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MINET Code Documentation

Prepared by G. J. Van Tuyle, T. C. Nepsee, J. G. Guppy

Brookhaven National Laboratory

Prepared for
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Abstract

The MINET computer code, developed for the transient analysis of fluid flow and heat transfer, is documented in this four-part reference. In Part 1, the MINET models, which are based on a momentum integral network method, are described. The various aspects of utilizing the MINET code are discussed in Part 2, The User's Manual. The third part is a code description, detailing the basic code structure and the various subroutines and functions that make up MINET. In Part 4, example input decks, as well as recent validation studies and applications of MINET are summarized.

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FOREWORD

Version 1 of the MINET computer code, as documented in this report, is currently a very usable and useful code, and reflects a considerable development and validation effort. However, further improvements and enhancements are continually being incorporated in the code library. In particular, a control system model and a "rotor" module are currently under development, and will be in Version 2 of MINET, available around late 1984 or early 1985. We will make every effort to keep this document as up-to-date as possible, at least for those copies that the authors have distributed directly. Should you wish to know whether the copy you have is up-to-date, or what improvements have been made recently, please contact us.

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VARIABLES USED IN MINET EQUATIONS

- a_j - coefficients of pump head curve
- A_h - heat transfer area in heat exchanger h
- A_i - flow area for node i
- A_{max_v} - maximum (full open) flow area through valve v
- A_{t_h} - tube cross-sectional area in heat exchanger h
- A_v - flow area through valve v
- C_{pt_i} - specific heat of heat exchanger tube material in node i
- D_{eq} - equivalent hydraulic diameter
- D_I - inner diameter of HX tube
- D_o - outer diameter of HX tube
- E_b - enthalpy at boundary module b
- E_i - node average enthalpy for node i
- E_{IM} - enthalpy entering segment from bordering module IM
- E_j - enthalpy at nodal interface j
- E_{mi} - enthalpy at inlet interface of segment m
- E_{mo} - enthalpy at outlet interface of segment m
- E_n - average enthalpy in accumulator n
- E_{OM} - enthalpy in segment outlet bordering module OM
- f_i - friction factor in node i
- f_{bi} - adjustment factor for heat transfer bridge i
- f_{ts}^{eff} - turbine stage efficiency adjustment factor
- f_{ah} - heat transfer area correction factor for heat exchanger h
- f_{k_i} - impedance coefficient for node i
- f_{l_n} - liquid level in accumulator n
- f_{v_n} - volume fraction of liquid in accumulator n

$F_{k_{tb}}$ - modified Stadola constant for turbine stage
 f_{v_v} - stem power factor for valve v (area = (stem) ^{f_{v_v}} · A_{max_v})
 g - gravitational constant
 H_p - head for pump p
 h_i - heat transfer coefficient inside tube
 h_o - heat transfer coefficient outside tube
 H_p - Pump Head
 H_{ref} - head for pump p at rated frequency and flow rate
 i - node number
 I_m - inertial term for segment m
 j - interface number
 k - current time step number
 k_i - heat exchanger tube conductivity in node i
 K_v - loss coefficient for valve v
 ℓ - advanced time step number
 M_d - number of segments in network d
 M_{f_d} - first segment number in network d
 $M_{\&_d}$ - last segment number in network d
 n - node number relative to the first node in segment; volume number
 N_d - number of volumes in network d
 N_m - numbers of nodes in segment m
 N_{b_d} - number of boundary modules in network d
 $N_{b_{i_d}}$ - number of inlet boundary modules in network d
 $N_{b_{o_d}}$ - number of outlet boundary modules in network d
 N_{f_m} - first node in segment m
 NH_m - number of heat exchangers in segment m
 $N_{\&_m}$ - last node in segment m

P_b - pressure at boundary module b
 P_{IM} - pressure in module at inlet of segment M
 P_m - pressure in segment m
 P_{mi} - pressure at inlet of segment m
 P_{mo} - pressure at outlet of segment m
 P_n - pressure in volume n
 P_{OM} - pressure in module at outlet of segment M
 P_{ib} - pressure at inlet boundary module
 P_{ob} - pressure at outlet boundary module
 Q_i - heat transfer rate into node i
 Q_m - heat transfer into segment m
 Q_n - heating rate in volume n
 QA_h - total heat transfer rate in heat exchanger h
 QA_m - total heat transfer rate in segment m
 r_m - pressure change across segment m
 S_v - stem position for valve v
 S_{dv} - demanded stem position for valve v
 t - time
 T_{c_i} - HX tube wall centerline temperature for node i
 V_i - volume of node i
 V_n - volume of volume n
 W_b - mass flow rate at boundary module b
 W_i - mass flow rate at node i
 W_j - mass flow rate at nodal interface j
 W_m - segment m average mass flow rate
 W_m^{est} - estimated advanced time mass flow rate for segment m

W_{mi} - segment m inlet mass flow rate
 W_{mo} - segment m outlet mass flow rate
 W_r - relative flow rate through pump
 W_{Cm} - choked mass flow rate limit for segment m
 W_{ib} - mass flow rate at inlet boundary module b
 W_{ob} - mass flow rate at outlet boundary module b
 W_p - mass flow rate through pump p
 W_{ref} - reference flow rate through pump p
 W_v - mass flow rate through valve v
 Z_{mi} - elevation at inlet of segment m
 Z_{mo} - elevation at outlet of segment m
 α_j - pressure loss factor for node i
 α_m - pressure loss factor for segment m
 β_m - pressure loss term for segment m
 δ_{ip} - 1 if pump at node i, otherwise, = 0
 δ_{iv} - 1 if valve at node i, otherwise, = 0
 ΔP_{aj} - pressure change due to acceleration
 ΔP_{fj} - pressure change due to friction
 ΔP_{gj} - pressure change due to gravity
 ΔP_{kj} - pressure change due to form loss across node
 ΔP_{nm} - presure difference between segment m junction and volume n
 average pressure
 ΔP_p - pressure change across pump p
 ΔP_v - pressure change across valve v
 ΔX_j - length of node i
 ΔZ_j - elevation change across node i

- ξ - relative convergence criteria
- ρ - density
- ρ_n - accumulator n average density
- ρ_{ti} - tube wall density in node i
- Ω_n - interior angle between vertical and a radian to the liquid level in
a cylindrical volume (see Fig. 1.2-2)
- τ_i - tube wall temperature time constant in node i
- τ_p - pump coastdown time constant for pump p
- τ_t - turbine coastdown time constant
- τ_v - valve time constant for valve v
- ω - pump impeller speed in rpm
- ω_{dp} - demanded impeller speed in pump p
- ω_t - turbine speed
- ω_{dt} - turbine demand speed
- ω_{ref} - reference impeller speed in pump p
- x - fluid quality

INTRODUCTION

MINET (Momentum Integral NETWORK) is a computer code developed for the transient analysis of intricate fluid flow and heat transfer networks, such as those found in the balance of plant in power generating facilities. It can be utilized as a stand-alone code, or interfaced to another computer code for concurrent analysis. Through such coupling, a computer code currently limited by either the lack of required component models or large computational needs can be extended to more fully represent the thermal hydraulic system, thereby reducing the need for estimating essential transient boundary conditions.

MINET is based on a momentum integral network method, which is an extension of the momentum integral method [1]. This method uses a two-plus equation representation of the thermal-hydraulic behavior of a system of heat exchangers, pumps, pipes, valves, tanks, etc. It is computationally faster than the three equation methods used in RELAP [2] and its descendants, yet represents the compression and expansion of water/steam due to changes in enthalpy and pressure.

The MINET representation of a system comprises one or more networks of volumes, segments, and boundaries. Networks are linked together via heat exchangers only, i.e., heat can transfer between networks, but fluids cannot. Volumes are used to represent tanks or other voluminous components, as well as locations in the system where significant flow divisions or combinations occur. Segments are composed of one or more pipes, pumps, heat exchangers (inside or outside of tubes), turbines and/or valves, each represented by one or more nodes. Boundaries are simply points where the network interfaces with the user or another computer code.

MINET calculations are performed at two levels, i.e., the network level (volumes), and the segment level. Equations conserving mass and energy are used to calculate the pressure and enthalpy within volumes. An integral momentum equation is used to calculate the segment average flow rate. In-segment distributions of mass flow rate and enthalpy are calculated using local equations of mass and energy. The segment pressure is taken to be the linear average of the pressure at both ends.

The computational speed and power of the MINET method results largely from the local suppression of sonics in flow segments. It is implicitly assumed that the propagation of pressure waves in pipes, pumps, heat exchangers, and valves takes place on a time scale much smaller (milliseconds) than the transient of interest (seconds to minutes). Of course, such an assumption would be incorrect regarding the large break loss-of-coolant accident (LOCA) often postulated for light water reactor primary loops. However, for balance of plant systems, one is generally more interested in representing slower transients and overall plant behavior than large break LOCA's.

With few exceptions, the system being represented is closed, and accessed only through the boundary modules. The exceptions involve certain variables which are control system related, e.g., pump and turbine speed and valve positions. Boundary modules receive user input data (or data from another code) regarding pressure or flow rate and temperature (used only if in-flow). MINET calculations advance the other module variable (flow rate or pressure) and temperature (if out-flow).

The current MINET version uses a homogeneous equilibrium model of two phase flow, supplemented by various two phase correlations. Extension of the method to include an improved representation of the two phase phenomena, whether through slip, drift, or two fluid models, should be straightforward. This is because the intricacies of these models are less likely to pose difficulties in the numerics of MINET than codes where local pressures are calculated via time-dependent equations.

This document includes four major topics; 1) model descriptions, 2) a user's guide, 3) a code description, and 4) an example problem and applications section. These four areas are included in this documentation because of two strong characteristics of the MINET code; 1) its generality and 2) its potential applications.

The first reason for such a lengthy description of MINET is that, as a fully generalized code, it is designed to continue calculations even under conditions of severe distortion. Thus, the user must take some care to state his problem correctly, or MINET may actually analyze an unintended or unrelated problem. The extent to which MINET is documented herein is to allow the user to gain sufficient knowledge to properly exercise the code's capabilities.

The second reason for detailing the MINET models and code description is that potential applications far exceed those allowed by the currently available component modules. With the component modules easily accessible to the user, a relatively minor code modification could allow the user to represent a component feature that we have not yet considered.

However, one must realize that the details provided in this documentation are not sufficient to allow an actual reproduction of MINET. Several parts of MINET are very sophisticated and would require a major effort to duplicate.

Furthermore, the momentum integral network method used in MINET contains numerical subtleties that require special handling. Thus, it is strongly recommended that a potential user start with MINET and make modifications to the existing code than to try to develop a special purpose code based on this documentation.

1. MINET MODELS

1.1 MOMENTUM INTEGRAL NETWORK METHOD

The method employed in the MINET code is a major extension of a momentum integral method developed by Meyer [1]. Meyer integrated the momentum equation over several linked nodes, called a segment, and used a segment average pressure, evaluated from the pressures at both ends. Nodal mass and energy conservation determined nodal flows and enthalpies, accounting for fluid compression and thermal expansion.

In MINET, a network structure was built around Meyer's momentum integral model for the flow segment. In this extended method, a system is represented using one or more flow networks, connected to one another only through heat exchangers. Each network is composed of segments, volumes, and boundaries. Segments contain one or more pipes, pumps, heat exchangers, turbines and valves, each of which is represented using one or more nodes. Volumes represent voluminous components and significant flow junctions. Volumes and boundaries are connected by segments.

The calculation of pressures in MINET centers on the volumes. Here, equations for the conservation of mass and energy are used to advance volume pressure and enthalpy

$$V_n \frac{d\rho_n}{dt} = \sum_{\text{Inlets}} W_{mo} - \sum_{\text{Outlets}} W_{mi} , \quad (1.1-1)$$

and

$$V_n \frac{d(\rho_n E_n)}{dt} = \sum_{\text{Inlets}} W_{mo} E_{mo} - \sum_{\text{Outlets}} W_{mi} E_{mi} + Q_n + V_n \frac{dP_n}{dt} \quad (1.1-2)$$

The equation of state is used to express the density time derivative in terms of pressure and enthalpy,

$$\frac{d\rho_n}{dt} = \left(\frac{d\rho_n}{dP_n} \right) \frac{dP_n}{dt} + \left(\frac{d\rho_n}{dE_n} \right) \frac{dE_n}{dt} \quad (1.1-3)$$

Note that the mass flow rate and enthalpy exiting the volumes are those entering the segment, and the same parameters exiting the segment are inlet values for the volumes.

Segment inlet and outlet pressures are calculated from those in bordering modules. If a boundary module is at the end of a segment, the pressure at that end is equal to the boundary module pressure. For the case of a volume at the segment end, the pressure differential between the volume port where the segment connects and the position where the volume average pressure is defined must be calculated. As volumes are considered to be stagnant, i.e., zero flow rate, only elevation head needs to be considered:

$$P_{mi} = P_{IM} - \rho g (Z_{mi} - Z(P_{IM})), \quad (1.1-4)$$

$$P_{mo} = P_{OM} - \rho g (Z_{mo} - Z(P_{OM})). \quad (1.1-5)$$

When the volume contents are taken to be homogeneously distributed, the volume average pressure is defined at the center. If the volume contents are separated into liquid and vapor regions, the volume average pressure is located near the middle of the liquid region. Equations (1.1-4) and (1.1-5) still apply, but greater care must be taken because the density differences between the region necessitate evaluating the elevation head in two pieces, i.e., above and below the liquid level.

The segment pressure is taken to be the average of the pressures at both ends, i.e.,

$$P_m = (P_{mi} + P_{mo})/2 \quad (1.1-6)$$

It is at this segment average pressure that saturation properties are calculated for the entire segment, a step that results in significant computational savings.

Similarly, a segment average flow rate, W_m can be defined as

$$W_m = \frac{N\ell_m}{\sum_{i=Nf_m}} \left(\frac{\Delta X_i}{A_i} W_i \right) / I_m, \quad (1.1-7)$$

where I_m is the segment inertia, defined as

$$I_m = \frac{N\ell_m}{\sum_{i=Nf_m}} \left(\frac{\Delta X_i}{A_i} \right). \quad (1.1-8)$$

This segment average flow rate is advanced using the segment integral momentum equation:

$$I_m \frac{dW_m}{dt} = P_{mi} - P_{mo} + r_m, \quad (1.1-9)$$

where r_m is the total pressure change across the segment.

$$r_m = \sum_{i=Nf_m}^{N\ell_m} (\Delta P_{g_i} + \Delta P_{f_i} + \Delta P_{a_i} + \delta_{iv} \Delta P_v + \delta_{ip} \Delta P_p + \Delta P_{k_i}). \quad (1.1-10)$$

The first three terms on the right hand side of Eq. (1.1-10) are pressure changes due to gravity, friction, and acceleration:

$$\Delta P_{g_i} = -\rho_i g \Delta Z_i, \quad (1.1-11)$$

$$\Delta P_{f_i} = -f_i |W_i| W_i \Delta X_i / 2 \rho_i A_i^2 D_{eq}, \quad (1.1-12)$$

and

$$\Delta P_a = \left\{ \frac{W_j^2}{\rho_j} - \frac{W_{j+1}^2}{\rho_{j+1}} \right\} / A_i^2. \quad (1.1-13)$$

The fourth and fifth terms are the contributions due to valves and pumps in the segment, and will be discussed in later sections. The sixth term is the form loss pressure change, and is used to account for miscellaneous losses due to bends, obstructions, etc. In MINET this term is calculated as:

$$\Delta P_{k_i} = \frac{-fk_i |W_m| W_m}{2 \rho A^2 D_{eq}} \quad (1.1-14)$$

when fk_i is a nodal loss coefficient, which is calculated from the user input module loss coefficient. In practice, this coefficient is selected to match pressures and flow rates to steady state operating conditions, and is maintained at the same value for transient calculations.

The enthalpy of flow entering a segment from a volume or boundary module is determined by conditions in that bordering module. If the flow is coming from a boundary module or a volume with homogeneously distributed contents, the segment inlet enthalpy is set to the enthalpy in the bordering module. If the flow is entering from a volume with two separated regions, each at saturation conditions, the segment inlet enthalpy is set to saturated liquid or vapor enthalpy, depending on whether the segment connects below (liquid) or above (vapor) the liquid level.

In-segment distributions of mass flow rate and enthalpy are calculated using nodal mass and energy equations:

$$V_i \frac{d\rho_i}{dt} = W_j - W_{j+1} \quad , \quad (1.1-15)$$

$$V_i \frac{d(\rho_i E_i)}{dt} = W_j E_j - W_{j+1} E_{j+1} + Q_i + V_i \frac{dP_m}{dt} \quad (1.1-16)$$

where, for a segment node:

$$\frac{d\rho_i}{dt} = \left(\frac{\partial \rho_i}{\partial P_m} \right) \frac{dP_m}{dt} + \left(\frac{\partial \rho_i}{\partial E_i} \right) \frac{dE_i}{dt} \quad (1.1-17)$$

At this point, all of the basic equations essential to MINET have been written. While certain auxiliary equations are needed for the various modules (see Section 1.2), the equations listed above form the core for our basic method. The method by which these equations are used to advance the representation in time is relatively straightforward.

In systems which can be represented by MINET, heat exchangers are frequently shared by segments in two networks, with the flow from one segment passing through the tubes and the flow from the other passing on the outside. In order to decouple these segments during a transient time step, the tube temperatures are treated explicitly in the heat transfer calculations, and are not advanced until the end of the step.

With the segments and networks thus decoupled, MINET transient calculations proceed in a three step process, repeated for each network. The initial step is to march through the network segments, loading the segment matrix equation:

$$\underline{\underline{A}}_S \underline{x}_S = \underline{\underline{B}}_S \underline{y}_S \quad , \quad (1.1-18)$$

and solving for the segment response matrix, $\underline{B}'_S (= \underline{A}_S^{-1} \underline{B}_S)$. For a segment s with N_S nodes, $2N_S+2$ linearized equations are loaded, including N_S nodal mass conservation equations, a segment momentum equation, and a total of N_S+1 donor-cell differenced nodal energy equations and segment inlet enthalpy boundary conditions. Vector \underline{x}_S contains nodal interface enthalpies and flows, and vector \underline{y}_S includes changes in enthalpy and pressure in the modules at the segment ends.

The second stage is to march through the network volumes, loading the network matrix equation

$$\underline{C}_n \underline{v}_n = \underline{D}_n \quad , \quad (1.1-19)$$

and solving to advance volume enthalpies and pressures. For a network n with N_n volumes, N_n conservation of mass and N_n conservation of energy equations are loaded. The terms for the mass and energy entering and exiting the volumes are evaluated using the segment response matrices, \underline{B}'_S , thereby linking the volumes.

The final step is to march through the network segments, using the solution from Eq. (1.1-19) to determine vector \underline{y}_S . The segment response matrix, \underline{B}'_S , is then multiplied by \underline{y}_S , and the nodal interface enthalpies and flows are advanced. After segment conditions are advanced in all networks, the heat exchanger tube temperatures are advanced.

Two features of the method account for the flexibility and speed of MINET. First, segment nodes connect only to immediately adjacent nodes, causing matrix \underline{A}_S to be banded, except for the momentum equation. This allows the storage of matrix \underline{A}_S , and the solution of Eq. (1.1-18), in close-packed form, i.e., with large blocks of zeroes suppressed. Thus, the complexity of the flow network is absorbed entirely in Eq. (1.1-19), where the matrices are lower order. Second, because a segment average pressure is used, saturation properties are evaluated once per segment per step.

1.2 MINET COMPONENT MODULES

Various component models, called "modules", are available in MINET, with multiple options available for each. These modules were developed to be compatible with the basic MINET methodology, and are similar to models found in other systems codes. Each MINET module can be used to represent one or more parallel components, in which the mass flow rate is divided equally among the parallel units.

1.2.1 PIPE

Pipes are the simplest components, and require minimal user input. The user has the option of specifying a non-zero heat source, which can be altered during the transient through value vs. time tables.

1.2.2 PUMP

A pump is modeled as a pipe with an additional pressure gradient term, due to the action of the pump. The pressure change across a pump is proportional to the pump head,

$$\Delta P_p = \rho_p g H_p . \quad (1.2-1)$$

The intricate relationship between the pump head, the relative pump speed, and the relative mass flow rate, is generally available in the form of homologous pump curves. For the pump model currently used in MINET, the pump head is given by:

$$H(\omega, W) = H_{ref}(\omega_{ref}, W_{ref}) \cdot \left(\frac{\omega}{\omega_{ref}} \right)^2 . \quad (1.2-2)$$

$$\left\{ a_1 + a_2 W_r + a_3 W_r^2 + a_4 W_r^3 + a_5 W_r^4 \right\} ,$$

where reference conditions are user input head, flow, and speed at some known operating condition, H is the pump head at given speed ω and relative flow W_r , given by:

$$W_r = \frac{W}{W_{ref} \cdot (\omega/\omega_{ref})} \quad (1.2-3)$$

Equations 1.2-2 and 1.2-3 effectively reproduce the classic head curves shown in Figure 1.2-1 [3]. Thus, by specifying three reference conditions and the Head vs. Flow characteristics at a given speed, the user is implying a family of curves valid for all flow rates and speeds.

1.2.3 VALVE

Representation of valves depends on whether choking conditions exist. If the flow is unchoked, a form loss is calculated for the valve,

$$\Delta P_V = -K_V |W_V| W_V / 2\rho_V A_V^2, \quad (1.2-4)$$

where K_V is the loss coefficient. The valve flow area is calculated from the valve stem position, and user input maximum flow area and stem power coefficient:

$$A_V = (S_V)^{f_V} A_{MAX_V} . \quad (1.2-5)$$

The user has the option of neglecting the choke flow calculation, as one might do with a valve controlled to regulate flow rate. If a choked flow calculation is called for, MINET will use an extended Henry-Fauske [4] model if subcooled, a Moody [5] model in two-phase flow, or an isentropic model if superheated, to calculate the choked mass velocity $G_C (=W/A)$. The valve flow area given by Eq. (1.2-5) is used to multiply this choked mass velocity to obtain a choked mass flow rate. If the mass flow rate through the valve at a given time is below the choked flow rate, calculations proceed normally.

In the case when the mass flow rate exceeds the choked flow limit, the mass flow rate must be set to the choke flow rate for the next step. Because

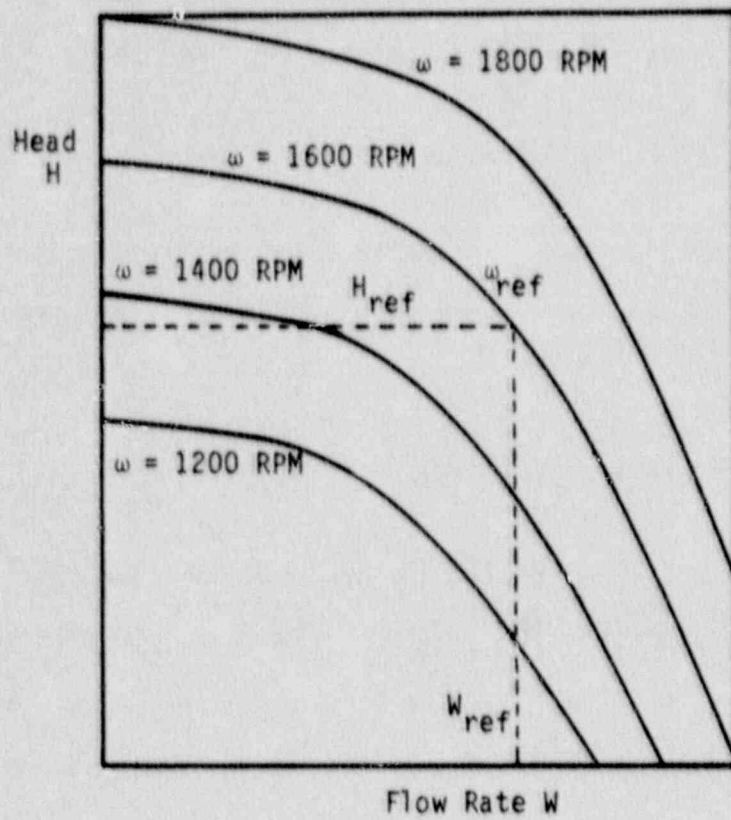


Figure 1.2-1. Pump Curves, Head vs Flow At Various Speeds [3]

this contradicts the segment integral momentum equation, care must be taken to isolate any valve where choking is allowed in a segment by itself. If choking occurs, the segment momentum equation is overwritten with the choke flow limit:

$$W_m = WC_m. \quad (1.2-6)$$

1.2.4 VOLUME

While much of the volume behavior is represented by Eqs. (1.1-1) and (1.1-2), additional equations are needed. Because the heating term, Q_n , in Eq. (1.1-2) is a user input and distributed uniformly throughout the volume, this does not present a problem.

If the user wants the contents of a volume separated into saturated liquid and vapor regions, one does so by specifying the L3PSEP parameter equal to 2 or 3 (separated in transient only). For volumes with uniform cross sectional area (i.e., $dA/dz = 0.0$), e.g., an upright drum, the volume fraction, fV_n , is equal to the level fraction, fL_n .

The quality, x , can be calculated as:

$$x = 1 / \left(1 + \frac{\rho_f}{\rho_g} \left(\frac{fV_n}{1 - fV_n} \right) \right), \quad (1.2-7)$$

when ρ_f and ρ_g are saturated liquid and vapor density, respectively.

One of the input options allows the user to specify volumes as horizontal cylinders. In the case where the contents of a horizontal cylinder are separated into two saturated regions, the relationship between the liquid level and the volume fraction occupied by liquid is not trivial. We define interior angle Ω_n (Figure 1.2-2) as the angle between the vertical and a vector

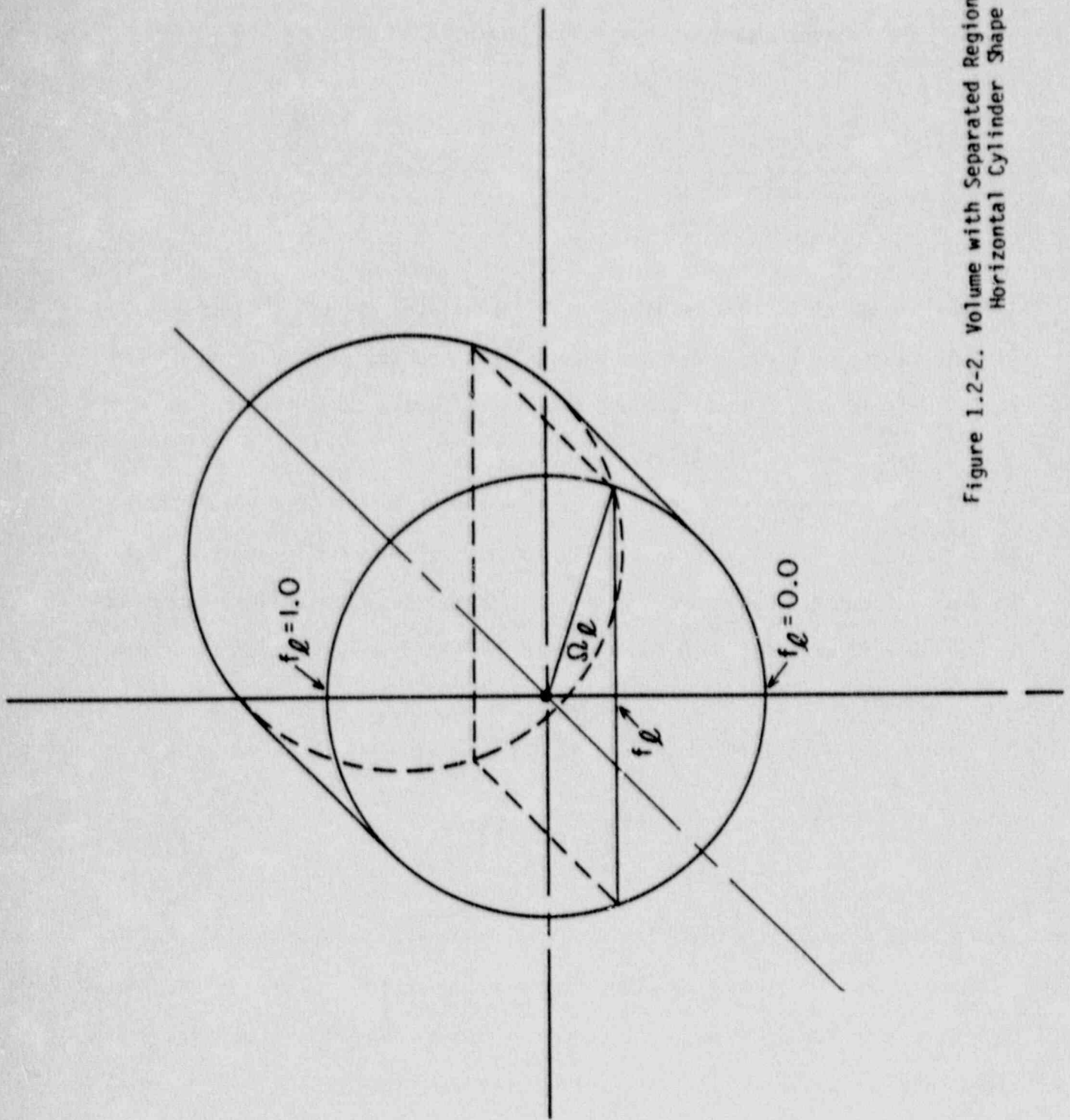


Figure 1.2-2. Volume with Separated Regions and Horizontal Cylinder Shape

running from the volume center line to the liquid level at the volume wall, such that:

$$f_{l_n} = \frac{1 - \cos \Omega_n}{2} \quad (1.2-8)$$

It can be shown that the volume fraction occupied by the liquid region is related to interior angle Ω_n by the expression:

$$f_{v_n} = \left(\Omega_n - \frac{\sin 2\Omega_n}{2} \right) / \pi \quad (1.2-9)$$

During steady state calculations, where f_{l_n} is user input, Eq. (1.2-8) is solved for Ω_n , Eq. (1.2-9) provides f_{v_n} , and Eq. (1.2-7) gives the quality, which in turn is used to set the volume average enthalpy. In the transient calculations, the enthalpy is advanced directly, and the same three equations are used in the reverse order to obtain the liquid level, f_{l_n} .

1.2.5 HEAT EXCHANGERS

Heat exchangers are among the most difficult plant components to represent, principally because of the complexity of two phase flow and heat transfer phenomena. A secondary complicating factor is the dependence of heat transfer on geometrical considerations, given the variety of heat exchanger designs. In addition to the heat exchangers designed for power plant use, there are several more exotic designs used in experimental systems. Representation of the experimental heat exchangers is desirable because much of the data useful for code verification comes from such units.

1.2.5.1 BASIC HEAT EXCHANGER MODULE REPRESENTATION

It is assumed that a single tube can be used to represent the heat exchanger. However, one could use more than one such tube by running parallel lines between volumes placed at both ends of the heat exchanger. The unit cell consists of the fluid inside the tube, the tube wall, and the fluid outside the tube, yet attributable to that tube, as shown in Figure 1.2-3.

The heat exchanger is divided into a user specified number of axial nodes, each containing two fluid nodes, and a tube node. One such node is shown in Figure 1.2-4.

For many heat exchanger calculations, the heat transfer process is uniform on each side of the tube. Thus, one calculates heat transfer Q between the tube centerline temperature (axial average) and the nodal average fluid temperature [6]:

$$Q = \pi \cdot D \cdot U \cdot (T_C - T(\bar{E})) , \quad (1.2-10)$$

where;

$$U = \frac{1}{\frac{1}{h} + \frac{\psi}{2k}} , \quad (1.2-11)$$

and geometric factor ψ depends on whether the heat transfer occurs inside or outside the tube, i.e.,

$$\psi = \begin{cases} D_I \ln (D_C/D_I) \\ D_O \ln (D_O/D_C) \end{cases} \quad (1.2-11a)$$

For heat exchangers involving multiple heat transfer regimes, the nodal calculation can become relatively complex. Ideally, the user will increase his nodalization for such a case. However, the MINET model can handle up to 5 heat transfer regions in a node, although some inaccuracy is likely to result.

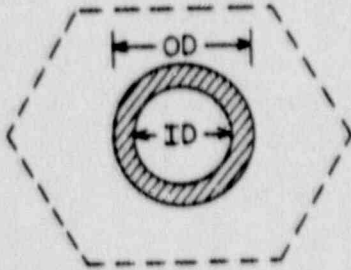


Figure 1.2-3. The Heat Exchanger Unit Cell

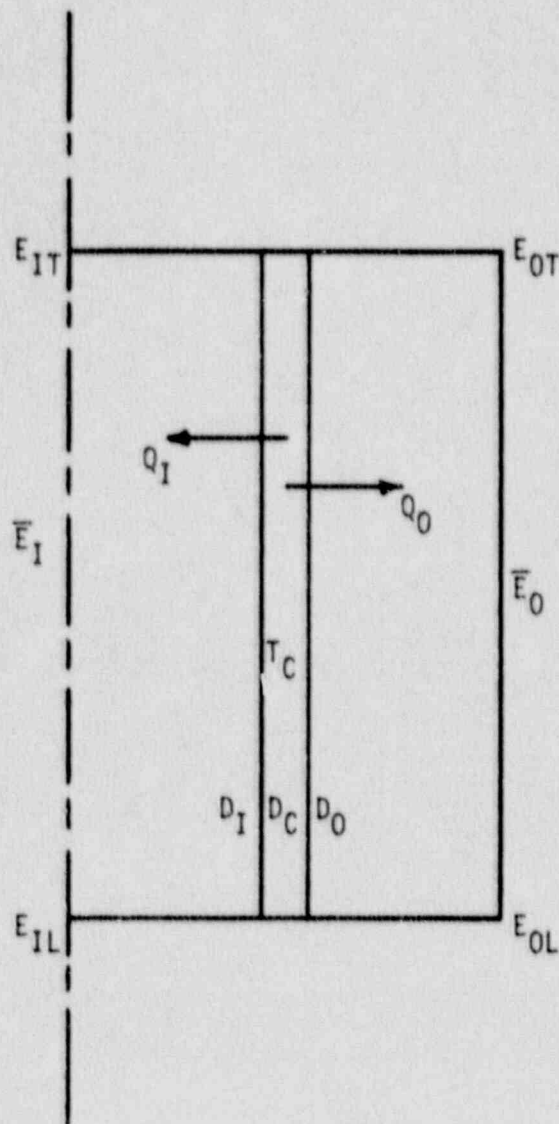


Figure 1.2-4. Heat Exchanger Node

The basic problem which arises with multiple heat transfer regimes in a node is that the axial temperature distribution becomes important (i.e., a distribution that can only be estimated using nodal parameters). The inlet, center, and outlet fluid enthalpies can be used, to a degree, to determine the local heat transfer regime. However, the tube temperature does not have a proper axial distribution, and to impose one would introduce numerical problems. (MINET allows for up to a 10K distribution in tube temperature, primarily to handle nodes in which the fluid temperatures are very close to one another).

The MINET approach is to divide the node using "switch" enthalpies, which indicate when the heat transfer regime is to be changed. Calculations proceed from the node inlet to the node outlet, until the node outlet enthalpy falls into the enthalpy bracket of the heat transfer regime of the last portion of the node. The total node heat transfer, Q_n , is the sum of the Q's from the various modes:

$$Q_n = \sum_{\text{modes}} f_{\text{mode}} \cdot Q_{\text{mode}} \quad (1.2-12)$$

where f_{mode} is the fraction of the node in which heat transfer is by a given mode.

The heat exchanger is made up of several of these nodes, linked by the fluid enthalpies passing from node to node. Tube temperatures are in no way linked from node to node.

Heat transfer correlations used in MINET are given in Section 1.5. Substitution of alternate correlations is possible, although the correlation switching logic should be considered when doing so.

In the steady state calculations, it is assumed that the user's knowledge of plant conditions is more accurate than the MINET heat transfer correlations. A heat transfer area correction factor is used to resolve any discrepancies. If the correction factor is significantly different than 1.0, either the plant conditions are unrealistic or the correlations are inappropriate.

1.2.5.2 HEAT EXCHANGER TYPES

Several heat exchanger types may be represented using the current MINET heat exchanger module, as shown in Figure 1.2-5. Representation of yet other types is also possible, provided the user can factor it into the current heat exchanger routines, which are moderately intricate.

On the appropriate heat exchanger performance specification record of the MINET input deck, the user designates variable F3CCFL as -1.0, 0.0 or +1.0. A value of -1.0 indicates a counter-current heat exchanger, typically the most common type. Setting F3CCFL to +1.0 indicates a parallel flow unit, a relatively uncommon type because of its lower efficiency. If F3CCFL is set to 0.0, the heat exchanger is treated as a cross flow unit of the tube-in-tank type.

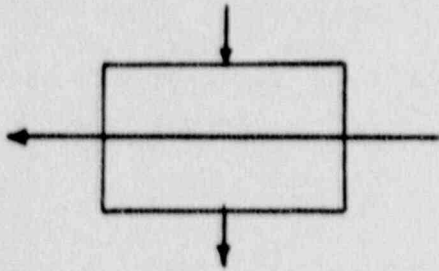
On the heat exchanger geometric record, two helical coil parameters are input, D3COIL and F3IT00. D3COIL is the diameter of the coils, used to adjust the frictional losses, and must be set to 0.0 for straight tube units. Variable F3IT00 is the ratio of the flow length inside the tubes to that outside, which is useful in representing coil in tank units, and must be set to 1.0 for non-coil or co-axial coil units.



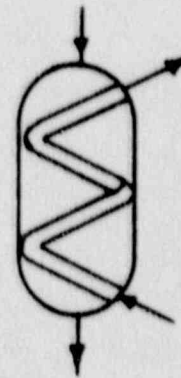
a. Counter Flow



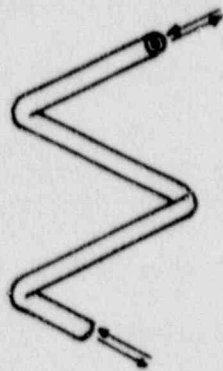
b. Parallel Flow



c. Cross Flow



d. Coil-In-Tank



e. Co-Axial H-Coil

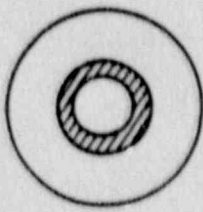
Figure 1.2-5. MINET Heat Exchanger Options

Of the five MINET heat exchanger options illustrated in Figure 1.2-5, all but the cross flow unit have sequential nodalization for the fluid passing outside the tube. Thus, for most cases, a heat exchanger with n nodes will have n tube nodes and $2n$ fluid nodes. For the cross flow option, only 1 node is used to represent the fluid outside the tubes, with $1/n$ of the flow assigned to each of the tube nodes. It is assumed that the enthalpy drop across each path is the same, which implicitly means that a small amount of flow distribution is allowed. However, for a tube in tank unit, the fluid outside the tubes is generally relatively slow moving, and these approximations are fairly safe. Of course, cross flow heat exchangers exist where a full two-dimensional treatment is needed, but for that case, the user would have to utilize a more sophisticated heat exchanger module than is currently available in MINET.

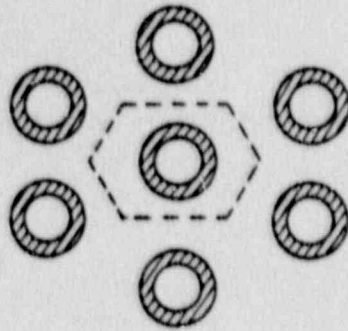
1.2.5.3 TUBE CONFIGURATION

While heat exchanger tubes are usually aligned in a hex arrangement, other configurations are possible, particularly in experimental units. For this reason, the three grid arrangements shown in Figure 1.2-6 are available as user input for each heat exchanger.

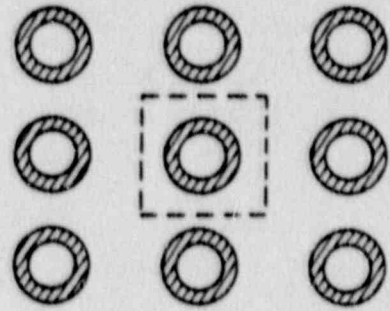
The flow area, A_0 , for the outside region of the unit cell must be determined from the tube configuration, as well as the tube outer diameter (OD), and the pitch to diameter ratio (POD). Specifications for the three MINET options are given in Table 1.2-1.



CO-AXIAL



HEX



SQUARE

Figure 1.2-6. Heat Exchanger Tube Configuration Options

Table 1.2-1. Flow Areas for Heat Exchanger Tube Configurations

| Grid Descriptions* | A_0 |
|--------------------|-----------------------------------|
| Co-Axial (1) | $\pi OD^2 (POD^2 - 1)/4$ |
| Square (4) | $OD^2 (POD^2 - \pi/4)$ |
| Hex (6) | $OD^2 (2 \sqrt{3} POD^2 - \pi)/4$ |

*Note: The number given parenthetically indicates the number of equidistant tubes that are closest to the reference (center) tube (see Fig. 1.2-6). This number is required as input for each heat exchanger.

1.2.5.4 STRUCTURE

Heat exchangers contain a certain amount of structure which can, due to its heat capacitance, alter the dynamic response of fluid passing outside the tubes. Furthermore, in the case of the EBR-II facility [7], a situation exists where a core tube is inserted into the tubes (to increase the flow velocity). Such masses can be represented in MINET, using the structural mass and metal type, the heat transfer area, and a simple energy equation that is explicitly integrated in time.

1.2.6 TURBINE STAGE

Turbines are generally modeled on two levels, detailed or thermodynamic. Turbine designers, by necessity, develop models based on geometric data. These models are very complicated, and, even if incorporated into a system

code would require design data is very difficult to obtain. Thus, system models generally resort to thermodynamic models, which rely on some knowledge of operating characteristics in order to project performance at various conditions. In the MINET code, the turbine stage model is based on 1) several semi-empirical relations, 2) one geometrical characteristic that can easily be defaulted (to 15.0 degrees), and 3) turbine performance at reference (design) conditions.

For a turbine stage, the flow-pressure relationship is approximated using a modified Stadola equation [8]:

$$W_{\text{stage}} = K_{\text{stage}} \sqrt{\rho_{\text{in}} P_{\text{in}} \left[1 - \left(\frac{P_{\text{out}}}{P_{\text{in}}} \right)^2 \right]}. \quad (1.2-13)$$

In MINET, K is determined for reference conditions and used to calculate the pressure drop across the stage ($P_{\text{in}} - P_{\text{out}}$). As MINET assumes that $W_{\text{in}} = W_{\text{out}}$ for the turbine and requires that the turbine stage be represented by a single node segment, then $W_{\text{stage}} = W_{\text{seg}}$.

The turbine inlet enthalpy is input from the adjoining module. The outlet enthalpy is calculated from the isentropic enthalpy change and the stage efficiency:

$$E_{\text{out}} = E_{\text{in}} - \eta_{\text{stage}} \cdot (E_{\text{in}} - E_{\text{out,isentrop}}), \quad (1.2-14)$$

where the isentropic outlet enthalpy can easily be calculated using the inlet pressure and enthalpy, the outlet pressure, and steam table functions.

Expressions are available in MINET for the turbine stage efficiency of two common stage types: 1) impulse (first stage) and 2) 50% impulse, 50% reaction. The expressions are:

$$\eta = 4 (V_B/V_F) (\cos \alpha - V_B/V_F) , \quad (1.2-15)$$

for the impulse and

$$\eta = 2 \left(\frac{V_B}{V_F} \right) \left[\frac{\sqrt{2} \cos \alpha}{2} - \left(\frac{V_B}{V_F} \right) + \cos \alpha \sqrt{1 + \left(\frac{V_B}{V_F} \right)^2} - \sqrt{2} \cos \left(\frac{V_B}{V_F} \right) \right] , \quad (1.2-16)$$

for the impulse reaction, where α is the absolute angle of approach of steam with respect to the blades, expressed in degrees (approx. 15 degrees). Velocity V_B is a measure of the turbine blade velocity and velocity V_F is the fluid velocity entering the moving blades. Since the kinetic energy is negligible entering and leaving the stage, the kinetic energy entering the moving blades is equal to the static enthalpy drop across the stage, which implies:

$$V_F = C \cdot (E_{in} - E_{out})^{1/2} \quad (1.2-17)$$

If we assume that the turbine is being operated at optimum conditions at plant reference conditions, then the efficiency function, Eq. (1.2-15) or (1.2-16), is maximized at that point, and:

$$\frac{V_B}{V_F} = \frac{1}{2} \cos \alpha \quad (1.2-18)$$

or

$$\frac{V_B}{V_F} = \frac{\sqrt{\frac{1}{\cos^2 \alpha} - 1 + \frac{\cos^2 \alpha}{2} - \frac{\sqrt{2}}{2} \cos \alpha}}{\frac{1}{\cos^2 \alpha} - 1} \quad (1.2-19)$$

Thus, the velocity ratio at reference conditions can be estimated, along with the pressures, enthalpies, flows, and speed (in RPM). Using these reference values, one can easily project the velocity ratio at any time using:

$$\left(\frac{V_B}{V_F}\right) = \left(\frac{V_B}{V_F}\right)_{\text{ref}} \cdot \left(\frac{V_{F \text{ ref}}}{V_F}\right) \cdot \left(\frac{V_B}{V_{B \text{ ref}}}\right), \quad (1.2-20)$$

where

$$\frac{V_{F \text{ ref}}}{V_F} = \sqrt{\frac{(E_{\text{in}} - E_{\text{out}})_{\text{ref}}}{(E_{\text{in}} - E_{\text{out}})}}, \quad (1.2-21)$$

and

$$\frac{V_B}{V_{B \text{ ref}}} = \frac{\text{Turbine Speed}}{\text{Speed at Ref Cond}} \quad (1.2-22)$$

This completes the turbine stage equation set, which provides a static thermodynamic representation suitable for systems simulation. In practice, a work adjustment factor (comparable to the heat exchanger area correction factor) enters during the steady state to match the enthalpy drop across the turbine to that needed to satisfy the rest of the system. Thus, the stage efficiency in Eq. (1.2-14) is adjusted by:

$$\eta_{\text{stage}} = \eta \cdot \eta_{\text{adjust}} \quad (1.2-23)$$

to account for deviations from the ideal efficiencies given by Eqs. (1.2-15) and (1.2-16).

The power provided to the generator and out to the electrical grid is calculated using a user input turbine stage to generator efficiency η_{gen} :

$$\text{Power} = \sum_1^{\text{stages}} \eta_{gen} \cdot \eta_{\text{stage}} \cdot W_{\text{stage}} \cdot \Delta E_{\text{stage}} \quad (1.2-24)$$

1.2.7 BOUNDARIES

Boundaries are simply interfaces between the system represented by MINET and the external world. The user can specify boundary conditions in tabular form, interface to another computer code which will exchange boundary conditions with MINET, or incorporate a controller that couples the boundary condition to the situation somewhere in the system being represented by MINET.

For the steady-state or initial conditions, the user must specify flow rates for inlet boundary modules. (The modules' form loss factors are to be used to adjust the pressure/flow distribution as necessary.) The user also specifies temperatures or enthalpies for inlet boundaries. A temperature/enthalpy condition may be specified as "fixed" for an outlet boundary, but only if there is a heat source available for MINET to adjust.

For the transient, the user may specify either pressure or flow at any boundary, and MINET will always calculate the other parameter. Temperature or enthalpy should be specified for all boundaries, although MINET will only use this temperature when the flow is entering the system from the outside.

A boundary module represents all parallel units. Thus, for example, if the boundary connects to 3 parallel pipes carrying a total of 300 kg/sec, the flow at the boundary is 300 kg/sec.

1.3 MINET STEADY STATE CALCULATIONS

A four step iterative process is used to determine steady state conditions in a system represented by MINET. The approach is built around the network structure of the underlying MINET methodology, and is somewhat different than classical marching or relaxation methods. The iterative process is begun with only estimates on system pressures, flows, and heat transfer rates, as well as user specified boundary conditions.

A system is represented as one or more flow networks, which are connected only through heat transfer. The user can intentionally or unintentionally force the transfer of a given amount of heat transferred between networks through specification of the problem. The first step of the iterative process is to determine which of these heat transfer bridges have to be adjusted and by how much.

Given a distribution of flows and pressures in a flow network, as well as the heat transfer into or out of various portions of the network, one can determine the enthalpies throughout. The second step in the iterative process is to calculate system enthalpies.

The third step in the MINET steady state calculations is to march through the system modules, calculating local enthalpy distributions and pressure drops. Adjustments in heat exchanger area correction factors and turbine stage efficiencies are calculated during this phase.

The fourth step in the process is to adjust network pressures and flows for each network in the system. This step includes re-evaluation of pressure drops in isolated pumps, valves, and turbines (always isolated), as the pressure change across these components can be very large, and highly dependent on segment pressure.

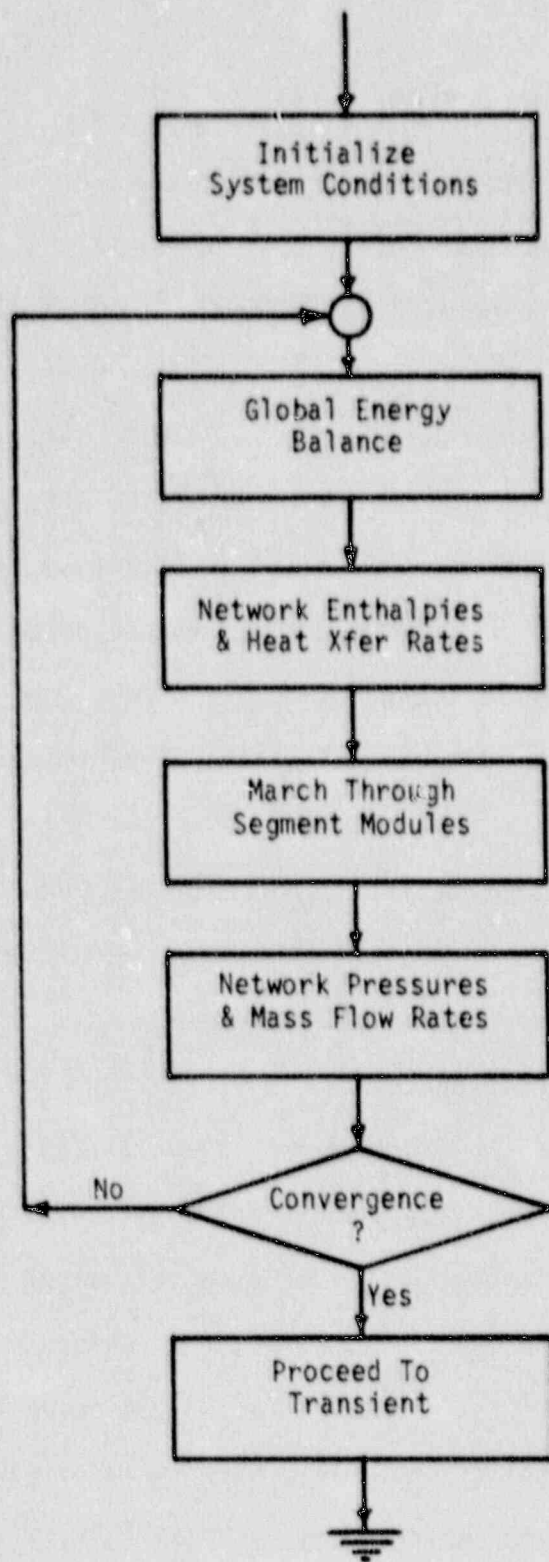


Figure 1.3-1. Steady-State Solution Strategy

The four step process is repeated until system enthalpies are no longer changing significantly from step to step. (When first testing an input deck, it is wise to set L3PRON = -1 on the 4000 card to get a print out after step 4 on each steady state iterative pass.)

1.3.1 GLOBAL ENERGY BALANCE

The MINET user inputs estimates of heating or total heat transfer (work done in the turbine looks like heating in this part of the calculation) for each module. A heat exchanger removes heat from one part of the system and adds it to another. The user also constrains the total heat transfer between parts of the system whenever he opts to fix a temperature at an outlet boundary or utilizes a volume that has separated contents, i.e., steam over water. In the separated volume case, the energy constraint enters because, for given pressures and flows, the total energy leaving the volume is fixed by saturation conditions. Thus, to assure an energy balance, the sum of the flow energy entering the volume must equal the flow energy leaving the volume.

An example of this global energy balance usage can be illustrated using Figures 1.3-2 and 1.3-3. Figure 1.3-2 is a schematic of a simple recirculation steam generator system, which utilizes an evaporator (301), a superheater (302), and a steam drum (101). Because the enthalpy at 404 is fixed, the sub-network between 403 and 404 must give off energy at a rate of $W_3 (E_3 - E_4)$. The steam drum creates a sub-network in the recirculation (recirc) line, because it must draw enough energy to raise the enthalpy of W_1 from E_1 to E_g . This situation is illustrated in Figure 1.3-3, where the 403-404 sub-network is designated number 3, the recirc line is number 1, and

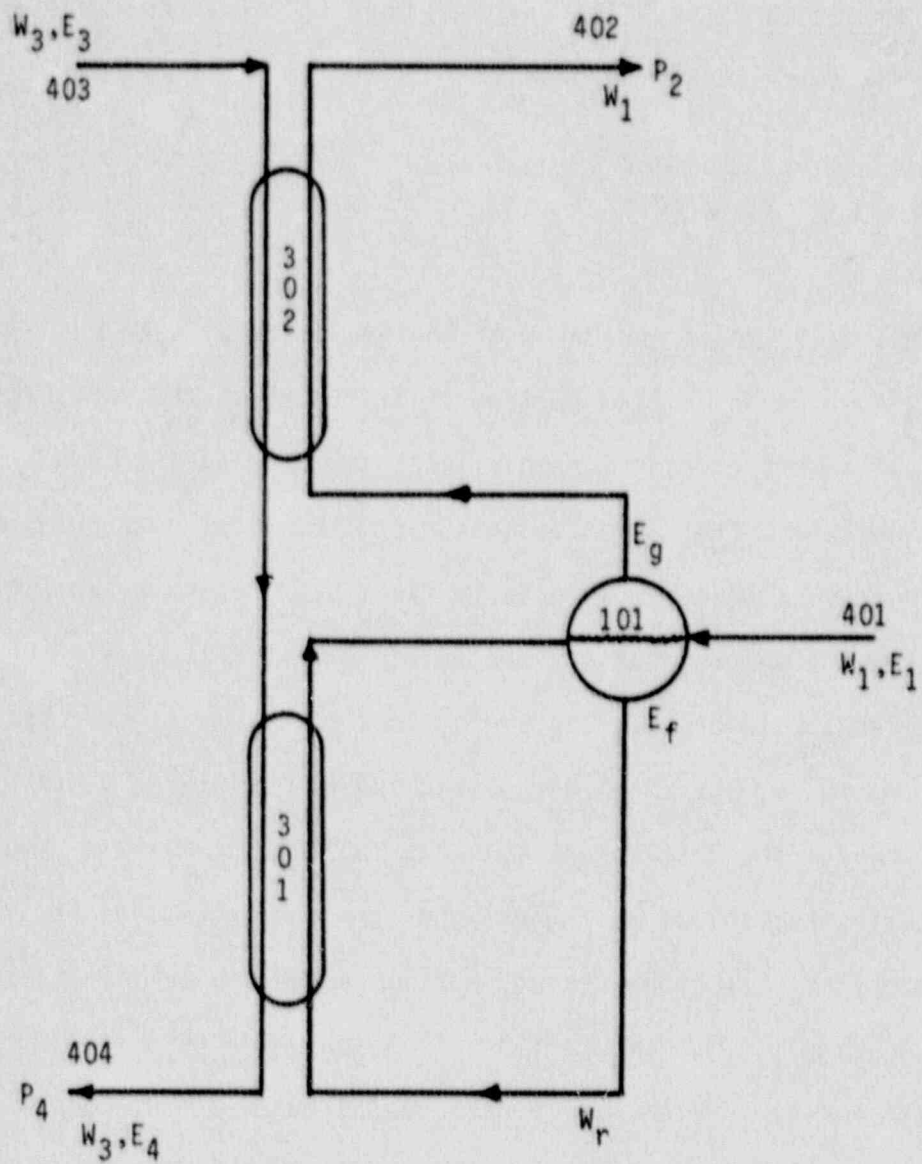


Figure 1.3-2. Example 1 for Global Energy Balance

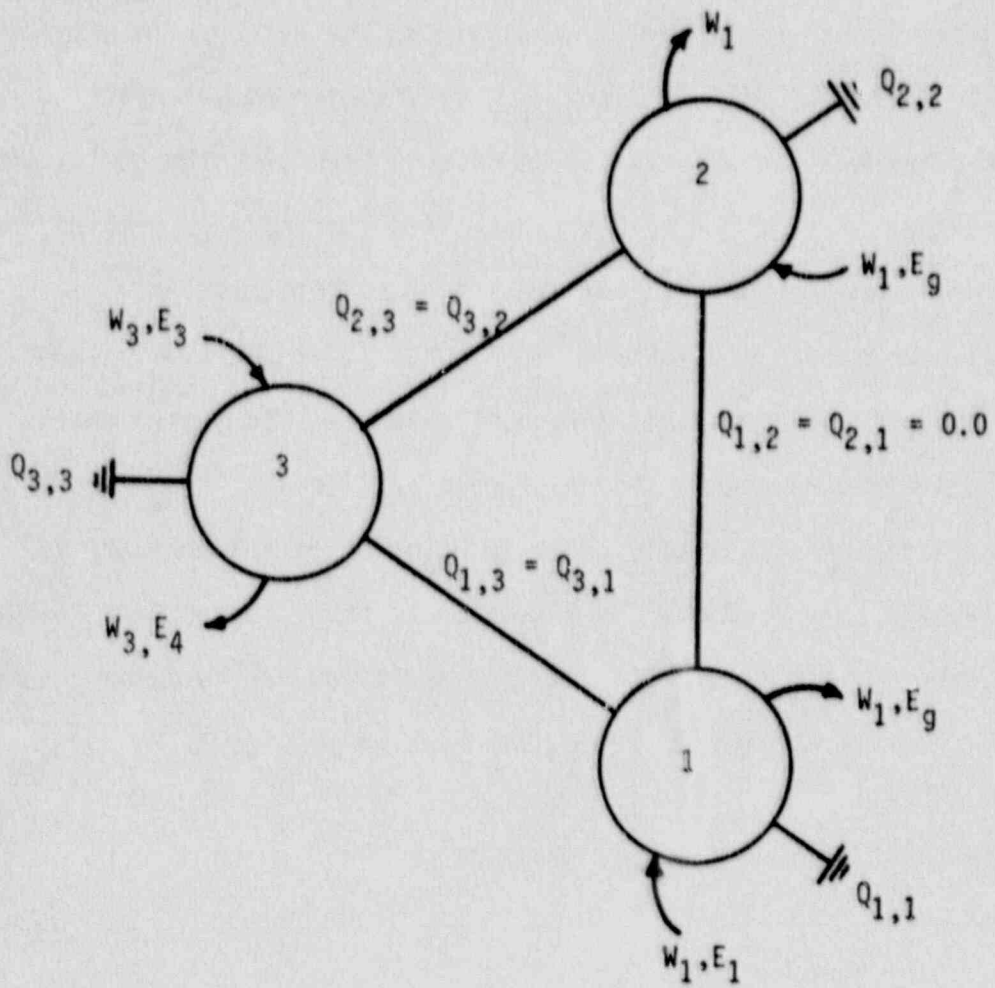


Figure 1.3-3. Sub-Network Abstract for Example 1

the superheater line is number 2. Each sub-network has flows in and out, heat transfer to ground (e.g., pipe heating), and heat transfer to all other sub-networks. Of the nine sub-network bridges, 3 are redundant ($|Q_{1,3}| = |Q_{3,1}|$), leaving six that could be adjusted to satisfy sub-network 1 and 3 constraints. If we assume there is no pipe (pump, valve, volume) heating, the bridges to ground have $Q = 0$. Thus, we must use bridges 1, 3 and 2, 3 to satisfy closed sub-network 1 and 3 constraints. We set $Q_{1,3}$ to provide energy to raise E_1 to E_g , and set $Q_{2,3}$ to transfer enough heat for the sub-network 3 outlet enthalpy to be E_4 . Note that the outlet enthalpy of sub-network 2 is not directly constrained, which is no problem for an open sub-network, as the user did not specify an outlet enthalpy.

A second example, illustrated in Figures 1.3-4 and 1.3-5, shows how flow splitting can complicate the process of balancing the system energy. This example consists of 3 boundaries, 3 pipes (1,2,3) and a volume (110) with homogeneously distributed contents. The enthalpy at outlet boundary 412 is fixed, and only pipe 1 is heated. The situation is shown in abstract in Figure 1.3-5, where $Q_{1,2} = 0.0$. With the flow splitting in the volume, each sub-network receives a fraction of Q_1 , the heating in pipe 1.

$$Q_{1,1} = \frac{W_2}{W_1} \cdot Q_1 \quad (1.3-1)$$

$$Q_{2,2} = \frac{(W_1 - W_2)}{W_1} Q_1 \quad (1.3-2)$$

Thus, in order to get E_2 as the fluid enthalpy at 412, we must adjust Q_1 . Of course, this will also put the enthalpy at 413 at E_2 , but because this is an open or floating sub-network (enthalpy not constrained), this is not a problem.

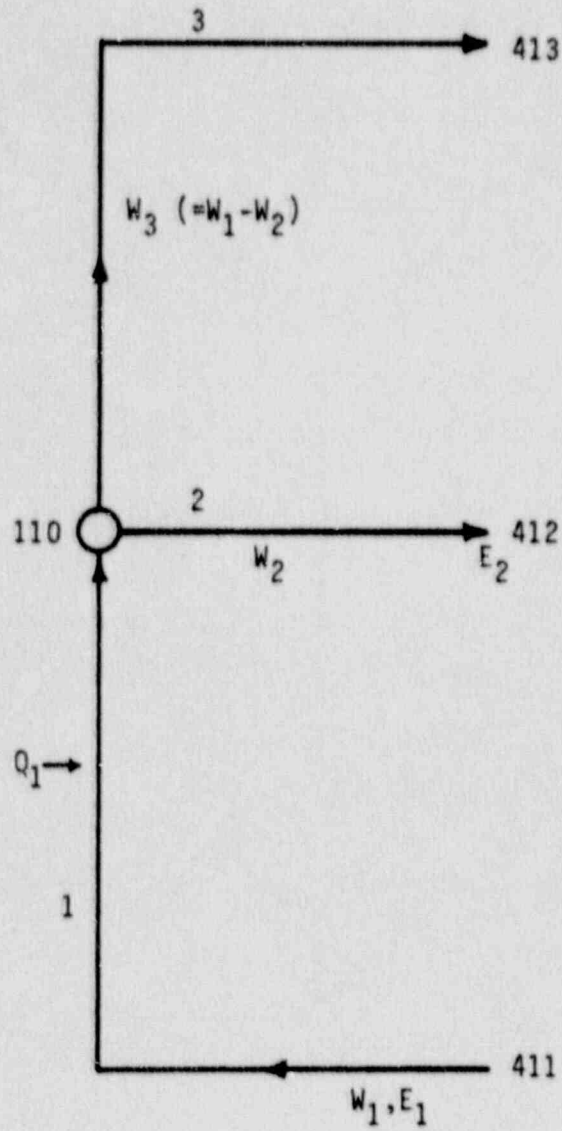


Figure 1.3-4. Example 2, Flow Splitting Considerations

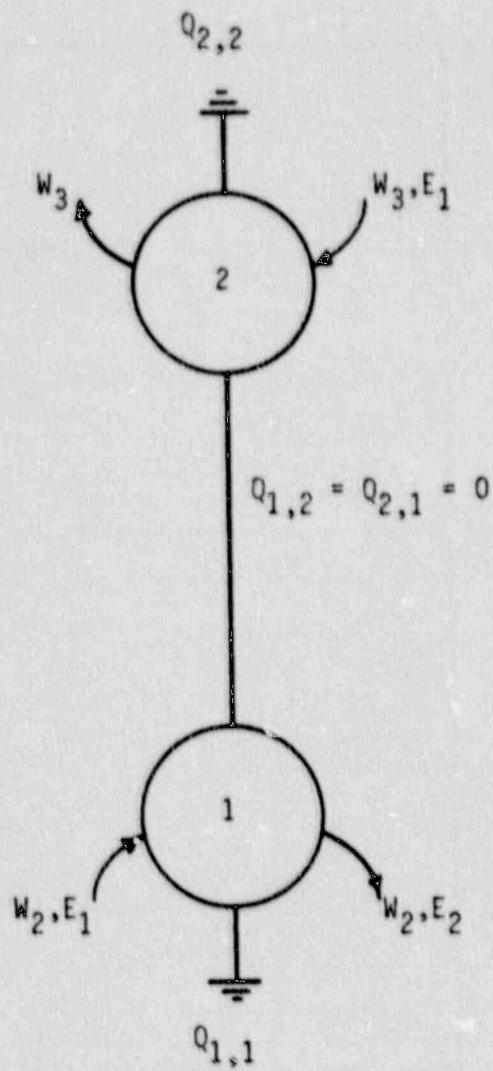


Figure 1.3-5. Example 2 Sub-Network Abstract

These examples are made in order to illustrate the reasons for some of the steps taken in the MINET steady state global energy balancing. The approach utilized is designed to work for situations that we envision coming up. However, the procedure contains many subtleties, including those to handle cases where multiple solutions are possible.

1.3.1.1 FLOW TRACEBACK

The process of flow traceback is important for a case like Example 2, where a heat source is shared by multiple sub-networks. Flow traceback is performed simply by beginning with outlet boundaries or separated volumes and tracing back to the source - either an inlet boundary or a separated volume. The fraction of flow from each segment or volume going to each sub-network is thus calculated.

For Example 1 (Figs. 1.3-2 and 1.3-3), there are no shared (by sub-networks) segments or volumes, and the flow fractions are either 1.0 or 0.0, and are quite obvious.

In Example 2 (Figs. 1.3-4 and 1.3-5), the segment with pipe 3 is entirely in sub-network 2, and the pipe 2 segment is in sub-network 1. However, only W_2/W_1 of volume 110 and the pipe 1 segment are in sub-network 1. The remaining $(W_1 - W_2)/W_1$ of the flow passes to sub-network 2, contributing to its energy balance.

1.3.1.2 PRINCIPAL SUB-NETWORK

When a segment or volume is shared by more than one sub-network it is necessary to assign it to a sub-network for possible adjustment. The goal is

to make certain that the energy balance for each sub-network can be satisfied. Of course, if the heating in one segment is adjusted, it is reflected in all sub-networks according to the flow fraction passing that way.

The process of assigning principal subnet numbers to the segment involves 4 considerations. These are as follows:

- 1) If there is only 1 sub-network in the network, each segment and volume is assigned to that sub-network.
- 2) If the fraction of flow going from a volume or segment to a sub-network is 1.0, then that volume or segment is assigned to the sub-network.
- 3) If a volume or segment is shared by an open (floating outlet temperature) and a closed (fixed outlet temperature) sub-network, it is always assigned to the closed sub-network. This is because the closed sub-network may need an adjustment in heat transfer, and the open sub-network never need be adjusted.
- 4) When a volume or a segment is shared by two or more closed sub-networks it is assigned to the most needy. The highest priority is to insure that each closed network has at least one heat source available for adjustment. If each of the sharing sub-networks is already assured of at least one source, then the shared volume or segment is assigned to the sub-network with the smallest total heat transfer.

We return to Example 2 (Figs. 1.3-4 and 1.3-5) to illustrate the use of these rules. There are 2 sub-networks in the flow network, so rule 1 does not apply. We can use rule 2 to assign the pipe 1 segment to subnet 1 (KPRNC (Seg. 2) = subnet 1) and the pipe 3 segment to subnet 2. We must use rule 3 for the pipe 1 segment, and assign it to the closed sub-network (no. 1). As a

result, a heat source is assigned to sub-network 1 which can be adjusted to give outlet enthalpy E_2 .

To illustrate rule 4, we consider a case where the enthalpy at 413 is also fixed, and the heating in pipe 3 is non-zero. As in the simpler case, pipe segments 2 and 3 are assigned to sub-networks 1 and 2, respectively, according to rule 2. Rule 3 no longer applies, because both sub-networks are now closed. In applying rule 4, we find that the heating in pipe 3 has already been assigned to sub-network 2, while sub-network 1 has yet to receive a heat source. Therefore, the heating in the pipe 1 segment is assigned to sub-network 1.

1.3.1.3 SUMMING UP BRIDGE HEATING

At this stage, each segment and volume has been assigned to a sub-network (the "principal" one), for the purpose of adjustment. Heating in pipes, valves, volumes, pumps, and turbines (work) are really between the sub-network and ground. Thus, to find the total bridge heating between sub-network i and ground, $Q_{i,i}$, we simply sum the heating terms in all segments and volumes with i as the principal sub-networks.

