATA	3.69E-05
NP233	******	9.93E-10	2 4 0 1 1 - 1 0	YU URIA	1.98E-09	NO DATA	2.878-05

TABLE 7.1-2

MISCELLANEOUS DOSE ASSESSMENT FACTORS - ADULT

 $U_a^M = 310 \text{ liters/yr}$

 $R_a = 8000 \text{ m}^3/\text{yr}$

 $U_a^P = 520 \text{ kg/yr}$

 $U_a^V = 64 \text{ kg/yr}$

 $U_a^F = 110 \text{ kg/yr}$

 $f_{p} = .76$

 $f_{V} = 1.0$

 $t_h = 0$ for pasture grass (milk and meat pathways)

 $t_h = 24 \text{ hr } (1 \text{ day for leafy vegetables})$

 $t_h = 1440 \text{ hr (60 days for produce)}$

 t_h = 2160 hr for stored feed (milk and meat pathways)

 $t_e = 720 \text{ hr} (30 \text{ days for milk and meat})$

t = 1440 hr (60 days for produce or leafy vegetables)

f_f = 1.0 May-October

 $f_f = 0.0 \text{ November-April}$

 $f_{q} = 0.5$

 $\lambda_w = .0021 \text{ hr}^{-1}$

TABLE 7.1-2 (Cont'd)

 $Y_v = 2.0 \text{ kg/m}^2$ for leafy vegetables and produce pathways

 $Y_v = 0.7 \text{ kg/m}^2$ for milk and meat pathways

 $t_{s} = 480 \text{ hr } (20 \text{ days})$

r = 1.0 (iodines)

0.2 (others)

 $W_f = 50 \text{ kg/day}$

 $t_M = 48 \text{ hr } (2 \text{ days})$

TABLE 7.1-3

MISCELLANEOUS DOSE ASSESSMENT FACTORS - INFANT

U^M = 330 liters/yr

 $u_{a}^{P}, u_{a}^{V}, u_{a}^{F} = 0$

 $R_a = 1400 \text{ m}^3/\text{yr}$

 $W_f = 50 \text{ kg/day}$

r = 1.0 (iodines)* 0.2 (others)

 $t_{M} = 48 \text{ hr } (2 \text{ days})$

 $\lambda_{w} = 0.0021 \text{ hr}^{-1}$

 $Y_{v} = 0.7 \text{ kg/m}^2$

t = 720 hours

th = 0 for pasture grass (milk pathway)

t_h = 2160 hr (stored feed and milk pathway)

f = 1.0 May-October

f = 0.0 November-April

 $f_{q} = 0.5$

K = 0.5 May-October

K = 0.0 November-April

^{*}The r factor provides for the non-deposition on grass of the organic forms of iodine.

TABLE 7.1-4
STABLE ELEMENT TRANSFER DATA*

	F	F _M (Cow)		
Element	Meat (d/kg)	Milk (d/l)		
Н	1.2E-02	1.0E-02		
C	3.1E-02	1.2E-02		
Na	3.0E-02	4.0E-02		
P	4.6E-02	2.5E-02		
Cr	2.4E-03	2.2E-03		
Mrs	8.0E-04	2.5E-04		
Fe	4.0E-02	1.2E-03		
Co	1.3E-02	1.0E-03		
Ni .	5.3E-02	6.7E-03		
Cu	8.0E-03	1.4E-02		
Zn	3.0E-02	3.9E-02		
Rb	3.1E-02	3.0E-02		
Sr	6.0E-04	8.0E-04		
Y	4.6E-03	1.0E-05		
Zr	3.4E-02	5.0E-06		
Nb	2.8E-01	2.5E-03		
Mo	8.0E-03	7.5E-03		
Tc	4.0E-01	2.5E-02		
Res	4.0E-01	1.0E-06		
Rh	1.5E-03	1.0E-02		
Ag	1.7E-02	5.0E-02		
Te	7.7E-02	1.0E-03		
I	2.9E-03	6.0E-03		
Cs	4.0E-03	1.2E-02		
Ва	3.2E-03	4.0E-04		
La	2.0E-04	5.0E-06		
Ce	1.2E-03	1.0E-04		
Pr	4.7E-03	5.0E-06		
Nd	3.3E-03	5.0E-06		
W	1.3E-03	5.0E-04		
Np	2.0E-04	5.0E-06		
Br	2.9E-03**	1.4E-02***		

^{*}Data presented in this table are from NRC Regulatory Guide 1.109, Revision 1, (Reference 6.5), October 1977.

^{**}Used value for I (no literature available).

^{***}W. C. Ng, "Transfer Coefficients for Prediction of the Dose to Man Via the Forage-Cow-Milk Pathway From Radionuclides Released to the Biosphere," UCRL-51939.

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TABLE 7.1-5
ATMOSPHERIC STABILITY CLASSES

DESCRIPTION	PASQUILL STABILITY CLASS	(SEE NOTE, BELOW)	TEMPERATURE CHANGE WITH HEIGHT (°C/100 m)
Extremely Unstable	A	>22.5°	<1.9
Moderately Unstable	В	17.5° to 22.5°	-1.9 to -1.7
Slightly Unstable	С	12.5° to 17.5°	-1.7 to -1.5
Neutral	D	7.5° to 12.5°	-1.5 to -0.5
Slightly Stable	Е	3.8° to 7.5°	-0.5 to 1.5
Moderately Stable	F	2.1° to 3.8°	1.5 to 4.0
Extremely Stable	G	0° to 2.1°	>4.0

NOTE: σ_{θ} is the standard deviation of horizontal wind direction fluctuation over a period of 15 minutes to 1 hour.

TABLE 7.1-6

WIND SENSOR THRESHOLD

LOCATION	ANEMOMETER WIND SPEED (mph)	VANE WIND DIRECTION (mph)
Dresden	0.8	0.9
Quad Cities	0.6	0.8
Zion	0.5	0.7
LaSalle	0.5	0.7
Braidwood	0.8	0.8
Byron	0.8	0.8
Carroll County	0.5	0.7

TABLE 7.1-7
HORIZONTAL AND VERTICAL DISPERSION PARAMETERS*

Horizontal Dispersion Parameters, σ_{y} , meters**

$$\sigma_y = aR^b$$

R = downwind range, meters

STATILITY CLASS	a	b
A	0.3658	0.9031
В	0.2751	0.9031
С	0.2089	0.9031
D	0.1471	0.9031
Е	0.1046	0.9031
F	0.0722	0.9031
G	0.0481	0.9031

Vertical Dispersion Parameters, $\sigma_{\rm Z}$, meters**

$$\sigma_z = aR^b + C$$

STABILITY	100 -	R < 100	00	R > 1000			
CLASS	a	ь	С		b	C	
A	0.00066	1.941	9.27	0.00024	2.094	- 9.6	
В	0.0382	1.149	3.3	0.055	1.098	2.0	
С	0.113	0.911	0.0	0.113	0.911	0.0	
D	0.222	0.725	-1.7	1.26	0.516	-13.0	
Е	0.211	0.678	-1.3	6.73	0.305	-34.0	
F	0.086	0.74	-0.35	18.05	0.18	-48.6	
G	0.052	0.74	-0.21	10.83	0.18	-29.2	

^{*}From Reference 6.21.

^{**}Values of $\sigma_{_{\mbox{\scriptsize y}}}$ and $\sigma_{_{\mbox{\scriptsize Z}}}$ are also limited to a maximum of 1000 meters.

AND 1.5 303.75

303.75 AND LE 326.25

326.25 AND LE 348.75

281.25

TABLE 7.1-8

WIND SPEED AND WIND DIRECTION CLASSES

Wind Direction Classes

				WITTE	01100		-				
			(050)	N	WIND	DIRECTION	GT	348.75	AND	LE	11.25
	DIRECTION		(DEG)			DIRECTION	GT	11.25	AND	LE	33.75
	DIRECTION		(DEG)	NNE			GT	33.75	AND	LE	56.25
WIND	DIRECTION	CLASS	(DEG)	NE		DIRECTION		56.25	AND	LE	78.75
WIND	DIRECTION	CLASS	(DEG)	ENE		DIRECTION	GT				101.25
	DIRECTION		(DEG	E		DIRECTION	GT	78.75	AND	LE	
	DIRECTION		(DEG)	ESE	WIND	DIRECTION	GT	101.25	AND	LE	123.75
	DIRECTION		(DEG)	SE	WIND	DIRECTION	GT	123.75	AND	LE	146.25
	DIRECTION		(DEG)	SSE	WIND	DIRECTION	GT	146.25	AND	LE	168.75
			(DEG)	S		DIRECTION	GT	168.75	AND	LE	191.25
	DIRECTION			SSW		DIRECTION	GT	191.25	AND	LE	213.75
	DIRECTION		(DEG)	-		DIRECTION	GT	213.75	AND	LE	236.25
	DIRECTION		(DEG)	SW			GT	236.25	AND	LE	258.75
WIND	DIRECTION	CLASS	(DEG)	WSW		DIRECTION		258.75	AND	LE	281.25
WIND	DIRECTION	CLASS	(DEG)	W		DIRECTION	GT	281.25	AND	15	303.75
	The same of the sa	the same and the same	/mmal	N 75.11 F	S. F. E. A. I. P.	DIDECTION	CT	101 17	25 FE L	Disk Kin	303113

NW

NNW

WIND DIRECTION GT

WIND DIRECTION GT

WIND DIRECTION GT

		ř	lind Speed	Classes					
WIND SPEED CLASS	(MPH)	1	WIND SP		GE GE	0.0 ST	AND	LT LE	ST* 3.5
WIND SPEED CLASS WIND SPEED CLASS	(MPH) (MPH)	3	WIND SP WIND SP	EED	GT	3.5	AND	LE	7.5
WIND SPEED CLASS	(MPH)	5	WIND SP WIND SP	EED	GT	12.5	AND	LE	18.5
WIND SPEED CLASS	(MPH) (MPH) (MPH)	7	WIND SP WIND SP	EED	GT GT	24.5	AND	LE	31.5
WIND SPEED CLASS WIND SPEED CLASS WIND SPEED CLASS	(MPH) (MPH)	9	WIND SP WIND SP	EED	GT GT	38.5	AND AND	LE	46.5

WIND DIRECTION CLASS (DEG) WNW

WIND DIRECTION CLASS (DEG)

WIND DIRECTION CLASS (DEG)

^{*} ST: Speed Threshold Value

AIRBORNE ISOTOPE DATA

Isotope	Decay* Constant (1/hr)	Average Per Disinte	egration	Linear Energy Absorption in air	Absorption Attenuation		Tissue Energy ** Absorption Coeff.
	$^{\lambda}\mathbf{i}$	$\overline{\mathbb{E}}_{G}$	$\overline{\mathbb{E}}_{\mathrm{B}}$	ua (1/meter)	(1/meter) =	u - ua ua	(cm²/g)
Kr-83m	3.79E-1	2.58E-3	3.82E-2	37	37	0	4.87
Kr-85	7.38E-6	2.23E-3	2.51E-1	50	50	0	4.87
Kr-85m	1.55E-1	1.58E-1	2.55E-1	0.0033	0.017	4.15	0.0279
Kr-87	5.45E-1	8.04E-1	1.33	0.0037	0.0092	1.49	0.0318
Kr-88	2.44E-1	1.98	3.49E-1	0.0031	0.0058	0.87	0.0259
7 Kr-89	1.31E+1	1.71	1.31	0.0029	0.0054	0.86	0.0251
2 Kr-90	7.72E+1	1.25	1.30	0.003	0.0056	0.87	0.0254
Xe-131 ^m	2.43E-3	2.00E-2	1.42E-1	0.065	0.098	0.51	0.533
Xe-133	5.51E-3	4.60E-2	1.35E-1	0.0066	0.028	3.24	0.0566
Xe-133 ^m	1.32E-2	4.15E-2	1.90E-1	0.0076	0.03	2.95	0.0574
Xe-135	7.63E-2	2.48E-1	3.17E-1	0.0036	0.015	3.17	0.0305
Xe-135m	2.66E+0	4.31E-1	9.58E-2	0.0038	0.012	2.16	0.0326 ≥ ₹
Xe-137	1.09E+1	1.82E-1	1.78	0.0035	0.016	3.57	0.0293 GUIS
Xe-138	2.93E+0	1.13	6.32E-1	0.0035	0.0075	1.14	0.0293 REVISION AUGUST 19
Ar-41	3.79E-1	1.28	4.64E-1	0.0034	0.0072	1.12	0.030 882

^{*}Computed from data in Reference 6.8

AOther values from Radiological Health Handbook, Revised Edition, January 1970.

^{**} The Constants (ut) were obtained from Radiation Dosimetry, Vol. I, Attix and Roesch, editors, 1958, Academic Press (Table XXII).

TABLE 7.1-10

MAXIMUM PERMISSIBLE CONCENTRATION OF DISSOLVED OR ENTRAINED NOBLE GASES RELEASED FROM THE SITE TO UNRESTRICTED AREAS IN LIQUID WASTE

NUCL	IDE
Kr 85	m
85	
87	
88	
Ar 41	
Xe 131	m
133	m
133	
135	m
135	

^{*}Computed from Equation 20 of ICRP Publication 2 (1959), adjusted for infinite cloud submersion in water, and R = 0.01 rem/week, $\rho_{\rm W}$ = 1.0 gm/cm³, and $P_{\rm W}/P_{\rm t}$ = 1.0.

TABLE 7.1-11

LISTING OF RADIOLOGICAL DECAY CONSTANTS $(\lambda_{i})^{\Delta}$

ISOTOPE	DECAY CONSTANT λ_{j} (hrs-1) *
H-3 C-14 Na-24 P-32 Cr-51 Mn-56 Fe-55 Fe-59 Co-60 Ni-65 Cu-64 Zn-65 Zn-69 Br-83 Br-84 Br-85 Rb-86 Rb-88 Rb-89 Sr-90 Sr-91 Sr-92 Y-90 Y-91 Y-92 Y-93 Zr-97 Nb-95	5.40E-6 1.38E-8 4.52E-3 1.04E-3 1.024E-3 1.024E-3 1.024E-3 1.024E-3 1.024E-4 1.53E-4 1.53E-4 1.55E-3 1.45E-4 1.45E-4 1.55E-3 1.45E-4 1.55E-3 1.45E-4 1.55E-3 1.45E-1 1.55E-3 1.45E-1 1.55E-3 1.64E-4 1.55E-3 1.64E-4 1.65E-4
Mo-99 Tc-99M Tc-101 Ru-103 Ru-105	1.05E-2 1.15E-1 2.93E+0 7.34E-4 1.56E-1

TABLE 7.1-11 (Cont'd)

ISOTOPE	DECAY CONSTANT \[\lambda_1 \left(\text{hrs}^{-1} \right) \]*
Ru-106	7.84E-5
Ag-110M	1.15E-4
Te-125M	1.15E-4 4.98E-4
Te-127M	2.65E-4
Te-127	7.41E-2
Te-129M	8.59E-4
Te-129	5.97E-1
Te-131M	2.31E-2
ma 101	1.66E+0
Te-131 Te-132 I-130 I-131 I-132	8.86E-3
I-130	
I-131	3.59E-3
I-132	5.61E-2 3.59E-3 3.01E-1 3.33E-2
I-133	
I-134	7.90E-1
I-135	1.05E-1
Cs-134	3.83E-5
Cs-136	2.20E-3
Cs-137	2.62E-6
Cs-138	1.29E+0
Ba-139	5.03E-1 2.26E-3
Ba-140	2.26E-3
Ba-141	2.28E+0
Ba-142	3.89E+0
La-140	1.72E-2
La-142	4.49E-1
Ce-141	8.88E-4
Ce-143	2.10E-2
Ce-144	1.02E-4
Pr-143	2.13E-3
Pr-144	2.41E+0
Nd-147	2.61E-3
W-187	2.90E-2
Np-239	1.23E-2
Sb-124	6.94E-4

^{*} λ_i = Radiological Decay Constant
Ti = Radiological Half-life
 (from Reference 6.8) λ_i = .693 / Ti
 Δ For unlisted nuclides, see References 6.8 and 6.9.

