James A. FitzPatrick Nuclear Power Plant P.O. Box 41 Lycoming, New York 13093 315 342-3840



Harry P. Salmon, Jr. **Resident Manager** 

March 12, 1993 JAFP-93-0136

United States Nuclear Regulatory Commission Document Control Desk Mail Station P1-137 Washington, D.C. 20555

SUBJECT: DOCKET NO. 50-333 LICENSEE EVENT REPORT:

93-006-00 - Inoperability of Fire Pumps

Dear Sir:

This report is submitted in accordance with 10CFR50.73(a)(2)(i). This report is also submitted as a special report required by Technical Specifications 3.12.A.1.C, 3.12.A.1.d.2 and 6.9.B.2.

Questions concerning this report may be addressed to Mr. W. Verne Childs at (315) 349-6071.

Very truly yours,

HARRY P. SALMON, JR.

HPS:WVC:tld

Enclosure

cc: USNRC, Region I USNRC Resident Inspector INPO Records Center

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The plant was shutdown and in the cold condition for a maintenance outage. At 1820 hours on 2/25/93 Fire Pump [KP] 76P-2 was declared inoperable due to inadequate pump discharge pressure and on 2/26/93 at 0207 Fire Pump 76P-1 was declared inoperable when engine overheating was evident during a pump test. A backup source of fire suppression water was provided by a third full capacity fire pump. Fire Pump 76P-1 was replaced with a new pump and Fire Pump 76P-2 will be replaced with a new or rebuilt pump. Procedure revisions and continued trending of performance data will reduce the probability of recurrence.

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#### Event Description:

The plant was shutdown and in the cold condition for a short maintenance outage. The Reactor had been shutdown by Manual Scram at 0140 hours on February 25, 1993, due to partial blocking of the cooling water intake structure [KE] with ice. A planned maintenance outage of approximately nine days was scheduled to start during the evening of February 26, 1993. The decision was made to commence outage work one day early. Refer to LER-93-004 for additional information concerning the partial blockage of the intake structure and resulting Reactor Manual Scram.

On February 25, 1993, at 1820 hours, Electric Motor Driven Fire Pump (76P-2) was declared inoperable based on engineering evaluation of pump performance testing data. The pump discharge pressure was approximately three pounds per square inch less than the minimum required value of 125 pounds per square inch (psig) at the rated flow of 2,500 gpm. Declaring Fire Pump 76P-2 inoperable resulted in entry into Technical Specification 3.12.A.1.c which is a seven day Action Statement for one inoperable fire pump.

On February 26, 1993, at 0207 hours, the West Diesel Engine Driven Fire Pump (76P-1) was declared inoperable when engine overheating was evident during a pump test. Declaring 76P-1 inoperable resulted in entry into Technical Specification Action Statement 3.12.A.1.d which requires:

- Establishment of a backup fire suppression water system within 24 hours, and,
- Submittal of a Special Report to the NRC by telephone within 24 hours, and,
- 3. Facsimile (or similar) confirmation of the telephone notification no later than the first work day following the event, and,
- 4. Submittal of a written Special Report within 14 days of the event. (Submittal of this Special Report is being made to satisfy the 14 day requirements of Technical Specification 3.12.A.1.d.2.c and 6.9.B.2.)

NRC FORM 366A U.S. NUCLEAR REGULATORY COMMISSION APPROVED OMB NO 3150-0104 EXPIRES: 4/30/92 ESTIMATED BURDEN PER RESPONSE TO COMPLY WTH THIS INFORMATION COLLECTION REQUEST 50.0 HRS. FORWARD COMMENTS REGARDING BURDEN ESTIMATE TO THE RECORDS AND REPORTS MANAGEMENT BRANCH (P.530), U.S. NUCLEAR REGULATORY COMMISSION, WASHINGTON, DC 20565, AND TO THE PAPERWORK REDUCTION PROJECT (SISGOJIGA), OFFICE OF MANAGEMENT AND BUDGET, WASHINGTON, DC 20503. LICENSEE EVENT REPORT (LER) TEXT CONTINUATION FACILITY NAME (1) DOCKET NUMBER (2) LER NUMBER (6) PACE (3) NUMBER NUMBER YEAR James A. FitzPatrick Nuclear Power Plant 0 5 0 0 0 3 3 3 9 3 0|0|6 - 0|0 0|3 OF1 TEXT (If more space is required, use additional NRC Form 356A's) (17)

