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An Estimate of the Damage to the TMI-2 Core

4. AUTHORS (If more than three, name first author followed by "and others".)

M.L.Picklesimer

5. OFFICE/DIVISION

RES/RSR

BRANCH/UNIT

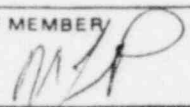
Fuel Behavior Research Branch

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July 23, 1980

7. RESPONSIBLE NRC STAFF MEMBER

M.L.Picklesimer



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b. TECHNICAL REPORT

c. CONFERENCE PAPER

ABSTRACT

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(2) DATE(S) OF CONFERENCE: November 17-21, 1980

(3) LOCATION OF CONFERENCE: Washington, D.C.

d. OTHER (Indicate type of item, e.g., thesis, speech, journal article, guide, etc.)

Abstract

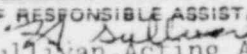
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11. SUBMITTED BY

a. NAME OF RESPONSIBLE ASSISTANT DIVISION DIRECTOR OR ABOVE  
CES  L.H. Sullivan, Acting Assistant Director, Water RSR

a. PATENT CLEARANCE NOT REQUIRED

b. PATENT CLEARANCE GRANTED

c. PATENT CLEARANCE DENIED

b. OFFICE/DIVISION

RES/RSR

d. PATENT COUNSEL'S SIGNATURE

DATE

8102020079 p

c. SIGNATURE (NRC Assistant Division Director or Above)

DATE

12/18/80

- The Legacy of TMI," Kemeny Commission Report, Washington, D.C. (Oct. 1979).
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Additional damage occurred to the core during the following hour, resulting in further changes in core geometry and condition. Though proof is lacking, the following is consistent with the limited system data available. Liquefied fuel continued to form in the debris bed to dribble down and freeze in the lower part of the bed. This eventually sealed off the bed from coolant flow, and a large steam bubble began to form below the debris bed. Eventually, the pressure head from the downcomer, the continued heatup of the debris bed, and the impingement of water released from the pressurizer combined to again disrupt the debris bed and shatter more embrittled cladding.

It is believed that, at 4 h, a 4-ft-thick debris bed existed in the core from about 4½ to 5 ft above the bottom of the fuel to about 3 ft from the top of the fuel, its density approached 90% of full density in some regions due to the formation of liquefied fuel, it rested on stubs of fuel rods 5 to 6 ft long, and drips of liquefied fuel from it penetrated

to within 10 in. of the bottom of the fuel. At least 50% of the Zircaloy in the core had been embrittled or converted to oxide, and between 700 and 820 lb of hydrogen had been produced. The debris bed may have been covered with water, but it was not quenched.

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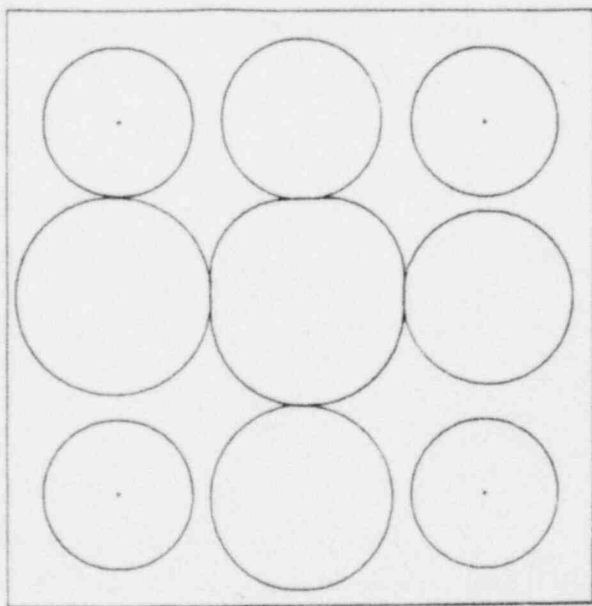


Fig. 1. Graphical representation of center pin bulging in CANSWEL-2.