TABLE 7.1-12

BIOACCUMULATION FACTORS TO BE USED IN THE ABSENCE OF SITE-SPECIFIC DATA (pCi/kg per pCi/liter)*

ELEMENT	FRESHWATER FISH		
Н	9.0E-01		
C	4.6E+03		
Na	1.0E+02		
P	1.0E+05		
Cr	2.0E+02		
Mn	4.0E+02		
Fe	1.0E+02		
Co	5.0E+01		
Ni	1.0E+02		
Cu	5.0E+01		
Zn	2.0E+03		
Br	4.2E+02		
Rb	2.0E+03		
Sr	3.0E+01		
Y	2.5E+01		
Zr	3.3E+00		
Nb	3.0E+04		
Mo	1.0E+01		
Tc	1.5E+01		
Ru	1.0E+01		
Rh	1.0E+01		
Te	4.0E+02		
I	1.5E+01		
Cs	2.0E+03		
Ba	4.0E+00		
La	2.5E+01		
Ce	1.0E+00		
Pr	2.5E+01		
Nd	2.5E+01		
W	1.2E+03		
Np	1.0E+01		
Ag	2.3E+00**		

^{*} Table A-1, of Reference 6.5.

^{**} S. E. Thompson, "Concentration Factors of Chemical Elements in Edible Aquatic Organisms," UCRL-50564, Revision 1, 1972.

TABLE 7.1-13 DOSE FACTORS FOR EXPOSURE TO A SEMI-INFINITE CLOUD OF NOBLE GASES*

	BETA AIR DOSE FACTOR L	BETA SKIN DOSE FACTOR $\bar{\mathbb{L}}_{\mathbf{i}}$	GAMMA AIR DOSE FACTOR X ₁	GAMMA WHOLE BODY DOSE FACTOR \bar{x}_i
NUCLIDE	ad/yr per uCi/m3)	(mrem/yr per µCi/m ³)	$(mrad/yr per \mu Ci/m^3)$	(mrem/yr per µCi/m ³)
Kr-83m	2.88E+02 **		1.93E+01	7.56E-02
Kr-85m	1.97E+03	1.46E+03	1.23E+03	1.17E+03
Kr-85	1.95E+03	1.34E+03	1.72E+01	1.61E+01
Kr-87	1.03E+04	9.73E+03	6.17E+03	5.92E+03
Kr-88	2.93E+03	2.37E+03	1.52E+04	1.47E+04
Kr-89	1.06E+04	1.01E+04	1.73E+04	1.66E+04
Kr-90	7.83E+03	7.29E+03	1.63E+04	1.56E+04
Xe-131m	1.11E+03	4.76E+02	1.56E+02	9.15E+01
Xe-133m	1.48E+03	9.94E+02	3.27E+02	2.51E+02
Xe-133	1.05E+03	3.06E+02	3.53E+02	2.94E+02
Xe-135m	7.39E+02	7.11E+02	3.36E+03	3.12E+03
Xe-135	2.46E+03	1.86E+03	.92E+03	7.81E+03
Xe-137	1.27E+04	1.22E+04	1.51E+03	1.42E+03
Xe-138	4.75E+03	4.13E+03	9.21E+03	8.83E+03
Ar-41	3.28E+03	2.69E+03	9.30E+03	8.84E+03
Gr-999***	4.00E+03	4.00E+03	6.37E+03	5.43E+03

^{*} From Table B-1 of Reference 6.5. ** 2.88E+02 = 2.88 x 10².

^{***} Parameters to assess a "gross" noble gas release, $\bar{E}_{\gamma}\sim$ 0.8 MeV, $\bar{E}_{\beta}\sim$ 0.56 MeV.

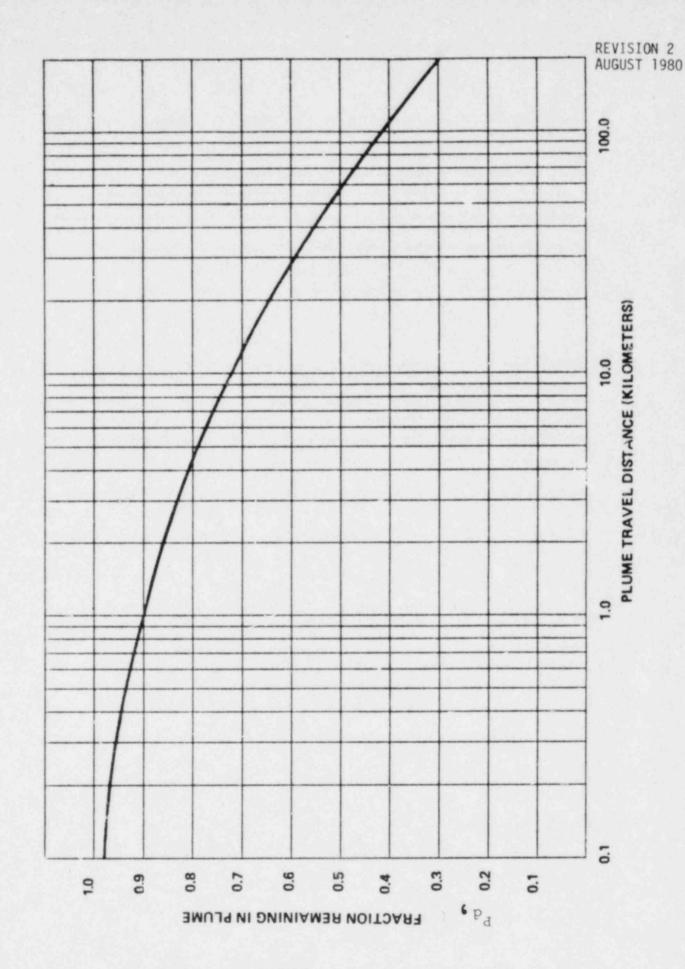
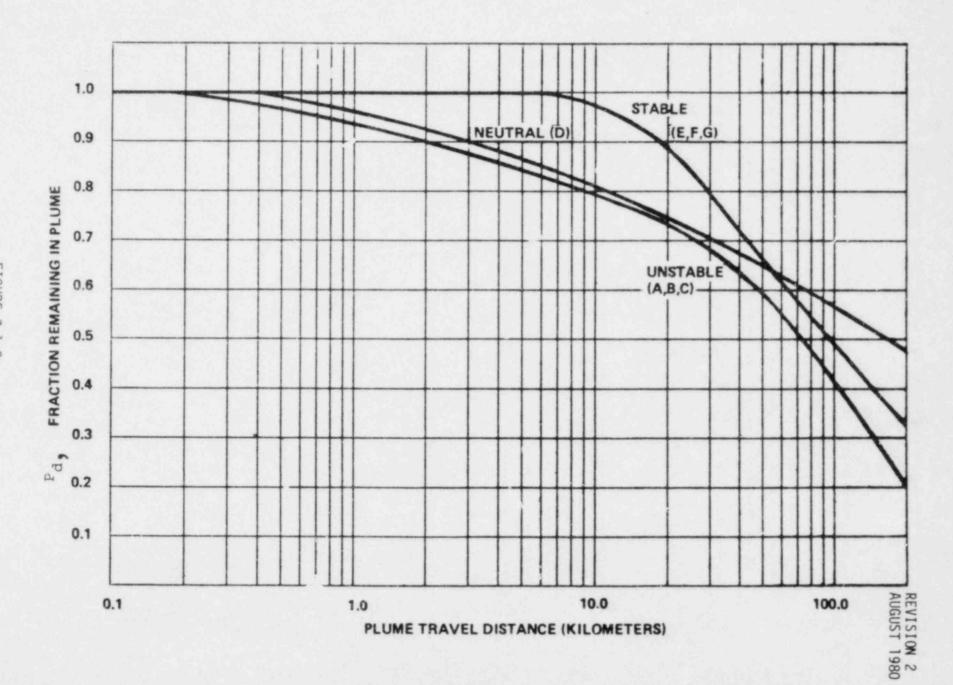


FIGURE 7.1-1

PLUME DEPLETION EFFECT FOR GROUND-LEVEL RELEASES
(ALL ATMOSPHERIC STABILITY CLASSES)
(FROM FIGURE 2 OF REFERENCE 6.4)



PLUME DEPLETION EFFECT FOR 30m RELEASES (LETTERS DENOTE PASQUILL STABILITY CLASSES) (FROM FIGURE 3 OF REFERENCE 6.4)

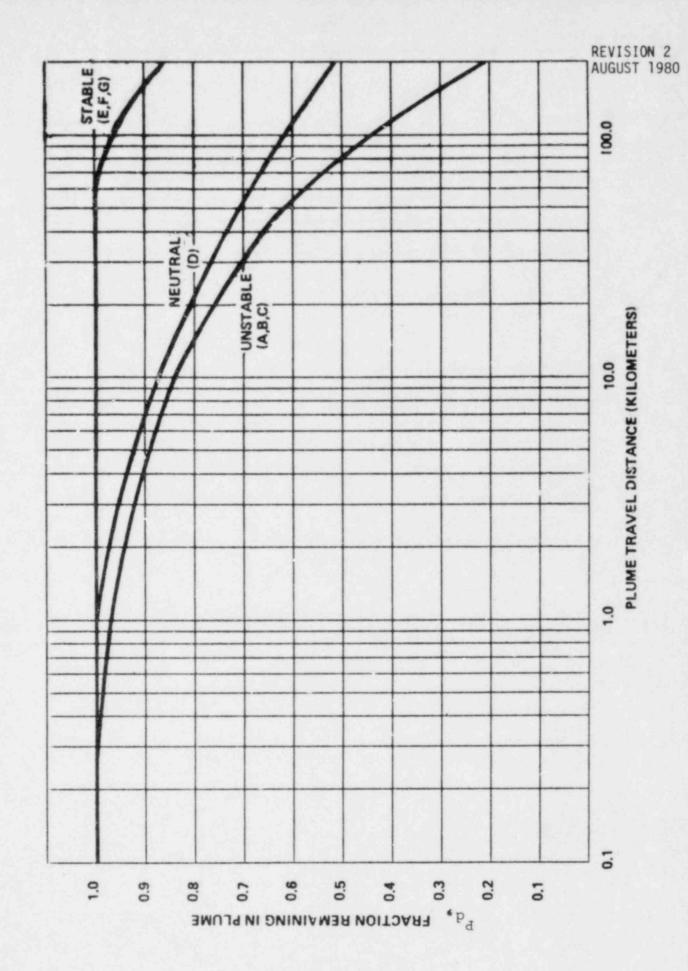


FIGURE 7.1-3

PLUME DEPLETION EFFECT FOR 60m RELEASES (LETTERS DENOTE PASQUILL STABILITY CLASSES) (FROM FIGURE 4 OF REFERENCE 6.4)

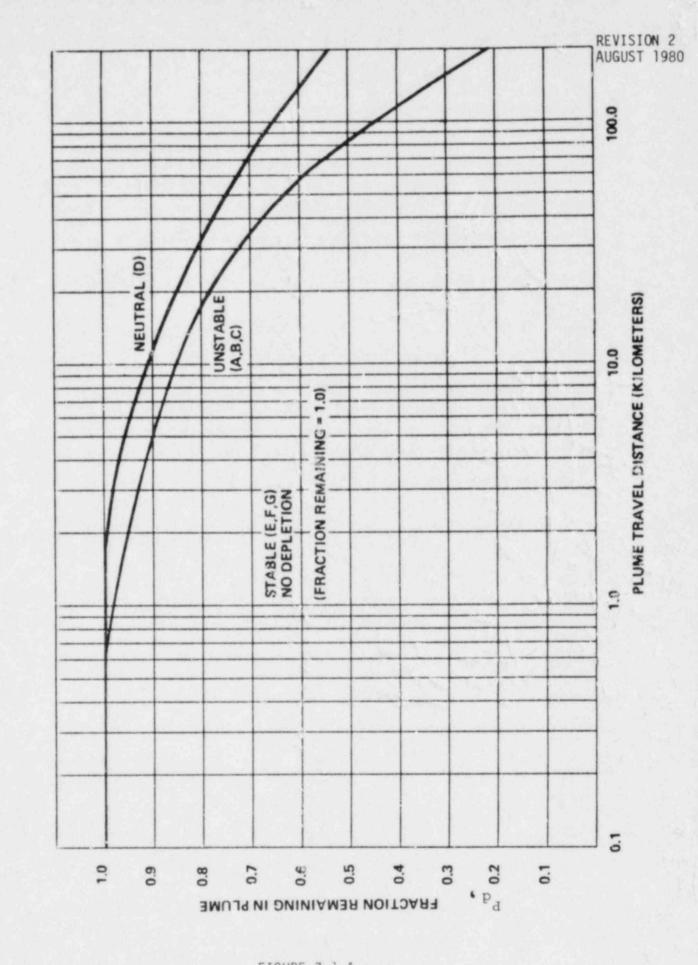


FIGURE 7.1-4

PLUME DEPLETION EFFECT FOR 100m RELEASES (LETTERS DENOTE PASQUILL STABILITY CLASSES) (FROM FIGURE 5 OF REFERENCE 6.4)