At the time that the second fire pump was declared inoperable, a backup fire pump 76P-4 was already inservice. Fire Pump 76P-4 is permanently installed to serve as a backup to Fire Pumps 76P-1 and 76P-2, as well as to provide additional fire protection capability to buildings such as the warehouses and training center. The third Fire Pump is briefly discussed in Technical Specification Bases 3.12.A/4.12.A and the NRC Safety Evaluation for Technical Specification Amendment 142 dated October 23, 1989. Fire Pump 76P-4 is essentially identical to the West Diesel Fire Pump (76P-1). It was designed and manufactured by the same vendor, has the same capacity, will automatically start when the fire water header pressure decreases to 85 psig, and can supply 100 percent of the potential demands on the High Pressure Water Fire Protection System in the event of fire. It should also be noted that when Electric Fire Pump 76P-2 was administratively declared inoperable on February 25, 1993 at 1820 hours, it was not physically removed from service. The pump remained capable of automatic starting when the Fire Water Header Pressure decreased to approximately 105 psig.

The NRC Emergency Operations Center was notified via the Emergency Notification System (ENS) telephone of the inoperability of Fire Pumps 76P-1 and 76P-2 at approximately 1900 hours on Friday, February 26, 1993. On Monday, March 1, 1993, the facsimile transmission of a letter which briefly described inoperability of fire pumps and establishment of a backup fire suppression water supply was completed to provide confirmation of the telephone notification.

Fire Pump 76P-1 was restored to an operable status at 1655 hours on March 4, 1993, after pump replacement and performance testing. This action resulted in the following conditions and status:

- West Diesel Fire Pump 76P-1 operable (in a normal standby condition) in accordance with Technical Specification requirements.
- Electric Fire Pump 76P-2 inoperable in accordance with Technical Specification requirements (but available for service in a normal standby condition and capable of delivering 2,500 gpm at slightly less than the required 125 psig).
- 3. Diesel Fire Pump 76P-4 (which is not required by Technical Specifications) available for service and capable of delivering rated flow and pressure following an automatic start at a fire header pressure of equal to or greater than 85 psig.

NRC FORM 386A U.S. NUCLEAR REGULATORY COMMISSION (6-39)			APPROVED OM5 ND. 3150-0104 EXPIRES: 4/30/82																				
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The sequence of events which ultimately resulted in Fire Pumps 76P-1 and 76P-2 being inoperable at the same time was different for each pump and is described below.

## Electric Motor Driven Fire Pump 76P-2

In November, 1992, plant Performance Engineering personnel completed an evaluation of 76P-2, which included trending of performance test data. It was concluded that 76P-2 had shown a steady decline in performance over the preceding time period of approximately seven years and would require replacement or rebuild to restore the pump to new (or nearly new) capability.

During performance testing of 76P-2 in the Fall of 1992, the pump was considered operable based on a measured flow of equal to or greater than 2,500 gpm and calculated discharge pressure of equal to or greater than 125 psig. Engineering evaluation of performance test data resulted in the pump being declared inoperable at 1820 hours on February 25, 1993, after it was determined that calculation of the pump discharge pressure included a correction for the elevation difference between the pump discharge pressure gage and water level in the forebay area. This elevation difference of approximately 13 feet resulted in correction of the observed discharge pressure by adding 0.433 psi for each foot of elevation difference to the observed discharge pressure. The actual correction should have been based on the elevation difference between the discharge pressure gage and the center line elevation of the pump discharge. The properly calculated pump discharge pressure was 122.4 psig compared to the minimum Technical Specification 4.12.A.1.e.3 requirement of 125 psig at 2,500 gpm.

It should be noted that calculation of the pump discharge pressure which includes correction for the elevation difference between the discharge pressure gage and the forebay level yields the total head produced by the pump. The total head value is the information necessary to compare pump performance against the manufactured pump curve to provide useful trend data. It is essentially the same method used to obtain performance data for safety related system pumps such as core spray [BM] or Residual Heat Removal/Low Pressure Coolant Injection (RHR/LPCI) [BO] pumps.