In general, heat exchangers link flow networks, and therefore subnets. Thus, the heat exchangers form bridges between subnets, as determined by the principal sub-network number for the segments attached to the insides and outsides of the tubes. The total heat transferred through all heat exchangers between any given pair of sub-networks is summed to give the total bridge heating $Q_{j,k}$. Note that for hypothetical cases where heat exchangers link merely different parts of a sub-network (or even a segment), the addition and

subtraction will cancel out, having no net impact of the global energy balance.

1.3.1.4 DETERMINING KEY BRIDGES TO ADJUST

In order to guarantee the outlet enthalpies of the fixed sub-networks, a like number of non-zero heat transfer bridges must be available for adjustment. If this is not the case, MINET will halt the calculations, because the problem is over specified.

The process of identifying the key bridges (to be adjusted) begins with an elimination process. A bridge is eliminated from consideration if:

- 1) It has a total bridge heating $Q_{i,j}$ of 0.
- 2) It connects two free sub-networks, and thus can do nothing for fixed sub-networks.
- 3) It connects a free sub-network with the ground.

If, after eliminating these three types of bridges, there are less bridges left than the number of fixed sub-networks, the calculations cease. When there are exactly enough heating bridges available for the fixed sub-networks, they are tagged and calculations proceed to the next phase.

Should there be more useful bridges than are needed, MINET carefully picks a set of key bridges that 1) will provide a solution, and 2) are the larger ones, so that any adjustment will be minimized. The process is one of assigning essential bridges to the needy sub-networks until more than one bridge is available for each remaining needy sub-network. At this point, the smallest unassigned bridge remaining is fixed. This process is repeated until the necessary number of heat transfer bridges are left for adjustment.

1.3.1.5 SUMMING SUB-NETWORK FLOW ENERGIES

In this phase of the calculations, the total flow energy (mass flow rate x enthalpy) going into and out of each sub-network is calculated. As all network outlet boundaries with free floating temperatures are assigned to an open or free sub-network, their contributions are totalled to get the flow energy out of the free sub-network. Inlet boundaries can contribute to multiple sub-nets, as determined by the segment flow fractions that were determined in the flow traceback phase. For sub-networks with incoming flow from a separated volume, enthalpies are easily determined from saturation conditions. The total flow energy leaving a sub-network that terminates at a separated volume can be calculated by summing the flow energy leaving the volume (at saturation), as the two sums must be equal at steady state (once adjusted for volume heating).

1.3.1.6 BALANCING THE SYSTEM

At this stage in the calculations, the groundwork has been set to fulfill the energy balance needs of each of the sub-networks. One heat transfer bridge is to be adjusted for each fixed (or closed) sub-network in the system. This amounts to finding a multiplier f_B , such that $f_B \cdot Q_{j,k}$ fulfills the need for a given fixed sub-network. Concurrently, the total flow energy leaving each of the floating (or open) sub-networks is calculated.

Appropriate equations for each sub-network are loaded into the matrix equation

$$\underline{E} \cdot \underline{x} = \underline{F} , \quad (1.3-3)$$

where \underline{E} is a square matrix dimensioned to the number of system sub-networks, \underline{x} and \underline{F} are vectors of the same dimension. The components of state vector \underline{x} are outlet flow energies of the floating (open) sub-networks and the bridge adjustment factors:

$$\underline{x} = \left\{ \sum WE_{0,i}^{flt}, \dots, f_{Bj}, \dots \right\} \quad (1.3-4)$$

One equation is loaded into Eq. 1.3-3 per sub-network. For a floating sub-network i , the equation is of the form

$$\sum WE_{0,i}^{flt} - \sum_j^{Nfloat} f_{Bj} \cdot ff \cdot Q_j = \sum WE_{I,i} + \sum_k^{Nfix} ff \cdot Q_k, \quad (1.3-5)$$

where ff is the flow fraction from the volume or segment contributing to the subnet, Q is the heating, and f_{Bj} is the adjustment factor assigned to adjustable bridge j . Note that this means that adjustment factors constrained by the fixed sub-network requirements are factored into the floating sub-networks any time the two share a heat source.

For a fixed sub-network, the equation to be loaded into Eq. 1.3-3 is of the form

$$- \sum_j^{Nfloat} f_{Bj} \cdot ff \cdot Q = \sum WE_{I,i} + \sum_k^{Nfix} ff \cdot Q_k - \sum WE_{0,i}^{fix}, \quad (1.3-6)$$

where the total flow energy leaving, which is fixed, now appears on the right hand side.

Once loaded, Eq. (1.3-3) is solved for the flow energy leaving the floating sub-networks and the bridge adjustment factors for the fixed sub-networks. The former are of little use, but the latter (factors) are critical to assuring system wide energy balances.

The bridge adjustment factors apply to only a few of the heat transfer bridges, which are identified by the sub-networks they connect. It is a routine matter to trace back to the segments and volumes assigned to the adjusted bridge and factor the heating terms. For heating in pipes, pumps, valves, volumes, and turbines, this factor is carried through the steady state (although adjusted from iteration to iteration) and into the transient. For a heat exchanger, it is absorbed into the heat transfer area correction factor, which again carries through the transient.

1.3.1.7 BALANCING IN PERSPECTIVE

The approach outlined in this section was developed to resolve real world problems, and is important to determining a reasonable steady state solution. There are subtleties involved in the solution of complex systems, particularly one with multiple solutions (i.e., excess heat transfer bridges). It is possible that flaws can be found in the current logic and that improvements can be made. However, the experiences gained thus far indicate that a user input error is far more likely than a logical error in the code.

A summary of the global balance and adjustment factors is printed with the steady state results. This printout should be carefully checked when testing a new deck. If the adjustment factors are significantly different than 1.0, the input should be reviewed for errors.

1.3.2 NETWORK ENTHALPY DISTRIBUTION (ENET)

Once the global energy balancing has been completed, enthalpies can be determined throughout each network. This straightforward process begins with a summing of the heat transfer into each segment

$$Q_{SEG} = \sum_{\text{modules}} f_{Bj} \cdot Q_{mod}, \quad (1.3-7)$$

where f_{Bj} could vary from heat exchanger to heat exchanger, depending on which sub-networks it connects.

The principal step in the ENET balance is the coupling of segment inlet enthalpy constraints and volume energy balance equations in a matrix equation of the form:

$$\underline{A} \underline{x} = \underline{B} \quad (1.3-8)$$

Square matrix \underline{A} and vectors \underline{x} and \underline{B} are dimensioned equal to the number of segments plus volumes. State vector \underline{x} consists of segment inlet enthalpies and volume enthalpies:

$$\underline{x} = \text{col} \left\{ E_{m1}, \dots, E_{n1}, \dots \right\} \quad (1.3-9)$$

Network segment inlet enthalpies are constrained by one of three equation types:

$$E_{m,in} - E_n = 0, \quad (1.3-10)$$

$$E_{m,in} = f(E_f, E_g), \quad (1.3-11)$$

or

$$E_{m,in} = E_{Bc}. \quad (1.3-12)$$

The first equation (1.3-10) applies when the segment begins at a volume with homogeneously distributed contents. Equation (1.3-11) applies when the segment inlet connects to a volume with separated regions, so that the incoming enthalpy is at saturation. The third equation (1.3-12) applies when an inlet boundary module is at the segment inlet, in which case the enthalpy is fixed.

The volume energy balance equation is essentially

$$\sum^{OP} (WE)_{out}^{vol} - \sum^{IP} (WE)_{in}^{vol} = f_{Bi} \cdot Q_{vol}, \quad (1.3-13)$$

where OP are the outlet ports and IP are the inlet ports. At this stage, the right hand term is known and the flow rates on the left side are known (current iterative values) for any segment. The volume outlet enthalpy is the inlet enthalpy for the attached segment, and is therefore available in state vector \underline{x} . The volume inlet enthalpies are segment outlet enthalpies, which are known from the equation

$$(WE)_{out}^{seg} = (WE)_{in}^{seg} + Q_{SEG}, \quad (1.3-14)$$

where QSEG is as calculated in Eq. (1.3-7).

The equation actually loaded in matrix Eq. (1.3-8) is a combination of Eqs. (1.3-13) and 1.3-14), i.e.,

$$\sum^{OP} W_m E_{mi} - \sum^{IP} W_m E_{mi} = f_{Bi} \cdot Q_{vol} + \sum^{IP} Q_m. \quad (1.3-15)$$

The volume energy equation, Eq. (1.3-15), is loaded unless the volume contents are separated. In this case, the volume enthalpy is determined by saturation conditions and the liquid level

$$E_{vol} = fcn(E_f, E_g, level). \quad (1.3-16)$$

Note that the separated volume energy balance was already used in the summing of sub-network flow energies (see Sect. 1.3.1.5). To use it in Eq. (1.3-8) would not only be redundant, it would do nothing to constrain the volume enthalpy, and matrix A would be singular.

Once segment inlet enthalpies are known, module inlet and outlet enthalpies can be defined. This is done by simply marching through the segments, incrementing the enthalpies using module heating, adjustment factors, and segment flow rate.

1.3.3 MODULE MARCH

The step of marching through all of the modules in each segment is necessary for the correct calculation of the segment pressure loss, r_m . Because the pressure loss terms are sometimes dependent on the square of the mass flow rate, two segment loss parameters, α_m and β_m are calculated such that

$$r_m = \beta_m - \alpha_m |W_m|W_m. \quad (1.3-17)$$

The terms of Eq. (1.1-10) are represented by α_m and β_m . Gravitational losses, which are independent of flow rate, accelerative losses, which are small, the pump contribution at steady state speed and zero flow rate, and the turbine stage contribution are included in the β_m term.

$$\beta_m = \sum_{i=Nf_m}^{Nl_m} \Delta P g_i + \Delta P a_i + \delta_{ip} \rho_i g H_p (\omega, W) + \delta_{it} \frac{P_i}{(P_i + P_o)} \cdot \rho_i \cdot f k_t \quad (1.3-18)$$

Frictional losses, valve form losses, and the module form losses, are included in α_m :

$$\alpha_m = \sum_{i=Nf_m}^{Nl_m} f_i / 2\rho_i A_i D_i + \delta_{iv} K_v / 2\rho_i A_v^2 + \frac{f k_i}{2\rho A_{eq}^2 D} \quad (1.3-19)$$

At the onset of calculations for a given heat exchanger, flow rates, pressures, inlet and outlet enthalpies, and total heat transfer rate are already known. To force the heat transfer rate, as indicated by correlations, tube conductivities, and heat transfer areas, to provide the required total heat transfer rate, an area correction factor, Fa_h , is used. Fa_h is used to factor the total heat transfer area up or down, as needed.

The steady state heat exchanger calculations include several layers of iterative schemes, with the area correction factor being the outermost. The next lower level is the nodal energy balance, where the heat transferred across the node is forced to match the flow and enthalpy change(s). This iteration is complicated by the allowance of up to five different heat transfer regimes within the node, with the switch interfaces determined within the iteration. Below the nodal energy balance calculation is the tube wall node centerline temperature iteration, which sets equal the heat fluxes between the tube centerline and the two fluids. The lowest iteration calculation is for

the tube wall temperature, which is calculated from the tube centerline temperature and fluid conditions, and is done so within the heat transfer correlation functions.

The heat exchanger calculations, especially in the steady state, are complicated by the various heat exchanger options. These schemes have been adjusted, re-adjusted, and continue to be tested to insure that they work for all options. The subtleties involved are too extensive to fully document, and should not be taken lightly by the user. Serious problems with steady state non-convergence, if not due to an input error, can usually be resolved by increasing the heat exchanger nodalization. It should be noted that any low level failure to converge is significant only on the last pass of higher level iterative schemes, when they are less likely to occur.

Module heating, adjusted during the global energy balance phase (Sect. 1.3.1) is used to determine the enthalpy distribution in pipes, pumps, and valves. For pipes, which can have more than one node, the heating per node is assumed to be uniform.

The work done in the turbine, also subject to adjustment during the global energy balance (Sect. 1.3.1) phase, is used to determine the enthalpy change across the turbine stage. Using the Stadola constant, determined from reference conditions, and the current flow rate, the pressure drop across the stage is calculated. The isentropic enthalpy change and ideal stage efficiency are then calculated for current conditions. This is compared to the work requirement coming from global balance consideration, and an efficiency adjustment factor is calculated

$$f_{ts}^{eff} = \Delta E_{global} / (\eta_{theory} \cdot \Delta E_{isentropic}). \quad (1.3-20)$$

This factor is like the heat exchanger area correction factor in that a value near 1.0 indicates a good match. The last step is to multiply the work done in the turbine by the generator efficiency to get the power delivered to the electric grid.

1.3.4 NETWORK PRESSURES AND FLOWS (PRFLOW)

The fourth and final step in the MINET steady state iterative process is to adjust the pressure and flow distribution in each system network. This is done by coupling, in a matrix equation, a number of equations equal to the number of network volumes, N_v plus segments (N_m) plus inlet boundary modules (N_{ib}):

$$\underline{C} \underline{x} = \underline{D}, \quad (1.3-21)$$

where \underline{x} is the state vector:

$$\underline{x} = \text{column} \left\{ W_{\text{seg}}, \dots, P_{\text{vol}}, \dots, P_{\text{Bc}}^{\text{inlet}} \right\}. \quad (1.3-22)$$

The first N_v equations are mass balances for each network volume:

$$\sum_{\text{Inlets}} W_{\text{seg}} - \sum_{\text{Outlets}} W_{\text{seg}} = 0, \quad (1.3-23)$$

where the flow rates passing through the volume ports are the segment flow rates, W_{seg} , which are in state vector \underline{x} .

The next N_m equations are segment momentum balances, which can be simplified as

$$P_{m,\text{out}} - P_{m,\text{in}} + \alpha_m |W_m| W_m = \beta_m, \quad (1.3-24)$$

where α_m and β_m are the segment pressure loss parameters described in Section 1.3.3, and $P_{m,in}$ and $P_{m,out}$ are segment inlet and exit pressures, respectively. Because segment pressures are not in state vector \underline{x} , these terms have to be written in terms of either volume pressures or boundary pressures, depending on which is attached at the end of the segment

$$P_m = P_{Bc}, \quad (1.3-25)$$

or

$$P_m = P_{vol} + \Delta P_g. \quad (1.3-26)$$

When the segment is attached to a boundary, the end pressure is identical to the boundary pressure, which is known if an outlet, or in state vector \underline{x} if an inlet. For a volume, the segment pressure must be calculated from the volume pressure and the gravitational head between the volume average value (in \underline{x}) and the junction level.

Because Eq. (1.3-24) is second order in segment flow, two steps are taken. First, Eq. (1.3-24) is actually loaded in Eq. (1.3-21) in linearized form. Second, Equation (1.3-21) is solved iteratively until the segment flows are no longer varying significantly from step to step.

Finally, the segment loss parameters, α_m and β_m can be large and sensitive to changes in flow and pressure in some pumps, valves, and turbines. If the user has isolated one of these components in a segment, these parameters will be updated during the iterative solution of Eq. (1.3-21).

The remaining N_{ib} equations are trivial, and merely connect the flow through inlet boundaries to the flow in the adjoining segment:

$$W_m = W_{ib}. \quad (1.3-27)$$

Equation (1.3-21) is solved to adjust segment flows, volume pressures, and inlet boundary module pressure. Immediately following, segment inlet and outlet pressures and outlet boundary module flows are adjusted.

1.4 TRANSIENT CALCULATIONS

The transient calculations are based on the momentum integral network method described earlier. Adjustment factors determined during the steady state calculations are applied consistently in the transient computations. Transients are driven by changes at the boundaries, via the pump and turbine speeds or valve positions, and through the heat sink term in non-heat exchanger modules. All of these parameters can be controlled through user-input value vs. time tables. Alternately, pumps and turbines can be tripped and coasted down and valves can be tripped open and closed in response to pressure (safety/relief) or flow (check). A compatible generic control system is planned, although not currently available.

The overall time step procedure is illustrated in Figure 1.4-1. The initial step is to advance the boundary conditions to the end of the current step, which is consistent with the semi-implicit differencing in MINET. Network calculations are then performed for each network in the system, with the heat exchanger tube temperatures lagged, so as to temporarily decouple the networks. Within a given network, all segment response matrices are first determined (see following section), which effectively predict the response throughout the segments to changes in the volumes and boundary conditions. Once these matrices are known throughout a network, the volumes can be coupled and advanced in time, and the segments can then be advanced. After all networks have been advanced, the heat exchanger tube temperatures are advanced.

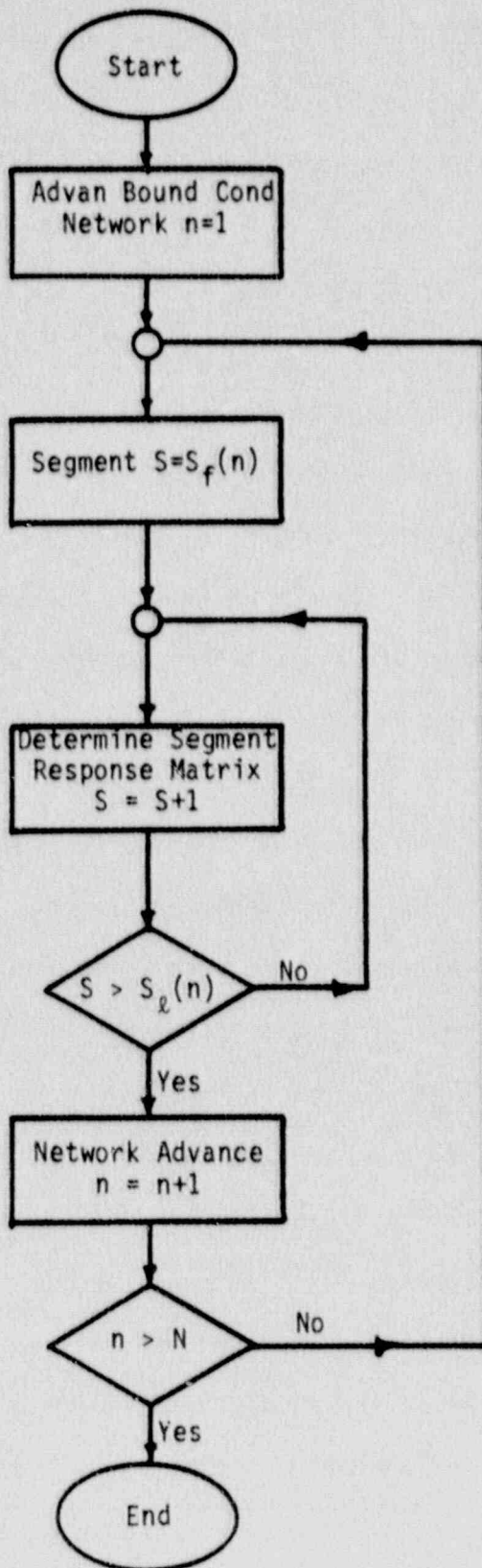


Figure 1.4-1. Transient Time Step Process

1.4.1 TIME STEP PREPARATION

At the beginning of a time step, several parameters including the time step size, must be set. The time step to be taken, Δt^k , advances the steam generator variables from current (t^k) values to advanced time values (t^k).

Most of the equations are integrated semi-implicitly in time, which allows time steps larger than the equation time constants to be used without introducing instabilities. However, the heat exchanger tube temperature is treated explicitly in the wall heat conduction equation, and thus, that equation has a limiting time constant τ_j :

$$\tau_j = \rho t_j C p t_j A t_h / f a_h (D_o h_o + D_i h_i) \quad (1.4-1)$$

While time constant τ_j in Eq. 1.4-1 is generally the limiting one, time constants for the heat exchanger structure temperature, the pump and turbine speeds and valve positions are also considered. Further, the rate of change in key enthalpies and pressures is also considered, and rapid changes can cause the time step size to be reduced. It should be noted that the increase in time step size, from one step to the next, is limited to 50%.

The second significant task in preparing for a time step is the updating of boundary modules and module heating. The only means of updating these required parameters at present is via user input value vs. time tables, which are interpolated to get current values. If the user has chosen to control any pumps, turbines, or valves in similar fashion, the appropriate tables are used at this time to update the corresponding pump and turbine speeds or valve positions.

There are two alternate means of controlling pump speeds, turbine speeds, and valve positions. A limited control option is available in MINET which manually trips and coasts down pumps and turbines or releases and resets safety valves on pressure settings and check valves on flow conditions. These limited control options are used to update pump and turbine speeds or valve positions when that module is updated. A more sophisticated control system model is planned, but not currently available. For the present, a special purpose controller can be inserted using code updates, should the user choose to do so.

1.4.2 SEGMENT CALCULATIONS

In this part of the transient calculations, the segment response matrix must be determined for the current segment pressures, local enthalpies, mass flow rates, heat fluxes, as well as pump and turbine speeds, and valve positions. The segment response matrix indicates the response of local enthalpies and mass flow rates to current conditions and changes in pressure and enthalpy in bordering modules.

1.4.2.1 LOADING THE SEGMENT EQUATIONS

At this point in the calculations, values are known for most variables, at the k step. Time, boundary module parameters, module heating, and, depending on the control option specified, pump speeds, turbine speeds, and valve positions, are known for the k step. The segment matrix equation is to be used, in conjunction with the network solution, to advance local enthalpies and mass flow rates to the advanced time step, $k+1$. The equation is of the form

$$\underline{\underline{A}} \underline{x} = \underline{\underline{B}} \underline{y}, \quad (1.4-2)$$

where, for a segment with N_m nodes, $\underline{\underline{A}}$ is a $2N_m + 2$ square matrix, $\underline{\underline{B}}$ is a $(2N_m + 2) \times 5$ matrix, \underline{x} is a $2N_m + 2$ vector, and \underline{y} is a 5 vector. The \underline{x} vector is composed of nodal interface values:

$$\underline{x} = \text{col} \left\{ \Delta E_{mi}, W_{mi}, \dots, \Delta E_j, W_j, \dots, \Delta E_{mo}, W_{mo} \right\}. \quad (1.4-3)$$

Vector \underline{y} is made up of changes in the enthalpy and pressure in the modules connecting to the inlet and outlet of the segment, and unity:

$$\underline{y} = \text{col} \left\{ \Delta E_{IM}, \Delta P_{IM}, \Delta E_{OM}, \Delta P_{OM}, 1 \right\} \quad (1.4-4)$$

1.4.2.1.1 NON-TURBINE SEGMENTS

For segments that do not contain turbines (turbines are always isolated in a segment), the standard momentum integral network equations are loaded. The $2N_m + 2$ equations loaded into matrices $\underline{\underline{A}}$ and $\underline{\underline{B}}$ depend on the conditions within the segment at step k . One momentum equation or choke flow constraint must be used for each segment,

$$I_m \frac{dW_m}{dt} = P_{mi} - P_{mo} + \beta_m - \sum_{i=Nf_m}^{Nl_m} \alpha_i |W_i| W_i, \quad (1.4-5)$$

$$\text{if } W_m^{\text{est}} < W_{cm},$$

or

$$W_m = W_{cm}, \quad \text{if } W_m^{\text{est}} \geq W_{cm}, \quad (1.4-6)$$

where W_m^{est} is the segment flow rate estimated with P_{mi} and P_{mo} remaining constant. Zero, one, or two equations must be written to constrain the segment end enthalpy when flow is entering the segment:

$$F_{mi} = E_{IM}, \quad \text{if } W_{mi} \geq 0, \quad (1.4-7)$$

and

$$E_{mi} = E_{OM}, \quad \text{if } W_{mo} \leq 0. \quad (1.4-8)$$

Mass must be conserved in each of the nodes

$$V_i \left(\frac{\partial \rho_i}{\partial E_i} \right) \frac{dE_i}{dt} = W_j - W_{j+1} - V_i \left(\frac{\partial \rho_i}{\partial P_m} \right) \frac{dP_m}{dt} \quad (1.4-9)$$

This accounts for N_m mass equations, giving $N_m + 1$, $N_m + 2$, or $N_m + 3$ equations, depending on the direction of flow at the segment end. The remaining $N_m + 1$, N_m , or $N_m - 1$ remaining equations come from the nodal energy equations.

That $N_m + 1$, N_m , or $N_m - 1$ equations are needed is seemingly in conflict with the ready availability of energy equations for the N_m nodes. At this point it is enthalpies at the nodal interfaces that are required, and the relationship between the constraint of these enthalpies and the nodal energy equations is not trivial.

The nodal energy equation can be written as:

(1.4-10)

$$V_i \left\{ \rho_i + E_i \left(\frac{\partial \rho_i}{\partial E_i} \right) \right\} \frac{dE_i}{dt} = W_j E_j - W_{j+1} E_{j+1} + Q_i - V_i \left\{ 1 - E_i \left(\frac{\partial \rho_i}{\partial P_m} \right) \right\} \frac{dP_m}{dt}$$

Before loading a conservation of mass equation, Eq. (1.4-9), into the matrix equation, the node average enthalpy time derivative term must first be eliminated. The nodal energy equation, Eq. (1.4-10) can be used to isolate the node average enthalpy time derivative:

$$\frac{dE_i}{dt} = \frac{\left\{ W_j E_j - W_{j+1} E_{j+1} + Q_i + V_i \left[1 - E_i \left(\frac{\partial \rho_i}{\partial P_m} \right) \right] \frac{dP_m}{dt} \right\}}{V_i \left\{ \rho_i + E_i \left(\frac{\partial \rho_i}{\partial E_i} \right) \right\}} \quad (1.4-11)$$

This expression is substituted into eq. (1.4-9) to obtain a conservation of mass equation used for all nodes. Equation (1.4-11) is eventually used to advance the node average enthalpies.

In order to use Eq. (1.4-10) to advance the nodal interface enthalpy, the derivative of node average enthalpy with respect to time has to be expressed in terms of the interface enthalpies. If the obvious replacement is made, i.e.,

$$\frac{dE_i}{dt} = 0.5 \left(\frac{dE_j}{dt} + \frac{dE_{j+1}}{dt} \right) \quad (1.4-12)$$

a not so obvious result occurs. Because the time constant for enthalpy transport is relatively long, a non-physical numerical "rocking" occurs, in which outlet enthalpies swing rapidly in response to changes in inlet enthalpy.

The donor-cell differencing scheme is used in lieu of the averaging indicated by Eq. (1.4-12). The assumption is that the rate of change in enthalpy throughout the node (except the inlet section) is uniform in response to changes in inlet enthalpy, and thus,

$$\frac{dE_{j+1}}{dt} = \frac{dE_j}{dt} \quad (1.4-13)$$

The donor cell differenced form of the conservation of energy is written:

$$V_i \left\{ \rho_i + E_i \left(\frac{\partial \rho_i}{\partial E_i} \right) \right\} \frac{dE_{j+1}}{dt} = W_j E_j - W_{j+1} E_{j+1} + Q_i + V_i \left[1 - E_i \left(\frac{\partial \rho_i}{\partial P_m} \right) \right] \frac{dP_m}{dt} \quad (1.4-14)$$

Thus, for a node with flow entering one end and exiting the other, Eq. (1.4-14) effectively projects changes in outlet enthalpy in response to changes in the inlet enthalpy, for current nodal conditions. This is true regardless of whether the flow direction is the same as steady state (forward flow), or the opposite (reversed flow). Of course, when the flow is reversed, the j -th interface is the node outlet, and Eq. (1.4-14) is written for dE_j/dt :

$$V_i \left\{ \rho_i + E_i \left(\frac{\partial \rho_i}{\partial E_i} \right) \right\} \frac{dE_j}{dt} = W_j E_j - W_{j+1} E_{j+1} + Q_i + V_i \left[1 - E_i \left(\frac{\partial \rho_i}{\partial P_m} \right) \right] \frac{dP_m}{dt} \quad (1.4-15)$$

When flow is not passing through a node, it is either entering (converging) or exiting (diverging) both ends. Neither condition is stable, i.e., likely to continue through the time step. For a diverging flow node, we assume the rate of change in enthalpy is uniform throughout the node, and therefore load both Eq. (1.4-14) and Eq. (1.4-15) into the matrix equation.

For a converging flow node, the enthalpy at both interfaces is determined from outside the node. Thus it is unnecessary to use the nodal energy equation to constrain interface enthalpy.

Thus, a node contributes zero, one, or two constraints on interface enthalpy, depending on whether the flow is converging, through, or diverging, respectively. For a converging flow segment, there must be one more converging node than diverging node. Similarly, a diverging flow segment must contain one more diverging flow node than converging node. A flow-through segment has an equal number of converging and diverging nodes. Therefore, the nodal energy equations account for $N_m - 1$, N_m , or $N_m + 1$ constraints, as are required.

The nodal equations are thus loaded into the matrices of Eq. (1.4-2) in semi-implicit form, i.e.,

$$y^k = f(x^k). \quad (1.4-16)$$

The loading logic is summarized in Table (1.4-1).

With the complexity involved in choosing the equation to be used in loading the segment matrix equation, care must be taken that mass and energy are conserved for each node. Because the nodal mass conservation equations are, in fact, responding to changes in node average enthalpy and segment pressure, and adjusting mass flow rates accordingly, mass is indeed being conserved. Energy is also being conserved, since Eq. (1.4-11) is subsequently used to advance the node average enthalpy in converging in diverging nodes. For flow-through nodes, back averaging of the nodal interface enthalpies is used to get the new node average enthalpy, as is standard with donor-cell differencing.

1.4.2.1.2 TURBINE SEGMENTS

As was discussed in Section 1.2.6, the MINET model for a turbine stage is based on operating characteristics and thermodynamics, rather than geometry. The model is also quasi-static. The reason for this type of modeling approach is that given the location of the turbine in the plant system, and its substantial complexity, it is best to take a simplified approach for this application.

While the equations loaded into the segment matrix equation (1.4-2) are slightly different for the one node segment containing a turbine stage, they are made to look very much like those in regular segments. Basically there are three differences:

Table 1.4-1 Logic Used in Loading Segment Matrix Equation

| Row | I | Load |
|--------------------|------------------------|---|
| 1 | $W_{mi}^k > 0$ | $\Delta E_{mi}^{\ell} = E_{IM}^{\ell} - E_{mi}^k + \Delta E_{IM}^{\ell}$ |
| . | . | . |
| . | . | . |
| . | . | . |
| 2n-1 | $W_j^k < 0$ | $(C_3 - W_j^k) \Delta E_j^{\ell} - C_7 W_j^{\ell} + W_{j+1}^k \Delta E_{j+1}^{\ell} + C_8 W_{j+1}^{\ell} = -C_4 \Delta P_m^{\ell} + Q_i^k - \left(\frac{\delta Q_i}{\delta W_i} \right) W_i^k$ |
| 2n | Any | $-C_5 W_j^k \Delta E_j^{\ell} + \{1 - C_5 E_j^k - C_6\} W_j^{\ell} - C_5 W_{j+1}^k \Delta E_{j+1}^{\ell} + \{C_5 E_{j+1}^k - C_6 - 1\} W_{j+1}^{\ell} = (C_2 - C_4 C_5) \Delta P_m^{\ell} + C_5 Q_i^k - 2C_6 W_i^k$ |
| 2n+1 | $W_{j+1}^k > 0$ | $-W_j^k \Delta E_j^{\ell} - C_7 W_j^{\ell} + (W_{j+1}^k + C_3) \Delta E_{j+1}^{\ell} + C_8 W_{j+1}^{\ell} = -C_4 \Delta P_m^{\ell} + Q_i^k - \left(\frac{\delta Q_i}{\delta W_i} \right) W_i^k$ |
| . | . | . |
| . | . | . |
| . | . | . |
| 2N _m +1 | $W_{mo}^k < 0$ | $\Delta E_{mo}^{\ell} = E_{OM}^k - E_{mo}^k + \Delta E_{OM}^{\ell}$ |
| 2N _m +2 | $W_m^{est} \geq W_c^k$ | $\sum_{i=Nf_m}^{N\ell_m} \left\{ \left[\frac{\Delta X_i}{A_i \Delta t^{\ell}} + \left(\alpha_i^k + F_{k_m} \frac{\Delta X_i / A_i}{I_m} \right) W_i^k \right] \frac{(W_j^{\ell} + W_{j+1}^{\ell})}{2} \right\} = \frac{I_m W_m^k}{\Delta t^{\ell}} + p_{IM}^{\ell} - p_{OM}^{\ell} + \beta_m^k$ |
| | $W_m^{est} > W_c^k$ | $\sum_{i=Nf_m}^{N\ell_m} \left\{ \frac{\Delta X_i}{2A_i} (W_j^{\ell} + W_{j+1}^{\ell}) \right\} = I_m W_c^k$ |

1.4-10

Table 1.4-1 (Continued)

where

$$C_1 = \frac{V_i}{\Delta t} \left(\frac{\partial \rho_i}{\partial E_i} \right)^k, \quad C_2 = \frac{V_i}{\Delta t} \left(\frac{\partial \rho_i}{\partial P_m} \right)^k, \quad C_3 = \frac{V_i}{\Delta t} \left[\rho_i + E_i \left(\frac{\partial \rho_i}{\partial E_i} \right) \right] - \frac{\partial Q_i}{\partial E_i}, \quad C_4 = \frac{V_i}{\Delta t} \left[E_i \left(\frac{\partial \rho_i}{\partial P_m} \right) - 1 \right],$$

$$C_5 = C_1/C_3, \quad C_6 = C_2 \left(\frac{\partial Q_i}{\partial W_i} \right) / 2, \quad C_7 = E_j^k \left(\frac{\partial Q_i}{\partial W_i} \right) / 2, \quad C_8 = E_{j+1}^k - \left(\frac{\partial Q_i}{\partial W_i} \right) / 2$$

- 1) The flow gradient across the segment is forced to zero by setting the density derivatives to zero. This is done because the dynamic response of flow in the turbine is very fast, and the flow out will nearly match the flow in.
- 2) The heating term in Eq. (1.4-11) is set to the current work being done on the turbine, which is generally negative, and causes a reduction in enthalpy.
- 3) The modified Stadola Equation, Eq. (1.2-13), is used in place of the momentum equation by setting β to zero and altering the definition of α in Eq. (1.4-5) to

$$\alpha = \frac{P_{in}}{((P_{in} + P_{out}) \cdot \rho_{in} \cdot Fk_{tb}^2)} \quad (1.4-17)$$

The segment inertia I is also zeroed out, converting Eq. (1.4-5) to a steady state equation.

1.4.2.2 SOLVING FOR THE SEGMENT RESPONSE MATRIX

Once the matrices of Eq. (1.4-2) have been loaded, the segment response matrix is available as:

$$\underline{\underline{B'}} = \underline{\underline{A}}^{-1} \underline{\underline{B}}. \quad (1.4-18)$$

While the expression of the segment response matrix as the inverse of matrix $\underline{\underline{A}}$ times matrix $\underline{\underline{B}}$ is simple enough, the computation involved can be significant, especially for large matrices. Because of the large number of zeros in the $\underline{\underline{A}}$ matrix, MINET loads and solves the segment matrix equation in close-packed

form. This step saves data storage space and significantly increases computational speed. Since a form of Gaussian elimination is still used to solve for the segment response matrix, there is little need to detail the process beyond making the following points.

- 1) Matrix $\underline{\underline{A}}$ is stored and solved as a six column matrix with $2N_m + 1$ rows plus a $2N_m + 2$ column matrix with one row (the momentum equation).
- 2) While the entries of matrix $\underline{\underline{A}}$ change somewhat under various flow conditions, the solver is general enough to handle any situation.
- 3) The solver is several times faster than full Gaussian elimination.

1.4.2.3 BOUNDARY ADJUSTED SEGMENT RESPONSE MATRIX

Before continuing on to evaluate the segment response matrices for the other segments, two steps are taken. First, matrix $\underline{\underline{A}}$ is discarded (data storage area de-allocated), as it is no longer useful. Second, advanced time (step ℓ) values are already known for the boundary modules, and these values are factored into the segment response matrix at this time. For a boundary module at the segment inlet with pressure and enthalpy specified as boundary conditions, these changes can be factored into column 5 of the matrix:

$$\left\{ \begin{aligned} B_{i,5}^k &= B_{i,5}^k + B_{i,1}^k \Delta E_{IM}^\ell \\ &+ B_{i,2}^k \Delta P_{IM}^\ell \end{aligned} \right\}, \quad i = 1, \dots, 2N_m + 2 \quad (1.4-19)$$

When mass flow rate is the boundary condition for the inlet boundary module, the change in pressure must be inferred from the equation for W_{mi} (after ΔE_{IM}^l is factored in),

$$\Delta P_{IM}^l = \{W_{IM}^l - B_{2,5} - B_{2,3} \Delta E_{OM}^l - B_{2,4} \Delta P_{OM}^l\} / B_{2,2} \quad (1.4-20)$$

This change in pressure is then factored into all of the rows.

$$\{B_{i,5}^k = B_{i,5}^k + (W_{IM}^l - B_{2,5}) B_{i,2} / B_{2,2}\}, \quad i = 1, 2N_m + 2 \quad (1.4-21)$$

$$\{B_{i,3}^k = B_{i,3}^k - B_{2,3} \cdot B_{i,2} / B_{2,2}\}, \quad i = 1, 2N_m + 2 \quad (1.4-22)$$

$$\{B_{i,4}^k = B_{i,4}^k - B_{2,4} \cdot B_{i,2} / B_{2,2}\}, \quad i = 1, 2N_m + 2 \quad (1.4-23)$$

If the mass flow rate is specified for a boundary module at the outlet end of a segment, it is the last row of the segment response matrix that is used to infer the change in outlet pressure. For the case when both ends of a segment connect to boundary modules, only the fifth column of the boundary adjusted segment response matrix is effectively non-zero, and the advancement of segment parameters to step k could be done immediately.

All of the segments in a network side are completed, and the boundary adjusted segment response matrices are stored, before the network volume pressure and enthalpy calculations are performed. First, however, the module advancement process, performed while the segment matrix equation is being loaded, will be discussed.

1.4.3 MODULE CONDITIONS UPDATE

In the transient calculations, the module level variables are advanced at the same time that the segment equations are being loaded. This saves on data storage space and reduces code complexity.

Essentially, there are two types of module level characteristics that must be known for segment level calculations to proceed correctly. These are pressure drops and heat transfer (or work) rates.

As was the case in steady state calculations, the pressure losses are broken into two parts, a constant term, B_m (see Eq. (1.3-18)), and a term proportional to the square of the mass flow rate, α . However, during transients, there is often wide variation in local mass flow rate, and the use of a segment loss factor, α_m , is impractical. Instead, a local loss factor, α_j , is evaluated for each node and is loaded into the segment momentum equation (see last row in Table 1.4-1). This local α_j is defined consistently with Eq. (1.3-19), i.e.,

$$\alpha_j = \frac{f_j}{2\rho_j A_j D_j} + \delta_{jv} K_v / 2\rho_j A_v^2 + \frac{Fk_j}{2\rho A^2 D_{eq}} \quad (1.4-24)$$

Pressure losses due to gravity, friction, and acceleration are evaluated at each segment node, for current time enthalpies, mass flow rates, and pressures. For the pump, turbine, and valve modules (one node each), an additional contribution is made to the pressure drop. In order to evaluate these pressure drop terms accurately, advanced time values of relative pump and turbine speed and valve stem position are needed. If a speed or valve position

has already been set, the module calculation can proceed. If alternate means of controlling pump and turbine speeds and valve position were specified, the speed or position must yet be advanced in time.

For a pump, the relative demand speed, $\omega_{d_p}^k$, is first calculated. The advanced time relative pump speed, ω^k , is calculated via the differential equation

$$\tau_p \left(\frac{d\omega_p}{dt} \right)^k = \omega_{d_p}^k - \omega_p^k, \quad (1.4-25)$$

where τ_p is the user input pump time constant. If the relative pump speed drops below the user-input pump seizure speed, it is set to zero. The relative demand speed can be tripped, i.e., changed from 1 to 0, at a user input time, through the limited MINET control option or other control system action.

For a valve, the relative demand stem position, S_d is first calculated. The advanced time valve stem position is calculated using the equation

$$\tau_v \left(\frac{ds}{dt} \right)^k = S_d^k - S^k \quad (1.4-26)$$

where τ_v is the appropriate user-input time constant. The stem position is limited by the user-input minimum "leak" position and full open. Furthermore, it is not allowed to cross past the current demand position during the step. The limited MINET internal controller is useful for safety valves which open ($S_d = 1.0$) and close ($S_d = 0.0$) at set pressures and time constants (τ_{vO} and τ_{vC}). In an alternate option, the user can specify a check valve, in which case the demand position responds to local flow rather than pressure.

For a turbine stage, the relative demand speed, ω_t^d , is first calculated. The advanced time relative pump speed, ω_t^l , is calculated via the differential equation

$$\tau_t \left(\frac{d\omega_t}{dt} \right)^l = \omega_t^d - \omega_t^k \quad (1.4-27)$$

where τ_t is the user input turbine time constant. Should the turbine speed drop below the seizure speed from user input, the speed is set to zero. The turbine can be tripped at a given time through user input, which resets the demand speed from 1 to 0.

The calculation of current time heat transfer rates is a more involved process, partly because the tube wall temperature depends on conditions in two otherwise disconnected segments. Because the time constants in the heat transfer process are not small, explicit treatment of the tube temperature, T_c^k , is possible.

When heat exchangers are analyzed during the segment marches, the heat transfer rate is evaluated using current fluid characteristics and tube wall temperatures,

$$Q_i^k = \pi D \Delta X_i \cdot h_i^k (E_i^k, p_m^k, T_c^k) \quad (1.4-28)$$

$$\cdot (T_c^k - T(E_i^k, p_m^k)).$$

The dependence of the heat flux on fluid enthalpy and mass flow rate are evaluated so that heat flux can be integrated implicitly with respect to these variables:

$$Q_i^l = Q_i^k + \frac{dQ_i^k}{dE_i^k} \Delta E_i^l + \frac{dQ_i^k}{dW_i^k} \Delta W_i^l \quad (1.4-29)$$

Only after all other system calculations are completed is the tube temperature advanced

$$T_{c_i}^k = T_{c_i}^{k-1} - \frac{\Delta t^k f a_h (D_I Q_{ii}^k + D_O Q_{oi}^k)}{A t_h \rho t_i C p t_i} \quad (1.4-30)$$

where subscript I and O refer to inside and outside the tube, respectively.

The explicit treatment of the tube wall temperatures greatly simplifies the calculational process, effectively decoupling the networks briefly while system variables are being advanced. However, it also introduces the time constant given in Eq. (1.4-1), which follows directly from Eqs. (1.4-28) and (1.4-30).

1.4.4 NETWORK VOLUME CALCULATIONS

Once the segment response matrices have been determined for all of the segments in one network, the volume pressures and enthalpies can be determined. Conservation equations for mass and energy in each of the N_d network volumes are coupled in the matrix equation,

$$\underline{C} \underline{V} = \underline{D}, \quad (1.4-31)$$

where \underline{C} is a $2N_d$ square matrix, \underline{D} is a $2N_d$ vector, and \underline{V} is the $2N_d$ vector

$$\underline{V} = \text{col} \{ \Delta E_1, \Delta P_1, \dots, \Delta E_{N_d}, \Delta P_{N_d} \}. \quad (1.4-32)$$

The individual equations loaded into Eq. (1.4-31) are implicit forms of Eqs. (1.1-1) and (1.1-2), with Eq. (1.1-3) used to eliminate the density time derivatives.

$$\frac{V_n}{\Delta t} \left(\frac{\partial \rho_n}{\partial E_n} \right)^k \Delta E_n^\ell + \frac{V_1}{\Delta t} \left(\frac{\partial \rho_n}{\partial P_n} \right) \Delta P_n^\ell = \overset{\text{Inlets}}{\Sigma W_{m0}} - \overset{\text{Outlets}}{\Sigma W_{m1}} \quad (1.4-33)$$

$$\frac{V_n}{\Delta t} \left\{ \rho_n + E_n \left(\frac{\partial \rho_n}{\partial E_n} \right)^k \right\} \Delta E_n^\ell + \frac{V_n}{\Delta t} \left[E_n^k \left(\frac{\partial \rho_n}{\partial P_n} \right)^k - 1 \right] \Delta P_n^\ell \quad (1.4-34)$$

$$\overset{\text{Inlets}}{\Sigma W_{m0}} E_{m0}^\ell - \overset{\text{Outlets}}{\Sigma W_{m1}} E_{m1}^\ell + Q_n^\ell$$

The process of loading Eqs. (1.4-33) and (1.4-34) into Eq. (1.4-31) is straightforward, with the exception of the inflows and outflows. Here the segment response matrices must be used to obtain the advanced time segment inlet and outlet mass flow rate and enthalpy as a function of changes in bordering pressures and enthalpies. As a simplification, for this part of the process it is assumed that the change in pressure at the segment boundary is equal to the change in pressure in the bordering volumes (even though the absolute pressures may be different). Thus, for a segment taking flow out of volume 1 and into volume 2, the second row of the segment response matrix is retrieved (volume outflow is segment inflow). Then, for the first volume mass equation, the first four columns of the segment response matrix, row 2, are added to the first four columns of matrix C, row 1. This accounts for changes in the mass flow rate going into the segment in response to changes in enthalpy and pressure in the inlet and outlet bordering volume. The fifth column entry of row 2 of the segment response matrix is then subtracted from the first row of vector D. Note that if the segment were connected at this outlet to a boundary module instead of a volume, the third and fourth columns of the segment response matrix would be ignored.

Loading Eq. (1.4-34) is slightly more difficult because the flow energy terms must be linearized.

$$W^k E^k = E^k W^k + W^k \Delta E^k. \quad (1.4-35)$$

Rows must be extracted from the segment response matrix for both W^k and ΔE^k , and substituted in Eq. (1.4-35). Second order " Δ " terms are dropped. The remaining terms are then loaded into Eq. (1.4-31).

After equations for all volumes in the network have been loaded into the matrices, Eq. (1.4-31) is solved for vector \underline{V} . This is done using full Gaussian elimination, as these matrices are generally small and have mostly non-zero elements.

$$\underline{V} = \underline{C}^{-1} \underline{D} \quad (1.4-36)$$

Vector \underline{V} contains changes in the network volume enthalpies and pressure during the time step.

1.4.5 ADVANCING NETWORK VARIABLES

Volume enthalpies and pressures are advanced using the changes indicated in vector \underline{V} . If the contents of the volume are separated, the new level is then calculated. Using vector \underline{V} and the boundary module adjusted segment response matrix, all of the nodal interface enthalpies and mass flow rates are then advanced.

The advancement of segment inlet and outlet enthalpy and mass flow is straightforward, as they are equal to the values for the just advanced interface enthalpies and mass flow rate at the inlet and outlet of the segment.

Similarly, the boundary module enthalpies and mass flow rates can be advanced, where appropriate, using segment inlet and outlet enthalpies and flows.

Segment inlet/outlet pressures and boundary module pressure are not always as easy to advance. If the segment connects to a volume, the segment inlet/outlet pressure is calculated using the advanced volume pressure and elevation head. In the case where the pressure option was chosen as the user input parameter for the boundary module, the pressure at the boundary module is advanced already, and the adjoining segment pressure is adjusted to match it. It is the case where one or both ends of the segment connect to boundary modules and where mass flow rate boundary conditions were specified that is most difficult. For such a boundary module at the segment inlet, Eq. (1.4-20) must be used (these matrix B entries are carefully preserved). A similar expression is used when a mass flow rate boundary condition is specified at the segment outlet. When a segment has mass flow rate boundary conditions on both ends, Eq. (1.4-20) and the equivalent at the segment outlet are coupled and solved for the pressure at both ends.

Once the segment inlet and outlet pressures have been advanced, a new segment average pressure is calculated. This advanced time pressure is compared against the current value, thus giving the change over the time step, to be used in advancing the node average enthalpies. The node average energy equation used is the linearized form of Eq. (1.4-11):

$$\begin{aligned} \Delta E_i = & \left\{ -C_4 \Delta P_m^{\ell} + W_j^{\ell} E_j^{\ell} - W_{j+1}^{\ell} E_{j+1}^{\ell} \right. \\ & \left. + Q_i^k + \left(\frac{\partial Q_i}{\partial W_i} \right) \Delta W_i^{\ell} \right\} / C_3 \end{aligned} \quad (1.4-37)$$

where C_3 and C_4 are as given in Table (1.4-1). If the flow is passing through the node at the beginning of the step, the node average enthalpy is over-written with the linear average of the junction enthalpies on either end. This is a standard step in the donor-cell differencing scheme used for the flow-through nodes. Thus, Eq. (1.4-37) is actually used (and is critical) only for converging and diverging flow nodes.

1.5 MINET CONSTITUTIVE RELATIONS

The equations detailed in previous sections were obtained from a physical and mathematical representation of the system, and its components. These are supplemented by various empirical and semi-empirical relations generally referred to as correlations. These constitutive relations are used to determine fluid and material properties, heat transfer and conductivity, as well as friction factors.

The constitutive relations used in MINET reflect, to some degree, on past, current, and intended applications. Should the user wish to make substitutions, the relevant functions are easily identified and can easily be modified.

1.5.1 FLUID PROPERTIES

The MINET fluid property functions provide values of dependent variables, e.g., density and temperature, as a function of the MINET independent variables, enthalpy and pressure. Properties are currently in place for water/steam, sodium, air, and NaK. The functions for water and steam are far more extensive than the others, as they span the subcooled, saturation, and superheated states, and are accurate over a wide range of pressure. Sodium and NaK are assumed to be subcooled and incompressible, but thermally expandable. Air is assumed to be an ideal gas.

Most of the fluid properties are programmed to parallel each other, allowing the use of the generic fluid functions listed in Table 1.5-1. These six

functions can be called with the fluid enthalpy (or temperature, if ENTH3C), pressure, fluid type, and the side parameter. The side parameter is used to take advantage of the segment average saturation properties, and can have values of 1, 2, or 3 meaning (1) inside the tubes or pipes, (2) outside the heat exchanger tubes, or (3) "other". In several cases, these functions are trivial for fluids other than water/steam, but their use simplifies the code logic, justifying the occasional overkill.

Table 1.5-1 Generic Fluid Properties

| Name | Function |
|--------|---|
| TEMP3C | T (E, P, Fluid, Side) |
| ENTH3C | E (T, P, Fluid, Side) |
| RHO3C | ρ (E, P, Fluid, Side) |
| DRDE3C | $\partial\rho/\partial E$ (E, P, Fluid, Side) |
| DRDP3C | $\partial\rho/\partial P$ (E, P, Fluid, Side) |
| VISC3C | μ (E, P, Fluid, Side) |

1.5.1.1 WATER AND STEAM

Because of storage considerations, functional fit steam tables are used in MINET, as opposed to tabular data. Many of these functions are based on those cited in the RETRAN-02 code documentation [9], and were simply converted from British Units to S.I. units. They were reported to be accurate from 0.7 KPa to 22.114 MPa (critical) within 1%, and usually are much closer to 1964 ASME tabular values. The S.I. versions incorporated in MINET appear to be equally accurate.

1.5.1.1.1 SATURATION PROPERTIES

A small number of MINET steam table functions are purely saturation properties, as opposed to subcooled or superheated properties evaluated at saturation conditions. These include saturation enthalpies, entropies, and surface tension.

The functions for saturated liquid and vapor enthalpies are given by the relations [9]

$$E_f(P) = \begin{cases} \sum_{i=0}^8 CF1_i (\ln(P'))^i & \text{if } 0.1 \text{ PSIA} < P' < 950 \text{ PSIA} \\ \sum_{i=0}^8 CF2_i (\ln(P'))^i & \text{if } 950 \text{ PSIA} < P' < 2550 \text{ PSIA} \\ \sum_{i=0}^8 CF3_i ((PCRIT-P')^{0.41})^i & \text{if } 2550 \text{ PSIA} < P' \leq 3208.2 \text{ PSIA} \end{cases} \quad (1.5-1)$$

and

$$E_g(P) = \begin{cases} \sum_{i=0}^{11} CG1_i (\ln(P'))^i & \text{if } 0.1 \text{ PSIA} < P' < 1500 \text{ PSIA} \\ \sum_{i=0}^8 CG2_i (\ln(P'))^i & \text{if } 1500 \text{ PSIA} < P' < 2650 \text{ PSIA} \\ \sum_{i=0}^6 CG3_i ((PCRIT-P')^{0.41})^i & \text{if } 2650 \text{ PSIA} < P' \leq 3208.2 \text{ PSIA} \end{cases} \quad (1.5-2)$$

where

$$P' \text{ (PSIA)} = P \text{ (Pa)}/6892.86, \quad (1.5-3)$$

and E is enthalpy in Joules/Kg. The coefficient for Eqs. (1.5-1) and (1.5-2) are given in Table 1.5-2. To insure a smooth transition, the functions are interpolated near the switch points, e.g., between 850 and 950 PSIA for saturated liquid enthalpy.

The saturated entropy functions are given by

$$S_f(P) = \sum_{i=1}^j A(i) P^{i-1}, \quad (1.5-4)$$

and

$$S_g(P) = \sum_{i=1}^j B(i) P^{i-1}, \quad (1.5-5)$$

where P is pressure in Pa, S is entropy in J/KG/K, and coefficients A and B are as given in Table 1.5-3 [10].

The surface tension, σ , for the surface between the liquid and vapor phases of saturated water is expressed as a function of saturation temperature in a correlation by Schmidt [9]:

$$\sigma = \frac{a_1 (T_K - T)^2}{1 + \beta (T_K - T)} + \sum_{n=2}^5 a_n (T_K - T)^n, \quad (1.5-6)$$

Table 1.5-2 Saturated Enthalpy Coefficients

| i | $CF1_i$ | $CF2_i$ | $CF3_i$ |
|-----|----------------|----------------|----------------|
| 0 | 1.621428516E5 | 1.955844733E9 | 2.107363079E6 |
| 1 | 7.763094766E4 | 8.460623122E8 | -3.318768201E4 |
| 2 | 5.39222795E3 | -1.077986251E9 | 3.540715284E3 |
| 3 | 4.281234467E2 | 2.629092545E8 | -1.622150763E3 |
| 4 | -1.220103831E1 | -1.011860544E5 | 4.054431208E2 |
| 5 | 6.694244345 | -9.069046525E6 | -5.395663361E1 |
| 6 | 4.078995306 | 1.557815108E6 | 3.940288541 |
| 7 | -1.00828835 | -1.100366955E5 | -1.5013799E-1 |
| 8 | 7.73557653E-2 | 2.942680883E3 | 2.332985206E-3 |

| i | $CG1_i$ | $CG2_i$ | $CG3_i$ |
|-----|-----------------|----------------|----------------|
| 0 | 2.572176571E6 | -5.196900383E9 | 2.107350942E6 |
| 1 | 3.342331204E4 | 2.863881997E9 | 1.293711324E4 |
| 2 | 1.965053933E3 | -4.602800148E3 | 7.987925031E3 |
| 3 | 37.6168376 | 4.326332190E4 | -1.49012646E3 |
| 4 | -3.491669097 | -6.433021266E3 | 1.376661588E2 |
| 5 | 0 | 2.4098148E6 | -6.339230554 |
| 6 | 0 | -4.985602203E5 | 1.164479972E-1 |
| 7 | 0 | 3.932121054E4 | - |
| 8 | 0 | -1.131441328E3 | - |
| 9 | -2.878833357E-2 | - | - |
| 10 | 6.989102705E-3 | - | - |
| 11 | -4.747120847E-4 | - | - |

Table 1.5-3 Saturated Entropy Coefficients

| Interval: | | | | | |
|--------------|--------------|--------------|--------------|--------------|--------------|
| P(Pa) Lower: | 6.893E2 | 6.893E3 | 6.893E4 | 6.893E5 | 6.893E6 |
| P(pa) Upper: | 6.893E3 | 6.893E4 | 6.893E5 | 6.893E6 | 2.206E7 |
| <u>i</u> | <u>A(i)</u> | <u>A(i)</u> | <u>A(i)</u> | <u>A(i)</u> | <u>A(i)</u> |
| 1 | -2.54745E2 | 2.38789E2 | 8.02999E2 | 1.44017E3 | -2.20848E4 |
| 2 | 5.53165E-1 | 6.20416E-2 | 7.47844E-3 | 1.10989E-3 | 1.442656E-2 |
| 3 | -2.60122E-4 | -2.82744E-6 | -3.32931E-8 | -5.90671E-10 | -3.49733E-9 |
| 4 | 7.94604E-8 | 8.55421E-11 | 9.91732E-14 | 2.25130E-16 | 4.62936E-16 |
| 5 | -1.40433E-11 | -1.51647E-15 | -1.73103E-19 | -5.41747E-23 | -3.59341E-23 |
| 6 | 1.30802E-15 | 1.42790E-20 | 1.60476E-25 | 7.82891E-30 | 1.63582E-30 |
| 7 | -4.95878E-20 | -5.49668E-26 | -6.08564E-32 | -6.18745E-37 | -4.04720E-38 |
| 8 | - | - | - | 2.05140E-44 | 4.20332E-46 |

| Interval: | | | | | |
|--------------|--------------|--------------|--------------|--------------|--------------|
| P(Pa) Lower: | 6.893E2 | 6.893E3 | 6.893E4 | 6.893E5 | 6.893E6 |
| P(pa) Upper: | 6.893E3 | 6.893E4 | 6.893E5 | 6.893E6 | 2.206E7 |
| <u>i</u> | <u>B(i)</u> | <u>B(i)</u> | <u>B(i)</u> | <u>B(i)</u> | <u>B(i)</u> |
| 1 | 9598.322/A | 7.91753E3 | 7.91753E3 | 7.18409 | 3.72952E4 |
| 2 | -.970369 | -8.59705E-3 | -8.59705E-3 | -9.78648E-4 | -1.79198E-2 |
| 3 | 4.7138E-4 | 4.06828E-8 | 4.06828E-8 | 5.51919E-10 | 4.31043E-9 |
| 4 | -1.44925E-7 | -1.23303E-13 | -1.23303E-13 | -2.15887E-16 | -5.65901E-16 |
| 5 | 2.5653E-11 | 2.16846E-19 | 2.16846E-19 | 5.26786E-23 | 4.36308E-23 |
| 6 | -2.38994E-15 | -2.01815E-25 | -2.01815E-25 | -7.68853E-30 | -1.97567E-30 |
| 7 | 9.05962E-20 | 7.66976E-32 | 7.66976E-32 | 6.12538E-37 | 4.86766E-38 |
| 8 | - | - | - | -2.04492E-44 | -5.03894E-46 |

where σ is in N/M^2 and T is in K. Values for the constants in Eq. (1.5-6) are:

$$\begin{aligned}
 T_K &= 647.3 \text{ K} & \beta &= 0.83 \\
 a_1 &= 1.160936807E-4 & a_4 &= 1.28627465E-11 \\
 a_2 &= 1.121404688E-6 & a_5 &= -1.14971929E-14 \\
 a_3 &= -5.75280518E-9 & &
 \end{aligned}$$

As this saturation function is dependent on T , we must first determine the saturation temperature using the pressure and saturated liquid enthalpy, using the subcooled temperature function discussed in the next section.

1.5.1.1.2 SUBCOOLED WATER PROPERTIES

There are six functions that provide the subcooled water parameters, corresponding to the pressure and subcooled enthalpy. These functions include temperature, density, thermal conductivity, absolute viscosity, specific heat, and entropy, although the latter two are not really independent functions, as such.

The subcooled water temperature can be expressed as [9]:

$$T = \sum_{i=0}^1 \sum_{j=0}^3 CT1_{ij} P^i E^j, \quad (1.5-7)$$

where P is pressure in Pa, E is enthalpy in J/KG, T is in K, and coefficients $CT1_{ij}$ are as given in Table 1.5-4.

Table 1.5-4 Coefficients $CN1_{ij}$ for Eq. 1.5-7

| i/j | 0 | 1 | 2 | 3 |
|-----|-------------|----------------|--------------|---------------|
| 0 | 273.42 | 2.332E-4 | 1.907097E-11 | -2.067247E-17 |
| 1 | 2.708826E-7 | -1.9388325E-12 | 2.411277E-18 | -7.558857E-25 |

The specific heat is equal to the derivative of enthalpy with respect to temperature, expressed in J/KG/K. The function is determined by taking the derivative of Eq. (1.5-7) with respect to enthalpy and inverting.

The density is determined by inverting a function fitted for the specific volume [9]:

$$\rho = 1/\exp \sum_{i=0}^2 \sum_{j=0}^4 CN1_{ij} P^i E^j, \quad (1.5-8)$$

where ρ is the density in KG/M^3 , and the coefficients $CN1_{ij}$ are as given in Table 1.5-5.

The thermal conductivity in W/M/K is represented using the expression [11].

$$K_g = \sum_{i=0}^3 A_i EN^i, \quad (1.5-9)$$

when EN is normalized enthalpy, $E(\text{J/KG})/5.815\text{E}5$, and coefficients A_i are given in Table 1.5-6.

Table 1.5-5 Coefficients $CN1_{ij}$ for Eq. 1.5-8

| i/j | 0 | 1 | 2 | 3 | 4 |
|-----|---------------|-------------|---------------|---------------|--------------|
| 0 | -6.891704 | -1.63856E-7 | 7.96312E-13 | -7.279005E-19 | 2.739196E-25 |
| 1 | -6.98704E-10 | 4.83059E-15 | -1.873972E-20 | 2.20968E-26 | -8.7246E-33 |
| 2 | -3.831966E-17 | 1.30374E-22 | -8.100242E-29 | -6.027144E-35 | 5.32613E-41 |

Table 1.5-6 Coefficients A_i for Eq. 1.5-9

| i | A_i |
|---|-----------|
| 0 | .5737386 |
| 1 | .2536104 |
| 2 | -.1454683 |
| 3 | .0138747 |

The absolute viscosity, μ ($N \cdot S/M^2$), for subcooled water is given by the three part function:

$$\mu = \begin{cases} \sum_{i=0}^4 FKL1_i (X1)^i - (P-PCON) \sum_{i=0}^3 FKL2_i, & E^i < .276E6 \\ \sum_{i=0}^3 FKL3_i E^i + (P-PCON) \sum_{i=0}^3 FKL4_i E^i, & .276E6 < E < .394E6 \\ \sum_{i=0}^4 FKL5_i Z^i, & E > .394E6 \end{cases} \quad (1.5-10)$$

where

$$\begin{aligned} \text{PCON} &= 6.894575\text{E}5 \\ \text{XI} &= 8.5812897\text{E}-6 * (\text{E}-4.265884\text{E}4) \\ n &= 6.484504\text{E}-6 * (\text{E}-5.53588\text{E}4) \\ Z &= 3.89208\text{E}-6 * (\text{E}-4.014676\text{E}5) \end{aligned}$$

and coefficients are as shown in Table 1.5-7 [9].

Table 1.5-7 Coefficient FKL for Eq. (1.5-10)

| <u>i</u> | <u>FKL1</u> | <u>FKL2</u> | <u>FKL3</u> | <u>FKL4</u> | <u>FKL5</u> |
|----------|--------------|--------------|----------------|---------------|--------------|
| 0 | 1.29947E-3 | -6.5959E-12 | 4.452605E-3 | -3.80635E-11 | 3.026032E-4 |
| 1 | -9.26403E-4 | 6.763E-12 | -6.988008E-9 | 3.92852E-16 | -1.836607E-4 |
| 2 | 3.81047E-4 | -2.88825E-12 | 1.52102303E-14 | -1.25858E-21 | 7.567076E-5 |
| 3 | -8.219444E-5 | 4.4525E-13 | -1.23032E-20 | 1.2860181E-27 | -1.647879E-5 |
| 4 | 7.022438E-6 | - | - | - | 1.4164576E-6 |

Subcooled entropy is calculated using the thermodynamic identity [12]:

$$Tds = dE - dP/\rho \quad (1.5-11)$$

and the saturated liquid entropy function, S_f . First, S_f is calculated at the given pressure, then S is calculated using the change in enthalpy from saturation:

$$S = S_f + \int_{E_f}^E \frac{1}{T} dE \quad (1.5-12)$$

Because temperature is roughly linear with respect to enthalpy, the integral in Eq. (1.5-12) can be approximated using a few intervals, evaluating an interval average temperature for each.

1.5.1.1.3 SUPERHEATED STEAM PROPERTIES

Six functions provide superheated steam properties, corresponding to pressure and superheated enthalpy. Included are functions for temperature, density, thermal conductivity, absolute viscosity, specific heat, and entropy, although the specific heat and entropy are not truly independent of the others.

The superheated steam temperature can be expressed as [9]:

$$T = \sum_{i=0}^4 \sum_{j=0}^4 CT3_{ij} P^i E^j \quad (1.5-13)$$

where P is pressure in Pa, E is enthalpy in J/KG, T is in K, and coefficients $CT3_{ij}$ are as given in Table 1.5-8. By taking the derivative of Eq. 1.5-13 with respect to enthalpy and inverting, we get the specific heat function.

The density is determined by inverting a function that was fitted for specific volume [9]:

$$\rho = 1 / \left(\sum_{i=-1}^2 \sum_{j=0}^2 CN2_{ij} P^i E^j \right), \quad (1.5-14)$$

where ρ is the density in KG/M³, and the coefficients $CN2_{ij}$ are as given in Table 1.5-9.

Thermal conductivity in W/M/K is determined using the expression [11]:

$$K_v = \sum_{i=0}^3 X1_i T^i + \rho \left(\sum_{i=0}^2 X2_i T^i + \frac{2.1482E5 \cdot \rho}{T^{4.2}} \right), \quad (1.5-15)$$

where T is temperature in C, ρ is density in KG/m^3 , and coefficients $X1_i$ and $X2_i$ are as given in Table 1.5-10. Before Eq. (1.5-15) is utilized, the density and temperature are calculated from the enthalpy and pressure, and 273.15 is subtracted from the temperature (K).

Table 1.5-8 Coefficient $CT3_{ij}$ for Eq. (1.5-13)

| i/j | 0 | 1 | 2 | 3 | 4 |
|-------|---------------|--------------|--------------|---------------|--------------|
| 0 | -6.29534E3 | 6.757606E-3 | -2.750097E-9 | 5.380348E-16 | -3.97061E-23 |
| 1 | 1.01245E-2 | -1.15508E-8 | 4.956197E-15 | -9.465447E-22 | 6.782646E-29 |
| 2 | -1.267194E-9 | 1.472029E-15 | -6.42424E-22 | 1.247552E-28 | -9.0904E-36 |
| 3 | 5.560932E-17 | -6.54272E-23 | 2.89918E-29 | -5.727995E-36 | 4.252915E-43 |
| 4 | -8.430666E-25 | 1.008109E-30 | -4.55535E-37 | 9.199409E-44 | -6.99126E-51 |

Table 1.5-9 Coefficients $CN2_{ij}$ for Eq. (1.5-14)

| i/j | 0 | 1 | 3 |
|-------|-----------------|----------------|-----------------|
| -1 | -6.0375846E5 | .33347807 | -1.66007553E-8 |
| 0 | 2.3829985E-2 | -1.4478263E-8 | 2.14067927E-15 |
| 1 | -5.84125397E-10 | 3.28542173E-16 | -4.54237911E-23 |
| 2 | 1.0280146E-17 | -5.5310121E-24 | 8.81492754E-31 |

Table 1.5-10 Coefficients $X1_i$ and $X2_i$ for Eq. (1.5-15)

| i | $X1_i$ | $X2_i$ |
|-----|-----------|------------|
| 0 | 1.76E-2 | 1.0351E-4 |
| 1 | 5.87E-5 | .4198E-6 |
| 2 | 1.04E-7 | -2.771E-11 |
| 3 | -4.51E-11 | - |

The superheated steam absolute viscosity ($N \cdot s/m^2$) is also a function of density and temperature in C, which must first be calculated from the pressure and enthalpy. A three part function is used [9]:

$$\mu_V = \begin{cases} V1 - \rho (1.858E-7 - 5.9E-10 \cdot T) & T(C) < 300 \\ V1 + \rho \left\{ \sum_{i=0}^3 F_i T^i + \sum_{i=0}^3 G_i T^i \cdot \sum_{i=0}^2 A_i \rho^i \right\} & 300 < T(C) < 375 \\ V1 + \rho \sum_{i=0}^2 A_i \rho^i & T(C) > 375 \end{cases} \quad (1.5-16)$$

where A_i , F_i and G_i are as given in Table 1.5-11 and

$$V1 = .407E-7 \cdot T(C) + 8.04E-6. \quad (1.5-17)$$

Table 1.5-11 Coefficients A_i , F_i , and G_i for Eq. (1.5-16)

| i | A_i | F_i | G_i |
|-----|-----------|---------------|----------------|
| 0 | 3.53E-8 | -.2885E-5 | .176E3 |
| 1 | 6.765E-11 | .2427E-7 | -1.6 |
| 2 | 1.021E-14 | -.6789333E-10 | .0048 |
| 3 | - | .6317037E-13 | -.474074074E-5 |

Superheated steam entropy is also calculated using the thermodynamic identity [12]:

$$Tds = dE - dP/\rho \quad (1.5-18)$$

and the saturated vapor entropy, S_g . Entropy S is calculated using the change in enthalpy from saturation

$$S = S_g + \int_{E_g}^E \frac{1}{T} dE. \quad (1.5-19)$$

The integral in Eq. (1.5-19) is approximated using 5 intervals in order to accurately account for non-linearities in temperature versus enthalpy.

