

Ref. 10CFR50.73(a)(2)(11)

Entergy Operations, Inc. P.O. Box B Killona, LA 70060 Tel 504-729-6650

W3B5-5 -0065 A4.05 QA

March 8, 1991

U.S. Nuclear Regulatory Commission ATTENTION: Document Control Desk Washington, D.C. 20555

Subject: Waterford 3 SES Docket No. 50-382 License No. NPF-38 Reporting of Licensee Event Report

Gentlemen:

Attached is Licensee Event Report Number LER-89-007-01 for Waterford Steam Electric Station Unit 3. This Licensee Event Report supplement is submitted to provide additional information resulting from investigation of the events described including inconsistencies with Design Basis Documentation and Surveillance procedures. This Licensee Event Report is submitted pursuant to 10CFR50.73 (a)(2)(ii).

Very truly yours,

J.R. McGaha General Manager - Plant Operations

JRM/LDC/rk Attachment

cc: Messrs. R.D. Martin G.L. Florreich J.T. Wheelock - INPO Records Center E.L. Blake D.L. Wigginton NRC Resident Inspectors Office

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ABSTRACT (Limit to 1400 spaces, i.e. approximately fifteen single	ADACA Typewritten Innex! (16)											

At 1100 hours on March 31, 1989, Waterford Steam Electric Unit 3 was Operating at 100% power when the issue of reportability was raised on the sizing of the Instrument Air (IA) accumulators which supply the Safety Injection (SI) Recirculation Sump Outlet Isolation Valves, SI-602A&B. Design requirements did not consider certain accident scenarios, with a postulated loss of IA where operation of the valves may be required. Manual operation of the valves was not considered an adequate backup due to potential radiation levels at the valve location. Therefore, the plant was operated in an unanalyzed condition since initial startup.

On February 6, 1991, a review of Surveillance Procedures revealed that the plant was operated with a nitrogen accumulator IV leakage rate of 57.6 psi/hr vice the 55 psi/hr required by Design Basis Documentation (DBD). Accumulator IV supplies nitrogen to operate the SI pump suction valves to the refueling water storage pool on loss of IA. This condition existed from November 23, 1990 through February 7, 1991.

The root cause of this event was an inadequate review of design requirements implemented as part of the post-TMI action plan. Phase one of DC 3195 has been implemented to provide a nitrogen source of gas to provide remote operation of SI-602A&B and a review of the DBD is being conducted.

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At 100 hours on March 31, 1989, Waterford Steam Electric Station Unit 3 was operating at 100% power when the issue of reportability was raised on the installed design of the instrument air (IA) accumulators (EIIS Identifier LD-ACC) which supply the Safety Injection Sump Recirculation Outlet Isolation Valves (SI 602A&B) (EIIS Identifier BP-V). The accumulators were designed to allow each valve to cycle once within one hour during a design large break loss of coolant accident (LOCA) coincident with a loss of IA. During a small break LOCA scenario the valves may be required to operate longer than one hour after the IA supply is compromised. The radiation levels in the vicinity of SI 602A&B would peak at 910 rem/hour during a design large break LOCA according to section 12.3A of the Final Safety Analysis Report (FSAR). Thi would not allow personnel to enter the SI 602A&B area after a LOCA. However, the radiation levels coincident with a design small break LOCA would be much lower and would likely not differ appreciably from normal levels, thus permitting access to the valves. Because an analysis is not available for radiation levels coincident with a design small break LOCA, loca' manual operation of SI 602A&B cannot be considered an adequate backup method for remote valve operation. Thus, the plant is considered to have operated is an unanalyzed condition since issuance of the operating license.

SI 602A&B are closed during normal operation and open upon receipt of a Recirculation Actuation Signal (RAS). A RAS is generated when two out of four Refueling Water Storage Pool (RWSP) (EIIS Identifier BP-TK) low level signals received with a Safety Injection Actuation Signal present. The RAS then opens SI 602A&L at a RWSP level of 10%. The suction of the Containment Spray Pumps (CSPs) (EIIS Identifier BE-P) and the High Pressure Safety Injection Pumps (EIIS Identifier BQ-P) can then transfer from the RWSP to the SI Sump during a LOCA. This transfer maintains an adequate supply of water for reactor coolant system (EIIS Identifier AB) cooling t roughout an accident scenario.