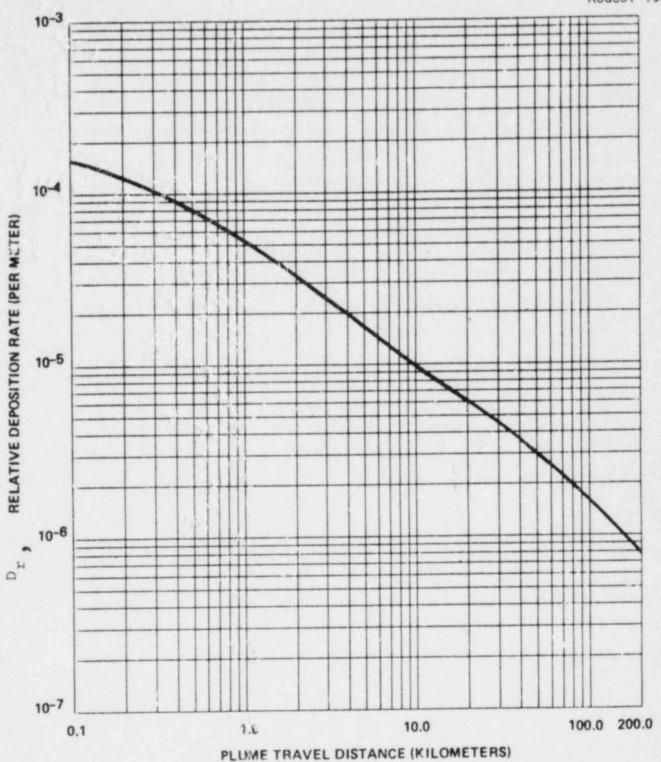


FIGURE 7.1-5

RELATIVE DEPOSITION FOR GROUND-LEVEL RELEASES
(ALL ATMOSPHERIC STABILITY CLASSES)
(FROM FIGURE 6 OF REFERENCE 6.4)

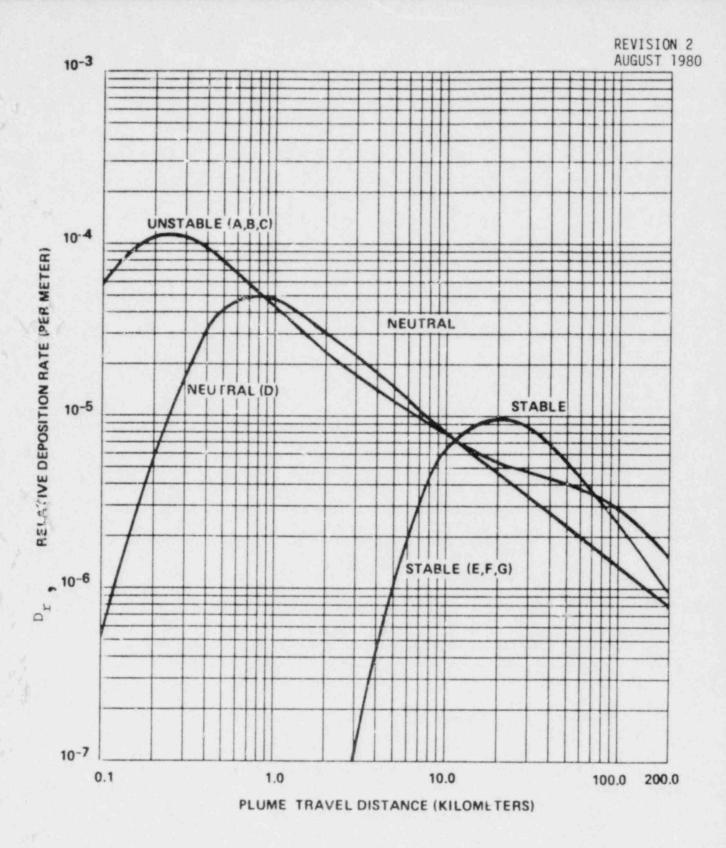


FIGURE 7.1-6

RELATIVE DEPOSITION FOR 30m RELEASES
(LETTERS DENOTE PASQUILL STABILITY CLASS)
(FROM FIGURE 7 OF REFERENCE 6.4)

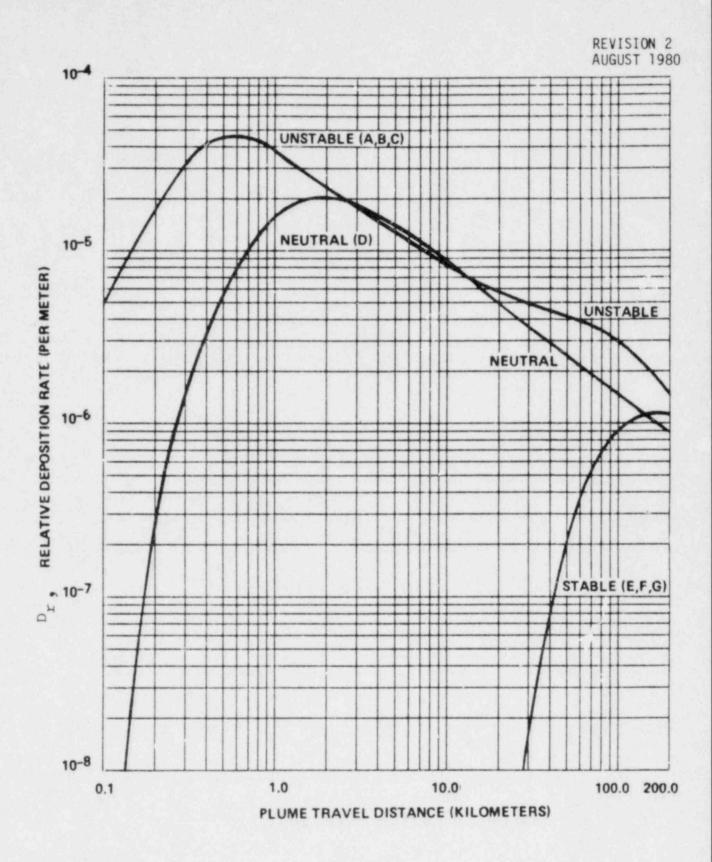


FIGURE 7.1-7

RELATIVE DEPOSITION FOR 60m RELEASES
(LETTERS DENOTE PASQUILL STABILITY CLASS)
(FROM FIGURE 8 OF REFERENCE 6.4)

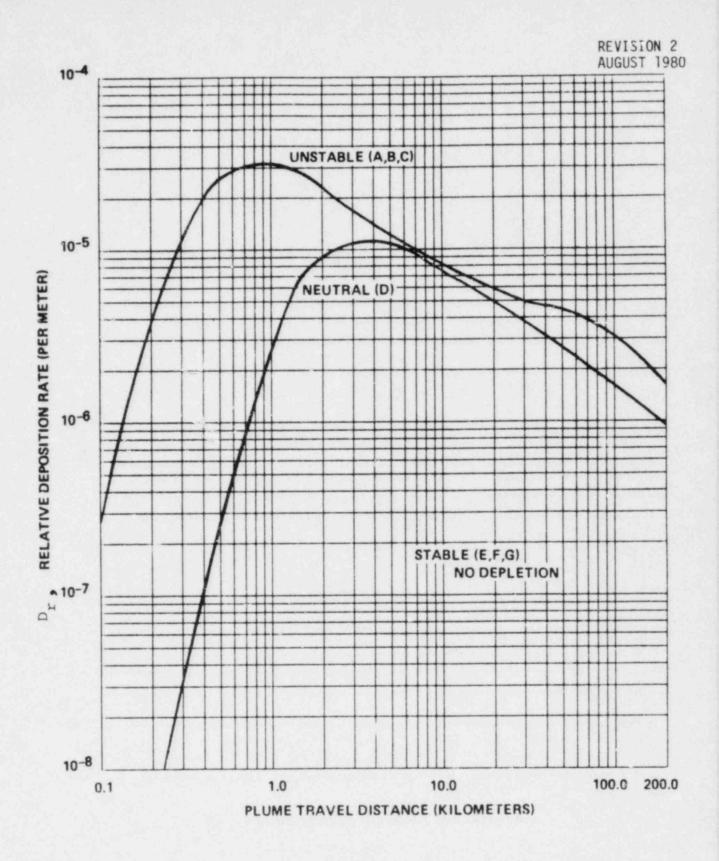


FIGURE 7.1-8

RELATIVE DEPOSITION FOR 100m RELEASES
(LETTERS DENOTE PASQUILL STABILITY CLASS)
(FROM FIGURE 9 OF REFERENCE 6.4)

REVISION 2 AUGUST 1980

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LIST OF FIGURES FOR SECTION 7.2

NUMBER

TITLE

7.2-1

Unrestricted Area Boundary

7.2 DATA SPECIFIC TO EACH STATION

This section contains site descriptions and data (particularly meteorological data) that is relevant only to a specific site.

TABLE 7.2-1

AQUATIC ENVIRONMENT DOSE PARAMETERS

PARAMETER	LA SALLE			
UW, water usage, liters/hr	0.042			
Uf, fish consumption, kg/hr	2.4×10^{-4}			
1/M ^W	1			
1/M ^f	1			
F ^W , ft ³ /sec	1.37×10^4			
F ^f , ft ³ /sec	1.37 x 10 ⁴			
t ^f , hr*	24			
tw, hr**	97			

B - Regulatory Guide 1.109, Revision 1, October 1977, Table A-1, Column 2 for freshwater fish. See Table 7.1-12.

Not Applicable. No outdoor tanks without overflow pipes connected to other storage tanks.

^{*}tf (hr) = 24 hr (all stations) for the fish ingestion pathway

^{**}tW (hr) = 97 hr (distance to Peoria is 97 miles; flow rate of 1 mph assumed)

TABLE 7.2-2

ANNUAL DESIGN OBJECTIVES SET BY 10 CFR 50, APPENDIX I FOR EACH REACTOR

TYPE OF DOSE

ANNUAL DESIGN OBJECTIVES

Airborne Releases

Gamma Air Dose	10 mrad
Beta Air Dose	20 mrad
Whole Body Dose	5 mrem
Skin Dose	15 mrem
Infant Thyroid Dose	15 mrem

Liquid Releases

Whole Body Dose	3	mrem
Thyroid Dose	10	mrem
Bone Dose	10	mrem
Skin Dose	10	mrem

TABLE 7.2-3

STATION: La Salle	INDUL	7.2-3		
LOCATION: 6 miles south	of Marseilles, Illi	nois - La Salle C	ounty	
CHARACTERISTICS OF ELEVA	TED RELEASE POINT			
1) Release Height =	112.8 m	2) Diameter =	5.6	m
2) Exit Speed =	18.3 ms ⁻¹	4) Heat Content = _	1.1E4	KCal s ⁻¹
CHARACTERISTICS OF VENT	STACK RELEASE POINT	(NA)		
1) Release Height =	m	2) Diameter =		m
3) Exit Speed =	ms - 1			
 Release Height = 0 Building Factor (D 		m		
METEODOLOGICAL DATA				
METEOROLOGICAL DATA A 400 ft. Tower	is Located 300	m SSW	of elevated	release p
Tower Data Used in Calcu	lations			
Release Point	Wind Speed and Direction		fferential mperature	
Elevated	375 ft		375-33 ft	
Vent	(NA)		(NA)	
Ground	33 ft		200-33 ft	

TABLE 7.2-4

CRITICAL RANGES

Direction	Site Boundary (m)	Nearest Resident (m)	Nearest Dairy Farm Range * (m)
N	1022	6155	
NNE	1330	2253	
NE	2408	3058	
ENE	4450	5311	
E	1996	5150	8047
ESE	838	2948	
SE	884	2736	
SSE	838	4506	
S	829	966	
SSW	829	2736	
SW	610	1609	
WSW	509	1448	
W	509	1448	
WNW	625	1448	
NW	732	2736	
NNW	848	2414	

^{*}Within 5 miles

TABLE 7.2-5

TERRAIN CORRECTION FACTORS (ht)*

 $(h_t = 0 \text{ to Stated Range, Then } h_t = Given Value)$

DIRECTION	RANGE	<u>ht</u>
N	-	0
NNE		0
NE		0
ENE		0
E		0
		0
SE		0
SSE	8.5 mi	13m
S	0.9 m2	0
SSW		17m
SW	1.5 mi	
WSW	1.0 mi	17m
W	1.0 mi	17m
WWW	1.0 mi	17m
NM	2.75 mi	17m
NNW		0

^{*} Within 10 miles

TABLE 7.2-6

X/Q AND D/Q MAXIMA AT DR BEYOND THE UNRESTRICTED AREA BOUNDARY

DOWNWIND	E	LEVATED(STAC	CK) RELEAS	E	MIXED MODE (VENT) RELEASE			GROUND LEVEL RELEASE		
DIRECTION	RADIUS (METERS)	X/Q+ (SEC/M**3)	RADIUS (METERS)	D/Q∆ (1/M**2)	RADIUS (METERS)	X/Q+ (SEC/M**3)	D/Q △ (1/M**2)	(METERS)	(SEC/M**3)	D/Q \(\(1/M**2 \)
N	2800.	2.552-08	1022.	9.928-10	1022	1.179-07	2.654-09	1022.	9.073-07	1.190-08
NNE	3000.	2.446-08	1330.	8.077-10		8.105-08	1.786-09	1330.	6.512-07	7.358-09
NE	2600.	2.420-08	2408.	4.660-10	2408.	4.772-08	7.377-10		2.444-07	2.349-09
ENE	4450.	2.374-08	4450.	2.845-10	4450.	3.055-08			9.947-08	8.018-10
E	2800.	3.322-08	1996.	8.853-10	1996.	6.215-08	1.328-09	1996.	3.575-07	3.941-09
ESE	2800.	3.199-08	838.	1.107-09	838.	1.522-07	3.538-09	838.	1.267-06	1.708-08
SE	2800	2.207-08	884.	6.366-10	884.	9.527-08	2.005-09	884.	8.673-07	1.052-08
SSE	3000.	2.234-08	1000	4.681-10	838.	7.312-08	1.506-09	838.	9.195-07	8.921-09
S	2600.	2.248-08	829.	5.442-10	829.	6.32€-08	1.272-09	829.	7.524-07	7.582-09
SSW	2800.	2.775-08	829.	7.249-10	829.	5.667-08	1.355-09	829.	9.809-07	7.715-09
SW	2600.	2.486-08	610.	9.944-10		9.495-08	2.336-09	610.	1.403-06	1.372-08
WSW	2800	1.986-08	509	8.853-10	509.	1.144-07	2.673-09	509.	1.345-06	1.643-08
W	509.	1.751-08	509	8, 196-10		1.255-07	2.657-09	509.	1.459-06	1.573-08
WNW	2800.	1.404-08	625.	4.956-10		9.074-08	1.777-09	625.	9.893-07	1.102-08
NW	3000	2.156-08	732	5.425-10		9.384-08	1.901-09	732.	1.247-06	1.128-08
NNW	3000.	1.856-08	348.	7.826-10		9.261-08		848.	9.930-07	1.048-08

⁺ Beta air, beta skin, and inhalation dose pathways.

 $[\]boldsymbol{\Delta}$ Produce and leafy vegetable pathways.