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at 100 percent rated the hours, the plant cooling approximately 900 feet f depth of approximately 1 became partially blocked cooling water intake flo area and pump suction ba the normal operation of two normal service water the intake resulted in w suction level for fire p manually scrammed to pro as described in more det related to inoperability February 25, 1993:	Armal power. Between ( y water intake structur from the shore line of 2 feet below the lake with ice. The blocks ow to an extent that way by within the screenho three circulating water three circulating water system [KG] pumps. The vater level decreasing pumps (239 feet, 6 inch betect the heat sink rec cail in LER-93-004. A y of the fire pumps is	0000 hours and 0143 re [KE] located Lake Ontario [BS] at a surface apparently age restricted the ater level in the forebay buse was drawn down by er system [KE] pumps and The partial blockage of to below the minimum hes). The reactor was juired for safe shutdown sequence of events presented below.
bood hours	power. Condenser [SC (after mixing with so 37F.	3] inlet temperature ome discharge water) was
0100 hours -	Condenser inlet temperapproximately 40F from level due to partial and the warming effected	erature had increased to om decrease in forebay intake blockage with ice ct of tempering flow.
0125 hours -	Electric Fire Pump 76 automatically on low (105 psig). Apparent had decreased to the Header Jockey Pump (2 momentarily, resultin pressure decrease.	5P-2 started fire header pressure tly forebay water level point where the Fire 76P-3) lost suction ng in a fire header
Between 0130		
and 0135 hours -	Electric Fire Pump 76 after verification of pressure by an operat dispatched to the are	5P-2 was shutdown locally f normal fire header tor that had been ea.

Control Room operators noted condenser inlet temperature was 58F.

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TEXT (Il more spece is required, use edditionel NRC Form 3	06.4 (s) (17) -	Control Room operator circulating water pump is consistent with dec pressure).	noted an increase in motor amperage (which creased suction
	-	Fire Pumps 76P-2 and 7 automatically on low f 95 psig and 85 psig re Load reduction to allo cooling water demand w	76P-4 started fire header pressure at espectively. ow a reduction in was initiated.
0138 hours	-	Circulating Water Pump reduced the total cool approximately 30 perce	o 36P-1C shutdown. This ling water demand ent
0140 hours		The operator dispatche screenhouse area report forebay area was an est normal. The shift sup reactor shutdown by Ma measurement of forebay	ed to the fire pump and rted water level in the stimated 10 feet below pervisor directed anual Scram. No actual y water level was made.
0143 hours		Condenser inlet temper approximately 67F. The system pumps and two re pumps continued in oper Room personnel were ex Operating Procedures Scram.	rature peaked at wo circulating water hormal service water eration as the Control kecuting Abnormal (AOPs) for Reactor
0147 hours		Fire Pumps 76P-1, 76P- Pump 76P-3 were shutdo placed in manual to pr starting and potential loss of suction.	-2, 76P-4 and Jockey own by operators and revent automatic 1 pump damage due to
0210 hours		Forebay water level has approximately 6 feet 1 (approximately 1 foot pump suction level). System Pumps and two 1 System Pumps continued	ad increased to below normal above the minimum fire Two Circulating Water Normal Service Water d in operation.

NRC FORM 266A	U.S. NUCLEAR REGULATORY COMMISSION	APPROVED DMB ND. 3150-0104		
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0213 hours -	Circulating Water Syst shutdown. One Circula and two Normal Service in operation. Total of approximately 40 perce flow.	tem Pump 36P-1A ating Water System Pump Water Pumps continued cooling water demand was ent of the pre-event		
0215 hours -	Forebay water level ha approximately one foot	ad increased to below normal.		
Between 0215				
and 0430 hours -	Fire Jockey Pump 76P-3 service to maintain no pressure of approximat Pump 76P-3 operation a and Fire Pumps 76P-1, restored to service wi automatic starting.	was returned to ormal fire header cely 140 psig. Jockey appeared to be normal 76P-2 and 76P-4 were th the capability of		
0430 hours -	Forebay water level no	ormal.		
0940 hours -	Testing of Electric Fi Diesel Fire Pump 76P-4 recirculation flow com satisfactory results. vibration or other ind	tre Pump 76P-2 and for 20 minutes on mpleted with No unusual noise, lications noted.		
1332 hours -	Electric Fire Pump 76F to false main turbine (The Turbine Bearing F Subsystem is a closed Thus the only flow of necessary to flood the sprinkler/spray heads unusual noise vibratic were noted and the pum normal fire header pre	2-2 automatic start due bearing fire signal. Fire Protection head pre-action system. water was that e system as none of the were fused.) No on or other indications ap was shutdown when essure was verified.		
1820 hours -	Electric Fire Pump 76F based on engineering e performance test data. tests conducted prior of the intake structur	2-2 declared inoperable evaluation of pump The data was from to the partial blockage re with ice.		
February 26, 1993:				
0207 hours -	West Diesel Fire Pump inoperable due to engi pump performance testi	76P-1 declared ne overheating during ng.		