1.5.1.1.4 PROPERTIES AT SATURATION

Saturated enthalpy, entropy, and surface tension are evaluated using fitted functions given in Section 1.5.1.1.1. However, several saturation properties are evaluated by other means.

Saturated fluid and vapor densities, thermal conductivities, specific heats, and dynamic viscosities are evaluated using saturated fluid and vapor enthalpies and functions described in Sections 1.5.1.1.2 and 1.5.1.1.3. The saturation temperature is evaluated at the saturated fluid enthalpy using the subcooled temperature function, Eq. (1.5-7).

Derivatives of saturated fluid and vapor enthalpy and density are also needed. These are evaluated by perturbing the pressure, re-evaluating saturated enthalpies and densities, and differencing, e.g.,

$$\frac{\partial E_f}{\partial P} = \frac{E_f' - E_f}{P' - P} \quad (1.5-20)$$

1.5.1.1.5 PROPERTIES IN WATER/STEAM MIX

MINET currently uses a homogeneous equilibrium model (HEM) of two phase flow, which means both phases are assumed to move at the same speed. Using this simple representation, the quality is defined as:

$$X = \frac{E - E_f}{E_{fg}} \quad (1.5-21)$$

where $E_{fg} = E_g - E_f$.

The mixture entropy can be calculated from the quality, and saturated fluid and vapor entropies. The expression is

$$S = (1 - X) S_f + X S_g \quad (1.5-22)$$

Mixture specific volume can be calculated using the same quality weighting as used in Eq. (1.5-22). Density, the inverse of specific volume, is therefore

$$\rho = 1 / \left\{ \frac{(1 - X)}{\rho_f} + \frac{X}{\rho_g} \right\} \quad (1.5-23)$$

The derivatives of density with respect to enthalpy and pressure are also needed, and can be determined analytically using Eqs. (1.5-21) and (1.5-23). It can be shown that the derivative with respect to enthalpy is

$$\frac{\partial \rho}{\partial E} = -\rho^2 \left(\frac{1}{\rho_g} - \frac{1}{\rho_f} \right) / (E_g - E_f) . \quad (1.5-24)$$

Similarly, the derivative with respect to pressure is

$$\frac{\partial \rho}{\partial p} = \rho^2 \left\{ \frac{(1-x)}{\rho_f^2} \frac{\partial \rho_f}{\partial p} + \frac{x}{\rho_g^2} \frac{\partial \rho_g}{\partial p} - \left(\frac{1}{\rho_g} - \frac{1}{\rho_f} \right) \frac{\partial x}{\partial p} \right\} , \quad (1.5-25)$$

where

$$\frac{\partial x}{\partial p} = - \left\{ x \left(\frac{\partial E_g}{\partial p} - \frac{\partial E_f}{\partial p} \right) + \frac{\partial E_f}{\partial p} \right\} / (E_g - E_f) . \quad (1.5-26)$$

1.5.1.2 SODIUM

MINET sodium properties were taken from the Super System Code (SSC), an LMFBR transient analysis code [11]. Because of this, many of the functions are expressed in terms of temperature, which is a state variable in SSC, unlike MINET. Further, because subcooled sodium is essentially incompressible, pressure does not appear in any of the functions.

The relation between subcooled sodium enthalpy and temperature is given by

$$E = \sum_{i=0}^3 c_i T^i , \quad (1.5-27)$$

where E is in J/KG, T is in K, and c_i are as given in Table 1.5-12. To determine temperature in terms of enthalpy, we solve for the only real root of Eq. (1.5-27). The specific heat is determined by taking the derivative of Eq. (1.5-27), to get $c_p = \partial E / \partial T$.

The density of subcooled sodium is approximated using the function

$$\rho = \sum_{i=0}^3 R_i T^i \quad , \quad (1.5-28)$$

where density is in KG/M³, and T is in K, and R_i are as given in Table 1.5-13. The derivative of density with respect to enthalpy is determined by taking the derivative of (1.5-28) with respect to temperature and dividing by the specific heat.

Thermal conductivity is determined using the function

$$k = \sum_{i=0}^2 CK_i T^i \quad , \quad (1.5-29)$$

where T is in K, k is in W/M/K, and CK_i are as shown in Table 1.5-14 [13].

Absolute viscosity, in N · S/M², is determined using

$$\mu = 10^{(-2.4892 - 220.65/T - 0.4925 \log_{10} T)} \quad , \quad (1.5-30)$$

where T is in K [13].

Table 1.5-12 Coefficients C_i for Eq. (1.5-27)

| i | C_i |
|-----|------------|
| 0 | -67511.0 |
| 1 | 1630.22 |
| 2 | -.41674 |
| 3 | 1.54279E-4 |

Table 1.5-13 Coefficients R_i for Eq. (1.5-28)

| i | R_i |
|-----|-------------|
| 0 | 1011.597 |
| 1 | - .22051 |
| 2 | -1.92243E-5 |
| 3 | 5.63769E-9 |

Table 1.5-14 Coefficients CK_i for Eq. (1.5-29)

| i | CK_i |
|-----|-----------|
| 0 | 109.7 |
| 1 | -.064499 |
| 2 | 1.1728E-5 |

1.5.1.3 AIR

The MINET air properties are most accurate at atmospheric pressure, and are based on the ideal gas law

$$\rho = P/RT \quad , \quad (1.5-31)$$

where T is in K, P in Pa, ρ in KG/M^3 , and $R = 287.0 \text{ J/KG/K}$ [14].

The air enthalpy at atmospheric pressure is determined using

$$E = \sum_{i=0}^3 CA_i T^i \quad , \quad (1.5-32)$$

where coefficients CA_i are as given in Table 1.5-15. Temperature is calculated from enthalpy by taking the only real cubic root of Eq. (1.5-32). Specific heat is determined by taking the derivative of Eq. (1.5-32) with respect to temperature.

Table 1.5-15 Coefficients CA_i for Eq. (1.5-32)

| <u>i</u> | <u>CA_i</u> |
|----------|--------------------------|
| 0 | 161800.2 |
| 1 | 984.36 |
| 2 | 0.012504 |
| 3 | 4.6751E-5 |

With the density determined by Eq. (1.5-31), the derivative of density with respect to pressure is

$$\partial \rho / \partial P = 1/RT \quad . \quad (1.5-33)$$

The density derivative with respect to enthalpy is

$$\partial \rho / \partial E = \frac{-P}{287 \cdot T^2} / C_p \quad , \quad (1.5-34)$$

where C_p is the specific heat.

The thermal conductivity of air in W/M/K is determined using the expression

$$k = \sum_{i=0}^3 CK_i T^i \quad , \quad (1.5-35)$$

where coefficients CK_i are as given in Table 1.5-16.

Table 1.5-16 Coefficients CK_i for Eq. (1.5-35)

| <u>i</u> | <u>CK_i</u> |
|----------|--------------------------|
| 0 | -9.153E-5 |
| 1 | 1.03E-4 |
| 2 | -6.633E-8 |
| 3 | 3.056E-11 |

Absolute viscosity is calculated from

$$\mu = \sum_{i=0}^3 CV_i T^i \quad , \quad (1.5-36)$$

where μ is in $N \cdot S/M^2$ and CV_i are as given in Table 1.5-17.

Table 1.5-17 Coefficients CV_i for Eq. (1.5-37)

| i | CV_i |
|-----|------------|
| 0 | 4.735E-6 |
| 1 | 4.932E-8 |
| 2 | -9.0E-12 |
| 3 | -3.639E-15 |

1.5.1.4 NaK

MINET NaK (eutectic) functions were determined from information provided in Sodium - NaK Engineering Handbook, Vol. 1 by Faust [15]. Subcooled NaK is virtually incompressible, so the state functions are independent of P.

The relation between NaK temperature and enthalpy is given by the function

$$E = \sum_{i=0}^3 CK_i T^i \quad , \quad (1.5-37)$$

where E is in J/KG, T is in K, and CK_i are as given in Table 1.5-18. To determine temperature in terms of enthalpy, we solve for the only real root of Eq. (1.5-37). The specific heat is determined by taking the derivative of Eq. (1.5-37) with respect to temperature.

Table 1.5-18 Coefficients CK_i for Eq. (1.5-37)

| i | CK_i |
|-----|------------|
| 0 | 0 |
| 1 | 1098.6 |
| 2 | -.27858 |
| 3 | 1.14527E-4 |

The density of subcooled NaK is approximated as

$$\rho = \sum_{i=0}^2 RK_i T^i, \quad (1.5-38)$$

where ρ has units of KG/M^3 , and RK_i are given in Table 1.5-19. By taking the derivative of Eq. (1.5-38) with respect to temperature and dividing by specific heat, we get the density derivative with respect to enthalpy.

Table 1.5-19 Coefficients RK_i for Eq. (1.5-38)

| i | RK_i |
|-----|-----------|
| 0 | 937.01 |
| 1 | -.2095 |
| 2 | -2.346E-5 |

Thermal conductivity is determined using the relation

$$k = \sum_{i=0}^2 KK_i T^i, \quad (1.5-39)$$

where k is in W/M/K and KK_i are as in Table 1.5-20.

Table 1.5-20 Coefficients KK_i for Eq. (1.5-39)

| i | KK_i |
|-----|---------|
| 0 | 14.109 |
| 1 | 0.03271 |
| 2 | -2.2E-5 |

Absolute viscosity, in $N \cdot S/M^2$, is determined using a two part fitted function

$$\mu = \begin{cases} 1.16E-5 \rho^{1/3} e^{.688\rho/T}, & T < 673 \\ 8.2E-6 \rho^{1/3} e^{.979\rho/T}, & T > 673 \end{cases} \quad (1.5-40)$$

where ρ is density in KG/M^3 and T is temperature in K.

1.5.2 HEAT TRANSFER CORRELATIONS

A library of heat transfer correlations for current fluid types and conditions are discussed in this section. While this group is not all inclusive, many systems can be represented with an acceptably small error. Modifications

and additions may be made to this library with relative ease, and a continuing expansion of the library can be expected. The heat transfer correlation is frequently cited in terms of the non-dimensional Nusselt number

$$\text{Nu} = hD/k \quad . \quad (1.5-41)$$

This is easily converted to h using the diameter D and thermal conductivity k .

1.5.2.1 WATER AND STEAM

Because the heat transfer properties of water/steam vary significantly with conditions, a collection of correlations is used, each with its own range. The six principal modes and their MINET identifier numbers are: 1 - subcooled convection, 2 - subcooled nucleate boiling, 3 - forced convection vaporization, 4 - film boiling, 5 - superheated convection, 6 - condensation. If multiple heat transfer regimes occur in one node, MINET will generate a combined identifier, e.g., mode 123 means started in subcooled convection, passed through subcooled nucleate boiling and into forced convection vaporization.

1.5.2.1.1 SUBCOOLED CONVECTION

Heat transfer mode 1 is subcooled forced convection. The Nusselt number for this model is given as [16]:

$$\text{Nu} = 0.023 \text{Re}^{0.8} \text{Pr}^{0.4} \quad , \quad (1.5-42)$$

where Re is the Reynolds number and Pr is the Prandl number.

1.5.2.1.2 SUBCOOLED NUCLEATE BOILING

The heat transfer for subcooled nucleate boiling is given as [17]:

$$h = S \cdot h_{NB} + F \cdot h_c, \quad (1.5-43)$$

where the nucleate boiling coefficient h_{NB} is given as:

$$h_{NB} = 0.00122 \left\{ \frac{K_l^{0.79} C_l^{0.45} \rho_l^{0.49}}{\Omega^{0.5} \mu_l^{0.29} \lambda_{fg}^{0.24} \rho^{0.24}} \right\} \Delta P^{0.75}, \quad (1.5-44)$$

where

- C_l = specific heat of liquid
- K_l = thermal conductivity of liquid
- Ω = surface tension
- λ_{fg} = latent heat of vaporization, and
- ΔP = difference in saturation pressure corresponding to the wall superheat.

The Reynolds number correction factor F , and the nucleate boiling suppression factor S are represented as:

$$F = \begin{cases} 2.84 \frac{1}{X_{tt}^{0.45}}, & \frac{1}{X_{tt}} < 2. \\ 2.57 + 0.7643 \frac{1}{X_{tt}}, & \frac{1}{X_{tt}} \geq 2. \end{cases} \quad (1.5-45)$$

$$S = \begin{cases} 1.05 - 1.3 \times 10^{-5} Re, & Re \leq 2.5 \times 10^4 \\ 0.83 - 4.3 \times 10^{-6} Re, & 2.5 \times 10^4 < Re \leq 10^5 \\ 0.32 \exp(-1.92 \times 10^{-6} Re), & 10^5 < Re \leq 6 \times 10^5 \\ 0.09, & Re > 6 \times 10^5 \end{cases} \quad (1.5-46)$$

and

$$Re = Re_g F^{1.25},$$

where X_{tt} is the Lockhart/Martinelli [18] parameter:

$$\frac{1}{X_{tt}} = \left(\frac{x}{1-x}\right)^{0.9} \cdot \left(\frac{\rho_g}{\rho_v}\right)^{0.5} \cdot \left(\frac{\mu_v}{\mu_g}\right)^{0.10} \quad (1.5-47)$$

The convective coefficient h_c is calculated from the Dittus Boelter equation based on liquid thermodynamic properties [16].

1.5.2.1.3 FORCED CONVECTION VAPORIZATION

The same correlation [17] is used for forced convection vaporization as is used for subcooled nucleate boiling. See Section 1.5.2.1.2.

1.5.2.1.4 FILM BOILING

The heat transfer for film boiling regime is given as [19]:

$$Nu = 0.0193 Re_g^{0.8} Pr_g^{1.23} \left(\frac{\rho_B}{\rho_g}\right)^{0.68} \left(\frac{\rho_l}{\rho_g}\right)^{0.068}, \quad (1.5-48)$$

where subscripts l and g denote, respectively, liquid and vapor phase at saturation and subscript B indicates a bulk property of the steam/water mixture.

1.5.2.1.5 SUPERHEATED CONVECTION

For superheated steam, the following heat transfer correlation for forced convection is used [20]:

$$Nu = 0.0133 Re^{0.84} Pr^{0.333} \quad (1.5-49)$$

Fluid properties used in Eq. (1.5-49) are evaluated at the film temperature, taken as the average of the tube wall and fluid temperatures.

1.5.2.1.6 CONDENSATION

It is assumed that all condensation is filmwise, as it is difficult to induce the more efficient dropwise condensation in any practical way in a power plant [21]. Three condensation correlations are employed in MINET, according to the geometry.

1.5.2.1.6.1 CONDENSATION ON VERTICAL SURFACES

This "correlation" is based on a simple representation [6]:

$$Q = k_f \frac{\Delta T}{\delta} \quad (1.5-50)$$

where k_f is the fluid conductivity, δ is the thickness of the film layer, and ΔT is the difference between the wall temperature and the saturation temperature. Knowing the flow area, the flow fraction that is fluid, relative densities, and the wall surface area, one can easily determine the film thickness, assuming it is uniform. The current MINET "correlation" will represent condensation inside or outside tubes or pipes, and could be extended to other geometries.

1.5.2.1.6.2 CONDENSATION INSIDE HORIZONTAL TUBES

Condensate flowing inside tubes tends to pool at the bottom, causing a non-trivial distribution of film. To handle this case, a correlation by Chato [21] was converted to SI units and applied:

$$h = 0.9821 \left[\frac{\rho_f (\rho_f - \rho_g) k_f^3 E'_{fg}}{\mu_f \Delta T D} \right]^{1/4}, \quad (1.5-51)$$

where

$$E'_{fg} = E_g - E_f + \frac{3}{8} c_{pf} (T_{sat} - T_{wall}) \quad (1.5-52)$$

1.5.2.1.6.3 CONDENSATION ON HORIZONTAL TUBE BANKS

Representation of this type of condensation becomes somewhat more empirical, as the film thickness will vary with tube position, etc. A correlation by Chen [21] was converted to SI units and incorporated as:

$$h = 1.288 \cdot \left[1 + 0.2 \frac{c_{pf} \Delta T}{E_{fg} (n-1)} \right] \cdot \left[\frac{\rho_f (\rho_f - \rho_g) k_f^3 E_{fg}'}{n D \mu \Delta T} \right]^{1/4} \quad (1.5-53)$$

where n is the number of tubes stacked vertically, and other parameters are as described in the two previous correlations.

1.5.2.1.7 CRITICAL HEAT FLUX

When the heat flux due to nucleate boiling exceeds a critical heat flux level, surface boiling ceases and heat transfer is by film boiling. Because film boiling is far less efficient, it is important to locate and simulate this transition point. At this time, one has to rely on various empirical correlations to determine this location. There are currently three options in MINET, one of which must be chosen by the user for each side of each heat exchanger.

1.5.2.1.7.1 SODIUM/STEAM GENERATORS

A correlation was determined by Harty [22] for sodium to water heat exchangers, particularly those planned for the Clinch River plant. The steam/water quality at the DNB point is given by:

$$x_{\text{DNB}} = \frac{4.38 \times 10^4 \rho_L}{E_{fg} \rho_g \sqrt{G/1350.0}} \quad \text{for } q > 6.3 \times 10^5 \quad (1.5-54)$$

or

$$x_{\text{DNB}} = \frac{4.38 \times 10^4 \rho_L \cdot (6.3 \times 10^5 / q)^{1.5}}{E_{fg} \rho_g \sqrt{G/1350.0}} \quad \text{for } q < 6.3 \times 10^5, \quad (1.5-55)$$

where E_{fg} is the latent heat of vaporization (J/kg), G is the mass flow rate per unit area (kg/s m^2), and q is in W/m^2 and calculated in forced convection vaporization.

1.5.2.1.7.2 WATER/STEAM GENERATORS

For the steam generators commonly used in pressurized water reactor systems, i.e., hot primary water to cooler secondary water and steam, the MacBeth [23] correlation is used. The water/steam quality at CHF is

$$x = 1.0 - 5.1933 \frac{\bar{q} D^{0.1}}{E_{fg} G^{0.51}}, \quad (1.5-56)$$

where q is in W/M^2 and evaluated in the forced convection vaporization regime, D is the equivalent hydraulic diameter, E_{fg} is the latent heat of vaporization (J/kg), G is the mass flow rate per unit area (kg/s/M^2).

1.5.2.1.7.3 FIXED QUALITY

The user has the option of locking the CHF quality at $x = 0.75$, which is particularly useful for helical coil steam generators, because the CHF point is smeared by the sloped flow path. This option should also be used whenever CHF is unlikely to occur, because it is simpler than the other options, and thus requires less calculations and reduces the likelihood of errors [24].

1.5.2.2 SODIUM HEAT TRANSFER CORRELATIONS

For liquid metal flow in a pipe or tube, Aoki's correlation [25] for heat transfer is used:

$$Nu = 6.0 + 0.025 (\bar{\phi} Pe)^{0.8} , \quad (1.5-57)$$

where

$$\bar{\phi} = \frac{0.014(1 - e^{-71.8x})}{x} ,$$

$$x = \frac{1}{Re^{0.45} Pr^{0.2}} .$$

In the laminar region,

$$Nu = 4.36 \quad \text{for } Re \leq 3000 . \quad (1.5-58)$$

For the shell side of a heat exchanger, the Nusselt number is obtained from the Graber-Rieger correlation [26]:

$$\begin{aligned} \text{Nu} &= A + B \text{Pe}^C & 110 \leq \text{Pe} \leq 4300 \\ & & 1.25 \leq P/D \leq 1.95 \end{aligned} \quad (1.5-59)$$

where

$$\begin{aligned} A &= 0.25 + 6.2(P/D) \quad , \\ B &= -0.007 + 0.032 (P/D) \quad , \end{aligned}$$

and

$$C = 0.8 - 0.024(P/D) \quad .$$

The range of applicability is also indicated above. For $\text{Pe} < 110$, we use a constant value for Nu (evaluated using Equation (1.5-59) at $\text{Pe} = 110$).

1.5.2.3 NaK HEAT TRANSFER CORRELATION

The NaK heat transfer film coefficient [27] is:

$$h = 0.625 \left(\frac{k}{D_e} \right)^{0.6} (G C_p)^{0.4} \quad [\text{J/m}^2 \text{Sec}^\circ\text{k}] \quad (1.5-60)$$

where k is the thermal conductivity of the NaK or sodium, D_e is the equivalent diameter based on the total flow area and the total heated perimeter, and G is the mass flow of NaK.

1.5.2.4 AIR HEAT TRANSFER CORRELATION

The heat transfer correlation for air in the laminar and transition regimes flowing across heated tube bundles is based on results given in graphical form [6]. The graph actually contains five ϕ vs Re curves for various tube configurations, where

$$h = \phi \cdot \left(\frac{c_p \cdot G}{Pr^{2/3}} \right), \quad (1.5-61)$$

and c_p is heat capacity, G is mass velocity, Pr is the Prandtl number, and h is the heat transfer correlation, applicable below $Re = 6000$. As MINET can make minor adjustments through the heat transfer area correction factor, it was necessary only to approximate these curves as

$$\begin{aligned} \phi &= Re^{-0.535} - 0.022, & Re < 200 \\ \phi &= Re^{-0.66} + 0.0067, & Re > 200. \end{aligned} \quad (1.5-62)$$

For turbulent flow ($Re > 6000$) over banks of tubes or pipes, regardless of their configuration, experimental data agree well with [6]:

$$h = 0.33 k Re^{0.6} Pr^{0.3}/D. \quad (1.5-63)$$

Thus, the heat transfer coefficient for air in MINET is applicable from the laminar and through turbulent regimes, across banks of pipes or tubes.

1.5.3 FRICTION

The pressure change due to friction is given by the relation:

$$\Delta P_f = - \phi_{TP} \cdot f \cdot L \cdot G^2 / 2 \rho D_{eq} , \quad (1.5-64)$$

where f is the friction factor, ϕ_{TP} is the Thom two-phase multiplier (when applicable), L is length, G is mass velocity, ρ is density, and D_{eq} is the equivalent hydraulic diameter, given by:

$$D_{eq} = \frac{4 \cdot \text{flow area}}{\text{wetted perimeter}} \quad (1.5-65)$$

In the transition and turbulent regions, the following relation [28] is used

$$f = 0.0055 \left(1 + \left[20000 \cdot \epsilon + \frac{10^6}{Re} \right]^{1/3} \right) , \quad (1.5-66)$$

where ϵ is the relative roughness factor by Moody [21]. The roughness of various piping materials is given in Table 1.5-21. Relative roughness is determined by dividing the roughness by the diameter D . The friction factor for laminar flow is given by [21]:

$$f = \frac{64}{Re} . \quad (1.5-67)$$

The two-phase multiplier, ϕ_{TP} in Eq. (1.5-64) is a fitted function of data provided by Thom [29]:

$$\phi_{TP} = Y_i(x) \left(\frac{p}{P_i} \right)^q , \quad (1.5-68)$$

Table 1.5-21 Roughness $e(M)$ of Various Piping Materials

| Material | $e(M)$ |
|---------------------|--|
| Drawn Tubing | 1.5×10^{-6} |
| Commercial Steel | 4.6×10^{-5} |
| Wrought Iron | 4.6×10^{-5} |
| Asphalted Cast Iron | 1.2×10^{-4} |
| Galvanized Iron | 1.5×10^{-4} |
| Cast Iron | 2.6×10^{-4} |
| Concrete | 3×10^{-4} to 3×10^{-3} |
| Riveted Steel | 10^{-3} to 10^{-2} |

Note: Relative Roughness $\epsilon = \frac{e(M)}{\text{Diam}(M)}$

where $Y_i(x)$ is a 5 part fitted function (vs. quality):

$$Y_i(x) = \begin{cases} 1 + 101.35x - 3.5x^2 & , P = 1.72 \text{ MPa} \\ 1 + 37.86x - 0.56x^2 & , P = 4.14 \text{ MPa} \\ 1 + 13.852x + 0.478x^2 & , P = 8.62 \text{ MPa} \\ 1 + 4.704x + 0.96x^2 & , P = 14.5 \text{ MPa} \\ 1 + .5032x + 3.1898x^2 - 2.2129x^3 & , P = 20.7 \text{ MPa} \end{cases} \quad (1.5-69)$$

Parameter q is for interpolating or extrapolating from Eq. (1.5-69), and is defined as:

$$q = \frac{\ln(Y_{i+1}(x)/Y_i(x))}{\ln(P_{i+1}/P_i)} \quad (1.5-70)$$

Thus, if one wanted to calculate ϕ_{Tp} at $P = 3 \text{ MPa}$ and $x = 0.3$, he would calculate $Y_1 (= 31.1)$, $Y_2 (= 12.31)$, $q (= -1.06)$, and finally $\phi_{Tp} (= 17.25)$.

1.5.4 CRITICAL FLOW

Three critical flow models are available in MINET, Extended Henry-Fauske [4] for subcooled water, Moody [5], and isentropic for superheated steam. To minimize on storage and computations, functions fitted for use in the RETRAN-02 Code [9] were converted to SI units and used in MINET.

For the subcooled region, the critical mass velocity G ($\text{kg}/\text{M}^2/\text{sec}$) is given as a function of enthalpy E (J/kg) and pressure P (pa) by the fitted Extended Henry Fauske relation:

$$G^{\text{HF}} = \begin{cases} \sum_{j=0}^5 \sum_{i=0}^5 H1_{ij} E^i P^j & , P < 2.067858E6 \\ \sum_{j=0}^5 \sum_{i=0}^5 H2_{ij} E^i P^j & , P > 2.067858E6 \end{cases} \quad (1.5-71)$$

where the coefficients are as given in Tables 1.5-22 and 1.5-23.

In the two phase region, the critical mass velocity is given by the fitted Moody relation:

$$G^{\text{MDY}} = \begin{cases} \text{EXP} \sum_{j=0}^5 \sum_{i=0}^5 M1_{ij} E^i P^j & , P < 1.378572E6 \\ \sum_{j=0}^5 \sum_{i=0}^5 M2_{ij} E^i P^j & , P > 1.378572E6 \end{cases} \quad (1.5-72)$$

where the coefficients are a given in Tables 1.5-24 and 1.5-25.

To avoid discontinuities at the saturated fluid interface, the functions are interpolated as suggested in the RETRAN-02 [9] guide:

Table 1.5-22 Coefficients $H1_{ij}$ for Extended Henry-Fauske, Eq. 1.5-71

| i/j | 0 | 1 | 2 | 3 | 4 | 5 |
|-----|---------------|---------------|---------------|---------------|---------------|---------------|
| 0 | 5.844785E+4 | -1.817882E-1 | -1.146214E-5 | 2.11432E-11 | -1.253541E-17 | 2.429848E-24 |
| 1 | -6.144985E-1 | 1.233208E-5 | 7.7054E-11 | -1.659309E-16 | 1.028924E-22 | -2.037626E-29 |
| 2 | 1.181158E-6 | -7.884145E-11 | -1.769177E-16 | 4.955322E-22 | -3.26443E-28 | 6.643456E-35 |
| 3 | 3.746133E-12 | 1.958905E-16 | 1.271247E-22 | -6.810723E-28 | 4.913027E-34 | -1.037707E-40 |
| 4 | -1.432334E-17 | -2.069124E-22 | 4.757484E-29 | 4.142854E-34 | -3.460373E-40 | 7.697998E-47 |
| 5 | 1.161263E-23 | 7.472281E-29 | -6.2246E-35 | -8.333039E-41 | 9.032233E-47 | -2.161096E-53 |

Table 1.5-23 Coefficients $H2_{ij}$ for Extended Henry-Fauske, Eq. 1.5-71

| i/j | 0 | 1 | 2 | 3 | 4 | 5 |
|-----|---------------|---------------|---------------|---------------|---------------|---------------|
| 0 | 5.857132E+4 | 2.380976E-2 | -3.550971E-9 | 4.076189E-16 | -2.256098E-23 | 4.214328E-31 |
| 1 | -1.396223E-1 | -6.599120E-8 | 2.157757E-14 | -2.772089E-21 | 1.56244E-28 | -2.957623E-36 |
| 2 | 2.303321E-7 | 2.360698E-13 | -6.773429E-20 | 7.950999E-27 | -4.247985E-34 | 7.890548E-42 |
| 3 | -1.710519E-13 | -3.246034E-19 | 8.518386E-26 | -9.341207E-33 | 4.798508E-40 | -8.778709E-48 |
| 4 | -8.882528E-20 | 2.38065E-25 | -5.45305E-32 | 5.424395E-39 | -2.610384E-46 | 4.617507E-54 |
| 5 | 5.478637E-26 | -6.687134E-32 | 1.416759E-38 | -1.30096E-45 | 5.822964E-53 | -9.827271E-61 |

Table 1.5-24 Coefficients M_{ij} for Moody, Eq. 1.5-72

| i/j | 0 | 1 | 2 | 3 | 4 | 5 |
|-----|---------------|---------------|---------------|---------------|---------------|---------------|
| 0 | 9.1254883 | 7.055917E-5 | -2.958198E-10 | 5.573495E-16 | -4.648165E-22 | 1.384205E-28 |
| 1 | -1.175828E-5 | -1.570065E-10 | 8.163449E-16 | -1.646365E-21 | 1.415426E-27 | -4.282857E-34 |
| 2 | 1.423839E-11 | 1.775119E-16 | -1.007318E-21 | 2.080396E-27 | -1.804020E-33 | 5.478421E-40 |
| 3 | -9.215581E-18 | -9.760617E-23 | 5.979624E-28 | -1.259719E-33 | 1.100075E-39 | -3.350315E-46 |
| 4 | 2.914638E-24 | 2.601702E-29 | -1.710693E-34 | 3.666980E-40 | -3.221719E-46 | 9.835850E-53 |
| 5 | -3.550224E-31 | -2.692578E-36 | 1.893676E-41 | -4.122780E-47 | 3.641617E-53 | -1.114157E-59 |

Table 1.5-25 Coefficients M_{ij}^2 for Moody, Eq. 1.5-72

| i/j | 0 | 1 | 2 | 3 | 4 | 5 |
|-----|---------------|---------------|---------------|---------------|---------------|---------------|
| 0 | 3.153195E-4 | 1.113838E-1 | -1.654592E-8 | -2.197688E-16 | 1.339861E-22 | -6.026818E-30 |
| 1 | -1.246415E-1 | -2.331657E-7 | 4.931444E-14 | -1.200296E-21 | -2.120770E-28 | 1.193308E-35 |
| 2 | 1.718246E-7 | 1.945935E-13 | -5.237650E-20 | 2.346933E-27 | 1.210697E-34 | -9.446506E-42 |
| 3 | -1.085987E-13 | -7.786264E-20 | 2.584825E-26 | -1.495814E-33 | -2.888144E-41 | 3.767468E-48 |
| 4 | 3.223748E-20 | 1.459423E-26 | -6.038175E-33 | 4.046313E-40 | 2.186939E-48 | -7.642817E-55 |
| 5 | -3.647161E-27 | -9.886719E-34 | 5.388276E-40 | -3.976274E-47 | 5.537702E-56 | 6.371815E-62 |

$$G_{\text{crit}} = \begin{cases} G^{\text{HF}} & , \quad E < ES \\ (1-\gamma) \cdot G^{\text{HF}} + \gamma \cdot G^{\text{MDY}} & , \quad ES < E < EF \\ G^{\text{MDY}} & , \quad E > EF \end{cases} \quad (1.5-73)$$

where

$$\gamma = \frac{E - ES}{EF - ES} \quad (1.5-74)$$

and

$$ES = \sum_{n=0}^8 A_n p^n \quad (1.5-75)$$

where A_n are as shown in Table 1.5-26.

Table 1.5-26 Coefficients A_n for Eq. 1.5-75

| n | A_n |
|-----|---------------|
| 0 | 3.964721E5 |
| 1 | 0.4987001 |
| 2 | -2.254622E-7 |
| 3 | 6.337852E-14 |
| 4 | -1.039562E-20 |
| 5 | 1.010939E-27 |
| 6 | -5.735412E-35 |
| 7 | 1.735412E-42 |
| 8 | -2.222367E-50 |

In the superheated region, the classic isentropic approach is used. Thus, the critical mass velocity is given by:

$$G_{\text{crit}} = \sqrt{-\left(\frac{\partial P}{\partial v}\right)_{S_0}} \quad (1.5-76)$$

where the derivative is for pressure with respect to specific volume at constant entropy.

1.5.5 STRUCTURE PROPERTIES

Density (kg/M^3), thermal conductivity ($\text{J}/(\text{sec}\cdot\text{M}\cdot\text{K})$), and specific heat ($\text{J}/\text{kg}/\text{K}$) are available in MINET for 10 common structural materials [30]. Values are provided in Tables 1.5-27 through 1.5-29. The specific heat for stainless steel is

$$C_p = 380.962 + 0.535104 \cdot T - 6.10413\text{E-}4 \cdot T^2 + 3.02469\text{E-}7 \cdot T^3. \quad (1.5-77)$$

Table 1.5-27 Conductivity of Structural Materials

| No. | Type | k ($\text{J}/(\text{sec} \cdot \text{M} \cdot \text{K})$) |
|-----|------------------|--|
| 1 | Stainless Steel | $9.01748 + .0162997 \cdot T - 4.80329\text{E-}6 \cdot T^2 + 2.18422\text{E-}9 \cdot T^3$ |
| 2 | 2 1/4 Chrom-Moly | $49.341695 - 0.0171228 \cdot T$ |
| 3 | Admiralty Metal | 146.01 |
| 4 | 90 - 10 Cu-Ni | 84.24 |
| 5 | 80 - 20 Cu-Ni | 51.48 |
| 6 | 70 - 30 Cu-Ni | 40.25 |
| 7 | Monel | 29.58 |
| 8 | Inconel | 18.72 |
| 9 | Carbon Steel | 59.9 |
| 10 | Aluminum | 179.71 |

Table 1.5-28 Specific Heat of Structural Materials

| No. | Type | C_p/C_p , Steel (-) |
|-----|------------------|-----------------------|
| 1 | Stainless Steel | 1.0 |
| 2 | 2 1/4 Chrom-Moly | 1.0 |
| 3 | Admiralty Metal | 0.84 |
| 4 | 90 - 10 Cu-Ni | 0.85 |
| 5 | 80 - 20 Cu-Ni | 0.86 |
| 6 | 70 - 30 Cu-Ni | 0.87 |
| 7 | Monel | 0.93 |
| 8 | Inconel | 0.96 |
| 9 | Carbon Steel | 1.0 |
| 10 | Aluminum | 1.95 |

Table 1.5-29 Density of Structural Materials

| No. | Type | ρ (KG/M ³) |
|-----|------------------|-----------------------------|
| 1 | Stainless Steel | 7849.8 |
| 2 | 2 1/4 Chrom-Moly | 7833.35 |
| 3 | Admiralty Metal | 8490.6 |
| 4 | 90 - 10 Cu-Ni | 8971.2 |
| 5 | 80 - 20 Cu-Ni | 9211.5 |
| 6 | 70 - 30 Cu-Ni | 9451.8 |
| 7 | Monel | 8811.0 |
| 8 | Inconel | 8330.4 |
| 9 | Carbon Steel | 7849.8 |
| 10 | Aluminum | 2723.4 |

1.6 CONTROL SYSTEM MODELS

Models for a generic control system representation are under development.

2. USERS GUIDE

In this section, the essential information needed for running the MINET code is provided. Other portions of this MINET documentation will provide important information, which could prove useful in setting up and testing your input deck. In employing the MINET code, the user should keep a few points in mind.

- 1) MINET is a developmental computer code and unexpected results may occur, although these will continually decrease in frequency. A serious problem should always be reported to the code developers so it can be corrected on a permanent basis.
- 2) MINET is written on two levels, the module level and the working level. The user will find that investigating the valve module, for instance, is relatively easy, as that portion of the code is easy to identify and read. Modification of such a model is quite feasible, in many cases. On the other hand, the working level of MINET is very sophisticated and should be avoided by the user. Fortunately, the working levels have been well tested, where as, at the module level, user options are continually being added and modified.
- 3) There is a negative aspect to the freedom provided the user in simulating a system using MINET, or any other generalized system code. That is, as long as the system described does not violate physical laws, MINET will analyze the case as stated by the user. Thus, if the user incorrectly states the problem, MINET will attempt (and often succeed) to solve the stated problem as is. As a result, what appears to be the wrong answer may, instead, be the right answer to the wrong question.

2.1 MACHINE AND STORAGE CONSIDERATIONS

The MINET code was designed, developed, and tested with the goal of minimizing machine dependencies and storage requirements, so as to facilitate its implementation on any medium to large scale high-speed computer. As a result, one may expect only minor difficulties in adapting MINET to a given computer (with the possible exceptions discussed in [24]).

MINET was developed and tested on a CDC 7600 computer, and was designed to execute in small core memory (SCM). Thus, the code has been routinely executed using 160,000 octal (around 57,000 base ten) 60-bit words of SCM. (For an extremely large test problem, one of the large arrays was transferred into large core memory (LCM), a fairly simple process that slows execution speed by 10-20%.) In order to use SCM, MINET is segmented, i.e., subdivided into computational modules that swing in and out of SCM as needed. The segmentation tree currently used is shown in Figure 2.1-1. For many of the larger computers, such steps to segment the code and otherwise limit the use of core space will most likely be unnecessary.

For a machine using a 32-bit word, the use of double precision is required for at least part of the code. This has not proved to be a problem, thus far.

MINET currently uses seven input/output device numbers, as shown in Table 2.1-1. It should be noted that these unit numbers are assigned at a high logical level and can be re-assigned with little difficulty. When MINET is interfaced with another host code, the host can set the I/O device numbers so as to avoid conflicts with its current usages of the devices.

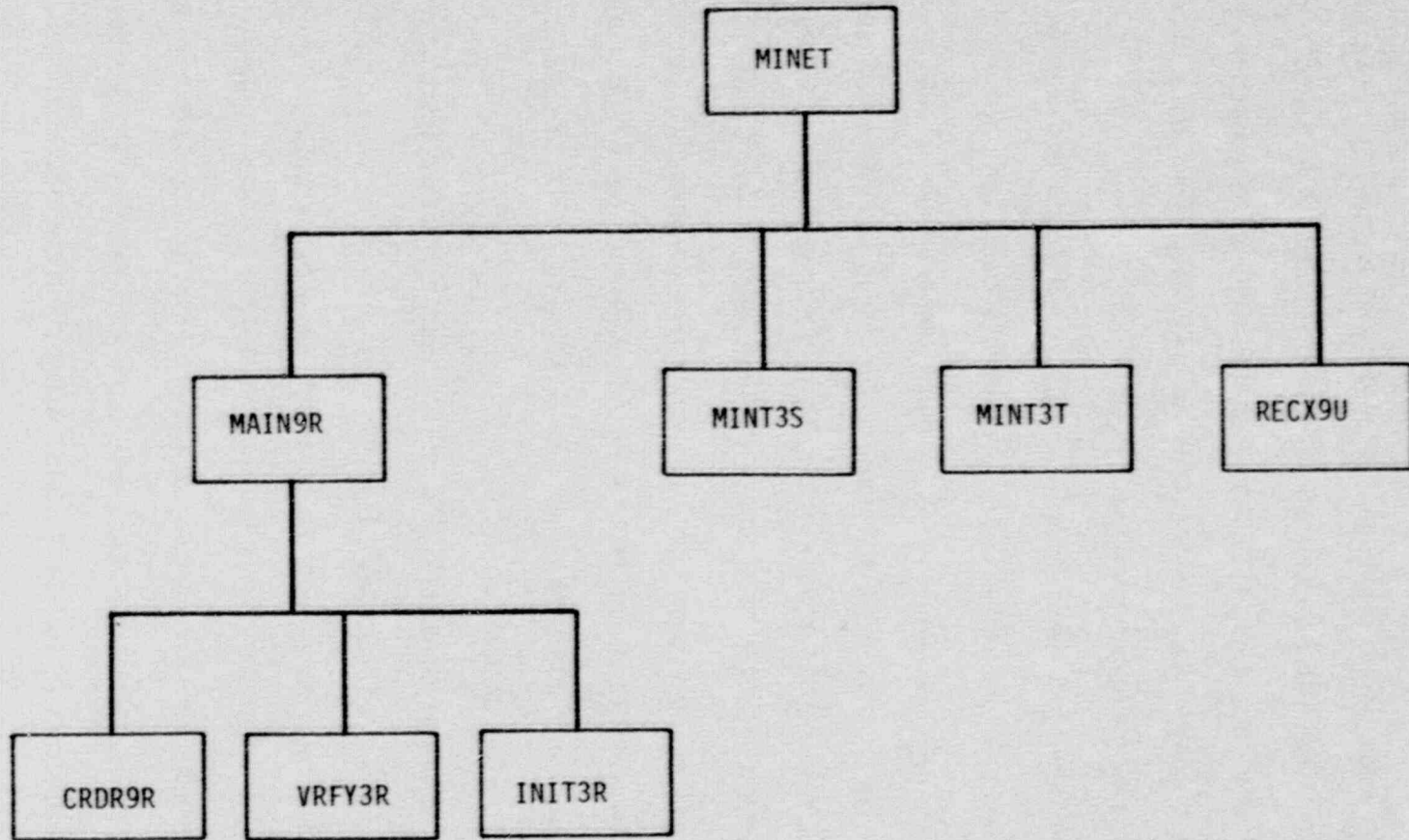


Figure 2.1-1. Current Segmentation for CDC-7600 Use

Table 2.1-1 Current I/O Device # Utilization

| <u>Device No.</u> | <u>Current Usage</u> |
|-------------------|--|
| 5 | Input Deck, i.e., Card Images |
| 6 | Formatted Print Out, e.g., from PRNT3C |
| 7 | Scratch Area (Reduces Storage) |
| 8 | Scratch Area (Reduces Storage) |
| 9 | Transaction Output, e.g., Plot Data |
| 10 | Save, i.e., Info. for Re-Start |
| 11 | Restore, i.e., Info. for Re-Start |

2.2 BUILDING AN INPUT DECK

Building a MINET Input Deck is relatively simple for a small system, and quite manageable even for a large and intricate system. An operating system is a little easier to represent than a hypothetical system, because one is less likely to attempt to create non-physical conditions, i.e., it is more fool-proof.

2.2.1 THE SYSTEM

Power plant thermal-hydraulic systems can be almost infinitely large and complex, particularly if one includes all the auxiliary and clean-up systems. Experimental configurations can be very simple. Both extremes may be represented using MINET, if a few basic rules are followed.

System boundaries must be chosen so that a reasonably accurate set of transient boundary conditions can be specified. An ideal boundary condition would be the pressure outside a relief valve, e.g., atmospheric pressure. A low, or a very predictable flow rate into a large tank is also a desirable boundary condition.

One MUST INCLUDE AT LEAST ONE INLET AND ONE OUTLET BOUNDARY IN EACH FLUID NETWORK. MINET needs these for reference. For a closed loop one should open it slightly by adding tightly closed (e.g. 10^{-6} relative) valves to boundaries. While this may seem a nuisance in isolated cases, it is a convention that allows MINET to do the generalized steady state solution that is missing from many other systems codes.

A fairly common component is a "separator" or tank where water occupies the lower portion with steam above, which is called a "separated volume" in MINET terminology. Under these conditions any flow leaving the volume will be either saturated or a mixture of saturated liquid and steam, as determined by the water level at the pipe entrance. This introduces the subtle fact that the sum of the flows entering the volume must have a certain flow energy ($W \cdot E$) for the system to be at equilibrium. To assure this, MINET will need a source of energy to adjust (see Section 1.3.1). The user should make certain that for each separated volume, there is a source of heating somewhere upstream, or the problem will effectively be overconstrained.

A situation similar to the separated volume comes up when the user fixes the temperature at an outlet boundary module. Again, if the user makes this constraint, a source of heating must be available for adjustment.

Of the MINET component modules, usages are relatively straightforward, particularly for the pipes. The valves and pumps are simply one node pipes, plus an extra term in the momentum equation due to a loss across the valve opening or a gain due to the pumping action. An optional choke flow calculation can be performed for the valve, and should be for valves to atmosphere. The heat exchanger simply represents the active heat transfer area, and other modules should be used for plena, downcomers, or separators. The turbine stage module is a simple in/out module, and should be used for parts of the turbine when accounting for extraction lines to the feedwater heaters. That is, for a turbine with an extraction line from the center, use two turbine stage modules with a volume in between, from which the extraction line is run off.

Usage of the volume for a tank or a point where multiple lines diverge or merge, e.g., a tee, is fairly obvious. What is subtle is the need to use a volume because of its dynamically calculated pressure. Any module that has a large (> 25% relative) pressure drop should be bracketed by volumes and/or boundaries. This is always true for turbine stages and valves where choking is expected. It can also be true for a large pump or valve, but need not be so for all valves or pumps. In the use of MINET, a major factor in the speed and accuracy of the calculations is the correct and optimum usage of the volume modules (and the heat exchanger nodalization, as well).

2.2.2 SYSTEM SCHEMATIC

At this stage the system to be represented should be drawn schematically using the basic MINET components. Module IDs should be attached, preferably using a "naming" convention such as the ones illustrated in Section 4. Each port of each module should be assigned a number. Elevations should be noted at each module interface.

It is highly recommended that photo-copies be made of the system schematic. They are very useful in interpreting MINET output, and are needed when extracting and piecing together information from common block dumps, which are automatically produced following an unexpected job termination (see Section 2.6).

2.2.3 INPUT DECK

This section provides a description of the input file, and will be updated from time to time. In the next section, a computer generated input description is provided, and it is likely to be updated more frequently.

The structure of the MINET input is drawn on the same modular lines as that which dominates the calculational portion of the code. The basic component of the input is the input record or card-image record. The entire sequence of input records constitutes the input file.

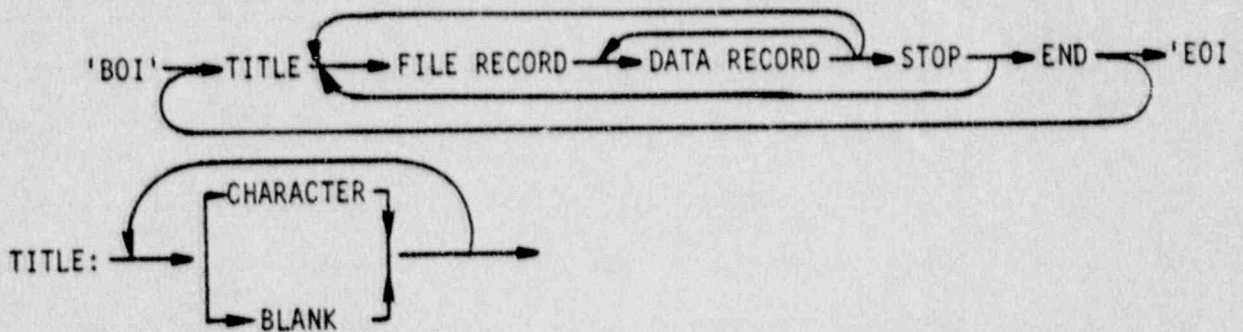
Input is processed by MINET in a three-fold operation. The interpreter, built around a version of the GENRD [31] processor, makes the initial pass over the input. Verification follows, checking for consistency within the data set and against the criteria detailed in the data dictionary. An inconsistency at this point causes the program to enter an error mode and generates a diagnostic message on the output file. The program is terminated at the end of this stage if any error has been detected. As a further check, all card-images are entered on the output file as they are interpreted, as are all decoded values assigned to all parameters.

With the verification complete, the third processor proceeds to initialize a series of internal parameters on the basis of the defined input. The steady state calculations are then initiated.

The list of input required to initialize MINET consists of a series of free-format card-image records. These records contain control specifications and/or data in columns 1 through 72. The record format is 'free' in the sense that as long as the sequence of data conforms to the ordering detailed in this

document, the physical placement of data fields as well as their degree of numerical accuracy is determined solely by the user.

A very rudimentary pseudo-grammar forms the basis on which the MINET input is constructed. The overall scheme in which this grammar operates is described in Figure 2.2-1. Its syntax is defined as follows:



TITLE:

A title will appear as part of the banner heading on major pages of the output file. It is limited to one record's length but may extend beyond the seventy-two (72) character limit to eighty (80) characters. Although a required portion of the input, this record is provided solely as a means of associating an input with the resulting calculation. The user may choose any degree of functionality desired to assign to the titles, since it is not otherwise processed.

```

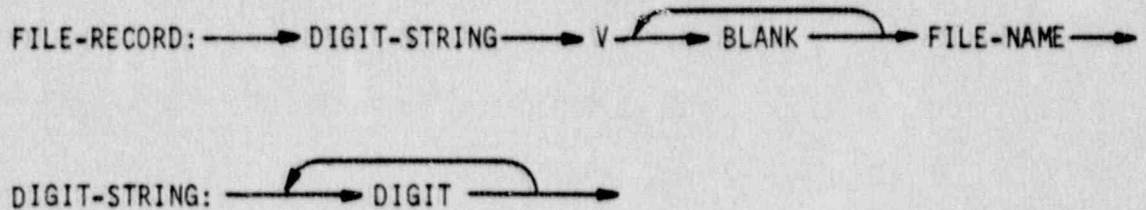
BEGIN
  GET NEXT-RECORD
  WHILE NEXT-RECORD IS NOT 'EOI' DO
    PROCESS TITLE
    GET NEXT-RECORD
    WHILE NEXT-RECORD IS NOT 'END" DO
      WHILE NEXT-RECORD IS NOT 'STOP" DO
        IF NEXT-RECORD IS FILE-RECORD
          THEN
            CLOSE PREVIOUSLY OPENED DATA FILE (IF OPENED FILE EXISTS)
            OPEN NEW DATA FILE
            GET NEXT-RECORD
          ELSE
            IF NEXT-RECORD IS DATA-RECORD
              THEN
                PROCESS DATA
                GET NEXT-RECORD
              ELSE
                ERROR CONDITION
                GET NEXT-RECORD
            END
            INITIATE PROCESSING (TO EXTENT SPECIFIED)
            GET NEXT-RECORD
          END
        END
      END
    END-STOP
  END

```

Figure 2.2-1 Psuedo-Grammer Format of MINET Input File

FILE RECORD:

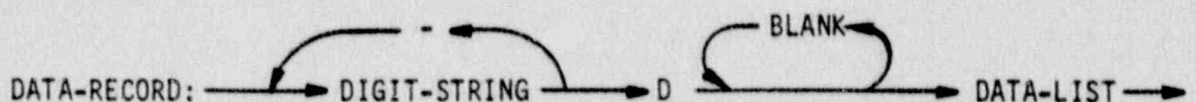
To open a data file, the following pseudo-grammar is appropriate:



The numeric sequence accumulated in this field is used to identify differing versions (V) of similar input files. It is provided as a convenience and is subsequently ignored by the processor. The FILE-NAME provides an associative link between the data of the accompanying data file and a particular computational module(s).

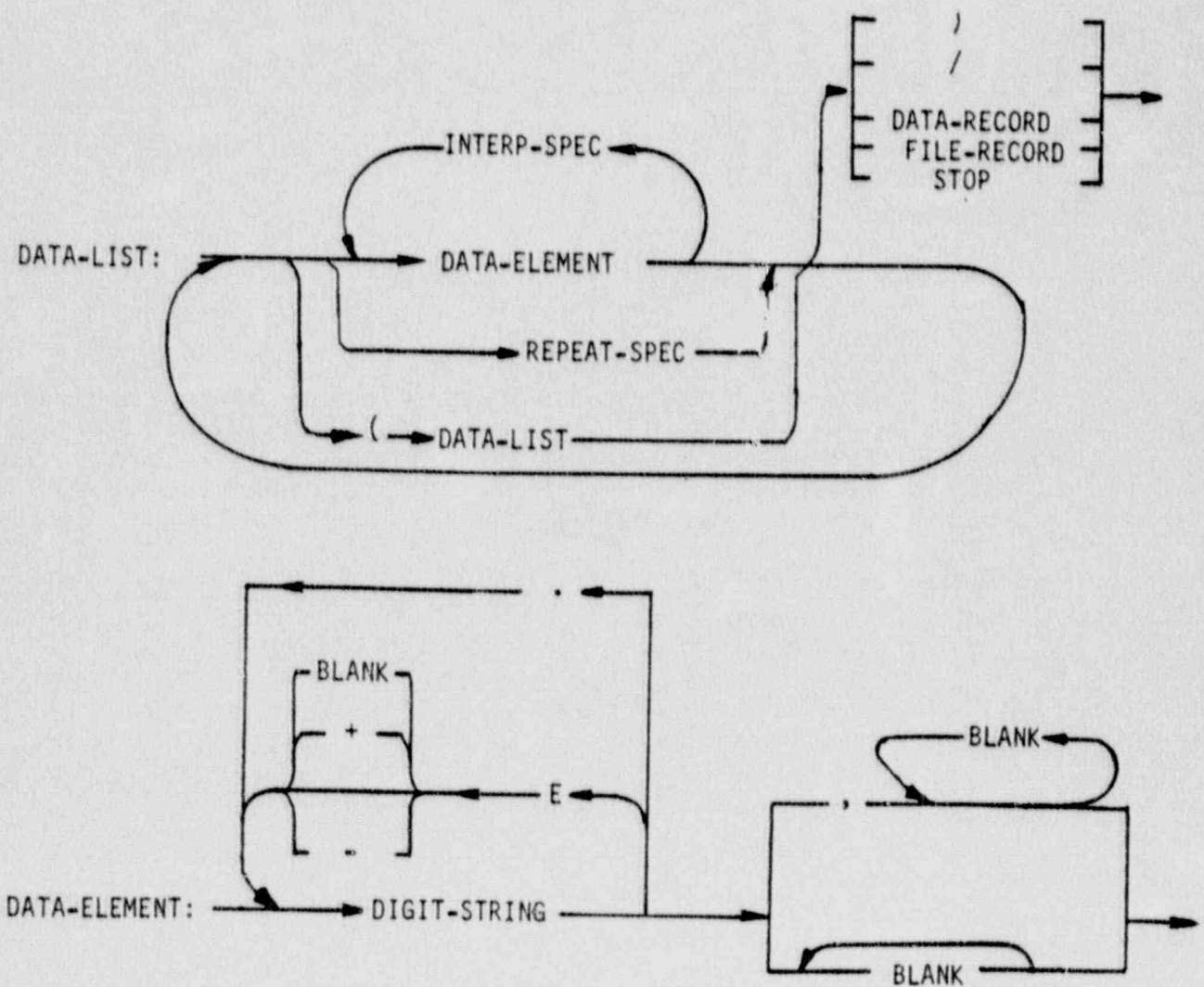
DATA RECORD:

The pseudo-grammar for an individual DATA-RECORD is:



For a DATA-RECORD to be properly processed, its DIGIT-STRING (or strings) must be among the set of defined record numbers of the corresponding data file. A list of all valid record numbers can be found later in this section.

A DATA-RECORD is completely processed before the next record is interpreted. A DATA-RECORD is implicitly defined to have a maximum length equal to one or more card-images (72 characters). It is terminated either by a slash (/) or by a column seventy-two (72) preceeding a DATA-RECORD, a FILE-RECORD or a STOP, as described below. Information following a slash (/) is not processed, nor is any information beyond column seventy-two (72). As a result, the user may find this to be a convenient place to annotate the data files. Within a given data partition, several options are available as described below:



Two shorthand constructs are provided for the specification of input.

The

INTERP-SPEC: \longrightarrow DIGIT-STRING \longrightarrow 'I'

and the

REPEAT-SPEC: \longrightarrow DIGIT-STRING \longrightarrow 'R'

Both are used to assign numeric data to consecutive memory locations. The REPEAT-SPEC stores a sequence of one or more constants. For example:

7.2, 3R

is equivalent to

7.2, 7.2, 7.2

and

(1.0, 15, 0.72), 4R

is equivalent to

1.0, 15, 0.72, 1.0, 15, 0.72, 1.0, 15, 0.72, 1.0, 15, 0.72

The 'I' specification provides a means of inserting one or more equally spaced values between two real (or two integer) end points. For example,

11, 7I, 19

is equivalent to

11, 12, 13, 14, 15, 16, 17, 18, 19

and

1.0, 3I, 2.0

is equivalent to

1.0, 1.25, 1.50, 1.75, 2.0

The integer preceding the 'I' specifies the number of equally spaced values to be inserted between the end points. The terminal points bound the sequence and are not strictly considered to be members of it, therefore, 11, 7I, 19 and not 11, 9I, 19 and 1.0, 3I, 2.0 and 1.0, 5I, 2.0 in the preceding examples. A check is made to determine the data type (real or integer) of the end points. Both points must be of the same type. If an integer interpolation is indicated, the resulting increment must also be of integer type.

2.2.3.1 INPUT RECORD DESCRIPTION (See Also Sec. 2.2.3.2)

Record 1D - Pipe Geometric Record

The first three parameters, pipe ID, inlet port number, and outlet port number are assigned by the user, to be used in communicating with MINET. The pipe length and diameter (inner) are self explanatory. The roughness factor is the ratio of the width of surface roughness over the pipe diameter, and typically runs from 10^{-3} for a small commercial grade tube to 5×10^{-6} for a very large drawn tube (pipe) (see Table 2.2-1). Any number of nodes may be used per pipe, and fluid transport time should be a principal factor in the choosing. The path parameter indicates how many identical components are being represented, and the total flow will be divided equally between the paths for determining pressure losses, etc.

Record 101D - Valve Geometric Record

The first several parameters for the valve geometric record are the same as for the pipe record, except only one node can be used for a valve. The maximum flow area through the valve when fully open is likely to be slightly less than the pipe flow area, if it is unknown. As a zero flow rate causes

Table 2.2-1 Roughness $e(M)$ of Various Piping Materials

| <u>Material</u> | <u>$e(M)$</u> |
|---------------------|--|
| Drawn Tubing | 1.5×10^{-6} |
| Commercial Steel | 4.6×10^{-5} |
| Wrought Iron | 4.6×10^{-5} |
| Asphalted Cast Iron | 1.2×10^{-4} |
| Galvanized Iron | 1.5×10^{-4} |
| Cast Iron | 2.6×10^{-4} |
| Concrete | 3×10^{-4} to 3×10^{-3} |
| Riveted Steel | 10^{-3} to 10^{-2} |

Note: Relative Roughness $\epsilon = \frac{e(M)}{\text{Diam}(M)}$

severe computational difficulties (less than or greater than is no problem), one should never close a valve beyond a minimum leakage level as given by the minimum stem position (recommended 10^{-6}). Finally the relation between the relative flow area and relative stem position will vary from valve to valve, with the general relation given by

$$A = S^f, \quad (2.2-1)$$

where f is the stem power factor, a user input. A value of 1.0 is usually a good estimate, although knowledge of valve design would facilitate a better guess.

Record 201D - Pump Geometric Record

The parameters for the pump geometric record are the same as for the pipe. Again, only one node may be used for the pump.

Record 301D - Heat Exchanger Geometric Record

The first several parameters are again the same as on the pipe geometric record, although several additional parameters are needed in this case. The inlet and outlet ID for the flowpath outside the tubes are again user assigned names for communication only. The outer diameter refers to the tube between the fluids. Pitch to diameter refers to the ratio of the tube center to center spacing over the tube outer diameter, and should be set to the ratio of the inner diameter of the outer tube to the outer diameter of the inner tube for the rare case of co-axial tubes. The number of tubes is per heat exchanger, and is multiplied (in MINET) by the number of paths in determining the flow per path. Ten structural materials are currently in the MINET library, and modifications and/or additions should require minimal effort. Tube configurations such as co-axial (1), square (4), and hex (6) (also called

triangular) are available as options, and alternate configurations could be substituted by modifying subroutine MODL3C. The helical coil heat exchanger diameter refers to coil (not tube) diameter, is used in modifying the frictional loss, and should be set to zero for a straight tubed unit. Fluid passing through tubes coiled or otherwise curved through a tank, travel farther than the tank fluid, and the ratio is input, and is again 1.0 for straight tubes. A core tube, albeit rare, can be inserted inside a heat exchanger tube to increase the (annular) velocity of the inner fluid. The diameter of such a tube is used to modify the flow area and account for heat storage, and it should be set to zero if there is no core tube. The mass and surface area of the heat exchanger structure, summed over all parallel units, is used to calculate heat storage in the transient.

Record 401D - Inlet Boundary Module Geometric Record

Only the boundary module ID number and an outlet port number need to be input. Essentially the user is controlling the inlet port, and need not assign it a number.

Record 402D - Outlet Boundary Module Geometric Record

Only the boundary module ID number and an inlet port number need to be output. Again, the user is controlling the other port, i.e., the outlet.

Record 501D - Volume Geometric Record

The volume ID is input on this record, but the port identification numbers appear on other cards because their count is not generally known. The shape parameter is really important only if the contents are separated, in which case the level fraction vs. volume fraction relation must be known. The user

should set the parameter to one if the horizontal area does not depend on height, to two if the component is a drum on its side, and contact the code developers for assistance otherwise. It is possible to represent a tank using more than one volume module (plus pipes), and this impacts some of the remaining input parameters. The volume of the volume is the space in the component represented by the MINET volume module. Volume height refers to the total height of the physical component, and is used so that the relative water level is referenced to the whole component volume and not just that portion represented by the module. The minimum and maximum relative levels are the MINET module bottom and top values relative to the component dimensions, e.g., 0.5 and 1.0 for a module representing the top half of a tank. The volume elevation is the vertical midpoint for the physical component. The path parameter is as it was for the pipes. The separation parameter is set to 1 for homogeneous (usual), 2 for separated, and 3 for homogeneous at steady state but could become separated during the transient. The third option should be chosen only if the contents will be entirely liquid or vapor under steady state conditions.

Record 511D - Volume Inlet Port Geometric Record

The volume module ID number and an ID number for an incoming port are specified. An inlet port is one through which fluid is entering the volume under steady state conditions.

Record 512D - Volume Outlet Port Geometric Record

The volume module ID number and an ID number for an outgoing port are specified. An outlet port is one through which fluid is leaving the volume under steady state conditions.

Record 601D - Turbine Stage Geometric Record

The turbine stage module ID number, and identifier numbers for the inlet and outlet ports are specified. The absolute angle of approach of steam with respect to the blades is also needed, but this number is very likely to be close to 15.0 (degrees), and an extensive search to determine a better value is unlikely to be necessary.

Record 801D - Network Geometric Record

The system is composed of one or more fluid networks, which are connected only by heat exchangers. On this record the fluid type for a given network is specified. As the network has no identifier number, the user need only specify any boundary or volume module in the network on this record. Note there will only be enough of these records input to assign a fluid type to each network.

Record 901D - Junction Record

This record is used to specify the elevation of a junction, and the modules and ports to be connected. One must be careful when connecting to a volume with separated contents that the junction is located dimensionally within the volume and not some computer round-off error (e.g., 10^{-14}) outside. Otherwise, unexpected results can occur when the tank runs dry or full.

Record 1001D - Pipe Performance Record

On this OPTIONAL record, the pipe identifier number and a form loss coefficient are input. Generally, one should assume a value of zero (the default), unless a better value is known or some adjustment is needed to obtain user desired steady state flows and pressures.

Record 1101D - Valve Performance Record

Again, the valve module identification number and form loss coefficient for the pipe-like portion are input. The valve form loss coefficient, for the gate opening, would typically be 0.5 to 1.0 for a simple valve, but could be much larger (i.e., greater than 1.0) for a series or group of valves represented as one. The choking parameter is used to specify whether a choke flow calculation should be done, in which case the valve should be in a (one-node) segment by itself. The last five parameters are a mini-control system useful in simulating the action of safety/relief or check valves. The J3VPRS parameter is the key, for if it is negative, the option is declined, and the last four parameters are meaningless and can be set to 0.0. If J3VPRS = 0, for a check valve, the next four parameters are: 1) the flow (per valve) below which trips closed (e.g., 0.0); 2) the time constant for doing so; 3) the flow above which it will trip back open (e.g., 0.1) and 4) the time constant for doing so. If J3VPRS is positive, it indicates a volume identification number where the pressure is being monitored. In this case the trip levels are for the pressure at which it trips open, and the pressure at which it trips closed.

Record 1201D - Pump Performance Record

The first two parameters are the pump module identification number and the form loss coefficient for the pipe-like portion. The next three parameters, as well as the five values of A3PUMP, indicate the pump head as a function of flow (per pump) and pump speed. For each pump there will be some reference or rated head at some reference speed and flow rate. The polynomial coefficients A indicate the relative head vs relative flow at the reference speed. Typically, the relative head will be about 1.2 at zero flow, 1.0 at 1.0 relative

flow, around 0.7 at 2.0 relative flow, and fall to zero around 3.0 relative flow. The last two parameters on this input record are used to coastdown the pump after a trip, with the first being a time constant and the second is the period until the pump rotor locks, i.e., stops moving entirely.

1301D - Heat Exchanger Performance Record

The first three entries on this record are the module identification number, and form loss coefficients for inside and outside the tubes, the latter of which can be large due to support structure. The level type parameters specify the critical heat flux (CHF) criterion, an index of 1 being an Atomic International correlation for sodium to water heat exchangers, 2 being MacBeth for PWR steam generators, and 3 being a quality of 0.75. If CHF is not expected, specify option 3, as it is more efficient to execute than the others. The counter/cross/parallel flow multiplier should be set to -1.0 for counter flow, 0.0 for cross flow, and 1.0 for parallel flow condition.

1601D - Turbine Performance Record

The turbine module ID is the first entry on this card, which actually more fully describes the turbine than the geometric card does, as the MINET turbine model is based on known performance rather than geometrical details. The stage type may be specified as an impulse type (generally only for the first stage) or the impulse reaction type (the rest). The efficiency of the generator is not currently a very significant parameter, and should be set to around 0.95. The next five parameters are used to make inferences about the pressure change across the turbine stage, and can be estimated easily from a plant design conditions diagram. The inlet temperature is the only tricky parameter, and that should be set at least a couple of degrees (K) above the

saturation temperature for the inlet pressure, if it is not known precisely. The last two parameters on this record are as they were for the pump in record 1201D.

2001D - Pipe Initial Condition Record

This optional record is used if the pipe is receiving a non-zero heat addition (0 = default). The module identification number and the total heat input over all parallel pipes are input.

2101D - Valve Initial Condition Record

The valve module identification number and total heating over all parallel valves represented are the first two entries on this card. The remaining entry is the initial valve stem position, which should be between the minimum valve stem position (record 101D) and full open, i.e., 1.0.

2201D - Pump Initial Condition Record

Again, the first two parameters are the pump module identification number and the heat input for all the parallel pumps being represented. The remaining parameter is the pump speed in revolutions per minute (RPM).

2301D - Heat Exchanger Initial Condition Record

The first parameter is the heat exchanger module identification number. The second parameter is the amount of heat being transferred from the fluid passing outside the tubes to the fluid within, and is the sum over all parallel heat exchanger paths.

2401D - Boundary Module Initial Condition Record

The boundary module identification number is the first entry. The boundary status options are 0 for an inlet boundary, 1 for an outlet boundary where MINET calculates the temperature, and 2 for an outlet boundary where the temperature is fixed by input (on this card). The next parameter indicates whether the enthalpy type input is actually an enthalpy (1), a temperature (2), or a quality (3). Note that a temperature boundary condition may be easier to determine, but is dangerous if it is close to the saturation temperature. The enthalpy type parameter is next, followed by the initial flow and pressure. MINET will use the flow and enthalpy for an incoming boundary and the pressure and perhaps (on status) enthalpy for an outlet boundary. The unused parameter may be used as an initial guess, so a reasonable value should be input.

2501D - Volume Initial Condition Record

Once again, the first two parameters are the module identification number and the total heating for all the volumes being represented. The third parameter is the initial water level in a separated homogeneous volume. The remaining parameter is an estimate of the initial pressure in the volume.

2511D - Volume Outlet Port Initial Condition Record

The first two parameters are module and port identification numbers. The remaining parameter is the estimated flow leaving through the volume port, and is the sum over all parallel volumes being represented as one.

2601D - Turbine Stage Initial Condition Record

The first parameter input is the turbine module identification number, which is followed by the initial turbine speed in RPM. The third parameter is the work done on the turbine stage (expressed in J/S), e.g., -1.0E8 J/S.

3011D - Pipe Heat Input Table Record

This is an optional record, with the default being that the pipe heating is maintained at the initial value. The first parameter is the module identification number. The remaining parameters are pairs of time and heating entries which are placed into a table and interpolated to determine pipe heating at any point in time.

3111D - Valve Heat Input Table Record

This record exactly parallels record 3011D.