LA SALLE COUNTY 1&2

AVERAGE WIND SPEED FOR EACH RELEASE MODE

Downwind Direction	Wind Speed (m/sec) Elevated Release
N	8.2
NNE	8.2
NE	7.9
ENE	7.7
E.	8.0
ESE	8.2
SE	7.5
SSE	6.8
S	6.1
SSW	5.5
SW	6.1
WSW	6.6
W	6.9
WNW	6.9
NW	7.1
NNW	7.7

TABLE 7.2-7

D/Q AT THE NEAREST MILK COW AND MEAT ANIMAL LOCATIONS WITHIN 5 MILES

DOWNWIND NEAREST MILK COW D/Q(1/M++2)						NEAREST MEAT ANIMAL D/Q(1/M**2)					
DIRECTION	RADIUS	ELEVATED	MIXED	GROUND	RADIUS	ELEVATED	MIXED	GROUND			
	(METERS)	RELEASE	RELEASE	RELEASE	(METERS)	RELEASE	RELEASE	RELEASE			
N	8047.	1.244-10	1.566-10	3.299-10	2253.	6.165-10	9.949-10	3.075-09			
NNE	8047.	1.133-10	1,454-10	3.196-10	2275.	5.751-10	9.306-10	2.929-09			
NE	8047	9.414-11	1.223-10	2.833-10	3219.	3.389-10	4.954-10	1.414-09			
ENE	8047.	1.192-10	1.419-10	2.5 17-10	4506.	2.803-10	3.506-10	7.847-10			
E	8047.	1.633-10	1.891-10	3.419-10	5150.	3.241-10	3.863-10	7.539-10			
ESE	8047.	1.603-10	1.885- 0	3.445-10	4345.	3.896-10	4.864-10	1.022-09			
SE	8047.	1.018-10	1.195-10	2.309-10	4345.	2.470-10	3.071-10	6.851-10			
SSE	8047.	9.203-11	1.026-10	1.799-10	5472.	1.663-10	1.891-10	3.557-10			
5	8047.	8.057-11	8.809-11	1.503-10	2575.	3.381-10	4.188-10	1.108-09			
SSW	8047.	8.487-11	9.057-11	1.529-10	2897.	3.325-10	3.836-10	9.167-10			
SW	8047.	9.830-11	1.050-10	1.669-10	1287.	6.657-10	1.024-09	4.064-09			
WSW	8047.	7.451-11	8.355-11	1.498-10	1448.	4.907-10	7.794-10	2.984-09			
W	8047.	5.574-11	6.705-11	1.435-10	1770.	3.618-10	5.698-10	2.030-09			
WNW	8047.	5.588-11	6.623-11	1.393-10	1609.	3.171-10	5.624-10	2.318-09			
NW	8047.	7.190-11	8.684-11	1.834-10	1609.	3.896-10	7.292-10	3.051-09			
NNW	8047.	8.559-11	1.041-10	2.153-10	1287.	5.964-10	1.243-09	5.242-09			

TABLE 7.2-8

LASALLE COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 83M

DOWNWIND RESTRICT		CTED ELEVATED(STACK) RELEASE				MIXED MODE (VENT) RELEASE			GROUND LEVEL RELEASE		
DIRECTION	AREA BOUND (METERS)	RADIUS (METERS)	S (MRAD/YR)/(SEAR	(METERS)	(MRAD/YR)/(VBAR UCI/SEC)	(METERS)	(MRAD/YR)/(GBAR UCI/SEC)	
N	1022.	1022.	2.556-06	2.308-07		1.388-05 9.525-06	1.253-06 8.601-07	1022.	9.844-05 6.766-05	8.889-06 6.109-06	
NNE NE	1330.	1330.	2.265-06	2.045-07		4.842-06	4.372-07	2408.	2.489-05	2.248-06	
ENE	4450.	4450.	2.038-06	1.841-07		2.754-06 6.632-06	2.485-07 5.988-07	4450. 1996.	8.937-06 3.579-05	8.070-07	
ESE	1996. 838.	1996.	3.246-06	2.740-07		1.808-05	1.633-00	838.	1.373-04	1.240-05	
SE	884.	884.	1.965-06	1.775-07		1.136-05 8.950-06	8.082-07	884.	9.472-05	8.553-06	
SSE	838.	838. 829.	1.627-06	1.470-07		7.535-06	6.804-07	829.	8.048-05	7.268-06	
SSW	329.	829.	2.392-06	2.160-07		7.049-06 1.132-05	6.365-07	829. 610.	1.004-04	9.065-06	
SW WSW	610. 509.	610. 509.	2.563-06	2.314-07		1.386-05	1.252-06	509.	1.542-04	1,792-05	
W	509.	509.	2.369-06	2.140-07		1.484-05	9.686-07	509. 625.	1.624-04	1.466-05 9.937-06	
NM	625. 732.	625. 732.	1.799-06	1.625-07		1.133-05	1.023-06	732.	1.320-04	1.192-05	
NNW	848.	848.	1.968-06	1.777-07	848.	1.108-05	1.000-06	848.	1.048-04	9.466-06	

LASALLE COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 85M

DOWNWIND RESTRICTED		ELEVATED(STACK) RELEASE			MIXED MODE (VENT) RELEASE			GROUND LEVEL RELEASE		
	AREA BOUND	RADIUS	S	SBAR	RADIUS	V	VBAR	RADIUS	G	GBAR
	(METERS)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)
N	1022.	1022.	1.438-04	7.665-05	1022.	1.940-04	1.022-04	1022.	5.816-04	2.999-04
NNE	1330.	1330.	1.145-04	6.100-05	1330.	1.473-04	7.775-05	1330.	4.292-04	2.217-04
NE	2408.	2408.	6.027-05	3.197-05	2408.	7.299-05	3.849-05	2408.	1.787-04	9.267-05
ENE	4450.	4450.	3.374-05	1.780-05	4450.	3.794-05	1.996-05	4450.	7.695-05	4.007-05
E	1996.	1996.	8.722-05	4.628-05	1996.	1.047-04	5.527-05	1996.	2.617-04	1.358-04
ESE	838.	838.	1.915-04	1.021-04	838.	2.585-04	1.363-04	838.	8.036-04	4.141-04
SE	884	884.	1.292-04	6.887-05	884.	1.708-04	9.010-05	884.	5.459-04	2.812-04
SSE	838.	838.	1.299-04	6.933-05	838.	1.628-04	8.607-05	838	5.638-04	2.904-04
S	829	829.	1.221-04	6.507-05	829.	1.456-04	7.705-05	829.	4.859-04	2.507-04
SSW	829.	829.	1.514-04	8.070-05	829.	1.730-04	9.176-05	829.	6.214-04	3.205-04
SW	610.	610.	1.875-04	1.000-04	610.	2.264-04	1.198-04	610.	8.484-04	4.363-04
WSW	509.	509.	1.723-04	9.191-05	509.	2.204-04	1.164-04	509.	8.171-04	4.196-04
W	509.	509.	1.682-04	8.973-05	509.	2.181-04	1.150-04	509.	8.254-04	4.230-04
WNW	625.	625.	1.246-04	6.647-05	625.	1.616-04	8.527-05	625.	5.801-04	2.978-04
NW	732.	732.	1.572-04	8.391-05	732.	1.976-04	1.044-04	732.	7.297-04	3.750-04
NNW	848.	848.	1.327-04	7.076-05	848.	1.720-04	9.078-05	848.	5.865-04	3.015-04

LASALLE COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 85

		EL EVAT	EDICTACK) DE	LEASE	MIXED !	MODE (VENT) R	ELEASE	GROUN	ND LEVEL REL	EASE
DOWNWIND	RESTRICTED AREA BOUND (METERS)	RADIUS (METERS)	ED(STACK) RE S (MRAD/YP)/(SBAR	RADIUS (METERS)	V (MRAD/YE)/(VBAR UCI/SEC)	RADIUS (METERS)	G (MRAD/YR)/	GBAR (UCI/SEC)
N NNE NE ENE ESE SSE SSW SSW WSW WNW NW	1022 . 1330 . 2408 . 4450 . 1996 . 838 . 884 . 838 . 829 . 829 . 610 . 509 . 509 . 625 . 732 .	1022 1330 2408 4450 1996 838 884 838 829 610 509 625 732 848	1.881-06 1.511-06 8.049-07 4.736-07 1.162-06 2.505-06 1.684-06 1.716-06 1.597-06 2.014-06 2.472-06 2.254-06 2.212-06 1.625-06 2.084-06	1.164-06 9.355-07 4.982-07 2.931-07 7.193-07 1.550-06 1.062-06 9.885-07 1.247-06 1.530-06 1.395-06 1.369-06 1.290-06	1330. 2408. 4450. 1996. 838. 884. 838. 829. 610. 509. 625. 732.	2.390-06 1.846-06 9.347-07 5.161-07 1.339-06 2.109-06 2.052-06 1.837-06 2.236-06 2.866-06 2.742-06 2.719-06 2.002-06 2.496-06 2.148-06	1.479-06 1.143-06 5.786-07 3.195-07 8.288-07 1.974-06 1.305-06 1.270-06 1.137-06 1.384-06 1.774-06 1.697-06 1.683-06 1.239-06 1.545-06 1.330-06	1022. 1330. 2408. 4450. 1996. 838. 884. 838. 829. 610. 509. 625. 732. 848.	6.395-06 4.827-06 2.045-06 9.484-07 2.993-06 8.870-06 5.982-06 6.290-06 5.385-06 7.013-06 9.339-06 8.869-06 8.993-06 6.313-06 8.111-06 6.504-06	5.567-06 3.908-06

LASALLE COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 87

DOWNWIND	RESTRICTED	ELEVAT	ED(STACK) RE	LEASE	MIXED #	MODE (VENT) R	ELEASE	GROUP	ND LEVEL REL	CORNEL CONTRACTOR CONT
DIRECTION		RADIUS	S	SBAR	RADIUS	V	VBAR	RADIUS	G	GBAR
	(METERS)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)
N	1022.	1022	6.081-04	4.444-04	1022.	7.471-04	5.442-04	1022.	1.780-03	1.285-03
NNE	1330.	1330.	4.687-04	3.424-04	1330	5.593-04	4.074-04	1330.	1.287-03	9.295-04
NE	2408	2408.	2.356-04	1.720-04	2408.	2.700-04	1.966-04	2408.	5.395-04	3.899-04
ENE	4450.	4450.	1.236-04	9.011-05	4450.	1.344-04	9.784-05	4450.	2.247-04	1.626-04
CHE	1996.	1996.	3.445-04	2.514-04	1996.	3.916-04	2.853-04	1996.	7.848-04	5.673-04
ESE	838.	838.	8.102-04	5.923-04	838.	9.967-04	7.261-04	838.	2.451-03	1.769-03
SE	884.	884.	5.514-04	4.031-04	884.	6.671-04	4.861-04	884.	1.679-03	1.212-03
SSE	838.	838.	5.399-04	3.947-04	838.	6.312-04	4.602-04	838.	1.672-03	1.207-03
235	829.	829.	5.106-04	3.732-04	829	5.758-04	4.200-04	829.	1.484-03	1.071-03
SSW	829.	829.	6.131-04	4.481-04		6.730-04	4.911-04	829.	1.813-03	1.308-03
SW	610.	610.	7.946-04	5.809-04	610.	9.027-04	6.584-04	610.	2.543-03	1.836-03
WSW	509.	509.	7.514-04	5.494-04		8.860-04	6.460-04	509.	2.511-03	1.813-03
W	509.	509.	7.274-04	5.319-04	509.	8.676-04	6.326-04	509.	2.510-03	1.811-03
WNW	625.	625.	5.393-04	3.944-04	625.	6.429-04	4.687-04	625.	1.784-03	1.288-03
NW	732.	732.	6.563-04	4.799-04	732.	7.693-04	5.610-04	732.	2.157-03	1.557-03
NNW	848.	848.	5.580-04	4.080-04	849.	6.677-04	4.867-04	848.	1.754-03	1.266-03

LASALLE COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 88

DOWNWIND	RESTRICTED	ELEVAT	ED(STACK) RE	LEASE	MIXED	MODE (VENT) R	ELEASE	The state of the s	ND LEVEL REL	
DIRECTION	AREA BOUND	RADIUS	S	SBAR	RADIUS	V	VBAR	RADIUS	G (MD + D (VD) / (GBAR
-	(METERS)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)
N	1022.	1022	1.526-03	1.177-03	1022.	1.841-03	1.415-03	1022.	4.243-03	3.229-03
NNE	1330.	1330.	1.193-03	9.205-04	1330.	1.399-03	1.076-03	1330.	3.130-03	2.383-03
NE	2408.	2408.	6.086-04	4.690-04	2408.	6.873-04	5.285 04	2408.	1.328-03	1.013-03
ENE	4450.	4450	3.292-04	2.534-04	4450.	3.544-04	2.725-04	4450.	5.809-04	4.437-04
E	1996	1996.	8.846-04	6.817-04	1996.	9.921-04	7.620-04	1996.	1.936-03	1.476-03
ESE	838.	838.	2.040-03	1.574-03	838.	2.461-03	1.892-03	838.	5.843-03	4.446-03
SE	884.	884.	1.379-03	1.064-03	884.	1.641-03	1.262-03	884.	3.977-03	3.025-03
SSE	838.	838.	1.381-03	1.066-03	838.	1.587-03	1.221-03	838.	4.061-03	3.090-03
S	829.	829	1.291-03	9.963-04	829.	1.439-03	1.107-03	829.	3.546-03	2.699-03
SSW	829.	829.	1.592-03	1.228-03	829.	1.727-03	1.330-03	829.	4.469-03	3.401-03
SW	610.	610.	2.009-03	1.550-03	610.	2.252-03	1.734-03	610.	6.116-03	4.651-03
WSW	509.	509	1.868-03	1.442-03	503.	2.173-03	1.672-03	509.	5.919-03	4.500-03
W	509.	509.	1.823-03	1.407-03	509.	2.140-03	1.646-03	509.	5.961-03	4.530-03
WNW	625.	625.	1.344-03	1.038-03	625.	1.579-03	1.214-03	625.	4.210-03	3.201-03
NW	732.	732.	1.682-03	1.299-03		1.938-03	1.491-03	732.	5.239-03	3.983-03
NNW	848.	848.	1.417-03	1.093-03		1.664-03	1.280-03	848.	4.237-03	3.223-03

TABLE 7.2-8 (Cont'd)