NRC FORM 386A (6.89)	APPROVED OMB NO. 3150-0104 EXPIRES 4/30/92									
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General Design Criterica 2 as stated in the Final Safety Analysis Report (FSAR) Section 3.1.2 requires components that are vital to the mitigation and control of accident conditions be designed to withstand the effects of a LOCA coincident with the effects of a Safe Shutdown Earthquake (SSE). SI 602A&B must therefore operate during a LOCA concurrent with a SSE. Because the 1A system upstream of the accumulators is not designed to survive a SSE, the stored air in the accumulators is required to operate SI 602A&B during the above conditions. The installation specifications required the accumulators to store adequate air pressure to cycle the valves once following a loss of IA lasting one hour post LOCA. This was the design criteria at the time of installation and was not reevaluated when NUREG 0737 was implemented.

n January 1988, Waterford Steam Electric Station Unit 3 received NRC Information stice No. (IEN) 87-29, Supplement 1, "Air Systems Problems at U.S. Light Water Reactors." Following a review of the IEN, recommendations were made to improve the air systems at Waterford 3. A concern in the review was testing air accumulators for leakage with their IA supply isolated. Subsequently, operations personnel issued Problem Evaluation Information Request (PEIR) 60951 for information to develop acceptable test criteria for the SI 602 accumulators. One question asked in the PEIR was, "What is the length of time the accumulators are required to maintain sufficient pressure to perform their function?" The response to the PEIR stated that "the Architect Engineer's specifications state that the accumulators were designed to maintain sufficient pressure to perform their function for one hour." This response was not satisfactory to Operations personnel. At this time, NRC Ceneric Letter 88-14, "Instrument Air Supply System Problems Affecting Safety Related Equipment," was received. A task force was formed to ensure the issues in this letter were evaluated and to draft a response. One issue the task force considered was the SI 602 accumulator design. In January 1989, PEIR 10673 was generated to resolve the issue that SI 602A&B may need to operate Leyond the current one hour as designed. This potential accumulator size discrepancy was reported to the NRC in the response to Generic Letter 88-14, letter W3P89-0028 dated February 21, 1989. The letter stated the issue was being reviewed under PEIR 10673.

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On March 3C, 1989, an on-site NRC inspection team reviewed the response to Generic Letter 88-14 with management. Nonconformance Condition Identification (NCI) 262265 was then issued to obtain a preliminary engineering evaluation. On March 31, 1989, the situation was determined to be reportable as an unanalyzed condition. The NCI was evaluated, and a graph of required IA header pressure versus maximum allowable accumulator pressure decay rate was developed. By maintaining IA pressure above the graph's curve, the accumulators would be able to maintain sufficient air pressure to operate SI 602A&B once within four hours following a loss of IA. The four hour time limit is a concern for a 0.01 ft small break LOCA. For this size LOCA, a RAS would occur at slightly less than four hours. However, one CSP must be operated continuously to assure that a RAS would occur within four hours. The area in the vicinity of SI 602A&B is considered to be a high radiation area in the event of a LOCA. For a break smaller than 0.01 ft, the time to a RAS will be greater that four hours FSAR Figure 15,6-173 indicates the core is not uncovered for breaks of 0.01 ft and smaller. Therefore, for breaks of 0.01 ft² and smaller there should not be a significant radiation field in the area and 5. 602A&B could most probably be manually operated.

Considering the available options, operating a CSP continuously until a RAS is not desirable. The actual leak rate of air from the accumulators combined with the normal operating pressure of IA ensures that the accumulators will have sufficient air pressure to operate SI 602A&B longer than four hours after a loss of IA. In a conference call on April 4, 1989, NRC Region IV personnel were informed that the CSPs would not be run continuously during an accident condition. The SI 602 accumulators are expected to maintain adequate air pressure much longer than four hours. During the next quarter the pressure decay rate of the accumulators was checked monthly rather than quarterly to demonstrate that sufficient air pressure could be maintained.