3121D - Valve Position Table Record

This, again, is an optional record. If it is not included, either the steady state position will be maintained, or the safety/relief or check valve control option will be used. The first entry is the valve module identification number, which is followed by paired data points that are used to create a position vs. time table.

3201D - Pump Transient Record

This record can be used to trip a pump at a given point in time. The entries are the module identification number and the trip time. Note, that if the user does not want the pump to trip, the trip time can be set to an arbitrarily large value.

3211D - Pump Heat Input Table Record

This record exactly parallels Record 3011D.

3221D - Pump Speed Table Record

This is another optional record, which may be omitted if the steady state speed is to be maintained until the trip time, as set in Record 3201D. If used, the record contains the module identification record, and pairs of time and pump speed table entries.

3411D - Boundary Condition Table Record

The first parameter is again the module identification number. Pressure or flow may be input, as indicated by the second parameter, 1 for flow, 2 for pressure. Again, a temperature or quality can be input instead of enthalpy, as keyed by the third parameter. The remaining fields, in groups of three, are time, enthalpy/temperature/quality, and flow/pressure to be used in tabular form.

3511D - Volume Heat Input Table Record

This record exactly parallels Record 3011D.

3601D - Turbine Trip Record

The turbine module identification number and the trip time are input on this record.

3611D - Turbine Speed Table Record

This record exactly parallels Record 3221D.

4000D - Run Control Record

The sole entry is the end of transient time.

4100D - Print Control Record

The first parameter is used to get frequent prints during the calculational process, and should be set to -1 for the first run of any deck, so as to get prints during the steady state calculations. This parameter can also be used for debug purposes. If, for example, a problem occurs at time step 3014, set this parameter to 3000 during the next job re-run submission to get prints at every step approaching the critical one. The second parameter, the print detail key, is set to 1 for the least detail and 3 for the most detail (3 is generally recommended). The remaining paired data entries indicate the print frequency up to a designated time, with less frequent prints generally needed as the transient progresses.

4200D - Context Save Control

The first parameter keys a restart. If it is zero, a new steady state will be calculated from the input data. If it is one, a restart file will be read in to handle the initialization. The second parameter indicates how many print intervals should pass between restart file writes. The user is also referred to Section 2.9.

2.2.3.2 INPUT RECORDS (Computer Generated)

The input record description on the following pages are computer generated. While the descriptions are somewhat brief, this section is easier to keep up to date, and generally supercedes descriptions in other parts of this code documentation.

Figure 2.2-2 Input Record Contents

TITLE CARD, E.O., MINET DECK X1, GJV 102083

0V MINETD

10 PIPE GEOMETRIC RECORD/

MODID - MODULE ID ASSIGNED TO PIPE
INLETID - PORT IDENTIFIER ASSIGNED TO INLET PORT
OUTLETID - PORT IDENTIFIER ASSIGNED TO OUTLET PORT
X3MOD M LENGTH OF MODULE
Y3ID M DIAMETER OF MODULE
E3PSI - SURFACE ROUGHNESS FACTOR, ROUGHNESS/SURFACE
N3NODE - NUMBER OF NODES TO BE USED FOR MODULE
N3PATH - NUMBER OF PARALLEL UNITS BEING REPRESENTED

1010 VALVE GEOMETRIC RECORD/

MODID - MODULE ID ASSIGNED TO VALVE
INLETID - PORT IDENTIFIER ASSIGNED TO INLET PORT
OUTLETID - PORT IDENTIFIER ASSIGNED TO OUTLET PORT
X3MOD M LENGTH OF MODULE (PIPE-LIKE PORTION)
Y3ID M DIAMETER OF MODULE (PIPE-LIKE PORTION)
E3PSI - SURFACE ROUGHNESS FACTOR, ROUGHNESS/SURFACE
N3NODE - FOR VALVE, MUST USE 1 NODE
N3PATH - NUMBER OF PARALLEL UNITS BEING REPRESENTED
A3VMAX M2 MAXIMUM FLOW AREA THRU VALVE WHEN OPEN
S3VMIN - MINIMUM VALVE POSITION, RELATIVE, MUST GT 0.0
F3STOA - FACTOR, POSITION TO AREA, AREA=POSITN**F3STOA

2010 PUMP GEOMETRIC RECORD/

MODID - MODULE ID ASSIGNED TO PUMP
INLETID - PORT IDENTIFIER ASSIGNED TO INLET PORT
OUTLETID - PORT IDENTIFIER ASSIGNED TO OUTLET PORT
X3MOD M LENGTH OF MODULE (PIPE-LIKE PORTION)
Y3ID M DIAMETER OF MODULE (PIPE-LIKE PORTION)
E3PSI - SURFACE ROUGHNESS FACTOR, ROUGHNESS/SURFACE
N3NODE - NUMBER OF NODES, FOR PUMP USE 1 NODE
N3PATH - NUMBER OF PARALLEL UNITS BEING REPRESENTED

3010 HEAT EXCHANGER GEOMETRIC RECORD/

MODID - MODULE ID ASSIGNED TO HEAT EXCHANGER
INLETID - PORT ID ASSIGNED TO INLET PORT, INSIDE TUBE
OUTLETID - PORT ID ASSIGNED TO OUTLET PORT, INSIDE TUBE
X3MOD M LENGTH OF MODULE (ACTIVE HT XFER LENGTH)
Y3ID M INNER DIAMETER OF HT XFER TUBES
E3PSI - SURFACE ROUGHNESS FACTOR INSIDE TUBES
N3NODE - NUMBER OF AXIAL NODES TO BE USED
N3PATH - NUMBER OF PARALLEL UNITS BEING REPRESENTED
INLETID - PORT ID ASSIGNED TO INLET PORT, OUTSIDE TUBE
OUTLETID - PORT ID ASSIGNED TO OUTLET PORT, OUTSIDE TUBE
Y3OD M OUTER DIAMETER OF HEAT TRANSFER TUBE
F3TBDP - PITCH TO DIAMETER RATIO (TUBE SPACING/DIAMR)
N3TUBE - NUMBER OF TUBES PER HEAT EXCHANGER
M3TYPE - MATERIAL TYPE IN TUBING
I3GRID - NO. TUBES EQUADISTANT FROM CENTR TUB, 1, 4, 6
D3COIL M HELICAL COIL DIAMETER, 0 FOR STRAIGHT TUBES
F3ITOO - RATIO OF FLOW LENGTH INSIDE TUBE TO OUTSIDE
Y3CORA M DIAMETER OF CORE TUBE (ZERO IF NONE)
M3CORT - MATERIAL TYPE OF CORE TUBE
M3STRC - MATERIAL TYPE OF HX SHELL AND STRUCTURE
A3STRC M2 SURFACE AREA BETWEEN STRUCTURE-FLUID, SUM-PATH
B3STRC KG MASS OF STRUCTURE, SUMMED OVER PARALLEL PATHS

**M3TYPE, M3CORT, M3STRC OPTIONS:

1-ST STEEL 2-2.25 CH-MLY 3-ADMRLTY 4-90-10 CU-NI
5-80-20 CU-NI 6-70-30 CU-NI 7-MONEL 8-INCONNEL
9-CARBON STEEL 10-ALUMINUM

4010 INLET BOUNDARY MODULE GEOMETRIC RECORD/

MODID - MODULE ID ASSIGNED TO INLET BOUNDARY
OUTLETID - PORT ID ASSGND TO BND OUTLET (SYSTEM INLET)

4020 OUTLET BOUNDARY MODULE GEOMETRIC RECORD/

MODID - MODULE ID ASSIGNED TO OUTLET BOUNDARY
INLETID - PORT ID ASSGND TO BND INLET (SYSTEM OUTLET)

5010 VOLUME GEOMETRIC RECORD/

MODID - MODULE ID ASSIGNED TO VOLUME
L3VSHP - COMPONENT SHAPE, 1-VERT CYL OR BOX, 2-HRZ CYL
V3VOL M3 VOLUME WITHIN MODULE (PORTION OF COMPONENT)
Y3VOL M TOTAL HEIGHT OF COMPONENT
F3VMIN - REL HEIGHT OF MODULE LOW PNT W.R.T. COMPNET
F3VMAX - REL HEIGHT OF MODULE HI PNT W.R.T. COMPNET
Z3VOL M ELEVATION OF COMPONENT VERTICAL MIDPOINT
N3PATH - NUMBER OF PARALLEL UNITS BEING REPRESENTED

L3PSEP - 1-HOMOGENEOUS,2-SEPARATED PHASES,3=ISS-2TRN
 511D VOLUME INLET PORT GEOMETRIC RECORD/
 MODID - MODULE ID ASSIGNED TO VOLUME
 INLETID - PORT ID ASSIGNED TO INCOMING VOLUME PORT
 512D VOLUME OUTLET PORT GEOMETRIC RECORD/
 MODID - MODULE ID ASSIGNED TO VOLUME
 OUTLETID - PORT ID ASSIGNED TO OUTGOING VOLUME PORT
 601D TURBINE STAGE GEOMETRIC RECORD/
 MODID - MODULE ID ASSIGNED TO TURBINE STAGE
 INLETID - PORT ID ASSIGNED TO INLET PORT
 OUTLETID - PORT ID ASSIGNED TO OUTLET PORT
 ALPHA DEGREE ABS ANGL OF APPROX STEAM W.R.T. BLADE,EG-15
 801D NETWORK GEOMETRIC RECORD/
 MODID - MODULE ID OF ANY BNDRY OR ACCUMLTR IN NETWK
 IFTYPN - FLUID TYPE,1-H2O,2-SODIUM,3-AIR,4-NAK
 901D JUNCTION RECORD/
 Z3JCTN M ELEVATION OF INTERFACE BETWEEN MODULE PORTS
 MODID1 - MODULE ID OF FIRST MODULE
 PORTID1 - PORT ID OF FIRST MODULE
 MODID2 - MODULE ID OF SECOND MODULE
 PORTID2 - PORT ID OF SECOND MODULE
 1001D PIPE PERFORMANCE RECORD/
 MODID - MODULE ID OF PIPE
 F3KM1 - LOSS COEFFICIENT (K) FOR MODULE
 1101D VALVE PERFORMANCE RECORD (IF CHOKED,MUST ISOLATE)/
 MODID - MODULE ID OF VALVE
 F3KM1 - MODULE LOSS COEFFICIENT-PIPE-LIKE SECTION
 F3VALV - LOSS COEFFICIENT ACROSS VALVE OPENING
 I3CHOK - CHOKE FLOW OPTION,0-NONE,1-CHOKING EXPECTED
 J3VPRS - VOLUME WHERE PRESSR TAKEN,NOT USED= -999
 P3VOPN PA PRESSURE AT WHICH VALVE TRIPS OPEN
 S3VOPN S VALVE OPENING TIME CONSTANT
 P3VCLO PA PRESSURE AT WHICH VALVE TRIPS SHUT
 S3VCLO S VALVE CLOSING TIME CONSTANT
 ** ALTERNATE USE OF LAST PARAMETERS ** FOR CHECK VALVE
 J3VPRS=0 FOR CHECK VALVE
 P3VOPN=FLOW/PATH (KG/S) TO OPEN
 P3VCLO=FLOW/PATH (KG/S) TO CLOSE
 1201D PUMP PERFORMANCE RECORD/
 MODID - MODULE ID OF PUMP
 F3KM1 - MODULE LOSS COEFFICIENT
 W3REFF KG/S REFERENCE FLOW RATE (PER UNIT)
 H3REF M REFERENCE PUMP HEAD
 F3REF RPM REFERENCE PUMP SPEED
 A3PUMP(1) - HEAD(SPEED,FLOW)=H3REF*(SPEED/F3REF)**2
 (2) - *(A3PUMP(1)+A3PUMP(2))*WRATIO
 (3) - +A3PUMP(3)*WRATIO**2+A3PUMP(4)*WRATIO**3
 (4) - +A3PUMP(5)*WRATIO**4,
 (5) - WHERE WRATIO=W/(W3REFF*(SPEED/F3REF))
 S3PTAU S PUMP COASTDOWN TIME CONSTANT,SPD=SPD0*E-T/TAU
 S3PSEZ S PUMP SEIZURE TIME AFTER TRIP
 1301D HEAT EXCHANGER PERFORMANCE RECORD/
 MODID - MODULE ID OF HEAT EXCHANGER
 F3KM1 - MODULE LOSS COEF, INSIDE TUBES
 F3KMO - MODULE LOSS COEF,OUTSIDE TUBES
 I3LVTI - DNB/DRYOUT OPTION,1-DNB,2-DRYOUT,3-X=0.75
 I3LVTO - SAME AS I3LVTI,BUT APPLIED OUTSIDE TUBES
 F3CCFL - FLOW DIRECTION,1.PARRLL,0.CROSS,-1.COUNTER
 1601D TURBINE PERFORMANCE RECORD/
 MODID - MODULE ID FOR TURBINE
 I3TYP - TURBINE STAGE TYPE,1-IMPULSE,2-IMPULS-REACT
 E3FGEN - EFFICIENCY TO ELECTRICAL GRID
 W3TRF KG/S REFERENCE FLOW RATE
 P3ITRF PA REFERENCE INLET PRESSURE
 P3OTRF PA REFERENCE OUTLET PRESSURE
 T3ITRF K REFERENCE INLET TEMPERATURE
 R3TSRF RPM REFERENCE SPEED
 S3TTAU S COASTDOWN TIME CONSTNT,SPD=SPD0*EXP(-T/TAU)
 S3TSEZ S SEIZURE TIME (AFTER TRIP)
 2001D PIPE INITIAL CONDITION (ALL QMOD'S SUBJECT TO ADJUST.)/
 MODID - MODULE ID OF PIPE
 Q3MOD J/S HEAT PUT INTO MODULE,SUM OVER PARALEL UNITS
 2101D VALVE INITIAL CONDITION RECORD/
 MODID - MODULE ID OF VALVE
 Q3MOD J/S HEAT PUT INTO MODULE,SUM OVER PARALEL UNITS

53VPOS - INITIAL STEM POSITION,RELATIVE,0.-CLSD,1.OP
 2201D PUMP INITIAL CONDITION RECORD/
 MODID - MODULE ID OF PUMP
 Q3MOD J/S HEAT PUT INTO MODULE,SUM OVER PARALEL UNITS
 F3PUMP RPM INITIAL PUMP SPEED
 2301D HEAT EXCHANGER INITIAL CONDITION RECORD/
 MODID - MODULE ID OF HEAT EXCHANGER
 Q3MOD J/S TOTAL HT XFER,OUT TO IN,SUM OVR PARLEL UNTS
 2401D BOUNDARY MODULE INITIAL CONDITION RECORD/
 MODID - MODULE ID OF BOUNDARY
 K3EBST - BOUNDARY STATUS,0-INLET,1-FLOATING,2-FIXED
 K3EBC - E3BC FLAG,1-ENTHALPY,2-TEMPERATURE,3-QUALTY
 E36J J/KG,K ENTHALPY,TEMPERATURE,OR QUALITY (IF H2O)
 W3BC KG/S MASS FLOW (TOTAL) USED FOR INLETS ONLY
 P3BC PA PRESSURE USED FOR OUTLETS ONLY
 2501D VOLUME INITIAL CONDITION RECORD/
 MODID - MODULE ID OF VOLUME
 Q3MOD J/S HEAT PUT INTO MODULE,SUM OVER PARALEL UNITS
 F3QLV - RELATIVE LIQUID LEVEL VS COMPONET HEIGHT
 P3VOL PA ESTIMATED VOLUME PRESSURE AT STEADY STATE
 2511D VOLUME OUTLET PORT INITIAL CONDITION RECORD/
 MODID - MODULE ID OF VOLUME
 OUTLETID - OUTLET PORT ID OF VOLUME
 W3VOUT KG/S ESTIMATE OF FLOW EXITING,SUM OVER PARL PATH
 2601D TURBINE STAGE INITIALIZATION RECORD/
 MODID - MODULE ID OF TURBINE STAGE
 R3TS RPM INITIAL TURBINE SPEED
 Q3MOD J/S WORK DONE ON TURBINE STAGE
 3011D PIPE HEAT INPUT TABLE RECORD (REPEAT 2 AND 3 ENTRIES)/
 MODID - MODULE ID OF PIPE
 S3QT S TIME OF TABLE ENTRY
 Q3MDT J/S HEAT INPUT FOR CORRESPONDING TIME
 3111D VALVE HEAT INPUT TABLE RECORD (REPEAT 2 AND 3 ENTRIES)/
 MODID - MODULE ID OF VALVE
 S3QT S TIME OF TABLE ENTRY
 Q3MDT J/S HEAT INPUT FOR CORRESPONDING TIME
 3121D VALVE POSITION TABLE RECORD-OPTIONAL (REPEAT ENTR 2,3)/
 MODID - MODULE ID OF VALVE
 S3VTIM S TIME OF VALVE POSITION TABLE ENTRY
 S3VPSN - RELATIVE VALVE STEM POSITION
 3201D PUMP TRANSIENT RECORD (CAN BE OVER-RULED BY 3221D REC)/
 MODID - MODULE ID OF PUMP
 S3PTRP S TIME AT WHICH PUMP IS TRIPPED
 3211D PUMP HEAT INPUT TABLE RECORD (REPEAT ENTRIES 2,3)/
 MODID - MODULE ID OF PUMP
 S3QT S TIME OF TABLE ENTRY
 Q3MDT J/S HEAT INPUT AT CORRESPONDING TIME
 3221D PUMP SPEED TABLE RECORD-OPTIONAL (REPEAT ENT 2,3)/
 MODID - MODULE ID OF PUMP
 S3PTIM S TIME OF TABLE ENTRY
 R3PMPT RPM PUMP SPEED AT CORRESPONDING TIME
 3411D BOUNDARY CONDITION TABLE RECORD (REPEAT ENT 4,5,6)/
 MODID - MODULE ID OF BOUNDARY
 I3BCTP - KEY,1-FLOW SPECIFIED, 2-PRESSURE SPEC.
 K3ETAB - KEY FOR ETAB,1-ENTHALP,2-TEMP,3-QUALTY
 S3TAB S TIME OF TABLE ENTRY
 E3TAB J/KG,K ENTH,TEMP,OR QUAL ENTRY
 P3WTAB KG/S,PA FLOW OR PRESSURE TABLE ENTRY
 3511D VOLUME HEAT INPUT TABLE RCD (REPEAT 2,3 ENTRIES)/
 MODID - MODULE ID OF VOLUME
 S3QT S TIME OF TABLE ENTRY
 Q3MDT J/S HEAT INPUT AT CORRESPONDING TIME
 3601D TURBINE TRIP RECORD (CAN BE OVERRULED BY 3611D RECD)/
 MODID - MODULE ID OF TURBINE STAGE
 S3TSTP S TURBINE TRIP TIME
 3611D TURBINE SPEED TABLE RECORD-OPTIONAL (REPEAT ENTRY 2,3)/
 MODID - MODULE ID OF TURBINE STAGE
 S3TSTB S TIME OF TURBINE SPEED TABLE ENTRY
 R3TSTB RPM TURBINE SPEED AT CORRESPONDING TIME
 4000D RUN CONTROL CARD/
 S3END S END OF TRANSIENT SIMULATION
 4100D PRINT CONTROL RECORD (REPEAT ENTRY'S 3,4)/
 L3PRON - STEP NO. TO START FREQUENT PRNTS,-1 FOR SS
 L3PRNT - KEYS PRINT DETAIL,1-BRIEF,2-MIDL,3-DETAILED
 S3PRIN S PRINT INTERVAL

S3PLIM B TIME LIMIT FOR CORRESPONDING PRINT INTERVAL VALUE
#2000 CONTEXT SAVE CONTROL RECORD/
L3REST - CONTEXT RESTORE CONTROL ,0-NO RESTORE,1-RESTORE CONTEXT
N3SINT - CONTEXT SAVE CONTROL,DEFINES PRINT COUNT BETWEEN SAVES

STOP
END

2.3 STEADY STATE PROCESSING AND PITFALLS

MINET contains a fully generalized steady state analysis package, unlike many systems codes. This approach has great advantages in that it allows widespread MINET applications, but has the disadvantage that one has to follow specified rules, and cannot just alter one local parameter (e.g., fix a heat exchanger pressure), without affecting other variables.

Flow rates are specified for inlet boundary modules and pressures are specified for the outlets, and at least one of each must appear somewhere in each network. All other flows and pressures are calculated, and the user can influence these directly only through the form loss factor. This should be viewed as an iterative process, and a few runs may be necessary before the steady state has the desired flow and pressure distributions.

The enthalpy and heat transfer distribution calculations include some adjustment factors that bear watching. Bridge factors, used to adjust the heat transfer rates between sub-networks, are critical in satisfying energy constraints, but can be troublesome when a large and a small heat transfer bridge are adjusted together. The heat exchanger heat transfer area correction factor compensates for inaccuracies in heat transfer coefficients. In both cases, the closer these adjustment factors are to 1.0, the better.

Our experience has been that the most difficult period in testing an input deck is before the first steady state printout, which comes after the first outer iteration has been completed, if L3PRON = -1. Until the first print, one must rely on common block dumps to pursue errors, which is tedious at best. Perhaps the best approach is to build a simple, yet physically correct, system first, and make adjustments later.

2.4 RUNNING THE TRANSIENT

Any time a new deck is run, or there is a change in steady state conditions, a "null", or "steady state", transient should be run. This means setting all transient boundary conditions so as to maintain a steady state. Such a transient should be run for about 20 seconds, and the results should be checked to verify that conditions are holding near the initial conditions. If conditions are not holding, a transient should not be run until the reason for such behavior is fully understood and judged to be acceptable.

In specifying boundary conditions, the user should avoid making large step changes, as these are non-physical and strain the code numerics. Previous experience indicates the most likely error of this type occurs when the user inputs flow with pressure indicated or pressure with flow indicated, either of which can be highly disruptive.

We recommend that the user utilize the MINET restart option to accomplish a transient in pieces, particularly for a long transient. This not only reduces the likelihood of wasting resources if non-physical conditions occur, but also can be very helpful in gaining job priority on a shared computer.

Generally, one should start with frequent print-outs and decrease the print frequency as the transient progresses. If a problem develops at some point well into the transient, the transient should be rerun with a high print frequency and maximum detail. A late-developing problem will usually trace to an event occurring in recently preceding time steps.

The basic MINET numerics are stable under most flow conditions, including forward reversal, convergence, and divergence. Instabilities can be introduced through parameters calculated explicitly, e.g., heat exchanger tube

temperatures, valve positions, pump speeds. The current MINET modules are quite stable, and have proved to be that way for several test cases. However, one must be careful in specifying time constants or inserting a "hard-wired" control system, as one can introduce stability problems. As instabilities also pose problems in physical systems, various means are often used to delay component response. Should the user choose to ignore these delays as a simplification, he may force MINET to analyze under unstable conditions.

2.5 ERROR MESSAGES AND SUGGESTED RESPONSE

Current error messages and their meanings are listed in Table 2.5-1. While the interpretation given in the table is brief, it should be adequate, in general. For some cases, it is necessary to elaborate further:

103 - Area Correction Factor

This error can have two possible causes, one which is serious and one which is minor. If current system-wide conditions are sufficiently off, they can occasionally cause problems in a heat exchanger, with this error as a possible outcome. The solution is to adjust the system-wide conditions via boundary conditions, loss coefficients, and module heating. If the error is occurring in a heat exchanger and the conditions appear plausible, it is best to increase the nodalization. Otherwise, this type of error can be difficult to resolve and contact with the code developer is in order.

111 - Big System

Subroutine SUBN3S contains a series of nested "do loops" that should be large enough for most systems. However, for a very large system it may be necessary to nest more "do loops" in the routine. It will be quite obvious how to do so from looking at the subroutine.

Table 2.5-1 Error Messages and Meanings

| ERR No | Source | Nature of Error |
|--------|--------|--|
| 103 | HX3S | Failed to Converge on Area Correction Factor; Check Initial Conditions |
| 104 | EVLV3S | Water Level Outside Range for Volume; Check FLQLV, FMIN, FMAX |
| 105 | MINT3S | Failed to Converge on Global Steady State Balance; Adjust Conditions |
| 110 | PRFL3S | Failed to Converge on Flow/Pressure Distribution; Adjust Loss Coefficients |
| 111 | SUBN3S | System Too Big for SUBN3S, Extend Subroutine (EASY) |
| 118 | SUBN3S | Problem With Segment Assignment; Check System Layout |
| 119 | SUBN3S | Problem With Volume Assignment; Check System Layout |
| 120 | HX3S | Temperatures Cross In Heat Exchangers; Check Conditions |
| 125 | BKEY3S | System Overconstrained; Reduce Constraints Or Add Heat Sources |
| 139 | HX3S | Trying to Transfer Heat From Cold to Hot, Check Conditions |
| 141 | ETX3C | Quality OK As Boundary Condition Only If Water/Steam |
| 201 | F V3T | Failed To Converge on New Water Level; Check Level and Enthalpy |

118, 119 - Segment Linkages

This problem is somewhat hypothetical in that it has never occurred to date. If it should arise, it would indicate trouble in the way the network is linked together. Contact with the code developer should be made.

120, 139 - Heat Exchanger Problems

The MINET heat exchanger module is programmed to recognize these impossible conditions and avoid the potential difficulty in performing a full iterative solution. Instead, a linear heat transfer is assumed, to generate enthalpy distributions and reasonable pressure drops, in the hopes that on the next pass conditions will be more physically correct. If this fix occurs on the last steady state iteration, the area correction factor will be identically 1.0000000, and any transient that follows will be questionable at best.

2.6 RECOVERING FROM AN ABNORMAL JOB TERMINATION

If a problem is not discovered through routine error checks, and instead leads to a fatal error, e.g., divide by zero, a run can be terminated abruptly in a "crash." As testing of MINET continues, such an occurrence will become increasingly unlikely. However, at this time, an abnormal termination is a very real possibility, and may be expected to occur from time to time.

The key to determining the reason for a crash is maximizing the amount of information about conditions at and just prior to the job termination time. This includes recent printouts, common block dumps, computer system diagnostics regarding the crash, and debug write statements subsequently inserted into the code.

In general, the immediate reason for a crash will be uncovered in a relatively short time. Often it will trace to an input error not yet detected.

The worst case is when the reason for an abnormal condition cannot be traced to the source. At this stage, knowledge of the code processing can be important, and we recommend that the user contact the code developer.

In order for the MINET developers to trace a problem, several pieces of information are needed. If the code was modified in any way, a revised listing will be needed. The input deck and output from the ill-fated run are needed. Content of the common blocks is useful. Finally, a schematic drawing of the representation is necessary.

2.7 INTERPRETING THE OUTPUT

In order to interpret printed MINET output, one needs a schematic of the system. This is necessary to interpret module ID numbers and visualize the configuration.

Three levels of print detail are available, designated 1 for the shortest, 2 for moderate detail, and 3 for full detail. These are described further below. Example outputs can be found in Section 4 of this report.

2.7.1 PRINT OPTION 1

The heading gives the current simulation time, the length of the most recent time step, and the transient time step number. Knowledge of the step number can be most useful when a problem develops at some point well into the transient, so that one can rerun the transient with heavy print detail turned on for the previous few seconds.

Conditions at the system boundaries appear next, with the boundary ID, the network number (MINET assigns), the flow, enthalpy, pressure and temperature,

as well as the fluid type, given for each boundary module. If water is in the network, it is wise to watch the enthalpy and temperature if conditions are anywhere near saturation.

In the steady state print only, a summary of the system sub-networks follows. Recall that sub-networks are added whenever a separated volume or an outlet boundary module with a fixed temperature is used. This printout merely indicates what adjustments had to be made to satisfy these additional constraints. A bridge is simply a heat transfer connection, Q_{ij} , between sub-networks or a sub-network and "ground," i.e., $i=j$. If the adjustment factors are near 1.0, this edit can be ignored. If this factor differs substantially from unity, the user should investigate why.

The next part of the printout is for the system volumes. Volume ID, pressure, enthalpy, temperature, water level, heat input, network number (MINET assigned), and the number of regions specified in the volume are given. The number of regions will be one for homogeneous, two for separated, or three for initially homogeneous, but separated during the transient. The water level is meaningful only for water/steam in a separated volume.

Next to appear in the printout is the segment condition summary. The segments are listed by their MINET number, which the code assigns while it is processing the input. At the right-hand side of the print, module ID numbers are given for the modules connecting at the segment inlet and outlet, which are helpful in identifying the segments. Segment parameters printed include: segment inlet, outlet, and average flow rate; inlet and outlet enthalpy and pressure; and pressure loss parameters α and β .

2.7.2 PRINT OPTION 2

When print option 2 is specified, additional print is provided to give in-segment distributions. Because the segment module IDs are printed for each segment, one can easily resolve any uncertainty as to which segment is which. For each node in each segment, the inlet, average, and outlet enthalpy, the inlet and outlet flow, the inlet, average, and outlet temperature, the average density, and the total heating (work) added to the node are given. Node number and nodal interface numbers are also provided, which are needed for the plot option.

2.7.3 PRINT OPTION 3

By specifying print option 3, the user gets, in addition, a description of conditions at the module level. For each module, the module number (MINET assigned), the module type ordinate number (MINET assigned, e.g., the 4th valve), module ID number (user assigned), and the number of parallel units being represented by one (user assigned) are given. These numbers are also needed for specifying variables for plotting.

For valves, the current valve position is given, along with the current choke flow limit. A large value for the choked flow limit may mean the choking option was declined, in which case MINET sets the choke limit extremely high so it will not be exceeded.

For pumps, the current pump speed, flow rate, and pump head are given. The flow rate is per parallel unit.

For heat exchangers, the area correction factor is first given, which indicates how closely the MINET heat transfer correlations agree with the steady state conditions. A value near 1.0 is desirable, but a value of exactly 1.0 indicates there may have been a problem in the steady state (see Section 2.5).

Also given for heat exchangers is a node-by-node detailing of current conditions. The tube node number, and the node numbers for the fluids passing inside and outside the tubes are given. Heat transfer per meter and node average temperatures are given, as are the heat transfer modes inside and outside the tubes, and the temperatures for the core tubes and structure. For water and steam, multiple heat transfer modes can occur in one node, in which case mode 45 would indicate that heat transfer began as film boiling (4) and passed on to superheat (5), for instance. It happens, occasionally, that a heat exchanger will be processed from opposite ends in the transient and steady state, in which case the mode could switch to 54, which represents a physical situation provided the total heat transfer is about the same. (Note: if, during the transient, the tube structure temperature swings wildly, it may indicate that the heat transfer area to structure mass ratio is too big.)

For the turbine module, current speed, efficiency, and "power from the generator" are printed. Note that the "power from the generator" will usually be negative, and the turbine usually provides power to the generator.

2.8 THE PLOT OPTIONS

As a user-option, MINET will (during normal printouts) write current values of key variables into a transactions file, which can be used for generating plots and other forms of output. This effort is still under development.

The user will be able to specify subsets of the variables listed in Table 2.8-1, or the table in its entirety. As a result, a chronologically ordered set of values will become available in the transactions file.

Access to the contents of the transaction file will be by a post-processor, which, for now, will be designated "RECALL". In the initial version of RECALL, the user will have to specify the variable name and the value (e.g., node number) of interest. It is hoped that, in later versions, one may gain access through more basic parameters, such as module ID number and other externally meaningful parameters.

Table 2.8-1 PLOTFILE Parameters

| Variable | Group | Parameter |
|----------|----------|--|
| D3QDWB | Node | Node Heating Derivative w.r.t. Pressure |
| T3JUNC | Node Inf | Nodal Interface (Junction) Temperature |
| T3TC | HX Nod | HX Tube Node Temperature |
| Q3PMI | HX Nod | Heating Per Meter, Inside Tube |
| Q3PMO | HX Nod | Heating Per Meter, Outside Tube |
| T3CORT | HX Nod | Core Tube Temperature |
| T3STRC | HX Nod | Structure Temperature |
| R3PUMP | Pump | Pump Speed, Relative to Reference |
| R3DMND | Pump | Pump Demand Speed, Relative |
| F3PUMP | Pump | Pump Speed in RPM |
| W3PUMP | Pump | Mass Flow Rate Per Pump |
| H3PUMP | Pump | Pump Head in Meters |
| S3VPOS | Valve | Valve Position, Relative |
| W3VALC | Valve | Mass Flow Rate at Choking |
| S3DMD | Valve | Valve Demand Position, Relative |
| P3VOL | Volume | Volume Average Pressure (Pa) |
| E3VOL | Volume | Volume Average Enthalpy (J/KG) |
| F3LQLV | Volume | Relative Liquid Level |
| T3VOL | Volume | Volume Temperature |
| R3VOL | Volume | Volume Average Density |
| D3VRE | Volume | Derivative of Vol Ave Dens w.r.t. Enthalpy |
| D3VRP | Volume | Derivative of Vol Ave Dens w.r.t. Pressure |
| E3BC | Boundary | Boundary Module Enthalpy |
| P3BC | Boundary | Boundary Pressure |
| W3BC | Boundary | Boundary Flow |
| T3BC | Boundary | Boundary Temperature |
| X3BC | Boundary | Boundary Quality |
| S3DELT | GLOBAL | Current Time Step Size |
| S3TAUM | GLOBAL | Minimum Time Constant Calculated |
| A3LPHA | Segment | Segment Pressure Loss Multiplier |
| B3ETA | Segment | Segment Pressure Loss Exclusive of Flow Squared |
| E3INSL | Segment | Segment Inlet Enthalpy |
| E3OTSL | Segment | Segment Outlet Enthalpy |
| P3INSL | Segment | Segment Inlet Pressure |
| P3OTSL | Segment | Segment Outlet Pressure |
| W3SEG | Segment | Segment Average Mass Flow Rate |
| W3INSL | Segment | Segment Inlet Mass Flow Rate |
| W3OTSL | Segment | Segment Outlet Mass Flow Rate |
| R3TS | Turbine | Turbine Speed in RPM |
| E3FTSG | Turbine | Turbine Operating Efficiency |
| P3WRGN | Turbine | Power from Generator (Negative If Turbine Operating) |
| R3TSDM | Turbine | Turbine Demand Speed in RPM |
| E3WSSG | Node Inf | Enthalpy at Nodal Interface |
| W3WSSG | Node Inf | Mass Flow Rate at Nodal Interface |
| E3CB | Node | Node Average Enthalpy |
| D3DRDP | Node | Node Average Density Derivative w.r.t. Pressure |
| D3DRDE | Node | Node Average Density Derivative w.r.t. Enthalpy |
| T3CB | Node | Node Average Temperature |
| Q3CB | Node | Node Heating (In = Positive) |
| R3CB | Node | Node Average Density |
| D3QDEB | Node | Node Heating Derivative w.r.t. Enthalpy |

2.9 RESTART

The MINET transient restart option can be very useful, particularly once a transient simulation has begun. It should be employed routinely for transients of significant duration, both as failure insurance and to improve access to shared computers where expected execution time influences job priority.

When a restart file is written, values for all relevant variables are transferred to the output device. A simulation can then be started up again from that point, by initializing current values from information in the restart file.

The user controls the frequency at which restart files are written. This is done through parameter N3SINT on input record 4200, which indicates how many printouts (see record 4100) take place between restart file writes. When a restart file is written, the previous contents are overwritten. Thus, with a 60 second run, having prints every 2 seconds and N3SINT = 5, a restart file will be written at 10, 20, 30, 40, 50, and 60 seconds. At the end of the run, only values for $t = 60$ seconds will be in the "save" (restart) file.

When the user wants to restart a run, the restore file is specified to be the restart save file from the previous run, and parameter L3REST on input record 4200 is set to 1. Thus, continuing the example in the previous paragraph, the job would be continued from conditions at $t = 60$ seconds.

Control of the restart option and the input/output device number is kept at a very high level in the MINET program logic. This facilitates transference of control to a host code, such as SSC [11], so that coordination and conflict problems can be resolved.

3. MINET CODE DESCRIPTION

The ideal computer code is written so that it can always be treated as a black box, i.e., details of the internals can be totally ignored. Unfortunately, a computer code with the size and scope of MINET is nearly impossible to perfect to such a degree. We tried to do the next best thing, i.e., to develop a code that is highly modular and quite readable so the user has a chance to cope with problems that may arise. This section of the MINET code documentation is written to facilitate the understanding of the MINET program, but can in no way describe every facet of the code.

Computer code documentation can be provided in three ways: (1) written, (2) computer generated, and (3) imbedded in the computer code. Much of this document is handwritten, which has the advantage of clarity and the disadvantage that it is cumbersome to update. Computer generated documentation can be tedious to develop, but is easy to update. In-code descriptions are particularly useful when reading the program library, but are not much use in formal reports. In order to keep this section as current as possible, much of it is computer generated.

3.1 CODE STANDARDS AND PHILOSOPHY

3.1.1 PROGRAMMING LANGUAGE

ANSI USA Standard FORTRAN language (ANSI X3.9-1966) is used as a basis for MINET code development. Some exceptions have, however been necessary for the sake of expedience. These fall into two categories:

- Required features not defined within the standard (character manipulation) have been implemented in such a way that machine dependencies due to work size can be overcome on most systems by global means rather than numerous local modifications.
- Overly-restrictive language limitations (indexing expressions, etc.) have been relaxed based on reasonable assumptions about the extensions available in most available compilers.

3.1.2 SUPPORT SOFTWARE

No external support libraries or system-dependent procedures are required.

3.1.3 GLOBAL COMMONS

All FORTRAN COMMON declarations with identical labels are implemented with identical variable lists wherever they appear. This avoids confusion due to "aliasing" of COMMON locations.

3.1.4 NAMING CONVENTION

Certain conventions have been established governing the choice of variable, labelled COMMON, and subprogram names.

- global variables are identified by having a numeric character in the second position according to the following rules:
 1. 9 signifies variables associated with utility and driver code
 2. 3 signifies variables associated with MINET computational code

- labelled global COMMON names use a numeric character in the next-to-last position following the above rules for global variables. The last character of global COMMON names is chosen according to the rules:

1. V signifies a block containing only REAL types
2. I signifies a block containing only INTEGER types
3. P signifies a block containing only global container POINTER types
4. U signifies a block containing implementation variables for utility code

SUBROUTINE names use a numeric character in the next-to-last position according to the rules:

1. 9 signifies driver and utility code
2. 3 signifies computational code

The last character of SUBROUTINE and FUNCTION names is chosen according to which of the major code divisions they belong:

1. R signifies Reader code
2. S signifies Steady-state code
3. T signifies Transient code
4. U signifies Universal code which is used in more than one division
5. C signifies COMMON code used in both the steady-state and the transient calculations

3.1.5 DESIGN PHILOSOPHY

The objective of the design philosophy adopted for MINET is to make the finished code easy to maintain and modify. Two major approaches, MODULARITY and the use of DATA MANAGEMENT UTILITIES have been used to accomplish this objective.

- The MODULAR approach involves dividing the code design into smaller parts, called modules, such that each can be dealt with individually. Although many methods exist for performing modular design, the end result exhibits similar desirable characteristics:
 - modules exhibit high strength in that the module contents are closely related by the operations they perform.
 - modules exhibit low coupling in that the contents and functions of any one module have minimal relationship to those of another.
- DATA MANAGEMENT UTILITIES are groups of subroutines designed to implement abstract data types not available in the programming language being used (FORTRAN in this case). Each abstract data type consists of a structured data object, such as a list, and a group of operations, such as CREATE, DELETE, INSERT, etc. All access to the data is performed by calls to members of a subroutine group, each of which performs one of the operations. Advantages include:
 - Data structures can be constructed to best fit the problem being solved so that computational code logic is cleaner.

- Potentially messy and confusing implementation details are effectively "hidden" from upper-level computational code.
- Flexibility is enhanced because the actual implementation of the abstract data types can be changed as needs require without having any effect on the upper-level code.
- Errors are easily detected by inserting appropriate parameter tests in members of the subroutine group.

3.2 CODE STRUCTURE

MINET is a carefully structured code, using modular subroutines and highly specific functions, as well as carefully managed common blocks. Argument lists are occasionally used to improve code modularity, but much of the code data resides in the global common blocks. Low level functions and subroutines rarely access the global common blocks, and never alter any of the values. This careful structuring and data management makes MINET relatively easy to read, understand, and modify.

3.2.1 TIER CHART & CROSS REF MAP

A computer generated tier chart is provided in the pages to follow. While the format by which the chart continues from page to page is far from ideal, the chart (as shown) is easy to keep up to date and should not be overly difficult to interpret. A subroutine and function cross reference map is included in the pages that follow the tier chart.

Figure 3.2-1 Tier Chart

§ = RECURSIVE TREE, * = PREVIOUSLY PRINTED TREE

```

.CHARCTR
.COMDUM
.PRTCON
.GCPR9U
.GCTE9U
.GCTP9U
.ABEND1
.CHARCTR
.INFO
.CHARCTR
.CODEB
*INFO
.SDUMP
.INSTRUC
.SSWTCH
.SSWTCH
.CHARCTR
.TRACE1
.ABEND
.COMDUM
.DISPLA
*GCPR9U
*GCTP9U
.EXIT9U
.REMARK
.SSWTCH
*TRACE1
.TRACE
.INGC9U
.INIT9U
.SECOND
.PAGE9U
.TIME
.SSCTIM
.INIT9U
.DATE
.SSCDAT
.INTNDG
.DCODNC
*EXIT9U
.ERRMSG
.INTERP
.INTNDG
.ISETHM
.ITRCK
.CDINPT
.INTNDG
.NAMEWD
.NNBLNK
.NSKIP
.SETFMT
.READHM
.REPEAT
*ERRMSG
.INTNDG
.GENRD
.NNBLNK
.ISTOP
.ITRCK
.NNBLNK
*EXIT9U
*EXIT9U

```

```

      .GETN9U..
      .NXTA9U.. *EXIT9U
      .GETD9U..
      .INPT9U
      .GETF9R..
      .NXTI9U.. *GETD9U
      .LOCR9U..
      .RLID9U.. *EXIT9U
      .INPT9U *EXIT9U
      .GETF9U.. *NXTA9U
      .CRDR9R..
      .UNIQ9U
      .ILNK3R..
      .INL9U..
      .INM9U..
      .INN9U
      .NEWN9U.. *EXIT9U
      .NEWM9U..
      .PUTN9U.. *EXIT9U
      .PUTD9U.. *NXTA9U
      .NEWL9U..
      .INPT9U
      .LNKN9U
      .NEWD9U.. *NEWN9U
      .NXTN9U
      .PUTD9U..
      .PUTN9U
      *NEWM9U
      *PUTD9U
      .ISU9R..
      .INPT9U
      *NEWD9U
      .PUTR9U..
      .PUTF9U.. *EXIT9U
      .NXTA9U
      .UNIQ9U
      .UNIQ9U
      .INRD3R..
      *NEWL9U
      *EXIT9U
      *GETD9U
      .INSL9U..
      *PUTD9U
      *NEWL9U
      .PUTF9R..
      *NEWN9U
      .NEWR9U..
      *PUTF9U
      *PUTD9U
      *EXIT9U
      *GETD9U
      *EXIT9U

```



```

      *GETF9U
      .GETR9U..
      .INPT9U
      *INSL9U
      .PUT19R..
      *LOC9BU
      *NEW9BU
      *PUTD9U
      *PUTR9U
      *EXIT9U
      *INSL9U
      .PUTR9R..
      *NEW9BU
      *PUTD9U
      *PUTD9U
      .REPS9R..
      *EXIT9U
      *GETN9U
      .INTG9U..
      .INPT9U
      *EXIT9U
      *GETF9U
      .REAL9U..
      .INPT9U
      .CTRL3R..
      .INPT9U
      .DS1Z9U..
      .NS1Z9U
      .JGCT9U
      .LPNT9U..
      .NS1Z9U
      .TABL9R..
      *EXIT9U
      .JGCT9U
      .PGCR9U..
      *NEW9BU
      *PUTF9U
      *REAL9U
      *DS1Z9U
      *GETD9U
      .DEFP3R..
      *EXIT9U
      *GETN9U
      .MID9U..
      .INPT9U
      *PUTD9U
      *DS1Z9U
      *GETD9U
      *DS1Z9U
      *GETD9U
      .GET19R..
      *GETR9U
      *RL1D9U
      *GETD9U
      .GETR9R..
      *MID9U
      .LOCL9U..
      *NXT19U
      *INSL9U
      *DS1Z9U
      *INTG9U
      *MID9U
      .KPRT3R..
      *PUTD9U
      .UNTQ9U

```



```

      *DS1Z9U
      *GETD9U
MARK3R
      *PUTD9U

      *MID9U
      *MORD3R
NET3R
      *MTYP9U
      *DS1Z9U
      *GETD9U
      *NX1M3R
      *RELM9U

      *DS1Z9U
      *DS1Z9U
      *GETD9U
      *GETD9U
      *PUTD9U
      *GETD9U
      *MID9U
      *DS1Z9U
      *GETD9U
      *NBR3R
      *MID9U

ORDR3R
      *NEW9U
      *DS1Z9U
      *GETD9U
      *NX1O3R
      *PUTD9U
      *PUTD9U
      *RELM9U
      *UNIQ9U

      *PGC19U
      *PGCR9U
      *PUTD9U
      *PUTJ3R

      *INT09U
      *JDAT3R
      *MARK3R
      *MID9U
      *MORD3R
      *NCL
      *HX3R
      *NX1
      *PGC19U
      *PGCR9U
      *PUTJ3R
      *REAL9U

      *LSTM3R
      *MID9U
      *MORD3R
      *MTYP9U
      *PGC19U
      *PGCR9U
SEG3R
      *INT09U
      *PIDS3R

      *INT09U
      *MID9U
      *MORD3R
      *NX1M3R
      *PIPE3R
      *PGC19U
      *PGCR9U
      *REAL9U
      *TABL9R

      *DS1Z9U
      *EXP
      *INT09U

```

```

      *LPNT9U
      *MID9U
      *MORD3R
      PUMP3R
      *NXTM3R
      *PGC19U
      *PGCR9U
      *REAL9U
      *TABL9R
      .COS
      *DSIZ9U
      .EXP
      *INTG9U
      *MID9U
      *MORD3R
      TURB3R
      *NXTM3R
      *PGC19U
      *PGCR9U
      *REAL9U
      *TABL9R
      *DSIZ9U
      *INTG9U
      *MID9U
      *MORD3R
      *NXTM3R
      VALV3R
      *PGC19U
      *PGCR9U
      *REAL9U
      *TABL9R
      *DSIZ9U
      *EXIT9U
      ZPRT3R
      *INTG9U
      *REAL9U
      *INTG9U
      *KPRT3R
      *MARK3R
      *MID9U
      *MORD3R
      *NXTM3R
      *DSIZ9U
      PCNT3R
      *GETD9U
      VOL3R
      *PGC19U
      *PGCR9U
      *PID53R
      *PUTJ3R
      *REAL9U
      *TABL9R
      *ZPRT3R
      SYS3R
      *EXIT9U
      NPNT9U
      *NXT19U
      *PCNT3R
      MAIN9R
      *GETD9U
      *NXT19U
      RISU9R
      *RELL9U
      *PAGE9U
      LIST3R
      VRFY3R
      ERR9U
      BKEY35

```

```

      .ADDABU
      .DENL3D .EXP
      .DENV3D
      .DENV3D
      .ESTL3H .ALOG
      .ESTV3H .ALOG
      .EVLV3S
      .ERRBU
      *DENL3D
      *DENV3D
      *ESTL3H
      *ESTV3H
      .VOLF3C .ACOS
      .SIN
      .ENET3S
      .GETABU
      .INA9U
      .LEQ3C
      .LEQ9U
      *EXIT9U
      .NEWA9U
      .PUTA9U
      *VOLF3C
      .ERR9U
      .INIT3S
      .PRHX3S
      .KPRC3S
      .MDST3S
      *ESTL3H
      *ESTV3H
      .ALOG
      .ATAN2
      .COS
      .CBRT3C
      .EXP
      .SIN
      .SQRT
      .TAIR3C
      *CBRT3C
      .TMNK3C
      .TEMP3C
      .TMPL3T
      .TMPV3T
      *CBRT3C
      .TNA3C
      .CROS3S
      *DENL3D
      *DENV3D
      *ESTL3H
      *ESTV3H
      .RHD3C
      *TAIR3C
      .RAIR3C
      *TMNK3C
      .RHNK3C
      *TNA3C
      .RNA3C
      .ALOG
      .THOM3C
      .DP3C

```

```

      *ESTL3H
      *ESTV3H
      *TAIR3C
      .VAIR3C
      .VISL3N
      .VISC3C
      .DENV3D
      .VISV3N
      .TMPV3T
      .ALOG1D
      .VSNA3C
      *TNA3C
      .EXP
      *RHNK3C
      .VSNK3C
      *TMNK3C

ERRBU
      .COND3C
      .CONL3K
      .CPL3C
      .HWFC3C
      .VISL3N
      .COND3C
      .HCIT3C
      .SQRT
      .HCOT3C
      *TNA3C
      .HCPN3C
      *TNA3C
      .TKNA3C
      .HNAF3C
      *VSNA3C
      .EXP
      *HCPN3C
      .HNAI3C
      *TKNA3C
      *VSNA3C
      *TAIR3C
      .CAIR3C
      *TAIR3C
      .CPAR3C
      .HTCA3C
      *VAIR3C
      *TMNK3C
      .CDNK3C
      .HTNK3C
      *TMNK3C
      .CPNK3C
      .HTC3C
      .SQRT
      .HWCN3C
      .DENV3D
      .CONV3K
      .TMPV3T
      .CPV3C
      .HWFB3C
      .CPV3C
      *ESTV3H
      .ENTV3H
      .TMPV3T
      *VISV3N

```

```

      *HWFC3C
      .CONL3K
      .CPL3C
      *ESTL3H
      .ROOT3C
      .PSAT3P
      .TMPL3T
      .HWNB3C
      .SQRT
      .VISL3N
      *CONV3K
      .CPV3C
      .HW5C3C
      *ENTV3H
      *VISV3N
      QPM3C
      *TEMP3C
      .ROOT3C
      .BCOR3C
      *TEMP3C
      .SQRT
      .XDNB3C
      .XDRY3C
      .COND3C
      *HWFC3C
      *QPM3C
      .IMOD3C
      *TEMP3C
      *XDNB3C
      .XDRY3C
      *QPM3C
      .ROOT3C
      .HXND3S
      .TCLM3C
      .TCRG3C
      *TEMP3C
      *RHO3C
      .HX3S
      .ROOT3C
      .SATM3C
      .CONL3K
      .CPL3C
      *DENL3D
      .DENV3D
      *ESTL3H
      .SATO3C
      *ESTV3H
      .STEN3S
      .TMPL3T
      .VISL3N
      *VISV3N
      *TEMP3C
      *VISC3C
      .ALOG
      .MODL3C
      .SQRT
      *DP3C
      *RHO3C
      .PIPE3S
      *TEMP3C
      .PUMP3S
      .MRCH3S
      .SATM3C
      .CONL3K
      .CPL3C
      *DENL3D
      .DENV3D
      *ESTL3H

```

```

.SATP3C..
*ESTV3H
.STEN3S
.TMPL3T
.VISL3N
*VISV3N

.EAIR3C
.ENA3C
.ENNK3C
.CPL3C
*ESTL3H
.ENTL3H..
.TMPL3T

.ENTH3C..
*ENTV4H
*ESTL3H
*ESTV3H
.TMPL3T

*ESTL3H
*ESTV3H
.SFWT3C

.ESW3C..
.SOWT3C
*ESTL3H
*ESTV3H
.SFWT3C
.SWAT3C..
.SOWT3C
.TMPL3T
.TMPV3T

*RH03C
.TBSG3S..
.SQRT
*SWAT3C
*TEMP3C

*ESTL3H
*ESTV3H
.GFSK3C

.CRIT3C..
.FXP
.GMDY3C..
.DENV3D
*ESW3C
.GSUP3C..
.SQRT
*SWAT3C

.VALV3S..

.ADDA9U
*DENL3D
.DENV3D
*ESTL3H

.DPSV3C..
*ESTV3H
*RHO3C

.ERR9U
.GETA9U
.INA9U
*LEQ9U
*MODL3C
*NEWA9U
*PIPE3S

.PRFL3S..
.PUMP3S
.PUTA9U
.RELA9U
*RHO3C
.SATM3C
*SATP3C
.SQRT
*VALV3S

```



```

. ADDA9U
. GETM9U
*LEQ9U
. NET3T ...
*NEWA9U
. PUTA9U
. RELA9U
*ETX3C
. PREP3T ...
. INTP9U
*PRNT3C
*ESTL3H
*ESTV3H
. VOLS3T ...
*FLV3T
*PRNT3C
*IPTS3R
*PAGE9U
. RECX3U ...
*EXIT9U
. REGC9U ...
*PAGE9U
. SVCX3U ...
. SVGC9U
. SDEL9T
. TIME3T ...

```

Figure 3.2-2 Subroutine/Function Cross Ref Map

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|--|--|---|
| ABEND | MINET | ABEND1 | |
| ABEND1 | ABEND | CHARCTR COMDUM ENDFIL GCPR9U GCTP9U INFO OUTCI OUT R SDUMP SPA SSWTCH TRACE1 | ABEND |
| ABORT | | ABEND1 | |
| ACOS | FLV3T VOLF3C | | |
| ADDA9U | ENET3S IOSG3T LOAD3T NET3T PRFL3S QBAL3S SGBC3T | | ADAB9U |
| ADDM9J | IOSG3T LOAD3T | SPA | ADAB9U |
| ADTB3T | MINT3T | DENS3C HCAP3C | GLOB3I GLOB3V HX3P LNK3P MODL3P MODL3P VD9V |
| ADV3T | MINT3T | DPSV3C DRDE3C DRDP3C FLY3T GETA9U GETM9U GOTOER PUTA9U RELA9U RH03C TEMP3C | BC3P GLOB3V LNK3P MODC3P NET3P MODL3P SEG3P TRND3P VD9V VOL3P |
| ALOG | CBRT3C ESTL3H ESTV3H MODL3C THOM3C | | |
| ALOG10 | VSNA3C | | |
| ATAN2 | CBRT3C | | |
| BCOR3C | HXND3S HX3T | COND3C GOTOER HWFC3C OUTFI QPM3C P00T3C SPA TEMP3C XDNB3C XDRY3C | MOD3I MOD3V SATM3V |
| BKEY3S | MINT3S | ERR9U | GLOB3I SNET3P VD9V |
| BND3R | NET3R | INTG9U MID9U MDRD3R NCLS3R OUTFI PGC19U POCR9U REAL9U TABL9R | |
| CAIR3C | HTCA3C | TAIR3C | |
| CALC3R | INIT3R | OUTFI | GLOB3I LNK3P VALV3P VD9V |
| CBRT3C | TAIR3C TMNK3C TNA3C | ALOG ATAN2 COS EXP SIN SPA SQRT XT01\$ | |
| CDINPT | GENRD | DCODNC ERRMSG INTER INTNDG JSETHM ITRPCK NAMEWD NNBLNK NSKIP READHM REPEAT | ITERP |
| CDNK3C | HTNK3C | TMNK3C | |

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|--|--|--|
| CHARCTR | ABEND1 INFO SDUMP TRACE1 | | |
| CODEB | SDUMP | | |
| COMDUM | ABEND1 EXIT9U | OUTC1 | GLOB31 GLOB3V MOD31 MOD3V NODE31 NODE3V SATM3V SATP3V |
| COVD3C | BCOR3C IMOD3C OPM3C | | |
| CONL3K | HWFC3C HWNB3C SATO3C SATP3C | | |
| CONV3K | HWFB3C HWSC3C | DENV3D TMPV3T XTOY\$ | |
| COS | CBRT3C FLV3T TURB3R | | |
| CPAR3C | DREA3C HTCA3C | TAIR3C | |
| CPL3C | ENTL3H HWFC3C HWNB3C SATO3C SATP3C | | |
| CPNK3C | DRNK3C HTNK3C | TMNK3C | |
| CPV3C | ENTV3H HWFB3C HWSC3C | | |
| CRDR9R | MAIN9R | GENRD GETF9R INR03R OUTC1 READ3R STOP | DATA9 SCR9H1 UNIT9U |
| CRIT3C | VALV3S VALV3T | ESTL3H ESTV3H GFSK3C GMDY3C GSUP3C | SATM3V |
| CRKR3T | CRKR9U | SPA | |
| CRKR9U | MRCH3T | CRKR3T | ADAB9U |
| CROS3S | HX3S | TEMP3C | MOD31 MOD3V NODE31 NODE3V |
| CTRL3R | DMOD3R | INTG9U REAL9U TABL9R | GLOB31 TIME31 TIME3V |
| DATE | SSCDAT | | |
| DCODNC | CDINPT | GOTOER INTNDG XTOI\$ | |
| DEFP3R | DMOD3R | DSIZ9U GETD9U MID9U OUTF1 PUTD9U SPA | DCON9U LNKS31 |
| DENL3D | DPSV3C DRDE3C DRDP3C ENET3S EVLV3S FLV3T IOSG3T RH03C SATO3C SATP3C WESM3S | EXP | |
| DENS3C | ADTB3T HX3T | | |

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|--|--|------------------------------------|
| DENV3D | CONV3K ENET3S IOSG3T VISV3N DPSV3C EVLV3S RH03C WESM3S DRDE3C FLV3T SAT03C DRDP3C GSUP3C SATP3C | | |
| DISPLA | EX1T9U | | |
| DMOD3R | READ3R | CTRL3R GET19R KPRT3R NEHL9U PUTD9U DEFP3R GETR9R LINK3R NEWM9U PUTR9U DS1Z9U GOTOER LOCL9U OUTC1 RELL9U DCON9U SCRH3R UNIT3I | |
| DPSV3C | ADV3T PRFL3S | DENL3D RH03C DENV3D ESTL3H ESTV3H VD9V VOL3P | |
| DP3C | HX3S HX3T PIPE3S PIPE3T | RH03C THOM3C VISC3C XTOY\$ | MOD3I MOD3V NODE3V SATM3V |
| DRDE3C | ADV3T HX3T PIPE3T VOLM3S | DENL3D DRNK3C DENV3D ESTL3H DREA3C ESTV3H DREN3C GOTOER | SATM3V |
| DRDP3C | ADV3T HX3T PIPE3T VOLM3S | DENL3D ESTV3H DENV3D GOTOER DRPA3C | SATM3V |
| DREA3C | DRDE3C | CPAR3C TAIR3C | |
| DREN3C | DRDE3C | HCPN3C TNA3C | |
| DRNK3C | DRDE3C | CPNK3C TMNK3C | |
| DRPA3C | DRDP3C | TAIR3C | |
| DS1Z9U | DEFP3R GETM3R NET3R PCNT3R VALV3R DMOD3R KPRT3R NXTM3R PUMP3R ZPRT3R FST03R MARK3R NXT03R TABL9R TURB3R GET19R NBR3R ORDR3R | INPT9U NS1Z9U | |
| EAIR3C | ENTH3C | | |
| ENA3C | ENTH3C | | |
| ENDFIL | ABEND1 | | |
| ENET3S | MINT3S | ADDA9U ESTV3H LEQ9U DENV3D EVLV3S NEWA9U GETA9U PUTA9U ESTL3H INA9U VOLF3C BC3P MODC3P SNET3P GLO93I MODL3P VD9V HX3P NET3P VOL3P LNK3P SEG3P | |
| ENNK3C | ENTH3C | | |
| ENTH3C | ETX3C TBSG3S | EAIR3C ENA3C ENNK3C ENTL3H | SATM3V |

3.2-20

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|--|---|---|
| | | ENTV3H ESTL3H ESTV3H GOTOER. TMPL3T | |
| ENTL3H | ENTH3C | CPL3C ESTL3H SPA. TMPL3T | |
| ENTV3H | ENTH3C HWFB3C HWSC3C | CPV3C ESTV3H SPA. TMPV3T | |
| ERRMSG | CDINPT GENRD | EXIT9U GOTOER. OUTC1. | ITERP |
| ERR9U | BKEY3S ETX3C EVLV3S FLV3T HX3S MINT3S PRFL3S SUBN3S | OUTC1. | UNIT9U |
| ESTL3H | CRIT3C DPSV3C DRDE3C DRDP3C ENET3S ENTH3C ENTL3H ESW3C ETX3C EVLV3S FLV3T IOSG3T PSAT3P RH03C SAT03C SATP3C SWAT3C TEMP3C VISC3C VOLS3T WESM3S | ALOG XTOY\$ | |
| ESTV3H | CRIT3C DPSV3C DRDE3C DRDP3C ENET3S ENTH3C ENTV3H ESW3C ETX3C EVLV3S FLV3T IOSG3T RH03C SAT03C SATP3C SWAT3C TEMP3C VISC3C VOLS3T WESM3S | ALOG XTOY\$ | |
| ESW3C | GSUP3C TBSG3S TBSG3T | ESTL3H ESTV3H SFWT3C SGWT3C SPA. SWAT3C | |
| ETX3C | PREP3T WESM3S | ENTH3C ERR9U ESTL3H ESTV3H GOTOER. TEMP3C | BC3P MOOL3P VD9V |
| EVLV3S | ENET3S | DENL3D DENV3D ERR9U ESTL3H ESTV3H VOLF3C | VD9V VOL3P |
| EXIT9U | ERRMSG GETD9U GETF9U GETN9U GETR9U INTG9U MAIN9R MID9U MINET MVGA9U NEWA9U NEWN9U NPNT9U NXTA9U PGC19U PGCR9U PUTF9R PUTF9U PUTI9R PUTN9U PUTR9R REAL9U REGC9U RL1D9U ZPRT3R | COMDUM DISPLA GCPR9U GCTP9U REMARK SSWTCH STOP. TRACE | |
| EXP | CBRT3C DENL3D GMDY3C HNA13C PUMP3R TURB3R VSNK3C | | |
| FLV3T | ADV3T VOLS3T | ACOS COS DENL3D DENV3D ERR9U ESTL3H ESTV3H SIN VOLF3C | VD9V VOL3P |
| FRAC3S | SUBN3S | | GLOB3I LNK3P SEG3P SNET3P VD3V VOL3P |

3.2-21

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|--|---|------------------------------------|
| FST03R | ORDR3R | DSIZ9U GETD9U PUTD9U SPA. | LNKS31 |
| FTNRP2 | MINET | | |
| GCER9U | INIT3R | GCTE9U OUTC1. SPA. | GC9U |
| GCPR9U | ABEND1 EXIT9U | OUTC1. PRTCON | GC9U VD9V |
| GCTE9U | GCER9U GCTP9U | GOTOER. OUTC1. | GC9U |
| GCTP9U | ABEND1 EXIT9U | GCTE9U OUTC1. | GC9U |
| GENRD | CRDR9R READ3R | CDINPT ERRMSG GOTOER. INPC1. INTNDG ISTOP ITRPCK NNBLNK OUTC1. REWIND. SPA. | SAVE |
| GETA9U | AJVN3T ENET3S IOSG3T PRFL3S QBAL3S SGB3C3T | | ADAB9U |
| GETB3U | | GOTOER. SPA. | BC3P GLOB31 LNK3P VD9V |
| GETD9U | DEFP3R DMOD3R FST03R GETF9R GETI9R GETM3R GETR9R INSL9U LINK3R LSTI9U LSTM3R MARK3R MORD3R NBR3R NCLS3R NXTI9U NXTM3R NXTO3R ORDR3R PCNT3R PUTI9R RELL9U RISU9R | EXIT9U GETN9U INPT9U | DCON9U |
| GETF9R | CRDR9R | GETD9U LOCR9U | DCON9U ISUV9R |
| GETF9U | GETR9U MVGA9U REAL9U RLID9U | EXIT9U NXTA9U | NDAB9U |
| GETI9R | DMOD3R | DSIZ9U GETD9U GETR9U RLID9U | ISUV9R |
| GETM3R | LINK3R | DSIZ9U GETD9U LOCL9U OUTC1. SPA. | DCON9U LNKS31 UNIT31 |
| GETM9U | ADV3T NET3T | SPA. | ADAB9U |
| GETN9U | GETD9U INTG9U MID9U MTYP9U | EXIT9U NXTA9U | NDAB9U |
| GETR9R | DMOD3R | GETD9U LOCL9U | DCON9U ISUV9R |
| GETR9U | GETI9R PUTI9R | EXIT9U GETF9U INPT9U | DCON9U |
| GFSK3C | CRIT3C | SPA. | |
| GMDY3C | CRIT3C | EXP SPA. | |
| GOTOER. | ADV3T BCOR3C DCODNC DMOD3R DRDE3C DRDP3C ENTH3C ERRMSG | | |

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|--|--|---|
| | ETX3C GCTE9U GENRD GETB3U HTC3C IMOD3C INSTRUC MRCH3S MRCH3T NET3R PRNT3C PUMP3T PUTB3U READ3R RHO3C ROOT3C SEG3R TBSG3T TEMP3C VISC3C | | |
| GSUP3C | CRIT3C | DENV3D ESW3C SQRT SWAT3C | |
| HCAP3C | ADTB3T HX3T | | |
| HCIT3C | HTC3C | OUTF1 SPA XTOY\$ | SATM3V |
| HCOT3C | HTC3C | OUTF1 SPA SQRT XTOY\$ | SATM3V |
| HCPN3C | DREN3C HNAF3C HNAI3C | TNA3C | |
| HNAF3C | HTC3C | HCPN3C TKNA3C VSNA3C XTOY\$ | |
| HNAI3C | HTC3C | EXP HCPN3C TKNA3C VSNA3C XTOY\$ | |
| HTCA3C | HTC3C | CAIR3C CPAR3C VAIR3C XTOY\$ | |
| HTC3C | QPM3C | GOTOER HCIT3C HCOT3C HNAF3C HNAI3C HTCA3C HTNK3C HWCN3C HWF3C HWF3C HWN3C HWSC3C | MOD3I MOD3V SATM3V |
| HTNK3C | HTC3C | CDNK3C CPNK3C XTOY\$ | |
| HWCN3C | HTC3C | SQRT | SATM3V |
| HWF3C | HTC3C | CONV3K CPV3C ENTV3H OUTF1 SPA VISV3N XTOY\$ | SATM3V |
| HWF3C | BCOR3C HTC3C IMOD3C | CONL3K CPL3C VISL3N XTOY\$ | |
| HWN3C | HTC3C | CONL3K CPL3C PSAT3P SPA SQRT VISL3N XTOY\$ | SATM3V |
| HWSC3C | HTC3C | CONV3K CPV3C ENTV3H OUTF1 SPA VISV3N XTOY\$ | SATM3V |
| HXND3S | HX3S | BCOR3C IMOD3C OUTF1 QPM3C ROOT3C TCLM3C TCRG3C TEMP3C | MOD3I MOD3V NODE3I NODE3V |
| HX3R | SEG3R | INTG9U JDAT3R MARK3R MID9U MORD3R NCL53R NXM3R OUTF1 PGC19U PGC99U PUTJ3R REAL9U | |
| HX3S | MRCH3S | CROS3S DP3C ERR9U HXND3S OUTF1 RHO3C ROOT3C SATM3C | HX3P MOD3I MOD3V NODE3I NODE3V NOOL3P VD9V |

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|---|--|---|
| | | SAT03C SPA. TEMP3C VISC3C XTOY\$ | |
| HX3T | MRCH3T | BCOR3C DENS3C DP3C DRDE3C DSDP3C HCAP3C IMOD3C LOAD3T QPM3C RH03C SPA. TLM3C TCRG3C VISC3C XTOY\$ | GLOB3V HX3P MOD3I MOD3V NODE3V NODL3P VD9V |
| IGA9U | IP153R | JGCT9U | GC9U |
| ILNK3R | INRD3R | UNIQ9U | LNK53I |
| IMOD3C | HXND3S HX3T | COND3C GOTOER HWFC3C QPM3C TEMP3C XDNB3C XDRY3C | MOD3I MOD3V SATM3V |
| INA9U | ENET3S MINT3T FRFL3S QBAL3S | | ADAB9U |
| INFO | ABEND1 SDUMP | CHARCTR | ABEND |
| INGC9U | INIT3U | | GC9U VD9V |
| INIT3R | MAIN9R | CALC3R GCER9U IPT53R MVGC9U SYS3R | SCRH3R TIME3I |
| INIT3S | MINT3S | | BC3P GLOB3I LNK3P NET3P SEG3P VD9V VOL3P |
| INIT3U | MINET | INGC9U | UNIT3I |
| INIT9U | MINET | INPCI. PAGE9U SSCDAT | DATA9 UNIT9U |
| INL9U | INRD3R | UNIQ9U | LDAB9U MDAB9U |
| INM9U | INRD3R | UNIQ9U | MDAB9U |
| INN9U | INRD3R | | DCON9U NDAB9U |
| INOR3R | SYS3R | UNIQ9U | ORD3I |
| INPBI. | RECX3U REGC9U | | |
| INPBR. | REGC9U | | |
| INPCI. | GENRD INIT9U LIST3R READHM | | |
| INPT9U | DSIZ9U GETD9U GETR9U INTG9U MID9U PUTD9U PUTR9U REAL9U RLID9U | | DCON9U NDAB9U |
| INRD3R | CRDR9R | ILNK3R INL9U INM9U INN9U ISU9R IUNI9U NEWL9U PUTF9R | DCON9U SCRH3R UNIT3I |