LASALLE COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 89

DOWNWIND	RESTRICTED	ELEVATI	ED(STACK) RE	LEASE	MIXED !	MODE (VENT) R	ELEASE	GROUN	ND LEVEL REL	EASE
DIRECTION	AREA BOUND	RADIUS	S	SBAR	RADIUS	V	VBAR	RADIUS	G	GBAR
	(METERS)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)
N	1022.	1022.	6.786-04	5.005-04	1022.	8.728-04	6.410-04	1022.	1.992-03	1.450-03
NNE	1330.	1330.	4.270-04	3.149-04	1330.	5.392-04	3.960-04	1330.	1.170-03	8.519-04
NE	2408.	2408.	1.232-04	9.078-05	2408.	1.504-04	1.105-04	2408.	2.940-04	2.142-04
ENE	4450.	4450.	2.630-05	1.935-05	4450.	2.999-05	2.202-05	4450.	4.808-05	3.510-05
E	1996.	1996.	2.265-04	1.669-04	1996.	2.703-04	1.985-04	1996.	5.104-04	3.720-04
ESE	838.	838.	9.713-04	7.165-04	838.	1.250-03	9.180-04	838.	2.915-03	2.123-03
SE	884.	884.	6.310-04	4.655-04	884.	7.964-04	5.851-04	884.	1.910-03	1.390-03
SSE	838.	838.	5.533-04	4.082-04	838.	6.826-04	5.017-04	838.	1.665-03	1.212-03
S	829.	829.	4.984-04	3.676-04	829.	5.891-04	4.332-04	829.	1.462-03	1.064-03
SSW	829.	829.	5.179-04	3.820-04	829.	5.982-04	4.400-04	829.	1.478-03	1.076-03
SW	610.	610.	8.875-04	6.547-04	610.	1.055-03	7.756-04	610.	2.731-03	1.989-03
WSW	509.	509.	9.934-04	7.330-04	509.	1.215-03	8.937-04	509.	3.258-03	2.372-03
W	509.	509.	9.133-04	6.739-04	509.	1.147-03	8.434-04	509.	3.113-03	2.266-03
WNW	625.	625.	6.671-04	4.923-04	625.	8.308-04	6.107-04	625.	2.201-03	1.602-03
NW	732.	732.	6.690-04	4.936-04	732.	8.424-04	6.191-04	732.	2.157-03	1.570-03
NNW	848.	848.	6.055-04	4.467-04	848.	7.674-04	5.638-04	848.	1.843-03	1.342-03

TABLE 7.2-8 (Cont'd)

LASALLE COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR KR 90

COLUMNITATIO	RESTRICTED	FLEVATI	ED(STACK) RE	LEASE	MIXED !	MODE (VENT) R	ELEASE	designation of the latest and the la	ND LEVEL REL	
DIRECTION	The second secon	RADIUS (METERS)	S (MRAD/YR)/(SBAR	RADIUS (METERS)	(MRAD/YR)/(VBAR UC1/SEC)	(METERS)	(MRAD/YR)/(GBAR UCI/SEC)
N NNE ENE E SE E S S S S S S S S S S S S	1022 1330 2408 4450 1996 838 884 838 829 610 509 625 732	1022 1330 2408 4450 1996 838 884 838 829 610 509 509 625 732	9.738-05 3.526-05 1.552-06 1.111-08 5.791-06 1.961-04 9.875-05 8.074-05 5.836-05 5.203-05 1.724-04 2.701-04 2.640-04 1.462-04 1.268-04	6.981-05 2.527-05 1.112-06 7.939-09 4.144-06 1.406-04 7.080-05 5.789-05 4.134-05 3.729-05 1.236-04 1.937-04 1.893-04 1.048-04 9.097-05	1330. 2408. 4450. 1996. 838. 884. 838. 829. 610. 509. 625.	1.348-04 4.800-05 2.017-06 1.299-08 7.210-06 2.685-04 1.340-04 1.070-04 7.640-05 6.493-05 2.240-04 3.623-04 3.658-04 2.021-04 1.787-04	9.601-05 3.419-05 1.437-06 9.260-09 5.137-06 1.913-04 9.549-05 7.649-05 4.631-05 1.597-04 2.583-04 2.607-04 1.440-04 1.273-04	610. 509. 509. 625. 732.	3.031-04 1.036-04 3.976-06 2.081-08 1.332-05 6.073-04 3.078-04 2.496-04 1.775-04 1.480-04 5.466-04 9.256-04 9.490-04 5.095-04 4.373-04 3.368-04	2.138-04 7.307-05 2.808-06 1.473-08 9.416-06 4.284-04 1.760-04 1.752-04 1.045-04 3.855-04 6.526-04 6.690-04 3.083-04 2.376-04

LASALLE COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR XE131M

DOWNWIND	RESTRICTED	ELEVAT	ED(STACK) RE	LEASE	MIXED I	MODE (VENT) R	RELEASE	GROU	ND LEVEL REL	EASE
DIRECTION	(METERS)	(METERS)	S (MRAD/YR)/(SBAR UCI/SEC)	(METERS)	V (MRAD/YR)/(VBAR UCI/SEC)	RADIUS (METERS)	G (MRAD/YR)/(GBAR UCI/SEC)
N	1022.	1022.	5.171-06	1.843-06	1022.	1.506-05	3.184-06	1022.	9.205-05	1.366-05
NNE	1330.	1330.	4.426-06	1.509-06	1330.	1.072-05	2.371-06	1330.	6.609-05	9.985-06
NE	2408.	2408.	3.332-06	8.918-07	2408.	5.649-06	1.216-06	2408.	2.488-05	3.942-06
ENE	4450.	4450.	2.663-06	5.844-07	4450.	3.338-06	6.840-07	4450.	1.013-05	1.694-06
Ε	1996.	1996.	4.682-06	1.274-06	1996.	7.730-06	1.708-06	1996.	3.641-05	5.777-06
ESE	838.	838.	6.599-06	2.431-06	838.	1.972-05	4.214-06	938.	1.286-04	1.900-05
SE	884.	884.	4.388-06	1.629-06	884.	1.259-05	2.741-06	884	8.763-05	1.291-05
SSE	838.	838.	4.146-06	1.632-06	838.	1.055-05	2.503-06	838.	9.261-05	1.361-05
S	829.	829.	4.589-06	1.587-06	829.	9.154-06	2.209-06	829.	7.573-05	1.132-05
SSW	829.	829.	5.308-06	1.957-06	829.	9.403-06	2.520-06	829.	9.912-05	1.479-05
SW	610.	610.	6.104-06	2.351-06	610.	1.374-05	3.387-06	610.	1.430-04	2.073-05
WSW	509.	509.	5.500-06	2.134-06	509.	1.548-05	3.462-06	509.	1.401-04	2.007-05
W	509.	509.	5.506-06	2.103-06	509.	1.623-05	3.512-06	509.	1.483-04	2.090-05
WNW	625.	625.	4.112-06	1.557-06	625.	1.183-05	2.582-06	625.	1.001-04	1.431-05
NW	732.	732.	4.795-06	1.955-06	732.	1.314-05	3.067-06	732.	1.258-04	1.812-05
NNW	848.	848.	4.456-06	1.680-06	848.	1.238-05	2.745-06	848.	9.977-05	1.443-05

TABLE 7.2-8 (Cont'd)

LASALLE COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR XE133M

DOWNWIND	RESTRICTED	ELEVAT	ED(STACK) RE	LEASE	MIXED !	MODE (VENT)	RELEASE	GROUP	NE LEVEL REL	EASE
DIRECTION	(METERS)	(METERS)	S (MRAD/YR)/(SBAR UCI/SEC)	(METERS)	(MRAD/YR)/	VBAR (UCI/SEC)	(METERS)	(MRAL/YR)/(GBAR UCI/SEC)
N	1022.	1022.	2.274-05	1.121-05	1022	3.868-05	1.563-05	1022.	1.631-04	5.029-05
NNE	1330.	1330.	1.857-05	9.044-06	1330.	2.883-05	1.192-05	1330.	1.192-04	3.744-05
NE	2408.	2408.	1.089-05	4.904-06	2408.	1.475-05	6.017-06	2408.	4.715-05	1.550-05
ENE	4450.	4450.	7.061-06	2.909-06	4450.	8.249-06	3.274-06	4450.	2.021-05	6.943-06
E	1996.	1996.	1.557-05	7.054-06	1996.	2.074-05	8.576-06	1996.	6.908-05	2.276-05
ESE	838.	838.	3.001-05	1.491-05	838.	5.121-05	2.080-05	838.	2.268-04	6.963-05
SE	884.	884.	2.011-05	1.001-05	884.	3.334-05	1.368-05	884.	1.541-04	4.713-05
SSE	838.	838.	2.016-05	1.016-05	838.	3.052-05	1.306-05	838.	1.622-04	4.948-05
S	829.	829.	1.955-05	9.559-06	829.	2.695-05	1.162-05	829.	1.352-04	4.198-05
SSW	829.	829.	2.412-05	1.199-05	829.	3.083-05	1.388-05	829.	1.764-04	5.471-05
SW	610.	610.	2.904-05	1.459-05	610.	4.136-05	1.801-05	610.	2.470-04	7.424-05
WSW	509.	509.	2.639-05	1.328-05	509.	4.216-05	1.754-05	509.	2.392-04	7.096-05
W	509.	509.	2.598-05	1.302-05	509.	4.271-05	1.747-05	509.	2.488-04	7.242-05
WNW	625.	625.	1.924-05	9.626-06	625.	3.141-05	1.291-05	625.	1.706-04	5.046-05
NW	732.	732.	2.417-05	1.230-05	732.	3.738-05	1.588-05	732.	2.158-04	6.441-05
NNW	848.	848.	2.074-05	1.036-05	848.	3.340-05	1.384-05	848.	1.719-04	5.155-05

TABLE 7.2-8 (Cont'd)

LASALLE COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR XE133

DOWNWIND	RESTRICTED	ELEVATI	ED(STACK) RE	LEASE	MIXED	MODE (VENT) R	ELEASE	GROU	NO LEVEL REL	EASE
DIRECTION	AREA BOUND	RADIUS	S	SBAR	RADIUS	V	VBAR	RADIUS	G	GBAR
	(METERS)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)
N	1022.	1022.	2.329-05	9.006-06	1022.	4.138-05	1.403-05	1022.	1.830-04	5.346-05
NNE	1330.	1330.	1.928-05	7.397-06	1330.	3.098-05	1.067-05	1330.	1.345-04	3.978-05
NE	2408.	2408.	1.163-05	4.236-06	2408.	1.607-05	5.502-06	2408.	5.352-05	1.527-05
ENE	4450.	4450.	7.840-06	2.709-06	4450.	9.213-06	3.114-06	4450.	2.308-05	7.199-06
E	1996.	1996.	1.666-05	6.095-06	1996.	2.263-05	7.818-06	1996.	7.857-05	2.392-05
ESE	838.	838.	3.074-05	1.196-05	838.	5.482-05	1.865-05	838	2.545-04	7.416-05
SE	884.	884.	2.058-05	8.019-06	884.	3.559-05	1.218-05	884.	1.725-04	5.012-05
SSE	838.	838.	2.048-05	8.058-06	838.	3.228-05	1.134-05	838.	1.819-04	5.277-05
5	829.	829.	2.020-05	7.770-06	829.	2.862-05	1.012-05	829.	1.522-04	4.469-05
SSW	829.	829.	2.474-05	9.629-06	829.	3.242-05	1.179-05	829.	1.988-04	5.834-05
SW	610.	610.	2.946-05	1.155-05	610.	4.342-05	1.542-05	610.	2.754-04	7.909-05
WSW	509.	509.	2.678-05	1.051-05	509.	4.443-05	1.531-05	509.	2.653-04	7.546-05
W	509.	509.	2.635-05	1.032-05	509.	4.493-05	1.530-05	509.	2.741-04	7.694-05
WNW	625.	625.	1.947-05	7.609-06	625.	3.312-05	1.132-05	625.	1.892-04	5.375-05
NW	732.	732.	2.432-05	9.621-06	732.	3.916-05	1.367-05	732.	2.405-04	6.878-05
NNW	848.	848.	2.110-05	8.241-06	848.	3.539-05	1.217-05	848.	1.914-04	5.484-05

LASALLE COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR XE135M

DOWNWIND	RESTRICTED	ELEVAT	ED(STACK) RE	LEASE	MIXED !	MODE (VENT) R	RELEASE	GROUN	ND LEVEL REL	EASE
DIRECTION	AREA BOUND	RADIUS	S	SBAR	RADIUS	V	VBAR	RADIUS	G	GBAR
	(METERS)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)
N	1022.	1022.	2.872-04	1.776-04	1022.	3.782-04	2.328-04	1022.	9.935-04	6.065-04
NNE	1330.	1330.	2.117-04	1.309-04	1330.	2.699-04	1.662-04	1330.	6.753-04	4.127-04
NE	2408	2408.	9.634-05	5.948-05	2408.	1.167-04	7.184-05	2408.	2.562-04	1.568-04
ENE	4450.	4450.	4.210-05	2.595-05	4450.	4.754-05	2.926-05	4450.	8.430-05	5.167-05
E	1996.	1996.	1.482-04	9.149-05	1996.	1.769-04	1.090-04	1996.	3.829-04	2.344-04
ESE	838.	838.	3.805-04	2.353-04	838.	5.045-04	3.106-04	838.	1.368-03	8.351-04
SE	884.	884.	2.620-04	1.620-04	884.	3.381-04	2.083-04	884.	9.497-04	5.797-04
SSE	838.	838.	2.387-04	1.476-04	838.	2.989-04	1.842-04	838.	8.694-04	5.307-04
S	829.	829.	2.309-04	1.427-04	829.	2.738-04	1.688-04	829.	8.031-04	4.904-04
SSW	829.	829.	2.540-04	1.570-04	829.	2.932-04	1.808-04	829.	8.790-04	5.369-04
SW	610.	610.	3.613-04	2.234-04	610.	4.333-04	2.672-04	610.	1.351-03	8.241-04
WSW	509.	509.	3.643-04	2.253-04	509.	4.548-04	2.802-04	509.	1.449-03	8.833-04
W	509.	509.	3.415-04	2.112-04	509.	4.358-04	2.683-04	509.	1.404-03	8.555-04
WNW	625.	625.	2.592-04	1.603-04	625.	3.283-04	2.022-04	625.	1.024-03	6.244-04
NW	732.	732.	2.854-04	1.765-04	732.	3.606-04	2.222-04	732.	1.112-03	6.783-04
NNW	848.	848.	2.537-04	1.569-04	848.	3.263-04	2.009-04	848.	9.335-04	5.696-04