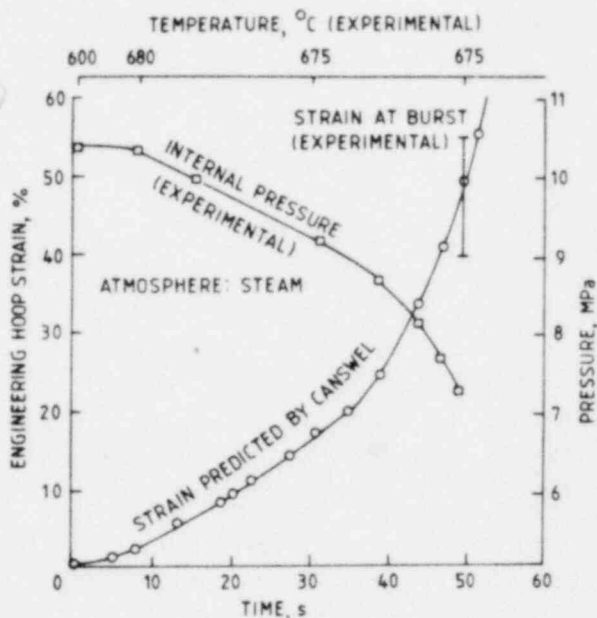


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The restraint model in the code accounts for the change in cladding stress after rod impingement. If the rod is trapped by its neighbors this contact brings about a reduction in cladding stress, because further deformation occurs by bulging between neighboring rods leading to a reduced radius of curvature. However, the cladding continues to thin, so the stress can eventually rise again. Flattening of the contact zone is modeled by assuming that the radius of curvature of the arc in contact is given by

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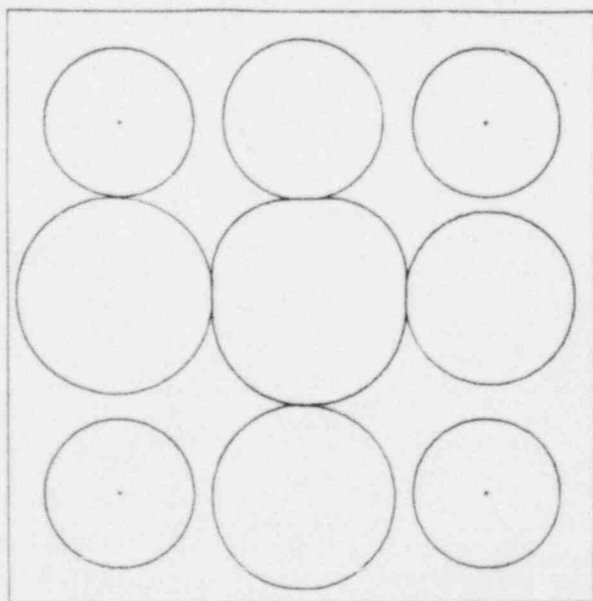


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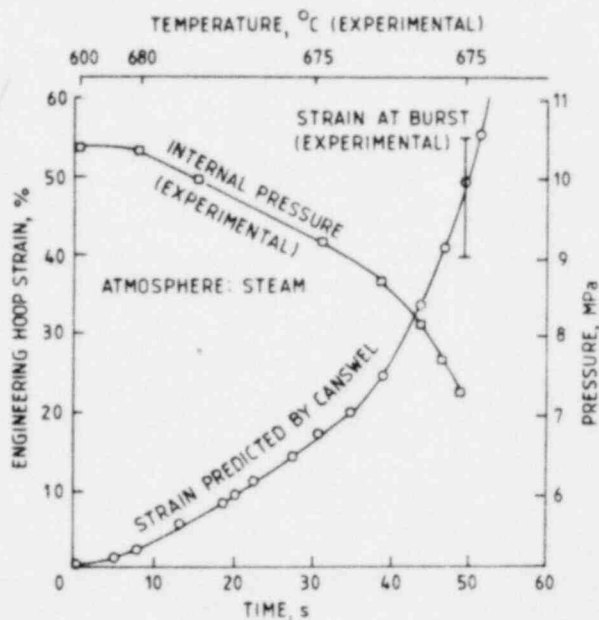


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