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|----------------------------|-----------------------------|------------------------------------|
| INSL9U | DMOD3R PUTF9R PUTI9R | PUTI9R PUTR9R REPS9R | |
| INSTRUC | SDUMP | GETD9U PUTD9U | DCONGU LDAB9U |
| INTERP | COINPT | GOTOER | |
| INTG9U | BND3R CTRL3R HX3R JOAT3R | EXIT9U GETNGU INPT9U | DCONGU |
| | KPRT3R NET3R PIDS3R PIPE3R | | |
| | PUMP3R TURB3R VALV3R | | |
| | ZPRT3R | | |
| INTMOG | COINPT DCOOVC GENRD NAME4D | SPA | |
| INTP9U | PREP3T | | |
| IOSG3T | MCH3T | | |
| IPTS3R | INIT3R RECX3U | ADD99U ADDW9U DENL3D DENV3D | LNK3P MODL3P |
| | | ESTL3H ESTV3H GETA9U NEWA9U | VALV3P V09V VOL3P |
| | | PUTA9U VOL3C | |
| | | IGABU | BC3P HX3P LNK3P MODC3P |
| | | | MODL3P NET3P PUMP3P TRND3P |
| | | | SEG3P SNET3P TIME3P |
| | | | TURB3P VALV3P VOL3P |
| | | | DCONGU NDAB9U |
| IRPT9U | | | |
| ISETH1 | COINPT | | |
| ISTOP | GENRD | NNBLNK SPA | |
| ISUR | INRO3R | NEAL9U NEAP9U PUTD9U PUTR9U | DCONGU ISUW9R |
| | | UNIG9U | |
| ITRCK | COINPT GENRD | | |
| IUNISU | INRO3R | | UNID9I |
| JRNAME | | | |
| JDAT3R | HX3R NET3R | INTG9U | ORD3I |
| JGCT9U | IGABU LPNT9U PGC19U PGC9U | SPA | GC9U |
| KPRC3S | MINT3S | PRH3S | LOB3I LNK3P MODC3P NET3P |
| | | | SEG3P SNET3P V09V VOL3P |
| KPRT3R | DMOD3R VOL3R | DS179U INTG9U MID9U | LNK53I |
| | | PUTD9U SPA UNIO9U | |

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|---|---|---|
| LCNT9U | | MTYP9U NXT19U | DCON9U |
| LEQ3C | LEQ9U | SPA. | |
| LEQ9U | ENET3S NET3T PRFL3S QBAL3S | LEQ3C | ADAB9U |
| LINK3R | DMOD3R | GETD9U GETM3R MID9U OUTC1. OUTF1. PUTD9U PUTR9U | LNKS3I UNIT3I |
| LIST3R | VRFY3R | INPC1. OUTC1. PAGE9U REWIND. | UNIT3I |
| LNKN9U | NEW9U RELD9U | | NDAB9U |
| LOA03T | HX3T PIPE3T TBSG3T | ADDA9U ADDM9U PUTA9U PUTM9U SPA. | GLOB3V MOD3V NODE3V SEG3P VD9V |
| LOCL9U | DMOD3R GETM3R GETR9R | MID9U NXT19U | DCON9U |
| LOCR9U | GETF9R PUT19R | NXT19U RLID9U | DCON9U |
| LPNT9U | PUMP3R TABL9R | JGCT9U NSIZ9U | GC9U |
| LSIZ9U | SYS3R | NXT19U | DCON9U |
| LST19U | | GETD9U MID9U | DCON9U LDAB9U |
| LSTM3R | NET3R SEG3R | GETD9U | ORD3I |
| MAIN9R | MINET | CRDR9R EXIT9U INIT3R RISU9R VRFY3R | |
| MARK3R | HX3R NET3R VOL3R | DSIZ9U GETD9U PUTD9U SPA. | ORD3I |
| MOST3S | MINT3S | | GLOB3I HX3P LNK3P MODC3P SEG3P SNET3P VD9V |
| MID9U | BND3R DEFP3R HX3R KPRT3R LINK3R LOCL9U LST19U NBR3R NET3R ORDR3R PIPE3R PUMP3R SEG3R TURB3R VALV3R VOL3R | EXIT9U GETN9U INPT9U | DCON9U MDAB9U |
| MINET | | ABEND EXIT9U FTNRP2. INIT3U INIT9U MAIN9R MINT3S MINT3T OUTF1. PRNT3C RECX3U STOP. SVCX3U TIME3T | UNIT9U |
| MINT3S | MINET | BKEY3S ENET3S ERR9U INIT3S KPRC3S MOST3S MRCH3S OUTC1. OUTF1. PRFL3S PRNT3C QBAL3S QBRG3S SECOND STOP. SUBN3S VOLM3S WESM3S | GLOB3I GLOB3V UNIT3I |

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|---|---|------------------------------------|
| NEWN9U | NEWD9U NEWM9U NEWR9U PGC19U PGCR9U | EXIT9U | DCON9U NDAB9U |
| NEWR9U | PUTF9R PUT19R | NEWN9U PUTF9U | MDAB9U |
| NID9U | RELD9U | | NDAB9U |
| NNBLNK | CDINPT GENRD ISTOP | | |
| NPNT9U | SYS3R | EXIT9U SPA | GC9U |
| NSIZ9U | DSIZ9U LPNT9U MVGA9U | | DCON9U NDAB9U |
| NSK1P | CDINPT | | |
| NXTA9U | GETF9U GETN9U PUTF9U PUTN9U | EXIT9U | DCON9U NDAB9U |
| NXT19U | LCNT9U LOCL9U LOCR9U LSIZ9U RISU9R SYS3R | GETD9U | LDAB9U |
| NXTM3R | HX3R NET3R PIPE3R PUMP3R TURB3R VALV3R VOL3R | DSIZ9U GETD9U RELM9U | DCON9U ORD31 |
| NXTN9U | NEWD9U RELD9U RELM9U | | NDAB9U |
| NXT03R | ORDR3R | DSIZ9U GETD9U PUTD9U SPA | LNKS31 |
| ORDR3R | NET3R | DSIZ9U FSTC3R GETD9U MID9U NBR3R NEWM9U NXT03R OUTFI PUTD9U RELM9U UNIQ9U | DCON9U ORD31 |
| OUTBI | SVCX3U SVGC9U | | |
| OUTBR | SVGC9U | | |
| OUTCI | ABEND1 COMDUM CRDR9R DMOD3R ERRMSC ERR9U GCER9U GCPR9U GCTE9U GCTP9U GENRD GETM3R LINK3R LIST3R MINT3S PAGE9U PRNT3C PRTA9U PRTCOM READHM READ3R RECX3U SDUMP SVCX3U TRACE1 | | |
| OUTCR | ABEND1 PRTA9U | | |
| OUTFI | BCOR3C BND3R CALC3R DEFP3R DMOD3R HCIT3C HCOL3C HWFB3C HWSC3C HXND3S HX3R HX3S KPRT3R LINK3R MINET MINT3S MRCH3S MVGA9U NBR3R NET3R ORDR3R PIPE3R PJMP3R RISU9R | | |

3.2-28

| ROUTINE | REFERENCED FROM | | | | REFERENCES TO | | | | COMMON DEFINED \$ = NOT REFERENCED | | | | |
|---------|-----------------|--------|--------|--------|---------------|--------|--------|--------|------------------------------------|--------|--------|--------|--|
| | SDUMP | SEG3R | SYS3R | TCRG3C | | | | | | | | | |
| | TURB3R | VALV3R | VOLS3T | VOL3R | | | | | | | | | |
| PAGE9U | INIT9U | LIST3R | PRNT3C | RECX3U | OUTC1 | SECOND | SSCT1M | | DATA9 | UNIT9U | | | |
| | SVCX3U | | | | | | | | | | | | |
| PCNT3R | SYS3R | VOL3R | | | DS1Z9U | GETD9U | SPA | | LNKS3I | | | | |
| PGC19U | BND3R | HX3R | NET3R | PIPE3R | EXIT9U | JGCT9U | NEWN9U | PUTN9U | GC9U | | | | |
| | PUMP3R | SEG3R | TURB3R | VALV3R | | | | | | | | | |
| | VOL3R | | | | | | | | | | | | |
| PGCR9U | BND3R | HX3R | NET3R | PIPE3R | EXIT9U | JGCT9U | NEWN9U | PUTF9U | GC9U | | | | |
| | PUMP3R | SEG3R | TABL9R | TURB3R | | | | | | | | | |
| | VALV3R | VOL3R | | | | | | | | | | | |
| PIDS3R | SEG3R | VOL3R | | | INTG9U | | | | ORD3I | | | | |
| PIPE3R | SEG3R | | | | INTG9U | MID9U | MORD3R | NXTM3R | | | | | |
| | | | | | OUTF1 | PGC19U | PGCR9U | REAL9U | | | | | |
| | | | | | TABL9R | | | | | | | | |
| PIPE3S | MRCH3S | PRFL3S | | | DP3C | RH03C | SPA | TEMP3C | MOD3I | MOD3V | NODE3V | NOOL3P | |
| | | | | | | | | | VD9V | | | | |
| PIPE3T | MRCH3T | | | | DP3C | DRDE3C | DRDP3C | LOAD3T | MOD3I | MOD3V | NODE3V | NOOL3P | |
| | | | | | RH03C | SPA | | | VD9V | | | | |
| PREP3T | MINT3T | | | | ETX3C | INTP9U | | | BC3P | GLOB3I | GLOB3V | LNK3P | |
| | | | | | | | | | MODC3P | PUMP3P | TRND3P | TURB3P | |
| | | | | | | | | | VALV3P | VD9V | | | |
| PRFL3S | MINT3S | | | | ADD9U | DPSV3C | ERR9U | GETA9U | BC3P | GLOB3I | LNK3P | NET3P | |
| | | | | | INA9U | LEQ9U | MODL3C | NEWA9U | SEG3P | TURB3P | VALV3P | VD9V | |
| | | | | | PIPE3S | PUMP3S | PUTA9U | RELA9U | VOL3P | | | | |
| | | | | | RH03C | SATM3C | SATP3C | SORT | | | | | |
| | | | | | VALV3S | | | | | | | | |
| PRHX3S | KPRC3S | | | | SPA | | | | HX3P | LNK3P | SEG3P | VD9V | |
| PRNT3C | MINET | MINT3S | MINT3T | | GOTOER | OUTC1 | PAGE9U | TEMP3C | BC3P | GLOB3I | GLOB3V | HX3P | |
| | | | | | | | | | LNK3P | MODC3P | MODL3P | NET3P | |
| | | | | | | | | | NODL3P | PUMP3P | SEG3P | SNET3P | |
| | | | | | | | | | TURB3P | UNIT3I | VALV3P | VD9V | |
| | | | | | | | | | VOL3P | | | | |
| PRTA9U | | | | | OUTC1 | OUTCR | | | ACAB9U | UNIT3I | | | |
| PRTCOM | | | | | OUTC1 | SPA | | | | | | | |
| PRCON | GCPR9U | | | | OUTC1 | SPA | | | | | | | |

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|---|--|--|
| PSAT3P | H4NB3C | ESTL3H ROOT3C SPA | TMPL3T |
| PUMP3R | SEG3R | DS1Z9U EXP INTG9U LPNT9U MID9U MOR03R NXM3R OUTF1 PGC19U PGL79U REAL9U SPA TABL9R | |
| PUMP3S | MCH3S PREL3S | | MOD31 MOD3V MODL3P FUMP3P VD9V |
| PUMP3T | MCH3T | GOTOER RH03C | MOD31 MOD3V MODL3P GLOB3V PUMP3P VD9V ADAB9U |
| PUTAGU | ADVN3T ENET3S 105G3T LOAD3T NET3T PREL3S QBAL3S SGB3T | | BC3P GLOB31 LNK3P VD9V DCON9U |
| PUTB3U | | GOTOER SPA | |
| PUTD9U | DEFP3R DM003R FST03R INSL9U ISU9R KPRT3R LNK3R MARK3R NEHL9U NXT03R ORD3R PUTF9R PUTI9R PUTJ3R PUTR9R REPS9R | INPT9U NEHD9U PUTN9U | |
| PUTF9R | INRD3R | EXIT9U INSL9U NEHL9U NEAR9U PUTD9U | ISUV9R |
| PUTF9U | NEAR9U PGC99U PUTF9U | EXIT9U NXTA9U | NDAB9U |
| PUTI9R | INR03R | EXIT9U GETD9U GETR9U INSL9U LOC99U NEAR9U PUTD9U PUTR9U | DCON9U ISUV9R |
| PUTJ3R | HX3R NET3R VOL3R | PUTD9U | ORD31 |
| PUTM9U | LOAD3T | SPA | ADAB9U |
| PUTN9U | NEAR9U PGC19U PUTD9U | EXIT9U NXTA9U | NDAB9U |
| PUTR9R | INRD3R | EXIT9U INSL9U NEAR9U PUTD9U | DCON9U ISUV9R |
| PUTR9U | DM003R ISU9R LNK3R PUTI9R | INPT9U NEHD9U PUTF9U | DCON9U |
| QBAL3S | MINT3S | ADDA9U GETA9U INA9U LE09U NEWA9U PUTA9U RELA9U | GLOB31 HX3P LNK3P MODC3P NET3P SEG3P SNET3P VD9V VOL3P |
| QBRG3S | MINT3S | | GLOB31 HX3P LNK3P MODC3P NET3P SEG3P SNET3P VD9V VOL3P |
| QPM3C | BCOR3C HXND3S HX3T IMC3C | CND3C HTC3C TEMP3C | MOD31 MOD3V |

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|--|--|------------------------------------|
| RAIR3C | RHO3C | TAIR3C | |
| READHM | CDINPT | INPC1. OUTC1. REWIND. SETFMT SPA. | |
| READ3R | CRDR9R | DMOD3R GENRD GOTOER. OUTC1. | SCRH9I UNIT3I |
| REAL9U | BND3R CTRL3R HX3R PIPE3R PUMP3R TABL9R TURB3R VALV3R VOL3R ZPRT3R | EXIT9U GETF9U INPT9U | DCON9U |
| RECX3U | MINET | INPB1. IPTS3R OUTC1. PAGE9U REGC9U | GLOB3I GLOB3V UNIT3I |
| REGC9U | RECX3U | EXIT9U INPB1. INPBR. | GC9U VDSV |
| REL49U | ADVNT NET3T PRFL3S QBAL3S SGBC3T | | ADAB9U |
| RELD9U | | LNKN9U NID9U NXT9U RELN9U | DCON9U |
| RELL9U | DMOD3R RISU9R | GETD9U RELM9U | DCON9U LDAB9U |
| RELM9U | NXTM3R ORDR3R REL9U | NXT9U RELN9U | DCON9U |
| RELN9U | MVGA9U RELD9U RELM9U | | DCON9U NDAB9U |
| REMARK | EXIT9U | | |
| REPEAT | CDINPT | SPA. | |
| REPS9R | INRD3R | PUTD9U | ISUV9R |
| REWIND. | GENRD LIST3R READHM SVCX3U | | |
| RHNK3C | RHO3C VSNK3C | TMNK3C | |
| RHO3C | ADVNT DPSV3C DP3C HX3S HX3T PIPE3S PIPE3T PRFL3S PUMP3T TBSG3S TBSG3T VALV3T VOLM3S | DENL3D DENV3D ESTL3H ESTV3H GOTOER. RAIR3C RHNK3C RNA3C | SATM3V |
| RISU9R | MAIN9R | GETD9U NXT19U OUTF1. REL9U | DCON9U ISUV9R |
| RLID9U | GET19R LOCR9U | EXIT9U GETF9U INPT9U | DCON9U MDAB9U |
| RNA3C | RHO3C | TNA3C | |
| ROOT3C | BCOR3C HXND3S HX3S PSAT3P | GOTOER. | |
| SATM3C | HX3S MRCH3S MRCH3T PRFL3S | | SATM3V SATP3V |

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|---|--|--|
| SAT03C | HX3S | CONL3K CPL3C DENL3D DENV3D ESTL3H ESTV3H STEN3S TMLP3T VISL3N VISV3N | SATH5V |
| SATP3C | MRCH3S MRCH3T PRFL3S | CONL3K CPL3C DENL3D DENV3D ESTL3H ESTV3H STEN3S TMLP3T VISL3N VISV3N | SATP3V |
| SDEL9T | TIME3T | | TIME3I TIME3P VD9V |
| SDUMP | ABEND1 | CHARCTR CODEB INFO INSTRUC OUTC1. OUTF1. SSWTCH | ABEND |
| SECOND | MINT3S PAGE9U | | |
| SEG3R | NET3R | GOTOER. HX3R LSTM3R M109U MOR03R MTYP9U OUTF1. PGT19U PGCR9U PIDS3R PIPE3R PUMP3R SPA. TURB3R VALV3R ZPRT3R | |
| SETFMT | READHM | | |
| SFWT3C | ESW3C SWAT3C | | |
| SGBC3T | MRCH3T | ADDA9U GETA9U PUTA9U RELA9U SPA. | BC3P GLOB3V LNK3P SEG3P TRND3P VD9V |
| SGWT3C | ESW3C SWAT3C | | |
| SIN | CBRT3C FLV3T VOLF3C | | |
| SPA. | ABEND1 ADDM9U BCOR3C CBRT3C CRKR3T DEFP3R ENTL3H ENTV3H ESW3C FST03R GCER9U GENRD GETB3U GETM3R GETM9U GFSK3C GMDY3C HCLT3C HCOL3C HWFB3C HWNB3C HWSC3C HX3S HX3T INTERP INTNDG ISTOP JGCT9U KPRT3R LEQ3C LOAD3T MARK3R NAMEWD NBR3R NET3R NEWA9U NPNT9U NXT03R PCNT3R PIPE3S PIPE3T PRHX3S PRTCOM PSAT3P PUMP3R PUTB3U PUTM9U READHM REPEAT SEG3R SGBC3T SWAT3C TRACE1 ZPRT3R | | |
| SQRT | CBRT3C G5UP3C HCOL3C HWCN3C HWNB3C MODL3C PRFL3S TBSG3S TBSG3T XDNB3C | | |
| SSCDAT | INIT9U | DATE | |

3.2-32

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|--|--|---|
| SSCTIM | PAGE9U | TIME | |
| SSWCH | ABEND1 EXIT9U SDUMP | | |
| STEN3S | SAT03C SATP3C | | |
| STOP | CRDR9R EXIT9U MINET MINT3S | | |
| SUBN3S | MINT3S | ERR9U FRAC3S | BC3P V09V GLOB3I VOL3P NET3P SNET3P |
| SVCX3U | MINET | OUTB1 OUTC1 PAGE9U REWIND. SVC09U | GLOB3I GLOB3V UNIT3I |
| SVGC9U | SVCX3U | OUTB1 OUTBR. | GC9U VD9V |
| SWAT3C | ESW3C GSUP3C TBSG3S TBSG3T | ESTL3H ESTV3H SFWT3C SGWT3C SPA TPL3T | |
| SYS3R | INIT3R | INOR3R LS129U NET3R NPNT9U NXT19U OUTF1 PCNT3R | DCON9U GLOB3I GLOB3V |
| TABL9R | BND3R CTRL3R PIPE3R PUMP3R TURB3R VALV3R VOL3R | DS129U LPNT9U PGR9U REAL9U | |
| TAIR3C | CAIR3C CPAR3C DREA3C DRPA3C RAIR3C TEMP3C VAIR3C | CBRT3C | |
| TBSG3S | MRCH3S | ENTH3C ESW3C RH03C SQRT SWAT3C TEMP3C | MOD3I MOD3V NODE3V NOOL3P SEG3P TURB3P V09V |
| TBSG3T | MRCH3T | ESW3C GOTOER LOAD3T RH03C SQRT SWAT3C | GLOB3V MOD3I MOD3V NODE3V NOOL3P SEG3P TURB3P V09V |
| TCLM3C | HXND3S HX3T | | |
| TCRG3C | HXND3S HX3T | OUTF1 | |
| TEMP3C | ADV3T BCOR3C CROS3S ETX3C HXND3S HX3S IMOD3C PIPE3S PRNT3C QPM3C TBSG3S VOLM3S | ESTL3H ESTV3H GOTOER TAIR3C TMNK3C TPL3T TMPV3T TNA3C | SATM3V |
| THOM3C | DP3C | ALOG XTOYS | |
| TIME | SSCTIM | | |
| TIME3T | MINET | SDEL9T | GLOB3V TIME3I TIME3V |
| TKNA3C | HNAF3C HNA13C | TNA3C | |
| TMNK3C | CDNK3C CPNK3C DRNK3C RHNK3C | CBRT3C | |

| ROUTINE | REFERENCED FROM | | | | REFERENCES TO | | | | COMMON DEFINED \$ = NOT REFERENCED | | | | |
|---------|------------------|------------------|------------------|--------|---------------|--------|--------|--------|------------------------------------|--------|-------|--------|--------|
| | TEMP3C | VSNA3C | | | | | | | | | | | |
| TPL3T | ENTH3C SATP3C | ENTL3H SWAT3C | PSAT3P TEMP3C | SAT03C | | | | | | | | | |
| TMPV3T | CONV3K VISV3N | ENTV3H | SWAT3C | TEMP3C | | | | | | | | | |
| TNA3C | DREN3C TKNA3C | HCPN3C VSNA3C | RNA3C | TEMP3C | CBRT3C | | | | | | | | |
| TRACE | EXIT9U | | | | TRACE1 | | | | | | | | |
| TRACE1 | ABEND1 | TRACE | | | CHARCTR | OUTC1 | SPA | | | ABEND | | | |
| TURB3R | SEG3R | | | | COS | DSIZ9U | EXP | INTG9U | | | | | |
| | | | | | MID9U | MORD3R | NXTM3R | OUTF1 | | | | | |
| | | | | | PGC19U | PGCR9U | REAL9U | TABL9R | | | | | |
| UNIT9U | ILNK3R ISU9R | INL9U KPRT3R | INM9U ORDR3R | INOR3R | | | | | | UNIT9I | | | |
| VAIR3C | HTCA3C | VISC3C | | | TAIR3C | | | | | | | | |
| VALV3R | SEG3R | | | | DSIZ9U | INTG9U | MID9U | MORD3R | | | | | |
| | | | | | NXTM3R | OUTF1 | PGC19U | PGCR9U | | | | | |
| | | | | | REAL9U | TABL9R | | | | | | | |
| VALV3S | MRCH3S | PRFL3S | | | CRIT3C | XTOY\$ | | | | MOD3I | MOD3V | NODL3P | VALV3P |
| | | | | | | | | | | VD9V | | | |
| VALV3T | MRCH3T | | | | CRIT3C | RHO3C | XTOY\$ | | | GLOB3V | MOD3I | MOD3V | NODL3P |
| | | | | | | | | | | VALV3P | VD9V | VOL3P | |
| VISC3C | DP3C | HX3S | HX3T | | ESTL3H | ESTV3H | GOTOER | VAIR3C | | SATM3V | | | |
| | | | | | VISL3N | VISV3N | VSNA3C | VSNA3C | | | | | |
| VISL3N | HWF3C VISC3C | HWNB3C | SAT03C | SATP3C | | | | | | | | | |
| VISV3N | HWF3C VISC3C | HWSC3C | SAT03C | SATP3C | DENV3D | TMPV3T | | | | | | | |
| VOLF3C | ENET3S WESM3S | EVLV3S | FLV3T | IOSG3T | ACOS | SIN | | | | | | | |
| VOLM3S | MINT3S | | | | DRDE3C | DRDP3C | RHO3C | TEMP3C | | GLOB3I | NET3P | VD9V | VOL3P |
| VOLS3T | MINT3T | | | | ESTL3H | ESTV3H | FLV3T | OUTF1 | | GLOB3I | VD9V | VOL3P | |
| VOL3R | NET3R | | | | INTG9U | KPRT3R | MARK3R | MID9U | | | | | |

3.2-33

| ROUTINE | REFERENCED FROM | REFERENCES TO | COMMON DEFINED \$ = NOT REFERENCED |
|---------|---|---|--|
| | | MORD3R NXTM3R OUTF1 PCNT3R PGC19U PGCR9U PIDS3R PUTJ3R REAL9U TABL9R ZPRT3R | |
| VRFY3R | MAIN9R | LIST3R | |
| VSNA3C | HNAF3C HNA13C VISC3C | ALOG1B TNA3C XTOY\$ | |
| VSNK3C | VISC3C | EXP RHNK3C TMNK3C XTOY\$ | |
| WESM3S | MINT3S | DENL3D DEPV3D ESTL3H ESTV3H ETX3C VOLF3C | BC3P GLOB3I LNK3P MODL3P NET3P SEG3P SNET3P VD9V VOL3P |
| XDNB3C | BCOR3C IMOD3C | SORT XTOY\$ | |
| XDRY3C | BCOR3C IMOD3C | XTOY\$ | |
| XTO1\$ | CBRT3C DCCDNC | | |
| XTOY\$ | CONV3K DP3C ESTL3H ESTV3H HC1T3C HCOT3C HNAF3C HNA13C HTCA3C HTNK3C HWFB3C HWFC3C HWNB3C HWSC3C HX3S HX3T THOM3C VALV3S VALV3T VSNA3C VSNK3C XDNB3C XDRY3C | | |
| ZPRT3R | SEG3R VOL3R | DSIZ9U EXIT9U INTG9U REAL9U SPA | LNKS3I |

3.2.2 SUBROUTINE AND FUNCTION DESCRIPTION

A computer generated subroutine and function description is provided in Table 3.2-1. Following each name are two letters. The first indicates module type (S denotes subroutine, F denotes function), while the second letter indicates to which major code division each module belongs (U -utility, P -property, S -steady-state, T - transient, C - common to S and T, I - input processor). Also included is a brief description of each module's use.

3.2.3 FOCUS ON SELECTED AREAS

There are several areas in the MINET code that require somewhat greater explanation than is provided elsewhere in this document. In some cases the explanation is needed because of local complexities that can be very confusing, if not fully explained. In other cases, a large number of functions and/or utilities can be overwhelming until they are integrated conceptually into a special purpose package. In this section, we will try to bridge some of the gaps, in order to clarify certain points.

Table 3.2-1 Subroutine & Function Description

ABEND S U SUPPLEMENT CDC SYSTEM ERROR DIAGNOSTICS AFTER CRASH
 ABEND1 S U CALLED BY ABEND AFTER A FATAL EXECUTION ERROR
 ADDA9U S U ADDS ENTRY TO CURRENT VALUE IN DESIGNATED POSITION IN DESGNTD ARRAY
 ADDM9U S U ADDS FLOATING POINT DATA VALUE TO CURRENT SPCD ENTRY IN SPCFD ARRAY
 ADTB3T S T ADVANCES HEAT EXCHNGR TUBE TEMPERATURES AT END OF TIME STEP
 ADVN3T S T ADVANCES NETWORK CONDITIONS AFTER NETWORK VOLUME EQNS ARE SOLVED
 BCOR3C S C BOUNDS THE ENTHALPY FOR CURRENT HEAT TRANSFER MODES, SETTING SWITCHPTS
 BKEY3S S S DETERMINES WHICH HEAT TRANSFER BRIDGES ARE TO BE ADJUSTED
 BND3R S I PROCESS BOUNDARY MODULE INPUT DATA
 CAIR3C F P CALCULATES AIR THERMAL CONDUCTIVITY
 CALC3R S I PERFORM INPUT PROCESSOR POST-PARSE CALCULATION
 CBRT3C S U SOLVES FOR ROOTS OF CUBIC POLYNOMIAL
 CDINPT S I DECODES AND STORES FREE-FORMAT INPUT
 CDNK3C F P THERMAL CONDUCTIVITY OF NAK
 CHARCTR U PART OF ABEND ERROR DIAGNOSTIC PACKAGE
 CODEB F U RETURNS NUMBER IN BASE B, INITIALLY IN BASE 10
 COMGUM S U WRITES OUT CONTENTS OF COMMON BLOCKS NOT WITHIN GLOBAL CONTAINER ARAY
 COND3C F P THERMAL CONDUCTIVITY OF STRUCTURAL MATERIALS, INCL HX TUBING
 CONL3K F P THERMAL CONDUCTIVITY OF SUBCOOLED WATER FOR ENTHALPY, PRESSURE
 CONV3K F P THERMAL CONDUCTIVITY OF SUPERHEATED STEAM FOR ENTHALPY, PRESSURE
 CPAR3C F P SPECIFIC HEAT OF AIR, CONSISTANT WITH TEMPERATURE FUNCTION
 CPL3C F P SPECIFIC HEAT OF SUBCOOLED WATER FOR GIVEN ENTHALPY, PRESSURE
 CPNK3C F P SPECIFIC HEAT OF NAK
 CPV3C F P SPECIFIC HEAT OF SUPERHEATED STEAM FOR GIVEN ENTHALPY, PRESSURE
 CROR9H S I CONTROLB PROCESS OF READING INPUT CARDS
 CRIT3C F P CRITICAL FLOW RATE FOR WATER/STEAM, CALLS CFSK3C, GMDY3C, GSUP3C.
 CRKR3T S T SOLVE SEGMENT MATRIX EQUATION
 CRKR3U S U CONVERTS ARRAYS FROM SEGMENT MATRIX EQN AND CALLS CRKR3T TO SOLVE
 CROS3S S S WHEN NON-PHYSICAL HX CONDITION, CROS3S SET NODAL ENTHALPIES AT ESTIMAT
 CTRL3R S I PROCESSES THE RUN CONTROL INPUT RECORDS
 DCODNC S I DECODES ARRAY B TO FORM NUMERIC CONSTANT, PART OF FREE-FORMAT READ PAK
 DEFP3R S I DEFINES A NEW PORT FOR MODULE
 DENL3D S P DENSITY OF SUBCOOLED WATER FOR GIVEN ENTHALPY, PRESSURE
 DENS3C F P DENSITY OF STRUCTURAL MATERIALS, INCL HT XCHNGR TUBING
 DENV3D F P DENSITY OF SUPERHEATED STEAM FOR GIVEN ENTHALPY, PRESSURE
 DMOD3R S I CONSTRUCTS NEW DATA MODULE FOR GIVEN DATA RECORD
 DPSV3C S C CALCULATES PRESSURE DIFFERENCE BETWEEN JUNCTION AND VOLUME AVERAGE
 DP3C S C DETERMINES PRESSURE CHANGE PARAMETRS FOR NOD; GRAV, FRIC, ACCEL, FORM
 DRDE3C F P DERIVATIVE OF DENSITY WITH RESPECT TO ENTHALPY FOR GENERIC FLUID
 DRDP3C F P DERIVATIVE OF DENSITY WITH RESPECT TO PRESSURE FOR GENERIC FLUID
 DREA3C F P DERIVATIVE OF DENSITY WITH RESPECT TO ENTHALPY FOR AIR
 DREN3C F P DERIVATIVE OF DENSITY WITH RESPECT TO ENTHALPY FOR SODIUM
 DRNK3C F P DERIVATIVE OF DENSITY WITH RESPECT TO ENTHALPY FOR NAK
 DRPA3C F P DERIVATIVE OF DENSITY WITH RESPECT TO PRESSURE FOR AIR
 DSIZ9U S U RETURNS THE SIZE OF THE SPECIFIED DATA FIELD IN SPECIFIED MODULE
 EAIR3C F F ENTHALPY OF AIR FOR GIVEN TEMPERATURE, PRESSURE
 ENA3C F P ENTHALPY OF SODIUM FOR GIVEN TEMPERATURE, PRESSURE
 ENET3S S S DETERMINES STEADY STATE ENTHALPY AND HEAT TRANSFER DISTRIBUTION
 DEGP3R F P DERIVATIVE OF SATURATED STEAM ENTHALPY WITH RESPECT TO PRESSURE
 ENNK3C F P ENTHALPY OF NAK FOR GIVEN TEMPERATURE, PRESSURE
 ENTH3C F P ENTHALPY OF GENERIC FLUID FOR GIVEN TEMPERATURE, PRESSURE, FLUID TYPE
 ENTL3H F P ENTHALPY OF SUBCOOLED WATER FOR TEMPERATURE, PRESSURE
 ENTV3H F P ENTHALPY OF SUPERHEATED STEAM FOR TEMPERATURE, PRESSURE
 ERRMSG S I WRITES ERROR MESSAGE, CALLED BY CDINPT AND GENRD
 ERR9U S U WRITES A NON-TERMINAL ERROR MESSAGE IN WRITTEN OUTPUT FILE
 ESTL3H F P ENTHALPY OF SATURATED LIQUID WATER FOR GIVEN PRESSURE
 ESTV3H F P ENTHALPY OF SATURATED VAPOR WATER FOR GIVEN PRESSURE
 ESW3C F P ENTHALPY OF WATER/STEAM FOR GIVEN ENTROPY, PRESSURE
 ETX3C S C LOADS BOUNDARY ENTHALPY, TEMPERATURE, AND QUALITY ARRAYS
 EVLV3S S S CALCULATES VOLUME AVERAGE ENTHALPY GIVEN LIQUID LEVEL, VOLUME SHAPE
 EXIT9U S U TERM, NATION ROUTINE, IF CRASHED, IT PRINTS COMMON BLOCK VALUES
 FLV3T S T ADVANCES THE LIQUID LEVEL IN VOLUME WITH SEPARATED PHASES
 FRAC3S S S USED WITH SUBN3S TO TRACE BACK FLUID SOURCE FOR SEGMENTS, VOLUMES
 FSTO3R S I RETURNS PORT IDENTIFIER OF FIRST OUTLET PORT IN MODULE
 GCER9U S U TEST FOR GLOBAL CONTAINER ALLOCATION ERRORS
 GCPR9U S U PRINTS THE ENTIRE GLOBAL CONTAINER ARRAY
 GCTP9U S U PRINTS THE ENTIRE GLOBAL CONTAINER TABLE
 GENRD S I THE MAIN CONTROL UNIT OF THE CARD INPUT PROCESSOR
 GETA9U S U RETRIEVES ENTRY IN DESIGNATED POSITION IN DESIGNATED ARRAY
 GETB3U S U HOST CODE INTERFACE TO RETURN DATA VALUE ASSOCIATED WITH BOUNDARY
 GETD9U S U RETRIEVES VALUES FROM THE MODULE DATA AREA SPECIFIED
 GETF9R S I OPEN A FILE SPECIFICATION ENTRY CORRESPONDING TO GIVEN FILE ID
 GETF9U S U RETRIEVES FLOAT PT DATA FROM NODAL STORAGE AREA DESIGNATED
 GCTE9U S U PRINTS ENTRY IN GLOBAL CONTAINER ARRAY

GET19R S I GET PARAMETERS FOR NEXT ITEM SPECIFICATION IN CURRNT OPN RCRD SPCFCN
 GETM3R S I GET MODULE FROM GEOMETRIC DATA LIST
 GETM9U S U GETS DATA ENTRY VALUE FROM SPECIFIED PLACE IN SPECIFIED ARRAY
 GETN9U S U RETRIEVES A GROUP OF INTEGER VALUES FROM NODAL STORAGE AREA DESIGNATED
 GETR9R S I RETRIEVES DATA FROM RECORD SPECIFICATION ENTRY
 GETR9U S U RETRIEVES REAL VALUES FROM DESIGNATED MODULE DATA AREA
 GFSK3C F P CRITICAL MASS VELOCITY FOR SUBCOOLED WATER, USES EXTEND HENRY-FAUSKE
 GMDY3C F P CRITICAL MASS VELOCITY FOR WATER/STEAM MIX, USES MOODY MODEL
 GSUP3C F P CRITICAL MASS VELOCITY FOR SUPERHEATED STEAM, ISENTROPIC MODEL
 HCAP3C F P HEAT CAPACITY (SPC HT) OF STRUCTURAL MATERIALS
 HC1T3C F P HEAT TRANSFER COEFFICIENT CONDENSING INSIDE HORIZONTAL TUBES
 HCO13C F P HEAT TRANSFER COEFFICIENT CONDENSING OUTSIDE (ON) HORIZNTL TUBE BANKS
 HCPN3C F P HEAT CAPACITY/SPECIFIC HEAT OF SODIUM
 HNAF3C F P HEAT TRANSFER COEFFICIENT FOR SODIUM PASSING OUTSIDE TUBES
 HNAI3C F P HEAT TRANSFER COEFFICIENT FOR SODIUM PASSING INSIDE TUBES
 HTCA3C F P HEAT TRANSFER COEFFICIENT FOR AIR PASSING OVER HEATED TUBES
 HTC3C F P HEAT TRANSFER COEFFICIENT FOR GENERIC FLUID; CALLS OTHER H FUNCTIONS
 HTNK3C F P HEAT TRANSFER COEFFICIENT FOR NAK, INSIDE OR OUTSIDE TUBES
 HWCN3C F P HEAT TRANSFER COEFFICIENT IN CONDENSING MODE, VERT SURFAC, FILM THICKNS
 HWF3C F P HEAT TRANSFER COEFFICIENT FOR FILM (WATER) BOILING, BISHOP CORRELATION
 HWF3C F P HEAT TRANSFER COEFFICIENT FOR SUBCOOLED WATER BY FORCED CONVECTION
 HWNB3C F P HEAT TRANSFER COEFFICIENT FOR NUCLEATE BOILING, INCL SUBCOOL'DvTWO-PHAS
 HWC3C F P HEAT TRANSFER COEFFICIENT FOR SUPERHEATED (STEAM) CONVECTION
 HXND3S S S PERFORMS NODAL ENERGY BALANCE CALCULATION FOR HX NODES
 HX3R S I PROCESSES HEAT EXCHANGER MODULE INPUT DATA
 HX3S S S HEAT EXCHANGER TEMPERATURE AND HEAT TRANSFER CALCULATIONS
 HX3T S I TRANSIENT CALCULATIONS FOR HT XCHNGR, NODE AVERAGE HEAT TRANSFER CALCD
 IG9U F U RETURNS GLOBAL ARRAY POINTER CORRESPONDING TO GIVEN CHARACTER STRING
 ILNK3R S I INITIALIZE MODULE LINKAGE FUNCTION CODE
 IMOD3C S C DETERMINES APPROPRIATE HEAT TRANSFER CORRELATION UNDER GIVEN CNDTIONS
 INA9U S U INITIALIZES THE ARRAY DATA ABSTRACTION
 INFO S U CALLED BY ABEND1, SDUMP, CONVERT WORD TO CHARACTER STRING.
 INGC9U S U INITIALIZES THE GLOBAL CONTAINER MANAGEMENT UTILITY
 INIT3R S I CONTROLS INITIALIZATION OF MINET INPUT DATA
 INIT3S S S INITIALIZE VOLUME, SEGMENT FLOWS, PRESSURES, ENTHALPIES FOR ITERATIVE
 INIT3U S U INITIALIZE I/O UNIT NUMBERS, GLOBAL CONTAINER ARRAY
 INIT9U S U READS THE TITLE CARD IN THE INPUT DECK
 INL9U S U INITIALIZES LIST TYPE DATA ABSTRACTION
 INM9U S U INITIALIZES THE MODULE DATA ABSTRACTION
 INN9U S U INITIALIZES NODE DATA ABSTRACTION
 INDR3R S I INITIALIZE MODULE ORDERING CODE
 INPT9U F U SCANS NODE CHAIN FOR NODE WITH GIVEN ID, RETURNS ARRAY POINTER
 INRD3R S I INITIALIZES MINET INPUT DATA READER
 INSL9U S U PLACES AN ITEM IN LIST AFTER LAST PREVIOUS ENTRY
 INSTRUCS U PART OF ABEND PACK, DECODES SUBROUTINE INSTRUCTIONS.
 INTERP S I PERFORMS THE REAL-INTERPOLATE OPERATION, PART OF FREE-FORMAT READ PAKG
 INTG9U F U RETURNS AN INTEGER VALUE FROM DESIGNATED PLACE IN MODULE DATA AREA
 INTNDG F I CHECKS IF ARRAY CONTAINS DIGIT STRING FOLLOWED BY NON DIGIT, FREE FRMT
 INTP9U S U INTERPOLATES TABULAR FUNCTIONS
 IOSG3T S T SETS UP SEGMENT RESPONSE MATRICE, LOADS SEG IN, OUT EQUATIONS, MOMENTUM
 IPTS3R S I SUBROUTINE SETS ! POINTERS FOR VARIABLE IN GLOBAL CONTAINER
 IRPT9U F U SCANS NODE CHAIN FOR NODE WITH GIVEN REAL NO. ID, RETURNS ARRAY POINTR
 ISETHM F I CALCS PARAMTRS NEEDED TO PROC A HOLERITH MESSG ON CARD IMAGE
 ISTOP F I TESTS IF FIRST NON-BLANK CHARCTRS ON CARD SPELL STOP
 ISU9R S I INITIALIZES INPUT SPECIFICATION UNIT MODULE CODE
 ITRPCK F I CHECKS INTERPOLATE FLAG TO DECIDE IF REAL-INTERP OPRATN CAN BE PRFRMD
 IUN19U S U INITIALIZES A UNIQUE NUMBER GENERATOR
 JENAME S U RETURNS JOENAME TO THE USER
 JDAT3R S I RETURNS INTEGER DATUM ASSOCIATED WITH MODULE
 JGCT9U F U RETRIEVE THE INDEX (OF THE ARRAY ENTRY IN CONTAINER) FOR VARIABLE NAMED
 KPRC3S S S SETS THE PRINCIPAL SUBNET NO. FOR SEGMENTS, VOLUMES, HEAT EXCHANGERS
 KPRT3R F I RETURNS DATA AREA ID FOR PORT PREVIOUSLY DEFINED BY DEFP3R
 LCNT9U F U RETURNS A COUNT OF THE NO. OF ITEMS IN LIST OF GIVEN MODULE TYPE
 LEQ3C S U SOLVES A SYSTEM OF LINEAR EQNS (MATRIX) BY GAUSSIAN ELIMINATION
 LEQ9U S U SOLVES MATRIX EQUATION OF ARRAY DATA ABSTRACTION FORM, CALLS LEQ3C
 LINK3R S I GENERATES GEOMETRIC LINKS FOR SYSTEM DATA MODULES
 LIST3R S I PRINTS FORMATTED LISTING OF MINET INPUT DATA FILE
 LNKN9U S U INSERTS LINK INFO INTO NODAL STORAGE SPACE, DIRECTS TO NEXT ONE
 LOAD3T S T LOADS NODAL CONSERVATION EQNS INTO SEGMENT MATRIX EQN
 LOCL9U F U SCAN THE LIST TO FIND ITEM WITH GIVEN MODID, RETURN THE POINTER
 LOCR9U F U LOCATE THE MODULE WITH REAL TYPE ID DESIGNATED, RETURN THE POINTER
 LPNT9U F U RETURNS LENGTH OF GLOBAL CONTAINER ARRAY
 LSIZ9U F U RETURNS SIZE OF LIST, WHERE SIZE IS THE NUMBER OF ITEMS CONTAINED
 LST19U F U RETURNS THE POINTER FOR THE PREVIOUS ITEM IN LIST
 LSTM3R S I RETURNS POINTER TO LAST-VISITED MODULE IN ORDER SET

MAIN9R S I INPUT PROCESSOR SUB-DRIVER
 MARK3R F I RETURN MODULE MARK STATUS FOR GIVEN MARK VALUE
 MDST3S S S SETS MODULE PRESSURES, FLOWS, AND ENTHALPIES
 MID9U F U RETURNS THE MODULE ID INDICATED BY GIVEN POINTER
 MINET P C MAIN PROGRAM, CALLS DRIVERS AND MANAGES EXECUTION
 MINT3S S S DRIVER FOR STEADY STATE CALCULATIONS
 MINT3T S T DRIVER FOR TRANSIENT CALCULATIONS
 MODL3C S C CALCULATES MODULE SCRATCH PARAMETERS FRM MOD VALUES, EG, AREA FRM DIAM
 MORD3R F I RETURN MODULE ORDINAL WITHIN MODULE ORDER SET
 MRCH2S S S MARCHES THROUGH SEGMENT MODULES, INITIALIZING AND CALCING PRESR LOSSES
 MRCH3T S T MARCHES THROUGH SEGMENT MODULES, DETERMINING SEGMENT RESPONSE MATRICES
 MTYPE9U F U RETURNS AN INTEGER ENCODED TYPE NUMBER FOR MODULE GIVEN BY POINTER
 MVG9BU S U MOVE ENTIRE GLOBAL ARRAY FROM DYNAMIC STORAGE INTO CONTAINER
 MVGC9U S U MOVES THE GLOBAL CONTAINER FROM DYNAMIC TO STATIC STORAGE
 NAME9D F I CHECKS IF L CHRCTRS IN ARRAY A, FORM LETTER-ALFANUMRC STRING, FREE FRMT
 NBS9R S I RETURNS LINK TO PORT IN NEIGHBORING MODULE, AS DEFINED BY INPUT LINKAGE
 NCLS3R F I RETURNS PORT CLASS NUMBER FOR MODULE IN CURRENT ORDER SET
 NET3R S I PROCESSES NETWORK INPUT DATA
 NET3T S T CALCULATE NEW PRESSURES AND ENTHALPIES FOR NETWORK VOLUMES
 NEW9BU S U CONSTRUCTS A MATRIX IN DATA ABSTRACTION STORAGE ARRAY
 NEW9BU S U CREATES A NEW DATA AREA FOR MODULE, ASSIGNS GIVEN DATA ID
 NEWL9U S U CREATES A NEW INSTANCE OF LIST, RETURNING A POINTER FOR IT
 NEWMBU F U CONSTRUCTS NEW INSTANCE OF MODULE WITH GIVEN ID AND TYPE
 NEWNBU F U CREATES NEW NODE STORAGE SPACE AND RETURNS POINTER FOR IT
 NEW9BU F U CREATES NEW INSTANCE OF MODULE WITH REAL TYPE MODULE ID
 NID9U F U RETURNS THE NODE ID VALUE FOR GIVEN NODE
 NNBLNK F I SEARCHES GIVEN ARRAY FOR A NON-BLANK CHARACTER, PART OF FREE-FORMAT PK
 NPNT9U F U ALLOCATES A NEW POINTER INTO THE GLOBAL CONTAINER ARRAY
 NSI29U F U RETURNS THE SIZE OF THE DATA AREA ALLOTTED FOR GIVEN NODE
 NSKIF F I PERFORMS THE SKIP-WORDS OPERATION, CALLED BY CDINPT
 NXT9BU F U RETURNS POINTER TO NEXT ATOM IN CHAIN, IF LAST ATOM, EXTENDS THE CHAIN
 NXT19U F U RETURNS THE POINTER FOR THE NEXT ITEM IN THE LIST
 NXTM9R G I RETURNS POINTER TO NEXT MODULE IN ORDER SET
 NXTNDU F U RETURNS THE VALUE IN THE NEXT FIELD OF THE GIVEN NODE DATA AREA
 NYT03R S I RETURNS PORT ID OF NEXT AVAIL OUTLT PRT CORRESPONDING TO GIVN INLT PRT
 JORD3R S I INITIALIZES ORDERED SET OF MODULES USING BACKTRACK REVERSAL
 PAGE9U S U PRINTS THE PAGE HEADING
 PCNT3R S I RETURN MODULE PORT COUNTS, E.G., NO. INLET, OUTLET, FREE INLET, FREE OUTLET
 PGCI9U S U PUTS AN INTEGER VALE IN NAMED GLOBAL CONTAINER ARRAY
 PGCR9U S U PUTS A REAL VALUE IN NAMED GLOBAL CONTAINER ARRAY
 PIDS3R F I RETURNS INLET AND OUTLET PORT IDENTIFIERS FOR CURRENT MOD IN ORDER
 PIPE3R S I PROCESSES PIPE MODULE INPUT DATA
 PIPE3S S S INITIALIZES THE PIPE MODULES, PIPE-PART OF VALVE AND PUMP MODULES
 PIPE3T S T PERFORMS TRANSIENT CALCULATION FOR PIPE MODULE, PIPE-PART OF VALV, PUMP
 PREP3T S T STARTS TIME STEP CALCULATIONS, ADVANCES BOUNDARY CONDITIONS, ETC
 PRFL2S S S PERFORMS STEADY STATE NETWORK PRESSURE AND FLOW BALANCE
 PRHX2S S S TADS HEAT EXCHANGER SIDE WITH SUBNET NUMBER
 PRNT3C S C PRINTS OUT CURRENT CONDITIONS IN SYSTEM, STEADY STATE AND TRANSIENT
 PRTABU S U FORMATTED PRINTER FOR ARRAYS IN DATA ABSTRACTION FORM
 PRTCOM S U PRINTS OUT COMMON AREA WITH VARIABLE NAMES
 PSAT3P F P SATURATION PRESSURE (WATER) FOR GIVEN TEMPERATURE (AND PRES. ESTIMAT)
 PUMP3R S I PROCESSES PUMP MODULE INPUT DATA
 PUMP3S S S INITIALIZES CONDITIONS IN PUMP MODULE, DETERMINES PRESSURE CONTRIBUTION
 PUMP3T S T PERFORMS TRANSIENT PUMP CALCULATIONS, CURRENT HEAD CONTRIBUTION
 PUT9BU S U PLACES ENTRY INTO DESIGNATED POSITION IN DESIGNATED MATRIX
 PUTB3U S U HOST CODE INTERFACE TO ASSIGN DATA VALUE ASSOC'D WITH BOUNDARY
 PUTDBU S U PLACES A GROUP OF VALUES IN DATA AREA FOR MODULE
 PUTF9R S I PUT NEW FILE SPECIFICATION ENTRY IN DATA BASE
 PUTF9U S U PLACES A GROUP OF FLOATING PT DATA INTO NODAL STORAGE AREA DESIGNATED
 PUTI9R S R PUT NEW INTOR ITEM SPECIFCTN ENTRY IN CURRNTL OPEN RECORD SPECIFICCTN
 PUTJ3R S I STORE INTEGER DATUM VALUE ASSOCIATED WITH MODULE
 PUTMBU S U PUTS DATA ENTRY IN ARRAY, IN GIVEN POSITION
 PUTNBU S U PLACES A GROUP OF INTEGER DATA INTO NODAL STORAGE AREA INDICATED
 PUTR9R S I PUT NEW RECORD SPECIFCTN ENTRY IN CURRNTL OPEN FILE SPECIFICATION
 PUTR9U S U PLACES A GROUP OF VALUE IN DESIGNATED MODULE DATA AREA
 QBAL3S S S ADJUSTS ENERGY TRANSFERS NEEDED TO FIT SUBNET NEEDS
 QBRG3S S S DETERMINES $Q3-HBRG(I,J)$ =TOTAL Q TRANSFERRED INTO SNT I FROM SUBNET J
 QPM3C F C DETERMINE HEAT TRANSFER FROM TUBE CENTER TO FLUID, PER METER OF TUB LNG
 RAIR3C F P DENSITY OF AIR
 READHM S I READS HOLERITH MESSAGE, FROM CARD IMAGE, INTO WORD ARRAY
 READ3R S I PROCESSES INPUT FROM THE FREE-FORMAT INPUT CARDS
 REAL9U F U RETURNS A REAL VALUE FROM DESIGNATED PLACE IN MODULE DATA AREA
 RECX3U S U RESTORES GLOBAL L VARIABLES AND ARRAYS FROM RESTART FILE
 RECC9U S U RESTORE GLOBAL CONTAINER CONTEXT FROM SAVE FILE
 REL9BU S U RELEASES PREVIOUSLY USED STORAGE SPACE IN DATA ABSTRACTION DATA ARRAY

RELE9U S U RELEASES DATA AREA OF SPECIFIED MODULE DATA FIELD
 RELLE9U S U RELEASES INSTANCE OF LIST DESIGNATED BY GIVEN POINTER
 RELM9U S U RELEASES ENTIRE MODULE, AS SPECIFIED
 RELN9U S U RELEASES STORAGE AREA PREVIOUSLY USED FOR GIVEN NODE
 REPEAT S I PERFORMS REPEAT-STORAGE OPRTN OF CONSTANT OR SET OF CONSTANTS, FREE-FM
 REP59R S I SET BEGINNING OF REPEAT SEQUENCE TO NEXT ITEM
 RHNK3C F P DENSITY OF EUTECTIC NAK
 RHO3C F P DENSITY OF GENERIC FLUID, CALLS OTHER DENSITY FUNCTIONS
 RISU9R S I RELEASE INPUT SPECIFICATION UNIT DATA STORAGE AREA
 RLID9U F U RETURNS A REAL TYPE MODULE ID FOR MODULE INDICATED BY POINTER
 RINA3C F P DENSITY OF SODIUM
 ROOT3C S U SOLVES FOR ROOTS OF CUBIC POLYNOMIAL
 SATM3C S C TRANSFERS REFERENCE SATURATION PROPERTIES ONTC ISIDE OF MODULE
 SATO3C S C CALCULATES SATURATION PROPERTIES FOR OTHER SIDE OF HX, IE, NOT SEGMENT
 SATP3C S C LOADS SATURATION PROPERTIES FOR REFERENCE PRESSURE
 SDELB9 F T RETURNS PRINT TIME INTERVAL FOR GIVEN TIME VALUE
 SDUMP S U CALLED BY ABEND1 AFTER CRASH, DUMPS SMALL CORE MEMORY CONTENTS
 SEG3R S I PROCESSES FLOW SEGMENT INPUT DATA
 SETFMT S I CONVERTS DECIMAL INTEGER TO P CONSECUTIVE HOLERITH CONSTANTS, FREE-FMT
 SFWT3C F P ENTROPY OF SATURATED WATER FOR GIVEN PRESSURE
 SGB3C T S T FACTORS BOUNDARY MODULE PRES, FLOW INTO SEGMENT RESPONSE MATRIX
 SOWT3C F P ENTROPY OF SATURATED STEAM FOR GIVEN PRESSURE
 SSGDAT F U K. CHINESE DEPENDENT ROUTINE DETERMINES CURRENT TIME
 SSGTIM S U MACHINE DEPENDENT ROUTINE DETERMINES CURRENT DATE
 STEN3S F P SURFACE TENSION BETWEEN WATER/STEAM AT GIVEN TEMPERATURE (SATURATION)
 SUBN3S S S TRACES BACK FLOW SOURCES FOR EACH SUBNETWORK
 SVCK3U S U SAVES CONTEXT OF GLOBAL VARIABLES AND ARRAYS FOR POSSIBLE RESTART
 SV3C9U S U SAVE GLOBAL CONTAINER CONTEXT ON SAVE FILE DEFINED BY INGC5J CALL
 SWAT3C F P ENTROPY OF WATER/STEAM FOR GIVEN ENTHALPY, PRESSURE
 SYJ3R S I PROCESS GLOBAL SYSTEM INPUT DATA
 TABLER S I MOVE TABLE DATA FOR INPUT DATA RECORD TO GLOBAL CONTAINER
 TAIR3C F P CALCULATES AIR TEMPERATURE AT GIVEN ENTHALPY, P=ATOMSH PRESSR
 TBSG3S S S INITIALIZES TURBINE STAGE CONDITIONS
 TBS3T S T PERFORMS TRANSIENT CALCULATIONS FOR TURBINE STAGE
 TCLM3C F C FUNCTION SETS NOJE END TUBE TEMPS CONSISTANT WITH TC, FLUID TEMPS, LMTS
 TOR3C S C CALCULATES TUBE TEMPERATURE AT AXIAL POSN, ALLOWING SLIGHT AXIAL DISTRN
 TEP3C F P TEMPERATURE OF GENERIC FLUID FOR GIVEN ENTHALPY, PRESSURE, FLUID TYPE
 THOM3C F P CALCULATES THOM TWO-PHASE FRICTION MULTIPLIER
 TIME3T S T RETURNS EVENT TIMING INFORMATION, END, PRINT, STORE, SAVE
 TKNA3C F P THERMAL CONDUCTIVITY OF SODIUM
 TMNK3C F P TEMPERATURE OF EUTECTIC NAK
 TML3T F P TEMPERATURE OF SUBCOOLED WATER FOR GIVEN ENTHALPY, PRESSURE
 TSPV3T F P TEMPERATURE OF SUPERHEATED STEAM FOR GIVEN ENTHALPY, PRESSURE
 TNA3C F P TEMPERATURE OF SODIUM
 TRACE S U CALLED FROM ABEND, TRACES THROUGH SUBROUTINE CALLS
 TRACE1 S U TRACEBACK STARTING AT GIVEN ADDRESS, PART OF ABEND PACKAGE
 TURB3R S I PROCESSES TURBINE MODULE INPUT DATA
 UNIQ9U S U GENERATES A UNIQUE NUMBER, INITIALIZED BY IUN9U CALL
 VAIR3C F P DYNAMIC VISCOSITY OF AIR
 VALV3R S I PROCESSES VALVE MODULE INPUT DATA
 VALV3S S S INITIALIZES VALVE CONDITIONS
 VALV3T S T PERFORMS TRANSIENT CALCULATIONS FOR VALVE MODULE
 VISC3C F P DYN VISCOSITY OF GENETIC FLUID, GIVEN ENTHALPY, PRESSURE, FLUID TYPE
 VISL3N F P DYNAMIC VISCOSITY OF SUBCOOLED WATER FOR GIVEN ENTHALPY, PRESSURE
 VISV3N F P DYN VISCOSITY OF SUPERHEATED STEAM FOR GIVEN ENTHALPY, PRESSURE
 VOLF3C F C CALCULATES VOLUME FRACTION BETWEEN TWO LEVELS IN HORIZONTAL CYLINDER
 VOLM3S S S LOOPS THRU NETWORK VOLUMES, LOADING PROPS FOR PRNT3C AND TRANSIENT
 VOLS3T S T ADVANCES CONDITIONS IN VOLUME MODULE, PARTICULARLY THE LEVEL
 VOL3R S I PROCESS VOLUME MODULE INPUT DATA
 VRFY3R S I MAIN DRIVER FOR MINET INPUT DATA VERIFICATION
 VSNA3C F P DYNAMIC VISCOSITY OF SODIUM
 VSNK3C F P DYNAMIC VISCOSITY OF NAK
 WESM3S S S SUMS UP FLOW ENERGY (FLOW X ENTHALPY) IN AND OUT EACH SUBNETWORK
 XDNB3C F P DETERMINES FLOW QUALITY AT DNB, ATOMICS INTRNL FOR SODIUM TO WATER
 XDRY3C F P DETERMINES FLOW QUALITY AT DRYOUT, MACBETH FOR WATER TO WATER
 ZPRT3R F I RETURNS ELEVATION OF MODULE PORT

3.2.3.1 INPUT PROCESSOR

The input processor forms an interface between the user and the computational code. Its main task is one of translation. On the user side, it must accept textual input describing the system which is to be modelled. This must be transformed into equivalent data in the correct form for use by the computational code. This task must be accomplished correctly for all combinations of valid input data as defined by the program specification. Further, the input processor must be able to handle incorrect input data in such a way that,

- the run does not terminate due to run-time error
- appropriate error messages are issued to the user
- remaining input is processed for further errors before the run is terminated

This applies to both simple syntactic errors as well as more subtle global consistency and semantic errors.

Other functions include generating formatted and unformatted listings of input data, listing optional features selected through the input data, and generating internal data storage maps.

3.2.3.1.1 DESIGN CONSIDERATIONS

A major design consideration for the MINET Input Processor is the requirement for a host-code interface. This interface allows MINET reader functions to be controlled by other codes in place of the stand-alone MINET program. Especially critical are those functions, normally controlled by input for the

stand-alone code, which require control from the external host in the interfaced version. It should be noted that subroutines MAIN9R and CRDR9R in the stand-alone version perform functions that would be replaced by host-code in the interfaced version.

3.2.3.1.2 INPUT PROCESSOR SUBTASKS

Input processor activity is divided into several subtasks which are invoked by either a stand-alone main driver or host-code. Each subtask is controlled by a separate subroutine whose name appears in parentheses after the subtask name.

- The READ (READ3R) subtask controls the reading of data from the input file. This requires various file management operations including positioning, reading of logical data records, and testing for end conditions. During this process, syntactic and data field type errors are identified and appropriate error messages are issued with the unformatted input data listing.
- VERIFICATION (VRFY3R) consists of a group of error tests designed to detect missing data, semantic errors, and global data inconsistencies.
- DATA INITIALIZATION consists of allocating storage and loading computational data from input data, subject to a predefined interpretation process. This is the most difficult task performed by the Input Processor because of the extreme flexibility required for representing the generalized class of systems to be modelled. Various types of input data errors may be detected during these

processes, requiring appropriate error messages to be issued to the user. In the case of storage overflow error during the allocation process, it is necessary to provide the user with an estimate of the additional storage required before terminating the run. This allows the user to determine exactly how much additional storage is needed to accommodate the data set.

3.2.3.1.3 MAJOR SUBROUTINES

The following descriptions summarize the functions performed by the major Input Processor subroutines. They are grouped according to the subtasks outlined above. Details are purposely left out for the sake of clarity.

3.2.3.1.3.1 MAIN DRIVER

MAIN9R controls the sequencing of the Input Processor subtasks (see also Figure 3.2-1). It first calls CRDR9R, a secondary driver which controls the reading of input data from the INPUT file. The verification subtask is then invoked by calling VRFY3R. Finally, the DATA INITIALIZATION subtask is invoked by calling INIT3R. An error count parameter is tested after each of the calls, and the run is terminated if it is nonzero. On return, an integer-encoded context restore ("restart") flag is passed back to the calling code to indicate whether or not the input data contained a context restore request.

CRDR9R sets up the proper conditions prior to the beginning of the actual data reading. It first calls INRD3R to initialize Input Processor internal code, then it positions the INPUT file at the beginning of the MINET data and

calls READ3R to do the reading. If an input file error is detected before the call to READ3R, an error message is issued and the run is terminated.

3.2.3.1.3.2 READER INITIALIZATION SUBTASK

INRD3R initializes various internals of the Input Processor. These include:

- global constants
- internal utilities
- MINET input file content definition (using ISU)
- data lists (using LISF data abstraction)

3.2.3.1.3.3 READ SUBTASK

READ3R controls the actual MINET input data file reading process. Consecutive records are read from the INPUT file until either an end-of-file condition or an end of MINET data is encountered. File access is indirect in that calls are made to a file manager, GENRD, which passes back one complete MINET input record at a time, along with flags to signal end conditions. This is done to unburden READ3R of the need to perform low-level syntax analysis related to the external INPUT file definition. It also simplifies read logic at this level by covering up the asynchronous nature of the read process created by continuation lines and varying end conditions. Each record is then passed to a record-processing subroutine, DMOD3R, unless GENRD flags a syntax error. In this case an error message is issued and the entire record is ignored.

DMOD3R tests interpreted input record data fields for errors and passes them to the appropriate destination for further processing. Error tests include:

- invalid record number
- incorrect record length
- duplicate record conflict
- incorrect data field type
- intra-record port identifier conflict
- module identifier type disagreement

3.2.3.1.3.4 VERIFICATION SUBTASK

VRFY3R performs error tests for missing data, semantic errors, and global data inconsistencies. LIST3R is called to write a formatted listing of input data record fields to the OUTPUT file. On return, a data error count is passed back to the calling code.

LIST3R writes a formatted listing of input data record fields as they were interpreted by the Input File Manager. In order to simplify processing logic and to minimize global data storage, the listing is actually generated earlier by DMOD3R and written to a scratch file. LIST3R only has to write a header and copy the scratch file contents to OUTPUT.

3.2.3.1.3.5 DATA INITIALIZATION SUBTASK

INIT3R controls the initialization of global computational data. If the MINET input data does not contain a context restore ("restart") request, then SYS3R is called to process system data. The global container is then loaded

and the pointers are defined. Finally, CALC3R is called to perform secondary processing of global data not possible earlier. On return, an integer context restore flag, indicating whether or not the input data contained a restore request, is passed back to the calling code. An error count is also returned.

CALC3R performs secondary processing of global data which can only be done after the initial data loading process.

IPTS3R sets global container pointers residing in global COMMON blocks. The pointer values are obtained from the Global Container Manager function IGA9U.

SYS3R processes system related input data. It is the top level of a group of subroutines designed to perform the task of interpreting the input to construct a representation of system structure. The approach used is related to that of parsing used by compilers to interpret high-level computer languages. It consists of traversing the entire set of system modules, following the interconnections defined by the input data, so that each module is visited at least once. Specific subroutines are called depending on module type to process module input data and to identify system structures. Proceeding in this way, computational data is allocated and initialized at the same time the system structures are being interpreted.

The basic rules governing the identification of system structures are:

1. each SYSTEM is comprised of one or more NETWORKs
2. each NETWORK is comprised of at least one inlet and one outlet BOUNDARY, one or more SEGMENTS, and zero or more VOLUMES

3. each segment is comprised of one or more of the following:

- PIPE
- HEAT EXCHANGER
- PUMP
- VALVE
- TURBINE

4. the above system modules may be interconnected arbitrarily as long as

- no module is connected to itself
- connections are only made between inlets and outlets
- each connection links exactly two modules
- all modules are fully connected

The entire group of system subroutines are given in the following list, where indenting is used to indicate the calling structure.

```
SYS3R
  NET3R
    BND3R
    SEG3R
      HX3R
      PIPE3R
      PUMP3R
      TURB3R
      VALV3R
    VOL3R
```

In operation, SYS3R first performs initialization of global counter variables for the system. Then it scans the data module list for network boundary modules. These are defined as modules with exactly one outlet and no inlets. Each boundary of this type is used as a starting point for a new network parse invoked by calling NET3R. This process is repeated until all networks have been parsed. Finally, the Global Container Manager function NPNT9U is invoked to allocate global container space used for steady state and transient computations but not directly initialized from the input.

3.2.3.2 STEADY STATE

There are three subroutines in the steady state portion of MINET in need of further elaboration. These routines are HX3S, HXND3S, and PRFL3S. The first two, which are used in determining the steady state temperature distributions in the heat exchangers, contain many subtleties and should be modified only as a last resort.

3.2.3.2.1 HX3S

Subroutine HX3S controls the steady state heat exchanger calculations, and is called twice for each heat exchanger module. On the first pass it initializes the temperature distributions on both sides of the unit. During the second pass, the second side pressure drop, corresponding to the temperature distribution calculated in the first pass, is determined. As the second pass is relatively simple, we focus here on the first pass, which proceeds as shown in Figure 3.2-3.

By the time that HX3S is called, the heat exchanger flows, pressures, and inlet and outlet temperatures have already been set, at least for the current iteration, based on system conditions. One of the first steps in the HX3S calculations is to check for two non-physical conditions, i.e., (1) temperature cross and (2) violation of the second law of thermodynamics. In either non-physical case, an error flag is set and an error message is written. However, the calculations continue in any case, because of the chance that on the next system wide iteration the conditions may become physically realistic.