LASALLE COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR XE135

DOWNWIND	RESTRICTED	ELEVAT	ED(STACK) RE	LEASE	MIXED	MODE (VENT)	RELEASE	GROU	ND LEVEL REL	EASE
DIRECTION	AREA BOUND	RADIUS	5	SBAR	RADIUS	V	VBAR	RADIUS	G	GBAR
	(METERS)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)
N	1022.	1022.	2.028-04	1.097-04	1022.	2.692-04	1.452-04	1022.	7.871-04	4.222-04
NNE	1330.	1330.	1.624-04	8.780-05	1330.	2.059-04	1.111-04	1330.	5.865-04	3.148-04
NE	2408.	2408.	8.581-05	4.637-05	2408.	1.028-04	5.545-05	2408.	2.161-04	1.322-04
ENE	4450.	4450.	4.879-05	2.634-05	4450.	5.445-05	2.937-05	4450.	1.092-04	5.869-05
E	1996.	1996.	1.239-04	6.697-05	1996.	1.473-04	7.949-05	1996.	3.610-04	1.939-04
ESE	838.	838.	2.703-04	1.462-04	838.	3.589-04	1.936-04	838.	1.088-03	5.835-04
SE	884.	884.	1.819-04	9.840-05	884.	2.370-04	1.279-04	884.	7.367-04	3.951-04
SSE	838.	838.	1.843-04	9.972-05	838.	2.278-04	1.230-04	838.	7.674-04	4.116-04
S	829.	829.	1.724-04	9.325-05	829.	2.035-04	1.099-04	829.	6.588-04	3.535-04
SSW	829.	829.	2.156-04	1.166-04	829.	2.443-04	1.320-04	829.	8.508-04	4.565-04
SW	610.	610.	2.650-04	1.434-04	610.	3.164-04	1.709-04	610.	1.148-03	6.155-04
WSW	509.	509.	2.423-04	1.311-04	509.	3.057-04	1.650-04	509.	1.097-03	5.881-04
W	509.	509.	2.371-04	1.283-04	509.	3.028-04	1.634-04	509.	1.109-03	5.941-04
WNW	625.	625.	1.753-04	9.485-05	625.	2.241-04	1.209-04	625.	7.793-04	4.176-04
NW	732.	732.	2.232-04	1.207-04	732.	2.764-04	1.492-04	732.	9.905-04	5.310-04
NNW	848.	848.	1.877-04	1.015-04	848.	2.397-04	1.293-04	848.	7.952-04	4.263-04

LASALLE COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR XE137

	DOWNWIND	RESTRICTED	ELEVAT	EC'STACK) RE	LEASE	MIXED !	MODE (VENT) F	RELEASE	GROUP	ND LEVEL REL	EASE
1	DIRECTION	AREA BOUND	RADIUS	5	SBAR	RADIUS	٧	VBAR	RADIUS	G	GBAR
		(METERS)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/	UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)
	N	1022.	1022.	9.192-05	5.953-05	1022.	1.227-04	7.926-05	1022.	3.048-04	1.960-04
	NNE	1330.	1330.	5.984-05	3.874-05	1330.	7.806-05	5.042-05	1839.	1.839-04	1.183-04
	NE	2408.	2408.	1.898-05	1.228-05	2408.	2.376-05	1.535-05	2408.	4.989-05	3.209-05
	ENE	4450.	4450.	4.730-06	3.058-06	4450.	5.476-06	3.536-06	4450.	9.264-06	5.964-06
	E	1996.	1996.	3.389-05	2.192-05	1996.	4.135-05	2.671-05	1996.	8.391-05	5.398-05
	ESE	838.	838.	1.291-04	8.360-05	838.	1.728-04	1.116-04	838.	4.409-04	2.835-04
	SE	884.	884.	8.501-05	5.506-05	884.	1.112-04	7.183-05	884.	2.927-04	1.882-04
	SSE	838.	838.	7.478-05	4.844-05	838.	9.532-05	6.161-05	838.	2.566-04	1.650-04
	S	829.	829.	6.855-05	4.440-05	829.	8.301-05	5.366-05	829.	2.286-04	1.469-04
	SSW	829.	829.	7.181-05	4.651-05	829.	8.471-05	5.478-05	829.	2.331-04	1.499-04
	SW	610.	610.	1. 187-04	7.586-05	610.	1.447-04	9.355-05	610.	4.158-04	2.673-04
	WSW	509.	509.	1.300-04	8.422-05	509.	1.641-04	1.061-04	509.	4.873-04	3.132-04
	W	509.	509.	1.195-04	7.743-05	509.	1.553-04	1.004-04	509.	4.654-04	2.991-04
	WNW	625.	625.	8.843-05	5.729-05	625.	1.138-04	7.352-05	625.	3.328-04	2.139-04
	NW	732.	732.	8.980-05	5.818-05	732.	1.168-04	7.549-05	732.	3.307-04	2.126-04
	NNW	848.	848.	8.141-05	5.274-05	848.	1.068-04	6.903-05	848.	2.822-04	1.814-04

TABL -8 (Cont'd)

LASA ... COUNTY 182

MAXIMUM OFFSITE FINITE PLUME GAMMA DOSE FACTORS FOR XE 38

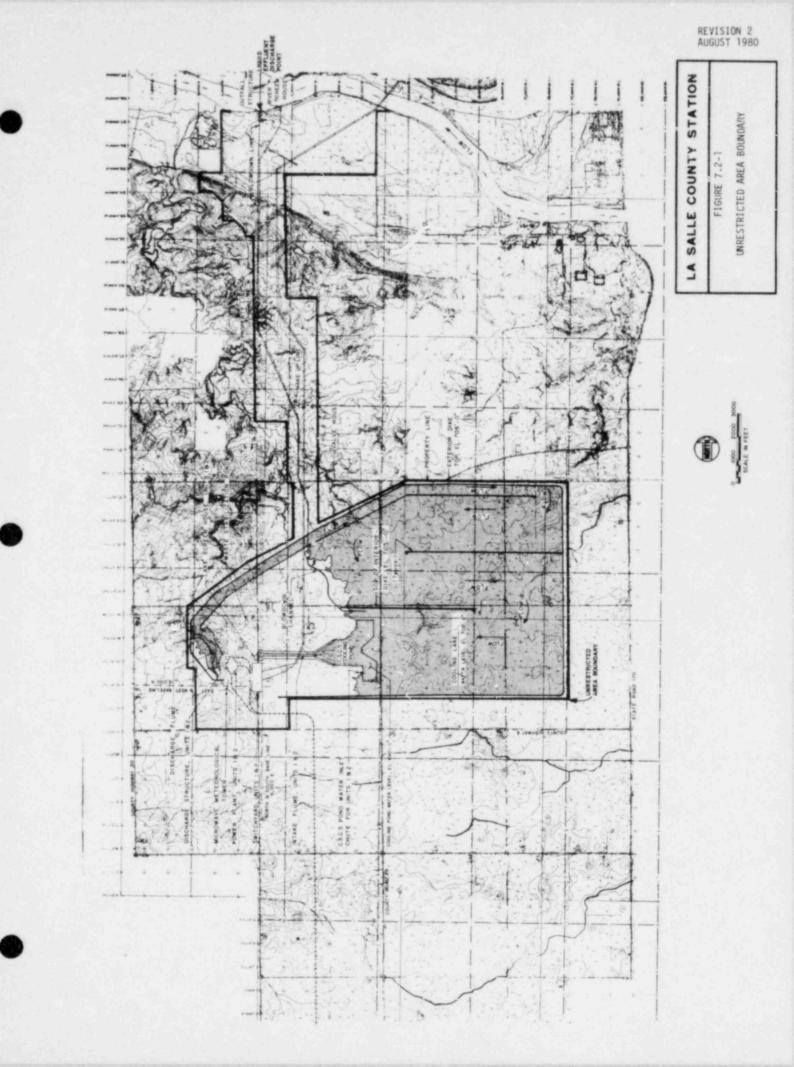
-				en/errow\ ne		MINER	HODE (WENT)	SELEACE	CDDIII	ND CTUEL DE	
	MIMIND	RESTRICTED	AND DESCRIPTION OF THE PERSON NAMED IN COLUMN	ED(STACK) RE	CONTRACTOR OF THE PARTY OF THE PARTY.	THE RESIDENCE PROPERTY AND THE PERSON NAMED IN	The second secon	RELEASE	Name and Address of the Owner, where the Owner, which is	ND LEVEL REL	ACCRECATION AND ADDRESS.
DIR	RECTION	AREA BOUND	RADIUS	5	SBAR	RADIUS	(11717)	VBAR	RADIUS	cuman (wm) (GBAR
-		(METERS)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MPAD/YR)/	(UCI/SEO)	(METERS)	(MRAD/YR)/	uci/sec)
	N	1022.	1022.	7.062-04	5.142-04	1092.	8.855-04	6.413-04	1022.	2.092-03	1.497-03
	NNE	1330.	1330.	5.154-01	3.751-04	1330.	6.294-04	4.559-04	1330.	1.419-03	1.015-03
	NE	2408.	2408.	2.283-04	1,660-04	2408.	2.679-04	1.940-04	2408.	3.375-04	3.850-04
	ENE	4450.	4450.	3.599-05	6.969-05	₹450.	1.065-04	7.713-05	4450.	1.766-04	1.268-04
	E	1996.	1996.	3.523-04	2.561-04	1996.	4.085-04	2.959-04	1996.	8.082-04	5.790-04
	ESE	838.	838.	9.410-04	6.854-04	838.	1 184-03	8.579-04	838.	2.869-03	2.052-03
	SE	884.	884.	6.470-04	4.713-04	884.	7.969-04	5.775-04	884.	1.993-03	1.425-03
	SSE	838.	838.	5.896-04	4.295-04	838.	7.075-04	5.130-04	838.	1.815-03	1.298-03
	S	829.	829.	5.682-04	4.138-04	829.	6.521-04	4.733-04	829.	1.680-03	1.201-03
	SSW	829.	829.	6.224-04	4.533-04	829.	6.990-04	5.075-04	829.	1.830-03	1.309-03
	SW	€10.	610.	8.907-04	6.488-04	610.	1.033-03	7.494-04	610.	2.823-03	2.018-03
	#SW	509.	509.	9.041-04	6.588-04	509.	1.083-03	7.858-04	509.	3.038-03	2.171-03
	W	509.	509.	8.464-04	6.168-04	509.	1.034-03	7.495-04	509.	2.938-03	2.100-03
	WNW	625.	625.	6.430-04	4.685-04	625.	7.797-04	5.654-04	625.	2.147-03	1.534-03
	NW	732.	732.	7.058-04	5.143-04	732.	8.540-04	6.193-04	732.	2.317-03	1.656-03
	NNW	848.	848.	6.270-04	4.567-04	848.	7.698-04	5.579-04	848.	1.954-03	1.397-03

TABLE 7.2-8 (Cont'd)

LASALLE COUNTY 182

MAXIMUM OFFSITE SINITE PLUME GAMMA DOSE FACTORS FOR AR 41

DOWNWIND	RESTRICTED	ELEVATED(STACK) RELEASE			MIXED MODE (VENT) RELEASE			GROUND LEVEL RELEASE		
DIRECTION	(METERS)	RADIUS (METERS)	S (MRAD/YR)/(SBAR UCI/SEC)	(METERS)	(MRAD/YR)/(UCI/SEC)	(METERS)	(MRAD/YR)/(GBAR UCI/SEC)
N	1022.	1022	9.121-04	6.430-04	1022.	1.128-03	7.954-04	1022.	2.759-03	1.945-03
NNE	1330.	1330.	7.085-04	4.995-04	1330.	8.496-0	5.989-04	1330.	2.011-03	1.418-03
NE	2408.	2408.	3.586-04	2.528-04	2408.	4.127-04	2.909-04	2408.	8.455-04	5.961-04
ENE	4450.	4450.	1.929-04	1.360-04	4450.	2.101-04	1.481-04	4450.	3.586-04	2.528-04
E	1996.	1996.	5.228-04	3.686-04	1996.	5.968-04	4.207-04	1996.	1.230-03	8.672-04
ESE	838.	838.	1.218-03	8.590-04	838.	1.508-03	1.063-03	838.	3.802-03	2.681-03
SE	884.	884.	8.260-04	2.823-04	884.	1.006-03	7.091-04	884.	2.596-03	1.830-03
SSE	838.	838.	8.186-04	5.771-04	838.	9.605-04	6.771-04	838.	2.623-03	1.849-03
5	829.	829.	7.699-04	5.428-04	829.	8.713-04	6.143-04	829.	2.304-03	1.625-03
SSW	829.	829.	9.379-04	6.613 04	829.	1.031-03	7.270 04	829.	2.862-03	2.018-03
SW	610.	610.	1.198-03	8.449-04	610.	1.366-03	9.628-04	610.	3.965-03	2.795-03
WSW	509.	509.	1.126-03	7.938-04	509.	1.334-03	9.403-04	509.	3.869-03	2.727-03
W	509.	509.	1.094-03	7.711-04	509.	1.311-03	9.239-04	509.	3.888-03	2.741-03
WNW	625.	625.	8.059-04	5.681-04		9.663-04	6.812-04	625.	2.754-03	1.942-03
NW	732.	732.	9.951-04	7.016-04	200000	1.171-03	8.253-04	732.	3.388-03	2.389-03
NNW	848.	848.	8.424-04	5.939-04	The same	1.013-03	7.139-04	848.	2.742-03	1.933-03



8.0 RADIOACTIVE EFFLUENT TREATMENT SYSTEMS, MODELS FOR SETTING GASEOUS AND LIQUID EFFLUENT MONITOR ALARM AND TRIP SETPOINTS, AND ENVIRONMENT RADIOLOGICAL MONITORING

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8.0 RADIOACTIVE EFFLUENT TREATMENT SYSTEMS, MODELS FOR SETTING GASEOUS AND LIQUID EFFLUENT MONITOR ALARM AND TRIP SETPOINTS, AND ENVIRONMENTAL RADIOLOGICAL MONITORING

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8.0 RADIOACTIVE EFFLUENT TREATMENT SYSTEMS, MODELS FOR SETTING GASEOUS AND LIQUID EFFLUENT MONITOR ALARM AND TRIP SETPOINTS, AND ENVIRONMENT RADIOLOGICAL MONITORING

8.1 GASEOUS RELEASES

8.1.1 System Design

8.1.1.1 Gaseous Radwaste Treatment System

A gaseous radwaste treatment system shall be any system designed and installed to reduce radioactive gaseous effluents by collecting primary coolant system off-gases from the primary system and providing for delay or holdup for the purpose of reducing the total radioactivity prior to release to the environment.

8.1.1.2 Ventilation Exhaust Treatment System

A ventilation exhaust treatment system shall be any system designed and installed to reduce gaseous radioiodine or radio-active material in particulate form in effluents by passing ventilation or vent exhaust gases through charcoal adsorbers and/or HEPA filters for the purpose of removing iodines or particulates from the gaseous exhaust stream prior to the release to the environment (such a system is not considered to have any effect on noble gas effluents). Engineered Safety Feature (ESF) atmospheric cleanup systems are not considered to be ventilation exhaust treatment system components.

8.1.2 Alarm and Trip Setpoints

Alarm and trip setpoints of gaseous effluent monitors at the principal points of release of ventilation exhaust air containing radioactivity are established to ensure that the release limits of 10 CFR 20 are not exceeded. The setpoints

are found by solving Equations 2.9 and 2.10 for each class of release.

For this evaluation the radioactivity mixture in the exhaust air is assumed to have the composition of gases listed in Table 3-3 from "Technical Derivation of BWR 1971 Design Basis Radioactive Material Source Terms," NEDO-10871, March 1973, General Electric Company. This mixture of radioactive gases is representative of the activity found at the point of release from the fuel; radioactive decay has not been included.

Equation 2.9 is rewritten using the fractional composition of each nuclide, f_i , and a total release rate, Q_t , for station vent stack* releases (the principal point of release of ventilation exhaust air containing radioactivity):

1.11
$$\sum_{i} \left[Q_{ts} \left(\overline{S}_{i} \times f_{i} \right) \right] < 500 \frac{mrem}{yr}$$
 (8.1)

fi Fractional Radionuclide
Composition
The release rate of radionuclide i divided by the total release of all radionuclides.