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On April 20, 1989, an addendum to NCI 262265 was approved. For the limiting 0.01 ft^2 small break LOCA, a RAS is predicted to occur within 16 hours without CSP operation. Because this scenario is the most limiting condition, another graph of IA header pressure versus accumulator pressure decay rate was produced. Operations issued Standing Instruction 89-04 to establish IA operation with the revised IA header pressure graph. If IA pressure drops below the normal 16 hour operating curve established in the addendum to NCI 262265, IA pressure will be restored above the curve within one hour or the plant will be placed in hot standby within the next six hours. Standing Instruction 89-04 also established operability of the SI +02 memory based on the 16 hour curve and instructed that IA pressure be maintained on the shift supervisor and control room supervisor turnover sheets.

Long term corrective action has been initiated with the approved Design Change (DC) 3195. DC 3195 will be installed in two phases. Phase I has been completed and provides safety related tubing connections to allow an alternate means to supply nitrogen backup for operation of SI-602A&R. The nitroger backup is located in an accessible area such that SI-602A&B can be operated in the limiting scenario, without radiological exposure concerns to the operators. Phase I of DC 3195 was completed on March 12, 1990, and as a result, Standing Instruction 89-04 was cancelled. Phase II of DC 3195 provides long term corrective action by installing motor operated valves for SI 602A&B.

The root cause of this event was an inadequate review of design requirements implemented as part of the post-TMI action plan. The SI 602A&B accumulator specifications were based on a large break LOCA with IA not available and a RAS generated within one hour. The accumulators were not reevaluated during construction to ensure they were adequately designed for the small break LOCA. PEIR 71128 was initiated to review the design basis of the air and nitrogen accumulators with respect to small break LOCAs.

NRC FORM 366A (6-89)	U.S. NUCLEAR REGULATORY COMMISSION	APPROVED OMB NO. 3180-0104 EXPIRES 4/30/92							
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As a result of the problems identified with accumulator sizing and questions concerning the design basis of the air and nicrogen accumulators, formulation of a Design Basis Document (DBD) was initiated. W3-DBD-014 for Safety Related, Air Operated Valves, was issued on March 21, 1990. PEIR 71128 and W3-DBD-014 spect fically documented the design basis of the air and nitrogen accumulators and the associated leak rate requirements.

On February 6, 1991, a review of Surveillance Tests revealed that an inccasistency existed between W3-DBD-014 and the Operations department leak rate testing procedures. Specifically, W3-DBD-014 requires Nitrogen Accumulator IV leak rate to be less that 55 psi/hr while Surveillance Operating Procedure (OP)-903-032, Quarterly Inser ise Test (IST) Valve Test, allows Mitrogen Accumulator IV leak rate to be less than or equal to 5 psi, over a 5 minute interval, which equates to a leakage rate of 60 psi per hour or less.

Nitrogen Accumulator IV provides the backup motive gas for the operation of SI-106A&B, the RWSP outlet isolation values to the SI pump suction. SI-106A&B are normally open, fail as is on loss e^{c} power or loss of air pressure supply, and are manually closed after a recirculation actuation signal (RAS) to prevent back flow from containment (as a result of high containment pressure and the failure of a check value to close which are in series with the RWSP suction values).

OP-903-032 tests the operability of check valves associated with Nitrogen Accumulators on a quarterly bas: s. Testing of check valve NG-704 for operability in accordance with OP-903-032, also provides some 'ndication of the Nitrogen Accumulator IV leakrate over a 5 minute interval. On November 23, 1990, OP-903-032 was performed and resulted in a leak rate of 4.8 psi in 5 minutes, equating to a 57.6 psi/hr leak rate for Accumulator IV.

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performed on Nitrogen Accumulator IV was completed on October satisfactory leakage rate of 50 psi/hr.

OP-903-032 and OP-903-033 will be revised prior to performance of the procedure to incorporate DBD data. The W3-DBD-014 basis is being re-examined to specifically address the operability requirements of SI-106A&B and other similar valves during a small break LOCA with loss of IA. The DBD will be compared to other procedures to identify if additional inconsistencies exist. A revision to this LER will be submitted after information related to this event and DBD is re-examined and/or additional corrective action implemented.

SIMILAR EVENTS

TEXT

NONE

PLANT CONTACT

G.M. Davis, Event Analysis, Reporting & Response Manager, 504/464-3153.