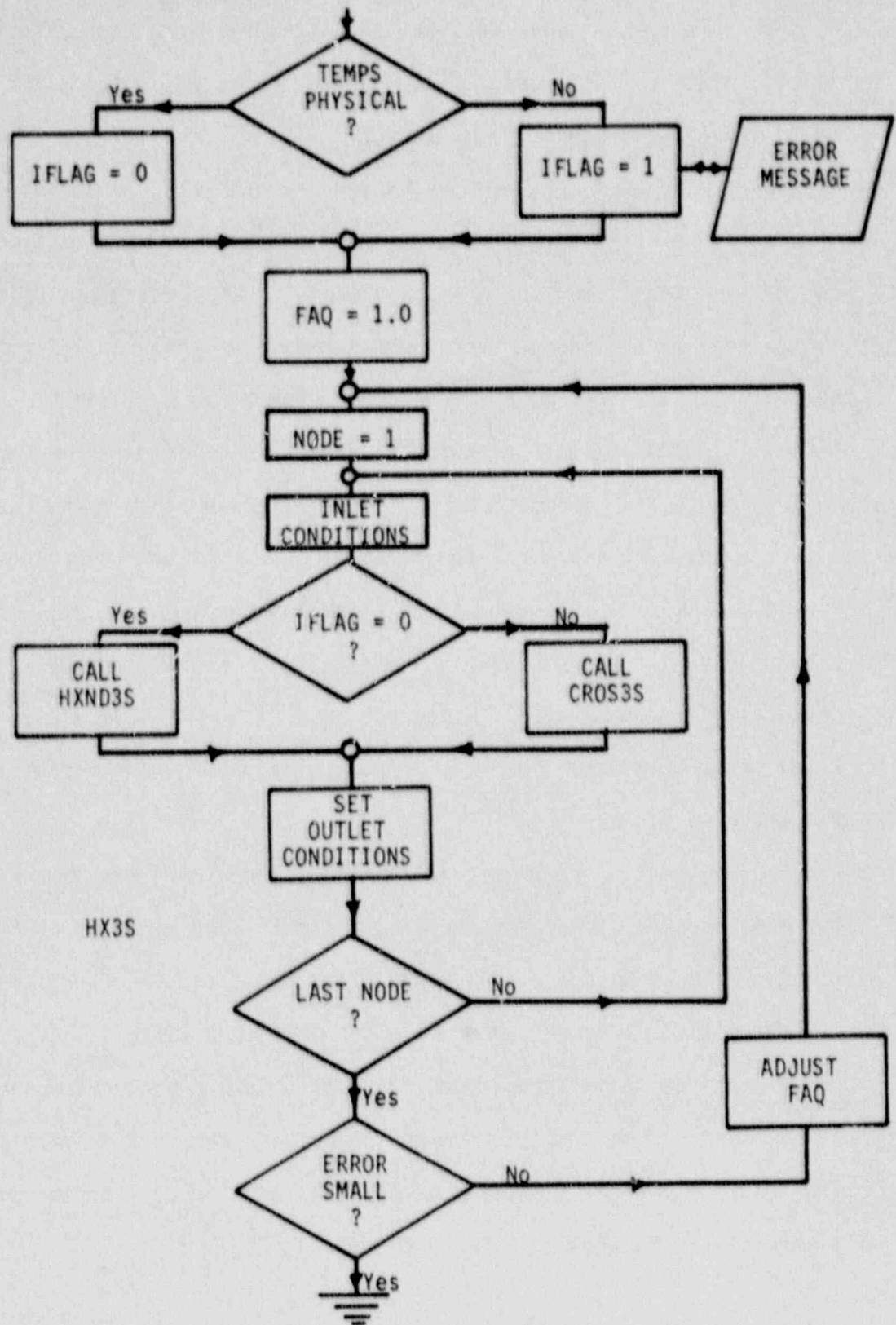


Figure 3.2-3 Flow Chart for Subroutine HX3S

To begin the calculations, the heat transfer area correction factor, FAQ, is set to 1.0. If the error flag was set, there is no iteration on FAQ, i.e., it is 1.0 for the single pass taken.

All the nodes in the heat exchanger are analyzed sequentially, with the node inlet conditions determined from either module inlet parameters, or the outlet conditions from the previous node. Under physical conditions, subroutine HXND3S is called to determine the node heat transfer and resulting enthalpy gradient. If, on the other hand, the error flag was set, subroutine CROS3S is called to set the enthalpy gradient indicated by module inlet and outlet conditions, assuming a linear heat transfer rate along the module.

When calculations have been completed for all the nodes, the calculated module outlet enthalpy is compared to the one required by system wide considerations. If the conditions are physically realistic, and yet there is some disagreement between the needed heat transfer rates and the rate indicated by correlations, the heat transfer area correction factor is adjusted for the next iteration.

Experience to date indicates that the number of iterations needed to determine the area correction factors is significant in terms of the total computation time needed for the steady state solution. Further, this factor consistently falls between .65 and 1.1 for various physically correct (experimental, operational, or designed) systems. Should problems arise with the calculation of the area correction factor, one should look very closely at the input heat exchanger geometric conditions, and the conditions coming from elsewhere in the steady state calculations.

3.2.3.2.2 HXND3S

Subroutine HXND3S performs the steady state calculations for each of the heat exchanger nodes, as long as the heat exchanger boundary conditions are physically possible. The basic calculational process is indicated in Figure 3.2-4.

At the time when HXND3S is called, only conditions at the node inlet (for both sides of the tube) are known. From these conditions, conditions at the node outlet, as well as the node average tube temperature are estimated. Using these estimates, the heat transfer rates on both sides of the tube are evaluated. Multiple heat transfer modes are possible, with up to five mode regions allowed. Energy balance requires that the heat transfer rates be equal on both sides of the tube, and the tube temperature is adjusted iteratively until this is true. Finally, the enthalpy gradient across the node and the heat transfer rate have to be consistent, so outlet conditions are adjusted iteratively until the agreement is close.

Subroutine HXND3S tends to be the point of discovery for many types of errors that slip through the routine error checks. This routine contains many subtleties that have been closely reviewed on a number of occasions. One should assume an error flagged in or near HXND3S is really caused elsewhere, at least until proven otherwise. This is particularly true for systems where the user is only estimating key parameters.

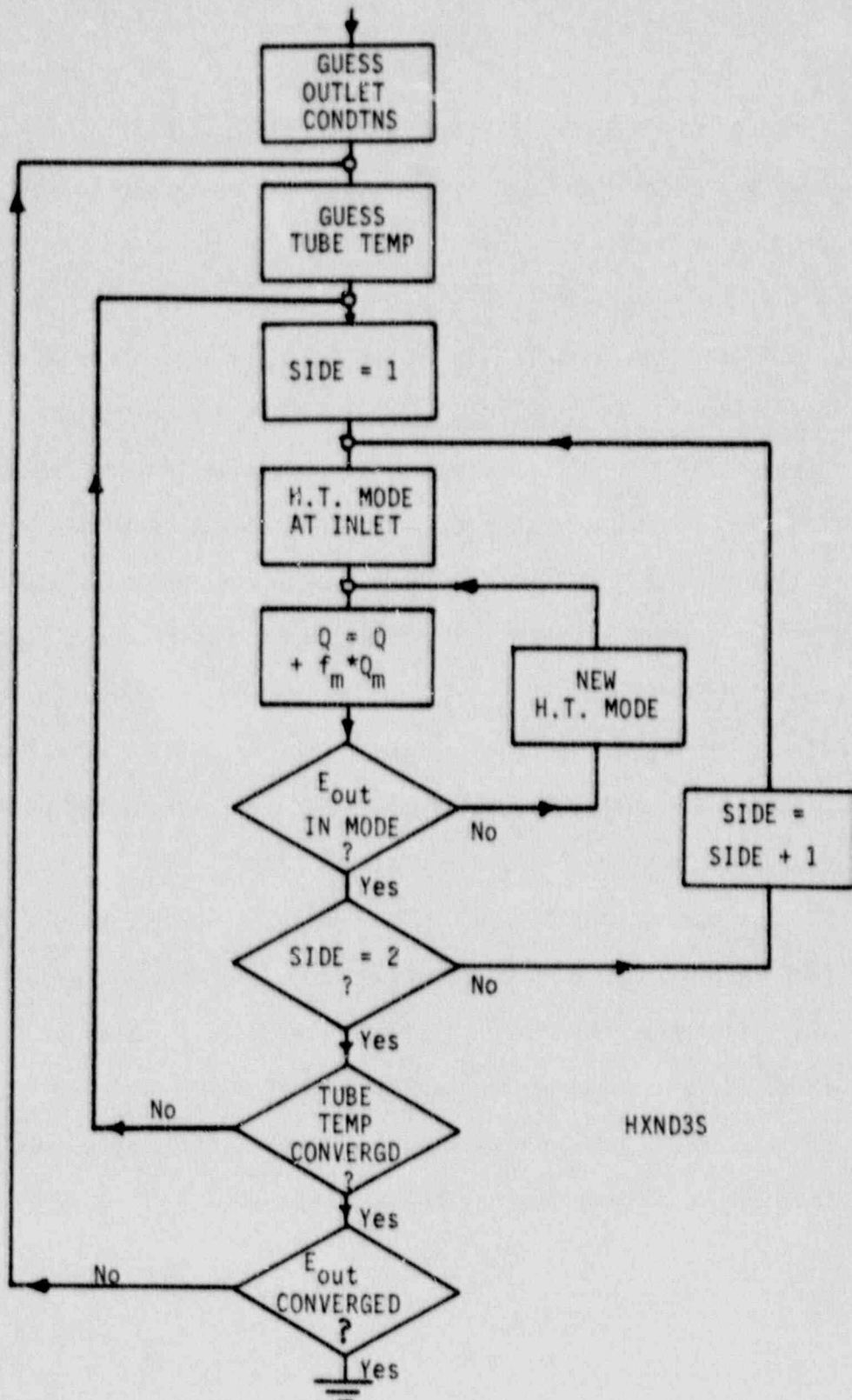


Figure 3.2-4 Flow Chart for Subroutine HXND3S

3.2.3.2.3 PRFL3S

Subroutine PRFL3S adjusts the pressures and mass flow rates in each of the system networks at the end of each system iteration. The calculational process is indicated in Figure 3.2-5.

Subroutine PRFL3S is essentially the iterative solution of a matrix equation that approximates the W^2 factor in a linearized matter. From iteration to iteration, only the flow rate contribution and the pressure gradient in isolated pumps, valves, and turbine stages, are updated. The pressure gradients through pipes, heat exchangers and imbedded pumps and valves are updated only during system iterations.

The most likely problem to arise in the execution of this subroutine is the calculation of negative pressures. While such pressures are forced to be positive, other complications can develop under these extreme conditions. The best solution is to adjust the form loss factors (including valve losses) and the initial guesses on the volume and inlet boundary pressures.

3.2.3.3 TRANSIENT

Most of the transient subroutines are relatively straightforward, and can be understood using information provided elsewhere in this documentation. The exception is subroutine HX3T.

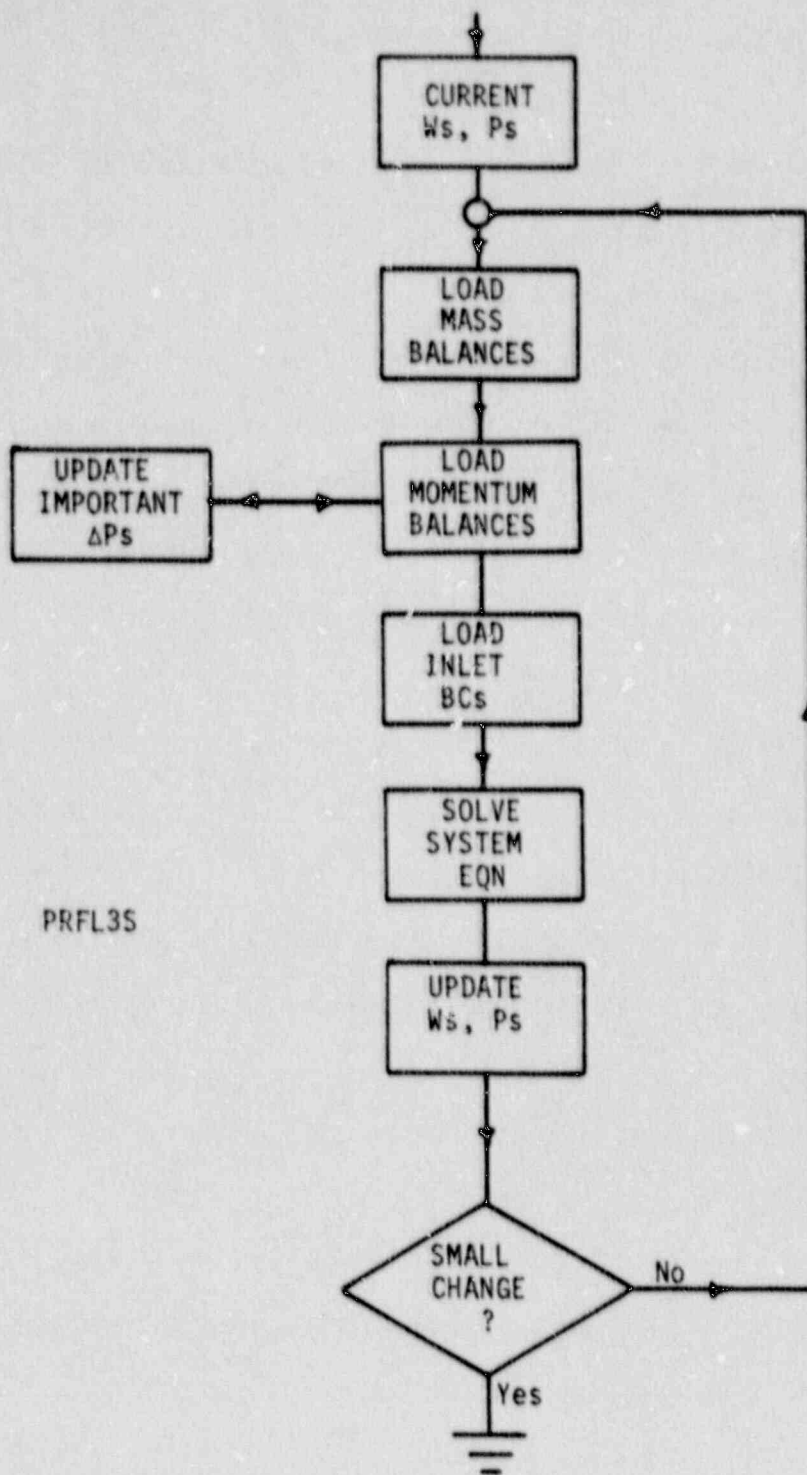


Figure 3.2-5 Flow Chart for Subroutine PRFL3S

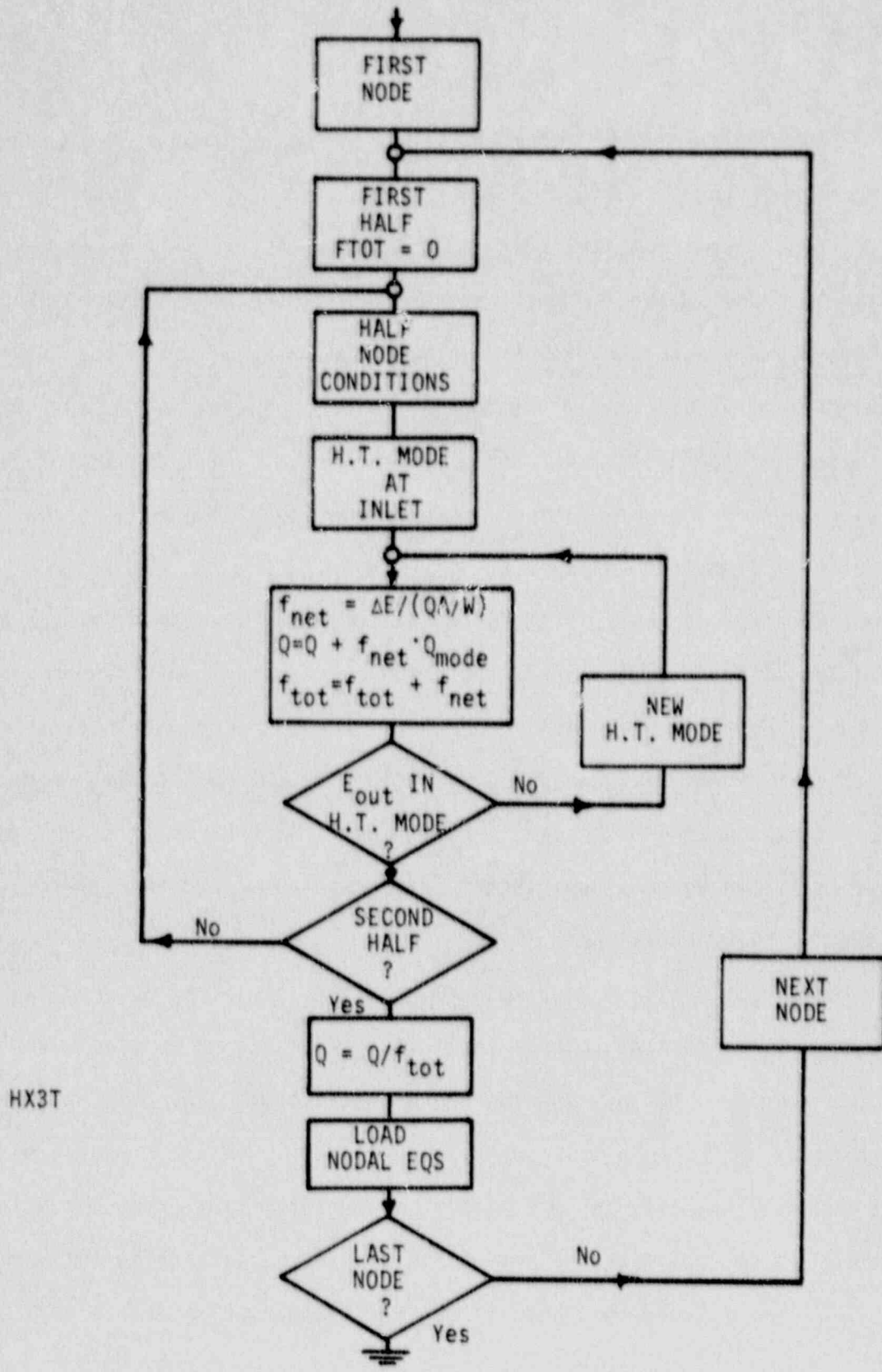
3.2.3.3.1 HX3T

Subroutine HX3T performs the consistent heat exchanger calculations. The process is shown in Figure 3.2-6.

Two factors complicate the calculations. First, it is possible to have node average enthalpies that are not the average of conditions at the ends. This happens when the flow was either converging or diverging in the node during the previous step, so donor cell differencing was not used. Second, because the node heating and enthalpy gradient can be inconsistent due to transient effects, determination of the proportion of the node in each heat transfer mode is more complicated.

Each node is calculated in two halves, with the assumption that the average enthalpy is unrelated to the enthalpy at either end. The heat transfer mode is determined at the half-node inlet and changed as often as necessary (up to 5 regimes for the whole node) to the half-node outlet, for both the first half-node and the second half-node. The node fraction in a given mode is estimated using a quasi-steady energy balance, and the total heating is divided by the total weighting.

The heat transfer mode weighting is best explained by example. Consider a node with subcooled water at the inlet, the onset of boiling exactly at the node average enthalpy, and boiling at the outlet. Further, assume that the enthalpy rise across the node is twice what is indicated by the heating and the mass flow rate. When considering the first half node, which is subcooled, we would determine that a heat transfer length approaching the whole node ($f_{net} \approx 1.0$) would be needed to get the enthalpy rise across only the first



HX3T

Figure 3.2-6 Flow Chart for Subroutine HX3T

half. Similarly, in the second half-node, the heat transfer rate would be such that a length approaching the whole node would be needed to get the enthalpy rise across the second half-node (again, $f_{net} \approx 1.0$). Thus, the quasi-steady heat flux would be exactly enough for the given flow and enthalpy gradient. However, this must be divided by the total required node fraction, f_{tot} (≈ 2.0), to get the actual heating in the node. The node heating and other node conditions are loaded in the segment matrix equation.

3.2.3.4 PROPERTY PACKAGE

More than 10% of the MINET subroutines and functions are property related. This group of functions, which constitutes the MINET property library, are all in SI units. The library is easily extended, and will grow according to our needs. These functions are grouped by use in the tables provided in this section.

The structural property functions are in Table 3.2-2. There are currently ten structural materials in the imbedded tables. The "TYPE" parameter is determined by the user through specification of M3TYPE, M3CORR, and M3STRC on the 301D input record(s) (see Figure 2.2-2).

Table 3.2-2. Structure Property Functions

| | |
|---------------|--|
| Conductivity | $k = \text{COND3C}(\text{TYPE}, T)$ |
| Heat Capacity | $c_p = \text{HCAP3C}(\text{TYPE}, T)$ |
| Density | $\rho = \text{DENS3C}(\text{TYPE}, T)$ |

General fluid property functions are in Table 3.2-3. These functions call the fluid-dependent property functions listed in the remaining tables. For a property that is identically 0.0, e.g., the derivative of the sodium density with respect to pressure, the function sets the value to 0.0. The fluid in each network is designated via the IFTYPN data specification in input record 801D.

Table 3.2-3 General Fluid Property Functions

| | |
|---------------|--|
| Enthalpy | E = ENTH3C (T, P, FLUID, SIDE) |
| Temperature | T = TEMP3C (E, P, FLUID, SIDE) |
| Density | ρ = RHO3C (E, P, FLUID, SIDE) |
| Viscosity | μ = VISC3C (E, P, FLUID, SIDE) |
| Derivatives | |
| | $\partial\rho/\partial P$ = DRDP3C (E, P, FLUID, SIDE) |
| | $\partial\rho/\partial E$ = DRDE3C (E, P, FLUID, SIDE) |
| Heat Transfer | |
| | h = HTC3C (SIDE, MODE, E, G, Tube Temp, k, T) (Fluid Type Implicit Via Commons, SIDE) |
| | G = mass velocity = ρV |
| | k = thermal conductivity of tube |

Water property functions are shown in Table 3.2-4. This is the largest set of property functions, both because of the two-phases and because our need has been greater. For instance, entropy functions are available only for water and steam because we have not wanted to run sodium, air, or NaK through the turbine module.

Sodium property functions are given in Table 3.2-5. These functions are simple and fast running because subcooled sodium is essentially incompressible.

Air property functions are listed in Table 3.2-6. These properties are accurate near atmospheric pressure, and are based largely on ideal gas behavior.

Table 3.2-4 Water Property Functions

Generic

Entropy S = SWAT3C (E, P)
 Enthalpy E = ESW3C (S, P)

Liquid

Temperature T = TML3T (E, P)
 Density ρ = DENL3D (E, P)
 Enthalpy E = ENTL3H (T, P)
 Viscosity μ = VISL3N (E, P)
 Heat Cap c_p = CPL3C (E, P)
 T Cond k_t = CONL3K (E, P)
 Derivatv $\partial\rho/\partial E$ = DRLH3D (E, P)
 Derivatv $\partial\rho/\partial P$ = DRLP3D (E, P)

Steam

Temperature T = TMPV3T (E, P)
 Density ρ = DENV3D (E, P)
 Enthalpy E = ENTV3H (T, P)
 Viscosity μ = VISV3N (E, P)
 Heat Cap c_p = CPL3C (E, P)
 T Cond k_t = CONV3K (E, P)
 Derivatv $\partial\rho/\partial E$ = DRVH3D (E, P)
 Derivatv $\partial\rho/\partial P$ = DRVP3D (E, P)

Saturation

Liq Enthalpy E_f = ESTL3H (P)
 Stm Enthalpy E_g = ESTV3H (P)
 Liq Entropy S_f = SFWT3C (P)
 Stm Entropy S_g = SGWT3C (P)
 Surf Tension σ = STEN3S (T_{sat})
 Sat Pressure P = PSAT3P (T, P_{guess})

Table 3.2-5 Sodium (Na) Property Functions

Subcooled

| | |
|-------------|---|
| Temperature | T = TNA3C (E) |
| Enthalpy | E = ENA3C (T) |
| Density | ρ = RNA3C (E) |
| Viscosity | μ = VSNA3C (E) |
| Heat Cap | c_p = HCPN3C (E) |
| T Cond | k_t = TKNA3C (E) |
| Derivatv | $\partial \rho / \partial E$ = DREN3C (E) |

NOTE: Assume $\partial \rho / \partial P = 0.0$

Table 3.2-6 Air Property Functions (Atmospheric)

| | |
|-------------|--|
| Temperature | T = TAIR3C (E) |
| Enthalpy | E = EAIR3C (T) |
| Density | ρ = RAIR3C (E, P) |
| Viscosity | μ = VAIR3C (E) |
| Heat Cap | c_p = CPAR3C (E) |
| T Cond | k_t = CAIR3C (E) |
| Derivatv | $\partial \rho / \partial P$ = DRPA3C (E, P) |
| Derivatv | $\partial \rho / \partial E$ = DREA3C (E, P) |

Properties for eutectic NaK are determined using the functions listed in Table 3.2-7. Eutectic NaK is also essentially incompressible in the subcooled state.

Table 3.2-7 NaK Property Functions

Subcooled

| | |
|-------------|--|
| Temperature | T = TMNK3C (E) |
| Enthalpy | E = ENNK3C (T) |
| Density | ρ = RHNK3C (E) |
| Viscosity | μ = VSNK3C (E) |
| Heat Cap | c_p = CPNK3C (E) |
| T Cond | k_t = CDNK3C (E) |
| Derivatv | $\partial\rho/\partial E$ = DRNK3C (E) |

NOTE: Assume $\partial\rho/\partial P = 0.0$

The current heat transfer functions are given in Table 3.2-8. This list is almost certain to increase in length as more heat exchanger types are considered.

Finally, some flow related functions are listed in Table 3.2-9. The friction factor functions, which are applicable for all fluid types, are imbedded (in-line functions) in subroutine DP3C. Critical flow models are currently limited to water/steam, but models for the other fluid could be incorporated easily. Note that the critical flow option can be bypassed for any given value by setting T3CHOK = 0 on the 1101D input record. As water/steam is the only fluid modeled with two-phases, the THOM two-phase (2- ϕ) multiplier is the only one included at this time.

Table 3.2-8 Heat Transfer Correlations

Water/Steam

| | |
|-----------------------|---|
| Forced Convection | H = HWFC3C (E, DEQ, G, P, EF) |
| Nucleate Boiling | H = HWNB3C (E, X, T, TC, D, DEQ, G, SIDE) |
| Film Boiling | H = HWFB3C (X, TC, CT, D, DEQ, G, SIDE) |
| Superhhd Convection | H = HWSC3C (T, TC, CT, D, DEQ, G, SIDE) |
| Condens On Vert Surf | H = HWCN3C (E, D, A, SIDE) |
| Conds In Horiz Tubes | H = HC1Y3C (TC, D, CT, SIDE) |
| Condens On Tube Banks | H = HCOT3C (TC, D, CT, NPATH, SIDE) |

Critical Heat Flux:

| | |
|--------|---|
| DNB | X = λ DNB3C (G, Q, RF, RG, EFG) |
| Dryout | X = XDRY3C (G, Q, D, EFG) |

Sodium

| | |
|--------------------|-----------------------------|
| Inside Tubes/Pipes | H = HNAI3C (E, G, DEQ) |
| Outside Tubes | H = HNAF3C (T, POD, G, DEQ) |

Air

| | |
|--------------|------------------------|
| Across Tubes | H = HTCA3C (E, G, DEQ) |
|--------------|------------------------|

NaK

| | |
|--------------|------------------------|
| In/Out Tubes | H = HTNK3C (E, G, DEQ) |
|--------------|------------------------|

Key:

| | |
|------------------------------|---------------------------|
| E = Enthalpy | X = Quality |
| T = Temperature | D = Diameter |
| G = Mass Velocity | DEQ = Equiv Hydr1 Diam |
| Tc = Tube Centerline Temp | POD = Pitch-to-Diam Ratio |
| Q = Heat Flux | SIDE = Side of Tubes |
| P = Pressure | R = Density |
| G = Mass Velocity = ρV | CT = Thermal Conductivity |
| NPATH = No. Tubes in Bank | |

NOTE: Several Access Saturation Property Common Block, Also.

Table 3.2-9 Flow Related Functions

Generic

Friction Factor - Imbedded In DP3C

Water

Critical Flow G = CRIT3C (E, P, SIDE)

Water G = GFSK3G (E, P)

Two-Phase G = GMUY3C (E, P)

Superheated G = GSUP3C (E, P)

Two-Phase Multiplier ϕ = THOM3C (P, X)

3.2.3.5 INTERNAL UTILITIES

Internal Utilities are procedures used internally by MINET to perform standardized functions such as equation solving, data management, or diagnostic analysis. Each utility is implemented as one or more subroutines, each of which performs one of a set of related functions on a shared data entity.

3.2.3.5.1 INPUT SPECIFICATION UTILITY (ISU)

ISU provides functions to construct and access standardized specifications for external data input files. These specifications are used by MINET during the Input Processing phase.

ISU input data specifications are based on the following hierarchy of abstract objects representing the major components of the generalized external input data file.

- FILE - a group of RECORDs identified under a common character-encoded file identifier (FILEID).
- RECORD - a sequence of one or more data ITEMs identified by an integer-encoded record number.
- ITEM - a sequence of one or more data FIELDs.
- FIELD - a character-encoded numeric data value of either INTEGER or REAL type.

ISU functions are implemented as a set of FORTRAN subprograms:

- ISU9R - Initializes internal implementation data.
- PUTF9R - Begins a new file specification entry.
- PUTR9R - Begins a new record specification entry

- PUTI9R - Puts a new item specification entry in the currently open record specification.
- REPS9R - Begins a repeating sequence of record items.
- GETF9R - Opens file specification for a given file identifier.
- GETR9R - Opens record specification for a given record identifier.
- GETI9R - Gets next item specification in currently open record.
- RISU9R - Releases ISU internal data storage for re-use.
- LSPC9R - Prints a formatted listing of all ISU specifications.

3.2.3.5.2 INPUT FILE MANAGER (IFM)

IFM provides functions supporting the interface between the external data input file and the data reading portion of the Input Processor.

IFM functions are currently being performed by GENRD [31], a free-format card input processor developed at Los Alamos National Laboratory. GENRD reads character-encoded MINET input records and decodes numeric fields, placing the resulting INTEGER and REAL type field values in arrays which are passed back to the calling code. Input record numbers, field counts, and syntactic error conditions flags are also passed back.

3.2.3.5.3 GLOBAL CONTAINER MANAGER (GCM)

GCM provides functions supporting the allocation and management of variably-dimensioned data storage residing in a globally-shared container array. Named blocks of contiguous array locations are allocated and referenced by means of pointers. Container maps and content listings are printed

on request. The entire container content may be saved on an external file and restored on request.

3.2.3.5.3.1 GLOBAL CONTAINER ARRAY

The global container array, referred to as CONTAINER, consists of a large one-dimensional FORTRAN array residing in a labelled COMMON block. Program units, requiring access to the CONTAINER data, include a declaration of the labelled COMMON. They then either access the array elements directly or indirectly by way of locally declared dummy arrays which are EQUIVALENCED to the CONTAINER.

3.2.3.5.3.2 ALLOCATION MANAGEMENT

Allocation of named data blocks in the CONTAINER is performed by GCM in response to external requests. These fall into two categories:

- VIRTUAL allocation occurs implicitly with requests to load data in specific named data blocks. This is accomplished through a set of subroutines which treat the blocks as abstract data types although they also reside in the CONTAINER. Each request specifies a block name, a block index, and a data value to be loaded at the indexed location. Data may be loaded in this way, extending block size or overwriting previous data until block size is fixed by a pointer value request (call to NPNT9U).

- IMMEDIATE allocation occurs in response to requests in which the block size and name are given. Each request results in both an allocation and the return of a pointer.

3.2.3.5.3.3 SUBROUTINE SPECIFICATIONS

GCM functions are implemented by the following subprograms:

- INGC9U - Initializes internal implementation data for GCM.
- PGCI9U - Puts INTEGER value in specified location of named virtual container block.
- PGCR9U - Puts REAL value in specified location of named virtual container block.
- NPNT9U - Returns pointer to named container block.
- LPNT9U - Returns length of named container block.
- GCTP9U - Prints a table of block names, lengths, and pointer values on OUTPUT file. Allocation errors are flagged with diagnostic messages.
- GCPR9U - Prints a detailed listing of container contents on OUTPUT file.
- SVGC9U - Saves container contents on external SCRATCH file.
- REGC9U - Restore container contents from external SCRATCH file previously generated by SVGC9U.
- GCER9U - Tests for container allocation errors and prints an error summary on OUTPUT file.

3.2.3.5.4 DATA MANAGEMENT UTILITY (DMU)

DMU provides high-level data management functions operating on abstract data types not provided as part of the FORTRAN language.

3.2.3.5.4.1 NODE DATA TYPE

A NODE data type consists of an indexable array, each element of which may be of either REAL or INTEGER type. Associated with each NODE is a node identifier (NODEID) and a pointer which may be used to point to another node. NODEs may be created dynamically as required and then released when no longer needed, the storage resource being available for serial re-use. The NODE array storage is allocated dynamically on demand as data is stored in it, eliminating the need for any preallocation.

NODE functions are implemented by the following subprograms:

- INN9U - Initializes internal implementation data.
- NEWN9U - Creates a new NODE and returns a pointer to it.
- LNKN9U - Links two NODEs by means of NODE pointer.
- NXTN9U - Returns a pointer to the next NODE in a NODE chain.
- PUTN9U - Stores an integer value in an indexed location of a NODE array.
- GETN9U - Returns an integer value stored in an indexed location of a NODE array.
- PUTF9U - Stores a REAL value in an indexed location of a NODE array.
- GETF9U - Returns a REAL value stored in an indexed location of a NODE array.
- INPT9U - Scans a NODE chain for a NODE with given NODEID and returns a pointer to it.

- NSIZ9U - Returns the size of a NODE array.
- NID9U - Returns the value of the NODEID for a given NODE.
- RELN9U - Releases a NODE for re-use.

3.2.3.5.4.2 MODULE DATA TYPE

A MODULE data type consists of a set of NODEs grouped under a common module identifier (MODID). MODULE data is addressed by the coordinate pair (NODEID, index), where INDEX is an INTEGER index into the NODE array. This coordinate pair may be thought of as addressing a data area within the MODULE as data storage requests are made. MODULES may be created dynamically as required and then returned when they are no longer needed. NODE storage within each MODULE is created dynamically on demand as storage requests are made.

MODULE functions are implemented as a group of FORTRAN subprograms:

- INM9U - Initializes internal implementation data.
- NEWM9U - Creates a new MODULE and returns a pointer to it.
- PUTD9U - Stores INTEGER data in a MODULE data area.
- GETD9U - Returns INTEGER data values stored in a MODULE data area.
- PUTR9U - Stores REAL data value in MODULE data area.
- GETR9U - Returns REAL data values stored in a MODULE data area.
- MID9U - Returns MODID associated with a MODULE.
- DSIZ9U - Returns size of a given data area within a MODULE.
- RELD9U - Releases specific data area storage within a MODULE.
- RELM9U - Releases data storage for an entire MODULE.

3.2.3.5.4.3 LIST DATA TYPE

A LIST data type consists of a doubly-linked list of MODULEs, also called ITEMS. LISTS may be created and deallocated dynamically as required. When a new LIST is created, a pointer is generated which points to a dummy LIST header item. New ITEMS may be inserted in and deleted from the LIST by means of pointers.

LIST functions are implemented as a group of FORTRAN subprograms:

- INL9U - Initializes internal implementation data; must be called once before LIST utility is used.
- NEWL9U - Creates a new instance of a LIST type and returns a pointer to the dummy head item.
- RELL9U - Deallocates entire LIST and resets head item pointer to NIL.
- INSL9U - Inserts an item in LIST following a given ITEM.
- NXTI9U - Returns a pointer to the successor of a given ITEM.
- LSTI9U - Returns a pointer to the predecessor of a given ITEM.
- LOCL9U - Returns a pointer to the next ITEM encountered having a specified INTEGER type MODID.
- LOCR9U - Returns a pointer to the next ITEM encountered having a specified REAL type MODID.
- LSIZ9U - Returns an INTEGER type count of the number of ITEMS in a given list, exclusive of the HEADER.
- LCNT9U - Returns a count of the number of ITEMS in a given LIST having a given MODID.

3.2.3.5.4.4 ARRAY DATA TYPE

An ARRAY data type consists of a two-dimensional array of REAL type elements. Each element is addressed according to its ROW and COLUMN indices. ARRAYS may be created and deallocated dynamically as required. On creation, the ARRAY dimensions are specified as maximum ROW and COLUMN index values (MAXROW and MAXCOL). Each ARRAY is accessed by means of a pointer provided as part of the creation process.

ARRAY functions are implemented as a group of FORTRAN subprograms:

- INA9U - Initializes internal implementation data; must be called once prior to first use of ARRAY utility; may also be called to deallocate and reinitialize entire ARRAY data storage.
- NEWA9U - Creates a new instance of a ARRAY type and returns a pointer to it.
- PUTA9U - Stores a REAL type value in a specified ELEMENT.
- GETA9U - Returns a REAL type value stored in a specified ELEMENT.
- ADDA9U - Adds a REAL type value to that stored in a specified ELEMENT.
- PRTA9U - Prints the values of all ELEMENTs for a given ARRAY on the OUTPUT file.
- LEQ9U - Solves a system of linear equations of the form $Y=A*X$, where A, Y, and X are pointers to ARRAY types.

3.3 CODE DATA STRUCTURE

3.3.1 LARGE STORAGE ARRAYS

In developing MINET, much effort was placed on optimizing the use of data storage, primarily because of the limited space available in small core memory in the CDC-7600 computer. There are only three significant arrays with fixed dimensions, and virtually all storage and computational space is contained within these arrays. Typically these arrays are dimensioned around 6000 words each, but through simple updates they could be changed to a much larger number, say 500,000 words. As a result, the code can be made to run an infinitely large and complex problem, as long as one has a computer with enough storage.

The first of these large arrays, referred to as the "container" (see Section 3.2.3.5.3), originated in the SSC code [11]. All of the variably dimensioned arrays, such as the pump head for each pump in the system, reside in the container array. This is accomplished by assigning a pointer into the container, referencing the location at which values for a given variable begin, and equivalencing each of the variable arrays to the container array. For example, one might have a pointer for the pump head, IH3PUM, with a value of 1092, in a deck with two pumps. The head for the first pump would be at location 1093 in the container, and the second pump head would be at location 1094. Of course, this is all fully automated and works quite smoothly.

The second of the large arrays is controlled by the Data Management Utility (see Section 3.2.3.5.4). It is used in the input processing phase to temporarily store incoming data, until it can be properly organized.

The third of these arrays is used for Array Data Type storage (see Section

3.2.3.5.4.4). It is used in performing various matrix calculations during the steady state and transient calculations.

There are a few variables that are not variably dimensioned. Almost always these are either scalars or of dimension 2, for the two sides of the heat exchangers. These fixed dimensioned values can in no way limit the size of the system that can be represented.

3.3.2 GLOBAL COMMONS AND USAGE (TABLE)

Many of the MINET variables reside in common blocks, which are shared by multiple subroutines and functions. In Table 3.3-1, the names of each subroutine and function having access to each of the common blocks is indicated.

3.3.3 NAMING CONVENTION

MINET was originally part of the larger SSC program library [11], and follows most of the naming conventions for that code. For this reason, the digit 3 appears in the second position in nearly all the MINET variables residing in common blocks. The naming convention for the initial letters of SSC variables is given in Table 3.3-2. Many of the variables in MINET do follow this convention, but we have, occasionally, strayed from these rules. The definitions provided in the next section, the data dictionary, take precedence.

3.3.4 DATA DICTIONARY

MINET variables are defined in the "Data Dictionary," shown in Table 3.3-3. Variables are listed alphabetically, along with their container pointer names, their dimensions, their definitions, and the name of the common block in which they reside.

Table 3.3-1 Common Block Usage

| COMMON | DEFINED IN | \$ = NOT REFERENCED | | | | | | | | | |
|--------|--------------------------------------|--------------------------------------|-------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|-------------------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| ADAB9U | ADDA9U RELA9U | ADDM9U | CRKR9U | GETA9U | GETM9U | IN49U | LE09U | NEWA9U | PRTA9U | PUTA9U | PUTM9U |
| BC3P | ADV3T SGBC3T | ENET3S | ETX3C WESM3S | GETB3U | INIT3S | IOSG3T | IPTS3R | PREP3T | PRFL3S | PRNT3C | PUTB3U |
| DATA9 | CRDR9R | INIT9U | PAGE9U | | | | | | | | |
| DCON9U | DEFP3R INTG9U NEWL9U RELD9U | DMOD3R IRPT9U NEWN9U RELL9U | GETD9U ISU9R NSIZ9U RELM9U | GETF9R LCNT9U NXTA9U RELN9U | GETM3R LOCL9U NXTM3R RISU9R | GETR9R LOCR9U ORDR3R RLID9U | GETR9U LSIZ9U PUTD9U SYS3R | INN9U LSTI9U PUTR9R | INPT9U MID9U PLTR9R | INRD3R NBR3R PUTR9U | INSL9U NET3R REAL9U |
| GC9U | GCER9U PGC19U | GCPR9U PGCR9U | GCTE9U REGC9U | GCTP9U SVGC9U | IGA9U | INGC9U | JGCT9U | LPNT9U | MVGA9U | MVGC9U | NPNT9U |
| GLOB3I | ADTB3T MINT3S SVCX3U | BKEY3S MRCH3S SYS3R | CALC3R VOLM3S | COMDUM PREP3T VOLS3T | CTRL3R PRFL3S WESM3S | ENET3S PRNT3C | FRAC3S PUTB3U | GETB3U QBAL3S | INIT3S QBRG3S | KPRC3S RECX3U | MDST3S SUBN3S |
| GLOB3V | ADTB3T PRNT3C | ADV3T PUMP3T | COMDUM RECX3U | HX3T SGBC3T | IOSG3T SVCX3U | LOAD3T SYS3R | MINT3S TBSG3T | MINT3T TIME3T | MRCH3T VALV3T | NET3T | PREP3T |
| HX3P | ADTB3T | ENET3S | HX3S | HX3T | IPTS3R | MDST3S | MODL3C | PRHX3S | PRNT3C | QBAL3S | QBRG3S |
| ISUV9R | GETF9R | GETI9R | GETR9R | ISU9R | PUTF9R | PUTI9R | PUTR9R | REPS9R | RISU9R | | |
| ITERP | CDINPT | ERRMSG | | | | | | | | | |
| LDAB9U | INL9U | INSL9U | LSTI9U | NEWL9U | NXTI9U | RELL9U | | | | | |
| LNKS3I | DEFP3R | FSTO3R | GETM3R | ILNK3R | KPRT3R | LINK3R | NBR3R | NXTO3R | PCNT3R | ZPRT3R | |
| LNK3P | ADTB3T MODL3C SGBC3T | ADV3T MRCH3S WESM3S | CALC3R MRCH3T | ENET3S NET3T | FRAC3S PREP3T | GETB3U PRFL3S | INIT3S PRHX3S | IOSG3T PRNT3C | IPTS3R PUTB3U | KPRC3S QBAL3S | MDST3S QBRG3S |
| MDAB9U | INL9U | INM9U | MID9U | MTYP9U | NEWN9U | NEWR9U | RLID9U | | | | |
| MODC3P | ADV3T | ENET3S | IPTS3R | KPRC3S | MDST3S | MODL3C | NET3T | PREP3T | PRNT3C | QBAL3S | QBRG3S |
| MODL3P | ADTB3T | ENET3S | ETX3C | IOSG3T | IPTS3R | MODL3C | PRNT3C | WESM3S | | | |
| MOD3I | BCOR3C PIPE3T | COMDUM PUMP3S | CROS3S PUMP3T | DP3C QPM3C | HTC3C TBSG3S | HXND3S TBSG3T | HX3S VALV3S | HX3T VALV3T | IMOD3C | MODL3C | PIPE3S |
| MOD3V | BCOR3C PIPE3S | COMDUM PIPE3T | CROS3S PUMP3S | DP3C PUMP3T | HTC3C QPM3C | HXND3S TBSG3S | HX3S TBSG3T | HX3T VALV3S | IMOD3C VALV3T | LOAD3T | MODL3C |

| COMMON | DEFINED IN | | \$ = NOT REFERENCED | | | | | | | | |
|--------|------------------|------------------|---------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|--------|
| NDAB9U | GETF9U PUTF9U | GETN9U PUTN9U | INN9U RELN9U | INPT9U | IRPT9U | LNKN9U | NEWN9U | NID9U | NSIZ9U | NXTA9U | NXTN9U |
| NET3P | ADV3T QBRG3S | ENET3S SUBN3S | INIT3S VOLM3S | IPTS3R WESM3S | KPRC3S | MRCH3S MRCH3T | NET3T | PRFL3S | PRNT3C | QBAL3S | |
| NODE3I | COMDUM | CROS3S | HXND3S | HX3S | | | | | | | |
| NODE3V | COMDUM | CROS3S | DP3C | HXND3S | HX3S | HX3T | LOAD3T | PIPE3S | PIPE3T | TBSG3S | TBSG3T |
| NODL3P | ADTB3T TBSG3T | ADV3T VALV3S | HX3S VALV3T | HX3T | IPTS3R | PIPE3S | PIPE3T | PRNT3C | PUMP3S | PUMP3T | TBSG3S |
| ORD3I | INOR3R | JDAT3R | LSTM3R | MARK3R | MORD3R | NCLS3R | NXTM3R | ORDR3R | PIDS3R | PUTJ3R | |
| PUMP3P | IPTS3R | PREP3T | PRNT3C | PUMP3S | PUMP3T | | | | | | |
| SATM3V | BCOR3C HWF3C | COMDUM HWN3C | CRIT3C HWSC3C | DP3C IMOD3C | DRDE3C RH03C | DRDP3C SATM3C | ENTH3C SAT03C | HCIT3C TEMP3C | HCOT3C VISC3C | HTC3C | HWCN3C |
| SATP3V | COMDUM | SATM3C | SATP3C | | | | | | | | |
| SAVE | GENRD | | | | | | | | | | |
| SCRH3R | DMOD3R | INIT3R | INRD3R | | | | | | | | |
| SCRH9I | CRDR9R | READ3R | | | | | | | | | |
| SEG3P | ADV3T NET3T | ENET3S PRFL3S | FRAC3S PRHX3S | INIT3S PRNT3C | IOSG3T QBAL3S | IPTS3R QBRG3S | KPRC3S SGBC3T | LOAD3T TBSG3S | MDST3S TBSG3T | MRCH3S WESM3S | MRCH3T |
| SNET3P | BKEY3S | ENET3S | FRAC3S | IPTS3R | KPRC3S | MDST3S | PRNT3C | QBAL3S | QBRG3S | SUBN3S | WESM3S |
| TIME3I | CTRL3R | INIT3R | SDEL9T | TIME3T | | | | | | | |
| TIME3P | IPTS3R | SDEL9T | | | | | | | | | |
| TIME3V | CTRL3R | TIME3T | | | | | | | | | |
| TRND3P | ADV3T | IPTS3R | PREP3T | SGBC3T | | | | | | | |
| TURB3P | IPTS3R | PREP3T | PRFL3S | PRNT3C | TBSG3S | TBSG3T | | | | | |
| UNID9I | IUN19U | UNIQ9U | | | | | | | | | |
| UNIT3I | DMOD3R SVCX3U | GETM3R | INIT3U | INRD3R | LINK3R | LIST3R | MINT3S | PRNT3C | PRTA9U | READ3R | RECX3U |
| UNIT9U | CRDR9R | ERR9U | INIT9U | MINET | PAGE9U | | | | | | |

| COMMON | DEFINED IN | \$ = NOT REFERENCED | | | | | | | | | | |
|--------|------------|---------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--|
| VALV3P | CALC3R | IOSG3T | IPTS3R | PREP3T | PRFL3S | PRNT3C | VALV3S | VALV3T | | | | |
| VD9V | ADTB3T | ADVN3T | BKEY3S | CALC3R | DPSV3C | ENET3S | ETX3C | EVLV3S | FRAC3S | GCPR9U | | |
| | GETB3U | HX3S | HX3T | INGC9U | INIT3S | IOSG3T | KPRC3S | LOAD3T | MODL3C | MRCH3S | | |
| | MRCH3T | MVGA9U | NET3T | PIPE3S | PIPE3T | PREP3T | PRFL3S | PRHX3S | PRNT3C | PUMP3S | PUMP3T | |
| | PUTB3U | QBAL3S | QBRG3S | REGC9U | SDEL9T | SGBC3T | SUBN3S | SVGC9U | TBSG3S | TBSG3T | VALV3S | |
| | VALV3T | VOLM3S | VOLS3T | WESM3S | | | | | | | | |
| VOL3P | ADVN3T | DPSV3C | ENET3S | EVLV3S | FLV3T | FRAC3S | INIT3S | IOSG3T | IPTS3R | KPRC3S | NET3T | |
| | PRFL3S | PRNT3C | QBAL3S | QBRG3S | SUBN3S | VALV3T | VOLM3S | VOLS3T | WESM3S | | | |

TABLE 3.3-2

Variable Naming Convention

| | | |
|---|--------------------------------------|------------------------|
| A | Area | m^2 |
| B | Mass | kg |
| C | Material properties; constants | |
| D | Density | kg/m^3 |
| E | Energy; enthalpy | J; J/kg |
| F | Fractions, factors | - |
| G | Mass flow rate per unit area | $kg/s\ m^2$ |
| H | Heat Transfer Coefficient | W/m^2K |
| L | Control flags, counters, etc. | |
| M | Maximum allowable dimension | |
| N | Actual dimension specified | |
| P | Pressure; power | N/m^2 ; W |
| Q | Surface heat flux; miscellaneous | W/m^2 ; -- |
| R | Angular Measure, Relative Speed | radians |
| S | Time | s |
| T | Temperature | K (not C) |
| U | Velocity, angular velocity or speed | m/s; rpm |
| V | Volume, Viscosity | m^3 , $N\cdot S/m^2$ |
| W | Mass flow rate | kg/s |
| X | Distance (length or radius) | m |
| Y | Distance (width or diameter) | m |
| Z | Distance (height or axial direction) | m |

Table 3.3-3 Data Dictionary

| | | | | |
|--------|--------|-------|---|----------|
| A3LPHA | IA3LPH | SGMNT | PR LOSS FACTOR, MULTIPLIES FLOW SQUARED | SEG3P |
| A3M | SCALAR | - | IDENTIFIER FOR SEGMENT MATRIX A | GLOBAL3P |
| A3NODE | - | 2 | FLOW AREA OF MODULE, PER PARRALEL PATH, PER TUB FOR HX | MOD3V |
| A3PUMP | IA3PUM | SPUMP | COEFFICIENTS OF HEAD VS SPEED, FLOW CURVE | PUMP3P |
| A3STRC | IA3STR | HX | SURFACE AREA BETWEEN STRUCTURE AND FLUID, SUM OVR PTHS | HX3P |
| B3ETA | IB3ETA | SGMNT | PR LOSS PARAMETER, INCLUDES GRAVITY | SEG3P |
| B3M | SCALAR | - | IDENTIFIER FOR SEGMENT MATRIX B | GLOBAL3V |
| B3STRC | IB3STR | HX | MASS OF STRUCTURE, SUMMED OVER ALL PARALLEL PATHS | HX3P |
| C3ATBS | IC3ATB | TURBN | COSINE OF ANGLE ALPHA, INPUT ON 601 CARD | TURB3P |
| C3M | IC3M | SGMNT | IDENTIFIER FOR SEGMENT MATRIX C | SEG3P |
| C3ONDF | - | - | THERMAL CONDUCTIVITY OF SATURATED FLUID | SATP3V |
| C3ONFM | - | 2 | THERMAL CONDUCTIVITY OF SATURATED FLUID | SATM3V |
| C3PLF | - | - | SPECIFIC HEAT OF SATURATED FLUID | SATP3V |
| C3PLFM | - | 2 | SPECIFIC HEAT OF SATURATED FLUID | SATM3V |
| C9ASTO | ARRAY | - | CONTAINER ARRAY FOR BLOCK STORAGE | ADAB9U |
| C9GNMS | ARRAY | - | GLOBAL CONTAINER BLOCK NAME TABLE | GC9U |
| C9GPTS | ARRAY | - | GLOBAL CONTAINER BLOCK POINTER TABLE | GC9U |
| C9NSTO | ARRAY | - | CONTAINER ARRAY FOR NODE DATA STORAGE | NDAB9U |
| C9VDIM | ANY | ALL | GLOBAL CONTAINER ARRAY | VD9V |
| D3ALOG | - | 2 | HX GEOMETRIC PARAM. 1-LN(DCENT/DIAM,1), 2-LN(DIAM,2/DC) | MOD3V |
| D3CENT | - | - | HX TUBE DIAMETER AT CENTER OF TUBE WALL, (OD+ID)/2 | MOD3V |
| D3COI | - | - | HELICAL COIL DIAMETER, 0.0 FOR STRAIGHT TUBE | MOD3V |
| D3COIL | ID3COI | HX | HELICAL COIL DIAMETER, 0 IF STRAIGHT TUBES | MODL3P |
| D3DRDE | ID3DRE | NODE | DERVITIVE OF NOD AVE DENSITY WITH RSPCT TO ENTHALPY | NODL3P |
| D3DRDP | ID3DRP | NODE | DERIVATIVE OF NODE AVE DENSITY WITH RESPECT TO PRESSUR | NODL3P |
| D3EFDP | - | - | DERIVATIVE OF SATURATED FLUID ENTHALPY WRT PRESSURE | SATP3V |
| D3EFPD | - | 2 | DERIVATIVE OF SATURATED FLUID ENTHALPY WRT PRESSURE | SATM3V |
| D3EODP | - | - | DERIVATIVE OF SATURATED VAPOR ENTHALPY WRT PRESSURE | SATP3V |
| D3EOPD | - | 2 | DERIVATIVE OF SATURATED VAPOR ENTHALPY WRT PRESSURE | SATM3V |
| D3EREF | ID3ERE | TURBN | SQUARE ROOT OF ENTHALPY DROP AT REFERENCE CONDITIONS | TURB3P |
| D3EQ | - | 2 | EQUIVALENT HYDRAULIC DIAMETER | MOD3V |
| D3QDEB | ID3QDE | NODE | DERIVATIVE OF HEAT TRANSFER(Q3CB) W.R.T. NOD AV ENTHP | NODL3P |
| D3QDEW | ID3QDW | NODE | DERIVATIVE OF HEAT TRANSFER(Q3CB) W.R.T. NOD AV FLOW | NODL3P |
| D3HPUM | ID3HPU | PUMP | DERIVATIVE OF PUMP HEAD W.R.T. MASS FLOW RATE | PUMP3P |
| D3IAM | - | 2 | DIAMETER, 1-INSIDE PIPE OR TUBE, 2-TUBE OUTER DIAMETER | MOD3V |
| D3M | SCALAR | - | IDENTIFIER FOR VOLUME MATRIX D | GLOBAL3V |
| D3QDE | - | - | DERIVATIVE OF HEAT TRANSFER RATE INTO NOD WRT ENTHALP | NODE3V |
| D3QDW | - | - | DERIVATIVE OF HEAT TRANSFER RATE INTO NOD WRT PRSSURE | NODE3V |
| D3RDE | - | - | DERIVATIVE OF NOD AVE DENSITY WRT ENTHALPY | NODE3V |
| D3RDP | - | - | DERIVATIVE OF NOD AVE DENSITY WRT PRESSURE | NODE3V |
| D3RFDP | - | - | DERIVATIVE OF SATURATED FLUID DENSITY WRT PRESSURE | SATP3V |
| D3RFPM | - | 2 | DERIVATIVE OF SATURATED FLUID DENSITY WRT PRESSURE | SATM3V |
| D3RGDP | - | - | DERIVATIVE OF SATURATED VAPOR DENSITY WRT PRESSURE | SATP3V |
| D3RGPM | - | 2 | DERIVATIVE OF SATURATED VAPOR ENTHALPY WRT PRESSURE | SATM3V |
| D3VRE | ID3VRE | VOLUM | VOL AVE DERIV OF DENSITY W.R.T. ENTHALPY | VOL3P |
| D3VRP | ID3VRP | VOLUM | VOL AVE DERIV OF DENSITY W.R.T. PRESSURE | VOL3P |
| D3Z | - | - | RATIO OF NODE LENTH TO AREA, USED FOR INERTIA | NODE3V |
| D3ZA | ID3ZA | NODE | LENGTH OVER AREA FOR NODE | NODL3P |
| E3BAR | - | 2 | NODE AVERAGE ENTHALPY | NODE3V |
| E3BC | IE3BC | BC | ENTHALPY OF FLUID PASSING THROUGH BOUNDARY MODULE | BC3P |
| E3CB | IE3CB | NODE | NODE AVERAGE ENTHALPY | NODL3P |
| E3F | - | - | SATURATED FLUID ENTHALPY | SATP3V |
| E3FGEN | IE3FGE | TURBN | EFFICIENCY TO ELECTRICAL GRID | TURB3P |
| E3FOM | - | 2 | E3OM-E3FM | SATM3V |
| E3FM | - | 2 | SATURATED FLUID ENTHALPY | SATM3V |
| E3FTSG | IE3FTS | TURBN | EFFICIENCY OF TURBINE STAGE AT GIVEN TIME | TURB3P |
| E3O | - | - | SATURATED VAPOR ENTHALPY | SATP3V |
| E3OM | - | 2 | SATURATED VAPOR ENTHALPY | SATM3V |
| E3IN | - | 2 | ENTHALPY AT NODE INLET | NODE3V |
| E3OUT | - | 2 | ENTHALPY AT NODE OUTLET | NODE3V |
| E3INSL | IE3INS | SGMNT | FLUID ENTH AT SEGMENT INLET | SEG3P |
| E3M | SCALAR | - | IDENTIFIER FOR VOLUME MATRIX E | GLOBAL3V |
| E3M11 | IE3M11 | MOD | ENTHALPY OF FLOW ENTERING MODULE, INSIDE TUBES IN HX | MODC3P |
| E3M10 | IE3M10 | HX NO | ENTHALPY OF FLUID ENTERING HX, TO PASS OUTSIDE TUBES | MODC3P |
| E3MOD1 | - | 2 | ENTHALPY OF FLUID ENTERING MODULE | MOD3V |
| E3MOD0 | - | 2 | ENTHALPY OF FLUID LEAVING MODULE | MOD3V |
| E3M01 | IE3M01 | MOD | ENTHALPY OF FLOW LEAVING MODULE, INSIDE TUBES OF HX | MODC3P |
| E3M00 | IE3M00 | HX NO | ENTHALPY OF FLUID LEAVING HX, AFTER PASSING OUTSID TBS | MODC3P |
| E3OTSL | IE3OTS | SGMNT | FLUID ENTH AT SEGMENT OUTLET | SEG3P |
| E3PS | - | 2 | SURFACE ROUGHNESS FACTOR | MOD3V |
| E3PS1 | IE3PS1 | MODUL | SURFACE ROUGHNESS TO DIAMETER RATIO | MODL3P |
| E3TAB | IE3TAB | NBCTB | ENTHALPY ENTRY FOR BOUNDARY TABLE | TRND3P |
| E3VOL | IE3VOL | VOLUM | VOLUME AVERAGE ENTHALPY | VOL3P |
| E3WSSG | IE3WSS | NDINF | ENTHALPY AT THE NODAL INTERFACE | NODL3P |
| F3AEFF | IF3AEF | TURBN | EFFICIENCY ADJUSTMENT FACTOR | TURB3P |
| F3AQ | IF3AQ | HX NO | AREA CORRECTION FACTOR, CALCD IN STEADY STATE HX CALCS | HX3P |
| F3CCF | - | 2 | FLOW DIRECTION MULTIPLIER, -1=COUNTER, 0=CROSS, 1=PARLL | MOD3V |
| F3CCFL | IF3CCF | HX | FLOW DIRECTION, 1.-PARALLEL, 0.-CROSS, -1.-COUNTER | MODL3P |
| F3HBRG | IF3HBR | SN*SN | HEAT TRANSFER BRIDGE FACTOR, =1 FOR NON-PRNCPL BRIDG | SNET3P |
| F3INLV | IF3INL | SGMNT | REL POSITON OF SEGMENT INLET JUNCTION WITH VOLUM OR B | SEG3P |

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| F31TO | - | - | RATIO OF AXIAL FLOW LENGTH INSID TUB TO OUTSID,1-STRT | MOD3V |
| F31TOO | IF31TO | HX | RATIO OF LENGTH,INSIDE TUB TO OUTSIDE,0 FOR STRAT TUB | MODL3P |
| F3KMI | IF3KMI | MODUL | FORM LOSS FACTOR,INSIDE TUBES IF HEAT EXCHANGER (HX) | MODL3P |
| F3KMO | IF3KMO | HX | FORM LOSS FACTOR OUTSIDE HX TUBES | MODL3P |
| F3KMOD | - | 2 | MODULE FORM LOSS FACTOR | MOD3V |
| F3KSTB | IF3KST | TURBN | STADOLA CONSTANT FOR TURBINE STAGE | TURB3P |
| F3LQLV | IF3LQL | VOLUM | RELATIVE VERTICAL POSITION OF TOP OF LIQUID REGION | VOL3P |
| F3NPAT | - | - | NUMBER OF PARALLEL FLOW PATHS,INCL TUBS FOR HX | MOD3V |
| F3NTUB | - | - | NUMBER OF TUBES IN HEAT EXCHANGER | PUMP3P |
| F3OTLV | IF3OTL | SGMNT | REL POSITON OF SEGMENT OUTLT JUNCTION WITH | SEG3P |
| F3PUMP | IF3PUM | PUMP | CURRENT PUMP SPEED | PUMP3P |
| F3QSEC | IF3QSE | SGMNT | ADJUSTMENT FACTOR FOR NON-HX MODS IN SEGMENT(*QMOD) | SEG3P |
| F3QVOL | IF3QVO | VOLUM | HEATING ADJUST. FACTOR FOR VOLUME,SEE F3QSEC | VOL3P |
| F3REF | IF3REF | PUMP | REFERENCE PUMP SPEED IN RPM | PUMP3P |
| F3SOSN | IF3SOS | SG*SN | FRACTION OF SEGMENT FLOW GOING TO GIVEN SUBNETWORK | SNET3P |
| F3STGA | IF3STO | VALVE | AREA-STEM POWER,AREA=A3VMAX*S3VPOS**F3STOA | VALV3P |
| F3TBDP | IF3TBP | HX | PITCH-TO-DIAMETER RATIO FOR HX TUBES | MODL3P |
| F3VALV | IF3VAL | VALVE | FORM LOSS COEFFICIENT FOR VALVE OPENING | VALV3P |
| F3VLSN | IF3VLS | VL*SN | FRACTION OF VOLUME FLOW GOING TO GIVEN SUBNETWORK | SNET3P |
| F3VMAX | IF3VMA | VOLUM | RELATIVE POSITION OF MODULE MAX ELEV,REL TO COMPNT HT | VOL3P |
| F3VMIN | IF3VM | VOLUM | RELATIVE POSITION OF MODULE MIN ELEV,REL TO COMPNT HT | VOL3P |
| G3BAR | - | 2 | NODE AVERAGE MASS VELOCITY,=W3BAR/AREA | NODE3V |
| H3PUMP | IH3PUM | PUMP | PUMP HEAD AT CURRENT CONDITIONS | PUMP3P |
| H3REF | IH3REF | PUMP | REFERENCE PUMP HEAD IN METERS | PUMP3P |
| I3BCTP | I13BCT | BC | KEYS PRESSURE FLOW ENTRY,1-FLOW,2-PRESSURE | TRND3P |
| I3CHOK | I13CHO | VALVE | CHOKING OPTION,0-IGNORE,1-CALCULATE CHOKE FLOW LIMIT | VALV3P |
| I3DLST | ARRAY | - | ARRAY OF POINTERS TO TEMPORARY INPUT STORAGE LISTS | SCRH3R |
| I3FTI | I13FTI | MODUL | FLUID TYPE IN MODULE,INSIDE TUBES IF HX | MODL3P |
| I3FTO | I13FTO | HX | FLUID TYPE PASSING OUTSIDE HX TUBES OF HX | MODL3P |
| I3FTYP | - | 2 | FLUID TYPE,1-WATER,2-NA,3-AIR,4-NAK | MOD3I |
| I3GRID | I13GRI | HX | HX TUBE CONFIGURATION,1-COAX,4-SQUAR,6-HEX(TRIANGULR) | MODL3P |
| I3LEVT | - | 2 | CRITICAL HEAT FLUX LEVEL TYPE,1-INSIDE,2-OUTSIDE TUBES | MOD3I |
| I3LVTI | I13LVI | HX | CRITICAL HEAT FLUX TYPE INSIDE TUBES | MODL3P |
| I3LVTO | I13LVO | HX | CRITICAL HEAT FLUX TYPE OUTSIDE TUBES | MODL3P |
| I3NFTP | I13NFT | NETWK | FLUID TYPE IN NETWORK,1-H2O,2-NA,3-AIR,4-NAK | NET3P |
| I3POPT | I13POP | PUMP | PUMP SPEED CONTROL OPTION INDICATOR | PUMP3P |
| I3SGVL | I13SGV | SGMNT | ORDINATE NUMBER OF LAST VALVE IN SEGMENT | SEG3P |
| I3TOPT | I13TOP | TURBN | TRANSIENT CONTROL OPTION FOR SPEED INDICATOR | TURB3P |
| I3TTYP | I13TTY | TURBN | TURBINE STAGE TYPE,1-IMPULSE,2-IMPULSE-REACTION | TURB3P |
| I3VOPT | I13VOP | VALVE | OPTION FOR CONTROLLING THE VALVE STEM POSITION | VALV3P |
| I9E1TM | SCALAR | - | POINTER TO DEFAULT ERROR ITEM SPECIFICATION | ISUV9R |
| I9F5PC | SCALAR | - | POINTER TO CURRENTLY OPEN FILE SPECIFICATION | ISUV9R |
| I9F5TA | SCALAR | - | POINTER TO BEGINNING FIRST ALLOCATED BLOCK | ADAB9U |
| I9F5TT | SCALAR | - | FIRST POINTER TABLE LOCATION | ADAB9U |
| I9I5PC | SCALAR | - | POINTER TO CURRENTLY OPEN ITEM SPECIFICATION | ISUV9R |
| I9L5TA | SCALAR | - | POINTER TO BEGINNING OF LAST ALLOCATED BLOCK | ADAB9U |
| I9L5TT | SCALAR | - | LAST POINTER TABLE LOCATION | ADAB9U |
| I9M5XA | SCALAR | - | LAST ARRAY LOCATION AVAILABLE FOR BLOCK STORAGE | ADAB9U |
| I9N5TO | SCALAR | - | OFFSET TO OF NEXT FREE NODE DATA STORAGE LOCATION | NDAB9U |
| I9R5PC | SCALAR | - | POINTER TO CURRENTLY OPEN RECORD SPECIFICATION | ISUV9R |
| J3BMOD | IJ3BMO | BC | CONVERTS BOUNDARY ORDINATE NO. TO MODULE NO. | BC3P |
| J3FHXX | IJ3FHX | HX NO | FIRST TUBE NODE IN HX | LNK3P |
| J3F1I | IJ3F1I | MODUL | FIRST NODAL INTERFACE IN MODULE,INSIDE TUBES IF HX | LNK3P |
| J3F1O | IJ3F1O | HX NO | FIRST NODAL INTERFACE OUTSIDE TUBES | LNK3P |
| J3LHXX | IJ3LHX | HX NO | LAST TUBE NODE IN HX | LNK3P |
| J3L1I | IJ3L1I | MODUL | LAST NODAL INTERFACE IN MODULE,INSIDE TUBES IF HX | LNK3P |
| J3FINF | - | 2 | FIRST NODAL INTERFACE NO.,IF 2,THEN OUTSIDE HX TUBES | MOD3I |
| J3FNI | IJ3FNI | MODUL | FIRST NODE IN MODULE,INSIDE TUBES IF HX | LNK3P |
| J3FNO | IJ3FNO | HX NO | FIRST NODE,OUTSIDE TUBES | LNK3P |
| J3LNO | IJ3LNO | HX NO | LAST NODE,OUTSIDE TUBES | LNK3P |
| J3FNOD | - | 2 | FIRST NODE NO.,IF 2, THEN OUTSIDE HX TUBES | MOD3I |
| J3FTNO | - | - | HX NODE NUMBER FOR FIRST NODE IN HX | MOD3I |
| J3LINF | - | 2 | LAST NODAL INTERFACE NO.,IF 2,THEN OUTSIDE HX TUBES | MOD3I |
| J3L1O | IJ3L1O | HX NO | LAST NODAL INTERFACE OUTSIDE TUBES | LNK3P |
| J3LNI | IJ3LNI | MODUL | LAST NODE IN MODULE,INSIDE TUBES IF HX | LNK3P |
| J3LNOD | - | 2 | LAST NODE NO.,IF 2,THEN OUTSIDE HX TUBES | MOD3I |
| J3LTNO | - | - | HX NODE NUMBER FOR LAST NODE IN HX | MOD3I |
| J3MDID | IJ3MDI | MODUL | MODULE IDENTIFICATION NUMBER,EG,MODULE 9 HAS ID 501 | LNK3P |
| J3ORD | IJ3ORD | MODUL | MODULE TYPE ORDINATE NUMBER,EG,MOD 24 IS VALV NO. 6 | LNK3P |
| J3SIDE | IJ3SID | SGMODS | CONVERTS SEGMOD NO. TO SIDE,=2 IF OUTSIDE HX TUBES | LNK3P |
| J3SMOD | IJ3SM | SGMODS | CONVERTS SEGMOD NO. TO MODULE NUMBER | LNK3P |
| J3VMOD | IJ3VMO | VOLUM | CONVERTS VOLUME ORDINAT NO. TO MODULE NUMBER | VOL3P |
| J3VPRS | IJ3VPR | VALVE | VOLUME WHERE PRSSUR MONITRD, ID INPUT,CONVRTD TO ORDNT | VALV3P |
| J9IFLD | SCALAR | - | INDEX OF ITEM FIELD COUNT IN K9I5PC | ISUV9R |
| J9IREP | SCALAR | - | INDEX OF FIRST REPEATING ITEM NUMBER ENTRY IN K9R5PX | ISUV9R |
| J9ITEM | SCALAR | - | INDEX OF CURRENT ITEM SPEC POINTER IN RECORD SPEC | ISUV9R |
| J9ITYP | SCALAR | - | INDEX OF ITEM TYPE ENTRY IN K9I5PC | ISUV9R |
| J9LNUM | SCALAR | - | INDEX OF LIST NUMBER ENTRY IN K9R5PX | ISUV9R |
| J9LSTI | SCALAR | - | INDEX OF LAST ITEM POINTER IN K9LNK2 | LDAB9U |
| J9MID | SCALAR | - | INDEX OF MODULE ID IN HEADER NODE | IDAB9U |