 $Q_{\text{ts}} \qquad \text{Total Release Rate,} \qquad \qquad (\mu\text{Ci/sec})$ Vent Stack Release The release rate for all radionuclides due to a station vent stack release. $Q_{\text{is}} = Q_{\text{ts}}f_{\text{i}} \qquad \qquad (8.2)$

Equation 8.1 can be solved for Qt for release limit determinations.

^{*}The term "vent stack", as used in this section, is to be considered synonymous with "stack" as used in Section 2.1.

Similarly, Equation 2.10 can be re-written:

$$\sum_{i} \left[\overline{L}_{i} (x/Q)_{s} Q_{ts} f_{i} \exp(-\lambda_{i} R/3600 u_{s}) + 1.11 s_{i} Q_{ts} f_{i} \right] < 3000 \frac{mrem}{yr}$$
(8.3)

Equation 8.3 can be solved for Q_{ts} and a corresponding release limit be determined. The most conservative release limit determined from Equations 8.1 and 8.3 will be used in selecting the appropriate alarm and trip setpoints for a vent stack release.

The exact settings will be selected to ensure that 10 CFR 20 limits are not exceeded.

Surveillance frequencies for gaseous effluent monitors will be as stated in Table 4.3.6.11-1 of the Technical Specifications. Calibration methods will be consistent with the definitions found in Section 1.0 of the Technical Specifications.

8.1.3 Station Vent Stack Monitor

Releases of radioactive noble gases from the station vent stack release point are monitored by an offline monitoring system consisting of two instrument channels, each of which uses a G-M tube sensing element. Samples of the effluent stream are taken by an isokinetic probe just prior to discharge into the atmosphere. Gas flow through the monitoring system, located largely on panel OD18-POO1, is ensured by the ram effect of the gas on the probe tips and by the vacuum pumps through a constant flow network.

Each monitoring channel consists of a G-M tube detector, a shielded sampling chamber, a pre-amplifier, and a log count rate monitor. The log count rate monitor includes an integral power supply, for providing high voltage to the detector,

and trip relays, whose output initiates high radiation alarm annunciators. The channels share a common two-pen recorder. The recorder, alarm annunciators, and remote control switches, for the station vent stack monitoring system, are located in the main control room. The sample panel, with pumps, detectors, and local controls, is located in the auxiliary building on elevation 815 feet just outside the turbine building exhaust fan room.

Power is supplied to the station vent stack radiation monitors from the Unit 1 125-Vdc battery systems via inverters. The monitor display has logarithmic scale with a range of 10⁻¹ to 10⁶ counts per second. The equipment identification numbers for the monitors are OD18-K602A and OD18-K602B.

8.1.4 Standby Gas Treatment Stack Monitor

Release of radioactivity from the standby gas treatment system (SGTS) stack is monitored by the SGTS monitoring system. Each SGTS monitoring channel consists of a beta sensitive scintillation detector for particulate; a beta sensitive scintillation detector for low-range noble gas; a beta sensitive scintillation detector for high-range noble gas; and a gamma sensitive scintillation detector for iodine. Provisions are made for system inlet and outlet grab samples.

The monitoring system uses a microprocessor to analyze the data from the beta and gamma scintillation detectors. This microprocessor performs background subtraction and compares the radiation values against operator entered alarm limits. A four-pen strip chart recorder records the monitoring system output. Alarms are located in the main control room.

Power is supplied to this monitor subsystem from Division 2 power. The equipment for each monitoring channel is skid mounted and located on the 786 ft 6 in. elevation in the auxiliary building.

8.1.5 SJAE Off-Gas Monitors

The steam jet air ejector (SJAE) monitor subsystem continually measures and records the gamma radiation in the off-gas as it is drawn from the main condenser by the steam jet air ejectors before it passes through the holdup line and carbon beds enroute to the station vent stack.

A continuous representative sample is drawn from the off-gas system via a stainless steel sample line. A 14 cc serum vial is inserted into the sample chamber, evacuated, then filled with a representative sample of off-gas. This sampling equipment is located on panel 1D18-J034 (2D18-J034).

This monitor system consists of two channels. One channel contains a gamma sensitive ionization chamber and a linear radiation monitor and the other channel contains a gamma sensitive ionization chamber and a logarithmic radiation monitor. The ion chambers sensitivity is 1 to 10⁶ mR/hr. The gamma sensitive ionization chamber RE-1D18-N002 (RE-2D18-N002) is connected to the logarithmic readout channel. This channel has alarm functions but no trip functions. Power is supplied from Unit 1 (2) 125-Vdc power supply via inverters and from the 120-Vac instrument bus for the recorder. The gamma sensitive ionization chamber RE-1D18-N012 (RE-2D18-N012) is connected to the linear readout channel. Power is supplied to this channel from Unit 1 (2) 24-Vdc power supply and from the 120-Vac instrument bus for the recorder. Both channels measure the radiation levels in the off-gas and their recorders are located in the control room.

8.1.6 Allocation of Effluents from Common Release Points

Radioactive gaseous effluents released from the plant vent stack are comprised of contributions from both units. Estimates of noble gas contributions from each unit will be allocated by considering appropriate operating conditions and measured SJAE off-gas activities. Allocation of radioiodine and radioactive particulate releases to a specific unit is not as practical and is influenced greatly by in-plant leakage. Under normal operating conditions, allocation will be made using reactor coolant iodine activities. During unit shutdown or periods of known major in-plant leakage, the apportionment will be adjusted accordingly. The allocation of the effluents will be estimated on a monthly basis.

8.1.7 Symbols Used in Section 8.1

SYMBOLS	NAME	UNIT
Q _{ts}	Total Release Rate, Vent Stack Release	(µCi/sec)
\overline{s}_i	Gamma Whole Body Dose Constant, Vent Stack Release	(mrad/yr per µCi/sec)
fi	Fractional Radionuclide Composition	
ī	Beta Skin Dose Constant	(mrem/yr per µCi/m ³)
$(x/Q)_s$	Relative Effluent Concentration, Vent Stack Release	(sec/m ³)
$^{\lambda}$ i	Radiological Decay Constant	(hr ⁻¹)
R	Downwind Range	(m)
u _s	Average Wind Speed, Vent Stack Release	(m/sec)
Q _{is}	Release Rate of Nuclide i, Vent Stack Release	(µCi/sec)
Si	Gamma Dose Constant, Vent Stack Release	(mrad/yr per µCi/sec)

8.1.8 Constants Used In Section 8.1

NUMERICAL VALUE	NAME	UNIT
1.11	Conversion Constant	(mrem/mrad)
3600	Conversion Constant	(sec/hr)

8.2 LIQUID RELEASES

8.2.1 System Design

A liquid radwaste treatment system shall be a system designed and installed to reduce radioactive liquid effluents by collecting the liquids, providing for retention or holdup, and providing for treatment by demineralizer or a concentrator for the purpose of reducing the total radioactivity prior to release to the environment.

8.2.2 Alarm Setpoints

Alarm setpoints of liquid effluent monitors at the principal release points are established to ensure that the limits of 10 CFR 20 are not exceeded in the unrestricted area. The concentration limit (C_{\lim}) in the discharge line prior to dilution in the initial dilution stream is:

$$C_{lim} = MPC \left[\frac{F_{ave}^d + F_{max}^r}{F_{max}^r} \right]$$
(8.5)

Clim Limiting Concentration (µCi/ml) in Discharge Line

The maximum concentration in the discharge line permitted to be discharged to the initial dilution stream.

MPC Weighted Maximum Permissible (μCi/ml)
Concentration

The lowest maximum permissible oncentration calculated using liquid effluent isotopic data.

F Maximum Flow Rate,
Radwaste Discharge

(ft³/sec)

The maximum flow rate of radwaste from the discharge tank to the initial dilution stream.

F^dave

Average Flow Rate, Initial Dilution Stream (ft³/sec)

The average flow rate of the initial dilution stream which carries the radionuclides to the unrestricted area boundary.

Surveillance frequencies for liquid effluent monitors will be as stated in Table 4.3.6.10-1 of the Technical Specifications. Calibration methods will be consistent with the definitions found in Section 1.0 of the Technical Specifications.

8.2.3 Liquid Effluent Monitors

The radwaste discharge line, Unit 1(2) service water effluent header and Unit 1(2) RHR service water effluent headers are continuously monitored for radioactivity by an offline monitoring system which uses a NaI (T1) activated scintillation detector. Liquid effluent flow through each monitoring system is ensured by a pump and a flow control valve located on local sample panels.

Each monitoring system consists of a scintillation detector, shielded sampling chamber, a preamplifier, and a log count rate monitor. The log count rate monitor includes an integral power supply, for providing high voltage to the detector, and trip relays, whose outputs initiate high radiation alarm annunciators. In addition, the radwaste discharge effluent monitor's trip relays initiate isolation of the liquid radwaste discharge header.

The service water effluent monitor provides a signal to a two-pen recorder which it shares with the RBCCW process radiation monitor.

The RHR service water effluent monitors share a common twopen recorder in the main control room.

The radwaste discharge effluent monitor provides signals to a recorder in the main control room and a recorder in the radwaste control room.

All the process liquid monitors have logarithmic scales with a range of 10⁻¹ to 10⁶ CPM. The monitors are powered from the Unit 1(2) 125-Vdc batteries via inverters, with the exception of the radwaste discharge monitor which is supplied from a local 120-Vac source through a d-c power supply.

The equipment identification numbers for the monitors are 0D18-K606, radwaste monitor; 1D18-K608 (2D18-K608), service water effluent monitor; 1D18-K604 (2D18-K604), RHR service water A effluent; and 1D18-K605 (2D18-K605), RHR service water B effluent.

8.2.4 Allocation of Effluents from Common Release Points

Radioactive liquids released from the radwaste treatment system are comprised of contributions from both units. Under normal operating conditions, it is difficult to apportion the radioactivity between units. Consequently, allocation will normally be made evenly between units. During refueling outages or periods of known major in-plant leakage, the apportionment will be adjusted accordingly. The allocation of the effluents will be estimated on a monthly basis.

8.2.5 Administrative and Procedural Controls for Radwaste Discharges

Administrative and procedural controls have been designed to ensure proper control of radioactive liquid radwaste discharge in order to preclude a release in excess of 10 CFR 20 limits. The discharge rate for each batch is calculated by a technician and then independently verified by operating staff personnel. All liquid radwaste discharges will be from one of two river discharge tanks, 1WF05T or 2WF05T.

The keylock hand switch, OHS-WF048, used for selecting high or low discharge flow is kept locked except when discharging. The key for this switch and the locked valves is under the administrative control of the Shift Engineer.

A documented valve checklist is prepared for each batch discharge. The proper valve line-up is made by the Operator and rechecked by the Radwaste Foreman. The actual discharge is authorized by the Shift Engineer.

The system is equipped with a radiation trip point which alarms and initiates automatic valve closure on the radwaste discharge line to prevent the violation of 10 CFR 20 limits.

8.2.6 Determination of Initial Dilution Stream Flow Rates

For those release paths which have installed flow monitoring instrumentation, that instrumentation will be used to determine the flow rate of the initial dilution stream. This instrumentation will be operated and maintained as prescribed by the Technical Specifications. For those release paths which do not have installed flow monitoring instrumentation, flow rates will be determined by use of appropriate engineering data such as pump curves, differential pressures, or valve position indication.

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8.2.7 Symbols Used In Section 8.2

SYMBOL	NAME	UNIT
C _{lim}	Limiting Concentration in Discharge Line	(µCi/ml)
MPC	Weighted Maximum Permissible Concentration	(µCi/ml)
Frmax	Maximum Flow Rate, Radwaste Discharge	(ft ³ /sec)
F ^d ave	Average Flow Rate, Initial Dilution Stream	(ft ³ /sec)

8.3 SOLIDIFICATION OF WASTE/PROCESS CONTROL PROGRAM

The process control program (PCP) shall contain the sampling, analysis, and formulation determination by which solidification of radioactive wastes from liquid systems is ensured.

8.4 ENVIRONMENTAL RADIOLOGICAL MONITORING

The environmental radiological monitoring program to be performed in the environs around La Salle County Station is given in Table 8.4-1 for the years 1982-1983, and in Table 8.4-2 for 1984 and later.

Figure 8.4-1 shows the 14 fixed air sampling sites and TLD locations; also shown are the "outer ring" (approximately 5 miles distant) TLD locations. Figure 8.4-2 shows the "inner ring" TLD locations. The TLD's are code numbered as follows: XYY-N.

Where:

X = 1 means inner ring,

X = 2 means outer ring, and

YY-N is an identification code.

The practical lower limits of detection for this program are given in Table 8.4-3.

TABLE 8.4-1

RADIOLOGICAL MONITORING PROGRAM

(1982 - 1983)

		SAMPLE	E MEDIUM	TYPE AND FREQUENCY OF ANALYSIS*	COLLECTION SITES	FREQUENCY OF COLLECTING	NONROUTINE REPORTING LEVELS
	1.	Airb	orne				
00			Particulate Filter	Gross beta - W. Sr 89, 90 - Q. comp. Gamma Spec Q. comp.	Seneca, Marseilles, Ottawa, Grand Ridge Streator, Ransom, Route 6 at Gonnam Road, Kernan, and six stations near the site (see Figure 8.4-1)	Weekly	Cs-134, 10 pCi/m ³ Cs-137, 20 pCi/m
8.4-2			Charcoal Cartridge	I-131	Same as for la	Every 2 weeks	0.9 pCi/m ³
	2.	Gamm Radi	a ation	TLD	Same as for 1a, plus 40 other sites distributed near the site boundary and at 5 miles (see Figures 8.4-1 and 8.4-2)	Quarterly	None
	3.	Surf	ace Water	Sr-89, 90 - Q. comp. Gamma Spec M. comp. Gross beta - W. Tritium - Q. comp.	Illinois River at intake of Illinois Nitrogen Corp. Illinois River at Marseilles Illinois River at Ottawa Illinois River at Seneca South Kickapoo Creek Cooling lake near recreation area	Week1y	**

TABLE 8.4-1 (Cont'd)

		SAMPLE MEDIUM	TYPE AND FREQUENCY OF ANALYSIS*	COLLECTION SITES	FREQUENCY OF COLLECTING	NONROUTINE REPORTING LEVELS
4	1.	Intake/Discharge pipes	Gross beta - W. Sr-89, 90 - M. comp. Tritium - M. comp. Gamma Spec M. comp.	I/D Pipes if pumping; if not pumping, collect in Illinois River near I/D structures	Weekly	None
5	5.	Precipitation	Gamma Spec Q. comp. Sr-89, 90 - Q. comp. Gross beta - M. Tritium - Q. comp.	Same 3 sites as milk collections	Monthly	None
6	5.	Well Water: Offsite	Gamma Spec. Sr-89, 90 Gross beta Tritium	Marseilles, Seneca, Ottawa, Ransom, Illini State Park	Quarterly	**
7	7.	Well Water: Onsite	Gamma Spec Q. comp. Sr-89, 90 - Q. comp. Gross Seta - M. Tritium - Q. comp.	One onsite well (the one chosen for pro- viding drinking water)	Monthly	**
3	8.	Vegetables	Gross beta Sr-89, 90 Gamma Spec. I-131 (for green leafy vegetables only)	Farms within 10 miles	As available at harvest time	*
9	9.	Cattle Feed and Grass	Gross beta Sr-89, 90 Gamma Spec.	Same three sites as milk collections	Quarterly: Grass: Summer Feed: Winter	None

TABLE 8.4-1 (Cont'd)

	S	AMPLE MEDIUM	TYPE AND FREQUENCY OF ANALYSIS*	COLLECTION SITES	FREQUENCY OF COLLECTING	NONROUTINE REPORTING LEVE	
10	0.	Milk	Gamma Spec. Sr-89, 90 - M. I-131 (Pasture Season)	3 nearby dairies or private animals, including the nearest, if possible	Monthly - November to April Weekly - May to October		3 70 50
1	1.	Sediment, Aquatic Plants	Gross beta Gamma Spec.	Just upstream of cooling lake inlet structure Just downstream of cooling lake discharge structure Cooling lake near recreational area	Three times a year, if available		
1	2.	Fish	Gross beta Gamma Spec. Sr-89, 90	Marseilles pool of Illinois River Cooling Lake	Three times a year	*	

^{*}If frequency of analysis is not given, it is the same as frequency of collection; W. - Weekly; M. - Monthly; Q. - Quarterly; Comp. - Composite.