NRC FORM 366A (6-89)	ON APPROVED OMB ND: 3150-0104 EXPIRES: 4/30/92						
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Fire Pumps 76P-1, 2, 3, and 4 are designed for a minimum suction level of 239 feet 6 inches above sea level in the pump suction bays. As noted above, partial blockage of the intake resulted in a drain down of forebay and pump suction bays of approximately 10 feet. This resulted in a forebay water level between 236 and 237 feet above sea level. The bottom of the suction bell for fire pumps is at elevation 234 feet 8.75 inches; approximately 2 feet below the level observed by the operator at 0140 hours.

Telephone conversations with fire pump vendor personnel indicate that a forebay water level between 236 and 237 feet elevation would not be expected to cause damage to an operating fire pump for short time period that the pumps were operating. The relatively low flow while a fire pump is operating on recirculation flow (approximately 250 gpm) would not be expected to result in vortices and air being drawn into the pump. Notwithstanding the conversations with pump vendor personnel it is apparent that the Fire Jockey Pump (76P-3) did have some air drawn into the pump due to vortices at the pump suction or due to level in the pump suction bay decreasing to below the pump suction bell for a short time. This momentary loss of suction (or drawing of air) was evident from the Fire Header Pressure decrease which resulted in automatic starting of Fire Pumps 76P-1, 76P-2 and 76P-4.

### West Diesel Fire Pump 76P-1

On February 26, 1993, Fire Pump 76P-1 was shutdown and declared inoperable when engine overheating was evident approximately seven minutes after engine start for performance testing. Engine cooling is provided by a portion of pump discharge flow which is directed to the engine cooling heat exchanger.

Inspection of a Y-strainer in the cooling water flow path revealed metal pieces which appeared to be from broken pump internal parts. The pump was removed and replaced with a new pump of the same design flow and developed head. Fire Pump 76P-1 was declared operable on March 4, 1993 at 1655 hours following performance testing.

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Cause of Event:

# Electric Fire Pump 76P-2

The low discharge pressure on Fire Pump 76P-2 is attributed to normal wear. The pump has been inservice since 1973 during the completion of plant construction and preperational testing. No major maintenance work such as replacement or wear rings or other internal pump parts had been conducted during the past 20 years. Following rebuild of the pump which was formerly in service as 76P-1 (or purchase of a new pump) the Electric Fire Pump will be replaced. The currently installed 76P-2 will then be disassembled and inspected. This inspection may provide additional information concerning the cause of the low discharge pressure.

Personnel did not recognize that the fire pump performance requirement of 2,500 gpm at 125 psig was different than the more common calculation of Total Developed Head (TDH) which is used for monitoring pump performance in systems such as Core Spray or RHR/LPCI.

# West Diesel Fire Pump 76P-1

- Engine Overheating: Overheating of the engine for Fire Pump 76P-1 was determined to be caused by plugging of the cooling water Ystrainer with broken parts from the pump internals.
- 2. Pump Failure: The cause of the pump failure is attributed to normal wear. The metal parts found in the engine cooling Ystrainer were from a pump shaft bearing support. The pump would perform normally with the failed bearing support which is intended to reduce harmonic vibration. Other pump bearings were also severely worn and the upper bearing near the pump packing indicated overheating which is attributed to inadequate lubrication (with water) during operation of the pump for a few minutes while the forebay water level was low.

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Analysis of Event:

The inoperability of Fire Pumps 76P-1 and 76P-2 at the same time would have seriously degraded the plant fire suppression capability if the third fire pump had not been previously installed and available for operation.