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| J9MTYP | SCALAR | - | INDEX OF MODULE TYPE ENTRY IN K9MHJR | MDAB9U |
| J9NDL | SCALAR | - | INDEX OF RECORD MODULE TYPE IN K9RSPX | ISUV9R |
| J9NFLD | SCALAR | - | OFFSET TO NODE DATA LENGTH ENTRY | NDAB9U |
| J9NID | SCALAR | - | INDEX OF FIELD COUNT ENTRY IN K9RSPX | ISUV9R |
| J9NXTI | SCALAR | - | OFFSET OF NODE ID | NDAB9U |
| J9NXTN | SCALAR | - | INDEX OF NEXT ITEM POINTER IN K9LNK2 | LDAB9U |
| J9PTBL | SCALAR | - | OFFSET OF LINK TO NEXT NODE | NDAB9U |
| J9RLST | SCALAR | - | POINTER TABLE IDENTIFIER | ADAB9U |
| J9RTYP | SCALAR | - | INDEX OF RECORD SPECIFICATION LIST POINTER IN K9COMP | ISUV9R |
| J9UNIT | SCALAR | - | INDEX OF RECORD TYPE ENTRY IN K9RSPX | ISUV9R |
| J9UNIT | SCALAR | - | INDEX OF ITEM UNITS ENTRY IN K9ISPC | ISUV9R |
| K3BCSG | IK3BCS | BC | SEGMENT NO. ATTCHD TO BOUNDRY, IF .LT. 0 FLOW INTO SEGMENT | BC3P |
| K3EBC | IK3EBC | BC | TYPE OF THERMAL PARAM SPECFD, 1-ENTH, 2-TEMP, 3-QUALITY | BC3P |
| K3EBST | IK3EBS | BC | STATUS OF BOUNDARY, CLOSED/FIXED OUTLET TEMP IF K3EB=2 | BC3P |
| K3ETAB | IK3ETA | BC | KEYS ENTHALPY/TEMP/QUAL, 1-ENTH, 2-TEMP, 3-QUAL | TRND3P |
| K3HBRG | IK3HBR | SN*SN | KEY TO HEAT TRANSFER BRIDGES, INDICATES IF ADJUSTABLE | SNET3P |
| K3NETW | IK3NET | BC | NETWORK TO WHICH BOUNDARY ATTACHES | BC3P |
| K3NTI | IK3NTI | HX NO | NETWORK IN WHICH FLUID PASSING INSIDE TUBES BELONGS | HX3P |
| K3NTO | IK3NTO | HX NO | NETWORK IN WHICH FLUID PASSING OUTSIDE TUBES BELONGS | HX3P |
| K3OPCL | IK3OPC | SN | KEYS WHETHER SUBNET IS OPEN(1) OR CLOSED(2)=FXD OUT E | SNET3P |
| K3SOPR | IK3SOP | SGMNT | DESIGNATES SUBNT TO WHICH SGMNT PRINCIPALLY CONTRIBTS | SEG3P |
| K3SNI | IK3SNI | HX NO | SUBNETWORK TO WHICH FLUID PASSNG INS. TUBES ASSIGNED | HX3P |
| K3SNO | IK3SNO | HX NO | SUBNETWORK TO WHICH FLUID PASSNG OUTS. TUBES ASSIGNED | HX3P |
| K3VLPR | IK3VLP | VOLUM | DESIGNATES SBNT NO. TO WHICH VOLM PRNCPALLY CONTRBUTS | VOL3P |
| K9ASTO | ARRAY | - | INTEGER EQUIVALENT TO C9ASTO | ADAB9U |
| K9CLAS | SCALAR | - | MODULE PORT CLASS DATA AREA | LNKS3I |
| K9COMP | SCALAR | - | FILE COMPONENT DATA AREA IDENTIFIER | ISUV9R |
| K9DAID | SCALAR | - | MODULE PORT DATUM DATA AREA IDENTIFIER | |
| K9ELEV | SCALAR | - | MODULE PORT ELEVATION DATA AREA | |
| K9ISPC | SCALAR | - | ITEM SPECIFICATION DATA AREA IDENTIFIER | LNKS3I |
| K9LHDR | SCALAR | - | IDENTIFIER FOR LIST HEADER MODULE | ISUV9R |
| K9LNK2 | SCALAR | - | LIST ITEM LINK DATA AREA IDENTIFIER | LDAB9U |
| K9MHDR | SCALAR | - | ID OF MODULE HEADER NODE | LDAB9U |
| K9NBRM | SCALAR | - | MODULE PORT NEIGHBOR MODULE POINTER DATA AREA | MDAB9U |
| K9NBRP | SCALAR | - | MODULE PORT NEIGHBOR PORT IDENTIFIER DATA AREA | LNKS3I |
| K9NSTO | ARRAY | - | INTEGER EQUIVALENT OF C9NSTO | LNKS3I |
| K9PIDS | SCALAR | - | MODULE PORT IDENTIFIER DATA AREA | NDAB9U |
| K9RCMP | SCALAR | - | RECORD COMPONENT DATA AREA IDENTIFIER | LNKS3I |
| K9RSPX | SCALAR | - | RECORD SPECIFICATION DATA AREA IDENTIFIER | ISUV9R |
| L3CNTR | SCALAR | - | LENGTH OF GLOBAL CONTAINER ARRAY | ISUV9R |
| L3PASS | IL3PAS | HX NO | USED IN STEADY STATE FOR HX STATUS, 2 IF SECOND PASS | GLOB3I |
| L3PRNT | SCALAR | - | PRINT OPTION, 1-SUMMARY, 2-SOME DETAIL, 3-MOST DETAILED | HX3P |
| L3PRON | SCALAR | - | STEP NUMBER TO BE REACHED BEFORE FREQUENT PRINTS | GLOB3I |
| L3PSEP | IL3PSE | VOLUM | VOLUME CONTENTS, 1-HOMOGENEOUS, 2-SEPARAT BY PHAS, 3-1;2 | GLOB3I |
| L3TYPE | IL3TYP | MODUL | MODULE TYPE, 1-PIP, 2-HX, 3-PMP, 4-VOL, 5-BC, 6-VALV, 7-TBSG | VOL3P |
| L3STEP | SCALAR | - | TIME STEP NUMBER, 0=STEADY STATE | LNKS3P |
| L3VSHP | IL3VSH | VOLUM | SHAPE OF VOLUME, 1-VERT CYLNDR OR BOX, 2-HORIZNTL CYLND | GLOB3I |
| L9ASIZ | ARRAY | - | GLOBAL CONTAINER BLOCK SIZE TABLE | VOL3P |
| L9ASIZ | SCALAR | - | SIZE OF ATOM DATA AREA | GC9U |
| L9F5PC | SCALAR | - | POINTER TO FILE SPECIFICATION LIST | NDAB9U |
| L9GC | SCALAR | - | CURRENT SIZE OF GLOBAL CONTAINER SEGMENT | ISUV9R |
| L9GCOU | SCALAR | - | LOGICAL UNIT NUMBER OF GCM OUTPUT FILE | ISUV9R |
| L9GCRE | SCALAR | - | LOGICAL UNIT NUMBER OF GCM SEGMENT RESTORE FILE | GC9U |
| L9GCSV | SCALAR | - | LOGICAL UNIT NUMBER OF GCM SEGMENT SAVE FILE | GC9U |
| L9ISPC | SCALAR | - | POINTER TO RECORD SPECIFICATION LIST | GC9U |
| L9ISPC | SCALAR | - | POINTER TO INPUT DATA ITEM SPECIFICATION LIST | ISUV9R |
| L9ISUJ | SCALAR | - | ISU STATUS FLAG | ISUV9R |
| L9NHDR | SCALAR | - | LENGTH OF NODE HEADER | ISUV9R |
| L9NIL | SCALAR | - | NIL VALUE | NDAB9U |
| L9NSTO | SCALAR | - | MAXIMUM LENGTH OF NODE DATA STORAGE AREA | DCON9U |
| M3CORE | IM3COR | HX | MATERIAL TYPE OF CORE TUBE | NDAB9U |
| M3ODEL | - | 2 | MOST RECENT HEAT TRANSFER MODE | HX3P |
| M3ODET | - | 2 | TOTAL HEAT TRANSFER MODE FOR NODE | NODE3I |
| M3ODI | IM3ODI | HXNOD | HEAT TRANSFER MODE FOR FLUID INSIDE TUBE | NODE3I |
| M3ODO | IM3ODO | HXNOD | HEAT TRANSFER MODE FOR FLUID OUTSIDE TUBE | HX3P |
| M3STRC | IM3STR | HX | MATERIAL TYPE OF HX SHELL AND STRUCTURE | HX3P |
| M3TYP | - | - | MATERIAL TYPE FOR HX TUBING | HX3P |
| M3TYPE | IM3TYP | HX | STRUCTURAL MATERIAL TYPE FOR TUBING | MOD3I |
| N3BCS | SCALAR | - | NUMBER OF BOUNDARY MODULES IN SYSTEM | MOD3I |
| N3ETID | IN3ETI | NETWK | IDENTIFICATION NUMBER OF NETWORK | MODL3P |
| N3FMLP | IN3FML | SGMNT | SEGMENT CNTR OF 1ST MODULE IN SEGMENT | GLOB3I |
| N3FNB | IN3FNB | NETWK | ORDINATE NO. OF FIRST BOUNDARY MODULE IN NETWORK | NET3P |
| N3FNSG | IN3FNS | NETWK | ORDINATE NO. OF FIRST SEGMENT IN NETWORK | NET3P |
| N3FNNS | IN3FNNS | NETWK | ORDINATE NO. OF FIRST SUBNETWORK IN NETWORK | NET3P |
| N3FNVL | IN3FNV | NETWK | ORDINATE NO. OF FIRST VOLUME IN NETWORK | NET3P |
| N3FP | IN3FP | VOLUM | ORDINATE NUMBER OF FIRST PORT ON VOLUME | NET3P |
| N3HXS | SCALAR | - | NUMBER OF HEAT EXCHANGERS IN SYSTEM | VOL3P |
| N3MLP | IN3ML | SGMNT | SEGMENT CNTR OF 1ST MODULE IN SEGMENT | GLOB3I |
| N3LNB | IN3LNB | NETWK | ORDINATE NO. OF LAST BOUNDARY MODULE IN NETWORK | NET3P |
| N3LNSG | IN3LNS | NETWK | ORDINATE NO. OF LAST SEGMENT IN NETWORK | NET3P |

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| N3LNSN | IN3LNN | NETWK | ORDINATE NO. OF LAST SUBNETWORK IN NETWORK | NET3P |
| N3LVN | IN3LV | NETWK | ORDINATE NO. OF LAST VOLUME IN NETWORK | NET3P |
| N3LVIN | IN3LVI | SGMNT | NUMBER OF MODULE ATTACHED TO SEGMENT INLET (VOL/BC) | SEG3P |
| N3LVOT | IN3LVO | SGMNT | NUMBER OF MODULE ATTACHED TO SEGMENT OUTLET (VOL/BC) | SEG3P |
| N3MODS | SCALAR | - | NUMBER OF MODULES IN SYSTEM | GLOB3I |
| N3NETS | SCALAR | - | NUMBER OF NETWORKS IN SYSTEM | GLOB3I |
| N3NB | IN3NB | NETWK | NUMBER OF BOUNDARY MODULES IN NETWORK | NET3P |
| N3NODE | IN3NOD | MODUL | NUMBER OF AXIAL NODES IN MODULE | MODL3P |
| N3NODS | - | - | NUMBER OF AXIAL NODES IN MODULE | MOD3I |
| N3NSEG | IN3NSE | NETWK | NUMBER OF SEGMENTS IN NETWORK | NET3P |
| N3NSNS | IN3NSN | NETWK | NUMBER OF SUBNETWORKS IN NETWORK | NET3P |
| N3NSVL | IN3NSV | NETWK | NUMBER OF SEPARATED VOLUMES IN NETWORK | NET3P |
| N3NVOL | IN3NVO | NETWK | NUMBER OF VOLUMES IN NETWORK | NET3P |
| N3OPSN | SCALAR | - | NUMBER OF OPEN SUB-NETWORKS IN SYSTEM | GLOB3I |
| N3PATH | IN3PAT | MODUL | NUMBER OF PARALLEL COMPONENTS REPRESENTED BY MODULE | MODL3P |
| N3PORT | IN3POR | VOLUM | NUMBER OF PORTS ON VOLUME | VOL3P |
| N3PT | IN3PT | PUMP | NUMBER OF ENTRIES IN PUMP SPEED TABLE | TRND3P |
| N3PUMS | SCALAR | - | NUMBER OF PUMPS IN SYSTEM | GLOB3I |
| N3QT | IN3CT | MODUL | NUMBER OF TIME TABLE ENTRIES FOR MODULE HEATING | TRND3P |
| N3ROWS | IN3ROW | SGMNT | NUMBER OF ROWS IN SEGMENT MATRIX EQ.(2*(NODES+1)) | SEG3P |
| N3SEOS | SCALAR | - | NUMBER OF SEGMENTS IN SYSTEM | GLOB3I |
| N3SNTS | SCALAR | - | NUMBER OF SUB-NETWORKS IN SYSTEM | GLOB3I |
| N3TAB | IN3TAB | BC | NUMBER OF TIME TABLE ENTRIES FOR BOUNDARY | TRND3P |
| N3TRBS | SCALAR | - | NUMBER OF TURBIN-STAGE MODULES IN SYSTEM | GLOB3I |
| N3TSTB | IN3TST | TURBN | NUMBER OF ENTRIES IN TURBINE SPEED TABLE | TRND3P |
| N3TUBE | IN3TUB | HX | NUMBER OF TUBES IN HEAT EXCHANGER | MODL3P |
| N3VALS | SCALAR | - | NUMBER OF VALVES IN SYSTEM | GLOB3I |
| N3VISB | IN3VIS | VOLUM | SEGMENT NO. ATTCHD TO VOLM PORT, IF LT.0 FLOW INTO SGM | VOL3P |
| N3VOLS | SCALAR | - | NUMBER OF VOLUMES IN SYSTEM | GLOB3I |
| N3VT | IN3VT | VALV | NUMBER OF ENTRIES IN VALVE POSITION TABLE | TRND3P |
| N9MHDR | SCALAR | - | SIZE OF K9MHDR | MDAB9U |
| N9SMAX | SCALAR | - | MAXIMUM SIZE OF GLOBAL CONTAINER SEGMENT | GC9U |
| N9TMAX | SCALAR | - | MAXIMUM SIZE OF GLOBAL CONTAINER BLOCK TABLES | GC9U |
| N9TSLZ | SCALAR | - | CURRENT SIZE OF GLOBAL CONTAINER BLOCK TABLES | GC9U |
| P3BC | IP3BC | BC | PRESSURE AT BOUNDARY | BC3P |
| P3INSL | IP3INS | SGMNT | PR AT THE SEGMENT INLET | SEG3P |
| P3ITRF | IP3ITR | TURBN | REFERENCE INLET PRESSURE | TURB3P |
| P3MDI | IP3MDI | MOD | PRESSURE IN MODULE (=SEGMENT AVE PRESSURE) | MODC3P |
| P3MDO | IP3MDO | HX NO | PRESSURE OF FLUID PASSING OUTSIDE HX TUBES | MODC3P |
| P3MOD | - | 2 | PRESSURE IN MODULE, 2 FOR HX FLUID OUTSIDE TUBES | MOD3V |
| P3OD | - | - | HX TUBE PITCH TO DIAMETER RATIO | MOD3V |
| P3OTRF | IP3OTR | TURBN | REFERENCE OUTLET PRESSURE | TURB3P |
| P3OTSL | IP3OTS | SGMNT | PR AT THE SEGMENT OUTLET | SEG3P |
| P3REF | - | - | PRESSURE AT WHICH SATURATION PROPERTIES EVALUATED | SATP3V |
| P3REFM | - | 2 | REFERENCE PRESSURE ON GIVEN SIDE OF TUBES | SATM3V |
| P3VCLD | IP3VCL | VALVE | PRESSURE AT WHICH SAFETY/RELIEF VALVE CLOSES | VALV3P |
| P3VOL | IP3VOL | VOLUM | PRESSURE, AVERAGE FOR VOLUME | VOL3P |
| P3VOPN | IP3VOP | VALVE | PRESSURE AT WHICH SAFETY/RELIEF VALVE OPENS | VALV3P |
| P3WRGN | IP3WRG | TURBN | POWER DELIVED TO GENERATOR AT GIVEN TIME | TURB3P |
| P3WTAB | IP3WTA | NBCTB | PRESSURE/FLOW ENTRY FOR BOUNDARY TABLE | TRND3P |
| Q3BAR | - | 2 | NODAL HEAT TRANSFER RATE, INTO NODE | NODE3V |
| Q3CB | IQ3CB | NODE | TOTAL HEAT TRANSFER RATE INTO NODE | NODL3P |
| Q3HBRG | IQ3HBR | SN*SN | ESTIMATED HEAT TRANSFER FROM SUBNET I TO SUBNET J | SNET3P |
| Q3MD | - | - | AMOUNT OF HEAT INTO MODUL PER SEC, OUT TO IN FOR HX | MOD3V |
| Q3MDT | IQ3MDT | NMDTB | HEATING ENTRY FOR MODULE HEATING TABLE | TRND3P |
| Q3PMI | IQ3PMI | HXNOD | HEAT TRANSFER PER METER OF TUBE, INSIDE TUBE | HX3P |
| Q3MOD | IQ3MOD | MOD | HEAT INPUT TO MODULE, HEAT OUT-TO-IN (TUBES) FOR HX | MODC3P |
| Q3PMC | IQ3PMC | HXNOD | HEAT TRANSFER PER METER OF TUBE, OUTSIDE TUBE | HX3P |
| Q3SEG | IQ3SEG | SGMNT | TOTL HT XFRD INTO SEGMENT, STEADY STATE AND UNADJUSTED | SEG3P |
| Q3SNET | IQ3SNE | SN | TOTAL HEAT TRANSFERRED TO SUBNET | SNET3P |
| Q3TOT | - | - | TOTAL HEAT TRANSFER RATE INTO NODE | NODE3V |
| R3BAR | - | 2 | DENSITY AT NODE AVERAGE ENTHALPY | NODE3V |
| R3CB | IR3CB | NODE | NODE AVERAGE DENSITY | NODL3P |
| R3DMND | IR3DMN | PUMP | PUMP DEMAND SPEED, E.G., AFTER TRIP DEMAND SPEED IS 0 | PUMP3P |
| R3F | - | - | SATURATED FLUID DENSITY | SATP3V |
| R3FM | - | 2 | SATURATED FLUID DENSITY | SATM3V |
| R3G | - | - | SATURATED VAPOR DENSITY | SATP3V |
| R3GM | - | 2 | SATURATED VAPOR DENSITY | SATM3V |
| R3PMPT | IR3PMP | NPMTB | PUMP SPEED ENTRY FOR PUMP SPEED TABLE | TRND3P |
| R3PUMP | IR3PUM | PUMP | PUMP SPEED, NORMALIZED TO REFERENCE PUMP | PUMP3P |
| R3PSEZ | IR3PSE | PUMP | RELATIVE SPEED AT WHICH PUMP SEIZES | PUMP3P |
| R3TS | IR3TS | TURBN | TURBINE SPEED IN RPM | TURB3P |
| R3TSDM | IR3TSD | TURBN | TURBINE DEMAND SPEED | TURB3P |
| R3TSEZ | IR3TSE | TURBN | TURBINE SPEED AT SEIZURE=EXP(-S3TSEZ/S3TTAU) | TURB3P |
| R3TSRF | IR3TSR | TURBN | REFERENCE SPEED FOR TURBINE | TURB3P |
| R3TSTB | IR3TST | NTBTB | TURBINE SPEED ENTRY FOR TURBINE SPEED TABLE | TRND3P |
| R3VOL | IR3VOL | VOLUM | VOLUME AVERAGE DENSITY | VOL3P |
| S3DELT | SCALAR | - | CURRENT TIME STEP SIZE | GLOB3V |
| S3DMD | IS3DMD | VALVE | DEMAND POSITION FOR VALVE, EG, 1 FOR HIGH PRESSURE | VALV3P |
| S3END | SCALAR | - | END TIME FOR TRANSIENT | GLOB3V |

| | | | | |
|---------|--------|-------|---|--------|
| S3PSEZ | IS3PSE | PUMP | TIME AFTER TRIP BEFORE PUMP SEIZES | PUMP3P |
| S3PTAU | IS3PTA | PUMP | PUMP COASTDOWN TIME CONSTANT | PUMP3P |
| S3PTIM | IS3PTI | NPMTB | TIME ENTRY FOR PUMP SPEED TABLE | TRND3P |
| S3PTRP | IS3PTR | PUMP | TIME AT WHICH PUMP IS TRIPPED | PUMP3P |
| S3QT | IS3QT | NMDTB | TIME ENTRY FOR MODULE HEATING TABLE | TRND3P |
| S3RTEN | - | - | SURFACE TENSION BETWEEN SATURATION PHASES | SATP3V |
| S3RTNM | - | 2 | SURFACE TENSION BETWEEN SATURATION PHASES | SATM3V |
| S3TAB | IS3TAB | NBCTB | TIME ENTRY FOR BOUNDARY TABLE | TRND3P |
| S3TAUM | SCALAR | - | MINIMUM TIME CONSTANT,USED TO SET NEW TIME STEP | GLOB3V |
| S3TIME | SCALAR | - | SIMULATION TIME,D.O=STEADY STATE | GLOB3V |
| S3TSEZ | IS3TSE | TURBN | SEIZURE TIME AFTER TRIP | TURB3P |
| S3TSTB | IS3TST | NTBTB | TIME ENTRY FOR TURBINE SPEED TABLE | TRND3P |
| S3TSTP | IS3TST | TURBN | TURBINE TRIP TIME | TURB3P |
| S3TTAU | IS3TTA | TURBN | TURBINE COASTDOWN TIME CONSTANT | TURB3P |
| S3VCLD | IS3VCL | VALVE | VALVE CLOSING TIME CONSTANT | VALV3P |
| S3VMIN | IS3VMI | VALVE | MINIMUM VALVE STEM POSITION,MUST BE GT ZERO | VALV3P |
| S3VOPN | IS3VOP | VALVE | VALVE OPENING TIME CONSTANT | VALV3P |
| S3VPOS | IS3VPO | VALVE | RELATIVE VALVE STEM POSITION | VALV3P |
| S3VPSN | IS3VPS | NVLTB | VALVE POSITION ENTRY FOR VALVE POSITION TABLE | TRND3P |
| S3VTIM | IS3VTI | NVLTB | TIME ENTRY FOR VALVE POSITION TABLE | TRND3P |
| T3BAR | - | 2 | TEMPERATURE AT NODE AVERAGE ENTHALPY | NODE3V |
| T3BC | IT3BC | BC | TEMPERATURE OF FLUID PASSING THROUGH BOUNDARY | BC3P |
| T3CB | IT3CB | NODE | NODE AVERAGE TEMPERATURE | NODL3P |
| T3CENT | - | - | HX TUBE CENTER TEMPERATURE | NODE3V |
| T3CORT | IT3COR | HXNOD | TEMPERATURE OF CORE TUBE NODE | HX3P |
| T3IN | - | 2 | TEMPERATURE AT THE NODE INLET | PUMP3P |
| T3ITRF | IT3ITR | TURBN | REFERENCE INLET TEMPERATURE | TURB3P |
| T3JUNC | IT3JUN | NDINF | TEMPERATURE AT THE NODAL INTERFACE | NODL3P |
| T3OUT | - | 2 | TEMPERATURE AT THE NODE OUTLET | PUMP3P |
| T3SAT | - | - | SATURATION TEMPERATURE | SATP3V |
| T3SATM | - | 2 | SATURATION TEMPERATURE | SATM3V |
| T3STRC | IT3STR | HXNOD | TEMPERATURE OF STRUCTURE TUBE NODE | HX3P |
| T3TC | IT3TC | HXNOD | HEAT EXCHANGER TUBE NODE TEMPERATURE | HX3P |
| T3VOL | IT3VOL | VOLUM | VOLUME TEMPERATURE (K) | VOL3P |
| V3ISCF | - | - | DYNAMIC VISCOSITY OF SATURATED FLUID | SATP3V |
| V3ISCV | - | - | DYNAMIC VISCOSITY OF SATURATED VAPOR | SATP3V |
| V3ISFM | - | 2 | DYNAMIC VISCOSITY OF SATURATED FLUID | SATM3V |
| V3ISGM | - | 2 | DYNAMIC VISCOSITY OF SATURATED VAPOR | SATM3V |
| V3LND | - | - | TOTAL VOLUME IN NODE,INCLDS PARALLEL PATHS | NODE3V |
| V3VOL | IV3VOL | VOLUM | TOTAL VOLUME (METERS CUBED) OF MODULE | VOL3P |
| V3OLND | IV3OLN | NODE | VOLUME OF NODE | NODL3P |
| V3RATR | IV3RAT | TURBN | RATIO OF BLADE TO FLUID VELOCITY AT REFERENCE CONDNTS | TURB3P |
| W3BAR | - | 2 | NODE AVERAGE MASS FLOW RATE | NODE3V |
| W3BC | IW3BC | BC | TOTAL FLOW RATE THROUGH BOUNDARY (SUM OVER PATHS) | BC3P |
| W3EINS | IW3EIN | SN | SUM OF FLOW ENERGY (MASS FLW *ENTHLP) INTO SUBNETWRK | SNET3P |
| W3EOTS | IW3EOT | SN | SUM OF FLOW ENERGY (MSS FLW *ENTHLP) OUT OF SBNETWRK | SNET3P |
| W3IN | - | 2 | NODE INLET MASS FLOW RATE | NODE3V |
| W3INSL | IW3INS | SGMNT | FLW RATE AT SEGMENT INLET | SEG3P |
| W3MDI | IW3MDI | MOD | TOTAL MODULE FLOW,FOR HX FLOW ISIDE TUBES | MODC3P |
| W3MDO | IW3MDO | HX NO | MASS FLOW RATE PASSING OUTSIDE HX TUBES | MODC3P |
| W3MOD | - | 2 | FLOW RATE THROUGH MODULE | MOD3V |
| W3OTSL | IW3OTS | SGMNT | FLW RATE AT SEGMENT OUTLET | SEG3P |
| W3OUT | - | 2 | NODE OUTLET MASS FLOW RATE | NODE3V |
| W3PUMP | IW3PUM | PUMP | MASS FLOW RATE THROUGH PUMP,PER UNIT | PUMP3P |
| W3REF | IW3REF | PUMP | PUMP REFERENCE MASS FLOW RATE,PER PARALLEL UNIT | PUMP3P |
| W3SEC | IW3SEC | SGMNT | SGMNT AVE MASS FLOW RATE | SEG3P |
| W3TRF | IW3TRE | TURBN | REFERENCE MASS FLOW RATE | TURB3P |
| W3VALC | IW3VAL | VALVE | CHOKED MASS FLOW RATE THROUGH VALVE | VALV3P |
| W3VOL'T | IW3VOL | VOLUM | ESTIMATED MASS FLOW RATE OUT PORT AT STEADY STATE | VOL3P |
| W3WSSG | IE3WSS | NDINF | FLOW AT NODAL INTERFACE | NODL3P |
| X3BC | IX3BC | BC | QUALITY OF FLOW THROUGH BOUNDARY | BC3P |
| X3INER | IX3INE | SGMNT | TOTL SEG INERTIA,SUM LENGTH/AREA | SEG3P |
| X3MOD | IX3MOD | MODUL | LENGTH OF MODULE | MODL3P |
| X3NODE | - | 2 | LENTH OF NODE | MOD3V |
| Y3CORO | IY3COR | HX | DIAMETER OF HX CORE TUBE,D.O IF NONE | HX3P |
| Y3ID | IY3ID | MODUL | INNER DIAMETER OF PIPE-LIKE PART OF MODULE | MODL3P |
| Y3OD | IY3OD | HX | OUTER DIAMETER OF HX TUBES | MODL3P |
| Y3VOL | IY3VOL | VOLUM | TOTAL HEIGHT OF COMPONENT | VOL3P |
| Z3MOD1 | I23MO1 | MODUL | ELEVATION DIFFERENCE ACROSS MODULE,INSIDE HX TUBES | MODL3P |
| Z3MOD0 | I23MO0 | HX | ELEVATION DIFFERENCE ACROSS HX,OUTSIDE TUBES | MODL3P |
| Z3NODE | - | 2 | ELEVATION DIFFERENCE ACROSS NODE | MOD3V |
| Z3VOL | I23VOL | VOLUM | ELEVATION OF COMPONENT VERTICAL MIDPOINT | VOL3P |

4. MINET APPLICATIONS

There comes a time when an example or two is more useful than further description, and presumably by now that point has been reached. Thus, this final section of our MINET code documentation is intended to show how the code has been used thus far. This should provide the user with some useful ideas and approaches, as well as indicate just how far the code has been applied and tested. The latter could be important for a person planning an application that is beyond our current experience, which is a very real possibility given the highly generalized nature of the MINET code.

Because one can develop infinitely different module configurations it is necessary to distinguish between the various system representations. This is done by designating a MINET Standard Input Deck name, e.g., Deck X2. Thus, after a new input deck has been developed and tested, it is documented and named as a standard input deck, with schematics of the module configurations and module identification numbers included. Approximately 15 such decks currently exist.

In this part of the MINET code documentation, five of these decks will be discussed. The first two, decks X1 and X2 are example decks which do not correspond to any particular system. As such, they can be examined in depth with no concerns as to proprietary information. The third deck, P2, resembles a PWR system and is interesting because it differs significantly from the other applications to date. Testing of this deck has not progressed to a degree where we would consider it appropriate for display, although preliminary findings were very encouraging. The fourth input deck, E1, is for part of the EBR-II system [7], and has been used repeatedly in code validation and check-out. There are features in this application that are unique, but because the

input deck contains material that is of a proprietary nature, it cannot be shown. However, the system schematics of the MINET representation are of interest and are presented. The fifth standard deck discussed, C4, is actually from a combined SSC/MINET analysis of the Clinch River Breeder Reactor (CRBR) plant. The results generated using this deck were compared against those provided by the CRBR project as part of the recently terminated licensing effort. As the specific input deck for C4 is applicable to an older version of MINET, it is not shown.

The input decks shown are representative of others that have been and currently are in use. While not all of the past analysis can be shown in detail, one could properly assume that experience gained from all of the applications are reflected in the current MINET code library.

4.1 MINET DECK X1

MINET standard input deck X1 is a simple example deck that utilizes each of the MINET modules at least once. The system schematic is shown in Figure 4.1-1 with module ID's as shown in Figure 4.1-2. One can easily recognize two networks, two sub-networks, and four flow segments.

The input deck card images are shown in Figure 4.1-3. Note that records 1-901 specify the geometry of the system, with linkages specified in the 901 cards. The 1001 - 1601 cards are used to specify module performance, e.g., the 1601 card indicates how the turbine performs at reference conditions. In the 2000 series cards, initial conditions are specified. Transient boundary conditions enter through the 3000 series cards, although many of these cards are trivial for this deck, e.g., the 3011 cards. Finally, the run control parameters enter through the 4000 series cards.

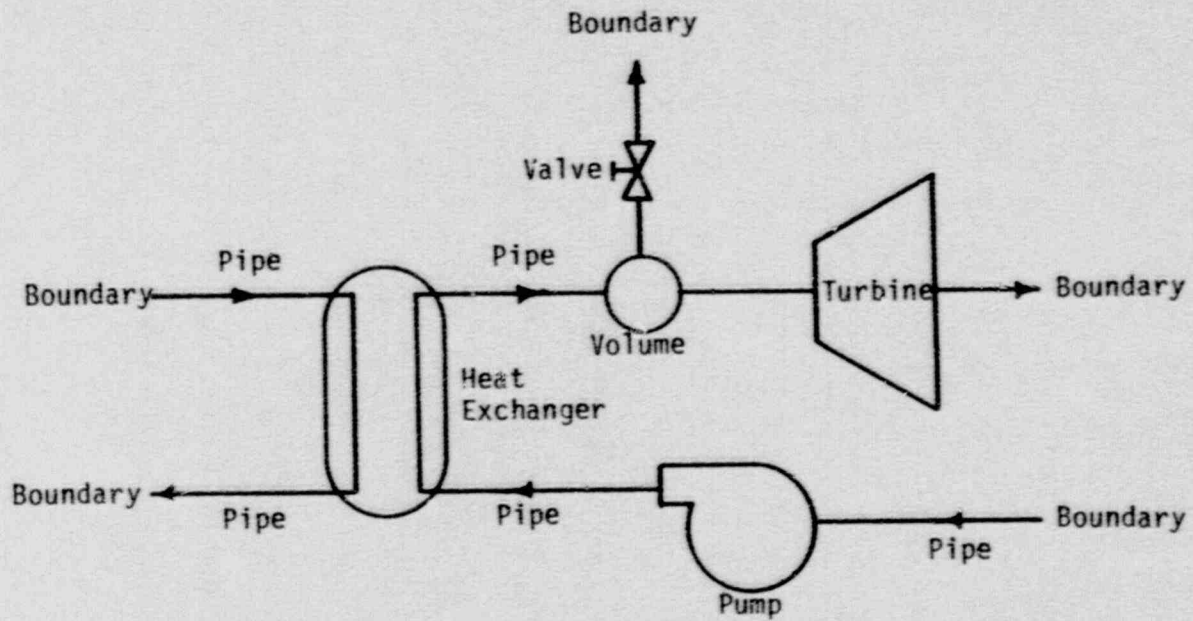


Figure 4.1-1. MINET Standard Deck X1, Example Case

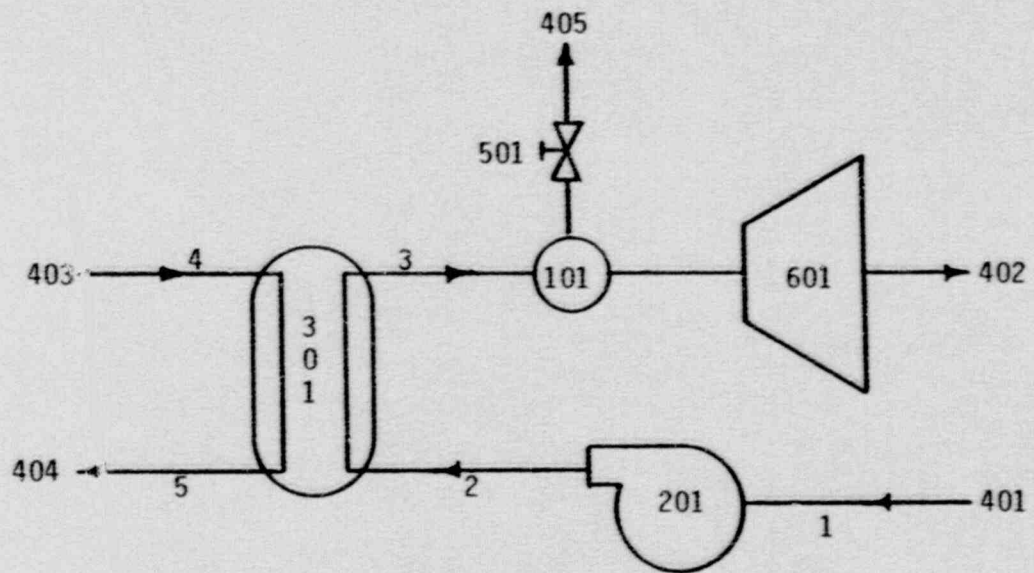


Figure 4.1-2. MINET Standard Deck X1, Module IDs

Figure 4.1-3 X1 Input Deck

STAND-ALONE MINET DECK X1. GJV 10/18/83

OV MINETD

1D 1,1,2,1.0,0.2,1.0E-6,1,2/
 1D 2,1,2,1.0,0.3,1.0E-6,1,1/
 1D 3,1,2,2.0,0.4,1.0E-6,1,1/
 1D 4,1,2,2.0,1.0,1.0E-6,1,1/
 1D 5,1,2,2.0,1.0,1.0E-6,1,1/
 101D 501,1,2,1.5,0.15,1.0E-6,1,1,0.1,1.0E-6,1.0/
 201D 201,1,2,1.0,0.3,1.0E-5,1,1/
 301D 301,1,2,4.0,0.03,1.0E-6,12,1,3,4,0.045,1.5,34000,
 2,6,0.0,1.0,0.0,2,2,0.001,1000.0/
 401D 401,1/
 401D 403,1/
 402D 402,1/
 402D 404,1/
 402D 405,1/
 501D 101,1,0.5,0.2,0.0,1.0,6.0,1,1/
 511D 101,1/
 512D 101,2/
 512D 101,3/
 601D 601,1,2,15.0/
 801D 401,1/
 801D 403,2/
 901D 1.0,401,1,1,1/
 901D 1.0,1,2,201,1/
 901D 2.0,201,2,2,1/
 901D 2.0,2,2,301,1/
 901D 6.0,301,2,3,1/
 901D 6.0,3,2,101,1/
 901D 6.0,101,3,601,1/
 901D 6.0,601,2,402,1/
 901D 6.1,101,2,501,1/
 901D 7.0,501,2,405,1/
 901D 6.0,403,1,4,1/
 901D 6.0,4,2,301,3/
 901D 2.0,301,4,5,1/
 901D 2.0,5,2,404,1/
 1001D 1,0.0/
 1001D 2,0.0/
 1001D 3,0.0/
 1001D 4,0.0/
 1001D 5,0.0/
 1101D 501,0.0,1.0,2,101,12.0E6,4.0,2.0E6,6.0/
 1201D 201,0.0,100.0,30.0,3600.0,1.0,0.0,0.0,0.0,0.0,9.0,35.0/
 1301D 301,0.0,0.0,3,3,-1.0/
 1601D 601,2,0.95,100.0,3.0E6,0.2E6,750.0,3600.0,8.0,20.0/
 2001D 1,0.0/
 2001D 2,0.0/
 2001D 3,0.0/
 2001D 4,0.0/
 2001D 5,0.0/
 2101D 501,0.0,1.0E-5/
 2201D 201,0.0,3500.0/
 2301D 301,2.7E+8/
 2401D 401,0,1,0.3E6,100.0,1.0E6/
 2401D 402,1,1,0.3E6,100.0,0.25E6/
 2401D 403,0,1,1.08E6,1000.0,1.0E6/
 2401D 404,2,1,0.8E6,1000.0,1.0E6/
 2401D 405,1,2,750.0,0.001,0.13E6/
 2501D 101,0.0,1.0,3.8E6/

```
2511D 101,2,0.01/  
2511D 101,3,99.99/  
2601D 601,3640.0,-4.0E7/  
3011D 1,0.0,0.0,999.0,0.0/  
3011D 2,0.0,0.0,999.0,0.0/  
3011D 3,0.0,0.0,999.0,0.0/  
3011D 4,0.0,0.0,999.0,0.0/  
3011D 5,0.0,0.0,999.0,0.0/  
3111D 501,0.0,0.0,999.0,0.0/  
3201D 201,999.0/  
3211D 201,0.0,0.0,999.0,0.0/  
3411D 401,1,1,0.0,0.3E6,100.0,  
      2.0,0.3E6,95.0,  
      4.0,0.3E6,100.0,  
      999.0,0.3E6,100.0/  
3411D 402,2,1,0.0,0.3E6,0.25E6,  
      999.0,0.3E6,0.25E6/  
3411D 403,1,1,0.0,1.08E6,1000.0,  
      999.0,1.08E6,1000.0/  
3411D 404,2,1,0.0,0.8E6,1.0E6,  
      999.0,0.8E6,1.0E6/  
3411D 405,2,2,0.0,750.0,0.13E6,  
      999.0,750.0,0.13E6/  
3511D 101,0.0,0.0,999.0,0.0/  
3601D 601,9999.0/  
3611D 601,0.0,3640.0,999.0,3640.0/  
4000D 1.0 /  
4100D 99999, 3, 0.2, 1.0, 0.5, 5.0 /  
4200D 0, 5 /  
STOP  
END
```

MINET steady state output for deck X1 is shown in Figure 4.1-4. Much of the output is self-explanatory, but some of it needs to be described in further detail, particularly the System Network and Sub-network (S.N. & S-N) part of the print. Using the boundary conditions edit, one can readily identify network 1 as the simple one to the left in Figure 4.1-1, and network 2 is the more complicated one on the right. In the first part of the S.N. & S-N edit, the sub-network numbers are indicated, as are the flow-energies (W·E) in and out. In the second part of the S.N. & S-N edit the adjustment of heat transfer bridges is indicated. Because we specified in the input that the enthalpy at boundary 404 is identically $0.8E6$ J/kg, exactly 280. MW must be removed from sub-network 1 to sub-network 2. The estimate for the heat transfer rate for the heat exchanger was 270. MW, so MINET makes a 3.7% adjustment to the bridge.

In the segment edit, 4 segments are identified and the flows, enthalpies, and pressures at both ends are given, along with pressure loss parameters α and β . The ID's for the modules attaching to the segment inlet and outlet are given, and one can usually make an excellent guess as to which segment is which at this stage.

The next level of output provides detailed information on conditions along each of the flow segments. Any confusion regarding which segments are which can be easily resolved using the module ID's given in this edit. Note that the node and nodal interface numbers are provided, as well.

The level three print provides more detail on the modules, and should remove any doubt as to how the modules fit in the representation. The edit for the heat exchanger is particularly useful, and is written to give enough information so as to enable the user to visualize conditions quite completely.

For this particular example, much of the heat transfer takes place in the bottom node (water inlet), and the water/steam passes through subcooled convection, subcooled nucleate boiling, forced convection vaporization, and into film-boiling in this node. Note that because the heat exchanger was analyzed from the top down, i.e., hot fluid inlet to outlet, some of the numbering looks backward. Using the other module edits, one can determine the current pump speed and head, the valve position and choked flow limit, and the turbine stage speed, efficiency, and power produced (negative work done on turbine by definition).

MINET output at $t = 0.2$ second for deck X1 is shown in Figure 4.1-5. Note first that there is no sub-network edit, as it is relevant only for the steady state conditions. In the segment edit, one can see the impact of compression and expansion in many of the nodes as small steady state mismatches, resulting from errors left over from the iterative solutions, are resolved. The effect is small in segment 1, which contains incompressible but thermally expandable sodium, and larger in the water/steam segment 2. In particular, there is a significant flow divergence in node 18, where a difference of 17 kg/s is evident. If we trace node 18 into the module edit for the heat exchanger, we find that there has been a 10% increase in heating since the steady state, which explains the divergence. The reason for this 10% increase traces to the heat transfer mode at 0.2 seconds, which is now 234. Because the water/steam contents of the unit are now considered inlet to outlet, rather than outlet to inlet (steady state), there is a slight change in the tube temperature distribution which eliminates the subcooled convection mode in favor of subcooled nucleate boiling. In time, the system will go to a slightly altered steady

state. The cause for this difference has been considered at length, and it was decided that the advantages involved with the current approach outweigh the disadvantages, and that the occasional small mismatch that arises is quite acceptable.

Figure 4.1-4 X1 Steady State Output

MINET. TIME# 0.00000 TIME STEP#0.00000 STEP NO. 0

SYSTEM BOUNDARY CONDITIONS:

| ID NETWORK | FLOW(KG/S) | ENTHALPY (MJ/KG) | PRESSURE (MPA) | TEMP(K) | FLUID |
|------------|------------|------------------|----------------|---------|-------|
| 403 | 1000.000 | 1.000000 | .967457 | 824.676 | NA |
| 404 | 1000.000 | .800000 | 1.000000 | 504.632 | NA |
| 401 | 100.000 | .300000 | 2.424984 | 344.261 | H2O |
| 405 | 2.005 | 3.100000 | .130000 | 587.939 | H2O |
| 402 | 99.995 | 2.699977 | .250000 | 400.512 | H2O |

SYSTEM NETWORKS AND SUB-NETWORKS

| NETWORK | SUB-NETWORK | SUM ME. IN(MM) | SUM ME. OUT(MM) |
|---------|-------------|----------------|-----------------|
| 1 | 1 | 1080.000000 | 800.000000 |
| 2 | 2 | 30.000000 | 270.000000 |

SUB-NETWORK BRIDGES

| SUBNET1 | SUBNET2 | G. BRIDGE(MM) | K. BRIDGE | F. BRIDGE |
|---------|---------|---------------|-----------|-----------|
| 1 | 1 | 0.000000 | 0 | 1.000 |
| 1 | 2 | 270.000000 | 1 | 1.037 |
| 2 | 1 | -270.000000 | 1 | 1.037 |
| 2 | 2 | -40.000000 | 0 | 1.000 |

SYSTEM VOLUMES

| SEG NETWORK | MIN(KG/S) | ENTHALPY (MJ/KG) | TEMP(K) | LEVEL (RELATIVE) | HEAT INPUT (MJ/S) | NETWORK | REGIONS |
|-------------|-----------|------------------|---------|------------------|-------------------|---------|---------|
| 101 | 2.685830 | 3.100000 | 513.955 | 1.000000 | 0.000000 | 2 | 1 |

SYSTEM SEGMENTS

| SEG NETWORK | MIN(KG/S) | WOUT (KG/S) | MBART(KG/S) | ENTH(MJ/KG) | EIN(MJ/KG) | EOUT(MJ/KG) | PIN(MPA) | POUT(MPA) | ALPHA_SEG | BETA(MPA) | CONNECTS TO: |
|-------------|-----------|-------------|-------------|-------------|------------|-------------|----------|-----------|-----------|-----------|--------------|
| 1 | 1000.000 | 1000.000 | 1000.000 | 1.080000 | 1.080000 | 1.080000 | 967457 | 1.000000 | 342E-10 | .032567 | 403 404 |
| 2 | 100.000 | 100.000 | 100.000 | .300000 | 3.100000 | 3.100000 | 2.424984 | 2.685830 | 164E-76 | .262485 | 401 101 |
| 3 | 2.005 | .005 | .505 | 3.100000 | 3.100000 | 3.100000 | 2.685820 | 1.500000 | 955E+05 | -.000046 | 101 405 |
| 4 | 99.995 | 99.995 | 99.995 | 3.100000 | 3.100000 | 2.699977 | 2.685830 | .250000 | 244E-03 | 0.000000 | 101 402 |

| IN-SEGMENT DISTRIBUTIONS | SEG MODID | MODE | EIN(MJ/KG) | EBAR(MJ/KG) | EDUT(MJ/KG) | MIN(KG/S) | MDUT(KG/S) | TIN(K) | TBAR(K) | TOUT(K) | DENS(KG/M3) | QA(MJ/S) | JIN | JOUT |
|--------------------------|-----------|------|------------|-------------|-------------|-----------|------------|---------|---------|---------|-------------|----------|-----|------|
| 1 | 1 | 1 | 1.080000 | 1.080000 | 1.080000 | 1000.000 | 1000.000 | 824.676 | 824.676 | 824.676 | 819.835 | 0.000 | 1 | 2 |
| 1 | 301 | 2 | 1.076513 | 1.076513 | 1.073026 | 1000.000 | 1000.000 | 824.676 | 821.974 | 819.132 | 820.503 | -6.974 | 2 | 3 |
| 1 | 301 | 3 | 1.065361 | 1.065361 | 1.056993 | 1000.000 | 1000.000 | 813.040 | 815.086 | 813.040 | 821.903 | -7.865 | 3 | 4 |
| 1 | 301 | 4 | 1.052742 | 1.052742 | 1.048490 | 1000.000 | 1000.000 | 803.017 | 803.017 | 806.393 | 823.435 | -8.368 | 4 | 5 |
| 1 | 301 | 5 | 1.045092 | 1.045092 | 1.041693 | 1000.000 | 1000.000 | 799.641 | 803.593 | 799.641 | 825.047 | -8.503 | 5 | 6 |
| 1 | 301 | 6 | 1.035173 | 1.035173 | 1.031173 | 1000.000 | 1000.000 | 791.650 | 796.943 | 794.246 | 826.507 | -6.797 | 6 | 7 |
| 1 | 301 | 7 | 1.028888 | 1.028888 | 1.025855 | 1000.000 | 1000.000 | 784.089 | 784.089 | 789.074 | 827.777 | -6.520 | 7 | 8 |
| 1 | 301 | 8 | 1.022855 | 1.022855 | 1.020655 | 1000.000 | 1000.000 | 779.307 | 784.089 | 779.307 | 828.997 | -6.285 | 8 | 9 |
| 1 | 301 | 9 | 1.019359 | 1.019359 | 1.017063 | 1000.000 | 1000.000 | 774.717 | 779.307 | 774.717 | 830.171 | -6.033 | 9 | 10 |
| 1 | 301 | 10 | 1.014282 | 1.014282 | 1.011501 | 1000.000 | 1000.000 | 772.514 | 774.717 | 770.312 | 832.376 | -5.562 | 11 | 12 |
| 1 | 301 | 11 | 1.008835 | 1.008835 | 1.005170 | 1000.000 | 1000.000 | 766.092 | 766.092 | 766.092 | 833.412 | -5.330 | 12 | 13 |
| 1 | 301 | 12 | 1.006170 | 1.006170 | 1.003256 | 1000.000 | 1000.000 | 604.632 | 604.632 | 604.632 | 853.335 | -205.829 | 13 | 14 |
| 1 | 301 | 13 | 1.000000 | 1.000000 | 1.000000 | 1000.000 | 1000.000 | 344.246 | 344.246 | 344.246 | 872.474 | 0.000 | 14 | 15 |
| 1 | 301 | 14 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 15 | 17 |
| 1 | 301 | 15 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 16 | 18 |
| 1 | 301 | 16 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 17 | 18 |
| 1 | 301 | 17 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 18 | 19 |
| 1 | 301 | 18 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 19 | 20 |
| 1 | 301 | 19 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 20 | 21 |
| 1 | 301 | 20 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 21 | 22 |
| 1 | 301 | 21 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 22 | 23 |
| 1 | 301 | 22 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 23 | 24 |
| 1 | 301 | 23 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 24 | 25 |
| 1 | 301 | 24 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 25 | 26 |
| 1 | 301 | 25 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 26 | 27 |
| 1 | 301 | 26 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 27 | 28 |
| 1 | 301 | 27 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 28 | 29 |
| 1 | 301 | 28 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 29 | 30 |
| 1 | 301 | 29 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 30 | 31 |
| 1 | 301 | 30 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 31 | 32 |
| 1 | 301 | 31 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 32 | 33 |
| 1 | 301 | 32 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 33 | 34 |
| 1 | 301 | 33 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 34 | 35 |
| 1 | 301 | 34 | 1.000000 | 1.000000 | 1.000000 | 100.000 | 100.000 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 35 | 36 |

STAND-ALONE MINET DECK XI. GUV 10/18/83

| SYSTEM MODULES | 1. MODID | 403. NPATH= | 0 | TOUTR(K) | DOOUTR(KJ/S/M) | MODE.1 | MODE.0 | T.CORE | T.STRC |
|---|----------|-------------------|---|-----------|----------------|--------|--------|--------|--------|
| MODULE 1 IS B.C. NUMBER | 1. | MODID 403. NPATH= | 0 | 685.01788 | -20.26723 | 4321 | 1 | 498.1 | 685.0 |
| MODULE 2 IS PIPE NUMBER | 2. | MODID 404. NPATH= | 1 | 768.20158 | -52134 | 4 | 1 | 498.1 | 768.2 |
| MODULE 3 IS H.X. NUMBER | 3. | MODID 301. NPATH= | 1 | 772.51431 | -54220 | 4 | 1 | 498.1 | 772.5 |
| THE HEAT FLUX AREA CORRECTION FACTOR IS .882565 | | | | 777.01197 | -56419 | 4 | 1 | 498.1 | 777.0 |
| T NOO 1 NOO 0 NOO 0 INR(KJ/S/M) T INR(K) T TUBE(K) | | | | 781.69800 | -58736 | 4 | 1 | 498.1 | 781.7 |
| | | | | 786.58126 | -61178 | 4 | 1 | 498.1 | 786.6 |
| | | | | 791.65965 | -63747 | 4 | 1 | 498.1 | 791.7 |
| | | | | 796.94348 | -66453 | 4 | 1 | 498.1 | 796.9 |
| | | | | 801.74304 | -67649 | 54 | 1 | 506.6 | 803.0 |
| | | | | 808.51688 | -82221 | 5 | 1 | 536.7 | 809.7 |
| | | | | 814.97666 | -75760 | 5 | 1 | 567.8 | 816.1 |
| | | | | 820.88970 | -69047 | 5 | 1 | 598.0 | 821.9 |
| MODULE 4 IS PIPE NUMBER | 2. | MODID 5. NPATH= | 1 | | | | | | |
| MODULE 5 IS B.C. NUMBER | 2. | MODID 404. NPATH= | 0 | | | | | | |
| MODULE 6 IS B.C. NUMBER | 3. | MODID 401. NPATH= | 0 | | | | | | |
| MODULE 7 IS PIPE NUMBER | 3. | MODID 1. NPATH= | 2 | | | | | | |
| MODULE 8 IS PIPE NUMBER | 1. | MODID 201. NPATH= | 1 | | | | | | |
| PUMP SPEED= 3500.000 PUMP FLOW= 100.000 KG/S | | | | | | | | | |
| MODULE 9 IS PIPE NUMBER | 4. | MODID 2. NPATH= | 1 | | | | | | |
| MODULE 10 IS PIPE NUMBER | 5. | MODID 3. NPATH= | 1 | | | | | | |
| MODULE 11 IS VOL. NUMBER | 1. | MODID 101. NPATH= | 1 | | | | | | |
| MODULE 12 IS VALV NUMBER | 1. | MODID 501. NPATH= | 1 | | | | | | |
| RELATIVE VALVE POSITION IS .000100 AND CHOKE FLOW IS | | | | | | | | | |
| MODULE 13 IS B.C. NUMBER | 4. | MODID 405. NPATH= | 0 | | | | | | |
| MODULE 14 IS TRSG NUMBER | 1. | MODID 501. NPATH= | 1 | | | | | | |
| SPEED IN RPM IS 3640.00. EFFICIENCY IS .93018. POWER FROM GEN | | | | | | | | | |
| MODULE 15 IS B.C. NUMBER | 5. | MODID 402. NPATH= | 0 | | | | | | |
| END SS TIME=23.06 | | | | | | | | | |
| MINET: END=1. PRINT=.2 STORE=.2 SAVE=1. | | | | | | | | | |

PUMP HEAD= 28.356 METERS

586E-02, AS DETERMINED USING OPTION 2

POWER FROM GEN --.380E+08

Figure 4.1-5 X1 t = 0.2s Output

STAND-ALONE MINET DECK XI. GJV 10/18/83

MINET. TIME= .20000 TIME STEP= .10000 STEP NO. 2

SYSTEM BOUNDARY CONDITIONS:

| ID | NETWORK | FLOW(KG/S) | ENTHALPY(MJ/KG) | PRESSURE(MPA) | TEMP(K) | FLUID |
|-----|---------|------------|-----------------|---------------|---------|-------|
| 403 | 1 | 1000.000 | 1.080000 | .957463 | 824.676 | NA |
| 404 | 1 | 1000.589 | .800000 | 1.000000 | 604.694 | NA |
| 401 | 2 | 99.500 | 300000 | 2.422935 | 344.262 | H2O |
| 405 | 2 | .006 | 3.099812 | .130000 | 587.848 | H2O |
| 402 | 2 | 99.927 | 2.699712 | .250000 | 400.512 | H2O |

SYSTEM VOLUMES

| ID | PRESSURE(MPA) | ENTHALPY(MJ/KG) | TEMP(K) | LEVEL(RELATIVE) | HEAT INPUT(MJ/S) | NETWORK | REGIONS |
|-----|---------------|-----------------|---------|-----------------|------------------|---------|---------|
| 101 | 2.683863 | 3.099679 | 613.800 | 1.000000 | 0.000000 | 2 | 1 |

SYSTEM SEGMENTS

| SEG | NETWK | MINI(KG/S) | WOUT(KG/S) | WBAR(KG/S) | 1000.291 | 1.080000 | 967463 | 800002 | 967463 | 1.000000 | 1.000000 | POUT(MPA) | ALPHA_SEG | BETA(MPA) | CONNECTS TO: | |
|-----|-------|------------|------------|------------|----------|----------|----------|----------|----------|----------|----------|-----------|-----------|-----------|--------------|-----|
| | | | | | | | | | | | | | | | IN | OUT |
| 1 | 1 | 1000.000 | 1000.589 | 1000.291 | 1.080000 | 967463 | 800002 | 967463 | 1.000000 | 1.000000 | 1.000000 | 342E-10 | .032567 | 403 | 404 | |
| 2 | 2 | 99.500 | 99.920 | 99.635 | 300000 | 3.099777 | 2.422935 | 2.683063 | 2.683063 | 167E-06 | 167E-06 | .262475 | 401 | 101 | | |
| 3 | 2 | .006 | .006 | .006 | 3.099798 | 3.099812 | 2.683954 | .130000 | .130000 | .744E+05 | .744E+05 | .000046 | 101 | 405 | | |
| 4 | 2 | 99.927 | 99.927 | 99.927 | 3.099798 | 2.599712 | 2.683863 | .250000 | .250000 | .244E-03 | .244E-03 | 0.000000 | 101 | 402 | | |

| IN-SEGMENT DISTRIBUTIONS SEG MODID MODE E (IN/100/KG) | EBAR (MU/KG) | EOUT (MU/100/G) | MINI (KG/S) | WOUT (KG/S) | TIN (K) | TBAR (K) | TOUT (K) | DENS (KG/M3) | QA (M/J/S) | JIN | JOUT |
|--|--------------|-----------------|-------------|-------------|---------|----------|----------|--------------|------------|-----|------|
| 1 4 | 1.080000 | 1.080000 | 1000.000 | 1000.000 | 824.676 | 824.676 | 824.676 | 819.835 | 0.000 | 1 | 2 |
| 1 301 | 1.075113 | 1.073026 | 1000.000 | 1000.002 | 824.676 | 821.904 | 819.132 | 820.503 | -6.962 | 2 | 3 |
| 1 301 | 1.069194 | 1.065361 | 1000.002 | 1000.002 | 813.040 | 815.096 | 813.040 | 821.903 | -7.641 | 3 | 4 |
| 1 301 | 1.056994 | 1.051177 | 1000.022 | 1000.022 | 806.393 | 809.717 | 806.393 | 823.435 | -8.296 | 4 | 5 |
| 1 301 | 1.048487 | 1.042741 | 999.948 | 999.948 | 805.393 | 803.016 | 799.639 | 825.047 | -8.831 | 5 | 6 |
| 1 301 | 1.041694 | 1.035091 | 999.948 | 999.967 | 799.639 | 796.943 | 794.247 | 826.507 | -6.701 | 6 | 7 |
| 1 301 | 1.034174 | 1.028174 | 999.967 | 999.985 | 794.247 | 791.660 | 789.074 | 827.777 | -6.440 | 7 | 8 |
| 1 301 | 1.028174 | 1.022889 | 999.985 | 1000.008 | 789.074 | 786.582 | 784.090 | 829.997 | -5.182 | 8 | 9 |
| 1 301 | 1.022889 | 1.017653 | 1000.008 | 1000.029 | 784.090 | 781.699 | 779.308 | 830.171 | -5.938 | 9 | 10 |
| 1 301 | 1.017653 | 1.012428 | 1000.029 | 1000.066 | 779.308 | 777.013 | 774.718 | 831.296 | -5.705 | 10 | 11 |
| 1 301 | 1.012428 | 1.007203 | 1000.066 | 1000.078 | 774.718 | 772.515 | 770.312 | 832.376 | -5.484 | 11 | 12 |
| 1 301 | 1.007203 | 1.001978 | 1000.078 | 1000.066 | 770.312 | 768.202 | 766.092 | 833.412 | -5.273 | 12 | 13 |
| 1 301 | 1.001978 | 0.996753 | 1000.066 | 1000.078 | 766.092 | 764.893 | 762.783 | 833.366 | -203.927 | 13 | 14 |
| 1 301 | 0.996753 | 0.991528 | 1000.078 | 1000.066 | 762.783 | 760.584 | 758.474 | 833.366 | -203.927 | 14 | 15 |
| 1 5 | 800002 | 800002 | 1000.585 | 1000.585 | 604.709 | 604.701 | 604.694 | 872.472 | 0.000 | 16 | 17 |
| 2 1 | 299999 | 299998 | 99.500 | 99.500 | 344.246 | 344.247 | 344.246 | 980.169 | 0.000 | 17 | 18 |
| 2 201 | 299998 | 299998 | 99.500 | 99.500 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 18 | 19 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 19 | 20 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 20 | 21 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 21 | 22 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 22 | 23 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 23 | 24 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 24 | 25 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 25 | 26 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 26 | 27 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 27 | 28 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 28 | 29 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 29 | 30 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 30 | 31 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 31 | 32 |
| 2 301 | 299998 | 299998 | 99.501 | 99.501 | 344.246 | 344.246 | 344.246 | 980.169 | 0.000 | 32 | 33 |
| 3 501 | 3.099798 | 3.099798 | 99.927 | 99.927 | 514.756 | 514.756 | 514.756 | 6.588 | -39.979 | 33 | 34 |
| 4 601 | 3.099798 | 3.099798 | 99.927 | 99.927 | 514.756 | 514.756 | 514.756 | 6.588 | -39.979 | 34 | 35 |

STAND-ALONE MINET DECK XI. GJV 10/18/83

| SYSTEM MODULES | 1. MODID | 403.NPATH | 0 | TOUTR(K) | QOUTR(KJ/S/M) | MODE.1 | MODE.0 | T.CORE | 1.STRC |
|--|----------|-----------|----------|-----------|---------------|--------|--------|--------|--------|
| MODULE 1 IS B.C. NUMBER | 18 | 13 | 22.85401 | 498.03000 | 657.51994 | 234 | 498.1 | 685.0 | |
| MODULE 2 IS PIPE NUMBER | 19 | 12 | .60197 | 498.03000 | 767.45522 | 4 | 498.1 | 768.2 | |
| MODULE 3 IS H.X. NUMBER | 20 | 11 | .62366 | 498.03000 | 771.73639 | 4 | 498.1 | 772.5 | |
| THE HEAT FLUX AREA CORRECTION FACTOR IS .889555 | 21 | 10 | .63952 | 498.03000 | 776.20087 | 4 | 498.1 | 777.0 | |
| T MOD 1 MOD 0 MOD QINR(KJ/S/M) T TNR(K) T TUBE(K) | 22 | 9 | .65540 | 498.03000 | 780.85182 | 4 | 498.1 | 781.7 | |
| | 23 | 8 | .67231 | 498.03000 | 785.69791 | 4 | 498.1 | 786.6 | |
| | 24 | 7 | .69118 | 498.03000 | 790.73714 | 4 | 498.1 | 791.7 | |
| | 25 | 6 | .71241 | 498.03000 | 795.97903 | 4 | 498.1 | 796.9 | |
| | 26 | 5 | .77750 | 506.43659 | 801.74295 | 45 | 506.5 | 803.0 | |
| | 27 | 4 | .85263 | 536.52325 | 808.51553 | 5 | 536.6 | 809.7 | |
| | 28 | 3 | .77212 | 567.71007 | 814.97601 | 5 | 567.8 | 816.1 | |
| | 29 | 2 | .69492 | 597.84636 | 820.88950 | 5 | 597.9 | 821.9 | |
| MODULE 4 IS PIPE NUMBER | 30 | 1 | | | | | | | |
| MODULE 5 IS B.C. NUMBER | 31 | 0 | | | | | | | |
| MODULE 6 IS B.C. NUMBER | 32 | 0 | | | | | | | |
| MODULE 7 IS PIPE NUMBER | 33 | 2 | | | | | | | |
| MODULE 8 IS PUMP NUMBER | 34 | 1 | | | | | | | |
| PUMP SPEED= 3500.000 PUMP FLOW= 99.750 KG/S PUMP HEAD= 28.356 METERS | 35 | 0 | | | | | | | |
| MODULE 9 IS PIPE NUMBER | 36 | 1 | | | | | | | |
| MODULE 10 IS PIPE NUMBER | 37 | 1 | | | | | | | |
| MODULE 11 IS VOL. NUMBER | 38 | 1 | | | | | | | |
| MODULE 12 IS VALV NUMBER | 39 | 1 | | | | | | | |
| RELATIVE VALVE POSITION IS .0000100.AND CHOKE FLOW IS | 40 | 0 | | | | | | | |
| MODULE 13 IS B.C. NUMBER | 41 | 0 | | | | | | | |
| MODULE 14 IS TRSG NUMBER | 42 | 1 | | | | | | | |
| SPEED IN RPM IS 3640.00. EFFICIENCY IS .93023. POWER FROM GEN | 43 | 0 | | | | | | | |
| MODULE 15 IS B.C. NUMBER | 44 | 0 | | | | | | | |

596E-02, AS DETERMINED USING OPTION 2

POWER FROM GEN - .380E+08

MINET: END-1. PRINT= 4 STORE= 4 SAVE=1.

4.2 MINET DECK X2

MINET Standard Input Deck X2 is a simple balance of plant deck, with modules linked as they would be for simulating a typical balance of plant. The schematic drawings for this deck are shown in Figures 4.2-1 and 4.2-2.

The input deck itself is shown in Figure 4.2-3. It should be noted that this deck was fitted together using crude estimates for component sizings, as well as system conditions and performance. Thus, one should not judge this deck for its accuracy or physical correctness. However, as explained earlier, it is actually easier to develop a representation of a physical system because it is more likely that a user can inadvertently create a non-physical situation.

The output from Deck X2, at steady state, is shown in Figure 4.2-4. Most of the energy/work is done in the turbine, and this helps identify sub-network 1. Sub-network 2 is actually the line running from the condenser, through the feedwater train, to boundary 402. The remaining portion of the system is sub-network 1. Note that MINET chose to adjust the turbine work to meet the energy constraint imposed at the condenser, which is the correct choice, because of the magnitude of the source.

As one reviews the segment edit, it becomes easier to visualize the system. For instance, the bleed lines running from the turbines, through the feedwater heaters, and on to the condenser are in the last few segments considered.