*pCi/kg wet veight	** Nuclide	pCi/l	Nuclide	pCi/1
Mn-54 3 x 10^4	H-3	20,000	Zr-Nb-95	400
Co-58 3 x 104	Mn-54	1,000	I-131	2
$Zn-65 2 \times 10^{4}$	Fe-59	100	Cs-134	30
Cs-137 2 x 10 ³	Co-58	600	Cs-137	50
Fe-59 1 x 104	Co-60	300	Ba/La-140	100
Co-60 1 x 10 ⁴	Zn-65	200		
Cs-134 1 x 10 ³				

TABLE 8.4-2

RADIOLOGICAL MONITORING PROGRAM

(1984 and Later)

SAMPLE MEDIA	COLLECTION SITE	TYPE OF ANALYSIS	FREQUENCY	NONROUTINE REPORTING LEVELS**
1. Air Monitoring	a. Onsite and near field*1. Nearsite Station 1	a. Filter - gross beta***	a. Weekly	Cs-134, 10; Cs-137, 20 pCi/m ³
	2. Onsite Station 2 3. Onsite Station 3 4. Nearsite Station 4	b. Charcoal - I-131	b. Biweekly [†]	0.9 pCi/m ³
	5. Onsite Station 5 6. Nearsite Station 6	c. Sampling Train - Test and Maintenance	c. Weekly	Not Applicable
	b. Far Field*			
	7. Seneca 8. Marseilles 9. Grand Ridge 10. Streator	a. Filter Exchange	a. Weekly	Cs-134, 10; Cs-137, 20 pCi/m ³ when analyses are made
	11. Ransom 12. Kernan 13. Route 6 at Gonnam Road 14. Ottawa	b. Charcoal Exchange	b. Biweekly [†]	0.9 pCi/m ³ when analyses are made
		c. Sampling Train - Test and Maintenance	c. Weekly	Not Applicable

TABLE 8.4-2 (Cont'd)

SAMPLE MEDIA	COLLECTION SITE	TYPE OF ANALYSIS	FREQUENCY	NONROUTINE REPORTING LEVELS**
2. TLD	a. Same as Item 1, Air Monitoring Sites*	Gamma Radiation	Quarterly	None
	b. Plus 40 other sites distributed about th site boundary and at 5 miles* [§]			
3. Fish	a. Marseilles Pool of	Gamma	Semi-annual	pCi/kg wet weight
	Illinois River	Isotopic		Mn-54 3 x 104 Co-58 3 x 104 Zn-65 2 x 103 Cs-137 2 x 104 Fe-59 1 x 104 Co-60 1 x 103 Cs-134 1 x 103
4. Milk	a. Three nearby dairies	I-131 ⁺⁺	a. Weekly	pCi/l
	or private animals including the neares if possible	t,	during grazing season, May to October	I-131, 3 Cs-134, 70 Cs-137, 60 Ba-La-140, 300
			b. Monthly, November to April	Same as above

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TABLE 8.4-2 (Cont'd)

S	AMPLE MEDIA		COLLECTION SITE	TYPE OF ANALYSIS	FREQUENCY	REPORTING	The state of the s
5.	Surface Water	a. b. c. d. e. f.	Illinois River at Marseilles Illinois River at Ottawa Illinois River at Seneca South Kickapoo Creek Illinois Nitrogen Corp. La Salle County Cooling Lake near recreation area	Gamma Isotopic	Monthly analysis of weekly composites	Nuclides H-3 Mn-54 Fe-59 Co-58 Co-60 Zn-65 Zr-Nb-95 I-131 Cs-134 Cs-137 Ba-La-140	pCi/l 20,000 1,000 100 600 300 200 400 2 30 50
6.	Cooling Water Sample	a. b.	Inlet ⁺⁺⁺ Discharge ⁺⁺⁺	Gross Beta	Weekly	None	
7.	Sediment	a.	Downstream of Cooling Lake Discharge Structure	Gamma Isotopic	Annua 1	None	

^{*}See Figure 8.4-1

**Average concentration over calendar quarter.

†††Provided by station personnel.

See Figure 8.4-2

^{***}A gamma isotopic analysis small be performed whenever the gross beta concentration in a sample exceeds by five times (5x) the average concentration of the preceding calendar quarter for the sample location.

†Biweekly shall mean that the frequency is once every other week.

TA gamma isotopic analysis shall be performed if I-131 from the plant is found above the LLD.

TABLE 8.4-3

PRACTICAL LOWER LIMITS OF DETECTION (LLD) FOR ENVIRONMENTAL RADIOLOGICAL MONITORING PROGRAM

SAMPLE MEDIA	ANALYSIS	LLD (4.66g)	UNITS
Airborne "Particulate"	Gross Beta* Gamma Isotopic Sr-89, 90	0.01 0.01 0.01	pCi/m3 pCi/m3 pCi/m3
Airborne I-131	Iodine-131	0.10	p?i/m³
Liquids	Sr-89 Sr- 90 I-131 Cs-134 Cs-137 Tritium Gross Beta* Gamma Isotopic	10 2 5** 10 10*** 0.2 5 <20	pCi/l pCi/l pCi/l pCi/l pCi/l pCi/l pCi/l pCi/l pCi/l
Vegetation	Gross Beta* I-131 Sr-89, 90 Gamma Isotopic	2 0.03 1 0.2	pCi/g wet pCi/g wet pCi/g wet pCi/g wet
Soil, Sediment	Gross Beta* Sr-89, 90 Gamma Isotopic	2 1 0.2	pCi/g dry pCi/g dry pCi/g dry
Animal Tissue	Sr-89, 90 I-131 - Thyroid Cs-134, 137 Gross Beta* Gamma Isotopic	0.1 0.1 0.1 1.0 0.2	pCi/g wet pCi/g wet pCi/g wet pCi/g wet pCi/g wet

^{*}Referenced to Cs-137.

***5.0 pCi/l on milk samples.

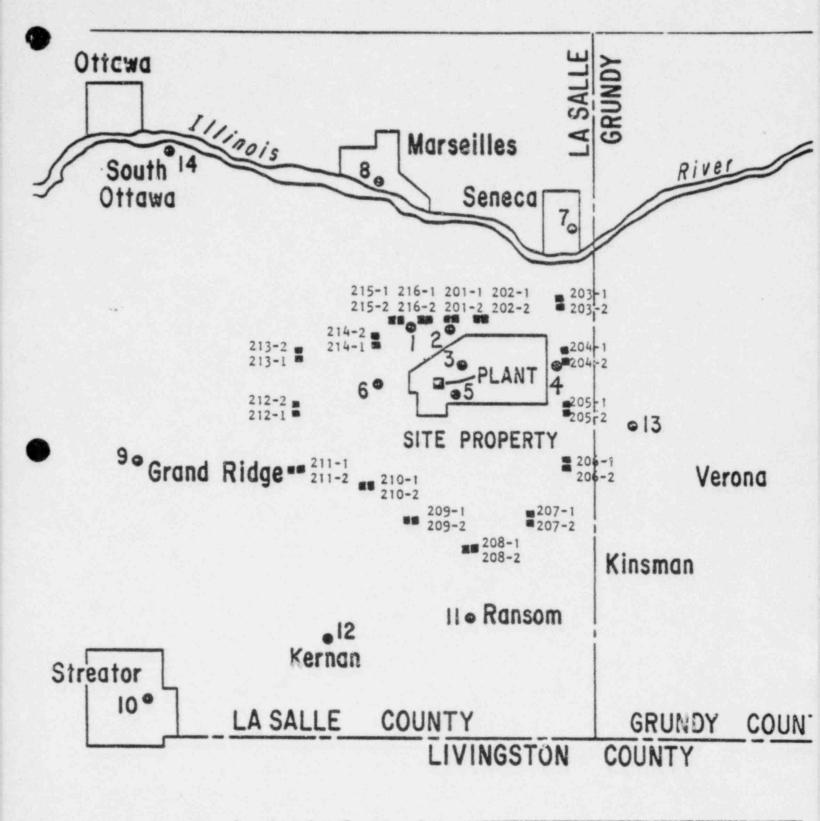
^{**0.5} pCi/l on milk samples collected during the pasture season.

TABLE 8.4-4
ENVIRONMENTAL RADIOLOGICAL MONITORING SAMPLING CODES

	MONITORING SITES	AIR	TLD	SURFACE WATER	FISH	AQUA AND	TIC PLAN SEDIMENT	TS MIL	PITATION, GRASS	VEGETABLES
L-01	Nearsite No. 1	Х	Х							
L-02	Onsite No. 2	Χ	X							
L-03	Onsite No. 3	Χ	Χ							
L-04	Nearsite No. 4	χ	χ							
L-05	Onsite No. 5	Χ	Χ							
L-06	Nearsite No. 6	X	Χ							
L-07	Seneca	X	Χ							
L-08	Marseilles	Х	χ							
L-09	Grand Ridge	Χ	Χ							
L-10	Streator	Χ	Χ							
L-11	Ransom	X	¥							
L-12	Kernan	X	Χ							
L-13	Route 6 at Gonnam Road	Х	Χ							
L-14	Ottawa	Х	Х							
L-15	Johnson Dairy							Χ	Χ	
L-16	Lowery Dairy							X	X	
L-17	Norsen Dairy							Х	X	
L-18	Sunny Isle Farm							Х	X	

	MONITORING SITES	AIR	TLD	SURFACE WATER		FISH	AQUATIC PL AND SEDIME	PRECIF	GRASS	VEGETABLES
L-19	Illinois River at Marseilles			Χ						
L-20	Illinois River at Ottawa			Χ						
L-21	Illinois River at Senera			X						
L-22	South Kickapoo Creek			X						
L-23	Illinois Nitrogen Corporation			X						
L-24	La Salle County Station (LSCS cooling lake near recreation area)		X		Х				
L-25	LSCS intake pipe/river			X						
L-26	LSCS discharge pipe/river			X						
L-27	LSCS onsite well				χ					
L-28	Marseilles well water				Χ					
L-29	Seneca well water				Χ					
L-30	Ransom well water				Χ					
L-31	Ottawa well water				X					
L-32	Illinois State Park				Х					
L-33	Just upstream of cooling lake inlet structure						х			
L-34	Just downstream of cooling lake discharge structure						Х			
L-35	Marseilles pool of Illinois River					Х				
L-36	Farm A - vegetables									X
1-37	Farm B - vegetables									X

8.4-10



SCALE: 0 2 3 4 5

LA SALLE COUNTY STATION

FIGURE 8.4-1

FIXED AIR SAMPLING SITES AND OUTER RING TLD LOCATIONS

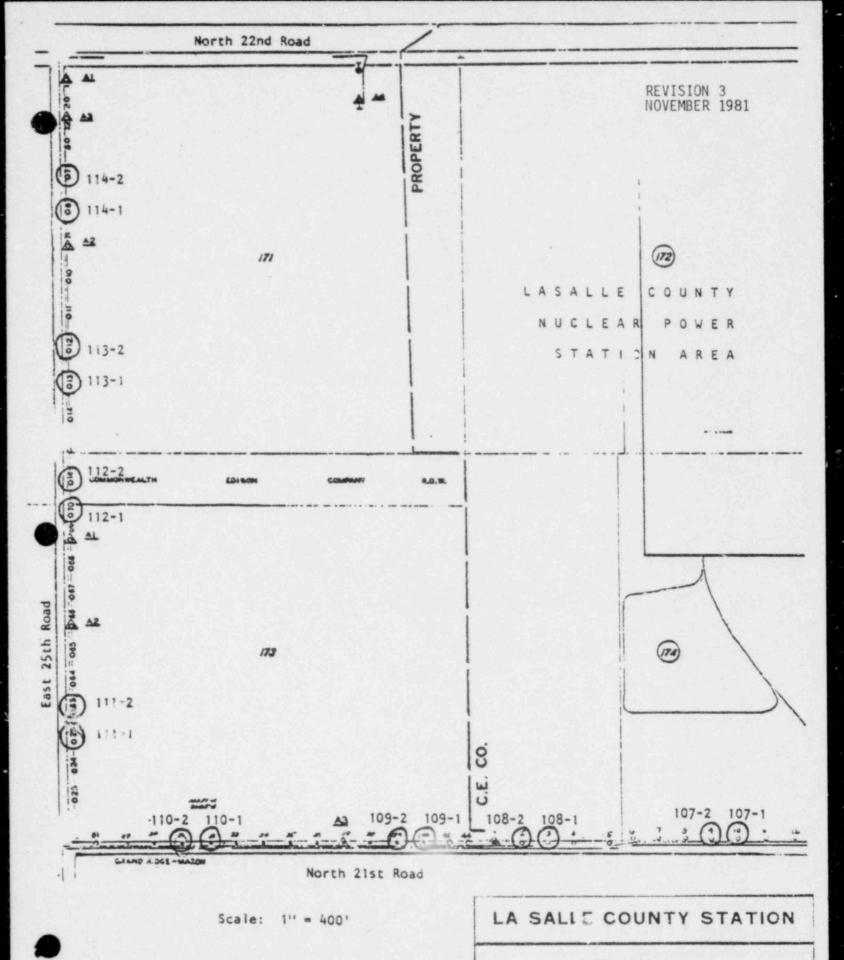


FIGURE 8.4-2

INNER RING TLD LOCATIONS