Partial blockage of the plant cooling water intake with ice was not safety significant. Reducing the cooling water demand allowed the water level in the forebay area and pump suction bays to quickly return to near normal level. Residual Heat Removal Service Water (RHRSW) [BI] pumps and Emergency Service Water (ESW) [BI] pumps are designed for a minimum pump suction water level of 235 feet.

The combined maximum cooling water necessary for RHRSW and ESW pumps is approximately 22,000 gpm. This is a small fraction of the cooling water demand for operation of the plant at 100 percent rated thermal power. Additional information concerning the safety significance of partial blockage of the intake structure with ice is contained in LER-93-004.

The event requires a report under 10CFR50.73(a)(2)(i)(B). That is, the improper calculation of Fire Pump 76P-2 discharge pressure resulted in unknowingly continued operation of the plant without corrective action to restore 76P-2 to a condition where the pump would meet minimum flow and discharge pressure.

This LER is also submitted to satisfy the 14 day Special Report requirement of Technical Specification 3.12.A.1.d.2.C due to inoperability of Fire Pumps 76P-1 and 76P-2 at the same time. Further, this LER is submitted to satisfy the 30 day Special Report requirement of Technical Specification 3.12.A.1.C due to Electric Fire Pump 76P-2 being inoperable for more than seven days.

#### Corrective Actions:

- Fire Pump 76P-1 was replaced with a new pump and returned to service after performance testing.
- Fire Pump 76P-2 will be replaced with a new or rebuilt pump as soon as possible but no later than June 1, 1993.

NRC FCRM 3564	US NUCLEAR REQULATORY COMMISSION		A REAL PROPERTY AND A REAL PROPERTY OF THE PRO						
(66-31		APPROVED OMB NO. 3150-0104 EKPIRES: 4/30/82							
LICENSEE EVENT REPORT (LER) TEXT CONTINUATION		ESTIMATED BURDEN PER RESPONSE TO COMPLY WTH THIS INFORMATION COLLECTION REQUEST 50.0 HRS. FORWARD COMMENTS REGARDING BURDEN ESTIMATE TO THE RECORDS AND REPORTS MANAGEMENT BRANCH (P630), U.S. NUCLEAR REGULATORY COMMISSION, WASHINGTON, DC 20565, AND TO THE PAPERWORK REDUCTION PROJECT (2150-0104), OFFICE OF MANAGEMENT AND BUDGET, WASHINGTON, DC 20503.							
FACILITY NAME (1)	DOCKET NUMBER (2)	LER NUMBER (6)	PAGE (3)						
James A. FitzPatrick Nuclear Power Plant	0   5   0   0   3   3   3	YEAR         SEQUENTIAL         REVISION           9         3         0         0         6         0         0	1 /1 OF 1 1						
TEXT (If more space is required, use additional NNC Form 366A's) (17)			land and a dealer dealer of						
<ol> <li>Fire pump performance te the proper steps for cal the next required perfor</li> <li>Additional corrective ac cooling water intake block</li> </ol>	est procedures will culation of pump d mance of that proc ctions related to d ockage are discusse	be revised to pro ischarge pressure edure. letecting and mitig d in LER-93-004.	ovide by ating						
Additional Information:									
Failed Components:	Fire Pump 76P-1								
Manufacturer:	Johnston Pump Com	ipany							
Previous Similar Events: No LERs have been previously submitted concerning inoperability of both fire pumps.									
Update Plans and Correction c	of Error in Prompt	Report:							
An update of this LER is NOT expected to be submitted unless examination of the fire pumps or other information results in a substantial change in the understanding of the potential consequences or safety significance of the event.									
The initial notification of t transmission contained an err following sequence of pump ir	chis event made via cor. The notificat noperability:	ENS and the facsi ions indicated the	mile						
- Diesel Fire Pump 76P-1 inoperable at 0207 on February 26, 1993									

- Electric Fire Pump 76P-2 inoperable at 1500 on February 26, 1993

The actual sequence was:

- Electric Fire Pump 76P-2 inoperable at 1820 on February 25, 1993
- Diesel Fire Pump 76P-1 inoperable at 0207 on February 26, 1993

The NRC Resident Inspector and Licensing Project Manager were both informed of the error verbally. The error did not have any effect on response to the event.