In the module edit, one may observe the type of adjustment MINET can make to the heat exchanger area correction factor. In this case, we input a very small heat transfer rate across the feedwater heaters (cards 2301), and MINET chose not to factor it (factoring the turbines instead). Thus, there was a

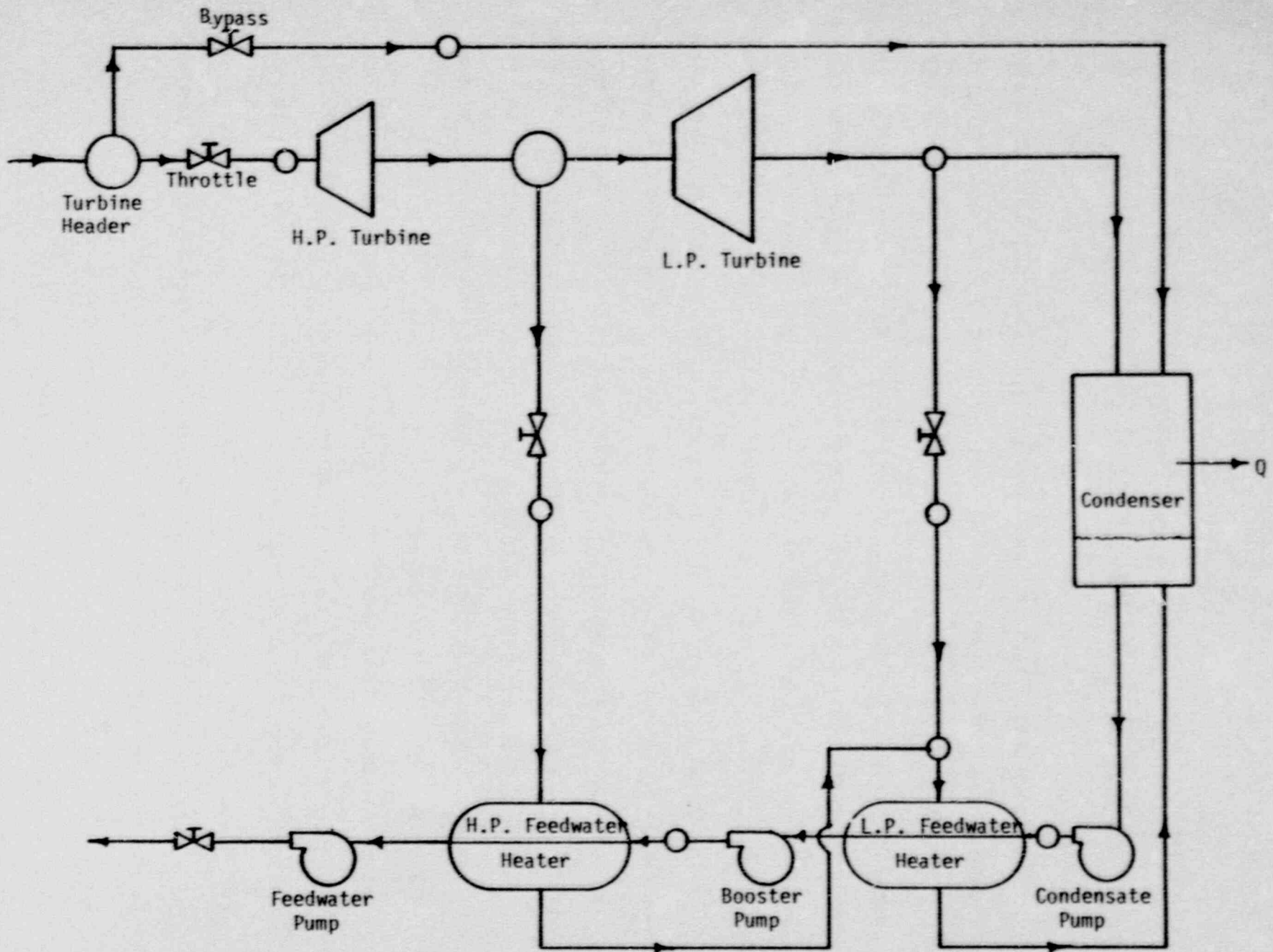


Figure 4.2-1. MINET Example Deck X2, Simple Balance of Plant

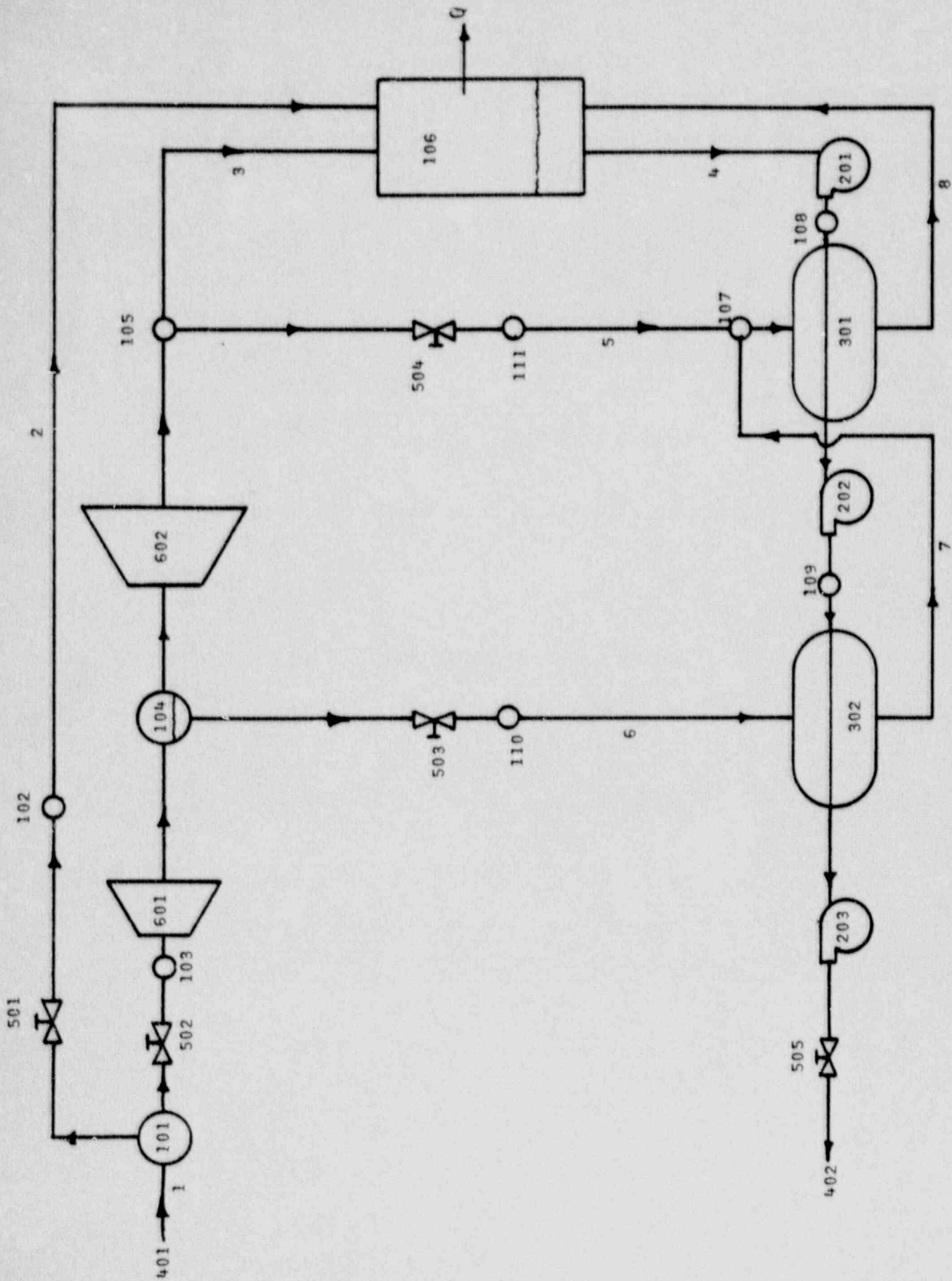


Figure 4.2-2. MINET Deck X2 Module IDs

Figure 4.2-3 X2 Input Deck

MINET DECK X2,EXAMPLE BOP DECK,GJV 11/24/83

0V MINETD

1D 1,1,2,1.0,1.0,1.0E-6,1,1/
 1D 2,1,2,20.0,0.2,1.0E-6,3,1/
 1D 3,1,2,7.0,1.2,1.0E-6,1,1/
 1D 4,1,2,4.0,0.8,1.0E-6,1,1/
 1D 5,1,2,8.0,0.3,1.0E-6,1,1/
 1D 6,1,2,8.0,0.3,1.0E-6,1,1/
 1D 7,1,2,14.0,0.2,1.0E-6,2,1/
 1D 8,1,2,16.0,0.6,1.0E-6,3,1/
 101D 501,1,2,5.0,0.3,1.0E-6,1,1,0.057,1.E-6,1.0/
 101D 502,1,2,2.0,1.0,1.0E-6,1,1,0.636,1.E-6,1.0/
 101D 503,1,2,6.0,0.3,1.0E-6,1,1,0.057,1.E-6,1.0/
 101D 504,1,2,6.0,0.3,1.0E-6,1,1,0.057,1.E-6,1.0/
 101D 505,1,2,4.0,0.8,1.0E-6,1,1,0.407,1.E-6,1.0/
 201D 201,1,2,1.0,0.8,1.0E-6,1,3/
 201D 202,1,2,1.0,0.8,1.0E-6,1,3/
 201D 203,1,2,4.0,0.8,1.0E-6,1,3/
 301D 301,1,2,20.0,0.03,1.E-6,3,3,3,4,0.04,1.5,625,2,
 4,0.0,1.0,0.0,2,2,1.0,5000.0/
 301D 302,1,2,20.0,0.03,1.E-6,3,3,3,4,0.04,1.5,625,2,
 4,0.0,1.0,0.0,2,2,1.0,5000.0/
 401D 401,1/
 402D 402,1/
 501D 101,2,2.0,1.0,0.0,1.0,10.0,1,1/
 501D 102,2,1.0,0.5,0.0,1.0,10.0,1,1/
 501D 103,2,1.0,0.5,0.0,1.0,10.0,1,1/
 501D 104,2,2.0,1.0,0.0,1.0,10.0,1,1/
 501D 105,2,1.0,0.5,0.0,1.0,10.0,1,1/
 501D 106,1,20.0,4.0,0.0,1.0,6.0,1,2/
 501D 107,1,1.0,0.2,0.0,1.0,3.5,3,1/
 501D 108,2,1.0,0.5,0.0,1.0,2.0,3,1/
 501D 109,2,1.0,0.5,0.0,1.0,2.0,3,1/
 501D 110,1,1.0,0.2,0.0,1.0,6.0,3,1/
 501D 111,1,1.0,0.2,0.0,1.0,6.0,3,1/
 511D 101,1/
 512D 101,2/
 512D 101,3/
 511D 102,1/
 512D 102,2/
 511D 103,1/
 512D 103,2/
 511D 104,1/
 512D 104,2/
 512D 104,3/
 511D 105,1/
 512D 105,2/
 512D 105,3/
 511D 106,1/
 511D 106,2/
 512D 106,3/
 511D 106,4/
 511D 107,1/
 511D 107,2/
 512D 107,3/
 511D 108,1/
 512D 108,2/
 511D 109,1/
 512D 109,2/
 511D 110,1/

512D 110,2/
511D 111,1/
512D 111,2/
601D 601,1,2,15,0/
601D 602,1,2,15,0/
801D 401,1/
901D 10,0,401,1,1,1/
901D 10,0,1,2,101,1/
901D 10,0,101,2,501,1/
901D 10,0,501,2,102,1/
901D 10,0,102,2,2,1/
901D 10,0,2,2,106,2/
901D 10,0,101,3,502,1/
901D 10,0,502,2,103,1/
901D 10,0,103,2,601,1/
901D 10,0,601,2,104,1/
901D 10,4,104,2,602,1/
901D 10,0,602,2,105,1/
901D 10,0,105,2,3,1/
901D 8,0,3,2,106,1/
901D 4,0,106,3,4,1/
901D 2,0,4,2,201,1/
901D 2,0,201,2,108,1/
901D 2,0,108,2,301,1/
901D 2,0,301,2,202,1/
901D 2,0,202,2,109,1/
901D 2,0,109,2,302,1/
901D 2,0,302,2,203,1/
901D 2,0,203,2,505,1/
901D 2,0,505,2,402,1/
901D 9,51,104,3,503,1/
901D 6,1,503,2,110,1/
901D 5,9,110,2,6,1/
901D 3,0,6,2,302,3/
901D 1,0,302,4,7,1/
901D 3,5,7,2,107,2/
901D 10,0,105,3,504,1/
901D 6,1,504,2,111,1/
901D 5,9,111,2,5,1/
901D 3,6,5,2,107,1/
901D 3,4,107,3,301,3/
901D 1,0,301,4,8,1/
901D 4,0,8,2,106,4/
1001D 1,0,0/
1001D 2,1,E5/
1001D 3,0,1/
1001D 4,0,5/
1001D 5,0,0/
1001D 6,0,0/
1001D 7,0,0/
1001D 8,0,0/
1101D 501,0,0,10,0,1,101,15,0E6,5,0,14,0E6,6,0/
1101D 502,0,0,1,0,0,-999,0,0,0,0,0,0,0,0/
1101D 503,0,0,21,0,0,-999,0,0,0,0,0,0,0,0/
1101D 504,0,0,4,0,0,-999,0,0,0,0,0,0,0,0/
1101D 505,10,0,1,0,0,-999,0,0,0,0,0,0,0,0/
1201D 201,0,5,333,3,230,0,3600,0,1,0,0,0,0,0,0,0,0,10,0,60,0/
1201D 202,0,5,333,3,460,0,3600,0,1,0,0,0,0,0,0,0,0,10,0,60,0/
1201D 203,0,5,333,3,695,0,3600,0,1,0,0,0,0,0,0,0,0,10,0,60,0/
1301D 301,0,5,0,0,3,3,0,0/

1301D 302,0.5,0.0,3,3,0.0/
1601D 601,1,0.95,1000.0,10.0E6,5.0E6,795.0,3600.0,5.0,30.0/
1601D 602,2,0.95,950.0,5.0E6,8.0E5,545.0,3600.0,5.0,30.0/
2001D 1,0.0/
2001D 2,0.0/
2001D 3,0.0/
2001D 4,-1.E7/
2001D 5,0.0/
2001D 6,0.0/
2001D 7,0.0/
2001D 8,0.0/
2101D 501,0.0,1.E-5/
2101D 502,0.0,0.95/
2101D 503,0.0,0.2/
2101D 504,0.0,0.3/
2101D 505,0.0,0.95/
2201D 201,0.0,3600.0/
2201D 202,0.0,3600.0/
2201D 203,0.0,3600.0/
2301D 301,5.E6/
2301D 302,5.E6/
2401D 401,0.1,3.E6,1000.0,8.96E6/
2401D 402,1,1,1.E6,1000.0,13.E6/
2501D 101,0.0,0.5,8.958E6/
2501D 102,0.0,0.5,0.767E6/
2501D 103,0.0,0.5,8.92E6/
2501D 104,0.0,0.3,5.06E6/
2501D 105,0.0,0.5,1.80E6/
2501D 106,-2.1E9,0.3,0.772E6/
2501D 107,0.0,0.5,0.918E6/
2501D 108,0.0,0.5,2.82E6/
2501D 109,0.0,0.5,6.89E6/
2501D 110,0.0,0.5,2.68E6/
2501D 111,0.0,0.5,1.25E6/
2511D 101,2,0.003/
2511D 101,3,1000.0/
2511D 102,2,0.003/
2511D 103,2,1000.0/
2511D 104,2,975.3/
2511D 104,3,24.9/
2511D 105,2,949.3/
2511D 105,3,25.5/
2511D 106,3,1000.0/
2511D 107,3,50.4/
2511D 108,2,1000.0/
2511D 109,2,1000.0/
2511D 110,2,24.9/
2511D 111,2,25.5/
2601D 601,3600.0,-0.5E9/
2601D 602,3600.0,-0.44E9/
3011D 1,0.0,0.0,999.0,0.0/
3011D 2,0.0,0.0,999.0,0.0/
3011D 3,0.0,0.0,999.0,0.0/
3011D 4,0.0,-1.E7,999.0,-1.E7/
3011D 5,0.0,0.0,999.0,0.0/
3011D 6,0.0,0.0,999.0,0.0/
3011D 7,0.0,0.0,999.0,0.0/
3011D 8,0.0,0.0,999.0,0.0/
3111D 501,0.0,0.0,999.0,0.0/
3111D 502,0.0,0.0,999.0,0.0/

```
3111D 503,0.0,0.0,0.999,0.0,0.0/
3111D 504,0.0,0.0,0.999,0.0,0.0/
3111D 505,0.0,0.0,0.999,0.0,0.0/
3121D 501,0.0,1.0E-5,999.0,1.0E-5/
3121D 502,0.0,0.95,999.0,0.95/
3121D 503,0.0,0.2,999.0,0.2/
3121D 504,0.0,0.3,999.0,0.3/
3121D 505,0.0,0.95,999.0,0.95/
3201D 201,999.0/
3201D 202,999.0/
3201D 203,999.0/
3211D 201,0.0,0.0,0.999,0.0,0.0/
3211D 202,0.0,0.0,0.999,0.0,0.0/
3211D 203,0.0,0.0,0.999,0.0,0.0/
3411D 401,1.1,0.0,3.0E6,1000.0,
      999.0,3.0E6,1000.0/
3411D 402,2.1,0.0,1.0E6,13.E6,
      999.0,1.0E6,13.E6/
3511D 101,0.0,0.0,0.999,0.0,0.0/
3511D 102,0.0,0.0,0.999,0.0,0.0/
3511D 103,0.0,0.0,0.999,0.0,0.0/
3511D 104,0.0,0.0,0.999,0.0,0.0/
3511D 105,0.0,0.0,0.999,0.0,0.0/
3511D 106,0.0,-2.1E9,999.0,-2.1E9/
3511D 107,0.0,0.0,0.999,0.0,0.0/
3511D 108,0.0,0.0,0.999,0.0,0.0/
3511D 109,0.0,0.0,0.999,0.0,0.0/
3511D 110,0.0,0.0,0.999,0.0,0.0/
3511D 111,0.0,0.0,0.999,0.0,0.0/
3601D 601,999.0/
3601D 602,999.0/
4000D 100.0/
4100D 99999,3,100.0,1000.0/
4200D 0,999/
STOP
END
```

Figure 4.2-4 X2 Steady State Output

MINET. TIME= 0.00000 TIME STEP=0.00000 STEP NO. 0

SYSTEM BOUNDARY CONDITIONS:

| NETWORK ID | NETWORK FLOW(KG/S) | ENTHALPY(MJ/KG) | PRESSURE(MPA) | TEMP(K) | FLUID |
|------------|--------------------|-----------------|---------------|---------|-------|
| 401 | 1 | 1000.000 | 8.950371 | 631.118 | H2O |
| 402 | 1 | 1000.000 | 13.000000 | 441.991 | H2O |

SYSTEM NETWORKS AND SUB-NETWORKS

| NETWORK | SUB-NETWORK | SUM WE, IN(MM) | SUM WE, OUT(MM) |
|---------|-------------|----------------|-----------------|
| 1 | 1 | 3000.000000 | 722.318900 |
| 1 | 2 | 722.318900 | 722.318900 |

SUB-NETWORK BRIDGES

| SUBNET1 | SUBNET2 | 0. BRIDGE(MM) | K. BRIDGE | F. BRIDGE |
|---------|---------|---------------|-----------|-----------|
| 1 | 1 | -3040.000000 | 1 | .746 |
| 1 | 2 | 10.000000 | 0 | 1.000 |
| 2 | 1 | -10.000000 | 0 | 1.000 |
| 2 | 2 | -10.000000 | 0 | 1.000 |

SYSTEM VOLUMES

| ID | PRESSURE(MPA) | ENTHALPY(MJ/KG) | TEMP(K) | LEVEL(RELATIVE) | HEAT INPUT(MJ/S) | NETWORK | REGIONS |
|-----|---------------|-----------------|---------|-----------------|------------------|---------|---------|
| 101 | 8.950209 | 3.000000 | 631.116 | -500000 | 0.000000 | 1 | 1 |
| 102 | 8.006687 | 3.000000 | 548.915 | 500000 | 0.000000 | 1 | 1 |
| 106 | 8.05769 | .744538 | 443.906 | -300000 | -2100.000000 | 1 | 2 |
| 108 | 2.850442 | .712319 | 441.282 | 500000 | 0.000000 | 1 | 1 |
| 109 | 6.902158 | .717319 | 441.790 | 500000 | 0.000000 | 1 | 1 |
| 103 | 8.312534 | 3.000000 | 630.809 | 500000 | 0.000000 | 1 | 1 |
| 104 | 5.049781 | 2.627025 | 537.313 | -300000 | 0.000000 | 1 | 1 |
| 105 | 1.806466 | 2.290409 | 480.359 | 500000 | 0.000000 | 1 | 1 |
| 111 | 1.256827 | 2.290409 | 463.576 | 500000 | 0.000000 | 1 | 1 |
| 107 | 9.39212 | 2.357826 | 450.365 | 500000 | 0.000000 | 1 | 1 |
| 110 | 2.691431 | 2.627025 | 500.842 | 500000 | 0.000000 | 1 | 1 |

SYSTEM SEGMENTS

| SEG | NETWK | WIN(KG/S) | WOUT(KG/S) | WBAR(KG/S) | E IN(MJ/KG) | E OUT(MJ/KG) | IN(MPA) | PI IN(MPA) | POUT(MPA) | ALPHA | SEG | BETA(MPA) | CONNECTS TO: | |
|-----|-------|-----------|------------|------------|-------------|--------------|----------|------------|-----------|----------|-----|-----------|--------------|-----|
| | | | | | | | | | | | | | IN | OUT |
| 1 | 1 | 1000.000 | 1000.000 | 1000.000 | 3.000000 | 3.000000 | 8.950371 | 8.950371 | 8.950209 | 162E-09 | 09 | 0.000000 | 401 | 101 |
| 2 | 1 | .003 | .003 | .003 | 3.000000 | 3.000000 | 8.950371 | 8.950209 | 8.006687 | .773E+06 | 06 | 0.000000 | 101 | 102 |
| 3 | 1 | .003 | .003 | .003 | 3.000000 | 3.000000 | 8.950371 | 8.006687 | 8.00358 | 312E+02 | 02 | 0.000000 | 102 | 106 |
| 4 | 1 | 1000.000 | 1000.000 | 1000.000 | .712319 | .712319 | 81.080 | 2.850442 | 2.850442 | .255E-08 | 08 | 2.041911 | 106 | 108 |
| 5 | 1 | 1000.000 | 1000.000 | 1000.000 | .717319 | .717319 | 2.850442 | 6.902158 | 6.902158 | .398E-08 | 08 | 4.055691 | 108 | 109 |
| 6 | 1 | 1000.000 | 1000.000 | 1000.000 | .717319 | .717319 | 6.902158 | 13.000000 | 13.000000 | 517E-07 | 07 | 6.149508 | 109 | 402 |
| 7 | 1 | 999.997 | 999.997 | 999.997 | 3.000000 | 3.000000 | 8.950209 | 8.912534 | 8.912534 | .376E-07 | 07 | 0.000000 | 101 | 103 |
| 8 | 1 | 999.997 | 999.997 | 999.997 | 3.000000 | 3.000000 | 8.912534 | 5.049781 | 5.049781 | .386E-05 | 05 | 0.000000 | 103 | 104 |
| 9 | 1 | 975.051 | 975.051 | 975.051 | 2.627025 | 2.627025 | 5.049781 | 5.049669 | 1.806466 | .341E-05 | 05 | 0.000000 | 104 | 105 |
| 10 | 1 | 949.666 | 949.666 | 949.666 | 2.290409 | 2.290409 | 1.806466 | 1.806466 | 1.806466 | .112E-05 | 05 | 0.00174 | 105 | 106 |
| 11 | 1 | 25.384 | 25.384 | 25.384 | 2.290409 | 2.290409 | 1.806466 | 1.806466 | 1.266819 | .838E-03 | 03 | 0.00401 | 105 | 111 |
| 12 | 1 | 25.384 | 25.384 | 25.384 | 2.290409 | 2.290409 | 1.266819 | 1.266819 | 9.39206 | .509E-03 | 03 | 0.00169 | 111 | 107 |
| 13 | 1 | 50.330 | 50.330 | 50.330 | 2.357826 | 2.357826 | 2.357826 | 2.357826 | 81.080 | .509E-04 | 04 | 0.00046 | 107 | 106 |
| 14 | 1 | 24.946 | 24.946 | 24.946 | 2.627025 | 2.627025 | 5.049781 | 5.049781 | 2.691416 | .379E-02 | 02 | 0.00621 | 104 | 110 |
| 15 | 1 | 24.946 | 24.946 | 24.946 | 2.627025 | 2.627025 | 2.691416 | 2.691416 | 9.39212 | .282E-02 | 02 | 0.00217 | 110 | 107 |

| IN-SEGMENT DISTRIBUTIONS | SEG | MODE | EIN(MJ/KG) | EBAR(MJ/KG) | EOUT(MJ/KG) | WTR(KG/S) | MDUT(KG/S) | TIN(K) | TOUT(K) | DENS(KG/M3) | QA(MJ/S) | JTN | JOUT |
|--------------------------|-----|------|------------|-------------|-------------|-----------|------------|---------|---------|-------------|----------|-----|------|
| 1 | 1 | 1 | 3.000000 | 3.000000 | 3.000000 | 1000.000 | 1000.000 | 631.115 | 631.115 | 36.868 | 0.000 | 1 | 2 |
| 2 | 501 | 2 | 3.000000 | 3.000000 | 3.000000 | .003 | .003 | 595.505 | 595.505 | 19.919 | 0.000 | 3 | 4 |
| 3 | 2 | 3 | 3.000000 | 3.000000 | 3.000000 | .003 | .003 | 548.910 | 548.910 | 3.250 | 0.000 | 5 | 6 |
| 3 | 2 | 4 | 3.000000 | 3.000000 | 3.000000 | .003 | .003 | 548.910 | 548.910 | 3.250 | 0.000 | 6 | 7 |
| 3 | 2 | 5 | 3.000000 | 3.000000 | 3.000000 | .003 | .003 | 548.910 | 548.910 | 3.250 | 0.000 | 7 | 8 |
| 4 | 4 | 6 | .722319 | .717319 | .712319 | 1000.000 | 1000.000 | 443.738 | 441.445 | 895.615 | -10.000 | 0 | 10 |
| 4 | 201 | 7 | .712319 | .712319 | .712319 | 1000.000 | 1000.000 | 441.445 | 441.445 | 895.769 | 0.000 | 10 | 11 |
| 5 | 301 | 8 | .712319 | .712319 | .712319 | 1000.000 | 1000.000 | 441.162 | 441.356 | 899.274 | 1.768 | 12 | 13 |
| 5 | 301 | 9 | .714087 | .714087 | .714087 | 1000.000 | 1000.000 | 441.356 | 441.749 | 898.681 | 1.662 | 13 | 14 |
| 5 | 301 | 10 | .715749 | .715749 | .715749 | 1000.000 | 1000.000 | 441.749 | 441.929 | 898.512 | 1.562 | 14 | 15 |
| 5 | 202 | 11 | .717319 | .717319 | .717319 | 1000.000 | 1000.000 | 442.110 | 442.110 | 898.331 | 0.000 | 15 | 16 |
| 6 | 302 | 12 | .717319 | .717319 | .717319 | 1000.000 | 1000.000 | 441.308 | 441.697 | 902.484 | 1.678 | 17 | 18 |
| 6 | 302 | 13 | .718997 | .718997 | .718997 | 1000.000 | 1000.000 | 441.697 | 441.890 | 902.105 | 1.642 | 18 | 19 |
| 6 | 302 | 14 | .720659 | .720659 | .720659 | 1000.000 | 1000.000 | 442.083 | 442.274 | 901.730 | 1.646 | 19 | 20 |
| 6 | 203 | 15 | .722319 | .722319 | .722319 | 1000.000 | 1000.000 | 442.468 | 442.468 | 901.540 | 0.000 | 20 | 21 |
| 6 | 505 | 16 | .722319 | .722319 | .722319 | 1000.000 | 1000.000 | 442.468 | 442.468 | 901.540 | 0.000 | 21 | 22 |
| 7 | 502 | 17 | 3.000000 | 3.000000 | 3.000000 | 999.997 | 999.997 | 630.961 | 630.961 | 36.722 | 0.000 | 23 | 24 |
| 8 | 601 | 18 | 3.000000 | 2.813512 | 2.627025 | 999.997 | 999.997 | 630.808 | 565.662 | 34.570 | -372.974 | 25 | 26 |
| 9 | 602 | 19 | 2.627025 | 2.458717 | 2.290409 | 975.048 | 975.048 | 537.305 | 514.208 | 21.219 | -328.217 | 27 | 28 |
| 10 | 3 | 20 | 2.290409 | 2.290409 | 2.290409 | 949.668 | 949.668 | 464.865 | 464.865 | 8.865 | 0.000 | 29 | 30 |
| 11 | 504 | 21 | 2.290409 | 2.290409 | 2.290409 | 25.380 | 25.380 | 472.549 | 472.549 | 10.474 | 0.000 | 31 | 32 |
| 12 | 5 | 22 | 2.290409 | 2.252407 | 2.290409 | 25.380 | 25.380 | 457.353 | 457.353 | 7.495 | 0.000 | 33 | 34 |
| 13 | 301 | 23 | 2.357926 | 2.308252 | 2.258579 | 50.329 | 50.329 | 447.356 | 447.356 | 5.880 | -5.000 | 35 | 36 |
| 13 | 8 | 24 | 2.258579 | 2.258579 | 2.258579 | 50.329 | 50.329 | 447.356 | 447.356 | 6.071 | 0.000 | 36 | 37 |
| 13 | 8 | 25 | 2.258579 | 2.258579 | 2.258579 | 50.329 | 50.329 | 447.356 | 447.356 | 6.071 | 0.000 | 37 | 38 |
| 13 | 8 | 26 | 2.258579 | 2.258579 | 2.258579 | 50.329 | 50.329 | 447.356 | 447.356 | 6.071 | 0.000 | 38 | 39 |
| 14 | 503 | 27 | 2.627025 | 2.627025 | 2.627025 | 24.948 | 24.948 | 521.227 | 521.227 | 21.532 | 0.000 | 40 | 41 |
| 15 | 6 | 28 | 2.627025 | 2.627025 | 2.627025 | 24.948 | 24.948 | 480.585 | 480.585 | 10.036 | 0.000 | 42 | 43 |
| 15 | 302 | 29 | 2.627025 | 2.526818 | 2.426612 | 24.948 | 24.948 | 480.585 | 480.585 | 10.641 | -5.000 | 43 | 44 |
| 15 | 7 | 30 | 2.426612 | 2.426612 | 2.426612 | 24.948 | 24.948 | 480.585 | 480.585 | 11.324 | 0.000 | 44 | 45 |
| 15 | 7 | 31 | 2.426612 | 2.426612 | 2.426612 | 24.948 | 24.948 | 480.585 | 480.585 | 11.324 | 0.000 | 45 | 46 |

MINET DECK K2.EXAMPLE BOP DECK.GUN 11/24/83

SYSTEM MODULES
 MODULE 1 IS B.C. NUMBER 1. MOO1D 401.NPATH= 0
 MODULE 2 IS PIPE NUMBER 1. MOO1D 1.NPATH= 1
 MODULE 3 IS VOL. NUMBER 1. MOO1D 10.NPATH= 1
 MODULE 4 IS VALV NUMBER 1. MOO1D 501.NPATH= 1
 RELATIVE VALVE POSITION IS .0000100.AND CHOKE FLOW IS
 MODULE 5 IS VOL. NUMBER 2. MOO1D 102.NPATH= 1
 MODULE 6 IS PIPE NUMBER 2. MOO1D 2.NPATH= 1
 MODULE 7 IS VOL. NUMBER 3. MOO1D 106.NPATH= 1
 MODULE 8 IS PIPE NUMBER 3. MOO1D 4.NPATH= 1
 MODULE 9 IS PUMP NUMBER 1. MOO1D 201.NPATH= 3
 PUMP SPEED= 3500.000 PUMP FLOW= 333.333 KG/S PUMP HEAD= 230.000 METERS
 MODULE 10 IS VOL. NUMBER 4. MOO1D 109.NPATH= 3
 MODULE 11 IS H.X. NUMBER 1. MOO1D 301.NPATH= 3
 THE HEAT FLUX AREA CORRECTION FACTOR IS .084280
 T NOO 1 MOD 0 QINR(KJ/S/M) TINR(K) T TUBE(K) TOUTR(K) QOUTR(KJ/S/M) MODE.1 MODE.0 T.CORE T.STRC

| T NOO | MOD | QINR(KJ/S/M) | TINR(K) | T TUBE(K) | TOUTR(K) | QOUTR(KJ/S/M) | MODE.1 | MODE.0 | T.CORE | T.STRC |
|-------|-----|---------------|---------|-----------|-----------|----------------|--------|--------|--------|--------|
| 1 | 8 | 23 | 1.67515 | 441.16177 | 444.76255 | 447.35631 | 1 | 6 | 441.2 | 447.4 |
| 2 | 9 | 23 | 1.57693 | 441.55710 | 444.94344 | 447.35631 | 1 | 6 | 441.6 | 447.6 |
| 3 | 10 | 23 | 1.48315 | 441.92862 | 445.11261 | 447.35631 | 1 | 6 | 441.9 | 447.9 |

MODULE 12 IS PUMP NUMBER 2. MOO1D 202.NPATH= 3
 PUMP SPEED= 3500.000 PUMP FLOW= 333.333 KG/S PUMP HEAD= 460.000 METERS
 MODULE 13 IS VOL. NUMBER 5. MOO1D 109.NPATH= 3
 MODULE 14 IS H.X. NUMBER 2. MOO1D 302.NPATH= 3
 THE HEAT FLUX AREA CORRECTION FACTOR IS .014175
 T NOO 1 MOD 0 QINR(KJ/S/M) TINR(K) T TUBE(K) TOUTR(K) QOUTR(KJ/S/M) MODE.1 MODE.0 T.CORE T.STRC

| T NOO | MOD | QINR(KJ/S/M) | TINR(K) | T TUBE(K) | TOUTR(K) | QOUTR(KJ/S/M) | MODE.1 | MODE.0 | T.CORE | T.STRC |
|-------|-----|---------------|---------|-----------|-----------|----------------|--------|--------|--------|--------|
| 4 | 12 | 29 | 9.47047 | 441.50254 | 462.18786 | 480.58461 | 1 | 6 | 441.5 | 480.6 |
| 5 | 13 | 29 | 9.38049 | 441.89019 | 462.36753 | 480.58461 | 1 | 6 | 441.9 | 480.6 |
| 6 | 14 | 29 | 9.29136 | 442.27405 | 462.54567 | 480.58461 | 1 | 6 | 442.3 | 480.6 |

MODULE 15 IS PUMP NUMBER 3. MOO1D 203.NPATH= 3
 PUMP SPEED= 3500.000 PUMP FLOW= 333.333 KG/S PUMP HEAD= 695.000 METERS
 MODULE 16 IS VALV NUMBER 2. MOO1D 505.NPATH= 1
 RELATIVE VALVE POSITION IS .9500000.AND CHOKE FLOW IS
 MODULE 17 IS B.C. NUMBER 2. MOO1D 402.NPATH= 0
 MODULE 18 IS VALV NUMBER 3. MOO1D 502.NPATH= 1
 RELATIVE VALVE POSITION IS .9500000.AND CHOKE FLOW IS
 MODULE 19 IS VOL. NUMBER 6. MOO1D 103.NPATH= 1
 MODULE 20 IS TBSG NUMBER 1. MOO1D 601.NPATH= 1
 SPEED IN RPM IS 3500.00. EFFICIENCY IS .87166. POWER FROM GEN -.354E+09
 MODULE 21 IS VOL. NUMBER 7. MOO1D 104.NPATH= 1
 MODULE 22 IS TBSG NUMBER 2. MOO1D 602.NPATH= 1
 SPEED IN RPM IS 3500.00. EFFICIENCY IS .96414. POWER FROM GEN -.312E+09

MODULE 23 IS VOL. NUMBER 8. MOO1D 105.NPATH= 1
 MODULE 24 IS PIPE NUMBER 4. MOO1D 504.NPATH= 1
 MODULE 25 IS VALV NUMBER 4. MOO1D 504.NPATH= 1
 RELATIVE VALVE POSITION IS .3000000.AND CHOKE FLOW IS
 MODULE 26 IS VOL. NUMBER 9. MOO1D 111.NPATH= 3
 MODULE 27 IS PIPE NUMBER 5. MOO1D 5.NPATH= 1
 MODULE 28 IS VOL. NUMBER 10. MOO1D 107.NPATH= 3
 MODULE 29 IS PIPE NUMBER 6. MOO1D 8.NPATH= 1
 MODULE 30 IS VALV NUMBER 5. MOO1D 503.NPATH= 1
 RELATIVE VALVE POSITION IS .2000000.AND CHOKE FLOW IS
 MODULE 31 IS VOL. NUMBER 11. MOO1D 110.NPATH= 3
 MODULE 32 IS PIPE NUMBER 7. MOO1D 6.NPATH= 1
 MODULE 33 IS PIPE NUMBER 8. MOO1D 7.NPATH= 1

RELATIVE VALVE POSITION IS .100E+21.AS DETERMINED USING OPTION 0
 RELATIVE VALVE POSITION IS .100E+21.AS DETERMINED USING OPTION 0
 RELATIVE VALVE POSITION IS .100E+21.AS DETERMINED USING OPTION 0
 RELATIVE VALVE POSITION IS .100E+21.AS DETERMINED USING OPTION 0

END SS TIME=14.2
 MINET: END=100. PRINT=100. STORE=100. SAVE=100.

Figure 4.2-5 X2 t = 100.0s Output

MINET DECK X2.EXAMPLE BOP DECK.GW 11/24/83

MINET. TIME= 100.00000 TIME STEP= .40000 STEP NO. 201

SYSTEM BOUNDARY CONDITIONS:

| SYSTEM ID | NETWORK | FLOW(KG/S) | ENTHALPY(MJ/KG) | PRESSURE(MPA) | TEMP(K) | FLUID |
|-----------|---------|------------|-----------------|---------------|---------|-------|
| 401 | 1 | 1000.000 | 3.000000 | 8.944160 | 531.067 | H2O |
| 402 | 1 | 1001.907 | .722428 | 13.000000 | 442.017 | H2O |

SYSTEM VOLUMES

| SYSTEM ID | PRESSURE(MPA) | ENTHALPY(MJ/KG) | TEMP(K) | LEVEL(RELATIVE) | HEAT INPUT(MJ/S) | NETWORK | REGIONS |
|-----------|---------------|-----------------|---------|-----------------|------------------|---------|---------|
| 101 | 8.944005 | 2.999975 | 631.028 | 500000 | 0.000000 | 1 | 1 |
| 102 | .801834 | 3.000356 | 549.095 | 500000 | 0.000000 | 1 | 1 |
| 106 | .806863 | .745884 | 443.963 | -290457 | -2100.000000 | 1 | 2 |
| 108 | 2.851191 | .712509 | 441.325 | 507000 | 0.000000 | 1 | 1 |
| 109 | 6.902584 | .717476 | 441.826 | 500000 | 0.000000 | 1 | 1 |
| 103 | 8.906424 | 2.999796 | 630.697 | 300000 | 0.000000 | 1 | 1 |
| 104 | 5.045985 | 2.627889 | 537.366 | 500000 | 0.000000 | 1 | 1 |
| 105 | 1.805257 | 2.293861 | 480.326 | 500000 | 0.000000 | 1 | 1 |
| 111 | 1.265732 | 2.290669 | 463.572 | 500000 | 0.000000 | 1 | 1 |
| 107 | .939887 | 2.358611 | 450.396 | 500000 | 0.000000 | 1 | 1 |
| 110 | 2.691421 | 2.627028 | 500.842 | 500000 | 0.000000 | 1 | 1 |

SYSTEM SEGMENTS

| SEG | NETWK | WTKG(S) | WOUT(KG/S) | WBAR(KG/S) | ETN(MJ/KG) | EOUT(MJ/KG) | PIN(MPA) | POUT(MPA) | ALPHA_SEG | BETA(MPA) | CONNECTS TO: | |
|-----|-------|----------|------------|------------|------------|-------------|----------|-----------|-----------|-----------|--------------|-----|
| | | | | | | | | | | | IN | OUT |
| 1 | 1 | 1000.000 | 1000.104 | 1000.052 | 3.000000 | 2.999977 | 8.944160 | 8.944005 | .162E-09 | .000007 | 401 | 101 |
| 2 | 1 | -.005 | .012 | .003 | 3.000186 | 3.000671 | 8.944005 | 8.01834 | .801E+06 | .000000 | 101 | 102 |
| 3 | 1 | .004 | -.001 | .002 | 3.000261 | 2.782970 | 8.01834 | 8.01828 | .754E+02 | .000000 | 102 | 105 |
| 4 | 1 | 1001.955 | 1001.943 | 1001.950 | .722462 | .712508 | 812016 | 2.851191 | .294E-08 | 2.041811 | 106 | 108 |
| 5 | 1 | 1001.941 | 1001.914 | 1001.928 | .712508 | .717476 | 2.851191 | 6.902584 | .396E-08 | 4.055529 | 108 | 109 |
| 6 | 1 | 1001.914 | 1001.907 | 1001.909 | .717475 | .722428 | 6.902584 | 13.000000 | .515E-07 | 6.149333 | 109 | 402 |
| 7 | 1 | 1000.340 | 1000.534 | 1000.437 | 2.999957 | 2.999927 | 8.944005 | 8.906424 | .376E-07 | .000013 | 101 | 103 |
| 8 | 1 | 1000.636 | 1000.636 | 1000.636 | 2.999931 | 2.627606 | 8.906424 | 5.045985 | .386E-05 | 0.000000 | 103 | 104 |
| 9 | 1 | 976.696 | 976.696 | 976.696 | 2.627321 | 2.291828 | 5.045985 | 1.805257 | .341E-05 | 0.000000 | 104 | 105 |
| 10 | 1 | 951.626 | 951.900 | 951.763 | 2.291274 | 2.291274 | 1.805257 | 8.01710 | .111E-05 | .00197 | 105 | 106 |
| 11 | 1 | 25.254 | 25.273 | 25.234 | 2.291597 | 2.291027 | 1.805257 | 1.266723 | .844E-03 | .000412 | 105 | 111 |
| 12 | 1 | 25.289 | 25.291 | 25.290 | 2.290509 | 2.290471 | 1.266740 | .939881 | .511E-03 | .00171 | 111 | 107 |
| 13 | 1 | 50.304 | 49.591 | 49.637 | 2.358463 | 2.261284 | 5.045985 | 8.12016 | .520E-04 | .000048 | 107 | 106 |
| 14 | 1 | 24.325 | 24.354 | 24.340 | 2.627321 | 2.627082 | 5.046121 | 2.691406 | .398E-02 | .000732 | 104 | 110 |
| 15 | 1 | 24.370 | 25.011 | 24.878 | 2.627050 | 2.427495 | 2.691435 | .939887 | .283E-02 | .000237 | 110 | 107 |

| IN-SEGMENT DISTRIBUTIONS | SEG | MODE | EIN(MJ/KG) | EBAR(MJ/KG) | EOUT(MJ/KG) | MIN(KG/S) | MDUT(KG/S) | TIN(K) | TBAR(K) | TOUT(K) | DENS(KG/MS) | QA(MJ/S) | JIN | JOUT |
|--------------------------|-----|------|------------|-------------|-------------|-----------|------------|---------|---------|---------|-------------|----------|-----|------|
| 1 | 1 | 1 | 3.000000 | 2.999989 | 2.999977 | 1000.000 | 1000.104 | 631.056 | 631.053 | 631.059 | 36.837 | 0.000 | 1 | 2 |
| 2 | 501 | 2 | 3.000186 | 2.999831 | 3.000671 | .005 | .012 | 595.549 | 595.423 | 595.720 | 19.932 | 0.000 | 3 | 4 |
| 3 | 2 | 3 | 3.000261 | 3.000304 | 3.000346 | .004 | .003 | 549.050 | 549.059 | 549.089 | 3.251 | 0.000 | 5 | 6 |
| 3 | 2 | 4 | 3.000346 | 3.000344 | 3.000342 | .003 | .001 | 549.089 | 549.088 | 549.087 | 3.251 | 0.000 | 6 | 7 |
| 3 | 2 | 5 | 3.000342 | 2.891642 | 2.782970 | .001 | .001 | 549.087 | 499.155 | 450.035 | 3.625 | 0.000 | 7 | 8 |
| 4 | 4 | 6 | .722462 | .717484 | .712505 | 1001.955 | 1001.946 | 443.770 | 442.630 | 441.488 | 895.567 | -10.000 | 9 | 10 |
| 4 | 201 | 7 | .712505 | .712507 | .712508 | 1001.946 | 1001.943 | 441.488 | 441.488 | 441.488 | 896.725 | 0.000 | 10 | 11 |
| 5 | 301 | 8 | .712508 | .713388 | .714267 | 1001.941 | 1001.932 | 441.002 | 441.204 | 441.407 | 899.232 | 1.763 | 12 | 13 |
| 5 | 301 | 9 | .714267 | .715095 | .715922 | 1001.932 | 1001.924 | 441.407 | 441.598 | 441.788 | 898.841 | 1.659 | 13 | 14 |
| 5 | 301 | 10 | .715922 | .716699 | .717477 | 1001.924 | 1001.916 | 441.788 | 441.967 | 442.147 | 898.473 | 1.561 | 14 | 15 |
| 5 | 202 | 11 | .717477 | .717476 | .717476 | 1001.916 | 1001.914 | 442.147 | 442.147 | 442.146 | 898.295 | 0.000 | 15 | 16 |
| 6 | 302 | 12 | .717475 | .718311 | .719146 | 1001.914 | 1001.912 | 441.344 | 441.538 | 441.732 | 902.450 | 1.678 | 17 | 18 |
| 6 | 302 | 13 | .719146 | .719973 | .720799 | 1001.912 | 1001.910 | 441.732 | 441.924 | 442.116 | 902.073 | 1.662 | 18 | 19 |
| 6 | 302 | 14 | .720799 | .721616 | .722430 | 1001.910 | 1001.908 | 442.116 | 442.305 | 442.495 | 901.699 | 1.646 | 19 | 20 |
| 6 | 203 | 15 | .722430 | .722433 | .722428 | 1001.908 | 1001.908 | 442.495 | 442.495 | 442.494 | 901.514 | 0.000 | 20 | 21 |
| 6 | 505 | 16 | .722430 | .722429 | .722428 | 1001.908 | 1001.907 | 442.494 | 442.494 | 442.493 | 901.515 | 0.000 | 21 | 22 |
| 7 | 502 | 17 | 2.999957 | 2.999942 | 2.999927 | 1000.340 | 1000.534 | 630.899 | 630.895 | 630.890 | 36.757 | 0.000 | 23 | 24 |
| 8 | 601 | 18 | 2.999931 | 2.813768 | 2.627606 | 1000.636 | 1000.636 | 614.574 | 565.659 | 558.369 | 34.606 | -372.563 | 25 | 26 |
| 9 | 602 | 19 | 2.627321 | 2.459575 | 2.291828 | 976.696 | 976.696 | 514.175 | 514.175 | 514.175 | 21.249 | -327.682 | 27 | 28 |
| 10 | 3 | 20 | 2.291557 | 2.291435 | 2.291274 | 951.626 | 951.626 | 469.879 | 464.879 | 464.879 | 8.877 | 0.000 | 29 | 30 |
| 11 | 504 | 21 | 2.291597 | 2.291312 | 2.291027 | 25.254 | 25.273 | 472.529 | 472.529 | 472.529 | 10.484 | 0.000 | 31 | 32 |
| 12 | 5 | 22 | 2.290509 | 2.290490 | 2.290471 | 25.289 | 25.291 | 457.373 | 457.373 | 457.373 | 7.500 | 0.000 | 33 | 34 |
| 13 | 301 | 23 | 2.358463 | 2.309884 | 2.261305 | 50.304 | 49.629 | 447.401 | 447.401 | 447.401 | 5.877 | -4.793 | 35 | 36 |
| 13 | 8 | 24 | 2.261305 | 2.261299 | 2.261293 | 49.617 | 49.617 | 447.401 | 447.401 | 447.401 | 6.064 | 0.000 | 36 | 37 |
| 13 | 8 | 25 | 2.261293 | 2.261287 | 2.261281 | 49.617 | 49.617 | 447.401 | 447.401 | 447.401 | 6.063 | 0.000 | 37 | 38 |
| 13 | 8 | 26 | 2.261287 | 2.261285 | 2.261284 | 49.604 | 49.591 | 447.401 | 447.401 | 447.401 | 6.063 | 0.000 | 38 | 39 |
| 14 | 503 | 27 | 2.627321 | 2.627202 | 2.627082 | 24.325 | 24.354 | 521.196 | 521.196 | 521.196 | 21.548 | 0.000 | 40 | 41 |
| 15 | 6 | 28 | 2.627050 | 2.627046 | 2.627042 | 24.370 | 24.374 | 480.608 | 480.608 | 480.608 | 10.043 | 0.000 | 42 | 43 |
| 15 | 302 | 29 | 2.627042 | 2.527268 | 2.427494 | 24.374 | 25.007 | 480.608 | 480.608 | 480.608 | 10.646 | -4.931 | 43 | 44 |
| 15 | 7 | 30 | 2.427494 | 2.427494 | 2.427495 | 25.007 | 25.009 | 480.608 | 480.608 | 480.608 | 11.327 | 0.000 | 44 | 45 |
| 15 | 7 | 31 | 2.427495 | 2.427495 | 2.427495 | 25.009 | 25.011 | 480.608 | 480.608 | 480.608 | 11.327 | 0.000 | 45 | 46 |

far greater heat transfer capacity in the feedwater heaters than was needed (according to the heat transfer correlation for condensation on horizontal tubes), so MINET factored the heat transfer area down significantly. Of course, if this type of adjustment occurs in a physically meaningful deck, the utilization of only 1.4% of the heat transfer area would be a sure sign of an error. However, for this deck, the adjustment is not particularly important.

The edit for Deck X2 after 100 seconds of null transient is shown in Figure 4.2-5. Perhaps the most interesting part of this edit is the small amount of flow redistribution which is still occurring to resolve errors leftover from the steady state iterative processes. This is a strong indication that the calculated steady state was fairly accurate, and that the conditions and the calculations are quite stable.

4.3 MINET DECK P2

MINET Deck P2 was developed to simulate part of a PWR system, as shown in Figures 4.3-1 and 4.3-2. This is a rather novel deck in that it is a very different representation than we envisioned during code development. The input deck was developed as part of a short term project by others outside the MINET development effort, as an alternative to the principal approach that was being pursued. As it turns out, their principal research path worked out and MINET Deck P2 was never fully verified. Even though we are not currently utilizing this representation, it has some unique features worth pointing out.

The first feature is the semi-closed system encompassing the high pressure injection (HPI) system, the reactor, the primary loop, and the pressurizer. Since an inlet and an outlet boundary are needed to use MINET, an extremely

small leakage out the relief valve, and an equally small makeup from the HPI system were postulated. MINET determined the pressurizer pressure from the area of the slightly open relief valve, the low flow rate, and the choked flow rate for steam. Of course, the valve opening had to be adjusted to set the desired system pressure, but this turned out to be fairly easy to do. It should be noted that the reactor was simulated using a heated pipe, with a heat vs. time table used to simulate decay heat levels after scram.

The second interesting feature of Deck P2 is the representation of a U-tube steam generator, with the primary fluid entering the bottom of the steam generator, passing upward, then curving and coming back down and out the bottom. The secondary water enters through a downcomer, where it is mixed with re-circ flow and then passes upward through the unit, and on to the steam separators. In the MINET representation we used a counter-flow and a parallel-flow heat exchanger in parallel to simulate the U, and separated volumes for the steam separator and the downcomer. The code calculated some flow redistribution between the heat exchanger modules, which is reasonable.

While this application was never completed, there were several indications that MINET would have provided a reasonably good representation as long as one avoided severe conditions for which the more detailed codes are designed to handle. Again, this deck is shown not because we recommend the usage of MINET in this part of a reactor system, but because it contains interesting features.

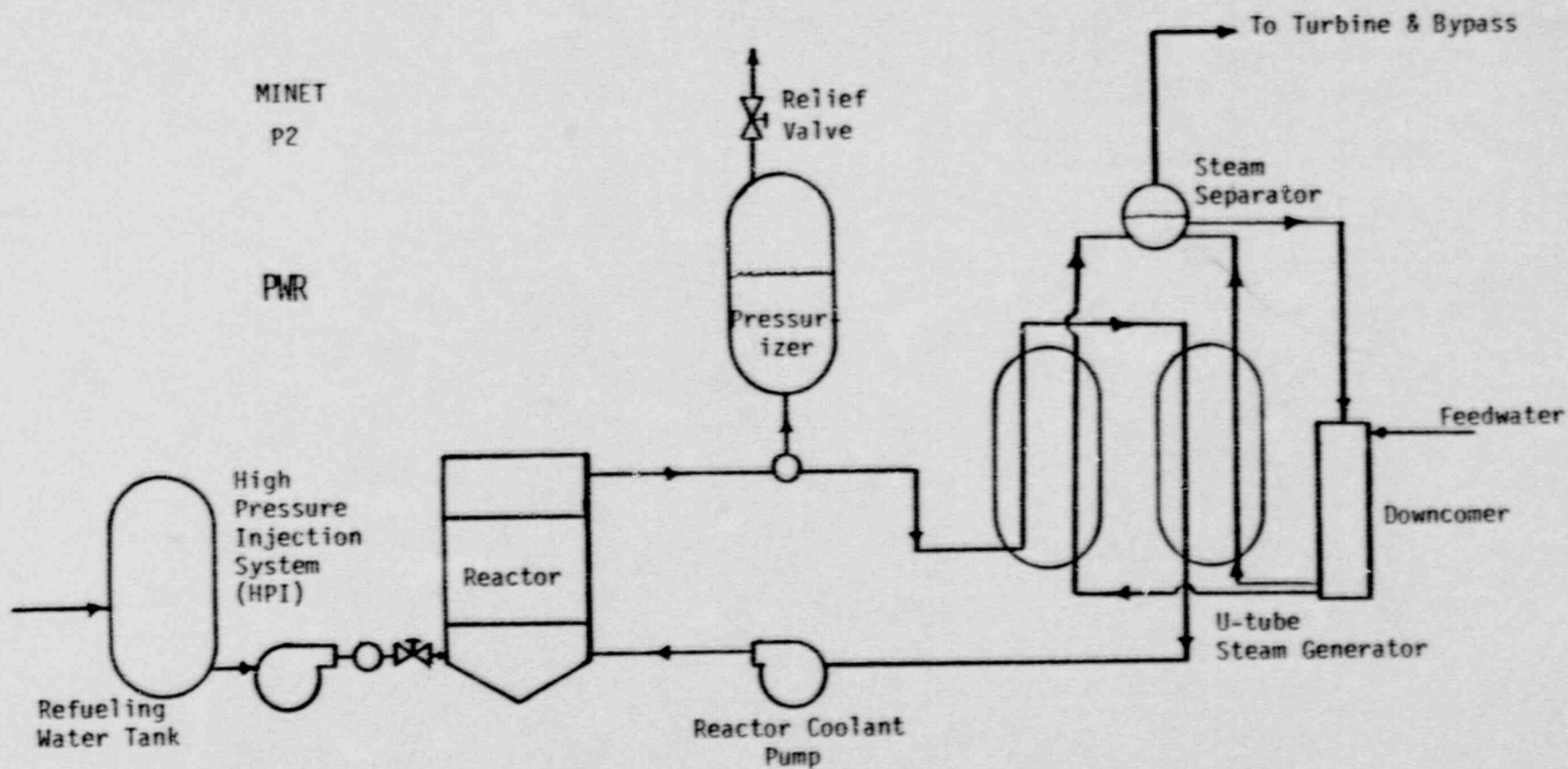


Figure 4.3-1. MINET Standard Deck P2

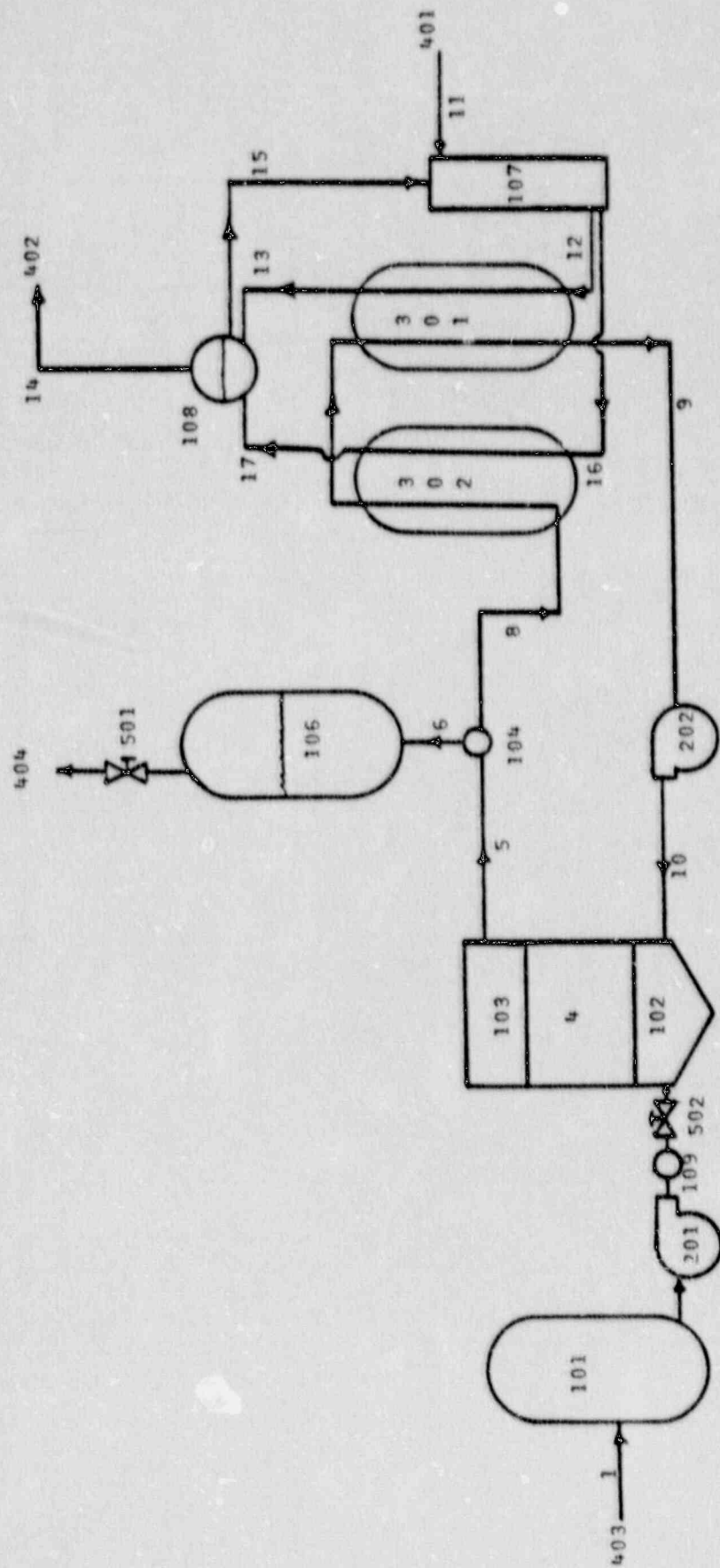


Figure 4.3-2. Deck P2 Module IDs

4.4 MINET DECK E1

MINET Deck E1, shown in Figures 4.4-1 and 4.4-2, is a representation of a part of the EBR-II system. It is a well tested deck, and has been validated against steady state and transient test data [7]. Unfortunately the data deck and output contain restricted data and distribution is currently very limited. However, that does not prevent a general discussion as to features of the MINET representation.

The MINET representation starts at the intermediate loop due to the way the SSC/MINET interface is accomplished. In general, boundaries were chosen according to the availability of data for boundary conditions. In particular, the intermediate loop mass flow rate and IHX outlet temperature, the feedwater flow rate and temperature, the drain (blowdown) flow rate, the turbine back pressure and the throttle and bypass valve behavior(s) were best known. (We did not know the flow out the auxiliary line, but managed to develop a good guess.)

Subcooled feedwater is injected into the bottom of the steam drum and mixed with saturated water coming down from the steam separators. This creates a stratified steam drum, with saturated steam on top, saturated water in the middle, and subcooled water on the bottom. In Deck E1, this is represented using two volumes and a short connecting pipe. Because the contents of the top volume are separated, and the drum is a horizontal cylinder in which the water level must be tracked, we have to use some of the volume module input options (the user should refer to Section 2.2.3, Record 501D). Since the location of the top of the subcooled region or the bottom of the saturated water region is not known precisely, a reasonable guess is used.

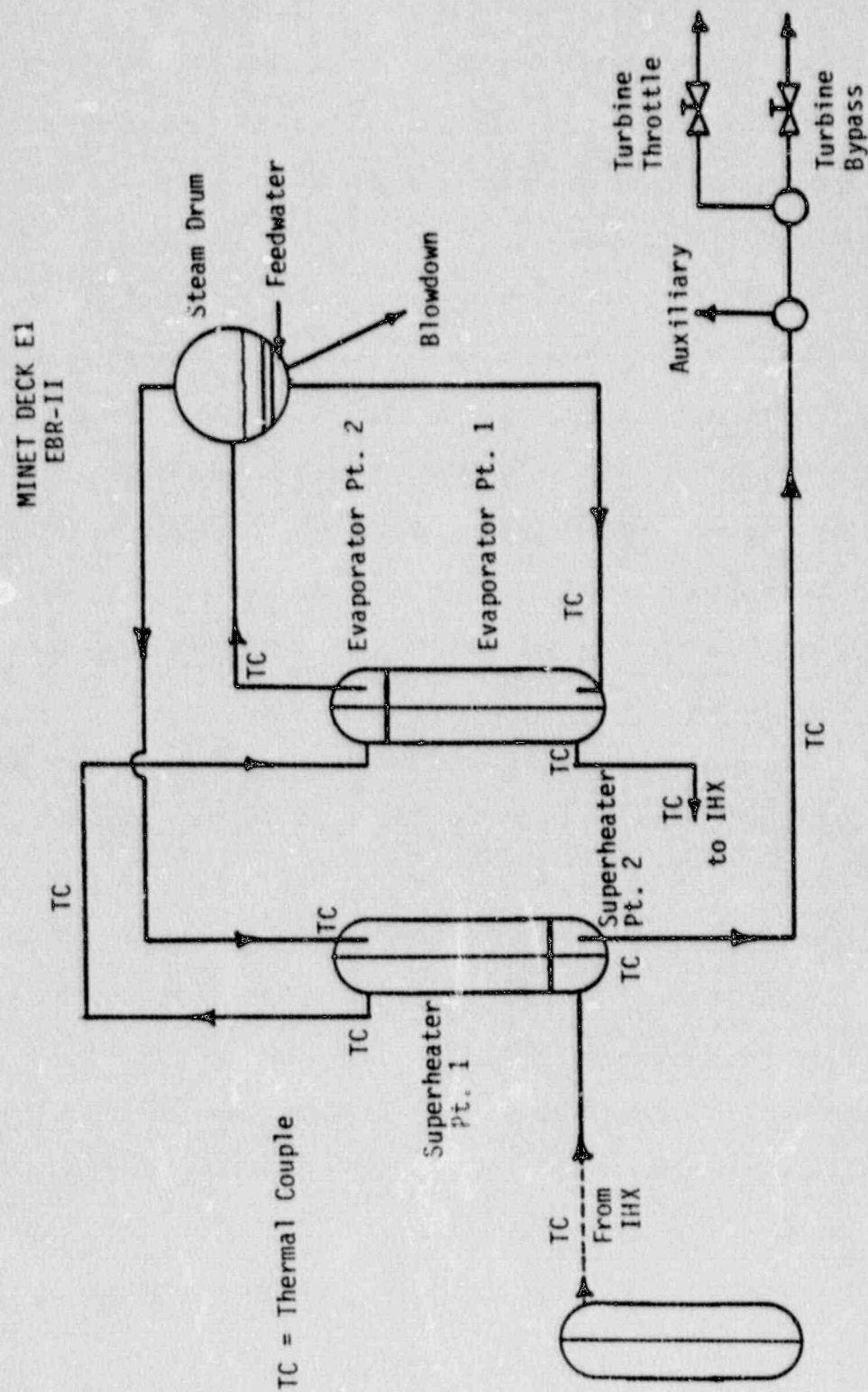


Figure 4.4-1. MINET Standard Deck E1. A One Loop EBR-II Deck

Note that the diameter of pipe 22 is chosen so as to give the right cross sectional area, and the length is consistent with the component height and the fraction not included in the two volumes.

The EBR-II steam generators have some unusual characteristics that lead us to split (axially) each one in two unequal pieces for the simulation. Under the test transient conditions, virtually all the heat transfer in the evaporator took place in the top 10% of the unit. Thus, we represented the bottom of the evaporator with a coarsely noded heat exchanger module, and the top with a heat exchanger module with fine nodalization.

The EBR-II superheaters are really modified evaporators. To increase the steam flow rate, they inserted core tubes into the steam flow area, creating annular flow and modeling problems. In order to model this, a special core tube model was incorporated, which results in some of the rather unusual data requirements on the 301 card.

In order to reduce thermal shock problems, EBR-II engineers inserted sleeves over the regular tubes near the sodium inlet. Thus, in MINET Deck E1, the superheaters are represented using two heat exchanger modules, both with core tubes, but with one having somewhat thicker tubes between the sodium and the steam.

4.5 MINET DECK C4

MINET was designed for ease of interfacing with other computer codes, partly as a result of its development as part of the SSC program. Thus, we will show one of the decks used in a combined SSC/MINET simulation of the Clinch River Breeder Reactor Plant (CRBRP) system. Because the version of

MINET currently used with SSC is a predecessor to the one documented herein, the input data itself is somewhat different and will not be shown.

MINET deck C4 is illustrated in Figure 4.5-1. Note the similarity between this system and the EBR-II system, particularly in the steam drum where the method of simulation is the same. Note also the large number of safety related lines, e.g., valves, auxiliary lines, and vents. Of course, these extra lines are easily represented using MINET. Their presence does, however, point up the need for considerable flexibility in doing licensing calculations for a plant where numerous safety systems may have to be represented.

This deck has also been well researched and tested, and results have been compared against those calculated independently. The MINET results substantially agreed with those generated independently, and all disagreements were successfully traced to limitations in the other calculations [32].

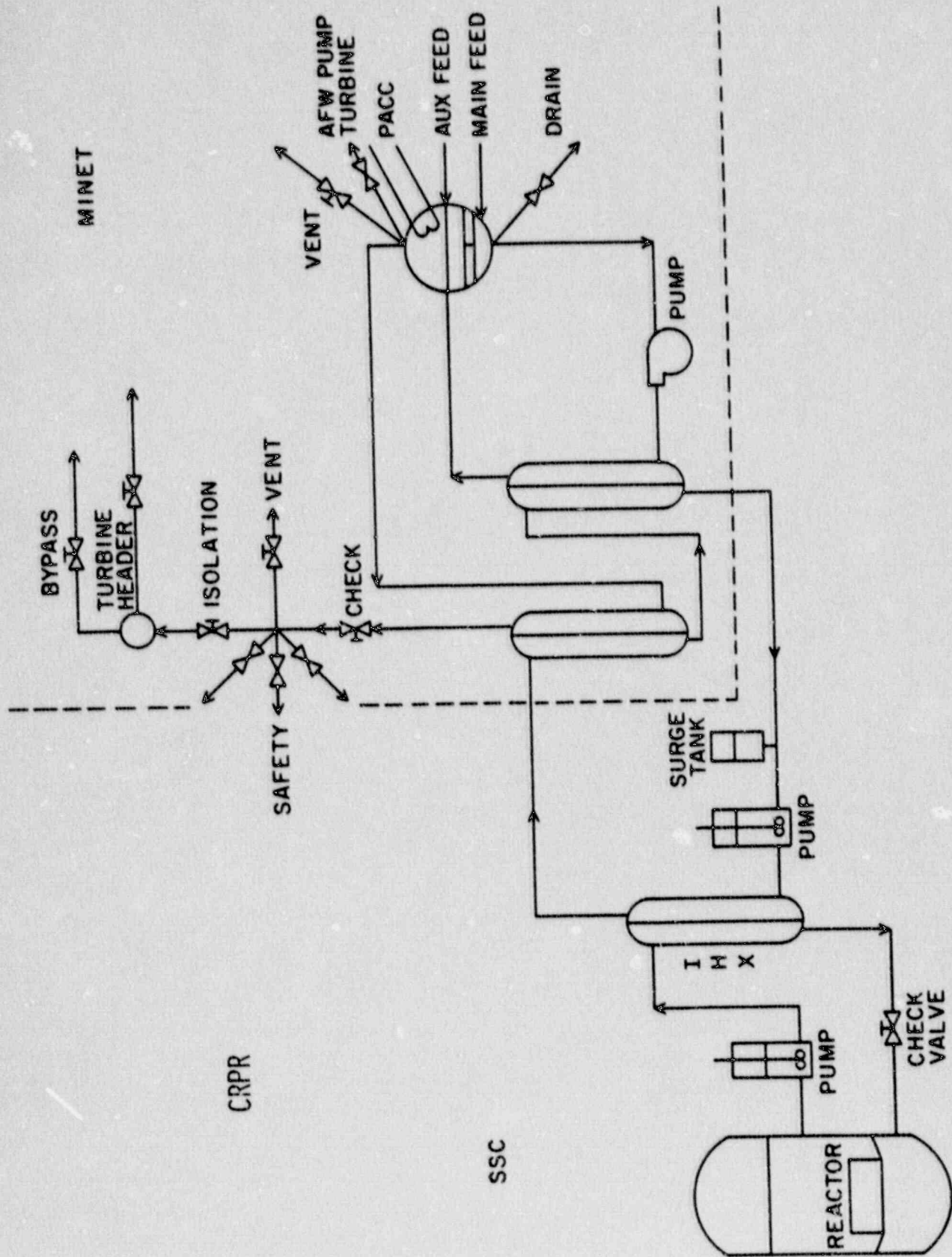


Figure 4.5-1 MINET Standard Deck C4

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11. ABSTRACT (200 words or less)

The MINET computer code, developed for the transient analysis of fluid flow and heat transfer, is documented in this four-part reference. In Part 1, the MINET models, which are based on a momentum integral network method, are described. The various aspects of utilizing the MINET code are discussed in Part 2, The User's Manual. The third part is a code description, detailing the basic code structure and the various subroutines and functions that make up MINET. In Part 4, example input decks, as well as recent validation studies and applications of MINET are summarized.

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